#### 4.4 Treatment Facilities

Cost functions for three different treatment processes, namely statilization pond, aerated lagoon, and oxidation ditch, are developed.

In developing the cost functions for treatment facilities, the following assumption are made;

- (a) Daily average number of operator is 2 (two) persons for 5,000 m<sup>3</sup>/day plant and 2.5 persons for 50,000 m<sup>3</sup>/day plant for stabilization pond and aerated lagoon processes, and for oxidation ditch process, 4 (four) persons for 5,000 m<sup>3</sup>/day plant and 8 (eight) persons for 50,000 m<sup>3</sup>/day plant are required,
- (b) Electricity is M\(\epsilon\)8/kWh and average salary of operator is M\(\partial\)20/day, and
- (c) Repairs and Overhauling of parts are estimated at one percent of capital cost of civil works and two percent of machanical and electrical works.

The operation and maintenance costs by capacity and treatment process are then estimated as shown in Table G-13 and Figures G-7, G-8 and G-9.

On the basis of these figures in Table G-13, functions for annual operation and maintenance costs of the three treatment plants are obtained as follows;

(1) For stabilization pond process  $c_{MS} = 1.263 \times 10^{-3} Q + 14.55$ 

(ii) For aerated lagoon process  $C_{MA} = 6.768 \times 10^{-3} Q + 31.29$ 

(iii) For oxidation ditch  $C_{MO} = 1.793 \times 10^{-2} Q + 22.29$ 

where C<sub>MS</sub>, C<sub>MA</sub>, C<sub>MO</sub>: Annual operation and maintenance costs, M\$ 1,000/year 3
Q: Daily average flow, m /day

Table G-13 Annual Operation and Maintenance Costs for Three Treatment Process by Capacity

					(M\$1,000)
Item	Capacity (m <sup>3</sup> /day)	5,000	10,000	30,000	50,000
(a)	Stabilization Pond			and the state of t	:
	. Salary	14.60	14.97	16.79	18.25
	. Electricity, etc.	*** .	· <u>-</u> ·	-	
	. Repairs & Replacement of Parts	7.05	10.62	37.22	58.81
	Total	21.65	25.59	54.01	77.06
					<del> </del>
(b)	Aerated Lagoon		:		•
	. Salary	14.60	14.97	16.79	18.25
	. Electricity, etc.	31.54	63.07	189.22	278.43
	• Repairs & Replacement of Parts	10.99	20.73	46.68	62.80
	Total	57.13	98.77	252.69	359.48
(c)	Oxidation Ditch				
	. Salary	29.20	43.80	51.10	58.40
	. Electricity, etc.	61.25	122.50	407.16	685.80
:	. Repairs & Replacement of Parts	19.53	37.12	102.92	174.10
	Total	109.98	203.42	561.18	918.30

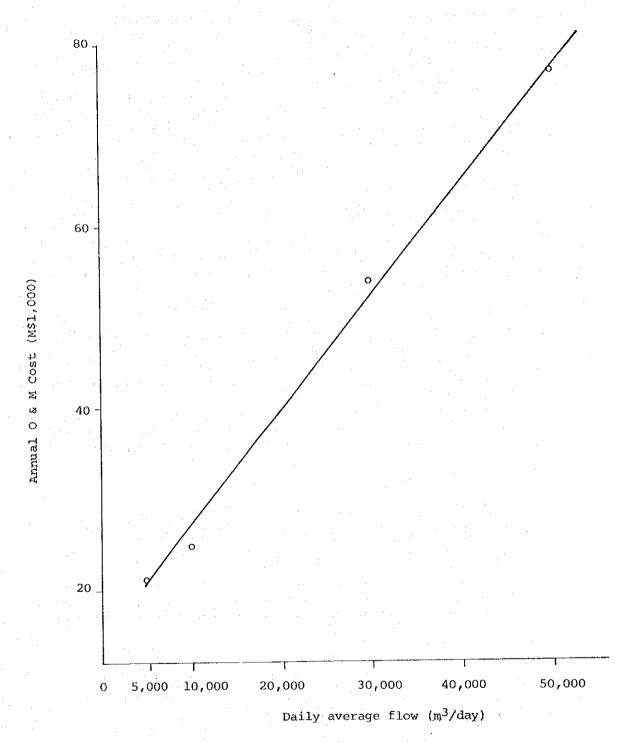


Figure G-7 Annual operation and maintenance cost for stabilization pond

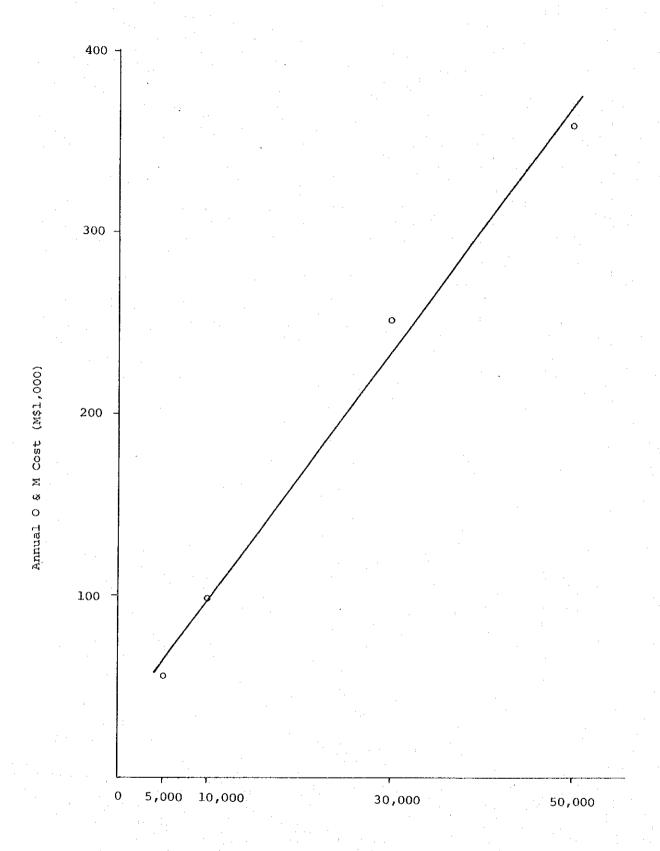


Figure G-8 Annual operation and maintenance cost for aerated lagoon

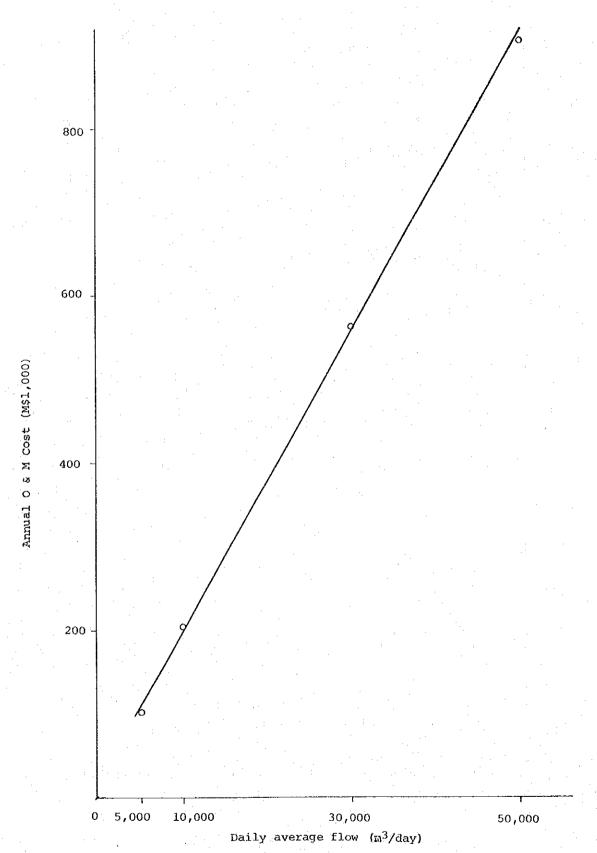


Figure G-9 Annual operation and maintenance cost for oxidation ditch process

# APPENDIX H

ESTIMATION OF CONSTRUCTION COST FOR BRANCH
AND LATERAL SEWERS

#### Unit Construction Cost Estimates for Branch and Lateral Sewers

The construction costs for the trunk sewers, which are described in Section 9 of Chapter 5 in the main report, are estimated by utilizing the method discussed in Section 1, Appendix G. On the other hand, the construction costs of branch/lateral sewers in "urbanized and/or urbanizing areas" and "the future development areas" are estimated by applying the basic unit costs as derived in section 9 of chapter 5 to the estimated branch and lateral lengthes by the reasonable preliminary engineering design of sewer networks upon the areas representing typical conditions of the two areas as shown in Figure H-1 and Figure H-2 respectively.

Based on Figure H-1, entire sewer lengths for branch and lateral sewers are measured in varying sizes in a typical urbanized and/or urbanizing area as shown in Table H-1 with additional major items for further construction cost estimates.

Table H-1 Unit Construction Cost for Branch/Lateral Sewers in Urbanized and/or Urbanizing Area

Total area (1)	167.8 ha
Area of open space, mosque etc (2)	24.6 ha
(1) - (2)	143.2 ha
Sewers	225-300 mm dia. Total length: 15,760 m
Sewer length per ha	110 m/ha
Total construction cost for sewer	M\$ 3,672,080
Construction cost per ha	M\$ 25,643/ha
the contract of the contract o	

It should be noted that the branch/lateral sewers in public areas (such as schools, mosques, open spaces, etc.) as well as housing development areas completed/planned are excluded from the sewer lengths measured and from unit construction cost estimates in Table H-1.

Similarly, based on Figure H-2, entire sewer lengths for branch and lateral sewers are measured in varying sizes in a typical existing housing development area as shown in Table H-2 with additional major items for further construction cost estimates as follow.

Table H-2 Unit Construction Cost for Branch/Lateral Sewers in Future Development Area

Total Area	(1)	122.0 ha
Area of Ope Mosque, etc	n Space, School,	15.9 ha
(1) - (2)		106.1 ha
	Sewer Facilities	225-300 mm dia. Length: 3,225 m
Government	Sewer Length per ha	30 m/ha
Portion	Construction Cost	M\$1,035,225
	Construction Cost per ha	M\$9,757/ha
	Sewer Facilities	225 mm dia. Length: 13,475 m
Private	Sewer length per ha	127 m/ha
Portion	Construction Cost	M\$2,681,525
	Construction Cost per ha	M\$25,273/ha

It should be noted that the construction cost for the branch sewers (shown in thick line) connecting the branch/lateral sewers (shown in thin line) serving for sectional areas to the trunk lines in Figure H-2, will be contributed by the Government, and the remaining cost for branch/lateral (shown in thin line) sewers are considered to be raised from direct beneficiaries. These sectional areas mostly within a range of 5 to 10 ha area assumed to be developed by developers based on a survey data obtained.

Table H-3 shows the component areas of sewerage zones as to (1) urbanized and/or urbanizing area, (2) future development area, and public areas and housing development areas completed/planned.

Table H-3 Component Areas in Sewerage Sub-zones

annæd	50000	Sub-total	(ha)	83.0	7.0	6.06	15.1	1.6	0.3	15.9	37.7	20.4	12.5	291.9
. & Completed/Planned	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	Estates	(ha)	8.6	0	17.8	1.2	0	0.3	0	6.7	С	1.3	35.9
) Public Areas		Open Space	(ha)	28.7	0	25.7	0	0	0	0	9.0	0	0	64
sing Devel	TUNUT STITE	Mosque	(ha)	8.8	0	12.9	8.2	1.0	0	Ó	2.1	0	0	33
(3)	300	School	(ha)	36.9	7.0	34.5	5.7	8.1	О	15.9	19.3	20.4	11.2	159
(2) Future	Development	Area	(ha)	51	331	10	281.8	43	26	321	26	154	52.4	1,296.2
(1) Urbanized	and/or	Urbanizing Area	(ha)	251	<u>გ</u>	358.1	113.1	49.9	160.7	90.1	324.3	95.6	60.1	1,601.9
	Total	Area	(ha)	385	437	459	410	102	187	427	388	270	125	3,190
	Name Of	Sub-zone	: '	A - 1	A - 2	B - 1	т Н	რ - ლ	C - 1	0 - 2	D = 1	D - 2	(c)	Total

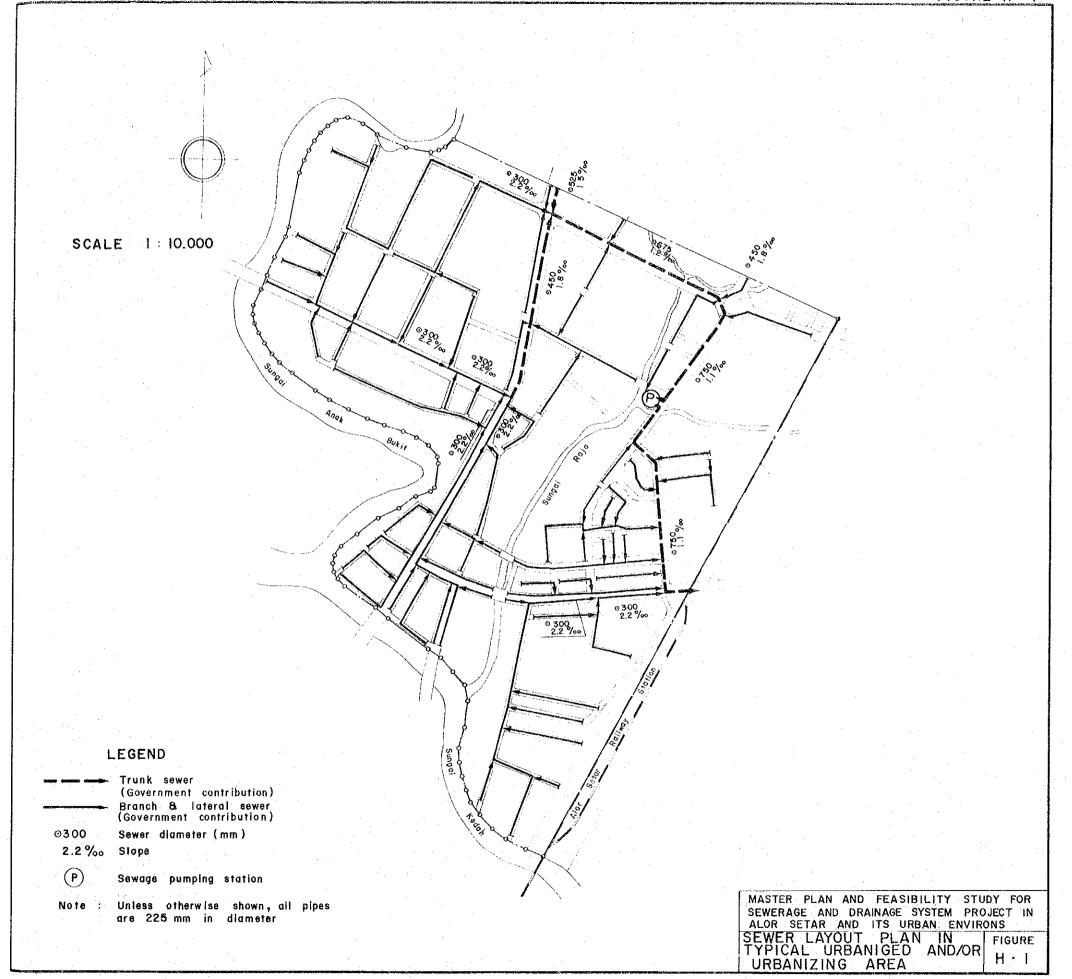
Note: (1) and (2) do not include public areas as well as new housing estates.

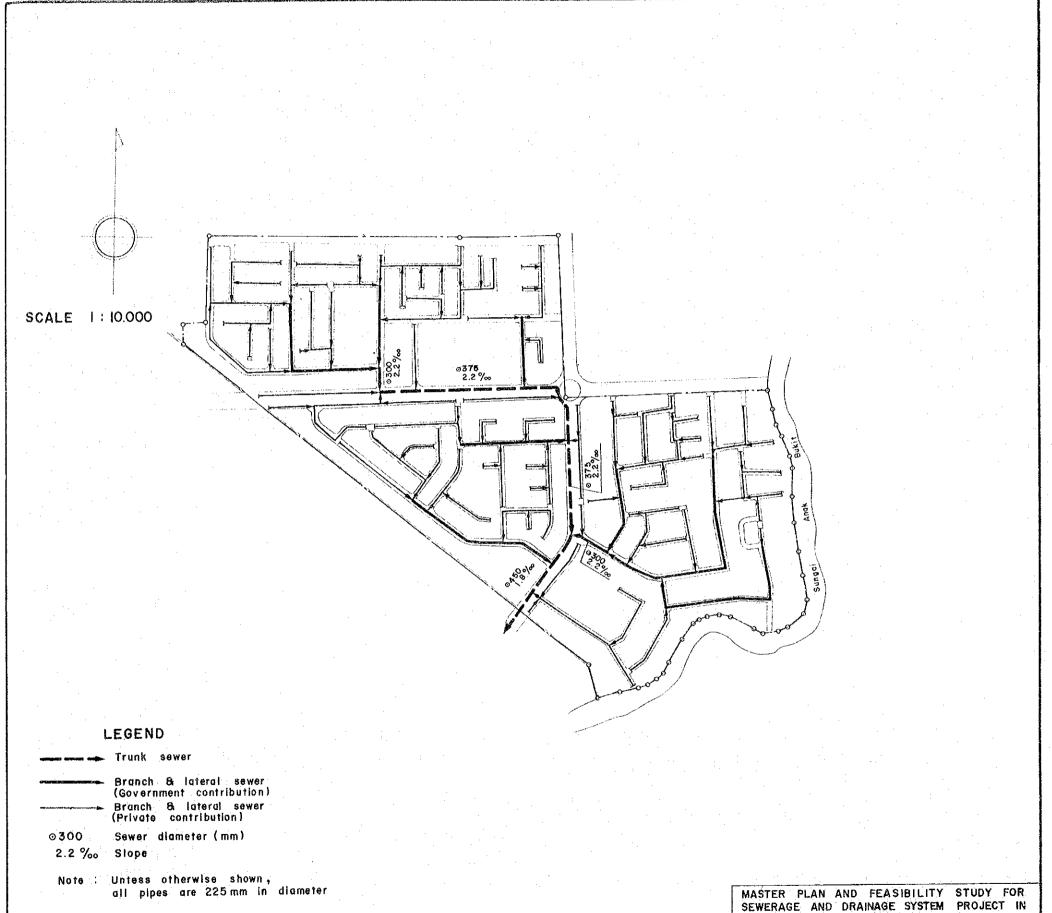
# 2. Proposed Financial Sources Constructing Branch and Lateral Sewers in the Study Area

Table H-4 summarizes estimated total lengths of branch/ lateral sewers in both "urbanized and/or urbanizing areas" and "future development areas" for each sewerage zone. Further, the same table provides construction costs to be contributed by both the Government and Private sources.

Table H-4 Proposed Financial Sources Constructing Branch/ Lateral Sewers in the Study Area

				(M\$1,	000 at 19	79 prive level)	
Name of	Gov∈	rnment Co	ontribution	Pı	Private Contribution		
Sewerage	Dia.	Length	Construction	Dia.	Length	Construction	
Sub-zone	(mm)	(mm)	Cost	(mm)	(mm)	Cost	
A - 1	225-300	29,140	6,933	225	6,480	1,288	
A - 2	225-300	20,820	5,768	225	42,040	8,365	
в - 1	225-300	39,691	9,279	225	1,270	252	
B - 2	225-300	20,900	2,863	225	35,790	7,121	
B - 3	225-300	6,780	1,699	225	5,460	1,086	
C - 1	225-300	18,460	4,374	225	3,300	657	
C - 2	225-300	19,540	5,442	225	40,770	8,112	
D - 1	225-300	36,450	8,569	225	3,300	657	
D - 2	225-300	15,140	3,954	225	19,560	3,892	
Е	225-300	8,180	2,052	225	6,650	1,324	
Total		215,100	50,933		164,620	33,754	





MASTER PLAN AND FEASIBILITY STUDY FOR SEWERAGE AND DRAINAGE SYSTEM PROJECT IN ALOR SETAR AND ITS URBAN ENVIRONS

SEWER LAYOUT PLAN IN TYPICAL FIGURE HOUSING DEVELOPMENT AREA

# APPENDIX I

SULFIDE CONTROL METHODS

#### 1. Introduction

Hydrogen sulfide and other undesirable gases associated with the operation of sanitary sewers are produced in an anaerobic environment. Therefore, the key to their control is keeping the wastewater aerobic. It has been observed that the rate of hydrogen sulfide buildup is closely related to sludge accumulation in the sewer. In other words, a well-designed, self-cleansing sewers should have little trouble from hydrogen sulfide.

Hence, the following three methods are brought into discussion for sulfide control;

- a. Keep sufficient flow velocity in sewers to prevent sulfide buildup without special sulfide corrosion protection measures.
- b. Use anti-sulfide corrosion pipe or lining pipe without special velocity control where sulfide buildup is expected.
- c. Inject air to keep sewage aerobic without special considerations on flow velocity and pipe material.

# Sulfide Controlling Velocities

The equation relating flow velocities to marginal EBOD (effective BOD) is:

Marginal EBOD = 
$$787 \text{ V}^{3/4} \text{ b/p}$$

where

$$EBOD = BOD_5 \times 1.07 (T-20)$$

T : temperature, °C

V : flow velocity, m/sec

b/P: surface width/wetted perimeter, dimentionless

The BOD concentration of the sewage for the year 2000 has been estimated at 200 mg/l. Therefore, the equivalent EBOD for the year 2000, at a temperature of 27°C, will be

$$200 \times 1.07^{27-20} = 321 \text{ mg/l}$$

Sulfide control velocity curve for the year 2000 condition is then developed, as shown in Figure I-1.

If peaking factor is expresses as P.F.=5/P<sup>1/7</sup> (where P: population in thousand persons), and population is estimated at 4,800 persons, the P.F. will be 4.0 that is, the daily average flow will be one fourth of peak flow in such areas which has population of 4,800. Because, for sanitary sewer, full pipe capacity of the design peak flow rate is provided, the pipe diameter for this population will be 300 mm. (Per capita sewage flow is estimated at 230 1/cap/day). This is the upper limit of VCP market size. The minimum design flow velocity should be determined at least on the basis of the daily average flow velocity of above pipe size. Hence, the minimum design flow velocity is determined at 75 cm/sec.

The Figure indicates that if the minimum design flow velocity is decided at 75 cm/sec, the sulfide generation will be controlled from 0.25 to 0.70 of peak design flow rate. The problem of sulfide control is much more severe during the initial year of service of sewer pipeline when flows are considerably less than future design flows. However, as shown in Figure I-1, it is impossible to keep the sulfide control velocity to meet all flow variations.

## 3. Anti-Corrosion Pipe

VCP, RCP, ACP, and Pitch Fibre Pipe are available in Malaysia. Among them VCP is the best pipe against sulfide corrosion. However, the available VCP market size is up to 300 mm in diameter, and larger sewers will be of concrete-bonded pipes, either centrifugally cast or cast in place, which are likely subject to sulfide attack.

Coatings and linings of acid-resistant materials, such as vinyl and epoxy resins, PVC sheet, and high alumina cement mortar, will be effective for protecting concrete pipes against the acid attack.

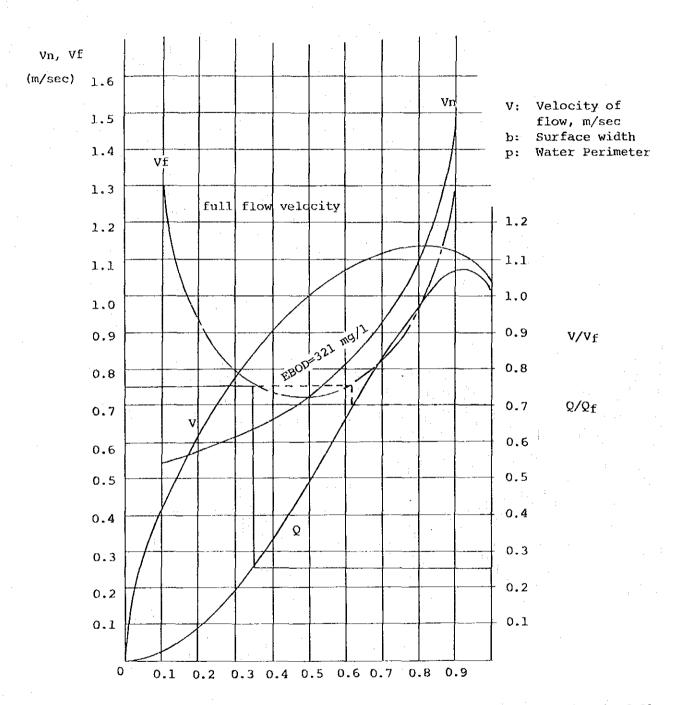
## 4. Air Injection to Sewer

This method is useful only in the force main.

#### 5. Conclusions

In view of the above considerations especially for future operation and maintenance problems of the sewerage system, it is concluded that all sanitary sewers shall be so designed and constructed to give mean velocity, when flowing full or half-full, of not less than 60 cm/sec for VCP, and for RCP or any cement-bonded pipe the minimum design flow velocity should be 75 cm/sec, and suitable lining or coating pipes should be used.

Pomeroy-Davy Formula for Marginal Effective BOD Marginal EBOD = 787 V4/3 b/P



d/D d: flow depth

D: pipe diameter

Vf: Velocity in full

flow

Qf: Quantity in full

flow

Vn: Velocity required

FIGURE I-1 Sulfide control velocity curve for sulfide control

APPENDIX J

PHASING CONSIDERATIONS

#### 1. Introduction

It is a task of tremendous magnitude to provide a complete sewerage system for entire Study Area with its large and expanding population.

A consideration is, therefore, given to build the required facilities in phases, according to the urgency of need and benefits to be derived. Phased construction will spread capital expenditure over an extended period of years, as well as saving interest on borrowed capital and reducing initial costs.

A study, hereunder, provides to determine the priority of implementation and the desirable phases of the sewerage sub-zones, taking into account the various important elements which affect sanitary conditions in the Study Area, applying a reasonable rating procedure.

## Rating of Sanitary Conditions

#### 2.1 Basic Consideration for Rating

The elements considered in the implementation priority of swerage sub-zones up to the year 2000 include the following six items, each of which has impacts on environmental sanitation in the Study Area.

- 1) Population density
- 2) Development condition
- 3) Waste load generation aspect
- 4) Excreta disposal system
- 5) Flooding condition
- 6) Incidence of water-borne diseases

Note: An evaluation item "availability of water supply" is not considered for this particular situation because the Study Area is almost uniformly served by the water supply system.

The above-mentioned six elements are assigned by the different evaluation points to reflect their relative importance to the sanitation, and each of the ten sewerage subzones is evaluated carefully and graded according to the rating for each element for the purpose of establishing sewerage implementation priority.

It is, however, noted that re-evaluation of these sewerage sub-zones should be made at the beginning of each implementation phase to reflect urbanization of these areas at the time, especially in the future development area.

#### 2.2 Application of Rating System

For the purpose of rating system, a total of 1,000 points is assigned over the six major elements, according to order of importance, as described below.

## (1) Population density

One of the most important factors is the number of persons

who will be benefited by the system. It is, therefore, particularly significant to provide sewerage facilities in high population density area, in order to gain the maximum benefit to the maximum population with the minimum expenditures thus making the benefit-cost ratio higher. Hence, highest point is assigned for the population density.

#### (2) Development Condition:

Development condition of the Study Area differs largely according to areas and land uses. The greater portion of the future development area lying periphery of the Study Area remains to be paddy field yet, thus unabling to provide sewerage system for the time being and in the immediate future.

## (3) Waste load generation aspect:

Three hundred points is assigned to the item of waste load generation. The waste load generated from the housing, commercial and industrial areas are generally discharged into drains and rivers without any treatment except septic tanks. It is, therefore, necessary to quantify the waste load in each of the sewerage zones to determine the urgency of the need of sewerage facilities.

## (4) Excreta disposal system:

Since there is no sanitary sewerage system in the Study Area, except a few local systems, most of the excreta produced in the area is disposed of either septic tank, bucket pit privy or directly to waterways, causing water pollution at many places in the Area. The existing excreta disposal system is, therefore, analyzed as to the present excreta disposal.

#### (5) Flooding Condition:

Although the Government has undertaken improvement works for the existing rivers and drains, flooding has occurred frequently and caused substantial damage in the built-up areas. Sanitary conditions in these areas have been significantly deteriorated, which can only be improved by the provision of the sewerage system.

# (6) Incidence of water-borne diseases:

Incidence of water-borne diseases, has also effected to sanitation conditions, but this is less critical than the above five elements, these giving the lowest points of 50.

In view of these factors, the six elements, all of which affect sanitary conditions, are given points arbitarily for the years 1979 and 2000 according to their importance for the rating.

The rating points are shown as followings:

		Poir	nt assig	ned
a)	Population density		300	
b)	Development condition		200	•
c)	Waste load generated		300	·
d)	Excreta disposal system		100	
e)	Flooding Condition		50	
f)	Incidence of water-borne diseases		50	
	Tota	al !	L,000	• .

Further applications on these factors are discussed in the following section.

# 2.2.1 Population Density

Population densities, both present and future, by sewerage sub-zones, range approximately from 6.8 to 125.1 persons per hectare, as presented in Table J-1 and Figures J-1 and J-2. For purpose of rating, 150 points are given to both present and future population densities respectively:

Assigned Point	Present Population Density (Persons/ha)	Future Pppulation Density (Persons/ha)
150	100 or more	120 or more
120	80 - 100	110 - 120
90	60 - 80	100 - 110
60	40 - 60	90 - 100
30	20 - 40	80 - 90
0	0 - 20	70 - 80

As shown in Table J-1, sub-zone B-1 gains 300 points, followed by sub-zone D-1 and Sub-zone C-1 and Sub-zone E.

Evaluated Points for Population Density by Sewerage Sub-Zone Table J-1

		19	1979	20	2000	Evalue	Evaluated Points	ints
Sewerage	Area * (ha)	Population (Persons)	Population Density (Persons/ha)	Population (Persons)	Population Density (Persons/ha)	1979	2000	Tota1
H 1 4	356.3	15,100	42.3	29,700	e e e e e e e	09	30	06
A - 2	437.0	3,700	ω Ω	38,000	87.0	O <sub>2</sub>	30	30
В Г	433.3	44,400	102.5	54,200	125.1	150	150	300
2 1 B	410.0	11,400	27.8	40,700	99.3	30	9	06
m L	102.0	1,300	12.7	11,100	108.8	0	06	00
c - 1	187.0	000,6	48.1	21,500	115.0	09	120	180
0	427.0	2,900	8.9	33,700	48.9	O	0	o.
D - 1	378.4	35,000	92.5	46,500	122.9	120	150	270
D - 2	270.0	7,700	28.5	30,000	111.1	30	120	150
臼	125.0	9,100	72.8	12,900	103.2	06	06	180
Total	3,126.0	139,600	44.7	318,300	101.8	1	-	

Note:

<sup>\*</sup> These figures do not include rivers, railway , parks and open spaces, etc.

# 2.2.2 Development Condition

Evaluation is made for each sub-zone in terms of percentage of estimated urbanization or industrialization for the coming several years as shown in Table J-2 and Figure J-3. Since the Study Area is assumed to be urbanized by 2000, evaluation for the year 2000 is not made.

Assigned Point	Percentage of Urbanization and Industrialization (%)
200	80 or more
150	60 - 80
100	40 - 60
50	20 - 40
0	0 - 20

Table J-2 Evaluated Points for Development by Sewerage Sub-Zone

05 670700		Area	
Sub-Zone	Total Area * (ha)	Developed and Developing Area (ha)	Ratio Evaluated Points (%)
1 &	385	305	79
A .	437	106	24
н П	459	423	500
B - 2	410	127	31 50
ო 1 p	102	59	28
ر ا ا	187	161	86 200
0	427	102	24
D - 1	388	352	91 200
D - 2	270	116	43
PL	125	64	51 100
Total	3,190	1,815	57

Note: \* These figures do not include areas of rivers and railway.

#### 2.2.3 Waste Load Generated

According to the investigation carried out in the Study Area, streams are generally polluted by the deposit of organic matters and industrial wastes, hence it is necessary to control the waste load discharging into waterways. For the purpose of rating, waste load originating in each sewerage sub-zone is estimated at per ha waste load generation basis both for 1979 (present) and 2000. Evaluated points are shown in Table J-3 and Figures J-4 and J-5.

In this rating, a maximum of 300 points is assigned, 150 points each for 1979 and 2000 waste load generation rates of 6-8 kg BOD/d/ha and 8 or more kgBOD/d/ha respectively, and a minimum of 0 point in case 0-2 kgBOD/d/ha and 2-4 kgBOD/d/ha for 1979 and 2000 respectively as shown below:

Assigned Point	Waste Load Generated in 1970 (kg BOD/d/ha)	Waste Load Generated in 2000 (kg BOD/d/ha)
150	6 - 8	8 or more
100	4 - 6	6 - 8
50	2 - 4	4 - 6
0	0 - 2	2 - 4

Evaluated Points for Waste Load Generated by Sewerage Sub-Zone Table J-3

		1	1979	2000	0	Eval	Evaluated Points	ints
Sewerage Sub-Zone	Area * (ha)	Waste Load (kg BOD/day)	Waste Load per ha (kg BOD/d/ha)	Waste Load (kg BOD/day)	Waste Load per ha (kg BOD/d/ha)	1979	2000	Total
A - 1	356.3	611.2	1.7	1,519.6	4.3	50	50	100
A - 2	437.0	130.6	0.3	1,760.2	4.0	0	20	50
ri M	433.3	2,327.6	5.4	3,685.0	ထိ	150	150	300
м П	410.0	397.4	0 ri	1,894.4	4.6	0	20	50
m I	102.0	46.8	0.5	516.0	ហ	0	20	50
C - 1	187.0	273.1	ប្	578.8	T.e	0	0	· .
υ 1	427.0	104.4	0.2	1,879.4	4.4	0	20	50
- C	378.4	1,407.4	3.7	2,529.8	6.7	100	100	200
D - 2	270.0	270.2	1.0	1,401.8	5.2	0.	20	20
印	125.0	741.6	თ <b>.</b> თ	3,888.8	31.1	100	150	250
Total	3,126.0	6,310.3		19,653.8	1	1	1	

Note: \* These figures do not include areas of rivers, railways, parks and open spaces, etc.

## 2.2.4 Excreta Disposal System

The existing excreta disposal system in the Study Area is represented by two systems, namely septic tank and bucket system. Most of the population in the new housing development areas use flush toilets with individual or communal septic tank and most of the population in the build-up areas are served by mixture of individual septic tank and bucket system, while rural population use bucket system dominantly.

Table J-4 shows estimated number of houses served either by bucket system or by various kinds of latrines (such as pit privy, over-river latrine, etc.) according to data in Section 8 in Chapter 3 with additional assumptions based on the field investigations. Assessment as to present excreta disposal situation is made considering the availability of bucket and latrine system which should be higher in priority to be replaced into sewerage system than septic tank system exists.

For the purpose of rating, a maximum of 100 points is assigned to sewerage sub-zones wherein more than 10 percent of households provided either bucket or latrine system, that is, the remaining 90 percent of households were provided with septic tanks, while a minimum of 0 point to sub-zones wherein 0 - 5 percent of households provided either bucket or latrine system or the remaining 95 - 100 % of households were provided with septic tanks as shown below.

Assigned Point	Bucket System or Latrine (%)
100	10 or more
50	5 - 10
O	0 - 5

Each sewerage sub-zone is evaluated as shown in Table J-4 and Figure J-6. B-1, D-1 and E come top in priority as to excreta disposal aspect gaining 100 points, followed by A-2 and B-2.

Evaluated Points for Existing Excreta Disposal System by Sewerage Sub-Zone

Sub-Zone	Number of Houses	Bucket System including over-river latrine System	cluding e System	: F
		Number	Ratio (%)	Evaluated Points
다   작	2,748	42	1.5	0
A - 2	667	<b>4</b> .	6.7	50
m i	8,296	1,347	16.2	100
77 1 12	2,074	170	8.5	50
г В	226		0	0
г 1 0	1,423	50.	3.0	0
N . 1 U	527	<b>172</b>	8	0
D I	6,368	1,009	15.8	100
7 1 0	1,398	10	0.7	0
ш	1,656	255	15.4	100
Total	25,383	2,938	1	e <b>T</b>

## 2.2.5 Flooding Condition

As shown in Figure J-7, flooding occurs in the Study Area except in zone C. However, sewerage zones (or sub-zones) heavily affected by flooding are limited into three, namely B-1, D-1 and E. More than 20 percent of area in sub-zone B-1 and zone E is liable to flooding and more than 14 percent of area in sub-zone D-1.

An assessment point for rating is given according to the extent of flooding in sewerage sub-zones as follows:

Assigned Point	Percentage Area Flooded
50	20 or more
25	10 - 20
.0	0 - 10

All sewerage sub-zones are evaluated based on the assessment points given in the above table as resulted in Table J-5.

Tabel J-5 Evaluated Points in terms of Flooding

		Area		
Sub - Zone	Area (ha)	Flooded Area (ha)	Ratio (%)	Evaluated Points
A - 1	385	4.2	1.1	0
B .	437	14.7	3.4	0
гч I М	459	93.4	20.3	50
m 1	410	28.9	7.0	•
м І м	102	e. 0	9.1	• • • • • • • • • • • • • • • • • • •
0 1	187		ı	0
61 I U	427	I	1	• • • • • • • • • • • • • • • • • • •
D 1	388	55.8	14.4	25
2 1 2	270	0.8	3.0	0
ជា	125	29.5	23.6	50
Total	3,190	243.8		

## 2.2.6 Incidence of Water Borne Diseases

For the purpose of rating on incidence of water borne diseases, cholera cases are taken as the indicator.

Cholera patients recorded are listed below on Mukim (administrative unit) basis in Alor Setar Areas, including the Study Area;

Mukim	Cholera Patient
Hutan Kampong	11
Anak Bukit	9
Alor Merah	<b>2</b>
Alor Malai	11
Kota Setar	19
Pumpong	7
Mergong	9
Pengkalan Kundor	25
Kuala Kedah	13
Total :	106

A maximum of 50 points are assigned and each of sewerage sub-zones are evaluated according to assessment points and the level of incidence as follows:

Assessment Point	No. of Cholera Patient
50	More than 2
25	1 - 2
0	0 - 1

The result of the assessment for each of sewerage sub-zones are shown in Table J-6 and Figure J-8.

Evaluated Points 20 25 23 0 Ö 0 Evaluated Points for Distribution of Cholera Cases by Sewerage Sub-Zone Ratio (Person/1,000 Perns) 0.13 1.36 0.20 0.88 1.61 0.13 2.07 0.09 0.39 0.44 Cholera Patients Number of 45 임 Population at 1979 (Persons) 3,666 1,243 2,897 35,025 7,689 9,105 7,827 15,112 45,629 139,600 11,407 Table J-6 Sub-Zone D - 2 A - 1 П — Д Total 1 • 1 ď ф ω щ ф

## 2.2.7 Overall Evaluated Points by Sewerage Sub-Zone

All points evaluated for six major items are listed in Table J-7 and Figure 5.3, Volume II, according to sewerage subzones.

Table J-7 Overall Evaluated Points by Sub-Zone

Sub-Zone	Population Density	Population Development Density Condition	Waste Load Generation	Excreta Dis- posal System	Flooding Condition	Incidence of Water-borne Disease	Total
A - 1	06	150	100	0	0	0	340
A + 2	30	20	50	0.0	0	25	205
П Д	300	200	300	100	50	0	950
В 1	06	0.00	S O	015	O .	0	240
ო     ტ	06	100	50	o	0	25	265
С Г Г	180	200	0	0	0	0	380
0 1 2	0	OS.	50	<b>o</b> :	0	50	150
П П	270	200	200	: . 0001	25	0	795
D - 2	150	100	50	0	0	0 · · · · · · · · · · · · · · · · · · ·	300
<b>–</b>	180	100	250	100	50	• • • • • • • • • • • • • • • • • • •	730

MASTER PLAN AND FEASIBILITY STUDY FOR SEWERAGE AND DRAINAGE SYSTEM PROJECT IN ALOR SETAR AND ITS URBAN ENVIRONS

EXISTING EXCRETA
DISPOSAL SYSTEM

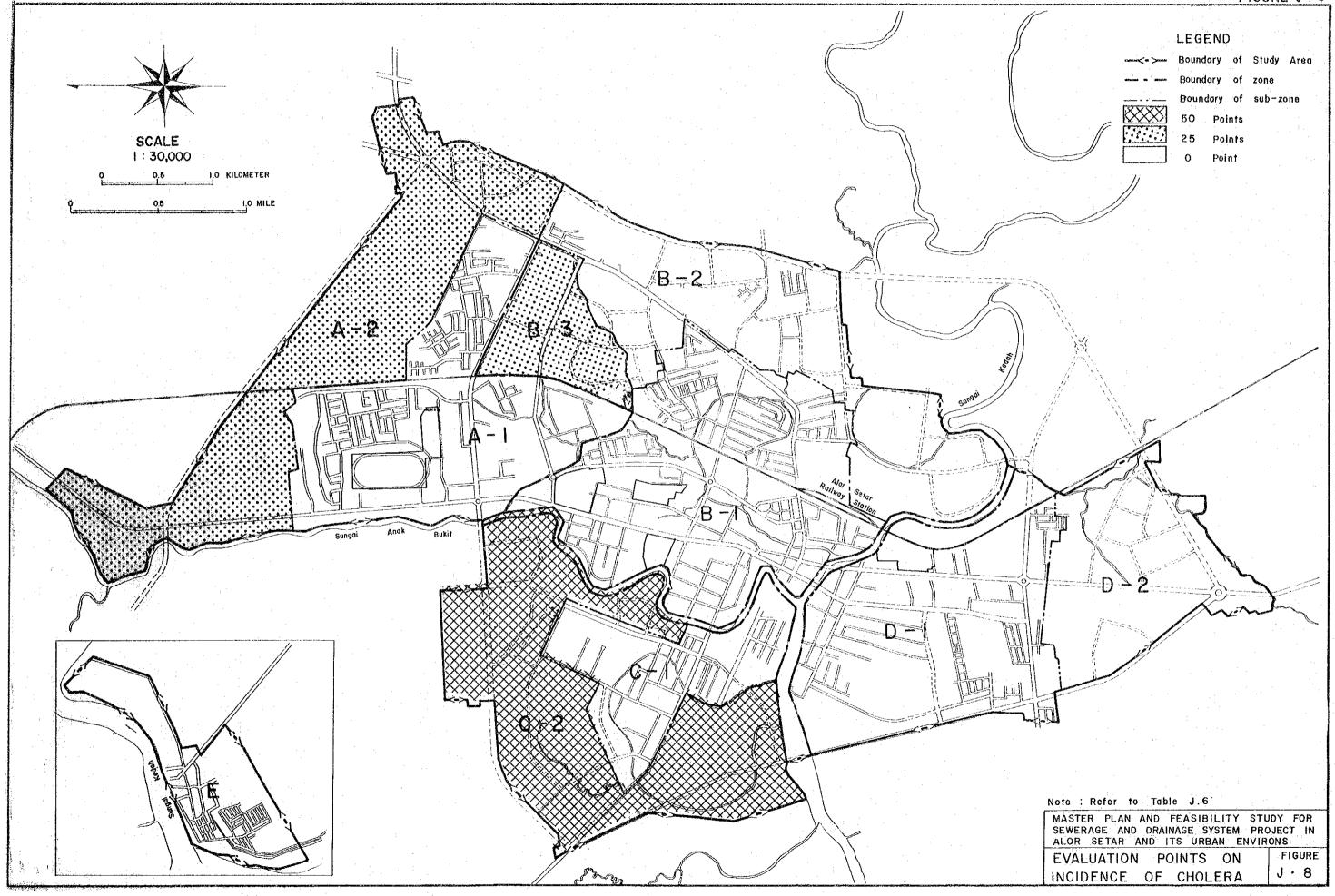
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FIGURE

J · 7

FLOODING

AREA



## APPENDIX K

COMPUTATION FOR TRUNK SEWER DESIGN

Separate sewerage system proposed collects and conveys all wastewaters from residential, commercial and industrial areas to stabilization ponds provided at the terminal of the system.

The design sewage flows are calculated for the conditions in the year 2000, including extraneous flows such as groundwater infillration.

Sewer capacity has been determined using the design criteria as discussed in Section 5, Chapter 5, Sewerage Master Plan Report.

Hydraulic computations are shown in Table K-1 for the trunk sewers in every sewerage zone shown in Figure 5-2 of the main report, applying the conveniently provided hydraulic computation chart in Table K-2 on the basis of Manning's Formula.

Zone - A

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191	Elevation Ground Surface Sewer Invert Elavation Earth Covering	E	250 1255 100	-0.72/	289 3000 5.67	001 5341 (06 8)	-12157 4 91	69 - 3 9 E.P.			2.94 1619 1.00	22 0.562		3065	(270)-1899 378	2 -255	CO. 4 3060 - CO.			256 0 000 100	2.22 0.92 18B		244 0270 190		11.50	0030	1	(188) -2727 383	0 - Oct 6 - 52 /
esigned Sewer	Cobacity (Full)	o/o m /sec m3/sec	28 061 0005 1280	P.P. 065 0007 (870)	2 0.65.0007	2 3000 130 80	55 0007	20 0.75 0096	& Scarion		しなきもり	8500 000 00		20 0.6/ 0025	2.2 0 6.5 0000	2 0.75 0.000	80001000	pide Seation		Coffee	7300 000 51		2.0 0.00	2 0.65 0 OKT	0.25 0086	4 0 0 0 0 0 0	7	0,007	14. 0.49 0.427
G	vetembiQ:	e EE	285 48500	300 545.00	7	225 4000	0000-000	0000 275	to De		500c = mart	o y	5,02	2 27 77E.00	8775 00	075 SPE 0	00000 050	50 P2 Pu		500c 45000	2000 2000		555	3000 585.00	2,000	000	, , , , , , , , , , , , , , , , , , ,	() ()	-1
	日 10 14 10 14	ha m5 ec sec	9000		0,000 0,000 S	* 3100 BOOO S.	0.000	2 130.0 200.0 40 2.		07 0 012 0 111 P)	3/00	0.013 0.121		01 5100 1000 86	18 0.003 0.006 11	21 0.005 0.001 12	04 6.006 8.093 13		04 000 G 0000 PO	A 0.00 0 0.09.0 14	21 2000 10008		21 2100100088	0.008 0.00.0	1 20000	7000	0 067 0.886	0007 0 #85	28 218 0 000 000
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Population	A Insmerani	ns ha hapersons	848	26.20 44.8	25.50		000	000 000			2580 448	26.80			2,10	6.50 6.60 257	860 257	-	0.00 257	860 857	407 04:36					3040	160 3690	3690	50 35.90 70
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No. of Sewers

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	Ared	tnamaioni g G G	27 7 46	3 6	20 20 20 30 50 50 50 50 50 50 50 50 50 50 50 50 50	8.51 19.42 19.42 5.02 7.290	5.67 32.00 9.98 46.24 9.98 46.24	\$ 1 d
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Population Area	- m	00°0	550	2000	98 6	equivalent value	I and I in Design	in the column Elevation	indicates the distance findicates for an exto	
Area by Land Use and	Areo Areo Areo Areo Areo Desidential Industrial School School Industrial School Industrial School Industrial School Industrial Areo Areo Areo Areo Deputation Deputat	0000 1000	7.56 9.26 3.038 3.59 7.506 1.800 1.40 1.39 2.00 2.00 1.40 1.39	3	18007200 106778038 1800 1.20 610 2255 18007200 1.20 610 2255 50 6007200 1800720 1800 1800 1800 1800 1800 1800 1800 18	Note: 13 All populations present	2) For Molleration columns	3) Figures in parentheses	a) For the remarks, a) U 100m: b) Drain	

	6																											,	
	0.610 (600)* 0.292 1.916 0.152	0	0.759	0.732	0.673	0.642	0.609	0.592	0.574	0.556	0.537	٠.	0.517	0.497	0.476	0.454	0.430	0.406	0.380	0.351	0.340	0.327		0.321	0.314	0.301	0.287	0.280	
		>	2.598	2.503	2.303	2.196	2.083	2.024	1.964	1.902	1.837		1.770	1.701	1.628	1.553	1.473	1.389	1.299	1.203	1.162	1.120		1.098	1.076	1.030	0.982	0.957	
	34 (525) * 24 78 33	d	0.532	0.513	0.472	0.450	0.427	0.415	0.402	0.390	0.377		0.363	0.349	0.334	0.318	0.302	0.285	0.266	0.246	0.238	0.229		0.225	0.220	0.211	0.201	0.196	
	0.534 0.224 1.678 0.133	5	2.377	2.291	2.107	5.009	1.906	1.852	1.797	1.740	1.681		1.620	1.556	1.490	1.421	1.348	1.271	1.189	1.101	1.063	1.025		1.005	0.984	0.942	668.0	0.876	٠
	57 (450)* 64 36 14	d	0.352	0.339	0.312	0.297	0.282	0.274	0.266	0.257	0.249		0.240	0.230	0.220	0.210	0.199	0.188	0.176	0.163	0.157	0.151		0.149	0.146	0.139	0.133	0.129	
	0.457 0.164 1.436 0.114	٨	2.143	2,065 1,984	1.900	1.811	1.718	1.670	1.620	1.569	1.515		1.460	1.403	1.343	1.281	1.215	 1.145	1.072	0.992	0.958	0.924		906.0	0.887	0.850	0.810	0.789	
	81 (375)* 14 97 95	a	0.216	0.209	0.192	0.183	0.174	0.169	0.164	0.158	0.153		0.147	0.142	0.136	0.129	0.123	0.116	0.108	0.100	0.097	0.093	-	160.0	0.090	0.086	0.082	0.080	
	0.381 0.114 1.197 0.095	<b>&gt;</b>	1.898	1.829	1.683	1.604	1.522	1.479	1,435	1.389	1.342		1.293	1.243	1.190	1.134	1.076	1.015	0.949	0.879	0.849	0.818		0.802	0.786	0.753	0.717	0.699	
٠,	0.304 (300) * 0.073 0.955 0.076	d	0.119	0.114	0.105	0.100	0.095	0.092	0.00	0.087	0.084		0.081	0.078	0.074	0.071	0.067	0.063	0.059	0.055	0.053	0.051		0.050	0.049	0.047	0.045	0.044	
		Þ	1.633	1.574 7.57	1.448	1.380	1.309	1.272	1.234	1.195	1.155	٠	1.113	1.069	1.024	976-0	0.926	0.873	0.817	0.756	0.730	0.704		0.690	0.676	0.647	0.617	0.602	
	29 (225) * 41 19 57		0.056	0.054	0.049	0.047	0.045	0.043	0.042	0.041	0.039		0.038	0.036	0.035	0.033	0.032	0.030	0.028	0.026	0.025	0.024		0.024	0.023	0.022	0.021	0.021	
	0.229 0.041 0.719 0.057	۸	1.352	1.303	1.198	1.143	1.084	1.053	1.022	0.990	0.956	-	0.921	0.885	0.847	0.808	0.767	0.723	0.676	0.626	0.605	0.583		0.571	0.560	0.536	0.511	0.498	
	53 (150)* 18 31 38	d	0.019	0.018	0.017	0.016	0.015	0.015	0.014	0	0.013		0.013	0.012	0.012	0.011	0.011	0.010	600.0	600.0	0.008	0.008		800.0	0.008	0.008	0.007	0.007	
	0.153 0.018 0.0481 0.038	<b>&gt;</b>	1.033	0.996	0.916	0.873	0.828	0.805	0.781	0.756	0.731		0.704	0.676	0.648	0.617	0.586	0.552	0.517	0.478	0.462	0.445		0.437	0.428	0.410	0.391	0.381	
	Dia. of Sewer (m) Sectional Area (m2) Wetted Perimeter (m) Hydraulic Radius (m)	Slope of Sewer (0/00)			0.11					7.5				0.9			4.5	0		3.0	ω	2.6		2.5			2.0	1.9	

\*(009) ot9-0 0.203 0.157 0.143 0.249 0.213 0.181 0.257 0.292 0.792 0.728 0.694 0.659 0.621 0.581 0.538 0.491 0.439 0.932 0.905 0.878 0.850 0.822 0.534 (525)\* 0.224 1.678 0.133 0.127 0.119 0.110 0.101 0.191 0.186 0.180 0.174 0.168 0.162 0.156 0.149 0.142 0.135 0.568 0.532 0.492 0.449 0.852 0.828 0.804 0.778 0.724 0.699 0.666 0.635 0.603 0.457 (450)\* 0.107 0.103 0.099 0.094 0.084 0.073 0.066 0.059 0.126 0.115 0.164 1.436 0.114 0.512 0.444 0.653 0.627 0.601 0.573 0.543 0.747 0.724 0.701 0.678 0.768 0.381 (375)\* 0.114 1.197 0.095 0.052 0.048 0.045 0.041 0.066 0.063 0.061 0.058 0.055 0.078 0.073 0.454 0.424 0.393 0.359 0.321 0.578 0.532 0.507 0.481 0.642 0.621 0.681 0.304 (300)\* 0.028 0.027 0.025 0.022 0.040 0.039 0.036 0.035 0.033 0.032 0.043 0.073 0.498 0.478 0.458 0.390 0.365 0.338 0.309 0.436 0.586 0.569 0.552 0.535 0.516 0.414 0.229 (225)\* 0.041 0.719 0.057 0.012 0.017 0.016 0.016 0.015 0.013 0.020 0.019 0.019 0.018 0.018 0.323 0.302 0.280 0.256 0.256 0.412 0.396 0.379 0.361 0.343 0.471 0.428 0.485 0.153 (150)\* 0.018 0.481 0.038 0.005 0.004 0.004 0.004 0.006 0.005 0.007 0.006 0.247 0.231 9.214 0.195 0.370 0.360 0.349 0.328 0.315 0.303 0.290 0.276 0.262 Dia. of Sewer (m) Sectional Area (m<sup>2</sup>) Wetted Perimeter (m) Hydraulic Radius (m) Table K-2 (continue) Slope of Sewer (00/0) 1.8

Note: V: Full Velocity (m/s) Q: Full Capacity (m<sup>3</sup>/s)

Note: V: Full Velocity (m/s) Q: Full Capacity (m<sup>3</sup>/s)

- continue -

	* (0)																								
	1.372 (1,850)* 1.478	310	543			2,364	2.298	2.229	2,158	2,085			2.00%	1.930	1.348	1.762	600	7.0.7	1.576	1.474	11	T- 200	1.246	1.114	
		4, (	o'		۸	1.599	1.554	1.508	1.460	1.410		,	4.359	1.306	1.250	1,192	1 6	707.7	1.066	700		0.925	0.843	0.754	
	1.219 (1,200)* 1.167	ج	. 05		d.	1.725	1.676	1.626	1.575	1,521	i i		1.466	1.408	1.348	286	) ( ) (	7-750	1,150	570 L	0.0	0.770	0.909	0.813	
		m	0		Δ	1.478	1.436	1,393	1.349	1,303	)	1	1.256	1.207	1,155	100	\$ L	T- 045	0.985	0000	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.853	0.779	0.697	
	66 (1,050)* 92	49	99		8	1.206	1.172	1.137	1.101	1.064	; ) )		1.025	0.985	0.943	000	0 0	508.0	0.804		707.0	0.696	0.636	0.569	
	1.066	3.3	0.2			1.352	1.313	1.274	1.234	192	1		1.149	1.104	1.057	100	` · ·	0.956	0.901.		7 1	0.780	0.712	0.637	
	15 (900)* 58	75	29		O	0,803	0.780	0.757	0, 733	802.0			0.682	0.655	0.627	0 0	0.0	0.568	533		TOCTO	0.463	0.423	0.378	)
	0.915	2.8	0.0		>	1 221	1.186	1.151	1.114	7.00	· · · ·		1.037	0.997	0.0 4.0		0.9TO	0.863	0.81A		79/.0	0.705	0.643	0.875	
	38 (825)* 52	33	10		Ø	A 25.	0.617	66.0	0.80	0.0	000.0		0.540	0.518	907	7 7 7	2.4.0	0.449	0.423	1 6	0.390	0.367	0.335	800	
	0.838	2.6	0.0		Λ		0	יוני מ נימ	1001	1 4	CTO - T		0.978	0.940	000	000	0.828	0.814	737 0		0.78	0.665	0.607	. K. C.	, ,
÷	0.762 (750)*	94	.91		Ø	6	0 C	7 7 7	450	) L	0.435		0.419	0.402	1 U	0 1	0.367	0.348	0000	0.70	0.307	0.284	0.260	0.030	
		2.3	0.3		Þ	000	1.050 1.050	000	980	0 0			0.918	0.882	0 0	0.040	0.802	0.764			0.674	0.624	0.569	0 0	
	0.685 (675)*	52	.71		O	170	30.0	000	330	0.00	0.327		0.315	20%		0.190	0.276	0.262	,		0.231	0.214	0.195	) u	0.1.0
		~			٥		F-000	0.00	0 to 0	n (	0.888		0.855	0000	0 0	0.797	0.750	0.712	į	1,0	0.628	0.581	0 0		7.4.0
	Dia. of Sewer (m)	Wetted Perimeter (m)	Hydraulic Radius (	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	(0/00)	•	o :	· .	0 u	C*T	1.4		E	) C	7.	T•T	7.0	6.0	(	».	0.7	9.0	) (	n •	4.0

Note: V: Full Velocity (m/s) (Q: Full Capacity (m<sup>3</sup>/s)

## APPENDIX L

ANALYSIS FOR WATER POLLUTION CONTROL

### 1. General

Alor Setar is a town developed in the tributary area of the Sg. Kedah and Sg. Anak Bukit. From the town wastewater including domestic, commercial and industrial wastes are discharged into the rivers through existing drains, and dominantly contribute to the present river pollution. Water pollution of the rivers is increasing with the expansion of Alor Setar. Thus it is evident that river pollution will become more severe in the future unless adequate pollution control measure is taken.

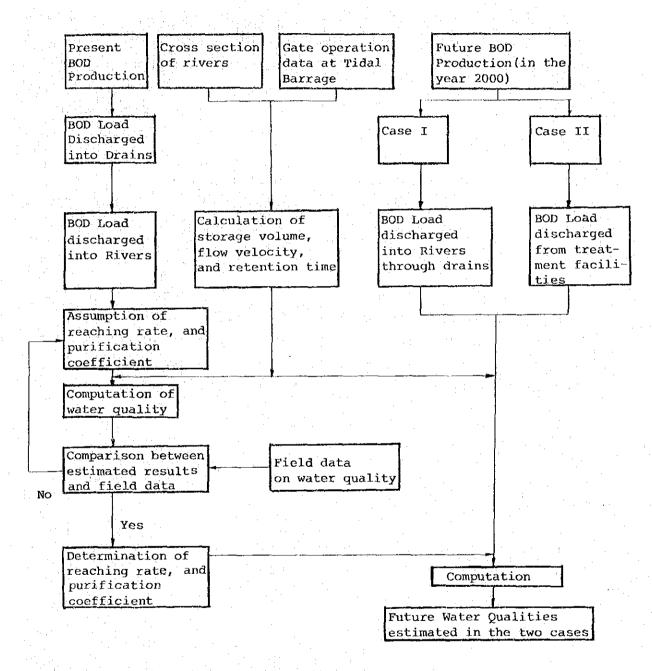
The two rivers had been tidal rivers before the barrage was constructed at the point of a little downstream from confluent point of the two rivers. After construction of the barrage, the flow rate and water quality of the rivers are greatly influenced by the gate operation.

The gate operation is largely changed by season. In rainy season, the gates are opened at least once a day, and especially in monsoon season, a whole day. In dry season, however, the gates are opened only once a few days, or for navigation of boats through the barrage (the gates operation data for past one year are attached at the end of this appendix).

In this Appendix the effects of sewerage system on water pollution control of the two major rivers are studied towards the future in contrast with the case without the system.

The system analysis on the simulation of BOD load to the river system is carried out on the flow sheet shown in Figure L-1.

Figure L-1 Flow Sheet for Waste Load Simulation



Note: Case I : No sewerage system is provided

Case II : Sewerage System is provided

# 2. Physical Conditions of the River System

## 2.1 Slope of River-bed and Cross Sectional Area

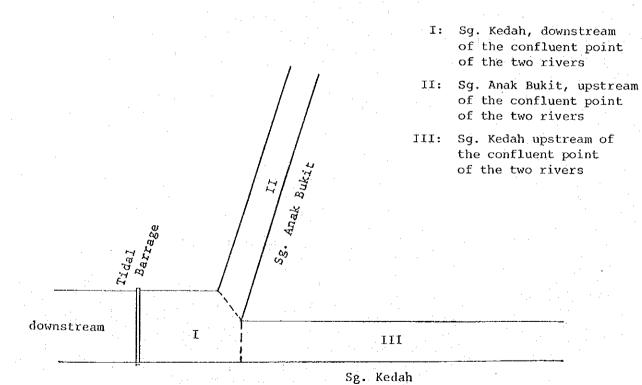
## a. Slope of River-bed

Based on the data obtained from MPKS, average slope of riverbed is assumed as 0.0084% for both rivers, i.e. Sg. Kedah and Sg. Anak Bukit.

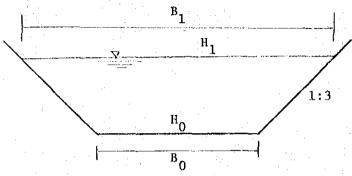
#### b. Cross section

For modelling the river system the two rivers in the Study Area are divided into three reaches as shown in Figure L-2, and the cross section of each is assumed as shown in Figure L-3.

Figure L-2 Schematic Plan of Rivers



(from the tidal barrage to the confluent point Sg. Kedah of the two rivers)



H<sub>1</sub>: River stage (m)

H<sub>0</sub>: River-bed elevation (m)

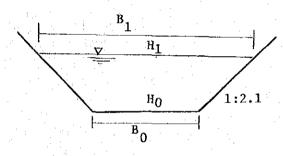
Width of water surface (m)

Width of river-bed (m)

$$B_0 = (H_0 + 15.7) \times 6.0$$

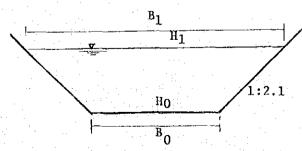
 $B_1 = (H_1 + 15.7) \times 6.0$ 

Sg. Anak Bukit II.



 $B_0 = (H_0 + 8.6) \times 4.2$   $B_1 = (H_1 + 8.6) \times 4.2$ 

( upstream of the confluent point of the Sg. Kedah two rivers)



 $B_0 = (H_0 + 13.4) \times 4.2$ 

 $B_1 = (H_1 + 13.4) \times 4.2$ 

Based on the assumptions and formulae developed and shown in Figure L-3, the elevation and width of the river-beds at key points of each reaches are calculated as shown in Table L-1.

Table L-1 Elevation and Width at Key Points along the Rivers

Distance	Sg. Kedah	Sg. Kedah		Sg. Anak Bukit		
from Tidal Barrage (km)	Elevation of River-bed (m)	Width of River-bed (m)	Elevation of River-bed (m)	Width of River-bed (m)		
0.00	-3.568	72.252	-	••		
1.44	-3.537	72.978	-3.537	21.265		
		41.425	•	*		
4.32	-3.295	42.441	-3.295	22.281		
7.20	-3.053	43.457	-3.053	23.297		
10.08	-2.811	44.474	-2.811	24.314		

### 2.2 Hydraulic Model

The elements of the hydraulic model are considered on the serial stretches of the rivers as shown in Figure L-4, and are presented by the following equations;

$$V_{Ni} = V_{(N-1)o},$$

$$V_{Nn} = V_{N(n-1)} - V_{No} + V_{Ni} - V_{Ne} + V_{Nw},$$

where

 $V_{Ni}$ : Inflow volume into stretch N (m<sup>3</sup>/day),

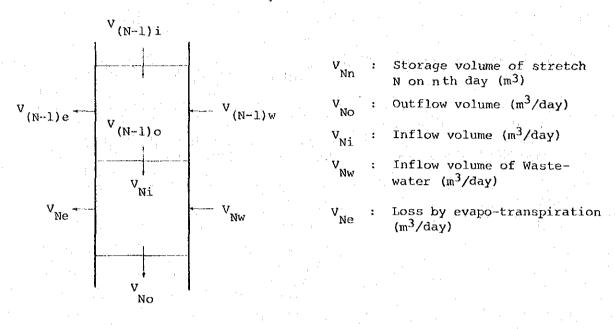
 $V_{NO}$ : Outflow volume from stretch N (m<sup>3</sup>/day),

 $v_{Nw}$ : Inflow volume of wastewater from the waterbed of stretch N (m<sup>3</sup>/day),

 $V_{Ne}$ : Loss by evapo-transpiration ( $m^3/day$ ),

 $v_{Nn}$  : Storage volume of stretch N on n th day (m $^3)$ 

Figure L-4 Schematic Hydraulic Model for a River System

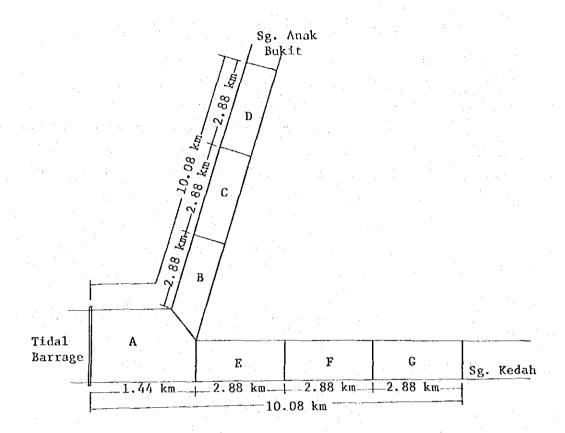


The study area of this river analysis is confined as the reaches from the tidal barrage to 10.8 km upstream of the rivers and their tributary areas inside the Study Area boundary of the Master Plan.

To make the hydraulic model of the river system, the reaches of the rivers are further divided into a 7 stretches as shown in Figure L-5. And the river stage of each stretch is assumed to be horizontal regardless upstream or downstream because the rivers can be considered as an isolated pond in the reaches studied.

Each element of the hydraulic model of the rivers are estimated as follows;

Figure L-5 Rivers Divided into Seven Stretches



### a. Storage Volumes of Each Stretch

Based on the cross section model shown in Figure L-3 and average slope of river-bed of 0.0084%, storage volumes of each stretch in the river system are calculated by using the derived formulae as follows:

$$V_{A} = 4.32 \text{ H}^{2} + 135.70 \text{ H} + 432.44$$

$$V_{B} = 6.05 \text{ H}^{2} + 104.05 \text{ H} + 284.75$$

$$V_{C} = 6.05 \text{ H}^{2} + 104.05 \text{ H} + 269.25$$

$$V_{D} = 6.05 \text{ H}^{2} + 104.05 \text{ H} + 253.04 \qquad (2-1)$$

$$V_{E} = 6.05 \text{ H}^{2} + 162.14 \text{ H} + 483.11$$

$$V_{F} = 6.05 \text{ H}^{2} + 162.14 \text{ H} + 453.56$$

$$V_{G} = 6.05 \text{ H}^{2} + 162.14 \text{ H} + 423.31$$

$$\Sigma V = 40.62 \text{ H}^{2} + 934.27 + 2599.46$$

where

H : River stage (m)

 $V_A - V_G$ : Storage volume of each stretch (in 1,000 m<sup>3</sup>)

b. Estimation of  $V_{\mbox{Ni}}$  and  $V_{\mbox{No}}$ 

 $V_{\rm Di}$  and  $V_{\rm Gi}$  are the inflow volumes of the rivers, Sg. Anak Bukit and Sg. Kedah. Those volumes can be estimated from the flow records, and are shown in Figure L-8 together with the other estimated volumes of each element.

As mentioned previously, the tidal barrage which has the main gates and the navigation lock is intermittently opened for flood control and/or navigation.

To estimate the outflowing volume,  $V_{\mbox{AO}}$ , through stretch A the records of the river stages and the gate operations were analyzed and summerized as follows:

- (1) The gate opening period differs significantly between dry and rainy seasons
- (2) The difference of the river stage before and after the gate opening ranges from 1.2 m to 0.25 m.
- (3) Average gate opening frequency is once in 4.7 days in dry season, and once in 0.7 day in rainy season.

Based on the data mentioned above and applying the equation (2-1), outflow quantities through the tidal barrage were assumed as follows:

- (a) Outflow quantity through a main gate operation:  $256,000 \text{ m}^3$
- (b) Outflow quantity through navigation lock: 3,000 m<sup>3</sup>/day

Therefore, average daily outflow volume through the barrage,  $\mathbf{V}_{\mathtt{AO}}$ , was obtained as follow:

- (c) In dry season:  $256,000/4.7 + 3,000 = 57,470 \text{ m}^3/\text{day}$
- (d) In rainy season:  $256,000/0.7 + 3,000 = 368,710 \text{ m}^3/\text{day}$

The gate operation frequency will be changed in the future by the increase of wastewater. The drequency and outflow volume in the year 2000 were estimated as follows.

- (1) In case no sewerage system is provided: once per 3.21 days  $82,690 \text{ m}^3/\text{day}$
- (2) In case sewerage system is provided: once per 2.09 days  $125,150 \text{ m}^3/\text{day}$

# c. Estimation of V

Inflow volumes of wastewater to each stretch ( $V_{Nw}$ ) were estimated on the basis of population and water consumption estimated, and are summerized in Table L-2.

Discharge points of wastewaters from tributary areas to each stretch of the rivers are assumed as shown in Figures L-6 and L-7 for two cases that sewerage system is not provided and is provided.

# d. Estimation of V

Average evapo-tranpiration rates in dry and rainy seasons are assumed to be 5.1 mm/day and 3.3 mm/day respectively, based on the record obtained from the Meteorological Station, ALOR SETAR.

Infiltration rate of the river water is disregarded in this study due to lack of data applicable.

The hydraulic model of the river system at present and in the future are summarized in Figure L-8.

Figure L-6 Discharge Points of Wastewater from Tributary Areas (In case sewerage system is not provided)

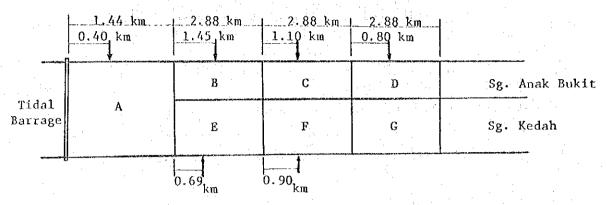
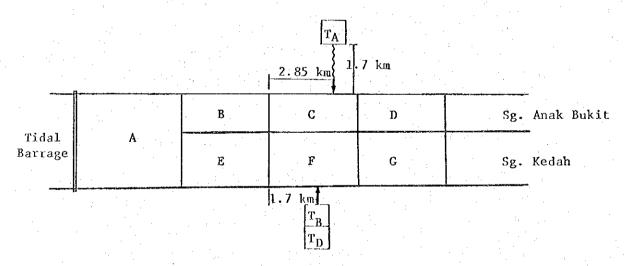


Figure L-7 Discharge Points of Wastewater through Treatment Facilities (In case sewerage system is provided)

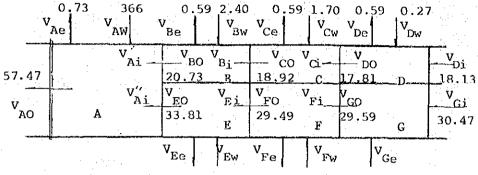


where

T: Treatment facilities

1. Dry season (Present Condition)

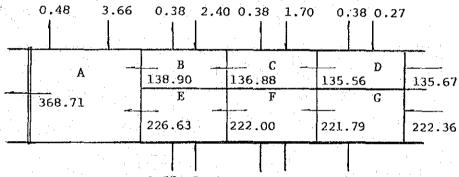
Unit 1,000 m<sup>3</sup>/day



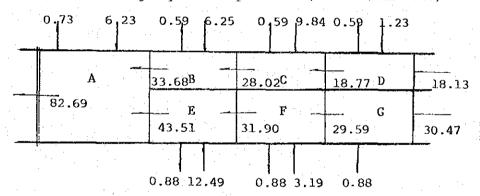
0.88 5.20

0.88 0.78 0.88

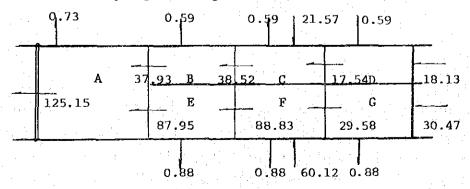
2. Rainy Season (Present Condition)



0.57 5.20 0.57 0.78 0.57 3. Case I : No sewerage system is provided (in the Year 2000)



4. Case II: Sewerage system is provided (in the Year 2000)



### 2.3 Flow Velocities in Each Stretch

Average flow velocity in a given stretch of the river system is obtained by dividing outflowing volume Vo by average sectional area of the stretch.

Estimated average flow velocities in each stretch of the rivers are summarized by case Table L-2.

Table L-2 Estimated Average Velocity in Stretches of the Rivers

	:	·	<u>. i j. v.</u>	- 14	1	<del></del>	(km/	'day)
G.				Sta	etch		:	
Çd	ise and the second	A	В	С	D	E	F	G
	Dry season	0.145	0.151	0.144	0.141	0.150	1.137	0.144
Present	Rainy season	0.927	1.013	1.039	1.075	1.002	1.028	1.080
Future sew	In case no sewerage system is provided	0.208	0.246	0.213	0.149	0.192	0.148	0.144
	In case sewerage system is provided	0.315	0.277	0.292	0.139	0.389	0.411	0.144

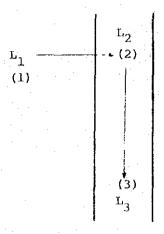
Note: Average river stage adopted is assumed to be 1.0 m.

# 3. Simulation Model for Waste Loads (BOD)

# 3.1 Model Develop

Waste organic load ( $L_1$ ) originated in a town area (point 1) is reduced in the drain system and discharged into the river. The amount of the wastes ( $L_2$ ) discharged into the river is further reduced by some mechanisms such as biodegradation and precipitation to the amount of  $L_3$  during travelling in the river (from point 2 to point 3).

Figure L-9 Fate of Waste Organic Load



L, : BOD load Produced at Point (1)(kg/day)

L<sub>2</sub>: BOD load which reaches a main river, Point (2) (kg/day)

L<sub>3</sub> : BOD load which arrives at Point (3) (kg/day)

Although BOD reduction rate in a river ( $\beta$ ) is affected by microbic condition, flow velocity, travelling time, etc. BOD content at a given point in the river ( $L_3$ ) is obtained by following equation (3-1) which is usually applied to a stabilization pond because the river conditions are almost similar to that of a pond in dry season.

$$L_3 = \beta . L_2 = \frac{L_2}{1 + kt}$$
 (3-1)

where

β : BOD reduction rate

k : purification coefficient

t : travelling time from inlet point to a given point

The value k=0.23 (base e) is adopted at 20°C, and its variation with temperature is described by equation (3-2).

$$k(T) = k(20) \times \theta^{T-20}$$
 (3-2)

where

k(T) : k value at T°C (1/day)

0 : Arrhenius coefficient, 1.08 for stabilization pond

Assuming water temperature as 30°C, k value is calculated as follow;

$$k(30) = 0.23 \times 1.08^{10}$$
$$= 0.495$$

Travelling time (t) is calculated by the following equation;

#### where

L : distance between points 2 and 3 (km)

v : velocity (km/day)

### 3.2 BOD Load Discharged

Present and future BOD Loads originating each source, i.e. human excreta and sullage water, are estimated based on the following steps;

- (1) to estimate present and future population in tributary areas of each stretch of the rivers,
- (2) to estimate population and BOD Load with respect to human excreta disposal systems,
  - a. BOD load removed through septic tank is assumed to be 50 percent, thus BOD load discharged from sources is calculated to be 6.5 g/cap.day.
  - b. BOD load discharged by Buket system is assumed to be nil.
  - c. BOD load discharged through latrine over waterways is assumed to be 13 g/cap.day.
- (3) to estimate BOD load with respect to sullage water.
- (4) to estimate BOD load through the sewerage facilities to be provided.

BOD Loads discharged or to be discharged into each stretch in the rivers are calculated and summarized in Table L-3. For the future BOD Loads, it is assumed, in case no sewerage system is provided, that septic tank system will be provided to remove human excreta from the Study Area. While in case sewerage system is provided, all sanitary wastes, i.e. toilet wastes are sullage water, are discharged through treatment facilities with the effluent quality of 50 mg/l (BOD).

Table L-3 Present and Future Wastewater Volumes and BOD Loads

	Present	Future (2000)			
	rresent	Case :	I	Case	ΙΙ
Stretch of River	Waste- BOD water (1,000 m <sup>3</sup> /day) (kg/day)	Waste- water	BOD Load	Effluent through Treatment Facility (1,000 m <sup>3</sup> /day)	through Treatment
A	7.31 1,054.1	12.47	1,973.8	A 21.57	1,078.4
• В	4.80 829.7	12.50	2,018.6	0	0
С	3.40 629.7	19.68	3,384.7	0	0
<b>D</b>	0.54 89.2	2.96	422.4	0	0
E	10.40 1,901.4	24.97	4,295.9	0	0
F	1.55 242.5	6.37	1,095.6	B 36.39 D 23.73	1,819.7 1,186.3
Total	28.00 4,746.6	78.45	13,191.0	81.69	4,084.4

Note: Case I : No sewerage facility is provided.

Case II : Sewerage facility is provided.

# 3.3 Existing Water Pollution in the River System

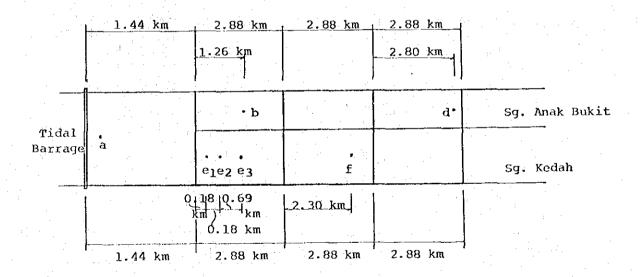
Field data on BOD content of the river water were obtained by the survey conducted for the Master Plan, and are summerized in Table L-4. The locations of the sampling points are shown in Figure L-10.

Table L-4 BOD Contents in Sg. Anak Bukit and Sg. Kedah

化光光 化基金光谱 医多种	
Dry Season	Rainy Season
14 (21/3)	3.8 (17/6)
16 (21/3)	7.0 (17/6)
	3.4 (8/7)
	3.6 ( 3/7)
17 (21/3)	2.1 (18/6)
	2.3 (18/6)
	1.4 (18/6)
	14 (21/3) 16 (21/3)

Note: Figures in parentheses indicate the date surveyed. Sampling points are shown in Figure L-10.

Figure L-10 Locations of Sampling Points



## 3.4 Fitting the Model to the Field Data

Three sampling points were selected as monitoring points of the water quality of the river system, which are Points a, b and e2 shown in Figure L-10. Those points are located at just upstream of the tidal barrage, Jl. Putera cross of Sg. Anak Bukit, and Jl. Sungai Korok cross of Sg. Kedah respectively.