

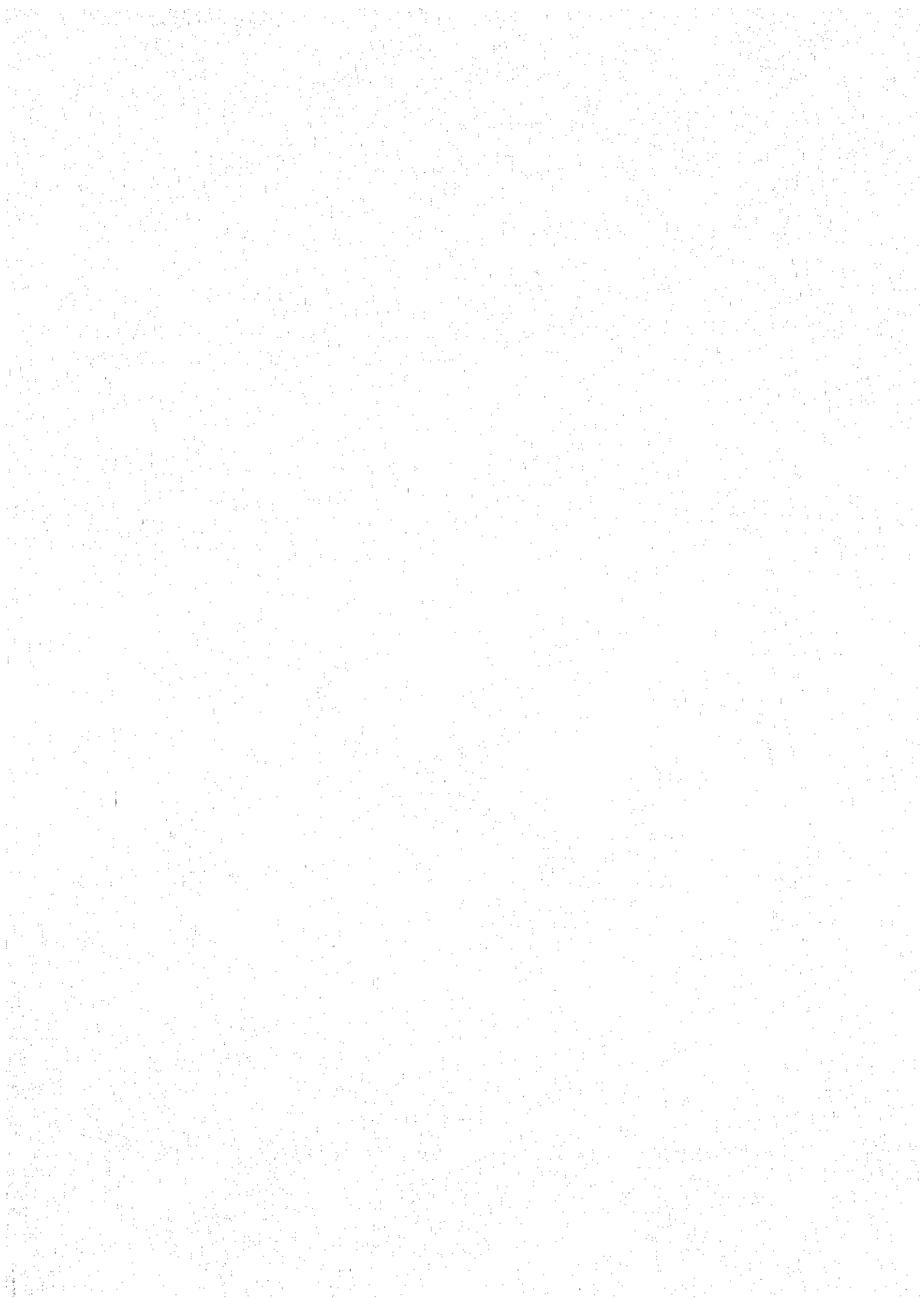
REPORT  
FOR  
THE FEASIBILITY STUDY  
ON  
THE REINFORCEMENT AND EXPANTION PLAN  
OF  
P.T. IKI MAKASSAR SHIPYARD AT UJUNG PANDANG  
IN  
THE REPUBLIC OF INDONESIA

SUPPLEMENTARY DATA

1. SURVEYING
2. INFRASTRUCTRE
3. SOIL INVESTIGATION

MARCH 1981

JAPAN INTERNATIONAL COOPERATION AGENCY



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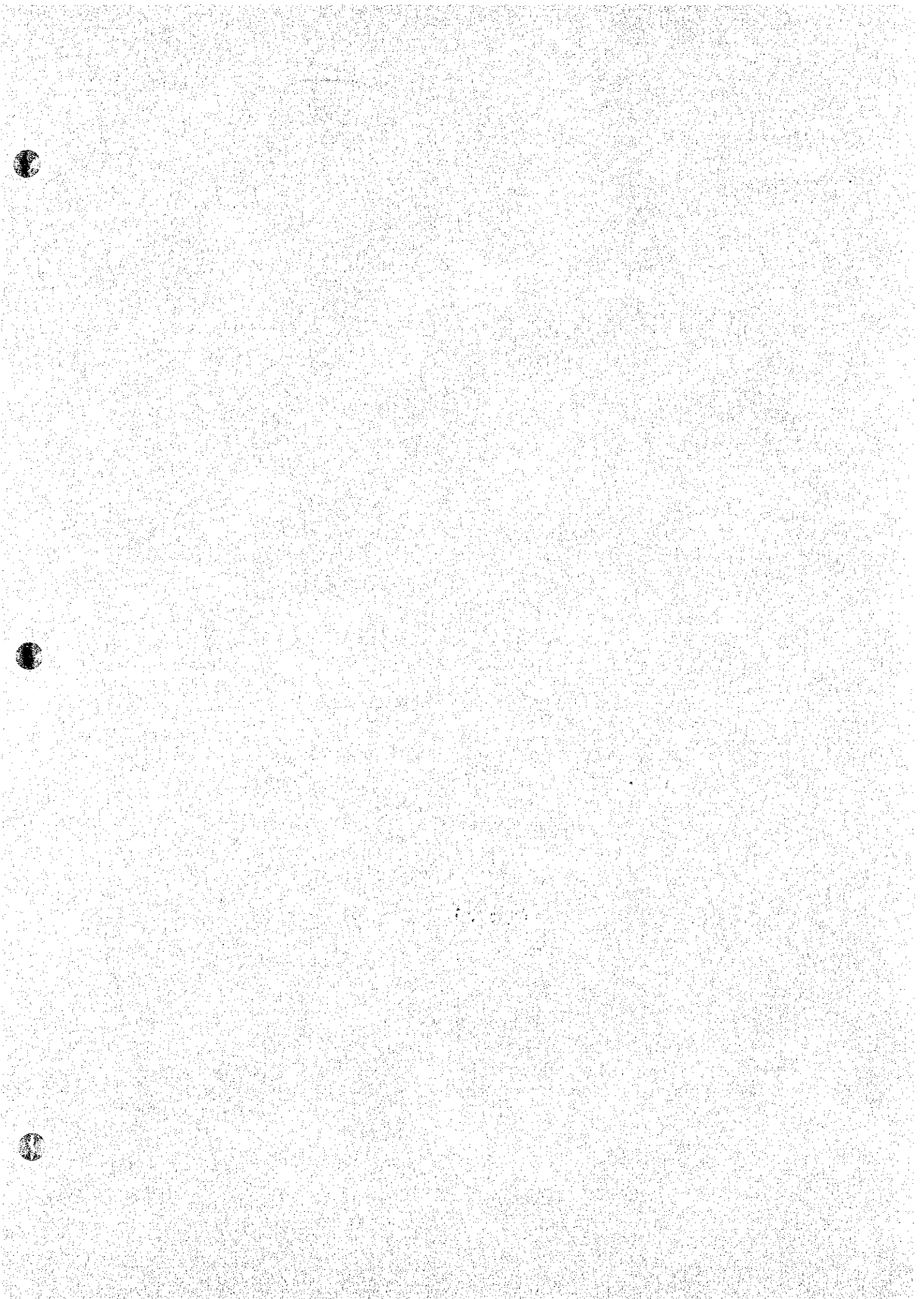
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## 1. SURVEYING

### 1.1 Purpose

The purpose of surveying and investigation is to acquire fundamental information required for improvement plan of Makassar Shipyard.

### 1.2 Items to be Surveyed

- (1) Control point surveying and traversing
- (2) Topographic surveying  
(cross-leveling)
- (3) Planimetric surveying
- (4) Sounding

### 1.3 Surveying Instruments Used

	<u>Manufactured by</u>	<u>Model</u>
(1) Theodolite	Sokkisha	TM-20D
(2) Auto-level	"	B-1
(3) Distance meter	Topcon	DM-C1
(4) Echo sounder	Kaijyo Denki	
(5) Kit for plane tabling		
(6) Tape, staff, pole, etc.		

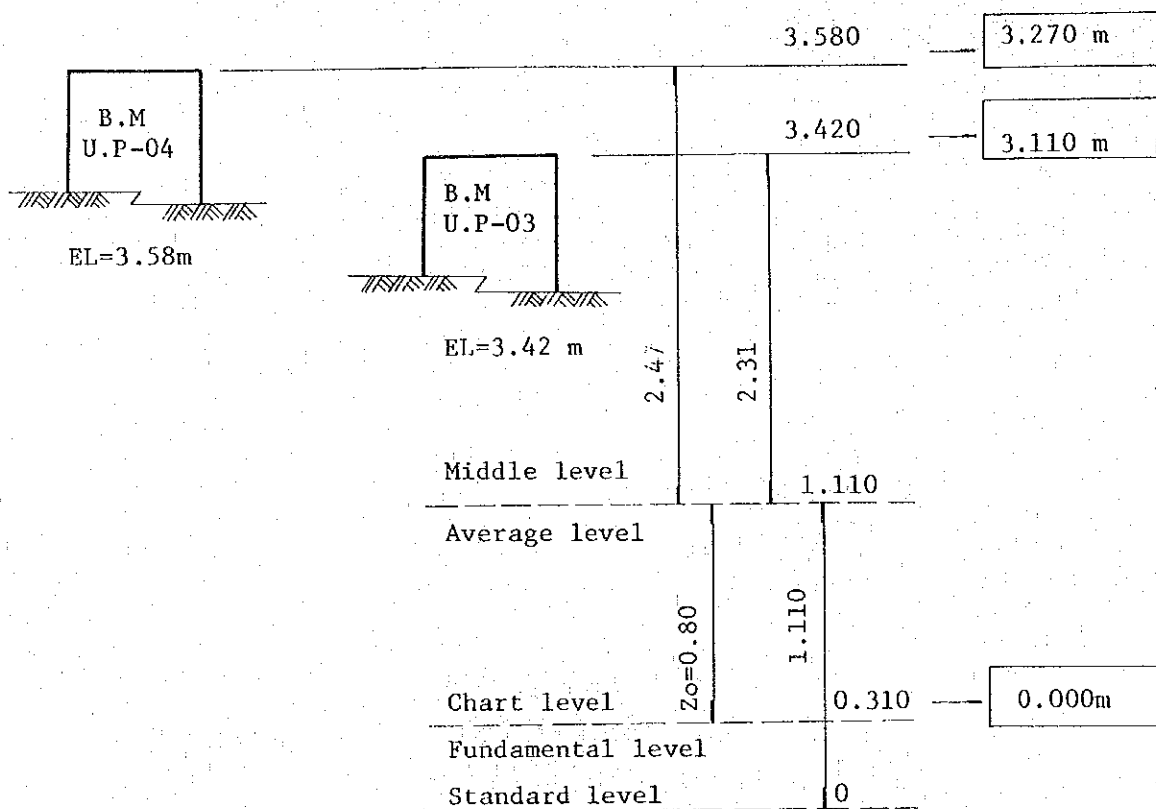
### 1.4 Method of Surveying

#### 1.4.1 Control Point Surveying

Fig. 1 shows the topography of the project area which is based on the result of a topographic survey and sounding.

The elevations in Fig. 2 are calculated on the basis of the data of the Ujung Pandang Port Office, on condition that the chart level is + 0.00m.

Fig. 2



: elevation with chart level + 0.00m  
 BM : bench-mark

The shipyard construction site was reclaimed about 18 years ago. It is mostly flat, 1.0m - 2.5m above the sea level. A part of the revetment in the northeastern site is broken down, and as a result of the outflow of sand and earth, the northeastern site is a low and swampy zone. Sea area around the shipyard is shallow over a long distance from the shore. Sea route was dredged at a depth of minus 4 meters, thereby facilitating the arrival and departure of vessels. However, further dredging will be required for vessels to be constructed at the shipyard in the future, because of narrow course and insufficient depth of water.

### Observation

Table 1 presents the results obtained by leveling from A & B routes between established bench marks (B.M-1). An error is proportionally allotted by the distance between B.M (UP-03) and B.M-1, and as a result, the error of closure is 4mm. (see Fig. 16)

Table 1. Observed error of bench mark

Bench mark	Length	Difference in distance of both ways between bench marks	Error of closure
B.M			
UP-03	-	-	-
No. 1	0.9 Km	2mm	-
No. 2	0.9	7	-
No. 3	0.9	2	-
B.M-1	1.3	4	4mm
Total	4.0	B.M-1	EL = 2.520m

### 1.4.2 Traversing

A driver pile is established by selecting a clear point within the proposed site.

After a traverse point is established, the trees and plants are cut down to secure the visibility of piles. (see Fig. 15)

### Observation

The driver pile is established at the desired place, and observation is made in each point.

Observation of angle and distance measurement is made by using a distance meter and theodolite.

As for the observed results, calculation is made by using an angle measurement, and a value measured by the distance meter. As for the coordinate value, calculation is made without employing the angle measurement and the measured value of distance.



Table 2. Observed error of driver net

Point	Error of closure	Ratio of closure
T-1	0.114	1/16,700
T-2	0.045	1/33,000
A-1	0.058	1/ 8,000
B-1	0.062	1/ 5,300
C-1	0.110	1/ 8,700

#### 1.4.3 Topographic Surveying (cross-leveling)

After establishing points for cross-leveling on a revetment at intervals of 25m prior to surveying, and cutting the trees and plants in the perpendicular to the revetment, elevation of topographic variation point is observed with an auto-level.

#### 1.4.4 Planimetric Surveying

Planimetric surveying is conducted in the projected site (about 14 ha.). The topographic plane of the site is drawn to a scale of 1:500, and the topographic plane of a harbor and sea is drawn to a scale of 1:1,000.

#### 1.4.5 Sounding

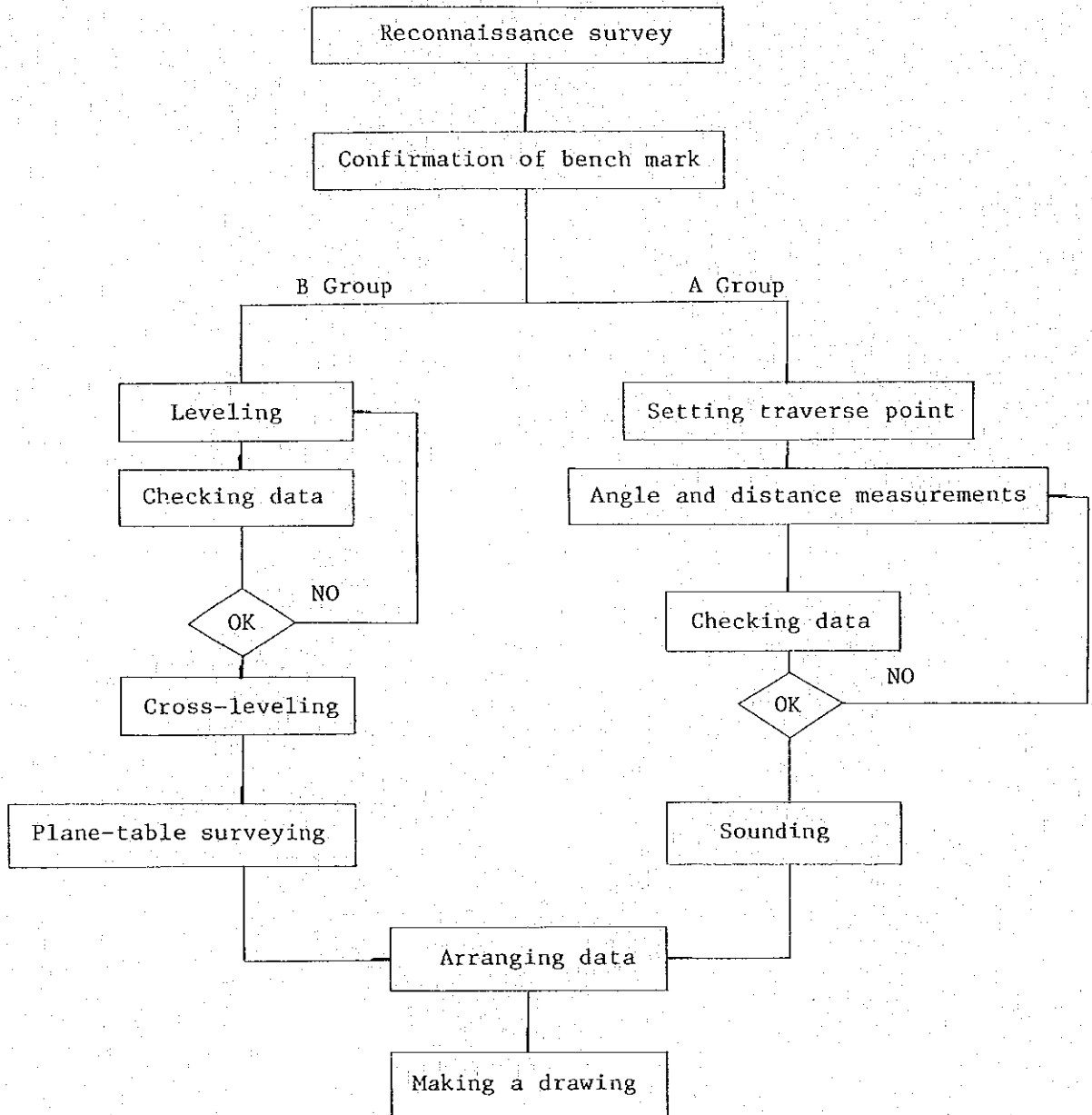
To investigate the condition of the seabed and topography within the proposed site, the following survey is made:

Sounding is performed using an echo sounder in the harbor and a range of 1600m along the revetment and 600m at sea. Points of 200m, 400m and 600m are measured applying a method of intersection and resectin and using a tape (for marine survey) at 200 meters' distance from the revetment and within the harbor.

#### 1.5 Observing Tide Level (see Fig. 3)

Setting up a staff gauge at the revetment of P.T. IKI Shipyard, a visual observation of tide level is regularly made, and the observed results are represented as a tide curve. Since the observation and record of tide level are made during a short period, a statistical analysis is not made.

Fig. 4 Flowchart of Surveying Works



## 2. INFRASTRUCTURE

### 1. Road

Fig. 5 shows the road network in the suburbs of Ujung Pandang city. Random asphalt-paving road accounts for about 80% of the city, and the remaining 20% is gravel road.

There is only Gowa-Jaya Road (about 20km in length) leading from the Hasanuddin Airport to the city, and the traffic situation of the existing road is very bad. For further development of South Celebesu, the government of Indonesia plans to widen the Gowa-Jaya Road and construct a bypass, of which the work will commence on 1981. The Tallo River Bridge is under construction with a target date of December, 1980 for completion.

### 2. Waterworks

Water supply capacity to the city is 500 lit./sec. A 50 mm $\phi$  pipe is used for supplying water to the shipyard where water consumption is currently only 10 tons per day.

A plan is underway to raise the water supply capacity. In the near future, 350 mm $\phi$  pipe will be installed at a main line located 500 meters away from the shipyard. As a result, the water supply capacity will increase to 1,500 lit./sec. (See Fig. 6.)

Therefore, the supply of the water required after the shipyard expansion will be possible.

### 3. Electric Power

Electric power for Ujung Pandang city is primarily supplied by a thermoelectric power station (equipped with two units of 12,500 KW steam turbine) along the Tallo River. Addition of 720 KW generated by a diesel engine and 9,250 KW generated by a Bontoard diesel engine amounts more than 40,000 KW, of which about 10% is an actual amount of electric power consumed. Thus, it is understood that the city is sufficiently capable of supplying electric power. (see Fig. 7.)

### 3. SOIL INVESTIGATION

#### 3.1 Methods

##### 3.1.1 Boring

Boring survey is conducted by use of two boring machines of hand-feed type (Bell 2).

Diameter of boring hole is 66 to 86mm $\phi$  at the places where the standard penetration test is performed, and 86 to 116mm $\phi$  at the places where the thin-walled sampling is performed.

To protect a wall for boring hole, a casing pipe is used to a depth of 6 to 8m below the surface of the ground that the wall for boring hole is able to stand itself. A slurry is used to a depth of more than 8m below the surface of the ground. The boring survey is conducted until the bedrock is confirmed to a depth of more than 5m. A marine survey is conducted on a scaffolding, the dimensions of which are 6m x 6m in width and about 4m in height. The location of boring points is shown on Fig. 17.

##### 3.1.2 Standard Penetration Test (SPT)

For the purpose of extracting samples of soil and studying a relative strength of soil, the SPT is conducted at all boring places at intervals of 1m. The SPT is not performed to a depth that a disturbed sample is extracted. A test method shall conform to the standards given in JIS-A-1219. The number of blows (N value) is measured to penetrate a sampler for the SPT to 30cm deep layer by dropping a knocking hammer weighing 63.5 kg from a height of 75cm. The sampler is penetrated to a depth of more than 30cm solely by the knocking hammer's own weight, because the clayey soil of the survey site is poor. In this case, the N value is recorded as zero. A part of samples obtained by the SPT is used for physical test, and the remainings are put into a sample bottle and stored in the site.

##### 3.1.3 Undisturbed Sampling

A thin-walled sampling is conducted to extract an undisturbed sample which is used as specimen for dynamic testing. A thin-walled sampler of fixed piston type, and stainless sampling tube having an ID of 75mm and a wall thickness of 1.5mm are used.

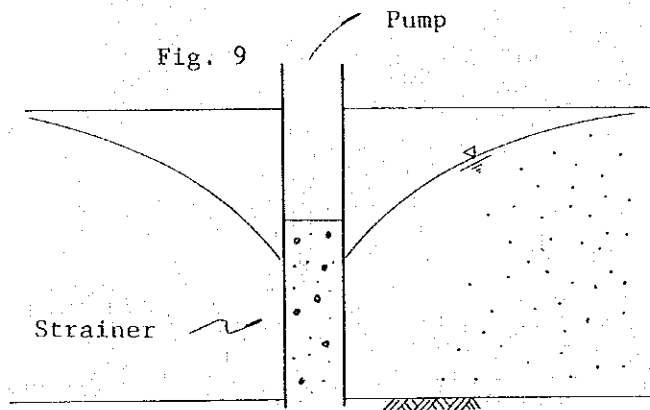
### 3.1.4 Swedish Sounding (SS)

Swedish sounding is performed for the purpose of determining a relative strength of soil and a depth of bedrock to facilitate the boring survey. The relationship between load and the amount of penetration is determined by using a testing machine as shown in Fig. 8 and applying a load of 5 to 100kg. When the penetration to 100kg load stops, the relation between a half rotation of handle and the amount of penetration is determined by rotating a handle of sounding. A half rotation reaches 700 to 800 times when converting data of this relation between them to the amount of penetration per 1m, the SS is judged to be impossible and the test is completed.

### 3.1.5 Field Permiability Test (FPT)

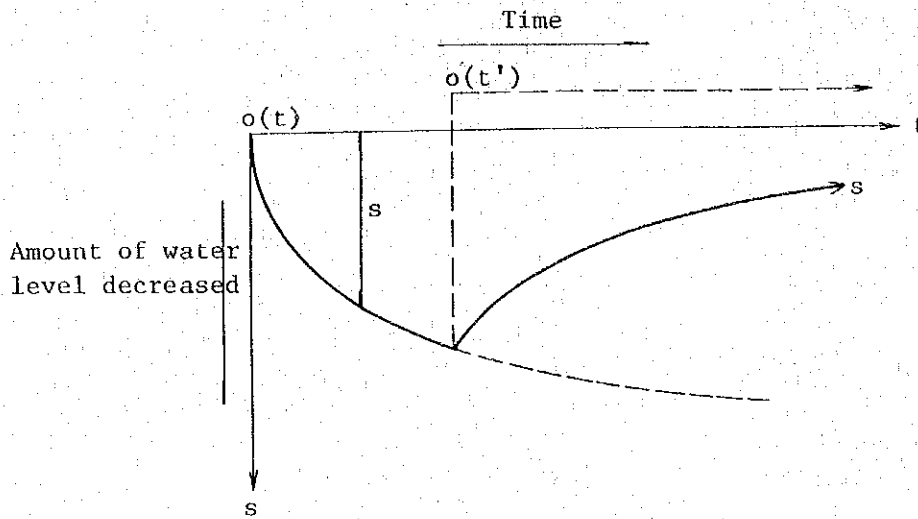
Water needs to be treated in conjunction with an excavation work, because about 7m-deep excavation must be done to construct a dock. For water treatment planning, it is necessary to determine the coefficient of permiability in the upper sandy layer, and the FPT is conducted at two places where a dock will be built. The test is done in accordance with recovery method by single well and by utilizing a boring hole.

(1) Recovery method by single well is applied by providing a pumping well as shown in Fig. 9.



During the test, the operation of puming-up continues for a given time and stops. Time( $t$ ) and the amount of water level decreased( $s$ ) after the operation of puming-up starts, and time( $t'$ ) and the amount of recovery( $s$ ) after the operation of pumping-up stops, are measured, and then the coefficient of permiability is given by the following equation:

$$T=(k \times D)=2.30Qp/4rs \times \log_{10}t/t'$$



where,  $T$  = coefficient of permeable amount, cm/sec  
 $k$  = coefficient of permeability, cm<sup>2</sup>/sec  
 $D$  = length of permeability, cm  
 $Q_p$  = amount of pumping-up, cm<sup>3</sup>/sec

- (2) FPT utilizing the boring hole is conducted by boring to a pre-determined depth and inserting a casing into the boring hole. The operation of pumping-up stops after the water level in a hole lowers to  $S_0$  by pumping-up. After the operation of pumping-up stops, time( $t$ ) and the amount of water level recovery( $S_t$ ) are measured, and then the coefficient of permeability is given by the following equation:

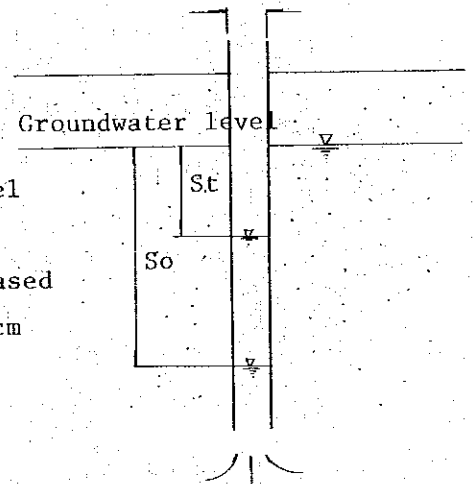
$$k = 2.30 \frac{r_0}{4t} \times \log_{10} \left( \frac{S_0}{S_t} \right)$$

where,  $r_0$  = diameter of boring hole, cm

$t$  = time, sec

$S_0$  = amount of initial water level decreased, cm

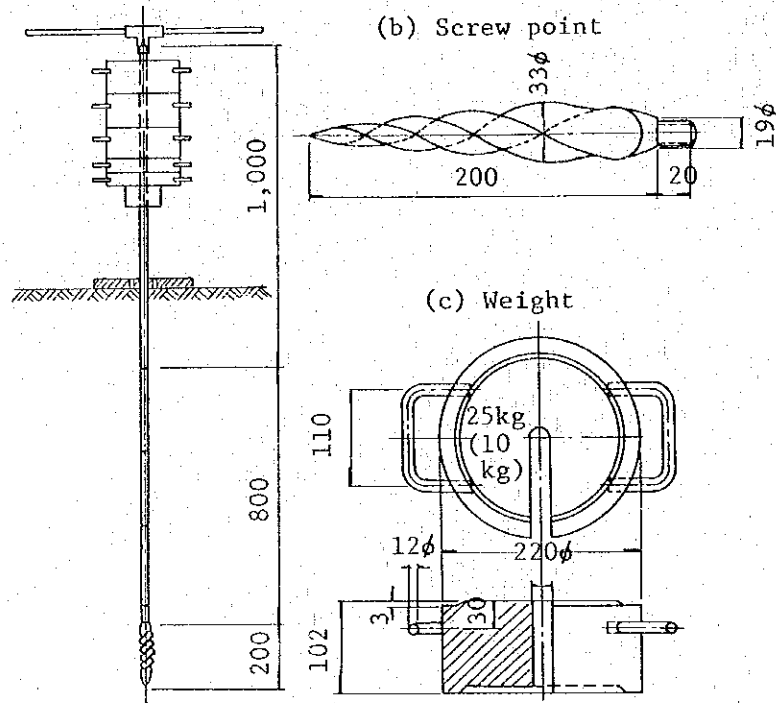
$S_t$  = amount of water level decreased after the time( $t$ ) elapses, cm



A mean value of coefficient of permeability for a sandy soil can be obtained by (1) the recovery method by single well. In the field permeability test employing the boring hole, the coefficient of permeability around the boring hole can be given.

Fig. 8 Sounding

(a) Swedish sounding machine



### 3.1.7 Laboratory Soil Tests

#### (1) Physical Test

The physical test is conducted on the items as summarized in Table 3 in accordance with the standards specified under JIS.

Table 3. Laboratory soil tests

Items	Method of test	To be tested
Specific gravity test	JIS-A-1202	for representative sampling
Natural water content test	-1203	for all samplings
Sieve analysis	-1204	for representative sampling
Liquid limit test	-1205	for representative sampling
Plastic limit test	-1206	for representative sampling

#### (2) Unit Weight Test

The test is conducted in accordance with method of trimming.

#### (3) Unconfined Compression Test

The test is made in accordance with the method as summarized in Table 4.

Table 4. Unconfined compression test

Method of test	JIS-A-1216
Kind of testing machine used	machine being capable of controlling a strain
Configuration and dimensions of specimen	cylindric shape, 5.0cm $\phi$ x 12.5cm(H)
Repeated sample	unconfined compression test is not performed for a repeated sample.
Rate of axial compression loading	1 %/min.
Max. strain	breaking strain + 2 to 3%
Summarized test result	the coefficient of deformation is calculated by a strain corresponding to $E_{50} = 1/2 \text{ qu}$ .

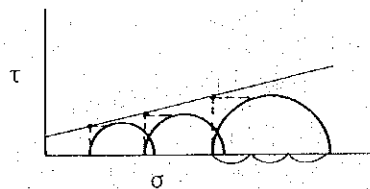


(4) Triaxial Compression Test

The test is conducted in accordance with the method specified in Table 5.

Table 5. Summary of triaxial compression test

Method of test	in accordance with the standards specified under the Japanese Society of Soil Mechanics and Foundation Engineering
Kind of test	consolidated undrained test
Dimensions of specimen	3.5cm $\phi$ x 8.0cm(H)
Kind of testing machine	Norway type
Necessity of drain	Use of paper drain
Lateral pressure	$\sigma_1=0.5\text{kg/cm}^2$ , $\sigma_2=1.0\text{kg/cm}^2$ , $\sigma_3=1.5\text{kg/cm}^2$ , $\sigma_4=3.0\text{kg/cm}^2$
Consolidation time	8 to 14 hours at $\sigma_1$ and $\sigma_2$ , 24 hours at $\sigma_3$ and $\sigma_4$
Rate of axial compression loading	1 %/min.
Summarized test result	



on condition that average main stress is constant

(5) Consolidation Test

The test is performed in accordance with the method described in Table 6 .

Table 6. Method of consolidation test

Method of test	in accordance with the standards specified under JIS-A-1217
Kind of consolidation box	fixed ring
Dimensions of specimen	6.0cm $\phi$ x 2.0cm(H)
Consolidation load	eight stages; p1 p2 p3 p4 p5 p6 p7 p8 0.1-0.2-0.4-0.8-1.6-3.2-6.4-12.8kg/cm <sup>2</sup>
Time of loading	24 hours at each stage
Unloading	Measurement of expansion by unloading is not made.
Determination of Cv	Square root of time fitting method is applied.
Determination of yield stress of consolidation	in accordance with the draft standard specified under the Japanese Society of Soil Mechanics and Foundation Engineering
Consolidated test result	It is expressed by $e \sim \log p$ , $\log p \sim \log C_v$ , $\log p \sim \log mv$ .

### 3.2 Result of Soil Investigation

#### 3.2.1 Soil Composition

Fig. 10 and Fig. 11 show assumed soil profiles drawn on the basis of the results of boring survey and Swedish sounding.

A typical soil profile of the survey site is shown in Fig. 12. and the general characteristics of each soil layer and representative values for testing are summarized in Table 7.

Fig. 12 Typical soil profile

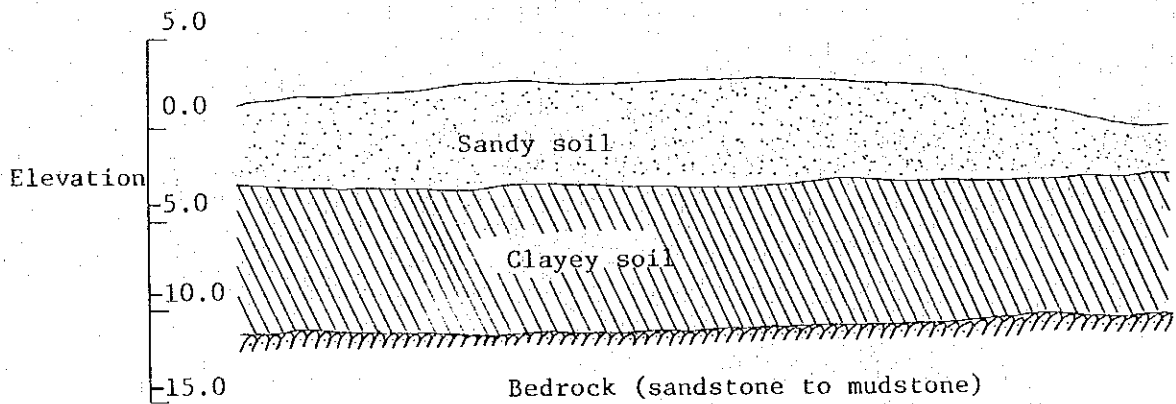


Table 7 . Representative values for testing

Description	N value	Water content Wn(%)	Specific gravity Gs	Unit weight $\gamma_t$ (g/cm <sup>3</sup> )	Compression index Cc	Unconfined compressive strength qu (kg/cm <sup>2</sup> )
Very loose, fine-grained sand having grain size of 2mm which contains a great amount of shell fragment and sand	10 - 2	8 - 40	2.6-2.7	-	-	-
Very soft, cohesive and uniform clay including a small amount of shell fragment and sand	0	75-100	2.5-2.6	1.5-1.6	0.8-1.2	0.2 - 0.6
Unsound rock containing sandstone or mudstone	above 50	-	-	-	-	-

The shipyard construction site was reclaimed about 18 years ago, and consists primarily of sandy soil, clayey soil and bedrock.

(1) Sandy Soil

Sandy soil is 5- to 7-meter thick, and composed of an original sedimentary layer and a reclaimed layer. The boundary between these layers is indefinite, because the former layer is identical with the latter layer in soil properties.

The sandy soil is of fine-grained sand having a grain size of about 2mm, and contains a small amount of shell fragment. The upper layer is dark brown in color, and the lower layer is black in color. The sandy soil at a depth of 1m below the surface of the ground contains a small amount of silt and clay, but at a depth of more than 1m includes a great amount of clay and silt. The N value of the upper sandy soil is 5 to 10, but the N value decreases to 2 or 3, because of the fact that the greater the depth, the greater the inclusion of silt or clay. As a result, it is very loose for the sandy soil.

(2) Clayey Soil

A 7 to 10cm thick marine clay formed in the alluvial epoch is deposited under the upper sandy soil. The clay is dark blueish gray and greenish gray in color, and great cohesive. The clay includes a small amount of shell fragment and sand, but is generally uniform. The N value of the clayey soil is zero, so that it is very poor.

On the other hand, apart from the other places, the soil layer of Boring Nos. 9 and 14 is composed of sandy soil including a great amount of clay, or cohesive soil containing a lot of coral fragments.

### 3.2.2 Results of Soil Tests

(1) Standard Penetration Test (SPT)

Fig. 14 shows depth distribution of N value as a comparative diagram on the basis of the results of SPT.

The N value of sandy soil ranges from 1 to 10, and the N value at a depth of 2m is 5 to 10, with the average N value of 7. The greater the depth, the greater the inclusion of silt or clay, and the average N value decreases to 3. In the majority of clayey soil, a rod penetrates to a depth of 60 to 70cm by a hammer weight, and the N value is zero. In the bedrock, the penetration by 50 times of blows is 8 to 15cm except where the upper layer is in a clayey state. It is obvious that the bedrock is very hard.

(2) Swedish Sounding (SS)

Fig. 14 shows the comparative chart of the results of Swedish sounding. A half rotation by 100kg load is 10 to 40 times at the upper sandy soil and 20 times at the lower sandy soil. A sounding instrument itself does not settle excessively when reaching the clayey soil from the sandy soil, and the half rotation by 100kg is about 10 times. The greater the depth, the greater the half rotation, and then 10 to 40 times of half rotation result. The half rotation per 1m is 800 to 1000 times when the sounding instrument reaches the bedrock, so that the SS is impossible to conduct.

The boundary between the sandy soil and the clayey soil is indefinite through the Swedish sounding, because the lower sandy soil has a great amount of clayey soil and a low strength. Since the effect of circle friction cannot be avoided, converting a constant of the clayey soil's strength by an empirical formula and the test results will become a problem in terms of the accuracy.

The purpose of Swedish sounding is to determine the depth of bedrock. The survey site proves to satisfactorily attain the purpose of the test.

(3) Field Permiability Test (FPT)

Table 8 indicates the result of FPT.

Table 8. Results of FPT

Method of test	Place	Depth	Time	Coefficient of permeability (cm <sup>2</sup> /sec)
Method of recovery by single well	B-7	-2.60	1	$7.3 \times 10^{-4}$
		-4.10	2	$1.0 \times 10^{-3}$
Employing a boring hole	B-13	-3.2	1	$2.2 \times 10^{-2}$
			2	$1.1 \times 10^{-2}$
		-4.1	1	$6.0 \times 10^{-3}$
			2	$4.2 \times 10^{-3}$
Average				$7.5 \times 10^{-3}$

The coefficient of permeability shows increased dispersion in depth, and ranges from  $7.3 \times 10^{-4}$  to  $1.1 \times 10^{-2}$ . The characteristics of grading is correlated with the coefficient of permeability.

According to the Hazen's theory, diameter at which 10% of the soil is finer and the coefficient of permeability are approximately given by the following equation:

$$k = 100 (D_{10})^2$$

where k = coefficient of permeability, cm<sup>2</sup>/sec

D<sub>10</sub> = diameter at which 10% of the soil is finer, mm

k is calculated as  $6.4 \times 10^{-3}$  cm<sup>2</sup>/sec by the above equation on condition that D<sub>10</sub> of the lower sandy soil is 0.008mm. This value shows to be identical with the test value.

#### (4) Water Content Test

Fig. 13 shows the depth distribution of natural water content. Water content of the upper sandy soil is about 10%, and water content has a great value of 40 to 60%, because the greater the depth, the greater the inclusion of clayey soil. The water content throughout the clayey soil shows a constant value, ranging from 70 to 100%.

(5) Liquid Limit Test (LL) and Plastic Limit Test (PL)

In Fig. 13, the results of LL, PL are plotted on a plastic chart, and the clayey soil of the survey site is distributed on A-line. A liquid limit ranges from 90 to 130%, and classified as CH (clayey soil of high plasticity) on the basis of the Unified Soil Classification of Japan and ASTM D-2488.

In general, the clayey soil classified as CH has a high compressibility, and low shearing strength. The distribution of a consistency ( $I_c = WL - W_n/I_p$ ) is shown in Fig. 13.

The consistency index represents a relative hardness of clayey soil, natural water content at  $I_c \geq 1$  is close to or less than the plastic limit, being in a state of stability.

On the other hand, natural water content at  $I_c \geq 0$  is near to or greater than the liquid limit, being in an unstable state.

The clayey soil of the site ranges from  $I_c = 0.2$  to  $I_c = 0.5$ .

It is common that  $I_c$  in the marine clay of the alluvial epoch is near to or below zero. The consistency index shows that the clayey soil of the survey site is stable for the marine clay of the alluvial epoch.

(6) Result of Sieve Analysis

Fig. 13 shows a comparative diagram and representative value of grain-size accumulation curve of each layer.

In a triangular classification system classified according to the characteristics of grain-size, the upper sandy soil, the lower sandy soil, and the clayey soil are classified as sand, silty sand and clay or silty clay, respectively.

(7) Results of Unit Weight and Specific Gravity Tests

Fig. 13 shows the depth distribution of unit weight, and Fig. indicates the depth distribution of specific gravity. The unit weight represents a constant distribution to the direction of depth, and averages 1.57 g/cm<sup>3</sup>. The specific gravity of sandy soil averages 2.60, and shows a constant distribution. The specific gravity of the clayey soil ranges from 2.45 to 2.60, showing the tendency that the specific gravity of the lower layer is great. This is attributable to a small amount of an organic matter included in the layer.



(8) Result of Unconfined Compression Test

Fig. 12 shows the depth distribution of unconfined compressive strength. The greater the depth, the greater the value of the unconfined compressive strength. The unconfined compressive strength of the upper layer and lower layer is 0.2 to 0.4kg/cm<sup>2</sup>, and 0.4 to 0.8kg/cm<sup>2</sup>, respectively. A line of effective overburden load (Po) is noted in Fig. 12.

From Po and a consistency increase rate (Cu/p), a theoretic cohesion (Co) is calculated by

$$C_o = C_u/p \times P_o$$

A distribution of theoretic cohesion is calculated, assuming that the consistency increase rate is 0.25 to 0.35. Comparing a half value of unconfined compressive strength (qu), which is called cohesion, with the theoretic value, the value of unconfined compressive strength of the survey site is greater than that of theoretic unconfined compressive strength. The clayey soil of the site is presumed to be slightly in an overconsolidated state.

(9) Result of Consolidation Test

Fig. 14 shows e - log p curve, log cv - log p curve, and log mv - log p curve on the basis of the result of consolidation test.

A compression index (Cc) determined as gradient of straight line on e - log p curve ranges from 0.8 to 1.2, and natural water content is 70 to 100%, which is a standard value for alluvial clay. On the other hand, particularly in the clayey soil of the survey site, a consolidated yield load (Py) becomes greater than the effective overburden load (Po). This will be attributed to sedimentation of cement and increased load of consolidated yield (Pc effect).

In calculating amount of settlement due to consolidation, the amount of settlement will be overestimated only when the compression index (Cc) is used, because the value of consolidated yield load is great.

The coefficient of consolidation (Cv) corresponding to Py is 0.15 cm<sup>2</sup>/sec, and the coefficient of volume compressibility(mv) is  $7.0 \times 10^{-2}$  cm<sup>2</sup>/kg. Natural water content is 70 to 100%, showing a standard value for the clayey soil.

(10) Triaxial Compression Test (Consolidated Undrained Test)

Fig. 14 presents a Mohr's stress chart on the basis of the result of triaxial compression test. A constant of strength ( $\phi_{cu}$ ) at a normally consolidated zone is  $14^\circ$  to  $18^\circ$ . The consistency increase rate,  $Cu/p = \tan \phi_{cu}$ , is 0.25 to 0.33.



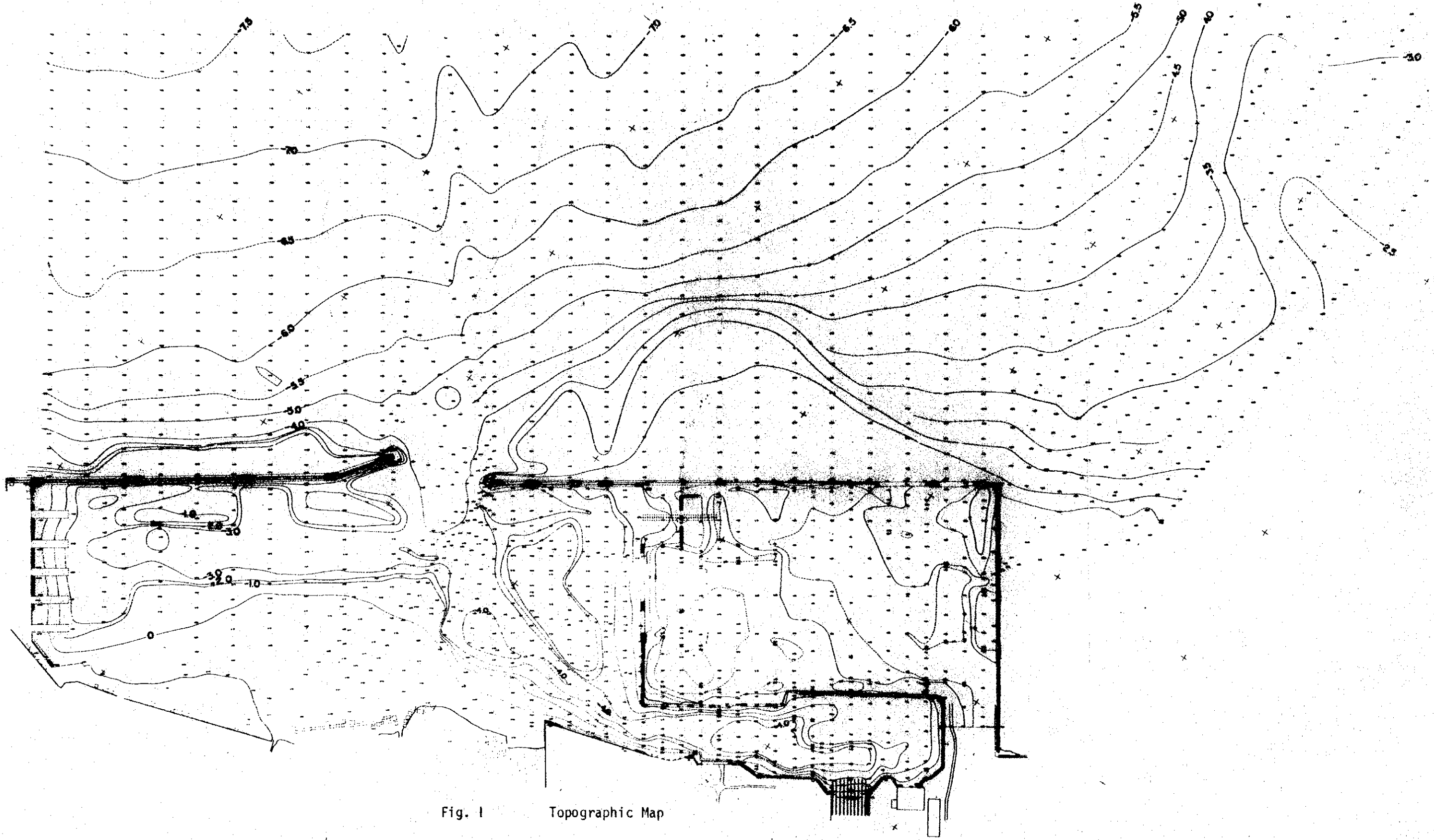


Fig. 1 Topographic Map

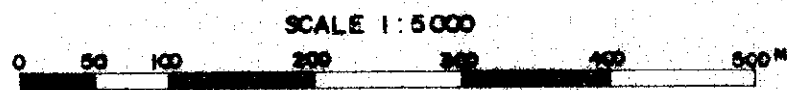
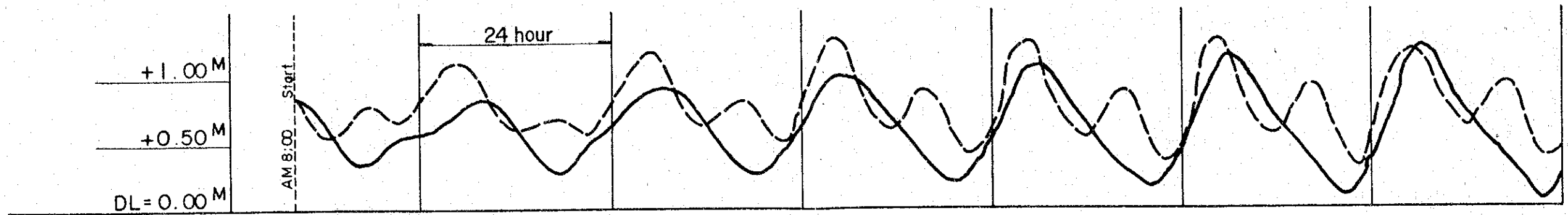
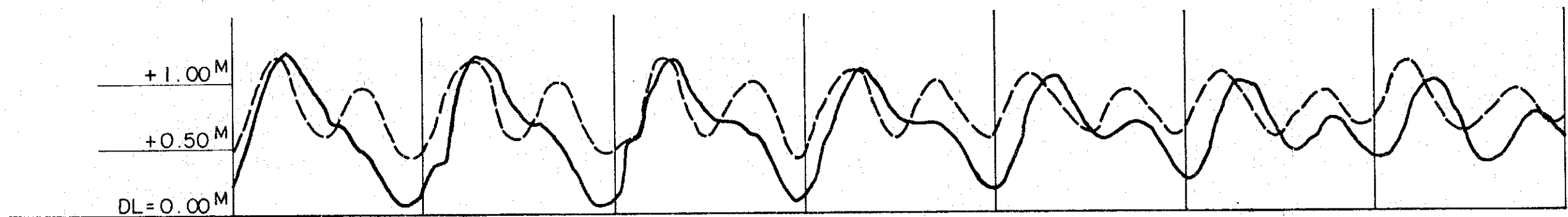


Fig. 3 TIDE CURVE

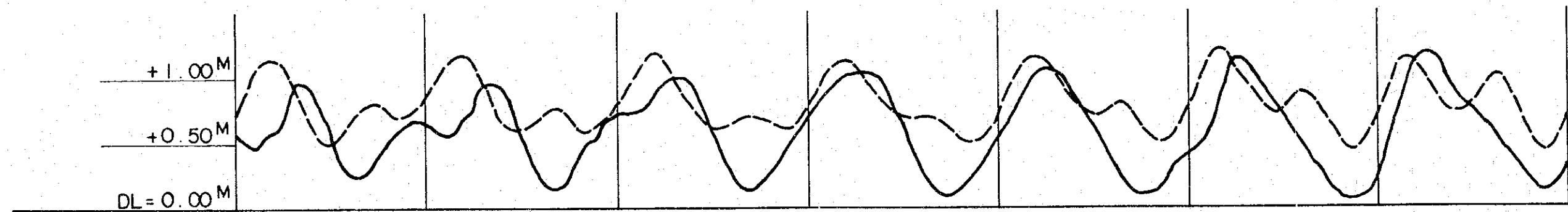
----- ANTICIPANT TIDE  
—— ACTUAL TIDE



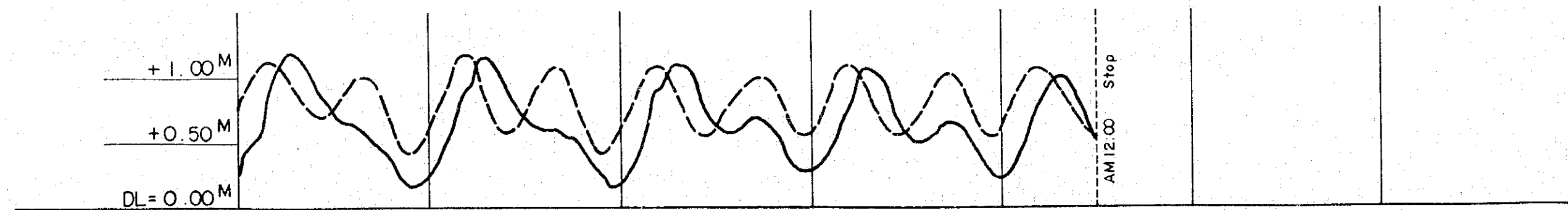
JUN 23 ~ JUN 29



JUN 30 ~ JUL 6



JUL 7 ~ JUL 13



JUL 14 ~ JUL 18

Fig . 5 ROAD PROJECT

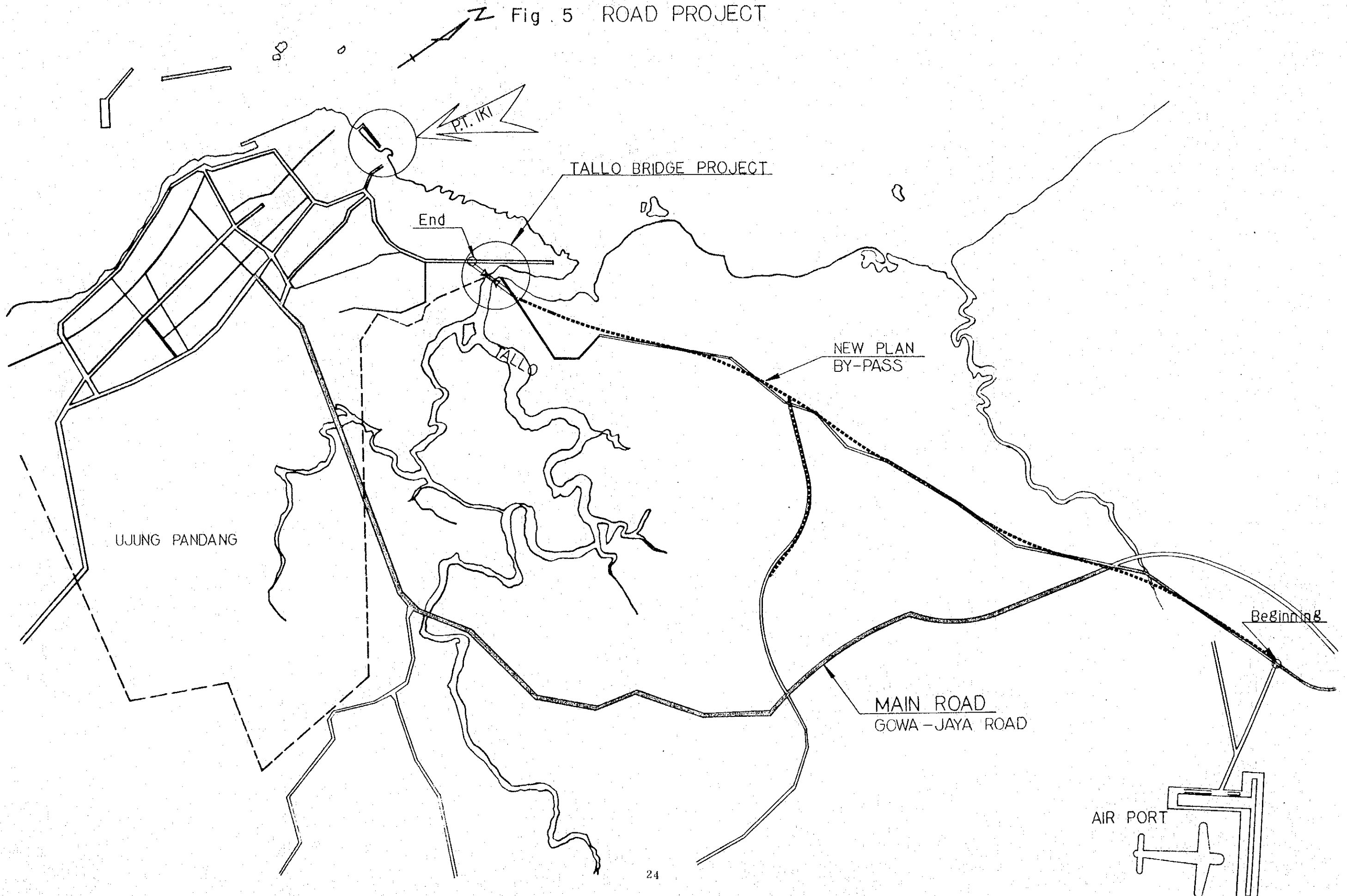


Fig. 6 WATER SUPPLY

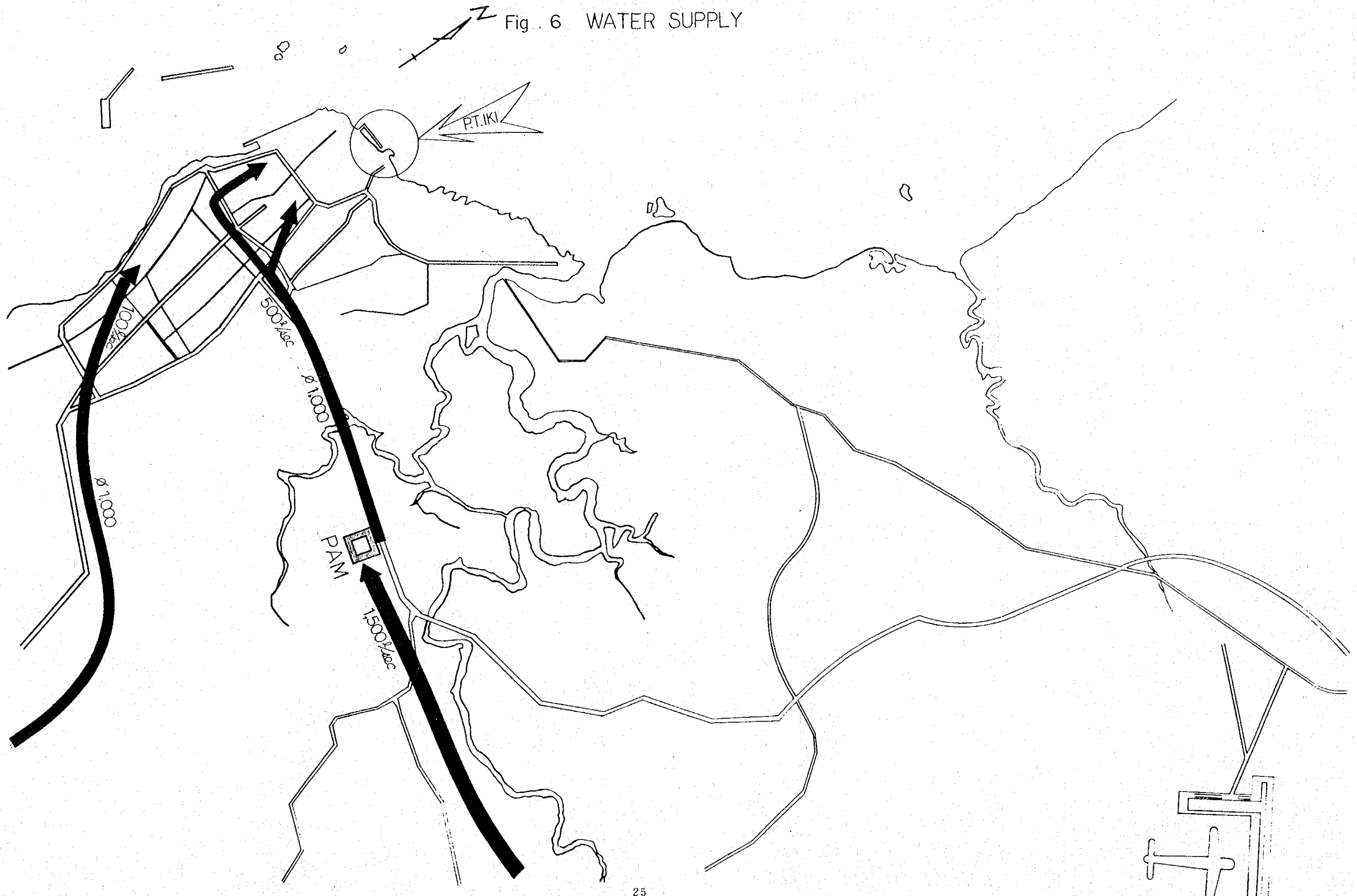
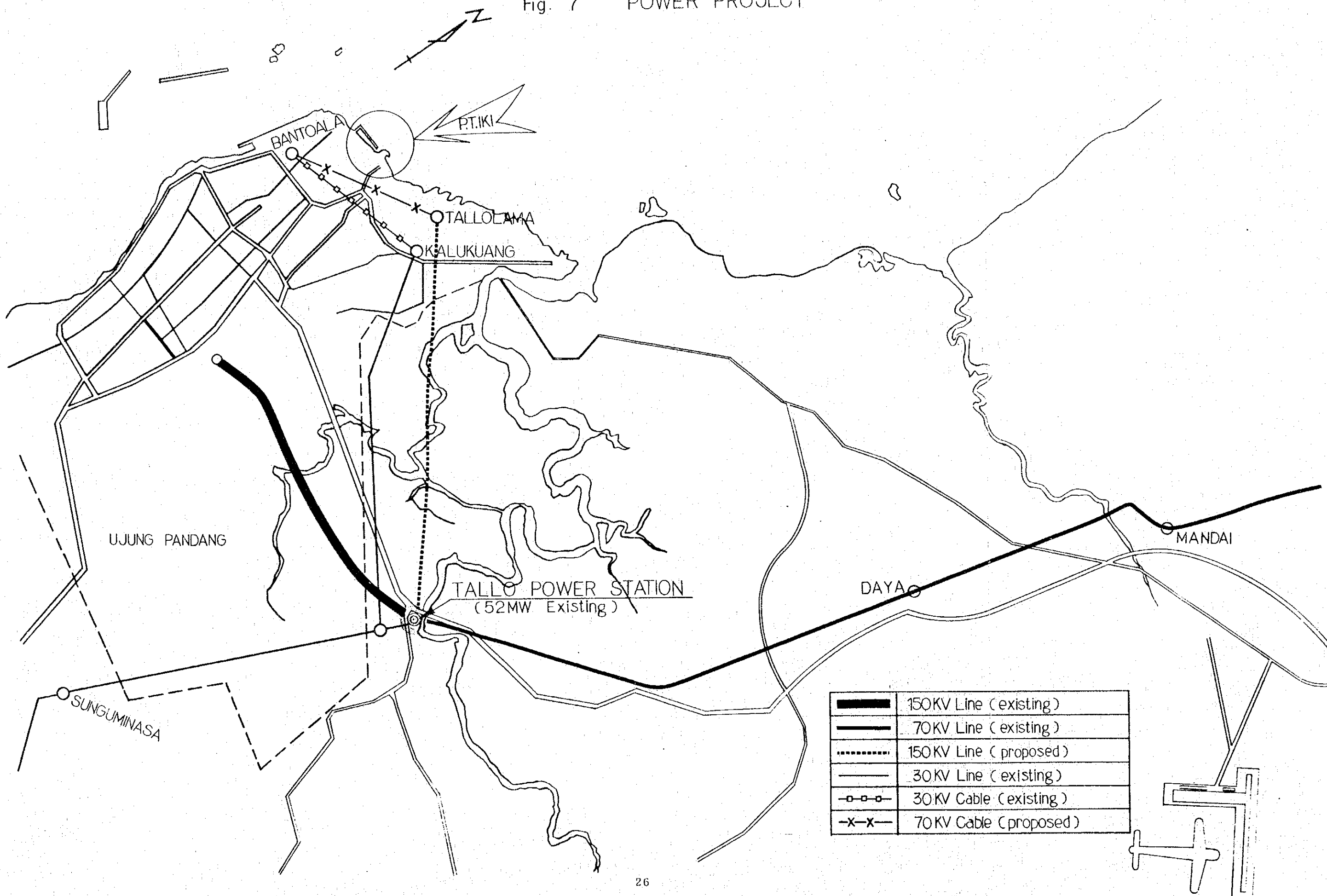
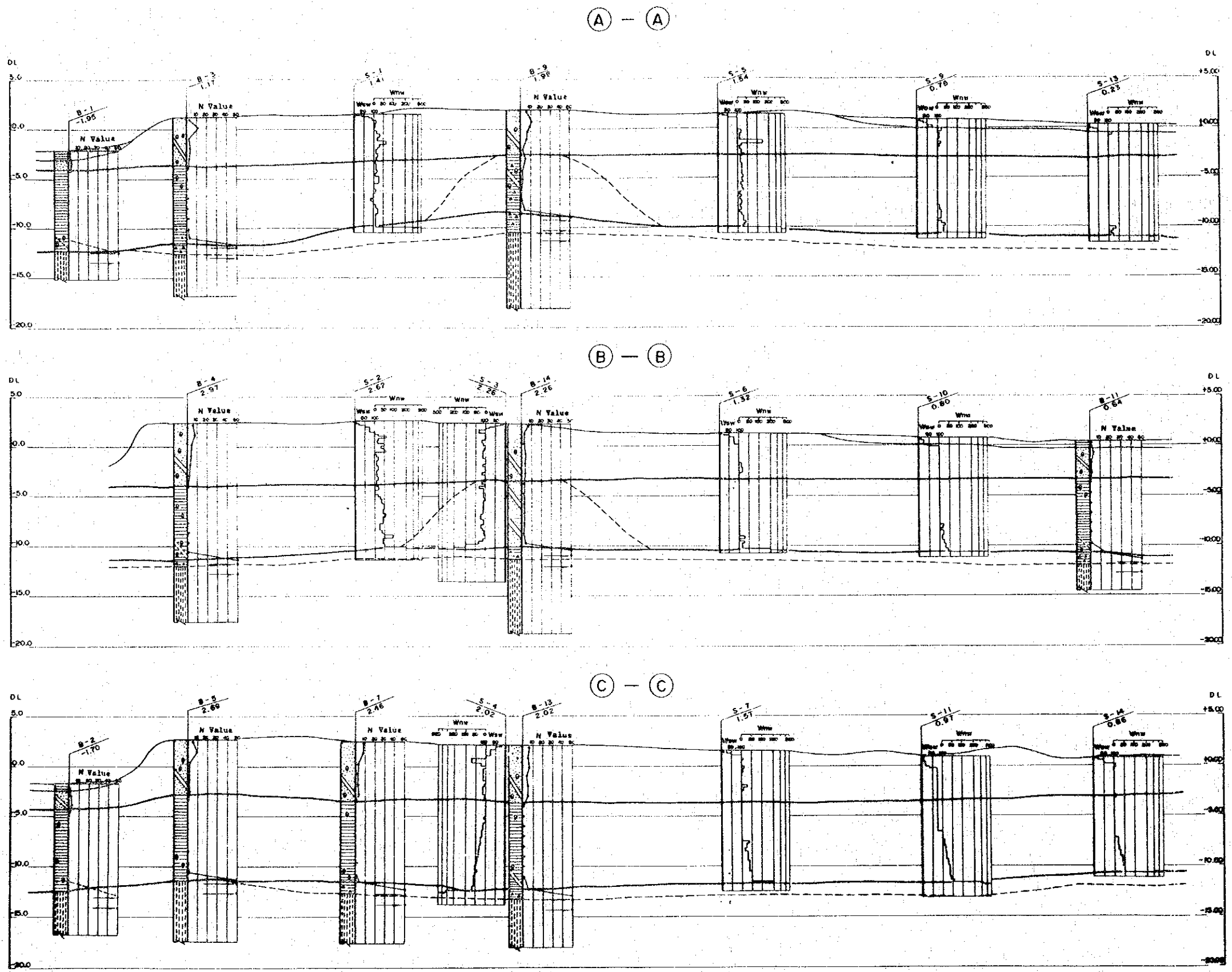


Fig. 7 POWER PROJECT

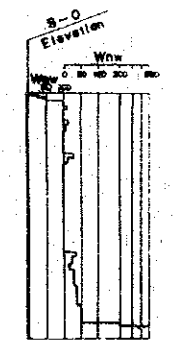






Soil No.	Depth (ft)	Moisture Content (%)	Relative Density	Description	Wn	Gs	Fi	Qu	Cc
1	0-1	2.8	—	Consisting of clayey or silty soil	—	2.8	—	—	—
2	1-2	2.7	—	Very loose sand	—	2.7	—	—	—
3	2-3	—	—	Uniform and very cohesive soil	75	2.5	1.5	0.2	0.8
4	3-4	—	—	Containing small quantity of shell fragments	100	2.6	1.6	0.6	1.2
5	4-5	—	—	Clay	—	—	—	—	—
6	5-6	—	—	Hard	—	—	—	—	—
7	6-7	—	—	Very hard	—	—	—	—	—
8	7-8	—	—	Hard	—	—	—	—	—

Wn : Natural Moisture Content  
 Gs : Specific Gravity  
 Fi : Wet Density  
 Qu : Unconfined Compressive Strength  
 Cc : Compression Index



S-0 : Swedish sounding No  
 Wnw : Lead  
 Wnw : Number of soil revolution per 100

Fig. 10 Soil Profile 1

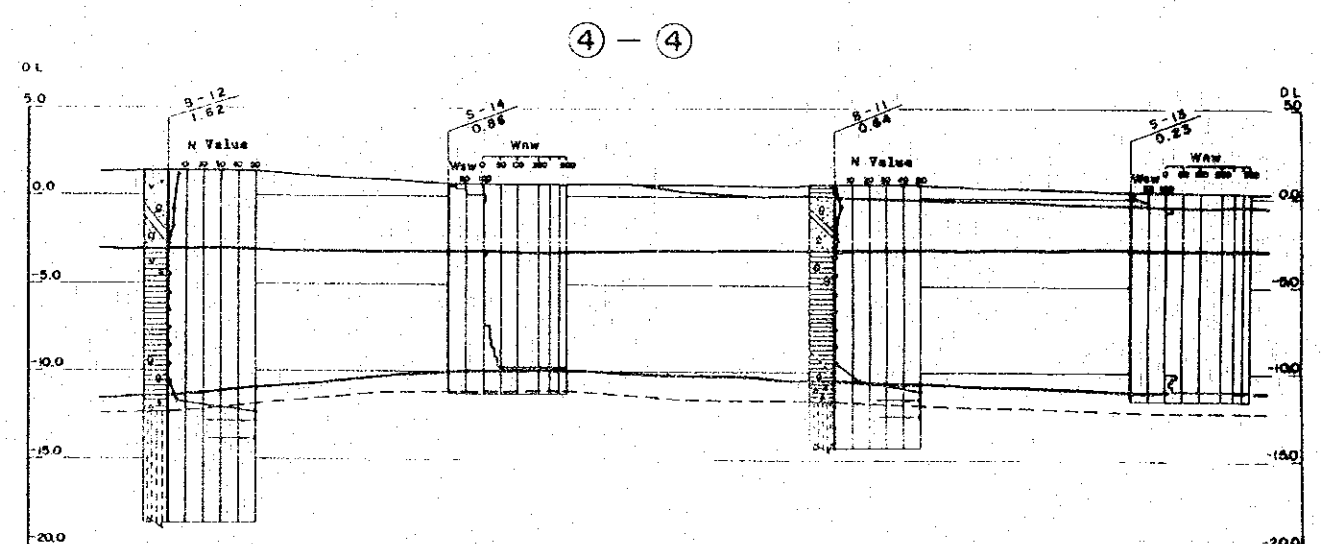
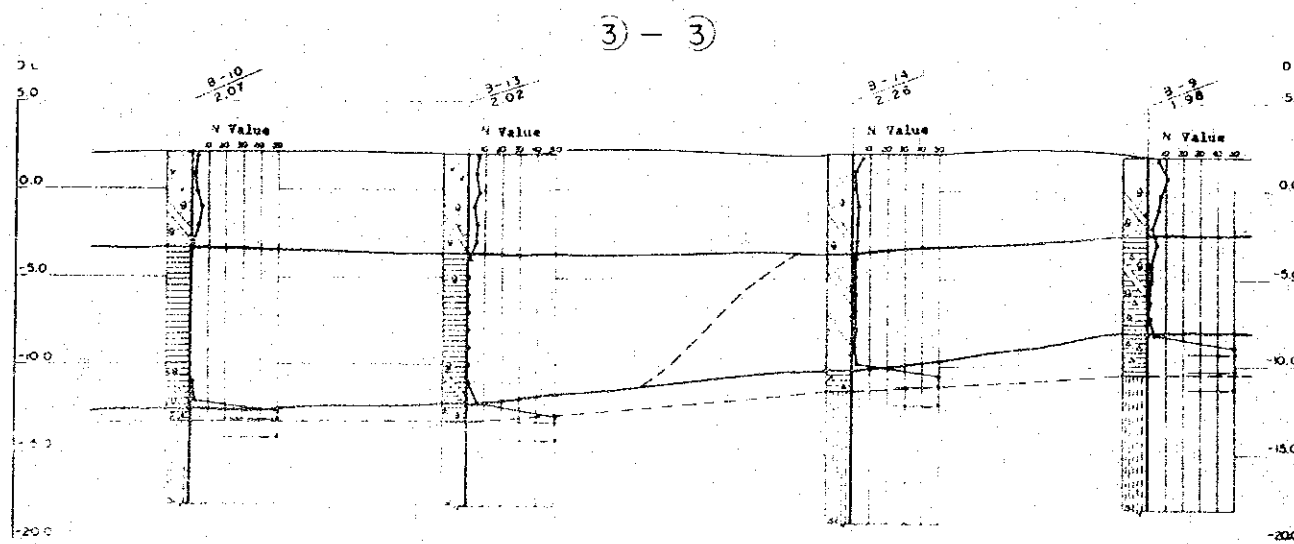
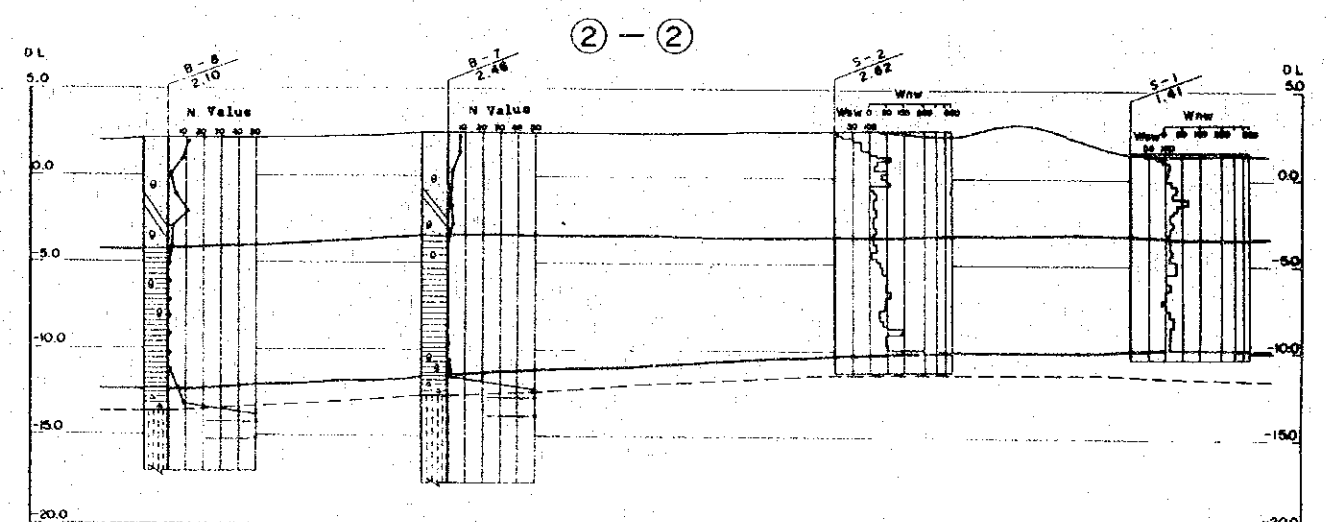
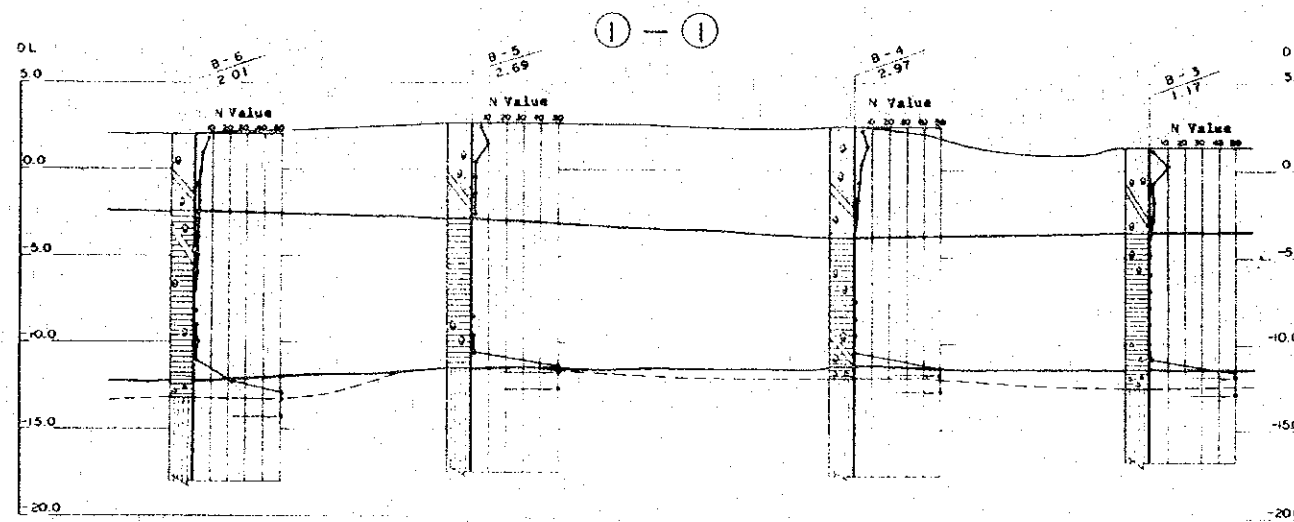
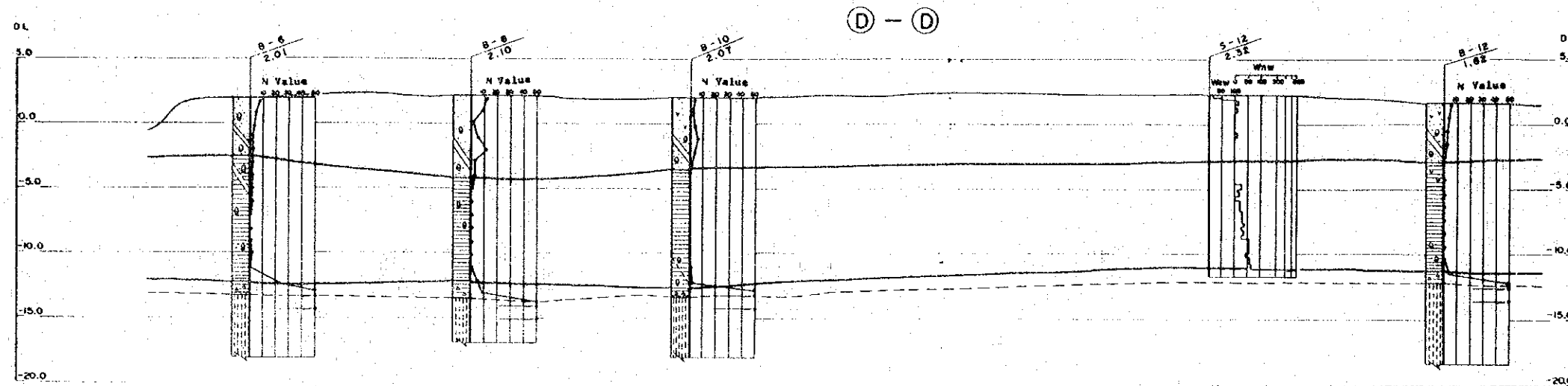


Fig. 11 Soil Profile 2

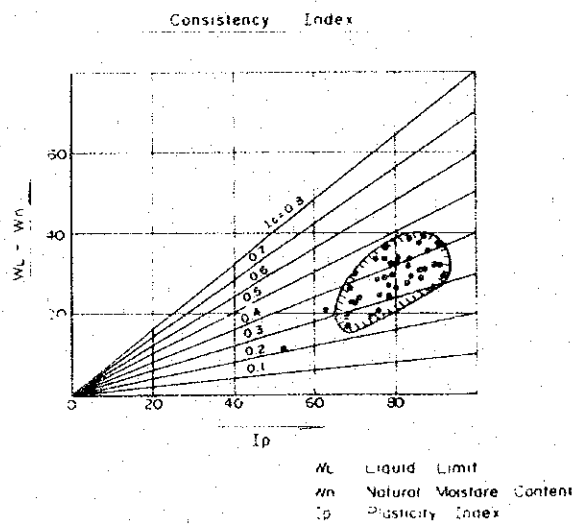
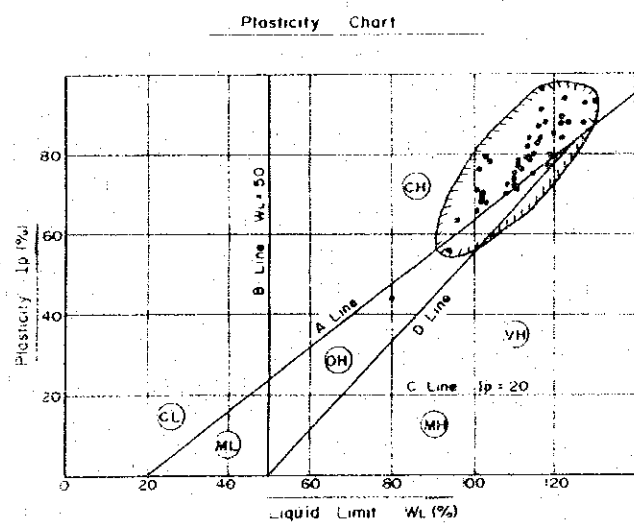
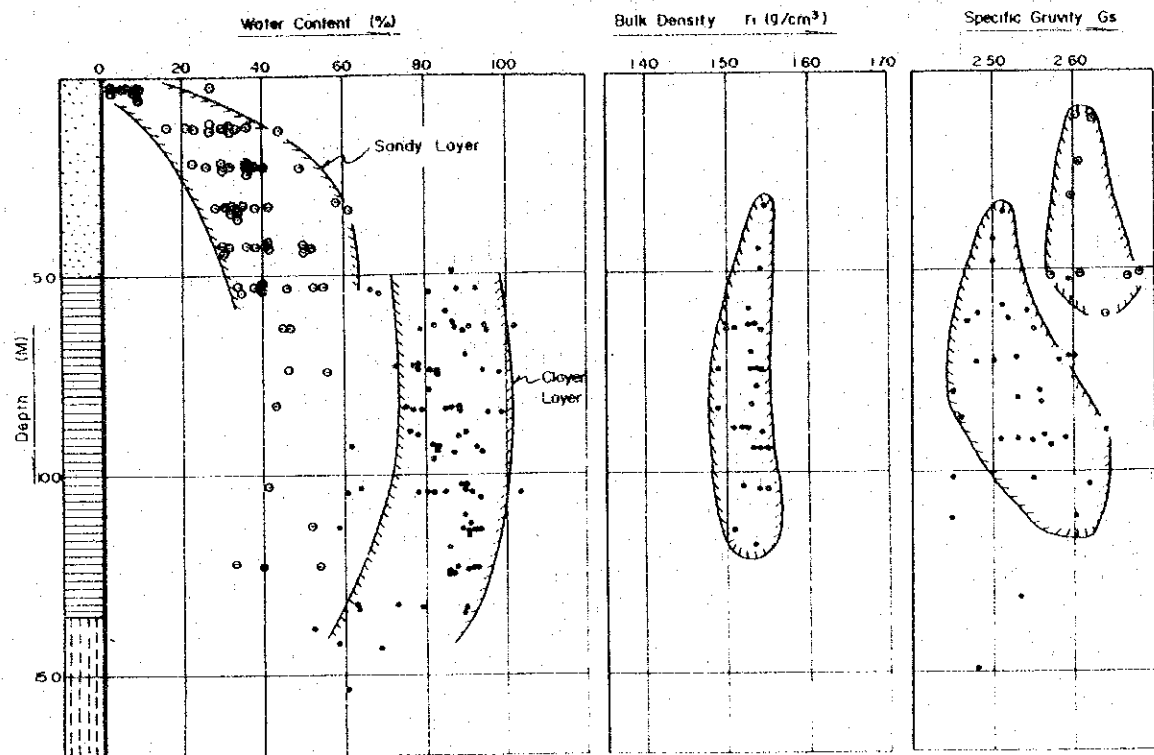
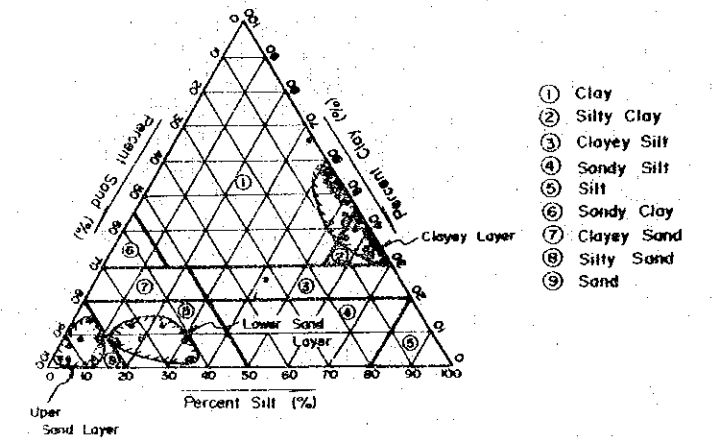
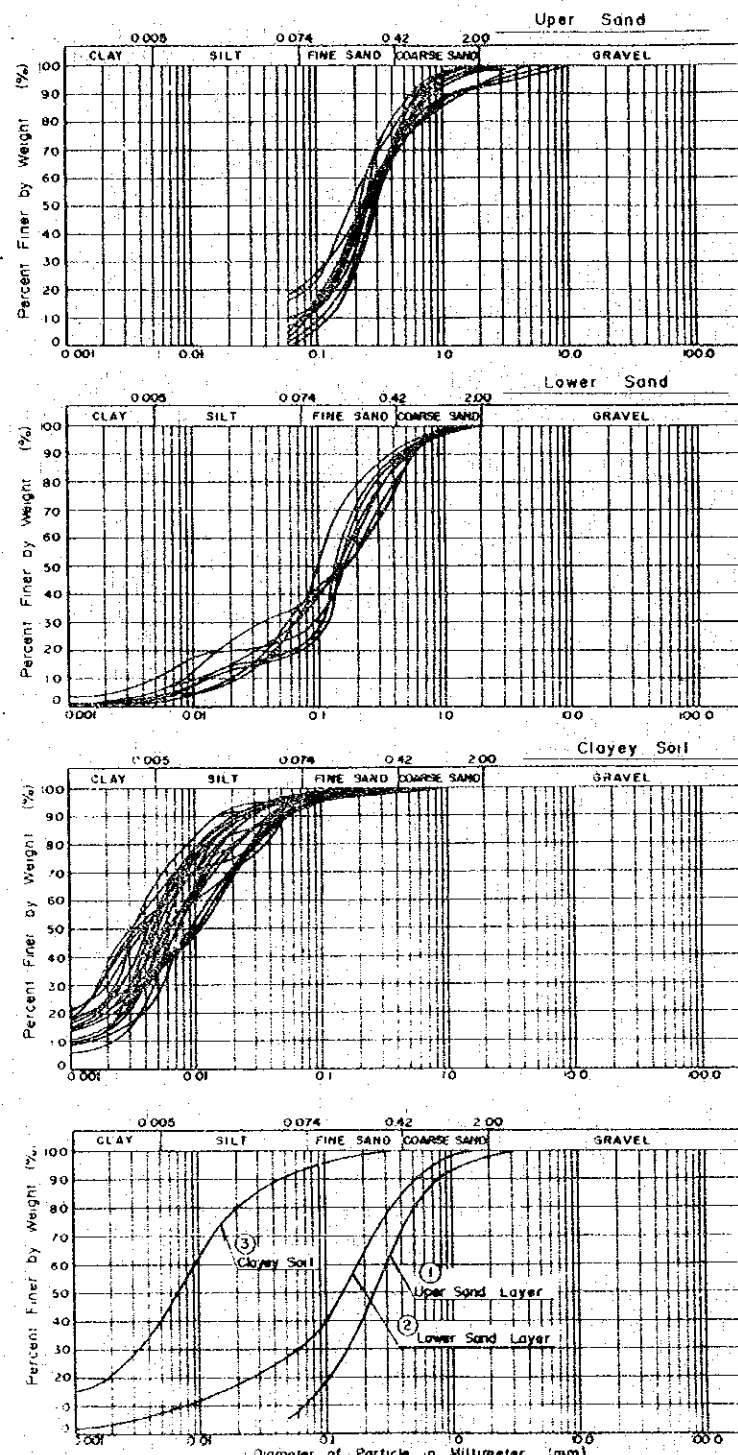


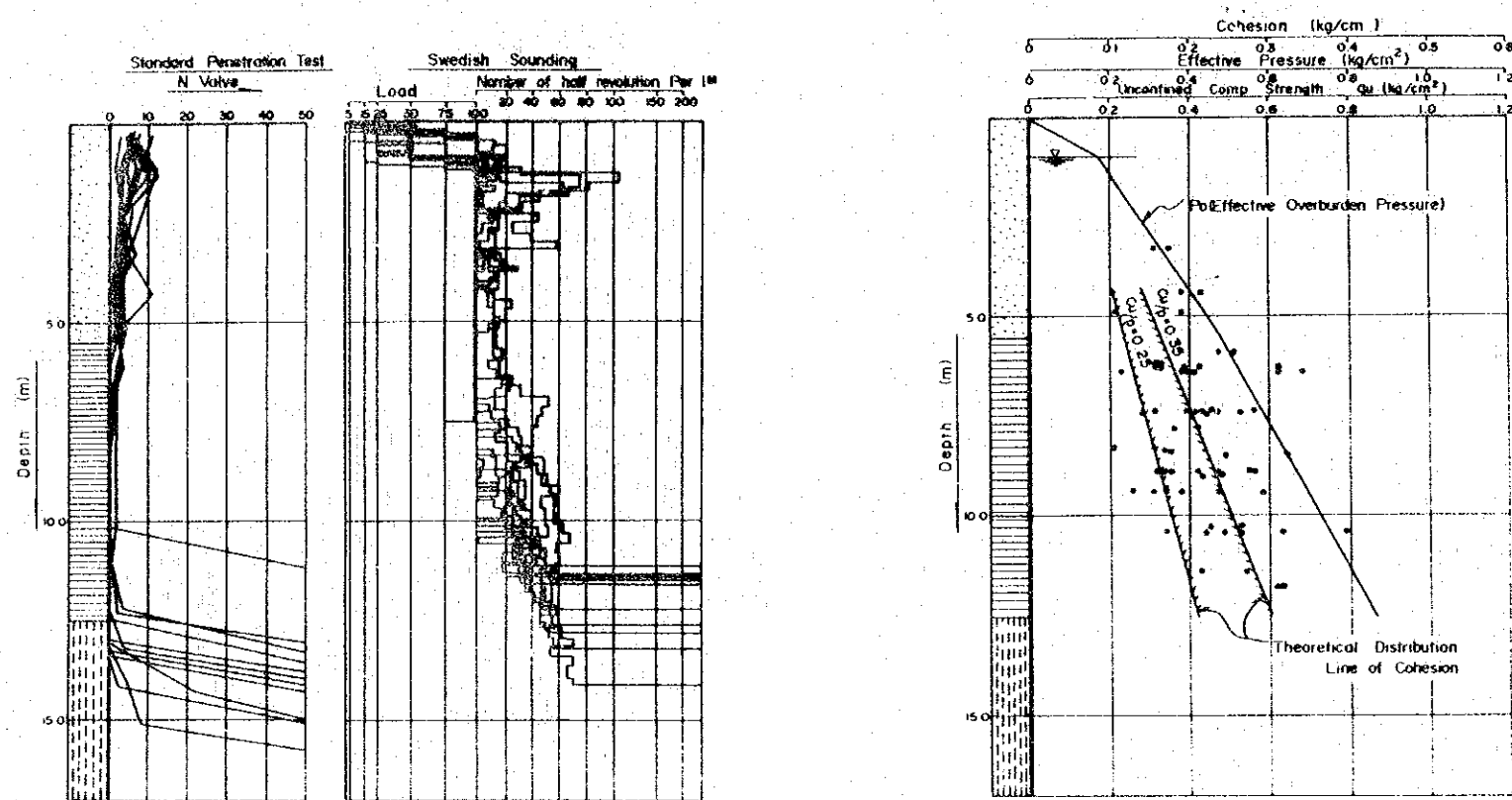
Fig. 13

Result of Soil Test (Fisical Test)

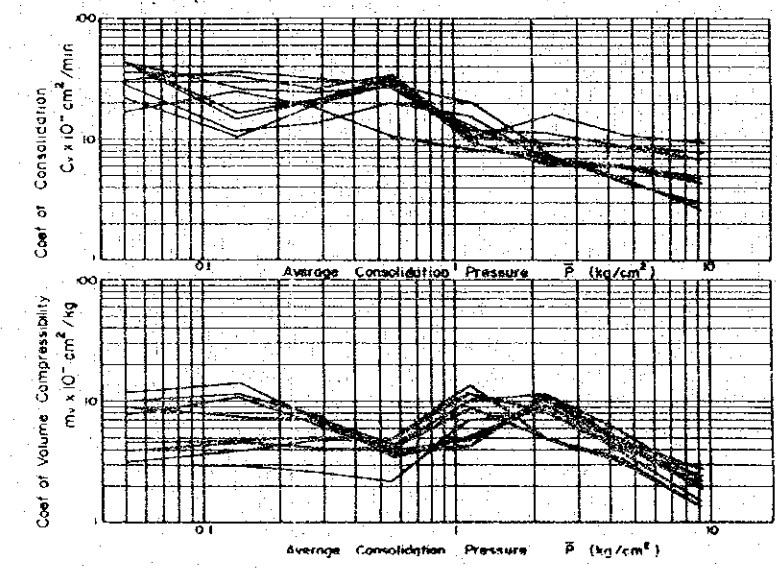
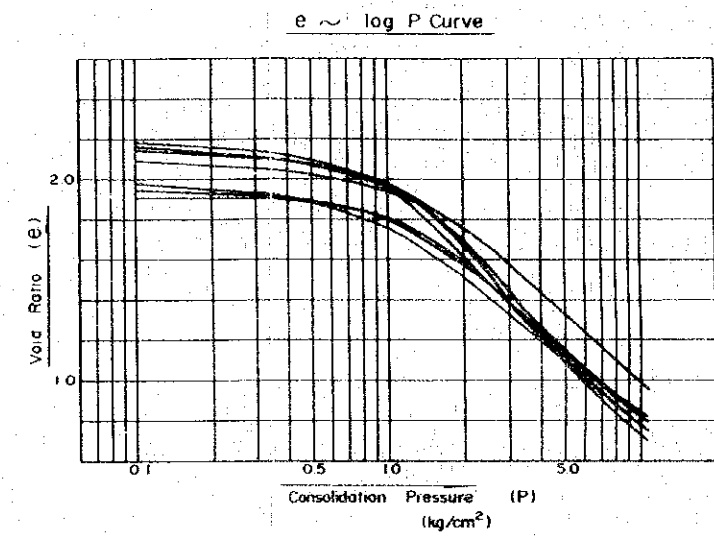


Sample No.	Gravel %	Coarse Sand %	Fine Sand %	Silt %	Clay %	Calcd. %	Umax mm	D60% mm	D30% mm	Uc	Uc %	Uc %	Uc %
1	2	25	61	12	—	2.00	0.30	0.07	4.3	98	73	15	—
2	—	15	52	21	11	1	1.50	0.17	0.006	21.3	100	55	34
3	—	—	6	52	27	18	0.42	0.009	—	—	100	100	34

Uc Uniformity Coefficient



Consolidation



Triaxial Compression

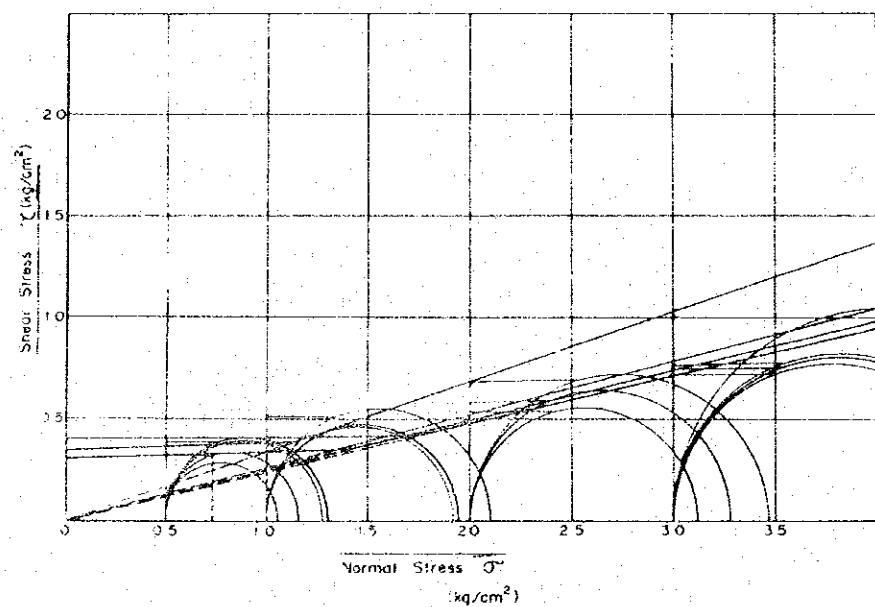
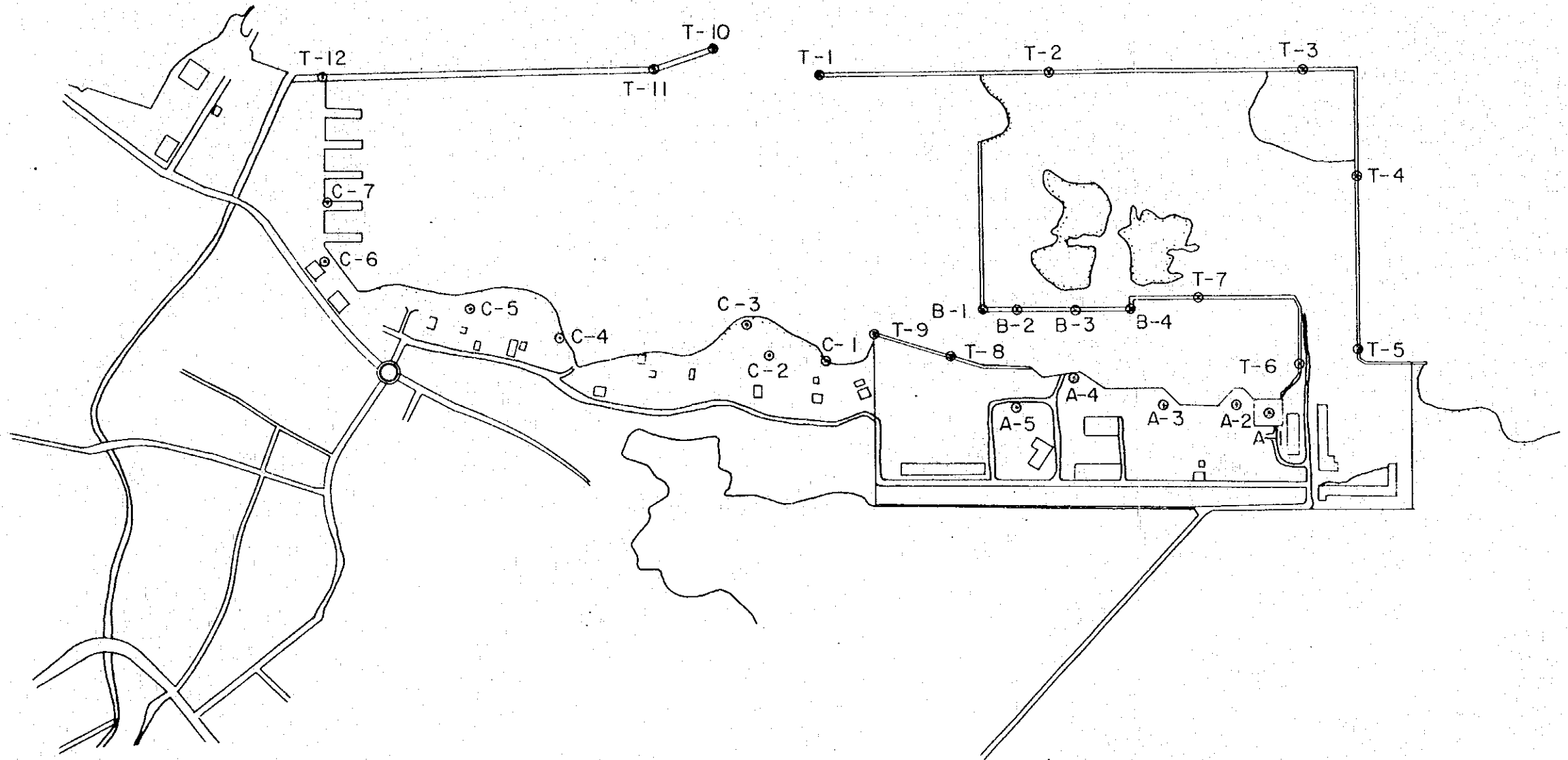


Fig. 14 Result of Soil Test (Dynamic Test)

Fig. 15 LOCATION OF TRAVERSE POINTS



No.	X	Y	No.	X	Y	No.	X	Y	No.	X	Y
T - 1	2,000 .000	2,000 .000	T - 8	1,793 .270	2,338 .715	A - 3	1,897 .768	2,577 .664	C - 1	1,713 .108	2,199 .949
T - 2	2,147 .801	2,231 .286	T - 9	1,765 .547	2,236 .424	A - 4	1,855 .856	2,469 .073	C - 2	1,676 .838	2,139 .322
T - 3	2,315 .566	2,492 .875	T - 10	1,952 .596	1,869 .443	A - 5	1,829 .549	2,419 .938	C - 3	1,698 .100	2,086 .819
T - 4	2,265 .458	2,626 .553	T - 11	1,889 .297	1,819 .786	B - 1	1,858 .048	2,329 .802	C - 4	1,549 .552	1,900 .434
T - 5	2,086 .248	2,742 .476	T - 12	1,665 .253	1,484 .618	B - 2	1,880 .547	2,367 .095	C - 5	1,516 .755	1,786 .166
T - 6	2,029 .201	2,694 .409	A - 1	1,963 .623	2,697 .088	B - 3	1,915 .908	2,425 .382	C - 6	1,477 .573	1,606 .494
T - 7	2,013 .370	2,543 .489	A - 2	1,948 .573	2,653 .172	B - 4	1,957 .715	2,484 .094	C - 7	1,532 .850	1,566 .055

Fig .16 LOCATION OF BENCH MARK

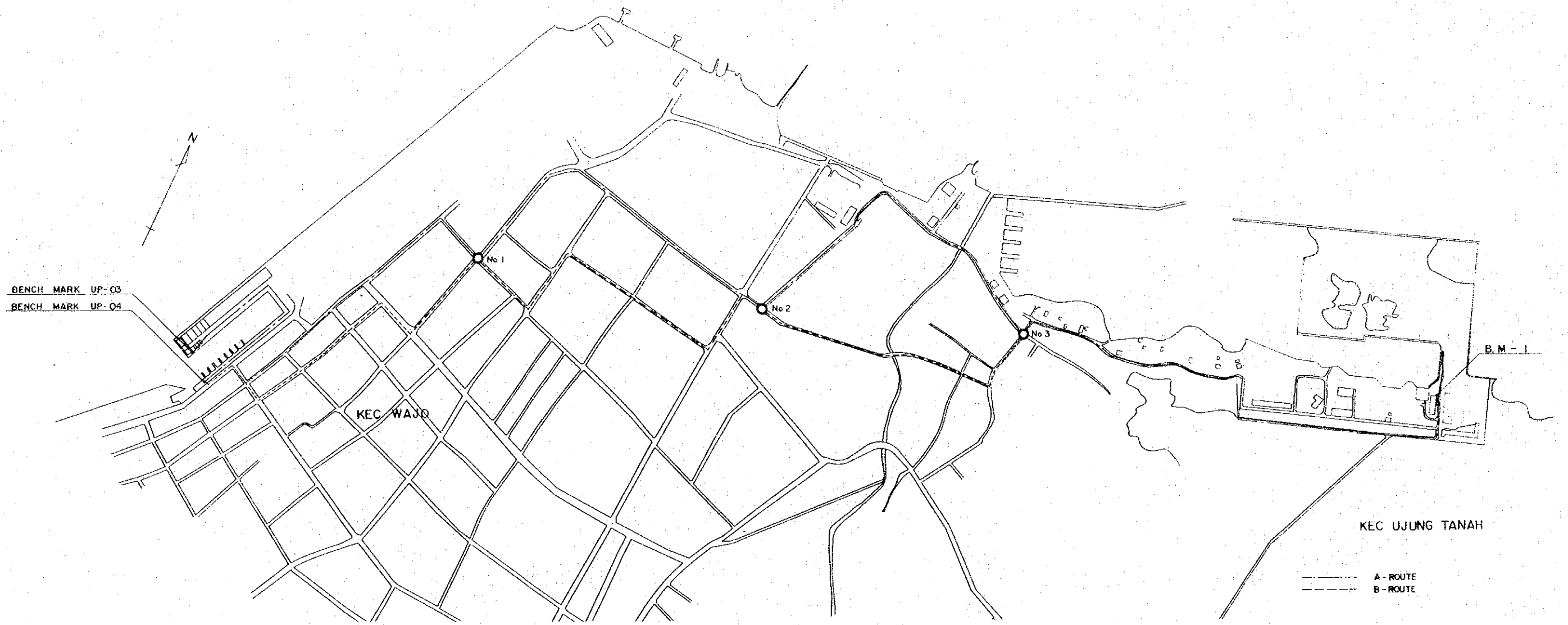
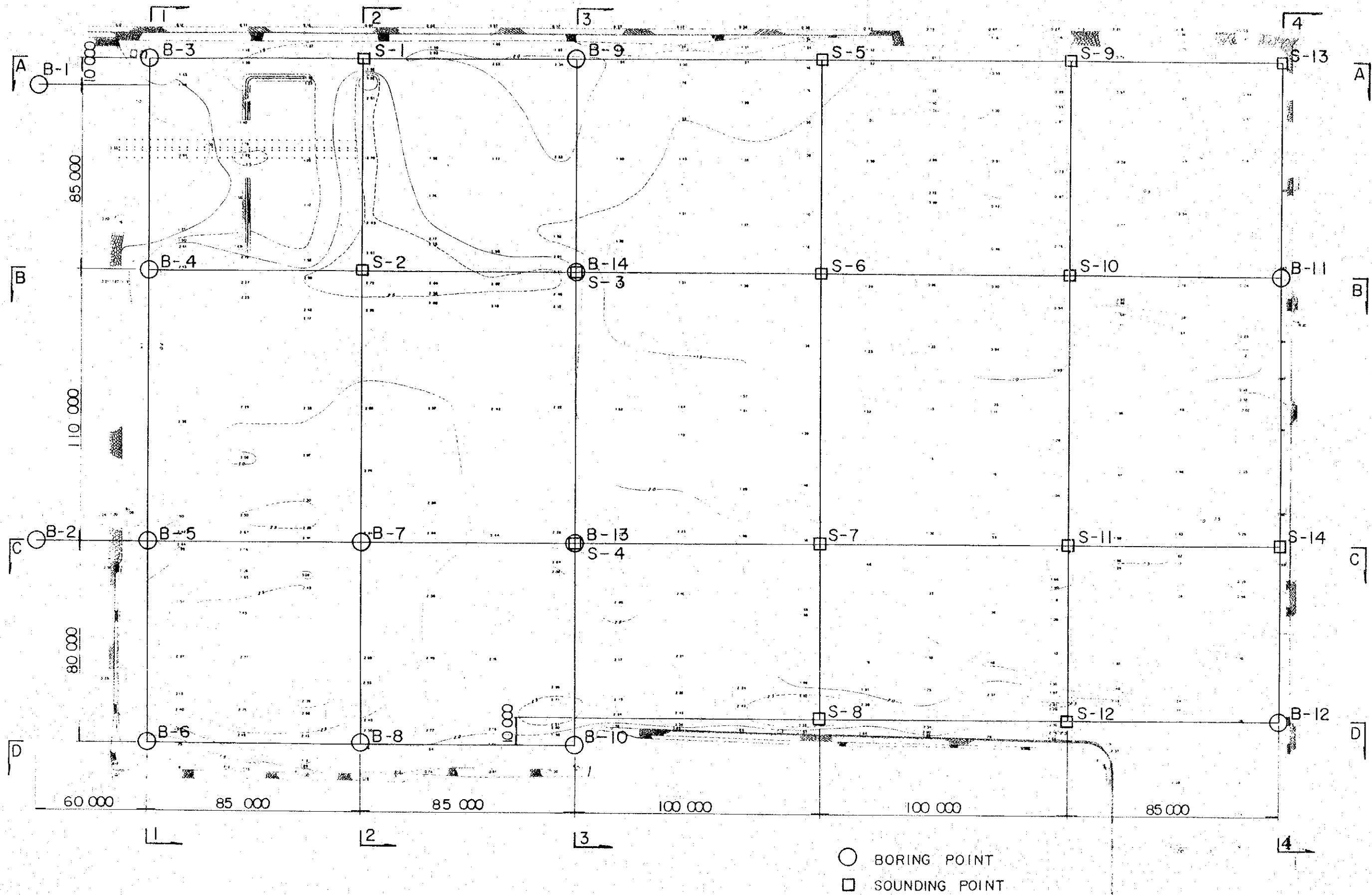


Fig. 17 LOCATION OF BORING & SWEDISH WEIGHT SOUNDING POINTS



# ボーリング柱状図

BORING LOG

調査名・調査地点  
Title, Investigation Place Makassar Ship Yard  
ボーリング孔番号  
Boring Hole No. B-1 (On Sea)

地盤標高  
Ground Elevation -1.95 m  
ボーリング孔径  
Diameter of Boring Hole 116~86 mm  
調査年月日  
Date 1980年JUL月8日  
調査担当者  
Tested By

孔内水位  
Water Level  
深さ  
Depth 15.0 m

標尺 Staff GL-m	標高 Elevation m	現場観察記録 Record of the Observation at Field				標準貫入試験 Standard Penetration Test			試料採取 Sampling		
		層厚 Stratum Thickness m	土質記号 Mark of Soil	土質名 Soil Name (JIS分類) (JIS Classification)	色 Colour	観察 Observation	深さ Depth m	10cmごとの 打撃回数 Blow Count Per 10cm		打撃回数 Number of Blows per 30cm	試料番号 Sample No.
1	1.05	1.05		Silty Clay	Darkgrey	Very soft	0.72	72			
2		1.05		Silty Sand	Darkgrey Black	Very loose Fine sand with lmm grain size Including shell frag- ment.	1.66	23	28		
3	2.91	1.86		Clay	Darkgreyish grey	Very cohesive and soft clay Containing shell fragment in places and uniform clay Inclusion of shell and sand increases at a depth of 8m to 10m.	2.15	1			
4							2.44	29	29		
5											
6											
7											
8											
9											
10		7.25					10.15	50	27	23	
11				Mudstone	Brown	Soft rock Upper portion is noticeably weathered	10.32	17	10	7	
12							11.15	50	50		
13				Sandstone	Darkgrey	Rate of core collec- tion using single core tube is about 80%.	11.23	8	8		
14											
15		15.00									
16											
17											
18											
19											
20											
21											
22											
23											
24											
25											
26											
27											
28											
29											
30											

備考  
レキ Gravel Sand  
シルト Silt  
粘土 Clay  
頁岩 Shale  
貝殻 Shell



# ボーリング柱状図

BORING LOG

調査名・調査地点  
Title, Investigation Place **Makassar Ship Yard**

地盤標高  
Ground Elevation **-1.70 m**

孔内水位  
Water Level

m

調査年月日  
Date

1980年7月5日 ~ 1980年7月8日

ボーリング孔番号  
Boring Hole No. **B-2 (On Sea)**

ボーリング孔径  
Diameter of Boring Hole **17.0 m**

深さ  
Depth **17.0 m**

調査担当者  
Tested By

標尺 Staff GL-m	標高 Elevation m	現場観察記録 Record of the Observation at Field			深さ Depth m	標準貫入試験 Standard Penetration Test			試料採取 Sampling 深さ Depth m	試料採取 方法 Sampling Method
		土質名 Soil Name	色 Colour	観察 Observation		10cm の 吹入回数 Blow Count per 10cm	10cm の 吹入回数 Blow Count per 10cm	打撃回数 Number of Blows		
1	0.71	Clay (Sedimental mud)	Darkgrey	Very soft	0.00	0	Knocking			
2	2.63	Siltsand Clayey sand	Darkgrey Black	Fine sand of 1mm grain size or less which contains shell fragment. Very loose	0.64	64	Stop			
3				This portion has a smell of organism.	1.15	1				
4			Darkgrey	Very cohesive and soft	1.50	35	35		4.00	TWS-1
5				Containing a small quantity of shell fragment and generally even clay.	2.15	2	1		4.77	
6		Clay			2.63	48	22 26		5.50	TWS-2
7					3.00	0			6.28	
8			Darkgreenish grey	This portion dose not include sand. Many shell fragments (2mm to 5mm dia) contains at a depth of 9.5m to 10.5m.	3.54	54			7.00	TWS-3
9									7.73	
10	10.70								8.50	
11	11.50	Clay	Darkgrey	Very hard clay Including many square gravels.	11.15	50	28 22		9.21	TWS-4
12		Mudstone	Brown	This portion is noticeably weathered.	11.30	15	10 5		10.00	TWS-5
13					12.15	50	50			
14					12.23	8	8			
15		Sandstone	Darkgrey	Unsound rock						
16				Rate of core collection by single tube is about 80%.						
17	17.00									

備考  
レキ Gravel  
砂 Sand  
シルト Silt  
粘土 Clay  
頁岩 Shale  
貝殻 Shell

# ボーリング柱状図

BORING LOG

調査名: 調査地点  
Title, Investigation Place **Makassar Ship Yard**

地盤標高  
Ground Elevation **1.17** m

孔内水位  
Water Level **-0.2** m

調査年月日 **1980年JUN月19日** - **1980年JUN月23日**  
Date

ボーリング孔番号  
Boring Hole No. **B-3**

ボーリング孔径 **86~66** mm  
Diameter of Boring Hole

調査担当者  
Tested By

深さ  
Depth **20.0** m

標尺 Staff GL-m	標高 Elevation m	現場観察記録 Record of the Observation at Field			深さ Depth m	標準貫入試験 Standard Penetration Test			試験採取 Sampling 深さ Depth m	試料番号 Sample No.	採取方法 Sampling Method
		土質記号 Mark of Soil	土質判定 現場標準分類(JISC) Soil Classification (JISC)	色 Colour		観察 Observation	10cmの 貫入回数 Blow-Count per 10cm	打撃回数 (N値) Number of Blows per 30cm			
1		○	Fine Sand	Darkgrey	0.15	5	2	1			
2		○		Darkgrey	0.46	31	11	10	10		
3		○	Silty Sand	Darkgrey	1.15	11	5	3	3		
4		○		Black	1.45	30	12	10	8		
5	4.95	○			2.15	2	1	1			
6	4.95	○			2.46	31	18	13			
7		○			3.15	3	1	2			
8		○			3.46	31	15	16			
9		○			4.15	2	1	1			
10		○			4.47	32	18	14			
11		○			5.00	0	Knocking				
12		○			5.76	76	Stop				
13		○			6.00	0	Knocking				
14		○			6.59	56	Stop				
15		○			7.00	0	Knocking				TWS-1
16		○			7.48	48	Stop				
17		○			7.76	0	Knocking				
18		○			8.00	0	Knocking				
19		○			8.61	61	Stop				
20		○			9.00	0	Knocking				
21		○			9.57	57	Stop				
22		○			10.00	0	Knocking				
23		○			10.51	51	Stop				
24		○			11.15	1	1				
25		○			11.71	56	56				
26		○			12.15	2	1	2			
27		○			12.67	52	25	27			
28		○			13.15	50	21	29			
29		○			13.29	14	10	4			
30		○			14.15	50	50				
31		○			14.26	11	11				

備考  
レキ Gravel  
砂 Sand  
シルト Silt  
粘土 Clay  
頁岩 Shale  
硬頁岩 Peat  
貝殻 Shell

# ボーリング柱状図

BORING LOG

調査名・調査地点  
Title, Investigation Place **Makassar Ship Yard**

地盤標高  
Ground Elevation **2.47 m**

孔内水位  
Water Level **GL-1.4 m**

調査年月日  
Date **1980年JUN月23日~1980年JUN月25日**

ボーリング孔番号  
Boring Hole No. **B-4**

ボーリング孔径  
Diameter of Boring Hole **116~86 mm**

調査担当者  
Tested By

深さ  
Depth **20.0 m**

標尺 Staff GL-m	標高 Elevation m	現場観測記録 Record of the Observation at Field				深さ Depth m	標準貫入試験 Standard Penetration Test			試料採取 Sampling 深さ Depth m	試料採取 Sampling 試料番号 Sample No.	試料採取 Sampling 採取方法 Sampling Method	
		土質記号 Mark of Soil	土質名 Soil Name	色 Colour	観察 Observation		10cm間の 打撃回数 Blow Count per 10cm	打撃回数 Number of Blows per 30cm	深さ Depth m				
1	0.80	△	Fine Sand	Brown	Max. grain size of about 1mm	0.47	32	2	3	11			
2		△	Darkgrey	Darkgrey	Containing 10mmφ to 20mmφ square gravel at a depth of 1m to 2m.	1.15	7	2	3	2			
3		△			The greater the depth, the greater the inclusion of silt and clay.	1.46	31	11	11	9			
4		△	Black	Black	Very loose	2.15	4	1	2	1			
5		△			Including a small quantity of humus.	2.48	33	14	12	7			
6	6.30	△			Very cohesive and soft clay	3.15	3	1	1	1			
7		△	Darkbrown	Darkbrown	Containing a small quantity of shell fragment (1mm to 2mm) with few inclusion of sand.	3.53	38	12	13	13			
8		△			Containing many shell fragments and sands at a depth of 12m to 13m.	4.15	2	1	1				
9		△	Clay	Darkgrey	Very hard clay Including 10mmφ to 20mmφ gravel	4.51	36	15	21				
10		△			Unsound rock	5.15	1	1	1				
11		△			The greater the depth, the greater the hardness. Rate of core collection is about 70%.	5.47	32	32					
12		△	Darkgreenish grey	Darkgreenish grey		10.00	0	Knocking	Stop				TWS-1
13		△				10.59	59						
14	13.70	△	Clay	Darkgreen		11.00	0	Knocking	Stop				
15		△				11.54	54						
16	14.40	△				12.00	0	Knocking	Stop				
17		△				12.51	51						
18		△	Sandstone (Bedrock)	Darkgrey		13.00	0	Knocking	Stop				
19		△				13.49	49						
20	20.00	△				14.15	50	16	34				
21		△				14.28	13	10	3				
22		△				15.15	50	50					
23		△				15.27	12	12					

備考  
レキ Gravel  
砂 Sand  
シルト Silt  
粘土 Clay  
頁岩 Shale  
頁石 Peat  
貝殻 Shell

# ボーリング柱状図

BORING LOG

調査名・調査地点  
Title, Investigation Place Makassar Ship Yard

地盤橋高  
Ground Elevation 2.69 m

調査年月日  
Date 1960年7月26日 ~ 1960年7月28日

ボーリング孔番号  
Boring Hole No. B-5

ボーリング孔径  
Diameter of Boring Hole 116~86 mm

調査担当者  
Tested By

深さ  
Depth 20.0 m

標尺 Staff GL-m	標高 Elevation m	現場観察記録 Record of the Observation at Field				標準貫入試験 Standard Penetration Test				試料採取 Sampling		
		層厚 Stratum Thickness m	土質記号 Mark of Soil	土質名 Soil Name (IC) 日本製土質分類(JQC)	色 Colour	観察 Observation	深さ Depth m	打撃回数 Blow Count per 10cm	打撃回数 Number of Blows per 30cm	深さ Depth m	試料番号 Sample No.	採取方法 Sampling Method
1				Fine Sand	Brown	Max. grain size of about 1mm.	0.15	33	0			
2				Silty Sand	Darkgrey	Containing a small quantity of shell fragment.	1.15	10	4	3		
3				Clayey Sand	Darkgrey	The greater the depth, the greater the inclusion of silt and clay. Including humus.	1.47	32	12	10		
4							2.15	2	1			
5				Clay	Darkgreenish grey	This clay is sand-witched partially by sand in lumps. Containing a small quantity of shell fragment.	2.53	38	13	25		
6							3.15	2	1			
7				Sandstone (Bedrock)	Darkgrey	Upper portion is noticeably weathered but the greater the depth, the greater the hardness. Unsound rock. Rate of core collection by single core tube is about 80%.	4.15	2	1			
8							4.51	36	24	12		
9				Sandstone (Bedrock)	Darkgrey	Upper portion is noticeably weathered but the greater the depth, the greater the hardness. Unsound rock. Rate of core collection by single core tube is about 80%.	5.15	2	1			
10							5.57	42	15	27		
11				Sandstone (Bedrock)	Darkgrey	Upper portion is noticeably weathered but the greater the depth, the greater the hardness. Unsound rock. Rate of core collection by single core tube is about 80%.	11.00	0	Knocking			
12							11.63	63	Stop			
13				Sandstone (Bedrock)	Darkgrey	Upper portion is noticeably weathered but the greater the depth, the greater the hardness. Unsound rock. Rate of core collection by single core tube is about 80%.	12.00	0	Knocking			
14							12.61	61	Stop			
15				Sandstone (Bedrock)	Darkgrey	Upper portion is noticeably weathered but the greater the depth, the greater the hardness. Unsound rock. Rate of core collection by single core tube is about 80%.	13.15	1	1			
16							13.56	41	41			
17				Sandstone (Bedrock)	Darkgrey	Upper portion is noticeably weathered but the greater the depth, the greater the hardness. Unsound rock. Rate of core collection by single core tube is about 80%.	14.15	50	45	5		
18							14.26	11	10	1		
19				Sandstone (Bedrock)	Darkgrey	Upper portion is noticeably weathered but the greater the depth, the greater the hardness. Unsound rock. Rate of core collection by single core tube is about 80%.	15.15	50	50			
20							15.24	9	9			

備考  
 Gravel 砾石  
 Sand 砂  
 Silt シルト  
 Clay 粘土  
 Silts 頁岩  
 Shale 頁岩  
 Peat 泥炭  
 Shell 貝殻

# ボーリング柱状図

BORING LOG

調査名・調査地所  
Title, Investigation Place Makassar Ship Yard

地盤標高  
Ground Elevation 2.01 m

孔内水位  
Water Level GL-1.0 m

調査年月日 1980年JUN月19日 ~ 1980年JUN月21日  
Date

ボーリング孔番号  
Boring Hole No. B-6

ボーリング孔径 86~66 mm  
Diameter of Boring Hole

調査担当者  
Tested By

深さ  
Depth 20.0 m

標尺 Staff GL-m	標高 Elevation m	現場観察記録 Record of the Observation at Field			観察 Observation	標準貫入試験 Standard Penetration Test		試料採取 Sampling		
		土質記号 Stratum Mark of Soil	土質名 Name of Soil (JIS)	色 Colour		深さ Depth m	打撃回数 Blow Count per 10cm		打撃回数 N 値 Number of Blows per 30cm	深さ Depth m
1	1.30	θ	Fine Sand	Brown	Containing a small quantity of shell fragment and grass root.	0.15	2	3		
2	1.47	θ	Fine Sand	Dark grey	The greater the depth, the greater the inclusion of silt and clay. Max. grain size of about 1mm.	0.47	3	9		
3	2.15	θ	Silty Sand			1.15	2			
4	2.45	θ				1.47	10			
5	3.15	θ				2.15	10			
6	3.68	θ				3.15	11			
7	4.15	θ				3.68	25			
8	4.45	θ				4.15	28			
9	5.15	θ				4.45	30			
10	5.71	θ	Clayey Silt	Black	Very soft Including a small quantity of shell fragment.	5.15	56			
11	6.15	θ				5.71	56			
12	6.65	θ				6.15	2			
13	7.15	θ				6.65	50			
14	7.47	θ				7.15	1			
15	7.47	θ				7.47	32			
16	8.15	θ				8.15	1			
17	8.66	θ				8.66	51			
18	9.15	θ				9.15	0	Nokking		
19	9.51	θ				9.51	36	Stop		
20	10.15	θ				10.15	0	Nokking		
21	10.58	θ				10.58	43	Stop		
22	11.15	θ				11.15	0	Nokking		
23	11.52	θ				11.52	37	Stop		
24	12.15	θ				12.15	1	Nokking		
25	12.79	θ				12.79	64	Stop		
26	13.00	θ				13.00	0	Nokking		
27	13.32	θ				13.32	32	Stop		
28	14.15	θ				14.15	22	2	19	
29	14.45	θ				14.45	30	14	6	
30	15.15	θ				15.15	50	25	25	
31	15.31	θ				15.31	16	10	6	
32	16.15	θ				16.15	50	50		
33	16.24	θ				16.24	9	9		

備考  
 レキ Gravel  
 砂 Sand  
 シルト Silt  
 粘土 Clay  
 頁岩 Shale  
 硬岩 Hard Rock  
 貝殻 Shell

# ボーリング柱状図

## BORING LOG

調査名・調査地点  
Title, Investigation Place **Makassar Ship Yard**

地盤標高  
Ground Elevation **2.46** m

調査年月日 **1980年6月30日** 1980 JUN 30

ボーリング孔番号  
Boring Hole No. **B-7**

ボーリング孔径  
Diameter of Boring Hole **116~86** mm

調査担当者  
Tested By

深さ  
Depth **20.0** m

標尺 Scale GL-m	高さ Elevation m	孔内水位 Water Level m	現場観察記録 Record of the Observation at Field			深さ Depth m	標準貫入試験 Standard Penetration Test			試料採取 Sampling		
			土質記号 Mark of Soil	土質名 Soil Name	色 Colour		観察 Observation	10cmの 吹入回数 Blow Count per 10cm	打撃回数 Number of Blows per 30cm		深さ Depth m	
1				Fine Sand	Brown	0.15	31	11	9	11		
2				Silty Sand	Darkgrey	0.46	31	11	9	11		
3						1.15	7	2	3	2		
4						1.47	32	12	11	9		
5				Clayey Sand	Black	2.15	3	1	2			
6	5.90			Clay	Darkgreenish grey	2.48	33	17	16			
7						3.15	2	1	1			
8						3.50	35	22	13			
9						4.15	2	1	1			
10						4.48	33	18	15			
11						5.15	3	1	1			
12						5.49	34	10	10	14		
13						12.00	0	Knocking	Stop			TWS-1
14	13.85					12.61	61					
15						13.00	0	Knocking	Stop			TWS-2
16						13.56	56					
17						14.15	3	1	1			
18						14.53	38	16	12	10		
19						15.15	50	50				
20						15.24	9	9				
21						16.15	50	50				
22						16.22	7	7				
23												
24												
25												
26												
27												
28												
29												
30												

備考  
レキ Gravel Sand  
シルト Silt  
粘土 Clay  
頁岩 Shale  
貝殻 Shell

# ボーリング柱状図

BORING LOG

調査名・調査地点  
Title, Investigation Place **Makassar Ship Yard**

地盤標高  
Ground Elevation **2.10 m**

孔内水位  
Water Level **GL-1.20 m**

調査年月日 **1980年JUN月21日** ~ **1980年JUN月23日**  
Date

ボーリング孔番号  
Boring Hole No. **B-8**

ボーリング孔径  
Diameter of Boring Hole **86~66 mm**

深さ  
Depth **21.0 m**

調査担当者  
Tested By

標尺 Staff GL-m	標高 Elevation m	現場観察測記録 Record of the Observation at Field			観察 Observation	標準貫入試験 Standard Penetration Test			試料採取 Sampling	
		土質名 Soil 現場判定 現場判定 三角座標分類(TC) 日本標準土質分類(JUC)	土質記号 Mark of Soil	土質色 Colour		深さ Depth m	10cmごとの 打撃回数 Blow Count per 10cm	打撃回数 N 値 Number of Blows per 30cm		深さ Depth m
1		Fine Sand		Brown	Max. grain size of about lmm. Very loose	0.15	10	10		
2		Silty Sand		Darkgrey	The greater the depth, the greater the inclusion of silt and clay.	1.15	8	2	4	
3						1.45	30	10	10	
4		Clayey Sand		Darkgrey	Containing clay in lumps, and shell fragment.	2.15	1	1		
5		Sandy Silt		Darkgrey		2.45	30	30		
6	6.35					3.15	5	2	2	
7						3.45	30	10	12	
8						4.15	11	3	3	
9		Clay		Darkgrey	Very soft and cohesive.	4.45	30	12	10	
10						5.15	1	1		
11						5.61	46	46		
12						6.15	2	1	1	
13						6.48	33	20	13	
14	14.20	Clay		Darkgreenish grey	Including a little shell fragment (lmm to 2mm), with a few inclusion of sand.	7.00	0	Knocking		
15						7.40	40	40	Stop	
16						8.00	0	Knocking		
17						8.85	85	85	Stop	
18						9.00	0	Knocking		
19						9.56	56	56	Stop	
20						10.00	0	Knocking		
21	21.00	Clay		Darkgreenish grey	Uniform clay layer.	10.55	55	55	Stop	
22						11.00	0	Knocking		
23						11.63	63	63	Stop	
24						12.00	0	Knocking		
25						12.68	68	68	Stop	
26						13.00	0	Knocking		
27						13.53	53	53	Stop	
28						14.00	5	1	2	
29						14.30	30	10	10	
30						15.15	9	2	3	
31						15.45	30	10	10	
32						16.15	50	30	20	
33						16.33	18	10	8	
34						17.15	50	41	9	
35						17.28	13	10	3	

備考  
レキ Gravel Sand シルト Silt 粘土 Clay 頁岩 Shale 貝殻 Shell

Rate of core collection is about 60%.  
Upper portion easily gets a finger nail scratch, the greater the depth, the greater the hardness.Unsound rock  
Containing gravel.  
Rigid clayUniform clay layer.  
Inclusion of sand.  
Including a little shell fragment (lmm to 2mm), with a few inclusion of sand.  
Very soft and cohesive.  
Containing clay in lumps, and shell fragment.  
The greater the depth, the greater the inclusion of silt and clay.  
Very loose  
about lmm.  
Max. grain size of

# ボーリング柱状図

## BORING LOG

調査名・調査地点  
Title, Investigation Place  
Makassar Ship Yard

地盤標高  
Ground Elevation  
1.98 m

孔内水位  
Water Level  
GL - 1.10 m

調査年月日  
Date  
1980 JUL 1 ~ 1980 JUL 3

ボーリング孔番号  
Boring Hole No.  
B-9

ボーリング孔径  
Diameter of Boring Hole  
86~66 mm

深さ  
Depth  
20.0 m

調査担当者  
Tested By

標尺 Staff GL-m	層厚 Stratum Thickness m	土質記号 Mark of Soil	現場観察記録 Record of the Observation at Field		深さ Depth m	標準貫入試験 Standard Penetration Test			試料採取 Sampling 深さ Depth m	試料採取 方法 Sample No. Method
			土質名 Soil Name (JIS分類) 日本製土質分類(JIS)	色 Colour		観察 Observation	10cm の 打撃回数 Blow Count per 10cm	打撃回数 Number of Blows per 30cm		
1		Gravel Sand	Brown	Backfilling embankment for reclaimed land.	0.15 0.49	6 34	2 11	3 10	13	
2		Siltsand Clayey Sand	Darkgrey Black	Irregularly containing clay and silt. Including shell fragment (2mm to 5mm).	1.15 1.46	11 31	5 10	4 10	2 11	
3					2.15 2.45	7 30	3 10	3 8	1 12	
4	4.50				3.15 3.45	6 30	1 10	2 10	3 10	
5	4.50				4.15 4.48	2 33	1 20	1 13		
6		Sandy Clay Clayey Sand	Darkgreenish grey	Including a lot of shell fragment (5mm to 10mm) and coral fragment (5mm to 20mm). Soft clay	5.15 5.46	5 31	1 11	1 10	3 10	
7					6.15 6.45	2 30	1 10	1 20		
8					7.15 7.48	2 33	1 20	1 13		
9					8.00 8.70	0 70	Knocking Stop			
10	6.00				9.00 9.65	0 65	Knocking Stop			
11		Clay	Brown	Rigid clay Including gravel.	10.15 10.50	4 35	2 14	1 10	1 11	
12	1.80				11.15 11.41	50 26	8 10	17 10	25 6	
13		Mudstone Sandstone	Brown Darkgrey	The upper portion is greatly weathered, but the greater the depth, the greater the hardness. Rate of core collection is about 70% to 80%. Containing a little fossiliferous shell fragment.	12.15 12.33	50 18	14 10	36 8		
14					13.15 13.22	50 7	50 7	50 7		
15										
16										
17										
18										
19										
20	20.00									
21										
22										
23										
24										
25										
26										
27										
28										
29										
30										

備考  
レキ Gravel  
砂 Sand  
シルト Silt  
粘土 Clay  
頁岩 Shale  
頁岩 Peat  
貝殻 Shell



# ボーリング柱状図

## BORING LOG

調査名 調査地点  
Title, Investigation Place **Makassar Ship Yard**

地盤標高  
Ground Elevation **2.07 m**

調査年月日  
Date **1980年JUN月22日**

北内水位  
Water Level **GL-120 m**

ボーリング孔番号  
Boring Hole No. **B-10**

ボーリング孔径  
Diameter of Boring Hole **116~86 mm**

調査担当者  
Tested By

深さ  
Depth **22.0 m**

標尺 Staff GL-m	標高 Elevation m	内水位 Water Level m	現場観測記録 Record of the Observation at Field				標準貫入試験 Standard Penetration Test			試料採取 Sampling 深さ Depth m	試料採取 方法 Sample No. Sampling Method
			土質記号 Soil Mark of Soil	土質名 Name Colour	色 Colour	観察 Observation	深さ Depth m	10cm の 打撃回数 Blow Count per 10cm	打撃回数 Number of Blows per 30cm		
1			Fine Sand	Brown		Max. grain size of about 1mm. Including humus (root of grass). Containing silt and clay in lumps.	0.50	35	0		
2			Silty Sand	Darkgrey		The greater the depth, the greater the inclusion of clay.	1.15	2			
3			Clayey Sand	Black		Entirely containing shell fragment.	1.50	35			
4			Silty Clay	Darkgrey		Including a little sand and shell fragment (1mm to 2mm), but uniform clay throughout the stratum.	2.15	3			
5			Clay	Darkgreenish grey		Very cohesive and soft	2.46	31			
6			Silty Clay	Darkgrey		Containing a lot of shell fragment and sand at a depth of 12m to 14m.	3.15	6			
7			Clay	Darkgreenish grey			3.45	30			
8			Silty Clay	Darkgrey			4.15	4			
9			Clay	Darkgreenish grey			4.45	30			
10			Silty Clay	Darkgrey			5.00	0	Knocking		
11			Clay	Darkgreenish grey			5.55	55	Stop		
12			Silty Clay	Darkgrey							
13			Clay	Darkgreenish grey							
14			Silty Clay	Darkgrey							
15			Clay	Darkgreenish grey							
16			Sandstone	Darkgrey							
17			Clay	Darkgreenish grey							
18			Silty Clay	Darkgrey							
19			Clay	Darkgreenish grey							
20			Silty Clay	Darkgrey							
21			Clay	Darkgreenish grey							
22			Silty Clay	Darkgrey							
23			Clay	Darkgreenish grey							
24			Silty Clay	Darkgrey							
25			Clay	Darkgreenish grey							
26			Silty Clay	Darkgrey							
27			Clay	Darkgreenish grey							
28			Silty Clay	Darkgrey							
29			Clay	Darkgreenish grey							
30			Silty Clay	Darkgrey							

備考

# ボーリング柱状図

BORING LOG

調査名・調査地点  
Title, Investigation Place **Makassar Ship Yard**

地盤標高  
Ground Elevation **0.64** m

調査年月日  
Date **1980年JUL月 9 日**

ボーリング孔番号  
Boring Hole No. **B-11**

ボーリング孔径  
Diameter of Boring Hole **18.0** mm

調査担当者  
Tested By

標尺 Staff GL-m	標高 Elevation m	現場観察記録 Record of the Observation at Field				深さ Depth m	標準貫入試験 Standard Penetration Test			試料採取 Sampling
		土質記号 Mark of Soil	土質名 Soil Name	色 Colour	観察 Observation		(N値) Blow Count per 10cm	10cm以上の 打撃回数 Number of Blows per 30cm	深さ Depth m	
1	0.75		Clay	Darkgrey	Very soft	0.00	0	0		
2			Silty Sand	Darkgrey	Very loose	1.15	4	2		
3			Clayey Sand	Black	Containing shell fragment.	1.47	32	12		
4	3.80					2.15	1	0		
5					Upper parting includes shell fragment.	2.47	32	10		
6					Very cohesive and soft clay.	3.15	1	1		
7			Clay	Darkgrey		3.70	55	55		
8					Containing a lot of shell fragment at a depth of 9.5m to 1.1m.	4.00	0	Knocking		
9						4.76	76	Stop		
10						5.00	0	Knocking		
11	11.20					5.68	68	Stop		
12	12.40		Clay	Darkgreenish grey		6.00	0	Knocking		
13			Sandstone (Bedrock)	Darkgrey		6.77	77	Stop		
14						7.00	0	Knocking		
15						7.78	78	Stop		
16						8.00	0	Knocking		
17						8.74	74	Stop		
18	18.00					9.00	0	Knocking		
19						9.75	75	Stop		
20						10.00	0	Knocking		
21						10.74	74	Stop		
22						11.15	16	4		
23						11.45	30	10		
24						12.15	50	7		
25						12.40	25	10		
26						13.15	50	50		
27						13.25	10	10		

備考

- Gravel
- Sand
- Silt
- Clay
- Siltstone
- Sandstone
- Shell

# ボーリング柱状図

BORING LOG

調査名・調査地点  
Title, Investigation Place  
Makassar Ship Yard

地盤標高  
Ground Elevation  
1.62 m

北内水位  
Water Level  
GL-0.70 m

調査年月日  
Date  
1980年JUL月4日~1980年JUL月5日

ボーリング孔番号  
Boring Hole No.  
B-12

ボーリング孔径  
Diameter of Boring Hole  
86~66 mm

調査担当者  
Tested By

深さ  
Depth  
20.0 m

標尺 Scale GL-m	深さ Depth m	土質 Soil	土質記号 Mark of Soil	現場観察記録 Record of the Observation at Field		観察 Observation	標準貫入試験 Standard Penetration Test			試料採取 Sampling	
				土質名 Name of Soil	色 Colour		深さ Depth m	10cmの 打撃回数 Blow Count per 10cm	打撃回数 Number of Blows per 30cm		深さ Depth m
1	0.15	Fine Sand	v v	Brown		Max. grain size of about 1mm. Very loose	0.15	2	3		
2	1.15	Silty Sand	v v	Darkgrey		Containing clay and silt in lumps.	1.15	4	10		
3	1.45	Clayey Sand	v v	Black		Including humus (root of grass) and shell fragment.	1.45	30	10		
4	2.15						2.15	3	1		
5	2.48						2.48	33	10		
6	3.15						3.15	3	1		
7	3.47						3.47	32	10		
8	4.00						4.00	0	Knocking		
9	4.81						4.81	81	Stop		
10	5.00						5.00	0	Knocking		
11	5.61						5.61	61	Stop		
12	6.00						6.00	0	Knocking		
13	6.70						6.70	70	Stop		
14	7.00						7.00	0	Knocking		
15	7.65						7.65	65	Stop		
16	8.00						8.00	0	Knocking		
17	8.55						8.55	55	Stop		
18	9.00						9.00	0	Knocking		
19	9.73						9.73	73	Stop		
20	10.00						10.00	0	Knocking		
21	10.70						10.70	70	Stop		
22	11.00						11.00	0	Knocking		
23	11.70						11.70	70	Stop		
24	12.00						12.00	0	Knocking		
25	12.75						12.75	75	Stop		
26	13.15						13.15	5	1		
27	13.45						13.45	30	10		
28	14.15						14.15	50	28		
29	14.30						14.30	15	10		
30	15.15						15.15	50	50		
31	15.23						15.23	8	8		

備考  
レキ Gravel  
砂 Sand  
シルト Silt  
粘土 Clay  
頁岩 Shale  
硬岩 Bedrock  
貝殻 Shell  
Pest  
試料採取方法  
Sample No.  
採取方法  
Sampling Method

# ボーリング柱状図

## BORING LOG

調査名・調査地点  
Title, Investigation Place **Makassar Ship Yard**

地盤標高  
Ground Elevation **2.02 m**

北内水位  
Water Level **GL-1.10 m**

調査年月日 **1980 JUN 28** 日 ~ **1980 JUN 30** 日  
Date

ボーリング孔番号  
Boring Hole No. **B-13**

ボーリング孔径 **86** mm  
Diameter of Boring Hole

調査担当者  
Tested By

深さ  
Depth **20.0 m**

標尺 Staff GL-m	標高 Elevation m	層厚 Stratum Thickness m	土質記号 Mark of Soil	現場観察測記録 Record of the Observation at Field		観察 Observation	深さ Depth m	標準貫入試験 Standard Penetration Test			試料採取 Sampling	
				土質名 Soil Name	色 Colour			貫入回数 (N値) (N value) 回/cm	10cm 貫入回数 Blow Count per 10cm	打撃回数 Number of Blows per 30cm		深さ Depth m
1			Fine Sand	Brown		Max. grain size of about 1mm.	0.15	6	3	10		
2			Silty Sand	Darkgrey		Containing shell fragment.	0.46	31	10	11		
3			~			Very loose	1.15	5	2	2		
4			Clayey Sand			Irregularly including clay.	1.46	31	12	12		
5							2.15	6	2	2		
6	5.70	5.70				This portion has a smell of organism.	2.47	32	12	11		
7			Darkbrown			Containing shell fragment in places.	3.15	4	1	2		
8			Clay	Darkgrey		Soft	3.45	30	10	10		
9						Very cohesive	4.15	5	2	2		
10						Including a lot of shell fragment and sand at a depth of 12m to 14m.	4.45	30	10	11		
11							5.15	5	2	1		
12							5.46	31	10	10		
13	14.20	8.50	Clay	Darkgreenish grey		Rigid (weathered rock stratum) Including gravel	6.00	0	Knocking	Stop		
14						Upper portion is noticeably weathered, but the greater the depth, the greater the hardness.	6.65	65	Stop	Stop		
15	15.23	1.03	Mudstone	Darkgrey		Rate of core collection is about 80%.	7.00	0	Knocking	Stop		
16							7.68	68	Stop	Stop		
17							8.00	0	Knocking	Stop		
18							8.75	75	Stop	Stop		
19							9.00	0	Knocking	Stop		
20							9.56	56	Stop	Stop		
21	20.00						10.00	0	Knocking	Stop		
22							10.75	75	Stop	Stop		
23							11.00	0	Knocking	Stop		
24							11.65	65	Stop	Stop		
25							12.00	0	Knocking	Stop		
26							12.50	50	Stop	Stop		
27							13.00	0	Knocking	Stop		
28							13.74	74	Stop	Stop		
29							14.15	6	2	2		
30							14.50	35	10	12		
							15.15	50	27	23		
							15.29	14	10	4		
							16.15	50	50			
							16.23	6	6			

備考

- Gravel 砾石
- Sand 砂
- Silt シルト
- Clay 粘土
- Shale 頁岩
- Peat 泥炭
- Shell 貝殻

# ボーリング柱状図

BORING LOG

調査名・調査地点  
Title, Investigation Place  
Makassar Ship Yard

地盤標高  
Ground Elevation 2.24 m  
北内水位  
Water Level GL-1.30 m

調査年月日 1980年JUN月29日 ~ 1980年JUL月1日  
Date

ボーリング孔番号  
Boring Hole No. B-14

ボーリング孔径 86~66 mm  
Diameter of Boring Hole

深さ 21.0 m  
Depth

調査担当者  
Tested By

標尺 Staff GL-m	標高 Elevation m	層厚 Stratum Thickness m	現場観察記録 Record of the Observation at Field		観察 Observation	標準貫入試験 Standard Penetration Test			試料採取 Sampling
			土質記号 Mark of Soil	土質名 Name Colour		深さ Depth m	打撃回数 (N値) Blow Count per 10cm	打撃回数 N 値 Number of Blows per 30cm	
1		1.50	Fine Sand	Brown	Max. grain size of about 1mm.	0.48	33	2	
2			Silty Sand	Darkgrey	Irregularly containing clay and silt. Including a little humus (root of grass) and shell fragment.	1.15	2	1	
3			Clayey Sand	Black		2.15	2	1	
4						2.46	31	16	15
5	5.70	5.70				3.15	4	2	
6					Mainly consisting of medium sand and fine sand, of which a cohesive clay accounts for 30% to 40%.	3.50	35	13	10
7						4.15	3	1	
8						4.46	31	10	11
9						5.15	3	1	
10						5.48	33	11	12
11						6.15	2	1	
12	12.31	6.61	Clayey Sand	greenish grey	Including a lot of shell fragment and coral fragment.	6.45	30	13	17
13			Clay			7.15	2	1	
14	13.55	1.24			Rigid clay Containing pumice (5mm to 8mm). Unsound rock	7.55	40	25	15
15			Mudstone			8.15	2	1	
16			Sandstone (Bedrock)	Darkgrey		8.54	39	26	13
17						9.15	2	1	
18						9.48	33	20	13
19						10.15	2	1	
20						10.53	38	21	17
21	21.00					11.15	1	1	
22						11.66	51	51	
23						12.15	3	1	2
24						12.49	34	18	16
25						13.15	50	28	22
26						13.30	15	10	5
27						14.15	50	50	
28						14.23	8	8	

備考  
レキ Gravel  
砂 Sand  
シルト Silt  
粘土 Clay  
頁岩 Shale  
貝殻 Peat  
Shell

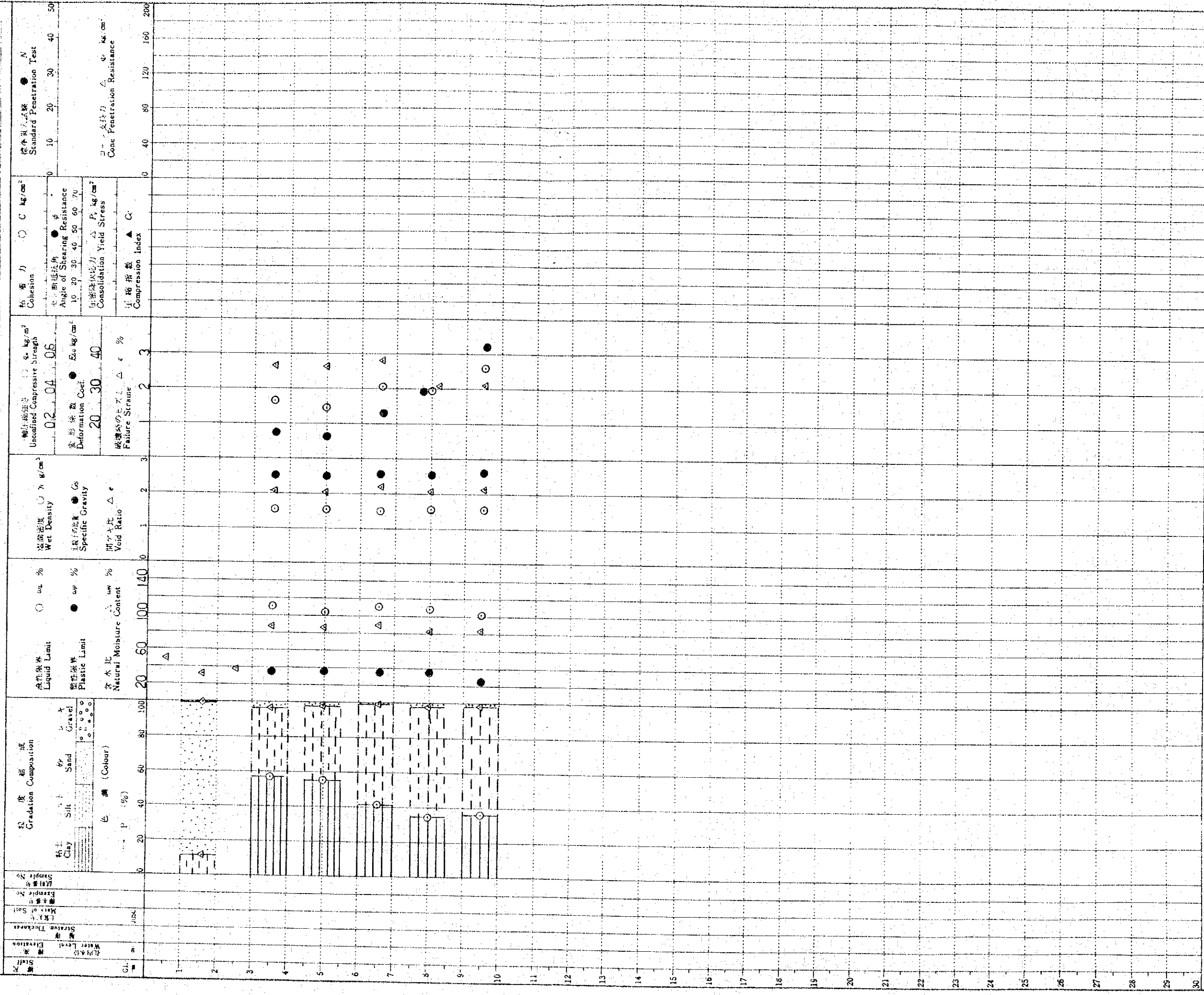
B-1

# 土質試験柱状図

## SOIL TESTS LOG

調査名・調査地点 Title, Investigation Place **Makassar Ship Yard** 地盤標高 Ground Elevation **-1.95** m 北内水位 Water Level 調査年月日 Date **80** 年 **7** 月 **10** 日 年 月 日

ボーリング孔番号 Boring Hole No. **B-1** 孔径 Diameter of Boring Hole **116 ~ 86** mm 深さ Depth 調査試験報告者 Tested By



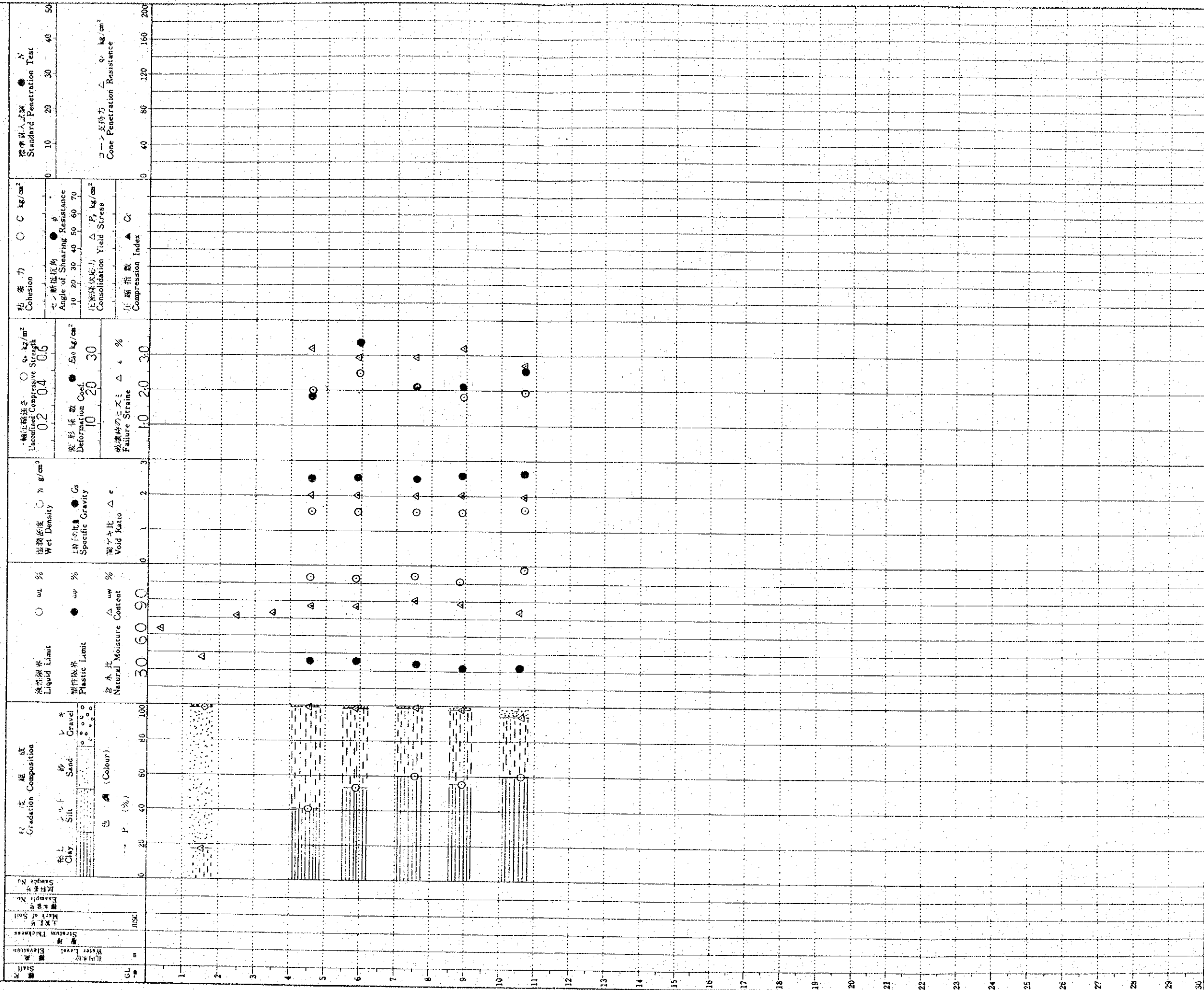
備考 (Remarks)

# 土質試験柱状図

## SOIL TESTS LOG

調査名・調査地点 Title, Investigation Place McKissack Ship Yard 地盤標高 Ground Elevation -170 m 調査年月日 60 年 7 月 9 日 60 年 7 月 19 日  
 調査場所・調査地点 Title, Investigation Place McKissack Ship Yard 地盤標高 Ground Elevation -170 m 調査年月日 60 年 7 月 9 日 60 年 7 月 19 日

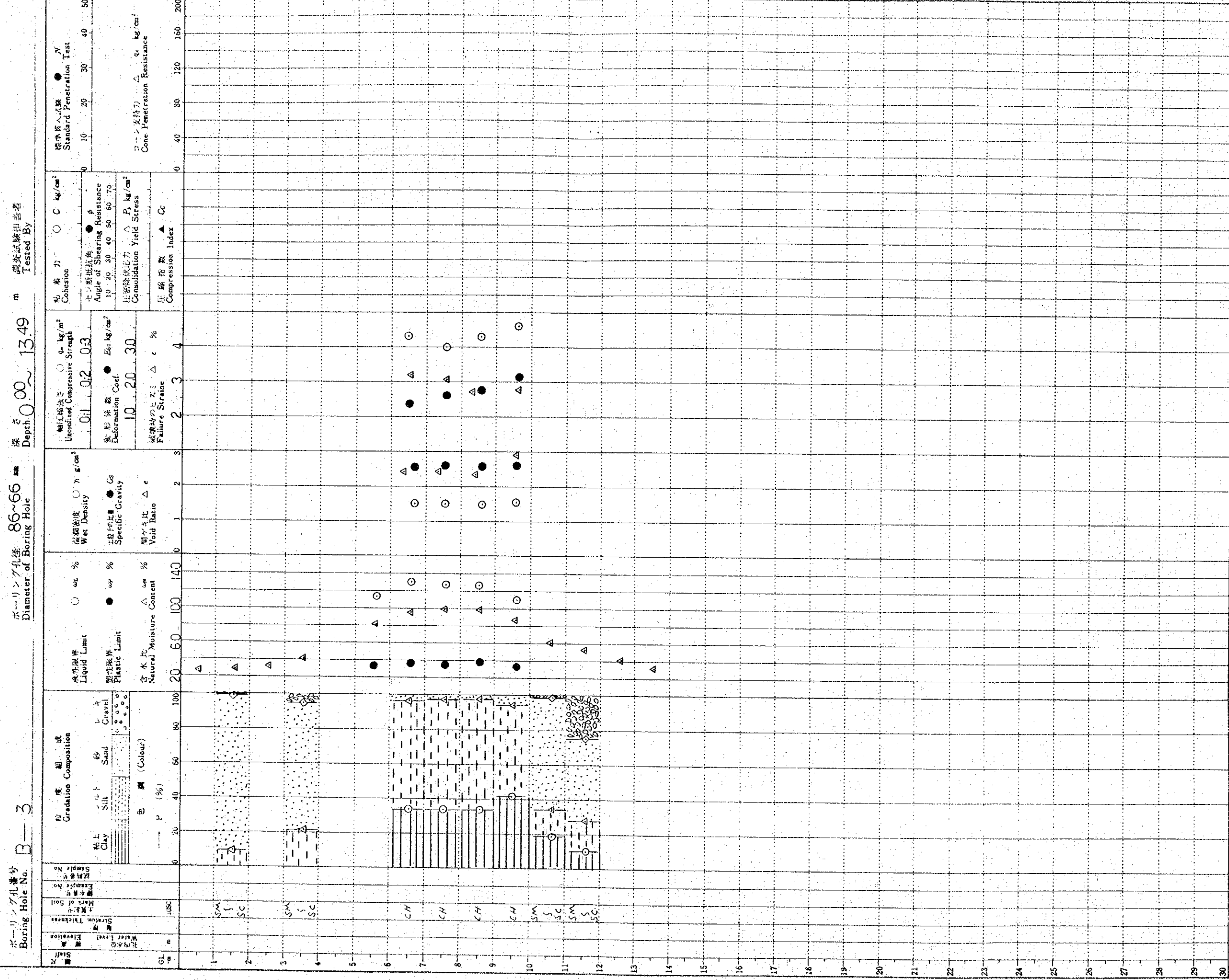
ボーリング孔番号 B-2 ボーリング孔径 116~86 mm 深さ 0.00~10.72 m 調査試験担当者 Tested By



備考 (Remarks)

# 土質試験柱状図 SOIL TESTS LOG

調査名: 調査地点 Title, Investigation Place Makassar Ship Yard 地盤標高 Ground Elevation 1.17 m 調査年月日 Date 80 6 27 年 月 日  
 ボーリング孔番号 Boring Hole No. B-3 ボーリング孔径 Diameter of Boring Hole 86~66 mm 深さ Depth 0.00~13.49 m 調査試験担当者 Tested By



備考 (Remarks)

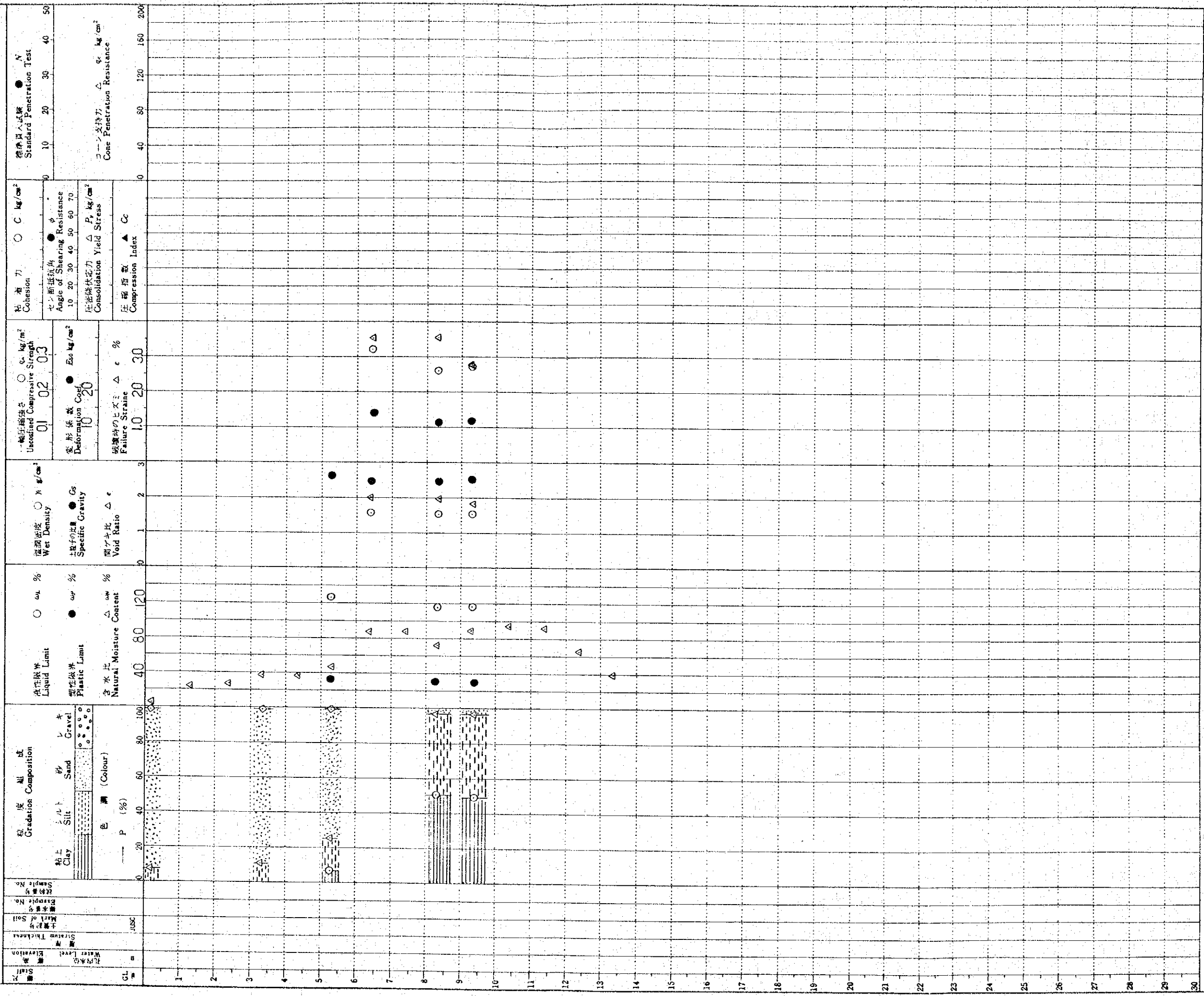


# 土質試験柱状図

## SOIL TESTS LOG

調査地・調査地点 Title: Investigation Place **Makassar Ship Yard** 地盤標高 Ground Elevation **2.47** m 孔内水位 Water Level 調査年月日 **80年6月25日** ~ **80年7月19日** m

ボーリング孔番号 Boring Hole No. **B-4** ボーリング孔径 **116~86** mm 深さ **0.00** ~ **14** m 調査試験担当者 Tested By



備考 (Remarks)

# 土質試験柱状図

## SOIL TESTS LOG

調査名・調査地点  
Title, Investigation Place Makassar Shi Yard

地盤標高  
Ground Elevation 2.69 m

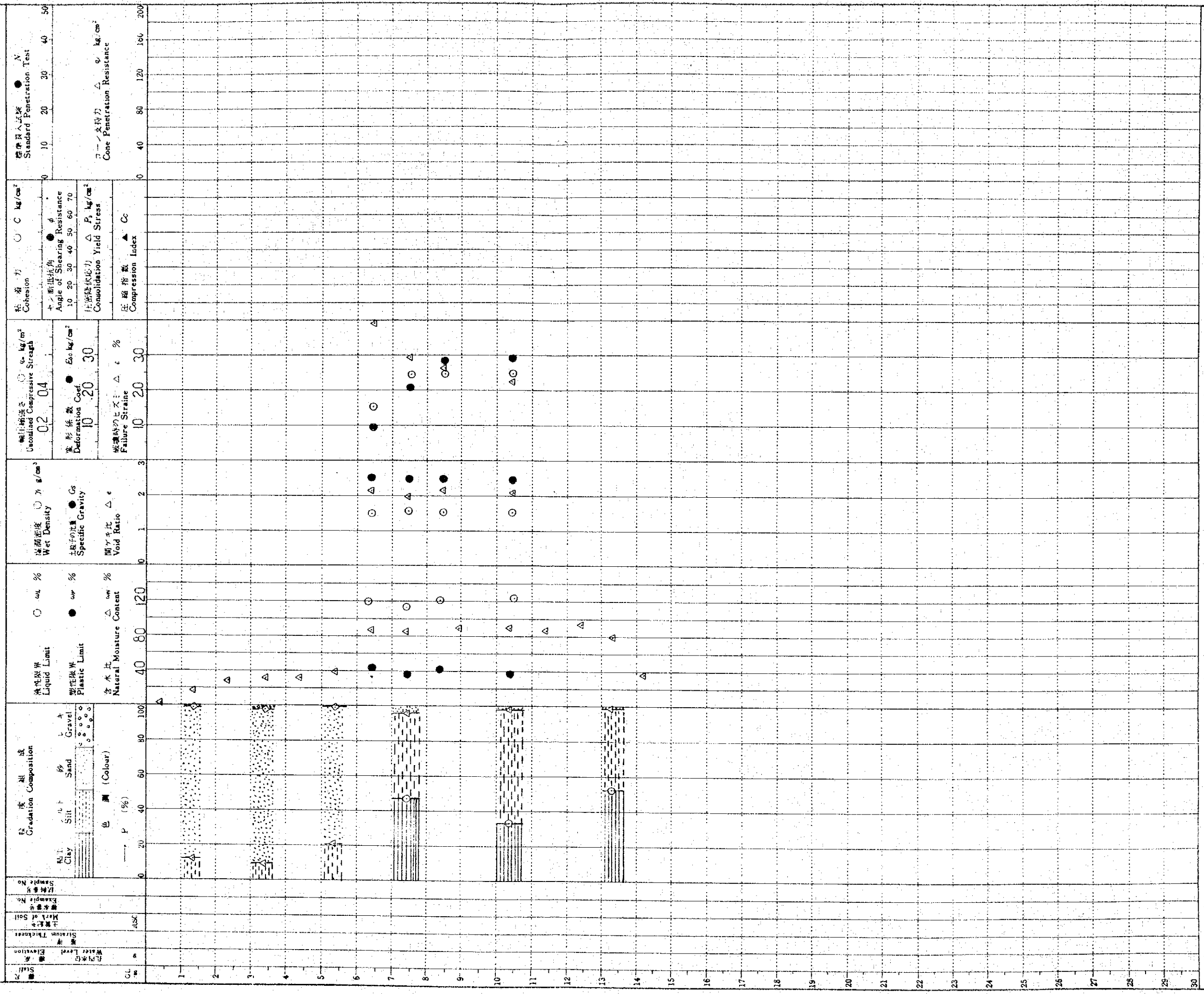
調査年月日 80年6月28日~80年7月19日  
Date

ボーリング孔番号  
Boring Hole No. B-5

ボーリング孔径 116~86 mm

深さ 0.00 ~ 14.26 m

調査試験担当者  
Tested By



備考 (Remarks)

# 土質試験柱状図

## SOIL TESTS LOG

調査名・調査地点  
Title, Investigation Place Makassar Ship Yard

地盤標高  
Ground Elevation 2.46 m

孔内水位  
Water Level

m

調査年月日  
Date 80 年 7 月 2 日

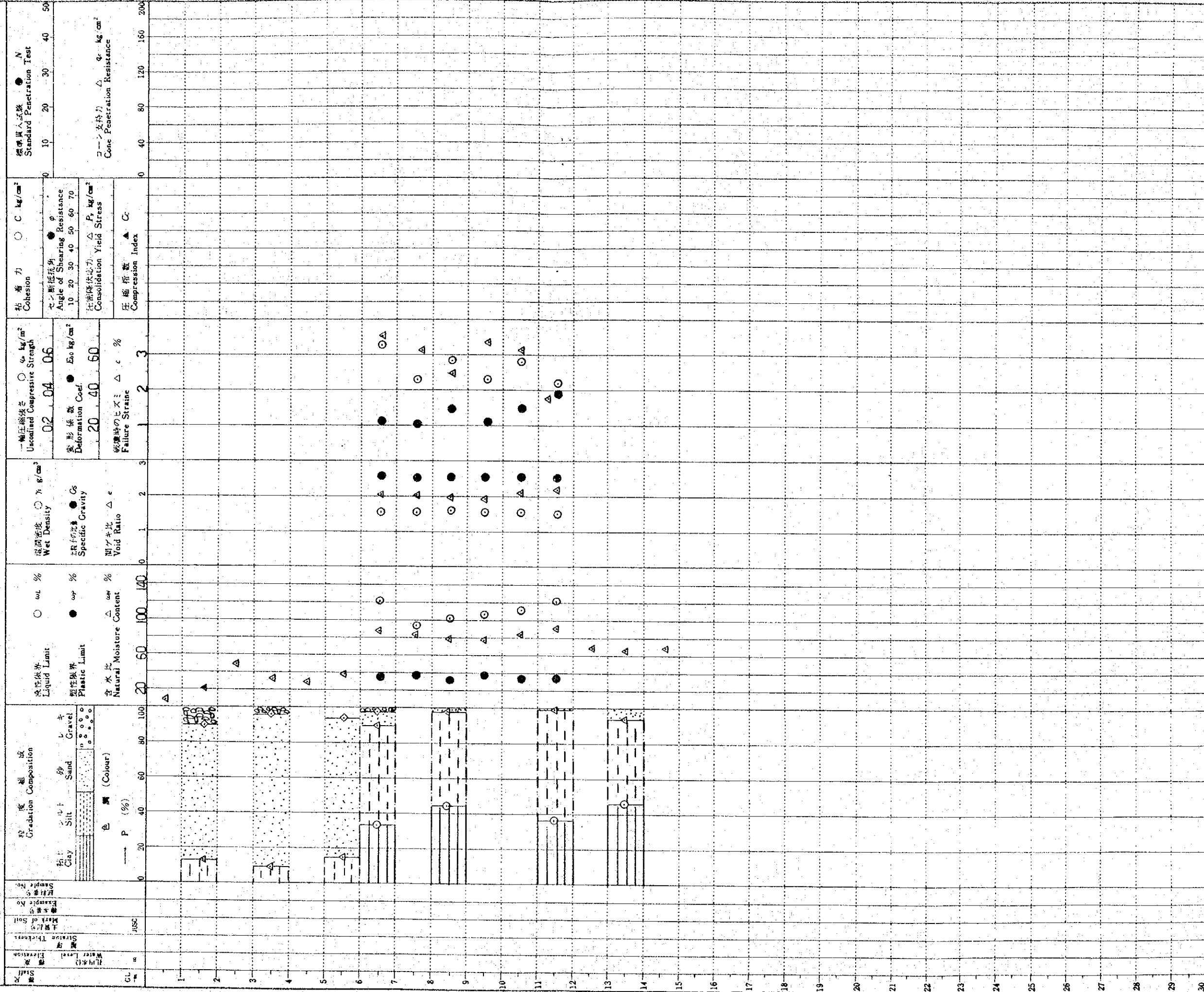
日  
80 年 7 月 2 日

ボーリング孔番号  
Boring Hole No. B-7

ボーリング孔径 116~86 mm

深さ 00 ~ 1453 m

調査試験担当者  
Tested By



備考 (Remarks)

# 土質試験柱状図

## SOIL TESTS LOG

B-10

調査名: 調査地点 Makassar Ship Yard

地盤標高 2.07 m

孔内水位 2.07 m

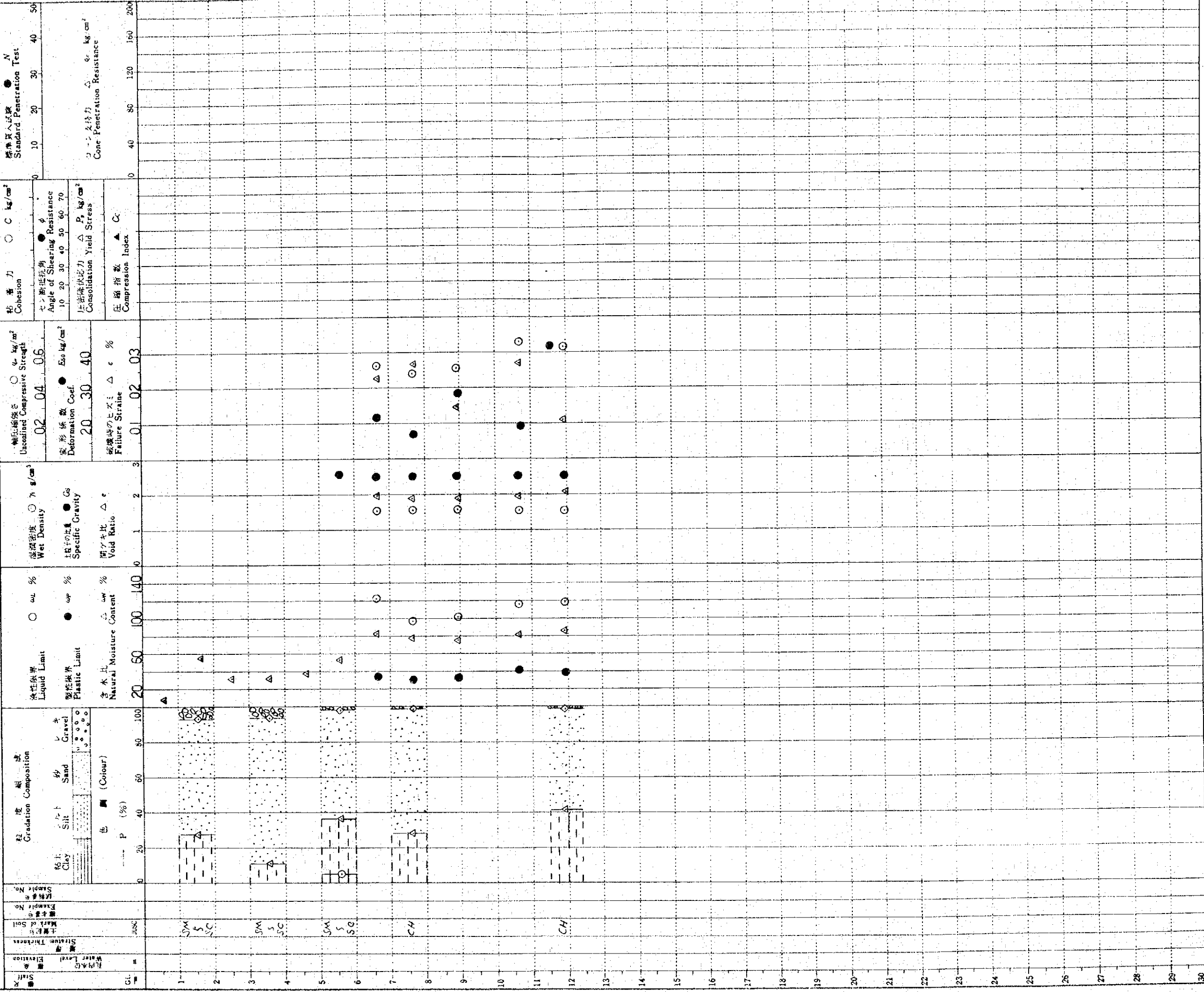
調査年月日 80.6.25 年 6 月 25 日

ボーリング孔番号 B-10

ボーリング孔径 116~86 mm

深さ 0.00~12.07 m

調査試験担当者 Tested By



備考 (Remarks)