Mr. Tammachart Sirivadhanakul, Director of Regulatory Division, National Energy Administration.

near Mr. Tammachart,

Re: LPG PRODUCTION FROM NATURAL GAS

I study LPG production from 100% of natural gas (from well head), and whether Thailand can export LPG to Japan or not.

I do not use computor, but the calculation is based on Fluor's report and Chiyoda's estimation, so the result is not so much different.

Then LPG is manufactured from 100% of natural gas (from well head), the dew point control unit is unnecessary. Therefore, the cost of dew point control operation must be minused from the cost of LPG unit. I suppose that the cost of dew point control unit is 15-30% on the cost of LPG unit. In my report, I apply for 15% of that.

#### LPG PRODUCTION QUANTITY IN THAILAND

| Natural Gas               | LPG Production |                    |                    |       |  |  |
|---------------------------|----------------|--------------------|--------------------|-------|--|--|
| Production                | T/Y            |                    |                    |       |  |  |
|                           | -              | C <sub>3</sub> LPG | C <sub>4</sub> LPG | Total |  |  |
| 350 MMscf/D (in 1983)     | -              | 196.2              | 107.8              | 304.0 |  |  |
| 500 MMscf/D (after 1984)  | In 1984        | 272.5              | 150.0              | 422.5 |  |  |
| 700 Midscf/D (after 1988) | In 1988        | 360.0              | 199•1              | 559.1 |  |  |
| LPG From Refinery         | In 1979        |                    |                    | 181.0 |  |  |

I suppose that LPG production from the refinery after the expansion and new refinery completion, LPG from these refineries is excess for domestic requirement, because these refineries will

 $_{
m have}$  2 lot of cracking units. Thai LPG demand in 1982 will be  $_{
m 244~HT}$ , so Thailand could not export before the completion of the  $_{
m expans}$ ion and new refinery.

Accordingly, the most of LPG from natural gas should be exported to Japan (Japan is the best LPG market for Thailand), to obtain foreign currency, but after the completion of the expansion and new refinery.

After 1983, Thailand will be available to export for 300 x  $10^3$ T/Y and after 1988 for 560 x  $10^3$ T/Y.

#### II LPG USAGE

Every countries are saving crude oil, therefore, they are going to substitute petroleum products (from crude oil) to natural gas and LPG.

New usage of LPG for Thailand

- 1. Motor car
- 2. Gas turbine fuel for electric generators of EGAT in province.
- Others (such as refrigerator)

#### III MARKETING RESEARCH IN JAPAN

Thai LPG Production from Natural Gas

in 1983 
$$304 \times 10^3 \text{ T}$$
  
after 1988  $559 \times 10^3 \text{ T}$ 

Japanese LPG Domestic Production and Import

|   | Domestic | in          | 1983 |       | 5,917 x  | 10 <sup>3</sup> T | 33.8  | %  |
|---|----------|-------------|------|-------|----------|-------------------|-------|----|
|   | Import   | in          | 1983 |       | 11,589 x | 10 <sup>3</sup> T | 66.2  | %  |
| , | •        | <del></del> | 1    | Total | 17,506 × | 10 <sup>3</sup> T | 100.0 | 95 |

Japan is very good LPG market for Thailand.

#### TV FEASIBILITY STUDY

FOB Price of  $C_{\overline{\mathbf{3}}}$  LPG and  $C_{\mathbf{4}}$  LPG

|          | , **  | C <sub>3</sub> LPG<br>\$/T | C <sub>4</sub> LPG |
|----------|-------|----------------------------|--------------------|
| 1979,    | Jan.  | 133                        | 111                |
| 1989     | Jan.  | 125.5                      | 115.50             |
| 1989     | April | 126.50                     | 127.50             |
| 1989     | July  | 160.00                     | 180.00             |
| Price on | Spot  | _                          |                    |
| 1989     | July  | 200.00                     | 300.00             |

Latest FOB price of  $C_3$  LPG is 160 L/T and  $C_4$  LPG is 180 L/T (before the 2nd cil crisis), the price up is according to tight of all over the world LPG market.

The FOB price of them will be going up very rapidly.

THAI LPG COST VS LPG FOR PRICE

| THAT BIG COST VO DIG TOS PRICE                   |   |        |        |        | : 用 - / |
|--|---|--------|--------|--------|---------|
| Natural Gas Price<br>(from pipeline)<br>\$/MMBTU | C <sub>3</sub> LPG \$/T<br>160<br>C <sub>3</sub> LPG \$/T | 168    | 177    | 187    | 192     |
| ,  | 180   | 189    | 199    | 210    | 216     |
| 1.50   | +12.26  | +20.16 | +30.16 | +40.16 | +45.16  |
| 1.70*1   | + 1.96  | + 9.86 | +19.86 | +29.86 | +84.86  |
| 1.78   | - 9.11  | - 1.21 | + 8.79 | +18.79 | +23.79  |
| 2.06*2   | -30.70  | -22.80 | -10.80 | - 0.8  | + 4.2   |

Note: \*1 1.70 \$/MMBTU may be current natural gas price including transportation fee.

Natural gas production is 500 MMscf/D.

<sup>\*2</sup> Fuel oil 1,200" equivalent price on calorific value.

x → \_ \_ ′ 

From the above mentioned table, at present status, if  $c_3$  LPG FOB price is 192  $^{\circ}$ /T and  $c_4$  LPG FOB price is 216  $^{\circ}$ /T, the profit is nearly zero. In other word, FOB LPG price should be higher than equivalent price of fuel oil 1,200". Anyhow,  $c_3$  and  $c_4$  FOB price will be immediately going up.

So, NGOT should watch a movement of LPG FOB price.

#### SALES NATURAL GAS IS DECREASED ACCORDING TO LPG PRODUCTION INCREASE

When LPG production is 100% from natural gas (from well head), the sales natural gas is decreased. Fluor LPG production is not from 100% of natural gas (from well head).

Unit: MMSCf/D 1981 1982 1983 1984 1985 Decreased Sales Natural 18.20 36.00 31.91 52.02 46.42 Gas Sales Natural Gas For 42.66 Existing Industry 8.77 18.55 30.57 55.23 (50%) 1989 1986 1987 1988 1990 Decreased Sales 44.45 46.16 51.61 36.97 Natural Gas 52.64 Sales Natural Gas For 64.47 66.80 62.13 Existing Industry 58.17 59.17 (50%)

#### VI LOCATION OF NATURAL GAS PROCESSING UNIT

Thailand has many water ways. LPG transportation cost by water is very cheap. And Thailand has possibility to export LPG to Japan. Therefore, the location of natural gas processing unit should not be far from sea-shore.

If LPG is increased production, NGOT can not supply sales natural gas to the existing industry even if 50% on total consumption,

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because sales natural gas is decreased according to LPG production increase.

I appreaciate if my report is useful for you.

Sincerely yours,

Y. Kawase

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## LPG PRODUCTION FROM NATURAL GAS

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#### LPG PRODUCTION FIOM NATURAL GAS

FOREWORD

I study LPG production from natural gas. Flour Ocean Services international Inc. reported LPG production from natural gas but not 100% of the gas from pipeline, cally 61% in 1990. LPG production from refineries which will be included LPG from the expansion and new refinery is guessed larger than domestic requirement, but nobody an estimate because plants of the expansion and new refinery are tot decided. It is evident that the expansion and new refinery should have much cracking units, so LPG production should be large.

Accordingly, whole or mostly of LPG which will be produced rom natural gas should be exported, to get foreign currency, but B production should make much profit.

Another way to utilize LPG must be developed to increase consumption, such as (1) motor car fuel (2) industrial (5) small gas turbine of EGAT in province.

#### II DEFINITION OF LPG

C<sub>3</sub> LPG is liquefied propane and propene, dnd C<sub>4</sub>

RG is liquefied butanes and butenes, and ordinary LPG is mixutee of

RG is liquefied butanes and butenes, and ordinary LPG is mixutee of

RG is liquefied butanes and butenes. Actually,,

RG and C<sub>4s</sub> which is propene, propene, butanes and butenes. Actually,,

RG and C<sub>4s</sub> cuts can not be perfectly separated to pure C<sub>3s</sub> and C<sub>4s</sub>,

RIWays mixed a small quantity of before and after cuts. For instance,

RG LPG is mainly C<sub>3s</sub> and a small quantity of C<sub>2</sub> and C<sub>4</sub> cut are mixed.

#### III PHYSICAL PROPERTY OF LPG

Physical property of LPG must be very important, when physical property of LPG is changed. TABLE-1 (ATTACH.1) shown the physical property of LPG for recalculation.

Vapor pressure of LPG is very important, because pressure lest of LPG vessel is very important when components are changed. Vapor pressure of C2, C3, C4, C5 mixture is calculated by vapor-liquid

equivalent calculation. This calculation takes long time without computer, but from Fig.1 VAPOR PRESSURE OF PROPANE AND PROPYLENE (ATTACH.2) and Fig.2 VAPOR PRESSURE OF BUTANES AND BUTENES (ATTACH.3), se can know outline.

When highest temperature of Thailand is 44.5  $^{\circ}$ C at Uttradit province on April 27, 1960, C<sub>3s</sub> and C<sub>4s</sub> vapor pressure at 44.5  $^{\circ}$ C is as follows:

When  $C_3$  percentage of  $C_3$  and  $C_4$  mixed LPG is high, LPG vapor pressure is closed to 17.8 atm., and if  $C_4$  percentage of  $C_3$  and  $C_4$  mixed LPG is high, LPG vapor pressure is closed to 3.5 atm. Maximum vapor pressure difference which is according to composition of  $C_3$  and  $C_4$  is nearly 17.8 - 3.5 atm. And when  $C_4$  LPG is used, heating for vaporisation is needed, so vapor pressure of  $C_4$  vapor pressure is higher than ordinal temperature.

The LPG specification of Thailand is 30% propane and 70% butanes, but LPG composition from natural gas is about 35.5% butanes and about 64.5% propane, thus vapor pressure of natural gas LPG is very higher than it of refinery LPG, but difference of vapor pressure is less than 14.3 atm. the pressure test of LPG vessel must be checked.

#### IV LPG SPECIFICATION

That industrial specification of LPG is shown in TABLE-2 (ATTACH.4). And Japanese industrial specification is shown in FABLE-3 (ATTACH.5).

Difference of LPG ( $C_3$  and  $C_4$  mixed LPG for household) between flailand and Japan is big. Rate of  $C_3$  and  $C_4$  component in Thailand is 30: 70, in Japan 80: 20 in winter and 70: 30 in summer.

Standard specification of LPG imported in Japan is shown in TABLE-4 (ATTACH.6).

#### V LPG DEMAND FORECAST

LPG demand forecast in Thailand (NEA), JAPAN (MITI) are shown in TABLE-5 (ATTACH.7). And it of Mitsui's estimation is shown in TABLE-6 (ATTACH.8).

In Japanese statistics (TABLE-5 and 6. ATTACH.7 and 8), LPG demand forecast and each service as break-down are shown. As TABLE-5 (ATTACH.7) LPG demand in Thailand is very small compared with Japan. Moreover in Japan, town gas which is very similar to LPG consumption is very big, but Thailand has no town gas. So, Thailand must be developed the utilization of LPG for household, commerce and industry.

#### VI LPG USAGE

LPG usage in Japan is shown in Japanese specification of TABLE-3 (ATTACH.5) and LPG demand forecast of TABLE-5 and 6 (ATTACH.7 and8). I explain the use of LPG more detail as follows:

#### VI.1 Household and Commerce

LPG is used as room heating, cooking, hot water and refrigerator for household and commerce.

#### VI.2 Industry

Butane utilization for industry has been increased recently.

Fuel of coal, fuel oil (kerosene, gas oil, fuel oil) have been replaced by LPG because of an economical point, preventing air pollution (low sulfur content) and no ash and soot (products are not contaminated by ash and soot), moreover, heating value is high, temperature control and randling are very easy.

- Metal industry (melting decarbonizing, gas reforming, hardening, quenching, annealing, cutting and scarfing forging)

- \_ Ceramic industry (pottery, tile, whetstone, lime calcining,  $_{
  m glass}$  melting and molding work)
- Textile industry (gassed thread, plastic thread, plastic treating and dyeing)
  - Foodstuffs (cake, ham, bread)
  - Printing and Painting
- VI.3 Agriculture Industry (drying of tobacco leaf, grain, pasture, and ageing of fluts, and green house, and poultry farming and pig raising)

VI.4 Town Gas

 $\mathbf{C_{3}}$  and  $\mathbf{C_{4}}$  are mixed with coal gas to increase calorific value.

#### VI.5 Internal Combusion Engine

- Taxis in big city are using LPG, octane number of  ${\rm C_3}$  is 96, and it of  ${\rm C_h}$  is 90.
  - Tractor
  - Forklift

#### VI.6 Petrochemical

Raw material of ethylene, ammonia, hydrogen and synthetic gas.

polyethylene (resin)
stylene butadiene (rubber)
polystylene (resin)
Tetoron (polyester fiber)
polyester (resin)
surface active gent (detergent)
ethanol (solvent, raw material)
polyvinyl chloride (resin)
polyvinylidene resin & fiber

Ethand -----

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4-ethyl lead (additive) dioctyl phthalate (plasticizer) buthyl acetate (solvent) acetic acid (raw material) ethyl acetate (solvent, raw material) pentacrythritol (resin) higher alcolols (detergent, plasticizer)

iso propyl alcohol (solvent) aceton (solvent) methacrylic resin epoxy resin urethane foam acrylic fiber detergent ·butyl rubber polypropylene glutamic acid (ajinomoto)

methylethylketon (solvent) polyester resin polybutene (rubber) stylene butadiene rubber nitrile butadiene rubber polybutene 1 (rubber) polybutadiene (rubber) Nylon 66 (fiber) butyl gum polyisoprene rubber

#### VII MARKETING RESEARCH IN JAPAN

n-butene

butadiene

isobutene

Propylene

C, cuts

VII.1 Japanese LPG Import by Supply Sources

Japan imported LPG from Middle East (Saudi Arabia, Kuwait, Iran), Australia, Canada and Venezuela as TABLE-7 (ATTACH.9) and about a half of total import is from Saudi' Arabia which is shown in FIG.3 (ATTACH.10).

#### VII.2 LPG Import Quantity of Each Company in Japan

LPG import quantity of each company in Japan is shown in TABLE-8 (ATTACH.11), and share of LPG import in Japan is shown in FIG.4 (ATTACH.12).

#### VII.3 Import Terminal Capacity in Japan

LPG import terminal in Japan is spreaded in mainland and Kyushu Island which is shown in FIG.5 (ATTACH.13).

LPG import terminal capacity by area is shown in TABLE-9 (ATTACH.14) and by company in TABLE-10 (ATTACH.15).

#### VII.4 LPG Sales Quantity of Each Company in Japan

LPG sales quantity of each company in Japan is shown in TABLE-11 (ATTACH.16), and share of LPG sales in Japan is shown in FIG;6 (ATTACH.17).

#### VII.5 LPG Supply and Demand Forecast in Japan

LPG supply and demand forecast was shown in TABLE-6 (ATTACH.8). In Japan, LPG demand is very big but domestic production is small.

| Import<br>Tota | %<br> | 63.8<br>100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0        |
|----------------|-------|---------------|-------|-------|-------|-------|--------------|
| 7              | 0/    |               | (= 7  | 64.2  | 65.7  | 65.6  | 66.2         |
| Domestic       | %     | 36.2          | 34.7  | 35.8  | 34.3  | 34.4  | <b>3</b> 3.8 |
| Supply:        |       | ,,,,          | .,,,, | ·     | :     | :     |              |
|                |       | 1978          | 1979  | 1980  | 1981  | 1982  | 1983         |

Japan is big LPG importing country, and LPG domestic production is growing up corresponding to crude oil throughput but LPG demand is growing up year by year more than LPG domestic production. Thus, domestic production percentage was 36.2% on demand in 1978 and will be 33.8% in 1983.

VII.6 Japan Petroleum Development Corporation (JPDC)

Japanese Government has 100% share of JPDC, he assists a half of investment for exploratory drilling in country and foreign countires. And when crude oil and natural gas is discovered and commercial production is commenced, the fund is returned to JPDC, and if well is dry, the fund is not necessary returned to JPDC. But, the fund is tax from nation thus if Thailand excess product from natural gas and wants to export, Japanese Government expects that Thailand export them to Japan in proportion to share hold.

VIII MATERIAL BALANCE OF C3 AND C4 LPG (FROM NATURAL GAS)

 $C_3$  and  $C_4$  cuts in the gas from pipeline is shown in TABLE-12 (ATTACH.18). As was noted previously,  $C_3$  and  $C_4$  cuts separation (yield) must be estimated by computer, and 100% of them can not be recovered, so, I assume that  $C_3$  yield is 90% on total  $C_3$  in natural gas, and  $C_4$  yield is 98% on total  $C_4$  in natural gas (see TABLE-12, ATTACH.18). These yields are based on Chiyoda's information.

I calculate material balance and heat balance of C<sub>3</sub> and C<sub>4</sub> LPG which are met the standard of specification of LPG imported in Japan (see TABLE-4, ATTACH.6), are shown in TABLE-13-1 and-2, (ATTACH.19-1 and -2). (13)-(19) of TABLE-13-2 shows calculation of heating value of C<sub>3</sub> LPG and C<sub>4</sub> LPG. These physical data are applied from TABLE-14-1 and -2 (ATTACH.20-1 and -2). SOURCE: DATA BOOK ON HYDROCARBONS), afterward I will use data from same tables.

Then, I calculate production of  $C_3$  and  $C_4$ , LPG, and show in TABLE-15 (ATTACH.21) as Lb/H.

 $C_3$  and  $C_4$  LPG production is shown in TABLE-16 (ATTACH.22) as ton.

 $C_3$  and  $C_4$  LPG value and their average value are shown in TABLE-17 (ATTACH.25).

Note: Then I calculated heating value, it is gross heating value not net heating value, because natural gas price is based on gross heating value. And T means MT and \$ means US\$.

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## IX LPG FOB BANGKOK PRICE (EXPORT LPG)

LPG price in Thailand (domestic LPG price) is very high, so LPG from natural gas is to make much profit according to Mr. Shishido's report last year.

LPG (CIF) price which was imported to Japan about 2 months ago was \$143/T, if freight rate between Thailand and Japan is assumed as about \$15/T, FOB Thailand might be \$128/T.

FOB price of Kuwait D/D LPG is shown in FIG.7 (ATTACH.23)  $^{\rm C}_3$  price was higher than  $^{\rm C}_4$  price, but recently both prices have been closed, because  $^{\rm C}_4$  LPG demand has been grown up.

o The Nippon Economic Newspaper reported as following:

Dated on June 24, 1979

Kuwait FOB Price (price in April - June in 1979)

. C<sub>3</sub> LPG

126.5 \$/T

Note: See the above mentioned

C<sub>4</sub> LPG

127.5 \$/T

\$128/T.

Price on spot at Houston, USA

C<sub>z</sub> LPG

150 \$/T

 $C_L$  LPG

300 \$/T

o The same newspaper

Dated on July 5, 1979

Kuwait FOB Price (in July 1979)

C<sub>3</sub> LPG

160 \$/T

 $\mathbf{C}_{l_4}$  LPG

180 \$∕T

Price on spot

C<sub>3</sub> LPG

200 \$/T

C<sub>L</sub> LPG

300 \$/T

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o FOB Persian Gulf (Mitsui & Co.estimated)

Freight of Persian Gulf to Japan may be  $22 - 25 \ \text{\ensuremath{\$/T}}$ . Freight of Siam Gulf to Japan may be 15 \text{\ensuremath{/T}}.

All over the world, LPG is very tight, because  $C_4$  is mixed in gasoline and used as petrochemical raw material (substituted naphtha).

The LPG price is risen in July 1979, being caused by LPG shortage not by crude oil price up. Change of crude oil standard price is shown in FIG.8 (ATTACH.24).

I calculate average price of C<sub>3</sub> and C<sub>4</sub> LPG produced from Siam Gulf natural gas (the gas from pipeline), and show it in IABLE-17 (ATTACH.25).

Ratio of  $C_3$  LPG and  $C_4$  LPG of produced from the gas from pipeline is 64.5 : 35.5 (wt), and average price is 167.1 \$/T when  $C_3$  LPG price is 160 \$/T and  $C_4$  LPG price is 180 \$/T.

According to Mr. Shishido's report (in 1978), exrefinery price of LPG in Thailand is as follows: (For your reference)

Exrefinery Price 3.1397 B/Kg = 154.096 \$/T

Note: \* Exrefinery price of LPG was not changed before July 1979.

The price of LPG in Thailand (in June 1979) was higher than the LPG of FOB Kuwait price (april and June 1977).

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X CASE-1 EXPENDITURE AND REVENUE IN CASE OF NATURAL GAS PRICE 1.50%/MMBTU, C<sub>3</sub> LPG PRICE 160%/T AND C<sub>4</sub> LPG PRICE 180 %/T (500 MMscf/D)

#### X.1 Operation Cost

#### X.1.1 Production

In Mr. Shishido's report "THE PRELIMINARY ECONOMIC STUDY OF LPG RECOVERY FROM NATURAL GAS", LPG production was estimated as follows:

My calculation of LPG production (in case of 500 MMscf/D natural gas production schedule) is as follows: (in 1987)

#### X.1.2 Construction Cost of LPG Production

Construction cost was estimated by Chiyoda Chemical Engineering and Construction Company based on 380,000 T/Y LPG production.

Designed recovery ratio is as follows:

C<sub>3</sub> : more than 90% C<sub>h</sub> : more than 98%

CO<sub>2</sub> removal unit is necessary when natural gas charge to LPG plant, CO<sub>2</sub> content must be less than 1%, because turboexpand is applied:

:

|                  | Chiyoda<br>Estimate        | Correction of Production rate                            | Correction<br>1979 Plant<br>Cost |          |
|------------------|----------------------------|--|----------------------------------|----------|
|                  | MM \$                      | MM \$  | # MM                             | L/T      |
| LPG Unit         | 70                         |  |                                  |          |
| CO2 Removal Unit | 16                         |  |                                  | ٨        |
| Total            | 86                         | 92,610*1   | 981112                           | 232.27*3 |
| Note: *1 86.000  | MM\$ X ( $\frac{422}{380}$ | $\frac{2,400 \text{ T/Y}}{0,000 \text{ T/Y}}$ ) $^{0.7}$ | 92.610 MM\$                      | :        |
| *2 ,92.610       |                            |  | 98.112 MM\$                      |          |
| 7:               | % up/year of               | construction co  | st                               |          |
| *3 98.112 1      | MM& ÷ 422.40               | ) MT =   | 232.27 \$/T                      |          |
| Fluor's es       | ,<br>timation of           | gas plant (the e   | nd of 1979)                      |          |

200 MMscf/D 68,301 MM\$

500 MMscf/D 
$$\times$$
 $\times = 68,301 M\$ \times (\frac{500}{200})^{0.7} = 129,714$ 

129,714 M\$  $\times (1 + \frac{0.07}{2}) = 134,254$ 
 $\frac{134,254}{98,112} \frac{M\$}{M\$} = 1.37 (37\% \text{ higher than Japan})$ 

The difference could not be clarify, it might be caused by different process and price of machine and equipment. And it is contained the cost of the dew point control unit.

# X.1.3 Dew Point Control Unit

When LPG recovery is from 100% natural gas (the gas from pipeline), the dew point control unit is unnecessary. Thus, LPG recovery acts as dew point control duty, the duty is not for LPG production. Thus, the operation cost of dew point control must be eliminated from the cost of LPG production.

The cost of dew point control can not calculate at this stage. I assumed for 15% of total operation cost of LPG production.

# X.1.4 Operation Cost \$/T of LPG Production Expense

#### A. Natural gas price is 1.5 \$/MMMBTU

|     |                                | % on Construction<br>Cost | \$/T  |
|-----|--------------------------------|---------------------------|-------|
| (1) | Depreciation (20 years)        | 5                         | 11.61 |
| (2) | Interest for Construction Cost | 5                         | 11.61 |
| (3) | Tax and Insurance              | 2                         | 4.65  |
| (4) | Maintenance                    | · 3                       | 6.97  |
| (5) | Administration                 | 2                         | 4.65  |
| (6) | Overhead                       | 2                         | 4.65  |
|     | Total                          | 119                       | 44.14 |

Note: Construction cost is 232.27 \$/T

# B. Interest of working capital C<sub>3</sub> and C<sub>4</sub> LPG average price is 167.1 \$/T (from TABLE-17, ATTACH.25)

167.1 
$$2/T \times 422,400 \text{ T/Y} = 70.58 \text{ MM } \$/Y$$
70.58 MM  $\$/Y \times \frac{1.5 \text{ Mon.}}{12 \text{ Mon.}} = 8.82 \text{ MM } \$/Y$ 
8.82 MM  $\$/T \times 8\% = 0.71 \text{ MM } \$/Y$ 
8% is interest.
0.71 MM  $\$/Y \div 422,400 \text{ T/Y} = 1.68 \text{ $\$/T}$ 

# C. Utility

Natural gas consumption is :

| For | LPG  | plant | 9  | MMscf/D |
|-----|------|-------|----|---------|
| Cor | co2  | plant | 18 | MMscf/D |
|     | Tota | al    | 27 | MMscf/D |

(Reating value of the natural gas was assumed as 1,050 BTU/scf by Mr. Shishido).

# Natural Gas Price

Mr. Shishido's Estimation

1.555 \$/MMBTU (compressor station at off-shore)

1.544 t/MMBTU (compressor station at on-shore)

Fluor's Report

1.50 \$/MMBTU

In the report, 2 natural gas prices were applied

1.75 \$/MMBTU

My Calculation

1.50 \$/MMBTU

The price is not included the transportation charge from the natural gas processing unit to end user. So, I apply for 1.50 \$/MMETU of natural gas charge.

27 MMscf/D x 1,050 BTU/scf x 
$$\frac{1.50 \text{ $\frac{1}{4}$}}{1 \text{ MMBTU}}$$
 = 42.525 \$\frac{1}{2}\$ D = 15.52 NM\$\frac{1}{2}\$ Y = 42.525 \$\frac{1}{2}\$ TM\$\frac{1}{2}\$ Y = 40.84 \$\frac{1}{2}\$ TM\$

#### D. Labor cost

15 persons x 4 shifts = 60 persons

Salary and other expense is assumed as 200 \$/Mon. Month

200 \$/Mon month x 60 persons x 12 months = 0.144 MM\$/Y

0.144 MM\$/Y ÷ 422,400 T/Y = 0.34 \$/T

#### E. Operation cost

| 7   | , .                             | b/T    |
|-----|---------------------------------|--------|
| (1) | Expense                         | 44.141 |
| (2) | Interest for<br>Norking Capital | 1.68   |
| (3) | Utility                         | 40.84  |
| (4) | Labor Cost                      | 0.34   |
|     | Total                           | .87.00 |

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- F. Operation cost minus the cost of dew point control unit 87.00 / T x (100 15)% = 73.95 / T
- X.2 Cost of Natural Gas Charge

50.92 MMBTU/T\*x 
$$\frac{1.5 \text{ b}}{\text{MMBTU}}$$
 = 76.38 \$/T

Note: \* is come from TABLE-20 (ATTACH.28).

TABLE-20 (ATTACH.28) is calculated from TABLE-18 and -19

(ATTACH.26 and 27).

#### X.3 Expenditure

|                         | \$/T   |
|-------------------------|--------|
| Cost Natural Gas Charge | 76.38  |
| Operation Cost          | 73.95  |
| Total                   | 150.33 |

Selling charge (including shipping) is assumed as 3% on total expenditure.

Expenditure is as follows:-150.33\$/T x (1 + 0.03) = 154.84 \$/T

#### X.4 Revenue

 $C_3$  and  $C_4$  LPG average FOB Bangkok price is 167.1 \$/T which is from TABLE-17-7 (ATTACH.25).

# X.5 Profit or Loss

In this case, projit is 12.26 \$/T. (see TABLE-21, ATTACH.29)

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X' CASE-1' EXPENDITURE AND REVENUE IN CASE OF NATURAL GAS PRICE 1.70 \$/MMBTU, C<sub>3</sub> LPG PRICE 160 \$/T AND C<sub>4</sub> LPG PRICE 180 \$/T (500 MMSCF/D)

In X, I applied 1.50 \$/MMBTU of natural gas, but actual natural gas price in 1979 may be 1.70 \$/MMBTU, so I calculate in case of 1.70 \$/MMBTU as follows:

#### X':1 Utility

27 MMscf/H x 1,050 BTU/scf x  $\frac{1.70 \text{ $\$}}{1\text{MM}}$  = 48,195 \$\tilde{\text{D}}\$  $= 17.59 \text{ MM $\$/Y$} \times \frac{422,400 \text{ T/Y}}{380,000 \text{ T/Y}} \div 422,400 \text{ T/Y} = 46.29 $\text{$\$/T$}$ 

# X'.2 Operation Cost

|     |                      | $T \setminus \vec{x}$ |           |
|-----|----------------------|-----------------------|-----------|
| (1) | Expense              | 44.14                 | no change |
| (2) | Interest for Torking |                       |           |
|     | Capital              | 1.68                  | no change |
| (3) | Utility              | 46.29                 |           |
| (4) | Labor Cost           | 0.34                  | no change |
|     | Total                | 92.45                 |           |

 $92.45 \ \text{$/$T} \times (100 - 15)\% = 78.58 \ \text{$/$T}$ 

# X1.3 Cost of Natural Gas Charge

 $50.92 \text{ MMBTU/T } \times \frac{1.7 \text{ } \$}{\text{MMBTU}} = 86.56 \text{ } \$/\text{T}$ 

#### X 4 Expenditure

| •4 Expenditure             | \$ <b>/</b> T |
|----------------------------|---------------|
| Cost of natural gas charge | 86.56         |
| Operation cost             | 78.58         |
|                            |               |

X'.5 Profit and Loss

167.1 \$/T - 165.14 \$/T = + 1.96 \$/T 1.96 \$/T = 165.14 \$/T = + 1.2%

In this case, profit is 1.96 t/T.

EXPENDITURE AND REVENUE IN CASE OF NATURAL GAS PRICE CASE-2 EQUIVALENT TO FUEL OIL PRICE (2.063 \$/MMBTU) (500 MMSCF/D)

XI.1 Natural Gas Price Equivalent to Fuel Oil 1,200"

Fuel Oil 1,200" 1.6157 1/lit (May 1, 1978)

1.6157 8/lit = 0.0792 \$/lit

. 1\$

= 20.4 g

Heating value (Gross)

400"

9,371 Kcal/lit

1,500"

9,826 Kcal/lit

1,200" 9,675 Kcal/lit (assumed)

9,675 Kcal/lit = 38,392.86 BTU/lit

1 Kcal

= 3.96825 BTV

 $0.0792 \text{ } \text{/lit} - 38,392.86 \text{ } \text{BTU/lit} \times \text{MMBTU} = 2.063 \text{ } \text{/MMBTU}$ 

XI.2 Utility

27 MMscf/D x 1,050 BTU/scf x  $\frac{2.063 \text{ b}}{\text{MMBTU}}$  = 58,486 \$/D

= 21.35 MM\$/Y

21.35 MMS/Y  $\times \frac{422,400 \text{ T/Y}}{380,000} \div 422,400 \text{ T/Y} = 56.18 \text{ $\sqrt{T}$}$ 

XI.3 Operation Cost

\$/T

(1) Expense

44.14 no change

Interest for Forking Capital 1.68 (2) no change

(3) Utility

56.18

(4) Labor Cost

0.34 no change .

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Total operation cost minus the cost of dew point control init.

XI.4 Cost of Natural Gas Charge

$$50.92 \text{ MMBTU/T} \times \frac{2.063 \text{ }\$}{\text{MMBTU}} = 105.05 \text{ }\$/\text{T}$$

#### XI.5 Expenditure

|                         | \$/T   |
|-------------------------|--------|
| Cost Natural Gas Charge | 105.05 |
| Operation Cost          | 86.99  |
| Total                   | 192.04 |

Selling charge (including shipping) is assumed as 3% on total expenditure.

$$192.04 \text{ } \text{ } /\text{T} \text{ } \text{x} (1 + 0.03)\% = 197.80 \text{ } /\text{T}$$

#### XI.6 Revenue

 $C_3$  and  $C_4$  LPG average FOB Bangkok price is 167.1 \$/T which is come from TABLE-17 (7) (ATTACH.25).

#### XI.7 Profit and Loss

$$167.1 \text{ $/$T} - 197.80 \text{ $/$T} = -30.7 \text{ $/$T}$$
  
-30.7 \tag{T} \div 197.80 \tag{F} = -15.5%

In this case, loss is 30.7 \$/T.

XII CASE-3 EXPENDITURE AND REVENUE IN CASE OF NATURAL GAS PRICE IS MIDDLE OF CASE-1 AND CASE-2 (1.78 \$/MMBTU) (500 MMscf/D)

# XII.1 Natural gas price

| CASE-1 | 1.50  | ↓/MMBTU  |
|--------|-------|----------|
| CASE-2 | 2.063 | ↓/MMBTU  |
| CASE-3 | 1.78  | \$/MMBTU |

Average of CASE-1 and CASE-2 is 1.78 \$/MMBTU.

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# XII.2 Utility

27 MMscf/D x 1,050 BTU/scf x 
$$\frac{1.78 \text{ \$}}{\text{MMBTU}}$$
 = 50,463 \$/D = 18.42 MM \$/Y

$$18.42 \text{ MM} \text{ M/Y} \times \frac{422,400 \text{ T/Y}}{380,000 \text{ T/Y}} \div 422,400 \text{ T/Y} = 48.47$$

#### XII.3 Operation Cost

5/T (1) Expense 44.14 no change (2) Interest for Working 1.68 Capital no change (3) Utility 48.47 (4) Labor Cost 0.34 no change 94.63 Total

Total operation cost minus the cost of dew point control unit  $94.63 \text{ g/T} \times (100 - 15)\% \approx 80.44 \text{ g/T}$ 

$$50.92 \text{ MMBTU/T} \times \frac{1.78 \$}{\text{MMBTU}} = 90.64 \$/\text{T}$$

#### XII.5 Expenditure

Selling charge (including shipping) is assumed as 3% on total expenditure.

$$171.08 \times (1 + 0.03)\% = 176.21 \ \text{$\sqrt{T}$}$$

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#### XII.6 Revenue

 $c_3$  and  $c_4$  LPG average FOB Bangkok price is 167.1 %/T which is come from TABLE-17 (7) (ATTACH.25).

# XII.7 Profit and Loss

167.1 \$/T - 176.21 \$/T = -9.11 \$/T-9.11 \$/T : 176.21 \$/T = -5.2 %

In this case, loss is  $9.11 \text{ $\ell/T}$ .

XIII RESULT OF CASE-1, CASE-1', CASE-2 AND CASE-3 (500 MMS6F/D)

When  $C_3$  LPG price is 160 \$/T and  $C_4$  LPG price is 180 \$/T, average 167.1 \$/T, natural gas price must be 1.66 \$/T at profit zero point which is shown in FIG.9 (ATTACH.30). These calculations are based on 272.52 x 10<sup>3</sup> T/Y of  $C_3$  LPG production, and 149.88 x 10<sup>3</sup> T/Y of  $C_4$  LPG production in 1984 (see TABLE-16, ATTACH.22).

In FIG.9 (ATTACH-30) another 4 lines of 175 5/T, 185 %/T, 195 %/T, 200 %/T for C<sub>3</sub> and C<sub>4</sub> LPG average price are as following :

Natural gas price vs  $C_3$  and  $C_4$  LPG average price is as under :

Natural gas production 500 MMscf/D

| NATURAL GAS   C <sub>2</sub> and C <sub>3</sub> LPG AVERAGE PRICE (\$/T)* |        |        |             |         |        |
|---|--------|--------|-------------|---------|--------|
| NATURAL GAS<br>PRICE  | 167.1  | 175 -  | 185         | 195     | 200    |
| \$/MMBTU  |        | PROFIT | OR LOSS (\$ | /T)     | -      |
| .CASE-1 1,50  | +12.26 | +20.16 | +30.16      | +49.16  | +45.16 |
| CASE-1' 1.70  | + 1.96 | + 9.86 | +19.86      | +29.86  | +34.86 |
| CASE-2 2.063  | -30.7  | -22.80 | -10.80      | - 0.80  | + 4.2  |
| CASE-3 1.78   | - 9:11 | - 1.21 | + 8.79      | +18 •79 | +23•79 |

Note: \* FOB Bangkok price

Then C<sub>3</sub> and C<sub>4</sub> LPG price is 167.1 \$/T and natural ges price is 1.50 \$/MMBTU (CASE-1), profit is 12.26 \$/T, but when these are 1.78 \$/T (CASE-3) and 2.063 \$/MMBTU (CASE-2) of natural gas price, all are loss. Namely, even if fuel oil equivalent 2.063 \$/MMBTU and C<sub>2</sub>LPG 1.955/T, profit is still not so big (see FIG.9, ATTACH.30).

In the above table,  $C_{\perp}$  and  $C_{\downarrow}$  average price is indicated, their average prices are breakdown as follows but approximately.

|      |       |      | 03       | c <sub>4</sub> |
|------|-------|------|----------|----------------|
|      |       |      | LPG      | LPG            |
| Line | 165.9 | \$/T | 160 \$/T | 180 \$/T       |
| Line | 175   | t/T  | 168 \$/Т | 189 ұ/т        |
| Line | 185   | \$/T | 177 \$/Т | 199 \$/T       |
| Line | 195   | \$/T | 187 \$/T | 210 \$/T       |
| Line | 200   | T\a  | 192 🎲 Т  | 216 \$/T       |

Note: Data of calculated. above number are approximately.

Natural gas price is 2.063 \$/MMBTU which is equivalent to fuel oil 1,200", when  $C_3$  LPG and  $C_4$  LPG prices are going up to 192 \$/T and 216 \$/T individually (price is going up about 40 \$/T higher than the present price of  $C_3$  LPG and  $C_4$  LPG), but it is almost no profit and loss.

As a consequence, NGOT will not able to produce  $C_3$  and  $C_4$  LPG at present price, but  $C_3$  and  $C_4$  LPG price will be going up. Tapidly in near future according to  $C_3$  and  $C_4$  LPG market is becoming tight.

CASE-4 EXPENDITURE AND REVENUE IN CASE OF NATURAL GAS PRICE 1.50 \$/MMBTU. C<sub>3</sub> LPG PRICE 160 \$/T C<sub>4</sub> LPG PRICE 180 1/T (700 MMSCF/D)

LPG production which was noted above is from 500 MMscf/D, LPG production from bigger size is cheaper than from smaller size.

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#### XIV.1 Construction Cost

380,000 T/Y

86 MM%

86 MM  $_{\odot}$  x  $\left(\frac{559.15 \text{ T/Y}}{380,000 \text{ T/Y}}\right)^{0.7} = 112.70 \text{ MM}$ 

= 120.59 MM 7% up

120.59 ММ% - 559.15 Т

= 215.67 %T

Note: \* come from TABLE-15 (ATTACH.21)

 $63.83 \text{ Kg/H} \times 24 \text{ h} \times 365 \text{ days} = 559.15 \text{ T/Y}$ 

#### XIV.2 Operation Cost

# XIV.2.1 Natural gas price 1.5 \$/MMBTU

|     | 9                         | on Construction<br>Cost | °\$/T  |
|-----|---------------------------|-------------------------|--------|
| 1)  | Depreciation (20 years)   | 5                       | 10.78  |
| 2)′ | Interest for Construction | on 5                    | 10.78  |
| 3)  | Tax and Insurance         | 2                       | . 4.31 |
| 4)  | Maintenance               | 3                       | 6,47   |
| 5)  | Administration            | 2                       | 4.31   |
| 6)  | Overhead                  | S                       | 4.31   |
| ٠   | Total                     | 19                      | 40.96  |

Note: Construction cost is 215.67 L/T

#### XIV.2.2 Interest of working capital

Same as X.1.4, B
Namely, it is 1.68 T/Y.

# XIV.2.3 Utility

Same as X.1.4, C

Namely, it is 40.84 %/T.

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#### XIV.2.4 Labor cost

16 persons x 4 shifts = 64 persons

Salary and other expense is assumed as 200 %/Man.Month.

200  $\phi$ /Man. Month x 64 persons x 12 months  $\div$  559.150 T/Y = 0.27  $\phi$ /T

# XIV.2.5 Operation cost

|     |                              | 5/T   |          |
|-----|------------------------------|-------|----------|
| (1) | Expense                      | 40.96 | (change) |
| (2) | Interest for Working Capital | 1.68  |          |
| (3) | Utility                      | 40.84 |          |
| (4) | Labor Cost                   | 0.27  | (change) |
|     | Total                        | 83.75 |          |

XIV.2.6 Total operation cost minus the cost of the dew point control unit

 $83.75 \ \$/T \ x (100 - 15)\% = 71.19 \ \$/T$ 

XIV.3 Cost of Natural Gas Charge

$$50.94^*$$
 MMBTU/T x  $\frac{1.5}{MMBTU}$  =  $76.41$ 

Note: \* come from TABLE-20 (ATTACH.28)

# XIV.3 Expenditure

Selling charge (including shipping) is assumed as 3% on total expenditure.

Expenditure is as follows:

$$147.6 \ \$/T \times (1 + 0.03)\% = 152.03 \ \$/T$$

# XIV.5 Revenue

Same as X.5

Namely, it is 167.1 \$/T

# XIV.6 Profit and Loss

167.1 
$$\$/T - 152.03 \ \$/T = 15.07 \ \$/T$$
  
15.07  $\$/T \div 152.03 \ \$/T = 9.0\%$   
In this case, profit is 15.07  $\$/T$ .

# XV COMPARISON OF LPG PRODUCTION FROM 500 MMSCF/D AND 700 MMSCF/D (NATURAL GAS PRICE 1.50 \$/MMBTU)

| •                         | Expenditure<br>\$/T | Revenue<br>\$/T | Profit<br>\$/T | Profit<br>% |
|---------------------------|---------------------|-----------------|----------------|-------------|
| From 500 MM/D Natural Gas | 155•59              | 167.1           | +10.31         | 6.6         |
| From 700 MM/D Natural Gas | 152,•20             | 167.1           | +15.07         | 9.9         |

LPG from 700 MMscf/D natural gas is 4.59 \$/T more profit, but LPG production unit can not be bigger than 700 MMscf/D unit.

#### XVI CONCLUSION

#### (1) Export LPG State

When LPG is exported, LPG must be separate  $C_3$  LPG and  $C_4$  LPG. And LPG state is not high pressure and atmospheric temperature must be low.

# (2) Expected LPG Production and LPG to Export to Japan

When Thailand intends to export the products and by products (energy) from Siam Gulf natural gas, Japan expects to import the products and by products on proportion to the share hold.

Thai natural gas production from 700 MMscf/D natural gas from pipeline and quantity of imported LPG in Japan are as follows :

Thai LPG Production from Matural Gas (from pipeline)

.in 1983

3.040x 10<sup>3</sup>T

(after 1988

5,590x 10<sup>3</sup>T)

Japanese LPG Bomestic Production and Import

Domestic in 1983

5,917 x 10<sup>3</sup>T

Import in 1983 (forecast)  $11,589 \times 10^{3}$ T/ , 66.2 %  $17,506 \times 10^{3}$ T 100.0 %

Total

Japanese import LPG will be grown up every year.

Japanese LPG market is good for Thailand.

#### (3) LPG price

I estimate the Thai LPG cost from natural gas as of 1979 before the 2nd oil crisis.

Calculation conditions of Thai LPG cost from natural gas CASE-2 are as follows :

Natural gas production

500 MMscf/D

Natural gas price'

2.063 \$/MMBTU

C3 LPG price

160 \$/T

C<sub>L</sub> LPG price

180 *↓/*T

C3 LPG : C4 LPG

64.5: 35.5

#### Regults are as follows:

C3 LPG and C4 LPG average FOB price

167.1 \$/T

Thai LPG selling price (cost) from natural gas

197.8 \$/T

Loss

30.7 \$/T

Note: come from XI.7

come from TABLE-17 (7) (ATTACH.25)

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According to the above table, the price of natural gas from pipeline is very high compared with other natural gas produced country, so Thai LPG cost from natural gas is very high.

In accordance with circumstances of Thai economics, the export LPG price must be higher than fuel oil price based on calorific power. If export LPG price is lower than fuel oil price, LPG can not export, because of big loss money.

As the above table, at present status, Thailand can not produce and export LPG from natural gas.

# (4) Possibility of LPG export

LPG FOB Kuwait price has been going up rapidly.

in 1979

| April              | - June     | July     | on Spot   |  |  |
|--------------------|------------|----------|-----------|--|--|
| C <sub>3</sub> LPG | 126.5 \$/T | 160 \$/т | 150 - 200 |  |  |
| C <sub>4</sub> LPG | 127.5 \$/T | 180 \$/Т | 300       |  |  |

The above mentioned price up is not according to crude oil price up, to tight of LPG market.

Therefore, it seems that LPG price will be going up more than 200  $\mbox{$b/T$}$  in very near future.

#### (5) Export port condition

In case of Japan, the port condition and vessel are as follows:

- Port condition
   75,000 M<sup>3</sup> cargo is acceptable.
- 2. Tanker size

50,000 בעים

LOA (length over all) 225 M

Draft 12 M

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3. Cargo lot: about 43,000 T

43,000 T of one LPG lot is following days production.

in 1982 -62 days

in 1984 37 days

in 1990 28 days

4. Fleight from Bangkok

Bangkok to Japan 15 \$/T

#### Comments

- (1) If NGOT exports LPG to Japan, he negotiates export port conditions with Japanese importer to fit production scale and port condition of Thailand.
- (2) According to NGOT plan, the gas processing unit is about 20 Km far from sea-shore. It is too far for low temperature and very low pressure LPG transportation by pipeline. It is better that the gas processing unit is very close to sea-shore.

Even if, LPG is not exported, LPG must be transported by tanker in inland, tanker transportation fee is cheaper than other way.

- (3)  $C_4$  LPG export price is higher than  $C_3$  LPG export price, so  $C_4$  LPG from the refineries is exported and  $C_3$  LPG from natural gas is back to the refineries on same heating value. Therefore, Thai LPG specification is needed to change when more  $C_4$  LPG is exported.
- (4) I assumed that the cost of dew point control is 15% on LPG production expense, it has big influence on LPG cost, so the cost of dew point control must be calculated exactly.

#### Summary

(1) Present LPG FOB price is not feasible for Thai LPG production from natural gas, but in near future LPG FOB price would be going

• -

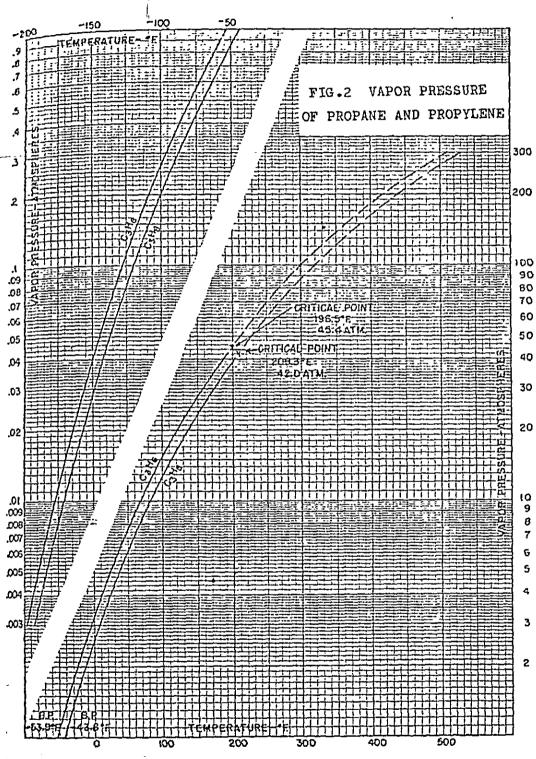
up and it will become feasible. NGOT should be watched a movement of LPG FOB price.

(2) Natural gas processing unit should be moved to sea-shore.

end.

|   | Propane                       | (Propylene)<br>Propene        | n-Butane                       | i-Butane                      | (i-Butylene)<br>i-But@ne      | 1-Butene                        | t-But@ne                      | c-Butene |
|---|-------------------------------|-------------------------------|--------------------------------|-------------------------------|-------------------------------|---------------------------------|-------------------------------|----------|
| Molecular Formular                              | с <sub>3</sub> н <sub>8</sub> | с <sub>3</sub> н <sub>6</sub> | с <sub>4</sub> н <sub>10</sub> | с <sub>4</sub> н <sub>8</sub> | с <sub>4</sub> н <sub>8</sub> | С <sub>4</sub> Н <sub>8</sub> . | C <sub>4</sub> H <sub>3</sub> | С4 Н8    |
| Molecular Weight                                | 44.1                          | 42.1                          | 58.1                           | 56.1                          | 56.1                          | 56.1                            | 56.1                          | 56.1     |
| Boiling Point (1 atm) (°C)                      | -42.1                         | -47.1                         | -0,5                           | -11.7                         | -6.3                          | -6.9                            | 0.9                           | 3.7      |
| Melting Point (1 atm) (°C)                      | -187.7                        | -185.3                        | -138.4                         | -159.6                        | -185.4                        | -140,4                          | -105.6                        | -138.9   |
| Specific Gravity Liquid (15 °C) (g/ml)          | 0.508                         | 0.523                         | 0.585                          | 0.563                         | 0,601                         | 0.601                           | 0.610                         | 0.627    |
| Gas (15 °C) (Kg/m <sup>3</sup> )                | 1,895                         | 1,805                         | 2.538                          | 2.529                         | 2.443                         | 2.442                           | -                             | 2.442    |
| Vapor Pressure (37.8 °C) (Kg/cm <sup>2</sup> A) | 13.4                          | 15.9                          | 3.6                            | 5.0                           | 4.4                           | 4.4                             | 3.5                           | 3.2      |
| Gross Heating Value (25 °C) (Kcal/Kg)           | 12.020                        | 11,690                        | 11,830                         | 11,800                        | 11,580                        | 11,510                          | 11,530                        | 11,550   |
| (15.6.°C) (Kcal/m <sup>3</sup> )                | 22,830                        | 21,120                        | 30,050                         | 29,850                        | 28,300                        | 28,110                          | 28,170                        | 28,210   |
| (60 °F) (BTU/lb)                                | 21,650                        | 21,040                        | 21,290                         | 21,240                        | 20,840                        | 20,720                          | 20,750                        | 20,780   |
| Net Heating Value (25 °C) (Kcal/Kg)             | 10,930                        | 10,940                        | 7 10,8 <del>9</del> 0          | 10,840                        | 10,830                        | 10,760                          | 10,780                        | 10,800   |
| (15.6 °C) (Kcal/m <sup>3</sup> )                | 21,000                        | 19,750                        | .27,730                        | 27,540                        | 26,450                        | 26,260                          | 26,330                        | 26,360   |
| (60 °F) (BTU/Kg)                                | 19,930                        | 19,690                        | 19,670                         | 19,610                        | 19,490                        | 19,370                          | 19,400                        | 19,430   |
| Latent Heat (3.P. 1 atm) (Kcal/Kg)              | 10,1.8                        | 104.6                         | 92.1                           | 87.6                          | 93.4                          | 94.2                            | 96.9                          | . 99.5   |
| Sensible Heat Gas) (25 °C) (Kcal/Kg °C)         | 0.399                         | 0.368                         | 0.401                          | 0.398                         | 0.365                         | 0.380                           | 0.374                         | 0.336    |
| Sensible Heat Liquid (25 °C) (Kcal/Kg °C)       | 0,602                         | 0.611                         | 0.575                          | 0.582                         | 0.549                         | 0,558                           | 0.544                         | 0.537    |
| Explosion Limit (in air) (vol %)                | 2.1 - 9.5                     | 2.0 - 10.0                    | 1.8 - 8.4                      | 1.8 - 8.4                     | 1,6 - 9,3                     | ·<br>•                          | -                             |          |
| Ignition Temperature (in air) (°C)              | 481                           | 548                           | 441                            | 544                           | 443                           | 443                             | ,                             |          |
| Gas Specific Gravity (15.6 C, 1 atm) (air = 1)  | 1.550                         | 1.477                         | 2.076                          | 2.068                         | 1.998                         | 1.997                           | -                             | 1.997    |

| ;                                      |                                       |  |
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| , * ;                                  |                                       | The state of the s |



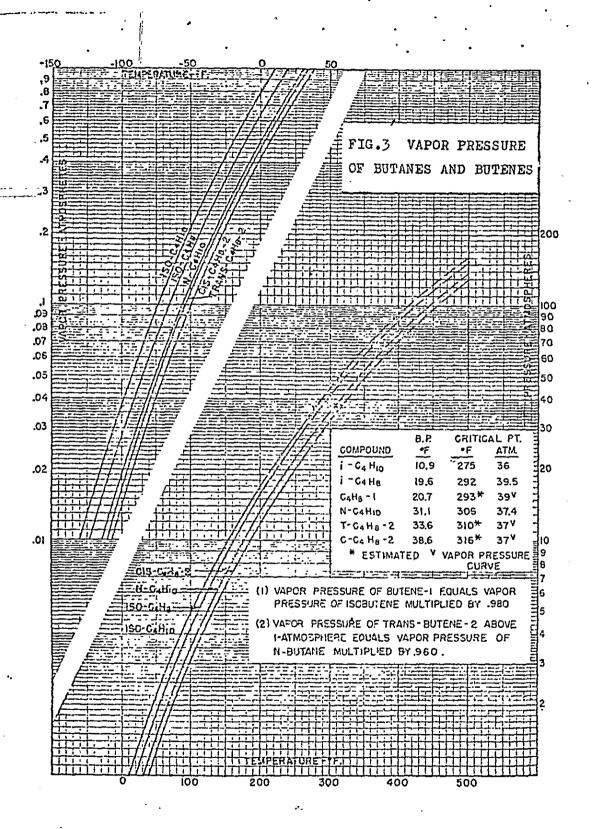


TABLE-2

THAI INDUSTRIAL SPECIFICATION OF LPG

|                                   |     | ,            |               |   |
|-----------------------------------|-----|--------------|---------------|---|
| · LIQUEFIED PETROLEUM GAS         |     | LIMITS       | TEST METHODS  | : |
| MMR PRESSURE @ 37.8°C             | MIN | 4.22         | ASTM-D-1267   |   |
| 75 BOILING POINT °C               | MAX | . 2.2        | ASTM-D-1837   |   |
| DEME AND HEAVIERS VOL % (VAPOR)   | MAX | 2            | ASTM-D-2163   |   |
| WIER STRIP CORROSION              | MAX | COPPER NO.1  | ASTM-D-1838   |   |
| MAL SULPHUR GRAINS/m <sup>3</sup> | MAX | 0.05         | ASTM-D-1266   | : |
| SIDUE AFTER EVAPORATION 100 ml    | NAX | 0.05         | . ASTM-D-2158 |   |
| O NATER                           |     |              |               | • |
| 30R                               |     | Marketable ` |               |   |
|                                   |     |              |               |   |

 $c_{36}: c_{46} = 3:7 \text{ (by volume)}$ 

|              | -                |            | JIS      | K2240 - 1972       |                                       |            |  |
|--------------|------------------|------------|----------|--------------------|---------------------------------------|------------|--|
| Item         |                  |            | -        | Component          | (% Low)                               | ,          |  |
| No.          | Vapor Pressure   | Sulfur     | Ethane + | Propane +          | Butanes +                             | Butadienes | Usage  |
| 1            | (40 °C) (Kg/cm²) | wt.8       | Ethylene | Propylene          | Butenes                               |            |  |
| ٠, ۴         | 15.8 Max.        | 0.02 Max.  |          | •uIM 06            | , , , , , , , , , , , , , , , , , , , | 1.         | Industry, Motor car, and Others.                 |
| <b>∩</b> 1   | 15.8 Max.        | 0.02 Max.  |          | 50 Min.<br>90 Max. | 1                                     |            |  |
| 2            | 12.7 Max.        | 0.02 Max.  |          | Í                  | 40 Min.<br>90 Max.                    | 1          | Industry, Motor car, and Others.                 |
| ተ            | 5.3 Max.         | 0.02 Max.  | 1        | 1                  | 90 Min.                               | 1          |  |
| ^ <b>c</b> # | 15.6 Max.        | 0.015 Max. | 8 Max.   | 60 Min.<br>80 Max. | 1                                     | 2 Max.     | Household (general use)                          |
| Ö            | 15.6 Max.        | 0.015 Max. | 8 Max.   | 80 Min.            | ī                                     | 2 Max.     | Household (for very cold weather area in winter) |
| -            |                  | ,          |          |                    | Ŷ                                     | ,          |  |
|              |                  |            |          |                    |                                       |            |  |

| •   |            |                                       |
|-----|------------|---------------------------------------|
|     | غیر<br>د م | <b>.</b>                              |
| · · |            | 1                                     |
|     |            |                                       |
| -   |            |                                       |
|     |            |                                       |
|     | · ·        | A A A A A A A A A A A A A A A A A A A |

TABLE-4 STANDARD OF SPECIFICATION OF LPG
IMPORTED TO JAPAN

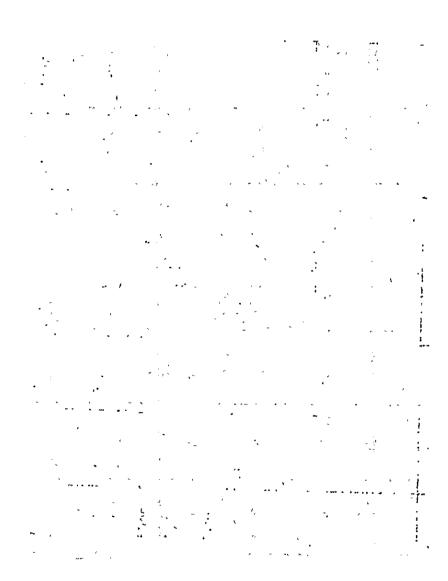
|                | C <sub>3</sub> LPG | C <sub>4</sub> LPG |
|----------------|--------------------|--------------------|
|                | Mol%               | Mol%               |
| c <sub>2</sub> | 2.0 Max.           | -                  |
| c <sub>3</sub> | 96.0 Min.          | <del>-</del>       |
| C <sub>I</sub> | 2.5 Max.           | 95.0 Min.          |
| C <sub>5</sub> |                    | 2.0 Max.           |

|      | · ^         | ر مارد<br>المراجعة المراجعة الم | ij.   |          | ,         |          |          |           |                               |              | -,     |  |
|------|-------------|---|-------|----------|-----------|----------|----------|-----------|-------------------------------|--------------|--------|--|
| 1985 |             | 444   | 254   |          | 6,461     | 4,853    | 1,345    | 1,786     | 1,041                         | ∞            | 15,494 |  |
| 1981 |             | 396   | 227   |          | 6,195     | 4,592    | 1,163    | 1,769     | 1,038                         | ∞.           | 14,765 |  |
| 1980 |             | 356   | 204   |          | 5,937     | 4,328    | 1,070    | 1,753     | 1,034                         | ∞            | 14,130 |  |
| 1979 |             | 317   | 182   |          | 5,690     | 4,093    | , 981    | 1,736     | 1,050,                        | 80           | 13,538 |  |
| 1978 |             | 292   | 167   |          | 5,453     | 3,627    | 222      | 1,707     | 226                           | <b>∞</b>     | 12,549 |  |
| 1977 |             | 540   | 138   | ,        | 5;275     | 3,067    | ħ29      | 1,677     | 932                           | -<br>-       | 11,626 |  |
| 1976 | 3           | . 223   | 128   | ,        | 5,265     | 2,750    | 269      | 1,655     | 806                           | 5.           | 11,173 |  |
| 1975 | -           | 197   | 123   |          | . 066. 4  | 2,438    | 563      | 1,558     | 998                           | <b>&amp;</b> | 10,423 |  |
| 1974 |             | 188   | 108   |          | 4,833     | 2,131    | €64      | 1,448     | 1,069                         | 10           | 9,990  |  |
| 1973 | ,           | 195   | 112   | 5°       | 4,616     | 2,009    | 401      | 1,495     | 1,194                         | 50           | 9,765  |  |
| 1972 |             | 147   | * 78- | à        | 4,208     | 1,586    | 407      | 1,506     | 1,087                         | 30           | 8,824  |  |
|      | IN THAILAND | 10 <sup>3</sup> K1  | 103፹  | IN JAPAN | Household | Industry | Town gas | Motor Car | Petrochemical Raw<br>Material | Export       | Total  |  |

\* Specific gravity  $G_{SS}$  0.5155 x 30% = 0.15465 0.04

Note:

147 x 0.573 = 84



| ,<br> | ;               | i      | -           | <u>`</u> | • •    | -      | ;           |                   |                 | ·        |                 |                     | • • •  | ,      |           |
|-------|-----------------|--------|-------------|----------|--------|--------|-------------|-------------------|-----------------|----------|-----------------|---------------------|--------|--------|-----------|
| 6001  | 5067            |        | - 5,917 -   | 11,589   | 17,506 |        | 6,288       | 4,439             | 1,485           | 1,523    | 1,814           | 1,576               | 0      | 17,265 | 1.,954    |
| 0001  | 2041            |        | 5,735       | 10,922   | 16,657 |        | 060'9       | 4,218             | . 1,243         | 1,597    | 1,795           | .1,553              | 40     | 16,537 | 2,713     |
|       | 1701            | -      | 5,483       | 10,456   | 15,969 |        | 5,898       | 4,010             | 996             | 1,436    | 1,776           | 1,522               | 9      | 15,650 | 1,593.    |
| 000   | 1900            |        | 5,244       | 9,413    | 14,657 |        | 5,712       | 3,798             | 509             | 1,344    | 1,748           | 1,471               | 40     | 14,621 | 1,274     |
|       | Total           |        | 4,930       | 9,259    | 14,189 |        | 5,532.      | 3,618             | 465             | 1,177    | 1,725           | 1,564               | 40     | 13,921 | 1,238     |
| 1979  | 2nd<br>hal t    |        | 2,610.      | 4,714    | 7,324  |        | 3,128       | 1,853             | 135             | 726      | 928             | 750                 | 20     | 7,489  | 1,238     |
|       | lst<br>holf     |        | 2,320       | 4,545    | 6,865  |        | 7,404       | 1,765             | 330             | 451      | 6¥8             | 614                 | . 50   | 6,433  | 1,402     |
| 1978  | )<br>           |        | 4,668       | 8,232    | 12,900 |        | 5,340       | 3,316             | 344             | 942      | 1,721           | 1,271               | £      | 12,975 | 02.6      |
| YEAR  | รบุคคุม หายเล่น | รมายกร | . DILSEWOG. | TROGNI   | TOIAL  | GN/KEG | nosmord use | "INDUSTRIAL FUEL" | HENDE DIVIDENT. | TOWN GAS | AUTOMOBILE FUEL | CHENTONT PEDDSTOCK. | TADETE | ror    | INVENTORY |

|              |                                       |        | <u> </u> |         | LINDS             | 1,000%/T |       | ,   |
|--------------|---------------------------------------|--------|----------|---------|-------------------|----------|-------|-----|
| YEAR         | . 1971 .                              | 1972   | 1973     | 761     | 1975              | 1976     | 1977  | *   |
| SAÜDI ARABIA | 1,003                                 | 1,101  | .1,750   | 2,654   | 2,799             | 3,464    | 3,911 | ; ' |
| AUSTRALIA    | 10<br>10                              | 152    | 1,029    | 1,008 . | 1,097             | 78011    | 1,255 |     |
| KUWAIT       | 1,158                                 | 1,1249 | 1,303    | 929     | . ; .<br>82<br>83 | 853      | 266   | •   |
| -            | 575                                   | 678    | 771      | 767     | 702               | 708      | 702   |     |
| CANADA       | 25.0                                  | 267    |          |         | <br>!?!           | 546      | . 241 |     |
| Venezusla    | 7                                     | . 259  | 103      | 27      |                   |          | . 26. |     |
| OTHERS       | · · · · · · · · · · · · · · · · · · · | . 130  | 75       |         | . 23.3            | . 27.    | 180   |     |
| TOTAL        | 5,621 .                               | 4,425  | 5,214.   | 5,678   | 5,9113            | 6,570    | 7,314 |     |
|              | _                                     | ,      |          |         | -                 |          | -     |     |

TABLE-7

JAPANESE LPG IMPORT BY SUPPLY SOUSCES

| •       | •               |                                     |                 | <b>:</b>               |                |                | . •            |         | •       |                | •      |        |
|---------|-----------------|-------------------------------------|-----------------|------------------------|----------------|----------------|----------------|---------|---------|----------------|--------|--------|
| . 2261  | 1,363           | 1,238                               | 919             | 859                    | 565            | 267.           | . 527          | . 397.  | 579     | 242            | 722    | 7,260  |
| 11974   | 1,385           | 1,297                               | 673             | 572                    | 530            | 501            | 414            | 354     | 507     | 250            | 398    | 5.5688 |
| 1975 .  | 1,332           | 1,146                               | . 638           | 432                    | . 248          | . 468          | . 727          | . 286   | . 222 . | . 252          | . 328  | 5,911  |
| : 4261  | 1/135           | 1,473                               | 652             | 767                    | 335            |                | 572            | 147.    | . 200   | . 235          | . 237  | 5,780  |
| 1973    | 777             | 19761                               | 372.            | 598                    | 227            | 181            | 616            | . 201   | 225     | <u> </u>       | 212    | 5,178  |
| 1973    | 681             | 1,326                               | 293             | 511                    | 191            | 217            | . 455          | . 150 · | 119     | 20<br>80<br>80 | . 195  | 125.45 |
| COMPANY | NIPPON PET, GAS | RITSUL & BRIDGESTONE LIG. GAS GROUP | IDEMITSU SEKIYU | MITSUBISHI<br>LIQ. GAS | GENERAL SEKIYU | MARUZEN SEKIYU | KYODO SEKIYU . | ESSO    | SHELL   | NIKKO LIQ. GAS | OTHERS | TOTAL  |

| CONSTRUCTION  SOCCO  SOCCO  SENDAL  NITSUBLEN  KASHIMA  K | CHIBA CHIBA  MITSUI  CHIBA CHIBA  MITSUI  TEPCO  112,CDD  3 74,0DD  3 74,0DD  3 74,0DD  3 74,0DD  22,CCD  TOWNG GAS   | KAWASAKI KAWASAKI<br>GENERAL MITSUI<br>35,000 56,000.<br>Efectric Power C             |
|--|--|---|
| BEING PLANNO BEING PLANNO NANNO NITSUI 60,000  | NITSUI ZAJODO ZAJODO SONKA WITSUI ZAJODO STEEL SODE STEEL SODE STEEL SODE STEEL SODE SOJODO S | CHITA HEKINAN KAMASAKI<br>IDEMITSU SHELL MIHON OIL<br>180,000 E 78,000 64,000         |
| SAKAI<br>SAKAI<br>NIEON OIL<br>152,000   | SAKAI<br>GENERAL<br>90,500<br>I 25,000<br>I 25,000<br>I 25,000<br>I 25,000   | UDESHT SUMETONS<br>WETAL<br>ASJCOO ASJCOO   |
| 2. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0.  |  | 32,000<br>32,000<br>1789<br>7000<br>7000<br>7000<br>7000<br>7000<br>7000<br>7000<br>7 |



| Tokyo Area (Kei-Yo Area)  |                              | Osaka Area (Ken-Hanshin Area) | Pea)   |
|---------------------------|------------------------------|-------------------------------|--|
| Chiba (Nitsui + Marubeni) | 80,000                       | Osake (Mitsui)                | 24,000   |
| Chiba (Idemitsu)          | 000'09                       | Kakegawa (Kobe Steel          | . ;  |
| Anegasoki (Tokyo Electric |                              | Sakai (Nitsui)                | 000.08   |
| Power Co.)                | .74,000 (under construction) | " (Nihon Oil)                 | 152,000  |
| Toyosu (Tokyo Electric    |                              | " (Maruzen)                   | 53,000   |
| Power Go.)                | 22,000                       | •                             | 50,000 (under construction)  |
| Ichihara (Mitsui/Mobil)   | 180,000 (under construction) | (General)                     | 000.06   |
| Sodegaura (ESSO)          | 131,000                      |                               | 25.000 (under construction)  |
| Negishi (Tokyo Gas)       | 30,000                       | " (Iwatani)                   | 80,000 (under construction)  |
| Kawasaki, (Mitsui)        | 36,000                       | Wakavama (Sumitono            | TOTAGE TARREST TOTAGE T |
| " (General)               | 36,000                       | - Metal)                      | 48,000   |
| " (Kyodo)                 | 40,000                       | Kobe (Nitsubishi)             | 000,009  |
| (Nihon Oil)               | 94,000                       |                               |  |
| Total                     | 753,000                      | Totel                         | 702,000  |
|                           |                              | Others                        | 716.000  |
| Nagoya Area (Chukyo Area) |                              |                               |  |
| Hekinan (Shell)           | 78,000 (under construction)  | Grand Total                   | 2,429,000  |
| Chita (Idemitsu)          | 180,000                      |                               | TTAC   |
| Total                     | 258,000                      |                               | H.14   |
|                           | _                            |                               |  |

## TABLE-10 LPG IMPORT TERMINAL CAPACITY BY COMPANY

|                | 5 4                                   | · . |          | . <b>T</b>     |          |            |       |
|----------------|---------------------------------------|-----|----------|----------------|----------|------------|-------|
| o Mitsui Group | · · · · · · · · · · · · · · · · · · · | -   |          | 388,000        |          |            | -     |
| : •            |                                       |     | ,        | 12,000         | (under   | construc   | tion) |
| Mitsui/Mobil   | ,                                     | :   | 1        | 180,000        | ( и      | 11         | )     |
| o Idemitsu     | •                                     |     | -        | 240,000        |          |            |       |
| *              |                                       | •   | •        | <u>8</u> 0,000 | (under   | construc   | tion) |
| Idemitsu etc.  | , ÷                                   |     | -        | 32,000         | ( "      | ır         | )     |
| Nohon Pet Gas  | J                                     |     | •        | 216,000        |          |            |       |
| Mitsubishi     |                                       |     | •        | 165,000        | ^        |            |       |
| Kyodo          |                                       | •   |          | 147,000        |          |            |       |
| ESSO .         | r 1                                   |     |          | 131,000        |          |            |       |
| General        | -                                     |     |          | 126,000        |          |            |       |
|                |                                       | . 1 | ,        | 25,000         | (under   | construct  | ion)  |
| Tokyo Electric | Power Co.                             | · · |          | 118,000        |          |            |       |
| • .            | 1                                     | ı   |          | 74,000         | (under   | construct  | ion)  |
| Nikko Liq. Gas | •                                     |     | •        | 94,000         |          | -          |       |
| Kobe Steel     | _                                     |     | -        | 60,000         |          |            |       |
| Maruzen        |                                       |     |          | 53,000         |          | ,          | -     |
|                | , ,                                   | :   |          | 30,000         | (under   | c^nstruct: | ion)  |
| Tokyo Gas      | , ,                                   |     | <b>b</b> | 52,000         |          |            |       |
| Sumitomo Metal | , -                                   | _   |          | 48,000         |          |            |       |
| Iwatani        | C <sub>1</sub> ×                      | -   |          | 80,000         | (under c | construct: | ion)  |
| Shell -        | J- / ),                               |     | -        | 78,000         | ( 11     | ţţ         | )     |
| -              | , ~.<br>, .                           |     |          | •<br>•         |          |            | •     |

2,429,000

| ,       |                | 1         | · · · · ·                   | •       |              | •       |                            | · .   |         | AT    | TACH.16  |          |
|---------|----------------|-----------|-----------------------------|---------|--------------|---------|----------------------------|-------|---------|-------|----------|----------|
| 2261    | 1,783.         | 1,521     | 1,1348                      | 1,273   | 1,042        | 986 .   | 764                        | 631   | 10.00   | 10.   | 1,829    | 12,665   |
| . 1976  | 1,790          | 17345     | 1,157                       | 1,317   | 912          | 975 .   | 7.7                        | 209   | 067     | 303   | in<br>co | 11,454   |
| . 1975  | .12612         | 1,214     | 10174                       | 1,092   | 83.22        | 921     | 783                        | 561   | 488     | 250   | 279.1    | 4,10,749 |
| 1974    | 1,7416         | 1,219     | 4,330                       | 1,092   | 793          | 788     | 512.                       | 463   | 422     | 200   | 1.978    | 10,511.  |
| 1973    | 1,178          | 1,209     | 1,437                       | 666     | 775          | 761     | to es                      | 725   | , 40ò   | 205   | 1,940    | 10,177   |
| 1972    | 1,031.         | 1,193     | 1,298                       | ю<br>10 | 767          | 740     | 7.01                       | 360   | 227     | 202   | 1.794    | 9,385    |
| COMPANY | Nippon Per GAS | Toel IIsu | MINSUI<br>BRIDGESTONE GROUP | 0000X   | NET SUBTRIET | MARUZEN | :<br>:<br>:<br>:<br>:<br>: | 71588 | GENERAL | SHOWA | 988      | TOTAL    |



| - ـ مّ ,       | <del>-</del> | in .                                 |                       |         |       |         |         |         |         | ·····.  |         |         | ····    |
|----------------|--------------|--------------------------------------|-----------------------|---------|-------|---------|---------|---------|---------|---------|---------|---------|---------|
|                | "(51)        | 24(14)                               | T/H                   | 6.2     | 10.5  | 12.5    | 12.9    | 12.9    | 20.3    | 20.3    | 23.2    | 23.2    | 23.2    |
| , ,            | (+1)         | (31)+379×58.12 <sup>2</sup> (41)+2.2 | 10 <sup>2</sup> 1b/H  | . 13.6  | 23.1  | 27.6    | 38.4    | 38.4    | 6.44    | 2.44    | 51.0    | 51.0    | 51.0    |
| ς <sub>h</sub> | (3:)         | (21)×98%                             | 10 <sup>3</sup> scf/H | 88.9    | 150.4 | 179.8   | 250.6   | 250.6   | 291.6   | 291.6   | 332.6   | 332.6   | 332.6   |
| ,              | (21)         | (11)×379÷10 <sup>3</sup>             | 10 <sup>3</sup> scf/H | 2.06    | 153.5 | . 183.5 | 255.7   | . 255.7 | 297.5   | 297.5   | 339.4   | 339.4   | 539.4   |
|                | (11)         | Gas From<br>Pipeline                 | Lb-Mol/H              | . 239.3 | 6.404 | 484.8   | 8.479   | 8.479   | 785.0   | 785.0   | 895.4   | 895.4   | 895.4   |
|                | (5)          | (4);2.2                              | T/H                   | 10.7    | 17.9  | 21.5    | 29.9    | 29.9    | 34.6    | 34.6    | 39.5    | 39.5    | 39.5    |
|                | (4)          | (3)÷379×44.09 <sup>42</sup>          | 10 <sup>3</sup> Lb/H  | 23.6    | 39.4  | 47.3    | 65.7.   | 65.7    | 76.2    | 76.2    | 86.8    | 86.8    | 86.8    |
| c <sub>3</sub> | (3)          | (2)×90%* <sup>3</sup> (3)            | 10 <sup>3</sup> scf/H | 203.2   | 358.9 | 4.904   | 564.8   | 564.8   | 655.1   | 655.1   | 745.7   | 745.7   | 7.547   |
|                | (2)          | (1)x379÷10 <sup>3</sup>              | 10 <sup>3</sup> scf/H | 225.8   | 376.5 | 451.6   | 627.5   | 627.5   | 6 222   | 6.727   | 828.6   | 828.6   | 823.6   |
| -              | (1)          | Gas From<br>Pipeline                 | Lb-Mol/H              | 595.7   | 4.566 | 1,191.6 | 1,655.7 | 1,655.7 | 1,920.6 | 1,920.6 | 2,186.2 | 2,186.2 | 2,186.2 |
|                | -            | -                                    | -                     | 1981    | 1982  | -1983   | 1984    | 1985    | 1986    | 1987    | 1988    | 1989    | 1990    |

Note: \*1 Fluor's report

\*2 Molecular Weight

 $\mathcal{S}$  Yield of  $\mathcal{C}_{\mathcal{S}}$  and  $\mathcal{C}_{\mathfrak{t}}$  recovery

| <br> | <u> </u>                      | · · · · ·          | <u> </u>    |                         |             |          |                          |              | · · · · · · |
|------|-------------------------------|--------------------|-------------|-------------------------|-------------|----------|--------------------------|--------------|-------------|
| (01) | 6) ÷ (6)                      | Bru/scf<br>(Gross) |             |                         |             | 2,522    |                          |              | 3,988       |
| (6)  | (8) × (4)                     | MM BTU             | 1.21        | 91.64                   | 2.72        | 95.57    | 121.12                   | 3.03         | 151.15      |
| (8)  | ٠                             | Bru/lb<br>(Gross)  | 22,300      | 21,650                  | 21,265*4    | -        | 21,265*4                 | 21,020,5     |             |
| (2)  | (6)x0.0267*3                  | NM <sup>2</sup>    | 18•2        | 971.4                   | 22.3        | 1,011.9  | 2.166                    | 20.2         | 1,011.9     |
| (9)  | (2) × 379 <sup>2</sup>        | scf                | 682.2       | 36;384.0                | 8.55.8      | 37,900.0 | 37,142.0                 | 758.0        | 37,900.0    |
| (2)  | (3) (4) × 0.4536 <sup>1</sup> | Kg                 | 24.55       | 1,920.10                | 58.00       | 2,002.65 | 2,583.60                 | 65.45        | 2,649,05    |
| (4)  | (2) × (3)                     | 1.0                | 54.12       | 4,233.02                | 127.86      | 4,415.00 | 5,695.76                 | 144.29       | 5,840.05    |
| (3)  | Molecular                     | Weight 1b          | 30.068      | 460*44                  | 58.120      |          | 58.120                   | 72.146       |             |
| (2)  | Adjusting Molecular           | Mol %              | 1.8         | 0*96                    | - cu<br>cu  | 10       | 98.0                     | 2.0          | 100•0       |
| (4)  | Specification                 | Mo1. %             | C, 2.0 Max. | c <sub>z</sub> 96.0 Min | C4 2.5 Max. | Total    | c <sub>4</sub> 95.0 Min. | C,5 2.0 Max. | Total       |
|      |                               |                    | C, LPG      | ···                     |             |          | Par to                   |              |             |

Note: data from TABLE-14-1 and-2 (ATTACH.20-1 and-2).

$$^{460}$$
 1 sef = 0.0283  $\times \frac{460}{460+(60-32)}$  = 0.0267

| いるというないから  | (19)<br>(17)x0.1746*9<br>(17)x0.1744 | (Net)     | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 3           | 6,363  |             | · •• •                  | •      | 5,545  | = 19,427 BTU/Lb   | A            | TTACH •19-22  |
|--|--------------------------------------|-----------|---------------------------------------|-------------|--------|-------------|-------------------------|--------|--------|---|--------------|---|
| A STATE OF THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUM | 6                                    | (Gross)   |                                       | *           | 6,113  |             | • •                     | -      | 7,309  | - ·i·   | .631         | 0.625<br>0.577<br>0.6177  |
|  | (15)x0.5556*8<br>Kcal/Kg             | (Net)     | ,                                     |             | 11,072 |             |                         |        | 10,909 | Pentanes (19,500 + 19,450 + 19,330)   | Pentanes     | = 1,481.695<br>= 40.428<br><u>0.574</u> 6                               |
| ,  | (14)x0.5556*8<br>Kcal/Kg             | (ego to)  | ·                                     |             | 12,027 |             |                         |        | 14,308 | <b>.</b>  |              | 0.563<br>0.5735<br>2,583.60 x 0.5735<br>65.45 x 0.6177<br>2,649.05 mean |
|  | (12)÷(4)<br>BTU/1b                   |           | ,                                     | -           | 19,928 |             | ,                       |        | 19,654 | 19,640 bru/ld   | ,<br>Butanes | ນ ກັນ<br>ເຂົ້າ  |
|  | (9)÷(4) BTU/1b (Gross)               |           | ,                                     |             | 21,647 | ,           |                         | רממ ער | 2004   | Kg.<br>≡  | •            | 9.182<br>975.441<br>33.263<br>5083                                      |
| (44)   | (12)<br>BE                           |           | -                                     | -           | 2.321  |             | -                       | 3.025  | 2012   | Butanes (19,670 + 19,610)<br>1 BTU/Lb = 0.5556 Kcal/Kg<br>Specific Gammital | 0.508        | 74- =   |
| (12)   | (4) x (11)<br>MMBTU                  | 1.11      | 94,36                                 | 2.51        | 87:98  | 111.86      | 2.80                    | 114.66 |        | *6 Butanes<br>*8 1 BTU/Lb<br>*9 Specific                                    |              |   |
| (11)   | BTU/1b<br>(Net)                      | 62 20,420 | C <sub>3</sub> 19,930                 | c4 19,640*6 | Total  | C4 19,640*6 | C <sub>5</sub> 19,429*7 | Total  |        | Notes   |              | . 5° 5° 5   |

| TABLE-14-1                                      | ·                                     | PHYS   | PHYSICAL          | CONSTANTS         |               | OF H            | DROC.        | HYDROCARBONS    | ,  |       |                               |  |
|---|---------------------------------------|--|-------------------|-------------------|---------------|-----------------|--------------|-----------------|--|-------|-------------------------------|--|
|   | Ponyora                               | MOLEC.   | BOILING           | MELTING           |               | DENSITY         | -            | CRITIC          | CRITICAL CONSTANTS   | NA TS | HEAT OF COMBUST<br>G 60°F-BTU | OXBUST<br>BTU/   |
| -   |                                       | WT.  | j.                | <b>,</b>          | "API          | Sp Gr<br>00,000 | Lb/gal       | <b>→</b> Å      | Αtm  | G/ml  | Gross                         | Z Z  |
| ORMAL PARAFFINS                                 | CH,                                   | 16.0   | -258.9            | -290.5            | 340           | 0.30            |              | 116 3           | 8 3 4  | 183   | 293                           |  |
| Ethane  | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 30.1   | -128.0<br>-1 43.8 | -207.8<br>-305.7  | 247           | .374            | E 4.         | + 90.1<br>206.3 | \$ C C C   | 223   | 22,300                        | 200<br>200<br>200<br>200<br>200<br>200<br>200<br>200<br>200<br>200 |
| Donten  |                                       | * 04   |                   |                   | ;;            | <b>t</b> 00.    |              | 90              | 4.75   | 222   | 21,290                        | 19,67  |
| Hexane  |                                       | 86.2   | 155.7             | - 139.5           | 81.0          | 23              | 5.25         | 386.5           | 32.6<br>29.6   | 232   | 21,070                        | 19.50  |
| Octane  |                                       | 114.2  | 209.2             | - 131.1<br>- 70.3 | 24.8<br>6.6.5 | 20.58           | 5.73<br>5.89 | 512.5           | 26.8<br>24.6   | 234   | 20,670                        | 19,167   |
| Nonane  | C,II,                                 | 128.2  | 303.4             | 9.43<br>1         | £.5           | 727             | 0.01         | 612¢            | 23   | 1     | 20,530                        | 19.050   |
| Undecane  | i ii                                  | 156.3  | 381.4             | 1 2 1 2 1 2 1     | 58.7          | 700             | 1.5          | 5 50            | in S   | 1     | 20,480                        | 19,020   |
| Dodecane  | Cullin                                | 170.3  | 421.3             | + 14.7            | 50.4          | 753             | 6.27         | 35.             | 18.  | 1     | 20,450                        | 18.98(   |
| SO-PARAFFINS<br>Isobutane                       | Cillie                                | 58.1   | 10.9              | -255.0            | 120           | .563            | 4.69         | 27.5            | 98   | 766   | 7076 16                       | 0,19   |
| 2-Methylbutane (Isopentane).                    | Cillin                                | 72.1   | 82.2              | -255.5            | 0.40          | .625            | 5.20         | 369.5           | 32.4   | 234   | 21,030                        | 19,450   |
| . pentane)                                      | Cilin                                 | 72.1   | 49.0              | +                 | 103           | .597            | 4.97         | 3294            | :. <u>.</u>  | ·<br> | 20.960                        | 19.330   |
| 2-Methylpentane (Isohevane).<br>3-Methylpentane | Calla                                 | 86.2<br>86.2   | 140.5             | -245<br>-180      | 83.5<br>80.0  | .659            | 5,48         | 437             | 30.  | .11   | 20,750                        | 19,210   |
| hexane)   | C,H,                                  | 56.2   | 121.5             | -147.6            | 84.9          | .654            | 5.44         | 415             | 31.  | i     | 20,700                        | 19,160   |
| isopropy I)                                     | Callia                                | 80.3   | 130.4             | -198.8            | 81.0          | .688            | 5.54         | 155             | 31   | .241  | 20,740                        | 19,200   |
| 2-Methylhexane (Isoheptane).                    | SE CO                                 | 100<br>100<br>100<br>100<br>100<br>100<br>100<br>100<br>100<br>100 | 194.1             | 180.8             | 75.7          | .683            | 5.68         | 490             | 28*  | ı     | 20,650                        | 19.140   |
| 3-Ethylpentane.                                 |                                       | 100.5  | 200.2             | 181.5             | 99.8          | 202             | 28.5         | 508             | 25 25 25 25 25 25 25 25 25 25 25 25 25 2                       | 11    | 20,660 .                      | 19,150   |
| 2.3-Dimethylpentane                             | Calla                                 | 100.2  |                   | 1                 | 2 02          | 200             | 5 8          | 3 00            | 2 6  | l     | 20,000                        | 19,090   |
| 2,4-Dimethylpentane                             | CHIL                                  | 100.1<br>100.2   | 176.9             | -183.1<br>-211.0  | 77.2          | 608             | 9.5.8        | 477             | 28.5   |       | 050,02<br>050,03<br>050,03    | 19,130   |
|   |                                       | _  |                   |                   |               |                 |              | : :             | ׅ֚֝֡֜֜֝֜֜֜֜֝֜֜֜֜֜֜֜֜֜֓֓֓֓֜֜֜֜֜֓֓֓֓֜֜֜֜֜֓֓֡֓֡֜֜֜֜֡֓֡֓֡֜֜֜֡֡֡֡֡֡ |       | 7                             | 11.6   |

,

| 2.2.3-Trimothylbutane (Trip-               |  | _          |             | L                            | -            | -         | -            |               |            |   |         |          |
|--|--|------------|-------------|------------------------------|--------------|-----------|--------------|---------------|------------|---|---------|----------|
| rano)                                      | CHIL                                   | 100.2      | 177.6       |                              | 73.1         |           |              |               |            |   |         |          |
| 2-Methylheptana (Isodelane)                |  | 114.9      | _           |                              |              | _         |              | <b>\$</b> 80. | 29 5       | 1   | 20,620  | 19,110   |
|  | Callar                                 | 114.2      | 245.4       | 3 J                          | 05.6         | 703       | 2. %<br>2. % | 549           | 26.        | 1   | 20,570  | 19,080   |
| Isobutyl)                                  | C. II.                                 | 114,2      | 1 228 4     | 130                          | -            |           | —.           |               | ç          | l<br>   | 20,570  | 19,080   |
| 4.2,4-1 rimothylpentane ("Iso-<br>Octane") |  |            |             |                              | <br>         | 869.      | 5.81         | 230           | 25         | 0.237   | 20,550  | 19,060   |
| OLEFINS                                    | <u> </u>                               | 114.2      | 210.0       | -161.2                       | . E          | .096      | 5.79         | 515           | 27•        | 1   | 20,540  | 10.050   |
| Ethylene,                                  | C311.                                  | 28.0       | -154.7      | -272.5                       | 27.1         |           |              |               |            |   |         |          |
| Propylona                                  | Cill                                   | 42.1       | د<br>د<br>ا |                              | _            | ?         |              | 3             | 5          | :23   | 21,549  | 20,290*  |
| Butene-1                                   | 511                                    |            | 3 6         | _                            | <u>-</u>     | _         | 4.35         | 196.5         | 45.4       | .233  | 21,040  | 19.690   |
| Cis-Butene-2.                              | J.                                     | 56.1       | 38.6        |                              | <u> </u>     | 9.69      | 2.00         | 293           | 30.        |   | 20.8404 | 19 4004  |
| Isobutene                                  | :::::::::::::::::::::::::::::::::::::: | 50.1       | 33.6        | 157.7                        |              |           | 0.22         | 200           | <u>ا</u> د | 1   | 20,780  | 19,430   |
|  | 113                                    | 60.1       | 19.6        |                              |              | -8        | 4.93         | 202 5         | 37.        | 1 8   | 20,750  | 19,400   |
| Cis. Pantage 9                             | ilio<br>C                              | 70.1       | 86.2        |                              | _            | :         |              |               | 3.3        | 1,7   | 20,720  | 19,370   |
| Trans-Ponteng-2.                           |  | 70.1       | 98.0        | -290.2                       | 82.0         | 3.8       | 5.38         | 382           | 36.        | I   | 20,710  | 19,360   |
| 2-Mathelbude .                             |  | 7.0        | 8.03        | _                            |              | .654<br>1 | 3.41         | 396           | 3 .        | 1   | 20,660  | 19,310   |
| 3-Methylbutene-1                           | CHI!                                   | 70.1       | 88 0        | i                            | 8.1.5        | 55        | 14           |               | 3 2        | 1   | 01-9'0: | 19,290*  |
|  | 7.11                                   | . 02       |             |                              |              |           | 2            | 20            | 36         | J   | 20,610  | 19,260   |
| 2-Methylbutene-2.                          | CHI                                    | 70.1       | 101.2       | -292.0<br>-207.0             | 92.0<br>80.0 | .633      | 5.27         | 363           | 37.        | 1   | 20,660  | 19.310   |
| Hexene-1                                   | Cellin                                 | 84.2       | 146.4       | -218 0                       | 44           |           | 3            | -<br>-<br>-   | ,          | 1   | 20,570  | 19,220   |
| Trans-Hexene-2                             |  | <u>2</u>   | 155.4       | -231.0                       | 73.9         | 820.      | 2.5          | 163           | ÷ ;        | 1   | 20,450  | 10,100   |
| Cis-Ilexene-3                              | : :<br>:::                             | 3 3        | 154.2       | -207.0                       | 7.5.7        | 683       |              | 2017          | -:         | 1   | 20,420  | 19,070   |
| Trans-Hoxene-3                             | CHE                                    | 2 2        | 153.7       | -211.0                       | 75.4         | .684      | 5.60         | 1 21          | -<br>-     | 11  | 20,100  | 19,050   |
| DIOLEFINS                                  |  | !          |             |                              | 70.0         |           | 5.68         | 473           | ÷          | 11  | 20.420  | 19,070   |
| Propadieno                                 | C,II,                                  | 40.1       | - 30.1      | -213.0                       | 100          |           |              |               | _          |   | 2       | 000.61   |
| Butadieno-1,2                              | CH                                     |            | + 50.5      | 2                            | 3 5          | cuo.      | 36.          | 219           | <br>0,     | 1   | 20,880  | 19,930   |
| · · · · · · · · · · · · · · · · · · ·      | CIII.                                  |            | 24.1        | -164 0                       | 0.0          | 623       | 20 t         |               | 1          | 1   | 1       | i        |
| Cin-Pentadiane-1,2,                        | 110                                    | 08.1       | 112.8       | 2                            | 5            | _         | 1            | 200           |            | !   | 20,230  | 19,180   |
| Trans-Pentadieno-1.3                       |  | 08.1       | 111.6       | 1                            | 3.17         | 3 6       | 08.0         | 420           | 1          | 1   | i       | 1        |
| Pontadione-14                              | : :                                    | 5          |             | 1                            | 26 0         |           | 5.08         | 4 10          | 1 1        | -   | 20,150  | 19,010   |
| 3-Methylbutndiene-1,2                      | -<br>-<br>-<br>-<br>-<br>-             | 2.5        | 78.9        | -231.0                       | 81.3         | . 065     | 5,53         | 350           | _          |   | 001.00  | 19,040   |
| Z-fitthylbutadiene-1,3 (Iso-               |  |            |             | 0.181-                       | 82.0         |           | 5.70         | 410           | -          | . <u>.                                   </u> | 20,320  | 19,210   |
|  | 1000                                   | 1.89       | 83.3        | -231.0                       | 74.8         | .686      | 5.71         | 395           |            |   | _       | <b>!</b> |
| * Most of combustion as a gas-             | in as a gas—otherwise as a liquid.     | s n liquic |             | Critical temperaturashoiting | Dernture.    | 1,011     |              |               |            | -   | 20.060  | 18,950   |

\* Hast of combustion as a gas-otherwise as a liquid,

'Critical temperature-boiling point correlation.

\* Vapor pressure eurve or correlation.

į

\* Mixture of cis- and trans-isomors

-

|                              |                      |                      |                      |                                | 1                    |                      |                   |
|------------------------------|----------------------|----------------------|----------------------|--------------------------------|----------------------|----------------------|-------------------|
|                              |                      | c <sub>3</sub> :     | LPG                  |                                |                      | C <sub>4</sub> LPG   |                   |
|                              | c <sub>2</sub>       | c <sub>3</sub>       | С <sub>4</sub>       | Total                          | C <sub>4</sub>       | c <sub>5</sub>       | Tot               |
|                              | 10 <sup>3</sup> Lb/н | 10 <sup>3</sup> Lb/H | 10 <sup>3</sup> Lb/H | 10 <sup>3</sup> Lb/Н           | 10 <sup>3</sup> Lb/н | 10 <sup>3</sup> Lъ/н | 10 <sup>3</sup> 1 |
| 1981 <sup>*1</sup><br>(Kg/H) | 0.44                 | 23.6 <sup>*1</sup>   | 0.54                 | 24.58 <sup>*3</sup><br>(11.17) | 13.06 <sup>*2</sup>  | 0.27                 | ر<br>13.<br>6.0)  |
| 1982<br>(Kg/Ḥ)               | 0.74                 | 39:4                 | 0.90                 | 41.04<br>(18.65)               | 22.20                | 0.45                 | (10.              |
| 1983<br>(Kg/H)               | 0.89                 | 47.3                 | 1.08                 | 49:27<br>(22:40)               | 26.52                | o <b>ì</b> 54        | 27.<br>(12.       |
| 1984<br>(Kg/H)               | 1.23                 | 65.7                 | 1.51                 | 68.44<br>(31.11)               | 36.89                | 0175                 | 37<br>(17         |
| 1985<br>(Kg/H)               | 1.23                 | 65.7                 | 1-51                 | 68.44<br>(31.11)               | 36.89                | 0175                 | 3.7<br>(17        |
| 1986<br>(Kg/H)               | 1.43                 | 76.2                 | 1.75                 | 79.38<br>(36.08)               | 42.95                | 0.88                 | 43.<br>(19.       |
| 1987<br>(Kg/H)               | 1.43                 | 76.2                 | 1•75                 | 79.38<br>(36.08)               | 42.95                | 0.88                 | 43.<br>(19        |
| 1988<br>(Kg/H)               | 1.63                 | 86.8                 | 1.99                 | 90.42<br>(41.10)               | 49.01                | 1.00                 | 50<br>(22         |
| 1989<br>(Kg/H)               | 1.63                 | 86.8                 | 1.99                 | 90.42<br>(41.10)               | 49:01                | 1.00                 | 50<br>(22)        |
| 1990<br>(Kg/H)               | 1.63                 | 86.8                 | 1.99                 | 90.42<br>(41.10)               | 49.01                | 1.00                 | 50 (<br>22 )      |

Note: \*1 come from TABLE-12 (4) (ATTACH.18)

\*2 TABLE-12 (4') (ATTACH.18) minus C<sub>4</sub> in C<sub>3</sub> LPG of this Table 13.6 - 0.54 = 13.06 Calculation way \*3

c<sub>2</sub> 1

С<sub>4</sub>

C3 AND C4 LPG PRODUCTION (LB/H) OF EACH YEAR TABLE-15

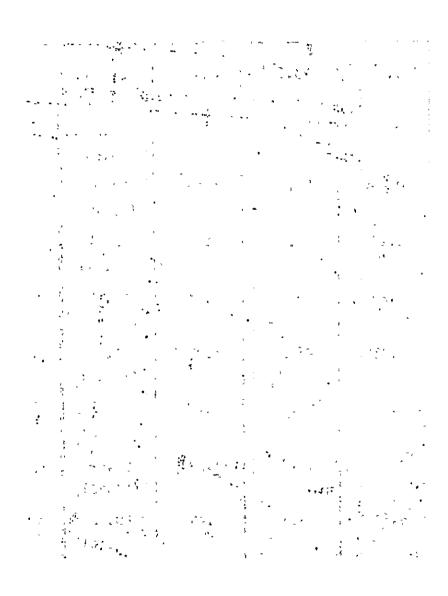
|                              |  | . c <sub>3</sub>                       | LPG                                    | -                              |  | C <sub>4</sub> LPG                     |                               |  |  | Total                                  |  |                               |
|------------------------------|--|--|--|--------------------------------|--|--|-------------------------------|--|--|--|--|-------------------------------|
|                              | с <sub>2</sub><br>10 <sup>3</sup> Lb/н | с <sub>3</sub><br>10 <sup>3</sup> lb/н | с <sub>4</sub><br>10 <sup>3</sup> Lb/н | Total<br>10 <sup>3</sup> Lb/H  | с <sub>4</sub><br>10 <sup>3</sup> lb/н | с <sub>5</sub><br>10 <sup>3</sup> lb/н | Total<br>10 <sup>3</sup> Lb/H | с <sub>2</sub><br>10 <sup>3</sup> Lb/н | <sup>С</sup> 3<br>10 <sup>3</sup> Lb/н | с <sub>4</sub><br>10 <sup>3</sup> Lb/н | с <sub>5</sub><br>10 <sup>3</sup> lb/н | Total<br>10 <sup>3</sup> Lb/H |
| 1981 <sup>*1</sup><br>(Kg/H) | 0.44                                   | 23.6*1                                 | 0.54                                   | 24.58 <sup>*3</sup><br>(11.17) | 13 <sup>1</sup> 06 <sup>*2</sup>       | 0.27                                   | 13.33 <sup>*4</sup><br>(6.06) | 0.44                                   | 23.6                                   | 13.6                                   | 0.27                                   | 37•91<br>(17•23)              |
| 1982<br>(Kg/H)               | 0.74                                   | 39:4                                   | 0.90                                   | 41.04<br>(18.65)               | 22.20                                  | 0.45                                   | 22.65<br>(10.30)              | 0.74                                   | 39•4                                   | 23.1                                   | 0.45                                   | 63.69<br>(28.95)              |
| 1983<br>(Kg/H)               | 0.89                                   | 47.3                                   | 1.08                                   | 49:27<br>(22:40)               | 26,52                                  | 0154                                   | 27.06<br>(12.30)              | 0.89                                   | 47•3                                   | 27.6                                   | 0154                                   | 76.33<br>(34.70)              |
| 1984<br>(Kg/H)               | 1.23                                   | 65.7                                   | 1.51                                   | 68.44<br>(31.11)               | 36 <b>.</b> 89                         | 0475                                   | 37.64<br>(17.11)              | 1•23                                   | 65•7                                   | 38.4                                   | 0.75                                   | 106.08<br>(48.22)             |
| 1985<br>(Kg/H)               | 1.23                                   | 65.7                                   | 1.51                                   | 68.44<br>(31.11)               | 36.89                                  | 0 •75                                  | 37•64<br>(17•11)              | 1.23                                   | 65•7                                   | 38,4                                   | 0.75                                   | 106:08<br>(48:22)             |
| 1986<br>(Kg/H)               | 1.43                                   | 76.2                                   | 1.75                                   | 79.38<br>(36.08)               | 42.95                                  | 0.88                                   | 43.83<br>(19.92)              | 1.43                                   | 76.2                                   | 44.7                                   | 0.88                                   | 123•21<br>(56•00)             |
| 1987<br>(к <sub>б</sub> /н)  | 1.43                                   | 76.2                                   | 1.75                                   | 79.38<br>(36.08)               | 42.95                                  | 0.88                                   | 43.83<br>(19.92)              | 1.43                                   | 76.2                                   | 44.7                                   | 0.88                                   | 123.21<br>(56.00)             |
| 1988<br>(Kg/H)               | 1.63                                   | 86.8                                   | 1.99                                   | 90.42<br>(41.10)               | 49.01                                  | 1.00                                   | 50.01<br>(22.73)              | 1.63                                   | 86.8                                   | 51.0                                   | 1.00                                   | 140.43<br>(63.83)             |
| 1989<br>(Kg/H)               | 1.63                                   | 86.8                                   | 1.99                                   | 90.42<br>(41.10)               | 49:01                                  | 1.00                                   | 50.01<br>(22.73)              | 1.63                                   | 86.8                                   | 51.0                                   | 1.00                                   | 140.43<br>(63.83)             |
| 1990<br>(Kg/H)               | 1.63                                   | 86.8                                   | 1.99                                   | 90.42<br>(41.10)               | 49.01                                  | 1.00                                   | 50.01<br>(22.73)              | 1.63                                   | 86.8                                   | 51.0                                   | 1.00                                   | 140.83<br>(63.83)             |

Calculation way

Note: \*1 come from TABLE-12 (4) (ATTACH.18)

\*2 TABLE-12 (4') (ATTACH.18) minus C4 in C<sub>3</sub> LPG of this Table
13.6 - 0.54 = 13.06

| *3             | c <sub>3</sub> L |           | * <b>Ļ</b>     |     | C <sub>4</sub> LPG<br>Lb/H÷0.98 |         |
|----------------|------------------|-----------|----------------|-----|---------------------------------|---------|
|                |                  | /H÷0•96 ' |                |     |                                 | Lb/H    |
|                | %                | Lib/H.    |                | %   |                                 | •       |
| c2             | 1.8              | . 0.44    | c <sub>4</sub> | 98  | . • • •                         | 13.06   |
| c <sub>3</sub> | 96.0             | 2360      | c <sub>5</sub> | 2   | . :                             | 0.27    |
| c <sub>4</sub> | 2.2              | 0.54      |                |     | •                               |         |
|                | 100-40           | 24.•58    |                | 100 | •                               | 13 • 33 |



| REMARK               | NATURAL GAS PRODUCTION MM scf/D | 150    | 300    | 350    | 500      | 500      | 009      | . 009    | 200      | 200      | 200      |   |
|----------------------|---------------------------------|--------|--------|--------|----------|----------|----------|----------|----------|----------|----------|---|
|                      | 10 <sup>3</sup> ፹/፻             | 150,93 | 253.60 | 303.97 | 422,40   | 422,40   | 490.56   | 490.56   | 559.15   | 559.15   | 559.15   | • |
| Total                | T/D                             | 413.52 | 694*80 | 883.80 | 1,157.28 | 1,157.28 | 1,344.00 | 1,344.00 | 1,531.92 | 1,531,92 | 1,531,92 |   |
|                      | T/H*                            | 17.23  | 28.95  | 34.70  | 48.22    | 48,22    | 56.00    | 26.00    | 63.83    | 63.83    | 63.83    |   |
|                      | 10 <sup>3</sup> T/Y             | 53.08  | 90,23  | 107.75 | 149,88   | 149.88   | 174,50   | 174.50   | 199-11   | 199.11   | 1199.11  |   |
| $\mathtt{c}_{4}$ LFG | T/D                             | 145.44 | 247.20 | 295.20 | 410.64   | 49.014   | 80°824   | 478.08   | 545.52   | 545.52   | 545.52   |   |
|                      | T/H                             | 90*9   | 10.30  | 12.30  | 17.11    | 17.11    | 19.92    | 19.92    | 22.73    | 22.73    | 22.73    |   |
|                      | 10 <sup>3</sup> T/Y             | 97.85  | 163.39 | 196.22 | 272.52   | 272.52   | 316.06   | 316.06   | 360.04   | 360.04   | 360.04   |   |
| . C <sub>2</sub> LPG | T/D                             | 268.08 | 9.644  | 537.6  | 746.64   | 746.64   | 865.92   | 865.92   | 04.986   | 04.986   | 04.986   |   |
|                      | T/H*                            | 11.17  | 18.65  | 22.40  | 31.11    | 31,11    | 36.08    | 36.08    | 41,10    | 41,10    | 41.10    |   |
|                      |                                 | 1981   | 1982   | 1983   | 1984     | 1985     | 1986     | 1987     | 1988     | 1989     | 1990     |   |

Note: \* from TABLE-15 (ATTACH.21)

