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FEASIBILITY REPORT KELKIT-KARATAS. HYDROELECTRIC PROJECT

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FEASIBILITY REPORT KELKIT-KARATAS HYDROELECTRIC PROJECT

(VOLUME II)

MARCH 1969

GOVERNMENT OF JAPAN

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Volume II Basic Studies and Data

CONTENTS

- II 1 Hydrology .
- II 2 Geology
- II 3 Construction Materials
- II 4 Size and Operation of Reservoir and Calculation of Sedimentation
- II 5 Load Forecast and Installed Capacity of Power Stations
- II 6 Irrigation Summary Reports of NIKSAR, ERBAA and LEEDSHILL for CARSAMBA

II 1 Hydrology

Contents

II 1-1	Hydrolog	gical Study and Data	1 - 1
	II 1-1-1	Runoff Gaging Stations and Meteorological Stations in the Yesilirmak Basin	1 - 1
	II 1-1-2	Verification of Data	1 - 1
	II 1-1-3	Evaporation Losses from Reservoir Surface	1 - 2
	s ` , ~	a) Evaporation	1 - 2
		b) Evapotranspiration	1 - 3
II 1-2	Flood Di	ischarge at Kilickaya	1 - 3
	II 1-2-1	Historical Flood Values	1 - 3
	II 1-2-2	Enveloped Curve Flood in Turkey	1 - 4
	II 1-2-3	Design Flood Curve in Turkey	1 - 4
	II 1-2-4	Statistical Method	1 - 5
	II 1-2-5	Physical Method	1 - 7
	II 1-2-6	Summary of the Results	1-10

-

Tables

ĵ,

٠

3

1

II 1-1	Carsamba Monthly Precipitation	1-11
II 1-2	Carsamba Monthly Temperature	1-11
II 1-3	Corum Monthly Precipitation	1-12
II 1-4	Corum Monthly Temperature	~ 1-12
II 1-5	Erbaa Monthly Precipitation	1-13
II 1-6	Erbaa Monthly Temperature	1-13
II 1-7	Merzifon Monthly Precipitation	1-14
II 1-8	Merzifon Monthly Temperature	1-14
II 1-9	Niksar Monthly Precipitation	1-15
II 1-10	Niksar Monthly Temperature	1-15
II 1-11	Tokat Monthly Precipitation	1-16
II 1-12	Tokat Monthly Temperature	1-16
II 1-13	Amasya Monthly Precipitation	1-Ì7
II 1-14	Evaporation Loss from the Reservoir	1-17 ·
II 1-15	Evaporation Loss from the Reservoir Evaporation at Samsun Station	1-18
II 1-16	Evaporation at Mezifon Station	1-18
II 1-17	Kilickaya Monthly Run-off	´ 1-19
II 1-18	Evaporation at Mezifon Station Kilickaya Monthly Run-off Ayvacik Monthly Run-off	1-19
II 1-19	Almus Monthly Run-off	1-20
II 1-20		1-20
II 1-21	Almus Monthly Regulated Discharge Design Flood in Turkey	1-21
II 1-22	Deriving Probable Maximum Flood at Kilickaya	1-22 -
	(Based on mean and standard deviation of precipitation)	
II 1-23	Deriving Probable Maximum Flood at Kilickaya	1-23

Figures

II 1-1	Location Map of Precipitation and Runoff Gaging Station	1-24
II 1-2	Yesilirmak Basin Gaging Station	1-25
II 1-3	Yesilirmak Basin Gaging Station Yesilirmak Water Shed Meteorological Station	1-26
II 1-4	Rating Curves	1-27
II 1-5 — 32	Hydrograph at Kale and Fatli	1-28
II 1-33	Hydrograph of Kale, Fatli and Amasya	1-32
II 1-34	Hydrograph of Kale, Fatli and Amasya Envelored Curve of Maximum Flood Flow in Turkey	1-33
II 1 - 35	Correlation between Design Flood and Catchment Area in Turkey	1-33
II 1-36	Daily Maximum Discharge Frequency of Fatli	1-34
II 1-37	Correlation between Peak Discharge and Daily Maximum Discharge	
	at Fatli	1-34
II 1-38	at Fatli Total Discharge Frequency in Storm Season of Fatli	1-35
II 1-39	Correlation between Peak Discharge and Total Discharge in Storm Season.	1-35
II 1-40	Distribution of Standardized Variate (K)	1-36
II 1-41	Unit Hydrograph of Kilickaya ;	1-36
II 1-42	Correlation between Annual Runoff of Fatli and Average Annual	
	Precipitation	1-37
II 1-43	Correlation between Total Runoff at Fatli and Precipitation in	
	Stormy Season	1-37
II 1-44	Correlation between Loss Water and Precipitation in Storm Season	1-37
II 1-45	Seasonal Variation of Several Factors of Probable Maximum Precipitation.	1-37
II 1-46	Recession Curve of Hydrograph at Fatli	1-38
II 1-47	Flood Flow Hydrograph and Precipitation in Storm	
	(March 1st to June 30th, 1952)	1-38
II 1-48	Flood Flow Hydrograph and Precipitation in Storm	
	(March 1st to June 30th, 1967)	1-38
II 1-49	Design Flood Hydrograph at Kilickaya	1-38

II 1 HYDROLOGY

II 1.1 Hydrological Study and Data

II 1-1-1 Runoff Gaging Stations and Meteorological Stations in the Yesilirmak Basin

There are 22 active gaging stations controlled by DSI and 16 by EIE, and 7 of them are located along the Kelkit and Yesilirmak Rivers downstream of Kale.

Of these stations, Fatil and Kale have records covering the longest periods since they were both built in 1938

Water surface level is generally measured by staff gage once or twice a day, except at Carsamba where it is made by a Limnigraf automatic water level recorder as well as staff gage. Kale gaging station is located at the confluence of the Yesilirmak and Kelkit, and about 60km upstream, Fatli gaging station is located along the Kelkit River. The catchment area of these gaging stations is 33,900 sq.km and 10,050 sq.km respectively. There are also rather new gaging stations on the proposed dam sites, which are controlled by DSI, such as Guvercinlik which was established on October 1, 1963 for the Kilickaya dam and Ayvacik which started on December 1, 1963 for the Ayvacik dam

Monthly total precipitation and monthly mean temperature records are available for the project area. First class meteorological stations controlled by the Turkish State Meteorological Service (DMI) in the Yesilirmak basin — Amasya, Corum, Mezifon, Samsun and Tokat — have recorded daily precipitation, daily temperature, and daily evaporation.

Locations and observation periods of each meterological and guaging stations within and near the basin area are illustrated in Fig. II 1-1, II 1-2 and II 1-3

Other stations which provide monthly total precipitation and monthly mean temperature records are shown in Table II 1-1 - II - 13.

II 1-1-2 Verification of Data

EIEI engineers in charge of hydrology have annually revised the rating curves to compensate for changes in river beds due to flood flow. It can be seen that the rating curves of Fatli and Kale gaging stations have been revised by repeated direct measurement with a current meter. In Fig. II 1-4 although there are not a great difference between the 1953, 1960 and 1965 curves, the cross section of the river bed at Kale have changed due to flood flow. Daily runoff records at Fatli and Kale are available from Apr. 1, 1938 to March 31, 1967 and Oct. 1, 1938 to March 31, 1967 respectively. Hydrographs of daily runoff of these gaging station are shown in Fig. II 1-5-II 1-33. It was found that these hydrographs are similar and also that their quantitative and time-lag relations are quite reasonable. Therefore, the data of both stations can be considered reliable for our studies.

Using these data, the amount of runoff at Kilickaya from April 1960 to March 1967 was adjusted, and it was found that the monthly runoff data at Guvercinlik which is located a few kilometers upstream from Kilickaya was too large. Adjusted figures are shown in Table II 1-17 - II 1-20.

The correlation between annual runoff and annual average rainfall within the catchament area is shown in Fig. II 1-42. According to these figures, there seems to be a good correlation between rainfall and runoff.

II 1-1-3 Evaporation Loss from Reservoir Surface

Evaporation loss for a newly constructed reservoir can be estimated by deducting the evaporanspiration of original ground surface from the evaporation of reservoir water surface.

a) Evaporation

Kilickaya Reservoir is located inland, and Ayvacik Reservoir is located along the Black Sea coast downstream of the confluence of the Kelkit and Yesilirmak Rivers. Samsun and Merzifon stations are first class Turkish State Meteorological Service (DMI) meteorological stations measuring evaporation loss and having records in the annual meteorological bulletin on areas located in and around the project area.

Samsun and Merzifon are the only stations which have reliable evaporation records. Although evaporation data from Corum, Amasya and Carsamba stations for January 1962 to December 1967 are supplied by the Meteorological Section of DSI, they cannot be used because they are about 30% incomplete for each year.

DMI data from 1950 to 1965, are shown in Table II 1-15–II 1-16 but there are no records prior to 1960 for the Merzifon station. The missing Merzifon evaporation data was estimated according to temperature data at the same site.

For estimation of evaporation loss from proposed reservoir surface, monthly maximum

evaporation data from a pan covering a period of five years (1961 - 1965) which is common to both Merzifon and Samsun stations was employed, and 70% of the evaporation value was used.

The result of these studies is shown in Table II 1-15-16.b

b) Evapotranspiration

The Blaney Criddle Formula is used for estimation of evapotranspiration. In this formula, crop coefficient "K" should be calculated on the basis of tests made of the crops or vegetation covering the proposed reservoir. In this study, a coefficient of 0.65, which is generally applied to a region covered with trees and bushes, was used.

As for the mean temperature, the average value of Erbaa and Tokat (value adjusted according to the difference of elevation between Tokat and Susehir) was used, and the monthly precipitation of Erbaa and Susehir was used.

The results of calculation are shown in Table II 1-14.

II 1.2 Flood Discharge at Kilickaya

The spillway flood discharge at Kilickaya dam site was assessed by employing the following five methods.

- 1. Historical flood values
- 2. Enveloped curve flood in Turkey
- 3. Design flood curve in Turkey
- 4. Statistical method
- 5. Physical method

II 1-2-1 Historical Flood Values

At Fatli Gaging Station on the Kelkit River, the two biggest floods ever recorded were in 1940 and 1952.

(1) 1940

	Peak discharge	April 27, 1940	802 cms (640)
	Daily maximum discharge	April 27, 1940	772 cms (620)
	Total discharge	March–June, 1940	2.506 million cu.m. (2,000)
	Annual total discharge	Oct. 1939-Sept. 1940	3,091 million cu.m. (2,470)
(2)	1952		
	Peak discharge	April 4, 1952	700 cms (560)
	Daily maximum discharge	April 4, 1952	680 cms (546)
	Total discharge	March–June 1940	1,981 million cu.m. (1,580)
	Annual total discharge	Oct. 1951-Sept. 1952	2,686 million cu.m. (2,150)

Note: The figures in parenthesis indicate values at Kilickaya obtained by multiplying the first number stated by 0.80 which is the ratio of the catchment area at Fatli to that of Kilickaya.

According to the above, the maximum peak discharge ever recorded at Kilickaya is estimated to be 640 cms.

II 1-2-2 Enveloped Curve Flood in Turkey

An enveloped curve of the maximum peak discharge was developed based on the maximum peak discharge records at many gaging stations on many rivers in Turkey from 1952 through 1967, as shown in Fig. II 1-34. From this enveloped curve, the maximum flood flow at Kilickaya which has a catchment area of about 8,202 sq.km is estimated to be about 3,000 cms.

II 1-2-3 Design Flood Curve in Turkey

The correlation between design flood discharge and catchment area in Turkey based on. design flood discharge for spillways of 18 dams which already have been constructed or are under construction is shown in Fig. II 1-35 and Table 1-21. In this figure, the solid line (----) indicates the average of all points and the dotted line (----) indicates the value near the project site. From both lines in this figure the maximum design flood flow at Kilickaya which has a catchment area of about 8,202 sq.km is estimated to be 2,200 to 3,700 c.m.s.

II 1-2-4 Statistical Method

The probability calculation was made based on flood records of Fatli Gaging Station from 1939 through 1967, employing Gumbel's Method.

The daily maximum discharge records and the frequency curve of Fatli are shown in Fig. II 1-35, and the correlation between the daily maximum discharge and peak discharge, which was obtained from data at Fatli, is shown in Fig. II 1-36.

The daily maximum discharge frequency at Fatli obtained from Fig. II 1-36 could be converted into the peak discharge at Fatli utilizing Fig. II 1-37, and the peak discharge frequency also could be converted into that at Kilickaya with the ratio of the catchment area. The flood discharge frequency calculated according to the above are as follows.

Fragmanau	Daily maximum	Peak discharge			
Frequency	discharge at Fatli (a)	Fatli	Kilickaya		
Year	cms	cms	cms		
5	630	660	530		
10	700	740	590		
20	780	820	660		
50	880	930	740		
100	950	1,000	800		
200	1,020	1,070	860		
1,000	1,200	1,310	1,050		
2,000	1,320	1,390	1,120		
5,000	1,400	1,470	1,200		
10,000	1,500	1,580	1,300		

Note: (a) = See Fig. II 1-36 (b) = (a) x 1.05 (See Fig. II 1-37) (c) = (b) x 0.80

The total discharge frequency in the stormy season (March-June) was studied as shown in Fig. II 1-38, and the correlation between the total discharge and the peak discharge mentioned above is shown in Fig. II 1-39. The peak discharge frequency at Kilickaya, swich was obtained on the basis of the total discharge frequency at Fatli employing the upper limit line in Fig. II 1-39, is as follows.

Frequency	Total discharge at Fatli(a)	Daily max. discharge at Fatli (b)	<u>Peak</u> Fatli	<u>c discharge</u> Kilickaya	
year	million cu.m	cms	cms	cms	
5	2,200	920	970	780	
10	2,500	1,020	1,070	860	
20	2,800	1,120	1,180	940	
50	3,180	1,260	1,320	1,060	
100	3,480	1,360	1,430	1,140	
200	3,730	1,440	1,510	1,210	
1,000	4,400	1,680	1,800	1,400	
2,000	4,680	1,780	1,870	1,500	
5,000	4,990	1,880	1,970	1,580	
10,000	5,350	2,000	2,100	1,700	

Note: (a) = See Fig. II 1-38 (b) = See Fig. II 1-39 (c) = (b) x 1.05 (d) = (c) x 0.80

The method for statistically estimating the probable maximum precipitation on proposed by David M. Hershfield, a meteorologist with the Hydro Service Div., U.S. Weather Bureau, was applied in Kilickaya Project.

According to this method the PMP is defined as the largest precipitation that will probably occur at the same time for a finite length of time "t", and this PMP can be estimated on the basis of mean and standard deviation by choosing an appropriate number "k", the standardized variance in the equation

$Xt = X_N + K.SN$

where Xt is the precipitation for return period t in years. This equation is applicable when a particular extreme-valued distribution is used. The terms X_N and S_N are the mean and standard deviation respectively for a series of N annual maximum;

At the point Xm, Km = K, and this calculation was based on 2,645 daily rainfall records in the U. S. A. The distribution of Km is shown in Fig. II 1-40. According to the figure, at the point 3.3 of Km (2,000 yrs. frequency), 50% of Km is included, and the maximum Km is 15. Since the probability that exceeds 10,000 years has practically no meaning, for the estimation of PMP in the Kilickaya Project, when K = 3.62 (10,000 years frequency), the PMP in March is estimated to be 267 mm.

The probable maximum peak flood flow calculated on the basis of the PMP, employing the

unit-hydrograph in Fig. II 1-41, is 4,400 c.m.s., and the flood volume is about 2,800 million cu. m. as shown in Table II 1-22.

II 1-2-5 Physical Method

The maximum prbable flood at Kilickaya would result from the maximum probable rainfall flood in combination with the maximum probable simultaneous snowmelt flood. Therefore, the factors contributing to the probable maximum rainfall of snowmelt should be studied to physically estimate the flood flow.

In the study of maximum probable flood, it is customary to maximize the record storm by determining the precipitable water during a storm and the maximum precipitable water for the time of occurence. The rainfall increments are then increased in direct ratio of the maximum to the actual precipitable water.

It also is customary to consider dewpoint (or air temperature) and wind speed as factors which contribute to the generation of a flood.

Dewpoint is the determination of precipitable water, which is the maximum amount of moisture that can be retained in a vertical column of air, and which has been found by reliable research observations to vary almost directly with surface dewpoint (or air temperature). For the estimation of precipitable water it is convenient to use the diagrams and tables prepared by the U.S. Weather Bureau.

Wind factor is the measurement of the time required to replace moisture that has been precipitated from the air with a new moisture supply. The product of precipitable water in the atmosphere and wind speed in defined as "Moisture Inflow Index". Ordinarily, in the study of depressive storms such as the monsoon, a maximum persisting 12-hour dewpoint and a maximum 24-hour average wind speed are used. Furthermore, in the study of such storms as the typhoon, a maximum persisting dewpoint for the hours during the typhoon and a maximum average wind speed for twice the hours before the typhoon are used.

Regarding wind speed, upper troposphere wind should be considered in addition to ground wind speed.

For the Kilickaya Project, the above data exists, although it would be advisable to have more.

Basic to the snowmelt runoff calculation is the determination of the melt rate factor, the runoff resulting from a given temperature factor. The temperature factor which best correlates with runoff is the weighted degree day. The melt rate factor will be calculated by analysis of records of floods which resulted primarily from snowmelt. The second way to analyze snowmelt is the estimation of the elevation covered by snow.

For the Kilickaya Project, there is not enough of the abovementioned data, however a melt rate factor of 3-5 mm/degree-day and a snow-line of about 1,500 m above M.S.L. may be applied in this project area, according to the hydrological survey of the Tigris River in Iraq and the results of investigation in the field.

The first step in flood studies is to analyze the correlation between annual precipitation in the basin and annual runoff.

Fig. II 1-42 shows the correlation between the annual runoff at Fatli and the average annual precipitation in the basin. The average annual precipitation in the basin was obtained on the basis of precipitation data at Kelkit, Susehri, Tokat. The application ratios of the these observatories, which were calculated by the Thiessen Method, are as below.

Kelkit : 0.46 Susehri : 0.54

For the years for which no data are available of Kelkit and Susehri the ratio for Tokat which is 1.00 were applied for the whole basin.

According to Fig. II 1-42, the correlation between annual runoff at Fatli and annual precipitation in the basin is good. This means that runoff is mainly caused by precipitation.

The correlation between precipitation and runoff in the stormy season (March - June) was studied with the same precedures and the result was good as shown in Fig. II 1-43. It was considered from this that the runoff in the stormy season is primarily caused by precipitation.

Base flow was separated in every year by approximating the ground water recession in July and August, extending it backward to the point of peak discharge and then connecting the resultant base flow peak with the first point on the flood hydrograph. The estimated base flow varied from about 40mm to 90mm. Therefore, the base flow which has increased in direct ratio of the maximum to the actual snowmelt perhaps can be adopted as the base flow for the probable maximum flood flow. Surface flow can be defined as total discharge minus base flow, and loss water is surface flow subtracted from precipitation. The correlation between loss water and precipitation in the stormy season is very good as shown in Fig. II 1-44, and the runoff coefficient varied from 20% to 80%.

The flood flows in 1952 and 1967 were selected as models for study of the maximum probable flood. The flood flow in 1952 was recorded as the second maximum peak discharge in the period for which flood data exist.

The procedure of deriving the probable maximum flood based on the 1952 and 1967 flood flow records is shown in Table II 1-23. In this table, the probable maximum surface daily peak flow was obtained by multiplying total runoff (10) by 18% which is the ratio of peak flow to surface flow derived from the hydrograph shown in Fig. II 1-45. The unit-hydrograph was estimated from 5 past flood hydrographs at Fatli. The recession curve of the unit-hydrograph was made on the basis of a recession curve which was prepared from 7 examples as shown in Fig. II 1-46.

Since the duration from beginning to peak of a unit-hydrograph is 6 days, a precipitation period for about 6 days should be applied in the design flood hydrograph; however, in view of safety and taking into consideration that data is inadequate and referring to the daily precipitation distribution as shown in Fig. II 1-47 and II 1-48, it was decided to apply a precipitation period for one month in March and April. The storm period should usually be used for snowmelt estimations. In this calculation for estimating the maximizing factor of base flow, it was assumed that a maximum temperature in March and April could be applied as the representation in a flood.

The temperature records at Tokat (EL. = 650m) were used for the calculation of a weighted degree day. The temperature at Tokat were converted into values at a weighted average location of about 1,900m over the snow-covered portion of the drainage area (1,500m-2,500m, about 8,000km²). A lapse rate of 0.6°C per 100 meters of increase in elevation was used to convert the temperature.

A melt factor of 4mm/degree a day for recorded storms and 5mm/degree a day for a probable maximum storm were used.

From the result of the above studies, it was estimated that the probable maximum peak and flood volume are as below.

Probable maximum peak flood:4,000 cms.Probable maximum flood volume:2,100 million cu.m.

II 1-2-6 Summary of the Results

*. · · · The results are summarized as follows.

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Method	Peak Flood Flood Volume (c. m. s.) (million cu.m
(1) Historical flood value Max. recorded flood (1940)	640 2,000
(2) Enveloped curve in Turkey	3,000 Not determined
(3) Design flood curve in Turkey	3,700
(4) Statistical method (10,000 year return period)	,, , , , , , , , , , , , , , , , , , ,
(Based on daily peak discharge)	1,300 -
(Based on total volume)	- 1,700 5,350
(Based on PMP derived from XN, SN)	4,400 2,800
(5) Physical method	4,000 2,100

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Note: Figures in parenthesis show the total discharge volume in the stormy season (March – June). . . .

Estimates (3), (4) and (5) are considered to coincide with each other.

Therefore, the flood to be used for the spillway design study, was decided to be 4,000 c.m. s at peak discharge and 2,100 million cu.m. at volume, adopting the physical method. The design flood hydrograph is shown in Fig. II 1-49.

	CARSAM	BA	STA				_ CATCHINEN	T AREA		sų kaP	recipitat:	ion	
	RIV	ER, IN THE E	ASIN OF	35	El	EVATION		•	UNIT		_5,	w	•
YEAR	Jan.	Feb.	Mer.	Apr.	Hay	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	ANNUAL
1944	87.2	49.7	126.8	47.9	63.9	33.9	18.2	14.2	32,8	75.8	194.4	64.4	869.2
1945	21.3	~ 98.7	70.5	85.3	12.5	61.7	18.7	11.2	51.9	81.4	41.1	74.5	628.8
1946	98.4	125.6	133.0	22.5	45.5	92.8	75.9	88.3	145.6	163.8	11.0	55.6	1,058.0
1947	166,5	57.5	78.4	21.9	30.4	23.5	16.1	3.3	71.2	88.5	208.0	16.4	781.7
1948	13.2	177.3	141.7	67,1	31.0	125.7	95.8	9.0	85.4	192.9	153.9	118.1	1,211.1
1949	106.5	72.1	44.5	141.3	19.7	55.8	(31.3	15.9	73.7	88.8	26.5	117.6	793.7
1950	192.0	117.8	82.7	5.0	47.6	85.3	37.6	49.5	18.0	58.8	95 O	21.0	810.3
1951	85.8	43.9	69.3	61.9	95.9	25.8	104.9	101,4	409.5	84.4	96.8	106.8	1,286.4
1952	107.7	109.3	135.6	48.9	58.4	56.6	18.4	23.8	61.1	41.5	52.0	36.1	749.4
1953	79.8	101.6	146,1	19.8	67.5	100.4	1.4	31.7	91.0	346.3	273.6	106.6	1,365.8
1954	169.7	64.3	55.7	76.9	33.5	50.8	35.8	5.8	12.0	72.6	136.4	173.2	887.7
1955	56.6	66.0	136.7	93.0	35.6	2.4	10.1	80,3	106.2	18.7	167.7	112.5	887.8
1956	72.5	132 8	120.2	46.8	53.6	37.8	17.1	0,3	49.2	51.4	107.0	119.3	808.0
1957	79.8	\$5.1	100.2	30.3	61.3	16.5	0.5	0.0	43.6	59.2	64.3	90.8	601.6
1958	169.6	53.9	128.1	44.9	17.7	40.5	69.1	19.6	129.7	73.9	77.7	131.7	956.4
1959	84.6	191.4	121.6	53.6	54.8	23.3	49.9	72.5	136.0	75.1	65.1	30.0	957.9
1960	115.8	111.3	44.5	61.7	37.1	65.4	15.2	222.0	29.1	25.2	95.9	24.7	847.5
1961	124.6	133.8	131.3	20.2	57.9	36.9	19.8	15.1	197.8	61.9	102.3	140.8	1,042.4
1962	123.1	155.6	65.5	43.0	24.3	24.5	22.3	17.8	21.2	149.0	6.9	240 8	894.0
1963	159.8	43.0	124.0	115.0	34.0	26.1	88.6	0.0	81.7	138.6	37.3	163.8	1,011.9
1964	64 0	58.5	65.3	46.5	42.5	20.7	36.1	63.4	60.6	35.6	126.8	50.6	670.6
1965	60.4	114.2	70.0	72.1	50.2	37.2	38.2	28.2	47.7	148.0	107.1	100.2	873.5
1966	97.6	18.9	101.2	51.2	109.1	18.0	106.2	70.7	86.8	11.4	37.3	267.8	978.2
1967	203.8	109.7	106.3	83.9	73.7	85.1	48.3	15.2	57.4	107.3	249.2	118.6	1,258.5
Total	2,540.3	2,262.0	2,401.2	1,360.7	1,157.7	1,146.7	976.5	1,019.2	2,101.2	2,250.1	2,533.3	2,481.9	22,230.8
Ave.	105.8	94.2	100.0	56.7	48.2	47 8	40.7	42.5	87.5	93.8	105 6	103.4	926.2
	Driest f	ive years	(1945, 19	47, 1952,	1957, 195	25	}	1	J	1	ļ	J	J
Total	439,3	379.1	450.0	232.9	205.1	179.0	89.8	101.7	288.4	306.2	492.2	268.4	3,432.1
Ave.	87.9	75.8	90.0	46.6	41.0	35.8	18.0	20.3	57.7	61.2	98,4	53.7	686.4

Table	11 1-2
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	Carsan	ba	STA				CATCHMEN	I AREA	<u> </u>	nd pro			
	RIV	ER, IN THE B	ASIN OF	35	EL	EVATION			UNIT		<u>s</u>	<u> </u>	•
YEAR	Jan.	Feb.	Mar.	Apr.	May	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	ANNUA
1944	* 6.1	* 9.6	*11.7	*15.1	+16.5	*21.4	*23.6	*21.5	*20.4	*19.5	*13.1	* 9.6	15.
1945	* 7.6	* 5.5	* 8.2	*13.3	*20.0	×19,9	*22.8	*24.3	*20.9	*15.9	*12.2	* 6.8	14.
1946	* 6.5	* 8.8	+10.3	*15.6	*19.0	*21 8	*23.2	*23.8	+21.9	*15.0	*14.9	*10.0	15.
1947	* 4.7	* 9.3	*14.7	*16.2	*19.8	*23.3	<u>*24_4</u>	*23.1	*19.8	*15.6	*13.5	*11.3	16.
1948	*11.3	* 8.3	* 7.1	*14.6	*19.7	*22.5	*24.1	*24.6	*19.9	*16.7	*10.1	* 5.3	15.
1949	* 5.1	* 3.7	* 9.2	*11.9	*20.5	*22.7	*23.6	*22.9	*19.5	*16.7	*13.7	* 9.8	14.
1950	* 3.3	* 4.7	*10.6	*19.6	*19.9	*21.5	*23.5	*22.8	*23.1	*16.0	*12.5	* 8.8	15
1951 -	* 8.4	· * 9.7	*13.9	*17.3	*20.2	+22.0	*24.4	*25.1	*21.6	*13.7	*13.3	* 5.2	16.
1952	* 7.7	* 9.0	*11.0	+15.3	*17.7	*20.5	*23.5	*25.2	*23.8	*19.4	*13 3	*11.4	16
1953	* 9.5	* 8.8	* 6.9	*15.0	*18.6	+22.4	*23.9	*24.2	*20.3	*17.0	* 8.9	* 2.7	14
1954	* 3.3	* 5.7	*11.6	*13.1	*20.3	*23.1	*25.4	*25.6	*22.0	*18.4	*14.2	*10.0	16.
1955	* 9.0	*11.7	~ *11.2	*13.6	*19.1	*22.5	*24.0	*22.7	*21.1	*19.9	*12.9	* 8.5	15
1956	* 8.0	* 6.7	* 7.0	*16.1	*16.6	*21.2	*22.4	*24.1	*18.5	*15.8	*10.6	* 6.4	14.
1957	* 4.2	, * 9.6	*10.1	*15.7	*18.7	*22.3	*25.1	*25.4	*22.9	*17.6	*12 3	* 9.3	16
1958	* 8.5	*10.9	*11.7	*15.4	*20.7	*22.5	*23.4	*24.3	*19.6	*16.1	*12,0	* 8.8	16
1959	* 9.2	* 4.7	* 9.5	*15.0	*19.0	*20.9	*24.9	*23.8	*18.7	*13.9	*12.1	*10.1	15
1960	* 7.6	* 6.2	*10.1	. *15.0	*19.7	+21.4	*24.0	*23.1	*20.0	*18.8	*14.1	*10.1	15
1961	* 5.5	* 7.3	* 9.6	*16.7	*19.6	*22.1	*23.7	*23.8	*18.7	*16.7	*13.4	*10.1	15
1962	* 7.4	* 8.4	*13.9	*15.1	*19.7	*22.2	*24,8	*25.2	*21.9	*17.6	*15.1	*10.1	16
1963	* 8.0	*10.2	· * 9.5	*14.4	, *18.4	*21.9	*24.6	*24.7	*21.8	*17.5	*12.2	* 8.7	16
1964	* 3.5	* 6.6	*11.9	±14.2	*17,8	*22.1	*23.7	*22.8	*19.7	*17.9	*11.7	* 9.5	15
1965	. 8.4	6.9	9.1	- 11.5	17.3	22.3	23.8	23.2	20.9	14.0	13.9	11.4	15
1966	10.1	11.7	11.0	14.3	16.8	20.7	24.6	24.7	19.4	19.6	16.4	11.3	16
1967	7,3	4.4	7.0	11.5	16.7	19.1	22.6	23 2	19.4	16.9	12.6	10.5	14
Total	170,2	188.4	246.8	355.6	452.3	522.3	574.0	574.1	495.8	406.3	309.0	216.0	4,510
Ave.	7.1	7.8	10.3	14.8	18.8	21.8	23.9	23.9	20.7	16.9	12.9	9.0	15
,		ive years			1957, 196		1 110 -	100 0		86.4		48.4	945
Tota 1(5)	27.7	40.0	55.9	74.7	94.0	108.1	119.5	120.8	107.1		63.0		
Ave. (5)	5.5	8.0	11.2	14.9	' 18.8	21.5	23.9	24.2	21.4	17.3	12:6	9.7	15
1							1	1	1				

* indicates value estimated in correlation with MERZIFON data

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ÇORUM				אסוד <u></u> 798		LEVATION					eq ks Precipitation			
	RIV	ER, IN THE B	ASIN OF	798	E.	LEVATION		*			_s	w		
YEAR	Jan.	Feb.	Mar.	Apr.	May	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	ANNUAL	
1944	55.1	33.8	81.1	27.5	44.9	42.4	17.3	0,7	2.0	6.3	- 45.5	- 26.2	382.	
1945	54.0	13.7	25.0	32.3	10.6	89.5	32.3	8.2	29.9	21.2	39.4	57.1	413.	
1946	10.2	43.8	71.1	65.8	51.1	39.4	64.1	8.9	0.0	54.3	17.0	58.7	484.	
1947	53.9	48 1	33.6	5.9	63.5	34.5	21.1	1.3	33.2	11.6	67.3	45.9	419.	
194B	47.4	58.9	43,2	27.2	109,9	82.1	2.2	1.0	24.8	54.7	6.9	5.3	463	
1949	31.2	27.5	33.1	50.7		41.4	7.9	0.0	33.3	9.6	14.7	38.4	373	
1950	48.4	40.9	54.3	35.2		51.1	16.0	1.7	0.8	22.1	11.6	17.2	406	
1951	12.4	13.4	81.7	27.0		39.1	26.4	3.0	5.1	32.3	41.4	34.0	413	
1952	47.7	35.4	44.6	16.6		42.4	10.3	0.2	4.7	9.3	44.5	8,4	-350	
1953	43.5	44.3	41.1	57.4		28.5	4.4	1.7	4.8	52.1	8.3	21.3	365	
1954	74.0	40.8	23.4	37.7		33.2	6.1	23.5	5.0	4.9	19.6	48.6	335	
1955	19.7	18.6	22.2	51.7		0.8	40.7	20.1	15.9	33.8	38.3	28.7	- 334	
1956	29.8	65.4	33.5	21.4		27.8	12.4	3.3	6.9	13.7	17.5	38.8	328	
1957	9.7	24.3	22.1	29.6		7.9	0.1	0.0	56 2	8.0	12.8	27.2	280	
195B	44.4	12.6	87.5	50.2		91.5	10.6	7.9	21.3	19.9	5.1	48.4	464	
1959	83.2	18.3	25.5	58.9		40.8	37.1	10.5	20.2	19.8	11.2	51.8 23.7	449	
1960	29.6	38.3	50.0	44.4	51.8	49.6	12.1	10.3	4.2	11.3	35.7		361	
1961 `	39.7	55.9	34.0	34.1	55 5	103.1	25.8	2.6	24.7	13.0	14.1	, 78.8	481	
1962	48.3	49.6	35.2	39.5	34.4	13.1	6.8	0.2	16.6	38.1 34.2	11.0	127.7	420	
1963	58.0	36.8	36.0	40.0	47.9	15,8	6.3	3.4	25.1	34.2 0.4	16.9	43.6 23.0	364	
1964	4.3	46.4	40.8	15.5	59.5	63.7	11.5	2.2	22.3		35.6	45.1	325 425	
1965	25.9	53.7	43,4	20.9	61.1	50.9	19.3	18.3	0.0	17.1	69.5			
1966 1967	88.9 24.9	6.1 21.6	37.7 69.1	64.2 74.4	45.6 100.5	19.6 110.5	8.6 0.8	8.6 0.8	12.6 18.2	0.1 17.1	15.4 64.2	58.1 37.9	365 540	
1907	24.9	21.0	07.1	/4.4	100.5	110.5	0.0	0.0	10.2	.,,,	04.2	27.5	540	
Tata 1	984.2	848.2	1,069.2	928.1	1.510.5	1.118.7	400.2	138.4	387.8	504.9	663.5	993.9	9,547	
Total Ave.	41.0	848.2 35.3	1,069.2	928.1	62.9	46.6	400.2	138.4	16.2	21.0		41.4	9,547	
Ave.	41.0	Driest f		(1954, 19		1957 196	4) ****	5.0	10.2	21,0	24.0	41,4		
Total	137.5	195.5	142.0	155.9		133.4	70.8	49.1	106.3	60.8	123.8	166.3	1,603	
Ave.	27.5	39.1	28.4	31.2	52.5	26.7	14.2	9.8	21.3	12.2	24.8	33.3	321	

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	ÇORUL		STAT		'98 FI		CATCHMENT			ng kan	Temperatur		
		ER, IN THE E	BASIN OF		<u>70 ET</u>	EVATION		<u> </u>	UNIT		<u>s</u>	w	•
YEAR	Jan.	Feb.	Mar.	Apr.	Мау	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	ANNUAI
1944	-0.9	4.0	6.4	10.6	13.4	19.1	21.3	19.1	17.0	15.0	7.3	3.6	11.3
1945	0.7	-1.3	1.9	8.7	17.1	17.0	20.4	21.9	16.2	11.6	6.6	-3.0	10.0
1946	0.0	2.5		11.1	15.6	18.9	20.8	21.0	18.3	9.4	9.2	3.1	11.
1947	-3.0	1.9	8.8	11.3	16.3	20.4	21.9	20.2	16.0	10.2	7.8	4.6	11.4
1948	4.4	1.8	0.6	9.3	15.0	18.9	21.5	22.0	16.2	10.8	2.6	-1.8	10,1
1949	-3.4	-4.5	1.5	6.8	16.3	19.1	20.1	19,2	14.9	11.2	8.3	3.9	9.
1950	-6.4	-5.2	4.1	14.9	15.4	17.5	20.1	19,6	20.0	10.5	6.1	2.7	10,
1951	1.7	2,9	8.1	12.3	15.7	18.4	21.6	22.0	18.0	8.3	6.8	-2.4	11.
1952	0.7	2.2	4.3	11.0	13.4	16.8	20.0	22.5	20.4	14.3	7.4	5.1	11.
1953	2.9	2.2	-1.3	10.0	14.4	19.2	21.2	21.7	16.2	12.3	3.2	-4.1	9.
1954	-4.4	-2.8	4.9	8.0		20.3	23.4	23.0	17.9	13.8	8.5	3.4	11.
1955	2.7	6.1	6.1	9.6		20.8	22.4	20.7	17.9	14.9	7.2	2.4	12.
1956	1.4	0.1	1.1	11.3		18.7	20.6	21.9	14.5	10.3	4.3	-0.8	9.
1957	-3.7	3.1	4.8	11.8	14.8	19.8	23.1	23.3	20.1	12.8	6.4	2,8	11.
1958	1.5	4.7	6:2	10.6	16.3	18.9	20.5	21.7	15.4	11.1	5.7	2,2	11.
1959	2.7	-3.5	4.d	10.4	14.8	17.3	21.8	20.5	13.8	8.6	5.9	3.8	10.
1960	1.8	-2.4	4.4	10.2	16.0	18.0	21.3	20.2	16.4	13.9	8.6	3.7	11.
1961 1962	-1.5 1.1	0.9	3.6	12.1	15.9	18.7	20.9	20.7	14.3	11.8	7.7	3.7	10.
1963	1.1	1.9 4.1	7.8	9.9	16.3	19.0	22.3	22.5	18.1	12.8	9.6	4.1	12.
1964	-4.1		3.4	9.7	14.1	18.4	21.2	21.6	17.8	12.8	6.8	2.4	11,
965		0.0	6.4	9.4	14.0	18.6	20.5	19.7	16.0	12.5	6.5	8.9	10.
1965	1.1 2.6	-1:0 5.6	6.6 6.6	9.8 12.1	14.7	19.5	20.8	20.8	17.7	8.8	6.5	4.2	10.
967	-1.1	-4.5	3.6	9.4	14.3	18.5	22.6	27.0	16.5	14.5	10.8	3.6	12.
····	-+	-4.3	3.9	9.4	14.9	17.0	19.6	- 20.5	16.4	12.8	5.8	3.5	9. 3,123.
otal	-1.6	18.8	109.3	250.3	363.3	448.8	509.9	513.3	406.0	285.0	165.6	54.6	260.
ve.	-0.1	0.8	4.6	10.4	15.1	18.7	21.2	21.4	16.9	11.9	6,9	2.3	10.
	Driest	five years	(1954, 195	5, 1956,	1957, 196	0							
otal	-8,1	6.5	23.7	50.1	73.4	98.2	110.0	108.6	86.4	64.3	32.9	11.7	54.8(6
ve.	-1.6	1.3	4.7	10.0	14.7	19.6	22.0	21.7	17.3	12.9	6.6	2.3	

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	ERB			TION	· ,		CATCHMEN	r AREA		sq Lu	Precipitat	ion	<u> </u>
		ER, IN THE B	ASIN OF	23	0 EI	EVATION	<u>'</u>	<u> </u>	UNIT		`S'	<u> </u>	•
YEAR	Jan.	Feb.	Har.	Apr.	Мау	Jun.	Jal.	'Aug.	Sept.	Oct.	Nov.	Dec.	ANNUA
1944	67.7	33.3	65.8	51.2	48.2	33.7	21.9	3.2	14.1	26.0	55.8	7.6	428
1945	26.6	41.0	44.8	30.6	21.6	52.2	•` 16.0	8.8	37.7	3.5	14.7	32.6	330
1946	19.2	47.4	64.3	27.2	50.8	50.7	87.1	17.8	5.0	51.5	4.1	13.1	438
1947 🕐	* 133.4	*16.1	*33.5	*13,7	*23.6	*7.8	*1,9	*19.8	*31.8	*36-2	*44.3	*29,1	391
1948	* 24.2	*106.4	*79.3	* *24.9	*31.2	*80.5	· *7 2	* 3.6	*25.5	*42.2	*40.9	*26.7	·492
1949	* 58.3	* 45.6	*36.5	* *59.5	*35-8	*30.2	*9.4	* 3.3	*29.2	*20.2	*16.0	*72 6	416
1950	* 107.3	* 56 5	*66.0	*16+5	*61.2		*8.3	. * 6.8	* 1.9	*36.3	*21.7	*15.6	407
1951	* 25.5	* 39.7	*68.4	*32.4	*57.4	+56.4	*2.4	*13.0	*32,9	*49.6	*35.8	*109.8	- 523
1952	* 42.1	* 61.4	*91.5	*46,1	*61,4	/ *19.7	*1.9	*11.1	*11.4	*26.9	*43.8	*26.6	443
1953	* 36.0	* 76.9	*59.0	*40.9	*39.9	; *19.7	*14.8	*10:3	*33.9	*47.1	*94.4	*27.2	- 500
1954	* 101.3	* 31.8	*48.3	*44.3	*49.5	*52.7	- *19.1	*24.5	*18.7	*21.0	*23.4	*88.1	522
1955	* 24.0	* 28.0	*61.2	*64.5	*29.6	* 1.9	*15.8	*11.2	*13.2	*13.0	*47.1	*30.1	339
1956	47.2	90.3	42.7	7.2	33.4	16.4	26.2	· 4.8	46.4	8.1	29.6	44.6	396
1957	· 27.7	26.1	56.2	18.7	70.8	25.5	0.2	` 0 . 0	17.5	5.9	9.6	45.4	303
1958	104.1	34.2	109.9	64.2	45.4	39.1	30.0	8.5	7.0	9,8	10.8	49.0	512
1959	23.2	76.4	48.0	675	- 48.6	37.8	2.9	' 13.2	34.3	34.0	14.7	17.9	418
1960	63.2	49.5	33.2	90.6	46 9	60.9	6.6	33.9	15.8	10.9	44.1	16.1	471
Ì961	81.6	34.2	58.2	34.2	45.5	57.0	10,9	0.3	36.7	3.2	35.6	73.7	471
1962	65.7	62.7	40.6	. 27.1	46.8	23.0	0.2	• 0.7	9.0	39.5	6.3	74.1	395
1963	104.9	23.0	- 68.4	65.6	54.6	37.1	- 8.3	12.7	30.1	72,1	26.3	32.9	536
1964	· 9.3	36.5	37.7	38.7	58.1	25.2	4.4	1.9	12.5	4.5	· 53.6	27.8	310
1965	27.8	68.3	49.5	45.3	50.1	71.6	15.3	11.2	5.5	34.2	55.2	\$3,4	517
1966	58.3	8.4	514	56.7	48.0	43.4	68.3	35.3	2.2	3.0	37.8	101.4	514
1967	94.7	. 46.3	98.6	56.3	75.1	95.1	0.0	· 0.3	27.0	31.1	91.2	58.8	674
Total		1,140.0	1,413.0	1,023.9	1,133.5		379.1	256.2	499.3	629,8	856.8	1,104.2	10,756
Ave. 🕤	57, 2		> 58.9	42.7	47.2	39.5	15.8	10.7	20.8	26.2	35.7	46.0	448
				47, 1955,					l				1
Total	221.0		233.4	166.2	203.7	112.6	38.3	· 41.7	112.7	63.1	169.3	165.0	1,674
Ave.	44.2	· 29.5	46.7	33.2	40.7	22.5	7.7	· 8.3	22.5	12.6	33.9	33.0	334
											! 1		

	El	REAA	ST/	TION			CATCHMEN	T AREA	· · · ·	69 km	Temper	ature	
	RIV	ER IN THE I	BASEN OF	.2	30	ELEVATION		•	UNIT	5110	<u>s</u>	<u> </u>	•
YEAR	Jan.	Feb.	Mar.	`Apr.	~ Hay	Jun.	Jul.	Aug.	-Sept.	Oct.	Nov.	Dec.	ANN
1944	* 3.8	* 7.9	*10.3	*14.1	*12.3	*21.3	*23.8	*21.4	*20.1	*19.1	*11.8	* 7.9	1
1945	* 5.5	* 3.1	* 6.2	*12.0	*19.7	*19.6	*22.8	*24.6	*20.6	*15.0	*10.7	* 4.7	1
1946	* 4.3	* 6.9	* 8.6	*14.7	*18.5	*21.7	*23.3	*24.0	*21.8	*13.9	*13.8	* 8.2	1
1947	* 2.3	* 7.5	*13.6	*15.3	*19.4	*23.4	*24.7	*23.2	*19.4	*14.7	*12.3	* 9.8	1
1948	* 9.8	* 6.3	* 5.0	*13.5	*19.3	*22.6	*24.3	*24.9	*19.6	*15.9	* 8.4	* 3.0	j 1
1949	+ 2.7	+ 1.1	* 7.4	+10.4	*20.2	*22.7	*23.7	*22.9	*19.1	*15.9	*12.5	* 8.0	1
1950	* 0.6	* 2.2	* 8.9	*19.2	*19.6	*21.4	*23.6	*22.8	*23.2	*15.1	*11.1	* 6.9	1
1951	* 6.4	* 7.9	*12.8	*16.6	*19.9	*21.9	*24.7	*25.4	*21.5	*12.5	*12.1	* 2.9	1
1952	* 5.6	* 7.1	* 9.3	*14.3	*17.1	*20.2	*23.6	*25.6	*24.0	*19.0	*12.1	* 9.9	
1953	* 7.7	* 6.9	* 4.8	+14.0	*18.0	*22.4	*24.1	*24.5	*20.0	*16.2	* 7.0	* 0.0	
1954	* 0.6	* 3.3	*10.1	*11.8	*20.0	*23.1	*25.8	*25.9	*22.0	*17.8	*13.0	* 8.2	
1955	* 7.1	*10.2	*'9.6	*12.4	*18.6	*22.5	*24.2	*22.7	*20.9	*19.6	*11.6	* 6.7	:
1956	* 6.0	* 4.5	* 4.9	*15.3	*15.7	*21.0	#22.4	*24.3	*17.9	*14.9	* 8.9	* 4.2	113
1957	* 1.7	* 7.9	* 8.3	*14.8	*18.1	*22.3	*25.4	*25.8	*22.9	*16.9	*10.9	* 7.5	:
1958	* 6.5	* 9.3	*10.3	*14.4	*20.4	*22.6	*23.5	*24.6	*19,2	*15.3	*10.5	* 6.9	1 3
1959	* 7.4	* 2.2	* 7.8	*14.0	*18.5	*20.7	*25.2	*24.0	*18.1	*12.7	*10.6	* 8.4	1 3
1960 1961	* 5.5 * 3.1	+ 3.9 + 5.2	* 8.4	*13.9 *15.9	*19.3	*21.3	*24.2	*23.2	*19.7	*18.3	*12.9	* 8.4	
		* 6.4			*19.2	*22.1		*24.0	*18.1	*15.9	*12.2	* 8.4	
1962	* 5.3		*12.8	*14.1	*19.3	*22.2	*25.2	*25.6	*21.8	*16.9	*14.1	* 8.4	
1963 1964	* 6.0 * 0.8	* 8.5 * 4.4	* 7.8 *10.4	*13.2 *13.0	*17.8 *17.2	*21.8 *22.1	*24.9 *23.9	*25.0 *22.8	*21.7 *19.3	*16.9	*10.3 *10.2	* 6.8	
1965	4.6	4.0	9.7	12.4	17.9	22.2	23.4	23.2	20.0	12.0	10.8	8.3	
						1			1	1			
1966	8.7	10.3	10.5	14.9	17.0	20.9	24.7	25.4	19.8	18.1	13.2	8.2	
1967	3.3	1.3	6.8	12.8	17.8	19.7	22.5	23.7	19.7	15.9	9.8	7.5	
Total	115.3	138.3	212.2	337.0	440.8	521.7	577.8	579.5	490.4	385.8	270.8	167.1	3:
Ave.	4.8	5.8	8.8	14.0	-18.4	21.7	24,1	24.1	20.4	16.1	11.3	7.0	1
	Driest	five year	(1945,	1947, 1955	1957, 1	l964)							
Total	17.4	33.1	48.1	67.5	93.0	109.9	121.0	119.1	103.1	83.5	\$55.7	36.6	1 7
Ave.	3.5	6.6	9.6	^13.5	18.6	· 22.0	· · 24.2	23.8	20.6	16.7	11.1	7.3	1

* indicates value estimated in correlation with NIKSAR data

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	MERZUFON		STAT	TION	FI	EVATION	CATCHINEN		UNIT	nd.pa	Precipita S	w	•
YEAR	Jan.	Feb.	Har.	Apr.	Нау	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	ANNUA
1944	42.5	53.8	105.9	32.1	\$55.9	25.3	32.0	0.0	10.3	16.8	45.9	15.7	436
1944	50.1	25.3	29.6	34.9	37.2	77.4	14.1	8.9	28.5	23.9	42.3	36.4	408
1945	17.3	35.9	68.5	62.6	60.3	45.1	38.8	13.5	5.9	43.1	8.7	34.8	434
1947	74.9	35.8	30.5	7.3	31.4	20.7	6.8	2.6	16.8	23.1	65.4	. 39.4	354
1947	20.8	59.1	29.0	21.1	40.5	135.3	6.1	3,4	20.2	29.7	30.0	6.6	40
	3Z.Z	32.4	22.9	60.2	33.3	51.3	3,3	0.0	24.3	7.	18.6	29.6	31
1949	34.Q	23.0	30.4	18.0	27.7	19.2	9.5	4.1	1.7	27.	13.0	13.8	22
1950 1951	23.1	32.2	45.0	28.5	41.7	29.6	3.1	1.0	10.5	30.3	48.7	26.8	32
1952	51.9	44.3	33.3	9.1	71.4	64.4	30.3	3.4	18.6	13.	42.9	- 26.6	40
1953	36.9	45.0		35.3	58.5	54.4	1.8	0.8	6.7	- 64.4	16.3	18.3	36
1954	61.2	39.2	23.8	43.4	. 62.0	21.2	9.2	4.7	1.5	10,9	17.2	39.9	33
1955	22.8	23.8	36.0	41.6	15,3	4.9	- 30.0	20.7	25.1	29.9	24.9	13.2	28
1956	19.0	78.2	27.8	5.5	49.3]	24.6	9.3	0.9	4.8	21.6	33.3	29.1	30
1957	12.6	10.7	24.2	29.7	117.3	5.4	0.7	0.0	36.9	5.9	20,0	41.6	30
1958	36.0	13.2	91.9	44.4	27.6	60.2		4.6	10.Q	24.5	1.7	30.4	35
1959	95.8	7.4	30.8	45.7	86.6	50.6	3.3	22.8	, 19.d	36.4	14.5	34.4	44
1960	37.7	23.3	28.5	56.8	70.6	38.2	7.0	16.8	12.6	. 20.3	28.2	19.d	35
1961	48.8	34.6	19.2	52.2	47.2	85.3	5.8	. 3.7	26.4	8.7	10.8	55.4	39
1962	37.3	40.4	35.4	17.7	59.8	19.1	3.7	0.0	. 17.7	37.4		92.5	37
1963	53.5	30.9	25.8	34.4	41.3	18.1	0.1	0.0	18.8	26.4		24.7	29
1964	4.1	44.2	42.3	45.9	54.0	66.9	10.9	0.0	3.3	1.8	51.7	15.7	34
1965	16.5	40.2	68.4	36.2	54.9	13.9	12.3	37.5	o.d	19.1	36.5	41.5	37
1966	59.3	5.1	33.3	51.6	28.8	. 39.3	. 2.5	42.1	7.7	0.0	15.1	66,1	35
1967	24.6	16.4	51.2	65.8	58.8	42.7	0.2	9,2	13.0	10.7	39.4	29.8	36
Total	912.9	795.5	959.1	880.0	1,231.4	1,013.1	252.4	200.7	340.3	533.5		781.3	8,56
Ave.	38.0	33.1	40.0	36.7	51.3	42.2	10.5	8.4	14.2	22.2	27.5	32.6	35
	Driest #		(1950, 1		1957, 19								
Total	141.9	167.7	144.2	129.2	250.9	72.2	49.6	25.7	87.3	111.3		122.4	1,41
Ave.	28.4	33.5	28.8	25.8	50.2	14.4	9.9	5.1	17.5	22.3	23.3	24.5	283

Table	11	3.9	

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	Rľ	VER, IN THE E	ASIN OF		563 EL	EVATION	`	M	UNIT		s	w	<u> </u>
YEAR	Jan.	Feb.	Mar.	Apr.	May	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	ANNUAL
1944	0.5	4.7	7.2	11.2	12.8	18.7	21.3	18.8	17.4	16.4	8.8	4.7	11.9
1945	2.3	-0.2	3.0	9.0	17.0	16.9	20.3	22.1	18.0	12.1	7.7	1.4	10.8
1946	1.0	3.7	5.5	11.8	15.8	19.1	20.8	21.5	19.2	11.0	10.9	5.1	12.1
1947	-1.1	4.3	10.7	12.5	16.7	20.9	22.2	20.7	16.7	11.8	9.3	.6.7	12.6
1948	6.7	3,1	1.7	10.6	16.6	20.0	21.8	22.4	16.9	13.1	5.3	-0.4	11.5
1949	-0.7	-2.3	4.2	7.4	17.6	20.2	21.2	20.4	16.4	13.1	9.5	4.9	11.0
1950	-2.8	-1.2	5.8	16.5	16.9	18.8	21.1	, 20.3	20.7	, 12.2	8.1	3.7	11.7
1951	3.2	4.8	9.8	13.8	17.2	19.3	22.2	23.0	18.9	9.5	.9.0	-0.5	12.5
1952	2.4	3.9	6.3	11.4	14.3	17.6	21.1	23.2	21.5	. 16.3	9.0	6.8	12.8
1953	4.5	3.7	1.5	11.1	15.3	19.8	21.6	22.0	17.3	13.4	3.8	-3.5	10.9
1954	-2.8	0.0	7.0	8.8	17.3	20,6	23.4	23.5	19.4	15.1	10.1	5.1	12.3
1955	3.9	7.1	6.5	9.4	15.9	19.9	21.7	20.2	18.3	16.9	8.6	3.5	12.7
1956	2.8	1.2	1.6	12.4	12.9	18.4	19.8	21.8	15.2	12.0	5.8	0.9	10.4
1957	-1.7	4.7	5.2	11.9	15.4	19.7	23.0	23.4	20.4	14.1	. 7.9	4.3	12.4
1958	3.3	6.2	7.2	11.5	17.8	20.0	21.0	ZŻ.1	16.5	12.4	7.5	3.7	12.4
1959	4.2	-1.2	4.6	11.1	15.8	18.1	22.8	21.5	15.4	9.7	7.6	5.3	11.2
1960	2.3	0.6	5.3	11.0	16.6	18.7	21.7	20.7	17.0	15.6	10.0	5.3	12.1
1961	-0.2	1.9	4.7	13.1	16.5	19.5	21,4	21.5	15.4	13.1	9.2	5.3	11.8 -
1962	2.0	3.2	9.8	11.2	16.6	19,6	22.7	23.2	19.2	14.1	11.2	5.3	13.2 -
1963	2.8	5.4	4.6	10.3	15.1	19.2	22.4	22.5	, 19.1	14.1	7.8	3.6	12.2
1964	-2.6	1.1	7.4	10.1	14.4	19.5	21.4	20.3	16.6	14.5	7.1	4.7	11.2
1965	2.4	0.4	7.2	9.8	15.1	19.5	20.6	_ 20.4	17.9	. 9.4	7.7	5.0	11.3
1966	3.8	6.5	7.2	13.6	14.6	18.0	22.4	22.0	16.4	16.5	11.4	4.4	13.1
1967	-0.4	-2.2	3.7	10.0	14.9	16.7	- 19.3	20.4	16.4-	13.9	6.8	4.0	10.3 (3,411.2)
Total	35.8	59.4	137.7	269.5	379.1	458.7	517.2	517.9	426.2	320.3	200.1	89.3	284.4
Ave.	1.5	2.5	5.7	11.2	15.8	19.1	21.5	21.6	17.8	13.3	8.3	3.7	11.9
	Driest .	five years	(1950, 19		1957, 196)				-		·	
Total	5.0	17.2	23.7	60,5	76.2	96.0	108.0	108.2	93.7	69.3	38.2	16.0	59.3(712:
Ave.	1.0	3.4	4.7	12,1	15.2	19.2	21.6	21.6	18.7	13.9	7.6	3.2	11.9
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r	NIKSAR		STAT		370 81		CATCHMENT			sq ha ,	Precipita	-	
<u> </u>		ER, IN THE B	ASIN OF		350 EL	EVATION		<u> </u>	יזאט		<u>s</u>		•
YEAR	Jan. '	Feb.	Mar.	Apr.	Нау	Jun.	Jal.	Aug_	Sept.	Oct.	Nov.	Dec.	ANNUA
1944	50.4	43.9	47.4	8.9	26.7	20.5	8.6	0.4	9.9	18.0	62.1	17.4	314
1945	58.7	73.4	103.3	68.5	39.9	84.2	2.1	6.6	25.1	14.7	5.9	58.6	541
1945	42.5	72.8	90.9	46.6	100.2	61.2	\$2.4	32.9	35 2	52.8	10.6	23.0	621
1947	- 145.5	15.8	35.0	13.1	24.1	6.6	0.0	19.9	33.1	38.0	47.0	30.1	408
1948 🕔	24.7	115.6	85.7	25.5	32.5	87.0	5.9	1.9	26.2	44.6	43.2	27.5	520
1949	62.4	48.4	38.3	63.8	37.5	31.4	8.4	1.6	30.3	20.3	15.6	78.3	436
1950	116.7	60.4	71.0	16.2	65.6	8.4	7.1	5.5	0.0	38.1	22.0	15.2	426
1951	26.2	41.9	73.6	33.8	61.4	60.3	0.6	12.3	34.3	52.8	37.5	119.4	554
1952	44.5	65.9	99.2	49.0	65.6	19.8	0.0	10.2	10.6	27.7	46.4	27.4	466
1953	37.8	83.0	63.2	43.2	42.1	19.7	14.3	9.4	35.4	50.0	102.4	28.0	528
1954	110.0	33.1	51.4	47.0	52.7	56.2	19.1	22.6	18.6	21.2	23,8	95.4	551
1955	24.5	28.9	65.6	69.3	30.7	0.0	15.4	10.3	12.6	12.3	50.1	31,3	351
1956	57.5	107.7	45.7	13.6	50.4	12.7	13.0	19.3	33.8	5.9	56.5	76.1	492
1957	43.0	40.3	61.8	23.6	72.7	20.9	0.0	0.0	27.4	9.5	7.0	35.8	342
1958	104.8	32.7	118.5	97.6	52 7	38.1	37.9	1.9	13.0	5.7	16.7	60.8	580
1959	55 7	134.4	47.6	59.8	65.7	49.5	0.0	47.6	23.0	51.0	38.2	22.0	594
1960	49.5	75.1	61.5	111.4	52.6	86.7	13.0	19.4	23.0	15.5	59.6	22.2	589
1961	83.7	34.3	102.2	35.6	26.6	74.8	3.4	0.0	44.9	10:5	64.1	75.7	\$55
1962	63.1	78.6	28.9	29.8	55.9	16.9	0.0	0.0	8.2	41.7	12.9	94.8	430
1963	98.1	. 26.5	83.7	72.8	65.6	24.9	37.8	0.0	42.4	28.7	21.7	34.2	j 536
1964	22.7	31.1	56.9	40.8	74.3	17.2	9.6	0.3	27.7	10.1	38.6	39.2	368
1965	15.4	60,2	39.1	66.6	69.5	35.8	1.3	12.5	8.7	36.6	42.9	52.5	441
1966	· 56.9	57.0	40.5	0.0	19.0	20.0	31.0	32.1	23.0	0.0	19.5	66.8	365
1967	63.8	. 37.6	38.5	33.2	0.0	8.0	0.0	1.3	28.2	56.2	103.7	68.1	438
Total	1,458.1	1,398.6	1,549.5	1,069.7	1,184.0	860.8	280.9	268.0	574.6	_661.9	948.0	1,199.8	,1453
Ave.	60.8	58.3	64.6	44.6	49.3	35.9	11.7	11.2	23.9	27,6	39.5	50.0	477
		ive years	-		1964, 196								ł
Total	197.5	201.2	272.2	142.6	223.4	78.6	64.6	43.1	100.1	49.9	177.3	190.5	1,741
Ave.	39.5	40.2	54.4	28.5	44.7	15.7	12.9	8.6	20.0	10.0	35.5	´ 38.1	348

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	PIN	ER. IN THE B	ASIN OF		350 E	LEVATION		-	UNIT	tani	_s		•
YEAR	Jan.	Feb.	Mar.	Apr.	Hay	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	ANNUA
1944	* 8.0	*11.9	*14.3	*18.0	*16.2	*25.0	*27.4	*25.1 *	*23.8	*22.8	*15.7	*11.9	18.
1945	* 9.6	* 7.3	*10.3	*15.9	*23.4	+23.3	*26.4	*28.2	*24.3	*18.8	*14.7	* 8.8	17.
1946	* 8.4	*11.0	*12.6	*18.5	*22.2	+25.3	*26 .9	*27.6	*25.4	*17.8	*17.7	*12.2	18.
1947	* 6.5	*11.6	+17.5	+19 1	*23.1	+27.0	+28.3	*26.8	*23.1	+18.5	*16.2	*13.8	19.
1948	*13.8	*10.4	+ 9.1	*17.4 1	*23.0	+26.2	*27.9	*28.5	*23.3	*19.7	· +12.4	* 7.2	18.
1949	* 6.9	* 5.3	*11.5	+14.4	*23.9	*26.3	*27.3	*26.5	*22.8	*19.7	*16.4	*12.0	17.
1950	*49	* 6.4	+12.9	*22.9	*23.3	*25.1	*27.2	*26.4	*26.8 -	*18.9	*15.1	*11.0	18.
1951	*10.5	*11.9	+16.7	+20.4	*23.6	*25.5	*28.3	*28.9	*25.2	*16.4	* 16.0	* 7.1	19.
1952	* 9.7	*11.2	+13.3	*18.2	*20.9	+23.9	*27.2	*29,1	*27.6	+22.7	+16.0	*13.9	19.
1953	*11.8	*11.0	* 8.9	*17.9	*21.8	*26.0	+27.7	*28.1	*23.7	*20.0	*11.1	* 4.3	17.
1954	* 4.9	* 7.5	*14.1	*15.7	*23.7	*26.7	*29.3	*29.4	*25.6	*21.6	*16.9	*12.2	19.
1955	*11.2	*14.2	*13.6	*16.3	*22.3	*26.1	*27.8	*26.3	*24.6	*23.3	*15.5	*10.8	19.
1956	*10.1	* 8.6	* 9.0	*19.1	*19.5	*24.7	*26.0	*27.9	*21.7	*18.7	+12.9	* 8.4	17.
1957	* 5.9	*11.9	*12.3	*18.6	*21.8	*25.9	+28.9	*29.3	*26.5	*20.7	*14,9	*11.6	19.
1958	*10.6	*13.3	*14.3	*18.3	*24.1	*26.2	*27.1	*28.2	*22.9	*19.1	*14.5	*11.0	19.
1959	+11.5	* 6.4	+21.6	*17.9	*22.2	+24.4	*28.7	*27.6	*21.8	*16.6	*14.6	*12.4	18.
1960	* 9.6	* 8.1	*12.4	*17.8	*23.0	*25.0	+27.8	*26.8	*23.4	*22.0	*16.8	*12.4	18
1961	* 7.3 -	* 9.3	±11.9	*19.7	*22.9	±25.7	+27.5	*27.6	*21.8	*19.7	*16.1	*12.4	18.
1962	* 9.4	*10.5	*16.7	*18.0*	*23.0	*25.8	*28.7	*29.1	*25.4	*20.7	*18.0	*12.4	19.
1963	'*10.1	*12.5	*21.6	*17.1	*21.6	*25.4	*28.5	*28.5	*25.3	+20.7	+14.3 +14.2	*10.9	19.
1964	* 5,1	* 8.5	*14.4	+16.9	*21.0	+25.7	*27.5	+26.4	*23.0	*21.1		8.8	15
1965	4.6	8.Z	- 9.7	16.3	16.4	19.8	22.9	25.1	23.7	13.4	11.7	12.2	17
1966	12.7	14.3	11.0	15.7	16.6	20.4	24.4	28.9	23.5	17.4	13.9		
1967	2.8	• 1.7	10.9	16.7	21.6	23.4	26.1	23.6	19.5	16.4	9.7	7.7	15.
Total	-205.9	233.0	307.7	426.8	521.1	598.8	655.8	659.9	574.7	466.7	355.3	257.3	439.
Ave.	8.6	9.7	12.8	17.8	21.7	24.9	27.3	27.5	23.9	19.4	14.8	10.7	18
		five year		955, 1957	1964 1								
Total	42.9	60.8	65.6	.85.5	97.9	123.1	136.0	136.0	121,4	105.3	74.2	58.4	92
Ave.	8.6	12.2	13.1	17.1	19.6	24.6	27.2	27.2	24.3	21.1	14.8	11.7	18
ave.	1 3.0			1		1 -4.0		I	-···•	1		1	1

* indicates value estimated in correlation with HERZIFON data

·	TOK			TION			_ CATCHMEN			69 kmY	recipitati		
		VER. IN THE	BASIN OF	623	E	LEVATION	· <u>· · · · · · · · · · · · · · · · · · </u>	¥	UNIT		s•	¥	•
YEAR	Jan.	Feb.	, Har.	Apr.	May.	Jun.	Jul.	. Aug.	Sept.	Oçt.	Nov.	Dec.	ANN
1944	76.9			36.1	50.1	46.8	12.0	2.8	- 14.7	- 32.1	. 58.1	15,1	45
1945	53.0	47.7		70.2		49.6	3.5	. 4.0	25.7	26.1	6.9	41.8	. 44
1946	28.2	44.8		42.8	75.6	78.2	6.4	14.3	33.5	60.9	15.2	19.2	49
1947	74.5	18.0	47.2	6.9	47.5	13.9	5.3	. 0.0	35.1	25.4	85.0	33.2	39
1948	26.4	76.7		27.0	78.2	62.9	• 1.2	3.8	12.9	35.2	38.6	24.0	44
1949	57.1	41.4		118,8	54.9	67.3	. 19.4	1.8	29.4	27.4	19.8	53.8	61
1950	123.6	38.7	73.2	22.0	80.8	- 55.3	× 2.0	1.7	0.0	, 30.3	11.5		45
1951	34.2	24.5	42.1	48.7	96.7	38.7	, S.5	67.2	31.6	63.1	29.9	55.0	53
1952	65.9	66,3	87.0	43.6	80.0	20.8	. 4.9	1.7	16.2	13.7	43.4	17.4	46
1953	44.9	68.7	43.5	38.1	62.3	47.1	. 6.3	- 6.3	27.2	26.5	58.9	26.6	45
1954	79.6	31.8	39.0	41.7	51.8	17.4	- 0.0	7.6	8.6	10.2	18.2	66.8	37
1955	25.3	46.4	38.7	79.8	30.8	0.3	18.8	5.3	12.2	24.4	38.1	37.1	35
1956	32.3	53.9	33.7	8.4	61.5	21.9	3.9	0.8	25.4	· 5.0	46.4	51.6	34
1957	15.0	39.2	42.4	19.3	84.3	10.0	0.9	0.0	, 18.7	5.4	25.2	28.3	28
1958	92.2	28.3	80.6	50.0	. 62.4	95.7	32.4	11.0	2.0	- 4.0	· 16.0	70,7	54
1959	46.2	71.0	27, 2	50.0	, 87.0	48.5	3.9	41.5	11.5	21.5	28.5	26.5	46
1960	49.6	47.0	36 8	116 0	38.5	39.3	4.1	26.5	22.5	12.9	53.8	21.3	46
1961	58.6	6.0	36.3	13.1	20.0	75.3	8.1	00	19.8	4.9	35.4	90.6	36
1962	44.3	67, 1	19.2	40.6	41.2	8.7	1.1	· 0.0	14.5	40.8	. 10.0	92.1	379
1963	100.9	41.2	50.7	53.4	50.3	46.0	7.5	- 1.0	33.7	51.6	23.3	57.2	51
1964	12.5	36.0	50.6	46.2	77.1	37.5	2.5	0.3	10.0	7.4	42.9	57.0	38
1965	9.8	23.1	27.9	42.1	48.6	19.4	5.6	3.6	10.7	25.8	-59.9	77.9	35
1966	72.3	14.1	40.4	58.1	35.5	. 26.8	33.5	4.4	19.4	. 0.0	39.5	103.0	44
1967	56.2	22.9	48.3	32.7	63.5	38.4	· 0.0	0.1	40.1	. 36.7	80.2	44.2	46:
Total	1,279.5	1,001.2	1,258.9	1,105.6	1,416.6	965.8	188.8	205.7	475.4	591.3	884.7	1,125.2	10,4
Ave.	53.3	41.7	52.5	46 .1	59.0	40.2	7.9	8.6	19.8	. 24.6	36.9	46.9	43
1		five/years		56, 1957.	1961, 19								1
Total	141.0	168.6	179.0	162.7	245.2	126.9	37.3	9.7	86.8	65,5	- 205.0	285.5	1,7
Ave.	28.2	33.7	35.8	32.5	49.0	25.4	7.5	1.9	17.4	13.1	41.0	57.1	34

· · · · ·		OKAT	BASIN OF		623 EI	EVATION	_ CATCHMEN		UNIT	eq km	Temperatu	• •	
	1	í -			· · · · ·				F		<u> </u>	<u> </u>	ANNUAL
YEAR	Jan.	Feb.	Mar.	Apr.	Kay	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	
1944	*'1.8	* 5.9	* 8.3	*12.2	*13.8	*19.5	/ *22.1	*19.6	+18.3	*17.3	* 9.9	* 5.9	12.9.15
1945	. * 3.5	* 1.1	* 4.2	*10.1	*17.9	*17.8	*21.1	*22.8	*18.9	*13.1	* 8.8	* 2.7	11.8:14
1946	* 2.3	* 4.9	* 6.7	*12.8	*16.7	*19.9	*21.6	*22.3	*20.0	*12.0	*11.9	* 6.3	13.1 11
1947	* 0.2	* 5.5	*11.7	*13.5	*17.6	*21.7	*22.9	*21.5	*17.6	*12.8	*10.4	* 7.8	13.6 10
1948	* 7.8	* 4.3	* 3.0	*11.6	*17.5	- *20.8	+22.6	*23.1	*17.8	*14.1	* 6.5	* 1.0	12.5 1
1949	+ 0.6	+-0.9	* 5.4	* 8.5	*18.5	*21.0	*22.0	*21.2	*17.3	*14.1	*10.6		12.0 14
1950	4.5	4.9	7.4	,17.4	17.2	18.7	20.7	, 20.1	20.9	12 1	8.8		13.1 19
1951	4.9	5.8	11.0	13.4	16.4	19.4	22.5	23.2	18.3	10.2	9.5		12.8 15
1952	2.5	4.2	6.1	11.7	15.7	18.5	21.6	22.7	21.1	16.0	9.0		13.1 1
1953	6.2	4.7	2.0	11.9	15 8	20.7	21.7	22.5	16.7	13.5	3.8		11.3 1
1954	-1.0	2.2	8.4	10.2	16.9	-21.8	25.0	24.9	20.1	15.1	9.0		13.1 1
1955	4.7	7.2	8.1	8.8	12.2	22.3	22.8	21.3	19.3	15.1	9.0		13.1 1
1956	4.3	1.9	4.4	14.1	14.1	20.4	20.6	22.6	16.1	13.0	7.0		11.7 14
1957	*-0.4	* 5.9	* 6.4	*12.9	*16.3	*20.5	*23.7	*24.1	*21.2	*15.0	* 9.0		13.3 16
1958	* 4.5	* 7.3	* 8.3	*12.5	*18.7	*20.8	*21.8	.*22.8	*17.4	*13.4	* 8.6		13.4 16
1959	* 5.4	* 0.1	* 5.8	*12.1	*16.7	*18.9	*23.5	*22.3	*16.3	*10.8	* 8.7		12.3 14
1960	+ 3.5	* 1.9	* 6.5	*12.0	*17.5	*19.5	, *22.5	*21.5	. *17.9	_*16.5	*11.0		13.1 1
1961	0.1	3.2	5.2	13.9	18.1	20.3	21.2	21.5	,15.2	13.1	8.1		22.2 14
1962	2.6	3.9	11.1	11.7	17.0	_20.4	23.0	22.3	_ .19.1	14.1	10.6		13.5 16
1963	-3.0	5.9	5.3	11.2	15.5	· . 19.2	16.0	21.6	18.3	14.1	7.6		11.3 11
1964	-4.1	0.9	7.7	10.9	15.1	- 19.7	21.2	20.7	17.2	13.4	8.0		11.4 1
1965	3.2	2.1	8,5	11.4	15.8	20.3	21.3	, 22.1	: 18.5	10.2	- 8.6		12.3 14
1966 1967	6.5	7.9	8.9	14.0	15.8	19.6	22.6	23.4	17.8	16.1	, 11.8	6.1	14.2 17
1907	0.2	-1.4	4.6	11.2	16.2	17.9	. 19.9	20.9	17.6	.14.4	7.3	2.8	11.2 13
Tota l	60.8	-89.4	165.0	290.0	393.0	479.6	- 523.9	531.0	. 438.9	329.5	213.5	114.7	3,629.
Ave.	2.5	3.7	6.9	12.1	16.4	20.0	21.8	- 22.1	18.3	13.7	8.9	. 4.8	12.
	Driest f	ive years	(1955, 19	6, 1957,	1961, 1965	}	*		-				
Total	11.9	20.3	32.6	61.1	76.5	103.8	109.6	`i11.6`	90.3	66.4	41.7	26.4	62.7(75
Ave.	2.4	4.1	6.5	12.2	15.3	20.8	21.9	22.3	` 18.1	` 13.3	.8.3	5.3	- 12.

* indicates value estimated in correlation with MERZIFON data

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1	AMASYA		STA'	110N	400 E1		CATCHMEN			sq baP	recipitati		
	RIV	ER. IN THE B	ASIN OF	<u> </u>	400EL	EVATION		······ •,	UNIT		_5	<u> </u>	•
YEAR	Jan.	Feb.	Mar.	Apr.	Hay	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	ANNUA
1944	63.4	42.5	86.1	41.1	32.3	13.3	0.0	0.0	3.7	29.3	38.1	11.0	360
1945	59.4	25.5	38.8	22,9	29.2	30.0	16,2	12.3	38.1	12.8	12.7	51.7	34
1946	31.0	70.5	49.6	30.4	56.0	23.9	60.7	9.3	2.0	48.5	10.6	21.5	41
1947	99.3	30.1	36.9	2,1	36_1	15.5	0.0	1.5	19.0	27. 2	92.3	22.8	38
1948	25.8	66.3	53.0	30.5	60.4	127.8	1.5	2.3	17.4	36.6	18,8	1.9	- 44
1949	35.0	27,3	25,2	36,8	36.5	34.8	3.7	0.0	25.1	6.5	32.7	44.8	· 30
1950	76.0	51:4	53.9	15.1	43.5	12.0	8.3	10.6	0.0	23.9	18.9	8.1	
1951	30.6	34.3	63.2	26 6	85.0	22.5	4.3	1.9	25.7	41,2	64.2	46.4	
1952	70.5	64.8	64.8	32.4	65.2	40.4	8.1	0.0	15.5	9.5	71.5	29.3	
1953	44.5	52.7		40.6	69.5	26.6	3.5	5.4	21.2	62.9		17.0	43
1954	121.6	41.3		57.6		16.0	0.0	7.8	2.1	11.4	12.5	68.7	41
1955	33.4	31.3		38.5		- 3,2	8.1	13.0	12.1	7.2	43.6	16.3	
1956	38.2	100.3	53.7	7.9		26.3	10.7	0.1	13.4	6.0		39.9	34
1957	14.1	39.0		24.2		8.7	0.0	0.2	30.4	8.0		50.1	340
1958	84.6	25.7		46.8		67.2	4.8	1.6	9.4	16.6	2.2	47.7	47
1959	97.6	32.5		42.8		54-9	10.8	28.2	18.1	44.3	17.7	43.1	47
1960	48.4	51.3	33.0	78.3		31.5	4.2	4.5	16.3	10.4	36.6	26.9	39
1961 1962	68.7	41.4	50.1	12.8		48.8	15.9	8.5	23.9	8.1	11.1	71.0	
	52.5	59.4	54.2	29.6	28.1	16.7	2.0	0.0	24.3	33.8		78.4	
1963	93.8	38.6	67.0	65.7	50.8	20.3	0.0	0.0	28.4	54.2		48.1	499
1964	9.5	58.6	38.4	49.7	76.9	33.0	16.5	0.0	7.5	2.7		29.9	38:
1965	25.9	73.7	55.1	39.0		11.2	9.0	25.3	3,8	31.7		92.7	48
1966	114.0	11.9		80.2	43.2	10.6	15.9	25.6	1.7	1.2		107.7	490
1967	60.2	31.6	103.6	92.4	55.2	68.5	0.0	7.5	25.7	16.5	82.3	56.6	60(
Total	1,398.0	1,102.0	1,334.7	944.0	1,187.1	763.7	204.2	165.6	384.8	\$50.5	823.8	1,031.6	9,89
Ave.	58.2	45.9	55.6	39.3	49.5	31.8	8.5	6.9	16.0	22.9	34.3	43.0	
		ive years			1955, 195							4510	1
Total	217.9	174.5		137.5	239.1	88.7	36.3	36.1	105.7	58.4	120.1	171.0	1,580
Ave	43.6	34.9	40.2	27.5	47.8	17.7	7.3	7.2	21.1	11.7	24.0	34.2	31

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F	EVAPORATIO	N LOSSES	STA	TION			_ CATCHMEN	T AREA		69 km			
		ER. IN THE	BASIN OF			LEVATION		M	UNIT	tan	_ s	W	•
YEAR	Jan.	Feb.	Mar.	Apr.	Мау	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	ANNUAL.
	Station			•									-
Max. Evap 1961-1965	• 30.2	44.8	119.8	165.9	232.7	223.5	356.2	319.9	193.8	132.9	75.3	41.0	- 1,936.0-
- 707	21.1	31,4	83.9	116.1	162.9	156.5	249.2	223.9	136.7	93.0	52.7	28.7	1,356.2
Evapotrat piration		37.5	48.0	50.0	59.5	35.0	8.9	3.3	16.9	21.0	30.5	38.2	386.6-
Evaporat Losses	on _	-	35.9	66.1	103.4	121.5	240.4	220.6	119.8	62,0	22.2	-	991.9
Samsun s	tation_		`										
Max. Eva [1961-196]	°*65.4	63.0	80.6	73.7	64.2	89.4	117.8	107.6	89.4	106.9	99.6	90.2	1,047.8 -
- 70%	45.8	44.1	56.4	51.6	44.9	62.6	82.5	75.3	62.6	74.8	69.7	63.1	733.4 -
Evapotran		44.5	54.0	40.0	44.0	37.5	15.5	10.5	20.5	26.0	35.5	43.0	415.9 -
Evaporati Losses	lon -	-	-	-	-	35.1	67.0	64.8	52.1	48.8	34.2	20.1	322.1 -
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able II 1	SAL	SUN	STA	TION	• •	· · · · ·	CATCHMED	IT AREA		sq in	Evaporat	ion	
	Ri	VER, IN THE	BASIN OF		F	LEVATION		•	- UNIT		_s`	w	•
YEAR	Jan.	Feb.	Mar.	Apr.	May	Jun.	Jul.	Aug.	Sept.	Oct,	Nov.	Dec.	ANNUAL
1950	52.3	83.5	48.3	68.2	46.2	- 91.5_	122.0	70.7	87.3	86.4	81.7	131.8	969.9
1951	85.6	43.5	56.1	44.4	56.8	74.5	87.5	77.4	70.8	34.9	53.3	73.0	757.8
1952	82.6	76.4	87.7	48.7	38.9	68.8	71.7	89.8	78.2	71.6	85.3	75.8	875.5
1953	66.8	63.3	50.7	35.6	37.0	58.2	98.0	91.6	76.4	41.0	27.3	51.3	697.2
1954	26.2	19.6	44.6	30.2	51.3	55.6	91.7	90.8	71.5	60.8	60.9	\$5.5	658.7
1955	67.2	77.0	35.0	40.9	48.1	66.8	87.2	75.0	69.3	58.8	67.3	68.6	761.2
1956	72.8	40,6	46.1	73.7	53.5	61.5	100.0	98.2	89.0	65.9	70.1	· 63.4	834.8
1957	51.0	50.1	38.6	57:2	36.2	70.6	110.7	105.0	71.1	51.4.	39.9	67.3	749.1
1958	60.1	69.6	36.4	41,6	52.6	84.5	104.0	98.5	69.0	60.1	41.9	75.1	793.4
1959	76.1	28.3	36.6	65.9	35.8	57.0	96.7	102.7	70.0	45.4	45.8	66.2	726.5
1960	79.8	60.6	32.3	19.5	46.1	61.8	92.5	95.7	61.6	106.9	60.0	81.4	798.2
1961	60.0	34.5	55.0	48.2	51.2	52.7	71.7	78.9	53.2	38.8	64.8	51.6	660.6
1962	51.5	40.9	80.6	39.9	64.2	70.8	84.6	95.1	75.5	49.3	57.3	58.8	768.5
1963	43.9	63.0	53.1	19.6	31.1	76.6	108.2	107.6	75.4	46.2	77.3	82.3	784.3
1964	43.5	58.2	34.7	64.4	38.9	91.4	117.8	104.7	89.4	81.6	56.3	66.9	847.8
1965	65.4	44.5	34.6	47.8	47.7	89.4	102.6	101.2	86.1	62.7	99.6	90.2	871.8
Total	984.8	853.6	770.4	745.8	735.6	1,131.7	1,546.9	1,482.9	1,193.8	961.8	988.8	1,159.2	12,555.3
Average	61.6	53.4	48.2	46.6	46.0	70.7	96,.7	92.7	94.6	60.1	61.8	72.5	784.7
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		ER. IN THE			E	LEVATION		· •	UNIT	mm	_s _•	w	•.
YEAR	Ĵan.	Feb.	Mar.	Apr.	May	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	ANNUAL
1950	_	•	46.3	176.8	181.7	204.9	232.9	223.2	228.1	124.4	74.4	20.7	1,513.
1951	14.6	34.2	95.1	143.9	185.4	211.0	246.3	256.1	206.1	91.5	85.4	-	1,569.
1952	4.9	23.2	52.4	114.6	150.0	190.2	232.9	258.5	237.8	174.4	85.4	58.5	1,582.
1953	30.5	20.7	-	111.0	162.2	217.1	239.0	243.9	186.6	139.0	22.0	- 1	1,372.
1954	-		61.0	82.9	186.6	226.8	261.0	262.2	212.2	159.8	98.8	37.8	1,589.
1955	23.2	62.2	54.9	90.2	169.5	218.3	240.2	222.0	198.8	181.7	80.5	18.3	1,559.
1956	9,8	-	- 1	126.8	132.9	200.0	217.1	241.5	161.0	122.0	46.3	- 1	1,257.
1957	-	32.9	39.0	120.7	163.4	215.9	256.1	261.0	224.4	147.6	72.0	28.1	1,561.
1958	15.9	51.2	63.4	115.9	192.7	219.5	231.7	245.1	176.8	126.8	67.1	- 20.7.	1,526.
1959	26.8	-	31.7	111.0	168.3	196.3	253.7	237.8	163.4	93.9	68.3	40.2	1,391.
1960	3.7	-	40.2	109.8	178.1	203.7	240.2	228.1	182.9	165.9	97.6	40.2	1.490
1961	16.5	27.9	85.5	165.9	232.7	196.8	356.2	319.9	184.6	114.5	75.3	28.9	1,804
1962	26.6	41.5	119.8	151.0	163.9	223.5	327.9	311.2	193.8	100.4	43.7	31.1	1,734
1963	28.6	44.8	71.4	90.3	99.3	170.9	238.9	284.4	153.0	87.1	39.0	41.0	1,348
1964	27.2	25.7	67.3	110.5	106.7	142.1	239.7	231.0	138.9	132.9	46.0	34.4	1,302
1965	30.2	28.2	51.4	96.9	103.3	153.6	178.1	191.7	138.3	64.5	50.2	28.2	1,114
Totai	258.5	392.5	879.4	1,918.2	2,576.7	3,190,6	3,991.9	4,017.6	2,986.7	2.026.4	1,052,0	428.1	23,718
Average	16.2	24.5	55.0	119.9	161.0	199.4	249.5	251.1	186.7	126.7	65.8	26.8	1,482
Average	10.2	14.5	55.0		10000					1.000	0210		
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Kelk	it Riv	ER, IN THE B	ASIN OF	(ilickaya	EL	EVATION	_ CATCHMEN		202.4 UNIT 10	,»գև» Cu.m.,	S	W	•
YEAR	Apr.	Kay	Jun.	Jul,	Aug.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	Mar.	ANNUA
1939	373.69	357.70	105.32	51.77	46.14	43,60	47.07	51,26	68.76	61.12	105.34	154.91	1,466.
1940	781.88	498.08	243.32	97.38	40.82	34.39	68,84	81.46	98,14	72.40	145.25	364.38	2,526.
1941	776.72	563.45	127.34	63.97	40.02	32.93	55.27	108.11	62,90	60.89	81,06	194,04	2,166.
1942	673.09	562.86	125.28	40.91	29.41	28.31	55.05	130.39	107.90	69.78	58.00	98,24	1,979.
1943	519.92	513.95	160.84	46.11	27.60	26,61	29,28	38.53	52.85	50.12	63.48	284.36	1,813
1944	401.45	565.82	237.17	63.23	33.49	32.34	38.27	69.80	53,28	43.49	39.47	71.95	1.649
1945	47.81	558.16	152.29	42.67	26,71	23.87	39.64	32.50	37.12	34.75	34.67	127,66	1,157
1946	514.12	561.36	226.04	56.57	35.97	27,93	82.13	44.23	35.95	46.22	68.05	308,44	2,007
-1947	269.10	121.16	66.95	27.55	18.69	23.74	25.38	80.84	44.39	46.83	52.18	62.02	
1948	558.62	541.58	219.42	37.01	25.14	24.65	28.16	27.93	29.81	26.68	27.18	85.71	1,631
1949	342.62	653.52	125.50	31.99	22.68	25.99	27.07	26.77	28.52	106.61	91.86	159.07	1,642
1950	699.36	501.00	115.35	42.19	27.53	25.08	54.17	47.66	42.31	45.49	39.09		1,854
1951	279.47	383.86	185,48	51.72	29.11	34.10	66.78	103.29	71.27	62.03	108,21	191.87	1,567
1952	672.91	413.54	153.81	49.26	30.15	27.34	28.70	32.94	37.98	33.90	52,03	74,78	1,607
1953	539.51	515.48	177.35	58.13	29,36	33,70	35.97	38.88	53.87	57.70	67.59	303.57	
1954	654.40	670.07	278.28	93.36	34.50	30.84	30.31	31.89	36.95	42.20	53.63	102.73	2,059
1955	236.98	214.91	52.61	21.30	19.05	18.68	21.40	24.70	35.85	35.65	70.82	90.30	
1956	533.81	393.79	186.33	46.73	25.08	32.68	29.85	36.08	70.22	39.68	59.49	250.50	
1957	388.92	435.39	208.67	49.40	26.04	25.60	28.85	31.57	37.63	36.72	45.82	160.19	
1958	483.44	339.90	190.21	43.73	26.13	25.03	29.50	29.11	34.66	36.41	30.66	130.72	
1959	400.32	366.86	202.25	50.03	23.04 * 39.58	21.76 *36.12	*41.39 *34.59	*47.80 *35.45	*41.52 *37.51	*45.18 *36.64	*94.93	*205.26	
1960	*804.05	*556.94	*167.86	* 67.67		*19.99	21.82	*35.45	71.84		*39.15	*89.17	
1961	*355.71	*200.83	*91.64	*22.06	*14.51					50.20	64.31	355.68	
1962	401.02	394.65	121.45	31.10	14.07	11.56	19.00	28,10 43,71	71.46	79.31	100.45	182.95	1,455
1963 1964	532.77 477.30	545.93 476.24	448.13 257.21	-101.51 52.36	35.24 24.73	34.07 27.28	30.36	43.71	37.65	41,21	44.69	156.83	2,044
1965	509.75	415.07	130.06	58.64	16.27	16.04	47.31	57.85	75.51	169.29	135.34	1	1,717
1966	509.17	465.53	198.95	65.65	21.74	24.37	28.31	34.29	54.44	45.71	43.40	104.98	1,596
Total	13,737.91	12,787.63	4,955.11	1.464.00	782.80	768.60	1,072.96	1.389.57	L,477.35	1.509.88	1,852.21	4,989.68	1
Average	490.64	456.70	•	· · ·	27.96		38.32	49.63	+	53,92	66.15		
							-		52.70	- 12	1	178.20	(139

* Value adjusted in correlation with Fatli data

Table II 1-18

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-18 Runoff		STAT	TON			CATCHMEN	T AREA _3	5,891.5	50 hr	YVACIK_T	URKEY	
irmakRIV	ER, IN THE B			k EI	EVATION	·		UNIT 10		_s		•
Apr.	May	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	Mar.	ANNUAI
904.99	713.36	278.38	152.07	132.28	143.51	192.52	208.0	302.06	534.60	629.08	803,96	4,994,84
2,187.90	1,305.58	687.38	304.13	134.64	117.82	174.37	222.74	311.68	411.45	718.85	1,522.54	8,099.08
1.914.90	1,032.10	265.55	166,10	101.03	96.32	138.92	219.60	182.88	192.08	312.22	741.72	5,363.42
1,572.50	1,130.29	301.85	119.98	86.75	96.71	146,22	280.02	326.30	263.91	250.68	430.86	5,006,0
1.544.96	1,191,40	508.82	155,32	95.44	91.72	103.51	127.47	164.67	191.27	286,49	876.89	5,337.96
1.020.30	1.085.13	476.34	170.53	96.69	91.91	103.99	160.55	143.36	131.01	120.16	240.04	3.840.01
1.		352.25	125.04	83.83	80.26	108.76	101.25	129.97	131.90	158.55	391.85	
1,145.01	1 074 01	451.58	178.57	129.63	101.67	184.67			189.07	425.78	911.70	5,063.73
632.06	285.63	158.41	89.76							265.36	381.53	2,582.7
1,545.61	1,246.64	648.19	132.72									4,804.68
												5,095.1
												4,069.3
												3,882.3
1,994.65	1,005.58	415.08	164.29	98.74								4,787.70
1,469.79	837.03	406.38	151.35	108.42								
1,902.36	1,579.44	622.41	214.63	108.74	93.79	91.35	102.59	133.75	186.43	205.83		5,567.14
570.68	523.83	136.40	64.96	60.40	70.15	145.09			355.74	587.75		3,731.53
1,164.07	810.69											4,314.60
783.68	931.13											3,987.91
1,167.75												4,059,63
1,032.96	835.94	552.30	105.17	71.24								3,852.91
											410,96	4,226.34
											959.28	3,803.36
792.86	580.86	211.98		52,03							749.18	3,960.42
1,461.97	1,267.79	907.81									709.69	5.976.32
913.42	789.22	490.54	106.50								733.23	3,861.46
											*/42./2	5.413.03
F1,181.83	*835.29	*367.00	*194.23	*104.84	*100.27	*117,63	+84.31	*209.06	*2/2.89	* 240,63	*890.33	4,598.31
34,684.70	26,762.75	11,838.33	4,068.04	2,402.66	2,429.79	3,209.77	3,951.71	5,190.24	6,729.33	9,022.09	19,597.26	129,886.
1,238.74	955.81	422.80	145.29	85.81	86.79	114.63	141.13	185.37	240.33	322.22	699.90	4,638.8
		•									4	(386.57)
	Runoff Itrmak	Runoff Itraak_RIVER, IN THE B Apr. Hay 904.99: 713.36 2,187.90 1,305.58 1,914.90 1,032.10 1,572.50 1,130.29 1,544.96 1,91.40 1,020.30 1,085.13 1,07.28 1,194.39 1,45.01 1,074.01 632.06 285.63 1,545.61 1,246.64 1,405.07 1,092.25 437.16 693.82 1,994.65 1,005.58 1,640.79 837.03 1,640.75 830.42 1,032.96 835.94 1,045.57 1,027.96 797.26 416.47 792.86 580.86 1,461.97 1,267.79 913.42 789.22 1,099.61 90.07 1,181.83 *835.29 34,684.70 26,762.75	Runoff STA1 17makRIVER, IN THE BASIN OF	Runoff STATION ItmakRIVER, IN THE BASIN OF Ayvac1 Ayvac1 904.99 713.36 278.38 152.07 2,187.90 1,305.58 687.38 304.13 1,914.90 1,032.10 265.53 166.10 1,572.50 1,130.29 301.85 119.98 1,544.96 1,914.40 508.82 155.32 1,020.30 1,035.13 476.34 170.53 1,107.28 1,194.39 352.22 125.04 1,45.01 1,074.01 451.55 178.57 632.06 285.63 158.41 89.76 1,465.01 1,246.64 648.19 132.72 1,465.01 1,246.64 648.19 132.72 1,465.01 1,246.64 648.19 132.72 1,465.01 1,262.25 258.24 100.16 1,465.01 1,264.64 648.19 137.31 1,994.65 1,005.58 415.08 151.35 1,902.36 1,579.44 622.44 <td< td=""><td>Runoff STATION ItmakRIVER, IN THE BASIN OF</td><td>Runoff STATON ItmakRIVER, IN THE BASIN OF Ayvacik</td><td>Runoff CATCHMEN STATION CATCHMEN ITERME_RIVER, IN THE BASIN OF Ayvacik ELEVATION Apr. Hay Jun. Jul. Aug. Sept. Oct. 904.99 713.36 278.36 152.07 132.28 143.51 192.52 2,187.90 1,305.58 687.33 304.13 134.64 117.82 174.37 1,914.90 1,032.10 265.55 166.10 101.03 96.32 138.92 1,545.496 1,191.40 508.82 155.32 95.44 91.72 103.51 1,020.30 1,085.13 476.34 170.53 96.69 91.91 103.99 1,107.28 1,194.39 352.21 125.04 83.83 80.26 108.76 1,45.01 1,207.401 451.53 178.57 129.63 101.67 184.67 632.06 285.63 158.41 89.76 74.10 78.30 83.39 1,465.01<td>Runoff CATCHMENT AREA CatCh Mort CatCh Not CatCh Not CatCh Not CatCh CatCh CatCh CatCh CatCh CatCh CatCh<td>Bunoff STATION CATCHMENT ARLA 35,891.5 Itmak_river, IN THE BASIN OF Ayvacik ELEVATION = UNIT 101 Apr. Hay Jun. Jul. Aug. Sept. Oct. Nov. Dec. 904.99 713.36 278.38 152.07 132.26 143.51 192.52 208.03 302.06 2,187.90 1,305.58 687.35 304.13 134.64 117.82 174.37 222.74 311.68 1,914.90 1,032.10 265.55 166.10 101.0 96.32 138.92 219.60 182.88 1,544.96 1,191.40 508.82 155.32 95.44 91.72 103.51 127.4 164.62 280.02 326.30 1,649.96 1,914.39 352.22 125.04 83.83 80.26 108.76 101.22 129.97 1,455.61 1,246.64 648.19 132.72 87.78 89.23 107.81 103.61 121.51 1,465.71 1,595.16</td><td>Runoff STATION CATCHMENT AREA 35,891.5 n+ 4 Itrusk_RVER, IN THE BASIN OF Ayvacik ELEVATION Nov. Dec. Jan. 904.99 713.36 278.36 152.07 132.22 143.51 192.52 208.03 302.06 534.60 1,914.90 1,032.10 265.55 166.10 101.03 96.37 2138.92 218.92 218.92 280.02 326.30 236.30 263.91 1,572.50 1,130.29 301.85 119.98 86.73 96.71 146.22 280.02 326.30 236.30 263.91 1,572.50 1,130.29 301.85 178.57 295.44 91.72 103.51 127.45 164.67 191.27 1,002.30 1,085.13 476.32 170.53 96.65 91.91 103.39 160.55 143.36 131.90 1,107.28 1,194.90 352.22 125.64 89.26 106.77 178.44 1,555.61 1,246.45 174.76 78.33<!--</td--><td>Runoff STATION CATCHMENT AREA 35,891.5 set Mark STATE Apr. Hay Jun. Jul. Aug. Sept. Oct. Nov. Dec. Jan. Feb. 906.99 7113.36 278.36 152.07 132.28 143.51 192.52 208.03 302.06 534.60 629.08 1,914.90 1,035.58 687.36 304.13 134.64 117.82 174.37 222.74 311.68 411.45 718.85 1,914.90 1,032.10 265.55 166.10 101.03 96.23 213.52 219.60 182.88 192.08 312.22 1,572.50 1,130.29 301.85 170.53 96.67 91.91 103.59 164.67 191.27 286.49 1,020.30 1,085.13 476.32 170.53 96.67 91.91 103.59 143.36 131.01 120.16 1,020.30 1,085.51 127.47 184.64 125.51 189.07 145.55 189.07 131.90</td><td>Runoff STATION CATCHNENT AREA 35,891.5 *** *YVACIK, TURKEY Apr. Hay Jun. Jul. Aug. Sept. Oct. Nov. Dec. Jan. Feb. Har. 906.99 713.36 278.36 152.07 132.22 143.51 192.52 208.03 302.06 534.60 629.08 803.96 219.66 11.68 411.45 718.85 1,522.54 166.10 101.03 96.22 139.22 219.66 182.88 192.08 132.22 741.72 1,522.50 1,103.29 301.85 119.98 86.73 96.71 146.22 220.02 326.30 263.91 250.68 430.66 1,002.30 1,085.31 476.32 191.00 108.52 132.74 166.67 191.27 286.49 137.92 1,072.30 1,085.31 352.21 125.64 91.72 103.51 127.41 164.67 191.127 286.49 91.72 1,020.20 1,285.61 182.37<</td></td></td></td></td<>	Runoff STATION ItmakRIVER, IN THE BASIN OF	Runoff STATON ItmakRIVER, IN THE BASIN OF Ayvacik	Runoff CATCHMEN STATION CATCHMEN ITERME_RIVER, IN THE BASIN OF Ayvacik ELEVATION Apr. Hay Jun. Jul. Aug. Sept. Oct. 904.99 713.36 278.36 152.07 132.28 143.51 192.52 2,187.90 1,305.58 687.33 304.13 134.64 117.82 174.37 1,914.90 1,032.10 265.55 166.10 101.03 96.32 138.92 1,545.496 1,191.40 508.82 155.32 95.44 91.72 103.51 1,020.30 1,085.13 476.34 170.53 96.69 91.91 103.99 1,107.28 1,194.39 352.21 125.04 83.83 80.26 108.76 1,45.01 1,207.401 451.53 178.57 129.63 101.67 184.67 632.06 285.63 158.41 89.76 74.10 78.30 83.39 1,465.01 <td>Runoff CATCHMENT AREA CatCh Mort CatCh Not CatCh Not CatCh Not CatCh CatCh CatCh CatCh CatCh CatCh CatCh<td>Bunoff STATION CATCHMENT ARLA 35,891.5 Itmak_river, IN THE BASIN OF Ayvacik ELEVATION = UNIT 101 Apr. Hay Jun. Jul. Aug. Sept. Oct. Nov. Dec. 904.99 713.36 278.38 152.07 132.26 143.51 192.52 208.03 302.06 2,187.90 1,305.58 687.35 304.13 134.64 117.82 174.37 222.74 311.68 1,914.90 1,032.10 265.55 166.10 101.0 96.32 138.92 219.60 182.88 1,544.96 1,191.40 508.82 155.32 95.44 91.72 103.51 127.4 164.62 280.02 326.30 1,649.96 1,914.39 352.22 125.04 83.83 80.26 108.76 101.22 129.97 1,455.61 1,246.64 648.19 132.72 87.78 89.23 107.81 103.61 121.51 1,465.71 1,595.16</td><td>Runoff STATION CATCHMENT AREA 35,891.5 n+ 4 Itrusk_RVER, IN THE BASIN OF Ayvacik ELEVATION Nov. Dec. Jan. 904.99 713.36 278.36 152.07 132.22 143.51 192.52 208.03 302.06 534.60 1,914.90 1,032.10 265.55 166.10 101.03 96.37 2138.92 218.92 218.92 280.02 326.30 236.30 263.91 1,572.50 1,130.29 301.85 119.98 86.73 96.71 146.22 280.02 326.30 236.30 263.91 1,572.50 1,130.29 301.85 178.57 295.44 91.72 103.51 127.45 164.67 191.27 1,002.30 1,085.13 476.32 170.53 96.65 91.91 103.39 160.55 143.36 131.90 1,107.28 1,194.90 352.22 125.64 89.26 106.77 178.44 1,555.61 1,246.45 174.76 78.33<!--</td--><td>Runoff STATION CATCHMENT AREA 35,891.5 set Mark STATE Apr. Hay Jun. Jul. Aug. Sept. Oct. Nov. Dec. Jan. Feb. 906.99 7113.36 278.36 152.07 132.28 143.51 192.52 208.03 302.06 534.60 629.08 1,914.90 1,035.58 687.36 304.13 134.64 117.82 174.37 222.74 311.68 411.45 718.85 1,914.90 1,032.10 265.55 166.10 101.03 96.23 213.52 219.60 182.88 192.08 312.22 1,572.50 1,130.29 301.85 170.53 96.67 91.91 103.59 164.67 191.27 286.49 1,020.30 1,085.13 476.32 170.53 96.67 91.91 103.59 143.36 131.01 120.16 1,020.30 1,085.51 127.47 184.64 125.51 189.07 145.55 189.07 131.90</td><td>Runoff STATION CATCHNENT AREA 35,891.5 *** *YVACIK, TURKEY Apr. Hay Jun. Jul. Aug. Sept. Oct. Nov. Dec. Jan. Feb. Har. 906.99 713.36 278.36 152.07 132.22 143.51 192.52 208.03 302.06 534.60 629.08 803.96 219.66 11.68 411.45 718.85 1,522.54 166.10 101.03 96.22 139.22 219.66 182.88 192.08 132.22 741.72 1,522.50 1,103.29 301.85 119.98 86.73 96.71 146.22 220.02 326.30 263.91 250.68 430.66 1,002.30 1,085.31 476.32 191.00 108.52 132.74 166.67 191.27 286.49 137.92 1,072.30 1,085.31 352.21 125.64 91.72 103.51 127.41 164.67 191.127 286.49 91.72 1,020.20 1,285.61 182.37<</td></td></td>	Runoff CATCHMENT AREA CatCh Mort CatCh Not CatCh Not CatCh Not CatCh CatCh CatCh CatCh CatCh CatCh CatCh <td>Bunoff STATION CATCHMENT ARLA 35,891.5 Itmak_river, IN THE BASIN OF Ayvacik ELEVATION = UNIT 101 Apr. Hay Jun. Jul. Aug. Sept. Oct. Nov. Dec. 904.99 713.36 278.38 152.07 132.26 143.51 192.52 208.03 302.06 2,187.90 1,305.58 687.35 304.13 134.64 117.82 174.37 222.74 311.68 1,914.90 1,032.10 265.55 166.10 101.0 96.32 138.92 219.60 182.88 1,544.96 1,191.40 508.82 155.32 95.44 91.72 103.51 127.4 164.62 280.02 326.30 1,649.96 1,914.39 352.22 125.04 83.83 80.26 108.76 101.22 129.97 1,455.61 1,246.64 648.19 132.72 87.78 89.23 107.81 103.61 121.51 1,465.71 1,595.16</td> <td>Runoff STATION CATCHMENT AREA 35,891.5 n+ 4 Itrusk_RVER, IN THE BASIN OF Ayvacik ELEVATION Nov. Dec. Jan. 904.99 713.36 278.36 152.07 132.22 143.51 192.52 208.03 302.06 534.60 1,914.90 1,032.10 265.55 166.10 101.03 96.37 2138.92 218.92 218.92 280.02 326.30 236.30 263.91 1,572.50 1,130.29 301.85 119.98 86.73 96.71 146.22 280.02 326.30 236.30 263.91 1,572.50 1,130.29 301.85 178.57 295.44 91.72 103.51 127.45 164.67 191.27 1,002.30 1,085.13 476.32 170.53 96.65 91.91 103.39 160.55 143.36 131.90 1,107.28 1,194.90 352.22 125.64 89.26 106.77 178.44 1,555.61 1,246.45 174.76 78.33<!--</td--><td>Runoff STATION CATCHMENT AREA 35,891.5 set Mark STATE Apr. Hay Jun. Jul. Aug. Sept. Oct. Nov. Dec. Jan. Feb. 906.99 7113.36 278.36 152.07 132.28 143.51 192.52 208.03 302.06 534.60 629.08 1,914.90 1,035.58 687.36 304.13 134.64 117.82 174.37 222.74 311.68 411.45 718.85 1,914.90 1,032.10 265.55 166.10 101.03 96.23 213.52 219.60 182.88 192.08 312.22 1,572.50 1,130.29 301.85 170.53 96.67 91.91 103.59 164.67 191.27 286.49 1,020.30 1,085.13 476.32 170.53 96.67 91.91 103.59 143.36 131.01 120.16 1,020.30 1,085.51 127.47 184.64 125.51 189.07 145.55 189.07 131.90</td><td>Runoff STATION CATCHNENT AREA 35,891.5 *** *YVACIK, TURKEY Apr. Hay Jun. Jul. Aug. Sept. Oct. Nov. Dec. Jan. Feb. Har. 906.99 713.36 278.36 152.07 132.22 143.51 192.52 208.03 302.06 534.60 629.08 803.96 219.66 11.68 411.45 718.85 1,522.54 166.10 101.03 96.22 139.22 219.66 182.88 192.08 132.22 741.72 1,522.50 1,103.29 301.85 119.98 86.73 96.71 146.22 220.02 326.30 263.91 250.68 430.66 1,002.30 1,085.31 476.32 191.00 108.52 132.74 166.67 191.27 286.49 137.92 1,072.30 1,085.31 352.21 125.64 91.72 103.51 127.41 164.67 191.127 286.49 91.72 1,020.20 1,285.61 182.37<</td></td>	Bunoff STATION CATCHMENT ARLA 35,891.5 Itmak_river, IN THE BASIN OF Ayvacik ELEVATION = UNIT 101 Apr. Hay Jun. Jul. Aug. Sept. Oct. Nov. Dec. 904.99 713.36 278.38 152.07 132.26 143.51 192.52 208.03 302.06 2,187.90 1,305.58 687.35 304.13 134.64 117.82 174.37 222.74 311.68 1,914.90 1,032.10 265.55 166.10 101.0 96.32 138.92 219.60 182.88 1,544.96 1,191.40 508.82 155.32 95.44 91.72 103.51 127.4 164.62 280.02 326.30 1,649.96 1,914.39 352.22 125.04 83.83 80.26 108.76 101.22 129.97 1,455.61 1,246.64 648.19 132.72 87.78 89.23 107.81 103.61 121.51 1,465.71 1,595.16	Runoff STATION CATCHMENT AREA 35,891.5 n+ 4 Itrusk_RVER, IN THE BASIN OF Ayvacik ELEVATION Nov. Dec. Jan. 904.99 713.36 278.36 152.07 132.22 143.51 192.52 208.03 302.06 534.60 1,914.90 1,032.10 265.55 166.10 101.03 96.37 2138.92 218.92 218.92 280.02 326.30 236.30 263.91 1,572.50 1,130.29 301.85 119.98 86.73 96.71 146.22 280.02 326.30 236.30 263.91 1,572.50 1,130.29 301.85 178.57 295.44 91.72 103.51 127.45 164.67 191.27 1,002.30 1,085.13 476.32 170.53 96.65 91.91 103.39 160.55 143.36 131.90 1,107.28 1,194.90 352.22 125.64 89.26 106.77 178.44 1,555.61 1,246.45 174.76 78.33 </td <td>Runoff STATION CATCHMENT AREA 35,891.5 set Mark STATE Apr. Hay Jun. Jul. Aug. Sept. Oct. Nov. Dec. Jan. Feb. 906.99 7113.36 278.36 152.07 132.28 143.51 192.52 208.03 302.06 534.60 629.08 1,914.90 1,035.58 687.36 304.13 134.64 117.82 174.37 222.74 311.68 411.45 718.85 1,914.90 1,032.10 265.55 166.10 101.03 96.23 213.52 219.60 182.88 192.08 312.22 1,572.50 1,130.29 301.85 170.53 96.67 91.91 103.59 164.67 191.27 286.49 1,020.30 1,085.13 476.32 170.53 96.67 91.91 103.59 143.36 131.01 120.16 1,020.30 1,085.51 127.47 184.64 125.51 189.07 145.55 189.07 131.90</td> <td>Runoff STATION CATCHNENT AREA 35,891.5 *** *YVACIK, TURKEY Apr. Hay Jun. Jul. Aug. Sept. Oct. Nov. Dec. Jan. Feb. Har. 906.99 713.36 278.36 152.07 132.22 143.51 192.52 208.03 302.06 534.60 629.08 803.96 219.66 11.68 411.45 718.85 1,522.54 166.10 101.03 96.22 139.22 219.66 182.88 192.08 132.22 741.72 1,522.50 1,103.29 301.85 119.98 86.73 96.71 146.22 220.02 326.30 263.91 250.68 430.66 1,002.30 1,085.31 476.32 191.00 108.52 132.74 166.67 191.27 286.49 137.92 1,072.30 1,085.31 352.21 125.64 91.72 103.51 127.41 164.67 191.127 286.49 91.72 1,020.20 1,285.61 182.37<</td>	Runoff STATION CATCHMENT AREA 35,891.5 set Mark STATE Apr. Hay Jun. Jul. Aug. Sept. Oct. Nov. Dec. Jan. Feb. 906.99 7113.36 278.36 152.07 132.28 143.51 192.52 208.03 302.06 534.60 629.08 1,914.90 1,035.58 687.36 304.13 134.64 117.82 174.37 222.74 311.68 411.45 718.85 1,914.90 1,032.10 265.55 166.10 101.03 96.23 213.52 219.60 182.88 192.08 312.22 1,572.50 1,130.29 301.85 170.53 96.67 91.91 103.59 164.67 191.27 286.49 1,020.30 1,085.13 476.32 170.53 96.67 91.91 103.59 143.36 131.01 120.16 1,020.30 1,085.51 127.47 184.64 125.51 189.07 145.55 189.07 131.90	Runoff STATION CATCHNENT AREA 35,891.5 *** *YVACIK, TURKEY Apr. Hay Jun. Jul. Aug. Sept. Oct. Nov. Dec. Jan. Feb. Har. 906.99 713.36 278.36 152.07 132.22 143.51 192.52 208.03 302.06 534.60 629.08 803.96 219.66 11.68 411.45 718.85 1,522.54 166.10 101.03 96.22 139.22 219.66 182.88 192.08 132.22 741.72 1,522.50 1,103.29 301.85 119.98 86.73 96.71 146.22 220.02 326.30 263.91 250.68 430.66 1,002.30 1,085.31 476.32 191.00 108.52 132.74 166.67 191.27 286.49 137.92 1,072.30 1,085.31 352.21 125.64 91.72 103.51 127.41 164.67 191.127 286.49 91.72 1,020.20 1,285.61 182.37<

* Value adjusted taking into consideration of assumed Almus natural flow

Table II 3	-19 Runoff		STA	TION			_ CATCHMEN	T AREA	2,352.8	149 ton	ALMUS, T	JRKEY	ł
Yesil	irmakRP	VER IN THE	BASIN OF	Almus	E	LEVATION		•	UNIT10	6 cu.m.	_s	¥	•
YEAR	Apr.	Нау	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	Mar.	ANNUAL
1939	154,0	149.0	47.0	32.4	29.5	28.2	30.0	32.0	43.0	37.0	47.3	76.8	706.2
1940	267.0	191.0	109.5	53.6	26.9	23.2	40.8	46.5	53.9	42.2	73.2	149.5	1,077 3
[1941	266.0	210.0	65.9	32.2	26.1	22.5	34.0	57.6	37.7	37.0	46.5	88.0	923.5
L 1942	242.0	210.0	65.4	26.8	20.6	20.0	34.0	67.2	58.0	41.0	35.2	53.8	874.0
1943	200.0	196.0	79.8	29.4	19.5	19.0	20.4	25.8	33.0	31.6	38.2	124.0	816.7
1944	160.0	211.0	107.5	38.0	23.0	22.1	25.4	41.0	33.2	28.2	26.0	42.0	757.4
_ 1945	180.5	209.5	76.0	27.7	19.1	17.3	26.1	22.4	24.6	23,6	23.5	66,8	717.1
- 1946	196.0	210.0	104.0	34.5	24.1	19.8	28.6	18.5	17.2	31.5	62.1	168.0	914.3
- 1947	116.0	71.5	29.3	17.3	12.7	14.0	13.9	34.6	30.1	36.5	46.6	67.8	490.3
- 1948	270.0	212.0	116.0	45.4	27.2	22.5	23.7	19.6	22.9	21.3	23.1	87.3	891.0
_ 1949	215.0	264.0	65.2	33.3	22.4	21.7	24.5	22.1	21.4	23.9	26.3	136.0	875.8
1950	267.0	163.0	59.0	33.0	25.4	20.9	24.3	21.9	23.6	23.3	20.8	73.1	755.3
- 1951	84.1	59.7	41.1	15.7	9.5	11.5	21.4	12.0	14.8	37.3	75.0	121.0	503.1 -
- 1952	239.0	179.0	75.1	30.5	18.9	14.3	20.0	22.6	25.4	23.0	32.5	43.2	723.5
1953	205.0	196.0	85.2	35.6	20.5	23.0	24.2	25.7	33.5	35.3	40.0	129.9	853.9
1954	237.0	240.0 105.7	121.5	51.4	23.4	21.4 13.5	23.8 11.5	23.6 13.8	29.7 20.5	46.1 22.7	54.0 56.3	85.0 81.8	956.9
1955	113.5 207.7		32.3 69.9	18.0 34.3	13.8 26.2	23.3	21.1	25.7	20.5	22.6	35.7	132.6	503.4 757.0
1950	131.4	128.9 138.3	62.6	24.0	13.4	12.6	13.0	13.0	13.9	22.6	39.0	108.0	589.6
F .			• •			24.5	24.8	23.9	26.1		1		799.7
- 1958 1959	231.1 229.9	139.2 143.0	89.8 101.4	45.3 28.8	28.9 22.6	18.1	19.0	23.9	19.1	21.4	27.5	117.2	775.1
1960	288.1	136.9	68.6	38.2	27.0	25.1	24.1	24.6	25.9	25.4	26.8	51.6	762.3
1961	155.0	98.0	52.8	16.8	11.8	15.6	17.8	24.6	39.2	33.5	38.8	155.0	658.9
1962	172.0	149.0	57.0	18.9	13.0	12.0	15.2	17.9	35.5	59.2	67.0	83.0	699.7
1963	226.0	225.0	180.5	69.4	31.4	29.8	+31.7	*38.1	*37.5	*22.9	*28.9	*87.2	1.008.4
1964	*174.2	*157.5	*99.3	+28.0	*16.5	+17.4	+18.9	*23.1	*29.6	*27.1	*25.1	*95.7	712.4
1965	*197.7	*180.3	*89.4	+33.9	*13.9	*13.6	+29.6	+34.3	+46.1	*80.2	*67.2	+105.9	892.1
1966	*175.1	*149.1	+77.0	+35.3	*16.7	+18.1	+20.0	+22.3	±30.5	*31.0	*26.3	*55.9	657.3
- Total	5,600.3	4,722.6	2,228.1	927.7	584.0	545.0	661.8	775.9	854.9	906.7	1,154.5	2,690.7	21,652.2-
Averige	200.01	168,66	79.58	33,13	20.86	19.46	23.64	27.71	30.53	32.38	41.23	96.10	773.29 (64.44

* Value estimated in correlation with Fatli data as-using without Almus reservoir

Table 11 1-20

Approximately regulated discharge

from the	ately regu reservoir		-	TION			CATCHMEN	T AREA _2	2,352.8	sq ka	ALHUS, TI	IRKEY	
	irmakRIN	TR IN THE E		Almus	EI	EVATION			UNIT	0 ⁶ cu.m.	_s _•	N	•
YEAR	Apr.	May	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	Jan.	Feb.	Mar.	ANNUAL -
1939	53.01	54.77	53.01	67.01	65.35	53.01	54.77	53.01	54.77	54.77	51.24	\$4.77	669.4
1940	104.28	190.26	107.36	67.01	65.35	53.01	54.77	53.01	54.77	54.77	49.47	54.77	908.8
1941	258.65	209.26	63.76	67 01	65.35	53.01	54.77	53.01	54.77	54.77	49.47	54.77	1,038.6
1942	106.45	209.26	63.26	67.01	65.35	53.01	54 77	53.01	54.77	54.77	49.47	54.77	885,9
1943	53.01	181.70	77.66	67.01	65.35	53.01	\$4.77	53.01	54.77	54.77	51.24	54.77	821.0
1944	53.01	139.23	105.36	67.01	65.35	53.01	54.77	53.01	54.77	54.77	49.47	54.77	804.5
1945	53.01	98.00	73.66	67.01	65.35	53.01	\$4.77	53.01	54 77	54.77	49.47	54.77	731.8
1946	53.01	86.20	101.86	67.01	65.35	53.01	54.77	53.01	54.77	54.77	49.47	54.77	748.0
1947	53.01	54.77	53.01	67.01	65.35	53.01	54.77	53.01	54.77	54.77	51.24	54.77	669.4
1948 1949	53.01 53.01	123.11 201.10	113 86 63.06	67.01 67.01	65.35 65.35	53.01 53.01	54.77 54.77	53.01 53.01	54.77 54.77	54.77 54.77	49.47 49.47	54.77 54.77	796.9 824.1
1950	81.45	162.26	56.86	67.01	65.35	53.01	54.77	53.01	54.77	54.77	49.47	54.77	807.5
1951	53.01	54.77	53 01	67.01	65.35	53.01	\$4.77	53.01	54.77	54.77	51.24	54.77	669.4
1952	53.01	54.77	53.01	67.01	65.35	53.01	54.77	53 01	54.77	54.77	49.47	54.77	667.7
1953	53.01	54.77	53.01	67.01	65.35	53.01	54.77	53.01	54.77	54.77	49.47	54.77	667.7
1954	53.01	208.67	119,36	67.01	65.35	53.01	54.77	53.01	54.77	54.77	49.47	54.77	887.9
1955	53.01	54.77	\$3.01	67.01	65.35	53.01	54.77	53.01	54.77	54.77	51.24	54.77	669.4
1956	53.01	54.77	53.01	67.01	65.35	, 53 .01	54.77	53.01	54.77	54.77	49.47	54.77	667.7
1957	53.01	54.77	53.01	67.01	65.35	53.01	54.77	53.01	54.77	54.77	49.47	54.77	667.7
1958	53.01	54.77	53.01	67.01	65.35	53.01	54.77	53.01	54.77	54.77	49.47	54.77	667.7
1959	53.01	85.05	99.26	67.01	65.35	53.01	54.77	53.01	54.77	54.77	51.24	54.77	746.0
1960	53.01	134.56	66.46	67.01	53.01	53.01	54.77	53.01	54.77	54.77	49.47	54.77	748.6
1961	53.01	54.77	53.01	67.01	65.35	53.01	54.77	53.01	54.77	54.77	49.47	54.77	667.7
1962	53.01	54.77	53.01	67.01	65.35	53.01	54.77	53.01	54.77 54.77	54.77 54.77	49.47 51.24	54.77 54.77	667.7
1963	53.01	145.76	178.36	67.01	65.35	53.01	54.77	53.01		54.77			885.8 793.0
1964	53.01	135.93	97.16	67.01	65.35	53.01	54.77	53.01 53.01	54.77 54.77	54.77	49.47 49.47	54.77 54.77	793.0
1965	53.01	88.50	87.26	67.01	65.35	53.01	54.77	53.01	54.77	54.77	49.47	54.77	812.8
1966	82.65	148.36	74.86	67.01	65.35	53.01	54.77	-					1
Tot 1	1,852.71	3,149.68	2,132.73	1,876.28	1,817.46	1,484.28	1,533.56	1,484.28	1,533.56	1,533.56	1 -	1,533.56	21,329.2
Average	66.17	112.49	76.17	67.01	64.91	53.01	54.77	53.01	54.77	54,77	49.91	54.77	761.7
	1												(63.4

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	Name	Ту	ре	D. A. (Km ²)	Annual Runoff (10 ⁶ m ³)	Average Precipitation (mm)	Design Flood (cms)
1.	Demirkopru	F	77	6,590	708	630	9,300
2.	Hirfanli	F	82	26,200	2,993	400	8,000
3.	Seyhan	F	77	19,194	4,200	600	7,000
4.	Keban	F	204	64,090	20,400	650	20,000
5.	Susurluk	F	,	6,028			6,200
6.	Manyas	F	-	1,981			3,560
7.	Kemer	CG	114	3,100	950	750	5,000
8.	Almus	F		2,353	759	900	2,200
9.	Cubuk			190			500
10.	Seyitler			295			450
11.	Selevir			722			675
12.	Altinapa			589			1,640
13.	May			1,411			535
14.	Medik	F	46	7,000	645	365	1,800
15.	Sariyar	CG	110	42, 196	2,500	300	8,000
16.	Sille			33			250
17.	Ayranci			1,335			500
18.	Damca			80			150
19.	Ayvacik			36,000	4,700	530	1 1,000
20.	Kilickaya			8,202	1,700	450	4,000

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Table II 1-21 Design Flood in Turkey •

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No.	Year	Precipitation in March, P(mm)	X =log. P	No.	Year	Precipitation in March, P(mm)	X = log. P
1	1940	59.6	1.77525	15	1954	47.1	1.67302
2	1941	88.5	1.94694	16	1955	30.4	1.48287
3	1942	41.2	1.61490	17	1956	20.3	1.30750
4	1943	28.1	1.44871	18	1957	33.1	1.51983
5	1944	59.1	1.77159	19	1958	52.4	1.7 1933
6	1945	74.0	1.86923	20	1959	26.1	1.41664
7	1946	78.5	1.89487	21	1960	33.2	1.52114
8	1947	47.2	1.67394	22	1961	30.9	1.48996
9	1948	56.1	1.74896	23	1962	49.8	1.69723
10	1949	126.4	2.10174	24	1963	63.3	1.80140
11	1950	40.1	1.60314	25	1964	89.4	1.95134
12	1951	32.1	1.50651	26	1965	53.5	1.72835
13	1952	87.0	1.93952	27	1966	53.9	1.73159
14	1953	15.0	1.17609	28	1967	58.7	1.76864

Table II 1-22 Deriving Probable Maximum Flood at Kilickaya (Based on mean and standard deviation of precipitation)

X = XN + K. SN

Xt = Precipitation for return period T, in years, when a paticular extreme-value distribution in used. N, SN = Mean and standard deviation for a series of N annual maximum

K =	Stan	d	a	r	đ	ized	۷

K = Standardized variance 5x = 46.88023	K	Frequency	X	P (inm)
= 1.67429	2.33	100 yrs	2.15893	144
	3.08	1,000 yrs	2.31493	207
$\Sigma x^2 = 79.69583$	3.62	10,000 yrs	2.42725	267
	4.00		2.50629	321
$SN = \int_{N}^{X^2} \frac{1}{X^2} = 0.04303$	5.50	(90% included)	2.81829	658
11	6.00		2.92229	836
t = X + SN. K	10.00		3.75429	5,680
= 1.67429 + 0.20800 K	15.00		4.79429	6,230

$$K = 5.5$$
 P = 658 mm

 $Q_{\text{peak}} = (0.80 \times 658 \times \frac{8,202}{86.40} \times 0.18 + 520) \times 1.05$ Volume = 0.8 x 0.658 x 8,202 + 1,000 = 5,400 mcm= (9,000 + 520) x 1.05 = 5,800 cms

K = 4.0 P = 321 mm

$$Q_{\text{peak}} = (0.80 \times 321 \times \frac{8,202}{86.40} \times 0.18 + 520) \times 1.05$$

$$= (4,380+520) \times 1.05$$

$$= 5,100 \text{ cms}$$

$$K = 3.62 (10,000 \text{ yr Frequency})$$

$$P = 267 \text{ mm}$$

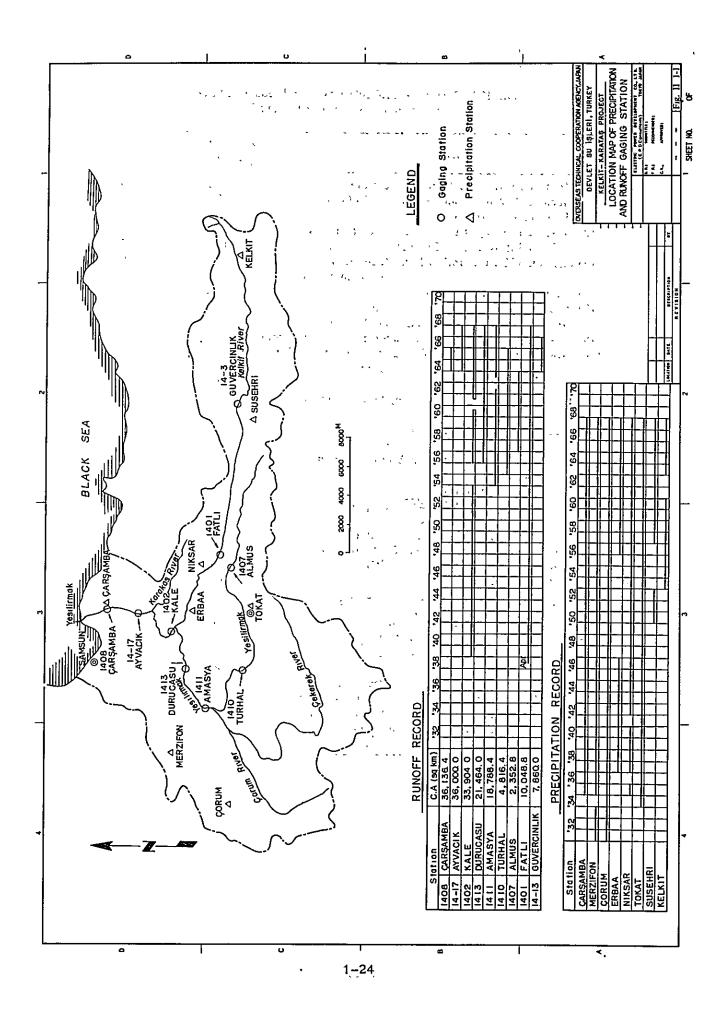
 $Q_{\text{peak}} = (0.80 \times 267 \times \frac{8,202}{86.40} \times 0.18 + 520) \times 1.05$ Volume = 0.80 x 0.267 x 8,202 + 1,000 = 2,800 mcm $= (3,700 + 520) \times 1.05$ = 4,400 cms

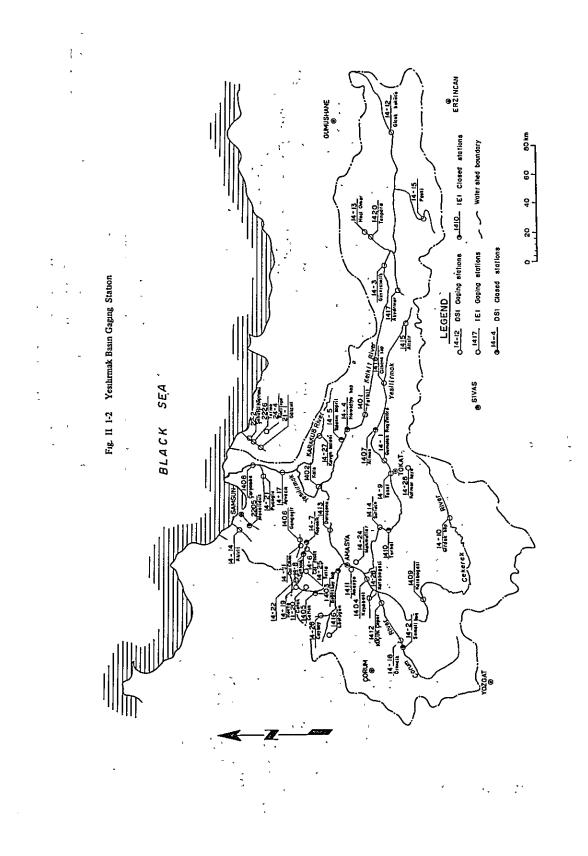
* Adopted the Probable Maximu Base flow of the storm-2 in Table 3

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Item	Storm - 1	Storm - 2
	March, 1952)	(April, 1967)
(1) Monthly Average 1,000 mb Temperature (°C)	7.5	15.0
(2) Precipitable Water from 1,900 m to 12,000 m	270	700
(Based on (1)), (mm)		
(3) Maximum Average Upper Wind Speed at Ankara (m/s)	37.5	34.0
(4) Moisture Inflow Index, (3) x (2), (1,000 mm, m/s)	10.2	23.8
(5) Maximum Moisture Inflow Index (See Fig. 11), (1,000 mm, m/s)	32.0	60.0
(6) Maximizing Factor (5)/(4)	3.1	2.5
(7) Precipitation in Storm (mm)	87.0	33.2
(8) Probable Maximum Precipitation in Storm (6) x (7) (mm)	270	83
(9) Probable Maximum Runoff for a Storm, (8) x 0.80 (mm)	216	67
(10) Probable Maximum Runoff for a Storm, (9) x $8,202$ km ² (10^6 m ³)	1,780	550
(÷. 86,400), (m ³ /s-day)	20,600	6,400
(11) Probable Maximum Surface Daily Peak, (10) x 18.0% (m ³ /s)	3,700	1,200
12) Maximum Temperature in the Storm at Tokat,	24.2	18.2
(El. 650 m) (°C)	17.2	11.2
 Maximum Temperature in the Storm at Center of Snowline, 1,900 m (°C) 	17.2	11.2
14) Snowmelt in the Storm	66	44
Snowme, 1,500 m (C) 14) Snowmelt in the Storm (13) x 4 mm/°C x $\frac{8,000 \text{ km}^2}{8,202 \text{ km}^2}$ (mm/day) 15) Best Maximum Temperature at Tokat (°C)		
(15) Past Maximum Temperature at Tokat (°C)	30.1	30.1
(16) Past Maximum Temperature at Center of Snowline,	23.1	23.1
1,900 m (°C)		
(17) Past Maximum Snowmelt	113	113
(16) x 5 mm/°C x $\frac{8,000 \text{ km}^2}{8,202 \text{ km}^2}$ (mm/day)		
(18) Maximizing Factor for Base Flow (17) / (14)	1.7	2.6
(19) Base Flow at Kilickaya: Total (m ³ /s - day)	3,700	4,400
Peak (m ³ /s)	105	200
(20) Probable Maximum Base Flow: Total (m ³ /s - day)	6,300	11,500
(18) x (19) Peak (m^3/s)	180	520
(21) Probable Maximum Daily Peak (11) + (20), (m^3/s)	3,880	1,720
(22) Probable Maximum Peak Flow (21) x 1.05 (m^3/s)	4,000	1,800
(23) Probable Maximum Flood Volume $(m^3/s - day)$ (10) + (20) (10 ⁶ m ³)	24,300 2,100	17,900 1,550

Table II 1-23 Deriving Probable Maximum Flood at Kilickaya
(Based on two floods in 1952 and 1967)





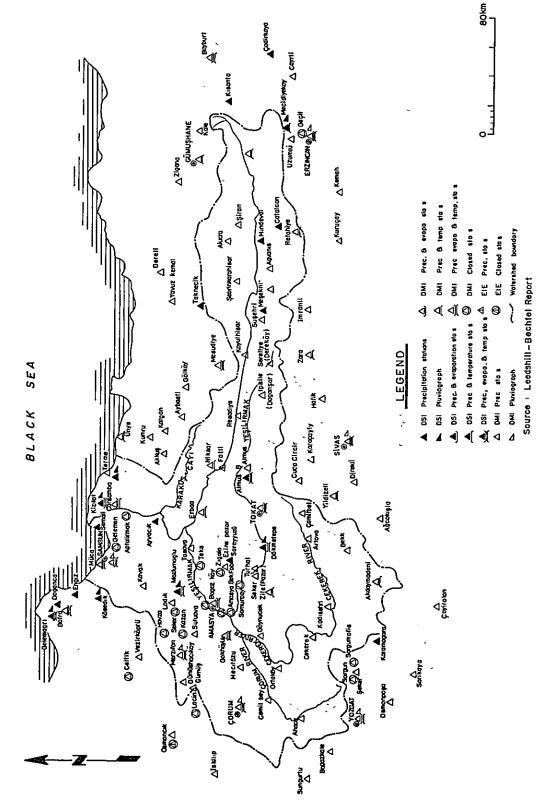
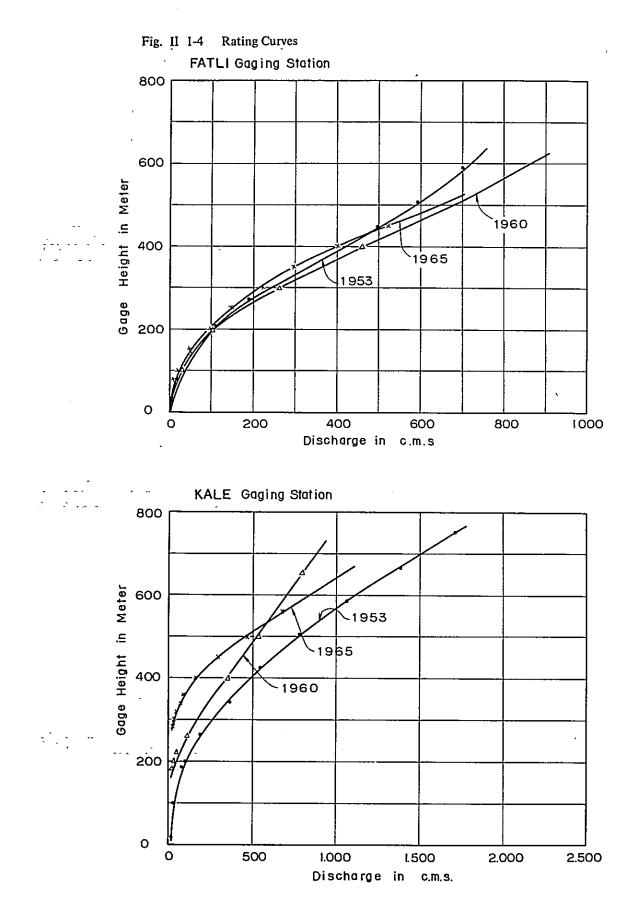
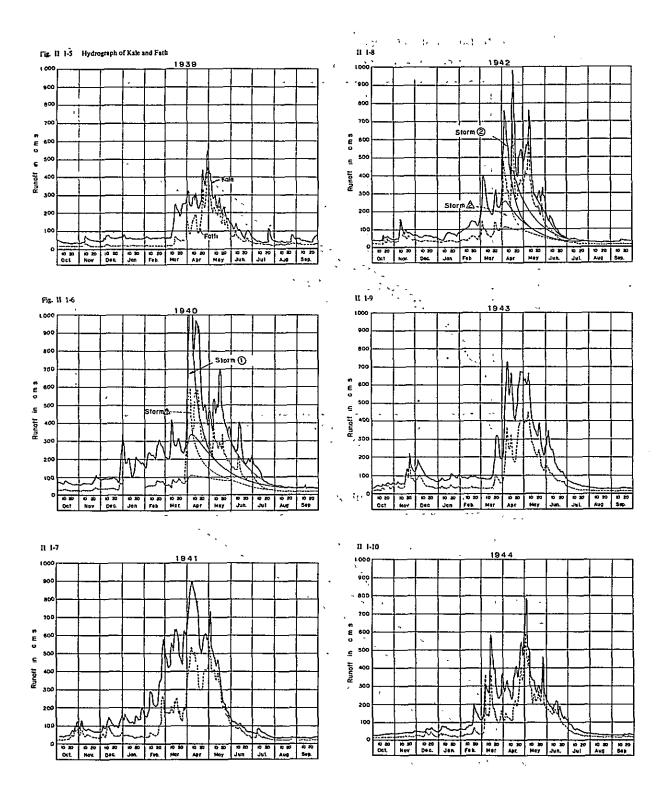


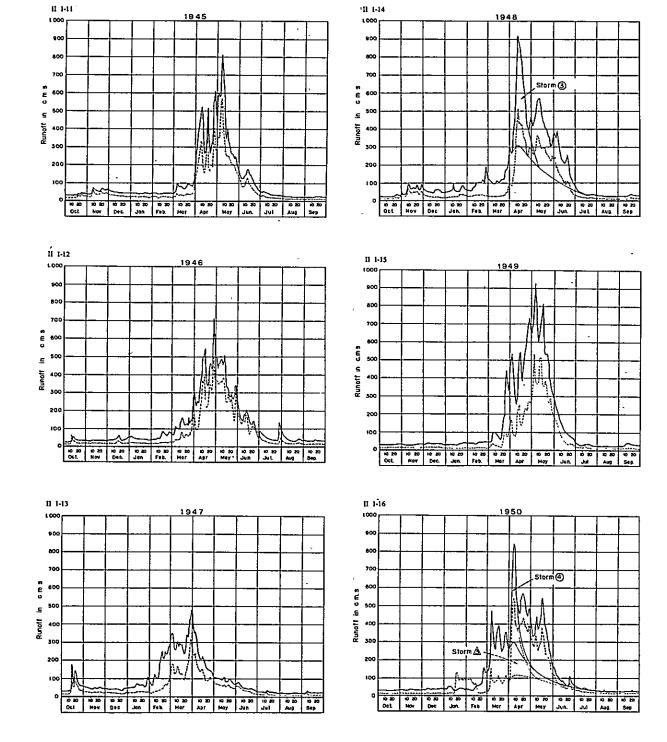
Fig. II 1-3 Yestlirmak Basin Meteorological Station

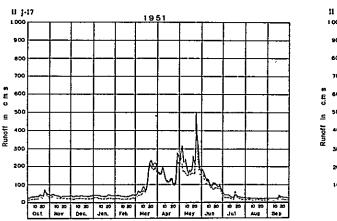
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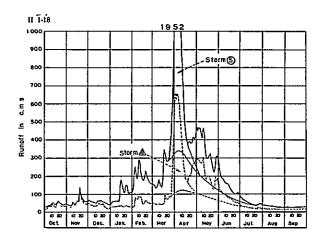


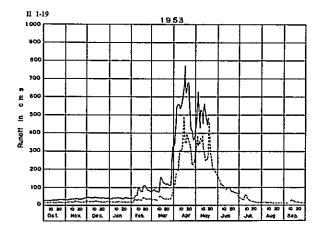


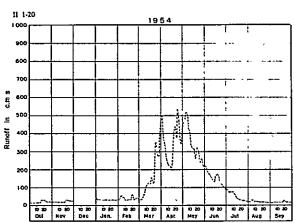


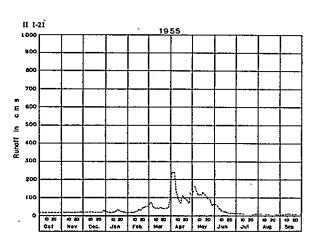


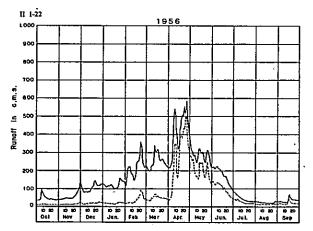
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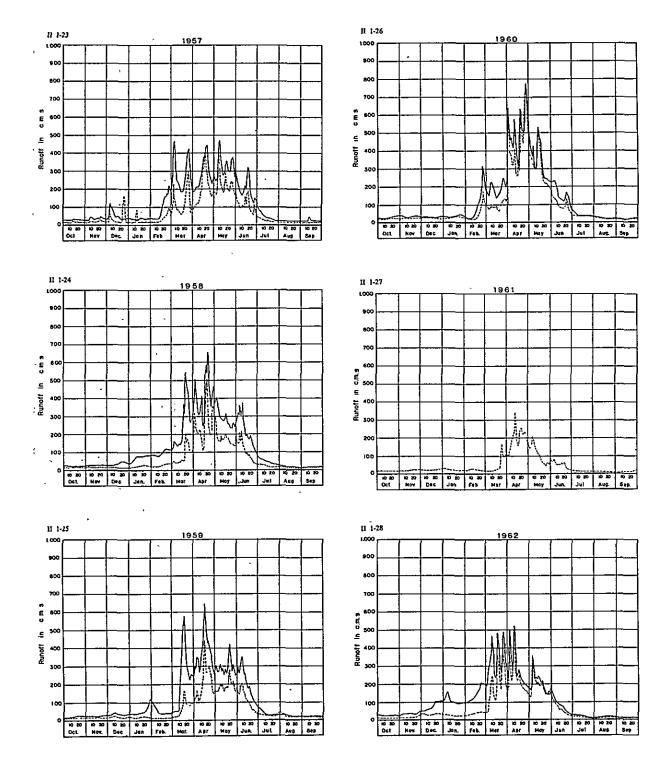


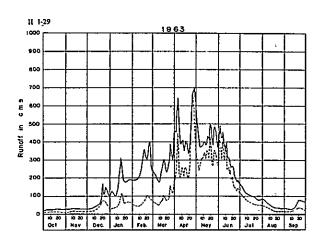


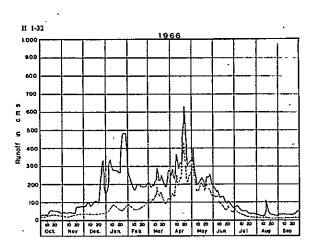


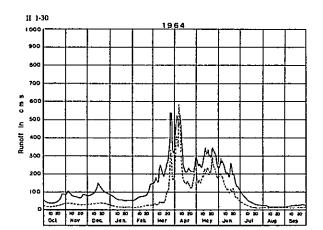


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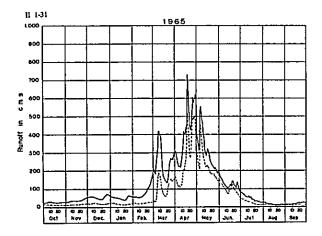
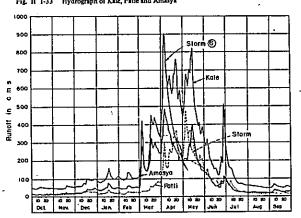
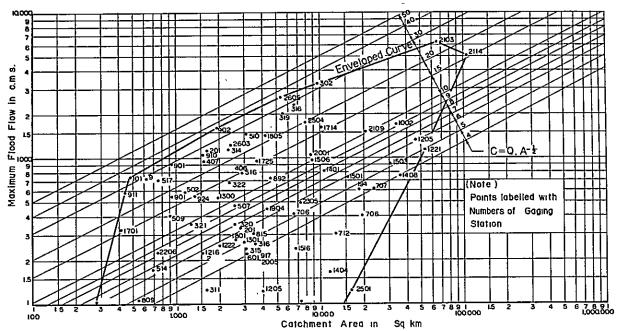


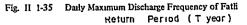
Fig. II 1-33 Hydrograph of Kate, Fatle and Amasya

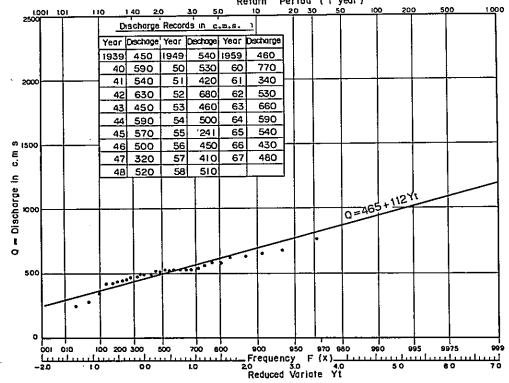






Fig, II 1-34 Enveloped Curve-of Maximum Flood in Turkey





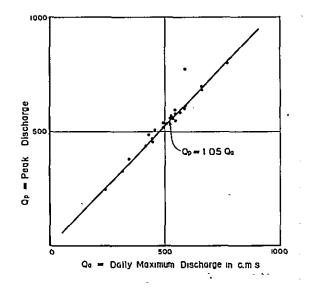
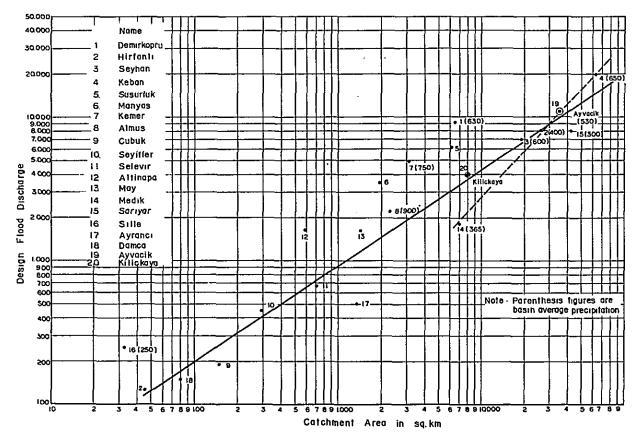


Fig. II 1-36 Corretation Between Peak Discharge and Daily Maximum Discharge at Fath

Fig. 11 1-37 Correlation Between Design Flood and Catchment Area in Turkey



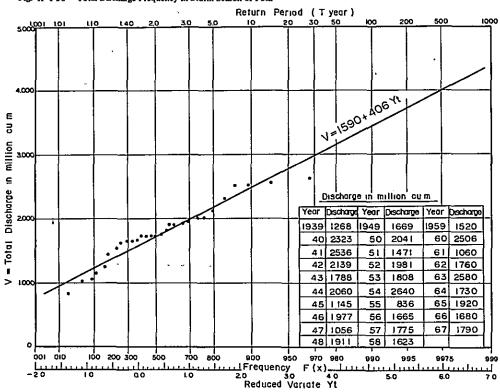
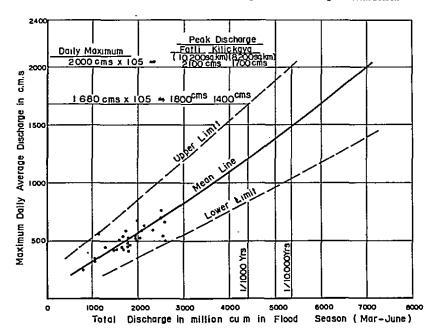
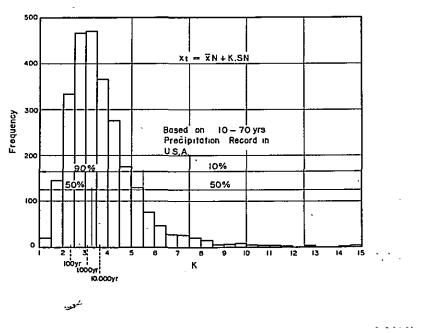


Fig. II 1-38 Total Discharge Frequency in Storm Season of Fatli

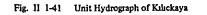
Fig. II 1-39 Correlation Between Peak Discharge and Total Discharge in Storm Season

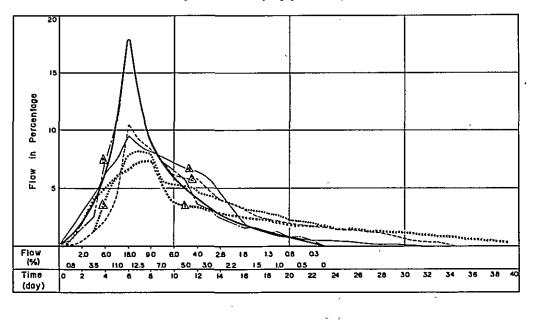


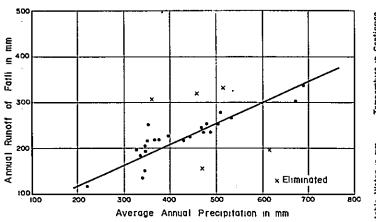


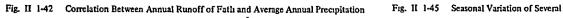
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Fig. II 1-40 Distribution of Standardized Variate (K)









40 40 40 (1) Monthly Average 10 (1) Monthly Average 1000mb Temperature 10 (1) Monthly Average 1000mb Temperature 10 (2) Precipitable Water from IOOOm to 200mb (Based on (1))

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Facters of Probable Maximum Precipitation

Fig. II 1-43 Correlation Between Total Runoff at Fath and Precipitation in Stormy Season

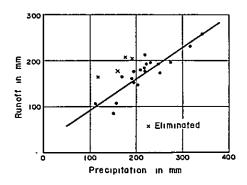
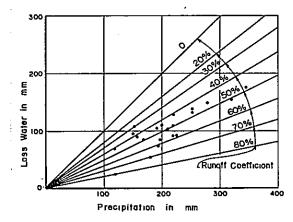
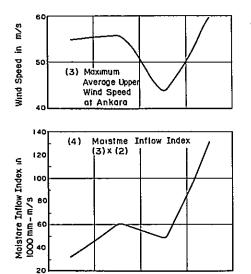


Fig. II 1-44 Correlation Between Loss Water and Precipitation in Storm Season



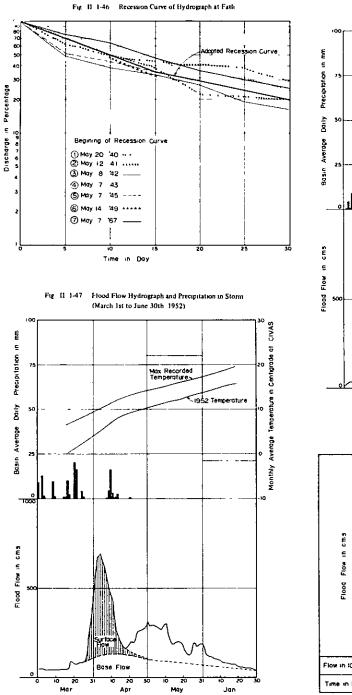


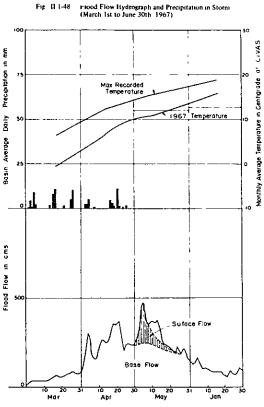
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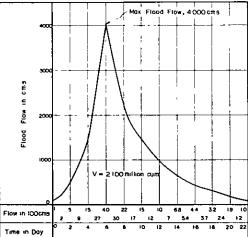
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II 2 Geology

Contents

II 2-1	Introduc	tion	2-1				
	II 2-1-1	Geologycal Studies Performed by the DSI	2-1				
	II 2-1-2 Geologic Studies Performed by the Japanese Government Survey Team and Summary of Results of Studies						
		Survey Team and Summary of Results of Studies	2-1				
II 2-2	Dam ⁻ Site	Topomphy .	2 . 3				
	II 2-2-1	Topography	2-3				
	II 2-2-2	Topography Stratigraphy Geologic Structure	2-4				
	II 2-2-3	Geologic Structure	2-6				
II 2-3	Reservoi	Geologic Structure	2-7				
	II 2-3-1	Topography	2-7				
	II 2-3-2	Stratigraphy	2-7				
		Geologic Structure					
II 2-4	Permeabi	lity Test and Water Pressure Test	2-12				
II 2-5	Explanation of the Geologic Log of Drill Hole						
	II 2-5-1	Core Recovery	2-13				
	II 2-5-2	Size of Core and Kind of Bit	2-13				
	II 2-5-3	Classification of Characteristics of Rock Shown in					
		Log Sheet of Core Boring	2-13				

		Table				۶
-						
2-1 List of I	Drill Hole			••••••	2-15	
				* v	•	
				•	ı	٩
		-	-	•		•
		Figures				
				~		
- ,				y w		
2-1-II 2-55	Geologic Log	of Drill Hole	• •		2-16	
	• .	3				
		aph of Thin Section	on		2-44	
		aph of Thin Secti	on		2-44	
		aph of Thin Secti	on	· · · · · · · · · · · · · · · · · · ·	2-44	•
		aph of Thin Secti	on	· · · · · · · · · · · · · · · · · · ·	2-44	• -
		aph of Thin Section	on		2-44	• • •
		aph of Thin Section	on	· · · · · · · · · · · · · · · · · · ·	2-44	•
		aph of Thin Section	on	· · · · · · · · · · · · · · · · · · ·	2-44	•
2-56II 2-59`		aph of Thin Section	on	ч , , , , , , , , , , , , , , , , , , ,	2-44	

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II 2 GEOLOGY

2.1 INTRODUCTION

2.1.1 Geology Studies Performed by the DSI

The geological studies concerning Kilickaya Dam were performed in 1967 by the DSI as follows:

A. Reservoir Area

Geologic mapping based on photogrammetrical topographic maps on the scale of 1/5,000 and 1/25,000.

- B. Dam Site
- a. Geologic mapping based on surveyed map on the scale of 1/1,000.
- b. Drilling 1,031m in total length in 16 holes
- c. Permeability test performed on drill holes (1.5 m long each) in the river deposits.
- d. Water pressure test performed drill holes (2m long each) in the rocks.
- e. Measurement of underground water table.... performed on all drill hole for the period up to December 16, 1967,

Drilling works were peroformed by engineers and operators of the DSI by using mainly NX size. High core recovery performed shows that their technical skill is excellent The drill cores are arranged in core boxes and kept in a storage in the suburbs of Samsun. Permeability test and water pressure test were proved successful, as mentioned below, to show the permeabilities of the river deposit and rock.

Geologic survey and core observation were performed by Mr. Gungor Syin, a geologist of the DSI. The results of these studies are contained in the report titled "Engineering Geology Planning Report of KILICKAYA DAM of Kelkit—Karatas Project", together with the geologic map and the log of drill hole. The report is an excellent and laborious work concerning the engineering geology of the dam site and the reservoir area.

2.1.2 Geologic Studies Performed by the Japanese Government Survey Team and Summary of the Results of the Studies. The Japanese Survey Team made geologic studies of the dam site and the reservoir area, and observation of all drill cores. It also performed a close study on the geologic data prepared by the DSI. It tried to make geologic interpretation by aerial photographs of the project area, but, unfortunately no such photographs were made available to the team.

The general topographic and geologic features of the project area are described in Volume I, 3-4, and engineering geologic explanations on the project structures and reservoir are given in Volume I, 7-3. Therefore, in this chapter, geologic features of the dam site and the reservoir area are given, and geologic log of drill holes and the photomicrographs covering thin section of rocks are attached.

The engineering judgment on the geology of the project is summarized as follows: Dam Site:

A. In the riverbed a deposit of gravel exists which is 31.5m in thickness. This deposit must be excavated and taken away from the place where the impervious core is to be founded. No excavation is necessary at the place where rockfill part is to rest.

B. Almost all the rock foundations are altered trachy andesite. The rocks which are heavily altered have tendency to be easily decomposed by water saturation. However, such altered portions are limited, and generally speaking, including heavily altered portions, it has enough stability as the foundation of the dam.

C. Weathering of foundation rocks is considerably heavy in the area from the riverside to the skirts of a hill on the right bank. In other area, the rock which has enough stability as dam foundation can be reached by excavation of about 2m in depth.

D. At the elevation of about 830m on the right bank of the river, there is a fault with a strike parallel to the river and having a dip of 65[°] to the mountain side. The fault has 5cm-wide openings produces of spring water. Therefore grouting is necessary in the fault part.

E. The foundation rock around the site has generally high water tightness. Accordingly, numbers of grouting holes and amount of injection necessiated will be less than in ordinary cases.

Appurtenant Structures:

A. Drilling is necessary to find thickness of talus deposits distributed at the areas where the power station and the switch-yard are proposed.

B. Concrete placing is necessary for the spillway and penstock line.

C. There will be no substantial problems in the excavation of diversion tunnel. Support works will be required only for limited portions. Sections where concrete lining is needed will be very few in consideration of geologic conditions.

Reservoir Site:

A. There is no topographical or geologic factors which suggests possible leakage from the reservoir.

B. As for the landslides which generally occur in the Tertiary group, further studies and observation are necessary. However, there is almost no fear of large and rapid landslides which may endanger the dam.

2.2 DAM SITE

2.2.1 Topography

The Kelkit river flows in the general direction from east to west, but, as it bends sharply at upstream and downstream of the dam axis, in the dam site area it flows in the direction from SSE to NNW. Each bank of the river facing the bending projects in the form of a peninsula. The elevation of the riverbed at the dam axis is 752m and the elevations of the ridges of the hills in both abutments are about 990m. On the left bank of the river at about 130m upstream of the dam axis, and on the right bank, at about 200m downstream, there are marshes of considerable coverage, respectively. The slope of the mountain has a number of creases. The slope is generally steep, and except for the talus deposits at the foot of the mountain the average gradient of the slope at the dam axis is 350 on the left bank and 40° on the right bank respectively. On the left bank above the elevation of 1,000m the slope is gentle. The width of the river is about 50m in the river-course and the valley is about 400m wide at the elevation of 850m. The section of the valley is very similar to that of a vessal's bottom in shape.

The density of plants near the dam site is, very poor due to extensive outcrop of rocks and dry climate. On a part of the riverside a small number of poplartrees are growing. On the mountain slope a few grasses and shrubs grow scattered.

2.2.2 Stratigraphy

The rocks around the dam site are mainly trachyandesites, and augite porphyrites intrudes at some parts. Above the elevations of 1,020m on the left bank of the river, the oligo-miocen strata are extensively distributed. Between these strata and trachyandsite, agglomerate and tuffs of 20-40M in thickness are distributed almost horizontally. But they will have no direct influence to the dam as the high water level of the reservoir is designed to be 850m in elevation and does not reach the elevations. The top soil of the mountain slope is thin. On the foot of the mountain there are rather thick talus deposits. The river channel is covered with gravel of 31.5m in thickness.

A. Top Soil and Talus Deposits

On the mountain side slope above elevation 770m on the left bank and 765m on the right bank of the dam axis rocks are exposed, and talus deposited below the elevations on the river side slope. The thickness of talus deposits at the drill spots are, on the left bank SK 2 (EL. 762.09m, vertical hole) 12.6m and on the right bank SK-M10 (EL 764.35m, 70° as to mountain side) 10.0m. At the marshes located at 130m upstream from the dam axis on the left bank and at 200m downstream on the right bank, there are large volume of talus deposits.

Talus deposits are generally composed of large and small blocks, though those at the upstream on the left bank are composed of more of soil ingredent and less blocks.

B. River Deposit

Drilling was performed at 7 spots in total at the river bed including 5 spots (SK-3, 4, 5, 6, 7) crossing the river at about 50m upstream of the dam axis, 1 spot (SK-8) at 80m downstream and 1 spot (SK-9) at 120 upstream. The depth of gravel deposit at each spot is, in numerical order from SK-3 to SK-9, as follows:

28,75m, 28.75m, 31.50m, 29,00m, 25.60m, 29.50m, 29;40m.

These gravel are almost all composed of volcanics, rarely including limestones. All the pebbles are hard.

As it is difficult to lift sand and pebbles by drilling from river deposits, exact composition of grain size can not be known. The core recovery of the river deposit at this site is less than 40%. Core observation shows that diameters of pebbles are mostly 5-10cm and rarely 20-50cm. The majority of big boulders are limestones. Judging from the feeling of drillers at drilling work, it is believed that the ratio of sand and silt is small and that they are not distributed in layers. The standard penetration test was performed. But no exact value was obtained as there existed too much gravel.

C. Trachyandesite

The dam foundation is generally composed of trachyandesite, augite trachyandesite distributed at a part of upstream area on the right bank.

The trachyands has rentirely been subjected to hydrothermal alteration. The degree of alteration varies according to locations. Colors of rocks are also multy-dark greenish gray, purplish red, light green, yellowish grey, etc. mixed finely together. Agglomeratic or flow structures are seen in part.

They are generally massive and have cracks. They can be broken with heavy strikes by a hammer. The heavily altered part has smaller specific gravity and its texture is porous. Among the drill cores which are recovered in the form of a stick, there are some which easily get disintegrated in water. The length of drill core is generally about 20cm, but on some occasion it is as long as 50cm. At deeper part cut plane of core is fresh and not stained by limestone. Some thin cracks are filled with secondary calcite.

The results of microscopic observation on this rock are given in Fig. II-2-56 and 57. Judging from the rock component minerals and texture it is rather akin to porphyrite. However, naming of the rock in this report follows in the previous reports.

D. Augite Porphyrite

Augite porphyrites are distributed extensively around the ridge of the hill which projects in the form of a peninsula on the right bank of the river at about 300m upstream from the dam axis. On the left bank, they are distributed over the from 150m to 200m upstream of the dam axis and at the elevations ranging from 860m to 930m. The dyke rocks of 2m in width existing near the intake site of the spillway on the left bank and the rock at the dam axis on the right bank is found to be augite porphyrites as the result of microscopic observation.

The rock has a porphyritic texture with dark gray color, its groundmass being a little glassy. A part of the mafic phenocrysts composed of augite, hornblend, biotite, etc. is replaced by calcite and chlorite. The rock is so hard that it is difficult to break it with heavy strike of hammer. When broken, it forms sharp edges. Columnar joints are seen on the rocks in the aforementioned rock mass of the right bank of the river. The results of microscopic observation are given in Fig. II-2-58 and 59. Among trachy andesites, mentioned in the preceding paragraph, those slightly altered ones are, as the result of microscopic observation, found to have strong resemblance to this augite porphyrite.

2.2.3 Geologic Structure

At the dam site, there are one or two small faults or open cracks, but no such one is found which might become obstacle to the project.

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A. Fault

In the vicinity of the dam site, a fault exists on the bank, of the river. The fault on the left bank is a small having a crashed zone of 20cm in width filled with secondary lime. Since this fault is located at an elevation of 880m and at about 200m upstream of the dam site, it has no direct influence over the project.

The fault on the right bank is at an elevation of about 830m. The fault continues upward for 80m from about 50m upstream of the dam axis. This fault has a strike parallel with the river (N 10° W) and a dip of 65° to the hillside. In some places, openings of about 5cm in width can be seen on outcrops. It seems like a fissure rather than a fault. KS 16 crosses this fault at 49m under the ground. Water still flows out of the drill hole.

B. Crack and Joint

Flow structure is seen on a part of trachyandesite and columnar joint on a part of augite porphyrite. Both of them have many cracks and joints. Judging from drill core observation, made, these cracks are mostly closed or dilled with calcite veins in the under ground though they have some openings at the surface of the earth.

At 100m downstream of the axis on the left bank and about 40m upstream of outlet site of the diversion tunnel, there are continuous open crocks running along the creases of the mountain. The width of opening of the former is 3cm and the latter 10cm.

2.3 RESERVOIR AREA

2.3.1 Topography

The Kelkit Reservoir lies along the main course of the Kelkit river and its tributaries including the Cat, Darubul, Karahisar, Degirmen and Susehri rivers. The Suschri River flows at 7.5Km south of the dam site from west to east. The Kelkit river in the section of 8km long at the upstream of proposed dam flows east to west. The reservoir will be formed in the shape of the letter U and has an opening to west, connecting both rivers. Between the two rivers, the Eyme Mountains (Elevation 1,500–1,600m) composed of limestones and ophiolitic series lie expanding east to west with a width of about 7.5km.

On both banks of the Kelkit river between the dam site and about 7.5km upstream, volcanic rocks crop out and the slopes are steep. However, higher than an elevation of 1,000m on the left bank, strata of oligo-miocene series are distributed and the slope is gentle. The Cat river flows from north to south through volcanic rocks and joins the Kelkit river in its right bank at about 700m upstream of the dam site. The valley of the Cat forms the shape of in cross, section. The Darabul and Karahisar rivers flow from NEE to SWW and join the Kelkit from the right bank at about 10km and 15km upstream of the dam site, respectively. Around each junction, an extensive alluvial plain is formed. These two tributaries and upper course of the Kelkit, flow through the oligo-miocene strata. They have wide valleys and gentle sloped mountains surrounding them. In the east of the junction of the Darabul and Kelkit, Dumatasi Mountain (elevation=2,740m) composed fo volcanic rock of 1.5km in diameter rises in the shape of a dome.

The Degirmen and Susehri rivers flow through the flat land. The proposed reservoir will be along these rivers in a width of about 3km.

In the vicinity of the reservoir, there is no saddle-like topography which may cause leakage from the reservoir.

2.3.2 Stratigraphy

The strata distributed in the reservoir area are, in chronological order, as follows:

Recent	Top soil and Talus deposit
· .	River deposit
Quaternary	River tarrace deposit
Tertiary (oligo –MioPliocene)	Sedimentary rocks
Upper Cretaceous	Volcanic facies (A part may possibly be Eocene)
	Flysch facies
	Limestone facies
	 Ophiolitic facies

A. Top Soil and Talus Deposit

The topography of the area where limestone, flysch facies and volcanics are distributed is steep. On the slope, rocks are exposed. While on the foot of the mountain, a thick talus is deposited. The topography of the area, which occupies a major part of the reservoir area and distributed by Tertiary system, is gentle and the surface of the earth is covered with a thick layer of residual soil.

In the DWG RESERVOIR AREA, GEOLOGIC PLAN, no particular descriptions are made concerning the surface soil. Regarding the talus deposit, only those places including the foot of the Eyme Mountains and the vicinity of the Damatasi mountain where the deposit is thick and extensive, are shown.

B. River Deposit and River Tarrace Deposit

The river terrace deposits are seen on the left bank of the Susehri river and the right bank of the Karabisar river. They are composed of silt, sand and gravel.

The river deposit occupies major parts of the Suschri Plain and also covers the riverbeds of the Kelkit and its tributaries. There are no rock bed exposed on these riverbeds. At the up and down parts of the dam site, there are widely spreading flood plane deposits which are exposed above the water level, except in case of flood. At the junction of the Kelkit and the Darabul at 6.5km upstream of the dam site, the width of the river reaches 750m. According to the drillings performed on the central spot of the river at the dam site, the depth of river deposit is about 30m. Sand and gravel on the river channel of these areas will be used as materials for concrete aggregate and filter of rock fill dam.

According to the grain size analysis, the composition of the deposits is less than 10% of silt or clay, 30-40% of sand and 60-70% of gravel. The largest diameter of gravel is about 30cm. The percentage of gravel larger than 12.5cm in diameter is less than 10%. These pebbles mainly consist of volcanic rocks and, in rate cases, of limestones. They are very hard.

C. Oligo-Mio-Pleiocene Sedimentary Rocks

The rocks which occupies a larger part of the reservoir area is that of tertiary sedimentary rocks. The covering area of the proposed reservoir is generally tertiary system. However, the area extending for about 6km upstream from the dam site are mainly compose of volconics and in the eastern end of the Eyme mountains are distributed ophiolitic facies and limestones. Though the exact epoch of the Tertiary system is not known, judging from the fact that it partially contains gypsum and lignite and from its rock facies, we can correlate with other area in Turkey. It is believed that the major part of it belongs to Oligo-Miocene.

In the conglomerate distributed on the left bank of the Kelkit river near the back water of the reservoir, fossils representing the Pliocene are often found. But, as there is only few outcrops, the area of distribution is not determined.

Oligo-Miocene strata is composed of alternation of conglomerates, sandstone and shales. Pebbles in conglomerates are mostly those of round shaped volcanic rocks of less than 10cm in diameter.

The matrix of conglomerates and sandstone contain a large quantity of fragments of quartz and lesser quantity of heldspar, hornblende, mica and chlorite. As the cement material, a large volume of limy material is contained. Infiltration of limonite is seen. On the right bank of the river and at 6–7km upstream of the dam site, some hard sandstones of reddish color are distributed. Sand stones distributed in other area are generally easily broken by heavy strokes of hammer. The strata have been folded. The dips of the strata are, though some spot shown degree of 50° , generally less than 20° .

The topography of the area where Tertiary system is distributed is generally gentle and the ground is covered with thick layer of residual soil made by weathering. Wheat cultivation is extensively practiced in the area. Exposed strata can be seen only at along some marshes which lie on the riverside or slopes. There are some places where cliffs of about 10m in height are formed due to erosion of river water. Those cliffs make the slopes unstabilized and causes landslides in various places. The thick layer of residual soil and the loosened strata are another cause of landslides.

D. Volcanic Rocks

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Volcanic rocks are distributed at the following 4 places in the project area.

a. On both banks of the Kelkit river between about 5km upstream and 4km downstream of the dam site.

b. Dome shaped huge mass of rocks of 1.5km in diameter rising on the right bank of the Kelkit river at 8km east of the dam site.

c. A mass of rocks extending for 6km east to west and 1km south to north distributed on the southwest slope of the Eyme mountain.

d. The mountain at the southern part of the Susehri plain.

These places are mostly located higher than the high water level of reservoir, and there^{-1 +} fore, they have no direct influence over the project. In "a" area; outcrop expands continuousely to north on the right bank of the river, but on the left bank above the elevation of 1,000m, volcanics are covered by Oligo-Miocene strata. It is said that volcanics in this region were made by volcanic activities in the Upper Cretaceous and the eocene epochs. "a" and "c" areas are considered to belong to the Upper Cretaceous and "b" and "d" belong mainly to the eocene, though not proved.

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In "a" area, trachy andesite, augite porphyrite, basalt, agglomerate and dyke rocks are distributed intricately. Augite porphyrite and dyke rocks seem to have intruded in the cocene epoch. As for Trachyandesites and augite porphyrites which are distributed at the dam site, descriptions were made before. The characteristics of them are that the former has strong hydrothermal alteration and the latter is nearly fresh and head. In this area trachy andesites are distributed rather extensively. At the upper parts of the Cat river and the Kelkit river, agglomerates and tuffs are distributed.

On the left bank of the river, at 3km downstream of the dam site, olivine basalt are distributed. On the left bank of the dam site, at an elevation of 1,000m, tuffs and agglomerate are distributed in 20m thickness covering trachy andesites.

These volcanic rocks are generally hard, but heavily altered portions, though very limited, are easily disintegrated when saturated with water. Generally speaking the area volcanic rock is distributed has steep slopes and rocks are exposed all over the slopes. Talus deposits are seen on the skirt of the slope.

E. Flysch Facies

Flysch facies are distributed at two places separately; on both banks of the river at about 6km upstream of the dam site and in the north slope of the Eyme mountain. In the former case distribution is mainly below the proposed high water level and is rather limited. Distribution of flysch facies in the slope of the mountan is very extensive above an elevation of 1,000m. Flysch facies are the stratified rocks composed of marl, limestone, sandstone and conglomerate alternation. Judging from the fossils of Hippuretes contained in flysch facies, it is considered that sedimentation was made on the shallow sea of the latter geosyncline of upper Cretaceous. The strata are hard, but have many cracks and are easily broken.

F. Limestone

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Concerning the limestones in this area, there are small masses in the ophiolitic facies and the strata which is distributed extensively to from the main body of the Eyme mountains. At the north slopes of the Eyme mountains, basal limestone is covered by Oligo-Miocene strata and crops out sporadically. This limestone can be found at the proposed reservoir area near the eastern end of the mountains. It is covered by a thick talus deposits.

The limestone is crystallized in some parts, and is solid and hard. The beddings of 5-25 cm spaces are developed, with many foldings and cracks. In a village to southeast of the dam site, water comes flowing from the limestone layer. No limestone cave is found.

G. Ophiolitic Facies

Ophiolitic facies is a name of serpentiniferous mesozoic complex. In this area, it constitutes the main body of the east half of the Eyme mountains. It further extends to east and reaches at the right bank of the Kelkit river near its junction with the Susehri river. As the south and north foots of the Eyme mountain are covered with the latter formation, the direct relation between the ophiolitic facies with the reservoir is seen only at the section where the Kelkit flows from south to north at the east end of the Eyme mountain. It includes the section between the junction with the Susehri river and about 2.5km downstream from it on the left side and the section of about 2km upstream and downstream from the junction on the right bank.

Ophiolitic facies distributed in this area belong to the upper Cretaceous. It was formed when basic or ultra basic rock effused or intruded in the geosynclinal sea-bed and caught the crystalline limestones and radiolarian cherts. As the intrusive rocks, there are serpentine, gabbro, diabase and spilite. Some of the radiolarian cherts have a trend of NW-SE. Generally speaking, the strata are disturbed and the rocks have many cracks and are highly weathered.

2.3.3 Geologic Structure

Project area locates in Alps-Himalayar Orogenic Zone, and those sedimentary rocks and volcanic rocks which belong to different epochs are distributed complicatedly. Affected by repeated orogenic movements, the strata are strongly folded and heavily faulted.

Ophiolitic facies, limestone and flysch facies which belong to upper Cretaceous are hardly disturbed. Details of the structure of Oligo-Miocene group can not be known since there are little outcrops found. Strikes and dips of strata differ area to area, showing a complex geologic structure. It seems that the whole area is controled by folding axis of east to west direction.

The Kelkit fault, which run in the direction of NWW-SEE at 7-8km south of the dam site, extends downstream along the river for about 15km downstream of the dam site. It is a large scale tectonic line. In the Eyme mountains, at the area where limestone and flysch facies are distributed, there are some topography which seem to be fault-scarps in paralle with the Kelkit fault. In the volcanic rock area, there is no remarkable fault.

2.4 PERMEABILITY TEST AND WATER PRESSURE TEST

A. Permeability Test

Permeability test was performed on all drill holes in the river deposits, in an space interval of 1.5m. A 1.5m-long drive pipe which have 420 holes of 6mm diameter was used in the test. Leakage under some water head was measured 3 times at 5 minutes' interval, that is, 15 minutes in total.

The result of the test shows that the river deposit in this site has a permeability coefficient ranging from 10^{-2} cm/sec to 10^{-3} /sec.

B. Water Pressure Test

The water pressure test was performed on all drill holes at an space interval of 2m to ascertain the water tightness of the foundation rocks. In the test, water was pressured-in between packer and bottom of holls (2m each in length) and measurement was conducted by water meter. Pumping-in pressure applied was 2, 4, 6, 8 and 10 atm., and leakage was measured for 10 minutes under each pressure.

The results of the tests were described in the geological log of drill holes. The Lugeon values which were calculated on the result of the test are given in figures in the geologic log of drill holes and also graphed in the DWG, "....... KILICKAYA DAM, GIOLOGIC SECTION. The Lugeon value shows leakage through of foundation rocks in terms of litres per minute per one meter length of drill hole under a poring pressure of 10 kg/cm². 1 Lugeon corresponds to approximately 1×10^{-5} cm/sec.

The watertightness of foundation rocks in this site was mentioned in Volume I, Chapter 7-3-1-E. They have high watertightness in general. There were no leakage at all throughout the test performed. Even in the cases leakage occured it was mostly less than 10 Lugeon (= 1×10^{-4} cm/sec.).

2.5 EXPLANATION OF THE GEOLOGIC LOG OF DRILL HOLE

2.5.1 Core Recovery

The core recovery is presented in percentage with histogram. Recovered ratio is shown in the histogram by oblique lines.

2.5.2 Size of Core and Kind of Bit

Size of core and kind of bit are shown in the same column, NX and BX mean the size of core, 74.8mm and 59.18mm in diameter, respectively. "D", and "M" are used as the abbreviations of diamond core bit and metal (cemented carbide) bit respectively.

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2.5.3 Classification of characteristics of rock shown in log sheet of core boring

In the sheet, some of the rock characters as observed in the core is classified with numerals from 1 to 5 in accordance with the degree of weathering, hardness and cracking as follows:

A. Degree of Weathering

Numerals

- 1 The rock is very fresh, and the rock forming minerals and grains are neither weathered nor deteriorated.
- 2 The rock is soild. Some of cracks and joints are slightly stained, but lack in veneer of clay or clayey materials. The rock forming minerals and grains are partially sustained with slight weathering and deterioration.
- 3 The rock forming minerals and grains excluding quartz are slightly softened due to weathering. Most of cracks and joints, sometimes rock itself, is tained by limonite, etc., and some of cracks and joints are filled with veneer of clay or clayey materials.
- 4 The rock forming minerals and grains, excluding quartz, are fairly softened by weathering with slight strokes it easely gets broken off along cracks or joints into

pieces of fragments. Among the joints and cracks, veneer of clay and clayey materials exist.

5. Owing to weathering, the rock forming minerals and grains are deteriorated and discolored, and the rock is remarkably softened and loosened.

Some types of rock have been extensively solved to include voids or cavities and their texture vary from impervious to porous.

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In the extreme case, rock has been completely decomposed and its character has been altered to that of soil or earthy materials. In some cases roots of plant have penetrated not only into the cracks and joints but also into the rock itself.

B. Degree of Hardness

The hardness mentioned herein after does not refer to the mineralogical hardness according to MORS scale and SHORE scleroscope, etc., but is concerned with analysis according to engineering geology which includes abrasive resistance, toughness, compression strength, and tensile strength, etc. that are determined by geologists in accordance with engineering judgement of the foundation for structures.

The criteria of harness are as follows:

Criteria

Numerals

- 1. The rock is very hard like granite and greywacke, etc. and fresh. It breaks by strong hammer blow into sharp edged pieces of fragments with sharp fractures.
- 2. The rock is fairly hard, like high quality concrete. It breaks, by strong hammer blow, into pieces of fragments accompanied by some amount of rock power.
- 3. The rock is generally hard, like common concrete, or abrasives. It breaks by hammer blow into pieces or fragments with some amount of rock dust and powder. In this criteria are included rocks whose feature shown hard in most parts and somewhat soft in other parts. The rock is generally soft or weak in cementation, like chalk, tuff, etc. and easily breaks by hammer blow, or sometimes shaped off by hand or can be whittled with a knife.

4. The rock is very soft, like lignite, and it is easily broken with finger squeeze

and can be scratched by finger nail or copper coin. Sometimes the rock is a loose material, like aluvial and glacial soils, owing to the lost of solidity.

Degree of Cracking

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Numerals

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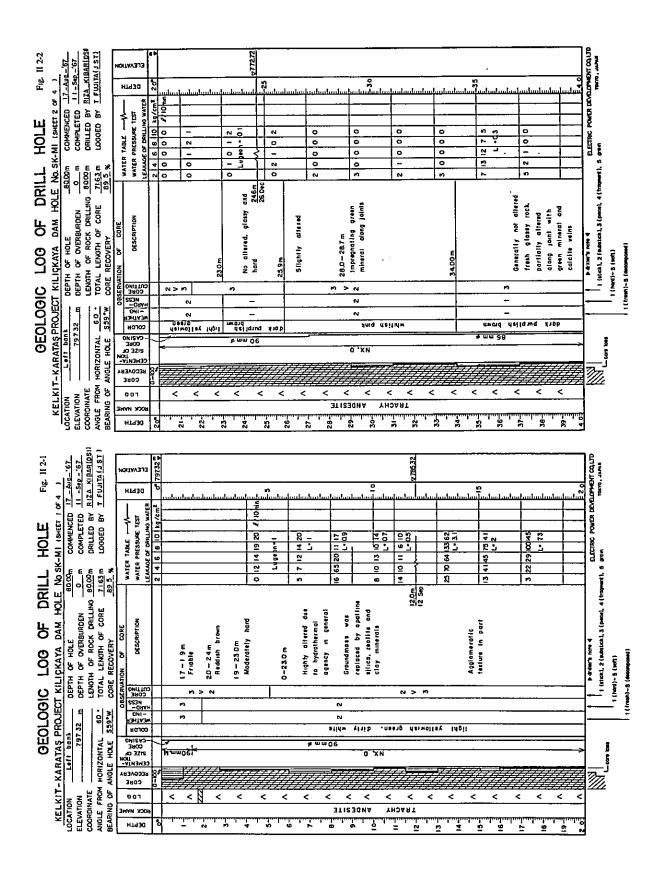
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Criteria

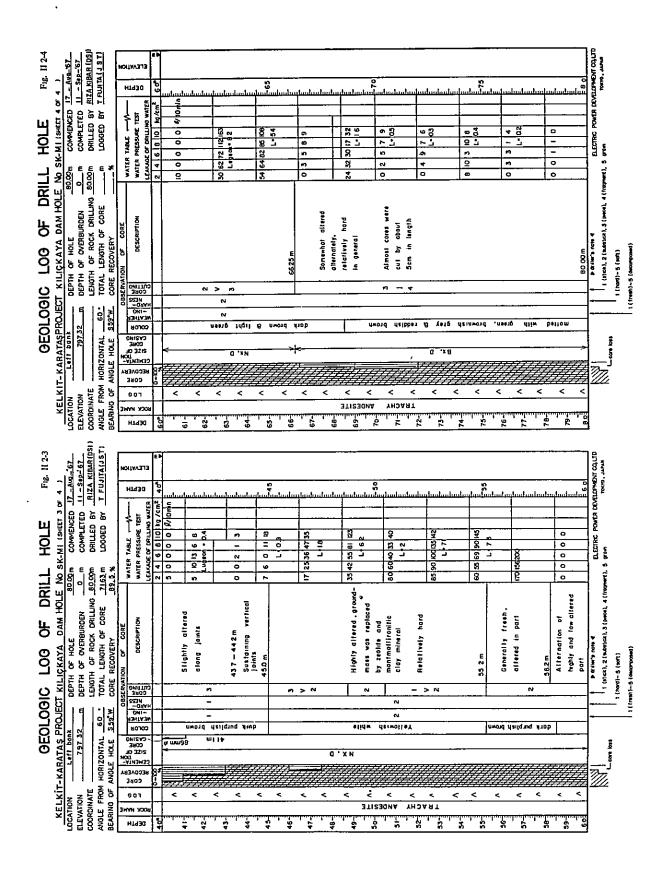
- 1. Cracks and joints are spaced more than 50 cm apart.
- 2. Cracks and joints are spaced 50 to 20 cm apart.
- 3. Cracks and joints are spaced 20 to 50 cm apart.
- 4. Cracks and joints are spaced less than 5 cm apart.
- 5. Cracks and joints are hardly sustained, the cores are broken into chips and grains.

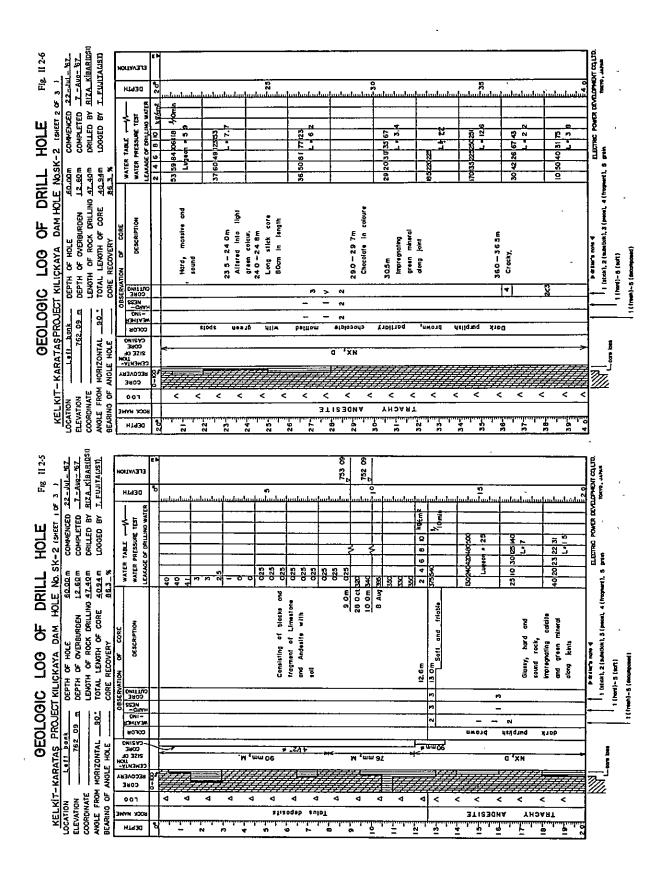
Hole Name	Location	Elevation	Direction of Hole	Depth of Hole	Depth of Over burden (m)		of Core Lengt ill- in Rock Drilling (m)	h Core Re- covery in Rock Drilling(%	Fig. No.
SK-MI	Left bank	797.32	S59 ⁰ W, 60 ⁰	80.00		80,00	71.63	89.5	1- 4
, _2	, n	762.09	Vertical	60.00	12.60	47.40	40.94	86.3	5-7
3	River bed	753.57	11	50.00	28.75	21.25	21.09	99.2	8-10
4	~ H	751.63	*1	50.00	28.75	21.25	18,25	85.1	11-13
5	**	751.66	11	80.00	31.50	48.50	43.32	88.4	14-17
· 6	17	751.54	**	50.00	29.00	21.00	18,55	88.5	18-20
7	11	752.38		50.00	25.00	24,40	19.70	80.8	21-23
8	1)	752.56	F1	60.00	29.50	30.50	29.42	96.0	24-26
9	**	755.00		60.00	29.40	30.60	30.41	99.5	27-29
M10	Right bank	764.35	S75°E, 75°	60.00	10.00	50.00	42.74	85.5	30-32
11	*1	824.82	Vertical	90.00	-	90.00	84.54	94.0	33-37
13	`Left bank	881.14	Ħ	40.00	-	40.00	36.93	86.7	38-39
15	**	838.55	11	76.00	-	76.00	70.80	81.0	40-43
M16	Right bank	820.34	S75°E, 45°	90.00	-	90.00	85.82	95.4	44-48
· 17	Left bank	1,056.00	Vertical	60.00	10.00	50.00	39.37	77.7	49-51
18	"	1,050.00		75.00	24.60	50.40	38.05	75.7	52-55
16 holes		1	,031.00		771.30	691.56	89.6		

Table II 2-1 List of Drill Hole

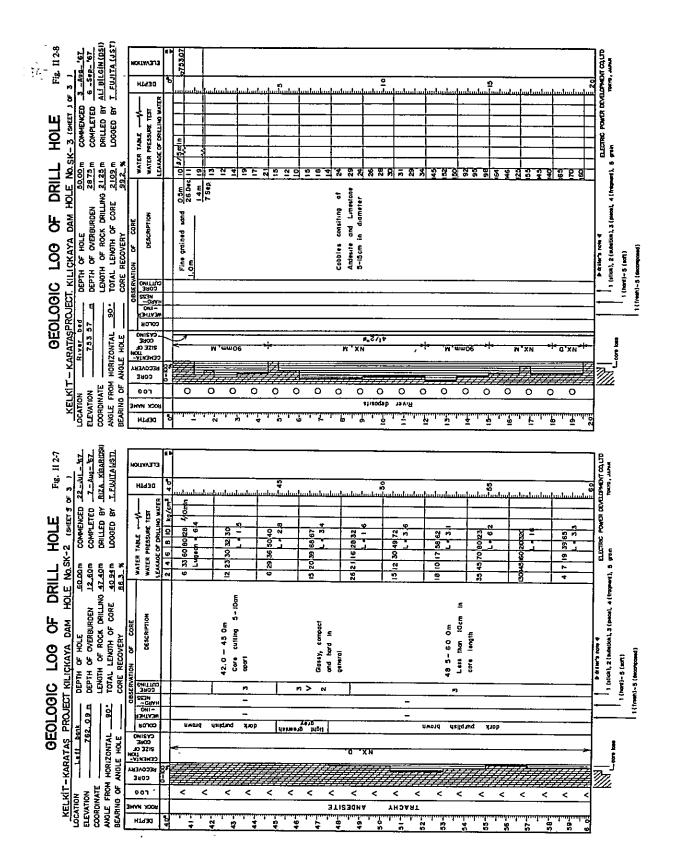






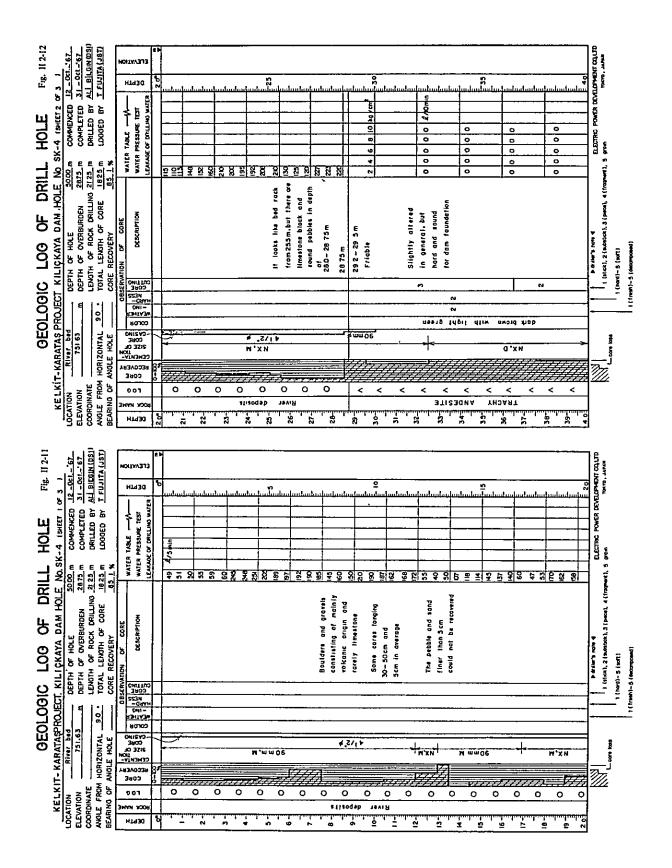


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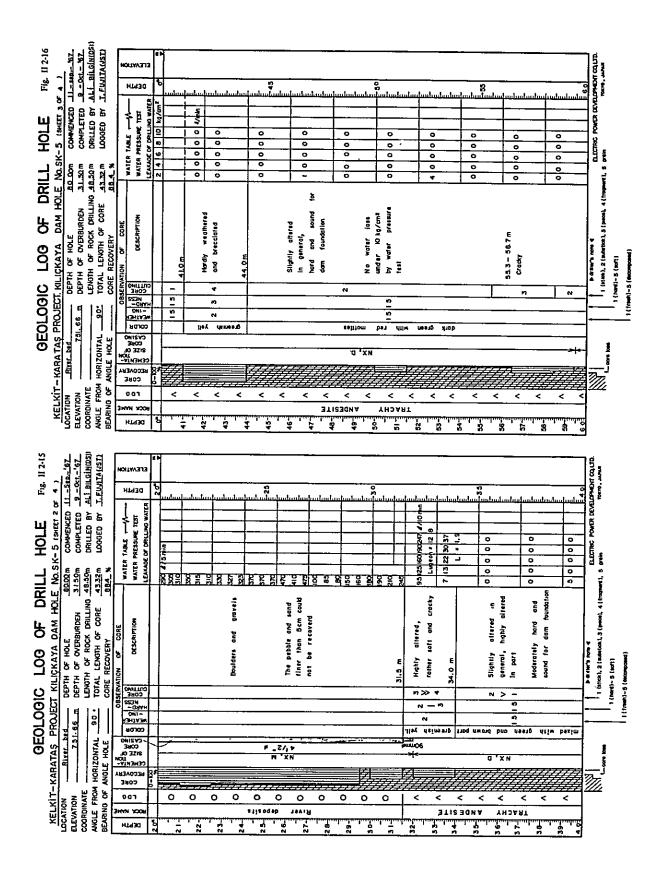


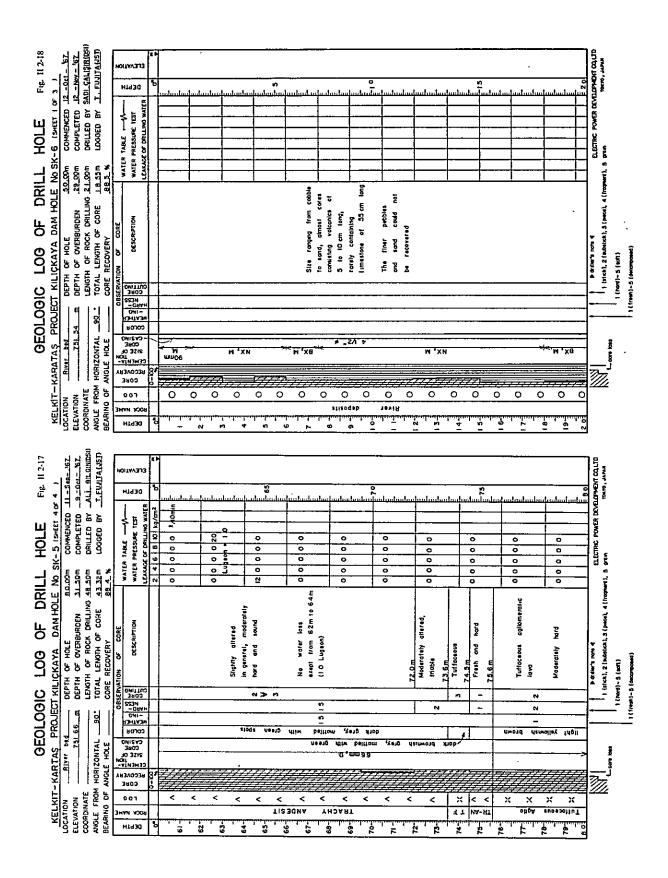
GEOLOGIC LOG OF DRILL HOLE Fig. 11 2-10 XELKIT - KARATAŞ PROJECT KILIÇKAYA DAM HOLE. No SK-3 ISHEET 3 OF 3 J CONTON River bed DEPTH OF HOLE No SK-3 ISHEET 3 OF 3 J CONTON RIVER DAM HOLE. No SK-3 ISHEET 3 OF 3 J CONTON RIVER DAM HOLE. No SK-3 ISHEET 3 OF 3 J CONTON RIVER DAM HOLE. No SK-3 ISHEET 3 OF 3 J CONTON RIVER DAM HOLE. No SK-3 ISHEET 3 OF 3 J CONTON RIVER DAM HOLE. NO SK-3 ISHEET 3 OF 3 J CONTON CONTON TOTAL LENDM OF AND READED CONFILE DAM HOLE D	OBSERVATION OF CORE	Somewhost altered in general, hughly altered and friable for dam foundation. 43.0 - 45.0 m bittle with vertical points. Points. Petimis nee 4. (1990), 4.(1990), 4.(1990), 4.(1990), 1-5.(1981), 2.(1990), 4.(1900), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1900), 4.(1900), 4.(1900), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1900), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1900), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(19900), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(1990), 4.(19900), 4.(1990), 4.(19900), 4.(19900), 4.(19900), 4.(19900), 4.(19900), 4.(199	1 (fresh)-5 (decomposed)
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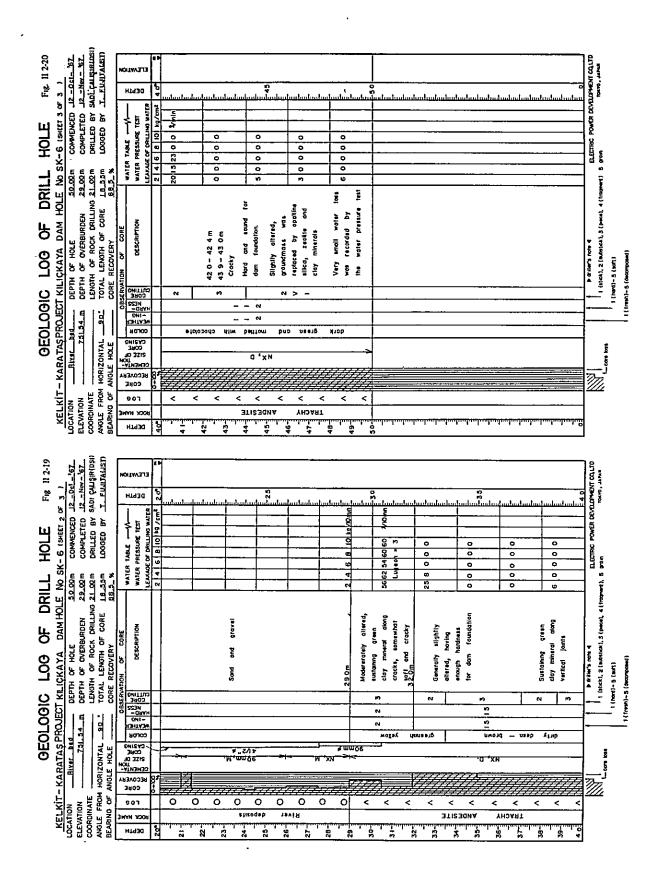
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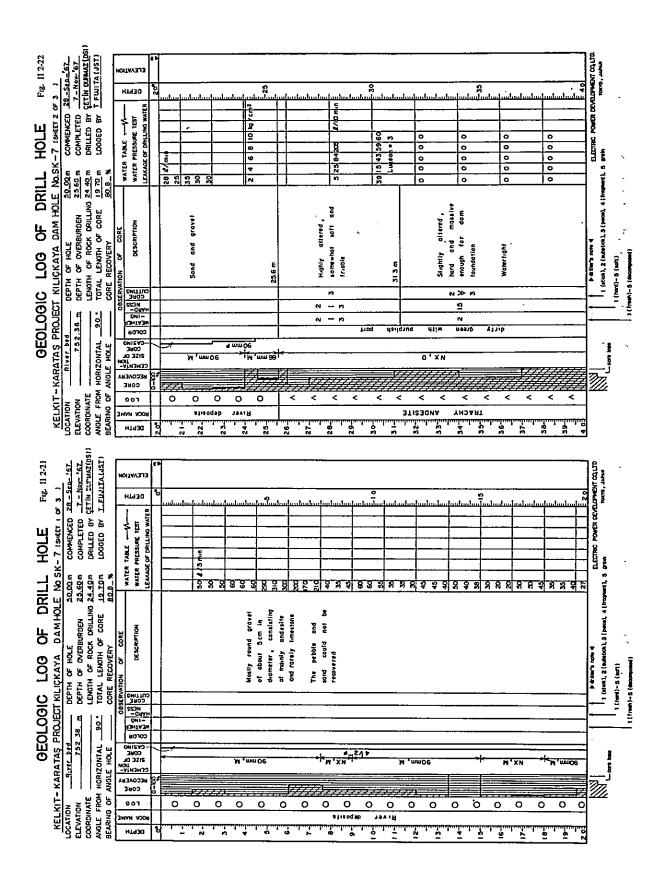


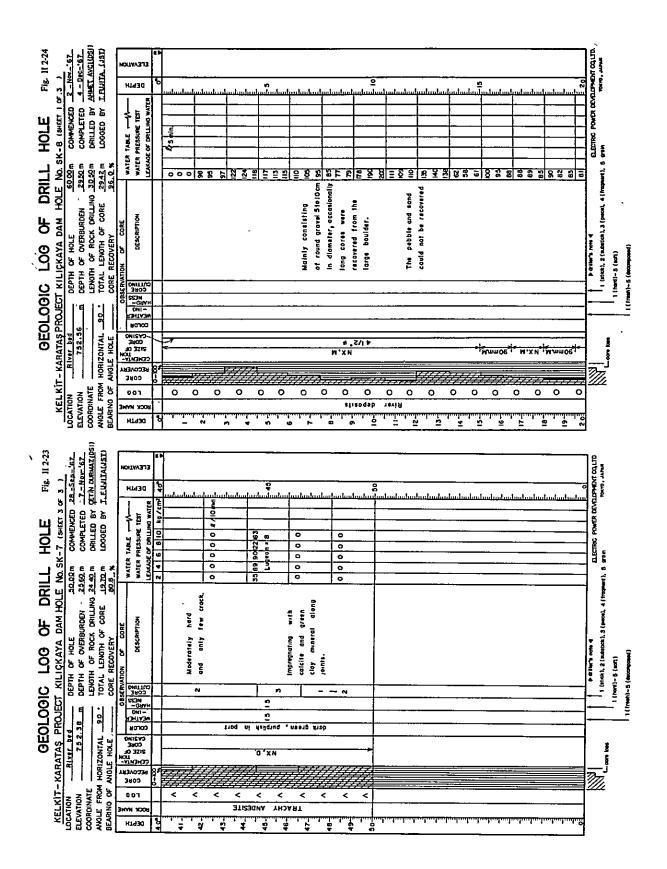
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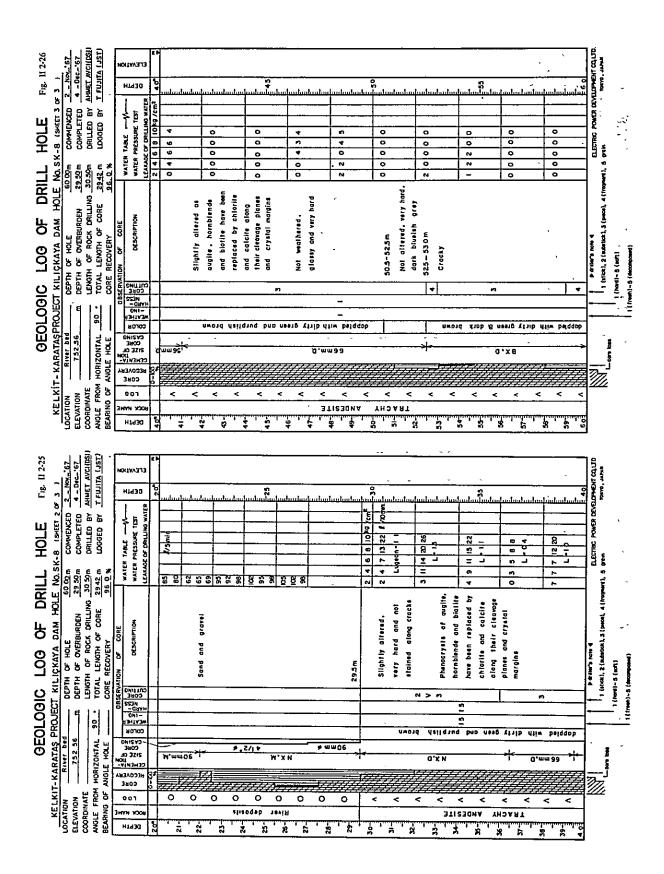




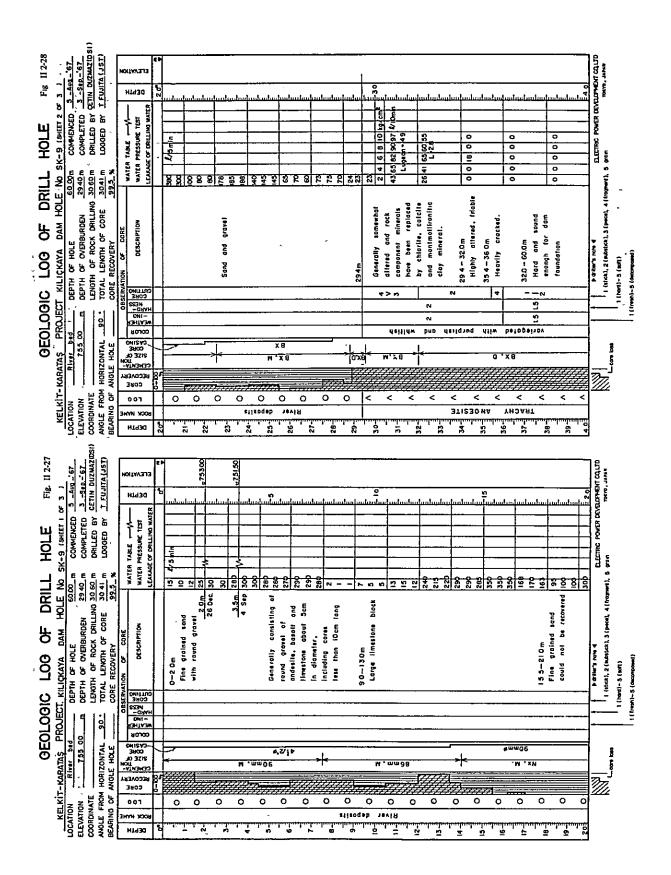




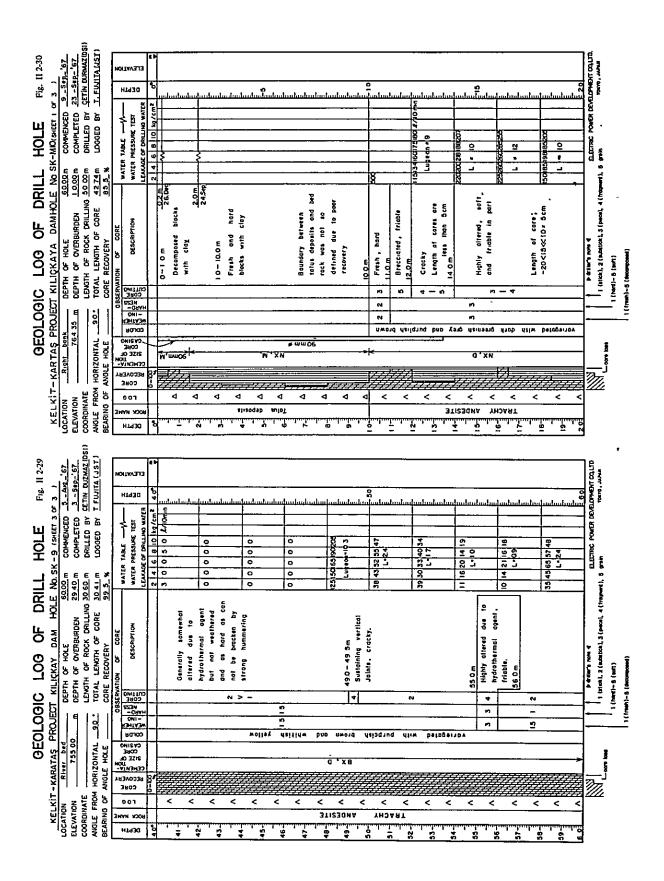


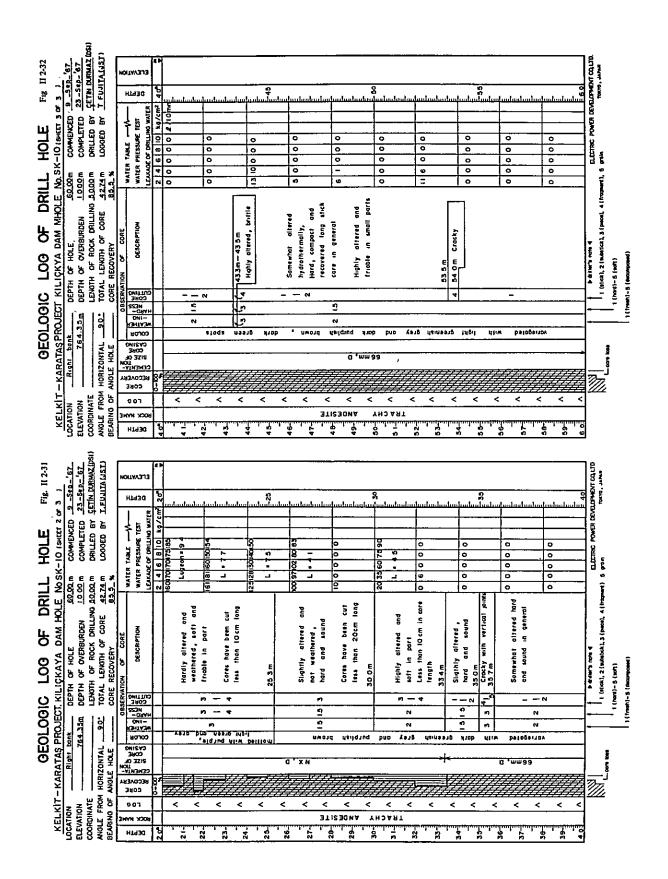


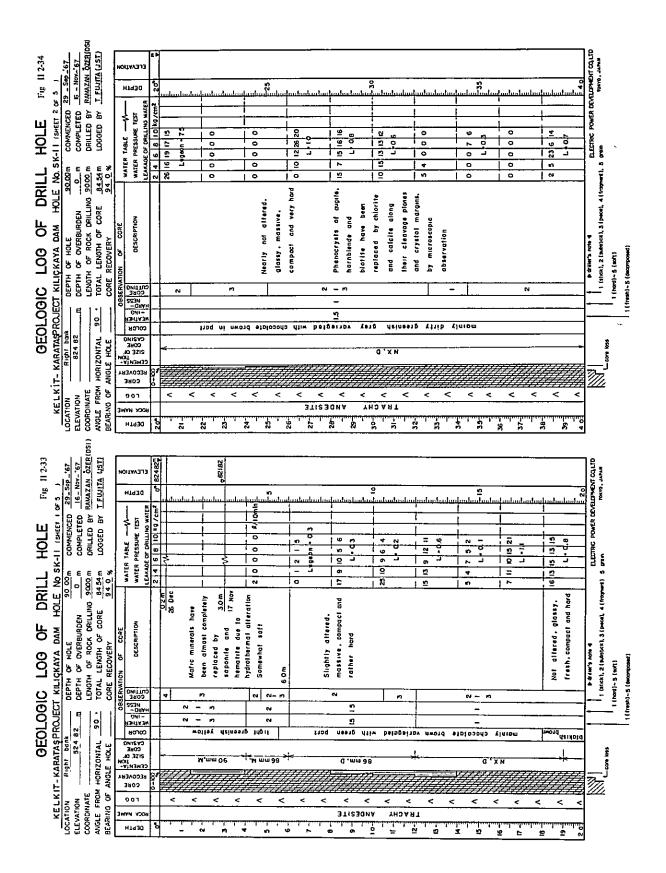
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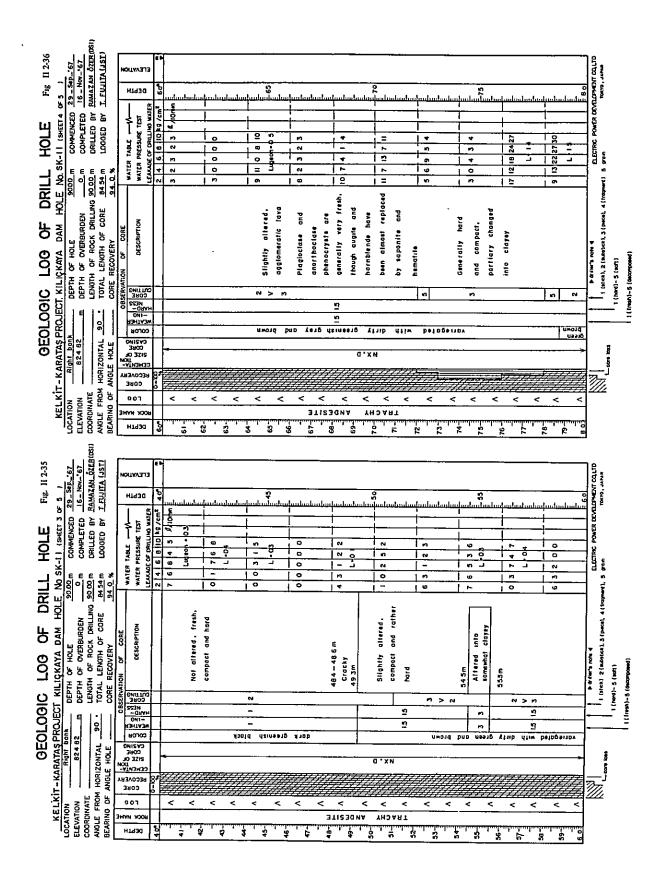


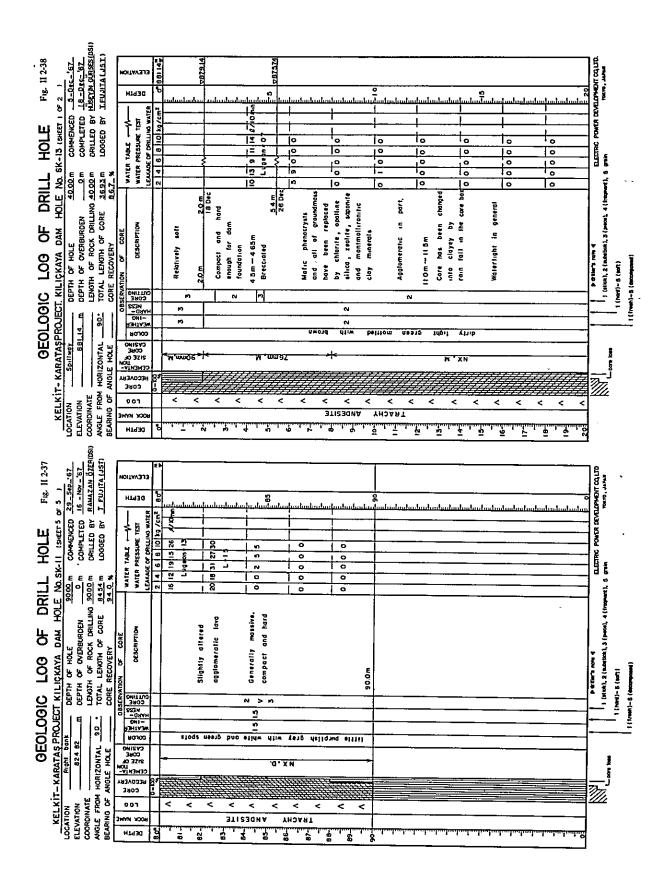
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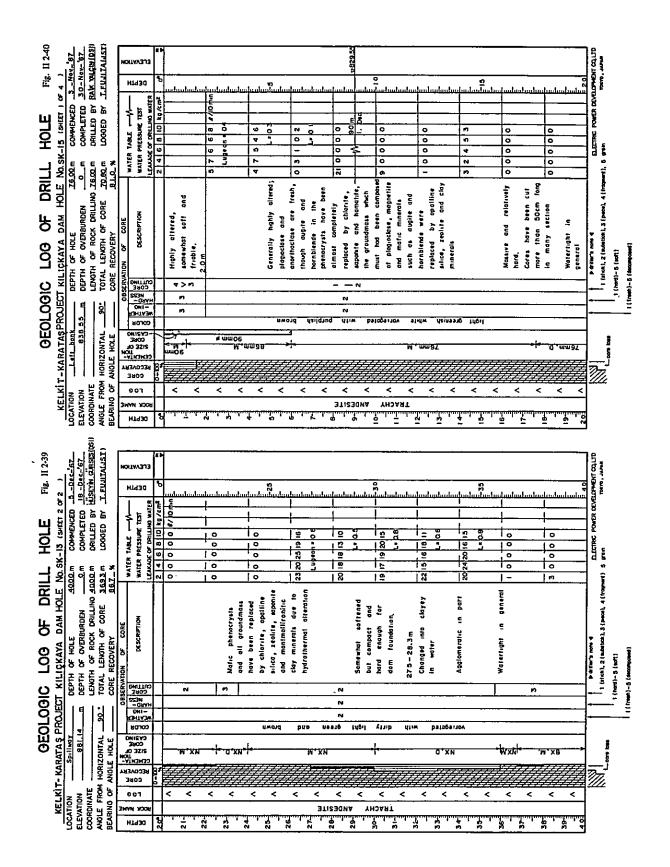


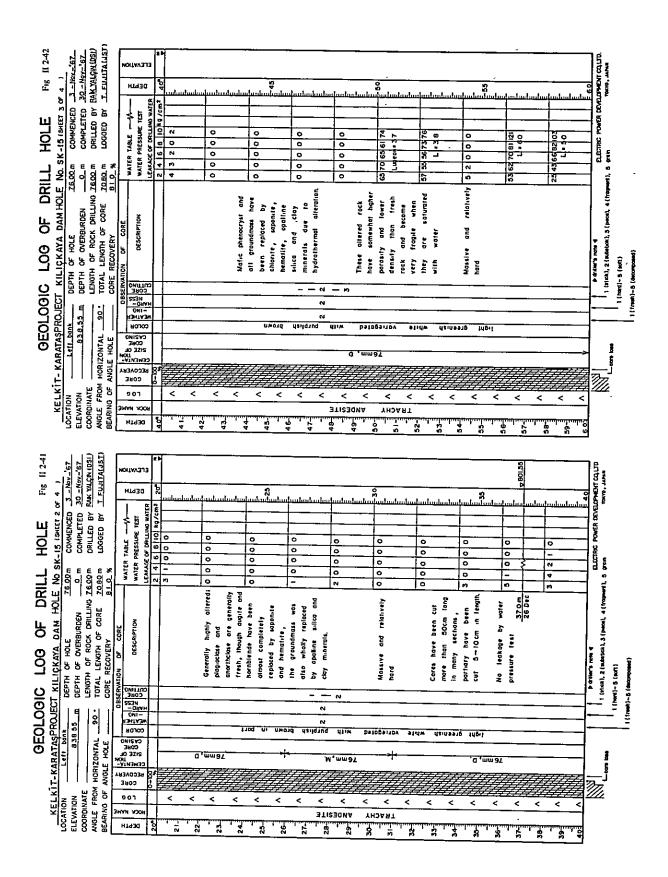


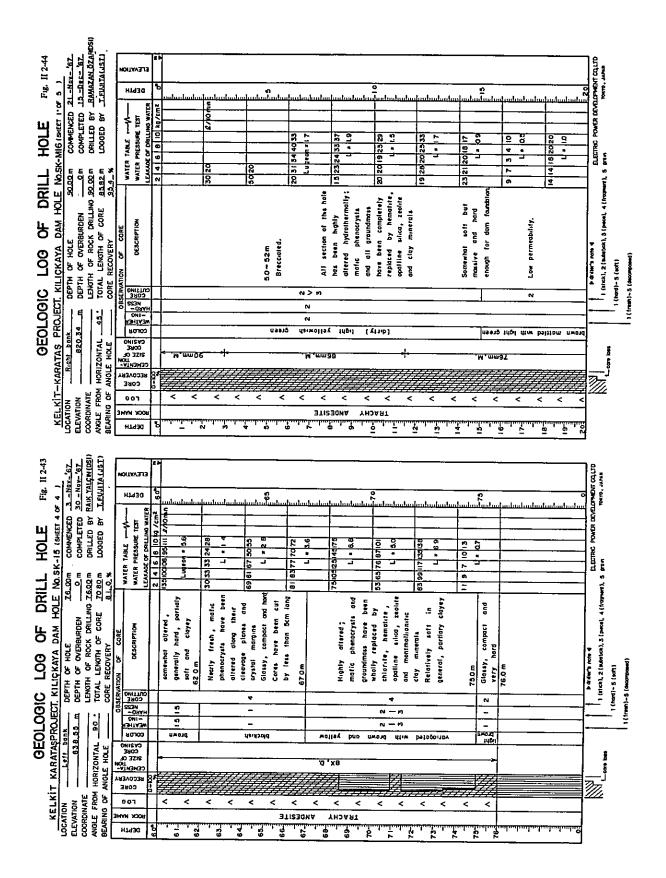


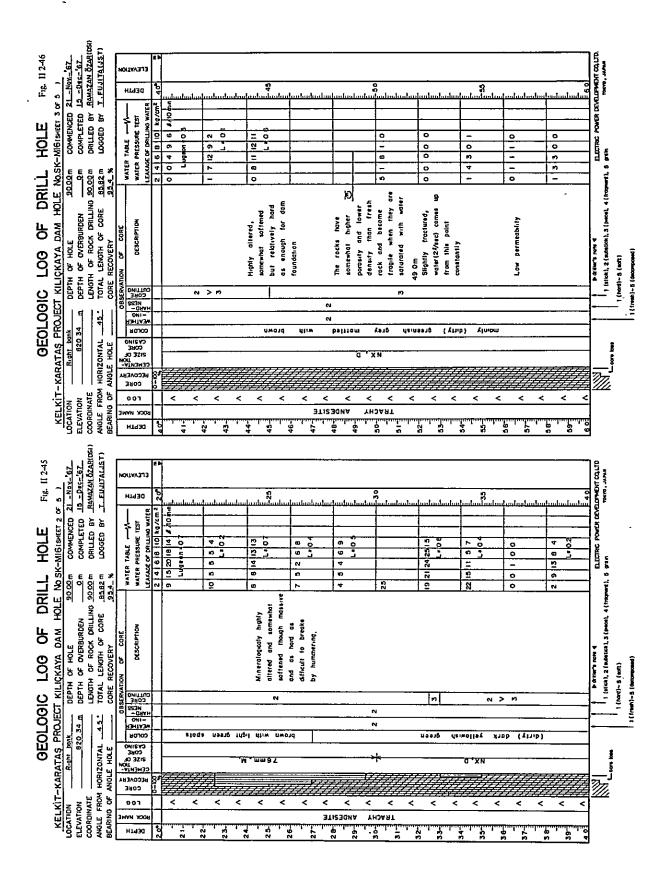




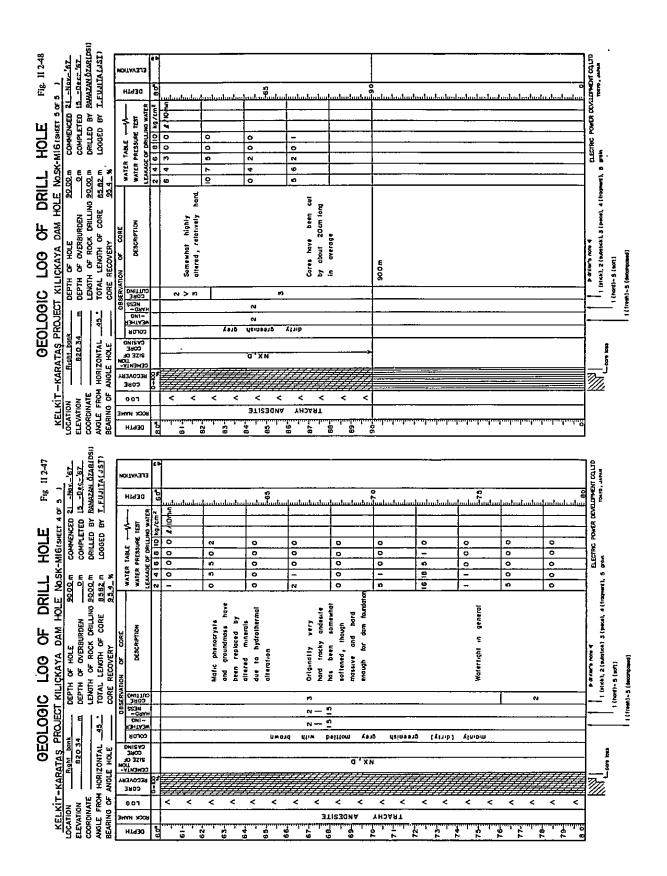


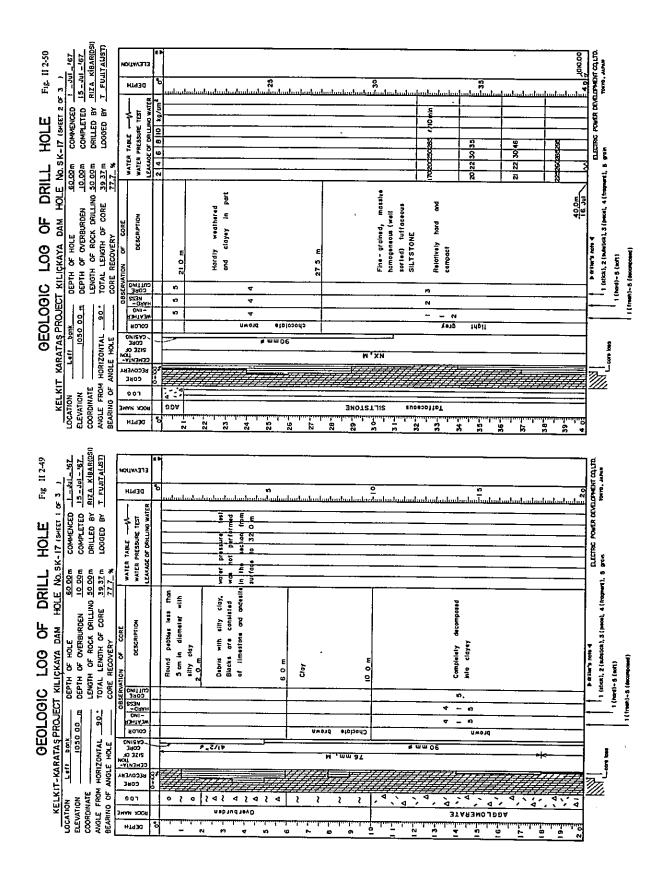


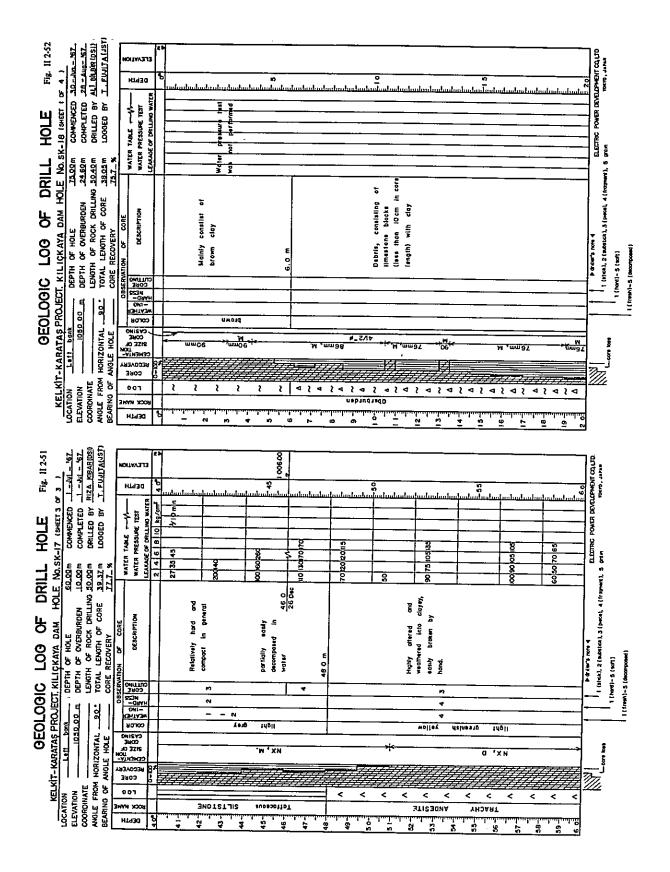


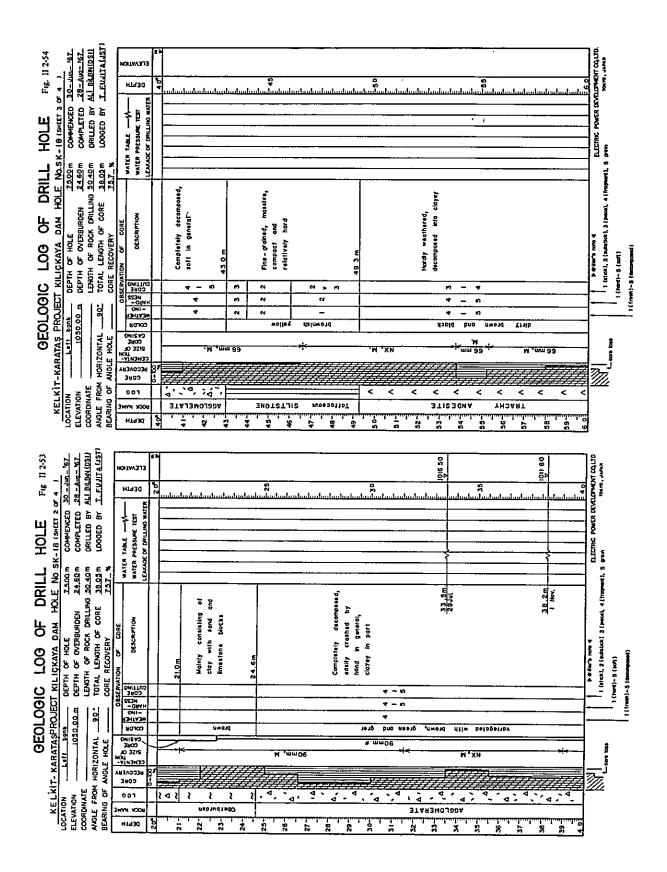


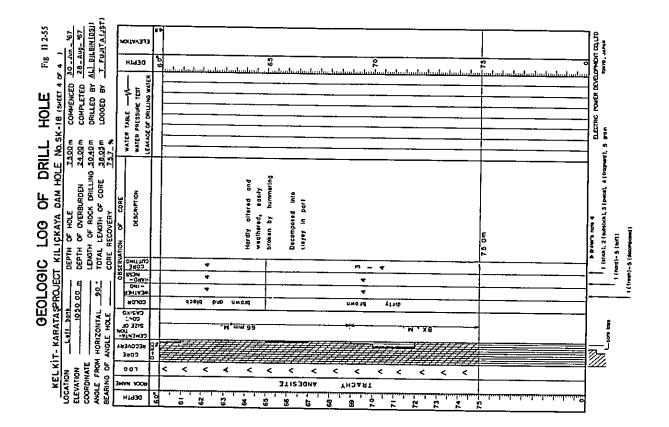






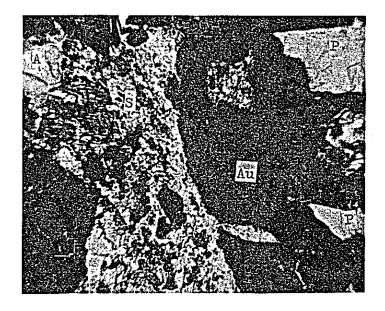






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Fig. II 2-56 Photomicrograph of Thin Section (1-4)



open nicols, x 50

- P Plagioclase phenocrysts
- A Anorthclase
- Au Augite replaced by saponite and hematite
- S Silicified and zelitized matrix part

Locality: Drilling Core, SK-11 85m Rock Name: Altered TRACHY ANDESITE Phenocrysts: Plagioclase, Anorthoclase, Augite.

> Piagioclase and anorthoclase phenocrysts are generally very fresh, through augite and hornblende have been almost completely replaced by saponite and hemetite.

Groundmass: The groundmass which must had been composed of plagioclase, magnetite and mafic minerals such as augite and hornblende was wholly replaced by opalline silica, zeolite and clay minerals.

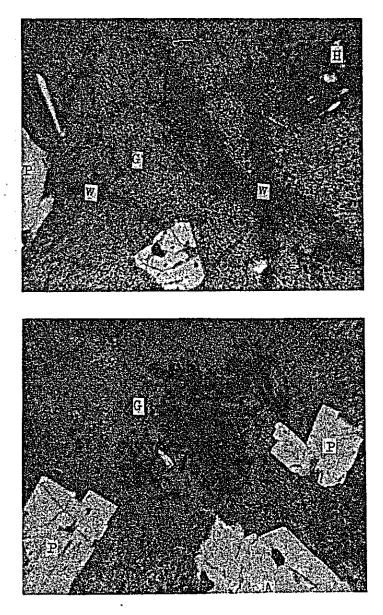


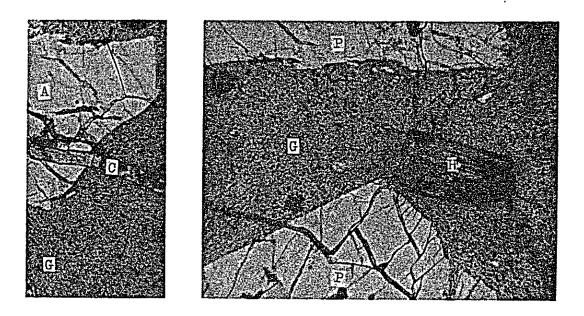
Fig. II 2-57 Photomicrograph of Thin Section (2-4)

open nicols, x 50

Locality: Drilling Cora SK-15, 65m Rock Name: Altered TRACHY ANDESITE

> See the weathering developed along the closed cracks. The weathered part (W) is mostly characterized by the development of hematite and chlorite. Hornbleded is mostly replaced by chlorite and calcite.

Fig. II 2-58 Photomicrograph of Thin Section (3-4)



open nicols, x 50

- P Plagioclase
- A Anorthoclase
- H Hornblende partly replaced by chlorite
- G Groundmass
- C Calcite vein

Locality: EL. 800m on the Dam A	Axis of Right Bank
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Rock Name: Augite PORPHYRITE

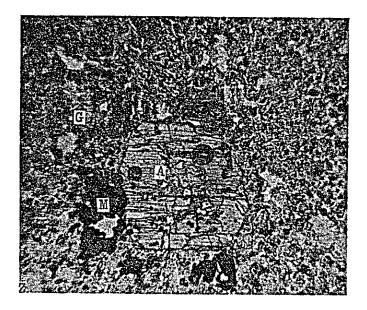
Phenocrysts: Augite, bytownite, anorthoclase, hornblende and biotite.

Augite, hornblende and biotite have been replaced by chlorite and calcite along their cleavage planes and crystal margins.

Bytownite plagioclase show strong zonal struture and Carlsbad twin.

Groundmass: Mainly consists of micrccrysts of sodic plagioclase, glass and hematite.

Fig. II 2-59 Photomicrograph of Thin Section (4-4)



open nicols, x 50

- A Augite
- M Magnetite
- G Groundmass composed of plagioclase, magnetite and augite
- Z Zeolite

 Locality:
 Dyke rock, at Intake of Spillway

 Rock Name:
 Augite PORPHYRITE

 Phenocrysts:
 Augite and bytownite

 Most of augite phenocrysts were strongly replaced by calcite and chlorite.

 Plagioclase phenocrysts show usually Carlsbad twinning and strong zonal structure.

 Groundmass:
 Chiefly composed of microcrysts of augite, plagioclase and magnetite with small amounts of zeolite. Zeolites are mostly filling small scale amygdales.

II 3 Construction Materials

Tables Result of Soil Tests II 3-1 3 - 1 II 3-2 Result of Soil Tests 3 - 1 II 3-3 Result of River Sand and Gravel 3 - 2 Result of Rock Tests II 3-4 3 - 2

Figures

II 3-1	Material Area		3 - 3
II 3-2	Logs of Test Pit at A Area		3 - 4
II 3-3	Logs of Test Pit at A & B Area	••••••	3 - 4
II 3-4	Logs of Test Pit at B & C Area		3 - 5
II 3-5	Logs of Test Pit at C Area	•••••	3 - 5
II 3-6	Logs of Test Pit at C Area	`·····	3 - 6
II 3-7	Logs of Test Pit at D Area	••••••	3 - 6
II 3-8	Logs of Test Pit at E & F Area		3 - 7
II 3-9—II 3-14	Grain Size Distribution Curves for	or Test Samples	3 - 8

Table II 3-1 Result of Soil Tests

	Barry Dife		a	Atte	rberg Lim	1	Gradation			ection
Survey Area	Test Pit No.	Unified Soil Classification	Specific Gravity	LL	PL	PI.	-4,8mm (%)	-0075mm (%)	Optimum Water Contents (%)	Maximum Dry Density (t/m ³)
						_				
A Ares	101	CL.	2.60	39 0	20.6	18.4	100	84	13.4	1 67
	102	CL	2.62	38 4	20.5	17.9	100	88	16 5	1 73
	103	CI.	2.78	40,0	20,7	19.3	99	60	17.5	1 72
	104	CH	2.67	62.6	28.Z	34 4	100	82	18 0	1.56
	105	CL	2.78	33.3	19.3	14 0	96	68	11 2	1,91
	106	CH	2.58	59.3	28.8	30.5	98	76	22.0	1.53
	107	KCB	2 75	52.1	28.9	23.2	100	89	17.5	1.68
	108	CR	2 55	60.0	40.1	20.9	99	94	22.2	1.49
	109	CL	2.65	31.8	216	10.3	100	66	15.0	1.82
	110	CL	2.75	43.3	16 4	26.9	100	86	16 5	I 43
	113	CL-ML	•	34.7	23.0	11.7	99	66	14 0	1.79
	114	а,	2 75	39.3	17.7	21.6	100	80	17.8	1 70
	115	CL	2,66	46.5	19.3	27.4	82	62	18 5	1.70
	116	CL.	2.70	41.2	16.1	25.1	98	68	17 0	1.69
	117	CR	2.66	54 4	14.4	40 0	99	92	15.0	1.66
	118	Ca	2.56	55 6	26 4	29 2	99	86	22 0	1 55
	119-4	CH	2 65	54.2	21.9	32.3	100	93	22 2	1 57
	119-Б	CL-HL	2.69	42.2	24.5	17.7	100	92	15 2	1 71
	120	CH	2 68	50.4	21 4	29 0	99	84	16 5	1 70
	121	CL-ML	2.74	43.5	24.7	18,8	100	80	15.5	1,74
В Атея	201	CL.	2.68	32.0	16 2	15 B	95	72	16 5	1.79
	203	CI,	2,69	40.4	18.2	22.2	97	70	17 0	1.72
	205	sc	2.60	43 3	12.9	30.4	-	48	15 0	1,82
	207	CL,	2.74	45.6	15.7	29 9	98	77	16.0	1 79
	208	CH	2.59	53 4	20.1	33.3	68	77	16 0	1 74
	209	C1.	2.49	46 6	15.0	31 6	99	92	17.5	1.73
	211	CL,	2 68	47.5	17.3	30.2	60	63	18.0	1 71
	213	CC,	2.66	36.7	14 0	22.7	29	20	14 0	1.81
	216	sc	2.10	34.5	16.2	18.2	100	46	15.0	1.88
	217	CI.	2 71	40.0	13.8	26 2	88	76	16 4	1.79
	218	CI,	2.72	44.8	13.4	31.2	96	89	15.5	1 83
	219	SC	2.72	30.4	16.5	13 9	55	25	11.0	2.02
	220	SC-CL	2,67	43.9	19.2	26.7	67	50	15.8	1 77
	221	CC	2.65	32 0	14.5	17.5	47	30	13 0	1 93
	222	SC	2 64	50.7	19.0	31.7	59	48	19.0	1.69
	223	CL	2.70	47.0	14.3	32.7	71	54	17.5	1 78
	224	SC	2.66	40.6	17 6	23,0	63	18	15.0	1.75
	225	CL	2 60	46 2	12 9	33.3	98	76	23.0	1.57

Table II 3-2 Result of Soil Tests

Burvey	Test Pit No.	Unified Soil Classification	Specific	Atte	rberg Liz	its	Gradation		Comp	action
Area			Gravity	LL	PL	PI	-4.8mm (%)	-0.075mm (%)	Optimum Water Contents (1)	Maximum Dry Density (%/m ³
C Ares	302	CH	2.56	51.0	19,0	32.0	81	62	17.0	1 71
D ALC-	302-ь	SC	2,56	39.8	18.0	21.8	80	36	17 0	1 64
	303-4	CL.	2 63	38.4	18.3	20.1	92	70	16.0	1.76
	303-ь	С.	2,61	43 2	17.7	25 5	98	80	18 0	1 76
	304	CL-ML	2.69	34.7	21.8	12.9	97	80	15 5	1 79
	305	CL	2.66	38.8	13.9	24.9	82	53	13.0	1 81
	306	CL	2 72	35.8	13.7	22.1	97	70	15.3	1.68
	309-#	Ca	2 71	52 1	17 0	35 0	97	84	190	1 67
	309-Ъ	SC	2,66	35.2	14.9	20 3	58	42	14 5	1.84
	310	c1.	2.71	50,1	15.4	34.8	98	60	19.0	1 70
	311	CL	2 65	49.8	15.6	34.2	99	74	15.5	1.71
	312	CL	2,70	42.3	19.0	23.3	100	87	18 0	1.69
	313	CL	2.68	41.0	17,2	23.6	97	83	17.0	1 11
	314-*	SC	2.59	48.4	18.1	30 3	60	46	14 0	1 74
	314-b	CL	2.62	47.2	16.6	30.6	100	90	14 Q	1.81
	315	CL.	2 58	39 2	12 8	26.4	99	98	12.0	1.85
	316-#	CL	2 71	39.1	22.9	16 2	100	80	16.5	1 74
	316-b	CT.	2.75	47.2	23.1	24.1	99	62	24 0	1.53
	317-a	CH	2 54	52.2	15.4	36.8	99	92	18.0	1.69
	317-6	CL-SC	Z 59	36 0	19.8	16.2	97	50	15.0	1 76
	318	CL	2 55	48.7	ZO 9	27.8	100	94	18.5	1.63
	319	CL	2 70	38 2	15.9	22.3	97	75	15.1	1 78
	320	CH	2.59	52.8	14.0	38 8	99	88	18.5	1.69
	321	CL	2 65	39.2	15.6	23 6	99	80	15.0	1.81
	322	CL	2 61	47.8	19.2	28.6	80	66	21 0	1 62
	323	CL.	271	35.4	14 4	21.0	99	66	15.0	1 87
	324	CL.	2.66	41.4	13 4	28.0	89	75	14.5	1.82
	325	CL.	2 63	46.5	13.4	33.1	94	82	15.5	1.80
	326	CH	2.54	56 2	22.5	33.7	99	92	20 0	1 58 1.73
	327	C1.	2.62	43.0	17.7	25 3	98	83	17 5	1.75
	328	SC	2 66	40.6	17.6	23.0	68	50	15 0	1.75
	330	CL	2 69	43.6	18.4	25.2	80	66	18 5	1 56
	331-#	СН	2.70	52.5	25 1	27.4	99	88	20 0	1 50
	331-Ъ	CT.	2 69	42.5	17 6	24.9	99	88	18.0	1 60
	332	CH	2.43	57 4	23.2	34.2	91	60	20 0	1 60
	333-a	CH	2.76	61 4	22.2	39.2	98	77 74	12.2	1 93
	334-8	CL.	2 68	30.0	15.7	14.3	91		21.0	1 54
	334-ь	ML.	2 68	49.0	31,4	17.6	99	60	15.8	1,68
	336	CL.	2.67	42 6	17 9	24.3	99	86	15.8	1,64
	337	CL	2 58	41.8	16 3	25.5	99	84	15.5	1 78
	338	CI.	Z.64	42.6	15.0	27.6	89	70	5.5	1 /0

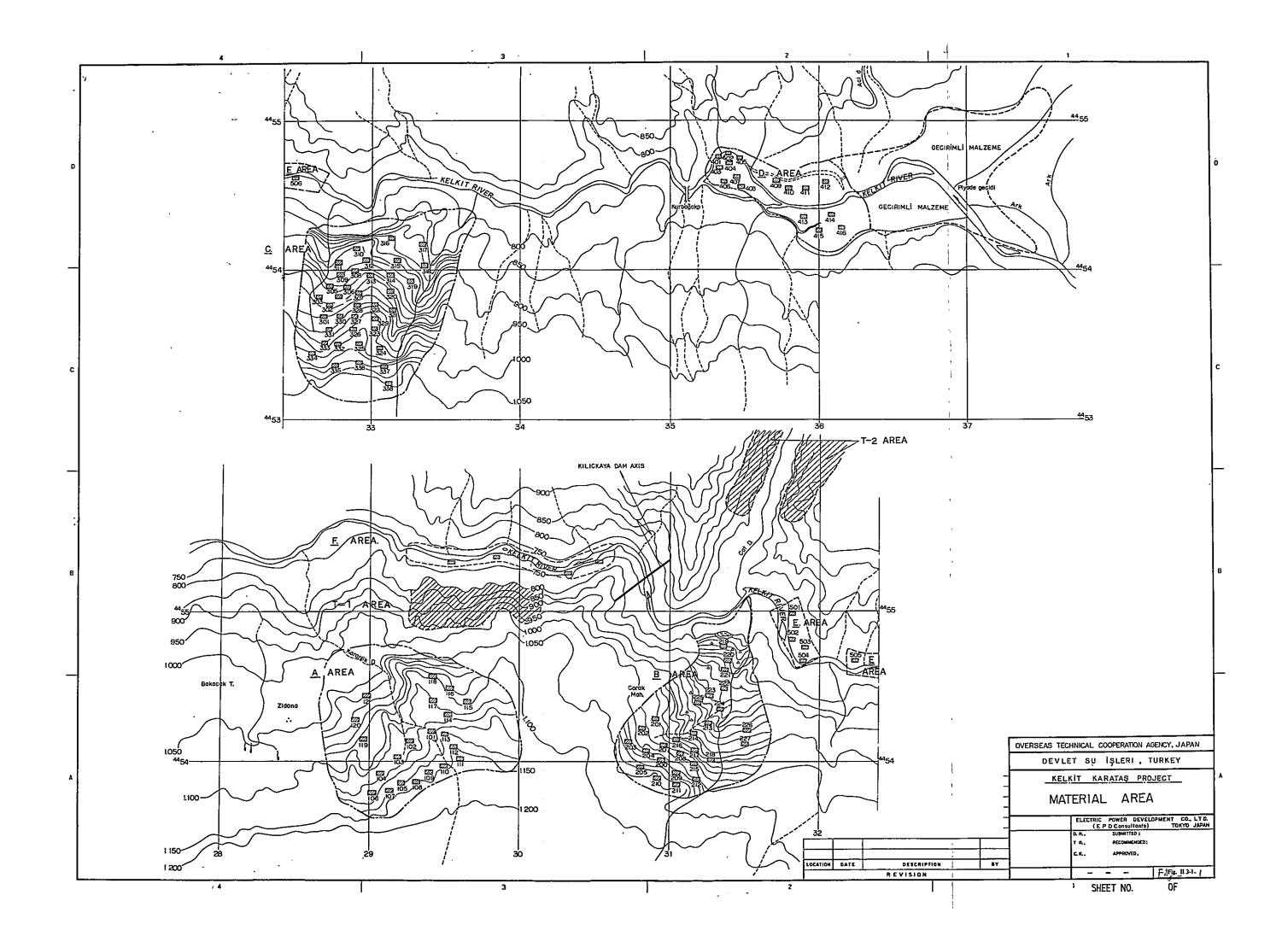
Table II 3-3 Result of River Sand and Gravel

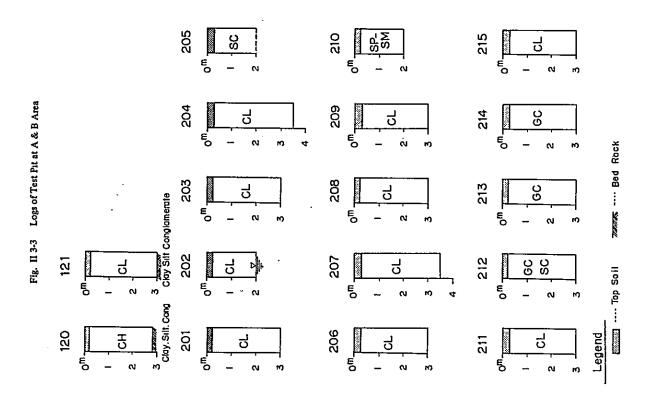
Area	Test Unified Soil Pit Classification No.	Gradation		Sand			Gravel							
		t Classification	-38. lan (%)	-4,8mm (%)		Specific Gravity	Absorption (%)	Bulk Density (kg/m ³)	Durability 'Na ₂ SO ₄ (1)	Specific Gravity	Absorption (%)	Durability Na ₂ SO ₄ (%)	Abrasion L 100 turns(%)	Angeles 500 turns(1
Azea	401	GV	61	31	1	2.60	1,9	1,733	10.0	2.63	0.4	14.1	3.2	18,3
	402	GP	79	46	1	2,61	2.3	1,761	9.1	2.76	0,5	10.9	1.4	17.0
	403	CP	21	38	1	2,66	1.1	1,690	10.0	2.66	0.3	20.8	3.5	20 6
	404	SW	95	53	2	2.66	0.1	1,720	7.5	2.45	2.2	13.1	68	34.9
	405	SP	99	85	Ō	2.77	2.6	1,632	-	2.53	1.6	-		-
	406	GP	69	33	ō	2.56	1.6	1,683	7.5	2 69	0.4	9.8	2.7	20.2
	407	GP CP	62	31	1	2.67	0.6	1,730	15.5	2.52	0.8	14.0	3.4	15.8
		GP	77	35	ō	2.66	1.2	1,810	10.7	2 63	0.8	11.4	3.3	19.8
	408			40	5	2.66	1.0	1,750	9.5	2.65	1.1	11.0	3.8	19.1
	409	GP	81		-					2.66	0.4	16.3	3.2	15.6
	409	GP	71	33	1	2.66	1.3	1,700	19.0		0.9	6.5	5.7	22 4
	410	GP	72	36	1	2.65	1.5	1,690	12.0	2,56			2.5	16.0
	411	CH .	52	25	1	2,65	0.8	1,700	8.5	2.67	0.5	10.8		
	412	GP	78	37	2	2 65	0.2	1,800	12.5	2.61	0.1	9.5	3.2	17.2
	414	GP	81	40	1	2,66	1.6	1,720	6.7	2.58	1.3	10.3	3.1	30.0
	415	GN	61	29	1	2 66	0.8	1,760	8.5	2.63	0.7	10.0	0.9	18.0
	416	GP	68	35	1	2.65	0,1	1,710	12.2	2.56	0.4	14 0	3.6	16.6
Ares	501	52	95	60	1	2 58	0.2	1,670	20.0	2.63	0.9	25.0	5.5	25.0
	502	GP	-	•	-	2.58	3.1		-	•		35.0	2.8	13.7
	505	Ci	57	25	1	2.63	0.2	1,661	20.0	2.64	0.4	25.0	3.5	18,3
Ares	601	GP	37	16	2	2.59	0.9	1,630	62	2.73	2.0	6.8	6.3	16 6 27 3
	602	GP	49	21	2	2.66	1.3	1,690	10.9	2.56	1.9 1.2	11.8 11.0	3.0 8.5	19.1
	603	GP	48	19	2	2.59	0.9	1,720	4.0	2.54	1.2	***0	0.3	19.1

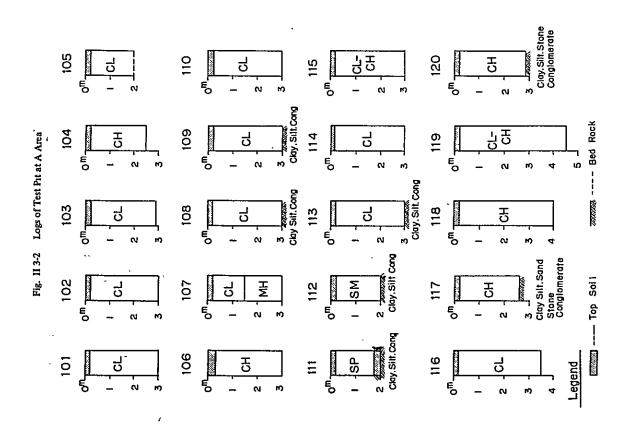
Table II 3-4 Result of Rock Tests

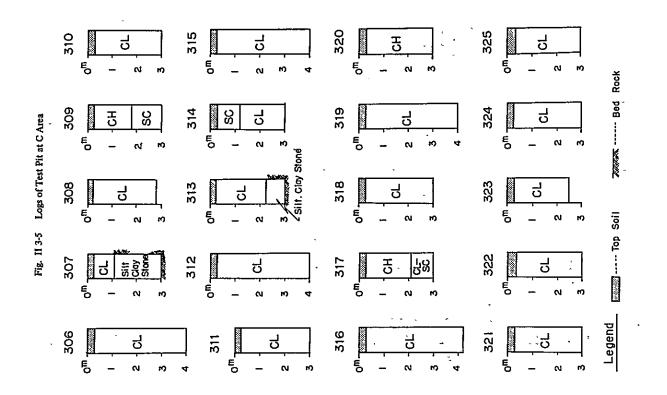
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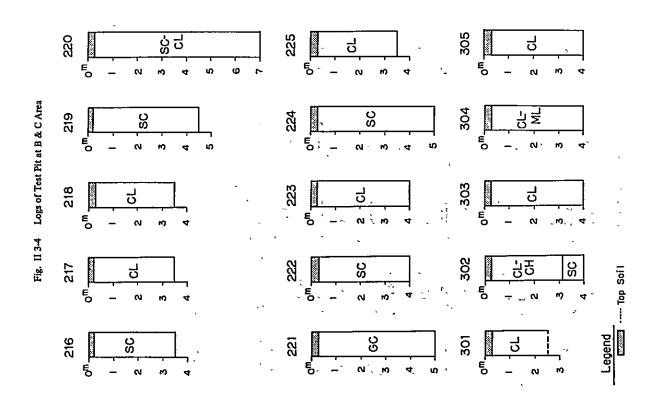
	Specific	Absorption	Durability	Abrasion Los Angeles		
Sevple	Grevity	(%)	N#2 ⁵⁰ 4 (1)	100 turn= (%)	500 turns (%)	
T - 1	2.59	0.03	3.9	3.7	14.2	
Ť - 2	2.58	0.05	5.2	4.8	16.8	
Dam Site Boring No. 13 Depth 13 m	2.38	3.40	62.7	4 3	17.3	

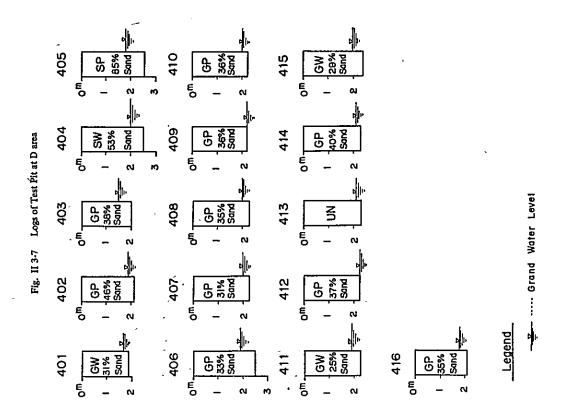


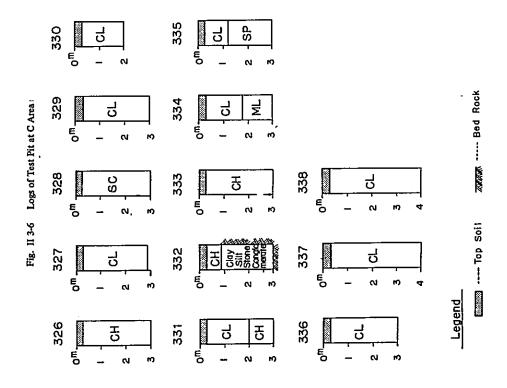












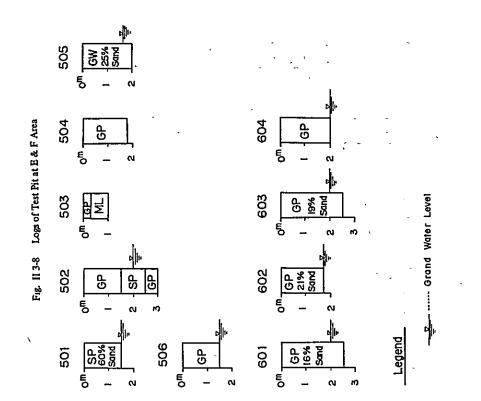
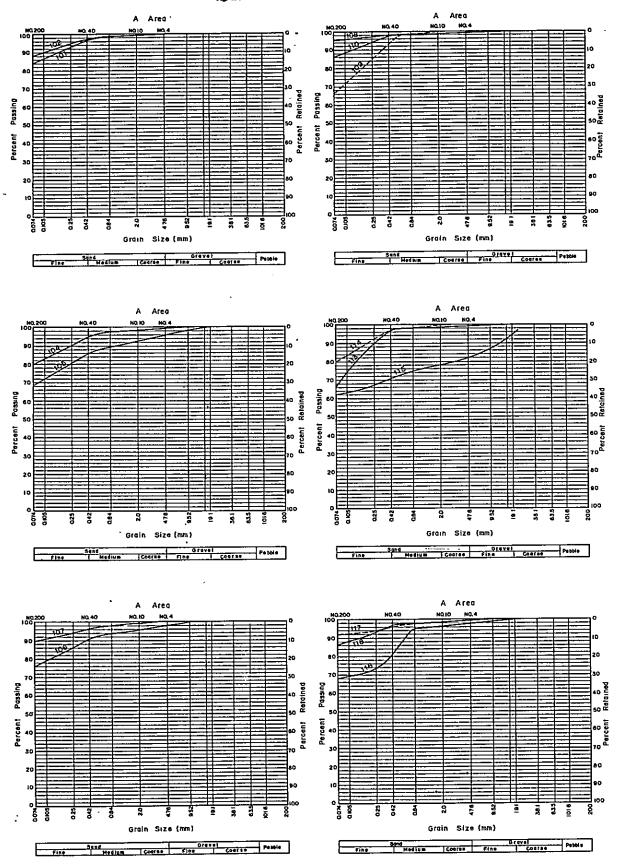


Fig. 11 3-9 Grain Size Distribution Curves for Test Samples







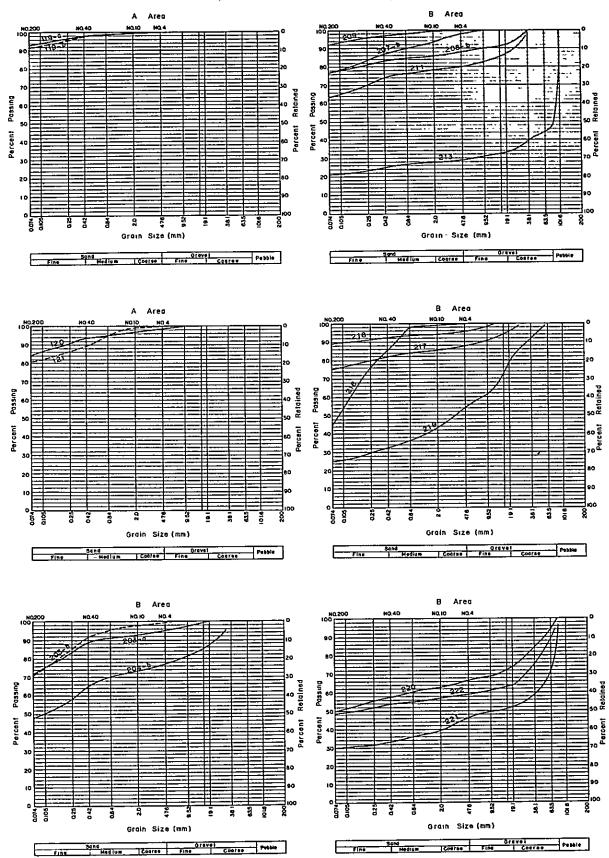
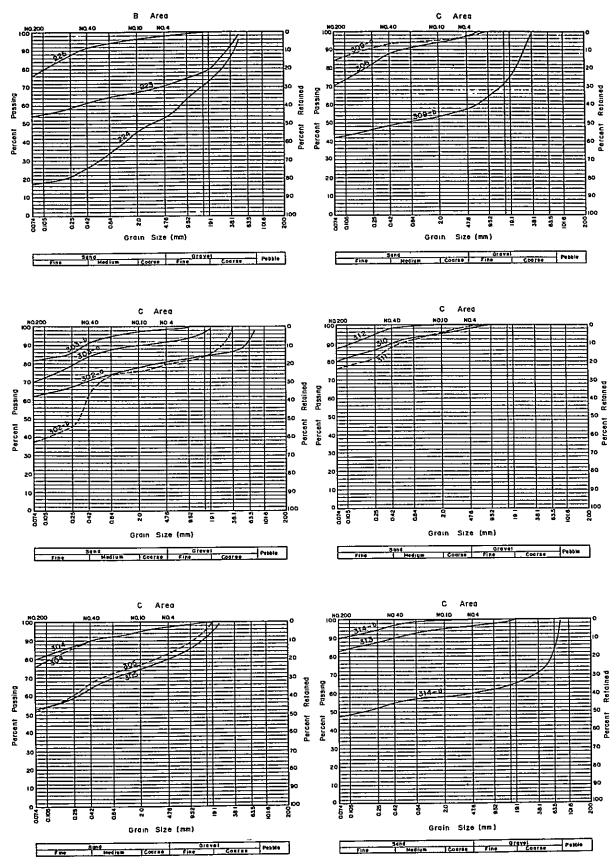
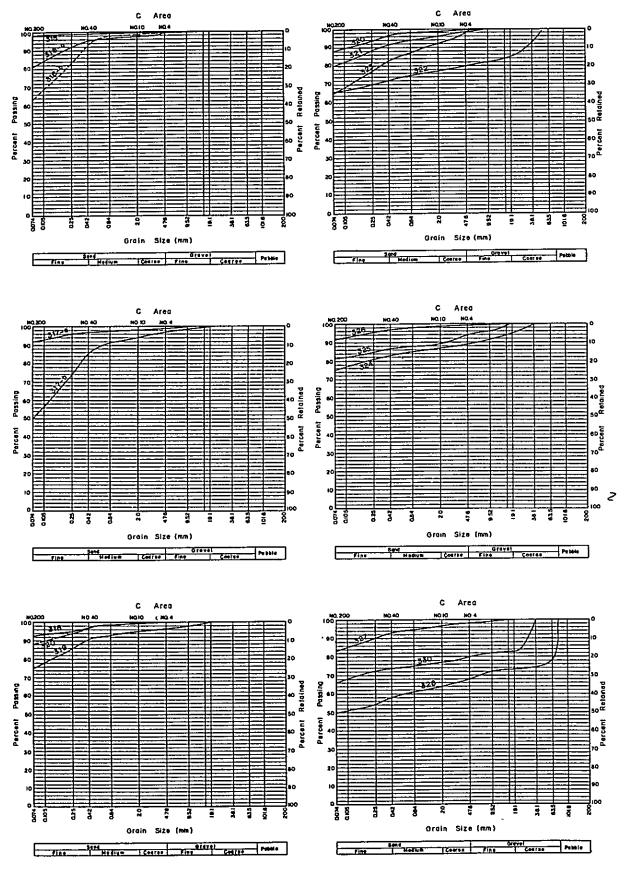


Fig. 11 3-11 Grain Size Distribution Curves for Test Samples



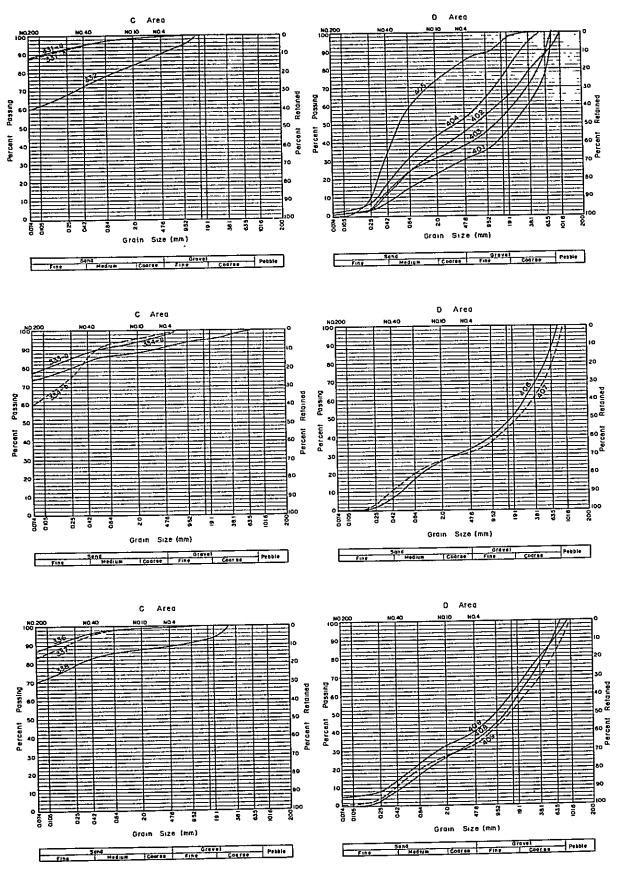
3–10





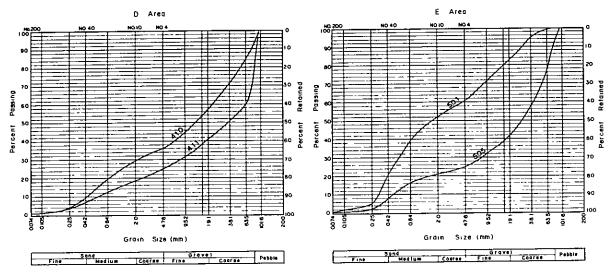


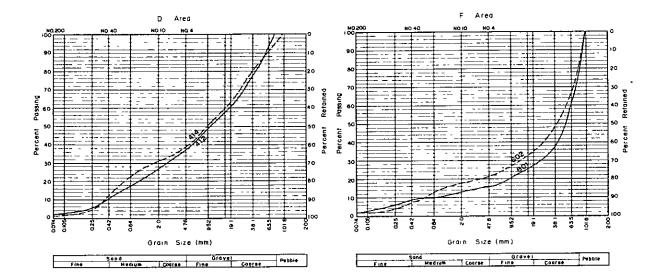


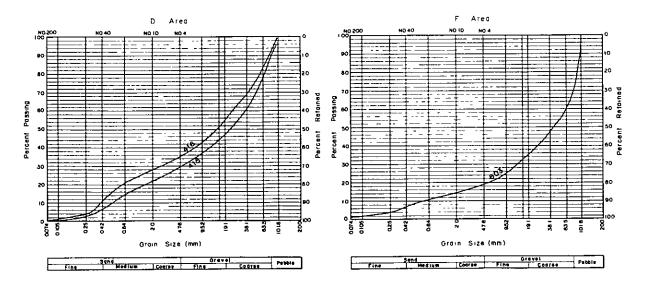


³⁻¹²

Fig II 3-14 Grain Size Distribution Curves for Test Samples









II 4 Size and Operation of Reservoir and Calculation of Sedimentation

Contents

II 4-1	Operation Study		4 - 1
II 4-2	Calculation of Sedim	entation	4 - 1

II 4-1 Program for Electronic Computer II 4-2 Power Study Summary Monthly Inflow 4 - 5 Monthly Evaporation II 4-3 4 - 5 ... Monthly Overflow Discharge II 4-4 4 - 6 22 II 4-5 Monthly Firm Discharge 4-6 ,, Monthly Secondary Discharge II 4-6 4.7 ,, Monthly Discharge for Generation 4-7 II 4-7 ,, II 4-8 Water Surface Elevation 4 - 8 II 4-9 Monthly Firm Energy'..... 4-8 II 4-10 22 Monthly Secondary Energy 4-9 II 4-11 Monthly Energy 4-9 Daily Power Study Example from April 1,1963 to March 31,1967 4-10 II 4-12 II 4-13 Kilickaya Power Production Summary Case 11 Water Surface E.L. 855 4-25 II 4-14 Case 14 Water Surface E.L. 850-4-25 ,, II 4-15 -Case 12 Water Surface E.L. 845 4-26 ,, II 4-16 Case 13 Water Surface E.L. 840 4-26 II 4-17 Ayvacik Power Production Summary Case 123 W.S.L. Kilickaya 850 Ayvacik 195 4-27 II 4-18 Case 124 W.S.L. Kilickaya 840 Ayvacik 195 4-27 >> II 4-19 Case 125 W.S.L. Kilickaya 855 Ayyacik 190 4 - 28** II 4-20 4 Case 126 W.S.L. Kilickaya 850 Ayvacik 190 4-28 ,, II 4-21 Case 127 W.S.L. Kilickaya 845 Ayyacik 190 4-29 •• Case 128 W.S.L. Kilickaya 840 Ayvacik 190 II 4-22 4-29 ,, II 4-23 Case 129 W.S.L. Kilickaya 850 Ayvacik 180 4-30 ,, II 4-24 Case 130 W.S.L. Kilickaya 840 Ayvacik 180 4-30 II 4-25 Kilickaya Sedimentation Amount Month -II 4-36 Junuary — December 4-31 II 4-37 Monthly Discharge Duration at Tepekisla (1-1) (Natural) 4-37[•] II 4-38 (1-2) (Natural) 4-37 ,, II 4-39 (2-1) (Regulated with After Bay) 4-38 II 4-40 1.5 . 22 (2-2) (-) 4-38 II 4-41 (3-1) (Regulated without After Bay) 4-39 II 4-42 . 99 (3-2) - (4-39) II 4-43. Annual Sedimentation Amount at Kilickaya and Tepekisla 4-40 II 4-44 Sedimentation Amount Coming to Ayvacik Considering the Discharge Regulation Effect by Kilickaya Dam 4-40

Figure

II 4-1

Tables

4-41

II-4 SIZE AND OPERATION OF RESERVOIR AND CALCULATION OF SEDIMENTATION

II-4.1 Operation Study

Reservoir operation studies were carried out with the aid of an electronic computor. This appendix includes the example of an program, summaries of inflow, discharge for power generation, summaries of inflow, discharge for power generation, energy production and etc. In this study, it is considered to release from Kilickaya discharge over 32.32 c.m.s. in July and 21.92 c.m.s. in August than normal firm discharge, 35.68 c.m.s. for irrigation purpose in Carsamba plain.

Summaries of power production which were used for selecting optimum size of reservoir are also included.

QI	; Inflow
Q_{EV}	, Evaporation from reservoir surface
Q _{SP}	, Spilled discharge
$Q_{\rm F}$, Firm discharge
Qs	; Secondary discharge
Q_E	; Discharge for generation
Н	, Water surface elevation (end of month)
V _K	; Effective volume of reservoir (end of month)
P _F	; Firm energy production
Ρs	; Secondary energy production
Р	; Energy production

II-4.2 Calculation of Sedimentation

Monthly discharge-sedimentation concentration curves arranged by DSI are used to obtain the sedimentation amout in Kilickaya reservoir. Monthly average discharge duration values are obtained by the data recored at Fatli with the following correlation formula:

Q _K	=	0.69 Q _F + 1 28
Q _K	;	value at Kihckaya
Q _F	;	value at Fatli

The data used come from 28 years period; 1939 - 1967. For the downstream effect, sedimentation at Tapekisla are directly calculated by using monthly discharge durations and discharge-concentration curves for 3 cases:

~

,

- (1) natural discharge
- (2) discharge regulated by Kilickaya
- (3) discharge regulated by Kilickaya and the regulating-pond of it.

To estimate the sedimentation amount flowing into Ayvacik reservoir, the portion coming from Yesilirmak and Cekerek river is regarded as the same as studied by DSI. Therefore, the effects of the existing Almus dam and the proposed Alsancak dam are not considered.

.

Monthly Duration Calculation of the Kelkit River

1. Data

.

1) Daily discharge at Fatli site gaging station											
Relea	sed and spilled discharge from Kilickaya P.S.	Q _{KD}									
Formula for calculation											
2.1	$\overline{DAY} (Q > Q_I) = \frac{\Sigma DAY (Q > Q_I)}{T}$	(1)									
2.2	Natural inflow at Kilickaya site										
	Q _K [±] C _K · Q _{FA} + 1.28	(2)									
2.3	Natural inflow at Tepekisla site	•									
	$Q_T = C_T \cdot Q_{FA}$	(3)									
2.4	Regulated discharge at Tepekisla (with after bay)										
	$Q_{TR} = Q_T - Q_K + Q_{KD}$										
	$= (C_T - C_K) Q_{FA} + Q_{KD} - 1.28$	(4)									
	Provided $[Q_{KD} = Q_E + Q_{SP}]$										
2.5	Regulated discharge at Tepekisla (without after bay)										
	$Q_{FA}(C_T - C_K) - 1.28 + 3.6 Q_F + Q_{SP}$	(5.1)									
	$Q_{TS} = Q_{FA}(C_T - C_K) - 1.28 + Q_{SP}$	(5.2)									
	and number of days corresponds to (5.1) is calculated by										
	DAY $Q_{TSI} = \frac{Q_E}{3.60} Q_F$										
	number of days corresponds to (5.2) is by										
	DAY $Q_{TSZ} = 1 - \frac{Q_E}{3.60Q_F}$ respectively										
	Relea Form 2.1 2.2 2.3 2.4	Released and spilled discharge from Kilickaya P.S. Formula for calculation 2.1 $\overline{DAY} (Q > Q_I) = \frac{\sum DAY (Q > Q_I)}{T}$ 2.2 Natural inflow at Kilickaya site $Q_K = C_K \cdot Q_{FA} + 1.28$ 2.3 Natural inflow at Tepekisla site $Q_T = C_T \cdot Q_{FA}$ 2.4 Regulated discharge at Tepekisla (with after bay) $Q_{TR} = Q_T - Q_K + Q_{KD}$ $= (C_T - C_K) Q_{FA} + Q_{KD} - 1.28$ Provided [$Q_{KD} = Q_E + Q_{SP}$] 2.5 Regulated discharge at Tepekisla (without after bay) $Q_{TS} = \begin{bmatrix} Q_{FA}(C_T - C_K) - 1.28 + 3.6 Q_F + Q_{SP} \\ Q_{TS} = \begin{bmatrix} Q_{FA}(C_T - C_K) - 1.28 + Q_{SP} \\ Q_{FA}(C_T - C_K) - 1.28 + Q_{SP} \end{bmatrix}$ and number of days corresponds to (5.1) is calculated by $DAY Q_{TSI} = \frac{Q_E}{3.60} \\ Q_F$									

21.6 The difference between max. and min. value chosen from the period is divided into 16 logarithmically equal intervals.Used in the calculation divide 16 equially

3. Symbols

Q_K : Discharge at Kilickaya (c.m.s.)

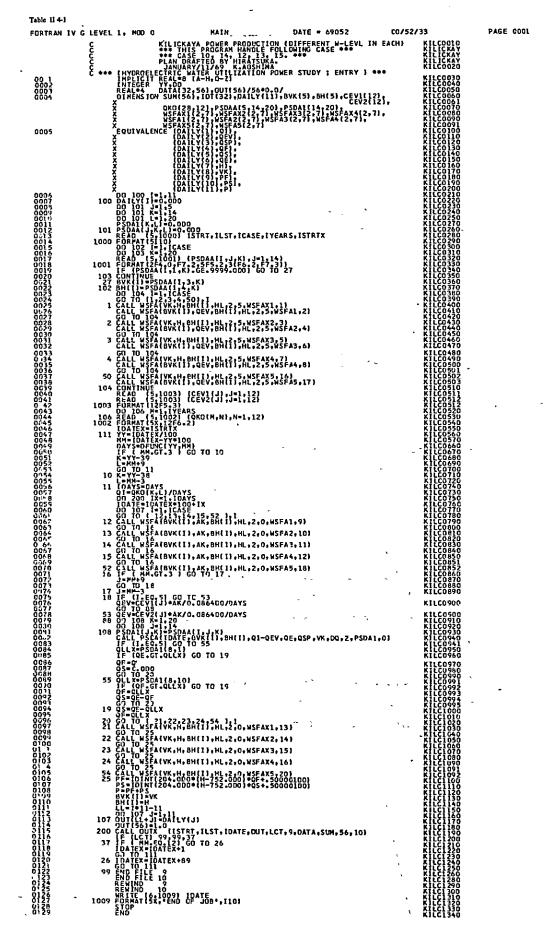
- Q_T : Discharge at Tepekisla (c.m.s.)
- Q_{FA} : Discharge at Fatli (Data of gaging) (c.m.s.)
- C_K : Coefficient of discharge ratio (Kilickaya / Fatli)
- C_T : Coefficient of discharge ratio (Tepekisla / Fatli)
- QTR : Regulated discharge at Tepekisla (With after bay) (c.m.s.)
- Q_{TS} : Regulated discharge at Tepekisla (Without after bay) (c.m.s.)
- Q_{KD} : Released discharge from Kilickaya (c.m.s.)

 $DAY(Q>Q_I)$ Numbers of days having discharge more than Q_I in the month respected

- T ; Observated period (shown by year)
- QI : Struta of discharge
- Q_E : Discharge for total energy production
- Q_F : Discharge for firm energy production

ľ

QSP : Overflow discharge from Kilickaya Dam



4-4

Table 11 4-2

Hydroelectric Water Utilization Power Study Summary Monthly Inflow cu. m. per Secper Day

NEN	4	5	. 6	7	8	9	KAMIKI	* 10	11	12	1	2	3	11-2	TOTAL
39	432512	414005	121898	59919	53403	50463	1132200	54479	59325	79583	70741	121921	175294	331574	1697547
40	904953	576481	281620	112708	47245	39803	1962810		94282				421736	459779	
41	898980	652141	147364	74039	46315	38113	1856976	· ·	125127			53815	224583	362222	2924CO1 25C7774
42	779038	651458	145000	47350	34035	32766	1689651		150514			67130	113704	423703	•
43	601759	594849	186157		31944	30799	1498876		44595			73472		237245	2250773 205913u
44	464641	654884	274502	73163	38762	37431	1543403		80787		50336	45683	63275	238473	1909445
45	55336	646019	176262	49387	30914	27627	985545	-	37616		40220	40127	147755	160926	1340106
46	595046	649722	261620	65474	41632	32326	1645820		51192			78762	356991	225056	2322527
47	311458	140231	77488	31867	21632	27477	610173	29375	93565		54201	60394	71782	259537	970667
48	646551	626829	253958	42836	25097	28530	1627801	32593	32326		30880	31458	95201	129166	1868761
49	396551	756389	145255	37025	26250	30081	1391551	31331	30584				184109	293703	1900694
50	809443	579861	133507	48631	31663	29028	1632533	62697	55162	48970	52650	45243	245687	202025	2146542
51	323461	44428Z	214676	59861	3369Z	39468	1115440	77292	119549	32488	71794	125243	222072	349074	1763878
52	778830	478634	178021	57014	34896	31644	1559039	33218	28125	43958	39236	60220	86551	171539	1850347
53	624433	596620	205266	67280	33581	39005	1566585	41632	45000	62350	66782	78229	351354	252361	2231532
54	757407	775544	322083	108056	39931	35694	2038715	35081	36910	42766	48842	62672	118900	190591	2383287
55	274282	248738	60891	24653	22649	21620	652233	24769	28568	41493	41262	81968	104514	193311	914827
56	617836	455775	215660	54086	29028	37824	1410209	34549	41759	81273	45926	68854	285931	237812	1972501
57	450139	503924	241516	57176	30139	29630	1312524	33391	36535	43553	42500	53032	185405	175624	1766944
58	559537	393403	2201 50	50613	30243	28970	1262916	34144	33692	40116	42141	35466	151296	151435	16 19 791
59	463333	424606	234086	57905	26667	25185	1231782	47905	55324	46056	52292	109673	237569	265545	1782801
60	930612	644606	194282	78345	45810	41806	1935461	40035	41630	43414	42407	45312	103206	172163	2250865
ē1	411701	232442	106065	25532	16794	23137	815671	25255	45139	83148	58102	74433	411667	260822	1513415
6Z	464143	456771	140567	35995	16285	13380	1127141	21991	325Z3	E27C8	91794	116262	211748	323267	1684167
63	616632	631863	518669	117466	40767	39433	1964872	35139	50590	43576	38970	51725	181516	184861	2366388
64	552431	551204	297697	60602	28623	31574	1522131	32951	41007	54468	47697	41725	248275	184897	1988254
65	589988	480405	150532	67870	18831	18565	1326191	54757	66956	87396	195937	156643	288345	506932	2176225
£6	589317	538808	230266	75984	25162	28206	1487743	32766	39687	63005	52505	50231	121505	205832	1847846
59	159003501	4800494	5735078	1694467	906018	889585	39925992	1241855	1598297	1659894	1747557	2143745		7149497	54052435
88	567870	528589	204824	60517	32358	31771	1425929	44352	57082	59282	62413	76562	206253	255339	1921 673

Table II 4-3

Hydroelectric Water Utilization Power Study Summary Monthly Evaporation ca.m. per Secper Day

NEN	4	5	é	7	8	9	KANIKI	10	11	12	1	2	3	11-2	TOTAL
34	3352	6330	8217	15117	12165	5944	51129	2857	551	o	o	a	1469	951	56406
40	3601	6733	8917	17214	14472	7185	58122	3534	1225	0	o	c	2102	1225	64583
41	3858	6808	8828	16512	13568	6667	56241	3232	1126	c	o	0	1714	1126	62313
42	3739	6807	8618	16329	13167	6383	55243	3072	1084	0	0	O	1671	1064	£1070
43	3602	6733	88 32	16663	13518	6568	55916	3117	1017	٥	0	c	1539	1017	61589
44	3563	6815	8974	17002	13995	6684	57237	3313	1116	0	0	0	1453	1116	63119
. 45	2497	4939	7653	14259	11138	5237	45723	2496	824	0	0	٥	1066	824	50109
46	2513	6202	8855	16909	13880	6810	55169	3348	1143	C	a	0	1707	1143	61367
47	3597	5672	6515	11210	6485	4035	39522	1909	647	0	0	0	829	647	42507
48	1998	5321	8260	15914	12706	6092	50291	2858	927	0	0	ΰ	1131	927	55207
49	2339	5791	- 6697	16096	12834	6160	51917	2894	\$36	0	0	0	1419	936	57166
50 S	351.3	6733	6732	16147	12586	6261	54372	3000	999	0	0	0	1399	995	5977C
51	3012	5875	8168	15590	12516	6035	51196	2925	1021	۵	Q	0	1581	1021	56723
52	3694	6571	8679	, 16372	13270	6440	55026	3049	98.3	0	0	0	1245	963	60303
53	2894	6560	, 8651	16909	13850	6788	55852	3261	1074	Q	0	C	1661	1074	61848
54	3785	- 7043	9076	17175	14365	7091	58539	3405	1118	0	٥	0	1441	1118	64503
55	2824	5103	6196	10478	- 7951	3768	36320	1793	583	٥	a	Q	613	583	39309
56	1734	4230	. 6271	11802	9030	4334	37401	2067	£75	C	0	0	1030	679	41177
57	2404	5434	7974	15357	12251	5842	49262	2737	896	0	٥	0	1196	876	54091
\$B	2832	6040	8176	15587	1243E	5946	51019	2787	909	Ó	0	Q	1164	909	\$5879
59	2568	5594	~ 7873	15115	12000	5673	48823	2675	892	C	0	a	1328	892	53718
60	3508	6791	8891	16914	13981	6910	56995	3327	1095	0	٥	۵	1373	1095	62790
61	2869	5384	6609	11535	8661	4097	39155	1929	635	0	O	C	1 C42	639	42765
62	2623	5739	7859	14364	11665	5126	46780	2398	779	- 0	0	O	1234	779	51191
63	3046	6734	9069	. 17296	14545	7205	57897	347Z	115C	0	o	٥	1504	1150	£4C23
£4	3443	6725	, 8919	16884	13757	6696	56424	3184	1036	٥	0	a	1428	1036	62C74
65	3443	6573	8605	16121	12597	6190	\$3929	2930	977	0	0	a	1882	977	59718
66	3823	6695	8856	17007	13946	, 6781-	57110	3224	1052	٥	0	a	1365	1052	62771
59	86674	171975	231376	433880	.349557	169148	1442610	80793	26880	O	C	0	38606	26880	1588889
88.	3096	6142	8263	15496	12464	- 6041,	51522	2685	960	٥	C	Q	1379	960	5674E

Table II 4-4		
Hydroelectric Water Utilization	Power Study Summary Monthly Overflow D	hscharge cu. m per Secper Day

TOTAL	11-2	` 3	2	ı	12	11	10	KAHIKI	9	8	۲	ć	5	4	NEN
č	· 0	0	, o	٥	o	C	0	. 0	٥	c	٥	0	٥	0	39
248386	٥	0	·/ o	a	٥	C	0	248386	0	0	o	0	0	24 83 86	4J
445723	o	,0	0	0	0	0	C	445723	0	C	0	0	0	445723	41
213422	0	a	C	0	C	· 0	G	213422	0	0	0	C	0	213422	42
54769	0	0	ο ľ	0	0	0	0	54769	0	C	۵	٥	0	54769	43
1518	c	0	۵	0	0	0	۰ ۵	1518	0	Q	۵	0	0	1518	44
O	¢.	0	- 0	0	٥	٥	` 0	0	C	C	0	G	Ű	0	45
0	٥	0	C	Q	0	G	0	٥	a	C	٥	0	C	0	46
0	a	ο '	٥	0,	O	0	o	o	0	۵	0	0	a	C	47
C	Q.,	0	0	O	0	C	0	0	o	C	0	C	C	0	48
C	C	0	0	C	0	C	0	0	0	C	c	٥	Ø	0	49
154347	° 0	a ~	· 0	Q	0	C	0	154347	0	C	a	0	O	154347	50
a	0	0	0	0	0	0	0	0	0	C	C	0	C	0	51
195343	0	O	C	a	٥	۵	٥	195343	0	٥	0	0	٥	195343	52
a	0	0	0 '	0	0	0	0	٥	G	C	a	C	0	0	53
294274	Õ	a	٥	0	٥	O	0	294274	0	a	C	C	73911	220363	54
Č O	0	0	0 /	C	0	0 .	٥	0	0	C	0	0	0	. 0	55
o	C	0	0	o	0	0	0	0	0	٥	0	0	0	C	56
o	0 -	0	٥	0	0	0	٥	٥	o	٥	0	0	0	C	57
o	٥	0	. 0	0	0	0	0	0	a	C	C	10	Q	0	58
c	Ċ	0	0	o	0	đ	0	0	0	o	۵	C	C	σ	59
230675	σ	0	0	o	C	C -	O	230675	0	0	0	a	0	230675	έŪ
° C	С.	- 0	Q	0	a	0	٥	0	a	C	0	¢	٥	0	61
a	- 0	0	Q	0 ĭ	٥	0	Ø	0	0	٥	0	C	0	a	62
48140	- 0	0	Û	0	0	C	0	48140	a	c	٥	48140	0	0	63
15403	Ο.	0	0	0	a	0	0	15403	0	0	e	0	٥	15403	64
27346	0	0	o	0	0	0	0	27346	٥	C	0	0	0	27346	65
103340	C	0	0	a	0	0	Q	103340	0	đ	٥	¢	0	103340	66
2032686	0	0	. 0	C	0	0	G	2032686	0	٥	0	48140	73911	1910635	59
72596	C	0	0	0	٥	0	٥	72596	e	C	O	1719	2640	68237	88

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Table II 4-5

Hydroelectne Water Utilization Power Study Summary Monthly Firm Discharge ca.m. per Sec. per Day

NEN	4	- 5	é	7	8	9	KAMEKI	10	11	12	1	2	3	11-2	TOTAL
39	107040	110608	1 07040	110608	110608	107040	652944	110608	107040	110608	110608	103472	110608	431728	1305888
40	107040	, 110608	107040	110608	110608	107040	652944	110608	107040	110608	110408	59504	110608	428160	13(2320
41	107040	110608	107040	110608	110608	107040	652944	110608	107646	110608	110608	59904	110608	428160	1302320
42	107040	110608	107040	110608	110608	107040	652944	110608	107040	110608	110608	99904	110608	428160	1302320
43	107040	110608	1 07040	110608	110608	107040	652944		•		110608	103472	110608	431728	1305888
44	107040	110608	107040	110608	110608	107040	652944	110608	107040	110608	110608	99904	110608	428160	1302320
45	107040	110608	107040	110608	110608	107040	652944	110608	107040	110608	110608	99904	110608	428160	1302320
46	107040	110608	107040	110608	110608	107040	652944	110608	107040	110608	110608	99904	110608	428160	1302320
47	107040	110608	107040	110608	110608	107040	652944	110608	107040	110608	110608	103472	110608	431728	1365888
48	107040	110608	107040	110608	110605	107040	652944	110608	107040	110608	110608	59504	110608	428160	1362320
49	107040	110608	107040	110608	110608	107040	652944	110608	107040	110605	110608	99904	110608	428160	1302320
50	107040	110608	107040	110608	110606	107040	652944	.110608	107040	110608	110608	99904	110608	428160	1302320
51	107040	110608	107040	110608	110608	107040	652944	110608	107040	110608	110608	103472	110608	431728	1305888
5Z	107040	110608	107040	110408	110608	107040	652944	110608	107040	110608	110608	99904	110608	428160	1302320
53	107040	110608	107040	110608	110608	107040	652944	110608	107640	1 1 0 6 0 8	110608	59504	110608	426160	1302320
54	107040	110608	107040	110608	110608	107040	652944	110608	107040	110608	11040B	99904	110608	428160	1302320
55	107040	110608	107040	110608	110608	107040	652944	110608	107040	110608	110608	103472	110608	431728	1365688
56	107040	110608	107040	110608	110608	107040	652944	110608	107640	110608	110608	59504	110608	428160	1302320
57	107040	110608	107040	110608	110606	107040	652944	110608	107040	110608	110608	99904	110608	428160	1302320
58	107040	110608	107040	110608	110605	107040	652944	110608	107040	110608	110608	· 59504	110608	428160	1302320
59	107040	110608	107040	110608	110606	107040	652944	110608	107040	110608	110608	103472	110608	431728	1305688
60	107040	110608	107040	110608	110408	107040	652944	110608	107040	110608	110408	- 99904	110608	428160	1302320
61	107040	110608	107040	110608	110608	107040	652944	110408	107640	110608	110608	59904	110608	428160	1302320
6Z	107040	110608	107040	110608	110608	107040	652944	110608	107040	110608	110608	99904	110608	428160	1302320
63	107040	110608	107040	110608	110608	107040	652944	110608	107040	110608	110608	103472	110608	431728	1305888
64	107040	110608	107040	110608	110608	107040	652944	110608	107040	110608	110608	99904	110608	428160	1302320
65	107040	310908	107040	110608	110608	107040	652944	110608	107040	110608	110608	99904	110608	428160	1362320
66	107040		1 07040	110608	110608	107040	652944	110608	107040	110408	110608	99904	110608	428160	1302320
99	2997120	3097024	2997120	3097024	3097024	2997120	18282432	3097024	2997120	30970Z4	3097024	2822288	3097024	12013456	36489936
88	107040	110408	107040	110606	110608	107040	652944	110608	107040	110608	110608	100796	110608	429052	1303212

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Table 11 4-6			
Hydroelectric Water Utilization Power Str	idy Summary Monthh	y Secondary Discharge cu.m. per Sec j	er Day

NEN	4	5	é	7	8	9	KAHIKI	10	11	12	1	2	3	11-2	TOTAL
39	93180	81092	20760	100192	67952	0	363176	۵	. 0	0	0	o	21452	٥	384628
40	234950	175040	125140	100192	67952	° o	703274	c	C	a	٥	c	254061	C	997335
41	342360	219542	65490	100192	67552	0	795536	٥	٥	0	a	G	87482	C	8€3018
42	269240	219542	65315		67552	a	722245	O	0	٥	٥	0	38492	C	760737
43	203976	193408	49791	100192	67552	C	615319	0	. 0	0	C	0	30504	o	645823
44	151209	219542	151501	100192	67952	a	650396	0	0	0	C	O	21452	0	711848
45 -	20760	21452	20760	100192	67952	0	231116	0	0	٥	0	٥	21452	٥	252568
46	27907	96002	84268	100192	67552	Q	376321	٥	0	0	G	0	64052	۵	440373
47	127315	47012	2076C	100192	67552	0	363231	0	0	o	Q	0	21452	٩	384683
48	20760	21452	20760	100192	67552	- o	231116	٥	. 0	٥	o	0	21452	a	252568
49	20760	44882	27150	100192	67552	٥	260936	0	0	Q	Ó	0	21452	a	262388
50	202723	178420	39930	100192	67952	0	589217	0	٥	Q	a	0	21452	0	610669
51	50580	38492	20760	100192	67952	0	277976	0	0	0	0	0	21452	0	299428
52	252608	125668	20760	100192	67952	0	567180	0	0	a	٥	0	21452	0	588632
53	51755	153512	42060	100192	67552	0	415471	0	C	0	a	0	55694	0	471165
54	286420	254182	212460	100192	67952	٥	921206	o	0	Q	٥	0	21452	a	942658
55	22151	21452	20760	100192	67952	0	232507	0	٥	0	0	0	14856	Q	247363
56	20760	21452	20760	100192	67952	o	231116	0	٥	0	0	0	21452	C	252568
57	20760	21452	2076C	100192	67952	0	231116	0	0	Q	0	0	21452	C	252568
58.	42545	51272	20760	100192	67552	a	282721	0	o	a	0	0	21452	0	304173
59	22890	21452	2076C	100192	67552	٥	233246	0	0	0	0	C	21452	0	2,4698
60	211708	219542	71465	100192	67552	0	670859	0	0	٥	¢	٥	21452	0	692311
61	39930	29972	20760	100192	67552	0	Z 58806	0	0	0	0	0	21452	0	260258
6Z	27150	26606	20760	100192	67552	0	242660	0	a	C	0	a	21452	0	264112
63	64694	204064	316637	100192	67952	0	753539	0	0	0	٥	0	21452	0	774991
64	139599	153512	141532	100192	67552	0	602787	0	Q	0	0	۵	21452	G	624235
65	149431	127129	20760	100192	67552	0	465464	0	0	0	Q	0	54494	0	559958
66	299270	153512	58357	100192	6755Z	0	679283	0	0	0	0	0	21452	٥	700735
99	3417391	3140657	1741740	2805376	1902656	0	13007820	0	0	0	٥	0	1108675	C	14116495
88	122050	112166	62205	100192	67952	0	464565	٥	٥	C	0	0	39596	C	504161

Table II 4-7

Hydroelectric Water Utilization Power Study Summary Monthly Discharge for Generation cum, per Sec per Day

NEN	4	5	6	۲	8	9	KAMIKI	10	11	12	1	2	3	11-2	TOTAL
39	200220	191700	127800	Z10800	176560	107040	1016120	110608	107040	110608	110608	103472	132060	431728	1690516
40	341990'	285648	2321êC	Z10800	176560	107040	1356218	110608	107040	110608	110408	59504	404669	428160	2259655
41	449400	330150	172530	210800	178560	107040	1448480	110608	107040	110608	110406	\$9904	158090	428160	2185338
42	376280	330150	172359	210800	178560	107040	13751.89	110608	107040	110608	110608	59504	149100	428160	2063057
43	311016	304016	156831	210800	178540	107040	1268263	110608	107040	110608	110608	103472	141112	431728	1951711
44	258249	330150	258541	210800	178560	107040	1343340	110608	107040	110608	110608	99904	132060	428160	2014168
45	127800	132060	127800	210800	178560	107040	884060	110608	107040	110608	110608	99904	132060	428160	1554688
46	134947	206610	191308	210800	17856C	107040	1029265	110608	107040	110608	110608	59904	174660	428160	1742693
47	234355	157620	1278CO	210800	178566	107040	1016175	110608	107040	110608	110608	103472	132060	431728	1690571
48	127800	132060	127800	210800	17856C	107040	884060	110608	107040	110608	110608	99904	132060	426160	1554888
49	127800	155490	134190	Z10800	178560	107040	913880	110608	107040	110608	110608	99904	132660	428160	1564708
50	309763	289028	146970	Z10800	17856C	107040	1242161	110608	107040	110608	110608	99904	132060	428160	1912989
51	157620	149100	127800	210800	178560	107040	930920	110608	107040	110608	110608	163472	132060	431728	1605316
52	359648	236276	127800	210800	17856C	107040	1220124	110608	107040	110608	110608	99904	132060	428160	1850952
53	158795	264120	149100	210800	17856C	107040	1068415	110608	107040	110608	110608	99904	166302	428160	1773485
54	393460	364790	319500	210800	17856C	107040	1574150	110608	107640	110608	110608	59904	132060	428160	2244978
55	129191	132060	127800	210800	178560	107040	885451	110608	107040	110608	110608	103472	125464	431726	1553251
56	127800	132060	127800	210800	178560	107040	864060	110608	107040	110608	110608	99904	132060	42816C	1554888
57	127600	132060	127800	210800	17856C	107040	. 884060	110608	107640	110608	110608	99904	132060	428160	1554088
58	149585	161880	127800	210800	178560	107040	935665	110608	107040	110608	110608	99904	132060	428160	1666493
59	129930	132060	127800	210800	178560	107040	886190	110608	107640	110608	110608	103472	132060	431728	1560586
60 (318748	330150	178505	210800	178566	107040	1323803	110608	107040	110608	110608	99904	132060	428160	1994631
61	146970	140580	127800	210800	178560	107040	911750	110608	107040	110608	110608	99904	132060	42816C	1562578
6Z	134190	137214	127800	Z10800	178560	107040	895604	110608	107640	110608	110608	99904	132060	428160	1566432
63	171734	314672	423677	210800	178560	107040	1406483	110608	107040	110608	110408	103472	132060	431726	2010875
64	246639	264120	248572	210800	178560	107040	1255731	110608	107040	110608	110608	\$9504	132060	428160	1926559
65	256471	237737	127800	210800	178560	107040	1118408	110608	107040	110608	110608	99904	205102	428160	1862278
66	406310	264120	165397	210800	17856C	107040	1332227	110608	107040	110608	110608	99904	132060	428160	2003055
99	6414511	6237681	4738860	5902400	4999680	2997120	31290252	3097024	2997120	2097024	3097024	2822288	4205699	12013456	50606431
68	229090	222774	169245	210800	17856¢	107040	1117509	110608	107040	110608	, 110608	100796	150204 -	429052	1807373

Table II 4-8	
Hydroelectric Water Utilization Power Study Summary Water Surface Elevation at the End of the Months	

NEN	4	5	ė	7	8	9	KANIKI	10	11	12	1	2	3	11-2	IOTAL	
39	84443	84796	84775	84508	84255	84133	566908	84012	83 907	83836	83740	83785	63892	335268	1010680	
40	84500	84939	E4993	84834	84608	64481	508355	84420	84395	E44CC	84351	84474	84500	337620	1014895	
41	84500	84981	84935	84711	84465	84332	507928	84237	84270	84197	84117	84105	84155	336625	1013009	
42	84500	84980	84932	84665	84395	84244	507716	84146	84230	84258	84200	84135	E4060	336823	1012745	
43	84500	84939	84967	84715	84448	84296	507865	84141	84012	83905	83 78 2	83708	84123	335407	1011536	
44	84500	84985	84994	84776	84528	84393	508176	84264	84211	84114	83990	83870	83751	336185	1012376	
45	83557	84607	84674	84372	84065	83683	505158	63722	83535	83347	83131	82945	82987	332962	1004829	
46	84170	84905	64988	84758	84513	84368	567702	84333	84224	84086	83969	83923	84288	336204	1012527	
47	84424	84382	84276	83887	83466	83219	503654	82959	82917	82723	82508	82325	82037	330473	959123	
48	63771	84710	84885	84603	84317	84154	506440	83989	83815	83629	83410	E3206	83096	334064	1007591	
49	83838	84908	84911	84624	84335	84176	506792	84009	83839	83647	83680	83697	83821	334863	1009485	
50	84500	84939	84909	84641	84364	84205	507558	84104	83995	83859	83719	83577	83867	335150	1010679	
51	84207	84715	84834	84572	84291	84149	506768	84076	84099	83936	83848	63897	84085	335780	1010709	
52	84500	84872	84930	84678	84412	84260	507652	84102	83935	63760	83599	83491	83357	334805	1009916	
53	84405	84923	84987	84759	84501	84368	507943	84232	84107	8400£	83913	83864	84244	335892	1012311	
54	84500	85000	84992	64826	84586	84451	508355	84307	84169	84032	83899	83811	83776	335911	1012345	
55	84090	84308	84167	. 83737	83285	83003	502590	82727	82419	82104	81745	81625	e1500	327893	954710	
56	83435	84185	84341	84009	83637	83436	503043	63203	82993	82907	B2692	82575	83095	331167	1000508	
57	63957	84642	84807	84537	84246	84081	506270	83912	83743	83570	83379	83239	83395	333931	1007508	
58	84326	84713	84840	84564	84276	84111	506830	63946	83775	83595	63406	· 83213	E3269	333989	1008034	
59	84095	84621	84776	84503	84201	84025	566221	83683	83759	83599	83439	83457	83734	334254	1008092	
60	84500	84971	64980	84769	64532	84405	508157	84268	84137	83999	83848	83716	83639	335700	1011764	
61	84219	84381	64329	83935	83512	83256	503632	82982	82788	82691	82489	82381	83327	330349	1000290	
62	84127	84690	84698	84375	84038	83820	505748	83591	83381	83298	83241	83291	83517	333211	1006667	
63	84468	84950	85000	64849	84613	84486	508366	84344	84235	84103	83954	83637	83946	336129	1012785	
64	84500	84934	64988	84751	64482	84334	567989	84179	84044	83925	83779	83632	83911	335380	1011459	
65	84500	84873	84893	84653	84354	84173	507446	84055	83969	83918	64098	84210	84364	336195	1012660	
66	84500	84917	84992	84779	84508	84355	508051	84201	84065	83965	83835	83715	83685	335580	1011517	
99	2359532	2373766	2374793	2367388	2359237	2354597	14189313	2350344	2346976	2343433	2339761	2337704	2341423	9367874	28248954	
68	84269	84777	84814	84550	84258	84093	506761	83941	83821	83694	83563	83485	83622	334567	1008891	

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TAble II 4-9

Hydroelectric Water Utilization Power Study Summary Monthly Firm Energy kWh

NEM	4	5	6	ז	â	g	KAMIKI	10	11	12	1	2	3	11-2	TOTAL
39	197762	212302	209298	212972	207094	196356	1235724	200163	191256	195645	193752	160754	154971	761407	2392265
40	200582	215166	213115	219155	214794	204010	1266826	208709	201042	207530	207020	187808	205818	803400	2468753
41	203076	21 5700	212579	217113	211836	200861	1261165	204959	197711	203808	202084	181610	201515	785213	2452852
42	201994	215690	212525	216548	210473	199096	1256326	202940	196306	204081	203710	182745	200459	786842	2446567
43	200523	215166	212654	217522	211648	200241	1257754	203458	193797	157605	195011	160356	157197	766773	2425182
44	200053	215746	213384	218509	213249	202187	1263128	205940	197322	202200	199708	177901	154264	777131	2440463
45	184567	201768	206174	210329	203438	191561	1197837	194081	184057	185950	181239	159630	175245	71097£	2278135
46	184718	211573	212812	216237	212862	201730	1241932	206451	198208	202046	159171	178229	201524	777654	2427561
47	200281	207264	199313	200377	191273	177756	1176264	177889	168557	171925	167298	152293	157474	660473	2172100
48	170976	275045	269666	215332	208906	197261	1207190	200137	190035	192311	187691	165196	179396	735237	2321560
49	181245	208674	211921	215858	209337	197693	1224728	200608	190476	1 \$ 2732	190589	173003	193178	747200	2365714
50	199575	215166	212084	216025	26566¢	198330	1251040	202011	193203	196885	193767	` 172137	152481	755952	2401524
51	193547	209104	209120	214393	208260	196921	1231345	201070	194073	158921	196092	163082	158478	772166	2403061
52	201534	214007	211863	216688	210824	199451	1254367	202602	192519	195322	191530	170649	185539	749420	2391928
53	191404	214010	212782	218241	212752	201607	1250796	205288	195819	199833	197654	177064	200432	770370	2426886
54	202453	217275	213899	219036	214450	203441	1270554	207071	197317	200800	197764	176374	153901	772255	2443781
55	190954	203157	197298	197510	187530	173426	1149865	172982	160996	159311	151684	136848	143191	608835	2074 E77
56	162194	195120	1 57 97 5	202457	194584	181991	1134321	183166	172399	174859	171471	151464	172711	670193	2160391
57	182739	205932	2CBU68	213692	207345	195677	1213453	158448	188359	190785	186674	165233	183229	731051	2326181
58	190596	210242	209175	214372	207991	196335	1226711	199174	189084	191425	18725e	165225	181457	732990	2342332
59	186203	207046	207491	212963	206465	194584	1214752	1 \$7509	188223	1\$1285	107673	174105	1 69598	741290	2343149
60	199492	215573	212947	218268	213195	202350	1261829	206114	196533	200058	196617	174876	191264	768284	2427491
£1	191459	205253	199899	201503	192345	178664	1169123	178594	167796	170101	166720	147420	173694	652037	2173448
6Z	187244	208135	207307	Z10631	203172	190584	1207073	1\$1884	180889	183638	182070	164410	16523B	711007	2295202
63	193703	215192	213905	219393	215021	204127	1261341	207894	198451	20234C	199170	183515	198163	783476	2448874
64	198777	215103	213129	218158	212440	201028	1258635	204311	194558	198188	195188	173307	193587.	761241	2417774
65	198781	214023	211440	215970	209680	197868	1247962	201104	192398	197280	198847	182542	205256	771067	2425385
éь	202787	214887	2 128 22	218526	213055	201545	1263622	204807	195028	158677	196287	174732	191774	764924	2425127
99	5399159	5903323	5864649	5989778	5814683	5486671	34457663	5569364	5306816	5405749	5324437	4751508	5283034	20828910	66138571
89	192827	21 0833	209452	213921	207646	195953	1230632	198906	189529	193062	190158	171140	168680	743885	2362107

Table II 4-10 Hydroelectric Water Utilization Power Study Summary Monthly Secondary Energy kWh

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Table II 4-11

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NEN ,	4	5	6	7	8	9	KAHIKI	10	11	12	1	2	3	11-2	TOTA
39	172983	154695	40593	192916	127228	۵	- 688415	0	۰ م	a	0	o	37614	. 0	72622
40	444297	340494	249089	198517	131959	0	1364356	٥	۵	Q	C	۵	557846	٩	192220
41	649526	428136	120194	196667	130142	C	1534665	a	Q	٥	٥	0	155382	0	16540
42	509801	428116	129831	196155	129304	0	1393207	C	0	0	Q	0	65852	C	14430
43	384827	376225	98844	197038	130026	0	1186960	0	۵	٥	ā	0	54698	0	12416
44	284108	428227	301980	197932	131005	0	1343256	0	0	0	0	0	37677	٥	13605
45	35796	39132	39987	190522	124982	a	430419 、	0	C	0	0	0	33988	٥	4644
46	48856	184160	167502	197686	130772	0	728976	٥	0	0	0	0	117256	٥	6462
47	238407	88163	38656	181507	11750\$	0	664242	0	0	0	0	C	30542	٥	6947
48	33160	39768	40664	195054	128341 .	0	436987	٥	۵	C	٥	0	34793	٥	4717
49	35152	86478	53747	195531	128606	0	499514	a	0	0	0	0	37466	, C	5265
50	382862	347069	79158	195682	128927	Ō	1133698	٥	0	C	a	0	37331	0	11710
51	91994	72097	40558	194204	127945	0.	52679E	0	٥	٥	0	0	36494	0	5652
52	477904	242463	41090	196282	129520	a	1087259	0	O	٥	۵	0	35985	٥	11232
53	94578	297022	83485	197689	130704	0	803478	0	C	0	٥	¢	101546	Q	9050
54		500514	424561	198409	131747	0	1758000	Q	0	0	0	0	37606	C	18356
55	39557	39402	- 38265	178911	115209	0	411344	0	۵	0	C	C	19294	a	4306
56	31457	37843	38397	183391	119543	0	410631	a	0	0	0	0	33497	٥	444)
57	35442	39940	40354	193568	127382	۵	436686	0	0	0	0	0	35537	٥	4723
58	77045	96804	40569	194185	127779	0	536382	0	0	0	0	0	35193	0	571
59	39978	40156	40242	192908	126842	a	440126	0	0	0	0	0	36772	Q	476
60	400099	427884	142118	197714	130979	0	1298794	0	O	٥	C	C	37095	a	1335
61	72179	55491	36770	182527	118167	o	467134	0	0	0	C	0	33687	C	500
62	47929	49783	40207		124816	C	453533	o	0	٥	0	0	15926	0	4894
63	119388	397602	632844	198733	132098	0	1480665	a	0	٥	0	0	36045	0	1518
64	262081	298540	281788	197614	130512	0	1170535	0	0	٥	0	Û	37545	0	1208
£5	280962	245329	41008		128940	o	891871	0	0	0	٥	0	175448	0	1067
66	567373	298241	115903	• • • • • • •	-	0	1310354	٥	0	0	0	0	37194	C	1347
60 99				5425717		0	24928285	0	0	a	0	0	1977509	۵	26905
69	228590	217135			127567	1 0	890297	0	C	C	۵	0	70625	۵	960

NG 10

Hydroelectric Water Ulikisation Power Study Summary Monthly Energy kWh NEN 4 5 6 7 8 9 KAMIKI 10 11 17 1 2 3 11-2 TOTAL

11514	-		-		-	•									
39	370685	366097	249891	405888	334322	196356	1924139	200163	19125e	195645	193752	180754	232785	761407	31 18 49 4
40	•••			417672		204010	2631180	206709	201042	207530	207020	167806	767664	80340C	4410553
41	852602	643837		413780			2795831	204959	197711	20380€	202084	181610	360897	785213	4146500
42	711795	643807		412703			2649534	202940	196306	204081	203710	182745	270311	786842	3969627
43	585350			414559		200241	2444712	203458	193797	1 5760 5	195011	180356	251895	766773	3666838
44	484161			416440		202187	2606384	205940	197322	202200	199708	177901	231541	777131	3821396
45	220362			400851			1628255	194081	184057	185950	181 339	159630	209234	710976	2742546
-	233574			415923			1970909	206451	198208	202046	199171	178229	318780	777654	3273794
46	438687			381884			1840505	177689	168957	171925	167298	152293	168016	660473	2866883
48	204137			410387	337247	197261	1644179	200137	190039	192311	187691	165196	214189	735237	2753742
49	216396	-		411389		197693	1724241	200608	190476	152732	190585	173003	230644	747200	2902693
50	582438			411707			2364739	202011	193203	1 96885	193767	172137	229812	755992	3572554
51	285541			406597			1758143	201070	194073	198921	196092	163082	236972	772168	2968353
52	679438			412969	340344		2341626	202602	192515	195322	191530	170049	221523	749420	3515171
53	285982	511032		415930			2054274	205288	195819	199833	197654	177064	301978	77037C	3331910
54	745222			417445			3068554	207071	197317	2C0800	197764	176374	231507	772255	4279387
55	230511	242559		376421			1561210	172982	160996	159311	151684	136848	162485	608839	2505516
56	193651		-	385848			1544952	183166	172399	174859	171471	151464	206208	670193	2664519
57	218180	-		407260			1650137	198448	188359	190785	186674	165233	218765	731051	2798401
58	. 267640			408557		196335	1765092	-199174	189084	151425	187254	165225	216650	732990	2913904
59	226182			405871		194584	~1654879	197509	188223	191289	187673	174105	226370	741290	2820048
60	599592			415982			2560623	206114	196533	200058	196817	174876	228359	768284	3763380
61	263638	260744		384030		178664	1636256	178594	167796	170101	166720	147420	207382	652037	2674269
62	235172			401427	-	190584	1660605	191884	180889	183638	182070	164410	221164	711007	2784660
63				418124		204127	2742008	207894	198451	202340	199170	163515	234208	763476	3967586
64	460857			. 415772		201028	2429169	204311	194558	-198188	195188	173307	231132	761241	3625853
65	479743			411602			2139832			1 97260				771067	3492707
66	. 770161						2573979	204607	195028	198877	196287	_174732	228968	764924	3772678
99	117996671						59385947	5569364	1306816	5405749	5324437	4791908	7260543	20828910	93044764
86				407696			2120927	198906	189525	193062	\190158	171140	259305	743889	1323027
	-	-			•	,					-				
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NG 11

	- Ie II 4-12 Droelect	RIC WATER	UTILIZAT	ION POW	ER STUDY	KILICKA	YA 850.0 I	METER A	YVACIK 190.0	PETER INSTA	LLED CAPACIT	Y 123,000 KW
	DATE	-	QEV	QSP	QF	05	CE	н	- VK	۶F	PS	Ρ
	0 0 0 0 0 0 0 0 0 0 0 0 0 0		001223456789123456780123 9000000000000000000000000000000000000	00000000000000000000000000000000000000	1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,	00000000000000000000000000000000000000	\$\$\$080885885858588888585888888888888888	4467188470076692071031660726600470731907 444655556666647703388909990000.00111 444655556666647778888909999000.00111111111111111111111111	4710320 47104733 4714733 4714733 4740132 4740132 4740132 4740132 558473 558473 558473 558473 558473 558473 558473 558473 558473 558473 558473 558473 558473 558473 558473 558473 558473 558473 57755 558473 57755 558473 57755 558473 57755 57508 57777 57508 57777 57508 57777 57508 57777 57508 57777 57508 57777 57508 57777 57508 577777 57508 577777 57508 577777 57508 5777777 57508 57777777 57508 5777777777777777777777777777777777777	5986932. 60021. 60022. 6002. 60022. 6002. 60022. 600	1114665488447. 1556665488447. 1114665488447. 1114665488447. 11147188691070316901. 11199900001. 1122212458497. 11222222223739480048. 1122222223739480048. 11222222373948007. 112222223739480. 112222223739480. 112222223739480. 112222223739480. 112222223739480. 112222223739480. 11222223739480. 11222223739480. 11222223739480. 1222223739480. 1222223739480. 1222223739480. 1222223739480. 1222223739480. 1222223739480. 1222223739480. 1222223739480. 1222223739480. 12223739480. 12223739480. 12223739480. 12223739480. 12223739480. 12223739480. 12223739480. 12223739480. 12223739480. 12223739480. 12223739480. 12223739480. 12223739480. 12237444. 1223440. 12237450. 1223750. 12237450. 1223750. 1235750. 1235750. 1235750. 1235750. 1235750. 1235750. 12357	7305099. 73357249. 73357249. 7357249. 74430370. 74430370. 74437322. 745722. 745722. 7558643. 7558643. 7558643. 7558643. 7558643. 7558643. 7558643. 7669099. 115613991. 1166368.
147-13 147-13 147-13 147-13 147-13 147-13 147-13 147-13 147-13 147-14<	620400										_	23517225.
DELECTAIC WATER UTILIZATION POWER STUDY KILICKAYA 850.0 METER AVVACIN 190.C PETER INSTALLEC CAPACITY 121,000 DATE DJ GEV DSP GF QS E H VK PF PS DEVEL Attage A	62000500512345 62000500512345 62000500512345 620005005112345 6200005112345 620005515515 660055220005515 6600552200055222 000552220055125 6600552220055222	1996 599 599 599 599 599 599 599 599 599	01-75790246802457911468023579 666566677777888888999902000 11111111111111111111111200000	000000000000000000000000000000000000000	22322222222222222222222222222222222222	\$9\$\$7\$\$2\$2\$2\$2\$\$ \$9\$\$9\$9\$9\$9\$9\$\$2\$2 \$4\$\$\$\$9\$9\$9\$9\$9\$\$ \$5\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$	60000 22.46000 22.46000 22.46000 22.46000 22.46000 22.46000 22.46000 22.46000 22.46000 22.46000 22.460000 22.460000 22.4600000000000000000000000000000000000	884444 4.4.4.8020 88444455.8520 884444555.9024 888444555.9024 888444555.9024 888444555.9024 888444555.9024 888444555.9024 888444555.9024 888444555.9024 888444555.9024 888444555.9024 888444555.9024 888444555.9024 888444555.9024 888444555.9024 888444555.9024 888444555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9024 88844555.9027 88844555.9027 88844555.9027 88844555.9027 88844555.9027 88844555.9027 88844555.9027 8884555.9027 8884555.9027 8884555.9027 8884555.9027 8884555.9027 88845555.9027 88845555.9027 88857 88757 877577 877577 877577 8775777 877577777777	0130 0120 0120 0120 0120 0120 0120 0120	6521493 6521493 6524495 6524495 65536 655376 655376 655376 655376 6663 6663 6663 66704 66704 66704 66704 66775 66704 66775 66704 66775 667555 667555 667555 667555 667555 6675555 6675555 66755555 667555555 6675555555555	2225 2225 2227 2227 2227 2227 2227 2227 2227 2228 2227 2228 2239 2228 2239 2339 23 23 23 23 23 23 23 23 23 23	788314. 792204. 792204. 79555. 7956056. 7956054. 800473. 800473. 803689. 8056252. 806816. 80881. 809946. 811510.
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27701 11.601 5.000 0.7 35.668 32.32 68.600 846.88 10910.81 690605. 625570. 1316175 02703 11.601 4.97. 0.0 35.68 32.32 68.600 846.88 10910.81 690605. 625570. 1316175 02703 11.601 4.97. 0.0 35.68 32.32 68.600 846.84 10910.81 690605. 625570. 131677. 02703 11.601 4.97. 0.0 35.68 32.32 68.00 846.49 10766.5. 688421. 6252999. 1310756. 02706 11.601 4.88 0.0 73.568 32.32 68.00 846.49 107655.51 687786. 6221800. 1300797 02707 11.61 4.885 0.0 73.668 32.32 68.00 846.97 10543.00 6857831. 6210201. 1306502 02707 11.61 4.875 0.0 73.668 32.32 68.00 846.97 68376.736. 6210201. 1306502 02707 11.61 4.875 0.									VK			Y 123,000 KW P
0711 11.61 4.76 0.0 35.64 32.32 68.00 845.78 10236.27 583326. \$616977. 1302303 0712 11.61 4.71 0.0 35.64 32.32 68.00 845.78 10237.15 682598.6 618318.1 1300916 0713 11.61 4.71 0.0 35.64 32.32 68.00 845.78 100145.95 681870 616973.1 1300916 0714 11.61 4.64 0.0 35.66 32.32 68.00 845.77 100145.96 681070 616973.4 1298503 0716 11.61 4.64 0.0 35.66 32.32 68.00 845.77 100145.96 680742 616774 1298506 0717 11.61 4.64 0.0 35.68 32.32 68.00 845.26 9870.93 678813 6149330 12927316 0717 11.61 4.64 0.0 35.68 32.32 68.00 845.36 9809.96 677285 612450 1290700 0718 11.61 4.64 <td< td=""><td></td><td>01 080676666666666666666666666666666666666</td><td>QEV 2.62 2.62 2.62 2.62 2.62 2.62</td><td>P 000000000000000000000000000000000000</td><td>G G G G G G G G G G G G G G</td><td>\$</td><td>E 8555555555555555555555555555555555555</td><td>H 9001122227373344545455555 6666666697733344566667977 88454666666667977 885679112227333445666667977</td><td>VK 109224.75 109226.39 109275.68 10933.45 10933.45 10933.45 10933.45 10944.14 10944.425 10944.44 10944.45 10944.55 10944.23 10942.45 109457.45 10945</td><td>PF 69075533 690787233 690787233 690787233 69078723 6907872 690788 6907886 6907964 6907964 6907964 6907964 6907964 6907964 6907964 6907964 6907964 6971114 69711114 697</td><td>PS 8</td><td>·</td></td<>		01 080676666666666666666666666666666666666	QEV 2.62 2.62 2.62 2.62 2.62 2.62	P 000000000000000000000000000000000000	G G G G G G G G G G G G G G	\$	E 8555555555555555555555555555555555555	H 9001122227373344545455555 6666666697733344566667977 88454666666667977 885679112227333445666667977	VK 109224.75 109226.39 109275.68 10933.45 10933.45 10933.45 10933.45 10944.14 10944.425 10944.44 10944.45 10944.55 10944.23 10942.45 109457.45 10945	PF 69075533 690787233 690787233 690787233 69078723 6907872 690788 6907886 6907964 6907964 6907964 6907964 6907964 6907964 6907964 6907964 6907964 6971114 69711114 697	PS 8	·
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HTUKUELEGI	-						HEICK P	170.C	NEVEN INSTAN	LLED CAPACITS	1 1239000 KW
DATE	QÌ	QEV	QSP		QS		н	VK	PF	PS	P
$\begin{array}{c} 620601\\ 6220603\\ 6320603\\ 64206056\\ 64206056\\ 64206056\\ 64206056\\ 64206056\\ 64206056\\ 6420601\\ 6420$	I BRANKARANANANANANANANANANANANANANANANANAN	988641977530864207553186442975330863 488887777876305555554444373337222 497576763777787753157555555555444373337222		80088888888888888888888888888888888888		40000000000000000000000000000000000000		98961544843 98961544843 888679474748 888679474748 888679474748 888679474748 888679474748 888679474748 888679474748 88867947474 88867947474 88867947474 888679474 888679474 888679474 888679474 888679474 888679474 888679474 8886794 8876794 8886794 887777777777777777777777777777777777	667095. 665366. 665366. 664310. 66637081. 66637081. 66637081. 66637081. 66637081. 665370705. 665370705. 655370705. 65537010. 65537010. 655300. 655300. 655400. 655500. 655000. 655000. 655000. 655000. 655000.	40088447012 40088447012 40088447012 40088447012 40070000000000000000000000000000000000	1076924 1075456 1073458 107328 107328 107328 1068346 1068346 1068346 1068346 1068346 1068346 1068357 1066357 10665764 1066320009 1059533 1059533 1059533 10595464 106532009 10595464 10653207 10595464 10653207 10595464 10653207 10595464 10653207 1059547
620800		110.69	0.0			1785.602		253705.53	20317164.	12481843.	32799007.
$\begin{array}{c} 620901\\ 6210902\\ 6210903\\ 6210903\\ 6210903\\ 6210903\\ 6210903\\ 6220912\\ 6220922\\ 622092\\ 6220920$ 6220920	44444444444444444444444444444444444444	1111 11111 11111 11111 11111 111111	000000000000000000000000000000000000000	55555555555555555555555555555555555555	000000000000000000000000000000000000000	6003886466866686668666686666666666666666	640.14 840.17 840.17 840.04 840.04 840.04 8530	$\begin{array}{c} 7314 \cdot .05\\ 7724 \cdot .004\\ 7724 \cdot .003\\ 7724 \cdot .003\\ 7714 \cdot .003\\ 7714 \cdot .004\\ 7714 \cdot .004\\ 7701 \cdot .004\\$	642784, 642784, 641765, 641765, 641765, 641378, 641761, 641761, 641761, 641761, 641761, 64177761, 64177761, 64177761, 64177761, 64177761, 64177761, 64177761, 64177761, 64177761, 64177761, 64177761, 64177761, 64177761, 64177761, 64177761, 64177761, 64177761, 64177761, 641777761, 641777761, 641777761, 641777761, 641777761, 641777761, 6417777761, 641777777777777777777777777777777777777	00000000000000000000000000000000000000	642784. 642744. 641765. 641765. 641819. 6419706. 6419706. 63392900. 63392900. 63392900. 63392700. 6337179. 6337179. 63361641. 6337179. 63361641. 63361641. 6334559. 6329689. 6329689. 6329689. 6329689. 6329689. 6329689. 6329689. 6329689. 6329689. 6329680. 63490. 63490. 63400. 63400. 63400. 63400. 63400. 63400. 63400. 63400. 634
620900	133.80	51.25	0.0	1070.40	0.0	1070.402	5178.37	205086.95	19058382.	0.0	19058382.
FYDROELECTR DAT E	RIC WATER	UT IL IZATI QE V	ON POW	ER STUDY I Of	KILICKA QS	YA 850.0 QE	METER A	444C1K 190-C VK	PETER INSTAL PF	LLEC CAPACITY PS	7 123,000 KH P
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DAT E 12000045678000123456780001402723456788 4621000060123456780001402723456788 462110000601404567800014027234556788 46211001050100101010707234556788 462100000788 462100000788 4621000000000000000000000000000000000000	1 000000000000000000000000000000000000	QE 11 0.8810 0.8800 0.877777 0.8777778 0.877778 0.87777778 0.8777777778 0.87777777777	A 000000000000000000000000000000000000	G 888888888888888888888888888888888888	\$ 000000000000000000000000000000000000	GE 48864884888888888888888888888888888888	H 3697550364743777258038764657457024699 887677777777777777777660866666666666666	VK 28444 94446267 9.0.1.0.2855264 3.0.0741857265766 6.6.272185766666 6.6.272185766676758 6.6.272185766666 6.6.275758 6.6.000777780 6.6.000777780 6.6.00077780 6.6.00077780 6.5.0077800000000000000000000000000000000	Ff 64.1.5 64.0.7.6 64.0.5 74.5 64.0.5 74.5 64.0.5 74.5 64.0.5 74.5 74.5 74.5 74.5 74.5 74.5 74.5 74	<pre>S</pre>	P 6 910,7 64,755,787,60 62,755,787,60 62,755,787,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7,7
DAT E 10007345667890 422100005789 422100005789 4221000057890 4221000057890 4221000057890 42210000057890 42210000057890 422100000057890 422100000057890 422100000057890 42210000000 42210000000 42210000000 42210000000 4221000000 4221000000 4221000000 4221000000 4221000000 4221000000 4221000000 4221000000 4221000000 4221000000 4221000000 42210000000 4221000000 42210000000 4221000000 42210000000 42210000000 42210000000 42210000000 42210000000 42210000000 422100000000 422100000000 422100000000 4221000000000 4221000000000 4221000000000 42210000000000 4221000000000 4221000000000000 422100000000000000000000 422100000000000000000000000000000000000	01 00000000000000000000000000000000000	¥ 11000009999988887777776666555555444 888888867777777777777777777777777777		0F 6888888888888888888888888888888888888	S 000000000000000000000000000000000000		H 3697550364743777258038764657457024699 887677777777777777777660866666666666666	K 8344670267970 901-1227067007000 901-1227067007000000000000000000000000000000	Ff 6225837807.6 6225837876.0 62258378760.0 62258378760.0 62222725588 62222725588.6 62222725588.6 62222725588.6 62222725588.6 62222725588.6 62222725588.6 62120595568.6 6613747870.0 661374780.0 661374780.0 661374780.0 661374780.0 661374780.0 66144101175.0 66144101175.0 66144100.0 66144100.0 66144100.0 66144100.0 66144100.0 6614400.00000000000000000000000000000000	<pre>S 000000000000000000000000000000000000</pre>	P 6

Table 114-12 (Continue; HYDROELECTRIC WATER UTILIZATION POWER STUDY KILICKAYA 850.0 METER AYVACIK 190.0 METER INSTALLED CAPACITY 123,000 KW

		G WATER	UTILIZATI	ON POWE	R STUDY	KILICKAYA	850.0	HE TER	YVACIK 190.C	METER INSTAL	LED CAPACITY	123,000 KW
	DATE	QI	QEV	QSP	QF	95	QE	н	VK	PF	PS	Ρ
	621222225 2012231 2012232 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 2012222222 20122222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 201222222 2012222 20122222 20122222 20122222 20122222 20122222 20122222 201222222 201222222 201222222 201222222 2012222222 2012222222 2012222222 2012222222 20122222222	88898988888888888888888888888888888888	000000000000000000000000000000000000000	000000000000000000000000000000000000000	₩₽₽₩₽₽₽₽₽₽₩₽₽₩₽₽₽₩₽₽₩₽₽₩₽₽₩₽₽₩₽₽₩₽₽₩₽₽₩	000000000000000000000000000000000000000	๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛		000 0100 0100 0100 000 000 000 0	548. 548. 559. 559. 559. 559. 559. 559. 559. 55	000000000000000000000000000000000000000	44. 5.0000 5.0000 5.0000 5.0000 5.0000 5.00000 5.00000 5.0000 5.000
	621200	827.08	0.0		1106-08			5834.94	141115.10	18363773.	0.0	18363773.
	630101 630102 630103 630104 630105 630105 630105 630105 630105 630110 630112 630112 630112 630113 630114 630117 630114 630114 630114 630114 6301120 6301221 6301223 630124 6301225 630124 630134 630134 630134 630134 630134 630134 630134 630134 630134 630134 630134 630134 630134 630134 630134 630134 630134 630134 630124 630124 63013	666161216661616161616161616161616161616		000000000000000000000000000000000000000	₩₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽	000000000000000000000000000000000000000	₩₽₽₩₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽₽		$\begin{array}{c} 036 \\ 036$	5825 5826 58206 58206 58206 58207 58007 580000000000	00000000000000000000000000000000000000	\$60,000,000,000,000,000,000,000,000,000,
	630100	917.91	0.0	0.0	1106.08	0.0 1	196.082	25813.40	133919.87	18206990.	0.0	18206990.
н	MOROELECTR I		UTILIZATI	ON POWEI	R STUDY	KILICKAYA	850.0	METER				4 133 000 KN
	630201	QI	QE V	OSP	QF	95	QE	н	VK	PETER INSTA	PS	P
	630201 630203 630203 630203 6300206 6300206 6300206 6300206 6300206 6300207 6300207 6300211 6300213 6300215 6300215 6300215 6300215 6300215 6300215 6300215 6300215 6300220 6300220 6300221 6300220 6300222 630022 630002 630022 630000000000		QE V 0.00000000000000000000000000000000000	SP 000000000000000000000000000000000000	F 8888888898888888888888888888888888888							
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TADIO 11412 (Continue) Mydroelectric water utilization power study Kilickaya 850.0 Meter Ayvacik 190.0 Meter installed capacity 123,000 kw

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4 306623 6 306657 6 306777 6 307777 6 3077777 6 30777777 6 3077777 6 30777777 6 30777777777777777777777777777777777777	q1 896999889099890999999999999999999999999				GS 8867842997878787878787878787878787878787878787			VK 412 12	PF 710330. 7103455 7103455 71235155 713555 713555 713555 715557 71557 7155777 7155777 715577 7155777 7155777 7155777 7155777 7155777 7155777 7155777 7155777 7155777 7155777 7155777 7155777 71557777 71557777 715577777 71557777777777	PS 140190106.141127720.14	2120247 2121977 2122576767 2122576767 2999480 2999860 2999860 29994800 29994800 299980000000000000000000000000
4 300 30 30 30 30 30 30 30 30 30 30 30 30	II 99999999999999999999999999999999999	VOLVENTANTUTUTUTUTUTUTUTUTUTUTUTUTUTUTUTUTUTU						VK 1282763.642 1282763.432 1282763.432 130776.000 130776 130776.000 130	PF 710330. 710415. 710217. 712217. 712315. 713325. 713325. 71055. 71055. 71055. 700100. 700000. 700000. 700000. 700000. 700000. 700000. 700000. 70000	PS 14019910. 1411277767. 14017767. 140177767. 140177767. 140177767. 140177767. 140177767. 140177767. 140177767. 140177767. 140177767. 140177767. 140177767. 140177767. 140177767. 140177767. 140177767. 140177767. 14077767. 140777767. 140777767. 140777767. 140777767. 14077777767. 140777777777777777777777777777777777777	212024 212137 212137 21212741 21212741 21212741 21212741 2094400 299450 2994400 2994400 2994400 2994400 2994400 2994400 2994400 2994400 2994400 2994400 2994400 2994400 2994400 2994400 299450 299450 299450 299450 2995400 2995555555555555555555555555555555555

	(Continue)		กม อุญษา	R STUDY I	K11 1 CKAN	A 850-0	METER A	YVACIK 190.0	METER INSTAL	LED CAPACITY	123.000 KM
			 QSP			QÉ	н	vĸ	 PF	PS	P
- DAT E 		5910865910864919864219754208759 699988888877777466646451515554444	000000000000000000000000000000000000000			\$3000000000000000000000000000000000000	1470258919781348375802479617577213 4722120591978437548775121 482588887777212545545474745454545454545454545454545454	11987745.85295532 11987745.85295532 11987725.85295532 11987725.85295532 1197725.85295532 1197725.85295532 1197725.85295 1197725.85295 1197725.85295 1197745.8529 1197745.8577 1197745.5777 1197745.5777 119775.5777 119775.5777 119775.5777 119775.5777 119775.5777 119775.5777 119775.5777 119775.5777 119775.5777 119777575.5777 119775.5777 119775.	70174. 700732. 700213. 699631. 699631. 699631. 699632. 69962. 69962. 69977. 69962. 69962. 69962. 69962. 69962. 69962. 69962. 69962. 69962. 69962. 69976. 69962. 69962. 69962. 69962. 69962. 69977. 69977. 69977. 69977. 69977. 69977. 69977. 69977. 69977. 699777. 699777. 699777. 699777. 699777. 699777. 699777. 69	$\begin{array}{c} \bullet \bullet$	1132031. 1132034. 11320389. 1129389. 1129389. 1129389. 1129389. 1129389. 1129389. 1129389. 1129389. 1129389. 1129389. 112938. 112939. 112938. 112939. 112939. 112938. 112939. 110939. 110930. 11000. 11000. 110000. 110000.
630600	407.96 13.14		0.0 0.0	1106+08 35+68	679.52 0.0	35.602	846.09		21502140. 684855.	13209836.	34711976. 684855.
$\begin{array}{c} 6309001\\ 6309003\\ 6309004\\ 6309005\\ 6309005\\ 6309005\\ 6309005\\ 6309005\\ 6309005\\ 6309010\\ 6309010\\ 6309010\\ 6309012\\ 6309112\\ 6309112\\ 6309125\\ 6309125\\ 6309205\\ 63092212\\ 6309221\\ 6309225\\ 6309225\\ 6309226\\ 6309227\\ 6309227\\ 6309227\\ 6309226\\ 630927\\ 630$		8776655447221-00998877665554473					88888888888888888888888888888888888888	100499, 752 10074, 084 10049, 14 10024, 21 9974, 23 9974, 23 9974, 37 9924, 55 9824, 55 9874, 75 9824, 96 9824, 96	- 644567. 644567. 645781. 645781. 645781. 645781. 645781. 645781. 6457451. 6457551. 6457555555. 645755555555555555555555555555555555555	00000000000000000000000000000000000000	
630900	394.20	72.05	0.0	1070.40	0.0	1070-403	25364.43	301854.14	20412660.	0.0	20412660.
HYDROELECTA											
	IC WATER U	JT ILIZATI	ION POW	ER STUDY	K IL ICKA	YA 850.0	METER	AYVACIK 190.C	METER INSTA	LLED CAPACIT	Y 123+000 KW
DAT E	RIC WATER (QI	JT ILIZATI QEV	CON POW QSP	QF	95	QE	н	VK	PF	LLED CAPACIT	Y 123,000 KW P
DAT E 631001 6631005 6631005 6631005 6631006 6631006 6631006 6631001 66310010 66310010 66310010 66310010 66310010 66310010 66310010 66310010 6631002 66310000 66310000 66310000000000							H 8444. 73 8444. 738 8444. 595 8444. 595 8444. 595 8444. 595 8444. 595 8444. 595 8444. 595	VK 96645,509 96645,509 96645,509 9757,70,1,505 9757,70,1,505 97547,70,1,505 974204,747 974204,747 974204,747 974204,747 974204,747 974204,747 974204,747 974204,505 974404,505 974404,505 974404,505 974404,505 974404,505 974404,505 974404,505 974404,505 974404,505 97440,505 97540,505 97440,505			
6331002 63310004 63310004 63310004 63310006 63310006 63310006 63310001 63310001 6331001 6331001 63310101 6331011 6331011 6331011 6331011 63310201 6331022 633102 6331000 63310000 6331000000000000000000		QEV 1006055554444433			55 00000000000000000000000000000000000			VK 964 95, 500 965 98, 101 965 97, 500 955 75, 613 965 97, 500 955 75, 613 965 97, 101 965 75, 103 965 97, 103 975 97, 103 9	PF 6750672 674502 674502 674502 674502 67737802 67757802 67757777802 67777802 677778000000000000000000000000000000000	PS 000000000000000000000000000000000000	P
631002 631004 631004 631006 631006 631006 631006 631001 631001 631001 631001 631001 631001 631001 631001 631001 631001 631002 631022 6310225 631025 63105		9 6665554444337352221111000009998888			55 00000000000000000000000000000000000			VK 965454000 965454000 965454000 96545200 96545200 965555 96474500 965555 96474500 965555 9747200 975555 97474500 975555 97474500 975555 97474500 975555 97474500 975555 97474500 975555 97474500 9755555 97474500 9755555 97474500 9755555 97474500 9755555 97474500 9755555 97474500 97555555 97474500 97555555 97474500 97555555 97474500 975555555 97474500 975555555 97474500 975555555 97474500 975555555 97474500 975555555 97474500 975555555 97474500 975555555 97474500 975555555 975555555 97555555 9755555555 975555555 975555555 975555555555	PF 675041. 674957. 674957. 674957. 674957. 67733786. 67733786. 67733786. 67733786. 67733786. 67729907. 672297. 672295. 672295. 672096. 645036. 666738. 666786. 66786. 666786. 66786. 66786. 66786. 66786. 66786. 66786. 667	PS 000000000000000000000000000000000000	P

Table II HYDRDE	4-12 (Ca Lectric	antinu≈) WATER U'	TILIZATIO	N POWE	R STUDY KI	IL I ČKÁVA	850.0 M	ETER ÁY	VÁCIK 190-0 :	RETER INSTALL	ED CAPACITY	123,000 KW
D/	ATE	01	QEV	QSP	QF	QS	QE ⁻	- H	VK	PF	P\$	Р
- 831	201 202	14.06 14.06 14.06	0.00	0.0	35.68 35.68 35.68	00000	35.68 35.68 35.68	842-31 842-27 842-23 842-18 842-18 842-14	8313.57 8291.94 8270.32 8248.70	657341. 657050. 656759. 656395.	0.0	657341. 657050. 656752.
	287 285	14.06 14.06 14.06	0.0 0.0 0.0	-0.0	35.68 35.68 35.68	0.0	35.68	842.18 842.14 842.10	8205-45	655813.	0.0 0.0 0.0 0.0	656395. 656104. 655813.
	2007	12.88	8:8	8:8	- 32:25	0.0	35.68 35.68 35.68 35.68	842 10 842 06 842 02 841 97 841 93	8183.82 8162.20 8140.58 8118.96	655522. 655230. 654866.	0.0	655522. 655230. 654866.
	216 212	14 06	0.0 0.0 0.0 0.0		35.68 35.68 35.68	0.0 0.0	33.68	821 82	8097.33 8075.71 8054.09	654575. 654284. 653993. 653629.		654284 653993 653629
	2) 2 2) 2 2) 2 2) 2 	14 06 14 06 14 06			35.68 35.68 35.68 35.68	0.00	35.68	841.80 841.76 841.72 841.68	8032-46 8010-84	653338. 653047. 652756.	0.0 0.0 0.0 0.0	653338. 653047. 652756.
- 631		14 06 14 06			35.68		12.28	841 63 841 59 841 55 841 55 841 50	7989.21 7967.59 7945.97 7924.35 7902.72	652392. 652101. 651809. 651455.	0.0 0.0 0.0	652392. 652101. 651809. 651445.
631 631	220	14.06 14.06	0.0	8:8	35.68 35.68 35.68 35.68 35.68		35.68	841.46 841.42 841.38	7681.10 7859.48 7837.86	651154. 650863. 650572.	0.0	651154. 650863. 650572.
631 - 631	2225	14.06 14.06 14.06			35.68 35.68 35.68	8.8	35.68	841-33 841-29 841-25	7816.23	650208. 649917. 649626.		650208. 649917. 649626.
- 631 631	227	14.06 14.06 14.06		0.0	35.68 35.68 35.68 35.68		35.68 35.68 35.68	841.20 841.16 841.12 841.07	7751.36 7729.74 7708.11 7686.49	649262. 648971. 648680. 648316.		649262. 648971. 648680. 648316.
631	230 231 _ .200	14.06 14.06 435.86	0.0 0.0	0.0	33:88	0+0	35.68 35.68	841.07 841.03 891.89	7664.87	648024. 20234042.	0.0 0.0	648024. 20234042.
640	181		0.0	0.0	35.68		35.68 35.68 35.68	840.98 840.93 840.89	7641.76 7618.65 7595.54 7572.43 7549.32	647661. 647297. 647095.		647661. 647297. 647005.
640	103 104 105	12257	0.0		35.68 35.68 35.68 35.68		35 68 35 68	840.84 840.79 840.75 840.70	7572.43 7549.32 7526.21 7523.11	646641. 646278. 645986. 645622.		646641. 646278. 645986. 645622.
- 640	107 108 109	14-24	0.0		35.68 35.68 35.68 35.68		35.68 35.68 35.68	840.65 847.61 849.56	7460.00 7456.89 7433.79	645259. 644967. 644603.	0.0	645259. 644967 644603.
	112	12+57 12+57 12+57 12+57 12+57	8.0	8.8	35.68	8.8	35.68 35.68	840.51 840.46 840.42 840.37	7410.67	644240. 643876. 643584.	0.0	644240 643876 643584
640 650		19:34			35.68 35.68 35.68		35.68	840.37 840.32 840.27 840.22	7341.34 7318.23 7295.12 7272.02 7248.91	643220. 642857. 642493. 642129.	0.0 0.0 0.0	642857 642493 642129
640	118	12 57			35.68 35.68 35.68	0.0	35+68 35+68 35+68 35+68	840.18 840.13 840.08	7248.91 7225.80 7202.69 7179.58	641838. 641474. 641110.	0.0	641838. 641474. 641110.
640 640 .640	121	12 57 12 57 12 57 12 57	0.0	0.0	35.68		35.68 35.68 35.68	840.03 839.98 839.94 839.94 839.89	7179-58 7156-47 7133-36 7110-25	640746. 640382. 640091. 639727.		640746. 640382. 640091. 639727.
640 640 640	124 125 126 127	13:57	0.0		35.68 35.68 35.68 35.68	0.0	35.68 35.68 35.68 35.68	839.84 839.79 839.74	7087.14 7064.04 7040.93 7017.82	639363. 638999. 638635.	0.0	639363. 638999. 638635.
640 640	129	12.57 12.57 12.57 12.57	0.0 0.0 0.0 0.0	0.0 0.0 0.0	35.68 35.68 35.68 35.68	0.0 0.0 0.0	35 68 35 68 35 68 35 68 35 68	839.69 839.64 839.59 839.54	7017.82 6994.71 6971.60 6948.49	638271. 637907. 637543. 637179.	0.0 0.0 0.0 0.0	638271 637907. 637543. 637179.
	0131 0100	389.67	0.0		1106+08		1106.082			19916983.	0.0	19916983.
0	AT E	QI	QE V	QSP	QF	QS	QE	H 839.50	VX 6930-64	METER INSTAL	PS	636889. 636597.
640 640 640	202	17.84 17.84 17.84 17.84	0.0		35.68 35.68 35.68 35.68 35.68	000000000000000000000000000000000000000	35-68 35-68 35-68 35-68	839.46 839.42 839.38 839.34 839.34	6912-80 6894-96 6877-11 6859-27	636306. 636015. 635723.		636306. 636015. 635723.
640 640	205	17.84	0.0	0.0	32.08		35.68	839+29	6841.43 6823.58 6805.74	635432. 635141. 634850.	0.0	635432 635141 634850 634850
640 640	2208 1209 1210 2211 2212	17.84 17.84 17.84 17.84	0.0	000000000000000000000000000000000000000	3555 6688888 3555 668888 3555 755 8688 355 868888 355 868888 355 8688888 355 86888888 355 868888888888888888888888888888888888		35.68 35.68 35.68	839.18 839.15 839.11 839.07	6787.89 6770.05 6770.05 6752.21 6734.36 6716.52 6698.68	634559. 634340. 634049. 633758.	0.0 0.0 0.0	634340 634049 633756
640 640	212 213 214 215 216	17.84 17.84 17.84 17.84	0.0	0.0	35.68 35.68 35.68		35.68	839.03 838.98 838.94 838.90	6716.52 6698.68 6680.83	633467. 633103. 632812. 632521.	0.0	633103. 632812
640 640	221 5 021 6 021 7	17.84 17.84 17.84	0.0 0.0 C.0		17.17.17.17.17.17.17.17.17.17.17.17.17.1	ö, ö	88888888888888888888888888888888888888	838.90 838.86 838.82 838.72 838.70	6662.99 6645.14 6627.30	632230	0.0 0.0 0.0	632230 631938 631647
640 640	1217 0218 0219 0220 0220	17.84 17.84 17.84 17.84	8:8	0.0	35.68 35.68 35.68		35.68	838.70 838.70 838.60	6591 61 6573 77 6555 93	631647. 631356. 631065. 630774.	8.8	631 156 631065 630774
		17.84	0.0 0.0 0.0 0.0	0.0	35.68	0.0	32+00	838.58	6538.08 6520.24 6502.39	630483. 630192. 629900. 629536.	0+0 0+0 0+0	630483 630192 629900 629536
640 640	02225 02226 02227 02228 02229	17.84 17.84 17.84 17.84 17.84 17.84 17.84			35.68 35.68 35.68 35.68 35.68		35.68 35.68 35.68 35.68	838.49 838.45 838.41 838.37	6698.63 6662.99 6662.99 6662.99 6662.99 6657.46 6577.73 6577.73 6573.90 6572.94 6572.95 6552.24 6552.25 6552.25 6456.81 6443.02	629245. 628954. 628653.	0.0 0.0	629245. 628954. 628663
	0200	517.36	0.0		1034.72		1034.722		193744.12	18351544. 628954.	0.0	18351544
- 641 641	0301 0302 0303	**************************************	776888888888888999999999999999999999999		35555555555555555555555555555555555555	00000000000000000000000000000000000000	20000000000000000000000000000000000000	838.41 838.44 838.51 838.55 838.55 838.55 838.55 838.55	50 50 50 50 50 50 50 50 50 50	628954. 629173. 629682. 629682. 629973.	121983. 122026. 122087. 122124. 122181. 122237.	750937 751199 751546 751806 752154 752501
641 641	0305 0305 0305 0306 0307 0307 0308	58.55 58.55 58.55	0.48 0.48 0.48	0.0	35.68 35.68	6.92 6.92	42.60	838.50 838.62 838.60	6523.89 6539.36 6554.84	630483. 630483. 630774.	1222376	15111
27	X3YX-	58-55 58-55 58-55	0.48 0.48 0.48	8.8	35.68 35.68 35.68 35.68	6.92 6.92 6.92	42.60	838.69 838.73 838.76	6585.79 6601.25	629973. 630266. 630483. 630774. 630992. 631283. 631502. 631502.	122435. 122477 122534	75397 75432
64	0311 0312 0313 0314 0315 0315 0316 0316 0318	58.55 58.55 58.55	0.48 0.48 0.48	000000000000000000000000000000000000000	35.68	6.92 6.92	42.60	838.83 838.87 838.90	6637.20 6647.67 6663.14	632011. 632302. 632521. 632812.	122576.	754939 755949 75554 75554 75580 75615 75641 75641
- 22		58 55 58 55	0.49	8.8	35.68 35.68 35.68	6.92 6.92 6.92	42.60	838.94 838.97 839.01	6694.07 6709.54 6725.01	633030. 633321. 633540. 633540. 63831. 634049.	122774. 122830. 122873.	75580 75615 75641
64 64	0319 0320 0321 0322	58 55 58 55 58 55	0.49		355.68 355.68 355.68 355.68	0.92 6.92 6.92	42.60 42.60 42.60 42.60 42.60 42.60 42.60 42.60 42.60 42.60 42.60 42.60 42.60 42.60 42.60 42.60 42.60 42.60		6709.54 6725.01 6740.47 6755.94 6775.94 6786.86 68027.32 6817.79 6833.25 6843.11 6843.11	633831. 634049 634340.		75736
64 64	0322 0323 0324 0325 0326	28.22	0.49		35.68	6.92 6.92	42.60 42.60 42.60	839.18 839.22 839.25	6786.86 6802.32 6817.79	634340. 634559. 634650. 635068. 635068.	123127- 123169- 123226-	75797 75823 75858
22	0327	58.55 58.55 58.55 58.55 58.55 58.55 58.55 58.55	0.49 0.49 0.49	0.0	35.68 35.68 35.68 35.68	6.92 6.92	42.60 42.60 42.60 42.60	839.32 839.32 839.35 839.42 839.46	6848.71 6864.16 6879.62 6895.00	635578 635796 636087 636206	123268. 123310. 123367. 123409. 123466.	75910 75910 75945 75971 76006
64	0329 0330 0331			0.0	33.00					636306. 636597. 19616294.	123466:	23420600
-		1815.05 23663.97	15.05		1106.08					2448 27524.	-	396758536
	agent 1	< 3003 · Ví	070464									

DAT E	qt	QEV	QSP	QF	Q5	QE	н	VK	PF	PS	P
$\begin{array}{c} 1 \\ 2 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4 \\ 4$				35.68	9212147 922247 922247 92229 92227 92227 92227 92227 92227 927 9	6060004657860090090090000000000000000000000000000	64554 96,0,36,9914911588 96,0,36,9914911588 96,0,36,9914911588 96,0,36,9914911588 96,0,36,9914911588 96,0,36,9914911588 96,0,36,9914911588 96,0,36,9914911588 96,0,36,9914911588 96,0,36,9914911588 96,0,36,9914911588 96,0,36,9914911588 96,0,36,9914911588 96,0,36,9914911588 96,0,36,9914911588 96,0,36,991491158 96,0,36,991491158 96,0,36,991491158 96,0,36,991491158 96,0,36,991491158 96,0,36,991491158 96,0,36,991491158 96,0,36,991491158 96,0,36,991491158 96,0,36,991491158 96,0,36,991491158 96,0,36,99149115 96,0,36,99149115 96,0,36,99149115 96,0,36,99149115 96,0,36,99149115 96,0,36,99149115 96,0,36,99149115 96,0,36,99149115 96,0,36,99149115 96,0,36,99149115 96,0,36,99149115 96,0,36,99149115 96,0,36,9914915 96,0,36,9914915 96,0,36,9914915 96,0,36,9914915 96,0,36,9914915 96,0,36,9914915 96,0,36,9914915 96,0,36,9914915 96,0,36,9914915 96,0,36,9914915 96,0,36,9914915 96,0,36,9914915 96,0,36,9914915 96,0,0000000000000000000000000000000000	7051-173 7732:30 77472:80 7760-222 7760-222 7760-222 80195-175 80195-10 80195-10 84555-123 85710-54 9710-54 9710-5	630780. 645075. 645186. 645186. 645075. 65505731. 6550593. 6550593. 6550745. 6550745. 6550745. 6550745. 6550745. 665089. 6652965. 6650745. 6650745. 6670475. 6770475. 6770475. 6770475. 676921. 676921.	1224913. 1224913. 1224913. 125131. 125131. 125131. 125131. 12552. 125255. 125555. 125255. 1255555. 1255555. 1255555. 1255555. 12555555	762669. 767797. 770317. 11651993. 11651993. 11651993. 11651924. 11982249. 11982249. 11982249. 11897108. 11897108. 11897108. 11897172. 10
640400	5524.70		154.04			2466.392		261585.35	19877673.	26208071-	46085744.
$\begin{array}{c} 640550045\\ 640550045\\ 6406550045\\ 6406550045\\ 6406550045\\ 6406550045\\ 6406550045\\ 6406550045\\ 6406550045\\ 6406550045\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 640655000\\ 6406005\\ 640005500\\ 640005500\\ 640005500\\ 640005500\\ 640005500\\ 640005500\\ 640005500\\ 640005500\\ 640005500\\ 640005500\\ 640005500\\ 640005500\\ 640005500\\ 640005500\\ 640000500\\ 640000500\\ 640000500\\ 640000500\\ 640000500\\ 640000500\\ 640000500\\ 640000500\\ 6400000\\ 6400000\\ 6400000\\ 6400000\\ 6400000\\ 6400000\\ 6400000\\ 6400000\\ 640000\\ 640000\\ 6400000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 64000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 640000\\ 64000$		44779002457801134477002885679 946790024578011344677002885679 94890000000000000000000000000000000000	00000000000000000000000000000000000000	04088808888888888888888888888888888888	49.522	83.5.22702000 83.5.22702000 83.5.227020000 83.5.2270200000 83.5.2770200000000000000000000000000000000	191772777777777777777777777777777777777	9870.461 9970.461 10055.457 1001243.176 10057.458 10057.458 100585.456 10075	670086, 67917, 680342, 68147, 68147, 68147, 68147, 68147, 68147, 68147, 68147, 68147, 68147, 68147, 68147, 68147, 69144, 70010, 700, 700, 700, 700, 700, 700, 7	941110- 9425424 942542- 9457727- 9457120- 9457120- 9501818- 9501818- 9501818- 9501818- 9501818- 9501818- 9501818- 9501818- 9501818- 950182- 95018- 95018- 95018- 950182- 950182- 950182- 95018- 95018-	1619196. 1621802. 1627401. 1627191. 1627191. 1637619. 1637619. 1637619. 1637619. 1637619. 1637619. 1637619. 1637619. 1642834. 1642834. 1642847. 1650897. 1671851. 1685416. 1685416. 1685416. 1685416. 1685416. 1687676. 1689767. 1699677. 1699777. 1699777. 1699777. 1699777. 1699777. 1699777. 1699777. 1699777. 1699777. 1699777. 1699777. 1699777. 1699777. 1699777. 1699777. 1699777. 1699777. 169977
640500	5512.11	67.26	0.0	1106-08	1535.12	2641.202	6267.23	348074.22	21510292.	25853569.	51364261.
HYDROELECTI DAT E	RIC WATER QI	UT ILIZAT QEV	ION POW QSP		K ILICKA QS	YA 850.0 Qe	METER A	4YVACIK 190+0 VK	NETER INSTA PF	LLED CAPACIT PS	Y 123,000 KW P
					S 5277727272727272 S 5565575272727272727272 44444444444444444444444						
DAT E 6406003 6406003 6406005 6406005 6406005 6406005 64060101 64060101 64060101 64061123 64061123 64061123 6406115 6406115 6406115 6406115 6406215 6406223 640623 640623 6	01 23233333333 99999999999999999999999999	¥ 44465551266665777777888889900000 7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.	, 000000000000000000000000000000000000	GF G87595050505050505050505050505050505050505	SSCACOLORS SSCALORS SSCACOLORS SSCALORS SSCACOLORS SSCALORS SS	GE 85.20000 85.20000 85.20000 85.20000 85.20000 85.20000 85.20000 8	H 67767215687012457740014770759124598 377367424444446455555566867877591 44499707025555555555687849494949494 444944444444449455555556556878498888 888888888888888888888888888888	VK 125605.4.8907.2343 12667.2017.2017.2017.2017.2017.2017.2017.201	PF 7086556. 708725. 708725. 700909. 700909. 7009311. 7009311. 7009320. 7009320. 7009320. 7009320. 7009320. 7009320. 7009320. 7009320. 7009320. 7009320. 7100035. 7110045. 7110004. 7110000000000. 71000000000000000000000	PS 9.0.2.2.5. 9.8.3.5.4.6.0.7.1.2.4.5.7.0.0.1.8.4.5.7.0.0.8.8.8.0.5.9.7.7.0.0.8.8.8.0.5.7.7.0.0.8.8.8.0.5.7.7.0.0.8.8.8.0.5.7.7.7.0.6.8.8.8.0.5.7.7.7.0.6.8.8.8.0.5.7.7.7.0.6.8.8.8.0.5.7.7.7.0.6.8.8.8.0.8.8.8.0.5.7.7.7.0.6.8.8.8.0.8.8.8.0.5.7.7.7.0.6.8.8.8.0.8.8.8.0.8.8.8.0.5.7.7.7.0.6.8.8.8.0.8.8.8.0.8.8.8.0.8.8.8.0.5.7.7.7.0.6.8.8.8.0.8	P 1692195- 1692493- 1692632- 1693753- 1693753- 1693753- 1694281- 1694281- 1694281- 16948075- 16948075- 1695480- 1695480- 1695480- 16955- 1700016- 170055- 170055-
DAT E 6406001 6406003 6406003 6406003 6406003 6406003 6406004 6406010 6406013 6406013 6406013 6406013 6406013 6406013 6406013 6406013 6406023 64062235 6406225 6406225 6406230	II 3779947979797979797979797979797979797979	U 444555532 2.22227222222222222222222222222222222	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	GF G87595050505050505050505050505050505050505		GE 20202020 0000000000000000000000000000	H 67767215687012457740014770759124598 377367424444446455555566867877591 44499707025555555555687849494949494 444944444444449455555556556878498888 888888888888888888888888888888	VK 8776551224257457895556436 925612370122757467895512975555693 12266575901277774657895556435 122656512244578955556435 12265657777746578955555555555555555555555555555555555	PF 7088556. 708872557 70809053. 7009311. 7099311. 7099311. 70993226. 70993226. 71001355. 71001355. 71001355. 71001355. 71001355. 71001355. 71001355. 71001355. 71001355. 71001355. 7110131. 71111131. 71111131. 71111131. 7111131. 7111131. 7111131. 7111131. 7111131. 71111131. 71111131. 71111131. 71111131. 711111131. 71111111. 71111111. 71111111. 71111111. 71111111. 71111111. 711111111	PS 98354442.5. 98354442.5. 98354442.5. 98854444.9. 99844444.5. 99844444.5. 9985456555. 9985456555. 9985456555. 9985456555. 9985456555. 998545455. 998545455. 998545455. 998545455. 998545455. 998545455. 998845440. 1414.	P 1692195. 1692195. 1692238. 1692238. 1693238. 1693759. 1694281.2. 1694281.2. 1694281.2. 1694281.2. 1694281.2. 1694975.2. 1694975.2. 1694976.2. 1694976.2. 1694976.2. 1694976.2. 1694976.2. 1695972.2. 1695972.2. 1695975.2. 1695016.2. 1700189.1. 1700516.1. 170075.2. 170075.

Table 114-12 (Continue) Hydroelectric water utilization power study kilickaya 850.0 meter ayyacık 190.0 meter installed capacity 123,000 kw

DATE		GEN		QF		QE	——— H	VK	PF	PS	
		1:78	-8:8-			-57:68-	翻:{:	11261.75 - 11208.68 -11155.62 -11102.59	694608. 693953. 	426732. 426330. 425972. 425615. 425257.	1121340 1120283 1119343
		2:8	-8.8		21.92	-57.60 -57.60 -57.60	847.18 841.10 -	-1102.59	692789.	425615.	1118404 1117463 1116405
		-2:53-	8:8		21.92	57.60	847.10	11049.58 10996.58 10943.61 10943.61 10890.65 10837.71 10784.79	690969. 690387.	424497.	1115466 1114526 1113468
					21.92		846.68 846.68 846.59 846.51		690387. 689732. 689149. 688494.	425257. 424854. 424497. 424139. 423736. 423379. 422976. 422976.	1112528
		4.52			-21.92-	57.60	846-51 846-42 846-34	10626-14	6891494 687912 687912 687257 686674 686674	422216. 421858. 421456.	1110530 1109473 1108532 1107475
		-1:1		17575555555555555555555555555555555555	<u></u>	57 60	846.34 846.25 846.16	10573-30 10520-47 10467-67	686019. 685364. 684782.	421456. 421053. 420696. 420293.	1106417
<u> \$\$8817</u>		444084470871	ŏ.ŏ.		21.92 21.92 21.92		845.99	10467.67 10414.88 10362.11 10309.37	685364. 685364. 684782. 684127. 683472. 682817. 682817. 682162. 681579.	420293. 419891.	1103363
640819 640820 640821 640821 640822		4-34			21.92 21.92 21.92 21.92 21.92 21.92 21.92 21.92 21.92 21.92 21.92	57.60	845.90 845.81 845.64 845.64 845.55 845.46 845.37	10203.93 10256.64 10203.93 10151.23 10098.56 10098.56 -9993.28 -9993.28 -9940.67	682162. 681579.	419891. 419488. 419086. 418728. 418326.	110230 110124 110030 1099250
				- 18:78	-21.92-	57.60 57.60 57.60	845.46 845.37	10045.91	680924 680269 679614 678959	417923. 417521. 41751.	109619 109713 109607
					21.92	- 57-60	845.28 845.19 845.10 845.01 845.01	- 9888.07 - 9885.50 9782.95 9730.41	678304.	416716-	1095020
	- 0.23 - 0.23 - 0.23		0.0	_ 35.68 _ 35.68 _ _35.68 _	21.92 21.92 21.92 21.92 21.92 21.92	57 60 57 60 57 60	845.01 844.91 844.62	9782.95 9730.41 9677.89	676994. 676266. 675611.	415911. 415464. 415061.	109290 1091730 109067
640831	266.13			1106-08			6230.64	324521.44	21243964.	13051223.	3429518
	-10.52 10.52 10.52 10.52 10.52 10.52	-2-37	8.0	35.688 35.699 35.6999 35.6999 35.6999 35.6999 35.6999 35.6999 35.6999 35.69999 35.6999 35.6999 35.69999 35.699999 35.699990 35.6999990 35.6990		35.68 35.68 35.68	844.77 844.68 844.63 844.58 844.53	9650.42 9622.96 9595.50 9568.04	675247. 674956. 674592.	0.0	67524 67495 67459 67459
	10.52	-2.30	- 0.0 - 0.0 - 0.0	35.68	0.0		844.63 844.50	9568.04 9540.59 9513.15 9485.71	674592. 674228. 673864. 673864. 673500.		67422 67386 67350
640905 640906 	10.52 10.52 10.52	2.29 2.28 2.28	0.0 0.0	- 16	- 8-8 -	- 35-65	844.48. 844.48.	9485.71 9458.28		0.0	67313
640909 640910 640911	10 + 52 10 + 52		0.0	35.68	8.8	35.68 35.68 35.68	844.53 844.43 844.43 844.39 844.39 844.29 844.29 844.24 844.19	9458-28 9450-86 9403-42 93748-62 93748-62 9321-21 9293-82 9265-43 9239-66 92391-66 9211-66 9214-23	672401. 672117. 671753. 671309.	8.0	67248 67211 67175 67138
640913	10 52	2.25	0.0 0.0	35.68 35.68 35.68 35.68		32.29	844.24 844.19 844.14	9321.21 9293.82	671025.	0.0	67102 67066
640914 640915 640916				35.68	8.8	35.68 35.68 35.68 35.68	844.19 844.19 844.09 844.04 844.04 843.99 843.99	- 9266.43 9239.04 9211.66	- 670297. 669933. 669569. 669206.		67029 66993 66956
640917 - 640918 - 640919	10.32	- 2.22		35.68 35.68 35.68		33.68	843.94 843.89 843.84	9184.29 9156.93 9129.56	668478.	0.0	66920 66884 66847 66811 66775
640920 640921	10.52	- 2.12	0.0 0.0 0.0	-35.68 35.68 35.68	8.8	35.68	843.84 843.79 843.74 843.69 843.64	9156-93 9129-56 9102-21 9074-86 9047-52 9020-18	668114. 667750. 667386. —		66738
<u>640923</u>		2.19 2.18 2.18	0.0	35.68 35.68 35.68 35.68	0.0	35-68 35-68 35-68 35-68	843.64 -843.59-	9020.18 8992.85 8965.52	667022. 666658 666294.	0.0	66702
640925. 640926 640927_ 640928	10 • 52 10 • 52	2.19 2.18 2.18 2.16 2.15 2.15		33.68	8.0	35.68 35.68 35.68	843.59 843.54 843.49 843.49 843.49 843.39 843.34	8938.20	665930.	0.0	66629 66593 66556 66520 66483
	10.52 10.52	215	0.0	35.68	8.8	35.68	843.39 843.34	8683.58 8856.28	665566. 665202. 664838.	0.0	66483
						-		-			
640900	315+60	66.97		1070.40	0.0	1070.402	5321.86	277588.62	20102506.	0.0	2010280
					0.0	1070.402	15321-86	277588.62	20102506.	0.0	2010280
					0.D -	1070.402	15321-86	_ 277588.62	20102506.	0.0	2010280
··· ,	315.60	66.97	D.O	1070.40	-						
	315+60	66.97 UTILIZATI QEV	D.0 ION PON QSP	1070.40 ER STUDY	K 1L 1CKA	YA 850.0 QE	METER AN	YVACIK 190. 0 VK	NETER INSTAL PF	LED CAPACIT	Y 123,000
	315.60	66.97 UTILIZATI QEV 1:07	D.0 ION POW QSP 0.0	1070.40 ER STUDY	K 1L 1CKA	YA 850.0 QE	METER AN	YVACIK 190. 0 VK	METER INSTAL PF 66410. 664110.	LED CAPACIT PS 0.0 0.0	Y 123,000
	315.60 	66-97	D.0 IGN POW QSP 0.0 0.0 0.0	1070.40 ER STUDY	K 1L 1CKA	VA 850.0 QE 35.68 35.68 35.68	METER A1 H 843.29 843.24 843.14	VVACIK 190.0 VK 8030.16 8074.04 8774.93 8725.70 8679.60 8699.60	METER INSTAL PF 664110. 663143. 663019. 663019.	LED CAPACIT PS 0.0 0.0 0.0 0.0 0.0	Y 123,000
HYDROELECTRI — 641001 — 641001 — 641001 — 641001 — 641001 — 641001 — 641001	315.60 C WATER 01 10.63 10.63 10.63 10.63	66.97	D.0 D.0 ION POW QSP 0.0 0.0 0.0 0.0 0.0 0.0	1070.40 ER STUDY OF 35.68 35.68 35.68 35.68 35.68 35.68 35.68	K1L1CKA QS 0.0 0.0 0.0 0.0 0.0	VA 850.0 QE 35.68 35.68 35.68	METER A1 H 843.29 843.24 843.14	VACIK 190.0 VX 8030.16 8504.04 8777.93 8751.83 8751.84 8754.00 8673.09	METER INSTAL PF 664410. 663746. 663383. 663019. 662727. 662264.	LED CAPACIT PS 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	Y 123,000 66447 66417 6637 6637 6637 6637 6637 6637 6637 66
HYDROELECTRI —	315.60 C WATER 01 10.63 10.63 10.63 10.63	66.97 UTILIZATI QEV 1.07 1.06 1.06 1.06 1.05 1.05	0.0 ICN POW QSP 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	1070.40 ER STUDY OF 35.68 35.68 35.68 35.68 35.68 35.68 35.68	K1L1CKA QS 0.0 0.0 0.0 0.0 0.0	VA 850.0 QE 35.68 35.68 35.68	METER A1 H 843.29 843.24 843.14	VYACIK 190.0 VX 8030.16 807.03 807.03 807.03 807.03 807.44 807.43 807.43 807.43 807.43 807.43 807.43 807.43 807.45	METER INSTAL PF 664410. 663746. 663383. 663019. 662727. 662264.	LED CAPACIT PS 0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-	Y 123,000 66447 66417 6637 6637 6637 6637 6637 6637 6637 66
HYDROELECTRI —	315.60 C WATER 01 10.63 10.63 10.63 10.63	66.97 46.97 QEV 1.07 1.06 1.06 1.06 1.05 1.05 1.05 1.05 1.05 1.05	D.0 D.0 ION POW QSP 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	1070.40 ER STUDY OF 35.68 35.68 35.68 35.68 35.68 35.68 35.68	K1L1CKÅ	VA 850.0 QE 35.68 35.68 35.68	METER A1 H 843.29 843.24 843.14	VYACIK 190.0 VX 8030.16 807.03 807.03 807.03 807.03 807.44 807.43 807.43 807.43 807.43 807.43 807.43 807.43 807.45	RETER INSTAL PF 664410. 663746. 663746. 663783. 66309. 662727. 662727. 662764. 662709. 662709. 660908. 660908. 660908. 660908. 660908. 660180. 6601	LED CAPACIT PS 0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-	Y 123,000 66447 66417 6637 6637 6637 6637 6637 6637 6637 66
HYDROELECTRI DATE	315.60 OI 0.63 10.63 10.63 10.63 10.63 10.63 10.63 10.63 10.63 10.63 10.63 10.63 10.63 10.63 10.63 10.63 10.63 10.63	66.97 46.97 QEV 1.07 1.06 1.06 1.06 1.05 1.05 1.05 1.05 1.05 1.05	10N POW 95P 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	1070.40 ER STUDY OF 35.68 35.68 35.68 35.68 35.68 35.68 35.68	K 1L 1CKA Q.O Q.O Q.O Q.O Q.O Q.O Q.O Q.O Q.O Q.O	VA 850.0 QE 35.68 35.68 35.68	METER A1 H 843.29 843.24 843.14	VYACIK 190.0 VX 8030.16 807.03 807.03 807.03 807.03 807.44 807.43 807.43 807.43 807.43 807.43 807.43 807.43 807.45	RETER INSTAL PF 664410. 663746. 663746. 663783. 66309. 662727. 662727. 662764. 662709. 662709. 660908. 660908. 660908. 660908. 660908. 660180. 6601	LED CAPACIT PS 0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-	6644 6644 6637 6637 6637 6637 66290 6679 6605 6605 6605 6605 6605
HYDROELECTRI DATE	315.60 IC WATER 01 0.63 10	66.97 46.97 QEV 1.07 1.06 1.06 1.06 1.05 1.05 1.05 1.05 1.05 1.05	10N POW 95P 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	ER STUDY OF 35.68	K 1L 1CKA Q.O Q.O Q.O Q.O Q.O Q.O Q.O Q.O Q.O Q.O	VA 850.0 QE 35.68 35.68 35.68	METER A1 H 843.29 843.24 843.14	VYACIK 190.0 VX 8030.16 807.03 807.03 807.03 807.03 807.44 807.43 807.43 807.43 807.43 807.43 807.43 807.43 807.45	RETER INSTAL PF 664110. 663746. 6637474. 6637477. 662764. 66200. 661050. 661050. 661050. 661050. 661050. 661050. 661050. 6659816. 65982. 65982. 65982. 65982. 65982. 65982. 65982. 65982. 65982. 65982. 65982. 6598. 6588.	LED CAPACI T PS 0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-0 0-	6644 6644 6637 6637 6637 6637 66290 6679 6605 6605 6605 6605 6605
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HYDROELECTRI DATE	315.60 IC WATER 01 0.63 10	4697 4697 UTILIZATI QEV 1.07 1.06		ER STUDY OF 35.68	K 3L 1 CKA QS 0.00 0.	VA 850.0 QE 35.68 35.68 35.68	METER A1 H 843.29 843.24 843.14	VYACIK 190.0 VX 8030.16 807.03 807.03 807.03 807.03 807.44 807.43 807.43 807.43 807.43 807.43 807.43 807.43 807.45	RETER INSTAL PF 664474. 6647140. 6647140. 6647140. 6647140. 6647140. 6647140. 6647072. 667070. 6670708. 6670708. 6570708. 657072. 65707	LED CAPACIT PS 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	Y 123,000 6644 6637 6637 6633 6620 6627 6627 6627 6627 6627 6627 6627
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HYDROELECTR	ALC MAILS C										
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650400	5899.80	34.45	273.48	1070.40		2564.712529	10.99	261744.56	19878111.	28096188.	4797429
- 65050 - 650050 - 6500	97777777777777777777777777777777777777	45789001245678002802734567802734578087878787 4******************************		626636465666986666868886868888888888888888888	<u>\$15500055555555555555555555555555555555</u>		55555555555555555555555555555555555555	9447.82 9915.864 99813.455 10051.024 10051.024 101186.50 1012524.299 104557.756 105257.456 105757.85 105575.166 105757.85 105757.85 105757.85 105757.85 105757.85 105757.85 105757.85 105757.85 117557.85 117557.85 117557.85 117557.85 117557.85 117557.85 117	$\begin{array}{c} 677794,\\ 677849,\\ 677849,\\ 67849,\\ 682016,\\ 882016$	940706. 9418029. 9418029. 9418029. 9418029. 941929. 941929. 941929. 941929. 941929. 941929. 941929. 95192. 95192. 955555. 95555. 95555. 95555. 95555. 95	1616201 1622454 1622454 162651 162651 162651 1636304 163754 163754 163754 163754 163754 163754 164505 16450
650500	4804.07	65.74	0.0	1206-08	1271.29	2377.372625	K7 30	338290.15	21402276.	24532881.	459351
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650801 650802 650803			QS P	QF	Q \$	QE	н	VK	PF	PS	
6500655 655056076 655056076 655056076 655056076 6550561123 65505616776 65505616776 65505616776 65505616776 65505616776 65505616776 65505616776 6550562776 655056276 655056276 6550562776 6550562776 6550562776 6550562776 6550562776 65505776 655057776 655057776 655057776 655057776 655057776 655057776 655057776 655057776 6550577776 6550577776 6550577776 655057777777777		44444498642086419753197531975319864208 444444933324222222222222222222222222222	000000000000000000000000000000000000000	10160000000000000000000000000000000000		86889888888888888888888888888888888888	43526798877003447221333444444444444444444444444444444	98073 66739 8,0,7,796 8,0,7,7,96 8,0,7,706 8,0,7,707 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,7,706 8,0,707	$\begin{array}{c} 687402.\\ 686747.\\ 6869747.\\ 6869747.\\ 6884707.\\ 6884707.\\ 6884707.\\ 6884707.\\ 6884707.\\ 6884707.\\ 6884707.\\ 688707.\\ 688707.\\ 6770250.\\ 677$	422305, 421902, 421902, 42045, 42045, 42045, 42045, 419301, 419302, 419394, 419340, 419340, 419340, 419340, 419340, 419340, 419340, 419340, 419355, 419305, 41	$\begin{array}{c} 11097070\\ 110074502\\ 110074502\\ 11007402\\ 11003207\\ 11003207\\ 11003277\\ 110030277\\ 100976372\\ 100976377\\ 10995373\\ 10995373\\ 10995373\\ 10995373\\ 10995373\\ 10995373\\ 1097532\\ 1097532\\ 1097532\\ 1097532\\ 1097532\\ 1097532\\ 10079537\\ 10079537\\ 10079537\\ 10079537\\ 10079537\\ 10079537\\ 10079537\\ 10079537\\ 10079537\\ 10079537\\ 10079537\\ 10076337\\ 10076337\\ 1077637\\ 1077637$
650800		129.97				1785.602	26195.48	•	20988040.	12893998.	33882038
12314 12		6654432210998776554332100998876 111411111100988776554332200098876		8650505085050505050505050505050505050505		56855580056688585666858666858666858668586685868586858685858555555	843.07 843.01 842.95 842.89 842.83 842.77 842.71	8595 8596 8596 8697 8697 8697 8697 8697 8697 8697 86	$\begin{array}{c} 655957.\\ 6457926.\\ 6457926.\\ 6457926.\\ 6457926.\\ 6457926.\\ 6457926.\\ 6457926.\\ 6457926.\\ 645926.\\ 645926.\\ 645926.\\ 645926.\\ 645926.\\ 645926.\\ 655926$		6404 6404
65 090 0	185.70	61.90	0.0	1070.40	0.0	1070.402	25278.45	254244. 89	19786837.	0.0	19786837

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651000	547.46	29.30	0.0	1106.08	0.0	1106.0826074.90	239141.62	20110375.	0.0	20110375.
6511004 65511004 65511004 655110056 655110000000000						55.468 840.47 35.468 840.47 75.468 840.47 75.468 840.47 75.468 840.21 75.468 85.768 75.468	74628.01 77386.01 77377.1.52 7737.1.52 7737.1.72 77370.1.72 77370.1.72 77370.1.72 77370.1.72 77370.1.72 77370.1.72 77255.00 77055.00 77050	443048 319948 443948 6439712 6439712 6439712 6439712 644224973 644224973 644224973 644225 644225 6442059 6442059 6442059 6442059 64410 64410 644000 644000 644000 644000 644000 644000 644000 644000 644000 644000 644000 64400000000	00000000000000000000000000000000000000	644312, 6443146, 6443146, 643512, 643512, 643512, 643512, 643517, 642517, 642517, 642514, 64251, 64251, 64251, 64251, 64251, 641
651100	669.60	9.76	0.0	1070.40	0.0	1070.4025203.30	216534.21	19239841.	0.0	19239841.

DATE	01	QEV	QSP	⁻ QF	QS	QE H	AK	PF	PS	
127745 860078901123456178901234 860080789012345617889012348 8600807890789012348561788 86008080789012348561788 8600808080808080808080808080808080808	999999999999999999999999999999999999999	000000000000000000000000000000000000000	000000000000000000000000000000000000000				0014.492 9412 9412 9412 9412 9412 9412 9412 9	638094 66879766 6677766 6677766 6677725 6677766 6677725 6677725 6677725 6677725 6677725 6677725 6677725 6677725 6677725 6677725 6677725 6677725 667776 6677725 667776 6677776 6677776 66777777		107884647323797878888888888888888888888888888888
651222 6512224 6512225 6512226 6512227 6512228 6512228 6512231	28.19 28.19 28.19 28.19 28.19 28.19 28.19 28.19 28.19	0.0 0.0 0.0 0.0 0.0	0.00	35.68 35.68 35.68 35.68 35.68		35.68 839.25 35.68 839.23 35.68 839.23 35.68 839.22 35.68 839.20 35.68 839.18	6809-73 6802-24 6794-75 6787-27	635068+ 634923- 634850- 634704- 634704-	0.0 0.0 0.0	6349 6348 6347 6345
651200	873.89	0.0	0.0 1	106.08		106.0826022.37	213887.05	19728025.	0.0 0.0	197280
66010102 66001035 66001035 66001035 66001035 66001035 66001035 66001035 66001101 66001103 66001103 66001103 66001103 66001203 66001223 66001223 66001223 66001223 66001223 66001223 66001223 66001223 66001223 66001223 66001223 66001223 66001223 66001230 66001231	21277277777777777777777777777777777777	00000000000000000000000000000000000000	000000000000000000000000000000000000000	80888000000000000000000000000000000000	000000000000000000000000000000000000000	241 241 241 241 241 241 241 241 241 241	4.73 844,07 844,07 844,07 844,07 844,07 844,07 844,07 844,07 844,07 844,07 844,07 844,07 844,07 844,07 844,07 844,07 844,07 84	$\begin{array}{c} 349965.\\ 6355942.\\ 6355942.\\ 6355942.\\ 6355942.\\ 6355942.\\ 635942.\\ 635942.\\ 635952.\\ 6379122.\\ 6379122.\\ 6389766.\\ 6389766.\\ 6389766.\\ 6389766.\\ 6389766.\\ 63997279.\\ 639972$	00000000000000000000000000000000000000	66597826115937900614997 3337367782800 3337367782900614997 3337367770577829700614977 33373879700614977 3337387770574401727155744577 34451770544577
	1959-51	0-0	0.0	1106.08	0.0	1106.0826043.90	224057.90	19884735.	0.0	19884
660100 HYDROELECTR	1959.51	0.0		1106.08 R STUDY K						
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660825 660827 660828 660829 660830 660831	8.12 8.12 8.12 8.12 8.12 8.12	4.274 4.227 4.4220		15555 1555 1555 1555 1555 1555 1555 15	22222222222222222222222222222222222222	57.60 57.60 57.60 57.60 57.60	845.45 845.36 845.27 845.18 845.08	10047.01 10043.24 9989.49 9935.76 9882.05 9828.37	680851. 680196. 679541. 678886. 678231. 677503.	418281. 417878. 417476. 417074. 416671. 4166224.
66 0800 66 0901	251.72 9.40		0.0 0.0	1106.08 35.68	679.5Z	1785.602	6239.09 845.03	329732.89	21305468. 677139.	13089009. 0.0
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	9.40	2:17	0.0	35.60	0.0	35.68	843.55	8972.21	666367.	ō,ŏ
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	TURUELELI		-			KILICKAT	A 850.0	METER A		PETER INSTA	LLED CAPACITY	123,000 KW
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	661200	630.23	0.0		1106.08	0.0 1	106-082	6044.31	224187-04	19887720.	0.0	19887720.
	670102,55 670102,55 670102,55 670102,55 670102,55 670102,55 670102,55 670102,55 670111,5 670111,5 670111,5 670111,5 670111,5 670112,5 670112,5 670112,5 67012,	17777777777777777777777777777777777777	00000000000000000000000000000000000000	00000000000000000000000000000000000000	00000000000000000000000000000000000000		898898468989888888888888888888888888888		6982-929 699451-075 699451-075 69874-683 69854-68 68854-68 68854-68 68854-68 68854-68 68854-68 68854-68 68854-68 687725-77 66865-77 667923-77 66865-47 66553-647 6553-647 6553-647 66424 6553-647 66424 6553-647 66424 6553-647 66424 6553-647 6553-	637689, 6377998, 6377908, 6377908, 637698, 63508, 6	00000000000000000000000000000000000000	637689, 637106, 637106, 63685, 63685, 6365243, 6355243, 635543, 635569, 635569, 635569, 635569, 635704, 634122, 6335649, 6344122, 6335649, 6344122, 6335649, 632885, 632885, 632885, 632885, 632885, 632885, 632885, 632885, 632885, 632885, 632885, 632885, 632885, 632885, 632885, 632885, 632885, 63288, 6348, 6348, 6348, 6348, 6348, 6348, 63
	670100	529.17	0.0	0.0	1106.08	0.0 1	106.082	6008.72	207814.72	19628670.	0.0	19628670.
н	YORDELECTI DATE	RIC WATER QI	UTILIZAT	TLON POW	ER STUDY OF	KILICKAY/ OS	4 850.0 Çe	METER #	YVACIK 190.0 VK	METER INSTA Pf	LLED CAPACIT	Y 123±000 KW P
н									VK 6406-001 63774-233 635774-235 63576-051 63100-051 62824-83 62824-83 62267-35			
н	DATE 670201 670203 670203 670204 670209 670209 670209 670209 670209 670209 670211 670209 670213 4702013 4702014 6702015 6702201 6702201 6702201 6702201 6702202 6702202 67022 67022 7 67022 7 67022 7 67022 7 67022 7 7 67022 7 7 7 7 7 7 7 7 7 7 7 7 7	01 9999499999999999999999999999999999999	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	95000000000000000000000000000000000000	F 80060000000000000000000000000000000000	20 20 20 20 20 20 20 20 20 20 20 20 20 2	E	H 3773940677965067994064777849 3888866888777477777777777777777777777777	VK	PF 45.4.5 627755567 627755567 627755567 627755567 627755567 627755567 627755567 627755567 627755567 627755567 627755767 6277575767 6277575767 6277575767 6277575767 6277575767 6277575767 6277575767 6277575777 6277577777 6277577777 62775777777 627757777777777	PS 0500000000000000000000000000000000000	P 627544 6277454 62773508 6264075 6264075 6264075 6264075 6264075 6264075 6264075 6264075 6264075 626476 6273508 627555 627555 627555 627555 627555 6275555 6275555 6275555 62755555 62755555 6275555555555
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Table 114-12 (Continue) Hydroelectric water utilization power study kilickaya 850.0 meter Ayvacik 190.0 meter installed capacity 123,000 kw

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Table 11 413	
Kilickaya Power Production Case 10 Reservoir High Water Level 855m	Firm Discharge 46.20m ³ /sec

NEN	4		5 (e :	7 0	9	KANIKI	10	11	1 13	: 1	2	. 3	11-2	IDTAL
39	482035	539264	3(739	295484	. 291490	278489	2154363	283906	271144	276982	273820	254319	*****	107/0/0	
40	485915					•	2932971							1076265 1106093	3826553
41	846688	1058480					3152083							1085710	4851818 4977685
4Z		943717	-		-		2659197							1087562	4382366
43	397208	609403	440011				2318439							1071254	3964095
44	386317	534199	568993	299090	295496		2365995				276953			1078551	4001441
45	256810	275739	277713	285177	260091		1641207				250847			984018	3125126
46	248667	201581	284163	293786	289760	275516	1673873			274135				1053364	3279101
47	270109	282453	271632	276246	270036	254832	1625308			245615				\$43505	3049341
48	235596	273671	277196	286035	260827	Z66409	1619738	265747			249752			960852	3166607
49	236919	27123e	275716	282175	276543	262002	1604591	264701			246079			967254	3061700
50	258766	344212	303095	295528	291125	277078	1769804	282117			269851			1053140	3371047
51	264408	283833	281527	290121	265598	271642	1677129	276776	265875	271544	266984	247773		1052176	3272874
52	368167	617726	368750	297583	253534	279686	2225446	284377	270505	274745	269863	Z29675		1054792	3826324
53	264203	373492	337369	29821¢	294271	280677	1848328	285794	272502	277725	274103	244650	338626	1065180	3542128
54	490343	988584	664182	299863	296505	283350	3023227	286540	275018	279625	275431	245348	265386	1075626	4656775
55	263294	277430	268635	272464	265700	249851	1557374	249993	233563	23243:	222207	155564	208207	868267	2943841
56	224060	261048	262522	270316	264252	248990	1531208	245915	234344	235786	228360	158520	221024	85741C	2963557
57	236973	266355	268430	277072	271722	256974	1577526	258840	243595	244329	236375	206219	226750	930522	2993678
58	238344	267465	266358	274310	268633	253549	1568659	254862	23924 <i>e</i>	239230	23030C	158585	215665	907765	2946551
59	225115	255677	258027	266216	255645	243480	1508164	243731	228518	226322	218537	198328	216272	874105	2842272
60	245282	286723	267075	295883	292294	278600	1686057	283751	270301	274790	269982	235478	261572	1054551	3265531
<i>e</i> 1	259393	276519		273303	266521	250662	1554841	250999	23528e	237685	230539	201957	233586	904867	2984653
€Z	248005	273744		277465	271296	255684	1597591	256454	240508	242314	237928	212494	227647	933244	3024536
63	246933	281673		300179	297404	283954	1862407	285280	276663	261273	276736	254821	271394	1088893	3521574
64	345736	481041		298894		280984	2223366	285805	272248	277176	272885	242405	268936	1064716	3842825
65	345923	441157		296485		277778	1961342	282499	269503	275558	276008	250532	426647	1072641	1716725
66	467148	739405		299200		281398	2562133	286198	272622	277753	27380E	243624	267146	1067805	4183282
59					1963606	7562752	55702365	7667260	7286310	7394995	7252115	6491218	7751695	2842473E	\$\$546C5E
88	332637	456204	356965	289051	284415	270098	1969370	273831	260225	264107	259004	231833	276846	1015165	2555216
88	255938	284802	261161	289051	784414	270098	1669435	273831							
				207031	601413	210048	1057433	273831	200225	264107	259064	231633	254320	1015165	3212755
														Firm Ener	87

Table 11 4-14 Kilickaya Power Production Case 14 Reservour High Water Level 850m Firm Discharge 41 80m³/sec

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NEN	4	5		± 7	e a	9	KAMIKI	10	11	ı ı :	2 1	. :	2 3	11-2	TOTAL
39	256714	377747	346604	251672	247931	236146	1718814	240125	228773	21127	1 230160	21373/	229992	905936	3054867
40	470838	911035				243701	2705464								
41	811837	911035	492876	253624	250139	237976	2957487								4369173 4314603
42	496151	911035	489393	253050	Z48701	236098	2634428	-					233532		4028767
43	340355	731060	527076	254060	249867	237223	2339641						i 228451	895967	3704362
44	30 49 81	643660	560589	257162	253746	Z41564	2261702							918983	3654271
45	216892	237046	2421 53	248998	244313	231342	1420744							852104	2714965
46	218706	372435	537888	256519	252966	240695	1879209							917751	3333043
47	346370	246868	237742	241673	235820	222229	1530702							821826	2772100
48	208915	253812	454637	253389	248662	236055	1695670	238927				-		870794	3015864
49	212751	277950	412050	252264	247454	234565	1637034	=						674164	2972234
50	346811	818717	477728	252651	248469	235719	2382295							886616	3731626
51	225706	245920	266065	253524	249462	237039	1477716							919082	2072533
52	479655	911035	526776	253816	249746	237176	2658204	240260	227552					860023	3953578
53	223253	434330	527422	254883	2510ec	238717	1929685	242349	230355					900325	3320555
54	497434	911035	626732	258333	255661	Z4356C	2792755		235296			208290		916750	4145636
55	225153	239529	232707	235586	226995	214457	1376427	213520	198536			167890		750814	2515789
56	194432	231474	234341	241891	236806	223799	1362743	225380	211986			183566		816146	2614322
57	216671	244710	327481	253447	249241	236507	1530057	239469	226968	229555		197528		878069	2866692
58	226419	274222	414995	253341	248996	236233	1654206	239173	226604	228939		156080		874826	2983096
59	22 00 94	244262	244582	252870	248558	235605	1445971	238752	227109	230390				891112	2801665
60	457803	911035	53009£	254820	251465	239450	2644691	243177	231067	234258		202547	-	897181	40(5515
61	221968	239774	233676	237793	231318	216952	1381483	216506	202259	203856				779053	2501324
62	220068	245021	243973	249885	244612	230949	1434528	232573	219155					856033	2743525
63	253751	620757	881647	256523	25604¢	244057	2514781	248116		240215		216348		928501	3922236
64	306465	626213	594112	257162	253300	240766	2278018	244232	231587			204524		903325	3653520
65	31 0845	569168	485520	253502	249267	236021	2104323	239231	228080	232950	233705	213635	359913	906370	3611837
66	470104	829020	540308	255952	252211	239473	2587068	242717		234032			222979	898015	3950779
99	89851621	44699051	2297431	7058638	6940636	584074	56335846	6669368						24732967	944(888)
88	32 0899	516782	439194	252094	247880	235146					225366			803321	1371747
														~~,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	42 64 131
EA	22,8853	250864	245994	252094	247680	235146	1460831	238192	226312	229758	225366	201885	222317	883321	2864661
														Time Zast	

Firm Energy

															,
NEN	4	5	6	ז	8	9	KAHIKI	10	11	12	1	2	3	11-2	TOTAL
39	404667	61.8535	283616	191722	188392	176825	1865781	181150	171976	175067	172622	160535	239121	680604	2966656
40	523055				193228				179452				496411	117365 -	3673636
41	666199	688405			189875		2216874	182167	175456	160721	178240	155691	268424	· 65415E	2361623
42	547871	688405			167588		2050568	119228	173474	181243	160604	161521	264206	697042	3231444
43	398543	688405	333225	193415	169436	178715	1981743	179704	169296	17097e	· 167128	153296	- 202712	ecose	2024655
44	368901	662284	483161	194199	190585	160754	2020288	- 182548	173816	177115	173338	152801	166651	677070	3105557
45	157439	229531	250636	193014	188656	177576	1237446	179186	168905	169565	164094	143133	157696	645697	2220025
46	241452	642137	472426	153657	1 502 95	179935	1919892	183159	175005	176694	172305	153135	252025	677142 °	3032215
47	360092	256247	1 8 1 1 3 8	183569	177652	165838	1324527	164927	155610	157733	152254	137566	/ 142178	603461	2235033
48	173107	561295	460565	192998	168613	177688	1754670	178430	167483	167414	160936	139245	150385	- 635G7E	2718562
49	158319	465202	297477	191916	187165	176118	1476201	176671	165565	165695	162631	147771	167102	641066	2461040
59	450811	688405	289801	191849	187587	176691	1965144	176402	169295	170874	166316	146610	165574	6:2495	2561615
51	219508	401977	389450	193453	189693	179302	* 1573422	162104	175652	179324	175464	163760	°267136	6542C0	2716661
52	537796	688405	324197	193357	189545	178946	2112250	- 175965	168553	169301	163602	143686	156249	645742	3654206
53	226974	628735	364413	193864	190342	179987	1784315	181651	` 171581	173505	170230	151594	232508	666910	2865384
54	554387	688405	568578	195062	192810	182669	2381911	184348	173910	175045	17042E	150543	165628	669926 -	3401613
55	167037	182971	179535	181039	174671	162470	1047727	160566	147921	144750	135817	121119	127593	549647	1885533
56	152552	311746	350706	153494	189454	178865	1376821	160121	169650	'17203€	168525	148865	154046	655CEC	2410668
57	342121	622535	437367	193401	189463	178661	1963548	175586	168867	169507	164156	143E45	160806		2950315
58	263865	538979	392311	193409	189303	178469	1756336	175377	168572				156715	643154	2725582
59	183807	395383	417031	193414	189395	176348	1557378	179604	170039		167112			663367	25 E354 B
60	530712	688405	352649	19392\$	191022	181107	2117024	182933	172725		168565			663832	3146197
61	176864	202665	183704	187000	101074	169110	1100417	168342	157061		154797	•		606821	2048192
62	338420	605091	292943	191779	186682	174748	1785663		162714		162281			* ⁶ 35788 ₂	2767147
63	366791	688405	666199	195290	193295	183317	2253301		175252					681202	3328286
€4	332908	662363	524801	143875	190036	179285	2083276		169797		166552			~61345E	3065383
65	343105	675483				177376	1878300		169601	-	175572				21072661
66	564686	688405	410157	194066	190540	179629	2227483		170027						2227043
59					5276295		51276726								
66	348286	555258	369281	192357	182435	177691	1831312	176921	169711	171116	167225	149577	202731	657129	2810093
40	176044	101400	107514	103363	1064.10	177454	1116741	110011	169211	131114	14777	145577	166205	657125	2117CI e
ยา	172966	145800	167510	122321	188435	11/651	1114/61	116411	-, 104511	, , , , , , , , , , , , , , , , , , , ,	111623		7 51		
														Firm Ene	TBY

Table II 4-16 Kilickaya Power Production Case 13 Reservoir High Water Level 840m Firm Discharge 35.10m³/sec

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NEN	4	5	6	7	8	\$	KAMIKI	10	11	12	1	2	3	11-2	TOTAL
									• • ·		- 1			•	- 1
39	186792				214151			206395						77516C	2432658
4U	514859				221755		2458574	215103			211742			822154	4040252
41	735464		337970	221861		207725	2512747	210995	202971		205528				° 2823411
42	546594				217076		2317066					18558C			2634081
43	371308	738492	367862	222375	218443	206937	~ 2125421	209043	- 197811		196324				2354101
44	343051	693081	`522974			208732	2210802	211536	201741	205760	201695	178458	154101	767854	3464293
45	184107	206005	214039		216235		1245433	206572	195369	156727	- 190997	167209	163641	750302	2365548
46	233023	617366	459072	222913	219525	208353	2000256	212411	203119	205785	201417	175168	252518	785453	3255678
47	309007	264403	207765	210921	205071	192399	1389566	152214		184109				706102	2455829
48	183464	454290	462173	222474	216243	206595	1767239	208555	196886	197988	191695	167216	181103	753765*	2910682
49	185751	441474	335809	220982	216387	204592	1604995		-				154756 -	155404	2761508
54	438750	791038	329892	220875	216685	205019	2202259	207719	197585	200044				765051	2368371
£1	198131	357892	303925	222887	215187	207990	1510012	211698	203862	208246	20435E	190309	367828	806775	2826213
5Z	546577	791038	360016	222290	218502	207085	2345512	205218	197460	156851	153332	170234	185217	759877	° 3455E22
53	233321	611004	387468	22304E	219531	206350	18€2720	211071	200142	202995		177733		780256	2155665
54	554239	791038	597527	224172	221736	210750	2559462	213497	202264	204464	155665	116560	· 1\$432C	783552	* 3750832
55	193475	208628	203595	2056,44	199068	185616	1156026	184004	170227	167700	158462	141640	148309 '	636025	
56	170689	207979	212051	219422	215136	203553	1226820	205468	194010	* 156747 (192659	170143	152681 `	753555	23E152E
57	302280	53 G 74 O	459702	222756	218902	207349	1941729	205461	197583	199705	194384	171696	150057	763168	2104415
58	268072	472466	344299	222584	218565	206979	1732965	209047	197488	198926	193368	169440	166122	755242	286737c
59	193757	345867	32066C	222742	218822	207063	* 1508911	209453	198954	201531	156929	162044	227331	77545E	2725153
£0	53 64 71	791036	376656	223063	220066	-209256	~ 2358552	212116	201065	203261	158354	174695	190493	777355	353856C
61	19411\$	212568	208033	211783	265683	192756	~1224942	192308	179753	181278	176925	155503	184518		2255627
é2	26914Z	451977	310828	220601	215681	203119	1671348	203878	191597	153788	191432	172341	154724	745158	' 281910E'
63	349814	730871	765520	224365	222157	211202	2504029	214216	203404	206148	201374	184017	156551	794943	3710135
£4	330502	671392	551262	223176	219402	207900	22036341	210118	198794	201125	196534	172551	154687	7694CE	13377247
65	342309	662645	341160	221785	217788	205555	1950582	207831	197842	201588	203540	167289	273131	796655	* 2362643
66	553645	791038	429835	223346	215830	208190	2425884	210354	198595	201598	197531	174400	151060	772524	2555842
59	94705331	54196961	0553975	6182557	6072152	5747813	53446730	5809075	5505593	1564474	5469244	4856295	6421475 -	21459610	87126890
68	338233	550703	376928	220806	216863	205275	1908812	~207467	196771	159446	1\$5330	174868	225338	766415	3112032
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ឹម	290375	215503	214992	220806	216863	205279	1278218	207467	196771	159446	155320	174868	153161	766415	2445261
								-					•	Fire En	ergy

Table 11 4-15 Kılıckaya Power Production Case 12 Reservoir High Water Level 845m Firm Discharge 38,20m³/sec

Table 11 4-17

Ayracik Power Production Case 123 Reservoir High Water Level Kilickaya 850m Firm Discharge 41.80m³/sec 1. A. 1. p.C. Reservoir High Water Level Ayvacik 195m Firm Discharge 94.80m / sec 12 1 3 11-2 TOTAL S KAMIKI . 10 11 6 Ł NEN 5 7 4 , 745747 1075067 863874 784787 770650 732285 4972410 751852 732985 773332 1734107 2214888 2135693 5455316 13315271 39 4921517 21529702 3835930 3966601*1958343`659042" 783472 748263 -12153652 761421 732418 765977 1147756 2275366 3653112 40 4025467 3114256 565427 784547 767940 722526 10380163 727289 690266 706456 705456 542926. 1170136 3045178 15322766 41 2635300 3420281 •776584 775239 755101 705491 •6011996 715311 683797. 716423 735659 959855 1110622 2534635:3124062 1649576 •786442.4 772847 730405 • 9557967 737570* 702471* 720159.7 721066 1010754 1326948 3135724 14033663 42 3154450 14816535 43 1725792 2155025 1352335* 785386 769526 *724506 . 7512574* 727605 688607 699971 689191 613134 679166 2690903 11610248 44 1084746 1954119³ 763670 -782833² 764556 -716871 6868837⁷ 721965 682765 655122 688421 621589 707186 -2687901 10985685 48 46" *1044892"1493018'1253451" 787206 *776537 738371 · 6093915 · 750632 720724. 741233 ,742018 1257305 1636523 3461284 11942354 47 *1139533 ** 801/752 * 741794 * 746932 * 722445 674998 4827458 674288 639317, 658092 659008 630158 711723 2586575 6800044 2002257 2142964 1791742 - 783437 764512 718875 - 8203792 724390 688601. 702895 695430 623738 801713 2710664 12440555 48 2412302-3053221 1643408*'782712''762908 717798 8752349 722302 684527 659042 679363 553596 592474 2010747 2944868--962722-'781748- 7605653-711153 8172203 710246 669463 676613 662244 585984 641826 2657328 13164453 49 2594304 12116575 - 50 £14892 ² 655506 16537131 655962 624503 1572378 13776954 561492 523292 5184351 557897 554626 1140190 2194250 7672266 - 51 3619402 2707990 1245044 786918 774034 731447 ... 5864835 .736605 698079 . 711381 703469 717600 762252 2830529 14154221 52 2224375 1612095 1151435 784195 769093 728173 6669368 740827 717631 750289 762367 1584414 2778406 3814701 14003302 53 3852911 4159649 1767020 -785442 770934 727941 12063897 731615 - 691602, 704653 701976 676388 705157 2274821 16279490 54 4150624 11212551 709375 -760818 737102 737042 706496 655674 4306507 665102 652133 708497 760692 2029302 2050318 - 55 1685869 1240802% \$\$3270- 784131 764852 718552 · 6187476 722903 684722. 697056 685685 624064 10\$8052 2691527 106\$9558 - 56 -~974650 1354106 733621- 711091 683461 630058 · 5066987 621341 578604. 569013 · 561162 535224 678253 2244003 8630584 57 1242016 1462777+1517812 784564 4764337, 711739 - 6483245 705890 657805 658987 646600 539708 656275 25431CC 10428510 2525003 9964132 1179359 1448948 1199468' 780880 757352 706324 6072331 - 701572 "654274 653131 620346 587252 665226 59. *821828/2821843-1337124 779157-748725 *689883 7158560 679924 633113 638080 642568 601192 7C6718 2514952 11100155 60 3154152 9974191 **747106 _778031 * 754850 - 774285 - 753587 * 704734 - 4512993 - 706641 - 668767 . 652450 * 717303 1075632 1660405 61 \$637600 962432 766840 720712 '714162 679547, 626756 4470849 621020 562355 557415 629874 992986 1743093 2802638 62 63 · 2361586 2762848°2655143° 810422° 783576 745356 10118931 765498 748050 908061°(803623 1585012°)465558 4044746 16524733 1121332 1583111 1332243 780853 754111 696857 6270507 653825 652220 665315 665242 613422 1025196 2596204 10585732 44 4954003 14063652 6564283 654233 654673 693250 1647671 1558405 1811133 1407937 1820926 1103493 779714 752581 699226 65 2097823 2269452 1030652 787765 177795' 739442 7702937 751691 713785 733830 753012/1154685 2250526 3395312 14100466 66 99 516202415685097633115672216768982104010119734088 204037576158250501882765815455206217292452835960736927880 88371720 349162626 1843580 2030392 1182703 774175 751432 704785 7287071 708038 672416 654825 776045 1012842 1318853 3156133 1247055

÷ 741957 780271 756558 771077 751432 704789 4566084 708038 672416 650535 697858 641454 731140 2702263 6647525 83 Firm Energy

Table II 4-18

Avvacik Power Production Case 124 Reservoir High Water Level Kilickaya 840m Firm Discharge 35.00m³/sec Reservoir High Water Level Ayracik 195m Firm Discharge 92.80m³/sec

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NEN	4	5	6	7	8	9	KANIKI	10	11	12	1	2	3	11-2	TOTAL
	۰,			•				••							
39	651057	1593941	796216		748721									5036022	
4U			1578185				12022807								21032704
41.	3946643	3122741	820531	762064	741645	692564	10080192								14550C21
42	3093217	3428766	742913	743780	717943	668561	\$3\$5180	668023	633463	661157	678155	772886	526472	2745665	1373734C
43							9887603		671603					2867366	14628570
44	1804915	2804464	1320443	767562	748501	700566	8147251	655425	657335	663294	647835	571563	628913	2540027	12015616
45	1469589	1975151	648275	1766059	745175	696678	6500931	• 695320	652983	660031	648854	582132	680593		10400245
46	15e174	2448225	1262505	769377	756479	715346	67CB106	,722950	690207	766014	70314¢	571628	1585557	3070995	12027608
. 47	1199989	812652	1728437.	730638	762940	652532	4827188	646837	608381	621562	617869	588287	665083	2436055	2575207
46	1624390	2903664	1879109	765600	743797	695210	. 6611770	656174	657314	666314	654361	582735	e7537e	2560724	12544044
49.	, 2095755	351 7670	950011	764885	742165-	694116	87£460£	654039	. 653535+	662316	637527	551091	762584	2504473	12725702
, 50	2315926	3310208	818280	759455	734646.	681290	8619805	674905	630629	631465	631447	534568	575088	2408105	12261907
51	. 551102	609865	645552	656063	621890	566652	3651124-	551220	479353	479951	543231	515658	1147564	2078193	7428101
52	3582041	2705628	1035071	769082	753505	706150	9553477	708521	667C86	675128	662787	597556	688753	2602557	13553308
53	1966077	1836006	\$76905	766360.	748466	704750	6958568	712737	687025	715527	725410	1264853	2755437	3342815	13855557
54	3897850	4071998	1775695	767611	- 750342	704504	11968300	703472	- 66CElE	668146	661235	596662	665911	2586659	15924042
55							3975759							3405355	\$828265
56							6264742					583104		2540850	10354292
57	1080001	2201047	. 724285	711018	681165	625335	6022853	613244	566715	551854	538381	510131	647843	2167081	\$451619
58	1140132								625722	620765	602813	535482	647161	2384786	10561832
59							6178441	672944	622052	614573	585254	540187	613604	2362106	9827295
							1450757							2356222	11116287
£1							4195633							2564094	8537830
62	. 1096222	1073043	74460C	746478	714850	-661284	5036477	656367	615230	627639	651591	1190214	1736168	3084674	10513686
63	2481490	3612645	2665192	774085	764482	724026	11021925	740293	. 721271 -	760604	768512	1435243	1526173	2665620	16576621
. 64							4751935							2442045	10634611
							6738540							4583405	13856587
66.		-							682865					3074066	14051330
							205839580	150159941	19035571	8286246	19840517	25123703	34467843	81154423	34447824C
							., ,7494285							2858372	12302794
	··			. .					•• .						
EA	71 5644	762231	740145	75305E	730351	680735	4326168	679143	639427	653GEC	659152	608155	455152	2555834	8324277
			•			-	· • • •		**					71rm Ener	£7

Table II'4-19

Ayvacik Power Production Case 125 Reservoir High Water Level Kibckaya 855m Firm Discharge 46.20m³/sec Reservoir High Water Level Ayracik 190m Firm Discharge 96 20m³/sec

NEN	4	5	6	۲		, 9	KAMIKI	10	. 11	12	, 1	2		11-2	
39		1258417	746300	764321	-747647	709564	5074049	729952	714977 .	778442	1830628-	2110967			. 13312583
40			1563294										•	485275E	
41			854305	-			9984545	-					-		11047877
42			762294				6317025						-	2992417	•
43	2589960	2663169	1430258	.766772	750955	707580	8916694	714082			-				14209785
44	1710122	1814929	1222826	765322	746737	700711	6960647	703100	665828	677952	668931	596435	663499	2609146,	10926392
45	.2063314	1913921	~ 749942.	763258	742165	695899	6928503	698611	661110	674455	669975	652576	.685341	2658124:	10574575
46	• 1189629	1380413	809807	767652	756218	717698	5621017	728790	701182	723125	726479	1408243	1482652-	, 35590 332	. 11350532
47	980766	753153	718660	721 74 5	697077	650382	4521787	649147	616482	637319	641437.	657410	766415	2552648	· E451597
48	2065925	2108938	1422674	762647	740485	694263	7754932	699528	665775	681143	675774	£30C85	910226	2652781;	12057467
49 :	2380505	2929589	841942	761674	738511	693022	8345243	657200	661703.	676883	658065	575391	1166112	.2572042	12780557
50	1815250	2048728	736811	747650	722361 -	671337	1 6744132	667873	658391	634768	621205	. 545634	8C3816	2433962	10445554
51	580221	62 5 8 9 4	628054	629312	557181	545774	3666436	507524	466433	529406	,55684C	667931	1435283	222061C	7773853
52	3437140	2132737	585673	-767436	75248C	708826	· 8784292	713047	676314	650542	684611	. 816739	763137	286820e	12128682
53	2173300	907476	823596	763679	746139	704921	~ 6119111	. 717616	697662-	723145	749408	1708889	2765830	3869108	13455665
54	3695530	3944186	1708990	765399	748492	704689	11567286	707511	669357	683137	682959	778376	678544	2813829	15767570 .
55	685378	742277	721559	720232	689717	639700	4158863								11246687
56			1021326		. –				•				1057623	2728763	10575385
57			70255					568678					-	1950542	8284545
58	· 1415911	1372376	1325211	764200	740346	686315	0 6304359			-		1.1.1.1			10222693
59	•••		1210619		731805								648241		\$762536
60			928841		721737	661870		649705						2412343	8987105
61	-		2366980				-	667115						• •	10066463
62			656816			600177		553483			-				\$521133
63			1761265					743894			-				14869314
64			1150698			671934	- 5675389	-		-			1058288		9923815
65			826576			672344	5994686						1823390		13414256
66			932039					728997							13341015
99	-	-					189781385								334157823
,8 8	1820865	1 180351	1013133	123014	152493		6111401	680225			, , -				11934208
98	720291	758885	736594	748149	725583	678761	4368692						1 706259		8367581
														Time Trees	

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Firm Energy

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Table 11 4-20	
Ayvacik Power Production	Case 129 Reservoir High Water Level Kiluckaya 850m Firm Discharge 41.80m ³ /acc Reservour High Water Level Ayracik 180m Firm Discharge 89 60m ³ /acc

								-							
NEN	4	5	6	7	Ċ	ç	KAHIKI	ນູ	ų	12	1	2	3	11-2	TOTAL
39	651954	941425	826845	734682	718551	681238	4553795	700351	685573	728763	1793804	2080064	2059070	5288224	12601440
40	3645200	3816351	1923855	828813	73458C	697718	11646517	708660	682457	717585	1204238	2138965	2558191	4743185	20656953
41	3790555	2996252	\$28065	733907	714643	669862	9833568	673445	635265	655384	652460	8859Ge	1275528	2840955	14623500
42	- 251 9367	3290725	732098	723118	~701077	657078	8623463	662017	633667	667285	689462	1036721	1031193	3027135	13343808
43	2524083	3006415	1588299	736275	726618	678497	19254188	684167	652064	669726	672712	\$46282	1425860	2940784	14364595
44	1620299	2088197	1302321	734876	716560	671873	7124126	673577	637247	648225	· 638915	569669	632562	2493456	10913721
45	1988141	1846275	751630	732891	712162	667234	6658333	669238	632689	644833	639931	594408	661847	2511861	10541275
46	1152187	1500343	115544C	737304	725693	687677	5958644	698357	671415	691937	654704	1345462	1520779	3403518	11581298
47	1062097	1748355	691317	693903	669738	624364	4489794	622597	590641	610005	613394	605686	736679	2419726	8268796
48	2033190	2063223	1735905	732303	710547	665660	7940828	670132	637199	651303	645535	580294	870760	25,143,21	11956051
49	\$2349432	2937569	1024334	731366	7086351	664477	8415817	667868	63325E	647178	628374	" 3486CB	1088433	2417418	12625536
56	-1912062	2849126	52479E	730311	706622	657615	* 7781532	655189	616910	623418	610352	540201	552939	2350881	11420541
' 51	569567	61 2 3 6 5	6151 87	617671	5873841	537981	3540155	526105	477573	506043	1534256	636540	3403613	2154414	7626487
52	3417943	2589662	1217467	736906	722094	679692	\$263764	683168	647399	66C416	654136	758075	731401	2720026	13458359
53	2102971	1059492	1083782	733293	715585	675932	6371456	687564	`668C05	761646	716956	1625301	2698552	3711908	12469480
54	3679505	3916953	1701295	734946	-718256	675705	11426664	677835	640668	653222	2652530	719715	651853	2666135	15422487
55	657565	711840	65155C	669635	6556101	610899	4021119*	620463	611556	669877	853462	2032765	2015597	416766C	10824835
56	1626979	1273273	561065	733208	710981	665304	5900810	668542	633054	645071	635145	665245	1016663	2582619	10168634
57	992462	1315221	679253	651410	62349C '	571113	4632949	555713	519452	433552	521781	503045	734192	1977830	6104684
58	1372238	1372510	1518735	733783	710406	658006	6365678	650241	604054	604069	592999	523069	737344	2334191	10017454
59	1189527	1363121	1199934	729001	702183	65216C	58 25926	• 645512	60015C	597583	575113	537777	617692	2310663	9469793
63	\$15979	2769386	1267683	72682¢	652458'	634434	7026606	622012	577033	580913	588473	556244	615211	2302661	18638692
61	845329	726601	707260	725487	70371 <i>E</i>	656017	4364410	657116	622024	646352	674425	1226245	1466475	3169190"	9677191
62	880468	71 3964	668368	659904	625307	573463	4121494	566035	530305	546150	583574	1100743	1655965'	2760776	914427G
63	2223276	2687916	2555777	782034	732482	694118 ⁵	9675603	713391 (700819	955124	773183	1519723	1508764	``3548845"	15846607
64	1041954	1537870	1283317	728972	658530	844142	5934785	637124	597573	61091C	-613242	569301	1018652	2391428	``\$981 9 87
65	1431779	1740355	1086965	727534	657222	64453E	6378391	637552	600616	640896	1703225	1849426	1783530	4794163*	13543636
66	2011180	2171450	1017790	738067	7267974	688940	7354224	699560	664053	684154	766672	1268256	2117248	3323135	13494167
99	502074505	45762753	18603542	02984301	\$5669711	8285755	1947452391	63355311	74071071	20516602	08670632	79812963	36350793	84347126	333832685
88	1793123	1949153	1137870	724944	658820	653063	6956973	654983	621682	646131	745252-	- 959332	1258243		11922596
						'n				·· •			•		
۴^	6723,42	33AZ 76	768851	72342t	658825	653063	4203773	654983	621682	&3847G	650520	196193	666236	2506863	6045657

. The Energy

- Table 11 4-21

Ayyacık Power Production Cese 127 Reservoir High Water Level Külickaya 845m Firm Discharge 38 20m³/sec Reservoir High Water Level Ayyacık 190m Firm Discharge 91.20m³/sec

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NĘN	4	_ 5	_ 6	7	8	\$	KANIKI-	10	11	12	ı	- 2	з	11-2	101AL
39	639261	71 3 7 8 4	701 845	716324	698019	659194	4128431	67554B	660065	701415	14=7785	2053262	2046204	4073333	11817600
4							11566416							4558811	
41			8(1730				9611655				627851				14172295
42	•		766467						*		651497				12123505
43	2546434	3254181	1405363	725868	708614	665151	9365611	666487			650850				14142151
44	1666469	2449797	1289475	724465	70456E	658526	7453300	657819			616100				11166295
45	1782196	1845915	7060 24	721351	698919	652604	6407009	652003						2407654	10102662
46	1016371	2029075	1216357	726884	713671	674361	6376719	682696	654375	672422	673265	1153632	1547548		11800065
47	1030468	751314	685125	686128	660333	613452 .								2328840	8013667
48	1953489	2371518	1802858	721928	658571	65233E	8200702	654336	619780	631021	622876	557785	703552	2431466	11550498
49	2321775	3223284	\$44384	720996	656672	651157	8558268	652059	615765	626607	605264	524507	\$17167	2372747	12500241
50	2084826	3180952	8C4252	715394	685658	639069	8114151	633385	593208	556056	579820	509706	556274	2278820	
51	53114E	583128	£C7459	610064	577634	526112	3435585	502266	423837	486236	525829	614784	1452557	2050686	7441054
52	3,434827	2561727	1062041	726493	710085	666361	9161538	667475	630139	640334	631717	616354	765435	2518544	13052592
53	2108294	1538757	909110	722908	763991	662588	<u></u> 6645650	671886	650976	682265	696102	1511266	2701062	3540629	13555227
<u></u> \$4	3693154	3866355	1765057	724549	706257	662359	11357731	662111	e2325e	£32,57E	630C7C	577477	£42290	2463821	15125952 -
55	646191	698121	676547	672957	635495	588665	3921060	594805	584918	641758	6\$8575	1920815	1987388	384607C	10349343
56	1595460	1161118	946975	722823	655003	651979	5781358							2410625	5821223
57	1030680	1821254	679390	660558	632213	579262 .						452837	657253	2005742	8673652
58			1369130										623588	22462C4	10085587
<u></u> \$9	1085555						5984293			575597	550185	511543	550563	2220342	\$465680
60			1113045	*			7218470			558892		532914		2214362	10673750
é1	. 668545						4119090				648495			2910157	5125471
62		-	697306				4215878			-				3075675	\$741562
63			2560862				10277195							3775902	16226636
64							6171197							2305817	10008402
65			\$44588		ч									4584625	13320423
€6			868717		-		7681871	-						3120026	13556390
59							1973180351							80514167	330988165
88	1896518	2110325	1087387	714153	687855	640794	1047072	635914	604074	625241	703537	\$42654	1256514	2875566	11021006
6	681557	120683	766513	711008	687855	640794	4142459	639914	634074	62G973	630965	579764	664C87	2435776	, 1863227

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Firm Energy

fable 11 4-22

Ayracik Power Production Case 128 Reservoir High Water Level Kihckaya 840m Firm Discharge 35.10m³/sec Reservoir High Water Level Ayracik 190m Firm Discharge 90.50m³/sec

NEN	4	5	t 1	8	9	K#PIKI	15	11	12	1	2	3	11-2	1G7AL
79	731035 15163	20 79211	19 716599	657073	656835	5110041	671321	654101	693601	1494473	2020875	2105024	4873044	12763440
4.4	2585354 38245	15 190446	1 775002	718164	678309	11465805						3567001		20145266
41	3712098 30044	55 77894	5 711845	685011	64CE71	5537229						1215060		13045653
42	Z\$1\$442 3298e	88 69510	2 690278	663474	615732	8862916	613647		610572			828305		13030268
43	2567028 34414	72 138389	5 719449	700517	655484	\$467849	656487	621104	633387			11:3786		14023571
44	- 1698952 27150	92 127163	4 718059	696455	648647	7749039	445644	605718	616826	596393	525883	580250		11313752
45	1581196 18896	0 82431	8 716106	692063	644206	6347489	641196	600592	607284	597484	527277	6 14 2 1 4	2343137	\$946536
46	873629 23743	121589	0 720467	705552	664761	6554649	670800	641C23	656608	655493	1045025	1510007		11723465
47	. 1119952 7633	54 67947	4 678573	650782	60195Z	44 \$4127	594606	558464	571737	570217	546665	624739	2247083	7960555
,48	1747355 28180	50 180913	8 .715522	. 650455.	642625	8423149	642110	605672	614044	603416	538020	625756	2361152	12056207
49	2181765 33527	14 \$1523	2 714594	68854Z	641435	8494283							2255960	12187394
50	2321112 31848	2 7 761 6	7 708658	681132	628640								2200771	11650043
51	50 283 7 5661 0	0 _60834	7 619330	56065	533107								2017633	7361 155
52	3402722 25546	3 105114	7 72007C	701550	656697	9087259 ,							2406265	12752950
53	2050543 176501	0 94370	2 716501	655886	652509	. 6824551							3331050	124(2167
- 55	3695950 383563	5 170964	1 718135	658152	652689	11310402				610782			2385036	14969345
55	623665 67420	3 65161	3 642871	605792	551098	3749242	552019	542035	555162	659542	1619826	1856034	3420565	5577864
<u></u> 56	1575546 133422	4 114123	3 716418	650883	642273	61 C0575	640486	501368	607544	592368	538391	848881	2329671	\$\$45613
57	1073001 215551	2 67278	5 654975	624612	569567	5750452	.554381	509645	367026	SCBCGC	465366	656339	1890041	6851213
58	1388247 184456	0 149640	Z, 716994	650305	634914	6771422	621734	571334	564197	,547016	466577	555616	2169124	10161896
59	917278.159932	1 148670	3 712260	682104	629019	6026685	616906	567289	557302	527843	468151	563892	2140786	\$348265
69	1315020 284112								539676	542205	511507	611727	2136826	16558773
61	646456 69615	0 67475	1 688034	66134E.	609194	- 3915733	602363	562925	580955	608131	654238	1273722	2606345	2452167
62	1018954 106643	9 69566	1 691715	658174	605731	4736678	598660	559511	57153e	600115	1223195	1685326	2554357	5975CZ1
63	2374101 347580	6 256544	6 728223	715658	674725	16533999	665818	674782	741515	726533	1473514	1448749	3616348	16268514
64	1124072 202429	6 123741	3 712234.	678475	620912	6357402	608338	564985	571482	568838	526143	757358	2233448	10034546
65	1288663 220505	5 87449	¥ 71080C	677171~	621309	6477492	602784	567771	603213	1409720	1610488	1756637	4391152	13234105
66	2487419 242440	9 53240	1 721022	706485	665828.	, 7937568	671784	633265	64832E	667793	99358 3	2020401	2942967	13512720
\$9	\$06243966324630	53089576	9197648441	20169651.	7650950	2012009461	75617821	64994061	68208151	88653732	46831513	3655676	76878745	~
68	. 1808014 225879	7 110342	705887	679235	630351	7185748	627207	589265	601101	673763	8E1541	1201996	2745670	
15	673270 71456												2366044	7740447

Firm Energy

Table II 4-23 Ayracik Power Production Case 129 Reservoir High Water Level Kilicksya 850m Firm Discharge 41 80m³/sec Reservoir High Water Level Ayracik 180m Firm Discharge 89 60m³/sec

NEN	4	5	6	۲	8	9	KAMIKI	10	13	12	1	2	3	11-2	TOTAL"
39	157576		769012	455440	63912A	604596	4058097	623123	614285	76119!	1653528	1876168	1513730	4925580	11520530
40	3269627 3						10581841				1214992				- 18859726
41	2385437 2					591785	8880736				581365			2513143	13265243
42	2384588 3			643849		578842	7918360		557153		670376			* 2735962	12183448
43	2497507 2						8631196	604682	576236	5\$3467	599541	848366	1421958	2617610	13275446
44	1516150 1						6551171	592480	559122	568745	560575	SCCC70	555429	2188517	· \$8\$1597
45	2020030 1					588515	6281953	567440	553E21	564808	562143	51Ž230	620078	2193002	\$ 5682473
46	1240998 1					611997	5584274	626872	598274	618647	624270	1258815	1467561	310001C	10772717
47	1034344						4056130	536010	510128	529966	53654E	53254E	- 174827	2109990	7479557
48	1926326 1						7330642	568473.	559070	572310	568603	512536	853448	2212515	10965482
49	2273665 2						7788561	585850	554482	567530	548597	477172	1056051	2146181	11578703
50	1882663 2			650687		-	720062	571394	535753	540702	529019	467929	515376	2073403	10360235
51	497156			555195			3153694	466554	411451	455152	467708	666218	1517067	2020525	1157864
52.	3180197 2					602831	8559229	603531	570871	58281C	578460	648291	765576	2380532	12353268
53	201 2 574					598497	5895308	608552	594403	629550	649061	⁷ 1534791	2606731	3407605	12518396
54	2343268 3					598243	10302051				576618				12812764
55			626779			544735	3763286	553764	551101	613472	1080605	1832493	1873824	* 4077751	10268625
56	151 5737 1		-			586296	5364416	586623			556619				* 5265404
57	941445 1	239767	557581	560787	531225	478490	4349295	431938	382074	314561	` 47C66C	462535	\$10582	1630234	* 7322049
58	1450467 1	285055	1358140	654436	62971 é	577848	5955662	565185	520731	517968	508377	459210	684649	2006292	9211788
59	1256340 1					571043	5440757	559635	516299	510265	426926	458603	1-542836 1	1572097	* 8515325
60	1015185 2	565323	1186639	646319	608585	550165	6572616	532388	468892	450152	502510	[×] 485675	668301	1967665	\$760974
61	872779	644676	630886	648057	625505	579242	4001145	577356	545473	570758	605174	1175488	1436086	2856853	8931482
έZ	663869	631356	587254	573569	536199	484564	3676811	471904	419019	461584	505381	1056212	1557372	24461 56	`8192283
63	2194756 2	512597	2354683	721125	65291C	617008	5053189	635529	6Z9243	\$64725	712303	1265739	1461530	3572010	1472225E
64	1024629 1	404395	1178449	648830	615584	561639	54 23 926	549875	513758	525965	53187ć	500 199	1047563	207195E	\$103362
65	1375529 1	606749	98430¢	647143	614463	562101	5750291		516827		1696724			4410947	12351695
£6	1977851 2							622242						3013642	12451574
59	4811047150	2266642	291 631 171	81178991	73282331	6089483									305819268
Éð	1718231 1	793817	1041540	647068	618865	574624	6354145	572468	541275	574972	685435	900425	1254820	2702111	10973544

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26 617452 651188 63275C 641374 619665 574624 3736253 572468 541275 555764 576171 53CG72 6CE745 22072FE 7124752 Firm Energy

Table 11 4-24 Ayvacık Power Production Case 130 Reservoir High Water Level Kılıckaya 840m Firm Discharge 35 10m³/sec Reservoir High Water Level Ayvacık 180m Firm Discharge 87 80m³/sec

AEN	4	5	6	7	8	9	KAHIKI	1,	11	12	1	2	3	11-2	TOTAL
39	624099	1378596	725865	639849	619532	581451	4569392	554822	583629	624722	1509265	1820885	1555567	4547915	11671696
40	3214536	3427994	1754852	714646	640615	6C2730	10255377	606805	581 6 C C	613699	982233	1887406	325190E	4064538	18279026
41	2217413	2767884	706172	63453E	610466	563288	8559761	557517	522110	53124E	520338	536665	1255147	12119745	12522170
42	2695026	3039133	620034	610419	58192e	534848	8065386	525366	501471	53161C	557592	71894e	877566	2309615	11801937
43	2501025	3170490	1275279	642120	622355	578748	8750057	576465	543917	555004	556508	736883	1192085	2352312	12950515
44	1646536	2487738	1171854	642497	617685	\$71079	7138393	563798	5259031	529131	515626	453590	5C2588	2024250	10229429
45	1637235	1720516	775532	638219	612557	565704	5950203	558572	520467	525115	516874	835334	541327	2025324	5079426
46	970495	2194506	1120500	643299	62826Z	589404	6146466	592011	566968	561774	583067	973214	1450521	2705123	16855121
47	1101134	680729	602545	597722	567575	519751	4069856	508239	474801	467627	489277	476047	1556963	1927752	706281C
48	1779429	2626752	1667035	637531	610734	563875	7867356	559650	525842	532754	523664	467613	558501	2049872	11055780
49	2191477	3047763	843517	636455	608532	562498	7850243	556922	521119	527965	502335	426899	758670	1978266	11184101
50	2200803	2934048	764521	630734	601266	549104	7620476	535830	495685	491883	471851	404186	440964	1863605	10460875
51	404375	502603	55541e	566596	533856	483588	3046438	467264	405209	431511	471414	°621597	1472175	1929731	6915608
52	3197359	2353481	\$68728	642842	624056	580135	8366641	575267	538249	543594	533876	485442	596982	2101161	11640651
53	2045437	1614943	E76302	638683	617C3G	575782	6368177	580497	562990	593156	609371	1256738	2578057	3022255	12548586
54	3317413	3427994	1 575372	640587	619650	575519	10156535	568910	530062	534984	5320CC	484312	547698	2081358	13354501
55	559392	61 3400	55495E	584004	546216	493572	3391542	494152	489500	550338	616271	1763671	1825634	3420180	\$131508
56	1467972	1202204	1662384	638575	611239	563465	5545839	557726	520890	525391	31095E	407564	841723	2025203	Ě970491
57	1114104	1973928	593154	568222	525113	479266	5263787	433811	349271	2 80664	457696	445702	751795	1533333	£022726
58	1477893	1729991	1370250	639247	610571	554835	6382787	535837	485951	473755	456254	406097	524402	1822057 (\$265683
59	1034338	1474805	1347178	633732	601078	547904	5639035	530227	461079	465211	250324	426170	506640	1723394	8359296
60	1541435	2617410	1020723	631223	525873	526765	6927429	501791	451255	413300	459381	444406	545394	1768342	5742556
61	675141	636283	6150Z6	627696	600677	550214	3765037	541416	505356	524338	55611ê	841744	1401535	2427554	[~] 8075542
62	993675	973939	621250	612753	576452	523955	4302024	512823	475827	427142	523437	1129530	1568909	261593e	8959692
63	2378895	3292121	2363751	671551	627725	598567	9812660	612312	603077	768065	662729	1234597	1401072	3268872	15134516
64	1098230	1844845	1143002	63370Z	596866	538301	5854946	520279	4783081	422694	483610	453813	'727G34 [*]	1897825	9000084
65	1416939	2050121	802030	632040	555356	538765	6035251	520791	481682	520172	1421106	1602339	1555653 -	4025300	12177195
66	2380637	2264378	831497	644024	629374	590706	7340616	594224	558115	572345	597027	906928	1560762	2634415	12530021
99	489894475	57960995	283087671	76715061	684717e1	5503819	1852817101	52683241	42801331	46551551	69795982	23507563	2232272	68305642	301111548
88	1749623	2070036	1011027	631125	661685	953708	6617204 `	546012	510005	524970	606414	798241	1151153	243563C	10713595
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88 600624 636351 621427 628021 6C1685 553708 3643826 546012 51005 520574 534783 458572 581275 2063934 6825051 Fim Energy

Rank	Discharge m ³ /s	Average Discharge m ³ /s	Duration day	Average days day	Inflow m ³ /s-day	Sediment. Concentra- tion p.p.m.	Ave. Sedim. Concent. p.p.m.	Sedimentation Amount 10 ³ ton .
1	93.74					5,400		
2	81.20	87.47	0.286	0.286	25.02	4,100	4,750	10.268
3	70.34	175.77	0.464	0.178	13.49	3,200	3,650	4.254
4	60.93	65.64	1.143	0.679	44.57	2,475	2,838	10,929
5	52.78	56.86	1.321	0.178	10.12	1,900	2,188	1.913
6	45.72	49.25	1,571	0.250	12.31	1,475	1,688	1.795
7	39.60	42.66	2.286	0.715	30.50	1,150	1,313	3,460
8	34.30	36.95	2.536	0.250	9.24	880	1,015	0.810
9	29.72	32.01	3.214	0.678	21.70	680	780	1.462
10	25.74	27.73	4.429	1.215	33.69	520	600	1.746
11	22.30	24.02	7.179	2.750	66.06	400	. 460	2,625
12	19.31	20.81	10.786	3.607	75.06	310	355	2.302
13	16.73	18.02	15.750	4.964	89.45	240	275	2.125
14	14.49	15.61	20.714	4.964	77.49	190	215	1.439
15	12.55	13.52	26.429	5.715	77.27	150	170	1.135
16	10.87	11.71	29.643	3.214	37.64	110	130	0.423
17	9.42 ·	10.15	31.000	1.357	13.77	85	98	0.116
Total				31.000				46.802

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Table II 4-25 Kilickaya Sedimentation Amount Month January

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Table 3	II 4-26	Kilickaya	Sedimentation	Amount	Month	February

Rank	Discharge [*] m ³ /s	Average Discharge m ³ /s	Duration day	Average days day	Inflow m ³ /s-day	Sediment. Concentra- tion p.p.m.	Ave. sedim. Concent. p.p.m.	Sedimentation Amount 10 ³ ton
1	181.51					14,700		·
2	151.40	166.46	0.107	0.107	17.81	12,000	13,350	20.543
3	126.29	138.80	0.179	0.072	9.99	9,500	10,750	9.279
4	105.34	115.82	0.214	0.035	4.05	7,650	8,575	3.001
5	87.87	96.61	0.321	0.107	10.34	6,200	6,925	6.187
6	73.30	80.59	0.714	0.393	31.67	5,000	5,600	15.323
7	61.14	67.22	1.393	0.679	45.64	4,000	4,500	17.745
8	51.00	56.07	2.893	1.500	84.11	3,250	3,625	26.343
9	42.54	46.77	4.143	1.250	58.46	2,600	2,925	14.774
10	35.48	39.01	6.214	2.071	80.79	2,100	2,350	16.404
[1	29.60	32.54	8.429	2.215	72.08	1,650	1,875	11.677
12	24.69	27.15	10.536	2.107	57.21	1,350	1,500	7,414
13	20.59	22.64	14.964	4.428	100.25	1,100	1,225	10.610
4	17.18	18.89	18.214	3.250	61.39	890	995	5.278
15	14.33	15.76	23.143	4.929	77.68	720	805	5,403
6	11.95	13.14	26,429	3.286	43.18	580	650	2.425
17	9.97	10.96	28.250	1.821	19.96	460	520	0.897
Fotal	21,489.820							173.303

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Rank	Discharge m ³ /s	Average Discharge m/s	Duration day	Average Days day	Inflow m ³ /s-day	Sediment Concentra- tion.p.p.m.	Ave. Sedim. Concent. p.p.m.	Sedimentatio Amount 10 ³ ton
1	351.80					17,600		
2	284.71	318.26	0.143	0.143	45.51	14,500	16,050	63.110
3	230.41	257.56	0.500	0.357	91.95	12,100	13,300	105.662
4	186.47	208.44	1.143	0.643	134.03	10,000	11,050	127.961
5	150.90	168.69	1.821	0.678	114.37	8,400	9,200	90.910
6	122.12	136.51	3.429	1.608	219.51	6,880	7,640	144.898
7	98.83	110.48	5.786	2.357	260.40	5,710	6,295	141.628
8	79.98	89.41	8.750	2.964	265.01	4,750	5,230	119.751
9	64.73	72.36	11.821	3.071	222.22	3,900	4,325	83.039
10	52.38	58.56	15.286	3.465	202.91	3,280	3,590	62,938
11	42.39	47.39	18.357	3.071	145.53	2,700	2,990	37.596
12	34.31	38.35	20.321	1.964	75.32	2,240	2,470	16.074
13	27.77	31.04	23.786	3.465	107.55	1,840	2,040	18.956
14	22.47	25.12	26.821	3.035	76.24	1,540	1,690	11.132
15	18.18	20.33	28.821	2.000	40.66	1,290	1,415	4.971
16	14.72	16.45	30.107	1.286	21.15	1,060	1,175	1,193
17	11.91	13.32	31,000	0.893	11.89	865	963	0.989
Total	56,474.860			31.000				1.030.808

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Table II 4-27 Kilickaya Sedimentation Amount Month March

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Table II 4-28 Kilickaya Sedimentation Amount Month April

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Rank	Discharge m ³ /s	Average Discharge 3/s	Duration day	Average Days day	Inflow m ³ /s-day	Sediment. Concentra- tion p.p.m.	Ave. Sedim, Concenet, p.p.m.	Sedimentation Amount 10 ⁹ ton
1.	533.96					11,900		
2	440.22	487.09	0.286	0.286	139.31	9,550	10,725	129.090
3	362.94	401.58	1.393	1.107	444.55	7,500	8,525	327.438
4	299.23	331.09	3.500	2.107	697.61	5,800	6,650	400.819
5	246.70	272.97	8.107	4.607	1,257.57	4,650	5,225	567.717
6	203.39	225.05	12.214	4.107	924.28	3,620	4,135	330.212
7	167.69	185.54	15.393	3.179	589.83	2,890	3,255	165.879
8	138.25	152.97	19.607	4.214	644.62	2,280	2,585	143.972
9	113.98	126.12	22.536	2,929	369.41	1,800	2,040	65.111
10	93.97	103.98	24.929	2.393	. 248.82	1,420	1,610	34.612
11	77.47	85.72	27.393	2.464	211.21	1,120	1,270	23.176
12	63.87	70.67	28.857	1.464	103.46	880	1,000	8.939
13	52.66	58.27	29.607	0.750	43.70	695	788	2.975
14	43.42	48.04	29.821	0.214	10.28	550	623	0.553
15	35.79	39.61	29.857	0.036	1.43	433	492	0.608
16	29.51	32.65	29.929	0.072	. 2.35	352	393	0.798
17	24.33	26.92	30.000	0.071	1.91	270	311	0.513
Total	158,536.890			30.000			•	2,202,412

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Rank	Discharge . m ³ /s	Average Discharge m ³ /s	Duration day	Average Days day	Inflow m ³ /s-day	Sediment. Concentra- tion p.p.m.	Ave. Sedim. Concent. p.p.m.	Sedimentation Amount 10 ³ ton
1	407.55					12,400	·· · · · · · · · · · · · · · · · · · ·	
2	347.85	377.70	0.500	0.500	188.85	8,900	10,650	173.772
3	296.90	322.38	1.179	0.679	218.90	6,400	7,650	144.684
4	253.41	275.16	3.250	2.071	569.86	4,700	5.550	273.259
5	216.29	234.85	6.179	2,929	687.88	3,500	4,100	243.675
6	184.61	200.45	10.179	4.000	801.80	2,480	2,990	207.134
7	157.57	171.09	14.571	4.392	751.43	1,760	2,120	137.638
8	134.49	146.03	19.214	4.643	678.02	1,300	1,530	89,629
9	114.79	124.64	23.679	4.465	556.52	955	1,128	54,238
0	97.97	106.38	27.000	3.32i	353.29	675	815	24.877
11	83.62	90.80	28.250	1.250	113.50	505	590	5.786
2	71.37	77.50	28.893	0.643	45.83	353	429	1.699
3	60,92	66.15	29.179	0.286	18.92	258	306	0.500
4	52.00	56.46	29.429	0.250	14.12	186	222	0.271
5	44.38	48.19	30.000	0.571	27.52	136	161	0.383
6	37.88	41.13	30.607	0.607	24.97	98	117	0.252
7	32.33	35.11	31.000	0.393	13.80	70	84	0,100
fotal	141,779,330	<u>-</u>		31.000				1,357.897

Table II 4-29 Kilickaya Sedimentaion Amount Month May

Table II 4-30 Kilickaya Sedimentation Amount Month June

Rank	Discharge m ³ /s	Average Discharge m ³ /s	Duration day	Average Days day	Inflow m ³ /s-day	Sediment. Concentra- tion p.p.m.	Ave. Sedim. Concent. p.p.m.	Sedimentation Amount 10 ³ ton
1	285.56		•			42,000		
2	231.54	258.55	0.250	0.250	64.64	35,500	38,750	216.415
3	187.75	209.65	0.429	0.179	37.53	23,800	29,650	96.143
4	152.23	169.99	0.786	0.357	60.69	15,200	19,500	102.251
5	123.44	137.84	1.750	0.964	132.88	9,450	12,325	141.501
6	100.09	111.77	4.714	2.964	331.29	6,000	7,725	221.116
7	81.16	90.63	8.607	3.893	352.82	3,700	4,850	147.846
8	65.81	73.49	12.964	4.357	320.20	2,580	3,140	86.869
9	53.36	59.59	17.321	4.357	259.63	1,440	2,010	45.088
t0	43.26	48.31	20.679	3.358	162.22	900	1,170	16.398
11	35.08	39.17	23.893	3.214	125.89	575	738	8.027
12	28.45	31.77	25.964	2.071	65.80	360	468	2.661
13	23.06	25.76	27.786	1.822	46.93	224	342	1.387
14	18.70	20.88	28.571	0.785	16.39	137	181	0.256
15	15.16	16.93	29.357	0.786	13.31	88	113	0.300
16	12.30	13.73	19.607	0.250	3.43	54	71	0.021
17	9.97	11.14	30.000	0.393	4.38	34	44	0.167
Total	55,506.430			30.000				1,086.846

Rank	Discharge m ³ /s	Average Discharge m ³ /s	Duration day	Average Days day	Inflow m ³ /s-day	Sediment. Concentra- tion p.p.m.	Ave. Sedim. Concent. p.p.m.	Sedimentation Amount 10 ³ ton
1	75.80					6,600		
2	65.20	70.50	0.357	0.357	25.17	4,850	5,725	12.450
3	56.08	60.64	0.571	0.214	12.98	3,600	4,225	4.738
4	48,23	52.16	1.179	0.608	31.71	2,600	3,100	8.493
5	41.48	44.86	1.571	0.392	17.59	1,860	2,230	3.389
6	35.68	38.58	2.321	0.750	28.94	1,350	1,605	4.013
7	30.69	33.19	3.429	1.108	36.77	990	1,170	3.717
8	26.40	28.55	5.179	1.750	49.96	730	860	3.712
9	22.70	24.55	8,000	2.821	69.26	520	625	3.740
10	19.53	21.12	11.321	3.321	70.14	390	455	2.757
11	16.80	18.17	15.857	4.536	82.42	280	335	2.386
12	14.45	15.63	19.250	3.393	53.03	210	245	1.123
13	12.43	13.44	24.179	4.929	66.25	150	180	1.030
14	10.69	11.56	27.071	2.892	33.43	110	130	0.375
15	9.19	9.94	28.643	1.572	15.63	82	96	0.130
16	7.91	8.55	29.643	1.000	8.55	76	79	0.058
17	6.80	7.36	31.000	1.357	9.99	44	60	0.052
Total	17,057.370			31.000				52.163

Table II 4-31 Kilickaya Sedimentation Amount Month July .

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Table II 4-32 Kilickaya Sedimentation Amount Month August

Rank	Discharge m ³ /s	Average Discharge m ³ /s	Duration day	Average Days day	Inflow m ³ /s-day	Sediment Concentra- tion p.p.m.	Ave. Sedim. Concent. p.p.m.	Sedimentation Amount 10 ³ ton
1						4,150		
2	30.65	32.53	0.071	0.071	2.31	3,120	3,635	0.725
3	27.30	28.98	0.179	0.108	3.13	2,380	2,750	0.744
4	24.33	25.82	0.393	0.214	5.53	1,800	2,090	0.999
5	21.67	23.00	0.536	0.143	3.29	1,340	1,570	0.446
6	19.31	20.49	0.821	0.285	5.84	1,026	1,183	0.597
7	17.20	18.26	1.679	0.858	15.67	780	903	1.223
8	15.33	16.27	3.893	2.214	36.02	580	680	2.116
9	13.65	14.49	5.857	1.964	28.46	440	510	1.254
10	12.17	12.91	8.464	2.607	33.66	340	390	1.134
11	10.84	11.51	14.643	6.179	71.12	250	295	1.813
12	9.66	10.25	21.107	6.464	66.26	195	223	1.277
13	8.60	9.13	24.429	3.322	30.33	151	173	0.453
14	7.66	8.13	26.679	2.250	18.29	116	134	0.212
15	6.83	7.25	29.179	2.500	18.13	89	103	0.161
16	6.08	6.46	30.536	1.357	8.77	67	78	0.059
17	5.42	5.75	31.000	0.464	2.67	49	58	0.014
Total	9,751.920			31.000				13.227

	Discharge	Average	Duration	Average	Inflow	Sediment	Ave. Sedam.	Sedimentation
Rank	m ³ /s	Discharge m ³ /s	day	Days day	m ³ /s-day	Concentra- tion p.p.m.	Concent. p.p.m.	Amount 10 ³ ton
1	38.54	_				13,600		
2	34.29	36.42	0,071	0.071	2.59	9,500	11,550	2.585
3	30.51	32,40	0.107	0.036	1.17	6,300	7,900	0.799
4	27.14	28.83	0.179	0.072	2.08	4,550	5,425	0.975
5	24.15	25.65	0.357	0.178	4.57	3,200	3,875	1.530
6	21.48	22.82	0.643	0.286	6.53	2,150	2,675	1.509
7	19,11	20.30	0.964	0.321	. 6.52	1,550	1,850	1.042
8	17.01 -	18.06	1.429	0.465	3.40	1,080	1,315	0.386
9	15.13	16.07	2.929	1.500	24.11	750	915 ,	1.906
10	13.46	14.30	4.679	1.750	25.03	520	635	1.373
11	11.98	12.72	8.643	3.964	50.42	360	440	1.917
12	10 ، 66	11.32	15.036	6.393	72.37	250	305	1.907
13	9.48	10.07	23.250	8.214	82.71	180	215	1.536
14	8.43	8.96	26.214	2.964	26,56	125	153	0.351
15	7.50	7.97	27.036	0.822	6.55	88	107	0.061
16	6.68	7.09	28.714	1.678	11.90	62	75	0.077
17	5.94	6.31	30.000	1.286	8,11	46	54	0.038
Total	9,501.080		•	30.000				17.992

Table II 4-33 Kilickaya Sedimentation Amount Month September

Table II 4-34 Kilickaya Sedmentation Amount Month October

Ran	Discharge m ³ /s	Average Discharge m ³ /s	Duration - da y	Average Days day	Inflow • m ³ /s-day	Sediment. Concentra- tion. p.p.m.	Ave. Sedim. Concent. p.p.m.	' Sedimentation Amount 10' ton
1	123.69					20,900		
2	103.04	113.37	0.071	0.071	8.05	16,000	18,450	12.832
3	85.83	94.44	0.071	0	0	10,600	13,300	0
-4	71.50	78.67	0.107	0.036	2.83	7,300	8,950	2.188
5	59.56	65.53	0.107	0	0	4,900	6,100	0
6	49.61	54.59	0.321	0.214	11.68	3,300	4,100	4.138
7	41.33	45.47	0.679	0.358	16.28	2,250	2,775	3.903
8	34.43	37.38	0.964	0.285	10.65	1,500	1,875	1.725
9	28.68	31.56	1.571	0.607	19.16	1,000	1,250	2.069
0	23.89	26.29	3.286	1.715	45.09	750	875	3.409
1	19.90	21.90	4.821	1.535	33.62	450	600	1.743
2	16.58	18.24	7.571	2.750	50.16	310	380	1.647
3	13.81	15.20	10.393	2.822	42.89	209	260	0.963
4	11.50	12.66	16.357	5.964	75.50	145	177	1.155
5	9.58	10.54	27.107	10.750	113.31	96	121	1.185
6	7.98	8.78	30.214	3.107	27.28	64	80	0.189
7	6.65	7.32	31.000	0.786	5.75	45	55	0.027
fotal	12,858.700			31.000				37.173

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Rank	Discharge m ³ /s	Average Discharge m ³ /s	Duration day	Average Days day	Inflow m ³ /s-day	Sediment. Concentra- tion. p.p.m.	Ave. Sedim. Concent. p.p.m.	Sedimentation Amount 10 ⁻² ton
1	137.14					9,800		
2	114.98	126.06	0.107	0.107	13.49	7,200	8,500	9.907
3	96.41	105.70	0.250	0.143	15.12	5,250	6,225	8.132
4	80.83	88.62	0.357	0.107	9.48	3,800	4,525	3.706
5	67.77	74.30	0.393	0.036	2.67	2,780	3,290	0.759
6	56.82	62.30	0.714	0.321	20.00	2,050	2,415	4.173
7	47.64	52.23	0.964	0.250	13.06.	1,460	1,755	1.980
8	39.95	43.80	1.571	0.607	26.59	1,070	1,265	2.906
9	33.49	36.72	2.536	0.965	35.43	770	920	2.816
10	28.08	30.79	4.429	1.893	58.29	565	668	3.364
11	23.55	25.82	6.286	1.857	47.95	410	488	2.022
12	19.74	21.65	9.000	2.714	58.76	295	353	1.792
13	16.55	18.15	13.250	4.250	77.14	220	258	1.720
14	13.88	15.22	16.679	3.429	52.19	159	190 -	0.857
15	11.64	12.76	23.357	6.678	85.21	115	137	1.009
16	9.76	10.70	18.929	5.572	59.62	87	101	0.520
17	8.18	8.97	30.000	1.071	9.61	63	75	0.062
Total	16,205.650			30.000				45.725

Table II 4-35 Killckaya Sedimentation Amount Month November

Table II 4-36 Kilickaya Sedimentation Amount Month Decmber

Rank	Discharge m ³ /s	Average Discharge m ³ /s	Duration day	Average Days day	Inflow m ³ /s-day	Sediment. Concentra- tion. p.p.m.	Ave. Sedim. Concent. p.p.m.	. Sedimentation Amount 10 ³ ton
1	114.72					9,200		
2	98.13	106.43	0.036	0.036	3.83	6,850	8,025	2.656
3	83.93	91.03	0.071	0.035	3.19	4,950	5,900	1.626
4	71.79	77.86	0.107	0.036	2.80	3,650	4,300	1.040
5	61.41	66.60	0.357	0.250	16.65	2,680	3,165	4.553
6	52.53	56.97	0.607	0.250	14.24	2,000	2,340	2.879
7	44.93	48.73	0.821	0.214	10,43	1,440	1,720	1.550
8	38.43	41.68	1.214	0.393	16.38	1,070	1,255	1.776
9	32.87	35.65	2.143	0.929	33.12	770	920	2.633
10	28.12	30.50	3.643	1.500	45.75	580	675	2.668
11	24.05	26.09	6.536	2.893	75.48	425	503	3.280
12	20.57	22.31	10.250	3.714	82.86	310	368	2.635
13	17.60	19.09	14.464	4.214	80,45	229	270	1.877
14	15.05	16.33	19.500	5.036	82.24	173	201	1.428
15	12.88	13.97	24.643	5.143	71.85	124	149	0.925
16	11.01	11.95	29.643	5.000	59.75	90	- 107	0.552
17	9.42	10,22	31.000	1.357	13.87	66	78	0.093
Total	17,154.840							32.171
						1	n Amount	6,096.119

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		an.		Feb.		lar. ·		pr		lay.	J	un.
Rank	Discharg cum/s	e Duration day	. Discharg cum/s	e. Duration day -	Discharge cum/s	Duration day	Discharge cum/s	Duration day	Discharge cum/s	Duration day	Discharge cum/s	Duration day
1	146.06		284.71		553.72		841.48		641.79		449.08	
2	125.48	0.286	235.56	0.107	445.04	0.143	691.52	0.286	546.51	0.536	361.13	0.250
3	107.80	0.500	194.90	0.179	357.69	0.536	568.28	1.429	465.37	1.250	290.40	0.429
4	92.6	1,250	161.26	0.214	287.49	1.143	467.01	3.679	396.28	3.286	233.52	0.821
5	79.56	1.393	133.42	0.321	231.06	2.036	383.79	8.321	337.45	6.286	187.78	1.964
6	68.35	1.607	110.39	0.857	185.71	4.000	315.39	12.321	287.35	10.286	151.01	5.286
7	58.72	2.357	91.33	1.714	149.26	6.179	259.19	15.750	244.69	14.679	121.43	9.250
8	50.45	2.607	75.57	3.107	119.97	9.107	213.00	19,964	208.36	19.571	97.65	13.821
9	43.34	3.357	62,52	4.571	96.42	12.143	175.04	22.821	177.43	24.143	78.52	17.857
10 -	37.23	4.857	51.73	6.643	77.50	15.857	143.84	25.107	151.08	27.071	63.14	21.429
11	31.99	8.179	42,80	8.821	62.29	18.821	118.21	27.607	128.65	28.250	50.78	24.250
12	27.48	12.321	35.41	11.143	50.06	21.143	97.14	28,964	109.55	28.893	40.83	26.393
13	23.61	17.214	29,30	15.536	40.24	24.179	79.83	29.714	93.29	29.179	32.83	27.929
14	20.28	21.429	24.24	19.036	32.34	27.500	65.61	29.821	79.44	29.429	26,40	28.679
15	17.42	27.321	20.06	23.429	25.99	29.000	53.91	29.857	67.64	30.107	21.23	29.357
16	14.97	29.750	16.59	26.679	20.89	30.143	44.31	29.929	57.60	30.607	17.07	29.607
17	12.86	31.000	13.73	28.250	16.79	31.000	36.41	30.000	49.05	31.000	13.73	30.000
A ∀ e.	30.50-		40,90		100.76		296.12		256.01		102.36	

Table II 4-37 Monthly Discharge Duration at Tepekisla (Natural)

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Table II 4-38 Monthly Discharge Duration at Tepekisla (Natural)

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		Jul.		ug.	5	Sep.		et.		ov.	t	ec.
Rank	Discharg cum/s	e Duration day	Discharge cum/s	Duration day	Discharge cum/s	Duration day	Discharge cum/s	Duration day	Discharge cum/s	Duration day	Discharge cum/s	Duration day
1	117.72		52.32		58.86		193.37		214.62		179.20	
2	100.05	0.357	45.94	0.071	51.69	0.071	159.04	0.071	178.15	0.107	152.00	0.036
3	85.03	0.607	40.34	0.214	45.39	0.107	130.81	0.071	147.87	0.250	128.92	0.071
4	72.26	1.250	35.43	0.429	39.86	0.179	107.59	0.107	122.74	0.357	109.35	0.179
5	61.41	1.750	31.11	0.607	35.00	0.393	88.49	0.143	101.88	0.536	92.75	0.429
6	52.19	2.714	27.32	0.964	30.74	0.643	72.78	0.393	84.57	0.714	78.67	0.643
7	44.36	3.679	23.99	2.036	26.99	1.036	59,86	0.714	70.20	1.071	66.73	0.857
8	37.70	5.964	21.07	4.964	23.70	1.857	49.23	1.143	58.27	1.750	56.60	1.500
9	32.04	9.250	18.50	6,500	20.81	3.393	40.49	1.964	48.37	3.036	48.01	2,607
10	27.23	12.821	16.24	10.286	18.28	6.107	33.31	3.607	40.15	4.893	40.72	4.429
11	23.14	17.036	14.26	17.500	16.05	11.286	27.39	5.536	33.32	6.857	34.54	7.643
12	19.67	20.571	12.53	22.964	14.09	18.536	22.53	8.179	27.66	9.607	29.29	11.036
13	16.71	25.750	11.00	25.357	12.38	24.357	18.53	11.429	22.96	14.071	24.85	15.357
14	14.21	27.536	9.66	27.786	10.87	26 . 750 [′]	15.24	20,607	19.06	17.250	21.07	20.286
15	12.07	28.714	8.48	29.464	9.54	27.679	12.54	28,000	15.82	25.179	17.88	25.607
16	10.26	29.750	7.45	30.536	8,38	29.107	10.31	30.464	13.13	29.036	15.16	29.750
17	8.72	31.000	6.54	31.000	7.36	30.000	8.48	31.000	10.90	30.000	12.86	31.000
Ave.	. 29.02		15.73		15.85		21.38		28.45		29.20	

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Rank	Discharge cum/s	Duration day	Dishcarge cum/s	Duration day	Discharge cu m/s	Duration day	Discharge cu m/s	Duration day	Discharge cum/s	Duration day	Discharge cu m/s	Duration day,
1	94.12		145.00	0.036	243.72		498.98		452.74		333.38	
2	89.91	0.179	134.88	0.071	219.80	0.107	434.18	0.643	398.40	0,643	294.39	0.286
3	85.88	0.321	125.46	0.107	198.23	0.214	377.79	1.214	350.57	1.964	259.95	0.571
4	82.04	0.464	116.71	0.143	178.78	0.643	328.73	1.357	308.49	3.464	229.55	0.786
5	78.37	0.607	108.56	0.179	161.23	1.179	286.04	2.321	271.46	6.143	202.70	1.071
6	74.86	1.214	100.98	0.214	145.41	2.000	248.89	3.786	238.88	9.286	178.99	1.393
7	71.51	1.321	93.93	0.286	131.14	2.714	216.56	6.500	210.21	11.571	158.05	3.893
8	68.31	1.429	87.38	0.357	118.27	3.536	188.44	9.821	184.97	14.036	.139.57	7.250
9	65.25	1.679	81.28	0.821	106.66	5.464	163.97	13,107	162.77	17.321	123.24	9.607
10	62.33	2.321	75.61	1.393	96.19	7.214	142.67	16.286	143.23	19.893	108.83	15.250
11	59.54	2.536	70.33	2.500	86.75	7,286	124.14	20.000	126.04	21.964	96.10	19.321
12	56.88	3.214	65.42	3.821	78.24	11.286	108.02	23.143	110.91	24.929	84.86	20.821
13	54.33	4.786	60.85	5.571	70.50	15.036	93.99	25.679	97.60	27.714	74.93	22.000
14	51.90	9.286	56.61	8.536	63.64	18.679	81.79	28.214	85.88	28.821	66.17	23.750
15	49.58	15.357	52.65	12.893	57.39	22,464	71.16	29.607	75.57	29.214	58.43	25.821
16	47.36	23.964	48.98	20.179	51.76	28.071	61.92	29.857	66.50	29.857	51.59	28.286
17	45.24	31,000	45.56	28.250	46.68	31.000	53.88	30.000	58.52	31.000	45.56	30.000
۸ve.	51.71		55.53		80.21		170.21		192.44		111.30	

Table II 4-39 Monthly Discharge Duration at Tepekisla (Regulated with Afterbay)

Table II-4-40 Monthly Discharge Duration at Tepekisla (Regulated with after bay)

Rank		ul. Duration day	A Discharge cum/s	ug. Duration day		ep. Duration day		ct. Duration • day		lov. Duration day	D Discharge cu m/s	ec. Duration day
1	83.72		59.72		62.12		111.48		119.28		106.28	
2	80.39	0.214	58.50	0.036	60.73	0.071	105.13	0.071	112.15	0.036	100.76	0.036
3	71.17	0.357	57.30	0.107	59.37	0.071	99.14	0.071	105.45	0.107	95.52	0.036
4	74.12	0.536	56.13	0.143	58.04	0.071	93.50	0.071	99.16	0.143	90.55	0.071
5	71.77	0.643	54.99	0.250	56.73	0.107	88.17	0.071	93.23	0.250	85.85	0.071
6	68.34	1.107	53.86	0.393	55.46	0.179	83.15	0.071	87.66	0,250	81.38	0.107
7	65.62	1.321	52.76	0.500	54.22	0.357	78.42	0.107	82.43	0.357	77.15	0.321
8	63.01	1.750	51.68	0.679	53.00	0.464	73.95	0.143	77.50	0.536	73.14	0.500
9	60.50	2.321	50.63	0.964	51.82	0.643	69.74	0.286	72.87	0.714	69.34	0.643
10	58.09	3.214	49.59	1.786	50.65	1.036	65.77	0.536	68.52 [°]	0.857	65.74	0.821
11	55.78	4.536	48.58	4.250	49.52	1.607	62.02	0.714	64.43	1.357	62.32	1.214
12	53.56	7.036	47.59	6.036	48.41	3.071	58.49	1.143	60.58	2.036	59.08	2.071
13	51.43	10.607	46.61	9.036	47.32	5.000	55.16	2.036	56.96	3.893	56.01	3.750
14	49.38	16.250	45.66	18.857	46.26	12.500	52.02	4.250	53.56	5.964	53.10	7.786
15	47.42	21.786	44.73	24.643	45.22	23,607	49.06	8.107	50.36	9.964	50.34	13.607
16	45.53	27.786	43.82	28,964	44.21	27.000	46.26	18.714	47.35	17.643	47.72	22.036
17	43.72	31.000	42.92	31.000	43.22	30.000	43.63	31.000	44.52	30.000	45.24	31.000
Ave.	51.17		46.29		46.33		48.37		50,96		51.23	

	1	lan.		Feb.		dar.	ł	Apr.	м	av.		Jun
Rank	Discharge cu m/s	Duration day	Discharge cu m/s	Duration day	Discharge cu m/s	Duration day	Discharge cum/s	Duration day	Discharge cu m/s	Duration day		e Duratio day
1	202.80		253.68	• •	352.40		502.46		456.22		336.86	
2	157.19	5.590	194.97	0.120	269.69	0.245	398.03	1.164	371.05	1.400	254.35	0.630
3	121.83	8.680	/149.85	7.910	206.40	1.957	315.30	2.840	301.77	4.491	192.05	6.080
4	94.43	8.680	115.17	7.910	157.96	9.002	249.77	6.712	245.43	11.351	145.01	14.859
5	73.19	8.680	88.51	7.987	120.89	9.759	197.85	11.360	199.61	16.893	109.49	14.864
6	56.73	8.680	68.03	8.039	92.52	10.296	156.73	14.299	162.35	18.112	82.67	14.974
7	43.97	8.911	52.28	8.039	70.80	11.240	124.15	17.364	132.04	19.470	62.42	15.735
8	34.08	9.451	40.18	8.450	54.19	13.166	98.35	19.730	107.39	20,996	47.13	17.768
9	26.41	9.709	30.88	9.299	41.47	15.505	77.91	22,970	87.34	23.362	35.59	20,250
10	20.47	10.377	23.74	10.661	31.74	18.374	61.72	25.329	71.03	25.822	26.87	23.015
11	15.87	10.763	18.24	12.487	24.29	21.383	48.89	27.045	57.77	28.155	20.29	25.133
12	12.30	12.563	14.02	14.339	18.59	13.106	38.73	28.652	46.99	29.122	15.32	26.884
13	9.53	15.803	10.78	17.193	14.23	25.806	30.68	29.614	38.21	29.524	11.57	28.298
14	7.39	21.074	8.28	20.536	10.89	27.991	24.30	29.871	31.08	29.740	8.73	28.971
15	5.73	25.394	6.37	24.341	8.33	29.560	19.25	29.897	25.28	30,100	6.60	29.537
16	4.44	29.791	4.89	26.939	6.38	30.383	15.25	29.949	20,56	30.666	4.98	29.717
17	3.44	31.000	3.76	28.250	4.88	31.000	12.08	30,000	16.72	31.000	3.76	30.000
Ave.	51.71		55.53		80.21		170.21		192.44		111.30	

Table II-4-41 Monthly Discharge Duration at Tepekisla (Regulated with after bay)

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Table 11-4-42 Monthly Discharge Duration at Tepekisla (Regulated Without Afterbay)

	1	lui.		ug.		Sep.		Oct.		٩ov.		Dec.
Rank	Discharge cu m/s	Duration day	Discharge cu m/s	Duration day	Discharge cum/s	Duration day	Discharge cu m/s	Duration day	Discharge cu m/s	Duration day	Discharge cum/s	Duration day
1	192.40		168.40		170.80		220.16		227.96	•	214.96	
2	144.26	8.680	123.10	8.680	126.61	8.400	163.20	0.683	172.84	0.400	166.00	0.850
3	108.17	8.680	89.99	8.680	93.86	8.400	120,98	8.680	131.05	8.400	128.20	8.680
4	81.10	8.680	65.79	8.680	69.57	8.400	89.68	8.680	99.37	8.400	99.00	8.680
5	60.81	8.680	48.09	8.680	51.57	8,400	66,48	8.706	75.34	8.426	76.46	8.680
6	45.60	8.680	35.11	8.680	'38.23	8.400	49.28	8.731	57.13	8.503	59.04	8.706
7	34.19	8.963	25.70	8.680	28.34	8,400	36.53	8.757	43.31	8.657	45.60	8.731
8	25.63	9.554	18.79	8.680	21.01	8.400	27.08	8.911	32.84	8.811	35.21	8.911
9	19.22	10.249	13.73	8.834	15.57	8.477	20.07	9.220	24.90	9.146	27.19	9.143
10	14.41	11.663	10.04	9.143	11.54	8.683	14,88	9.786	18.80	9.814	21.00	9.529
11	10.81	14.774	7.34	10.274	8.56	9.146	11.03	11,251	14.32	11.563	16.22	10.557
12	8.10	19.146	.5.36	13.669	6.34	10.843	8.18	13.386	10.85	13.491	12.52	12.743
13	6.07	23.157	3.92	21.280	4.70	16.191	6.06	16.034	8.23	16.166	9.67	16.394
14	4.55	27.940	2.87	26.809	3.49	24.934	4.49	21.820	6.24	19.971	7.47	20.406
15	3.42	29.251	2.10	29.251	2.58	27.737	3.33	28.840	4.73	25.217	5.77	25.111
16	2.56	30.023	1.53	30.640	1.92	28.946	2.47	30.691	3.59	29.229	4.45	29.843
17	1.92	31.000	1.12	31.000	1.42	30,000	1.83	31.000	2.72	30.000	3.44	31,000
A v e.	51.17		46.29		46.33		48.37		50.96		51.23	

Location Condition		Jan.	Feb.	Mar.	Apr.	May	Jun.	Jul.	Aug.	Sep.	Oct.	Nov.	Dec.	Total
KILICKAYA Natural Dis-	Inflow 10 ⁶ m ³ Sediment 10 ³ t	55.15 46 80	66.32	174.26	489.19	437.49	171.28	52.63	30.05	29.32	39.67	50,00	52.93	
charge					14.202.2	06.766,1	1,086.85	52.16	13.23	18.00	37.17	45.73	32.17	6,096.12
TEPEKISLA	Inflow	81.69	69.83	296.88	767.54		265.32		42.13	41,08	57,26	73.74	78.21	
Natural	Sediment	149.44	198.96	2,200.42	9,427.49	4,559.79	2,032.28	205.00	32.33	61.53	85.01	153.66	72.74	19.178
TEPEKISLA	Inflow	138.50	135.54	214.83	441.18	515.43	288.49	137.05	123.98	120.09	125.55	132.09	137.31	•
Afterbay	Sediment	149.44	199.63	870.73	2,737.34	2,199.24	1,874.38	466.55	32.33	61.53	85.01	153.66	72.74	8,902.58
TEPEKISLA	Inflow	138.50	135.54	214.83	441.18	515.43	288.49	137.05	123.98	120.09	125.55	132.09	137.21	
Regulated without Sediment Afterbay	¹⁶ Sediment	149.44	157.20	1,263.69	3,192.34	2,531.19	3,176.71	2.439.30	32.33	61.53	85.01	153.66	72 74	12 215 12
EDIMENT comfi	SEDIMENT coming with Afterbay	102.6	112.9	355.5	1,636.1	1,520.2	1,330.9	440.5	19.1	43.5	47.8	108.0	40.5	5.757.6
o TEPEKISLA	to TEPEKISLA without Afterbay	102.6	70.5	748.49	2,091.1	1,852.2	2,633.2	2,413.2	19.1	43.5	47.8	108.0	40.5	10.170.2

From FEB. to JUL. Sediment coming to Tepekısla is got reducting half of the amount caught in Kilickaya from the value caluculated at Tepekisia according to the regulated discharge.

 From AUG, to JAN. Sediment coming to Tepekisla is got reducting the amount caught in Kilickaya from the value caluculated at Tepekisla according to the matural discharge. Sedimentation Amount Comming to Ayracik Considering the Discharge Regulation Effect by Killckaya Dam Table II 4-44

	-	Upstream Area:	rea:		Ayvacik	ıcik	
Discharge Condition	Tepekisla.	Тазоуа	between Tepekisla, Tasova & Ayvacik	Primary Sediment Load	Bed load	Tatal Load 10 ³ ton	Total Volume 10 ⁶ m ³
Natural	19.179	9.818 2.233	2.233	31.230	6.246	37.476	30.00
Regulated with Afterbay	5.758	9.818 1.475	1.475	17.051	3.410	20.461	16.35
Regulated without Afterbay	10.170	9.818 1.829	1.829	21.817	4.364	26.181	20.96

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Note : 1. From Tasova, Almus dam effect is not considered.

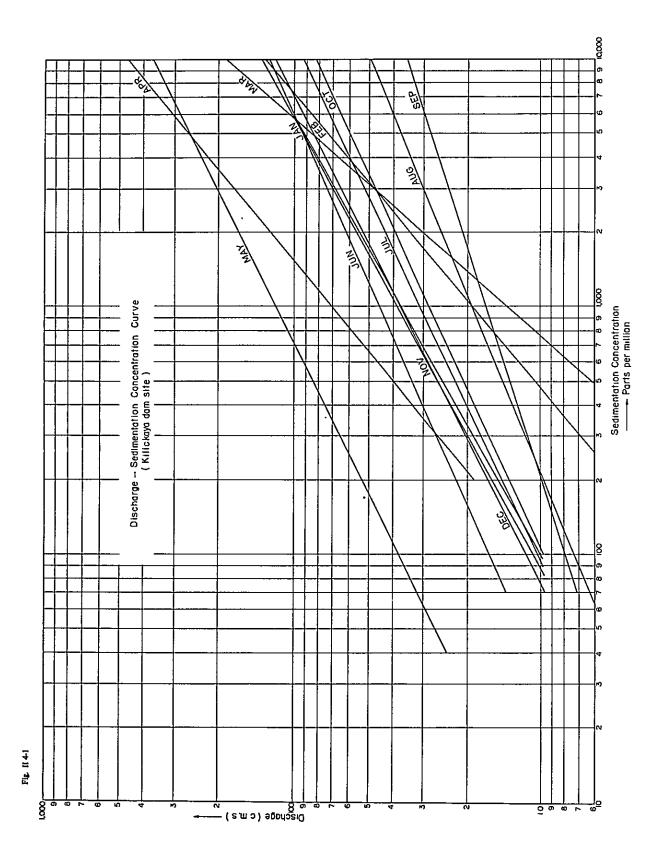
2. Sediment amount/produced in the area between Tepekisia, Tasova and Ayracik is approximately modified considering the discharge regulation.

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3. For the addition of bed load, 20% factor is applied.

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II 5 Power Study .

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	Preparation of Development Plan	5 - 1
II 5-2	'Evaluation of Development Plan	5 - 2
П 5-3	Supply and Demand Balance	5 - 4 .
¥. ~ `	II 5-3-1 Annual Load Factor and Daily Load Factor	5 - 4
	II 5-3-2 KW Balance.	5 - 4
	II 5-3-3 KWh Balance	5 - 5

Tables

II 5-1-1	Expansion Plan – 6	5 - 6
II 5-1-2	Expansion Plan – 6	5 - 6
II 5-2-1	Recommende Program Development Plan (EPDC)	5 - 7
II 5-2-2	Recommended Program Development Plan (EPDC)	5 - 7
II 5-3-1	Investment Schedule No. 6 Plan	5 - 8
II 5-3-2	Investment Schedule EPDC Plan	5 - 8
II 5-4	Annual Cost Factor	5 - 9
II 5-5-1	No. 6 Plan Benefit and Cost Over 50 years (Interest Rate 5%)	5 - 9
II 5-5-2	EPDC Plan Benefit and Cost Over 50 Years (Interest Rate 5%)	5-10
II 5-5-3	No. 6 Plan Benefit and Cost Over 50 Years (Interest Rate 8%)	5-10 ·
II 5-5-4	EPDC Plan Benefit and Cost Over 50 Years (Interest Rate 8%)	5-11
II 5-6	Load Factor in whole Turkey	5-11 ¹ 2
II 5-7-1	Hydroelectric Plants	5-12
II 5-7-2	Thermal Power Plant	5-12
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Figure

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II 5-1

KW Balance in Tuckey (1975 - 1983)

5-13

II-5 POWER STUDY

II-5.1 Preparation of Development Plan

Power demand in Turkey is increasing at the rate of about 13% annually. To meet this demand in the most economical and technically reliable manner, it is necessary to select a reasonable combination of hydro and thermal power and determine the start-up time of each power plant. Such a development plan is being studied from every points of view, and six proposals have been presented by Etibank. Since the No. 6 plan is considered the most appropriate, facility expansion plans and other plans are being studied on the basis of this plan. The No. 6 plan, as shown in Table II 5-1, covers the development project up to 1977. It dose not envisage any means of direct supply of power to meet the demand in the Eastern Black Sea system, but proposes instead the construction of 380 kV transmission lines between Keban and Trabzon.

Against the proposed of Etibank the supply of power to the Eastern Black Sea system was made the essential core of the present studies and a development plan was worked out which includes both the Ayvacik and Kilickaya Project with the following considerations.

(1) Among the projects proposed in the No. 6 plan which covers the period up to 1977 those that are scheduled to start operation by 1972 are seemingly at construction stage by present time and will allow no change. Therefore the present plan was formulated for the period from 1973 to 1977 with the inclusion of the Ayvacik and Kilickaya Projects.

Because of the need for the study of kw balance and economic evaluation, a project for the period from 1978 to 1983 was also formulated as additional information.

(2) The EPDC plan calls for the postponment of the Oymapinar 216MW Project of the No. 6 plan to 1977, and instead suggests to move the Ayvacik1st stage250 MW power plant to 1975. The starting time of operation of Ayvacik powerstation was decided in view of an expected shortage in the supply capacity of the Eastern Black Sea system in 1974 and the estimated construction period of the project.

(3) Operation of Kilickaya Project, in view of its function to protect Ayvacik Reservoir from sedimentation and to supply irrigation water to Carcamba Plain in the downstream area, was proposed for 1977 in order to start construction as early as possible after the completion of Ayvacik Project. It was also proposed to expand the Ayvacik powerplant in second stage since its firm discharge will increase with the completion of Kilickaya Project.

(4) Operation of nuclear power generating facilities was proposed for 1982 taking into account the current progress in this field in foreign countries.

(5) The EPDC proposal approximates the power capacity of the No. 6 plan. In other words, the dependable capacity, firm energy and reserve capacity would be the same as those under the No. 6 plan.

The EPDC development plan is shown in Table II 5-2.

II-5.2 Evaluation of Development Plan

Comparative evaluation of the development plan was made from two different aspects, namely, the amount of investment and the surplus benefit, as well as from a technical point of view. As described in paragraph 1 of the previous section, the only difference between the No. 6 plan and the EPDC plan lies in the period from 1973 to 1977 (a substantial difference lies in the period from 1975 to 1977), and therefore the comparison was made only for this period.

(1) Amount of Investment

A comparison was made by calculating the required funds for both plans for each calender year and converting them to the current worth in 1969. Data for both the Ayvacik and Kilickaya Project is based on EPDC's interim results (for power only after allocation to irrigation), and all others are based on Etibank's data. Present worth was computed at the interest rate of 8% and 5% respectively, and in both cases the present worth under the EPDC plan is found to be lower than that under the No. 6 plan. Although the No. 6 plan includes the cost of the 380 kw transmission line between Keban and Trabzan, computation reveals the superiority of the EPDC plan even when the cost of the transmission line is not included. (See Table II 4-3)

(2) Surplus Benefit

Benefit and cost were calculated for a service life of 50 years on the following conditions and converted into the present worth in 1975, at interest rates of 8% and 5%, upon which an equalized annual cost and benefit over 50 years was calculated, From this figure the surplus benefit was calculated.

For the kw for hydro power.dependable capacity or the December output was taken, and for alternative thermal power installed capacity was adopted. Kwh for hydro power was obtained in two cases, namely, firm energy and average available energy, and for thermal power it was obtained on an assumed plant factor. In the case of thermal power it would not be practical to consider that a high plant factor of 70% to 80% could be maintained throughout the entire period of service life and there is a possibility of overevaluating kwh value of thermal power. A thermal power plant can be operated with a high plant factor for 5 years or so after start-up, but thereafter it is operated with a decreasingly lower plant factor until in the end it is for stand-by use only. For this reason, the power energy to be generated was obtained by using a lower factor of 15%, the plant factor at the initial stage of operation, as the plant factor for the entire period of service life. As for gas turbine power, since it was considered to be used for relite purposes for a short period of time, and no kwh was considered to incur after a five years period, it was designated for stand-by use.

To simplify the calculation, it was assumed that one-half of the power energy generated would be effectively used in the first year of operation and the total energy was presumed to be used effectively from the second year.

As for the unit price of the benefit, the kw and kwh cost for the oil-burning 300 MW unit standard thermal power plant of the central system, calculated in the chapter for economic evaluation, was adopted. For the kw value, however, a kw compesation factor was adopted to make the reliability of hydro and thermal power even, and a factor of 1.15 was adopted for hydro power and 1.0 for thermal power.

As for the annual cost factor, the value shown in Table II 5-4 was adopted for each category of the facilities such as hydro power and thermal power. For fuel cost, calculation was made on the basis of heavy oil for thermal plants, at a unit price of 253 TL/ton, the price agreed on with Etibank and diesel oil at a unit price of 455 TL/ton for gas turbine plants. For the fuel cost for nuclear power generation, 2.0 mill per kwh or 1.8 kr/kwh was adopted.

Results of the calculations made under the conditions described above are summarized in Tables Table II 5-5. These results show the EPDC plan is superior to the No. 6 plan at both 8% and 5% interest rates, and the superiority is greater when the interest rate is 8%.

It is not conceivable that the No. 6 plan would be more advantageous than the EPDC plan even when the transmission line between Keban and Trabzon is excluded from the plan. Also with fuel cost for nuclear power generation, it is obvious that the superiority of the EPDC plan over the No. 6 plan will be kept even when the cost drops to 1.5 mill./kwh level.

II 5-3 Supply and Demand Balance

II 5-3-1 Annual Load Factor and Daily Load Factor

As shown in Table II 5-6, the annual load factor for the entire area of Turkey was a considerably low rate of 48.9% in 1965 and 47.7% in 1966.

The interconnected system, on the other hand, because of its coverage in many industrialized districts, had a load factor of 63.6% in 1965 and 62.1% in 1966, about 15% higher than the former. Data on the daily load factor is available only for the interconnected system, and it ahows a factor of around 75%. However, in the future when the interconnected system program is extended and low demand density districts come under the system, it is conceivable that the daily load factor will drop accordingly.

In this load forecast a constant load factor was used for the entire period of forecast with an annual load factor of 60% and a daily load factor of 71.5%. A model load duration curve was provided on the badis of these daily load curves for the convenience of the study of supply and demand balance and the study of kw balance.

II 5-3-2 KW Balance

The most critical month in the supply and demand balance is December. During this month the power supply capacity of hydro power plants drops because of the decrease in river flow while the demand reaches the highest level of the year. Therefore, the kw balance was based on the daily load curve for weekdays of December, and the study was made with the use of the model daily load curve described in the preeding section. For the demand in this case, an annual maximum demand was obtained on the basis of Etibank's load forecast and the supply power from the EPDC plan. As for hydro power supply capacity, either the dependable capacity or the December output was adopted. For daily power generation, 1/365 of the annual firm energy was adopted because of the inadequacy of available data. For thermal power supply capacity installed capacity was adopted and flat operation with a 100% plant factor was considered. Details of the elements of each supply capacity, used for the study of balance, are shown in Table II 5-7.

In preparing the kw balance the thermal power plant was presumed to take over the basic portion of the load in the system. The hydro electric-system was divided into the runof-river type and the reservoir type with regulating ability. The run-of-river type were presumed to take charge of flat operation and the reservoir type, the peak portion. Whichever comes first into operation was designated to take over the peak portion before the other. However, even the hydro power plants with an extremely higher power energy (designed for a higher plant factor) compared with the installed capacity such as the Keban and the Lower Firat were designated to take over the basic portion of the load in the system.

The study covered every year during a period of 9 years from 1975 to 1983. Since the operation of the Kilickaya power plant is scheduled for 1977, this coverage is considered sufficient for the study of the effectiveness of the Kilickaya power plant facilities.

The results of the study are shown in Fig.II 5-1. It shows that the Kilickaya power plant will have an effective 50MW as against a dependable capacity of 76MW in December 1977, the year of initial operation. It clearly shows that the whole dependable capacity is used effectively in 1979, two years later.

II 5-3-3 KWH Balance

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Annual kwh balance shown in Table II 5-2-2 shows that there is a 1.6% or more reserve capacity even in terms of firm energy and sufficient supplying capacity.

5-5

Table	11 5-1-1	Expansion	Plan-6
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Power St	ation	Туре	Date	Output
Ambarli	4	T	Aug. 1970	150
Ambarl1	3	т	Sept. 1970	115
Ambar 11	5	Ţ	Oct. 1970	150
Hopa		н	May 1970	- 50
logankent		н	May 1970	12
Dogankent (E	xtension)	R	May 1970	8
Fortum (E	xtension)	н	Jan. 1971	7
Gokcekaya	1	ĸ	Aug. 1971	100
Seyitomer	1	т	Aug. 1971	150
Gokcekaya	2	н	Nov. 1971	100
Kovada II		н	Jan. 1972	, 51
Gokcekaya	3	н	Feb. 1972	100
(adincik I		, H	Mar. 1972	70
Keban	1.2	н	Mar. 1972	310
lagcag		н	Mar. 1972	9
iersin (Exte	•	T	Mar. 1972	50
leban	3	н	Jun. 1972	155
Keban	4	Ħ	Nov. 1972	155
)ymap ina r	1	н	Jun. 1975	72
Keban	5	٠н	Aug. 1975	155
)ymapinar	2	н	Sept, 1975	72
)ymapinar	3	н	Nov. 1975	72
leyitomer	2	T	Aug. 1976	150
leban	6	н	Sept. 1976	155
as Turbine		T	Aug. 1977	75
luclear		Т	Sept. 1977	, 500

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Table II 5-1-2 Expansion Plan-6

	Syst	em Capa	city	De	mand		Reserve						
fear 	MW	Ave GVH	Firm GWH	нw 	GWH	ми	7.	GWH	z	Dry CWH	7		
1968	1,185	5,934	5,466	1,095	5,300	90	8.2	\$34	12.0	166	3.0		
1969	1,305	6,098	5,625	1,235	6,337	70	5.6	-239	-3.7	-712	-11.0		
1970	1,804	7,943	7,296	1,550	8,100	254	16.4	-157	-1.9	-804	-11.1		
1971	2,169	10,881	10,019	1,920	9,262	252	13.1	1,633	17.6	757	8.1		
1972	3,162	15,906	14,855	2,260	11,842	902	40.0	4,063	34.3	3,013	25.0		
1973	3,162	18,193	16,977	2,550	13,672	612	24.0	4,521	33.0	3,305	23.0		
1974	3,162	18,193	16,977	2,900	15,222	263	9.2	2,971	19.5	1,755	11,5		
1975	3,534	19,073	17,957	3,180	16,700	354	10.8	2,373	14.2	1,257	7.5		
1976	3,839	20 •933	19,617	3,520	18,500	319	9.1	2,433	13.1	1,117	6,1		
1977	4,414	22,553	21,237	3,920	20,600	494	12.6	1,953	9.5	637	3.1		

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			Plant Capabili	Lty	S	ystem Capabilin	ty
Year	Project	Dependable (Dec.)Output MW	Ave. Energy Gwh	Firm (Dry Year) Energy (Gwh)	Dependable (Dec.) Output MW	Ave. Energy GWh	Firm (Dry Year) Energy (GWh)
1974	· · · · ·	-		-	3,162	18,193	16,977
1975	Ayvacik 1, 2	175	1,100	600			
	Keban 6	155	800	550	3,492	20,093	18,127
1976	Seyitomer 2	150	1,120	1,120			
	Keban. 6	155	200		3,797	21,413	19,247
1977	Kilickaya	76	337	280			
	Oymapinar 1 - 3	216	1,440	750			
	Ayvacik 3,4	175	100	200			
	Gas Turbine	75	460	460	4,339	25,750	20,937
1978	Lower First 1 - 3	540	4,300	4,300	4,879	28,050	25,237
1979	Lower First 4, 5	360	2,290	1,320	5,239	30,340	26,557
1980	Izmir (Nuclear)	500	3,700	3,700	5,739	34,040	30,257
1981	Keban 7, 8	310	270	-			
	Elbistan l	300	2,100	2,100	6,349	36,410	32,357
1982	Lower First 6 - 8	540	3,500	3,500	6,889	39,910	35,857
1983	Lower First 9, 10	360	3,400	3,400			
	Elbistan 2	300	2,100	2,100	7,549	45,410	40,357

Table II 5-2-1 Recommended Program of Development Plan (EPDC)

Table II 5-2-2 Recommended Program of Development Plan (EPDC)

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			bility	Den	and	Reserve						
Year	Dependable (Dec.) Output (HM)	Ave. Energy (GWh)	Firm (Dry Year) Energy (GWh)	Peak Demand (MW)	Energy Demand (GWh)		endable) Output	Åve	. Energy		(Dry Year) rgy	
	(114)			((194))	HW	z	CWh	r	GWh	7		
1974	3,162	18,193	16,977	-	-	-	-	-	•	-	-	
1975	3,492	20,093	18,127	3,180	16,700	312	10.1	3,393	20.3	1,427	8.5	
1976	3,797	21,413	19,247	3,520	18,500	277	7.9	2,913	15.7	747	4.0	
1977	4,339	25,750	20,937	3,920	20,600	419	10.7	3,150	15.3	337	1.6	
1978	4,879	28,050	25,327	4,310	22,650	569	13.2	5,400	23.8	2,587	11.4	
1979	5,239	30,340	26,557	4,740	24,850	499	10.5	5,480	22.0	1,707	6.9	
1980	5,739	34,040	30,257	5,210	27,400	529	10.1	6,640	24.2	2,857	10.4	
1981	6,349	36,410	32,357	5,730	30,100	619	10.8	6,310	21.0	2,257	7.5	
1982	6,889	39,910	35,857	6,300	33,100	589	9.4	6,810	20.6	2,757	8.3	
1983	7,549	45,410	40,357	6,880	36,200	669	9.7	9,210	25.4	4,157	11.5	

										ť	lnit: 10 ⁶	TL
Total Con- struction Cost	1969	1970	1971	1972	1973	1974	1975	1976	1977			
700.0	_		50.0	100.0	200.0	300.0	50.0					
70.0						40,0	30.0					
361.2 70.0						43.3	227.6 40.0	90.3 30.0				
100.0 1,080.5	13.5	8.0	8.0	8.0	8.0	160.1	384.1	30.0 405.4	70.0 85.4			
128.7	0.2	10.2	63.5	50.0	4.7							
2,510.4	13.7	18.2	121.5	158.0	212.7	543.4	731.7	\$\$5.7	155.4			
	0.9524	0.9070	0.8638	0.8227	0 7835	0.7462	0.7107	0.6768	0.6446			
9 1,832.5	13.0	16.5	105.0	130.0	166.7	405.5	520.0	376.1	99.7			
	0.9259	0.8573	0.7938	0.7350	0.6806	0.6302	0.5835	0.5403	0 5002			
9 1,533.3	13,1	15.6	96.4	116.1	144,8	342.5	426.9	300.2	77.3			
	struction Cost 700.0 70.0 361.2 70.0 1,080.5 128.7 2,510.4 9 1,832.5	struction Cost 1969 700.0 - 70.0 - 361.2 - 70.0 - 100.0 13.5 128.7 0.2 2,510.4 13.7 0.9524 9 9 1,832.5 13.0 0.9259 0.9259	struction Cost 1969 1970 700.0 - - 70.0 - - 361.2 70.0 - 70.0 13.5 8.0 128.7 0.2 10.2 2,510.4 13.7 18.2 0.9524 0.9070 9 1,832.5 13.0 16.5 0.9259 0.8573	struction Cost 1969 1970 1971 700.0 - 50.0 70.0 - 50.0 361.2 - - 70.0 - - 100.0 13.5 8.0 8.0 128.7 0.2 10.2 63.5 2,510.4 13.7 18.2 121.5 0.9524 0.9070 0.8638 9 1,832.5 13.0 16.5 105.0 0.9259 0.8573 0.7938	struction Cost 1969 1970 1971 1972 700.0 - 50.0 100.0 70.0 - 50.0 100.0 100.0 13.5 8.0 8.0 8.0 128.7 0.2 10.2 63.5 50.0 2,510.4 13.7 18.2 121.5 158.0 0.9524 0.9070 0.8638 0.8227 9 1,832.5 13.0 16.5 105.0 130.0 0.9259 0.8573 0.7938 0.7350	struction Cost 1969 1970 1971 1972 1973 700.0 . 50.0 100.0 200.0 361.2 70.0 . 50.0 100.0 200.0 100.0 13.5 8.0 8.0 8.0 8.0 128.7 0.2 10.2 63.5 50.0 4.7 2,510.4 13.7 18.2 121.5 158.0 212.7 0.9524 0.9070 0.8638 0.8227 0.7835 9 1,832.5 13.0 16.5 105.0 130.0 166.7 0.9259 0.8573 0.7938 0.7350 0.6806	struction Cost 1969 1970 1971 1972 1973 1974 700.0 - 50.0 100.0 200.0 300.0 70.0 - 50.0 100.0 200.0 300.0 361.2 70.0 - 43.3 100.0 13.5 8.0 8.0 8.0 160.1 128.7 0.2 10.2 63.5 50.0 4.7 2,510.4 13.7 18.2 121.5 158.0 212.7 543.4 0.9524 0.9070 0.8638 0.8227 0 7835 0.7462 9 1,832.5 13.0 16.5 105.0 130.0 166.7 405.5 0.9259 0.8573 0.7938 0.7350 0.6806 0.6302	Total Con- struction Cost 1969 1970 1971 1972 1973 1974 1975 700.0 - 50.0 100.0 200.0 300.0 50.0 70.0 - 50.0 100.0 200.0 300.0 50.0 361.2 - 43.3 227.6 40.0 300.0 100.0 13.5 8.0 8.0 8.0 160.1 384.1 128.7 0.2 10.2 63.5 50.0 4.7 - 2,510.4 13.7 18.2 121.5 158.0 212.7 543.4 731.7 9 1,832.5 13.0 16.5 105.0 130.0 166.7 405.5 520.0 0.9259 0.8573 0.7938 0.7350 0.6806 0.6302 0.5835	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$			

Table II 5-3-1 Investment Schedule No 6 Plan

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Table II 5-3-2 Investment Schedule EPDC Plan

									Unit:	10 ⁶ TL	
Power Plant	Total Con- struction Cost	1969	1970	1971	1972	1973	1974	1975	1976	1977	1978
Ayvacik 1,2 Keban 5	365.0 70.0			36.5	66.0	87.5	84.0 40.0	62.0 30.0	29.0		
Seyitomer 2 Keban 6	361.2 70.0						43.3	227.6 40.0	90.3 30.0		
Kelkit Oymepinar 1, 2, 3	263.0 700.0					26.5 50.0	47.0 100.0	63.0 200.0	60.5 300.0	45.0 50.0	21.0
Ayvacik 3,4 Gas Turbine	110.0 100.0								65.0 30.0	45.0 70.0	
Total	2,039.2			36.5	66.0	164.0	314.3	722.6	604.8	210.0	21.0
5% Interest Rate											
Present Worth Fa Present Worth in		0.9524	0,9070	0.8638 31.5	0.8227 54.3	0.7835 128.5	0.7462 234.5	0.7107 442.5	0.6768 409.3	0.6446 135.4	0.6139 12.9
8% Interest Rate											
Present Rate		0.9259	0.8573	0.3938	0.7350	0.6806	0.6302	0.5835	0.5403	0.5002	0.4632
Present Worth in	1969 1,192.0			29.0	48.5	111.6	198.1	363.3	326.8	105.0	

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Table II 5-4 Annual Cost Factor

· · · · · · · · · · · · · · · · · · ·	Serviceable Year	Interest Rate,	Interest and Depreciation		Insurance	Operation and Maintenance	Administration	Total
								-
Hydro	50	5 🔬	5,478	0.20	0.056	0.7	0.3	6,734
		8	8,174	0,20	0.056	0.7	0.3	9,430
Thermal	35	5	6,107	0.35	0.200	2.2	0.3	9.157
THEE MAY		, 5 , 8	8,580	0.35	0.200	2.2 2.2	0.3	9,157 11,630
Nuclear	35	5	6,107	0.35	0.750	. 2.2	0.3	9,707
AUCTEST .	55	8	8,580	0.35	0.750	2.2	0.3	12,180
Gas Turbine	25	- c	7,095	0.50	0.202	2.2	0,3	10,297
CES INCOME	25	5	9,368	0.50	0 202	2.2	0.3	12,570
Transmission Line	e 50	5	5,478	0.05	• - 、	2.5	0.5	8,525
IT AUSAISSION LIN	2 30	8	8,174	0.05	-	2.5	0.5	11,224
	- <u>,</u> ,	,	-			-		

Table II 5-5-1 No. 6 Plan benefit and Cost Over 50 Years (Interest Rate 5%)

		_								Cost	Unit	: 10 ⁶ TI		
		Capabili				enefit Wh	Tot	· • 1		LOSE		Surplus Benefit		
	Dependable Output (MW)	Energy (GMH)	Average Year Energy (GWH)	(1) / KW	Firm(2)	Average(3)	(4) (1)+(2)	al (5) (1)+(3)		Fuel	(6) Total	(4)-(6)	(5)-(6)	
)ymapinar	216	750	1,440	562.1	, 745.0	1,431.3	1,307.1	1,993.4			835.7			
Keban 5	155	550	800	404.0	518.2	794.8	922.2	1,198.8	83.6		83.6			
Seyitomer 2	150	~ 790	790	323.1	748.4	748.4	1,071.4	1,071.4	558.7	736.6	1,295.3			
Keban 6	155	-	200	384.8	-	189.7	348.8	574.5	79.6	-	79.6			
Gas Turbine -	75	- 400	400	- 154.0	78.3	78.3	232.3	232.3	166.0	237.7	403.7			
Nuclear	500	3,070	3,070	1,027.5	2,767.2	2,767.2	3,794.7	3,794.7	1,691.5	891.8	2,583.3			
Fransmission Line (Keban - Trabzon)	-	-	-	-	•	-	-	-	296.3	-	296.3			
Cotal Present Worth in 1975	<u>.</u>	Y		_	*		7,712.5	8,865.1	3,711.4	1,866.4	5,577.5	2,135.0	3,287.	
Qualized Annual Benefit and Cost Over 50 years (Capital Recovery Factor: 5.478%)	~			-			422.4	485.6	203.3	102.2	305.5	117.0	180.	

Table 11 S-5-2 EPDC Plan Benefit and Cost Over 50 Years (Interest Rate 5%)

											Uni	t: 10 ⁶ Τ!	•		
		Capabil	ity -	-						- Cost			. Surplus Benefit		
	Dependable Output (MH)	Firm Energy (GWH)	Average Year Energy (GWH)	кч ⁽¹⁾	Firm(2)	Average(3)	(4) ¹⁰ (1)+(2)	tal(5) (1)+(3)	Fiexed	Fuel	(6) Total	(4)-(6)	(5)-(6)		
Ayvacik 1, 2	175	600	1,100	456.4	595.5	1,098.6	1,051.9	1,555.0	436.5	,	611.7				
Keban 5	155	550	800	403.5	547.7	794.8		1,198.3	83.7		117.3				
Seyitomer 2	150	790	. 790	323.4	748.8	748.4	1,071.8	1,071.8	560.1	736.6	1,447.7				
Keban 6	155	-	200	384.2	-	189.7	384.2	573.9	79.7		111.7	,			
Kilickaya	76	280	337	178.7	253.1	303.1	431.8	491.8	285.4		399.9				
Dymapinar	216	750	1,440	510.7	675.7	1,298.1	1,186.4	1,808.8	759.4		1,064.3				
Ayvacik 3, 4	175	200	100	414.0	180.6	90.3	594.6	504.3	119.7		-167.7	-			
Gas Turbine	75	400	400	153.6	78.3	78.3	241.9	241.9	166.0	237.7	403.7				
Total Present Worth in 1975	-	-	i	-	• •		[°] 5,913.8 [°]	7,445.8	2,490.6	974.3	3,464.9	2,446.9	3,980.9		
Equalized Annual Ber and Cost over 50 ye							324.0	407.9		53.4	189.8	134.2	218.1		

Equalized Annual Benefit and Cost over 50 years (Capital Recovery Factor: 5.478%)

		Tabl	e II 5-5-3 No 6	Plan Ben	efit and Co	ost Over 50 Yea	a rs (I nterest	Rate 8%)			- Unit	. 10 т	-`~ L ~^^ `
	Dependable Output (HW)	Capabili Firm Energy (GWH)	Average Year Energy (GMR)	(1) Ku		Senefit Wh Average ⁽³⁾	(4) ^{T(} (1)+(2)	otals) (1)+(3)	Fixed	Cost Fuel	(6) Total		s Benefit (5)-(6)
ygapinar	216	750	1,440	478.3	493.2	947.4	971.5	1,425.7	776.9		776.9		
leban 5	155	550	800	343.7	361.3	526,1	705.0	869.8	77.7	-	77.7		
Seyitomer 2	150	790	790	267.3	481.6	481.6	748.9	748.9	457.7	474.1	931.8		
leban 6	155	-	200	318.2	-	122.1	318.2	440.3	71.9	-	71.9	- - (*	-
as Turbine	75	400	400	123.7	67.8	67.8	191.5	191.5	127.1	205.8	332.9		
uclear	500	3,070	3,070	826.4	1,731.6	1,731.6	2,558.0	2,558.0	1,327.9	558.0	1,885.9		· · ·
ransmission Line Keban - Trabzon)	-	-	-	-	-	-	-	-	213.6	-	213.6	• ,	v
otal Present Worth in 1975		<u></u>					5,493.1	6,234.2	3,052.8	1,237.9	4,290.7	1,202.4	1,934.5

Table II S-S-4	EPDC Pian Benefit and Cost Over 50 Years (Interest Rate 8%)
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		··.									Ünit	: 10 ⁶ TL	ı
		Capabili	ty		. В	enefit				Cost		Surplus	Benefit.
а -	Dependable Output (MJ)	Firm Energy (GWH)	Average Year Energy	(1)	Firm(2)	KWh(3) Average (3)	(4) ^{Tot} (1)+(2)	(1)+(3)	Fixed	-Fuel	Total ⁽⁶⁾		
Ayvacik 1, 2	175	600	1,100	387.5	395,3	722.2	782.8	1,109.7	404.9	-	404.9		
Keban 5	155	550	800	343.7	361.3	526.1	705.0	869.8	- 77.7	-	77.7		
Seyitomer 2	150	790	790	267.3	481.6	481.6	748.9	748,9	457.7	474.1	931.8		
Keban 6	155	-	200	318.2	-	122,1	318.2	440.3	71.9	-	71.9		
Kilickaya	76	280	337	144.5	158.3	189.7	302.8	334.2	250.2	-	250.2		
Oymapinar	216	750	1,440	410.1	422.8	812.2	832.9	1,222,3	666.0	-	666.0		
Ayvacik 3, 4	175	200	100	332.5	112.4	56.5	454.9	389.0	104.9	-	104.9		
Gas Turbine	75	400	400	123.5	68.0	68.0	191.5	191.5	127.1	205.8	332.9		
Total Present Worth in 1975							4,337.0	5,305.7	2,160.4	679.9	2,840.3	1,496.7	2,465.4
Equalized Annual Be and Cost over 50 y (Capital Recovery)	ears	74%)	2				354.5	433.7	176,6	55.6	232.2	122.3	201.5

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Table 11 5-6 Load Factor in whole Turkey

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Year	Peak Load	Annual Consumption	Average Power	Annual Load Factor
	(167)	(Gvfl)	(197)	(%)
1955	366	1,347	153.8	41.2
1956	399	1,545	176.4	40.6
1957	434	1,757	200.6	46.1
1958	50.1	1,962	224.0	44.7
1959	558	2,170	247.7	44.3
1960	617	2,396	273.5	44.3
1961	694	2,585	295.1	42.5
1962	725	3,059	349.2	48.2
1963	829	3,406	388.8	46,9
1964	884	3,750	428,1	48.4
1965	980	4,202	479.7	48.9
1966	1,127	4,707	537.3	47.7
1967	1,272			

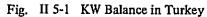
Table 11 5-7-1	Hydroelectric Plants	,		
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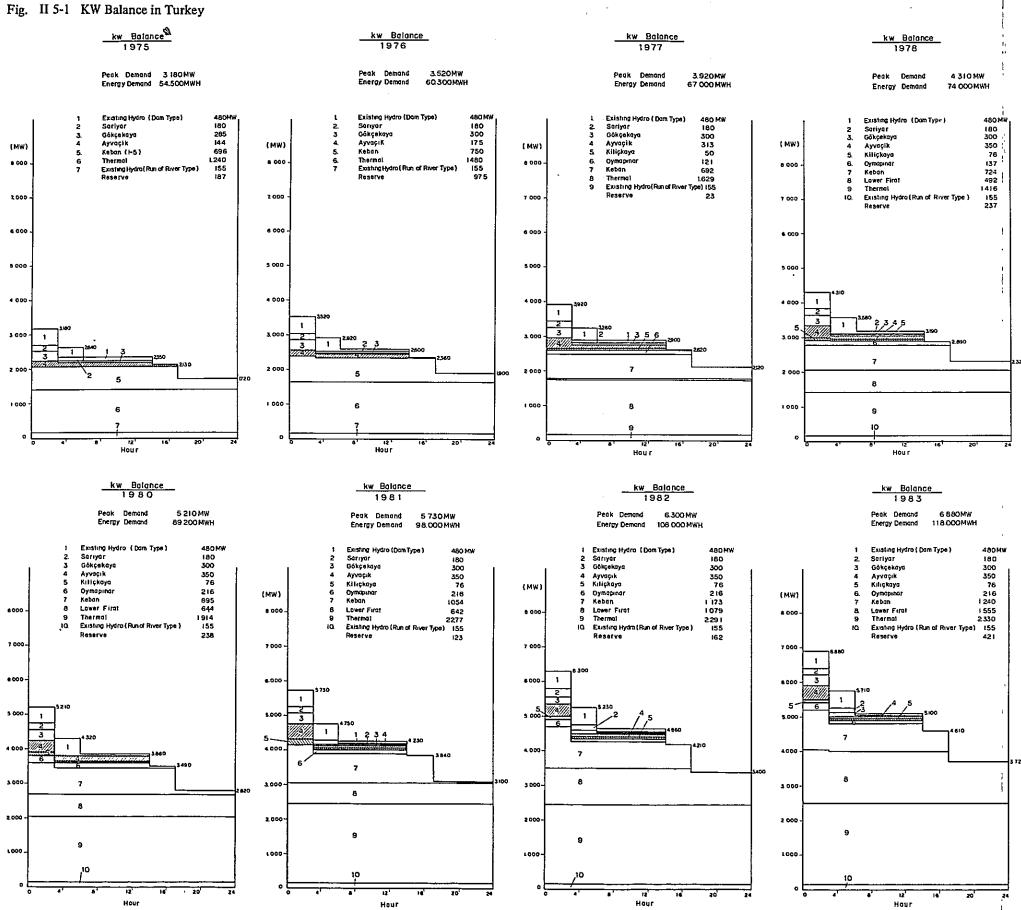
					Annua 1	Energy		
Power Plant	Туре	Year of Initial - Operation	In+talled - Capacity MW	Dependable (or Dec.) Output HW	Average Year	(or Dry year) CWH	· - ••	· -
Sariyar	D	1956	4 x 40	180	430	310		• •
Hrifanli	D	1959	3 x 32	93	320	200		
Kesikkopru	D	1967	2 x 38	76	210	160		
Demirkopru	• D	1960	3 x 23	- 72	200 '	130		
Keme r	D	1958	3 x 16	48	160	130		
Almus	D	1966	27 .	- 27	66	35		
Kazar I & II	D	1957	20 + 10	30	168	158		
Seyhan	D	1958	54	- 50	352	- 248		
Kadincik	D	1970	2 x 35	70	315	190		
Dogankent	R	1970	32.8	20	228	190		
fortum	D	1970	$11 + 2 \times 7$	13	130	69		
Kovađa II	R	1972	48	51.2	- 220			
Gokcekaya 1+2	D	1971	2 x 100	200	500	220		
Gokcekaya 3	D	1972 -	1 x 100	100	70	500		
Keban 1-4	Ð	1972	4 x 155	620			•	
fiscellaneous Run of River type	R	-	121.6	81.8	4,600 665	4,600 517		
lyvacik 1, 2	D	1975	2 x 125	175	1,100	600		~
(eban 5	D	1975	1 x 155	155	800	550		
Keban 6	D	1976	l x 155	155	200	310		
Cilickaya	Þ	1977	2 x 60	76	337	280		
)ymapinar	Þ	1977	3 x 90	216	1,440	750		
iyvacik 3, 4	D	1977	2 x 125	175	100	200	``	
ower First 1, 2, 3	Þ	1978	3 x 180	540	4,300	- 4,300 -		
ower First 4, 5	D	1979	2 x 180	360	2,290			
(eban 7, 8	D	1981	2 x 155	310	270	1,320		
ower First 6, 7, 8	Ð	1982 -	3 x 180	- 540 -	3,500	· 7 . roo `		
over First 9, 10	D	1983	2 x 180	360	3,400	3,500 3,400		

* Note: D: Dam Type R: Run of River Type

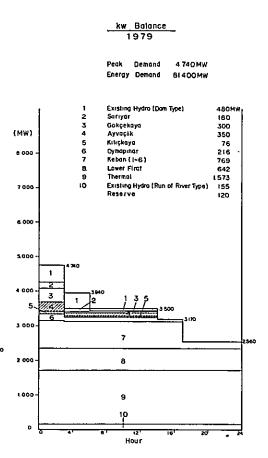
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	Table II :	5-7-2 Thermal Power Plant		
Power Plant	Year of Initial Operation	Installed Capacity (MW)	Maximum Continuous Rating (MW)	Annua] Energy _ (GWH)
Catalagzi	1948	6 x 20	120	775
Tuncbilek	1956	2 x 32 + 60	120	830
Ambarli	1967	2 x 110	230	1,610
Silahtar	1913	120	80	500
Mersin	1963	4 x 25	100	700
Ambarli 3	1970	1 x 110	115	800
Ambarli 4, 5	1970	2 x 150	300	2,100
Hopa	1970	2 x 25	50	350
Miscellaneous	-	193	165	825
Seyitomer 1	1971	1 x 150	150	1,120
Seyitomer 2	1976	1 x 150	150	1,120
Gas Turbine	1977	1 x 75	75	450
Nuclear	1980	1 x 500	500	3,800
Elbistan 1 Elbistan 2	1981 1983	1 × 300 1 × 300	300 100	2,100 2,100





5-13



II 6 Irrigation

Contents

II 6-1	Summary of NIKSAR Report	6-1
II 6-2	Summary of ERBAA Report	6-4
II 6-3	Summary of LEEDSHILL Report	6-6

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Tables

.

II 6-1	Economic Justification of Proposed Project	6-9
II 6-2	Economic Analysis of Carsamba Plan Irrigation for Various Areas	6-9

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II 6 IRRIGATION

(EXISTING REPORT)

II-6.1 Summary of NIKSAR Report

Project Site

Niksar plain spreads along the Kelkit River around the town of Niksar and is located just upstream of Erbaa Plain.

Introduction of the Project

In order to obtain the utmost benefit out of the Kelkit River, the following development schemes have been proposed.

1. Construction of a diversion dam for irrigation purpose at the Fatili site.

2. Irrigation system for 6,714 hectares of land based on land classification of 10,215 hectares of the Niksar plan i.e., a 32,400 meter canal on the left bank to provide irrigation water to 2,021 hectares and a 29,600 meter canal on the right bank to beed 4,693 hectares of lands.

3. A drainage canal system which is to discharge the return flow from the irrigation system. The system will also serve drain the intermittent creaks and the swamp areas which cover about 570 hectare on the left bank.

4. Construction of dikes for the intermittent creaks to protect the plain against flood.

The charcteristics

1. Agricultural

Total plain area	10,215 ha
Irrigable land	7,273 ha
Average elevation of Agricultural land	995 m
Growing season	March 15–Nov. 5 (236 days)
Population in the irrigation area (1955)	17,522
Estimated population (1969)	24,800
Annual increase of population	2.5%

2. Irrigation

Land classification		а с Х		
Irrigation area				
Land class	Right bank	Left bank	Total	- '
I	655	264	919	
II	484	1,162	1,646	
III	882	3,267	4,149	
Total	2,021	4,693	6,714	

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Net irrigated area at the end of the development

Right bank	Left bank	Total
1,710	3,970	5,680

Note: As a result of the DSI investigation, total irrigated area at the end of the development has been changed to 6,871 ha.

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- * Irrigation water requirement (including losses) per hectare 8,730 m³/year Total (for 5,680 ha) 49.59 x 10⁶ m³/year Max. irrigation water requirement 0.796 *l*/sec/ha ,
- 3. Drain system

Deep drain area

570 ha.

4. Improvement of the river

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	Right bank	Left bank	Total
Protected irrigable land	415 ha	3,525 ha	• 3,940 ha
Length of the dike	10,500 m	23,150 m	33,650 m

ECONOMY

1.	Costs:	
	Multi-purposes-structures	49,400,165 T.L.
	(For power and irrigation)	- ,
	Irrigation system and improvements	33,339,252 T.L.
	Power plant	36,340,000 T.L.
	Land acquisition	3,774,000 T.L.
	Total	122,853,417 T.L.
2.	Annual costs (Allocated)	
<i>.</i>	For irrigation and reclamation	3,132,342 T.L.
	For power	5,882,488 T.L.
	Total	9,014,830 T.L.
3.	Annual benefits	
	a. Irrigation and reclamation	
	Annual increase of income (per hectare) 1)	1,285.90 T.L.
	Annual increase of income (per hectare) 2)	2,403.50 T.L.
	Total annual increase of income (for 4,510.2 net ha) (1)	5,799,666 T.L.
	Total annual increase of income (for 1,170.0 net ha) (2)	2,812,095 T.L.
	Total	8,611,761 T.L.
4.	Benefit-cost ratio	
	For irrigation and reclamation	R = 2.75
	For power-plant	R = 3.37
	For the whole project	R = 3.16
5.	Operation, maintenance and replacement cost	s
	Per hectare	74 T.L.
	For the whole project (6,714 gross ha)	497,642 T.L.
6.	Cost characteristics	
	Irrigation and reclamation cost per hectare:	
	Costs for irrigation and reclamation Gross irrigation area = 6,41	7 T.L.
	Annual irrigation and reclamation costs per he	ctare:
	Total annual costs of irrigation and reclamatio	'n
	Net irrigated area	= 552 T.L.

'II 6-2 Summary of Erbaa Report

Project Site

The irrigation area of Erbaa plain lies in the North of Tokat in the junction of Kelkit-Yesilirmak, on the left side of Kelkit on the right side of Yesilirmak.

Introduction of the Project

This project supply water for an area of 4,760 ha in Erbaa plain receiving water from the Kelkit by pump. The project includes the rehabilitation of old network and development of irrigation area.

1. Rehabilitation of Old Network

a.	Agricultural area	
	The area to be irrigated with project	3,970 ha
	Growing season	April 1 – November 30
	Irrigation water demand	15,643 m ³ /ha/year
b.	Structure	
	Length of main canal	23,800 m
	Max. capacity of main canal	3,375 m ³ /s.

2. Network in New Pump Area

Max. capacity of main canal

а.	Agricultural area	
	Irrigation area .	790 ha
	Growing season	April – November 30
	Irrigation water demand	22,084 m ³ /ha/year
b.	Structures	
	Length of main canal	10,927 m

1,138 m³/s.

General Knowledge about Erbaa Project

Agr	icultural Area	
The	area which will be irrigated according to the project	4,760 ha
Anr	ual irrigation water demand	80 x 10 ⁶ m ³ /year
Anr	ual Expenses	
	•	1,636,000 T.L.
b.	Initial expenditures which will be added by the improvement project	1,314,321.28 T.L.
c.	Total annual expenses	2,951,133.28 T.L.
Anr	uual Incomes	
a.	Gross National Agricultural Income from an area of 987.06 ha in the year 1965	2,737,822.36 T.L.
Ъ.	Gross National Agricultural Income per ha existing area in 1965	2,793.50 T.L.
c.	Gross National Agricultural Income from an area of 4,760 ha in 1965	13,297,060.00 T.L.
d.	Gross National Income per ha after the improvement project	4,288.50 T.L.
e.	Annual Gross National Income from an area of 4,760 ha after the improvement project	20,413,260.00 T.L.
f.	Increment of Annual Gross National Agricultural Income by the aid of improvement project	7,116,200.00 T.L.
Ben	efit Cost Ratio	
a.	At present (3a/2a)	1.67
b.	After the project (3f/2c)	2.41
Cha	racteristics of Cost	
a.	Cost of irrigation facilities per ha	619.99 T.L.
b.	Cost of 1 m^3 water at the irrigation area	4 kurus
	The Anr Anr a. b. c. Anr a. b. c. d. c. d. e. f. f. Ben a. b. Cha a.	 b. Initial expenditures which will be added by the improvement project c. Total annual expenses Annual Incomes a. Gross National Agricultural Income from an area of 987.06 ha in the year 1965 b. Gross National Agricultural Income per ha existing area in 1965 c. Gross National Agricultural Income from an area of 4,760 ha in 1965 d. Gross National Income per ha after the improvement project e. Annual Gross National Income from an area of 4,760 ha after the improvement project f. Increment of Annual Gross National Agricultural Income by the aid of improvement project Benefit Cost Ratio a. At present (3a/2a) b. After the project (3f/2c) Characteristics of Cost a. Cost of irrigation facilities per ha

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However, the land classification at the Erbaa plain revealed the following facts:

Irrigation Area		
Classification	Area, ha	Ratio, %
1st Class	1,559	10.22
2nd Class	2,658	17.43
3rd Class	5,077	33.88
1 + 2 + 3	9,294	60.93
5th Class	1,257	8.25
6th Class	4,702	30.82
Total	15,253	100.00

As can be seen from the above table, there is an irrigable area of 9,294 ha in this district, but DSI is planning to develop 5,500 ha of land, or 3,000 ha by the end of 1969 in the first stage of the project, and 2,500 ha in the second stage.

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II 6-3 SUMMARY OF LEEDSHILL REPORT

The Carsamba plain development project constitutes part of the Lower Yesilirmak project which involves construction of dams at Ayvacik and Balahor and irrigation of arable land of 80,500 ha in the Carsamba plain.

		Land Class	sification		
	Rig	ht Bank	Lef	't Bank	Total
	above 2m	below 2m	above 2m	below 2m	
1st Class	11,510	270	3,690		15,470
2nd Class	16,760	1,110	11,390	440	29,700
3rd Class	14,120	8,400	11,000	1,840	35,360
Total	42,390	9,780	26,080	2,280	80 , 53 <u>(</u> 0

Carsamba Plain

Proposed project data

1.	Hydrology	
	Drainage area:	36,000 km ²
	Annual mean precipitation	530 mm
	Runoff at Kale:	
	Period of record	1939-1963
	Average annual	4,200 x 10 ⁶ m ³
	Maximum annual	6,832.6 x 10 ⁶ m ³
	Minimum annual	2,176.5 x 10 ⁶ m ³

	Streamflow at Kale:	
	Average	133.2 m ³ /s
	Maximum	1,706 m ³ /s
	Minimum	10.7 m ³ /s
	Estimated Flood Peak	5,000 m ³ /s
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2.	Irrigation Service Area	
	Location	Right bank Yesilirmak above 2m contour
	Area:	
	Gross	46,540 ha
	Gross irrigated	33,890 ha
3.	Irrigation and Drainage Facilities	
	Main irrigation canal:	
	Capacity at intake	$47.4 \text{ m}^3/\text{s}$
	Total length	47.2 km
	Section	Trapezoidal
	Secondary canals:	-
	Total length	289.8 km
	Tertiary flumes:	
	Area served	33,890 ha
	Main and lateral drain:	
	Total length	124.8 km
	Area requiring drainage:	
	Surface only	5,500 ha
	Surface and subsurface	29,150 ha
	Surface, subsurface and on farm	11,890 ha

Required Capital Investment for Proposed Project

	Local Currency Millions of T.L.	Foreign Exchange Millions of \$
Ayvacik Dam and Power Plant	287.9	34.2
Lower Balahor Dam and Power Plant	65.8	6.5
Transmission Facilities	80.7	7.3
Irrigation and Drainage Facilities	212.5	5.5
Total	646.9	53.5
Total in T.L.	1,128.4	

Costs of Proposed Project

	the second second
Project Capital Costs:	5% Interest Rate
Dams, power plants, transmission facilities	43.1
Irrigation and drainage facilities	. 13.1
Subtotal	56.2 ·
Operation and Maintenance Costs:	•
Dams, power plants and transmission facilities	7.5
Irrigation and drainage facilities	2.4
Subtotal	9.9
Total Reimbursable Costs	66.1
Non-project Capital Costs	5.8
Total Costs	` 71.9

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(Equivalent Annual Values in Millions of T.L.)

All costs discounted at 5% interest

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Table II 6-1 Economic Justification of Proposed Project (Equivalent Annual Values in Millions of T.L.)

	5% Interest Rate		
	Power	Agri.	Total
Primary Benefits	69.0	40.3	109.3
Allocated Costs	38.9	27.2	66.1
Net Benefits	30.1	13.1	43.2
Benefit Cost Ratio	1.77	1.48	1.69

All costs and benefits discounted at 5% interest

Table II 6-2

Economic Analysis of Carsamba Plain Irrigation for Various Areas

	Project direct profits	Irrigation network cost	Profit cash	Balance % of total	Allocated from Dam	Total irriga- tion costs	Ratio direct profit to cost	Indirect profit	Total profit	Total ratio profit to cost
Yesilirmak Right Ban	k									
-Above 2 m. el.	40.30	15.49	24.81	73.70	13.87	29.36	1.37			
-Below 2 m. el.	2.88	1.51	1.37	4.07	0.77	2.28	1.26			
Yesilirmak Left Bank										
-Above 2 m. el.	15.45	8.17	7.28	21.67	4.08	12.25	1.26			
-Below 2 m. el.	0.65	0.46	0.19	0.56	0.10	0,56	1.16			
Total	59.28	25.63	33.65	100.00	18.82	44.45	1.33	8.92	68.20	1.53
If only Yesilirmak R.H. bank irrigated above 2 m. elevation	40,30	15.59			18.82	34.31	1.17	6.48	46.78	1.36

Interest = 5%, Annual equivalent cost = 10^6 TL.

Source : Lower Yesilirmak project planning report revision summary

