

Fig - 12.26 Scheme H Extended Tailrace Plan

		First Year		Second Year	Z p	ear sar	<u> </u>	Thi	Third Year	Yea	L.
Work I tem	Quantity	1 3 5 7	l °	11 6	13 1	15 17	13	21			
A. Temporary Work						:		******			
1. Access Road	L=2,500m		•								
B. Tunneling Work	L= 37m										
C. Open Excavation Work	`										
1. Culvert Work	L=1,463m										
2. Open—Cut Work	L= 110m										

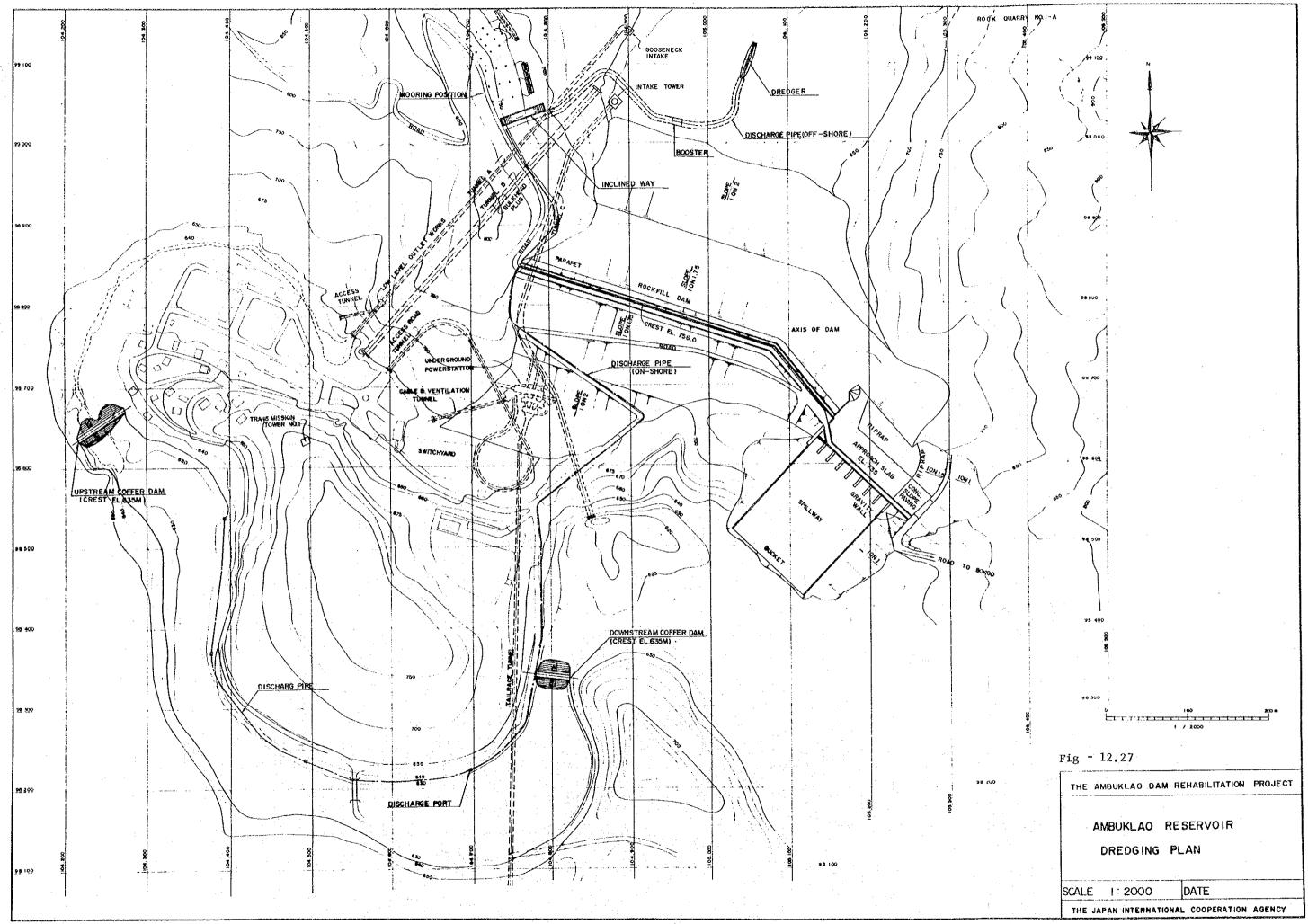
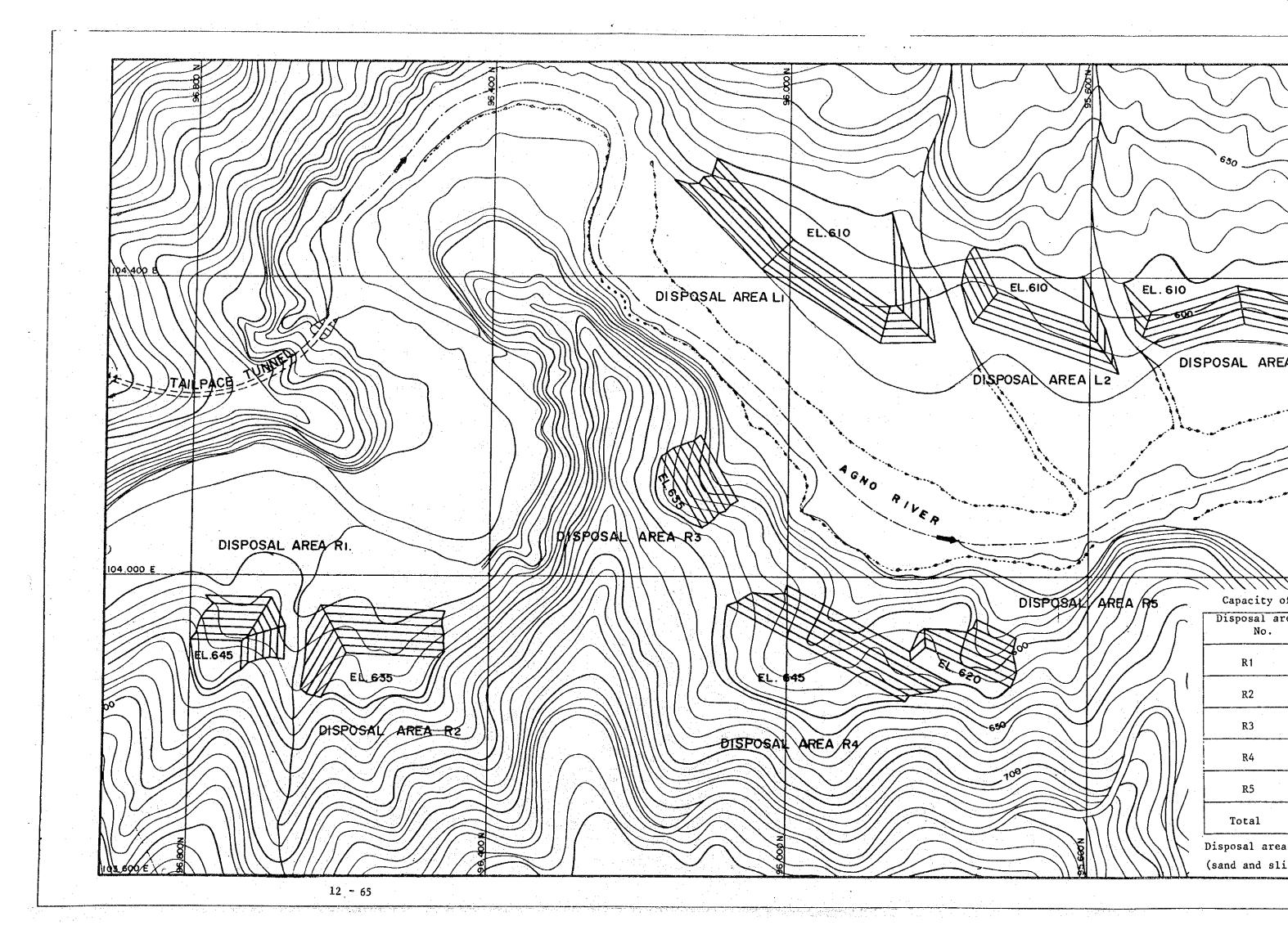
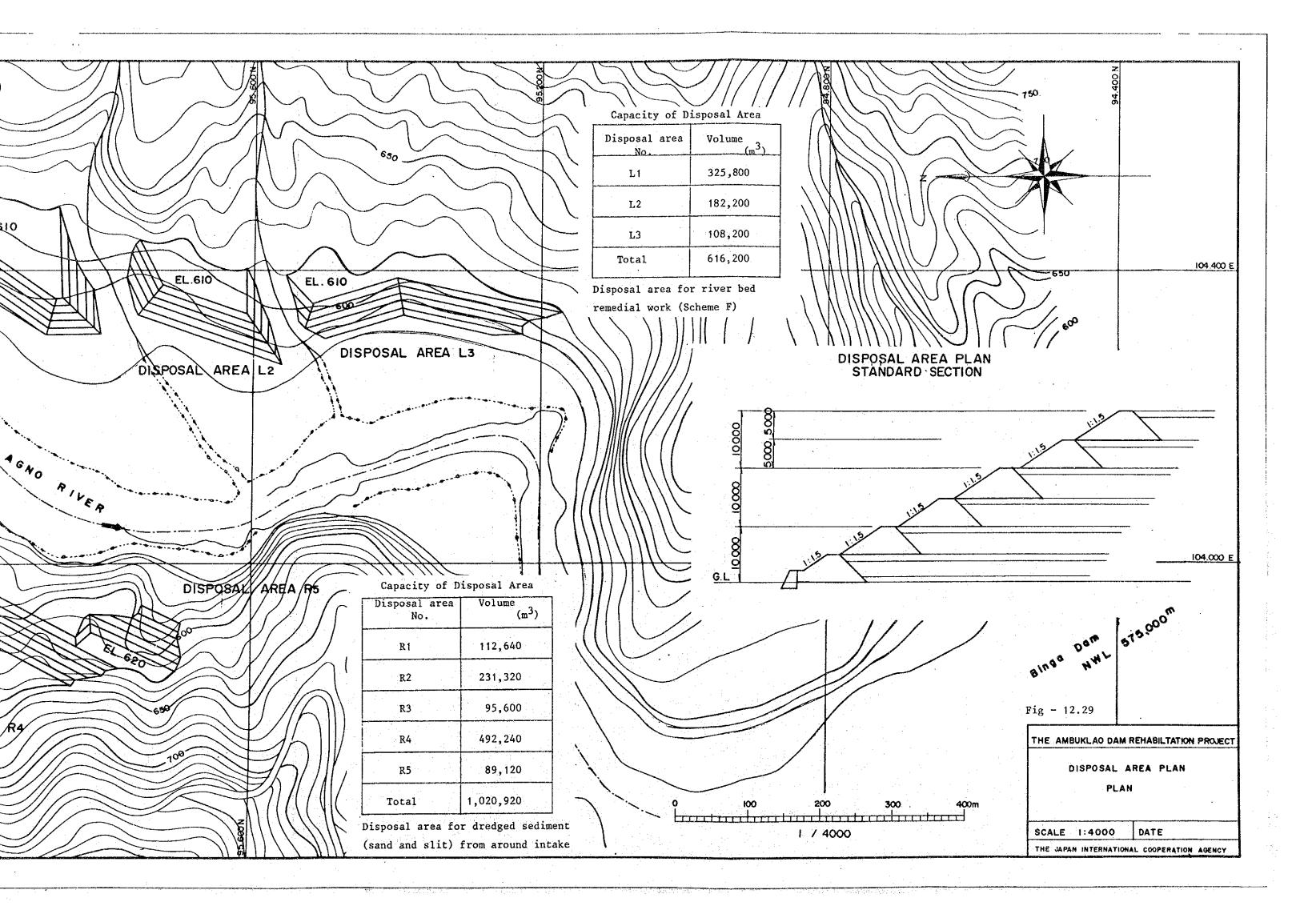


Fig. - 12.28 Scheme 0 : Dredging Around Intake Tower

			1	st Y	ear		Т	418 page 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	2n	d Ye	ear			_	Caracian de Santo	T			3r	d Ye	ear	<u></u>	-THE-BOACE PF.					41	th Y	ear					2412	1 AA	51	th Y	ear		160	TRAT	54 5	th	Yea	ir 58	Remarks	ana amandah nikita
Item	Q'	'ty	ŢÌ.	2 3	14	5 (17	[8.]	9 10	111	[2]	13 [14	[5]	16 1	7 [8	Ĭ9	201	21 2	2 23	24	25	26 2	7 25	29 Feb	30 3	31: 32 or Mo	2 33 Vilia	34 Jul A	35 36 Jua Se	3 37 p Oct	38 Nov [39 40 Dec Ja	O 41 In Feb	42 Mar 4	43 44 Apr Mg	4 46 14 Jun	# 4 Ji A	/ 48 Jg Sep	Oct N	oy De	c Jan	Feb	Mor Ar	r Mo	y Jun	弧		
			OctiN	ov IDeo	กิดบ	Febine	ir IADi	MAXA	กับ รถ	Aug	200	SET INO	Uec	van r	edi Migi	ADI	YEIY	701195	ari wa	4 365	VII	EINLE	**1	11.00		-				1				П						Ì	1	l i						
· · · ·					4			 			 	_									╂─┤			╁	 -		-				++		+-	╁╌╁	_	1						1						
A Civil Wo	rks												11			<u> </u>				ļ	\vdash		_ _	-		+	-				╁╌┼			╂╌╂		-		+	┝─┼		•	1 1						
						l	1							ĿĿ						<u> </u>											11			11-				_	├ }-		-	┼	{		-	┞╌╂		
Civil work																-			1	1.			1	.																		↓	\perp	1		├ ─┤		
dradging f					-			-					1			1						-		1							1	ĺ									1							
	1	1 sec			╁╌┤			╂			+		1-1			-		-		┼─	╀┈┨		+		tt-		 	 		+-	1-1		1															
<u></u>		<u>-</u>	_		1_1			1-1			├ ── ├		+	-		+					 			+	-		+			+	╁┼			+				1	1		1			1				
													1												╁┈╁						╁┷╁			╁┼								+			-	1-1		
2 Disposal B	i Sagin l	sec											:					ς .		L	Ш													$\downarrow \downarrow \downarrow$			1_				-				-	\vdash		
																																					•				<u> </u>					1 1		
	+		+		+		+	++		1	1-1	1	171			1-		-†		1-	1	\top		7			T			Π^{-}	I I										_[
				-+-	+		+	╅╾╂				+	╅╾┥	+	+				+	+	1-1				1 1	-	1	1		+-	1-1			1 1	\top	1		\top				\sqcap						
·				\bot	\perp		+	\sqcup		+	├		1-1		+		├─┤	\dashv	+	-	\vdash	-+		+			+	 - 	-	+	+	\dashv	-+	╅	+	+	-		1		+	1 1		1	1			
B. Facilit	у.									Щ.	$\bot \bot$	\perp				1			\bot	4-				 	-			+	-		1 1	\dashv	-	╁╌╁		+			\vdash		+	+-	\vdash		+	┼┤		
			IT	1.						1									\perp									 			1			11				+	├ ┼				-		-	 —		
Design/ Manufactur		LS.	XXX	XXX		$\propto k$	XXX		XXXX	XI																												:						լ		11		
•• Manufactur	·		3.C.V. /	-	***	- 1	T	1 1		\top	1 1		1 1			1						$\neg \uparrow$		T						T													<u> </u>					
			$\vdash \vdash$		-		+	╂╌╂			<u> </u>	+	+			+	┼╌┼	-			+				1 1	_	-	1 1			1			1 1														
2. Delivery		L.S			ļ		-1-	1-1					+		—	+						-		-	-+	-	+	+		+-	+			╅╌╂				+	1		-	+-		\dashv	十一	1 1		····
. <u> </u>	_1_			[_	<u>L</u>											_	\sqcup			_	ļ		-		╁╌╂	-		\vdash			+			┼╌┨					1 -1		 	+-	╂╼╌╂╌			11		
3. Test Opera	/ I	L.S.					1:	1 1													1.			1				1_1		\bot	1			$\downarrow \downarrow$					1				}}-	+		╁╌┪		<u></u>
u. test upera							\top	1 1															100										-									↓			<u> </u>			
			\vdash	+			-	╁╌┼			1-1	+	+	\vdash		1	1 1			+-				 		$\neg \vdash$				\top			.							.			1 1					
								+-+			╂╼╁		+-					1			1			٠				1															()				(to be continu	
C. Dredging	Work	K						4		_ _	1-1	\perp	- -				-			-					T			T		-											\top				\top		continu	ed)
													1		1.	4_	\sqcup				-				11		<u> </u>	╁┈┤		_	4			+			╂┷┼		1	-	+-	+	╁┈╁╴			+		
					İ					.						1	1 1											<u> </u>		\perp				$\downarrow \downarrow \downarrow$					1				\bot					
	1									\Box						T											:			1												1						
			\vdash		+		+	1-1		+	1-1		1			1	11			1-	1		-						- 1															-		1		
			\vdash		┿	├				\dashv	+			┝╌┼			╂┈╂		-	1	╁┈			1	1-1	_		1-1	-†	_														T				
			╀╌┼		Jac	Foh A	1 A	- W.	Jue Ji	ıı Aiv	Seni	Oct No	v Dec	Jan	eb Mo	r Apr	May	Juni	Jul Á	io Se	ol Oct	Nov	Dec Jo	in Fet	Mor	Apr M	ay Jun	Jul	Aun \$	ер Ос	t Nov	Dec	Jan Fe	b Mor	Apr b	nul yon	Jul /	Aug Se	o Oct	Nov D	ec Jo	n Fet	p War 1	or M	XX Jur	Jul		
Reservoir			1		_ Arin	10013			A 211 43			***									1	ᅵ႕			11													- 1	A				J					
Vacer Level.	17	50.00		=	_						1_1	+							_	-			_	1	1-1	_	_	1		$=$ \vdash	$\pm E$	1						-1/				1			Λ	1	1	
				\Rightarrow	\pm		士			=	11		1							1		╁╂╌┼	+		1-1						+H-	+						$\backslash \!\!\! \perp$				1	1	\mathcal{X}	#1	1/	1	
	7.	40.00			\pm						/		\pm			#				_ _	1	1/-1	1							\equiv	$oldsymbol{H}_{-}$						/	<u> </u>	1		$\forall Z$	4-	\mathbb{A}			\bigvee	l	
		. –			1			##					11			1	1-1			-			1	\dashv			\perp	\Box		Λ	$\exists F$	\exists					/				¥	1	V	_	1	1	1	
	_	30.00		士	#		\downarrow	1 1		-17	1		\dashv			-1				+1		1	-	7-			\equiv	F=		H	A =	T					/	\perp			1	1	† †	士		1	1	
	†	30.00		_	#=		_	+		1	‡=‡		-		=	+	Ħ		_				_	\pm		$\equiv \pm$				H			\pm			1/			1				11			1	1	
							_			/	1		1	1		-			1	\forall	\perp			\pm					\forall		1			#		_/_	1-1				_	+	11			1	1	
	7	20.00		\perp	+		#	+			1-1		—			-				Y	-			-		$\pm \mathbb{F}$	\pm					 		<u> </u>	!	#	1		1		==	_	+-+	\Rightarrow		#	1	
	:				+		#	-			1-1	_	1-			1	\Box		H	\exists	\pm		-					$\pm E$		士	+-	1		\mathcal{J}		/	1-1	===	1				 	_	_	#	1	
	,	10.00	 		1		#	11			1	#		T	_	-	F		1	-	Ŧ					-1		$\perp L$		\pm		卌		4	<i>V</i>		1-1	二二	#		#	_	 	#		#	 	
<u> </u>		12.22	1 +		十一		$\neg \vdash$	1-1		一	1	_	1			T			\prod		T	Π											1	7		///// 44 48	<u> </u>				1	1	d et	7	d			
	P.	pressob pres 20	pp Ly															[_:_					L					11		K	4	4.1	A7	2 25	.	44	3 21	4 44	KR I	RE I	FS		
			† † †	2 3	14	5	6 7	1 8 1	9	o Ti	12	T3 14	1 15	16	7	ৰ ছ	T20	2 1	22 2	3 2	125	26	27 2	8 29	130	31 13	2 33	134	35 3	56 J 3	7 78	39	40 4	1142	1431	44 1 40	146	3(14)	1.43	יו עט	فلله	2 0	1	-	التابد	100	<u> </u>	-





12.3. Construction Cost

The construction costs for Schemes A, B, C, D, E, F and H were computed and are shown in Table 12.3 through 12.9. The most economical alternatives were selected by making a comparative study of various schemes investigated.

Economic comparison of schemes A, B, D, E, F and H is given in Table-12.10.

The economic studies were made using the following assumptions:

: 14 years from 1992 to 2005 Period

: 10, 12, 14, 16% Discount rate

US\$1 = P21 = \$150Exchange rate

Unit cost for evaluation : $16 \text{ Wh} = 26.071 \times 10^3 of generated energy

This value was obtained by calculating only the variable costs based on oil fired powerplants, now in operation, which have relatively poor thermal efficiency.

14.311 \$/bbl Fuel Price

6.21 MBTU/MWh Heat content 10.753 MBTU/MWh

(corresponding to thermal efficiency 31.74%)

Variable O/M Ratio 1 %

4 % Station Use Rate

The costs were calculated after converted to 1991 values by the following three classifications:

(a) Initial construction cost

Heat Rate

- (b) Maintenance cost thereafter
- Cost for evaluation of generated energy

The calculation results are summarized in Table-12.11. The most economical scheme is Scheme (E) among Plans (A), (B), (D) and (F). The additional work for Schemes (F) and (H) produce less additional generated energy as compared with the construction cost involved, and, therefore they are considered to be uneconomical.

Table-12.3 Scheme A: Removal of Sediments by Big Dredging Boat

				:				Unit:	Unit: US\$ 1,000
Work Item	Quantity	Amount	Unit Price	1992	1993	1994	1995	1996	1997
1. Associated Work for Dredging	I ES	400		160	240				
2. Disposal Pond	1 LS	1,000	·	400	009				3
3. Dredging Equipment	T TS	22,640		6,792	15,848				
4. Dredging Work	2,250 × 10° m²/year	18.000				4,500	4,500	4,500	4,500
Total		42,040		7,352	16,688	4,500	4,500	4,500	4,500

Table - 12.4 Scheme B: Heightening of the Existing Intake Tower

-									
Work Item	Quantity	Amonnt	Unit Price	1992	1993	1994	1995	1996	1997
Construction Road	L= 500m	640		6 4 0					
Crusher-run	15,000m³	: -							C-A-C-A-C-A-C-A-C-A-C-A-C-A-C-A-C-A-C-A
Slope Protection	500m					-			
Concrete Pavement	700m³								
Excavation		2,910		700	750	750	710		
Cutting									A.T. V.
Steel Pile Foundation	5m×80PCS								- Al-Carden Marie - Al-Carden
3. Piling Work		17.950		950	5,000	5,000	5,000	2,000	
Steel Pile	80m×80PCS								
Concrete	3,620m								Charles and and
Reinforcement of Intake Tower		2,500			:			2,500	
Removal of Top of Intake Tower	1 LS	1,550					1,550		
6. Manufacture of Ring	1 LS	850					500	350	
7. Installation of Ring	1 LS	9,170						4,430	4,740
Disassenbly of Barge	1 LS	300	•						300
Total		35,870		2,290	5,750	5.7 5 0	7,760	9,280	5,040
1					7				

Table - 12.5 Scheme C: Provision of a Large Capacity Sediment Removal Facility

		:						Unit:US\$	US\$ 1,000
Work I tem	Quantity	Amount	Unit Price	1992	1993	1994	1995	1996	1997
. Civil Work		3 2,5 5 0		2,1.7.7	9,271	12,525	8,577		recognistic reco
1. Tunneling Work		8,400		5 1 9	3,007	2,593	2,281		
Temporary Facility	1 LS							~	
Excavation	65,100m								·
Concrete	9,700m								
Inlet		606		205	452	246	-		
Concrete	2,580m				·	:			
3. Discharge-zone Work		23,247		1,453	5.812	9,686	6,296		A CAMPA AND AND AND AND AND AND AND AND AND AN
Temporary Facility	1 LS								
Excavation	223,330 m								
Concrete Embankment &	71,800m							Anna Canada de V	
Disposal of Sediment	223,33Uiir								
I. Gate Work		17,150		507	6.724	1,344	6,019	2,5 5 6	
1. Temporary Work	1 LS	1,762			881		176	705	
	-	•						-	
2. Manufacture of Gate	1046	9,118		507	4,052		4,052	507	
Transport & Installation Cost	1 LS	6,270			1,791	1,344	1,791	1,344	
Total		49,700		2,684	15,995	13,869	14,596	2,556	
The second secon									

Table - 12.6 Scheme D: Provision of a New Intake Tower (Inclined Type)

1997														
1996				·							.830	300	1,130	
1995				:			610	610		1,550	3,8 2 0		5,980	
1994					3,500		1,670	1,500	170		1,780		6,950	
1993			0 0 9		2,500		200		200		7,510		10,810	
1992	6 4 0		009			:				:			1,240	
70.1 10.1	: "													
Amount	640		1.200		0.000		2,480			1,550	13,940	300	2 6,1 1 0	
Quantity	L = 500m 15,000m	500m 700m		5m×33PCS		60m×33PCS 1,300m				250m²	1 LS	1 LS		<u> </u>
Work I tem	1. Construction Road Crusher-run	Slope Protection Concrete Pavement	2. Excavation	Cutting Steel Pile Foundation	3. Piling Work	Steel Pile Concrete	4. Concreting of Support	Under Water	On the Water	5. Removal of Top of Intake Tower	6. Slide Gate	7. Disassembly of Barge	Total	
	I tem Quantity Amount Price 1992 1993 1994 1995 1996 1	Work Item Quantity Amount Price Price 1992 1994 1995 1996 1 Construction Road L= 500m 640 640 640 640 6940 696<	Work Item Quantity Amount Price Price 1992 1994 1995 1996 1 Construction Road L= 500m 640 640 640 640 640 Crusher—run 500m 500m 500m 640 640 640 640 Concrete Pavement 700m 700m 640 640 640 640 640	Work I tem Quantity Amount Price Price 1992 1994 1995 1996 1 Construction Road L= 500m 640 640 640 640 690 690 690 690 690 600	Work Item Quantity Amount Price Price 1992 1993 1994 1995 1996 1 Construction Road L= 500m 640	Work I tem Quantity Amount Price 1992 1993 1994 1995 1996 1 Construction Road L= 500m 640	Work Item Quantity Amount Price 1992 1994 1995 1996 1 Construction Road L= 500m 640 640 640 1995 1996 1 Crusher—run 500m² 500m² 500m² 1200m² 1200m² <td< td=""><td>Quantity Amount Price 1992 1993 1994 1995 1996 1 L= 500m 640 640 640 640 640 660 600</td><td>Work Item Quantity Amount Price 1992 1994 1995 1996 1 Construction Road L= 500m 640 640 640 1995 1994 1995 1996 <</td><td>L= 500m 640 640 640 1993 1994 1995 1996 1996 15.000m² 640 640 1995 1996 1996 1996 500m² 600m² 1,200 600<td>Quantity Amount Price 1992 1993 1994 1995 1996 1 L= 500m 640 640 500m 700m 640 600 600 600m 33PCS 5m×33PCS 6000 600 3.500 610 60m×33PCS 1,300m 600 600 600 610 2,480 200 1,670 610 1,550 610 1,550 1,550 1,550</td><td>Quantity Amount Price 1992 1993 1994 1995 1996 1 L= 500m 500m 700m 700m 700m 1.200 600 600 600 5m×33PCS 6,000 6,000 2,500 1,500 6,100 6,100 1,550 1,550 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580</td><td>Quantity Amount Prile 1992 1994 1995 1996 1 L= 500m 640 640 640 1500m 1995 1995 1996</td><td>Quantity Amount Price to the control of the contro</td></td></td<>	Quantity Amount Price 1992 1993 1994 1995 1996 1 L= 500m 640 640 640 640 640 660 600	Work Item Quantity Amount Price 1992 1994 1995 1996 1 Construction Road L= 500m 640 640 640 1995 1994 1995 1996 <	L= 500m 640 640 640 1993 1994 1995 1996 1996 15.000m² 640 640 1995 1996 1996 1996 500m² 600m² 1,200 600 <td>Quantity Amount Price 1992 1993 1994 1995 1996 1 L= 500m 640 640 500m 700m 640 600 600 600m 33PCS 5m×33PCS 6000 600 3.500 610 60m×33PCS 1,300m 600 600 600 610 2,480 200 1,670 610 1,550 610 1,550 1,550 1,550</td> <td>Quantity Amount Price 1992 1993 1994 1995 1996 1 L= 500m 500m 700m 700m 700m 1.200 600 600 600 5m×33PCS 6,000 6,000 2,500 1,500 6,100 6,100 1,550 1,550 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580</td> <td>Quantity Amount Prile 1992 1994 1995 1996 1 L= 500m 640 640 640 1500m 1995 1995 1996</td> <td>Quantity Amount Price to the control of the contro</td>	Quantity Amount Price 1992 1993 1994 1995 1996 1 L= 500m 640 640 500m 700m 640 600 600 600m 33PCS 5m×33PCS 6000 600 3.500 610 60m×33PCS 1,300m 600 600 600 610 2,480 200 1,670 610 1,550 610 1,550 1,550 1,550	Quantity Amount Price 1992 1993 1994 1995 1996 1 L= 500m 500m 700m 700m 700m 1.200 600 600 600 5m×33PCS 6,000 6,000 2,500 1,500 6,100 6,100 1,550 1,550 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580 1,580	Quantity Amount Prile 1992 1994 1995 1996 1 L= 500m 640 640 640 1500m 1995 1995 1996	Quantity Amount Price to the control of the contro

Table - 12.7 Scheme E: Provision of a New Intake (Vertical Type)

		1.21 - 1011			: : : : :			Unit:	Unit: USB 1,000
Work I tem	Quantity	Amount	Unit Price	1992	1993	1994	1995	1996	1997
1. Construction Road	L= 500m	970		970					y nggandy pick a transferri
Crusher-run	26,000m	820						g-mysel Shad	
Slope Protection	500m	80							
Concrete Pavement	700m²	70							
2. Work shop									
Cutting	25,000m	200		200					
3. Pneumatic Caisson		1,7 0 0			1,000	200			
Excavation	5,000m	325						The second second	
Concrete	1,100m²	198							
Temporary Facility	LS	1,177							
4. Shaft		3,910				3,300	0 1 0		
Drilling	7,000m	280							
Concrete	3,100m	775							
Temporary Facility	1 LS	2,855							
5. Plugging Work	550 m	350					350		
6. Intake Tower	8 gates	520					520		
7. Sylinder Gate	1 1.8	11,700			5.637	3,283	2,4 1 0	370	
Total		19,350		1,170	6,637	7,283	3,890	370	

Table - 12.8 Scheme F: Rever-bed Excavation

				- 1	ŀ	ē		Unit	Unit:US\$ 1,000
Work Item	Quantity	Aniount	Price	1992	1993	1994	1995	1996	1997
1. Access Road	L= 2,500m	152						1 22	
Excavation	4,000m²							:	
Slope Protection	500m²		· .						, in the second sec
Pavement Work	400 m²								
2. Riverbed Arrangement Work		1,181						1,181	
Temporary Work	1 LS		 					-	•
Excavation	75,000m²		·		:				
Disposal of Sediment	75,000 m		:	:	:		**		OPOVIA POTENTIAL PARTIES PARTI
Others	L S								
Tota1		1,333						1,333	ing the graph of the graph and and
							: 		
		L							

Table - 12.9 Scheme H: Tailrace Extension

				1					
Quantity	tity	Amount	Price	1992	1993	1994	1995	1996	1997
L= 2.5	m 0 0	640				640			
75,000m² 3,500m³ 700m²	5,000 m ³ 3,5 00 m ³ 700 m ³								
1 1 6		3.6.0					160	200	
2,143 u ² 360u ² 245u ²	143 ur 360 ur 245 nr								M. COLOMBIA COLOMBIA MARIANA COLOMBIA
		10,900				3,500	7.300	100	
1 LS 152,600m ² 20,544m ²	0 m² 4 m²								
ı Ls		009					200	100	
19,250 m² 622 m²	250 m² 622 m²								
		11,900				4,140	7,460	300	

2030 2035

	Statement of the statem	18.7	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2005	2010	2015	2020	2025	2030	2035
Gene	erated Energy Estimate (GV (Potential)	νη) 	352.2	358.7	358.3	358.0	357.6	357.3	357.0	356.8	356.5	356, 2	355.9	355.4	355.1	354.7	354, 2	351.3	345.7	339.2	325, 1	315.7	314.5
~		Physioglady in the Principle of the Constitution of the Constituti	giftemanika maran sila banan sali dayar melakkaba	and the state of t		gangan awarefuse dun semen	aligne and control of the state	-	agin about indig a Marija wa Marija wa a	_	ngir distribili infonfisiona kalap navoran			وجود ماشد مستعد جمع موجود التر	ga.,Nooga.Wayaaga.Waxee								
Schei		Year Item	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2005	2010	2015	2020	2025	2030	2035
	Removal of Sediments by Big Dredging Boat	Generated Energy (GWH)	352.2	358.7	358.3	358.0	357.6	357.3	357.0	356.8	356.5	356.2	355.5	355.2	355.1	354.7	354.2	351, 3	345.7	339.2	325.1	315.7	314.5
Α	213, 040	Construction Cost						7352	16688	4500	4500	4500	4500	4500	4500	4500	4500	4500	4500	4500	4500	4500	4500
A	· ·	Suspension of Current (S/C)									_	_ :				_							
		Energy to be used (GWH)		_	_		_				27.0	27.0	27.0	27,0	27.0 —	27.0	27.0	27.0	27.0	27.0	27.0	27.0	27.0
	Heightening of the	Generated Energy (GWH)	352.2	358.7	358.3	358.0	357.6							355.2	354.9	354.6	352.5	350.4	345.7	339.8	325. 1	316.4	314.5
	Existing Intake Tower 51,281	Construction Cost						2290	5750	5750	7760	9280	5040	00012			5137	. 000.4	5137	000.0	5137		014.0
В	V1,201	Suspension of Current (S/C)	-					S/C	s/c	s/c	s/c	S/C	S/C				0101		0101		2101		
		Energy to be used (GWH)								3/ 0			3/ 0										
-	Provision of a Large	Generated Energy					0.57.0					<u> </u>		055.0	054.0		050	050	A 15 -	000			
	Capacity Sediment Removal Facility	(GWH) Construction Cost	352.2	358.7	358.3	358.0	357.6						355.5	355.2	354.9	354.6	352.5	350.4	345.7	339.8	32 <u>5.</u> 1	316.4	314.5
C	49, 700	Suspension of					· · · · · · · · · · · · · · · · · · ·	2684	15995	13869	14596	2556											·
		Current (S/C) Energy to be used			· · ·			<u> </u>						·									:
	Provision of a New Intake	(GWH) Generated Energy							· · · · · · · · · · · · · · · · · · ·														
	Tower (Inclined Type)	(GWH)	352.2	358.7	358.3	358.0	357.6						355.5	355.2	354.9	354.6	352.5	350.4	345.7	339.8	325.1	316.4	314.5
D	26, 110	Construction Cost Suspension of						1240	10810	6950	5980	1130											
		Current (S/C) Energy to be used	<u>:</u>						s/c	s/c	s/c	S/C											ļ ————
	Provision of a New Intake	(GWH)								···													
- 1	Trovision of a New Intake Tower (Vertical Type)	(GWH)	352.2	358.7	358.3	358.0	357.6	391.7	342.9	342.0	339.1	333.6	355.5	355.2	354.9	354.6	352.5	350.4	345.7	339.8	325.1	316.4	314.5
E	19, 350	Construction Cost Suspension of	:					1170	6637	7283	3890	370											
		Current (S/C)						Plant Operated at LWL))	S/C	"											
		Energy to be used (GWH)						Jan∼Mar	Apr∼Jun Jan∼Mar	Apr∼Jun Jan∼Mar	Apr∼Jun Jan∼Mar	Apr∼Jun									·		
	Rever-bed Excavation	Generated Energy (GWH)							3.0	3.0	2.7	2.6	2.7	2.7	2.7	2.7	2.7	2.7	2.7	2.6	2.5	2.4	2.4
F	13, 800	Construction Cost										1333		733		733		3667		3667		3667	
<u>,</u>	,	Suspension of Current (S/C)																					
		Energy to be used (GWH)																			,		
	Tailrace Extension	Generated Energy (GWH)					; ;						1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.1	1, 1	1.0	1.0
	11,900	Construction Cost								4140	7460	300	1, 4	1 • 4	1.4	1.2		1,4	116	1. [. 1, 1	1. V	1,0
H		Suspension of Current (S/C)										ovv Apr∼Ma y											
		Energy to be used (GWH)									jan~mar	apa mety					1 .			:			
		12 - 75											L	<u> </u>			L		<u> </u>			L	<u> </u>

Table - 12.11

Calculation Result (1)

	_		Discount R	ate (%)	
Scheme	Cost	10	12	1 4	16
	(a)	3,3 1 7.0 0	3,1 8 6.9 5	3,0 6 4.4 7	2,9 4 8.9 8
	(b)	5,4 3 5.1 6	4,7 0 7.2 9	4,099.27	3,5 8 8.2 6
Α	Total	8,7 5 2.1 6	7.894.24	7,1 6 3.7 4	6,5 3 7.2 4
	(106 \$)	(65.12)	(58.74)	(53.30)	(48.64)
	(a)	3,7 5 9.1 8	3,5 2 0.8 0	3,3 0 3.7 1	3,1 0 5.5 8
	(b)	202.92	1 5 7.6 8	1 2 3.0 7	96.48
В	Total	3,962.10	3,6 7 8.4 8	3,4 2 6.7 8	3,2 0 2.0 6
	(10 ⁶ \$)	(29.48)	(27.37)	(25.50)	(23.82)
	(a)	3.01 0.3 3	2,8 6 6.9 9	2,7 3 3.6 4	2,6 0 9.3 8
D	(10°\$)	(22.40)	(21.33)	(20.34)	(19.42)
Е	(a)	2,2 8 4.9 2	2,179.35	2,0 8 0.9 4	1,9 8 9.0 5
E	(10 ⁶ \$)	(17.00)	(16.22)	(15.48)	(14.80)
	(a)	287.27	282.14	277.19	272.41
	(b)	1,4 2 0.6 7	1,261.77	1,1 2 7.4 7	1,0 1 3.2 0
F	Total	1,7 0 7.9 4	1,5 4 3.9 1	1,4 0 4.6 6	1,285.61
	(106 \$)	(12.71)	(11.49)	(1045)	(9.57)
	(c)	(0.465)	(0.414)	(0.371)	(0.334)
	(a)	1,2 5 8.8 0	1,178.69	1,1 0 5.0 7	1,0 3 7.2 9
Н	(106 \$)	(9.37)	(8.77)	(8.22)	(7.72)
	(c)	(0.112)	(0.095)	(0.080)	(0.069)

(Note) Unit: 100 Million Yen, However Unit in parenthesis is US\$ 106

Calculation Result(2) Cost for evaluation of generated energy in plan(A)

0.1				Discount	Rate (%)	
Scheme	Cost	*	1 0	12	1 4	16
Α	(106\$)		(3.43)	(2.97)	(2.59)	(2.27)

12.4. Total Cost and Further Investigation for Rehabilitation Work

12.4.1. Estimate of Total Cost for Rehabilitation Work

The total cost for the proposed rehabilitation work including the rehabilitation work required for the intake tower, Scheme E, is shown in Table 12.12. The cost of the construction work in foreign and local currencies and the associated yearly expenses are summarized in Tables-12.13 through 12.19.

12.4.2. Further Investigation for Rehabilitation Work

It is essential to undertake additional survey and investigation prior to the implementation of the rehabilitation program as mentioned below, so as to ensure a smoother progress of the detailed design work. Such survey and investigation should be commenced from 1989 and completed by the end of 1990 at the latest. (See Table-12.20)

(1) Topographic Survey

A considerable area was covered by the additional topographic survey work done for this report, but further survey will be needed to confirm the adequacy of the proposed sites for the new intake tower and dredging facilities, and the proposed quarry site and spoil bank. Also additionally needed is sounding survey of the upstream side slope of the dam and route survey for the construction of access roads to the tailrace.

(2) Boring Tests

A series of additional geological survey will be needed to support the study of designing and construction methodology of structures. To be covered by the survey is the geology of the proposed site for the new intake tower, particularly for the vertical shaft and its connection to the existing headrace tunnel, and the distribution of base rock masses at the quarry site. Boring tests will also be needed for clarifying the geology and soil properties of the proposed spoil bank and two sedimentation basins for dredging. Some 20 bores with a total length of about 800 m will be required for the purpose.

(3) Geophysical Prospecting

Upon confirmation to some extent of the geology of the quarry site by boring tests, further detailed investigation by means of seismic prospecting and exploratory drilling should be done to clarify the distribution of rock masses. Field rock tests should also be done, utilizing a drain adit installed on the left bank of the spillway.

(4) Other Tests

Laboratory tests of soil and rock materials for the dam embankment and the spoil bank foundation should be done on the samples taken from the boring tests and other geological investigations to support the design work. Soil and rock materials in the fault zone in the vicinity of the left bank of the spillway should also be tested for future design work. It may also be useful for the future dredging program to make laboratory tests on the samples of sand silts in the reservoir, including among others congulation test, sedimentation test and consolidation test.

Besides, it may be necessary to check the state of the turbine inlet valves to support the planning of repair and replacement. Chances of repairing turbines should be utilized for the check. It may also be necessary to check the state of the inlet of the existing intake tower to prepare for the future design work and the planning of work schedules. The check may be done in detail by sending a diver down to the inlet at the time when the reservoir water level comes down and the plant can be taken out of service.

Table - 12.12 Summary of Rehabilitation Cost for Ambuklao Dam

Unit: US\$ 1Million

	·		Unit : U	S\$ 1 Million
	Work Item	Foreign Portion	Local Portion	Total
1.	Cost for Rehabilitation Work			
	Improvement of Intake Tower	1 2.5 2 2	6.8 2 8	1 9.3 5 0
	Improvement of Turbine Inlet Valve	1.8 0 0	0.3 3 3	2.1 3 3
	Riverbed Arrangement at Tailrace Outlet	0.347	0.986	1.333
	Dredging around Intake Tower	3.1 8 0	2.2 7 6	5.4 5 6
	Dam Upstream Face Rehabilitation	1.907	5.4 2 6	7.333
	Subtotal	1 9.7 5 6	1 5.8 4 9	3 5.6 0 5
2.	Cost for Investigation			
	Boring		0.1 1 3	0.1 1 3
	Physical Prospecting	_	0.020	0.020
	Survey	_	0.180	0.180
	Tests	<u> </u>	0.057	0.057
	Subtotal		0.3 7 0	0.3 7 0
3.	Right of way Cost	· · · -	0.5 0 0	0.5 0 0
4.	Engineering Fee	1.8 0 0	_	1.8 0 0
5.	NAPOCOR Administration Fee	_	0.6 0 0	0.6 0 0
6.	Contingency	1.9 4 1	1.6 2 0	3.5 6 1
7.	Total	2 3.4 9 7	1 8.9 3 9	4 2.4 3 6
		4		I

Table - 12.13 Yearly Expenses for Rehabilitation Work

	Warly Item	Total Cost	1 080	1990	1001	1 900	1 00 3	1004	C	7000
	ווסוע דינווו	n l	1.503	9	•	3	5	1 234	1880	1220
- V/E		1,000 \$								
	1. Rehabilitation Cost									
	Intake Tower	19,350.0				1,170.0	6,636.7	7,283.3	3,890.0	370.0
	Turbine Inlet Valve	2,133.0								2,133.0
	Tailrace Outlet Area	1,333.0								1,333.0
	₹X	(5,456.0)		4.6.6.6	1.346.6	1.426.7	27 25 25 25 25 25 25 25 25 25 25 25 25 25	83 103 203	80 H 80	20 20 20 20 20 20 20 20 20 20 20 20 20 2
	Tillane tower Area	3,705.3			1333	::22£0::	五季6季		五字D至二	13. 李①李…
	Dam Upstream Face	7,333.0					2000	2.200.0	2,666.7	2,266.3
	4777844 B B F F F B B B B B F F F B B B B B B	☆ (35,605.0)		(406.6)	(1,479.9)	(3,120.7)	(7,241.4)	(9,888.0)	(6,961.4)	(6,507.0)
12	* I E 1 O 1 O N O	33,854.3			133.3	1,694.0	7,598.7	10,245.3	7,318.7	6,864.3
- 81	2. Investigation Cost	370.0	200.0	170.0						
	3. Right-of-way Cost	500.0			166.7	166.6	166.7			
	4. Engineering Fee	1,800.0	466.6	466.7	466.7	400.0				
	5. NAPOCOR Administration Fee	600.0		66.7	66.7	93.3	93.3	93.3	93.3	93.4
	6. Contingency	(3,561.0)		40.7	148.0	312.1	724.1	988.8	696.1	651.2
		会(42,436.0)	(666.6)	(1,150.7)	(2,328.0)	(4,092.7)	(8,225.5)	(10,970.1)	(7,750.8)	(7,251.6)
	**************************************	40,685.3	9.999	744.1	981.4	2,666.0	8.582.8	11,327.4	8,108.1	7,608.9

★:
*:
*:
*:
*:

Table-12.14(a) Scheme E (Vertical Intake Tower) Construction Cost (Na 1)

						UIII U	: 02 2 1
Work Item	Specification	Q'ty	Unit	Unit Price	F.C.	L.C.	Total
A. Civil Work		:					
1. Construction Road						970,000	970,000
Excavation		5,000	щ³	8		40,000	40,000
Crusher-run		26,000	ım³	30		780,000	780,000
Slope Protection		500	m	160		80,000	80,000
Concrete Pavement		700	m³	100		70,000	70,000
2. Working Area							
Excavation	Cutting	25,000	m³	8		200,000	200,000
3. Pneumatic Caisson					470,800	1,229,200	1,700,000
Temporary Facility					470,800	655,200	1,126,000
Excavation		5,000	LU3	65		325,000	325,000
Concreting		1,100	m³	180		198,000	198,000
Re-bar		51	ton	1,000		51,000	51,000
4. Shaft					1,091,200	2,818,800	3,910,000
Temborary Facility		1	LS		1,091,200	1,518,800	2,610,000
Excavation		7,000	m,	75		525,000	525,000
Concreting		3,100	m'	250		775.000	775,000
5. Plugging Work				:	74,000	276,000	350,000
Temporary Facility	.i :	1	LS		74,000	102,950	176,950
Removal of Concrete		70	u,	115		8,050	8.050
Concreting		550	m³	300		165,000	165,000
6. Stop log					353,000	167,000	520,000
Setting of log		1	LS		115,000	142,000	257,000
Setting Equipment		1	LS		160,000	. —	160,000
Others		1	LS		78,000	25,000	103,000
Total					1,989,000	5,661,000	7,650,000

Table-12.14(b) Scheme E (Vertical Intake Tower) Construction Cost (Na 2)

The second secon		·		·		UNI	t: US \$ 1
Work Item	Specification	Q'ty	Unit	Unit Price	F.C.	L.C.	Total
B. Intake Tower Construction	Tower						
1. Temp or ary Facility	Crane etc	1	LS		467,000	133,000	600,000
2. Embedded Portion					867,000	367,000	1,234,000
Manufac ture		F.C70 L.C70	ton ton	7,640.00 3,330.00		233,100	767,900
Installation		. 1	LS		332,200	133,900	466,100
3. Intake Tower	-				6,246,000	267,000	6,513,000
Manufac ture		600	ton	7,640.00	4,584,000	_	4,584,000
Installation		1	LS		1,662,000	267,000	1,929,000
4. Sleeve Gate					1,140,000	67,000	1,207,000
Manufacture		110	ton	7,640.00	840,400		840,400
Installation	·	1	LS	1.1	299,600	67,000	366,600
5. Hoisting Winch			·		1,813,000	133,000	1,946,000
Manufacture		180	ton	7,640.00	1,375,200	-	1,375,200
Installation		1	LS		437,800	133,000	570,800
6. Bridge			· · · · · · · · · · · · · · · · · · ·		- Production	200,000	200,000
Manufacture		40	ton	3.330.00		133,200	133,200
Installation		1	LS	1 00 T + 00 00	_	66,800	66,800
Total					10,533,000	1,167,000	11,700,000
Grand Total					12,522,000	6,828,000	19,350,000

Table - 12.15 Cost for Turbine Inlet Valve

	·	·					UIIIV	· US \$ 1
	Work I tem	Specification	Q'ty	Unit	Unit Price	F.C.	L.C.	Total
	l. Civil Work						11,000	11,000
	Temporary Facility		1	LS		_	4,100	4,000
	Foundation Work for Accessory Equipment			1		_	2,400	2,400
	Removal of Old Foundation		5	m,	120		600	600
	Concreting for New Foundation		6	m³	300		1,800	1,800
	Foundation Work for Valve			.*			4,500	4,500
	Removal of Old Foundation		10	m³	120		1,200	1,200
	Concreting for New Foundation		11	m³	300		3,300	3,300
2	Construction Work for Valve							2,122,000
	Cost of Manufacture		90	ton	10,700	963,000		963,000
	Removal of Old Valve	THE CONTRACTOR OF THE CONTRACT	60	ton	5,350	321,000		321,000
	Installation	Removal of Old Valve, Transport & Installation of New Valve				516,000	322,000	838,000
_		Of Lifem AS ING						
	Total					1,800,000	333,000	2,133,000
Щ.								

Table - 12.16 Scheme F: Riverbed Arrangement Cost

	T	T		-		Uni	t: US \$ 1
Work Item	Specification	Q ty	Unit	Unit Price	F.C.	L.C.	Total
1. Access Road						152,000	152,000
Exeavation		4,000	m²	8		32,000	32,000
Slop Protection		500	m³	160		80,000	80,000
Concrete Pavement		400	m³	100		40,000	40,000
2. Reverbed Arrangement				· .	347,000	834,000	1,181,000
Temporary Work		1	L S		35,000	30,000	65,000
Excavation		75,000	m,	11.0	248,000	577,000	825,000
Disposal of Sediment		75,000	m³	3.2	64,000	176,000	240,000
Others		1	LS			51,000	51,000
Total					347,000	986,000	1,333,000

Table - 12.17 Dredging Cost Around Intake Tower

·		* 1 - B-80 - B-04 - C-70 - C-7				OHIL	
Work Item	Specification	Q ty	Unit	Unit Price	F.C.	L.C.	Total
A. Civil Work					0	374,000	374,000
1. Associated Work for Dredging Equipment					0	170,000	170,000
Pipe Foundation	Reinforced Concrete	430	points	132	0	56,760	56,760
Inclined Way	ditto	. 1	Ls		0	33,300	33,300
Mooring Facility		-1	LS		0	26,7 00	26,700
Working Base, Road		1	LS		0	26,7 00	26,700
Others		1	LS		0	26,540	26,540
2.Disposal Pond					0	204,000	204,000
Drainage Work	50 cm× 50 cm	800	m	34	0	27,200	27,200
Embankment	Core Type	1	LS	٠.	0	75,000	75,000
Inside Embankment		1	LS		0	90,000	90,000
Others					0	11,800	11,800
B. Dredging Equipment					2,653,333	283,334	2,936,667
Dredger	Steel-made 150 ton	1	Unit	1,727,000	1,586,334	140,666	1,727,000
Booster	125 KW	1	LS		316,000	21,000	337,000
Pipe Line	land 1,300m	1	Ls		376,666	11,334	388,000
	on water 500m	1	LS				
Electric Facility	700 KVA	1	LS		124,000	24,600	148,600
Transmission Facility		1	LS		0	83,000	83,000
Tugboat	long 12m, 150 PS	1	Unit		179,333	1 97	179,530
Other Accessory	Dredger Cable 750 m	1	LS		71,000	2,537	73,537
C. Design Cost		1	LS		526,667	0	526,667
D. Dredging Cost		1	LS		0	1,618,667	1,618,667
Total					3,180,000	2,276,000	5,456,000

Table-12.18

Breakdown of Rehabilitation Cost on Dam Upstream Face

<u> </u>	Work Item Spe	d. Qty	Unit	Unit Price	F.C.	L.C.	Total
1.	Direct Construc- tion Cost			A CONTRACT	1,254,800	3,678,400	4,933,200
	Clearing of Quarry Site	50,000	m ²	0.20\$	0	10,000	10,000
	Removal of Surface Soil	200,000	m ³	3.6 \$	200,000	520,000	720,000
	Land Grading of Disposal Area	100,000	m ³	0.6 \$	0	60,000	60,000
	Excavation - Cutting and leveling	35,000	m ³	8.0 \$	65,000	215,000	280,000
	Collection, Transport and Embankment of Rock Materials	30,000	m ³	10.1 \$	86,000	217,000	303,000
	Riprap	110,000	m ³	8.5 \$	266,000	669,000	935,000
	Excavation - Cutting and leveling under water level	25,000	m ³	31.0 \$	224,000	551,000	775,000
	Riprap-Under water level	90,000	m ³	20.0 \$	413,800	1,386,200	1,800,000
	Others	1	LS		0	50,200	50,200
2.	Common Temporary Facilities				348,900	884,400	1,233,300
3.	Site Operation				129,900	369,600	499,500
4.	Overhead		i.		173,400	493,600	667,000
	Total				1,907,000	5,426,000	7,333,000

Table-12.19 Breakdown of Rehabilitation Cost on Dam Upstream Face (Slope Gradient 1: 1.75)

	Work Item	Qty	Unit	Unit Price	F.C.	L.C.	Total
1.	Direct Construc- tion Cost				1,025,200	3,030,300	4,055,500
	Clearing of Quarry Site	50,000	_m 2	0.2	0	10,000	10,000
	Removal of Surface Soil	200,000	_m 3	3.6	200,000	520,000	720,000
	Land Grading of Disposal Area	100,000	_m 3	0,6	0	60,000	60,000
	Excavation - Cutting and leveling	49,000	_m 3	8.0	91,000	301,000	392,000
	Collection, Transport and Embankment of Rock Materials	8,000	_m 3	10.1	23,000	57,800	80,800
	Riprap	115,000	_m 3	8.5	278,000	699,500	977,500
	Excavation - Cutting and leveling under water level	15,000	_m 3	31.0	134,400	330,600	465,000
	Riprap-Under water level	65,000	m ³	20.0	298,800	1,001,200	1,300,000
	Otehrs	. 1	LS		0	50,200	50,200
2.	Common Temporary Facilities				286,800	727,100	1,013,900
3.	Site Operation				106,800	303,800	410,600
4.	Overhead				142,500	405,500	548,000
	Total				1,561,300	4,466,700	6,028,000

Valve Chamber al				Damage inspection of value butter- fly 3 spheri-
Tailrace Longitudinal and cross- sectional leveling for the access road of 2,500 m				
Intake Tower Topographical survey 15,000 m ²	Vertical shaft 100 m x 2 + 50 m x 2 = 300 m		Visual Check of Inlet (Divex - one day)	Turbine inlet valve
Dredging Topographical survey for mooring facilities and slipway cover- ing 20,000 m	Sedimentation basin dam 15 m x 2 x 2 places = 60 m	Silty adimixture		
Upstream Side Slope Sounding on 21 sections down to EL 680 m				
Spoil Bank (R) Spoil Bank (L) Upstream Side Dredging Slope Topographical Topographical Sounding on Topograph survey and to mooring 600,000 m ² EL 680 m facilities slipway.	10 m × 5 m 550 m × 5 m	Foundation Soil		
Spoil Bank (R) Topographical survey 600,000 m ²	10 m × 7 ·= 70 m	Foundation Soil		
Quarry Site Topographical survey 50,000 m ²	50 m x 6 = 300 m 3,000 m 3,000 m	material	in the second se	
Bed Rocks of the left Bank of the Spillway		Fault material	4 x 2 kinds Rock shearing test using drain adit	
Surveying	Boring Test Geophysical Prospecting Rock Pro-	perties Test Soil Pro- Perties	Field Rock Test Investi- gation of the Existing Intake Tower	Valve Inspec- tion

12.5. Economical Analysis

12.5.1. Method of Analysis

As a result of the screening test, and as explained in Paragraph 12.1.1, above, it was found that, of the five schemes studied for the problem of the reservoir sedimentation, Scheme E was the most advantageous.

An economic analysis on a system wide basis was made to determine whether an overall rehabilitation of the Ambuklao Project as described in Section 12.4, above, was economically more suitable, or substitution of the Ambuklao by another power source could be more advantageous. The above analysis was based on the data given in the "Power Development Program, 1987 to 2000", a study of power requirements made by NAPOCOR and issued in June 1987.

The above study includes energy and demand forecasts, data on the power expansion program, outputs of various power sources, and economic conditions for fixed and variable cost computations.

The basis of the analysis and its results are described below.

12.5.2. Purpose of the Analysis

In accordance with the findings of the Power Development Program of NAPOCOR (NAPOCOR Program), the expected year of retirement for the Ambuklao powerplant is 2006 or 2007, counting from its commissioning year. Loss or decrease of generation by the Ambuklao powerplant according to the program is not anticipated until after 2000.

However, the studies presented in this Report indicate that, if no measures against sedimentation are taken, loss or decrease of power generation by the Ambuklao powerplant will occur no later than 1996.

In order to prevent the above from happening, two basic alternative measures were studied. They were:

- (a) Alternative "A" Rehabilitation of the Ambuklao Project, as described in Section 12.1, above, Items (1) thru (4).
- (b) Alternative "B" Instead of the above, construction of a new geothermal plant (1 x 55 MW) with the same production capability as that of the Ambuklao powerplant. Include this in the NAPOCOR Program.

The analysis was made to determine which of the above two alternatives was more economical from point of view of the overall power system operation.

In addition to the above, a third alternative was also studied. This alternative was based on the assumption that no measures will be taken for the rehabilitation of the Ambuklao Project, but, the loss of power at the Ambuklao would be supplemented by additional power generation from the other existing plants.

This alternative is to assume no rehabilitation of the Ambuklao dam to be done and the resultant losses in capability (kW) and energy (kWH) to be made up by those attainable from the employment of the system's reserve marging capacity at the cost of the system reliability.

12.5.3. Assumptions

(1) Load demand forecast

The load demand forecast used in this analysis was in accordance with the NAPOCOR program.

(2) Power development program

Based on the NAPOCOR Program for the 1987 to 2000 period, the following alternatives were considered.

- (a) Alternative "A" Rehabilitation of the Ambuklao Project, no change to the NAPOCOR Program.
- (b) Alternative "B" No rehabilitation of the Ambuklao Project, but add a geothermal plant (1 x 55 MW) to the NAPOCOR Program.
- (c) Alternative "C" No rehabilitation of the Ambuklao Project and no change to the NAPOCOR Program.

This alternative is to assume a scenario in which the demand and energy needs would be met by placing the system's reserve margin capacity into service as a temporary measure, and should be considered as a case for reference only.

The operation and maintenance costs for the above three alternatives were taken into consideration. They were combined as required with the construction costs discussed in Section 12,3, above, and used in the economic evaluation of the above alternatives. As discussed further below, for economic comparison, the Internal Rate of Return for each alternative was computed and comparison made.

(3) Period of analysis and cost computation

The power demand forecast and the required power development given in the NAPOCOR's Program cover the period to year 2000.

Reduction in generation of the Ambuklao powerplant will start in 1990, if no rehabilitation work is carried out, and its operation will be discontinued in or after 1996. Therefore, the system wide analysis was made for five years covering the period from 1996 to 2000. The cash flow from 2001 to 2050 was calculated assuming that 90 percent of the initial investment cost will be reinvested at every depreciation period of the powerplant, and there would be no change in the O/M cost.

The cost for the Ambuklao Dam rehabilitation was assumed to be disbursed from 1992 to 1996.

(4) Measures for shortage of power generation during rehabilitation

The work on the dam rehabilitation will be carried out during the dry seasons, from 1992 to 1994, by lowering the reservoir water level. During the dry seasons from 1995 to 1996, the generation will have to be suspended intermittently. However, since dead discharge is not considered during the above period, the influence of the decrease in generation of the Ambuklao powerplant on the whole system could be ignored from point of view of system wide analysis as the decrease could be supplemented by the operation of other plants.

Therefore, no investment was considered for measures against shortage of power generation during rehabilita-

tion. The power demand-supply balance for the period of no operation of the Ambuklao powerplant is covered in the following Section.

(5) Evaluation of the output decrease after completion of the rehabilitation

Even after the completion of the rehabilitation of the Ambuklao Project, the power output may decrease due to the increase in sediment. The annual output at normal water level in 1996 is estimated at 356.2 GWh, and for 2000, at 354.6 GWh. Since the estimated decrease will be only 1.6 GWh (0.45%), the output for each year between 1996 and 2000 was assumed for the system wide analysis the same as that for 2000.

(6) Cost calculation

To calculate the cost for each alternative, the investment cost for Alternative "A" consists of the investment cost provided in the NAPOCOR's Program plus rehabilitation work cost. For Alternative "B", the investment cost consists of the one shown in the NAPOCOR's Program plus the cost of a new geothermal plant, and for Alternative "C", the investment cost is assumed to be the same as that in the NAPOCOR's Program.

For calculation of operation and maintenance cost (0/M), a system wide analysis for each alternative was made to determine the optimum load sharing by each power source. After that, the cost for each type of fuel was calculated. The results are shown in Table-12.5.21.

12.5.4. Outline of the Results

The Internal Rate of Return (IRR) of Alternative "A" with regard to Alternative "B" was 42.84 percent, and that of Alternative "A" to Alternative "C", 17.78 percent.

Therefore, or the basis of the above, it is judged that the rehabilitation of the Ambuklao Project as described in Section 12.1, and specified as Alternative "A", above, is the most advantageous solution.

12.5.5. Procedure used for the Analysis

The procedure used in the analysis was as follows:

(1) Energy and demand forecast

Table-12.5.1 shows the energy and demand forecasts given in the NAPOCOR Program. For these studies, the values at the sending end were used. The sent out energy and demand at the sending end were regarded to be 96% of the generation level value.

Normally, generation level values are not used for this type of studies, as the evaluation of the station used portion is considered to be difficult.

The above rate of 96% was roughly determined, but it is considered to be adequate, as the purpose of the studies is comparison of alternatives.

Table-12.5.2 shows the analysis of the actual records of hourly demand for 1986. A year is divided into following four periods:

Designation

Period

I	January - March
II	April - June
III	July - September
TV	October - December

In Figs.-12.5.1-7, the values of Table-12.5.2 are presented graphically. Each figure indicates the load factor for the period.

Table-12.5.3 shows the modified load duration curve for each period (P.U.).

Table-12.5.4 shows the maximum MW ratio for the period so that the yearly load factor is 70% when the ratio of the load factor to the generated energy for the period does not change.

As the yearly load factor for the future is estimated to be 70%, as shown in Table-12.5.1, the duration curve for each future year is assumed to show the same pattern as that in 1986. The load demand for each period of each year is calculated using the demand at the sending end shown in Table-12.5.1, modified load duration, given in Table-12.5.3, and the tabulated data for load demand, shown in Table-12.5.4.

(2) Installed capacity and output at the sending end

A list of installed capacities of the existing powerplants is given in Table-12.5.5.

Table-12.5.6 shows installed capacities, classified by plant type, as given in the NAPOCOR Program for the

period from 1986 to 2000 and considering the power expansion program.

The output at the sending end for 1995 classified by plant type are given in Table-12.5.7.

Table-12.5.8 shows output at the sending end of the reservoir type hydro powerplants which are expected to be developed after 1996.

Table-12.5.9 shows the total output at the sending end of the run-of-river type hydro powerplants.

Table-12.5.10 shows the output of the reservoir type hydro powerplants from 1996 to 2000, classified by alternative.

Table-12.5.11 shows the output of the geothermal powerplants sending end from 1996 to 2000, classified by alternative.

The output of the geothermal powerplants to be developed after 1996 is calculated using the condition of geothermal plants shown in Table-12.5.7. The output of Coal "A" (2 x 150 MW) and Coal "B" (2 x 55 MW) plants are calculated, using the condition for Isabela plant shown in Table-12.5.7.

Table-12.5.12 shows the output at the sending end of Alternative "A" from 1996 to 2000, classified by plant type.

(3) Average generation

Table-12.5.13 shows the average monthly generation by

hydro powerplants. The values are calculated, based on the NAPOCOR's actual and planning data, however, those of the Ambuklao powerplant are estimated.

Tables-12.5.14 and 15 show the average generation (at the sending end) of the reservoir type hydro and run-of-the river type hydro powerplants, respectively, for each period.

Table-12.5.16 shows the average generation (at the sending end) of the reservoir type hydro powerplants, for each alternative.

(4) Unit cost calculation

Table-12.5.17 shows the annual fixed costs (\$/kW-year) for the Ambuklao Project, and the geothermal (1 x 55 MW) powerplant.

The Table-12.5.18 shows the variable costs (\$/MWh), classified by plant type. All these values are unit costs/kW and MWh at the sending end.

With regard to the data shown in Table 12.5.18, the following should be noted:

The variable cost of gas-turbine powerplants is highest, followed by oil-fired (Manila, Sucat, Malaya), oil fired (Bataan), coal-fired (Isabela) and coal-fired (Calaca) powerplants.

Assuming that the pumping-up efficiency is 70%, the variable cost for pumping-up of coal-fired (Calaca) is lower than that at oil-fired (Manila, Sucat, Malaya) powerplants. The variable costs for pumping-up of oil-

fired and coal-fired powerplants are lower than that of gas-turbine powerplants.

(5) Loading order of thermal power plants

On the basis of the above variable cost comparison, it is judged that the loading order of thermal powerplants should be as follows:

- (1) Coal-fired (Calaca).
- (2) Coal-fired (Isabela and Equivalent).
- (3) Oil-fired (Bataan).
- (4) Coal-fired (Calaca) for pumping up.
- (5) Oil-fired (Manila, Sucat, Malaya).
- (6) Coal-fired (Isabela and Equivalent) for pumping up.
- (7) Oil-fired (Bataan) for pumping up.
- (8) Oil-fired (Manila, Sucat, Malaya) for pumping up.
- (9) Gas-turbine.

The criteria for the optimum operation of the powerplants should be as follows:

Most power generation should be made by operating to the maximum possible extent the available geothermal and coal-fired plants. If surplus energy generated is made available during the off-peak time, it should be used for pumping up. By operating the pumped storage plants, power generation by oil-fired plants (Manila, Sucat, Malaya) should be reduced as much as possible.

When the output at the sending end does not meet the system peak demand, although the oil-fired plants (Manila, Sucat, Malaya) are fully operated, it should be supplemented by pumped storage energy made possible by the use of the off-peak available energy.

If additional energy is required during peak demand, gas-turbine plants should be operated.

(6) Optimum output and generation mix by plant type

The optimum output and generation mix by plant type are computed for each alternative in accordance with load orders and summarized in Tables 12.5.19 (1) to (3) and Tables-12.5.20 (1) - (3), respectively. In these computations, Min./Max. Ratio, shown in Table-12.5.7, were considered.

In Table-12.5.21, the O/M costs of each alternative for the period from 1996 to 2000 are listed. This was obtained by multiplying the variable O/M cost of each plant by the generated energy, based on the computation results shown in Tables-12.5.20 (1) to (3). The coalfired (300 MW/unit) were assumed to be in full operation for each alternative.

The data shown in Table 12.5.21 include pumping up energy shown in parenthesis in Tables 12.5.20(1) to (3).

(7) Calculation of Internal Rate of Return (IRR)

Based on the investment and operation and maintenance costs, a cash flow was developed to calculate the IRR, assuming the Ambuklao Rehabilitation, Alternative "A", as COST, and Alternatives "B" and "C", as BENEFIT.

The results of the above are shown in Tables-12.5.22 & 23 and in Fig.-12.5.8. & 9.

(8) Balance of power demand and supply caused by interruption of power generation by Ambuklao during rehabilitation

Intermittent suspension of power generation at the Ambuklao Project during rehabilitation will be necessary during the periods January - March and April - June 1995, and April - June 1996. The balance of power demand and supply for the period April - June 1996 was examined.

In such cases, the power demand and supply balance is normally adjusted by rearranging the regular repair program for thermal plants, or by changing the reservoir utilization program of other hydro powerplants as required for covering the above balance.

The worst case of when none of the above measures have been taken at the time of suspension of the Ambuklao powerplant operation is presented below.

Alternative "C" studied above is a case for which the operation of the Ambuklao powerplant has been suspended since rehabilitation of the project has not been carried out. The situation for Period II in 1996 shown in Table -12.5.19 (3) is almost the same as that at the time of suspension of plant operation due to rehabilitation.

In Table-12.5.24, the above situation is shown again with the potential capacity at that time. The parenthesis in Table-12.5.24 shows the potential capacity disregarding economic considerations. This table shows the system still has sufficient reserve margin even when the consumption for forced outage, maintenance and station use, have been taken into account.

Therefore, even without any special provisions for additional power supply during suspension of power generation, the rehabilitation work carried out on the Ambuklao Project is not expected to adversely affect the balance of power demand and supply.

12.5.6. Conclusion

The economic justification for the Ambuklao Rehabilitation Project was evaluated by a system wide analysis covering the entire Luzon Grid of NAPOCOR.

The benefit of attaining the increased capability (kW) and energy (kWH) by the rehabilitation of the Ambuklao dam is by far the most advantageous, as clearly indicated by the above The IRR of the measure is found to be as high as study. 42.24% when compared with the Alternative "B", and 17.69% even against the Alternative "C". The Alternative "B" is to assume the addition of a geothermal capacity (1 x 55 MW) as a substitute power source. The Alternative "C" is to assume no addition of such substitute power source and any output requirements to be met only by putting the reserve margin capacity into service with the resultant degradation of the system reliability. In this scenario, the required system output would be obtained by increasing the capacity factor of power sources with relatively high variable costs, which could in turn result in the increment of variable costs in operating the whole system.

The comparison of the alternatives for the economic analysis should be made under the equal condition in the system reliability. The Alternative "C" is an exceptional case in which the demand would be met by employing the reserve margin capacity at the cost of the system reliability.

Since development of substitute resources do not increase the energy generated by the existing powerplants with high variable cost, the above leads to the increase of the variable cost for the whole system.

Table - 12.5.1 Energy and Demand Forecast in Luzon Grid

F. Y	Sales level (GWh)	Generation level (GWh)	Generation level (MW)	Sentout Energy (GWh)	Demand at Sending End (MW)	Load factor (%)
1986	1 3,4 6 1	14,756	2,4 3 5	14,169	2,3 3 8	6 9.1 8
1987	1 3,9 0 8	1 5,36 2	2,5 0 5	1 4,7 4 7	2,4 0 5	7 0.0 0
1988	1 4,5 6 4	16,004	2,6 1 0	1 5,3 6 7	2,5 0 6	7 0.0 0
1989	1 5,2 2 6	1 6,7 3 2	2.7 2 9	1 6,0 6 6	2,6 2 0	7 0.0 0
1990	15,974	1 7.5 5 3	2.863	16,851	2,748	7 0.0 0
1991	1 6,8 1 0	1 8,4 7 2	3,0 1 2	1 7.7 3 4	2,892	7 0.0 0
1992	1 7.8 2 9	1 9.5 9 2	3.1 9 5	1 8.8 0 7	3,0 6 7	70.00
1993	1 8,9 3 1	2 0,8 0 3	3,3 9 3	1 9,9 7 2	3.2 5 7	70.00
1994	2 0,1 2 9	2 2,1 2 0	3.6 0 7	21,235	3,4 6 3	70.00
1995	21,392	2 3,5 0 8	3,8 3 4	2 2,5 7 2	3,6 8 1	70.00
1996	2 2,6 9 3	2 4,9 3 7	4,0 6 7	23,939	3,9 0 4	7 0.0 0
1997	2 4,0 4 1	26,419	4,308	2 5,3 6 2	4,1 3 6	7 0.0 0
1998	25,453	27,970	4,5 6 1	26,852	4,379	70.00
1999	26.862	2 9.5 1 9	4,814	28,336	4,6 2 1	7 0.0 0
2000	28,352	31,156	5,0 8 1	2 9,9 1 2	4,8 7 8	7000

Note: Demand at Sending End = Generation level (MW) \times 0.96

Table - 12.5.2 Load Duration (by NAPOCOR'S Data : from Jan. to Dec. 1986)

Per	i od	a Alleng i Sirrey — Allen S. Levy Alleng St. Marting S. Carpel		I	ARTHUR STATE OF THE STATE OF THE STATE OF	n ann, de stare e anne anne anne anne anne anne anne							, , , , , , , , , , , , , , , , , , ,	<u>N</u> I	70. julio 1800. julio 2018. 1800. julio		 	and the second s	IV			Yea	rly
Mont MW	th	Jan	Feb	Mar	*	Duration (%)	Apr	May	Jun	*	Duration (%)	Jul	Aug	Sep	*	Duration (%)	Out	Nov	Dec	*	Duration (%)	*	Duration (%)
240	0										•							4		4	0.18	4	0.0 5
230	0			3	3	0.14	14	1 4	1 0	38	1.7 4						4	11	. 14	3 3	1.4 9	7 4	0.84
220	0	2	3	1 4	2 2	1.02	3 4	5 4	4 3	169	7.7 4	8	13	2 2	4 3	1.95	28	3 4	17	112	5.07	346	3.9
210	0	1 1	16	3 9	88	4.0 7	111	9 7	8 5	462	2 1.1 5	51	5 4	5 7	205	9.28	6 0	6 6	29	267	1 2.0 9	1,0 2 2	1 1.7
200	0	4 0	3 1	7 4	233	1 0.7 9	89	88	7 9	718	3 2,8 8	89	114	103	511	2 3.1 4	101	113	6 7	548	2 4.8 2	2,0 1 0	2 2.9
190	0	56	7.1	7 3	4 3 3	2 0.0 5	60	5 7	7 3	908	4 1.5 8	9 1	8 2	80	764	3 4.6 0	78	5 6	8 2	764	3 4.6 0	2,869	3 2.8
180	0	8 5	84	6 1	663	3 0.6 9	51	5 6	5 9	1,074	4 9.1 8	76	4 9	51	940	4 2.5 7	44	5 2	3 9	8 9 9	4 0.7 2	3,576	4 0.8
170	0	9 0	5 2	6 2	867	4 0.1 4	5:5	56	41	1,226	5 6.1 4	5 7	5 5	5 1	1,103	4 9.9 5	.50	42	5 5	1,0 4 6	4 7.3 7	4,242	4 8.4
160	0	5 9	5 0	5 1	1,0 2 7	4 7.5 5	5 3	7 0	7 4	1,423	6 5.1 6	5 6	6 1	48	1,268	5 7.4 3	60	6 0	6 5	1,231	5 5.7 5	4,949	5 6.5
150	0 .	7 3	73	7 2	1,2 4 5	5 7.6 4	8 5	101	105	1,714	7 8.4 8	83	7 5	74	1,500	6 7.9.3	. 7 5	6 5	7 1	1,442	6 5.3 1	5.901	6 7.4
140	0	5 8	62	93	1,4 5 8	6 7.5 0	105	103	145	2.0 3 7	9 3.2 7	104	90	9 1	1,785	8 0.8 4	100	9 5	9 2	1,7 2 9	7 8.3 1	7,009	8 0.0
130	0	7 0	88	8 9	1,705	7 8.9 4	51	3 4	3 4	2,156	9 8.7 2	81	101	8 9	2.0 5 6	9 3.1 2	87	79	102	1,997	9 0.4 4	7,914	9 0.3
120	0	1 0 5	82	68	1,960	9 0.7 4	7	14	2	2,1 7 9	9 9.7 7	3 1	4 3	4 3	2,173	9 8.4 1	28	3 4	7 1	2,1 3 0	9 6.4 7	8.442	9 6.4
110	0	6 9	47	34	2.1 1 0	9 7.6 9	1	0	0	2,180	9 9.8 2	5	2	11	2,191	9 9.2 3	1 3	9	3 4	2.1 8 6	9 9.0 0	8,667	9 8,7
100	0	26	1 3	1.1	2.1 6 0	1 0,0 0 0	4	0	0	2,184	1 0 0.0 0	12	5	0	2,208	1 0 0.0 0	16	0	6	2,208	1 0 0.0 0	8,760	1 0 0.0
Max. I	мw	2,217	2.2 4 0	2,3 4 2	2,3 4 2		2,3 5 7	2,375	2,3 6 5	2,3 7 5		2,261	2,275	2.265	2,274		2,3 6 3	2,4 1 2	2,361	2,4 1 2		2,4 1 2	
Min. 1	MW	1,032	1,004	1,0 5 8	1,004		1,007	1,214	1,217	1,007		1,001	1,041	1,151	1,001		1,026	1,130	1,071	1,0 2 6		1,001	
Load	(01.)			6 8.1 8 7					7 5.5 9 6					7 5.1 2 0					7 0.5 5 1			7 (0.5 1 5
factor	(%)		· · · · · · · · · · · · · · · · · · ·			7 1.4	141									7 0.	689						7.U I U

Note: * are cumulative total hours.

Table $-12.5\cdot3$ Modified Load Duration (P.U)

I	One to the same of some of the same of the			I	I	7	1
X	Y	X	Y	Х	Y	X	Y
0.0 0 0 0	1.0000	0.0 0 0 0	1.0000	0.0 0 0 0	1.0 0 0 0	0.0 0 0 0	1.0000
0.0014	0.9821	0.0 1 7 4	0.9684	0.0 1 9 5	0.9675	0.0018	0.9950
0.0102	0.9394	0.0 774	0.9 2 6 3	0.0 9 2 8	0.9 2 3 5	0.0149	0.9 5 3 6
0.0 4 0 7	0.8 9 6 7	0.2115	0.8842	0.2 3 1 4	0.8795	0.0 5 0 7	0.9121
0.1 0 7 9	0.8 5 4 0	0.3288	0.8 4 2 1	0.3460	0.8355	0.1 2 0 9	0.8706
0.2005	0.8113	0.4158	0.8000	0.4 2 5 7	0.7916	0.2482	0.8 2 9 2
0.3069	0.7686	0.4918	0.7 5 7 9	0.4995	0.7476	0.3 4 6 0	0.7877
0.4014	0.7 2 5 9	0.5614	0.7158	0.5 7 4 3	0.7036	0.4072	0.7 4 6 3
0.4755	0.6832	0.6 5 1 6	0.6737	0.6 7 9 3	0.6596	0.4737	0.7 0 4 8
0.5 76 4	0.6405	0.7848	0.6 3 1 6	0.8084	0.6157	0.5 5 7 5	0.6633
0.6 7 5 0	0.5978	0.9327	0.5 8 9 5	0.9312	0.5 7 1 7	0.6 5 3 1	0.6219
0.7894	0.5 5 5 1	0.9872	0.5 4 7 4	0.9841	0.5 277	0.7 8 3 1	0.5804
0.9074	0.5 1 2 4	0.997.7	0.5053	0.9923	0.4837	0.9044	0.5 3 9 0
0.9769	0.4 6 9 7	0.9 9 8 2	0.4632	1.0000	0.4402	0.9647	0.4975
1.0000	0.4 2 8 7	1.0000	0.4240	1.0000	0.0000	0.9900	0.4 5 6 1
1.0000	0.0 0 0 0	1.0000	0.0000			1.0000	0.4254
						1.0 0 0 0	0.0000

Table - 12.5 4 Tabulated Data for Load Demand

Period	I	П	Ш	IV	Yearly
Load factor	0.68187	0.75596	0.75120	0.70551	0.7 0
Hours	2,1 6 0	2,184	2,2 0 8	2,2 0 8	8,760
Max. MW Ratio (P.U)	0.9 5 6 5 5	0.97003	0.94285	1.00000	1.00000

Table - 12.5.5 Existing Power Plant (Luzon Grid, as of June 1987)

• 7	Capacity (MW)	(Units × MW)
(Hydro)		
Reservoir Type		,
Caliraya	3 2.0 0	4 × 8
Ambuklao	7 5.0 0	3 × 2 5
Binga	1 0 0.0 0	4 × 2 5
Angat	2 2 8.0 0	$4 \times 50, \ 3 \times 6, \ 1 \times 10$
Pantabangan	1 0 0.0 0	2 × 50
Magat	3 6 0.0 0	4 × 9 0
Kalayaan	3 0 0.0 0	2 × 150
Subtotal	1,1 9 5.0 0	
Run of River Type	,	
Botocan	1 6.9 6	2 × 8, 0.96
Buhi -Barit	1.80	
Cawayan	0.4 0	
Masiway	1 2.0 0	
Subtotal	3 1.1 6	
Total	1,226.16	
(Oil-fired)	(MW)	(Units × MW)
Mani la	200.00	2×100
Sucat	8 5 0.0 0	$1 \times 150, 2 \times 200, 1 \times 300$
Bataan	2 2 5.0 0	1 × 7 5, 1 × 150
Malaya	6 5 0.0 0	$1 \times 300, 1 \times 350$
Total	1,9 2 5.0 0	
(Coal-fired)	(MW)	
Calaca	3 0 0.0 0	1 × 300
(Geothermal)	(MW)	
Tiwi	3 3 0.0 0	6 × 5 5
Mak – Ban	3 3 0.0 0	6 × 5 5
Total	6 6 0.0 0	
Grand Total	4,1 11.16	

Table - 12.5.6 Installed Capacity (MW) by Plant type in Luzon Grid

F.Y	Oil-fired	Gas the rmal	Sub-total	Pumped Storage	Run of River	Reservoir	Sub-total	Coal-fired	Geo-thermal	Total	Expansion Program
1986	1,925		1,925	300	3 1	895	1,2 2 6	3 0 0	660	4,1 1 1	Rehab.Malayal (300)
1987	1,925	 	1,925	300	3 1	895	1,226	300	660	4,111	Rockwell (180)
1988	1,925(180)		1,9 2 5	300	3 1	895	1,2 2 6	300	660	4,1 1 1	
1989	1,925(180)	150	2.0 7 5	300	3 1	895	1,2 2 6	300	660	4,2 6 1	Gas-T. (3×50), Rehab. Sucat 1 (150)
1990	1,925(180)	350	2.2 7 5	300	3 1	895	1,226	300	660	4,4 6 1	Gas-T. (4×50), Rehab. Sucat 4 (300)
1991	1,925 (180)	3 5 0	2.2 7 5	300	3 1	895	1,2 2 6	300	770	4,571	Geo (2×55)
1992	1,925	350	2,275	300	3 1	895	1,2 2 6	600	770	4,871	Calaca∥(300), Retire Rockwell(△180)
1993	1,925	350	2.2 7 5	300	5 4	895	1,2 4 9	600	990	5,114	Pantay H. (23). Geo (4×55)
1994	1,925	350	2,275	300	5 4	895	1,249	600	1,210	5,334	Geo (4×55)
1995	1,925	3 5 0	2,2 7 5	300	5 4	895	1,2 4 9	900	1,210	5.634	Isabela (2×150)
1996	1,925	350	2.275	300	5 4	1285	1,639	900	1,210	6,0 2 4	San Roque H. (390)
1997	1,925	3 5 0	2.2 7 5	300	5 4	1,5 5 3	1,907	900	1,2 1 0	6,292	Casecnan H. (268)
1998	1,925	3 5 0	2.2 7 5	3 0 0	5 4	1,728	2,0 8 2	900	1,320	6.577	Binongan H. (175), Geo (2×55)
1999	1,925	3 5 0	2,2 7 5	300	5 4	1,728	2,082	1,200	1,3 2 0	6,877	Coal A (2×150)
2000	1,925	3 5 0	2.275	300	5 4	1,7 2 8	2.0 8 2	1,500	1,320	7.1 7 7	Coal B (2×150)

Table - 12.5.7 Tabulated Data for MW Capacity (in 1995)

Plant	Installed Capacity (MW)	Max. Limit (MW)	Min. Limit (MW)	Min./Max.	EFOR (%)	SMD (days/year)	SUR (%)	Decrease factor	Output at Sending End (MW)
Gas-turbine	7 × 5 0	7×40	<u></u>		8	0	1	0.911	2 5 5.1
Hydro	2 4 9	1,249			0.5	-	0.3	0.9 9 2	1,2 3 9.0
Oil-fired				· · · · · · · · · · · · · · · · · · ·	-	·			
Bataan 1	7 5	70	5 0		10	4 9	4	0.7 4 8	5 2.4
2	150	150	80		10	4 9	4	0.748	1 1 2.2
Sub-total	225	220	130	0.5 9 1					1 6 4.6
Manila 1	100	100	3 0		10	49	4	0.7 4 8	7 4.8
2	100	100	3 0		10	4 9	4	0.7 4 8	7 4.8
Sucat 1	150	150	4 0		1 0	4 9	4	0.7 4 8	112.2
2	200	160	120		1 4	4 9	4	0.7 1 5	1 1 4.4
3	200	1 4 0	120		1 4	4 9	4	0.7 1 5	1 0 0.1
. 4	3 0 0	300	120		1 6	5 6	4	0.683	2 0 4.9
Malaya 1	3 0 0	300	120	•	16	5 6	4	0.6 8 3	204.9
2	3 5 0	350	150		1 4	5 6	4	0.699	2 4 4.7
Sub-total	1,700	1,600	730	0.4 5 6					1,130.8
Total	1,925	1,8 2 0	860						1,295.4
Coal-fired									
Calaca	2×300	2 × 3 0 0	2×230	0.7 6 7	1.7	5 6	8.5	0.6 4 3	3 8 5.8
I sabe la	2×150	2×150	2×115	0.767	1 2	4 9	8.5	0.6 9 7	2 0 9.1
Geothermal	2 2 × 5 5	22×50	22×30	0.600	4	3 5	1 0.0	0.7 8 1	8 5 9.1

Note: EFOR = Equivalent forced outage rate, SMD = Scheduled maintenance days, SUR = Station use rate.

Decrease factor = $(1-EFOR) \times (1-\frac{SMD}{365}) \times (1-SUR)$, Output at sending End = Max. Limit × Decrease factor.

Table - 12.5 \cdot 8 Output of Reservoir Type Hydro (MW) \sim at Sending End \sim

Plants	Output (MW)
Existing (Ambuklao)	1,1 8 5.4 6 (7 4.4 0)
San Roque	3 8 6.8 9
Casecnan	2 1 1.3 0
Binongan	1 7 3.6 0
Total	1,957.25

Table - 12.5.9 Output of Run of River Type Hydro (MW) \sim at Sending End \sim

Plants	Output (MW)
Existing	5 3.7 3

Table - 12.5.10 Output of Reservoir Type Hydro at Sending End (MW)

Alternatives F.Y	(a)	(b)
1996	1,5 7 2.4	1,4 9 8.0
1997	1,783.7	1,7 0 9.3
1998	1,9 5 7.3	1,882.9
1999	1,9 5 7.3	1,8 8 2.9
2000	1,9 5 7.3	1,8 8 2.9
Remarks	With Ambuklao	Without Ambuklao

Table - 12.5 · 11 Output of Geothermal Power Plant at Sending End (MW)

Alternatives F.Y	(a) (c)	(b)
1996	8 5 9.1	8 9 8.2
1997	8 5 9.1	8 9 8.2
1998	9 3 7.2	9 7 6.3
1999	9 3 7.2	9 7 6.3
2000	9 3 7.2	9 7 6.3
Remarks		+ Geothermal (1×55MW)

Table - 12.5.12 Output at Sending End (MW)

>	, i	Oil-fired	ired	Pumped	Run of River	Reservoir	Coal-fired	1,400	Tota1
	Gas - tu! 01116	(Bataan)	(Others)	Storage	(in May)	(a)	(a)	reo ruerum r	(a)
1996	255.1	164.6	1,130.8	2 9 7.6	2 4.4	1,5 7 2,4	594.9	859.1	4,898.9
1997	255.1	164.6	1,130.8	2 9 7.6	2 4.4	1,783.7	594.9	859.1	5,110.2
1998	255.1	164.6	1,130.8	2 9 7.6	2 4.4	1,9 5 7.3	594.9	9 3 7.2	5.361.9
1999	255.1	164.6	1,130.8	2 9 7.6	2 4.4	1,957.3	804.0	937.2	5,571.0
2000	255.1	164.6	1,130.8	2 9 7.6	2 4.4	1,957.3	1,013.1	937.2	5,780.1

Note: Alternative (a); With Ambuklao

Table - 12.5 · 13 Average monthly Generation (GWh)

	Installed					II.			Ш		arciante mine co 2004 anny 1100 - Ingelige (1945) Tipina Malanan	ľV		
	Capacity (MW)	Jan 31	Feb 28	Mar 31	Apr 30	Мау 31	Jun 30	Jul 31	Aug 31	Sep 30	Oct 31	Nov 30	Dec 31	Total 365
Reservoir Type														
Caliraya	3 2	8.1 9	8.3 1	4.9 2	5.2 2	4.6 3	4.99	4.6 3	5.8 3	6.2 4	6.4 7	9.18	8.1 5	7 6.7 6
Ambukl ao	7 5	1 2.0 9	1 0.6 9	1 1.5 9	1 0.9 5	1 1.5 4	1 0.7 1	5 2.7 7	5 4.3 0	5 3.2 9	5 4.5 0	5 3.8 0	1 8.3 3	3 5 4.5 6
Binga	100	1 8.2 1	21.96	1 7.9 4	1 9.2 7	2 6.3 0	2796	4 3.5 9	6.5.97	7 5 0 2	5 5.6 8	4 9.2 9	2 9.3 3	4 5 0.5 2
Angat	228	3 9.1 4	4 2.9 5	3 2.3 7	2 8.0 6	1 5.9 2	3 1.9 2	3 9.7 5	3 6.0 9	4 4.3 2	4 6.6 2	7 0.9 2	5 8.3 6	4 8 6.4 2
Pantabangan	100	2 5.2 1	2 8.5 4	2 5.4 3	2 2.1 7	6.4 8	2.1 6	6.1 8	7.28	6.0 2	7.9 1	5.5 5	9.95	1 5 2.8 8
Magat	360	5 4.3 0	5 3.1 6	3 8.0 3	2 7.3 9	6492	8 9.2 9	8 6.5 6	1 3 6.9 0	1 3 9.3 1	1 2 8.1 5	1 6 8.5 0	8 3.3 4	1,069.85
Sub-total	1,195(1,185.5)	1 5 7.1 4	1 6 5.6 1	1 3 0.28	1 1 3.0 6	1 2 9.7 9	1 6 7.0 3	2 3 3.4 8	3 0 6.3 7	3 2 4.2 0	299.33	3 5 7.2 4	2 0 7,4 6	2,5 9 0.9 9
		4	53.03(451	.67)	4 (9.88(408.	65)	8 6	4.05 (861.	46)	86	4.0 3 (8 6 1.4	4)	:
San Roque	390	3 8.2 6	2 8.4 3	2 9.3 7	3 2.0 8	5 9.1 5	1 0 3.4 4	1 5 5.5 5	182.77	1 8 2.3 1	1 5 2.3 4	8 3.5 8	5 1.9 1	1,0 9 9.1 9
Caseenan	213	107.64	6 2.4 6	6 3.7 7	6 5.60	9 2.7 7	1 1 5.7 0	1 3 3.1 6	1 4 3.8 9	1 5 2.3 6	162.38	1 6 6.0 5	1 4 8.4 5	1,4 1 4.2 3
Bi nongan	175	4 0.7 9	3 0.3 6	2 4.6 2	2 2 0 6	3 6.6 2	6 4.3 1	8 9.3 9	1 0 5.0 5	9 9.0 3	8 2.6 1	6 6.9 2	5 9.1 9	7 2 0.9 5
Sub-total	778(771.8)	1 8 6.6 9	1 2 1.2 5	1 1 7.7 6	1 1 9.7 4	1 8 8.5 4	2 8 3.4 5	3 7 8.1 0	4 3 1.7 1	4 3 3.7 0	3 9 7.3 3	3 1 6.5 5	2 5 9.5 5	3,2 3 4.3 7
· · · · · · · · · · · · · · · · · · ·		4	25.70(424	.42)	5 9	173(539	96)	1,24	3.5 1 (1,2 3	9.78)	9 7	3.43(970.	51)	
Total	1,973(1,957.2)	8	78.73 (876	.09)	1,00	0 1.6 1 (9 9 8.	61)	2,1 0	7.5 6 (2,1 0	1.24)	1,8 3	7.46 (1,83	1.95)	
Run of River Type										-				
Botocan	1 6.9 6	4.4 5	3.66	5.17	4.78	2.8 2	6.3 9	6.37	4.97	5.60	5.5 7	1 0.6 4	1 0.20	7 0.6 2
Buhi-Barit	1.80	1.14	1.1 2	0.7 0	0.63	0.3 6	0.3 5	0.6 1	0.7 4	0.7 9	0.8 9	1.0 5	1.09	9.4 7
Cawayan	0.40	0.2 3	0.23	0.18	0.19	0.13	0.1.1	0.28	0.27	0.1 3	0.14	0.1 4	0.18	2.21
Masiway	1 2.0 0	4.95	5.30	5.2 2	5.2 4	2.34	0.4 6	1.46	1.5 9	1.5 8	1.70	1.30	2.60	3 3.7 4
Pantay	2 3.0 0	1 2.5 0	1 2.5 0	1 2.50	1 2.5 0	1 2.5 0	1 2.5 0	1 2.5 0	1 2.5 0	1 2.5 0	1 2.5 0	1 2.5 0	1 2.5 0	1 5 0.0 0
Total	54.16(53.7)	2 3.2 7	2 2.8 1	2 3.7 7	2 3.3 4	1 8.1 5	1 9.8 1	2 1 2 2	2 0.0 7	2 0.6 0	2 0.8 0	2 5.6 3	2 6.5 7	2 6 6.0 4
			6 9.8 5 (6 9.6	4)		51.30(61.1	2)	6	5 1.8 9 (6 1.7	0)	7	3.0 0 (7 2.7	8)	

Note: () shows Sending End Values.

Table - 12.5·14 Average Generation of Reservoir Type Hydro (GWh) \sim at Sending End \sim

Period Plants	I	II	Ш	īV
Existing (Ambuklao)	451.67 (34.27)	408.65 (33.10)	861.46 (159.88)	8 6 1.4 4 (1 2 6.2 5)
San Roque	9 5.7 7	1 9 4.0 9	5 1 9.0 7	286.97
Casecnañ	2 3 3.1 7	273.25	428.12	4 7 5.4 5
Binongan	9 5.4 8	1 2 2.6 2	29259	2 0 8.0 9
Total	8 7 6.0 9	9 9 8.6 1	2,101.24	1,8 3 1.9 5

Table - 12.5·15 Average Generation of Run of River Type Hydro (GWh) \sim at Sending End \sim

Period Plants	I	II	Ш	IV
Existing	6 9.6 4	6 1.1 2	6 1.7 0	7 2.7 8

Table - 12.5.16 Average Generation of Reservoir Type Hydro at Sending End (GWh)

Alternatives		(a) with Ar	with Ambuklao			(b) and (c) without Ambuklao	thout Ambukla	0
Period F.Y	}	П	Ħ	N)-wed	П	Ħ	A
1996	547.44	602.74	1,380.53	1,148.41	513.17	569.64	1,2 2 0.6 5	1,022.16
1997	780.61	875.99	1,808.65	1,623.86	7 4 6.3 4	8 4 2.8 9	1,648.77	1,497.61
1998	876.09	998.61	2,101.24	1,831.95	841.82	965.51	1,941.36	1,705.70
1999	8 7 6.0 9	998.61	2,101.24	1,831.95	841.82	965.51	1,941,36	1,705.70
2000	876.09	998.61	2,101.24	1,831.95	841.82	965.51	1,941.36	1,705.70

Table - 12.5.17 Fixed O/M Cost

		Installed	Construction	Installed Construction Construction Life Time Residual Forced	Life Time	Residual Value Rate	Forced	Maintenance	Station	Fixed OAM	Maintenance Station Fixed O'M Annual Fixed Cost
Plants	Type	Type Capacity Cost(c) (MW) (8/KW)	(s/kw)	(year) (year	(n) (year)	(2)	Outage Kate (%)	(2) Outage Kate days/year Use Rate Cost(m) 8/KW- (%) (days) (P.U) 8/KW- month	Use Rati	Use Rate Cost(m) (P.U) 8 KW- month	(8/KW-year)
Ambuklao Hydro	Hydro	75	542.47	∞	30	0.1	0.5	1	0.003	0.45633	5.520
Coalfired(2)		300	1,162.10	4	30	0.1	12.0	ଟ୍ୟ	0.085	1.28475	22,116
Geothermal	1	100	624.60	4	30	0.1	4.0	3.5	0.100	0.47000	7.220

Note: Annual Fixed O/M Cost (\$/KW-year) = (m x 12) + ((1-Forced Outage Rate)(1-Maintenance days)(1-Station Use Rate)) * Max.Limit

Disbursement Ratio (Rk) of Construction Cost

Total Construction Cost (unit: 104)

		~~~	
L.C	381.234	1,563.0	347.8
Plants	Ambuklao	Coalfired(2)	Geothermai
꾭	18.702	3,	ŀ
Ro	19.929	100	100
R.	27.842 19.929	100	100
Rz	21.096	100	100
R3	6.553	100	100
R.	2.412	Į.	I
Rs	1.829	ı	l
Re	1.638	I	1
Plants	Ambuklao	Coalfired (2)	Geothermal

Plants	J.1	F.C US\$	Equivalent US\$
Ambuklao	381.234	22.531	40.585
Coalfired(2)	1,563.0	2742	348.63
Geothermal	347.8	45.9	62.46

Table - 12.5.18 Variable

Plant Type	Fuel Cost	Heat Content	Fuel Cost (& MBTU)	Heat Rate (There (MBTU/MWh)	n al Efficiency) (%)	Heat Rate (Thermal Efficiency) Variable O. MRatio Station use Rate Variable Cost (MBTU/AWh)	Station use Rate (%)	Variable Cost (s/MWh)
Gas - turbine	 		3.00	14.841	23.00		1.0	45.422
Oil -fired		:						
(1) Manila, Sucat, 14.311\$/5bi	14.311\$ Jobi	6.21 MBTU/bb1	2.3045	10,753	31.74	groud	4.0	26.071
(2) Bataan	13.831\$ 6b1	6.248 MBTU/bb1	2.2136	9.484	35.98	7	4.0	22.087
Coal - fired								
(Calaca)	35.63 \$/t	21.630MBTU/t	1.6472	9.484	35.98	7	8.5	17.244
(Isabela)	35.74 \$/t	18.739 MBTU/t	2.0673	9.484	35.98	Ħ	8.5	21.642
Geothermal			*0.2526		:	1:	10.0	13365
			12					

Note: Variable Cost at Sending End (& MWh) = Fuel Cost (& MBTU) × Heat Rate (MBTU/AWh) × (1+Variable Q/M Ratio×10-2) 1 - Station Use rate × 10-2

Variable Cost for Pumping up = Variable Cost + Pumping up Efficiency (0.7)

Plants	Variable cost	Variable cost for Pumping up (\$ AWh)
Dil-fired (Manila, Sucat, Malaya)		37.244
Oil-fired (Bataan)		31,553
Coal (Calaca)		24.634
Coal (Isabela)		30,917
Geothermal		19,093

F . Y	<del>ana ana ana ana ana ana ana ana ana ana</del>	1 (	9 5			1 9	9 6			1 9	9 7	
Period Plants	I	11	IU	IV	I	П	Ш	iV	ı	П	m	ľV
Gasturbine												
Pumped Storage					2 9 7.6	1 0 5.3	6 4.3	1 6 2.7	2 9 7.6	6 9.1	1 2.7	7 8.7
Reservoir					983.7	9 4 5.9	1.4 6 3.3	1,4 1 1.0	1,2 1 3.3	1,226.5	1,7 7 1.0	1,7 0 5.3
Oil-fired (1)				·	8 0 2.2	1,089.2	5 0 6.7	6 7 8.7	7 9 4.5	1,0 6 9.8	4 6 9.3	7 0 0.4
Oil-fired (2)					1 6 4.6	"	"	"	<i>"</i>	"	"	"
Coal-fired (150MW units)	; ;				20 9.1	"	"	"	, ,,	"	"	"
Coal-fired (300MW units)					3 8 5.8	<i>"</i>	"	"	<b>//</b> .	"	. "	"
Geothermal		·			8 5 9.1	"	"	"	"	"	"	"
Run of River				:	3 2.2	2 8.0	2 7.9	3 3.0	3 2.2	2 8.0	2 7.9	3 3.0
Total					3,7 3 4.3	3,7 8 7.0	3,680.8	3,9 0 4.0	3,9 5 6.2	4,0 1 2.0	3,8 9 9.5	4,1 3 6.0

F Y		1 9	9 8			199	9 9			200	0 0	
Period Plants	I	П	Ш	N	I	П	Ш	IV	I		Ш	IN
Gasturbine									·			
Pumped Storage	2 9 7.6	6 8.7	0.8	5 4 0	2 9 7.6	7 8.8	2 8.9	1 1 5.0	2 9 7.6	9 0.6	6 0.2	1.8 3.2
Reservoir	1,337.6	1,3 5 2.3	1,9 5 6.5	1,903.4	1,3 9 3.9	1,382.8	1,9 2 8.5	1,8 4 3.0	1,4 5 3.0	1,4 1 2.8	1,8 9 7.4	1,7 7 5.9
Oil-fired (1)	8 2 4.5	1,1 0 2.1	4 4 6.7	6 9 1.9	7 9 0.6	1,087.1	4 6 5.7	7 2 4.2	7 6 8.3	1,085.5	4 9 8.7	7 7 1.0
Oil-fired (2)	1 6 4.6	"	, ,	"	"	"	"	"	"	"	"	
Coal-fired (150MW units)	2 0 9.1	"	"	<b>U</b> , :	4 1 8.2	"	"#	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	6 2 7.3	"	<i>11</i>	"
Coal-fired (300MW units)	3 8 5.8	<i>ji</i>	"	"	"	"	"	"	"	"	"	<i>"</i>
Geothermal	9 3 7.2	"	"	ji	"	"	"	"	"	"	"	″
Run of River	3 2.2	2 8.0	2 7.9	3 3.0	3 2.2	2 8.0	2 7.9	3 3.0	3 2.2	2 8.0	2,7.9	3 3.0
Total	4,1 8 8.6	4,2 4 7.8	4,1 2 8.6	4,37 9.0	4,4 2 0.1	4,4 8 2.5	4,3 5 6.8	4,6 21.0	4,6 6 6.0	4,7 3 1.8	4,5 9 9.1	4,8 7.8.0

Note: Oil-fired(1) are Oil-fired (Manila, Sucat, Malaya), Oil-fired(2) are Oil-fired(Bataan).

F . Y	<u>na ngana nganggang pala pika mana na manang pala pika Pa</u>	1 9	9 5			1 9	9 6			1 9	9 7	
Period Plants	I	Ш	Ш	īV	· I	1	Ш	īV	I	П	Ш	[V
Gasturbine												•
Pumped Storage			,		297.6	1 2 1.0	9 1.4	2 1 7.4	297.6	7 5.5	3 7.8	1 2 6.8
Reservoir					9 5 6.4	9 0 2.7	1,3 5 2.6	1,28 3.0	1,189.0	1,1 9 6.4	1,6 7 1.6	1,5 8 3.4
Oil-fired (1)					7 9 0.3	1,0 7 7.5	5 5 1.1	7 1 2.9	7 7 9.6	1,054.4	5 0 4.5	7 3 5.1
Oil-fired (2)					1 6 4.6	"	"	"	"	<i>11</i> ·	11	"
Coal-fired (150MW units)					2 0 9.1	"	"	"	"	, ,,,	"	"
Coal-fired (300MW units)					3 8 5.8	"	"	.//	, , , ,	. "	"	"
Geothermal			·		8 9 8.2	"	"	"	"	<i>"</i>	"	"
Run of River					3 2.2	2 8.0	27.9	3 3.0	3 2.2	28.0	2 7.9	3 3.0
Total					3,7 3 4.2	3,7 8 6.9	3,680.7	3,9 0 4.0	3,9 5 6.1	4,0 1 2.0	3,8 9 9.5	4,1 3 6.0

F.Y		1 9	9 8			1 9	9 9			200	0 0	
Period Plants	I	II	П	ľV		Ц	Ш	IV	I	П	n	ĪV
Gasturbine												
Pumped Storage	297.6	7 4.1	2 2.8	1 0 0.5	2 9 7.6	8 5.9	5 3.9	1 6 6.9	297.6	1 0 0.6	8 5.2	2 4 1.0
Reservoir	1,3 1 3.8	1,324.4	1,8 6 0.1	1,7 8 2.9	1,3 6 9.8	1,3 5 2.3	1,8 2 9.2	1,7 1 7.5	1,4 2 8.5	1,3 7 8.8	1,7 9 8.2	1,6 4 5.1
Oil-fired (1)	8 0 9.2	1,0 8 5.5	482.0	7 2 6.8	775.6	1,071.4	5 0 0.9	7 5 8.7	7 5 3.7	1,0 7 0.4	5 3 3.7	804,9
Oil-fired (2)	1 6 4.6	. "	"	"	ll .	"	. "	"	"	"	"	"
Coal-fired (150MW units)	2 0 9.1	"	"	"	4 1 8.2	"	<i>"</i>	"	6 2 7.3	"	"	"
Coal-fired (300MW units)	3 8 5.8	<i>"</i>	//	"	"	"	"	"	<b>"</b>	"	"	<b>"</b>
Geothermal	976.3	"	"	"	"	"	"	."	"	"	"	"
Run of River	3 2.2	2 8.0	2 7.9	3 3.0	3 2.2	2 8.0	2 7.9	3 3.0	3 2.2	2 8.0	2 7.9	3 3.0
Total	4,1 8 8.6	4,247.8	4,1 2 8.6	4,3 7 9.0	4,4 2 0.1	4,4 8 2.5	4,356.8	4,6 2 1.0	4,6 6 6.0	4,7 3 1.8	4,5 9 9.0	4,878.0

Note: Oil-fired (1) are Oil-fired (Manila, Sucat, Malaya), Oil-fired (2) are Oil-fired (Bataan).

F Y		1 9	9 5			1 9	9 6	·		1 9	9 7	
Period Plants	I	П	Ш	ľV	ı	II	Ш	įV	l	II	Ш	[V
Gasturbine	: -						·		·			
Pumped Storage					2 9 7.6	111.1	8 1.7	1 9 7.9	2976	7 0.9	2 8.1	1 0 7.4
Reservoir					954.4	9 1 2.4	1,3 6 7.6	1,302.0	1,188.1	1,2 0 1.0	1,681.3	1,6 0 2.5
Oil-fired (1)	.*				8 3 1.5	1,1 1 6.9	5 8 5.0	7 5 2.5	8 1 9.7	1,093.5	5 4 3.6	7 7 4.5
Oil-fired (2)		-			1 6 4.6	"	, "	"	"	<i>"</i>	"	<b>"</b>
Coal-fired (150MW units)					2 0 9.1	"	, "	".	. "	#	"	"
Coal-fired (300MW units)					3 8 5.8	"	"	"	"	<i>"</i>	"	<b>"</b>
Geothermal					8 5 9.1	"	"	' //	"	"	"	"
Run of River					3 2.2	2 8.0	2 7.9	3 3.0	3 2.2	2 8.0	2 7.9	3 3.0
Total					3,7 3 4.3	3,7 8 7.0	3,680.8	3,9 0 4.0	3,9 5 6.2	4,0 1 2.0	3,8 9 9.5	4,1 3 6.0

F . Y		199	9 8			1 9 9	9 9			200	0	
Period Plants	I	П		N	I	П	П	IV	I	П	Ш	N .
Gasturbine												
Pumped Storage	2 9 7.6	7 0.5	1 3.1	8 2.6	2 9 7.6	8 0.8	4 4.3	1 4 5.8	2 9 7.6	9 3.8	7 5.6	2 1 8.8
Reservoir	1,313.1	1,3 2 7.9	1,8 6 9.8	1,8 0 0.6	1,3 6 8.9	1,3 5 7.3	1,8 3 8.8	1,7 3 8.2	1,4 2 7.3	1,3 8 5.5	1,8 0 7.8	1,6 6 6.6
Oil-fired (1)	8 4 9.0	1,1 2 4.7	5 2 1.1	7 6 6.1	8 1 5.6	1,110.6	5 4 0.0	7 9 8.2	7 9 4.0	1,1 0 9.6	5 7 2.9	8 4 4.7
Oil-fired (2)	1 6 4.6	"	"	"	. "	"	"	"	"	"	"	. "
Coal-fired (150MW units)	2 0 9.1	"	#	"	4 1 8.2	"	<i>#</i>	"	6 2 7.3	"	"	. "
Coal-fired (300MW units)	3 8 5. 8	<b>#</b>	#	"	"	"	<b>"</b>	<b>//</b>	"	"	<b>"</b>	"
Geothermal	9 3 7,2	"	"	,,	, , , , , , , , , , , , , , , , , , ,	"	"	<b>//</b>	"	"	"	"
Run of River	3 2.2	2 8.0	27.9	3 3.0	3 2.2	2 8.0	2 7.9	3 3.0	3 2.2	2 8.0	2 7.9	3 3.0
Total	4,1 8 8.6	4,2 4 7.8	4,1 2 8.6	4,3 7 9.0	4,4 2 0.1	4,4825	4,3 5 6.8	4,6 2 1.0	4,66 6.0	4,7 3 1.8	4,599.1	4,8 7 8.0

Note: Oil-fired(1) are Oil-fired (Manila, Sucat, Malaya), Oil-fired(2) are Oil-fired (Bataan).

F.Y	3	A art and the second	1 9 9 5					1996					1997		
Plants	I	II .	Ш	IV	Total	I	П	Ш	ĮV	Total	I	I	Ш	N	Total
Gas turb ine				-											
Pumped Storage						15.4	1.8	0.7	2.4	20.3	4.6	0.7	0.0	0.6	6.0
Reservoir						547.4	602.7	1,380.5	1,148.4	3,679.0	780.6	876.0	1,8 0 8.6	1,623.9	5,089.1
Oil-fired (1)			•			1,426.1	2,059.3	1,092.0	1,295.0	5,872.4	1,498.8	2,153.5	1,024.8	1,176.2	5,853.3
Oil-fired (2)						334.2	3 5 5.7	361.8	3 5 8.4	1,410.1	344.9	35 8.5	362.7	360.8	1,426.9
Coal-fired (150MW units)						440.7	455.5	460.8	459.1	1,8 1 6.1	446.4	456.3	461.4	460.7	1,824.8
Coal-fired (300 MW units)						(13.4) 819.9	$\begin{pmatrix} 1.4 \\ 841.2 \end{pmatrix}$	(0.9) 850.9	(2.6) 849.2	(18.3) 3,361.2	(4.8) 828.5	(0.4) $842.2$		(0.7) 851.1	
Geothermal						(8.6) 1,847.1	(1.2) 1,875.1			(10.7) 7.515.1	( 2.0) 1,8 5 3.7	(0.6) 1,875.7	1,8 9 6.9	(0.0) 1,896.9	(2.6) 7,5 2 3.2
Run of River						69.6	61.1	61.7	7.2.8	265.2	6 9.6	61.1	61.7	72.8	265.2
Total						(22.0) 5,500.4	(2.6) 6,252.4	(1.0) 6,105.2	(3.4) 6,081.4	(29.0) 23,939.5	(6.8) 5,827.2	(1.0) 6,624.0	(0.0) 6,467.9	(0.7) 6,443.0	(8.5) 25,362.1

F.Y			1998			·		1999					2000		
Plants	I		Ш	N	Total	1 .	I	Ш	IV	Total	I	I	П	ľV	Total
Gasturbine									_						
Pumped Storage	3.9	0.7	0.0	0.3	4.9	6.2	0.8	0.1	1.0	8.1	9.0	1.0	0.5	2.5	1 3.0
Reservoir	876.1	998.6	2,101.2	1,8 3 2.0	5,807.9	876.1	998.6	2.101.2	1,831.9	5,807.8	876.1	998.6	2,101.2	1,832.0	5,807.9
Oil-fired (1)	1,574.3	2,249.3	939.4	1,1 72.9	5,935.9	1,478.1	2,181.6	857.8	1,093.4	5,610.9	1,408.9	2,1 3 9.2	800.4	1,040.9	5,389.4
Oil-fired (2)	346.3	358.7	362.9	361.6	1,429.5	341.6	358.1	362.3	359.4	1,421.4	3 3 5.6	3 5 6.9	361.6	356.4	1,410.5
Coal-fired (150 MW units)	447.3	456.4	461.6	461.0	1,8 26,3	8 9 0.1	912.3	922.4	919.9	3,6 4 4.7	1,328.8	1,367.5	1,382.5	1,376.4	5,4 5 5.2
Coal-fired (300MW units)	(4.0) 829.3	(0.4) 842.2	(0.0) 851.8	(0.3) 851.5	(4.7) 3,374.8	(5.7) 827.6	$\begin{pmatrix} 0.4 \\ 842.2 \end{pmatrix}$	(0.1) 851.7	(1.3) 850.5	i	(7.8) 825.5	(0.5) 84 2.1		(2.4) $849.4$	
Geothermal	(1.6) 2,022.8		2,069.3	2,069.3	(2.1) 8,207.7	(3.2) 2,021.2	(0.7) 2,046.1	2.069.3	2,069.2	(4.0) 8,205.8	(5.1) 2,019.3	(0.9) 2,045.9	( 0.0 ) 2,0 6 9.3	2,068.2	(7.1) 8,202.7
Run of River	69.6	61.1	61.7	7 2.8	26 5.2	69.6	61.1	61.7	72.8	265.2	6 9.6	61.1	61.7	72.8	265.2
Total	(5.6) 6,169.6	(0.9) 7,013.3	(0.0) 6,847.9	(0.3) 6,821.4	(6.8) 26,852.2	(8.9) 6,510.5	(1.1) 7.400.8	(0.1) 7,226.5	7,198.1	(11.5) 28,335.9	(12.9) 6,872.8	(1.4) 7,812.3	(0.6) 7,628.4	(3.5) 7,598.6	(18.4) 29,912.1

Note: () shows Pumping up Energy.

Table - 12.5 · 20(2) Generation Mix at Sending End by Plant Type (Alternative (b))

F.Y		<u> </u>	1995		<del>no na kaona na mpokin dia 100 di</del> dapara			1996	OHECO COMPANY (\$4.50 COMPANY C				1997		
Plants	1	Π	III	N	Total	I	11	Ш	IV	Total	I	II	Ш	IV	Total
	<u> </u>		<u> </u>												
Gasturbine						2 0.7	2.3	1.5	4.5	29.0	7.0	0.9	0.2	1.4	9.5
Pumped Storage						513.2	569.6	1,220.6	1,022.2	3,325.6	746.3	842.9	1,648.8	1,4 9 7.6	4,7 3 5.6
Reservoir						1,384.7	2,009.6	1,166.6	1,339.2	5,900.1	1,4 5 3.1	2,101.8	1,099.1	1,218.5	5,872.5
Oil-fired (1)						330.4	354.0	361.4	355.9	1,401.7	342.8	358.2	3 6 2.3	3 5 9.6	1,422.9
Oil-fired (2)		,				438.0	454.8	460.5	458.2	1,811.5	4 4 5.0	4 5 6.1	461.2	459.9	1,8 2 2.2
Coal-fired (150MW units)	·					(16.6) 816.7	(1.8) 840.8		1	(24.1) 3,355.4	(6.8) 826.5	(0.5) 842.1	(0.3) 851.5	(1.7) 850.1	(9.3 3,3 7 0.2
Coal-fired (300 MW units)						(12.9) 1,927.2			(2.2) 1,981.1	(17.3) 7,851.0	1		1,983.2	(0.3) 1,982.9	7,863.9
Geothermal								61.7	72.8	265.2	69.6	61.1	61.7	72.8	26 5.2
Run of River			<u> </u>			6 9.6	61.1		·				(0.3) 6,468.0	(2.0) 6.442.8	(13.6 25,362.
Total		1				(29.5) 5,500.5	(3.4) 6,252.3	(2.0) 6,105.3	6,8 0 1.4	(41.4) 23,939.5	(10.0) 5,827.2	6,624.0	6,468.0	6.442.8	20,362.0

F . Y			1998					1999					2000		
Plants	ı	n I	П	N	Total	I .	11	Ш	IV	Total	I	П	Ш	ĮV .	Total
: :	1	<u> </u>	<u></u>												
Gasturbine	5.8	0.8	0.1	0.8	7.5	8.7	1.0	0.4	2.2	1 2.3	1 2.1	1.3	1.0	4.3	1 8.7
Pumped Storage Reservoir	841.8	9655	1,941.4	1,705.7	5,454.4	841.8	965.5	1,9 4 1. 4	1,705.7	5,454.4	841.8	965.5	1,941.4	1,705.7	5,454.4
Oil-fired (1)	1,5 28.1	2,1 9 7.4	1,013.5	1,214.7	5.9 5 3.7	1,434.2	2,130.0	932.3	1,136.6	5,6 3 3.1	1,367.6	2,0 8 8.8	875.2	1,087.0	5,418.6
Oil-fired (2)	344.4	358.5	362.6	360.5	1,426.0	3 3 8.9	357.8	361.9	358.2	1,416.8	332.7	3 5 5.7	361.3	354.0	1,403.7
Coal-fired (150 MW units)	446.0	456.3	461.3	460.4	1,824.0	887.5	911.9	921.9	918.4	3,639.7	1,3 2 4.1	1,366.9	1,381.8	1,373.4 (3.7)	5,446.2 (15.5)
Coal-fired (300MW units)	(5.5) 827.8	(0.4) 842.2	(0.1) 851.7	(1.1) 850.7	3,372.4	(7.8) 825.5	(0.5) 842.1		(2.2) 849.6	(11.0) 3,368.5	(10.1) 823.2	(0.7) 841.9		848.1	3,364.0 (11.1)
Geotherma l	2,106.1	(0.6)	2,155.7	(0.1) 2,155.6	(3.4) 8,549.0	2,104.2	(0.9) 2,131.3	(0.1) 2,155.6	2,154.8	(6.5) 8.545.9	2,101.6	2,131.1	(0.4) 2,155.3	(2.4) 2,153.3	8,5 4 1.3
Run of River	69.6	61.1	6 1.7	7 2.8	265.2	69.6	61.1	61.7	7 2.8	265.2	6 9.6	61.1	61.7	72.8	265.2
Total	(8.2) 6,169.6	(1.0) 7,013.4	(0.1) 6,848.0	(1.2) 6,821.2	(10.5 26,852.2	(12.4) 6,510A	(1.4) 7,400.7	(0.6) $7,226.5$	7.1 9 8.3	(17.5) 28,335.9	(17.3) 6,872.7	(1.8) 7,812.3	7,6 2 8.5	(6.1) 7,598.6	(26.6) 29,912.1

Note: () shows Pumping up Energy.

Table - 12.5.20(3) Generation Mix at Sending End by Plant Type (Alternative (e))

F . Y		and the state of t	1995					1 9 9 6					1997		
Plants	I	П	Ш	V	Total	I	II .	III	N.	Total	I	П	Ш	N	Total
Gasturbine															
Pumped Storage						1 7.3	2.0	1.2	3.6	2 4.1	5.5	0.7	0.1	1.0	7.3
Reservoir						513.2	56 9.6	1,220.6	1,022.1	3,3 2 5.5	746.3	842.9	1,648.8	1,497.6	4,735.6
Oil-fired (1)						1,463.8	2,093.3	1,25 2.6	1,4 2 3.7	6,233.4	1,534.6	2,186.8	1,185.1	1,303.8	6,210.3
Oil-fired (2)						332.7	355.1	361.5	357.1	1,406.4	344.2	358.4	3 6 2.5	360.1	1,4 2 5.2
Coal-fired (150MW units)						439.6	455.3	460.6	458.5	1,814.0	445.9	456.3	461.3	460.2	1,823.7
Coal-fired (300 MW units)						(14.6) 818.7	(1.5) 841.1	(1.2) 850.6	(3.6) 848.2	(20.9) 3,358.6	(5.4) 827.9			(1.3) 850.5	(7.2) 3,372.3
						(1 0.2) 1,84 5.5	(1.3) 1,875.0	(0.4) 1,896.5	(1.5) 1,895.4	(13.4) 7,512.4	(2.4) 1,853.3	(0.7) 1,875.6	1,896.9	(0.1) 1,896.8	(3.2) 7,5 2 2.6
Geothermal						6 9.6 .		6 1.7	72.8	265.2	6 9.6	61.1	61.7	7 2.8	26 5.2
Run of River Total	<u> </u>			<u> </u>	<u> </u>	(24.8) 5,500.4	i		(5.1) 6,0 81.4	(34.3) 23,939.6	(7.8) 5,827.3	(1.1) 6,624.0	(0.1) 6,468.1	(1.4) 6,442.8	(10.4) 25,362.2

F. Y		<u> </u>	1 9 9 8					1999		İ			2000		
Plants	1	1	Ш	IV	Total	1	II	II	N	Total	I	II .	III	ĮV	Total
Gasturbine													·		
Pumped Storage	4.5	0.7	0.0	0.6	5.8	7.0	0.9	0.3	1.7	9.9	1 0.1	1.1	8.0	3.5	1 5.5
Reservoir	841.8	965.5	1,941.4	1,705.7	5,454.4	841.8	965.5	1,94 1.4	1,705.7	5,454.4	841.8	96 5.5	1,941.4	1,705.7	5,454.4
Oil-fired (1)	1,609.9	2,282.5	1,099.6	1,300.3	6,2 9 2.3	1.514.5	2,2 1 5.0	1,018.3	1,221.6	5,969.4	1,446.2	2.172.9	961.0	1,170.8	5,750.9
Oil-fired (2)	345.6	358.7	362.7	360.9	1,427.9	340.8	3 58.0	362.0	358.8	1,4 19.6	334.6	356.6	361.4	3 5,4.9	1,407.5
Coal-fired (150 MW units)	4.4.6.8	456.4	461.4	460.7	1,825.3	889.2	912.2	9 2 2.1	919.0	3,6 4 2.5	1,327.1	1,367.3	1,382.1 (0.9)	1,374.7	5.451.2 (13.3)
Coal-fired (300MW units)	(4.5) 828.8	(0.4) $842.2$	(0.0) 851.8	(0.8) 851.0	(5.7) 3,373.8		(0.5) 842.1	(0.4) 851.4	(1.8) 850.0	(9.1) 3,370.4	(8.6) 824.7	(0.6) 84 2.0	1	(3.2) 848.6 (1.8)	(13.3) 3,366.2 (88)
Geotherma l	(2.0) 2,022.4	(0.5) 2,046.3	(0.0) 2,069.3	(0.0) 2,069.3	(2.5) 8,20 <b>7</b> .3	(3.7) $2.020.7$	(0.8) 2,046.0	2,069.3	(0.5) 2,068.8	(5.0) 8,204.8	(5.8) 2,018.6	(1.0) 2,045.8	2,0 6 9.1	2,067.5	(8.8) 8,201.0
Run of River	69.6	61.1	6 1.7	72.8	265.2	6 9.6	6 1.1	61.7	72.8	26 5.2	69.6	61.1	61.7	72.8	265.2
Total	(6.5) 6,169.4	(0.9) 7,013.4	(0.0) 6,847.9	(0.8) 6,821.3	(8.2 26,852.0	(10.1)	(1.3) 7.4008	7,226.5	(2.3) 7,198.4	(14.1) 28,336.2	(1 4.4) 6,8 7 2.7	7.812.3	7,628.4	(5.0) 7,598.5	(22.1) 29,911.9

Note: () shows Pumping up Energy.

Table - 125 · 21 Total O & M Cost

Units: 1,000 USS

Alternaitives	Original Plan + Rehab. Ambuklao (a)	Original Plan + Geothermal (b)	No Change O.P.
1996	3 9 8,8 0 9.1	4 0 3,5 8 7.7	4 0 7,6 3 6.6
1997	4 0 0,2 2 0.9	4 0 4,9 7 8.2	4 0 9,0 3 8.2
1998	4 1 3,1 4 3.8	4 1 7,8 9 7.7	4 2 1,9 5 4.9
1999	4 4 3,8 0 4.2	4 4 8,5 7 0.1	4 5 2,6 2 9.2
2000	476,911.1	4 8 1,7 0 6.0	4 8 5,7 3 9.6

Table - 12.5.22 I.R.R. and Present Value Case: (a) - (b)

		APEU	KULAL .						
CASE - A		20							
		7441	faty	COLAL BAYE	OC DETURY	· · · · · · · · · · · · · · · · · · ·			
		TAELE	181	ERNAL RATE	OFRETUR'				
	<b>.</b>	C631			BENEFIT		PRESE	NTVALUE	1 R F
YEAR INV	ESIMENT	5 <u>.</u> 5	LIALAL	INVESTMENT	0_&_m	LATAL	cost_	BENEFIT	DISCATAC
1987.	26646	<b>(.</b> .	20045.	2664ō.	0	26648.	26648.	26648	1.000
	167526. 239513.	0.	167526.	167520.	0.	167526.	117769.	117769.	0.703 0.494
	306150.	0. 6.	239513. 306153.	. 238847. 30540o.	3.	305406.	118365	118036. 106101.	0.347
1991	421065		421655.	420704.		420704.	102986.	102747.	0.244
	352904. 313786.		352904. 313756.	358046. 313011.	0.	358046. 313011.	60589. 37872.	61472.	0.171 0.120
1994	300282.	<b>.</b>	306262.	296762.	9.	296762.	25478.	25179	0.084
1995. 1996	296456. 316365.	0. 398804.	296458. 715174.	. 296157• 30 <del>8</del> 756•	: 0. 403588.	296157. 712344.	17683. 29988.	17665. 29869.	0.059 0.041
1997	238704	400221.	638925	238704	404978	643682	18833	18974	0.029
	173105∙ .86553.	413144.	556244.	173105	417898. 448570	591003.	12146.	12247.	0.020
2000		443804 476411.	. 530357 476911.	36553	461706.	481796 ·	7726. 4884.	7795 4933	0.010
2001		476911.	476911	0 •	481706	481706	3433.	3468.	0.007
2002 2003	3• 	476911. 476911.	476911. 476911.	() . () .	481706. 481706.	481706. 481706.	2414. 1697.	2438. 1714.	0.005 0.003
2004	0.	476911.	476913.	٤.	481706.	451706.	1193.	1205.	0.002
2005 2006	<u></u>	476911: 476911:	476911 475911 .	0 •	481706*	481706. 481706.	838 589.	847. 595.	0.001
2007	23963.	476911.	500894	23983	481706.	505689.	435.	439	0.000
2006	55864.	476911. 476911.	532715+ 506732	55804. 31821.	481706.	537510.	325. 218.	328. 221.	0.000
2009 2016	31521. 0•	470911.	505732. 476911.	215×1.	481706.	513527. 481706.	144.	145.	0.000
2011		476911	476911		481706.	481706	101	102	0.000
2012		476911. 476911.	476911. 476911	0	481706. 481706.	481706. 481706.	71. 50	72. 51.	00000
2014	0.	476911.	476911.	0.	481706.	481706.	35.	36.	0.000
2015 2016	0.	476911.	476911 476911.		481706. 481706.	481706. 481706.	25. 17.	25. 18.	0.000
2017	0.	47.6911	475911		48) 706.	4817.00	12	12.	0.000
2018	83076.	476911.	559957.	8307ē	481706.	564784	10.	10.	0.000
	12317, 41665.	476911.	589225. 617976.	111717.	481706. 481706.	593423. 622101.	7. 5.	6.	0.000
20212	00061.	476911.	676972	199176.	481706*	680884.	4	<u>\$</u>	0.000
	38156. 14844	476911. 476911.	515069. 591755	142786. 114146.	481706. 481706.	624492. 595852.	3.	3.	0.000
2024 1	02696.	476911.	579601.	99522•	481706.	581228.	1.	1.	0.000
	99243 76696.	476911. 476911.	576160. 653605.	98976. 169648•	481706. 481706.	580684 651554.	1.	1	0.000
2027	93631.	476911.	670742.	193831.	481706.	675537。	1		0.000
2028 2 2029 1	11599. 09719.	476911. .476911.	688510. 586630.	211599. 109719.	481706 - 481706 -	693305+ 591425+	.0.	0.	0.000
2030	0+	476911.	476911	0.	481706.	481706.	0.	0.	0.000
2031		_426911	976911		481706.	481706	0.	0.	0.000
2032 2033	0 • 	476911. 476911.	476911•. 476911•	0.	481706. 481706.	481706. 481706.	0.	0.	0.000
2034	0.	476911.	476911.	0.	481706.	481706.	0.	0.	0.000
2035 2036	<u>Q.</u>	476911. 476911.	476911. 476911.	0.	481706.	481706. 481706.	0.		0.000
		•							
TOTAL 50	34592.	19301689.	24336261.	5016629.	19498155.	24514783.	698963.	698963.	
		: · · · · · · · · · · · · · · · · · ·			<del></del>	<del> </del>			
A	MBUKULAL						ر. دونسور میشون به میشون		
CASE - A-E								11.4	
	l aRaßa .:	42.24 5 8	X &				<del></del>		··
<u>.: </u>			<del></del>			<u> </u>	<u> </u>	<u> </u>	
			TABL	Ł PR	ESENT VALUE			<u> </u>	
DISC. RATE(%)	(5)	(10)	(12)	(20)	(25)	(30)	(35)	(40)	
COST	2742465	1045714	1740770	1250650	1664541	000413	740004	A75188.	
INVESI.	2761465. 5429341.	1965716+ 2084547•	1768739. 1510046.	1250489. 514439.	293540+	889611. 176970.	769804.	72199»	
TOTAL	8190826.		3278787	1764928	1338107	1066580	881001	747387.	<u></u>
RENEFIT	4.5			<u> </u>	<u> </u>	<u> </u>		<u>to ja o</u> ta saj	<u> </u>
INVEST.	2753977.	1961301.	1765013.	1248394.	1043022.	888443.	768890	674451.	
O' & M TOTAL	5485394. 8239371.	4067722.	1525994. 3291607.	519993. 1768387.	296751. 1339773.	178921.	112434. 881324.	73008.	
							<u> </u>		
		1.0043	1.0037	1.0026	1.0012	1.0007	1.0004	1.0001	
B/C	1.0059	110042	1.003	140050		2			
	48545.	17459.	12220.	3460.	1666.	783.	323.	72.	<del></del>

	• • • •	AME. 121	ILAD						
		Anduki	/LP =			· 			
CASE -	A-C	EJEAT	†MTE	RNAL RATE OF	RETURN				
-		COST			BENEFIT		PRESEN	TVALUE	1=R=R=
		3 3. K		INVESTMENT	0 8 6	TOATAL	COST	RENEFIT	DISCATAC
YEAR_	INVESTMENT				J•	26648	26648	26648*	1.0000
1987 1988	167526•	C • C • '	167525.	26643. 167520.	Û.	167526.	142338.	142338.	0.8497 0.7220
1989 .	239513+	0	239513	238847. 30540t.	. 0. 0.	238847• 305406•	187780 •	172423. 187323.	0.6135
1990	306156 • 421685 •	. O.	306150. 421635.	420704	 	420704	219756	219245	0.5213
1992	352904	0.	352964.	350236.	C.	350238. 305203	156260. 118049.	155080. 114820.	0.3764
1993 1994	313786+ 300282+	. U+ G•	313756 300282 ·	268954•	. 0.	288954.	95984.	92363,	0.3198
1995.	296450	6.	296455.	288350.	0	2883501 7163934	80514. 165027.	.78312* 165309*	0.2717 0.2309
1996 1997	316365 • 238764 •	398809. 400221.	715174. 638925.	309756 238764	407637• 409039•	647743	125266.	126995.	0.1962
1998	173105	413144.	586249.	173105.	421955	595060+	97657 <b>.</b> 75063	99125.	0.1667 0.1416
1999 .	85553	476911.	.530357 476911.		452629 a 485740 a	.539182• 485740•	57350.	58412.	0.1204
2000	G •	476911.	476911		485740	485740	48727.	49629.	0.0869
2002	٥.	476911.	476911.	δ. 0	485740. 485740.	485740 485740	41401. 35176.	35827	0.0738
2003	0.	476911. 476911.	476911	6	485740•	485740•	29887.	30441.	0.0627 0.0533
2005	0	476911	47.6911.	0	485740 485740.	485740* 485740*	25394 21576.	25864 21975.	0.0453
2006. 2007	0. 23983	.476911. 476911	476911. 503894	0. 23983.	485740	509722	19254	19593	0.0385
2008	55804	476911.	532715.	55864+	485740	541544. 517561.	17398. 14117.	17686. 14362.	0.0327 0.0278
2009	31B21.	476911. 476911.	506732. 476911.	31821	485740 • 485740 •	485740 •	11244.	11452.	0.0236
2010 2011.	0. 	476911	476911	G	485740	485740	9553	9730 8267 •	0.0170
2012	0 •	476911.	476911.	0 • Q •	485740 • 485740 •	485740 •	8117. 6897		0.0145
2013_ 2014		476911.	476911 476911.		485740 •	485740.	5860.	5968.	0.0123 0.0105
2015.	G .	476911.	476911		485740. 485740.	485740 • 485740 •	4979. 4230.	5071. 4308.	0.0089
2016	0 • 	476911. 476911.	476911. 476911.	0.	485740	485740.	3594	3661.	0.0076
2018	83078	476911.	559989.	83078.	485740	568817• 597457•	3586. 3206	3642. 3250	0.0064 0.0055_
2019	112317	476911. 476911.	589223. 617976.	111717. 140395.	485740 • 485740 •	626134	2857.	2894.	0.0046
2020 2021	1410ò5• 2000ò1•	476911.	676972	199176.	485740.	684917.	2659	2690. 2074.	0.0039 0.0033
2022	138158.	476911.	615069.	135759 107119	485740. 485740.	621498• 592859•	2052. 1678	1681	0.0028
2023_ 2024	102696	476911. 476911.	591755 579601•	92495	485740.	578235+	1396.	1393.	0.0024
2025	99248.	476911	576165	91951	485740	577691. 655588.	1179. 1137.	1182. 1140.	0.0021 - 0.0017
2026 2027	176696.	476911. 476911.	653606+ 676742+	169845 193831	485740 • .485740 •	679571	991.	1004.	0.0015
2028	211599.	476911.	688510.	211599.	485740 •	697338+	864. 626.	875. 635.	0.0013
2029	199719	476911. 476911.	58663U	109719	485790 • 485740 •	595458 485740•	432.	440.	0.0009
2030 2031	0	475911	:476911.	O	485740.	485740.	367. 312.	374	0.000B
2032	0.	476911 476911	476911. 476911.	0.	485740. 485740.	485740• 485740•	265.	270	0.0006
<u>2033</u> 2034	G	476911.	476911.	0.	485740.	485740.	225.	229.	0.0005
2035	0	476911	476911-	0	485740 • 485740 •	485740+	191 163.	166.	0.0003
2036	0+	476911.	476911.					2052184.	
TOTAL	5034592.	19301659.	24336251+	4957290.	19663624.	24620914.	2052185.	20321041	
	AMBUKULAS								
CASS		. *			·				
CASE •	2.1								
	*** 1.R.S	. = 17.69 \$ 3	***						<u> </u>
<del></del>		· · · · · · · · · · · · · · · · · · ·	TAB	LE PRI	SENT VALUE				
DISC.	RATE(%) (	5) (10)	(12)	(20)	(25)	(30)	(35)	(40)	
COST IN	VEST. 276148	1965716	1762739.	1250469.	1044561	A89611.	769804	675188.	
	& H 542934	2084547.	1510048.	514439.	293546.	176970.	111198. 881001	72199• 747387•	
	IIAL 819082	4050263	3278787.	1764928.	1338107	1066580+			
BENEFI		7 1067835	1749489.	1238610.	1035461.	882519•	764195.	670693.	
	VEST. 272645		1749489+ 1539456+	524634.	299467	180525	113683	73694	
	TAL 825912		3288957.		1334927.	1063094.	877678.	744386.	
B/C	1.00	1.0045	1.0031	0.9991	0.9976	0.9967	0.9962	0.9960	
	6829		10169.	·	-3179.	-3487•	-3324•	-3000.	
B-C							<u>.</u>		
. : :	·								
				12 -	126				
					A 1 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO 10 TO	· ·=			

Table  $-12.5 \cdot 24$  MW Balance in Period I of 1996

	Capacity (MW)	at Sending End
Plants	(c ₁ )	(c ₂ )
Gas-turbine	( 255.1)	( 255.1)
Pumped Storage	111.1	75.0 (1,245.0)
Reservoir	912.4	1,143.7
Oil-fired (1)	1,116.1 (1,130.8)	1,130.8
Oil-fired (2)	164.6	164.6
Coal-fired (150MW units)	209.1	0
Coal-fired (300MW units)	385.8	385.8
Geothermal	859.1	8 5 9.1
Run of River	2 8.0	28.0
Total	3,787.0 (4,248.8)	3,787,0 (4,068.4)
Reserve Margin after considering Forced Outage, Maintenance and Station use.	4 6 1.3 MW 1 2.2 %	2 8 1.4 MW 7.4 %

Note: ( ) shows Potential Capacity at Sending End

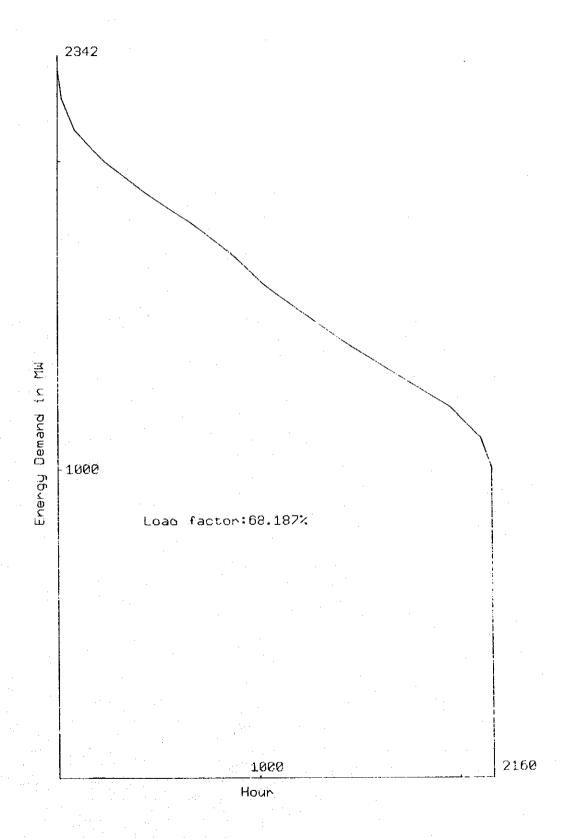


Fig - 12.5.1 Duration Curve I (from Jan. to Mar. 1986)

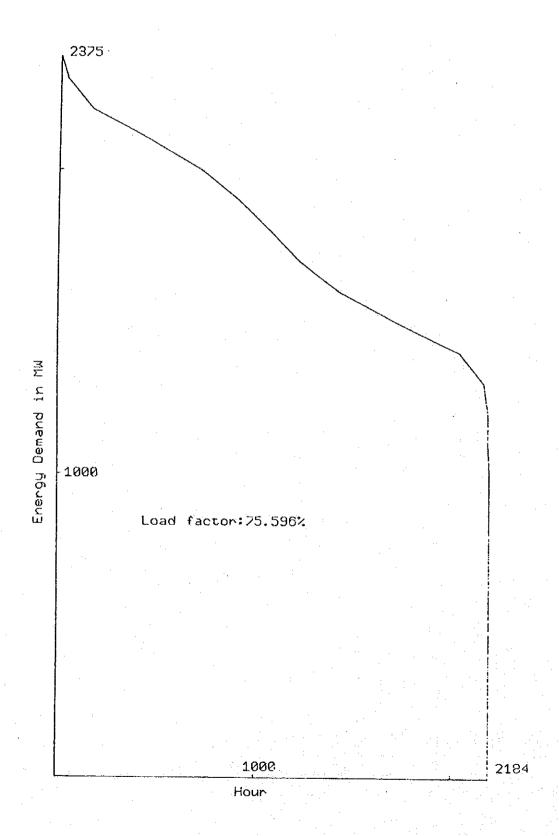


Fig - 12.5.2 Duration Curve [ (from Apr. to Jun. 1986)

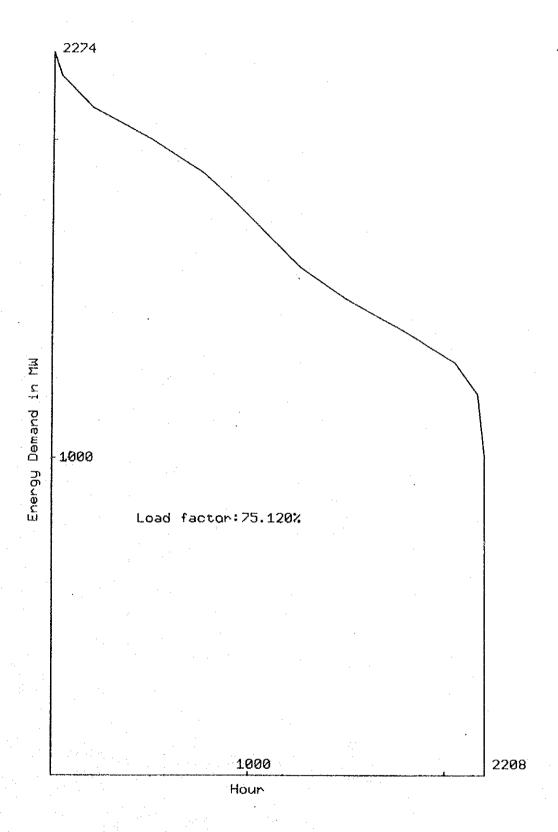


Fig - 12.5.3 Duration Curve I (from Jul. to Sep. 1986)

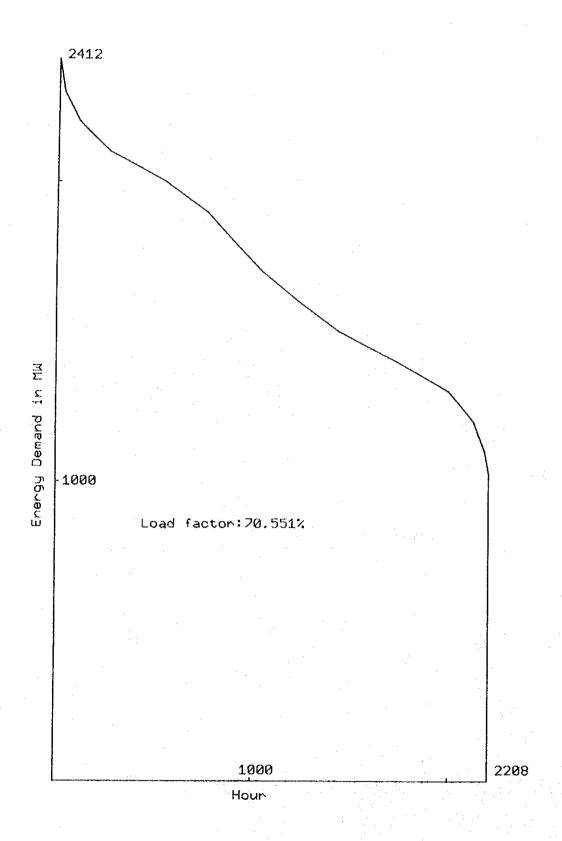


Fig - 12.5.4 Duration Curve W (from Oct. to Dec. 1986)

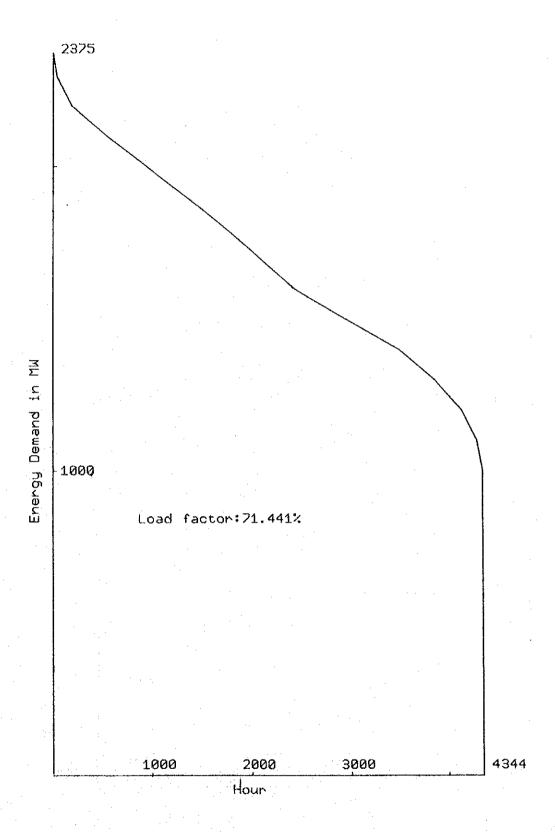


Fig  $-12.5 \cdot 5$  Duration Curve (from Jan. to Jun. 1986)

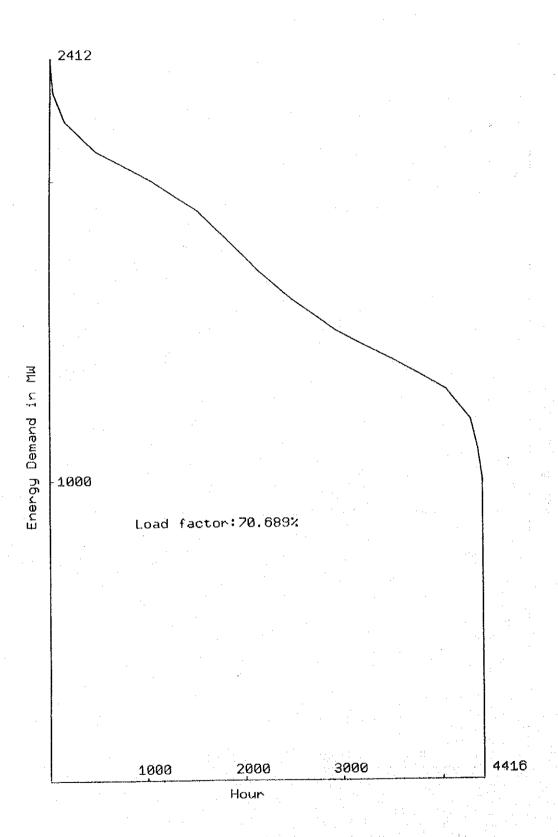


Fig - 12.5.6 Duration Curve (from Jul. to Dec. 1986)

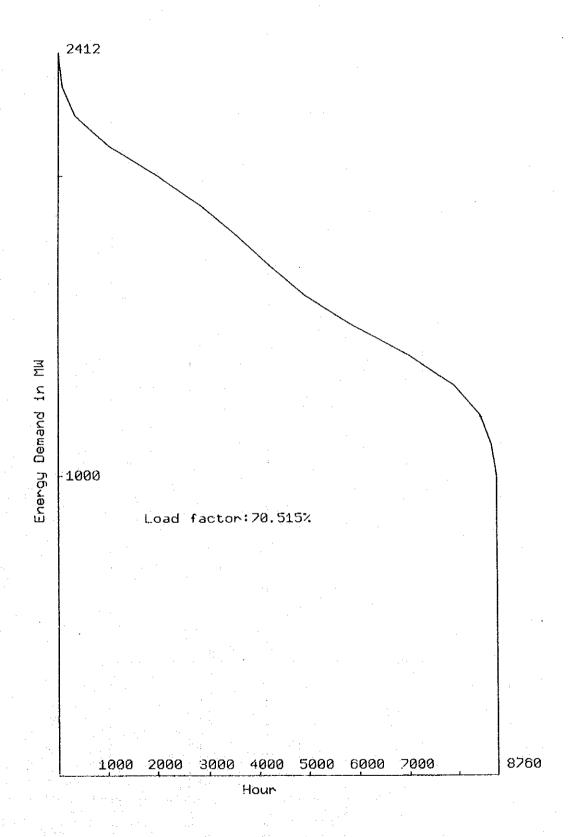


Fig - 12.5:7 Duration Curve (from Jan. to Dec. 1986)

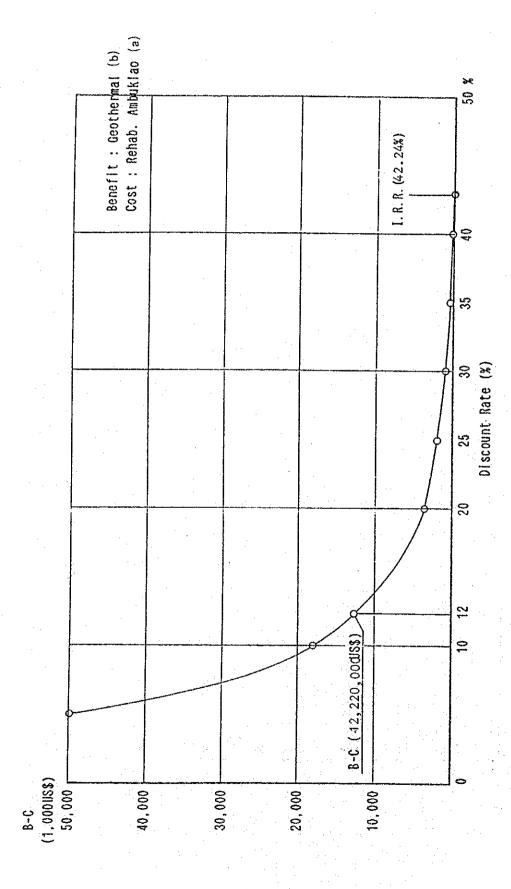


Fig-12.5.8 B-C, Discount Rate Curve (a-b)

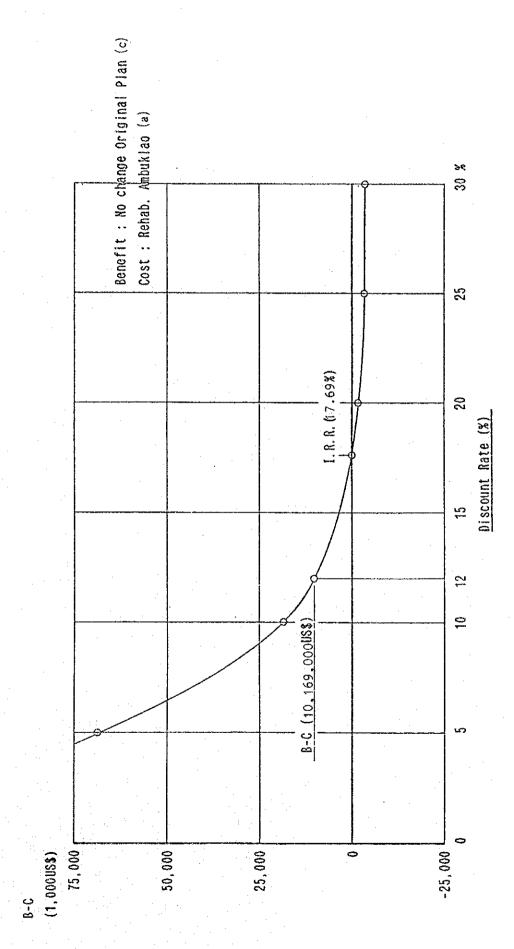


Fig-12.5.9 B-C, Discount Rate Curve (a-c)

13. Dam Safety Control System

# 13. Dam Safety Control System

## 13.1. General

The general safety control requirements for the Ambuklao Project were discussed in Chapters 4 and 10, above.

The safety control of hydropower facilities cover wide area, such as safety against landslides at or near the project structures and around the reservoir, safety against floods and sedimentation, safety of the dam and its foundations, underground structures, generating equipment and facilities, and environmental conservation.

In this Section, safety control for the rockfill dam is discussed in greater detail, taking into account the effects which the earthquake of April 1985 had on the stability of the dam.

For safety of rockfill dams, prevention of the following is important:

- (1) Flow over the top of the dam
- (2) Seepage through the dam or its foundations
- (3) Collapse of face of the dam caused by large earthquakes.

Inspection, surveillance and maintenance of the dam and its auxiliary structures are, therefore, very important, for the safety of the project.

For this, the following measures are required:

- (1) Monitoring
- (2) Inspection and surveillance
- (3) Detail inspection and further investigations
- (4) Maintenance

# 13.2. Monitoring

It is proposed to change the existing monitoring system in accordance with the proposed three stages described below. As over 30 years have passed since the completion of the Ambuklao Dam, it will be natural to assume that the Ambuklao Project should be placed in the third stage. However, considering the earthquake of April 1985 and the installation of boring holes for underground water observations, it is proposed that the second stage be applied. The second stage should be modified as required. Table-13.1 shows the proposed monitoring items and frequency of monitoring.

Description of the monitoring systems follows.

## (1) First Stage

This is the stage which covers the initial reservoir filling period. The water pressure load acts on the dam for the first time. The dam shows variable reactions until the water reaches the maximum reservoir level. This first stage of observations is, no doubt, the most important for the safety of the dam. Monitoring, therefore, must be carried out carefully and frequently. The monitoring results must be analyzed quickly in order to evaluate the behaviour of the dam and its safety and to decide the mode and sequence of further water level rises.

#### (2) Second Stage

During the period of this stage, monitoring is performed in order to determine whether the operating conditions of the dam could be judged to be normal, including the conditions of seepage through the foundation rock. This period could cover 3 to 5 years.

# (3) Third Stage

This stage covers the period during which monitoring of the dam is done with a purpose of maintaining the proper function of the dam through its lifetime. The period of this stage is the longest of the three stages.

The following table describes the frequency and type of monitoring normally used for embankment dams:

Table-13.1
Embankment Dams
Type of Monitoring and Frequency

		Monitoring Items			
Stage	Dam type	Seepage	Deformation	Seepage line	
	U/S* facing	everyday	once a week		
1	zoned	ditto	ditto		
	homogenious	ditto	ditto	once a week	
	U/S facing	once a week	once a month		
2	zoned	ditto	ditto		
h	homogenious	ditto	ditto	once a month	
	U/S facing	once a week	once 3 months	et e	
3	zoned	once a week	once 3 months		
	homogenious	once a week	once 3 months	once 3 months	

U/S: Upstream

For the Ambuklao Dam, the following specific type of monitoring and respective frequencies are proposed:

Table-13.2

Ambuklao Dam

Type of Monitoring and Frequency

Monitoring Items	Frequency	Remarks
Precipitation	once a day	
Reservoir Water Level	once a day	
Seepage at the Dam	once a week	
Seepage at the Powerstation	once a day	to be reduced in the future
Water Level at the Openpipe Piezometer	once a month	to be reduced in the future
Water Level at the Openpipe Piezometer on the Dam Crest	once a week	
Water Level at the Inclinometer Hole	once a week	
Water Level at the Spillway Left Abutment	once a week	to be reduced in the future
Dam Displacement, Alignment-1	once a month	to be reduced in the future
Dam Displacement, Alignment-2	once a month	to be reduced in the future
Inclinometer	once a month	

# 13.3. Inspection

Inspection of structures is very important for prevention of problems and, failures. Inspection of the dam on a regular basis and in accordance with some predetermined pattern can be very effective in preventing major problems or even failures from developing. In addition to the regular inspections, inspections to be performed after occurrence of a major event, such as large floods or earthquakes, are also highly desirable.

The above inspections and their frequencies are presented in the following tabulation:

Table-13.3

Type of Inspections and their Frequency

Type of Inspection	Frequency	<u>Activity</u>
Periodic inspection	Once a month	Measurement and sur- veillance reading
Inspection after earthquake	If stronger than on the Richter Scale	ditto
Inspection after flood	If bigger than 3-year return period	ditto
Inspection after heavy rain	If bigger than 3-year return period	ditto

# 13.4. Detail Inspection and Further Investigations

If abnormal behaviour or conditions are detected during the periodic inspection or from the collected monitoring data, a detail investigation must be undertaken to determine the causes for the above.

The extent of the investigation will depend on the importance of the problem or the structure.

For the Ambuklao Dam, the abnormal flood of December 1976 or the earthquake of April 1985, belong to the events for which further investigation would be required.

As reported such proper measures were actually taken at the time of the occurrence of the above flood and earthquake.

# 13.5. Maintenance

When it is found, as a result of the routine inspection or inspection after the occurrence of a big flood or earthquake, or simply from the monitoring data, that the dam or certain parts of the dam require to be maintained and repaired, such work should be carried out immediately and without any delay.

