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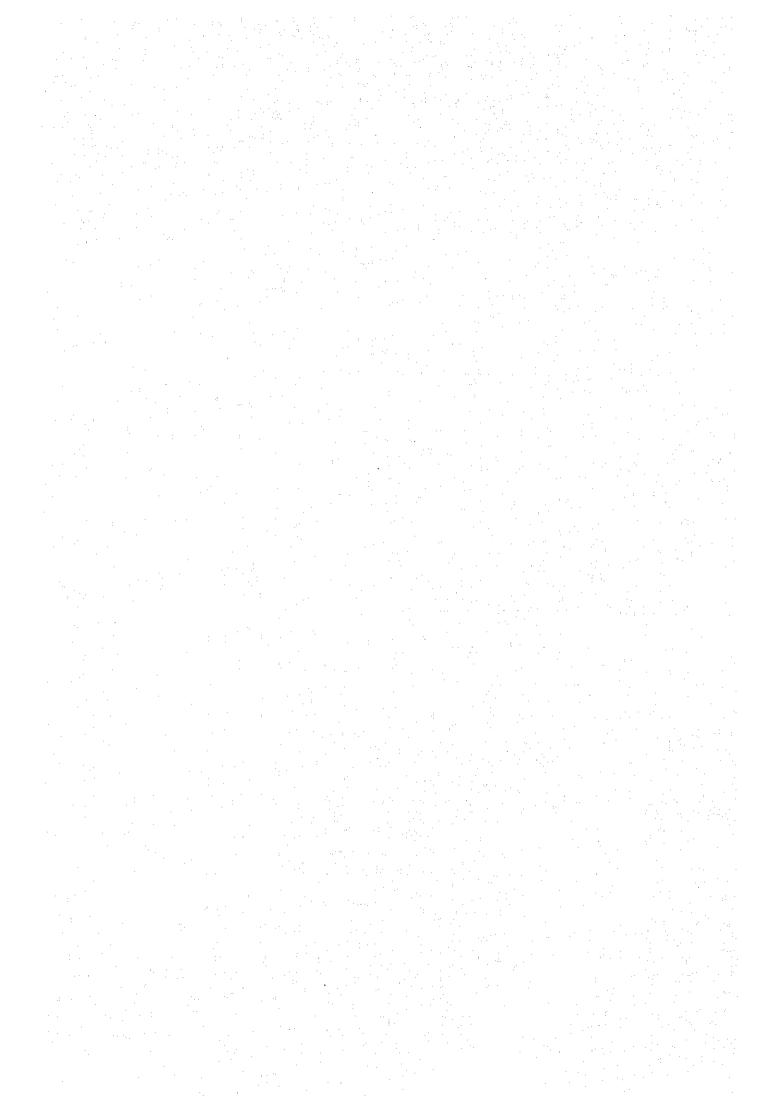
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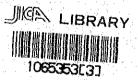


FEDERATIVE REPUBLIC OF BRAZIL

FINAL REPORT ON THE ITAJAI RIVER BASIN FLOOD CONTROL PROJECT

PART I
MASTER PLAN STUDY

SUPPORTING REPORT



JANUARY 1988

JAPAN INTERNATIONAL COOPERATION AGENCY
TOKYO, JAPAN

ABBREVIATION

JICA : Japan International Cooperation Agency

ACARESC : Associacao de Credito e Assistencia Rural de Santa Catarina

CASAN : Companhia Catarinense de Aguas e Saneamento

CEDEC : Coordenacao Estadual de Defesa Civil

CELESC : Centrais Eletricas de Santa Catarina

CEPA: Instituto de Planejamento e Economia Agricola de Santa

Catarina

CIDASC : Companhia Integrada de Desenvolvimento Agricola de Santa

Catarina

DNAEE : Departamento Nacional de Agua e Energia Eletrica

DNER : Departamento Nacional de Estradas de Rodagem

DER : Departamento de Estradas de Rodagem

DNOS : Departamento Nacional de Obras de Saneamento

EMATER : Empresa de Assistencia Tecnica e Extencao Rural

EMBRAPA : Empresa Brasileira de Pesquisa Agropecuaria

EMATER : Empresa de Assistencia Tecnica

EMPASC : Empresa de Pesquisa Agropecuaria ria de Santa Catarina

FATMA : Fundacao de Amparo a Tecnologia e Meio Ambiente

FGV : Fundacao Getulio Vargas

GAPLAN : Gabinete de Planejamento e Coordenacao Geral

IBDF : Instituto Brasileiro de Desenvolvimento Florestal

IBGE : Instituto Brasileiro de Geografia e Estatistica

IBRD : Internatinal Bank for Reconstruction and Development

ITAG : Instituto Tecnico de Administracao e Gerencia

MA : Ministerio da Agricultura

MDUMA : Ministerio do Desenvolvimento Urbano e Meio Ambiente

PORTOBRAS : Empresa Brasileira de Portos

SAMAE : Servico Autonomo Municipal de Agua e Esgoto

SUDEPE : Superintendencia do Desenvolvimento da Pesca

ABBREVIATION OF MEASUREMENT

Length Time

mm : millimeter s or sec : second

cm : centimeter min : minute

m : meter h or hr : hour

km : kilometer d : day

y or yr : year

Area Others

cm² : square centimeter % : percent

m² : square meter °C : degree centigrade

ha : hectare 103 : thousand

km² : square kilometer 106 : million

109 : billion

Volume Derived Measure

cm³ : cubic centimeter m³/s : cubic meter per second

1 : liter kwh : kilowatt hour

m3 : cubic meter

Weight Money

g : gram Cz\$: Cruzado

kg : kilogram Cr\$: Cruzeiro

ton : metric ton US\$: US dollar

Exchange Rate (in March 1986)

US\$ 1 : Cz\$ 13.80

ABBREVIATION OF ECONOMIC TECHNICAL TERMS

GDP : Gross Domestic Product

GRDP : Gross Regional Domestic Product

GVA : Gross Value Added

VA : Value Added

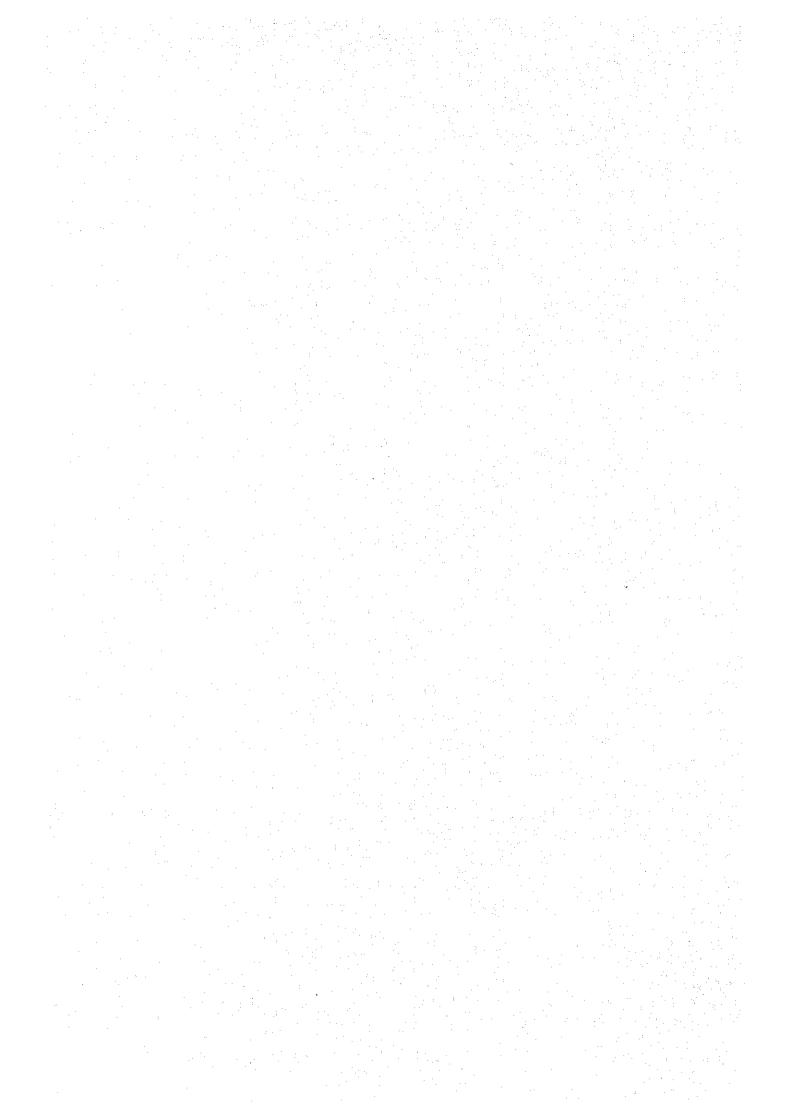
PV : Production Value

SUPPORTING REPORT

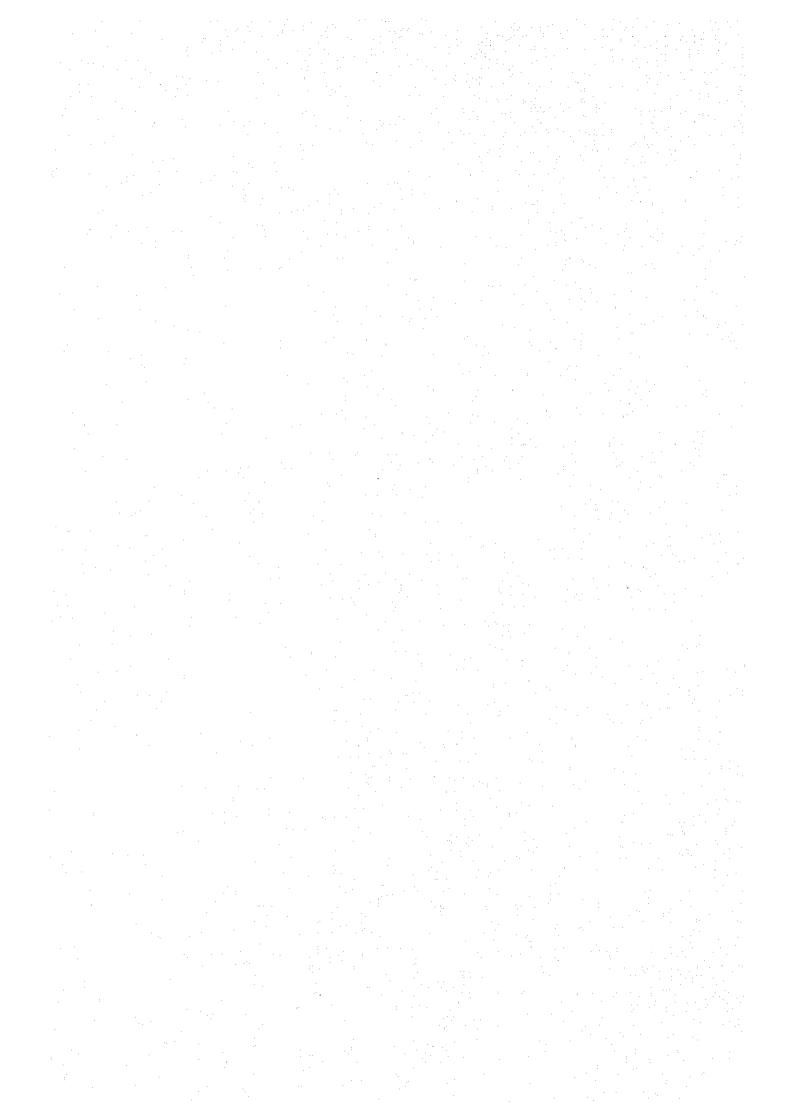
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- III. GEOTECHNICAL INVESTIGATION
- IV. SOCIO-ECONOMY
- V. FLOOD DAMAGE STUDY
- VI. FLOOD CONTROL PLAN



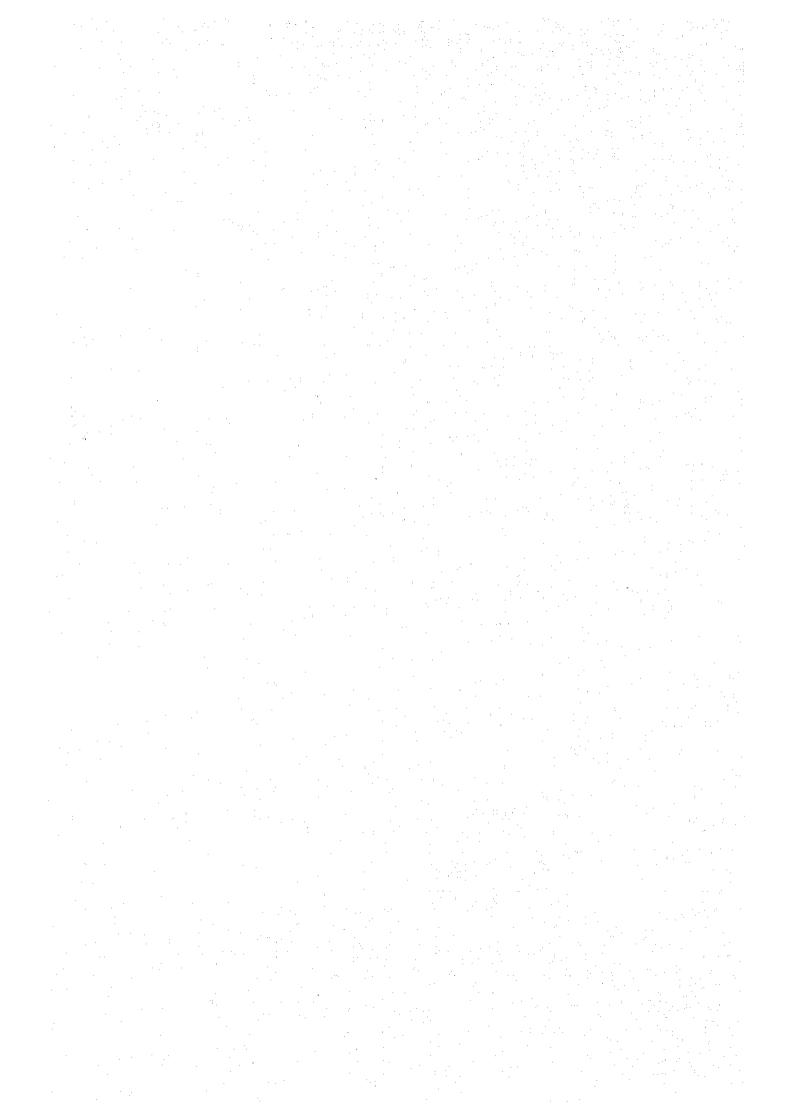
ANNEX I. TOPOGRAPHIC SURVEY



I. TOPOGRAPHIC SURVEY

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1. INTRODUCTION

The topographic survey for the study includes;

- Collection and check of available topographic data,
- Arrangement of topographic data for use of master plan study, and
- Execution of additional river cross sectional survey.

The topographic data such as topographic maps, aerial photographs, river profile and cross sections were collected from DNOS and organizations concerned.

The collected data were reviewed and arranged for master planning uses. From the result of review, the additional river cross sectional survey were executed in cooperation with DNOS's surveying staff under instruction by the JICA TEAM.

2. DATA COLLECTION AND THEIR REVIEW

2.1 Available Data

The topographic maps of several kind of scale were collected from IBGE and main cities through DNOS. These maps are divided into the national base maps and the city planning topographic maps. The list of collected maps is shown in Table I.1.1.

The stereoscopic aerial photographs with a scale of 1:25,000 which were shot in 1978 and 1979 and cover along the Itajai river were borrowed from FATMA. These photographs were used for planning of master plan.

The river profile and cross sectional data were collected. These data were prepared for use of the river improvement plan of the Itajai river by DNOS. The list of collected cross sectional data is shown in Table I.1.2.

The data of horizontal and vertical national ground control points were obtained from IBGE for the purpose of an additional river cross sectional survey and photogrammetric mapping in the feasibility study.

2.2 Review of Available Data

2.2.1 Topographic maps

(1) National base map

National base map on a scale of 1:50,000 covering the east of longitude 50° W at the Itajai river basin, were collected from IBGE. The map consists of 29 sheets of colour printed maps with 20 m contour interval which were prepared in 1981. Since national base map of 1:50,000 in the west of longitude 50° W at the project area is not yet published, the map on a scale of 1:100,000 which was prepared in 1973 was collected. This map consists of 3 sheets of colour printed and 50 m contour interval.

The datum of these national base maps are;

(i) Vertical : Imbituba, Santa Catarina

(ii) Horizontal : SAD - 69. (South American data in 1969)

(iii) Projection : Universal Transverse Mercator (referred as UTM)

The index map of the national base maps is shown in Fig. I.1.1.

(2) Large scale topographic maps

(i) Scale of 1:2,000

Large scale topographic maps in Blumenau and Brusque cities on a scale of 1:2,000 with 1 m contour interval were obtained. These maps were prepared by the aerial photogrammetric method and cover whole city area. The horizontal and vertical datum of map is the same as national base map. However, since they were made more than ten years ago, namely 1972 in Blumenau and 1975 in Brusque,

it is necessary to consider the change of social infrastructures and geographical features for use of planning.

(ii) Scale of 1:4,000 and 1:5,000.

The topographic map on a scale of 1:4,000 and 1:5,000 were collected. They are scale of 1:4,000 with 5 m contour interval in Timbo city, a scale of 1:5,000 with 2 m contour interval in Picarras city and with 5 m contour interval in Rio do Sul city.

These maps have not the coordinates and the datum of altitude is not clear, therefore, they can not be used for master planning.

(iii) Scale of 1:10,000

The scale of 1:10,000 topographic maps in Blumenau, Brusque and Gaspar cities were collected. The contour interval is 5 m in Blumenau and Gaspar, and 10 m in Brusque. The datum of map is the same as the national base map.

The maps in Blumenau and Brusque were reduced and compiled from the map with a scale of 1:2,000 in 1972 and 1975. In case of Gaspar, they were prepared in 1978 by aerial photogrammetric method but did not cover the whole city.

Besides, the same scale of topographic maps along the upstream of the Itajai river, the Benedito and the Itajai do Norte, Oeste and Sul rivers were obtained. These maps were prepared in 1959 by the aerial photogrammetric method and covers about 1 km in width in both sides of the river. The projection of map is U.T.M, but coordinates are local system. The datum of altitude is the same as national base map. Therefore, these maps are only available for check up of topographic feature.

The index map of the above collected large scale topographic maps is illustrated in Fig. I.1.2.

2.2.2 Aerial photographs

The aerial photographs which were borrowed from FATMA were shot in 1978 and 1979 by whole Santa Catarina aerial photography program. These monochrome photographs on a scale of 1:25,000 were shot by means of 60% stereoscopic overlap and 30% sidelap in average.

Aerial camera which is used for R.M.K. is a wide angle of format $23\,\mathrm{cm}$ x $23\,\mathrm{cm}$, and the attached pleogon is a distortion free lens. The negative films are stored in the aerial photographed firm under the regulation.

2.2.3 River profile and cross sectional data

(1) The Itajai river

(i) Barra - Blumenau

The river profile and cross sectional survey data from Barra to Blumenau were collected. These data were prepared for use of study for river improvement in the downstream of Blumenau by DNOS in 1983 to 1984. The surveyed river cross sections are in about 45 km in distance with 200 m interval, and they are drawn in a scale of 1:1,000 in horizontal and 1:100 in vertical. The datum of vertical is the same as national base map.

The drawings of profile were plotted only height of cross section's base points on a scale of 1:2,000 in horizontal and 1:100 in vertical but the height of riverbed and banks are not shown.

(ii) Salto Pilao - Rio do Sul

The same kind of data for Salto Pilao to Rio do Sul were collected. These data were prepared in 1984 and they are being used for planning by DNOS for river improvement in the downstream of Rio do Sul. The surveyed river cross sections are about 24 km in distance with 400 m interval. The drawing of cross sections were plotted on a scale of 1:2,000 in horizontal and 1:200 in vertical. Scale and presenting condition for the drawings of profile are the same as (a).

(2) The tributaries

(i) The Itajai do Oeste and Sul rivers

The river profile and cross sectional data of the Itajai do Oeste and Sul rivers were obtained. The distance of the surveyed data are about 5 km from the confluence with the Itajai main stream to the Oeste and 3 km in the Sul river. They are prepared by DNOS.

(ii) The Itajai Mirim river

The cross sectional data of the Itajai Mirim river were collected from DNOS. The surveyed data are 41 km in total distance from the confluence of the Itajai river to Brusque city.

(iii) Floodway

The cross sectional data for the proposed floodway route were collected. These data were compiled based on the topographic map, not by actual survey work, because of refusal on entrance permission for the sugar cane fields.

3. ADDITIONAL RIVER CROSS SECTIONAL SURVEY

As the result of review on collected river cross sectional data, more than 60 additional river cross sections were surveyed in this stage in cooperation with DNOS's surveying staff.

The additional river cross sections are listed in Table I.1.3 and the index map of river cross sections is shown in Fig.I.1.3.

The drawings of survey data were plotted on a scale of 1:1,000 in horizontal and 1:100 in vertical.

(1) The Itajai river

(i) Itajai - Barra

The bathymetric data of the river mouth were collected from PORTOBRAS. The datum of PORTOBRAS is not same as national base map, therefore, the data were converted to the datum of national base map.

The additional survey were executed for the river stretch from 7 km upstream to 30 km from river mouth. The surveyed data were connected to national bench marks in Itajai city and along the national route.

(ii) Blumenau - Salto Pilao

The river stretch along the flood prone areas in the Indaial and Ascurra cities was surveyed in short interval of about 500 m, and the remaining stretch was surveyed in an interval of 5 km. The cross section at the water gauging station located at Indaial, Warnow and Apiuna cities was also surveyed. The surveyed data were tied with national bench marks in the main cities and on the Route BR - 470.

(2) The tributaries

(i) The Itajai do Norte river

The surveys were executed in the confluence of the Itajai river to upper Ibirama city and connected with national bench marks in Ibirama city and on the BR - 470.

(ii) The Itajai do Sul river

The seven cross sections at Ituporanga and Aurora cities were surveyed. The surveyed data were connected to the record of topographic map, because there was no national bench mark in this area.

(iii) The Itajai do Oeste and the Trombudo river

At the close by the confluence of two rivers, each one cross section was surveyed and connected to national bench mark.

(iv) The Benedito river

At the downstream of the Benedito river, three cross sections were surveyed and connected to national bench marks in Indaial city.

Tables

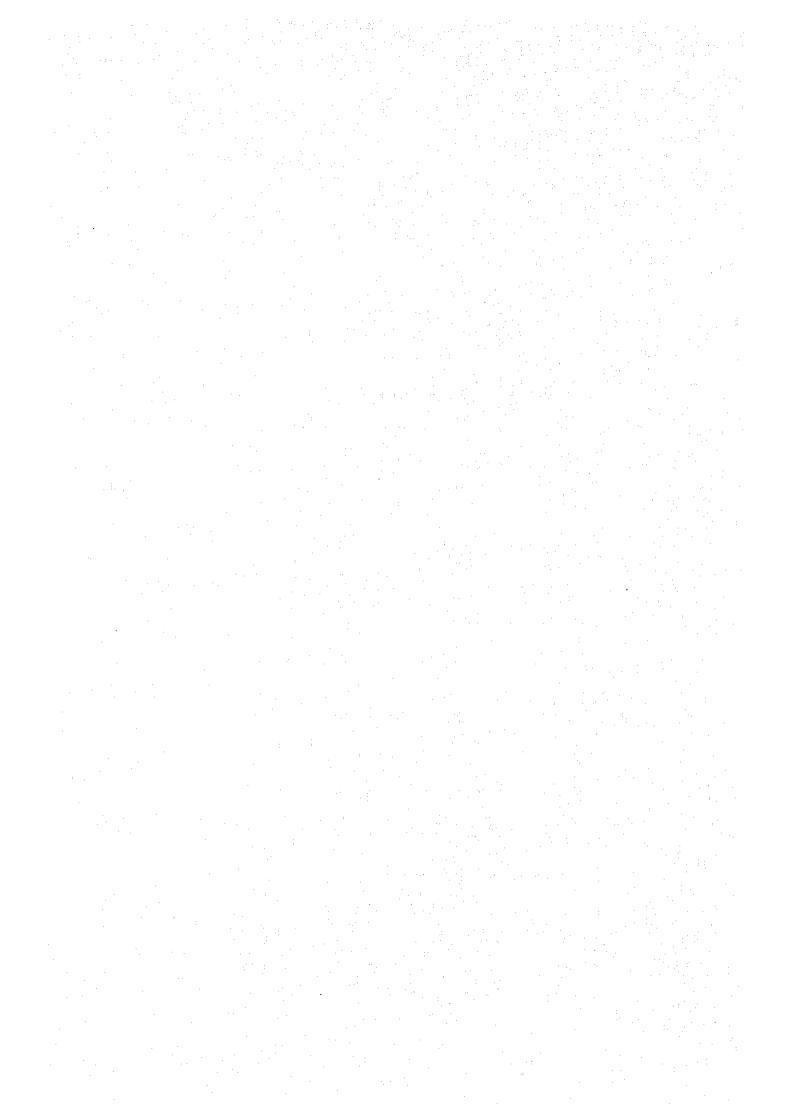


Table 1.1.1 COLLECTED TOPOGRAPHIC MAPS

•		Contour	Coordi	nates	_		
Area	Scale	Interval (m)	Interval (km)	Projection	Datum	Mapping	Remarks
Itajai river basin	1/50,000	20	2	MTU	National	1981	•
(East of long. 50 W) Itajai river basin	1/100,000	50	5	UTM	National	1973	
(West of long. 50 W) Blumenau city	1/2,000	1	0.2	UTM	National	1972	
Blumenau city	1/10,000	5	1	UTM	National	1972	
Itajai city	1/10,000	5	0.2	UTM	National	. –	2.0
Rio do Sul city	1/5,000	.5	None			1983	Partial area
Brusque city	1/2,000	1	0.2	UTM	National	1975	
Brusque city	1/10,000	10	1	UTM	National	1975	
Gaspar city	1/10,000	5	1	UTM	National	- v	Partial area
Picarras city	1/5,000	2	None	-		1978	•
Timbo city	1/4,000	5	None	÷ ,		1975	
Itajai river	1/10,000	10	1	MTU	Local	1959	
(Blumenau-Rio do Sul)							
Itajai do Norte, Sul ar	1/10,000	10	1	UTM	Local	1959	

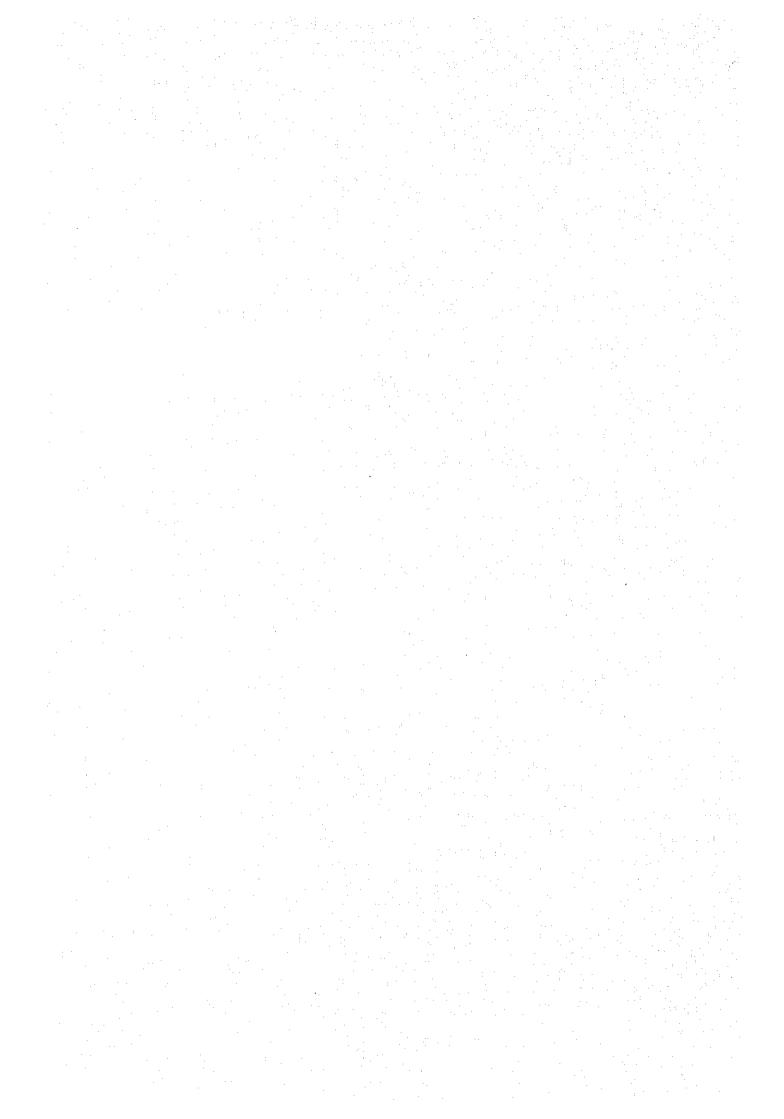
Table 1.1.2 COLLECTED RIVER CROSS SECTIONS

		Distance	Interval	Sca	le	Remarks
Name of River	Section	(km)	(m)	Н	V	
Itajai	Barra-Blumenau	45	200	1/1,000	1/100	
Itajai	Salto Pilao-	24	400	1/2,000	1/200	
	Rio do Sul	•				
Itajai do Oeste	Rio do Sul	5	400	1/2,000	1/200	
Itajai do Sul	Rio do Sul	3	400	1/2,000	1/200	•
Itajai Mirim	Itajai-Brusque	41	1000	1/200	1/100	
Picarras floodway	Picarras-Barra	10	200	1/1,000	1/100	Planning route

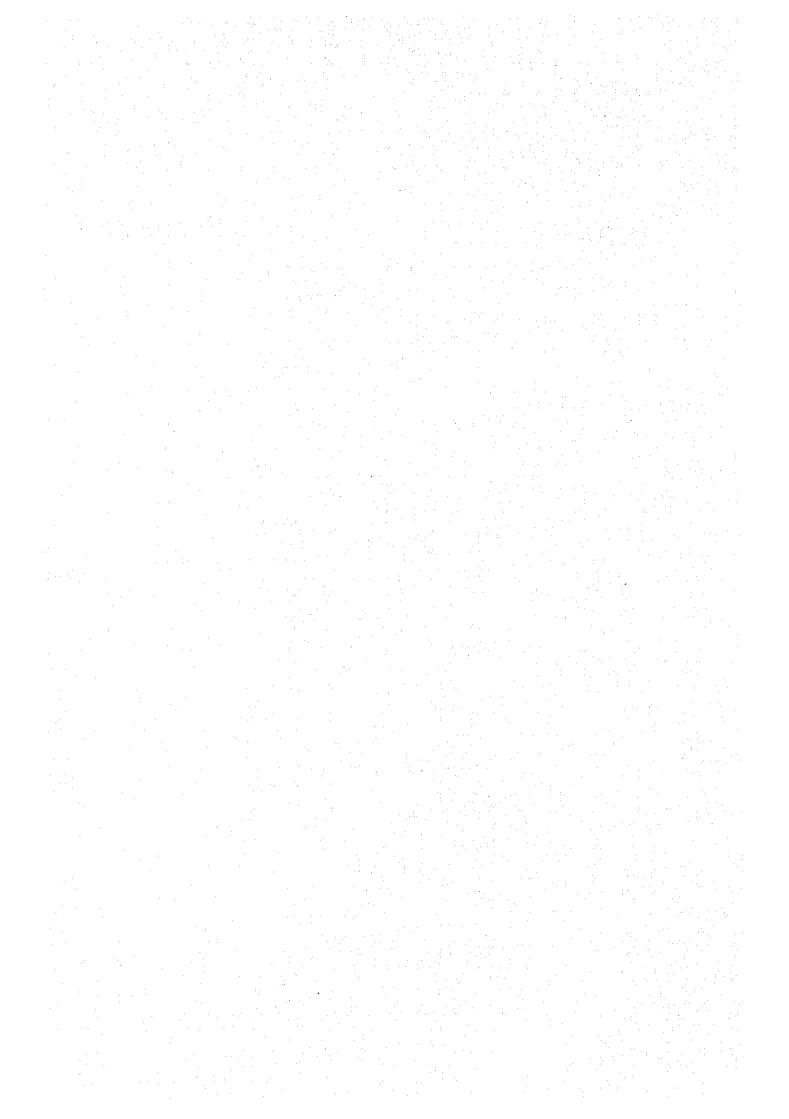
Table 1.1.3 ADDITINAL RIVER CROSS SECTIONS

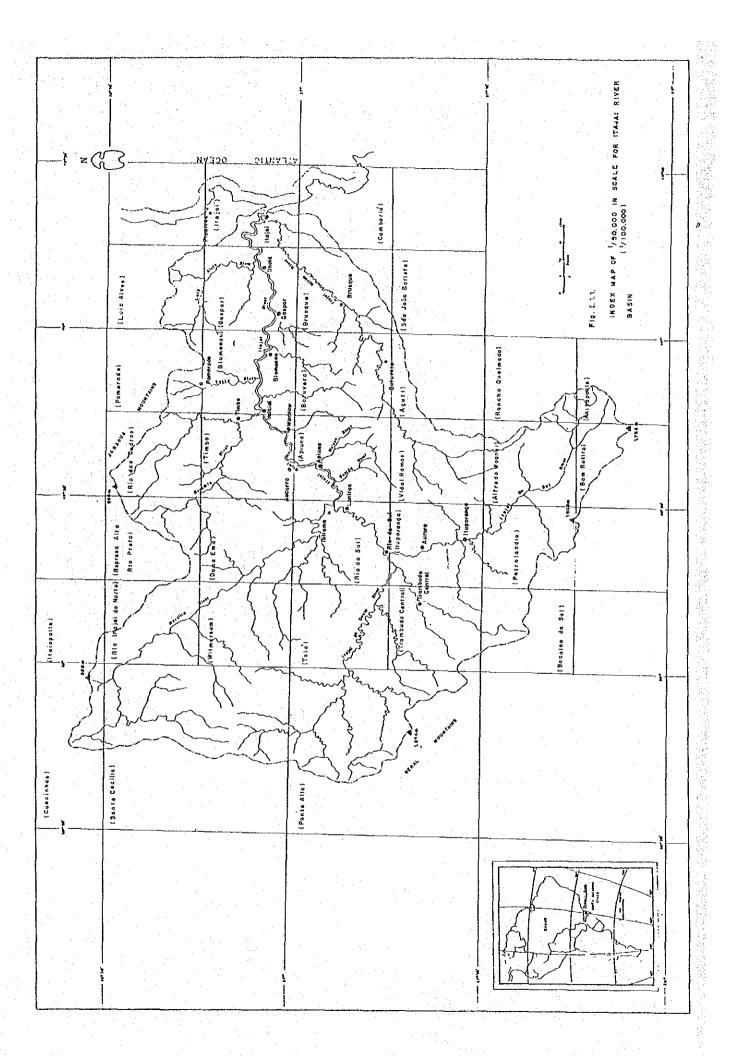
		Distance	Interval	Sc	ale	Remarks
Name of River	Section	(km)	(km)	Н	v	
Itajai	Itajai-Barra	30	1	1/1,000	1/100	
Itajai	Blumenau-Indaial		0.5 - 5	1/1,000	1/100	
Itajai	Indaial-Ascurra	20	0.5 - 4	1/1,000	1/100	•
Itajai	Ascurra-	40	4 - 5	1/1,000	1/100	
	Salto Pilao					
Itajai do Norte	Itajai Acu-	6	2 - 4	1/1,000	1/100	•
	Ibirama	•			1	
Itajai do Sul	Aurora,	4	0.5 - 1	1/1,000	1/100	
	Ituporanga			•		
Itajai do Oeste	Rio do Sul	2	2	1/1,000	1/100	
Benedito	Indaial	1	0.5 - 0.8	1/1,000	1/100	•
Trombudo	Trombudo	0.5	0.5	1/1,000	1/100	

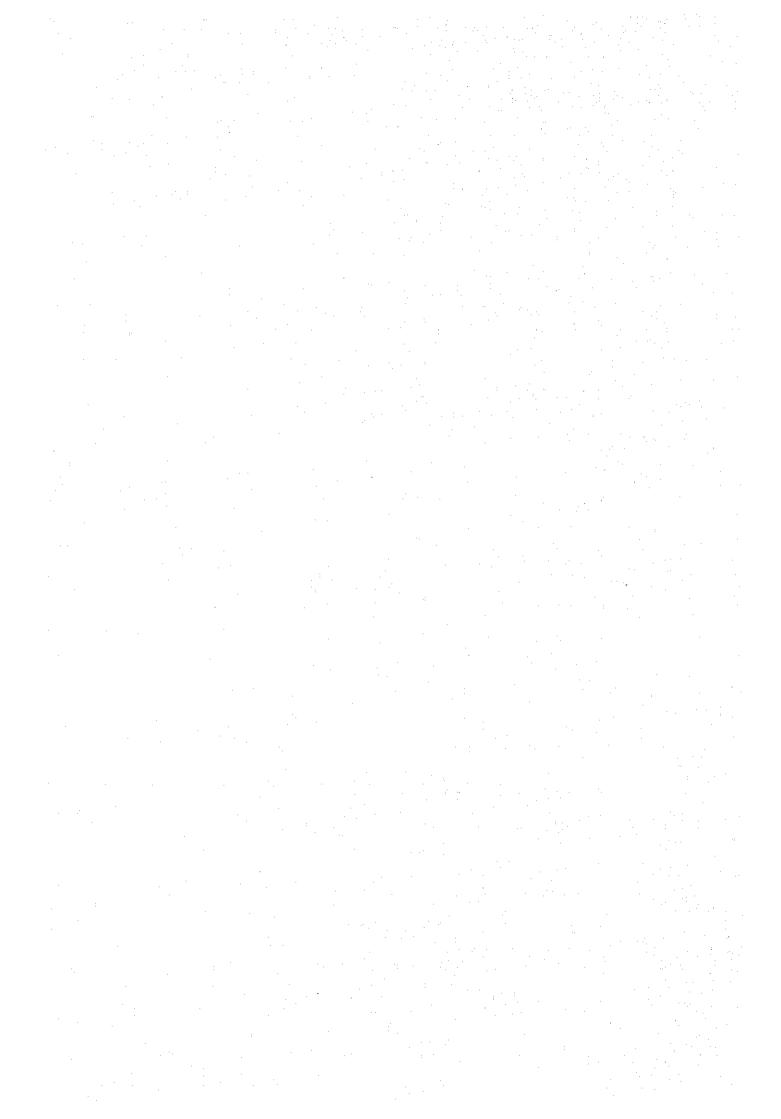
Note: H: Horizontal V: Vertical

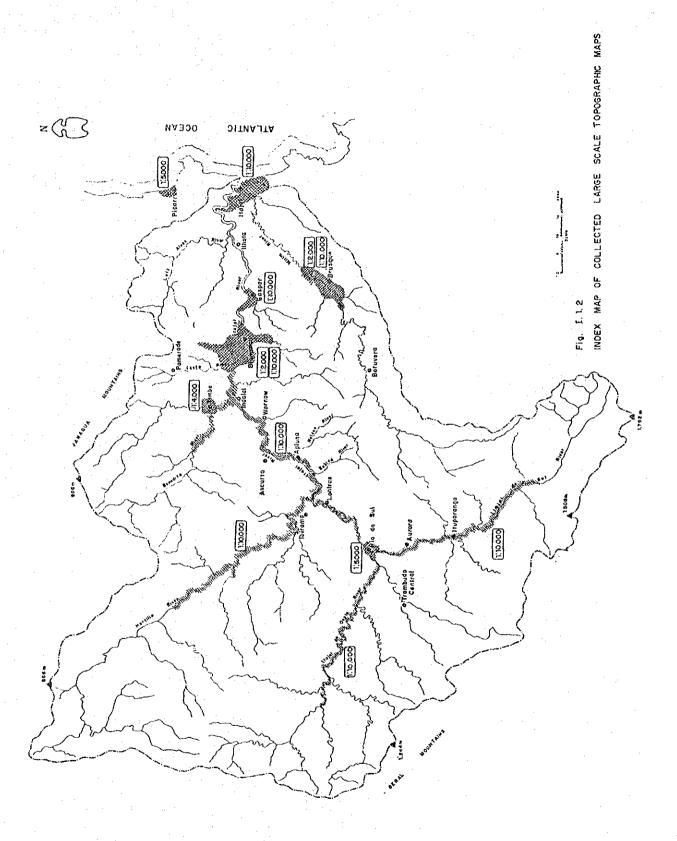


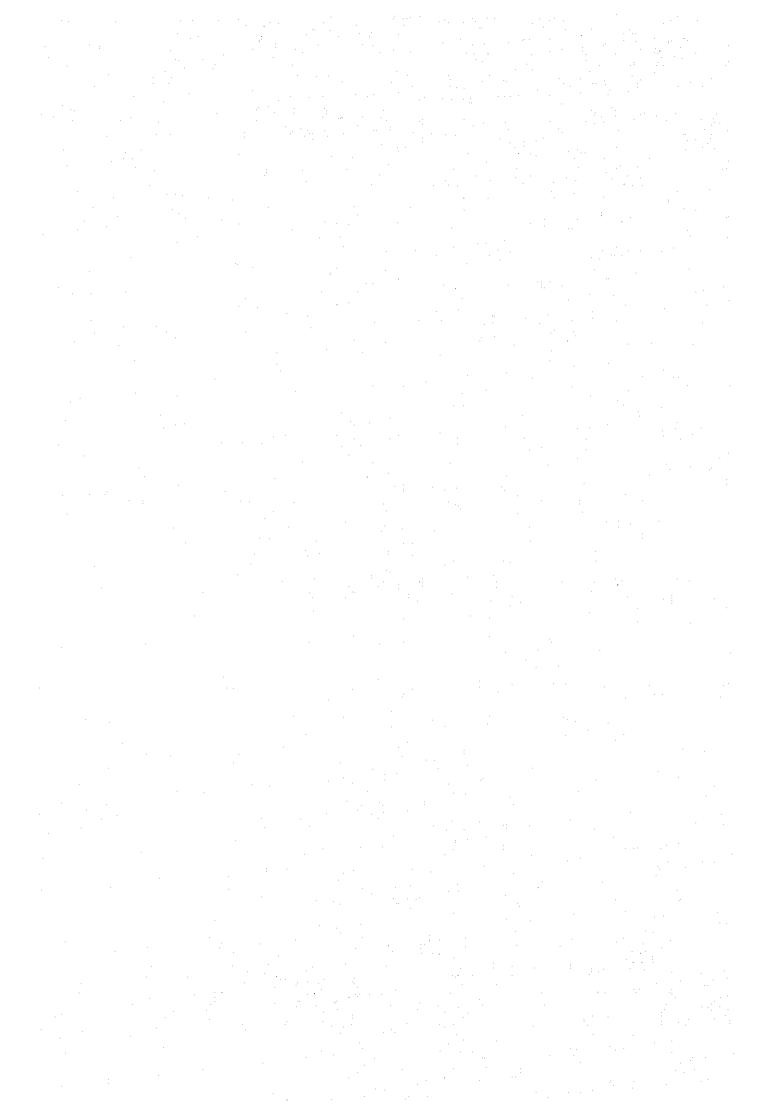
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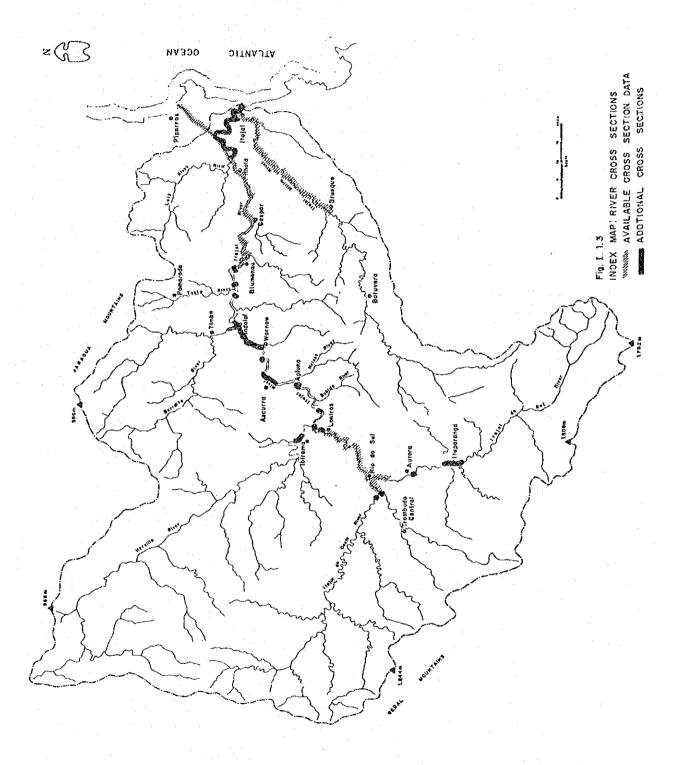


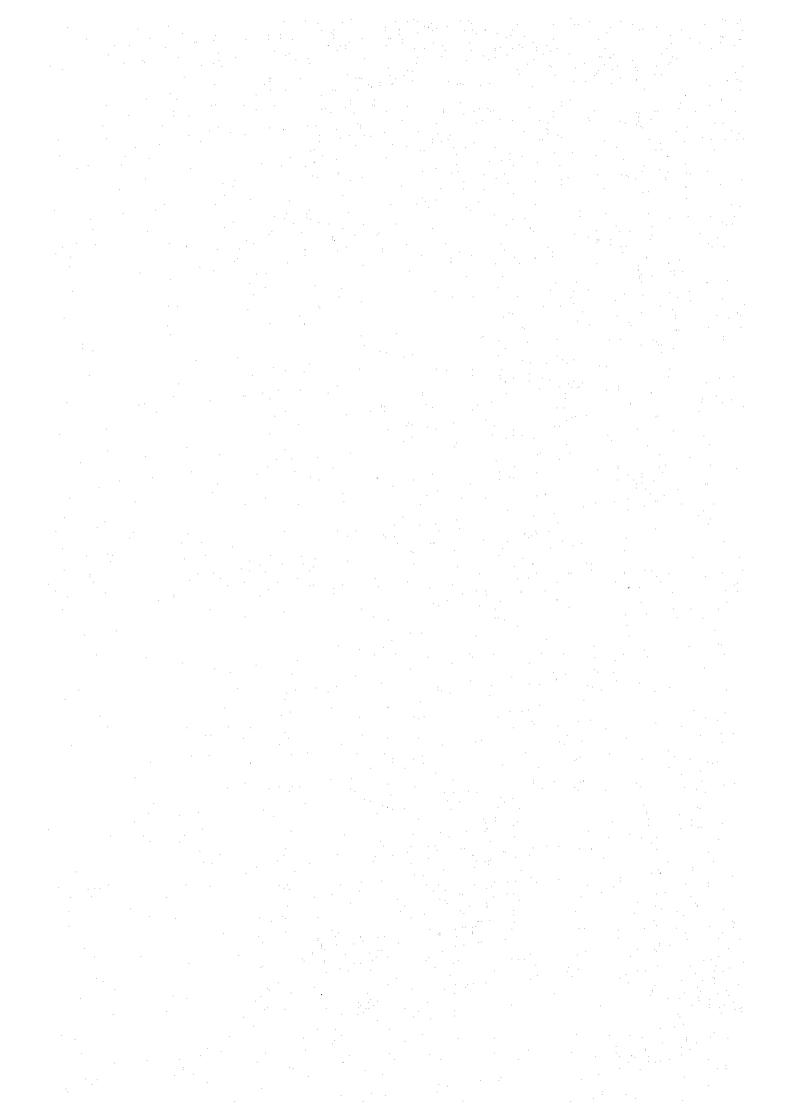




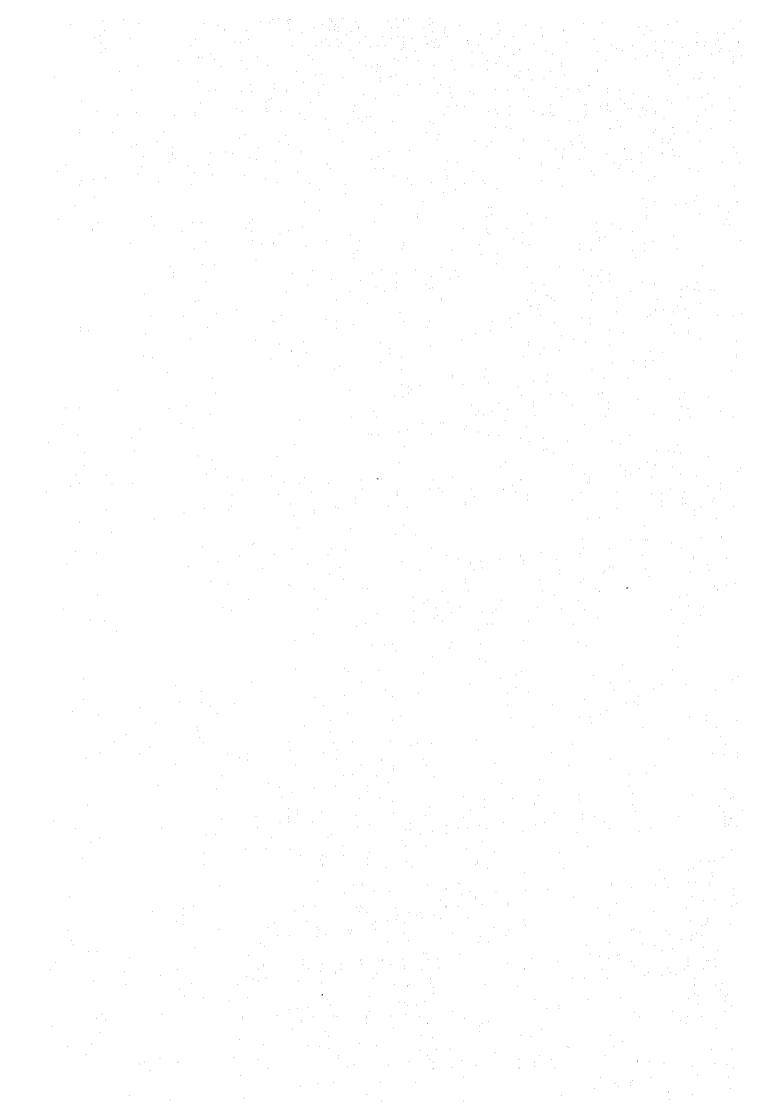








ANNEX II. HYDROLOGY



II. HYDROLOGY

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INTRODUCTION

Hydrological analysis aims at grasping hydrological characteristics and formulating the probable flood discharge distribution under present condition and with flood prevention works proposed in the flood control plan through the basic hydrological analysis and flood runoff analysis using the mathematic simulation model which is able to evaluate the effect of the river improvement and flood control facility for the reduction of flood peak discharge.

Therefore, the following studies were carried out in the hydrological analysis:

- hydrological data collection such as meteorological records, rainfall data, discharge data including hydrograph records, and tide water level records which affects the flood water level in the river channel,
- rainfall analysis comprising basin mean rainfall and probable rainfall estimates against design rainfall duration time,
- establishment of simulation model being able to express the relation between rainfall and runoff, and
- estimate of probable flood discharge and establishment of design flood discharge distribution againt the selected retern period.

2. METEO-HYDROLOGICAL DATA

(1) Meteorological data

Meteorological observation such as a temperature, relative humidity, evaporation, wind velocity and atmospheric pressure have been carried out at 9 meteorological observatories as shown in Fig.II.2.1 by INMET and EMPASC since 1911 in and around the Itajai river basin. Table II.2.1 shows the observation period in each meteorological observatory.

(2) Rainfall data

There exists 69 rainfall gauging stations in and around the Itajai river basin at which the daily rainfall amount has been observed at 7 o'clock every morning by DNOS, DNAEE, INMET, CELESC, EMPASC and SOUZA CRUZ. The location of the above stations is shown in Fig.II.2.1.

As shown in Fig.II.2.1, 19 stations are located around the basin and other 50 stations are densely distributed along the Itajai river and its tributaries in the basin.

Among the above 69 stations, 6 stations were installed in 1930's, and 20 stations in 1940's, and most of others in 1970's. And then, the observation at 12 gauging stations were discontinued.

Hourly rainfall observation was commenced at Indaial city in 1970 and 15 stations are installed in the Itajai river basin at present. 11 stations were constructed after the large flood in July, 1983.

Figs.II.2.2 and II.2.3 show the observation period of daily/hourly rainfall respectively.

(3) Water level and discharge

Water level observation and discharge measurement were commenced in 1920 and 36 water level gauging stations in Fig.II.2.1 which are operated by DNAEE, DNOS and CELESC, are installed along the Itajai river and its tributaries at present.

Water level at the above stations is observed twice a day at seven o'clock in the morning and five o'clock in the evening. Water level observation by an automatic recorder was commenced at Apiuna on August, 1971. At present, 7 stations, namely, Apiuna, Rio do Sul Novo, Brusque, Taio, Ituporanga, Ibirama, and Blumenau are installed and operated.

Discharge measurement is carried out about 10 times a year using current-meter by the preceding organization. Discharge rating curve for converting water level to discharge is made periodically by using the discharge measurement records.

Figs.II.2.4 and II.2.5 show the observation period of daily/hourly water level and discharge respectively.

(4) Tigal data

The lower reach downstream from Blumenau city has gentle river bed slope of around 1/15,000. Therefore, the fluctuation of tide water level affects the flood water level along the lower reach.

The tide water level fluctuation is recorded at the Itajai harbor by PORTBRAS since 1983. The location of the observation site is shown in Fig.II.2.1.

(5) Sediment data

Sediment concentration of suspended load on the Itajai river and its tributaries are observed several times a year after 1976 at Rio do sul, Apiuna, Indaial, Barra do Prata and Brusque by DNAEE. However, in regard of wash and bed loads, no observation has been carried out up to present.

3. METEO-HYDROLOGICAL CONDITION OF THE ITAJAI RIVER BASIN

3.1 Climate

The climatic records are shown in Table II.3.1.

The annual mean temperature in the Itajai river is 19.70C at Itajai and 20.10C at Blumenau in the lower area, and 18.40C at Ituporanga in the mountainous area.

The minimum temperature is 13.20C at Ituporanga in June and the maximum is 25.50C at Timbo in January.

The basin mean annual evaporation amount is estimated to be around 800mm in the Itajai river basin which is corresponding to the evaporation rate of 2.2 mm/day.

The maximum monthly evaporation amount is 104 mm at Itajai and Timbo which is corresponding to the evaporation rate of 3.3 mm/day.

Annual mean relative humidity is 85.7% at Itajai and 77.0% at Indaial which are the maximum and the minimum in the basin. The monthly mean relative humidity from June to August is higher than other months.

Fig.II.3.1 shows the isohyetal map of annual mean rainfall in the Itajai river basin for the period from 1976 to 1985. The basin mean annual rainfall is estimated to be 1630 mm ranging from 1,500 mm in the mountainous area of the upstream of the Benedito river and Sul river to 1,800 mm along the main Itajai river.

3.2 Low Flow

Monthly discharges for the period from 1976 to 1985 at the water level gauging station of Rio do Sul and Indaial in the main Itajai river, Timbo in the Benedito river, Ibirama in the Itajai do Norte river, Ituporanga in the Itajai do Sul river, Taio in the Itajai do Oeste river and Brusque in the Itajai Mirim river are shown in Table II.3.2.

As shown in this table, monthly mean discharge from July to December is larger than the annual mean discharge at each station. From this fact, it can be said that a wet season is from July to December, and a dry season is from January to June in a year. Monthly mean discharges for the above periods and annual mean discharge are summarized as below.

		ischarge (
Name of Station	JanJun.	JulDec.	Annual Mear
Rio do sul	104.7	162.9	135.1
Indaial	205.8	347.2	286.3
Timbo	40.7	50.8	47.7
Ibirama	55.7	100.6	80.5
Ituporanga	39.3	58.8	50.9
Brusque	25.3	35.4	31.5

The runoff coefficient at Indaial water level gauging station is estimated to be 0.48 from the runoff depth of 786 mm at Indaial and basin mean annual rainfall amount of 1,630 mm.

3.3 Flood Flow and Rain Storm

According to the flood records at Indaial in Table II.3.3 and Blumenau in Table II.3.4, four large scale floods after construction of Sul and Oeste dams occurs on December 1978, December 1980, July 1983 and August 1984. Flood peak discharge at 6 stations are listed up as below.

Name of Station	Dec.1978	Flood Peak Dec.1980		(m ³ /sec) Aug.1984
Rio do sul Novo	720	850	1,970	1,860
Ibirama	1,010	1,380	2,480	2,070
Timbo	560	690	760	860
Apiuna	2,300	3,690	4,310	4,320
Indaial	2,900	3,500	4,740	5,030
Brusque	550	320	540	w-

Flood hydrographs in 1978,1980 and 1984 shown in Fig.II.4.11 have the rising rimb of 1 to 2 days and depression of 3 to 4 days. The flood in 1983 is characterized by the long duration time of flood peak.

Rain storm which causes the flood is characterized by regional and hourly rainfall distribution. According to the isohyetal map of the rain storm as shown in Fig.II.3.2, the heavy rainfall occurs in the entire Itajai river basin and it is intensive in the mountainous area of main tributaries which are the Benedito river, the Itajai do Norte river, the Itajai do Oeste river, the Itajai do Sul river, the Itajai Mirim river. Especially, the rainfall of around 150 mm a day falls in the Itajai Mirim river basin.

Basin mean 1-day maximum rainfall and rainfall amount of rain storm are 110 mm and 124 mm in 1978, 65 mm and 138 mm in 1980, 64 mm and 324 mm in 1983, and 110 mm and 210 mm in 1984 respectively. Rain storm in 1983 is characterized by the great quantity of rainfall amount of 324 mm.comparing with the other storms.

According to hourly rainfall distribution recorded in July 1983 and August 1984 as shown in Fig.II.3.3, the maximum hourly rainfall in a range of 10 to 25 mm/hour is observed in 1983 and 1984 in the basin and those are seemed to be not intensive. Hourly rainfall records in 1978 and 1981 are not available in this study.

3.4 Tide Water Level

Tide water level at the Itajai harbor is shown in Table II.3.5. Mean monthly highest / lowest tide water level and mean tide water level are summarized as below:

- Mean monthly highest tide water level 1.01 m
- Mean monthly lowest tide water level -0.60 m

- Mean tide water level

0.20 m

The fluctuation of tide water level is in a range of around 0.8 m.

3.5 Sedimentation

According to the sediment concentration records of suspended load in Table II.3.6 and Fig.II.3.4, the relation between flow discharge and suspended load is described by the following formula.

 $0s = 0.334 \ 0.1.651$

where, Qs: Suspended load (ton / day)

Q : Flow discharge (m3/sec)

Based on the above formula and daily mean discharge at Rio do Sul, Apiuna, Indaial, Ibirama and Brusque, the specific sediment loads are estimated to be 65, 113, 135, 59 and 30 m³/km²/year as shown Table II.3.7 respectively.

FLOOD RUNOFF ANALYSIS

4.1 General Procedures

In the Itajai river basin, there exists the Sul and the Oeste dams as a flood control dam. Besides, the Norte dam is under construction and the river improvement works along the reach of the Itajai river between Gaspar and Blumenau cities, and lower reach of Itajai Mirim river are under execution at present. DNOS has a dam construction plan for prevention of large scale flood such as serious flood in 1983 and 1984.

Flood runoff analysis aims at the following objects:

- to evaluate the flood scale of the past maximum flood,
- to grasp the retardation effect for flood peak discharge by existing dams, on-going dam and proposed dams, and
- to formulate probable flood discharge distribution under present condition and with flood control works proposed by this Study.

For establishing the above objectives, the following study on flood runoff analysis is needed so as to simulate flood hydrograph at major site in the Itajai river basin.

- modelling of the river basin and channel,
- construction of a river system model in which the river basins and channels are linked,
- rainfall analysis for determining the design rainfall duration, rainfall amount and pattern, and
- runoff calculation for the present river condition and with proposed flood control works using the river system constructed and results of rainfall analysis.

Fig. II. 4.1 shows the general procedures in flood runoff analysis.

4.2 Methodology

4.2.1 Simulation model

Probable flood discharge are estimated from probable rainfall using the storage function model developed in Japan because it is required to work out the flood hydrograph for evaluation of simulation of the retardation effect for flood control dams, river improvement works and other flood prevention facilities.

Detailed methods and procedures are mentioned as follows.

(1) Base point and sub-base point

Base point, which are evaluation point of flood probability, is decided at the river mouth of the Itajai river because this flood control plan objects to prevent from the flood occurring in the entire Itajai river basin.

Sub-base points which are the site for estimating the probable flood discharge are distributed at the following site.

- Before/after the confluence with the major tributaries
- Proposed/existing dam site
- Proposed/existing flood diversion site
- Beginning/ending point of river stretches divided from the flood control plan.

(2) Construction of river system model

The Itajai river basin and its river course are divided into subbasins and river channels taking into account the base point and subbase points.

River system model is a flow diagram of flood discharge in which subbasin and river channels are linked on the basis of topo-map of 1/50,000 for present condition and flood control plan.

(3) Flood runoff from sub-basin

Flood runoff from each sub-basin is estimated by means of storage function method. The basic formula of storage function method is expressed by the following equation.

S = KOP

dS/dt = (1/3.6) f.r.A - Q

Where, S: Basin storage (m3)

Q : Runoff from basin (m3/ sec)

K,P : Constants

t : Time (sec)

f : Runoff coefficient

r : Basin mean rainfall (mm/hr)

A: Catchment area (km2)

Constants of K, P and lag-time in the equation are initially estimated by means of the following empirical formula which are described by average river bed slope in sub-basin. And then, those are calibrated using the flood records.

 $K = 118.84 \cdot i0.3$

P = 0.175 i - 0.235

where, i: Average river bed slope.

In the study, lag-time in sub-basin is roughly estimated by the following empirical formula.

Tl = L / V

where, Tl: Basin lag-time (hour)

L : River length (km)

V : Flow velocity (m/sec)

V = 3.5 m/sec i> 1/100

V = 3.0 m/sec 1/200 < i < 1/100

V = 2.1 m/sec i < 1/200

i : Average river bed slope

(4) River channel model

River channel has a retardation effect for flood peak discharge due to the rise of water level in case that the river bed slope is gentle or that water level is affected by tidal effect.

The storage function of river channel is estimated from the river cross-section, river bed slope, and length using the non-uniform flow or uniform flow calculation method.

The basic formula of storage function is shown as follows:

S = K Q P

where, S: Storage volume (m3/sec.)

Q: Flood discharge (m3/sec.)

K,P : Constant

Lag-time of river channel model is estimated from the preceding empirical formula.

(5) River structure model

(i) Dam/reservoir

The retardation effect of flood control dam is simulated based on the relation between reservoir water level, storage volume and outflow from the spillway and outlet facilities using the following equation.

ds/dt = I - O

where, S: Storage volume (m3)

I: Inflow into reservoir (m3/sec)

O: Outflow from reservoir (m3/sec)

(ii) Floodway

Flood discharge just before the floodway site is distributed to the floodway and to the downstream reach from the floodway site based on distribution ratio which is expressed as follows.

R = (Qp - Qcp) / Qcp

where, R : Flood distribution ratio,

Qp : Flood peak discharge just before the floodway

site, and

Qcp : Discharge carrying capacity of the downstream

reach designed by flood control plan.

4.2.2 Runoff coefficient

Runoff coefficient for flood runoff (R) is examined at major water level gauging station using the rainfall and flood records.

R = (Flood runoff volume) / (Rainfall amount)

4.2.3 Base flow

Base flow for examining runoff coefficient is defined as the discharge just before flood occurs, and that for probable flood is determined from mean monthly discharge for the wet season.

4.2.4 Converting flood runoff to water level

It is needed to convert the flood peak discharge to water level at the major points along the Itajai river and its main tributaries for examination of simulation model which is able to evaluate the inundation during flood.

Rating curves for the conversion is used for the analysis in accordance with the following procedures:

- (1) The rating curve based on the results of discharge measurement is prepared.
- (2) For the site at which discharge measurement is not carried out, the rating curve is prepared by mean of uniform flow calculation based on the river cross-section, assuming that the roughness coefficient is 0.035 in river channel and 0.050 in the flood plain.

4.2.5 Rainfall analysis

(1) Basin mean rainfall

Basin mean daily rainfall is estimated by means of Thiesen's method. However, the daily records in Itajai do Norte river basin are available after 1977. But it is required for estimation of basin mean probable rainfall to use annual maximum basin mean rainfall more than 30 years. Therefore, the correlation analysis is carried out for grasping the relation between basin mean rainfall estimated by using the records in the Itajai do Norte river basin and rainfall except Itajai river basin. Results of correlation analysis is applied to estimation of basin mean rainfall before 1977.

(2) Basin mean probable rainfall

Basin mean probable rainfall is estimated by means of log-normal distribution method, Gumbel method and Pearson III type distribution method. The most suitable method among the above is applied for estimation of probable rainfall comparing the results with the plotting position by Thomas method.

(3) Duration time and pattern of probable rainfall

Design duration time and pattern of probable rainfall is decided on the basis of the observed rainfall duration time and patterns.

- 4.3 Results of Study
- 4.3.1 Simulation model
- (1) Basin division and river system model

The Itajai river basin having a catchment area of 15,221 km² and its river course are divided into 42 sub-basins and 26 river channels in consideration with the base point and sub base points as shown in Figs.II.4.2 and II.4.3. The Itajai river is also divided into 26 river channel which have a retarding effect for flood peak reduction judging from the river bed slope and shape of river cross section. Sub-basins and river channels are linked by the river system model for the flood routing as described in Fig.II.4.4.

(2) Runoff coefficient

Runoff coefficient is estimated from flood volume and rainfall amount. Flood volume is calculated from discharge hydrograph converted from water level by discharge rating curve. Fig.II.4.5 shows the discharge rating curves at major water level gauging stations which are made by DNAEE on the basis of results of discharge measurement. However, the discharge measurement records at high water level in each station are not sufficient. In this study, the discharge rating curves at high water level are checked by uniform / non-uniform flow calculation as sown in Fig.II.4.5. Table II.4.1 shows the flood peak discharges based on the DNAEE's and JICA's rating curves. As seen in the table, the difference except at Rio do Sul are less than 20 % against DNAEE's value and the rating curves are judged to be applicable. Rating curve at Rio do Sul gauging station are revised by JICA's curve based on uniform flow calculation.

Table II.4.2 shows the flood volume, rainfall amount and runoff coefficients of large floods recorded on Dec. 1978, Dec. 1980, Jul. 1983 and Aug. 1984. Runoff coefficient changes from 0.5 against rainfall amount up to 200 mm to 0.7 against rainfall amount more than 200 mm. From this result, it can be said that runoff coefficients are reasonable values and that rating curves are applicable for converting water level to discharge.

Fig.II.4.6 shows the relation between flood runoff depth and rainfall amount. As seen in the figure, the saturated rainfall which is turning point from preliminary runoff coefficient is 200 mm.

From the above, runoff coefficient in this simulation is modelled as below.

Runoff coefficient: 0.5 (R < 200 mm)

1.0 (R > 200 mm)

(3) Base flow

The Itajai river have wet and dry seasons and flood usually occurs in a wet season. Base flow in a wet season is considered to be large because of occurrence of frequent rainfall. The following table shows the monthly mean discharge and its specific discharge at the principle station.

Name of Station	Catchment Area (km²)	Monthly Mean Discharge (m ³ /sec)	Specific Discharge (m3/sec/km²)
Rio do sul	5,230	162.9	0.031
Indaial	11,491	347.2	0.030
Timbo	1,450	50.8	0.035
Taio	1,585	52.2	0.033
Ibirama	3,341	100.6	0.030
Ituporanga	1,461	58.8	0.040
Brusque	1,220	35.4	0.029
Mean			0.033

Base flow in sub-basin in the simulation model is estimated from the specific discharge of $0.033 \text{ m}^3/\text{sec/km}^2$.

4.3.2 Rainfall analysis

(1) Duration time of probable rainfall

Fig. II. 4.7 shows the relation against basin mean daily rainfall in 1978 and 1980, and mathematic average of hourly rainfall in 1983 and 1984. Rainfall more than 70 % of total amount falls within 4 days. Table II. 4.3 shows the basin mean annual maximum rainfall of 4 days / 7 days from 1951 to 1984. As seen in the table, the duration time of 7 days of the rain storm on December 1983 is abnormal and rain storm having a duration time of 4 days is normally occurred in the basin in consideration with the past rain storms.

Judging from the above mentioned, the duration time of 4 days are adopted as a design duration time of probable rainfall.

(2) Hourly rainfall distribution

It is not sufficient for estimation of basin mean hourly rainfall to use the Thiesen's method because the hourly rainfall availability is limited. However, the recorded hourly rainfall distribution as shown in Fig.II.3.4 is very similar in each rain storm. Therefore, the average of the recorded hourly rainfall pattern is adopted as a basin mean hourly rainfall in sub-basin for the rain storm in 1983 and 1984 in which hourly rainfall data are available. Hourly rainfall distribution for 1978 and 1980 flood is estimated from hourly records more than 50 mm of daily amount in 1983 and 1984 because of lack of hourly rainfall records and daily rainfall amount is calculated by thiesen method. Estimated hourly rainfall pattern in a day is shown Fig.II.4.8. Fig.II.4.9 shows the estimated basin mean hourly rainfall distribution in 1978, 1980, 1983 and 1984 floods. Hourly rainfall distribution of probable rainfall is worked out by multiplying the following enlarging ratio to recorded hourly rainfall distribution.

n = 4-day probable rainfall / 4-day observed rainfall
where, n : Enlarging ratio

(3) Probable Rainfall

Basin mean 4-day probable rainfall will be estimated on the basis of annual maximum basin mean rainfall which are worked out by means of Thiesen's method and the correlation analysis. Thiesen polygon and its weight are described in Fig.II.4.10. The frequency curve by means of Pearson III type distribution is shown in Fig.II.4.11, and probable rainfall and enlarging ratio are listed in Table II.4.4.

4.3.3 Formulation and Calibration of Simulation Model

Formulation and calibration of simulation model is carried out by using observed rainfall distribution and simulation model. In the calibration, storage function of all the sub-basins are changed by multipling the ratio as below.

 $K = a K_1$

where, κ_1 : Coefficient estimated by empirical formula. a : constant

Other factor and storage function of river channels are fixed in the study. Finaly, constants of strage function in sub-basins are taken up by multipling 1.3 times to the initial K-value estimated by the preceding empirical formula.

The storage functions of sub-basins and river channels are listed up in Tables II.4.5 and II.4.6, and the simulated and observed hydrographs are shown in Fig.II.4.12. The fitness of the model is considered to be sufficient judging from availability of hourly rainfall records. Fig.II.4.13 shows the result of non-uniform flow calculation and flood marks in 1983 flood. Judging from the results, the simulation model is able to express the hydrological characteristics in the Itajai river basin and is applicable for the flood control study.

4.3.4 Dam/Reservoir Operation Study during Flood

Dam and reservoir operation study is carried out for discharging the inflow into reservoir from dam smoothly. In this study, the following methods are examined.

- (1) Without flood control dam for evaluating the flood control effect of the existing dams against the floods.
- (2) Existing operation method with / without Norte dam

Existing reservoir operation method is mentioned as below.

- Conduit valves are fully opened in normal condition.
- All the valves are closed in principle, when rain storm is observed at dam site.
- All the valves are closed in principle, when reservoir water level is over 10 m depth from river bed.
- (3) All the conduit valves are closed, when discharge at Blumenau over 1,000m3/sec.
- (4) All the existing conduit valves are fully opened, and when reservoir water level is over the crest elevation of spillway, outflow from

spillway based on the rating curve is added to the discharge from the conduit valves.

- (5) Additional outlet for the Sul dam is installed since the existing conduits have small discharge capacity against a large flood such as in 1983. It is difficult for Oeste and Norte dams to install the additional outlet judging from topographic and geological condition. The feature of additional outlet is decided from the discharge capacity of 800 m³/sec at Ituporanga city.
 - Outlet tunnel diameter 6.7 m, 1 lane
- (6) Additional spillway gates to heighten the flood water level to the following maximum flood water level are installed. When reservoir water level is over maximum flood water level, outflow corresponding to inflow is discharged from spillway under the condition that all the existing conduit valves are fully opened.
 - Sul dam EL.406.2 m (3.8 m below dam crest)
 - Oeste dam El.362.4 m (1.8 m below dam crest)
 - Norte dam El.306.5 m (3.0 m below dam crest)

The above maximum water levels are decided by adding free board 1.5 m (concrete dam type 1.0 m) to wave height. The feature of spillway gates are as below.

- Sul dam Width 7.50 m @ 6 Nos.
- Oeste dam Width 7.55 m @ 10 Nos.
- Norte dam Width 12.4 m @ 20 Nos.

Fig.II.4.14 shows the flood peak discharges at major sites and flood hydrographs at Blumenau city. As seen in the results, the effect of the additional conduit and spillway gates are corresponding to the flood peak reduction less than 200 m³/sec at Blumenau and they are not effective for flood peak reduction considering the cost effectiveness. Flood peak discharge of method (1) to method (4) at Blumenau are summarized as below.

	F16	ood Peak Dis	oharoo /m³	/sog)
Method	1978	1980	1983	1984
(1)	2,920	4,310	5,930	5,730
(2) (without Norte dam)	2,770	3,890	5,100	5,170
(2) (with Norte dam)	2,260	2,930	5,070	4,220
(3)	2,480	3,110	5,060	4,340
(4)	2,490	3,360	4,850	4,620

In the above table, since flood pattern in 1978, 1980 and 1984 have the duration time less than 4 days, the retardation volume in the reservoir contributes to the flood peak reduction. In flood pattern in 1983 which has a large flood volume, the existing method is not so effective and method

(4) is better than existing one. However, the flood in 1983 seems to be abnormal case because its duration period lasts about 7 days, while majority of floods except 1983's flood have a duration time of 4 days. Therefore, the existing method is proposed in this study.

4.3.5 Probable Flood Discharge Distribution

Probable flood discharge distribution is worked out by the probable flood hydrographs estimated at the base point and sub-bases point by simulation study using the probable rainfall, and is studied under the present river condition with the Norte dam and under the existing reservoir operation method. And probable flood discharge without the existing flood control dams is examined for comparing the past flood records.

Fig.II.4.15 shows the probable flood discharge distribution without the existing flood control dams, which is selected as a maximum value comparing with flood peak discharge among four flood patterns in Table II.4.7. The probable flood peak discharge at Blumenau is compared with flood discharge converted from the water level records using rating curves based on the non-uniform flow calculation and shown in Fig.II.4.16. The estimated probable flood discharges are fit for the plotted flood records with return period more than 10 years. But the estimated values less than 10 years probability are greater than the observed flood. This difference is considered to be caused by the reason why the selected four flood patterns are greater than 2 years flood. From the mentioned, the results of this study is applicable for making the flood control plan.

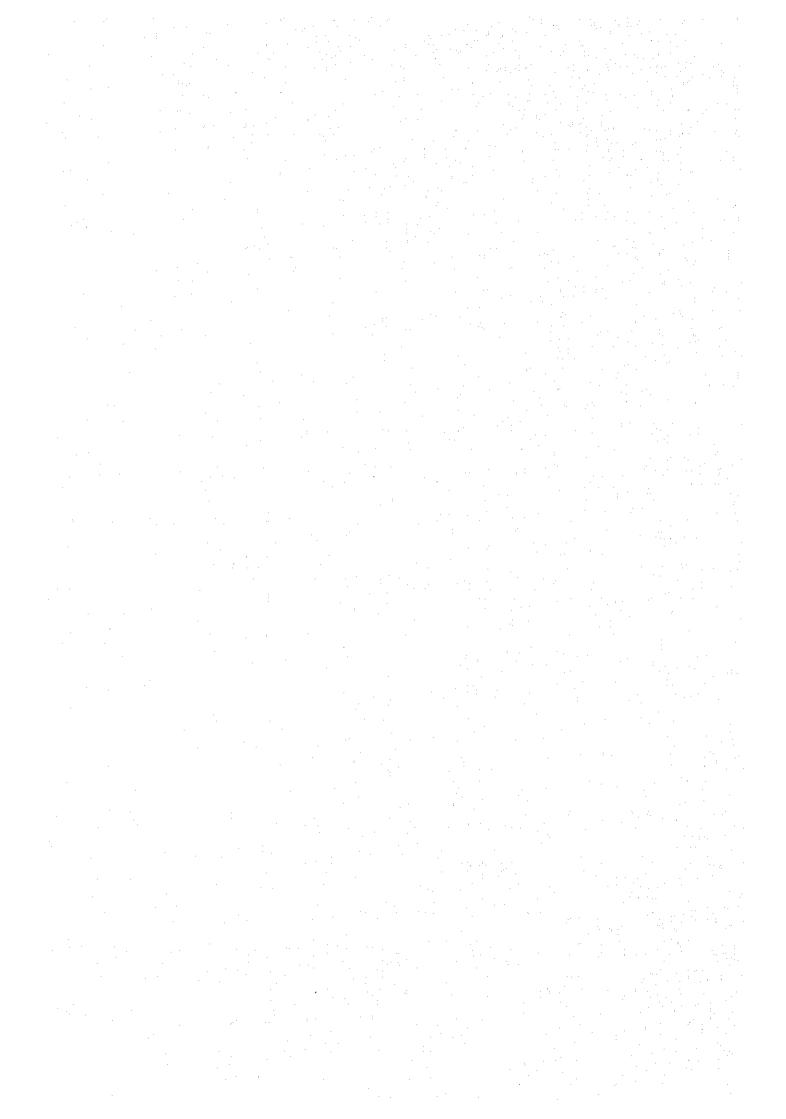
Fig. II. 4.17 and Table II. 4.8 show the probable flood discharge distribution and probable flood peak discharge of four patterns with the existing three dams.

Flood peak discharges at Blumenau with/without flood control dams are summarized as below.

	Peak Discharge (m3/sec								
Return Period	Without	With							
	F.C.D	F.C.D							
		<u> </u>							
2-year	3,300	2,300							
5-year	4,100	2,800							
10-year	4,700	3,200							
25-year	5,400	3,800							
50-year	6,200	4,900							
80-year	6,600	5,200							
100-year	7,000	5,500							

Note: F.C.D means the existing flood control dams.

From the above table, the flood peak reduction of 1,000 to 1,500 m3/sec is expected by the existing dams against the flood peak discharge without flood control dams. Fig.II.4.18 shows the probable flood hydrographs with/without the existing flood control dams.



Tables

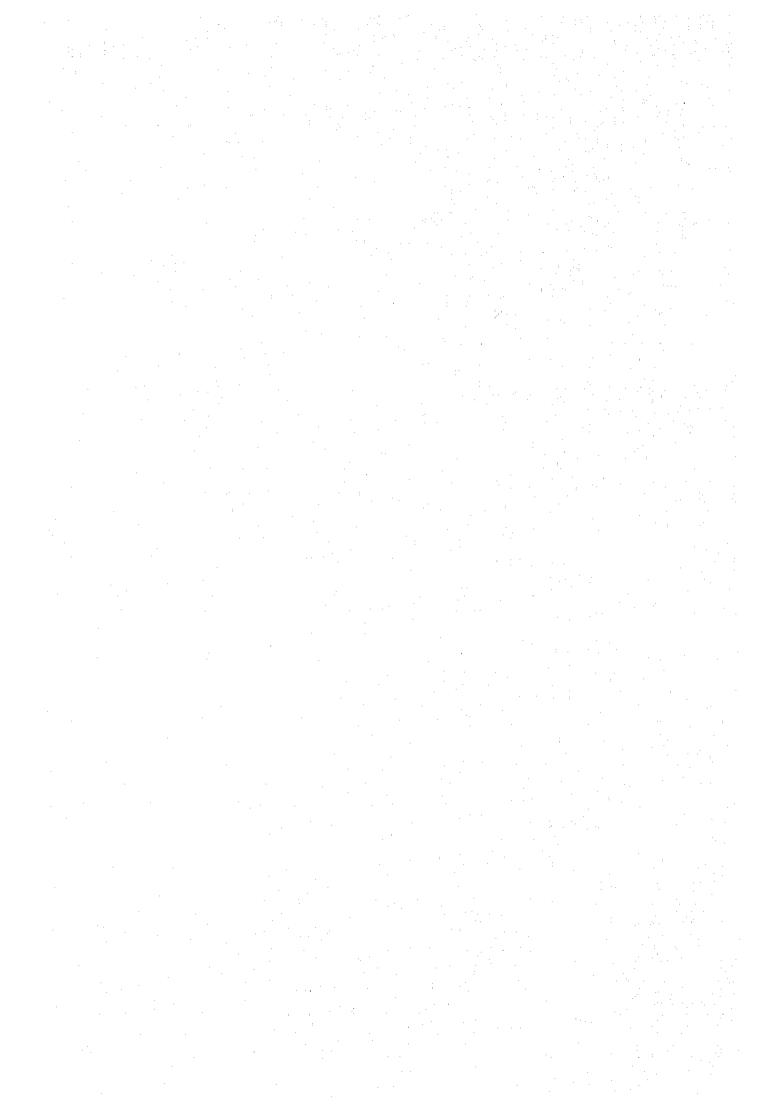


Table II.2.1 LIST OF METEOROLOGICAL OBSERVATORIES
IN AND AROUND THE ITAJAI RIVER BASIN

Name of Station	Observatin Period	Institution
Blumanau	1911-1969	INMET
Brusque	1911-1966	INMET
Camboriu	1912-1983	INMET
Curitibanos	1913-1958	INMET
Indaial	1971-up to present	INMET
Itajai	1980-up to present	EMPASC
Ituporanga	1979-up to present	INMET/EMPASC
Lages	1925-up to present	EMPASC
Timbo	1955-1969	INMET

Table II.3.1 MONTHLY METEOROLOGICAL DATA

(1) TEMPERATURE

Name of		:				•	;					. U	nit: ^O C.	
Station	Jan	Feb	Mar	Ąpr	May	Jun	Jul	Aug	Sep	Oct	NOV	Dec	Mean	
Indaial	24.5	24.7	23.8	21.0	18.9	15.6	15.8	16.9	17.9	20.1	21.8	23.8	20.4	
Itajai	24.0	24.6	22.9	20.2	18.2	15.3	15.4	15.9	16.7	19.2	21.5	22.9	19.7	
Ituporanga	22.8	23.4	21.9	18.8	17.0	13.8	13.2	14.6	15.2	17.7	20.2	21.8	18.4	:
Lages	20.3	20.1	18.8	15.8	13.1	11,2	19.9	12.2	13.7	15.5	17.4	19.3	15.7	
Timbő	25.5	24.4	23.3	20.9	17.5	15.7	15,5	16.6	18.1	20.4	21.9	23.2	20.1	
Ouritibano	s19.4	19.1	18.1	15.3	12.8	11.1	10.6	12.2	13.5	15.0	16.9	18.4	15.2	.1
Blumenau	24.5	24.4	23.2	21.0	18.1	16.3	15.5	16.4	17.9	19.6	21.5	23.4	20.1	
Brusque	24.4	24.1	23.2	20.5	17.8	15.7	15.1	16.0	17.6	19.3	21.2	23.0	19.8	
Camboriú	23.5	23.8	23.1	20.6	17.9	16.0	15.0	15.7	17.0	18.0	20.5	22.3	19.5	

(2) EVAPORATION

												Unit	: ma
Name of Station	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	0ct	Nov	Dec	Total
Indaial	97	75	71	. 67	63	50	57	59	61	79	89	94	868
Itajai	104	82	79	58	60	61	53	41	68	77	82	94	860
Ituporanga		_		_			_	-	***	_	٠ _	-	· . .
Lages	68	52	58	44	40	34	41	49	48	55	65	74	628
Timbo	104	86	76	64	59	44	50	58	57	77	90	97	863
Curitibanos	57	46	43	36	32	33	43	58	49	55	61	62	576
Blumenau	59	50	54	43	38	31	34	38	39	47	53	61	544
Brusque	75	58	63	45	41	34	38	40	37	50	62	68	716
Camboriu	83	72	73	64	58	46	50	55	58	73	74	91	797

(3) RELATIVE HUMIDITY

Name of													Unit: %
Station	Jan	Feb	Mar	Apr	May	Jun	Jul	· Aug	Sep	Oct	Nov	Dec	Mean
Indaial	73.7	77.7	76.7	77.7	77.4	79.5	80.2	77.6	77.8	76.7	75.1	73.9	77.0
Itajai	83.2	85.6	85.0	87.3	87.8	88.1	89.4	87.9	84.8	82.5	82.8	83.7	85.7
Ituporanga		-	_	-		-	-	-		-			. -
Lages	77.5	80.0	80.4	81.4	82.4	83.5	80.8	80.4	81.0	79.7	76.6	75.2	79.9
Timbó	79.4	81.4	83.4	84.3	85.1	86.6	86.9	84.9	85.3	82.8	80.1	80.2	83.3
Curitibanos	81.9	83.1	84.4	85.7	8526	85.7	82.8	80.0	82.5	81.4	78.7	79.1	82.6
Blumenau	82.1	83.7	84.3	85.1	85.8	87.2	86.2	85.2	85.2	83.5	81.2	81.0	84.2
Banzone	83.1	84.3	848	86.1	86.5	87.4	87.2	86.5	86.9	85.7	83.9	82.8	85.4
Camboriú	85.1	86.1	86.5	86.8	87.5	88.3	88.1	87.9	87.6	85.8	84.5	84.3	86.5

Data Source: EMPASC

Table II.3.2 MONTHLY MEAN DISCHARGE (1/2)

						Du	e. nott Loma	1			٠.			Runoff
YEA	R Jan	Feb.	Mar.	Apr.	May	Jun.	noff (cms Jul.	Aug.	Sep.	Oct.	Nov.	Dec.	Mean	Dopth (mm)
Rìo do Sul	(Catch	iment are	ea : 5,23	O sq.km) 				:					
197	6 176.0	65.9	144.0	45.9	128.0	191.0	83.0	234.0	122.0	92.0	65.2	24.5	114.3	686.1
197	7 281.0	255.0	125.0	87.3	45.4	29.1	36.3	255,0	89.7	284.0	203,0	77.7	147.4	884.8
197	8 67.6	55.2	82.2	24.0	16.2		53.4	34.8	115.0	46.4	90.3		60.9	365.4
197	9 49.7				133.0		56.8	60.2			168.0		99.5	597.2
198	£		177.0	58.6	63.2	55.1	167.0		256.0				155.3	932.1
198		110.0			31.3	29.7	43.3		68.3			97.3	67.0	402.1
. 198		188.0		53.6	40.8	88.4	123.0	98.4	4 10 10			140.0	121.0	726.2
	3 190.0						939.0		216.0					1711.5
198		and the second second	107.0		110.0		174.0	504.0	159.0	178,0	176.0	0.001	165.2	991.7
198				120.0		1126	1000	212.7	100.4	104 1	454.0	100.0	4004	010.0
Mea	n 125.7	103.7		69.2	97.1	113.6	186.2	213.7	128.4	104.1	101.6	133.3	135.1	810.8
										:				
Indaial	(Catch	ment are	ea:11,49	91 sq.km	1)								,	1 1
107	6 353.0	1660	323.0	135.0	293.0	466.0	216.0	444 0	253.0	198.0	192.0	390 0	285.8	784.2
	7 460.0				93.7	70.9	95.2		163.0				280.5	769.8
	8 153.0					57.5	117.0		252.0	- F - 1			146.1	400.9
	9 107.0			110.0			142.0		196.0		4 7 4		188.9	518.5
	0 239.0						391.0		520.0			and the second second	333.3	914.8
	1 384.0					67.1	91.0		122.0				162.5	446.1
	2 110.0						315.0		131.0				273.4	750.4
	3 406.0							and the second second	503:0				562.8	1544.5
	4 216.0							1134.0					343.2	941.8
198	5 -	-	-			1.0	-	-,	-	-		-		-
Mea	n 242.8	217.5	244.7	136.9	213.9	179.0	411.5	423.3	273.6	293.8	334.6	346.7	286.3	785.7
						:							,	
Timbo	(Catch	ment are	aa 1 45/) sa kmi										
TITIDO	Calci	mon ar		ouj	100							•		
197	6 56.2	47.1	77.7	32.8	54.8	67.4	38.8	49.6	37.6	32.5	34.2	36,4	47.1	1024.2
197	7 54.7	49.1	61.4	52.8	25.9	18.0	15.1	27.0	19.2	91.5	56.1	36.5	42.3	919.4
197	8 32.8	40.0	57.4	16.7	11.6	12.6	16.1	19.4	35.0	24.8	26.8	45.7	28.2	614.2
197	9 17.6	14.5	18.2	24.0	65.5	23.2	24.9	18.6	28.4	77.8	72.3	49.6	36.2	787.7
198	0 43.7	53.2	55.5	29.9	20.4	17.9	53.9	55.8	56.0	52.4	54.6	105.0	49.9	1084.4
198	1 77.6	68.8	41.6	30.0	21.3	14.9	19.9	13.1	14.5	42.0	43.3	58.8	37.2	808.0
198	2 28.7	67.7	50.6	33.9	32.7	41.9	43.4	32.4	23.0	50.6	87.1	52.8	45.4	987.4
198	3 72,5	77:1	87.7	46.3	116.0	91.9	240.0	86.9	81.2	61.2	43.8	81.2	90.5	1967.9
198	4 42.2	35.4	48.7	41.1	40.1	45.9	39.7	139.0	51.7	46.1	70.4	31.1	52.6	1144.4
198	5 -	•			- 1.	4.5	- :	:		•	•	-	- '	-
Mea	n 42.6	45.3	49.9	30.8	38.8	37.1	54.6	49.1	38.5	53.2	54.3	55.2	47.7	1037.5
Ibirama	(Catch	ment are	a :3,341	sq.km)										
		00.5	60.0		00.0	440.0	57 A	4400	: 00.0	- 4	04.0	04.0	70.0	694.5
197			63.9	37.2		142.0	57.0	116.0	80.9		64.0		73.6	
	7 105.0		62.0	65.2	20.1	14.7	21.9	60.8			79.6		57.6	543.8
197.			61.2	12.6	10.1	14.5	41.2	35.8		41.0	43.6	80.4	37.9	358.0
197			15.4		151.0	40.6	49.7	39.5			138.0		76.6	723.2
198			1.06.0	39.6	35.3	40.5	167.0	166.0		87.7		205.0	99.9	943.4
198				25.4	20.7	17.9	24.3	20.7	31.3	42.5	48.9	99.9	40.2	379.1
198			58.6	33.6		91.9	124.0	70.9			233.0		89.3	843.0
198		117.0			222.0		653.0	154.0		87.6	50.0	85.7 40.4		1598.2
198			59.7	41.8	D1.4	105.0	79.2	259.0	81.7	76.6	97.2	40.4	80.4 -	759.2
198		41.9	62.5	34.8	62.4	74.2	135.3	102.5	76.4	99.4	92.8	97.4	80.5	760.2
Mea	ii 30.1	41.9	02.3	. 34.0	76.4		100.0	104.3	, 0.4	33.4	J4.0	J/ .4	00.0	

Table II.3.2 MONTHLY MEAN DISCHARGE (2/2)

										Runoff				
YEAR	Jan.	Feb.	Mar.	Apr.	May	Rur Jun.	noff (cms Jul.) Aug.	Seo.	Oct.	Nov.	Dec.	Mean	Depth (mm)
		:			171217	yun.	VUI.	nug.			. INOV.		100001	<u> </u>
Ituporanga	(Calchn	nent area	1 :1,461	sq.km)						100			* **	
1976	55.6	16.0	32.9	11.8	41.0	46.3	31.9	86.1	31.8	23.5	22,7	63.9	38,6	833.7
1977	64.5	103.0	22.7	22.9	10.0	7.9	12.0	88.8	31.2	66.7	75.7	23.5	44.1	951.3
1978	23.8	27.7	23.9	6,8	5,5	6.5	12.8	8.7	30.7	15.0	22.0	36.3	18.3	395.2
1979	16.0	11.7	8.5	11.3	23,6	15.4	14.8	24,5	19.7	128.0	48.6	34.2	29.7	641.0
1980	31.1	16.8	41.2	15.5	17.2	12.6		116.0	81.6	43.0		100.0	45.5	
1981	63.5	29,6	12.8	10.0	.8.2	8.9	16.0	11.0	18.7	26.1	15.6	16.1	19.7	425.4
1982	8.5	34.1	15.7	7.8	7.3	23.5	26.3	23.2	12.5	49.1	96.5	37.8	28.5	615.7
1983	42.2	42.4	54.2	42.4	101.0	121.0	309.0	157.0	64.7	29.7	31.2	67.1	88.5	1910.1
1984	33.4	19.3	17.3	20.4	24.4	68.2	82.4	193.0	57.7	45.4	36,9	28.7	52.3	1128.0
1985	-	-	-	-	-	-		•	-				-	-
Mean	33.9	30.1	22.9	14.9	23.8	34.5	60.6	78.7	38.7	47.4	42.2	45.3	40.6	875.9
Taio	(Catchn	nent area	a :1,585	sq.km)										
1976	63.7	30.7	57.5	16.4	49.7	76.5	23.7	56.8	42.5	34.7	29.0	86.7	47.3	941.6
1977	110.0	57.2	59.8	37.6	12.9	9.6	10.9	74.8		119.0	50.0	25.0	49.5	983.9
1978	24.2	16.8	37.0	7.8	4.9	6.3	20.4	15.0	41.2	26.7	27.6		22.2	442.4
1979	14.6	10.4	25.0	19.4	81.2	22.8	22.1	24.1	33.1	132,0	61.4	54.1	41.7	829.4
1980	34.9	20.1	93.2	17.1	19.9	20.2	60.0	95.6	79.8	50.0	36.8	120.0	54.0	1073.7
1981	63.7	50.5	16.9	15.9	10.5	10.2	13.6	12.7	29.3	25.8	26.5	44.2	26.7	530,2
1982	18.2	97.5	59.3	27.1	22.6	43.5	57.6	39.9	23.1	69.9	152.0	60.8	56.0	1113.4
1983	90.1	97.5	87.4	41.9	126.0	113.0	332.0	122.0	77.1	50,9	47.0	64.0	104.1	2070.7
1984	34.6	24.6	52.2	39.7	49.4	68.6	35.8	156.0	43.8	55.1	78.7	37.9		1121.5
1985		-	~	-	-	-	-	-	-	-	-	: -	-	-
Mean	45.4	40.5	48.8	22.3	37.7	41.2	64.0	66.3	44.1	62.7	56.6	59,1	50.9	1011.9
Brusque	/ Catchn	nent area	1 220	l en kml										4.
			1.							;				
1976	47.6	28.5	37.0	20.0	40.5	51.0	36.3	58.4	29.4	22.5	27.2	31.2	35.8	925.4
1977	38.5	55.4	27.1	25.6	12.3	9.2	10.7	51.0	29.0	63.8	53.3	26.2	33.5	866.1
1978	25.3	21.2	22.5	9.5	8.1	10.3	12.6	8.8	22.8	17.8	18.6	38.2	18.0	464.6
1979	14.3	12.3	10.2	23.7	31.8	15.7	14.9	12.8	22.9	61.7	35.7	22.7	23.2	600.3
1980	20.9	16.9	24.7	19.3	12.6	10.7	31.4	47.0	40.1	36.3	30.1	62.2	29.4	758.7
1981	34.3	23.3	21.4	16.1	13.2	12.3	13.1	10.9	11.1	33.0	23.9	28.6	20.1	519.6
1982	16.9	43.9	25.0	19.8	17.2	23.2	22.8	20.7	15.0	28.7	49.1	25.5	25.7	663.0
1983	52.9	50.1	57.8	37.4	83.8	66.7	197.0	83.3	54.7	36.5	30.7	59.2	67.5	1745.0
1984 1985	38.0	33.7	27.7 -	22.7	22.6	30.4	30.8	-	47.0	43.0	43.3	27.1	30.5 -	789.0
Mean	28.9	28.5	25.3	19.4	24.2	25.5	41.1	32.5	30.2	38.1	34.7	35.7	31.5	814.6

Table II.3.3 RECORDED ANNUAL MAXIMUM DISCHARGE AT INDAIAL

Year	Date	Flood Discharge (cms)		Year	Date	Flood Discharge (cms)
Risk transport to temporary (1994) Pla	The second secon		•			
1934	Apr.26	1,037		1971	Jun. 9	2,356
1935	Sep.24	2,684		1972	Aug.28	2,340
1936	Aug. 6	1,913		1973	Aug.29	2,900
1937	Oct.16	1,279		1974	Jan. 9	1,244
1938	Jun.27	1,995		1975	Oct . 2	2,980
1939	Nov.26	2,590		1976	May.29	1,830
1940	Aug.26	1,256		1977	Nov.12	1,995
1941	Nov.18	996		1978	Dec.26	2,830
1942	Feb.20	1,410		1979	Oct. 9	2,308
1943	Aug. 3	2,220		1980	Dec.21	3,700
1944	Mar.14	645		1981	Dec.23	1,197
1945	Feb.20	849		1982	Nov.15	1,920
1946	Feb. 2	1,755		1983	Jul. 9	4,791
1947	Oct.26	1,256		1984	Aug. 7	5,026
1948	Aug. 2	2,372		1985	Jun.16	1,380
1949	Jun.12	760			•	
1950	Oct.17	2,308			•	
1951	Oct.19	1,545			•	
1952	Sep. 7	1,332				. "
1953	Nov. 1	2,724				٠
1954	May.18	1,845				
1955	May.19	3,060				•
1956	Sep.20	1,079				
1957	Aug.18	5,468				
1958	Mar.19	1,545		-	•	
1959	Sep. 2	1,126			•	
1960	Aug.18	1,425				•
1961	Nov. 2	2,468				
1962	Sep.20	1,740				
1963 1964	Sep.29	2,010 795			•	
1965	May. 2	1,965	-			
1965	Aug.21 Feb.10	2,180				
1967	Feb. 27	1,256				
1968	Dec.25	760				
1969	Feb.20	1,560			•	
1970	Jul. 2	1,338		•		
1910	VUL. Z	- F 5 5 5 C				•

Table II.3.4 PAST LARGE FLOOD WATER LEVEL AT BLUMENAU

	Year	Date	Water Level (m)	:	Year	Date	Water Level (m)
NAME	1000000000000000000000000000000000000	And the state of t	<u> سرچه دخیمه بی سب به ماه های ماه</u>		White the state of		too and additional and a second
	1852	Nov.16	16.00		1954	May 18	8.90
	1855	Nov.20	13.00		1954	Oct.22	11.84
	1864	Sep.17	10.00		1955	May.19	9.96
	1868	Nov.28	13.00		1957	Jul.21	8.68
	1869	Jul.22	11.00		1957	Aug.20	12.42
	1870	Nov.10	10.00		1961	Sep. 13	9.52
	1880	Sep.23	16.80		1961	Sep. 30	8.98
	1891	Jun.18	13.50		1961	Nov. 1	11.70
	1898	May. 3	12.00		1962	Sep. 9	8.64
	1898	Dec.24	11.00		1963	Sep.30	8.58
	1900	Jun. 2	12.50		1966	Feb. 13	9.42
	1911	Oct. 2	16.60		1967	Feb.18	10.20
	1911	Oct.30	9.56		1969	Apr. 6	9.00
	1925	May.15	9 80		1971	Jun. 9	9.50
	1925	May.24	10.00		1972	Aug.16	10.40
	1926	Jan.13	9.70		1972	Aug.29	10.65
	1927	Nov. 9	12.00		1973	Jun.25	10.55
	1928	Jun.18	11.46		1973	Jul.22	8.70
•	1928	Aug.15	10.52		1973	Aug.29	11.84
	1928	Sep.17	10.00		1975	Oct.3	12.15
	1930	Feb.16	9.05		1976	May.29	10.55
	1931	Apr. 1	10.90		1978	Dec.26	11.05
	1931	May. 2	10.44		1979	May.10	9.30
	1931	Sep.14	10.62		1979	Oct. 9	9.78
	1931	Nov.17	12.30		1980	Dec.22	12.95
	1932	May.25	8,90		1983	Mar. 4	9.95
	1933	Oct. 4	10.90		1983	May.20	12.06
	1935	Sep.24	10.60		1983	Jul.8-18	15.37
	1939	Nov.27	11.08		1983	Aug. 2	11.20
	1943	Aug. 3	9.82		1983	Sep.24	11.10
	1946	Feb. 2	8.80		1984	Aug.6-9	15.46
	1948	May.18	11.20				
	1950	Oct.17	8.80			•	* .
	1953	Nov. 1	9.30	•			

Source : " Bacia do Rio Itajai " , DNAEE

Table II.3.5 TIDE WATER LEVEL AT ITAJAI HARBOR

Monthly Highest Tide Water Level

	<u> </u>					Month						Unit	. El.m
Year	Jan.	Feb.	Mar.	Apr,	May	Jun,	Jul.	Aug.	Sep.	Oct.	Nov.	Dec.	Mean
5.00		5			1.00			31					
1983	100	10 miles		40.0		1.16	1.96	1.17	1.16	•	-	0.96	1.28
1984	1.02	0.88	- · · · · · ·	1.14	1.32	1.06	1.29	1.11	1.11	0.92	0.71	0.91	1.04
1985	0.81		-	- .		-	*	0.86	0.96	0.97	0.77	0.86	0.87
1986	0.62	0.77	0.91					1 1					0.77
	1.5				- 2	1000						400	

Monthly Lowest Tide Water Level

		<u> </u>				Month			100			Uı	nit . El.m
Year	Jan.	Feb.	Mar.	Арт.	May	. Սսո.	Jul.	Aug	Sep.	Oct.	Nov.	Dec.	Mean
					100			4	•				- :-
1983	1.1			12 3		-0.34	-0.14	-0.44	-0.44			-0.39	-0.35
1984	-0.44	-0.62		-0.54	0.20	-0.48	0.53	-0.49	-0.69	-0.74	-0.62	-0.49	-0.53
1985	-0.81			1	·		· · · <u>-</u>	-0.84	-0.95	-0.79	-0.94	-0.76	-0.87
1986	-0.64	-0.74	-0.79							•			-0.72
									4 C				

Mean monthly towest tide water level

Mean monthly highest tide water level

-0.60

Monthly Mean Tide Water Level

·					1.5	Month	4.	· .				Uni	it : El m
Year	Jan.	Feb.	Mar.	Apr.	May	Jun.	Jul.	Aug.	Sep.	Oct.	Nov.	Dec.	Mean
1983	•					0.44	0.73	0.34	0.28			0.13	0.38
1984	0.16	0.16	-	0.35	0.47	0.45	0.37	0.40	0.11	0.04	0.12	0.10	0.25
1985	0.03	-	÷ .					0.11	0.05	0.12	0.04	0.02	0.06
1986	0.06	0.09	0.01										0.05

Mean tide water level

0.20

Table 11,3.6 SEDIMENT CONCENTRATION RECORDS

(1) Apiuna			:	 (2) Barra d	lo Prata		
Date	Gage Helght (m)	Discharge (cms)	Sediment Concentration (ppm)	Date	Gage Height (m)	Discharge (cms)	Sediment Concentration (ppm)
				يوسي واستعاده مستان والأواناية المستادة واليوان			
Mar.20 '81	0.58	62.3	49.9	May.19 '79	1,55	35.8	15.6
Jun.16	0.50	44.7	45,8	Mar.19 '81	0.97	8.0	109.0
Sep.21	0.58	56.2	37.8	Jun.9 '81	0.81	4.0	53.2
Dec.27	1.30	280.0	52.5	Sep.27	1.63	43.4	268.5
Jan.16 '82	0.58	64.6	29.9	Dec.26	1.48	28.8	18.9
dar.17	0.69	84.3	9.1	Jan.12 82	1.37	23,1	43.8
Sul.8	0.90	142.0	50.3	 Mar.23	1.50	28.3	93.3
Sep.8	0.85	129,0	35.8	Sep.15	1,18	14.9	44.2
Nov.19	1.90	553.0	31.6	Nov,31	2,03	89.0	49.2
Apr.25 '83	1.36	298.0	68.8	Apr. 29 83	1.35	24.1	22.4
Jun.22	1.58	344.0	39.1	Jun 29	1,94	61.5	16.4
Oct .21	1.12	208.0	180.9	Oct .23	1.88	62.0	251.3
Jan.20 '84	1.06	177.0	244.7	Jan.17 '84	1.20	14.5	108.4
Mar 2	1.48	317.0	144.0	Jan 22	1.26	16.5	138.5
Jul.21	1.50	351.0	56.5	Apr.23	1.30	19.4	18.1
Jan.25 '85	0.62	67.0	41.0	Jul.20	0.90	5,1	13.1
Oct.20	1.08	178.0	81.8	Jul.21	1.52	34.4	28.4
				Oct .17	1.26	17.7	18,4

(3) Brusque				(4) Rio do	Sul Nov	o .	
	Gage	Discharge	Sediment Concentration	Data	Gage	Discharge	Sediment Concentration
Date	Height	(ema)		Date	Height	(cms)	(ppm)
	(m)	(Cmis)	(ppm)		<u>(m)</u>	(6.113)	(13)10)
Apr.22 '77	1.31	19.5	23.7	Feb.26 79	0.87	22.3	91.2
Aug.29	1.47	27.0	46.0	May.5	1.68	82.4	25.1
Oct.19	2.36	71.6	183.1	Mar.17 '81	1.06	32.3	57.1
Aug.7 '78	0.98	7.8	20.2	Jun.11	1.06	32.3	65.9
Oct.6	1.05	10.1	29.3	Sep.23	1.68	82.4	35.1
Bec.8	1.21	15.8	53.0	Dec.10	1.40	57.7	54.7
Mar.8 '79	0.99	8.1	64.7	Jan 14 82	1.14	38.0	18.2
Feb.21 '81	1.41	24.0	159.7	Mar.24	2.22	122.0	90.2
May.12	1.09	11.9	44.2	Sep.9	1.45	62.7	176.8
Aug.24	0.99	7.9	78.1	Nov.22	3.72	303.0	58.4
Nov.27	1.14	. 11.8	43,7	Jan.24 '83	1.80	92.0	26.4
Feb.19 '82	1.54	32.0	253.0	Mar.15	1.17	43.3	32,9
Jun.ll	1.19	14.6	43.9	Apr.26	2.30	126.0	63.2
Aug.6	1.18	15.2	38.4	Jun.27	4.39	433.0	32.3
Oct.8	2.90	125.0	820.8	Jul.17	3.70	268.0	93.6
Dec.4	1.63	43.2	136.3	Oct .23	2.40	130.0	120,6
Dec.22 '83	2.28	81.2	203.9	Oct 9 84	5.70	522.0	324.3
Feb. 21 84	1.41	22.1	21.3	Jan.15 '85	1.08	34.3	70.1
May.12	1.26	15.9	42.8				,
May.25	2.30	64.7	169.1				
Nov.23	1.71	38.1	80.6				
May 23 '85	1.04	16.6	32.8	•			
λυσ. 25	0.78	9_0	23.6				

	Gage	Discharge	Sediment
Date	Height		Concentration
	(m)	(cms)	(ppm)
Oct 27 76	1.75	223.9	79.9
Dec.9	3.15	849.0	282.0
Dec.12	3.04	784.0	120,4
May .17 '77'	1.27	84.0	35.2
Sep.21	1.49	138.0	45.8
Nov.17 '78	1.26	82.0	23.2
Mar.17 '79 .	1.15	62.0	7.0
May.29	1.56	161.0	22.5
Mar.22 '\$1	1.30	90.0	57.8
Jun.17	1.16	72.0	62.8
Sep.20	1.06	50.0	37.5
Dec.5	1.47	140.0	37.5
Jan.9 '82	1,40	123.0	33.9
Mar.16	1.44	132.0	15.8
Sep.22	1.30	106.0	62.2
Nov.18	3.05	854.0	71.6
Apr.18 '83	1.98	312.0	105.3
Jun.18	2.40	485.0	113.8
Oct.20	2.10	348.0	104.2
Jan.18 '84	1.70	212.0	459.7
Mar.24	1.98	310.0	96.0
Jul.23	2.29	398.0	224.3
Oct .22	1 62	181.0	116.0
Jan.26 '85	1.26	70.5	86.1
Jan.11	1.45	135.0	109.4

		<u> </u>		Unit : Mil	lion cm)
		S	tatio	n	
Year	Rio do Sul	Apiuna	Indaial	Ibirama	Brusque
1976		0.74	1.20	0.13	0.04
1977	***	0.84	1.26	0.11	0.04
1978	0.12	0.29	0.49	0.07	0.02
1979	0.25	0.69	1.03	0.17	0.02
1980	0.47	1.17	1.64	0.20	0.03
1981	0.11	0.26	0.46	0.06	0.02
1982	0.29	0.73	1.11	0.15	0.02
1983	0.66	3.59	4.86	0.69	0.12
1984	0.56	1.30	1.95	0.20	0.02
1985	0.27			. -	-
Total	2.73	9.61	14.00	1.78	0.33
Mean	0.34	1.07	1.56	0.20	0.04
Catchment Area (km2)	5,230	9,487	11,491	3,341	1,220
Specific Sediment load (m3/km2/year	·	113	135	59	30

Table II.4.1 COMPARISON OF FLOOD PEAK DISCHARGE BASED ON RATING CURVES BY DNAEE AND JICA TEAM

Name of	Gage Height	Flood Peak	Discharge	Differ	ence
Station	(m)	DNAEE	JICA	(cms)	(%)
Dec. 1978		1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			
Rìo do Sul	6.80	720	700	20	(2.8)
Ibirama	4.43	1,010	1,070	-60	(5.9)
Apiuna	5.47	2,300	2,100	200	(8.7)
Timbo	6.46	560	470	90	(16.1)
Indaial	5.92	2,900	2,400	500	(17.2)
Brusque	7.58	550	490	60	(10.9)
Dec. 1980					
Rio do Sul	7.57	850	860	-10	(1.2)
Ibirama	7.30	2,480	2,950	-470	(19.0)
Apiuna	7.70	3,690	3,250	440	(11.9)
Timbo	7.28	690	590	100	(14.5)
Indaial	6.60	3,500	2,900	600	(17.1)
Brusque	5.45	320	290	30	(9.4)
Jul 1983					
Rio do Sul	13.28	1,970	2,560	-590	(29.9)
Ibirama	7.30	2,480	2,950	-470	(19.0)
Apiuna	8.64	4,310	3,900	410	(9.5)
Timbo	_	1.00	. —	-	-
Indaial	7.78	4,760	4,200	560	(11.8)
Brusque	7.54	540	480	60	(11.1)
		•			
Aug. 1984	• •		1:	4	
Rio do Sul	12.80	1,860	2,370	-510	(27.4)
Ibirama	6.56	2,070	2,430	-360	(17.4)
Apiuna	8.66	4,320	3,950	370	(8.6)
Timbo	8.26	860	800	60	(7.0)
Indaial	8.02	5,030	4,500	530	(10.5)
Brusque	- -	-			

Dete Flood Characteristic Stil dem Ceste dam Rio do Stil Dittens Apluna Timbo Incétial Brisage Catchedent area (eq.km) 1,290 860 5,230 3,44 9,487 1,490 11,491 1,220 Dete Catchedent area (eq.km) 1,290 860 5,230 3,44 9,487 1,490 11,491 1,220 Dete Catchedent area (eq.km)			-			Water Lev	el Gauging	Station			
Catchment area (eq.km) 1,290 860 5,230 3,341 9,487 1,450 11,491 1,22 Flood discharge (cms) 330 240 720 1,010 2,290 560 2,840 85 Flood clascharge (cms) 34,77 (44.2) (34.6) (44.6) (44.6) (48.1) (40.5) (45.9) Flood clascharge (cms) (34.7) (44.2) (34.6) (44.6) (44.6) (44.6) (44.6) (44.6) (48.1) (40.5) (45.9) Flood clascharge (cms) (32.0) (108.0) (108.0) (106.5) (102.9) (49.1) (40.5) (45.9) Flood clascharge (cms) (32.0) (108.0) (108.0) (108.0) (108.2) (102.9) (109.2	Date		eristic	ام ام	este dam	တ ဝ	Ibirama	Apiuna	Timbo	1	zus.
Flood discharge (cms) 330 240 720 11,010 2,280 560 69.8 465.5 56 8 Runoff depth (mm) 34.7 (442.0 181.0 149.0 369.5 69.8 465.5 56 8 Runoff depth (mm) 32.0 92.9 92.9 181.0 149.0 36.9 179.0		Catchment area	(sq.km)	O	· (o	ന	3,341	4,	, 45	11,491	1,220
Flood discharge (cms) 330 240 1720 1,010 2,230 64.6 5.5 56 Runoff depth (mil. m3) 44.7 38.0 136.0 144.6 108.9 1.254.8 2.5 56 Runoff depth (mil. m3) 22.0 0 22.9 2.9 37.3 1 16.0 1 10.0									 -		
Flood volume	1978		(cms)	330	240	720	1,010	2,290	560	2,840	550
Nuncif depth	Dec.		(mil. m3)	44.7	38.0	181.0	149.0	369.5	8.69	465.5	10
Beain mean rainfall (mil. m3) 120.0 92.9 508.9 387.6 1,00.4 178.2 125.8 176.5 Rainfall amount trainfalt (mm) 0.37 (106.0) (106.5) (105.9) (109.2) (144.3 Runoff coefficient (mm) 680 660 680 2,500 3,690 690 3,500 <t< td=""><td>25-31</td><td>Runoff depth</td><td>(mm)</td><td>7</td><td>•</td><td>4.</td><td>4,</td><td>80</td><td>(48.1)</td><td>(40.5)</td><td>G</td></t<>	25-31	Runoff depth	(mm)	7	•	4.	4,	80	(48.1)	(40.5)	G
Rainfall amount (mm) (93.0) (108.0) (37.3) (116.0) (106.5) (122.9) (149.2) (144.2) Plood discharge (cms) 680 660 680 2,500 3,690 690 3,500 3 Plood discharge (cms) 680 660 680 2,500 3,690 690 3,500 3 Plood discharge (cms) 73.5 1,677.7 20.5 7,44,4 13.12 - 5.4 Runoff depth (mm) 7,15.7 20.21 204.6 904.8 528.2 1,577.7 250.6 - 170 Runoff depth (mm) 1,15.7 20.4 0.44 0.43 0.55 - 170 Runoff coefficient (mm) 1,470 940 1,730 2,480 4,310 - 4,740 5 Flood volume (mil.m3) 284.0 1,730 2,2480 4,310 - 2,564.2 2,564.2 2,564.2 2,564.2 2,564.2 2,564.2 2,564.2 2,564.2			(mil. m3)	\sim	c.	508,9	387.6	٠ <u>و</u>	178.2	1254.8	ι'n.
Flood discharge (cms) 680 660 660 875 87			(mm)	'n	98	7	v.	90	N.	(109.2)	Δ, ω
Plood discharge (cms) 680 660 680 2,500 3,690 690 3,500 5		Runoff coefficient		0.37	\circ	0.36	0.38	O	0.39	0.37	0
Flood discharge (cms) 680 660 660 2,500 3,690 690 3,500 3,500 590 5,500 5,500 5,690 690 3,500 5,690											
Plood discharge (cms) 680 660 680 2,500 3,690 690 3,500 5,50				8							
Flood volume (mil. m3) 94.8 137.1 395.8 326.7 744.4 131.2 - 54 Runoff depth (mm) (73.5) (159.4) (75.7) 97.8 (78.5) (90.5) - (44.9 Runoff coefficient (mm) (156.7) (237.9) (173.0) (188.1) (166.3) (172.8) - (137.9 Runoff coefficient (mm) (156.7) (237.9) (173.0) (188.1) (166.3) (172.8) - (137.9 Flood discharge (cms) 1,470 940 1,173.0 2,480 4,310 - 2,564.2 (237.8) Runoff depth (mm) (220.2) (230.2) (224.3) (226.6) (236.5) (236.5) - (2233.1) (183.0 Runoff depth (mm) (mm) (220.2) (230.2) (224.3) (226.6) (236.5) (236.5) - (2233.1) (183.0 Runoff depth (mm) (mm) (365.2) (320.2) (224.3) (326.3) (345.3) - (346.3) (338.4 Runoff cefficient (mm) (mm) (136.2) (323.9) (361.2) (326.3) (346.3) (365.3) (365.2) (326.3) (365.3) (365.3) (365.3) (365.3) (365.3) (366.2) (324.2) (366.6) (224.2) (220.3) (260.6) (224.2) (260.6) (224.2) (260.6) (1980	Flood	(cms)	680	099	680	2,500	3,690	069	0	320
Runoff depth	Dec.	Flood v	(mil. m3)	94.8	137.1	395.8	326.7	744.4	131.2		54.8
Basin mean rainfall (mil. m3) 202.1 204.6 904.8 528.2 1,577.7 250.6 - 170 Rainfall amount (mm) (156.7) (237.9) (173.0) (158.1) (166.3) (172.8) - (139.9 Runoff coefficient (mm) 284.0 198.0 1,77.0 2,480 4,310 - 2,564.2 223 Runoff depth (mm) (220.2) (230.2) (224.3) (226.6) (236.5) - (223.1) (183.0 Basin mean rainfall (mil. m3) 471.1 278.6 1,889.1 1,090.2 3,275.9 - 3,979.3 412 Runoff depth (mm) (365.2) (323.9) (361.2) (326.3) (345.3) - (346.3) (346.3) (365.2) (366.2) (3	19-28	Runoff depth	(mm)	(73.5)	· 🚓	(75.7.)	ς.	(78.5)	(30.5')		4
Rainfall amount (mm) (156.7) (237.9) (173.0) (158.1) (166.3) (172.8) — (139.9) Runoff coefficient 0.47 0.67 0.67 0.44 0.62 0.50 — (139.9) Flood discharge (cms) 1,470 940 1,970 2,480 4,310 — 4,740 5 Flood volume (mil. m3) 2284.0 198.0 1,173.0 2,243.3 — 2,564.2 223.1 Runoff depth (mm) (220.2) (230.2) (226.6) (236.5) — (223.1) (183.0) Rainfall amount (mm) 365.2) (323.9) (361.2) (326.3) (345.3) (338.4 Runoff coefficient (cms) 2,450 1,130 1,860 2,070 4,320 860 5,030 Flood discharge (cms) 2,450 1,130 1,860 2,070 4,320 860 5,030 Flood discharge (cms) 2,450 1,130 1,130 1,130 1,130 1,130		fall	(mil. m3)	202.1	2	904.8	(7)	1,577.7	250.6	ı	r~
Flood discharge (cms) 1,470 940 1,970 2,480 4,310 - 2,564.2 223 1,740 2,243.3 - 2,564.2 223 1,173.0 2,243.3 - 2,564.2 223 1,173.0 2,243.3 - 2,564.2 223 1,173.0 2,243.3 - 2,564.2 223 1,173.0 2,243.3 - 2,564.2 223 1,173.0 2,243.3 - 2,564.2 223 1,173.0 2,243.3 - 2,564.2 223 1,173.0 2,243.3 - 2,564.2 223 1,173.0 2,243.3 - 2,564.2 2,233.1 1,830.2 1,889.1 1,090.2 3,275.9 - 3,979.3 412.3 880.1 3,275.9 - 3,979.3 412.3 861.2 3,275.9 - 3,979.3 4,232.0 3,275.9 - 3,979.3 1,233.9			(mm)	(156.7)	~	(173.0)	œ	(166.3)	(172.8.)	1	·on
Flood discharge (cms) 1,470 940 1,970 2,480 4,310 - 4,740 223		Runoff coefficient	: .	0.47	O	0.44	0.62	0.50	0.52		0.32
Flood discharge (cms) 1,470 940 1,970 2,480 4,310 - 4,740 5 Flood volume (mil. m3) (220.2) (230.2) (224.3) (226.6) (236.2 223 Runoff depth (mil. m3) (220.2) (230.2) (224.3) (226.6) (236.5) - (223.1) (183.0 Basin mean rainfall (mil. m3) (365.2) (361.2) (361.2) (365.3) (365.3) (365.3) (365.3) (366.2) (366.2) (3						: '					
Flood discharge (cms) 1,470 940 1,970 2,480 4,310 - 2,564.2 223 Runoff depth (mil. m3) 284.0 198.0 1,173.0 757.0 2,243.3 - 2,564.2 223 Runoff depth (mil. m3) (220.2) (224.3) (226.6) (236.5) - (225.1) (183.0 Basin mean rainfall mil. m3) 471.1 278.6 1,889.1 1,090.2 3,275.9 - 3,979.3 412 Rainfall amount (mm) (365.2) (361.2) (326.3) (345.3) - (346.3) (338.4 Runoff coefficient (cms) 2,450 1,130 1,860 2,070 4,320 860 5,030 Flood volume (mil. m3) 195.7 114.1 804.1 379.6 1,448.7 187.1 1,615.9 Runoff depth (mm) (151.7) (153.7) (113.6) (152.7) (129.0) (140.6) Basin mean rainfall mil. m3) 297.3 167.9 1,233.8 665.2 2,118.4 377.9 2,576.3 Runoff coefficient (mm) (230.5) (195.2) (235.9) (195.1) (222.3) (260.6) (224.2) Runoff coefficient (mm) 0.66 0.68 0.65 0.57 0.68											
Flood volume (mil. m3) 284.0 198.0 1,173.0 757.0 2,243.3 - 2,564.2 223 Runoff depth (mm) (220.2) (224.3) (226.6) (236.5) - (223.1) (183.0 Basin mean rainfall (mil. m3) 471.1 278.6 1,889.1 1,090.2 3,275.9 - 3,979.3 412 Rainfall amount (mm) (365.2) (361.2) (326.3) (345.3) - (346.3) (361.2) (362.3) (345.3) - (346.3) (361.2) (362.3) (36	1983		(cms)	1,470	940	1,970	ά.	4,310	•	4,74	W
Runoff depth (mm) (220.2) (230.2) (224.3) (226.6) (236.5) - (223.1) (183.0) Basin mean rainfall (mil. m3) 471.1 278.6 1,889.1 1,090.2 3,275.9 - 3,979.3 412 Rainfall amount (mm) (365.2) (323.9) (361.2) (326.3) (345.3) - (346.3) (388.4 Runoff coefficient 0.61 0.71 0.62 0.70 0.68 - (346.3) (388.4 Flood discharge (cms) 2,450 1,130 1,860 2,070 4,320 860 5,030 Flood discharge (mil. m3) 195.7 114.1 804.1 379.6 1,448.7 187.1 1,615.9 Runoff depth (mm) (151.7) (153.7) (153.7) (113.6) (140.6) 377.9 2,576.3 Rainfall amount (mm) (230.5) (195.2) (235.9) (199.1) (222.3) (260.6) (256.6) 0.53	Jul.		(m11. m3)	80	러	1,173.0	757.		1.	564.	223
Basin mean rainfall (mil. m3) 471.1 278.6 1,889.1 1,090.2 3,275.9 - 3,979.3 412 Rainfall amount (mm) (365.2) (323.9) (361.2) (326.3) (345.3) - (346.3) (338.4 Runoff coefficient (cms) 2,450 1,130 1,860 2,070 4,320 860 5,030 Flood discharge (cms) 2,450 1,130 1,860 2,070 4,320 860 5,030 Flood discharge (mil. m3) 195.7 114.1 804.1 379.6 1,448.7 187.1 1,615.9 Runoff depth (mm) (151.7) (153.7) (153.7) (129.0) (140.6) Basin mean rainfall (mil. m3) 297.3 167.9 1,233.8 665.2 2,118.4 377.9 2,576.3 Rainfall amount (mm) (230.5) (195.2) (235.9) (199.1) (222.3) (260.6) (224.2) Runoff coefficient (mm) 0.66 0.68 0.65 0.57 0.68	6-15		(mm)	ó	ö	(224.3)	9.			rd . t	3.0
Rainfall amount (mm) (365.2) (323.9) (361.2) (326.3) (345.3) - (346.3) (338.4) Runoff coefficient (coefficient (coefficien		Basin mean rainfall	(mil. m3)	4	S	1,889.1	060		1	979.	412
Flood discharge (cms) 2,450 1,130 1,860 2,070 4,320 860 5,030 Flood discharge (mil. m3) 195.7 114.1 804.1 379.6 1,448.7 187.1 1,515.9 Runoff depth (mm) (151.7) (153.7) (153.7) (153.7) (153.7) (153.7) (160.6) Basin mean rainfall (mil. m3) 297.3 167.9 1,233.8 665.2 2,118.4 377.9 2,576.3 Rainfall amount (mm) (230.5) (195.2) (235.9) (199.1) (222.3) (260.6) (224.2) Runoff coefficient (ms) 0.66 0.68 0.65 0.57 0.68 0.50		Rainfall amount	(mm)	65.	m'	(.361.2.)	6.3			6.	₹†.
Flood discharge (cms) 2,450 1,130 1,860 2,070 4,320 860 5,03 Flood volume (mil. m3) 195.7 114.1 804.1 379.6 1,448.7 187.1 1,615. Runoff depth (mm) (151.7) (132.7) (113.6) (152.7) (129.0) (140.6 Basin mean rainfall (mil. m3) 297.3 167.9 1,233.8 665.2 2,118.4 377.9 2,576. Rainfall amount (mm) (230.5) (195.2) (235.9) (199.1) (223.3) (260.6) (224.2 Runoff coefficient 0.66 0.68 0.57 0.68		Runoff coefficient		0.61	0.71	0.62	0.70	0.68	1	w	
Flood discharge (cms) 2,450 1,130 1,860 2,070 4,320 860 5,03 Flood volume (mil. m3) 195.7 114.1 804.1 379.6 1,448.7 187.1 1,615. Runoff depth (mm) (151.7) (132.7) (113.6) (152.7) (129.0) (140.6 Basin mean rainfall (mil. m3) 297.3 167.9 1,233.8 665.2 2,118.4 377.9 2,576. Rainfall amount (mm) (230.5) (195.2) (235.9) (199.1) (223.3) (260.6) (224.2 Runoff coefficient 0.66 0.68 0.57 0.68			*		-						
Flood discharge (cms) 2,450 1,130 1,860 2,070 4,320 860 5,03 Flood volume (mil. m3) 195.7 114.1 804.1 379.6 1,448.7 187.1 1,615. Runoff depth (mm) (151.7) (132.7) (113.6) (152.7) (129.0) (140.6 Basin mean rainfall (mil. m3) 297.3 167.9 1,233.8 665.2 2,118.4 377.9 2,576. Rainfall amount (mm) (230.5) (195.2) (235.9) (199.1) (223.3) (260.6) (224.2 Runoff coefficient 0.66 0.68 0.57 0.68								:			
Flood volume (mil. m3) 195.7 114.1 804.1 379.6 1,448.7 187.1 1,615. Runoff depth (mm) (151.7) (153.7) (113.6) (152.7) (129.0) (140.6 Basin mean rainfall (mil. m3) 297.3 167.9 1,233.8 665.2 2,118.4 377.9 2,576. Rainfall amount (mm) (230.5) (195.2) (199.1) (222.3) (260.6) (224.2 Runoff coefficient 0.66 0.68 0.57 0.68 0.50	1984	Flood	(cms)	2,450	1,130	•	2,070	4,320	860	- 8	
Runoff depth (mm) (151.7) (132.7) (113.6) (152.7) (140.6) Basin mean rainfall (mil. m3) 297.3 167.9 1,233.8 665.2 2,118.4 377.9 2,576. Rainfall amount (mm) (230.5) (195.2) (235.9) (199.1) (260.6) (224.2 Runoff coefficient 0.66 0.68 0.57 0.68 0.50	Aug.		(mil. m3)	195.7	114.1	\circ	379.6	1,448.7	187.1	615.	
ainfall (mil. m3) 297.3 167.9 1,233.8 665.2 2,118.4 377.9 2,576. int (mm) (230.5) (195.2) (235.9) (199.1) (223.3) (260.6) (224.2 (2010)) (200.6) (200	5-15		(mm)	F-1	(132.7)	ω,	13.	(152.7)	(129.0)	9.0	1
(mm) (230.5) (195.2) (235.9) (199.1) (222.3) (260.6) (224.2 ent 0.66 0.68 0.65 0.57 0.68 0.50 0.6		Basin mean rainfall		(/)	167.9	23	9	2,118.4	377.9	576.	١,
0.66 0.68 0.65 0.57 0.68 0.50 0.6		Rainfall amount	(mm)	\circ	(195.2)	in	ó	(223.3)	(260.6)	4.2	1
		Runoff coefficient		0.66	0.68	0.65	0.57	0.68	0.50	w	1

Table II.4.3 ANNUAL MAXIMUM BASIN MEAN 4 DAYS / 7 DAYS RAINFALL

			1	•		
Year	Date	4-day (mm)	Date	7-day (mm)	(7-day)- (4-day) (mm)	(4-day)/ (7-day) %
			_			
1951	OCT. 15	90	OCT. 14	145	55	62.1
1952	SEP. 3	87	OCT. 13	103	16	84.5
1953	OCT. 28	93	OCT. 27	101	.8	92.1
1954	MAR. 31	101	OCT. 16	1.37	36	73.7
1955	MAY. 16	115	MAY. 15	126		91.3
1956	SEP. 16	56	SEP. 14	94	38	59.6
1957	AUG. 16	118	AUG. 13	133	15	88.7
1958	MAR. 13	121	MAR. 13	152	31	79.6
1959	AUG. 30	88	AUG. 29	124	36	71.0
1960	JUL. 31	89	JUL. 30	97	8	91.8
1961	SEP. 9	138	SEP. 6	193	55	71.5
1962	SEP. 18	89	SEP. 17	100	11	89.0
1963	SEP. 26	138	SEP. 25	176	38	78.4
1964	APR. 28	57	OCT. 20	66	9	86.4
1965	AUG. 16	91	AUG. 16	104	13	87.5
1966	FEB. 9	121	FEB. 9	166	45	72.9
1967	SEP. 18	56	SEP. 18	86	30	65.1
1968	DEC. 22	103	DEC. 20	115	12	89.6
1969	FEB. 16	93	MAR. 30	110	17	84.5
1970	FEB. 2	69	FEB. 1	96	27	71.9
1971	MAY. 5	66	APR. 16	100	34	66.0
1972	AUG. 25	146	AUG. 22	165	19	88.5
1973	AUG. 26	108	AUG. 22	149	41	72.5
1974	JUL. 22	99	JUL. 19	115	16	86.1
1975	SEP. 30	102	SEP. 27	127	25	80.3
1976	MAY. 26	90	MAY. 23	108	18	83.3
1977	AUG. 15	125	AUG. 13	137	12	91.2
1978	DEC. 25	118	DEC. 24	122	. 4	96.7
1979	MAY. 7	106	MAY. 8	141	35	75.2
1000	DBC 10	161	DEC 10	164	1 2	92.1
1980	DEC. 19	151	DEC. 18 DEC. 21	102	13 3	97.1
1981	DEC. 21	99				86.5
1982	FEB. 3	96	FEB. 4	:111	15 108	
1983	JUL. 6	216	JUL. 6	324		66.7 82.2
1984	AUG. 5	213	AUG. 2	259	46	02.2

Table II.4.4 PROBABLE RAINFALL AND ENLARGING RATIO

	Return	Probable		Observed Ra	ainfall (mm)	
	Period	Rainfall	Dec.1978	Dec.1980	Jul.1983	Aug.1984	
_	(year)	(mm)	118	151	216	213	
	2	110	0.932	0.728	0.509	0.516	
	5	140	1.186	0.927	0.648	0.657	
	10	160	1.356	1.060	0.741	0.751	
	25	185	1.568	1.225	0.856	0.869	
	50	210	1.780	1.391	0.972	0.986	
	100	230	1.949	1.523	1.065	1.080	

Note : ∠1 Actual 4-day rainfall (mm)

Table II.4.5 STORAGE FUNCTION OF SUB-BASIN

Basin	Catchment	River	River Bed	Coeff. of S		Lag-time
NO.	Area	Length	Slope	Function		(hour)
La Managaria de La Carta de La	(sq.km)	(km)	وزيرنس فال <u>رشد و في استقار موجود شاها</u> الاستورار الاستورار	K	P	The state of the s
1	860.0	45.0	1/130	35.87	0.549	4.0
2	725.0	56.0	1/90	40.05	0.504	4.0
3	866.0	70.0	1/1,300	17.98	0.944	9.0
4	116.0	20.0	1/220	30.63	0.622	3.0
5	300.0	35.0	1/100	38.81	0.516	3.0
6	183.0	22.5	1/250	29.48	0.641	3.0
7	440.0	26.0		38.81	0.516	2.0
8	850.0	32.4	1/425	25.14	0.726	4.0
. 9	159.0	28.5	1/220	30.63	0.622	4.0
10	326.0	28.2	1/200	31.52	0.608	3.0
11	217.0	28.0	1/170	33.10	0.585	3.0
12	174.0	26.6	1/60	45.23	0.458	2.0
13	854.0	43.1	1/435	24.97	0.730	6.0
14	584.0	48.4	1/170	33.10	0.585	4.0
15	880.0	32.8	1/140	35.08	0.559	3.0
1.6	611.0	44.9	1/355	26.54	0.696	6.0
17	431.0	59.8	1/285	28.34	0.661	8.0
18	348.0	17.9	1/95	39.41	0.510	1.0
19	657.0	41.1	1/105	38.24	0.522	3.0
20	50.4	7.5	1/100	38.81	0.516	1.0
21	314.0	29.1	1/120	36.74	0.539	3.0
22	205.0	34.4	1/65	44.16	0.467	3.0
23	606.0	43.0	1/100	38.81	0.516	3.0
24	779.0	52.4	1/55	46.43	0.449	4.0
25	64.9	8.9	1/540	23.40	0.768	1.0
26	71.1	9.0	1/165	33.39	0.581	1.0
27	405.0	37.7	1/305	27.77	0.671	5.0
28	262.0	38.2	1/160	33.70	0.577	4.0
29	197.0	21.6	1/220	30.63	0.622	3.0
30	191.0	22.9	1/270	28.81	0.652	3.0
31	15.2	3.2	1/180	32.53	0.593	0.0
32	61.2	7.1	1/670	21.93	0.808	1.0
33	590.0	49.0	1/980	19.57	0.883	6.0
34	111.0	11.4	1/210	31.06	0.615	2.0
35	640.0	66.0	1/145	34.71	0.564	6.0
36	457.0	58.0	1/675	21.88	0.809	8.0
37	170.0	15.7	1/55	46.43	0.449	1.0
38	179.0	15.0	1/55	46.43	0.449	1.0
39	116.0	14.1	1/145	34.71	0.564	1.0
40	122.0	20.1	1/510	23.80	0.757	3.0
41	14.5	1.7	1/240	29.84	0.634	0.0
42	18.4	1.5	1/500	23.95	0.754	0.0
			-			

Total Catchment Area: 15,220.7 sq.km

Table 11.4.6 STORAGE FUNCTION OF RIVER CHANNEL

Name of Stretch	River	River Bed	Coeff.	of Storage	Function	Lag-time
	Length	Slope	K	P		Tl
	(km)					(hr)
IT1	7.6	1/12,000	21.519	0.704	Q < 1,000	1.0
111	•••		0.677	1.204	Q > 1,000	
IT2	11.7	1/12,000	27.915	0.749	Q < 1,000	2.0
200		,	0.581	1.307	$\tilde{Q} > 1,000$	
IT3	15.0	1/12,000	46.457	0.700	Q < 1,200	2.0
			0.329	1.398	Q > 1,200	
IT4	3.7	1/12,000	12.910	0.671	Q < 1,200	0.0
			0.403	1.160	Q > 1,200	
1T5	8.0	1/12,000	34.066	0.642	Q < 1,600	1.0
			0.512	1.211	Q > 1,600	
176	13.0	1/12,000	37.507	0.629	Q < 2,700	2.0
			0.662	1.140	Q > 2,700	
117	14.0	1/12,000	42.507	0.675	Q < 2,500	2.0
			1.307	1.120	Q > 2,500	
BTI	19.0	1/500	27.443	0.681	•	3.0
1T9	4.2	1/1050	6.261	0.669		1.0
IT10	18.0	1/1050	24.006	0.677		2.0
1711	4.0	1/2,500	6.479	0.683	Q < 2,500	1.0
			2x10-7	2.870	Q > 2,500	
IT12	42.0	1/100	9.239	0.711		3.0
IT13	22.0	1/5,000	29.626	0.740	Q < 800	1.0
			0.141	1.540	Q > 800	
Benedito river			0.000			
BN1	8.6	1/1,000	10.531	0.657		1.0
Itajai do Norte rive			0.000			
IN1	7.5	1/240	8.274	0.637		1.0
<u>Itajai do Oeste rive</u>			0.000			
101	6.0	1/5,000	14.853	0.738	Q < 200	1.0
			0.777		Q > 200	
102	15.1	1/5,000	15.801	0.745	Q < 800	2.0
			0.060	1.578	Q > 800	
Itajai do Sul river			0.000			• •
IS1	12.0	1/4,000	20.552	0.781	Q < 700	2.0
			0.060	1.648	Q > 700	20.00
IS2	13.0	1/1,000	12.898	0.669	2 4 000	2.0
IS3	3.4	1/600	5.262	0.683 1.190	.Q < 800	1.0
**			0.111	1.190	Q > 800	
Itajai Mirim river	0.4	1/10,000	0.000	0.805	Q < 100	1.0
IMI	8.4	1/10,000	11.309	2,032	Q > 100	1.0
TWO	8.4	1/2,300	7.515	0.735	Q < 200	1.0
IM2	0.4	1/2,300	0.001	2.341	Q > 200	1.0
TWO	9.2	1/2,900	0.201	1.559	Q < 200	1.0
IM3	9.4	1/2,300	0.077	1.740	Q > 200	1.0
IM4	13.4	1/2,600	2.403	1.087	Q < 200	2.0
TIMA	13.4	1,2,000	1.104	1.234	Q > 200	.,
IM5	9.0	1/2,000	0.966	1.211	Q < 200	1.0
Ttan	<i>9.</i> 0	1,2,000	0.250	1.466	Q > 200	4.0
Luiz Alves river			0.000	2,400	× , 200	
LA1	2.0	1/10,000	4.853	0.610	Q < 100	1.0
2222	,0	2,20,000	0.001	2.810	Q > 100	_,,

(km2) (km		1978 1980 1983 1984	1976 1980 1983 1984	1978 1980 1983 1984	1978 1980 1884	1978 1980 1983 1984	1978 1980 1983 1984
15,221 13,504 13,504 10,393 12,741 12,535							
13,504 10,393 12,741 12,741 12,555	3,120 3,100[3,190]	3,770 3,850 3,830	1016.4	4.810 4.9301 5.070 5.020	5.600 5.780 6.050 5.830	6.030 6.120/ 6.600	6.500 6.520 7.210 6.476
12, 393	2, 800 2, 930 2, 870 2, 930	3, 623 3, 550	4.070	0 17 0 039 5	5.350	5.6601 6.130	6.030 6.603
12,741 12,726 12,535	2, 870 3, 026 2, 685 3, 006	3, 750 3, 570	4, 230 4, 020	4,850, 4,730	5,710	5,530 5,890 6,190 5,560	5,970 6,260 6,670 5,870
12,726	2,950 3,180 2,840 3,070	4,000	4,550 4,010	5,240 4,520	050'9	6,400 6,180	6,840 6,680
12, 535	3,190 2,850 3,080	3,660 4,010 3,560 3,830	•	4,629	6,050 5,680	6,410 6,180	059 9 058 9
	3,210 2,840 3,080	4,040 3,560	4,610 4,030	5, 320 4, 630	6,120 5,670	6,480, 6,170	6,340 6,670
12, 338 2, 49	2, 450 3, 230 2, 830 3, 670			4,740 5,360 4,630 4,900	6,170 5,430 5,	6,530 6,130	6,990 8,630
157	1 32 40 56	48 48	98 84	56 72	54 80	72 88	72 104
F 93	1 18 21 32	21	39 25 32 50	46 28 43 57	35 50	35 50	39
tver 56.	7 21 14 20	1.7 1.7	52	20 . 26	31 23 28 40	34 26 31 43	37
12,076 2,94	3,240 2,820 3,050	4,090 3,540	4,670 4,010	5,380 4,610	6,180 5,590	6,530 6,020	095'5 066'3
12,671 2,80	2,860 3,150 2,750 2,970	3,990 3,450	4,550 3,910	4,490	6,540	٠	6,830 6,350
9, 24.5	2, 440 2, 690 2, 380 2, 590	3,390 3,000	3,860 3,400	4,450 3,920	5,170 4,580	5,500 4,940	5,890 5,300
2, 380	2, 380 2, 620 2, 350 2, 590	3, 310 2, 950	3,770 3,350	4,350 3,860	5,020 4,530	5,400	
9,581 2,30	2, 620 2, 340 2, 330	3, 330, 2, 970	3,310, 3,390	4,440 3,940	5,200 4,740	5,560 5,130	6,000 5,530
1713 5,570 1,360	1,380 1,250 1,640	1,730 1,750 1,580 2,040	ì	2,210	2,610 2,550	2,710 2,770 2,700 3,190	1
THI-THI	1000 1000 1000	000	01.0				
		2 0	,	077	30 520	780	
	200	001	200	130	210 160	0.1	332
IM3 1, 562 640	360	910	950	000	250	0 0 0	230
1,446	390 240	300	550 340	540	160 480	000	000
IMS 1,267	350 220	940	0.10	580 350	670 420	720 650	
22.0	160 110	210 140	240	280			550 750 230 7
(216)	(160) (110) (250)	(270) (210) (140) (380)	1691	(400) (280) (180) (520)	(310) (210)	(330) (320)	
BN1 1,521 440	440 440 350 410	540 500 520 550	646 700 600 650	750 246 720 780	870 980 1,000	960 1,040 5,130 960	0,01, 0,270 0,11,1 0,00,1
	1,010/1,250/1,130 980			630	616		
Norte dam 2,318 680			1,350 1,230	1.590	1.240 1.900 1.300	2 080 2 110	2017 000 7 000 7 000
(680)	(900) (830) (6	(1,170) (1,070)	(1,350) (1	(1, 580) (1,450) ((1, 900) (1, 920) (1, 360)	(2,080) (2,110) (1,420)	(2, 290) (2, 260) (3
101 3,050 869	840 7801 0001	1.5%0 1.320 1.500	1.00	480	1 750		0.00
\$65	150 140	190 180	210 210	240 230			310
300	30 70	100 90	120 110	140		170 270	08:
_	(80) (70) (1	(100)	(120) (210)	(140) (130)	(160)	(070) (070)	(180)
Trembude 116 40	00	0	20.	20	50 70	60	30
Carl (8)	(35) (36) (37)	(69) (69) (69) (69)	150) (40)	(05)	(20)	(60) (70)	(20)
2	(310) (320)	(400) (410) (4	(370) (460) (520)	(130) (540) (560)	(720) (670)	(500) (760) (760) (750)	(530) (910) (850) (790)
	673	1					
152 1.992 530	200	000 000 000 000 000 000 000 000 000 00	750 790 1 090 1 000	1,300	0 :	1,080	1,190 1,140 1,620 1,050
27,1	490 500	639 860	720	9401 1,320	à	1, 630	720 1 720
	370 440	1087	240	000	7367	2,010,1	000
[400]	(370) (440) (5	(470)	5	(630) (630) (1,120) (880)	0.2503	11.3701 (1.100)	(890)
	ij]

Note : ' () ' means outflow discharge from dam,

																		6	
8.0	Potchmont	27.0	1 = 4 × 1 × 1	10-vear	2	25-Vene	F 1 0 d	7	٦				, a	2000			1.00 ×	,	
İ	Area (Km2)	1978 1980 1983 1984	1978 1980 1983 1984	1978 1980 1983 1984	1978	. 1	1983 1984		3,61	1980 1983	3 1984	1978	13%	1983	7861	1978	1980	1983	1984
ITI	15,221	2,450 2,320 2,260 2,570	2,870 2,780 3,190	30 3,110	3,940	_ `	3,940 4,040			250 5,160	•	4,810		1.		\$,100	4,780	6,110	5,220
2 L	13,504	2,130 2,110 2,020 2,220	2,580 2,480 2,730	90 2,810	3,350						٠.	4,040			•	4,280	€, 200	5,580	4,360
	13,393	2,170 2,170 2,016 2,280	2,580 2,550 2,476 2,810	90 2 880	3,430		3,750 3,550				•	9				0,7,7	25.	5,610	6,470
TTS	12,726	2,190	2,770 2,39012,830	20 2.900	3.430							4.200				057	230	2	9 4
951	12,535	2,180	2,360 2,820	3,030 3,130 2,890 3,170	3,480	3,600	3,750 3,610		3,960 4,	4,010 4,90	32,7	917.7	4,280	3,210	4,260	4,420	4,550	5,510	4.4
121	12,338	2,160	2,760 2,320 2,800	30 2,890	3,450						1	4,150			Ĭ	7,390	4,550	5, 490	4.460
Garcia river	157	48 32 40	48 48 72	49 56	27							96			Ŀ	104	27	104	:28
Jichpava ziver	83	28 18	35 21 21 63		46					35 50		ß				57	39	7.	75
Velha zivez	98	17 21 14	=	20 71	56		.				أ	34				37	92	37	45
SEH	12,076	2,120	2,740	20 2,860	3,380						Ĺ.	4,060			Ľ	4,340	\$,520	5,420	4.410
113	11,671	2,030	2, 630		3,200	3,470 3	3,500 3,3		3,630 3,	3,890 4,70		3,830		_		4,110	4,350	5,270	6,170
1110	9,945		2,020	2,130 2,290 2,360 2,360	2, 430	٠	_					3,020				3,240	3,310	4,530	3,320
IT11	9, 631	1,510 1,590	1,940	2,040 2,190 2,310 2,280	2,320							2, 900			_	3,110	3 200	4,436	3,250
1712	135'6	1,330		2,020 2,170 2,300 2,270	2,300							2,900				3,110	3 200	4,450	3,190
1213	5,570	840 880 790 1,040	1,030 1,100 1,300 1,350]	2	1,320	╛	_		,600 1,	2,5	1,360	1,790		1		1,990	2,189	2,78	2,430
1M1+1M2	1,699	450 410 270 490	L	356 370	710	959		ig ig			1	873			1.	920	820	0.00	1096
IMI		130 120 901 140	160 150 100 170	120	200	180		8				240				6	240	90	260
IMS		290 190		400 260	850	39		É	230	250		903				929	5.50	30	1007
EKI	1,562	440 390 250	490 310	550 350	120	630						906				98	830	\$80	1,020
IMA	1,446	440 390 240	490 300	550 340	760	640	390		870	_	430 1,010	940		520		1,020	865	570	1.160
IMS	1,267	350	059	500 310	069	280						860				940	780	200	1,110
Milin dam	640	210 160 110 290 (210) (160) (110) (290)	(270) (210) (140) (380)	(320) (240) (160) (450)	400)	280 (280)		520	470 (470) (3	310 210	10 620	520	330	. 8	650)	550	350	230)	927
39.1	1,521	440 440 390 410	560 600 320 550	640 7001 600 650	750	840		٠.	:	֓֡֡֞֞֩֡֡֡֡֡֡֡	_ ا	940		Ľ	١	3,030	بيا	1.270	1,040
					1 (.,				H	. ,						1 1		
INI	3,369	540 570 520 510	640 680 620 610	700 760 690 680	770	860	. '					1,020				1,120	1,160	1,720	940
NOZE BID	מין מין	(220) (240) (260) (3	(260)	(250) (270) (320) (250)	(276)	لل	(500) (260)		(280) (3	(319) (350)	1,360	1,370	(325)	0.1.020	(280)	(300)	(330)	(3,245)	(280)
101	3,050	630 619 510 710		770	000		L	_	•		L	220	1	-		1097		5.00	1.550
102	565	150 140	190 180	210 210	250				230	280 280	60	310	1		\$30	970	310	340	100
Trombudo	300	80 70	100 30	120 110	82				_	_		140			270	150	180	180	290
dam (A)		(80) (70) (12	(100) (001)	(110)	(120)		_		_	160) (160		(140)			(270)	(150)	(380)	(180)	(250)
Trombudo	116	30	40 40	20 40	2		_		_	_	٠,	8			8	8	6	g S	110
(8) 1000		(40) (30) (30)	(00) (00)	(20) (40)	(10)			S :				(30)	ı		(96)	(86)	ê	(89)	
Odnica com	200	100	(0) (10) (180) (20)	(0) (180) (250) (50)	(40)	£ 66 8 69 100 100 100 100 100 100 100 100 100 10	(340) (110)	e e	490 (60)	510) (520)	0) (260)	(86)	(570)	67.5	(300)	0 (e : :	(670)	(630)	(370)
181	9 3 6 6	220 020 020	320 300	1,000	691	1	_	é	4	L		600		- 1	_	4	Ļ	1	,
152	1,992	150 200 470	260 840	240 250 1,030 370	450		1,240	510	230	390 1,420	101	840				9,6	5,0	1,56	1,150
183	1,775	110 140 450	180 800	210 980	430			80	700			810				900	8	1,470	1,050
Sul dan	1,290	(50) (50) (10 <u>50)</u> (50)	(100) (50) (710) (120)	\$50 \$40 900 750 (170) (90) (850) (200)	(350)	(10) 83 10)	1,120 s	580 350) (3	5	720 1,290	0) (600)	910 (690)	(300)	(1,210)	(700)	1,000	(350)	1, 270)	(800)

Note: ' () * means outflow discharge from dam.

Figures

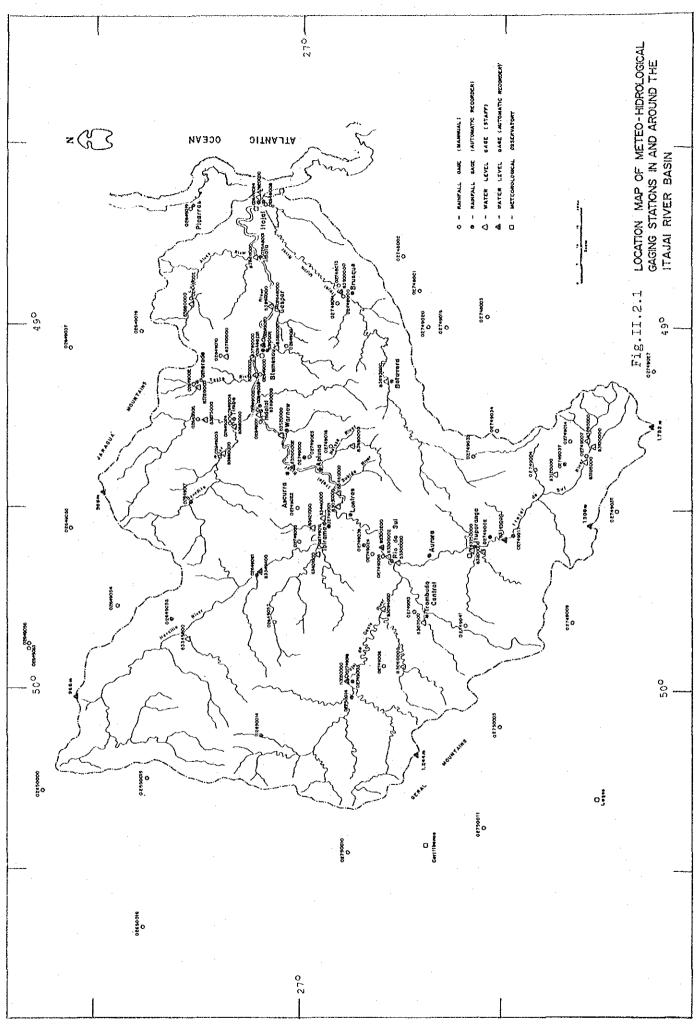


Fig. II.2.2 AVAILABLE DAILY RAINFALL RECORDS IN AND AROUND THE ITAJAI RIVER BASIN (1/2)

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Name of Station	ID. Number	Institution	Observation Period.
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Gaspar	02648000	01	▗▗▗▗▗▗▗▗▗▗▗▗ ▗ ▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗▗
Ilhota Luiz Alves	02648001 02648002	01	
Itajai	02648008	02	
Picarras	02648019	01	
Passo Manso	02649000	01	▕ ▗▕▕▕▗░░░░░░░░░░░░░░░░░░░░░░░░░░░░░░░░
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Pomerode	02649002	01.	▗▐▗▐▐▐▐▐ <mark>▜▜▐▜▜</mark> ▜▜▜▜▜▜▜▜▜▜▜▜▜▜▜▜₽₽₽₽₽₽₽₽₽₽₽₽
Bonedito Novo	02649003 02649004	01	
Timbo Indaial	02649005	01	
Blumenau	02649007	01	
Rio dos Cedros	02649008	01	
Garcia	02649009	0.1	
.Itoup Central	02649010	0.1	▗▗▎▗░░░░░░░░░░░░░░░░░░░░░░░░░░░░░░░░░░
Dr. Pedrinho	02649017	01	
Massaranduba Blumenau	02649019 02649020	02	
the second second	02649024	05	
Timbo Jaragua do Sul		01	
Indaial	02649038	05	
Witmarsum	02649053	01	
Itaiopolis	02649054	01	
Rio Negrinho Itaiopolis	02649055 02649056	01	
Barta do Prate		01	
Barragem Norte	02649061	02	
Itaiopolis	02649013	02	
Papanduva	02650000	01	
Rio do Campo	02650014	01	
Monte Castelo Santa Cecilia	02650015 02650016	01	
Brusque	02748000	01	
Major Gercino	02748001	01	
Nova Trento	02748002	ot -	
_ Angelina	02748003 .	01	
Brusque	02748014	05	
Brusque Indaial	02748015 02749000	01	
Ibirama	02749000	οί	
	02749002	01	
Taio	02749003	02	
Vilicedo Magner	ł .	01	
Nova Bremen Pouso Redondo	02749005 02749006	01	
Lomba Alta	02749007	01	
Rio do Sul	02749007	01	
Pres. Getulio	02749011	οî	
Tromb. Central	1	01	─────────────────────────────────────
Barracao	02749014	01	
Faz.Boa Esper.	02749015	01	
Neisse Central Barragem Sul	02749016 02749017	01	
Barragem Oest		01	
Rancho Queimad	o 02749020	01	
Ibirama	02749022	15	
Rio do Sul	02749024	15	
Apiuna Anitapolis	02749025 02749027	15 01	
Vidal Ramos	02749027	01	
Leoberto Leal	02749033	01	
Saltinho	02749037	oi .	
Rio do Sul Nov		01	
Agrolandia	02749041	01	
L.T. Instit		DNAEE	
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Fig. II.2.2

AVAILABLE DAILY RAINFALL RECORDS IN AND AROUND THE !TAJA! RIVER BASIN (2/2)

LI Period '65 '70 '75 '80 '8 Observation
'45 '50 Nome of Station 1D. Number Institution 02750003 01 hages. 02749009 02750010 01 Lages Curitibanos 01 Ponte Alta Bom Retiro 02750011 01 02749032 01 Institution DIDNAEE

FIG II.2.3 AVAILABLE HOURLY RAINFALL RECORDS
IN THE ITAJAI RIVER BASIN

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Indaial	02649038	0.5				111					! 				1 1 1 1 1 1 1 1 1
Barra do Prata	02649058	01			111	Ш				Ш	[[]]				
Barragem Norte	02649061	01	-		Ш	111									
Rio do Campo	02650014	01	-	[]]]]]]]]					1111			
Apiuna	02749000	01			Ш	Ш				Ш					
Ibirama	02749001	01	-		Ш	III		[[[[]	ШШ	[[[[[[[]]		!!!!!		
Ituporanga	02749002	01	-						1111]][]]				
Taió	02749003	01			Π										
Barragem Sul	02749017	01	i												
Saltinho	02749037	01	-		Ш			[11111	
Rio do Sul	02749039	01	1		111									11111	
Barragem Oeste	02749018	01			Ш	Ш	ШШ		Ш.						
lastitution	OI DHAEE						*****								
	OS INMET														

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Fig. II.2.4 AVAILABLE DAILY WATER LEVEL / DNSCHARGE IN THE ITAJAI RIVER BASIN (1/2)

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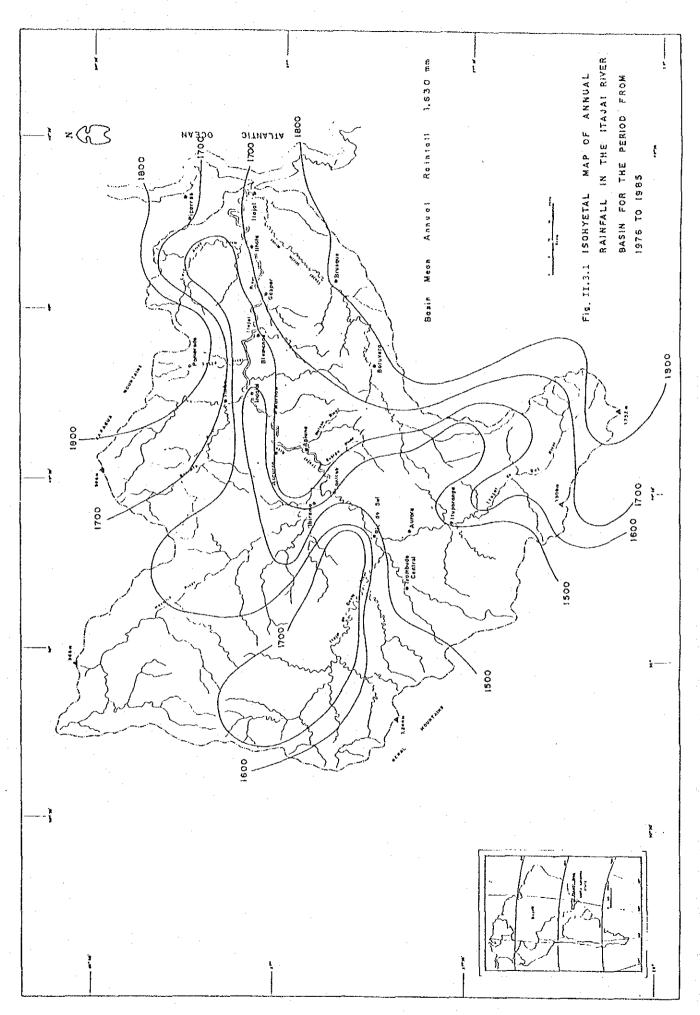
FIG. II.2.4 AVAILABLE DAILY WATER LEVEL/ DISCHARGE IN THE ITAJAL RIVER BASIN (2/2)

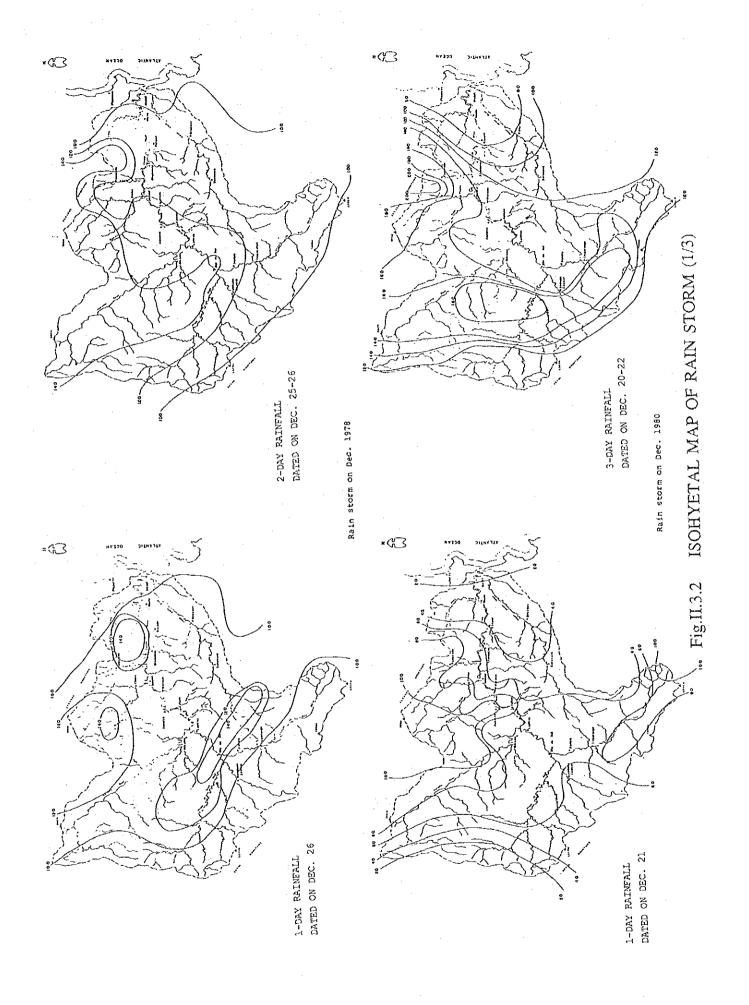
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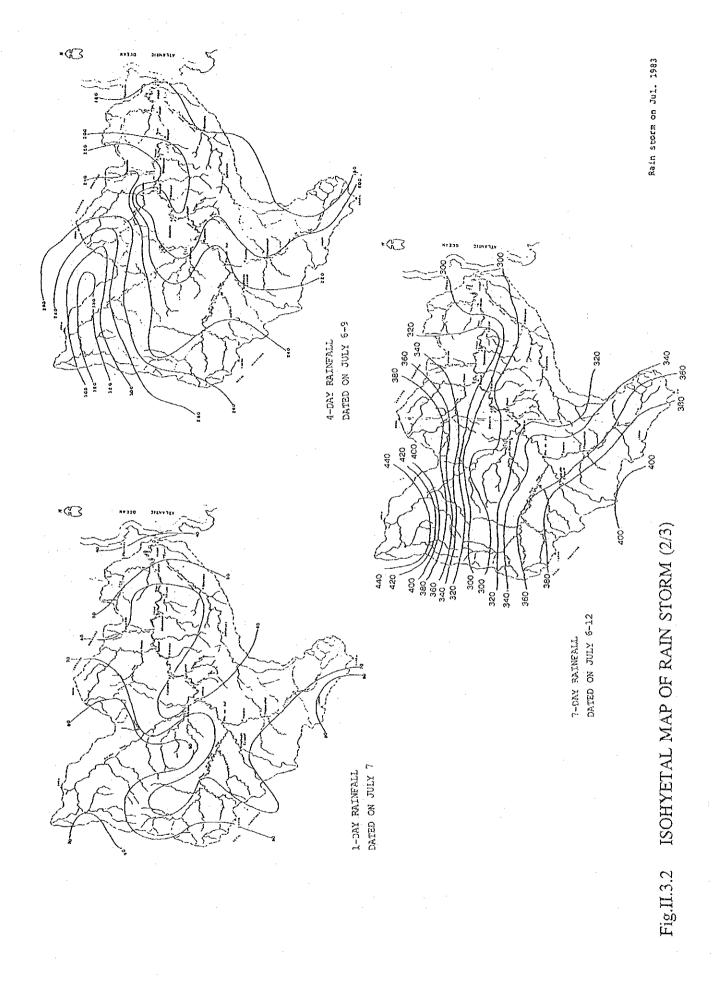
Fig. II.2.5 AVAILABLE HOURLY WATER LEVEL RECORDS
IN THE ITAJAI RIVER BASIN.

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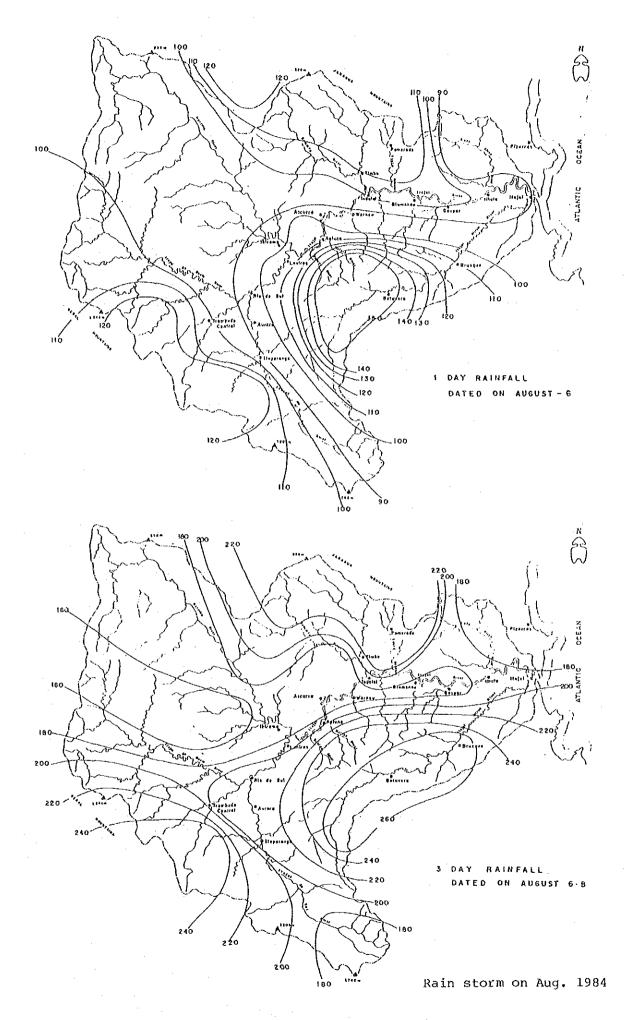
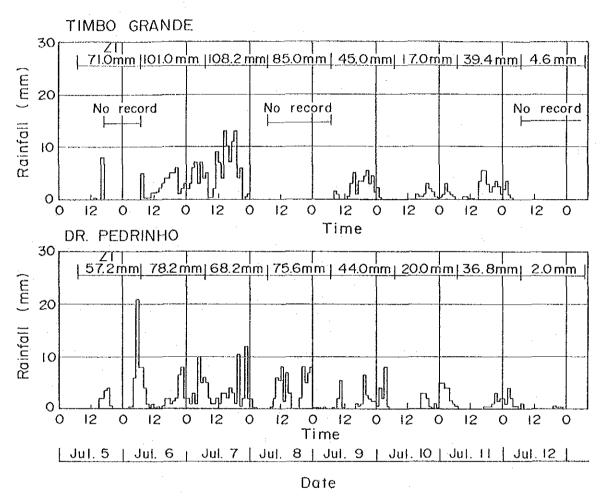


Fig. II.3.2 ISOHYETAL MAP OF RAIN STORM (3/3)



∠I: I-day rainfall amount

Fig. II.3.3 HOURLY RAINFALL DISTRIBUTION (1/3) (July 1983)

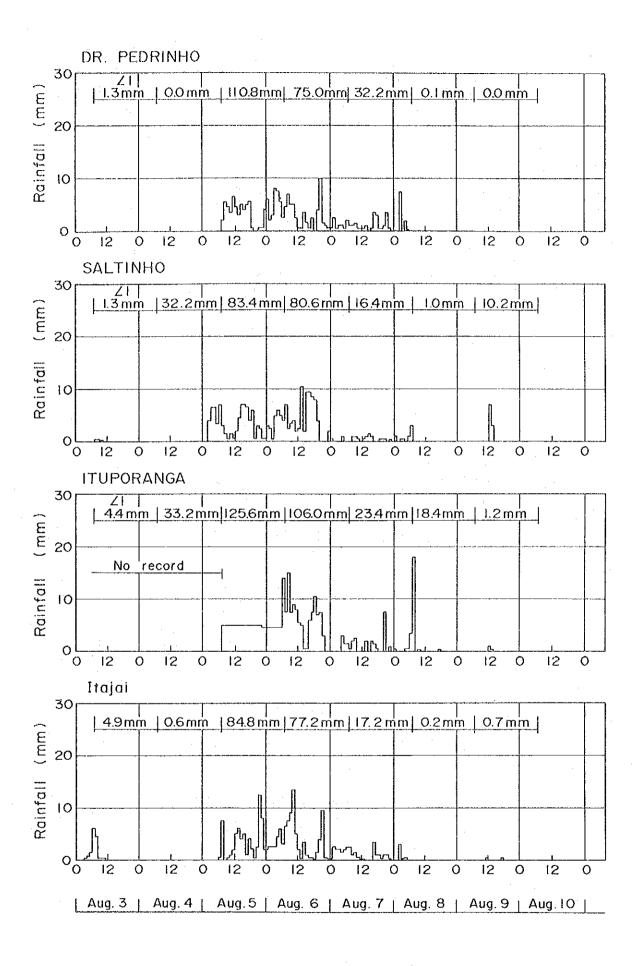
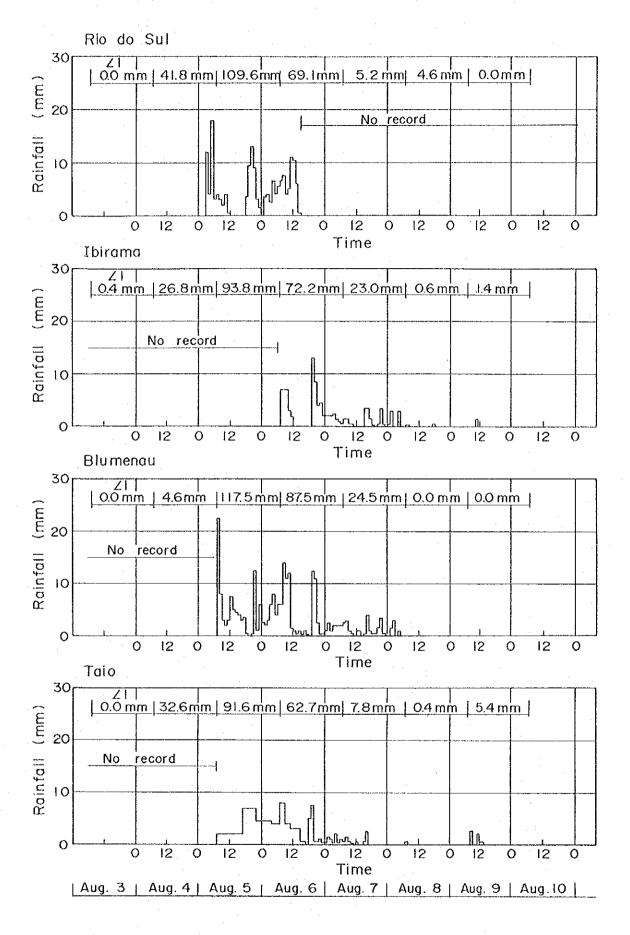


Fig. II.3.3 HOURLY RAINFALL DISTRIBUTION (2/3) (August 1984)



ZI: I-day rainfall amount

Fig. II.3.3 HOURLY RAINFALL DISTRIBUTION (3/3)
(August 1984)

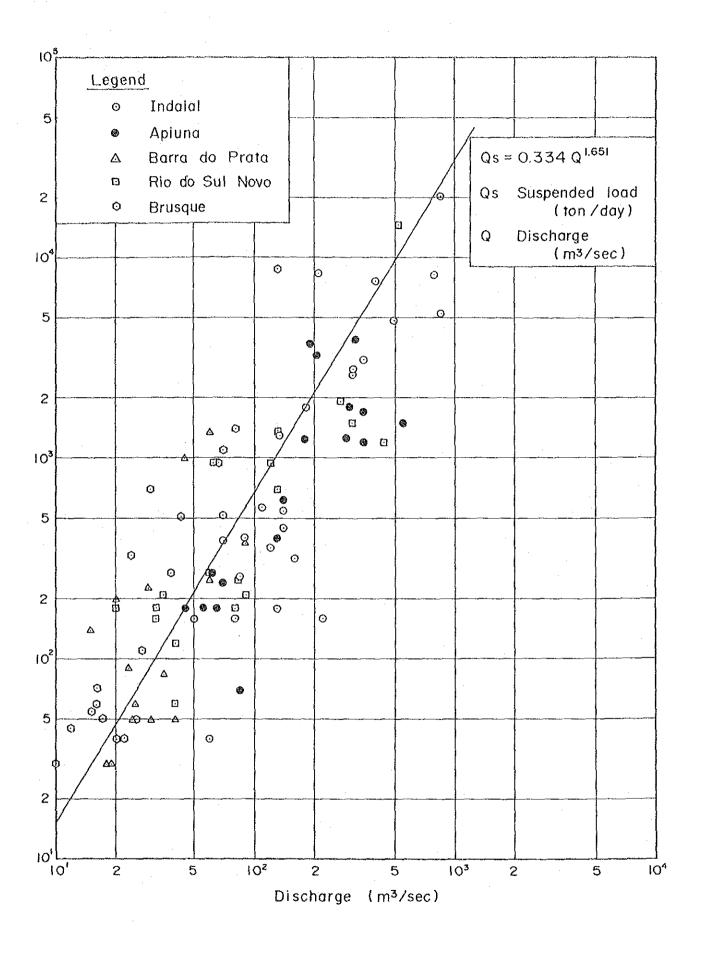
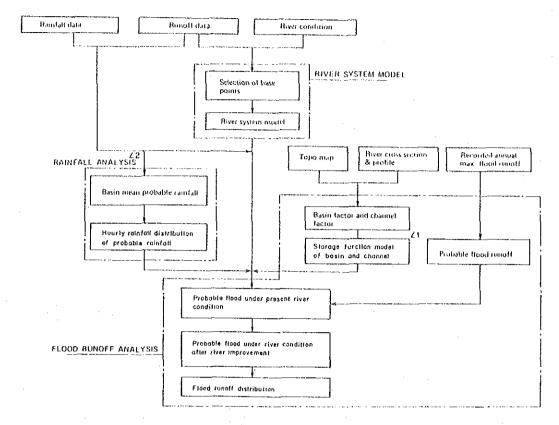
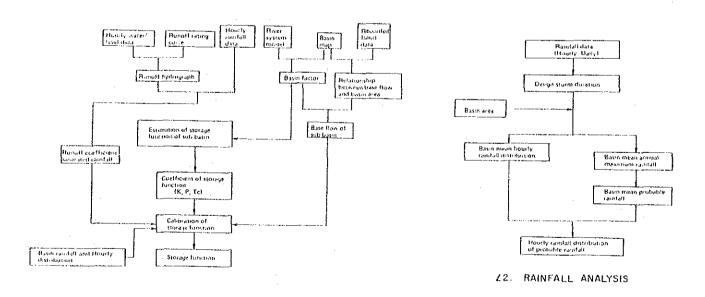


Fig. II.3.4 RELATION BETWEEN SUSPENDED LOAD AND DISCHARGE

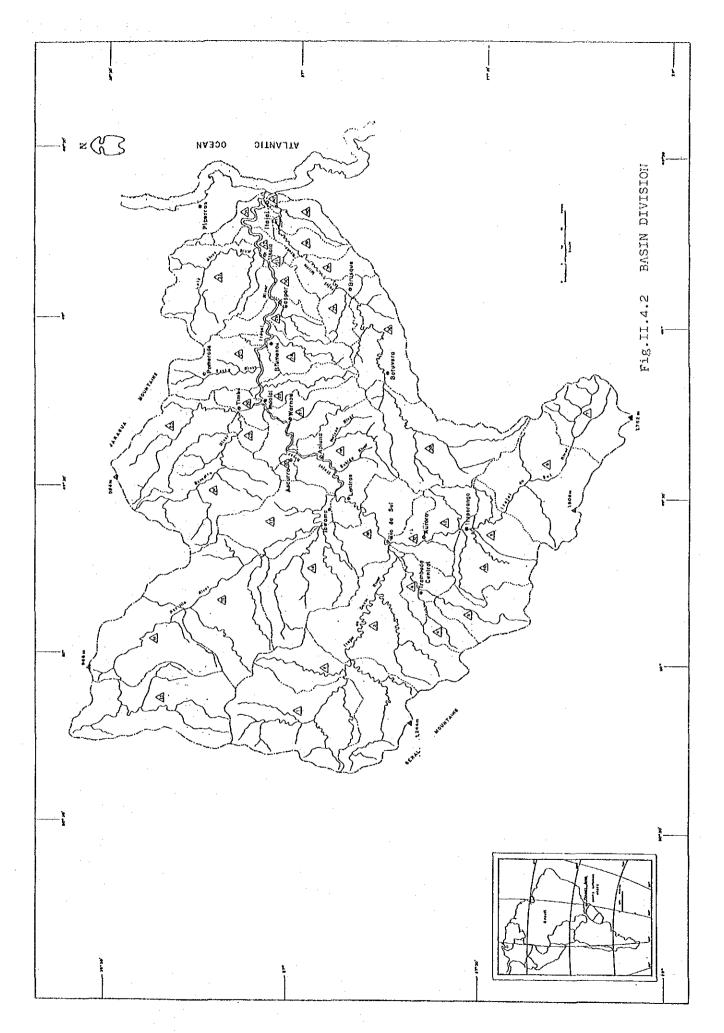


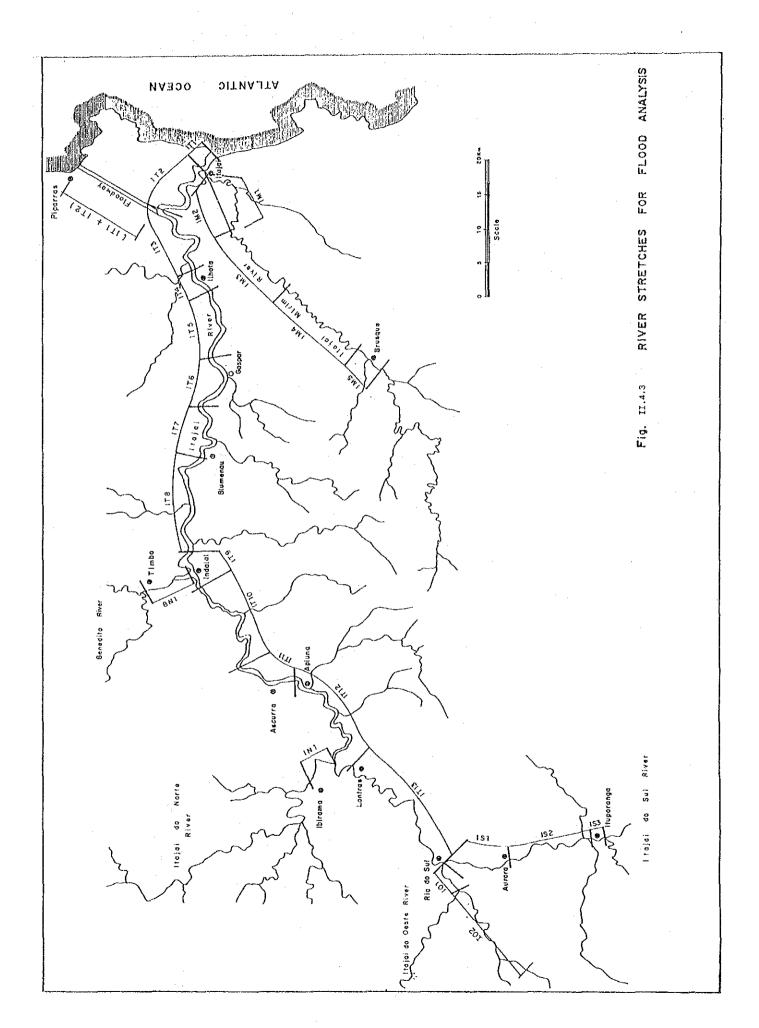
GENERAL FLOW CHART OF FLOOD ANALYSIS



Z1. STORAGE FUNCTION MODEL OF BASIN AND CHANNEL

Fig. II.4.1 GENERAL PROCEDURE





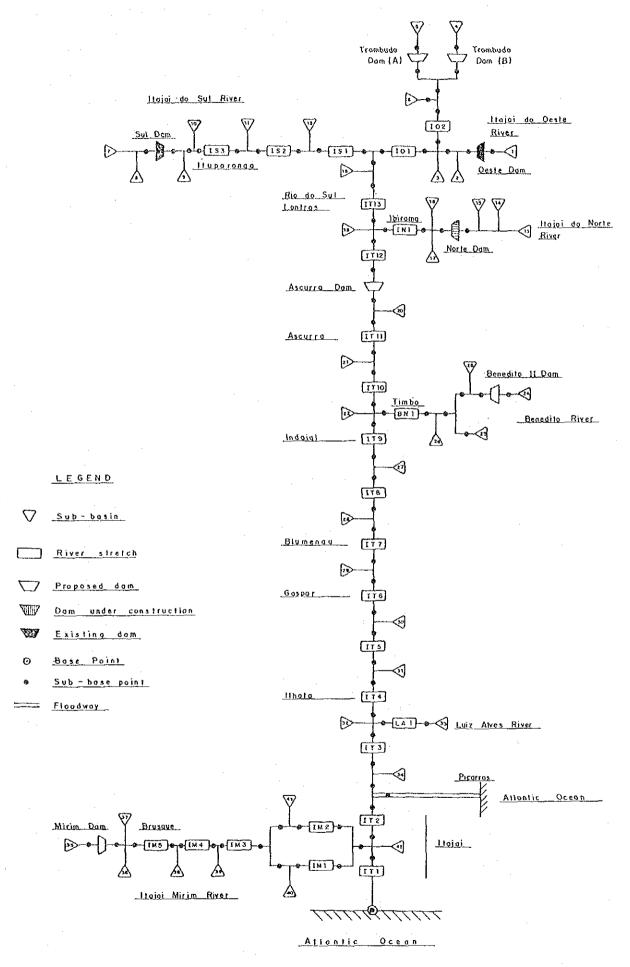


FIG. II.4.4 RIVER SYSTEM FOR FLOOD ROUTING

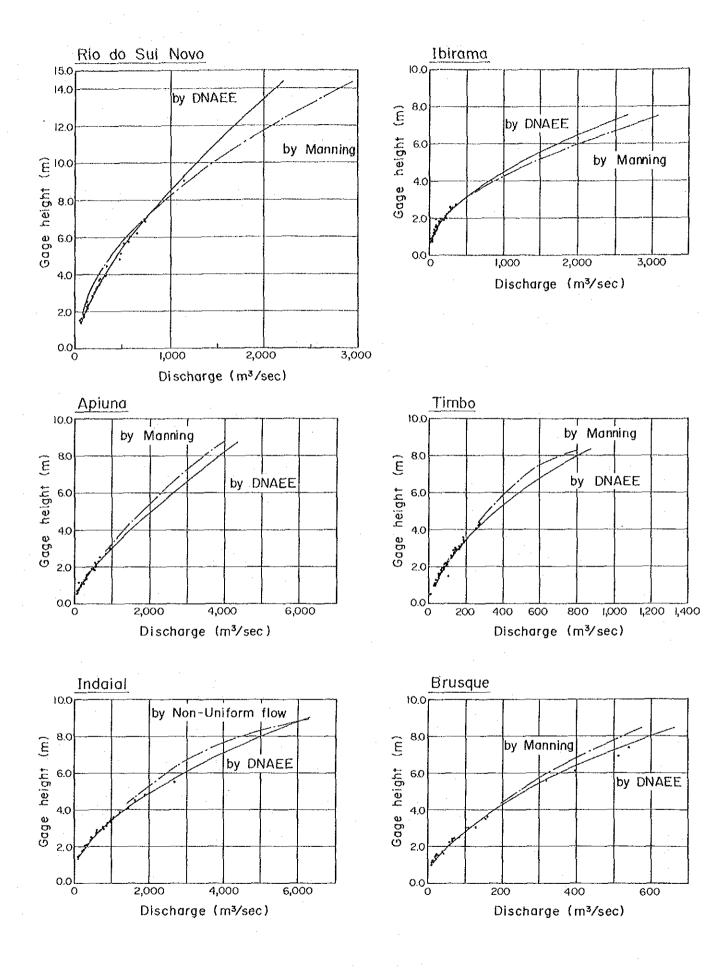


Fig. 11.4.5 RELATION BETWEEN GAGE HEIGHT AND DISCHARGE

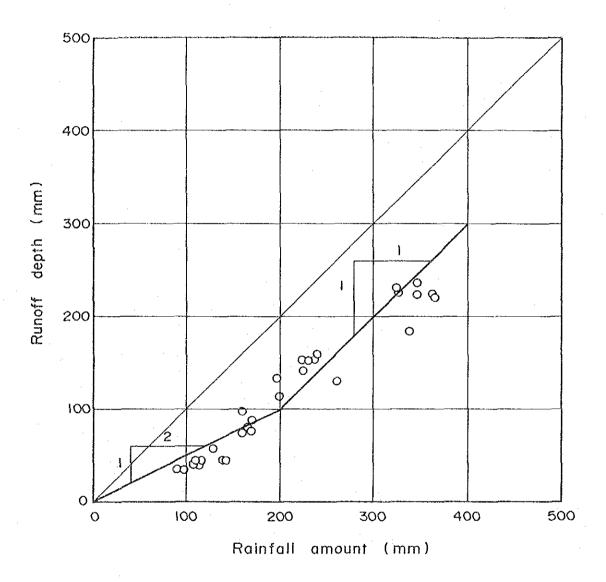


Fig. II.4.6 RELATION BETWEEN RAINFALL AMOUNT AND RUNOFF DEPTH



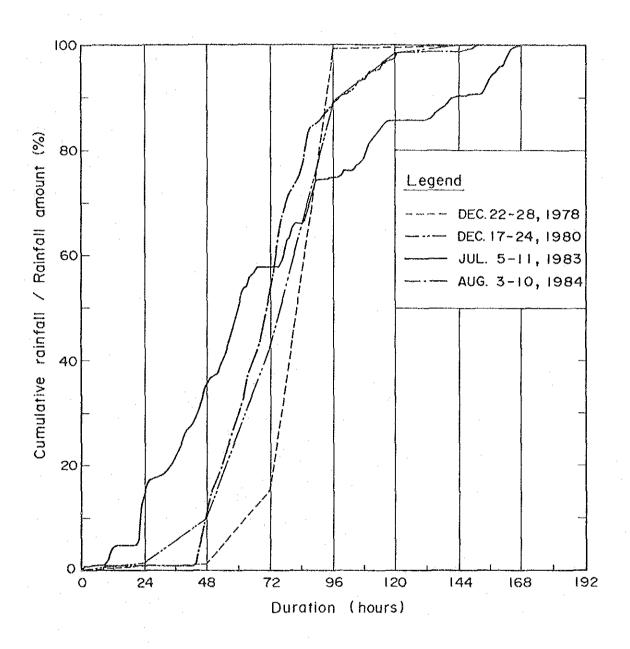


Fig. 11.4.7 RELATION BETWEEN BASIN MEAN RAINFALL AND DURATION DURING RAIN STORM

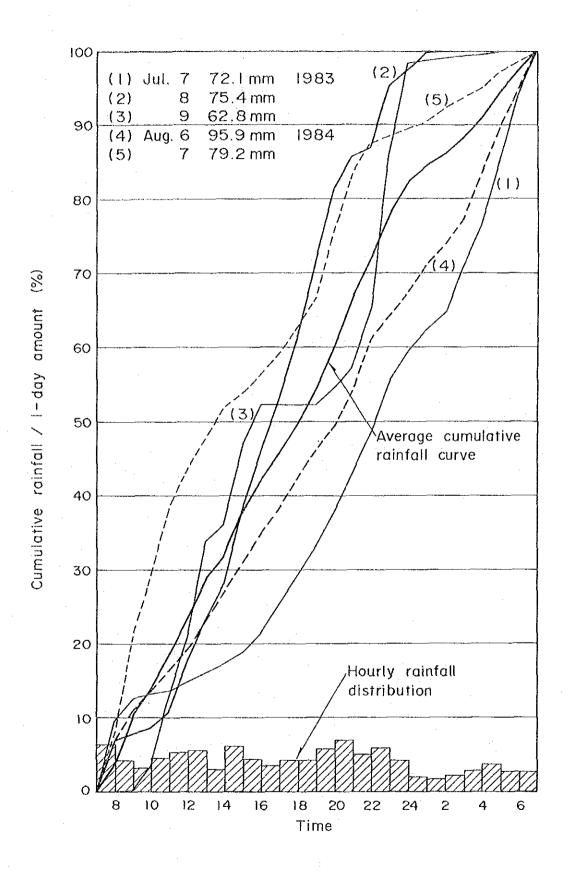


Fig. 11.4.8 ESTIMATED DAILY RAINFALL PATTERN

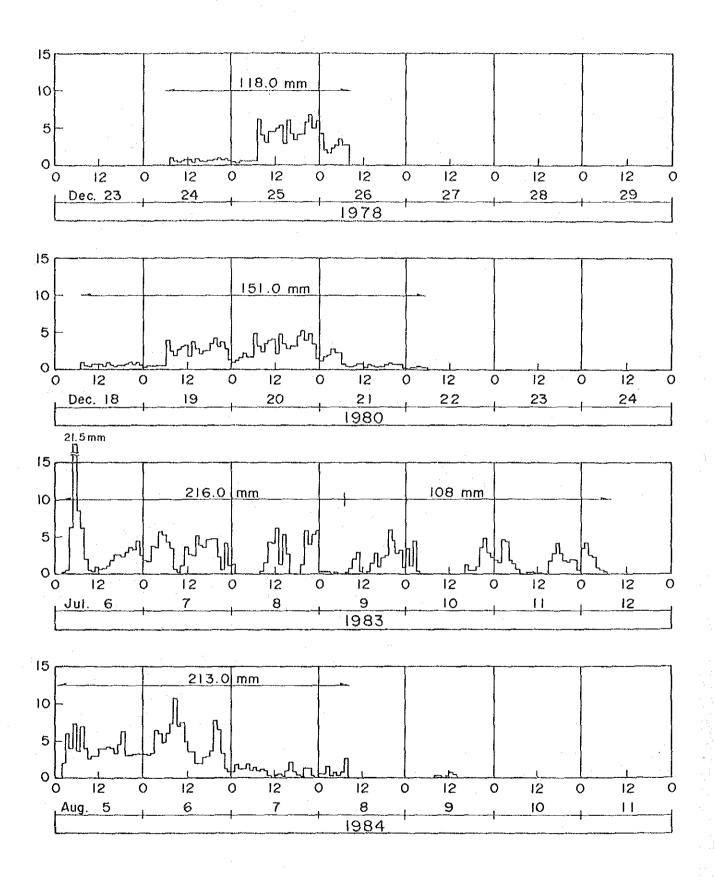
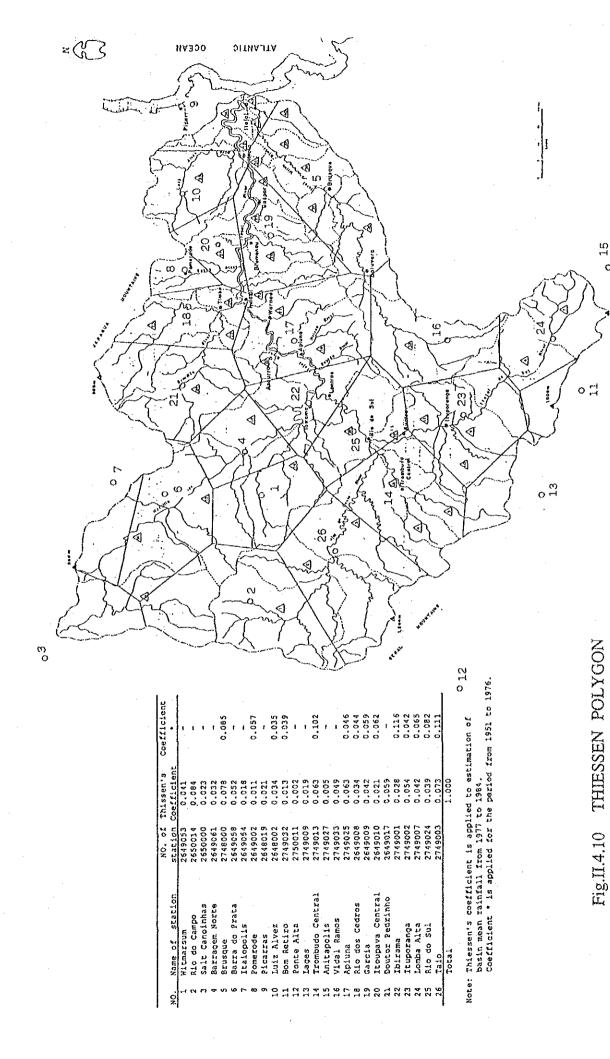


Fig. II. 4.9 BASIN MEAN HOURLY RAINFALL DISTRIBUTION



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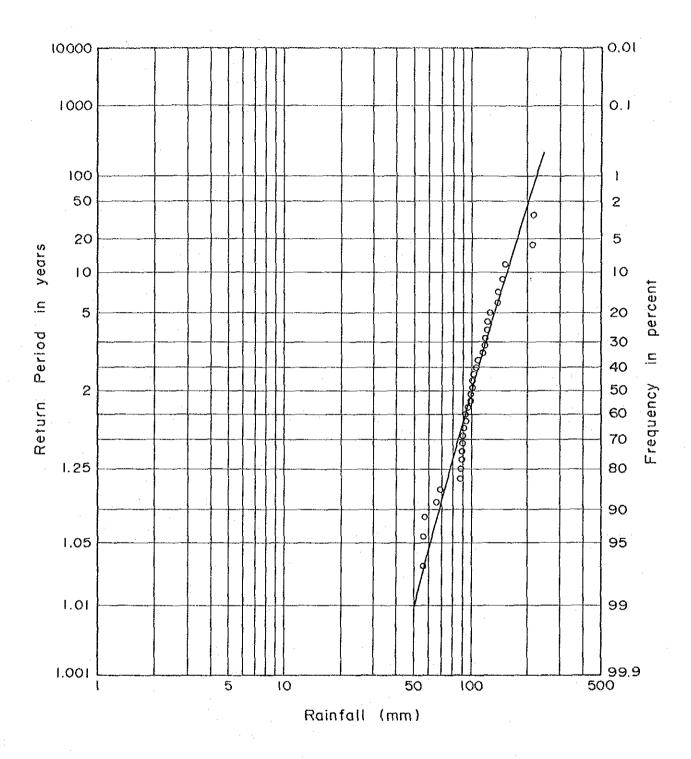


Fig. II.4.11 FREQUENCY CURVE OF ANNUAL MAX. 4-DAY RAINFALL