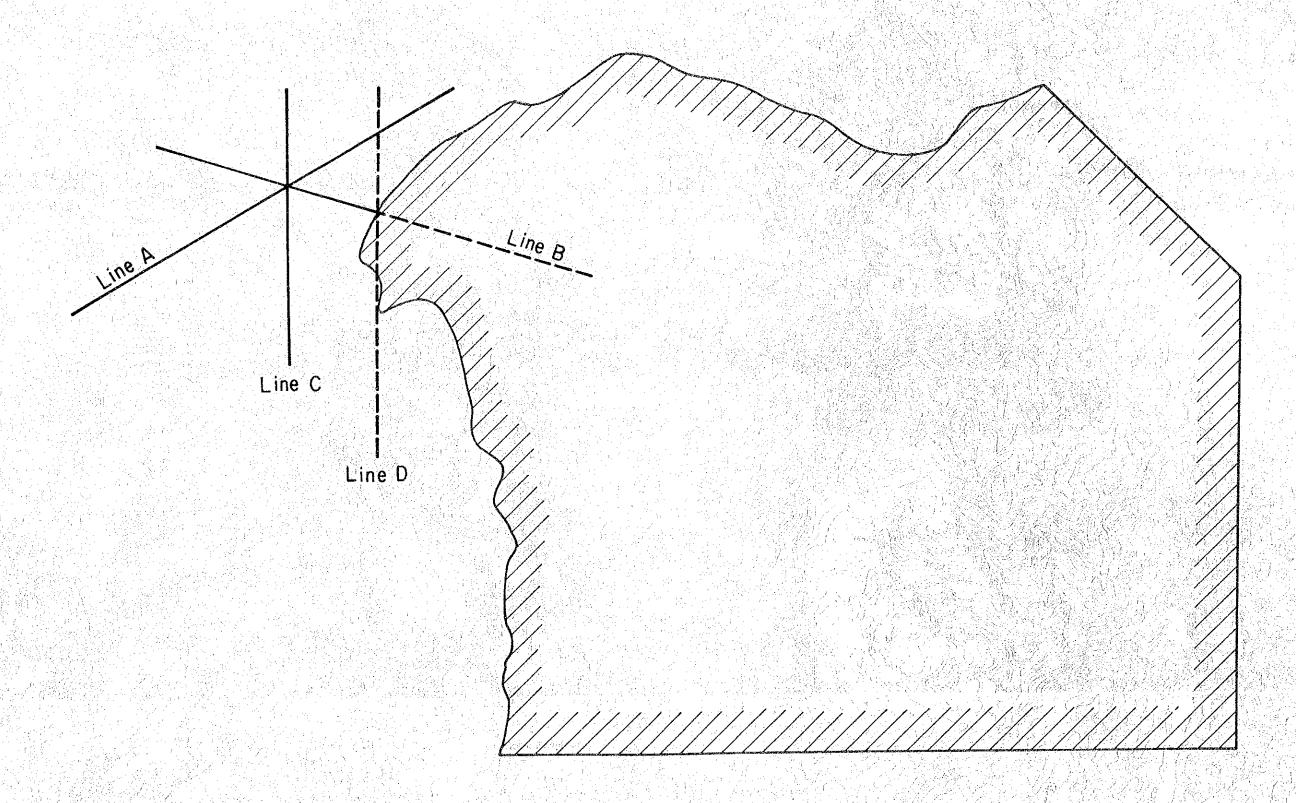
Proposed Electrical Survey Line

Alternative



Proposed Survey Area in Ifugao Province

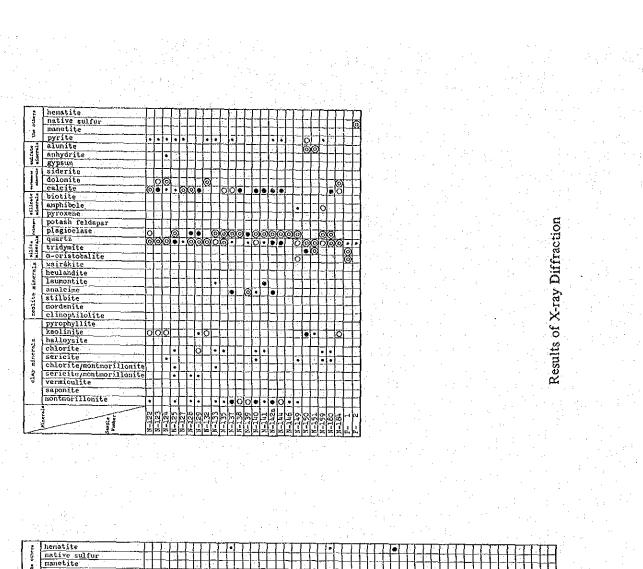


## Appendices

- O Results of X-ray Diffraction
- O Results of Microscopic Observation of Thin Section
- O Chemical Analysis of Whole Rock and Normative Mineral Composition
- O Computed Results of Gravity Survey
- O Computed Results of Magnetic Survey

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The Electronic State (1998)



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Results of Microscopic Observation of Thin Section

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Sample No	M-52	M-77	N-96	N-112	N-125	M-110	N-61	N-62	N-63	N-132	D-1
SiO <sub>2</sub>	68.65	45.00	55.10	60.25	47.90	73.03	58.50	73.83	45.36	46.14	86.42
TiO <sub>2</sub>	0.29	1.09	0.71	0.72	0.93	0.23	0,68	0.19	0.42	0.44	0,53
$Al_2O_3$	15.92	20.62	14.06	17.44	17.38	13.14	18.60	15.11	21.27	12.42	1.27
$Fe_2O_3$	0.99	3,03	3.68	3.75	3,45	1.95	0.87	1.32	0.60	0.44	2.44
FeO	1.83	6.68	3.66	1.58	3.88	0.54	2.73	0.29	0.14	2.87	0.07
Fe					0.57		1.07			1.12	
MnO	0.09	0.16	0.21	0.12	0.17	0.11	0.09	0.01	0.01	0.11	0.01
MgO	1.01	5.70	4.64	2.98	4.29	0.63	2.51	0.20	0.01	4.68	0.14
CaO	1.29	9.80	9.31	5.89	8.92	1.76	0.45	0.17	0.13	10.76	0.18
Na <sub>2</sub> O	3.85	2,77	1.71	3.90	3.37	3.39	0.52	4.50	1.62	0.03	0,10
K <sub>2</sub> O	1.53	0.48	1.14	1.42	0.69	1.99	1.32	1.48	2.63	0.28	0.03
$P_2O_5$	0.10	0.14	0.23	0.18	0.19	0.08	0.14	0.04	0.19	0.11	0.03
$CO_2$	1.98		0.98		1.90	0.42	4.06	0.0	0,17	14.15	0.05
S	1.50	12.00	0.50		0.66	0.12	1.23			1.29	
SO₃					0.00		0.26		20.23	1.29	0.47
H <sub>2</sub> O(+)	2.11	4.12	3.19	0.95	3.93	2.02	5.40	1.33	5.46	4.73	3.80
$H_2O(-)$	0.14	0.24	1.82	1.28	0.92	1.08	0.86	0.98	1 1 1 1 1		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
TOTAL	99.78	99.83	99.44	99.46		99.37		1.0	1.48	0.16	4.14
IOIAL	99.76	79.63	99,44	99.40	99.28	99.37	99.29	99,45	99.54	99,73	99.63
Q	39.43		21.42	16.04	5.04	44.40	53.01	41.44	45.35	44.31	85.21
С	7.93					5.11	16.80	5.89	2.04	12.07	0.82
or	9.04	2.84	0.83	8.39	4.08	11.76	7.80	8.75		1.65	0.18
ab	32.58	23.44	14.47	33.00	28.52	28.69		38,08		0.25	0.85
an		42.41	30.27	25.89	30.26	0.81	1.02	0.58		0.25	0.70
ne			50.5	30.0	00.20	0.01	1.02	0.50			0.70
wo		2.21	3.65	0.90	1.73						
di en		1.39	2.65	0.78	0.56						
fs	2.12	0.69	0.66	0.70	0.09	+ :	. :				
, en	""	2.83	8.91	6,64	10.12	1.57		0.50	0.02	1.82	0.35
hy fs		1.40	2.24	0,04	10.12	1.57		0.50	0.02	1.02	0.55
fo		6.99	2.27								
i ol		3.82									
fa	1 144		5.24	2.40		1.42	0.20	0.40	0.00	0.26	
mt ll	1.44	4.35	5.34	3.40		1.43	0.29	0.42	8.05	0.36	0.17
)	0.61	2.07	1.35			0.44	1.36	0.36	0.28	0.76	8.17
hm	0.21	1.20	0.52	1.41		0.96	0.67	1.03	0.57	0.19	2.44
ар	0.31	1.32	0.53	0.42		0.19		0.09	0.25	0.31	0,07
pr			17 14			1.55	2.28			2.40	
th							Talana and a				43.
cc	2.00		2.12			0.91	0.10			18.92	
(MgCO <sub>2</sub> )	2.11						5.23			8.26	
(FeCO <sub>2</sub> )							3.56			4.05	
al									43.93		
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TOTAL	97.57	94.76	94.43	98.23	93.57	96.27		97.14	92.49		

Chemical Analysis of Whole Rock and Normative Mineral Composition

Computed Results of Gravity Survey

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								in with			
	NO	LATITUDE	LONGITUDE	ALTITUDE	2.00	2.30	2.40	2.50	2.50	2.70	
		1643.366	12049.563	1394.860L	77.06	60 . 52	55.01	49.50	43.99	38.47	1.17
	5	1643.550	12049.383	1427 656L	77.66	60.84	55.23	49.62	44.01	38.40	
	3	1643.744 1643.990	12049.375	1441.719L 1434.156L	78.00 78.42	60.94 61.46	55,25 55,80	49,56 50,15	43.87 44.50	38.19 38.85	
	5	1644.090	12049.570	1420.438L	78.23	61.46	\$5.87	50.28	44.70	39.11	
	6		12049.460	1433,974L 1429,925L	78,79 78,68	62.02 61.87	56.37 56.26	50.71 50.66	45.06 45.05	39.40 39.45	
	8	1644.769	12049,530	1429 388L	78.24	61.40	55.78	50:17	44.56	38.94	
	9 10		12049.810 12049.995	1452.178L 1437.188L	80,69 79.00	63.64 62.16	57.96 56.55	52.28 50.94	46,60 45.32	40.92 39.71	
	ii	1645.163	12050,200	1468.276L	79.32	62.03	56.27	50.51	44 . 75	38.99	
	i2 13	1645.342 1645.522		1509, 439L 1569, 177L	80.41 81.63	62.27 62.64	56.23 56.32	50.19 49.99	44.14	38.10 37.33	
	14	1645.740	12050.110	1632 288L	82.03	62.06	55.40	48.74	42.08	35.42	
	15 16		12050.008	1618.150L 1604.726L	81.32 80.69	61.56 61.09	54.97 54.56	48.39 48.03	41.80	35,21 34,97	et 1,100.
	17.	1646.442	12049.817	1609.160L	84.35	64.67	58.11	51.55	44.99	38.43	
	18 19	1646.786 1647.078	12049.978 12050.040	1604 814L 1598 374L	81.87 82.98	62.30 63.46	55.78 56.95	49.26 50.44	42.74 43.94	36.22 37.43	
	50	1647.440	12049.863	1598.506L	84.28	64.64	58.10	51.55	45.81	38.46	1 1 1
	55 51	1647.698 1647.920	12049.700 12049.714	1602.792L 1634.080L	84.41 85.43	64.70 65.34	58.12 58.65	51.55 51.95	44 . 98 45 . 25	38.41 38.56	: ,
	53	1648.045	12049.564	1704 4741	86.91	85.94	58.95 59.66	51.76 52.31	44.97 44.97	<b>37 .98</b> 37 .62	
	24 25	1648.343	12047.118	1813 413L 1819 886L	89.05 88.19	67.01 66.06	58.69	51.31	43 . 94	36 . 56	
	26 27	1647,790 1647,533	12049 143 12048 970	1807 490L 1845 532L	86.65 87.52	64.60 65.20	57.2S 57.76	49.91 50.32	42.56 42.88	35.21 35.44	
	- 58	1647.223	12048.831	1850 454L	88.39	65.90	58.40	50.90	43.40	35.90	
	29 30	1647,090	12048.592	1906 108L 1950 103L	90.65 91.47	67.82 68.16	60.20 60.39	52.59 52.62	44 . 98 44 . 85	37 .37 37 .08	
	31	1646.829	12048.373	2006.590L	92.93	69 48	46.16	53.85	46. Û3	38.21	
	32 33		12048.320 12048.236	2042 161L 2048 458L	91.25 91.54	67.24 67.36	59.23 59.30	51.23 51.23	43.22 43.17	35.21 35.11	1
	34	1646.040	12048.350	2053.694L	92.66	68.38	60.28	52.19	44 10	36.00	
	35 35		12048.252 12048.216	2076 660L 2098 146L	90 80 92 36	66.09 67.43	57.85 59.11	49.62 50.80	41 38 42 48	33 .14 34 .16	٠.
	37	1645.192	12048.000	2121.5551	92.89	67 79	59 . 42	51 06	42 . 69	34 . 32	
er en en en en en en en en en en en en en	36 39	4.0	12047.934 12047.882	2147.546L 2167.691L	93.28 94.53	67 94 69 03	59.49 60.53	51.05 52.03	42.60 43.53	34.15 35.03	
	40	1644.372	12048.024	2194 450L	93.67	68.04	59.50	50.96	42 42	33.87	
	41° 42		12047.987 12048.153	2214 341L 2102 263L	93.35 92.80	67 35 67 98	58.69 59.71	50 02 51.44	41 36 43 16	32 .69 34 .89	
	43	1443.609	12048.352	1966 7476	85.64	65 10	57.26	49 41	41.57	33.72	
	44 45		12048.521 12049.713	1909.300L 1870.598L	87.76 85.78	64 97 63 35	57.37 55.88	49_77 48_4û	42 17 40 93	34.57 33.46	
	46	1643.140	12048.942	1690 900T	84.18	61.56	54.85	48.15	41.45	34.75	
	47 48		12049.140 12047.713	1543.360T 2237.100L	79.23 96.14	69 75 69 75	54.85 60.95	48.75 52.15	42.66 43.35	36.56 34.55	
	47	1643.858	12047.430	2268 572L	99.59	72 81	63.88	54 95	46.02	37 . 19	٠.
	50	1643.840	12047.124	2319 484L	101 95	74 52	65.38	56.24	47.10	37.95	2.4
		e tage de									
			San San San San	42°						4 4.	

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NO	LATITUDE	LONGITUDE	ALT TYUDE	2 00	2.30	2.40	5.50	2.60	2.70
51	1643.590	12046.862	2336 433L	103 94	76,42	67:25	58.07	48 90	39.73
52	1643.479	12046.672	2337 3681	104,47	76.73	67,49	58.24	48 99	37.75
53	1643,410	12046.333		106.77	77.16	69.96	60.76	51.56	42.35
54	1643.175	12046 100	2333.064L	107.05	79.42	70.22	61.01	51 80	42, 60
55.	1642.973	12045 926	2331 674	107.43	79.82	70.62	61.41	52.21	43.01
56	1643.370	12049.285	1382,0501	76.71	60.63	55.27	49.91	44 55	39.19
57	1643.140		1391 118L	75.87	59.36	53.86	48.36	42.86	37.35
58		12049,841	1437 773L	76.70	59.61	53.91	48.21	42.51	36.81
59	1642.680	12050,090	1440 626L	75.67	58.68	53.01	47.35	41 69	36.03
60	1642.720	12047.831		79.13	61.22	55.25	49.28	13 31	37 34
61		12049.910	1534.313L	79.28	60.81	54.65	48.49	42.33	36.18
62	The second second	12049 792	1592 7981	80 44	61.16	54.73	48.30	41 .87	35 44
63	1642.000	12049.947	1570.225L	79,50	60.65	54.37	48.09	41.81	35.53
64		12049.974	1593.439L	81.23		55.67	49 . 28	42.89	-:
.55		12050 491	1564 324	82.16	63.54	57.33	51.12	44.91	38.71
66	1643,149	12049.360	1314 200B	71.58	56.46	51 . 42	46.38	41 34	36.30
67	1642.790	***	1304 300B	71.04	56.01			40.97	35.96
68	1642.555	and the second second	1294 3008	70.07	55.35	50.44	45.53	46 62	35.70
69	1642.268	12049 443	1444 1006	75.75	58.50	52.76	47.01	41.26	35.51
70	1641,980	and the second second	1446,4001	76.41	59.25	53.53	47.81	42 09	36.37
71	1641.665	12049 : 373	1255.6008	70.31	55.15	51.43	46.71	41.99	37.27
. 72	1541.314		1350,7000	73.54	57.75	52.49	47.23	41 97	36 71
73	1641 080	12049.372	1369,0001	73.59	57 88	52 54	47.20	41.86	36.52
74	1541,462	12047 680	1458.8008	76.77	59.36	53.56	47 76	41.76	36 15
75	1641 285	12056 026	1575.895L	82,21	53.49	57.13	50,35	44.59	36.52
76	1541.133	12049.839	1577 8736	81.35	62.58	56 . 22	49.94	43.56	57 36
77	1640.870	12049 840	1558.400L	52 07	63.52	57.34	51.16	44,98	38.65
73	1540,608	12049,595	1527 472L		64.56	58.56		45.36	40 29
79	1540, 429	12049,949	1495,0331	83 7	55.78	59.99	54.10	48,40	12.60
80	1640.160	12047.850	1511.313L	82.68	54.32	58.40	52.48	16.55	40 54
81	1637.857	12049:746	1447 073L	81 10	63 83	58.15	52 41	46.57	46.93
82	1639.563	12049,576		. 77.¢a	52.94	57:55	52.17	46.79	11 41
83	1639.386	12049.740	1226,054L	74.58	51.23	56 65	52.67	47 49	42.90
84		12049.814	1233.834L	77 82	54.i0	57.53	54.98	50 39	45 . 82
23	1638,702	12047.626	1188.41aL	74.33	61:52	57.08	52.65	48.21	43.77
કંદ	1838,521	12049.598	1185.038L	75.12	61.73	57 .26	52.60	48.33	43 . 87
87	1638.213	12049,430	1237,641L	78.17	54.13	59.44	54.75	50 Oc	45.38
88	1639,106	12049,753	1363,486L	79.39	546	59.22	54.18	49.14	44 10
87	1637,924	12049.952	1290.428L	78.63	63.56	58.54	53.52	48, 49	43.47
.98	1637 5B6	12049.975	1224,607L	77.03	£3.00	58.32	53.65	48 . 37	44.29
91	1637 692	12050.210	1180.272L	77 . 47	64.24	59.83	55.42	51.0i	46.60
92	1637.492	12050,222	1184.109L	76.23	62-72	58.22	53.72	49.21	44.71
93	1642.760	12048.848	1775.669L	84.St	63.13	55.00	48.67	41.74	34.51
94	1642 442	12048.790	1704.8441	83.10	δ2 . 5Ŷ	55 76	48.92	42.08	35 25
95	1642.169	12648.842	1668.3011	82.07	62.06	55 37	48.71	42.04	35.37
76	1641.908	12048.845	1612.051L	49.08	61.43	54.96	48.48	42.61	35 . 53
47	1641.651	12048.955	1633.760L	81.61	:62.15 -	66. 22	49.18	42 67	36.21
93	1641 . 420	12048 970	1598 812L	. 81.69	62.53	58.15	. 49 . 76	43 . 36	37 (U
59	1641.126	12048 927	1607 781L	81.87	63.02	co.73	50.44	44.15	37.86
100	1640.752	12048.953	1578 537_	85 83	64.17	57.95	51.73	45 52	37 30

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	ΝŪ	LATITUDE	LONGITUDE	ALTITUDE	5.00	2.34	. 2.40	2 50	2.60	2.70
		1/A0 E73	10630 667	4CM 075	04 00	17 64	PB			40.400
	102	1640.532 <sub>:</sub> 1640.290	12048.993	1506.836L 1464.962L	81.72 80.81	63.76 63.77	58.04 58.09	52.12 52.41	46.21 46.73	40.29 41.05
	103	1640.010	12049,035	1374 . 467L	79.58	63,69	58.39	53.10	47.80:	42.50
	104	1639 . 732	12048.940	1178.000B	73.59	δ0.85	56.60	52.35	48.10	43.86
		1637.755	12049,228	1353.927L	78.73	63.15	57.95	52.76	47.56	42.37
•	106	1639.770	12049.540	1415.592L	81.48	63.29	57.66	52.ú3	46.41	40.78
	107 108	1643.615 1643.745	12052.270 12052.005	2042.576L 2007.158L	92.27 91.51	67.38 67.11	59.08 58.9B	50.78	42.48	34 . 19
	109		12051.760	1957.761L	89.43	65.52	57.55	50,85 49,58	42.72 41.61	34.59 33.64
	110	1643.353	12051.480	1880.014L	88.06	65.02	57.34	49.66	41.98	34.30
	iii	1644.084	12051.300	1849.739L	86.87	64.15	56.58	49.00	41.43	33 .85
	112	1644.136	12051.107	1831 . 242L	86.16	63.72	56.24	48.76	41.28	33.80
	113	1644 . 262	12050:916	1792.028L	86.72	64.73	57.40	50.08	42.75	35 . 42
	114 115	1644.451	12050.683 12050.380	1756.700L 1709.576L	87.99 88.55	65.42 67.76	59.23 50.83	52.04	44.85	37.67
1	115	1644.240	12050.081	1626.579L	86.06	66.39	59.83	53,90 53,28	46.97 46.72	40.04 40.16
	117:	1644.170		1538 : 683L	82.97	64.62	58.50	52.38	46.26	40 . 14
	118	1643.343	12052,130	2130.082L	92.80	67,15	58.60	50.04	41.49	32.94
	119	1643.120	12052.241	2241 . S90L	93.17	66.49	57.59	48.76	39.81	30.71
4 1 1	120 121 -	1642.971 1643.068	12052:171 12051:789	2255.382L	73.51	6a.51	57.51	48.51	39.51	36.51
	122	1643.137	12051.767	2151 576L 2047 333L	72.13 70.69	. 66 , 27 . 65 , 87	57.56 57.58	49.04 49.32	40.42 41.05	31.80 32.78
	123	1643.250	12051.198	1972 4701	91.44	67.6E	59.73	51.8u	43.87	35.94
	124	1643.230	12050.925	1904 570L	88.38		57.56	47.65	42.14	54.44
•	125	1643.240	12050.620	1804 953L	65 88	54.01	55.72	49.43	42.14	34.84
	126	1643.297	12650 . 425	1741 923L	84.80	63.68	56 56	49.50	42.44	35 38
-	127 128	1643.340 1643.382	12050,120 12049,900	1629 - 4521. 1560 - 0271.	83.35 81.68	- 88, 56 - 88, 56	56.95 56.61	50,35 50,34	43.75 44.68	37 15
	129	1644.302	12048.345	2000.5901	89 39	34.71	56.82	48.93	41.64	37 81 33 15
	1.30	1644.362	12048.631	1846.200T	83 74	61 60	54:22	46.84	39.46	32.08
	131	1644,270	12048.806	1739±180T	82.63	51 : 24	54 31	4738	40 44	33.51
	132	1644.170	12048:970	1651.100T	30 17	£0.4E	53.92	47.35	40.80	34124
	133 134		12049,270 12049,208	1480.836T 1349.000B	78.2i 73.5i	60 58 58 :0	54.70 52.76	48 82 47 82		37:07
	135		12047.166	1381 000B	74 16	58 09	52.75	47.42	42.58 42.08	37.54 36.74
•			12050.224	1691 837L	85.74	21.23	58, 29	51.43	44.57	37.70
	137		12050.020	1634 175L	84 57	64.83	58.25	51.67	45.07	38,51
	138		12049.740	1565 499L	82.66	63.78	57.49	51.20	44.91	38.62
		1645.518		1719.200B	93 49		65.82	58.90	51.98	45 . 06
**		1645.622 1645.525		1675 7008 1651 3008	89 87	69.81	63.12	56.43	49.75	43.06
		1645.592		1594.300B	88 59 86 49	68.74 67.61	62.12 61.32	55.51 55.03	48 .89 48 .74	42 . 27 · · 42 . 44
			12051 885	1623 1308	88 21	68.80	62.33	55.86	49.39	42,92
	144	1645.484		1607.600B	84 74	65.41	58.97	52.52	46.08	39.64
		1645.360		1605 9008	84 27	84 93	58.49		45.59	39.15
	146		12051.139	1558.200B	79.88		54.73	48.69	42.45	36 .21
	147 · 148		12050 927 12050 662	1574 7006 1620 3008	79.60 30.2i	60 51 66 47	54.14 53.89	47.77 47.31	41.41	35.04 34.14
	149		12050 453	1592.400B	80.29	50 47 50 93	54 48	48.62	41 :57	35.12
	152	1642.631	12050,350	1457 0008	75 72	58 55	€3.84	47 12	41.41	35,69

		1 4 S 1 2 1 1 1		The state of the s						100
	. 110	LATITUDE	LONGITUDE	ALTITUDE	2 00	2,30	2.40	2 50	2.60	2.70
	151	1642 659	12050 571	1497,4008	76.94	59.59	53 80	48.02	42 23	36:45
	152	1642,645	12050.772	1552 700k	80 42	62.27	56 23	50 18	44 13	38 .09
	153		12051.010	1601 300B	79.67	60.89	54.62	48.36	42.10	35.84
	154	1642.698	12051 260	1776,800B	87.18	65.70	58.54	51.38	44.22	37 06
	155	1642.700	12051 411	1898.300B	89.78	66.76	59.08	51:41	43.73	36.06
•	156	1642.864	12051 062	4004.1581	86.80	64,49	57.05	49.61	42.18	34.74
	157	1642 847	12050.824	1805.200B	86.00	64.18	56.90	49.63	42.35	35.07
	158	1642,950	12050.643	1744 1008	82.63	61.45	54.40	47 . 34	40 28	33 . 23
	159	1643,110	12050.550	1751 100B	82.76	61.45	54.34	47.24	40 13	33.03
	160	1644.630	12050.980	1706 400B	86.71	65.79	58.81	51.84	44 87	37 89
	161	1644 857	12050 932	1655.300B	83.43	63,23	56.50	49.76	43.03	36.38
	162	1645,150	12050 775	1555 700B	80.40	61.56	55 . 28	49.00	42 72	36 44
•	163		12050.570	1475.200B	78.12	60,45	54.56	49 67	42.78	36.89
	164		12050 405	1468 500B	78.66	61.03	55 . 22	47 36	43.50	37 63
	165		12051 038	1496.6809	80 10	62.17	56.19	50.22	44.24	38.27
	166		12049.680	1544.700B	84.54	65.97	59.81	53 . 63	47 . 45	41 . 27
•	167		12049 892	1669,600B	83.89	63.74	57.02	50.31	43.59	36.87
	168		12050 154	1794 1008	84.58	62.89	55.66	48 . 43	41 20	33 . 97
•	169		12050 422	1880 8008	86.63	63.98	56.42	48.87	41.32	33.77
	178	1643.520	Contract of the Contract of th	1974 200B	89.33	65.56	57.63	49.70	41.78	33 .85
	171 172		12050,912 12051,570	2050 9008	88.91	64.43	56.34	48.20.	40.08	31.92
	173	1643.540	12051 .570	1991,000B 1907,500B	90.69	66.40	58.30	50 . 21	12.11	34 01
	174	1643.913		1795,600B	67,81 86,31	64.47	56, 69 56, 88	48.71 49.52	41.13	33.35
	175		12051.200	1733 6008	85 36	64.23	57.19	50 14	42 17 43 16	34.81 36.85
	175	and the second second second	12050.825	1708,2008	86 14	85.35	58.43	51.50	14 57	37. 64
	177		12050:760	1786 80CB	87.85	65.97	58.67	51 38	44.09	35.79
	178	1642,410	12048 550	1556.80(B	78,44	59.83	53.62	47 .42	41.21	35 . 01
	179	1642,460	12048,257	1585 700B	79,43	å6.45	54/12	47.79	41.46	35.13
•	189	1642.491	12048 027	.605.600B	83.49	64.44	58.18	51.73	45 . 33	39.63
	151:	1642.484	12047.739	1650,4009	87,44	67 94	61.44	54.54	48 44	41.74
	182	1542,546	12047 493	1705.00GB	89.76	89,45	62.67	55 90	49.13	42.36
	: 83	1642,569	12047 213	.758.100B	91.76	70.95	64.02	57.08	50.14	43.21
	184		12046,980	1841.6008	96.31	74.69	<b>57.48</b>	66 . 27	53.05	15 . 85
	185		12052.419	2280.134L	163.69	75.54	66.49	57.34	46.19	39.04
	186	1640.650	12052 153	2340.162L	103.10	75.46	86.25	57.04	47.82	39 6i
	187		12051.920	2261 . 282L	105:44	78.73	69.83	60.93	52.03	43.13
	185		12051.660	2212,080L	103.68	77.36		59.82	51.05	12 . 28
	189 190	1640,582	12051 350	2136 485L	99.82	74.27	65.78	57 27	48.76	40.25
	171		12051 . 046 12050 . 803	2066.752L 1966.033L	98.08 96.07	.73.41. 22.54	65.18	56.96	48.73	40.51
	192		12050.595	1877, 4511.	91.64	69.23	64 70 61 76	56.85 54.29	49.01 46.82	41.17 39.35
	193		12050.290	1783 977L	87.63	68.23	61.08	53.93	46.78	39.63
	194	1640.620	Annual Control of the	1698.54cL	87.22	67.12	61.42	53.72	47 úz	40.32
	195		12049 925	1573 366L	84.92	66.03	57.73	53.43	47.13	40.93
	196		12050.050	1619.50UB	83.24	63.91	57.46	51:01	44.57	38 12
	3 97	1640.856	12050.100	1694.6008	84.91	64.61	57.84	51.07	44.31	37.54
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Computed Results of Magnetic Survey

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: 3	43 81	2	2.0	9:51 9:53	40421	-6	3	40484 40543	-477 -413		393	81.2	, <b>Ş</b> .	10:34 10:35	40435 40521		4	40431 40617	-530 -344	)
	45 81	2	7 0	7:57	41179 40632	_9		41239 40691	278 -270		376	31 2	9	10:44	40519 40258		2	40517 40255	-444 -706	
3	48 8i	. 2	7.1	0 : 0 i		-9	Š	40461 40723	-238 -500		378		9	10:45 10:47	40239 39758	. :	3 4	40236 39754	-729 -1207	
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466	OF GRS. Bi 2 7	46 55	2027.6	CHANGE	VALUE	-1507	AP z	OF OBS.	(r ar	40475	CHANGE	VALUE	F 7 7
402	1			6 9	39454 4009B	-863	452	81 2 10		40435 40045	11 16	40424 40035	-537 -926
463				ý	39796	-1165		81 2 10		40572	9	40563	-378
404			39842	10	39832	-1155	454	81 2 10	15:45	40617	· 8	40609	-352
409			40128	ii	40117	-844		81 2 10		40532	7	40525	-436
	812 9 812 9		40164	11 11	40153 40622	-808 -339		81 2 10 31 2 10		40593 40546	6 6	40587 40540	-374 -421
408			40730	ii	40719	-242		81 2 10			5:	40347	-614
409				ii	40878	-83	459	81 2 10		40398	5	40393	-578
410			40918	11	40907	-54	460	Bi 2 10		40772	5	40767	-194
411			40986	11	40975	14	461	81 2 10			4	40792	-169
	912 9 812 9		41133	11 11	41116	160 155	462 463	81 2 18			3 23	42390 41063	1429 102
414			41052	12	41040	79	464	81 2 11			25	41003	42
419			41007	11	40996	3c	465	8i 2 ii			26	40936	-25
416		11:31	40746	11	40934	-27	466	81 2 11			29	41003	42
417 418			40976	11	40985	-24		81 2 11			30	41103	142
419			40743 40984	<b>33</b> 33	40710 40950	-25i -1!	468 469	81 2 11 81 2 11		100	30 31	41269 41403	308 442
420			41107	34	41072	iii	470	31 2 11			32	46997	36
421	81 2 11	10:17	41375	35	41340	379		81 2 11			32	41397	435
422			41267	35	41232	271		81 2 11			33	41203	242
423 424	1 -		40979 40510	36 37	40943 43473	-18 -488	473 474	81 2 11 81 2 11			34 38	41347 41201	385 240
425			40505	37	40468	-493	475	81 2 11			.38	41019	58
420	81 2 10	10:36	40871	33	40833	-128	476	81 2 11			37	41236	275
427			41293	38	41254	293	477	81 2 11	4 1 to 1 to 1		41	41397	436
428	and the second of the second		41071	39	41032 41129	71	478	31 2 11		41445	41	41484	443
429 430	2.14		41166	39 40	41936	168 75	479 480	81 2 11 81 2 11		41325 41272	41 42	41284 41230	323 259
431			40987	40	46747	- <u>1</u> 4	481	81 2 11	4.1	40921	42	40879	-32
432		and the second	40729	41	40698	-273	482	81 2 11		41358	41	41317	356
433			40720	41	40679	-585	493	81 2 11			35	40971	10
434 439			40697 41038	42 44	40855 40994	-106 33	484 485	81 2 11 81 2 11		41395	34 34	41361 41331	406 370
436	and the second second		40910	45	40865	-96	485	81 2 11		and the second second	34	41231	276
437	81 2 10	11 61	40534	45	40489	-472	487	81 2 11			33	41274	313
	81 2 10		41297	45	41252	291		31 2 11			33	41428	467
439 44ŭ	81 2 10 81 2 10			45 46	41109 40652	148 -309	489 490	81 2 11 81 2 11			32 32	41542 41304	581 343
	81 2 11		40535	45	40488	-473		81 2 11			32	40996	35
	81 2 10		40537	47	49470	-471		81 2 11			31	41145	184
	81 2 10			46	39788	973		81 2 11			31	40971	10
	81 2 10 81 2 10			45 46	46293 40750	-211 -668		81 2 11 81 2 11			30 29	46818 41148	-143 187
	81 2 10			46	40752	21		81 2 11			29	41304	343
	81 2 10		41301	12	41289	328		81 2 11			28	40910	-51
	81 2 10		40782	12	40770	-191		81 2 11			28	41067	106
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	:	502	81 2	11 14:15 11 14:19	41215	26 25	41049 41190	529 88		551 552	81 2 13 31 2 13			19 19	40902 41167	-59 206
•		504	81.2	11 14:22 11 15:12	41320	25 15	41307 41305	346 344			81 2 13 81 2 13			19 19	41439 41172	478 211
		506	81.2	11 15:15 11 15:17	41528 48999	14 13	41514 40986	553 25			81 2 1 81 2 1			19 19	41362 41234	40i 273
		507 508		11 15:20 11 15:24		i2 i2	40736 41150	-225 189	try 11.		81 2 1 81 2 1	3 09:52	41135	20 21	41115 41263	154 302
				11 15:26 12 08:42	40839 41358	ii -i	40828 41359	-133 358		959 560	81 2 1 81 2 1	3 10:01	41253	. 21 22	41232 41472	271 511
		511	8i 2	12 08:50 12 09:00	41296	-i -0	41296 41338	335 427		561 562	81 2 1 81 2 1	3 10:15	42045	22 22	42023 41515	1062 554
:		513 514	81.2	12 09:05 12 09:11	41098	O J	41097 41471	136 510		563 564	81 2 1	3 10:21	41566	22 23	41543 41461	582 500
-			81 2	12 09:17 12 09:35		. 2 8	41530 41432	569 471		565	8i 2 i	3 10:32	42174	23 24	42150 41835	1189 874
		517	81.2	12 09:40 12 09:44	41560	iù ii	41550 41439	589 478	2 A	567	81 2 1 81 2 1	3 10:37	42226	23	42203	1242
:	. * • *		81.2	12 10 12 12 11 40	41435	14 35	41 <i>422</i> 41832	461		567	81 2 1. 81 2 1.	10:42	40803	23 23	41265 40785	304 -176
		521 522	81 2	12 12:00 12 12:33	41234 41582	34 31	41200	239		571	81 2 i	3 10:55	41329	23 24	41304	285 343
	45	523	81 2	12 13:25	41302	3.)	41551 41278	590 317		572 573	81 2 1. 81 2 1.	3 11:01	41364	25 24	41957 41339	996 378
			81.5	12 13:30 12 13:35	46926 46348	36 3)	40875 40318	-65 -543		575	81 2 1 61 2 1	3 ii:05	41538	24 24	41527 41514	556 553
4		526 527	<b>8i</b> 2	12 13:40 12 13:49	40689	27 23	46496 40651	-465 -300	: ".	577	81 2 1 81 2 1	3 10:30	41177	24 70	41390 41107	146
		528 529	81.5	12 13:50 12 13:55	41996	28 27	40969 40969	-52		570 579	61 2 I	3 10:34	41125 40775	7ú 70	41055 40705	74 -256
		531	8i 2	12 14:06 12 14:10	40806	25 25	40983 40781	-78 -180		581		3 10:39	40854	79 70	40929 40784	-32 -177
		532 533	81 2	12 14:15 12 14:20	41174	24 24	41104 41150	143 189		582 583	91 2 1 81 2 1			71 71	48833 40635	-128 -326
		534 535		12 14:39 12 14:45		22 21	41135 41192	174 231	- 5 - 1	584 585	81 2 1 81 2 1			71 71	40931 41973	-30 112
		536 537		12 14:50 12 14:59	41110 41183	20 18	41090 41155	129 204			81 2 11 81 2 1			72 72	40787 40949	-174 12
				12 15:10 12 15:20		15 13	49957 40951	-4 -10			81 2 1 81 2 1			73 73	40887 40794	-74 -167
		540	81 2	12 15:30 13 09:07	41021	10 13	41010	49 -297	and a	590	81 2 1 81 2 1	3 11:04	41041	73 73	40968 48943	7 13
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		546	81.5	13 09:22 13 09:24	41011		40995 41048	34 87		596	81 2 1	8 11:25		77 79	40971 41033	10 72
		548	81.5	13 09:26 13 09:29	40830	17 18	40813 40914	-148 -47		598	81 2 1 81 2 1	8 11:30	40833	80 80	40753 40759	-508
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	602 603	81 2 18		41188	8i 61	41107	146 178	652 653	81 2 20 81 2 20		40807 40902	68 69	40739 40833	-222 -128
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	505	81 2 18		40977	81	40396	-65	655			40946	71	40875	-86-
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1	608	81 2 18			80	40901	~60	658	The second second		40868	73	40795	-166
	609	81 2 18	11:56	41147	80	41067	106	659	81 5 50	09 41	40828	73	40755	-206
	610 611	81 2 18 81 2 18		41031 41127	80 80	40951 41047	-10 86	661 661				74	40838 40928	-123 -33
	612	81 2 18		40941	61	40780	-181	652	4 4 4	200 0 0 0		75 75	40865	-156
	613	Bi 2 18	13:01	41095	61	41934	73	663	81 5 50	10:26	40886	88	40798	-1.63
: .	- 614	81 2 18			59 56	41015	54	664			48964	89	40875	-83 75
	.615 616	81 2 18 81 2 18		41111	59 56	41052 46969	9i 8	665 656	tian in the time of		41126 41066	90 91	41036 40975	/5 14
	617			41074	54	41040	79	667	81 2 20	10:45	46881	91	40790	-17i
	618	81 2 18			53	40956	-5	668	1.1		40942	96	40846	-115
+ 4	619 620	81 2 18 81 2 18		40918	49 47	40869 40731	-92 -189	659 670	The second second		40915 40925	91 52	40824 40833	-137 -128
		81 2 18	9 6 6	40594	44	40650	-311	671	81 2 20	10:56	40730	93	46637	-361
	622	81 2 18		40531	42	40487	-472	672			46987	93	40894	-67
	623 624	81 2 18 81 2 18		41015	39 39	40776 40716	15 -245	673 674	1 - 1			94: 94	40868 40461	-93 -500
		81 2 18		40776	35	40740	-22i	675				94	40937	24
	636	81 2 17		40717	72	40845	-116	678				95	40747	-14
	627 628	81 2 19 81 2 19		40819	71 71	40748 40404	-213 -557	677 678				88 87	40917 41015	··44 54
* .	£29	81 2 19		40251	71	40180	-781	679	81 2 20	12:55		68	41194	233
	630	81 2 19		40809	74	40735	-326	£30	81 2 20		40797	85	40912	-47
	631 632	81 2 19 81 2 19		40877 40217	. 25 77	40902 40140	-32i	. 163 223	81 2 20 81 2 20		40882	85 84	40797 40937	-164 -24
	633	81 2 19		40453	92	40376	-585	683				84	41017	56
		81 2 19			83	40530	-43i	684			40635	83	40552	-469
	535 636	81 2 19 81 2 19		40713 40370	85 85	40628 40285	-333 -676	283 383			40831 40468	83 83	40748 40385	-2i3 -576
	637	81 2 19		40130	84	40046	-7i5	487			40945	83	40862	59
		81 2 19			84	39739	1222	<b>6</b> 88				82	40976	9
		81 2 17 81 2 19			84 84	39821 37906	-1140 -3055		91 2 20 81 2 20			82 80	40959 40889	−2 -72
	541	81 2 19	11:50	39715	83	39632	-1329		3i 2 20			80	40811	-i50
		81 2 19			83	40466	-495		81 2 20			79	40758	-203
		81 2 19 81 2 19			84 85	40685 40685	-275 -276		81 2 20 81 2 20			79 79	40209 40746	-152 -215
		81 2 19			85	40580	-381		81 2 20			79	41194	233
		81 2 19			84	40893	~68		81 2 20			78	40966	5
		81 2 19 31 2 19			84 84	40718 40757	-243 -264		81 2 20 81 2 20			76 74	41007 40636	46 -325
		81 2 19			83	40613	-348		81 2 20			73	40848	-113
	650	81 2 19	12:10	40730	83	40647	-314	700	81 2 20	14:14	40932	72	40860	-101
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	701	81 2 20			71	40788	-173	751	81 2 21			58	40139	-822
	702	81 5 50		41079	70	41009	48	752	81 2 21		40920	60	40860	-101
	703	81 2 20		40938	70	40868	-93	753	81 2 21		40049	61	39988	-973
	704	81 2 20			70	41421	460	754	87 5 57		4106B	16	41007	46
	705	81 2 20		41683	70	41613	625	4 7 4 74	81 2 21			61	41057	96
	706	81 2 20			70	40715	-246	756	81 5 51			60	40810	-151
	707			40398	74	40324	-537	757	81 2 21			60	40798	-163
	708	81 2 20	14:39	41122	76	41046	85	758	81 2 21	11:16	40861	60	40800	-161
	709	81 2 20	14:44	41238	75	41163	202	759	81 2 21	11:18	41017	60	48957	-4
	710	81 2 20	14:45	41438	75	41363	402	760	81 2 21	11:23	40970	60	40710	-51
	711	81 2 20		40779	73	40706	-255	761	81 2 21	11:26	41040	68	40780	19
the second	712	81 2 20	14:51	40900	71	40829	-132	762	81 2 21	11:37	41277	61	41216	255
4	713	81 2 20	14:55	40911	69	40842	-119	763	81 2 21	11:38	41142	61	41081	120
	714	81 2 20	15:00	41274	67	41207	246	764	81 2 21	11:45	41187	60	4i126	165
	715	Bi 2 20	15:01	41157	66	41091	130	765	81 2 21	11:49	41304	61	41243	282
	716	81 2 20	15:05	40936	64	46872	-89	766	81 2 21	11:52	41146	61	41085	124
	717	81 2 20	<b>i</b> 5 i0	40874	63	40811	-159	757	81 2 21	13:55	40740	40	40960	-61
	718	81 2 20	15/12	40707	62	40847	1:4	769	81 2 21	14 00	49829	37	40796	-i7i
	719	81 2 20	15:15	41164	61	41103	142	769	61 2 21	14:65	41232	36	41196	235
: .	726	81 2 20	15:20	40126	59	40057	-874	770	81 2 21	14:10	41393	33	41360	399
Section 1	721	81 2 20	15.29	41004	56	41943	-13	771	81 2 21	14:11	41132	33	41699	138
G 11 G 4	722	81 2 20	15:33	40807	53	40754	-267	772	81 2 21	14 20	41176	27	41143	:82
	723	31 2 20	15:35	40934	. 25	40932	-27	773	81 2 21	14:25	- 41114	26	41088	127
	724	81 2 20	15:40	41070	50	41020	59	774	81 2 21	14.29	41031	24	41007	46
	725	81 2 21	08:43	40696	28	40667	-274	775	81 2 21	14:35	41037	21	41016	55
	726	81 2 21	08:47	40585	23	40557	-404	776	81 2 21	14 41	40778	26	40758	~203
	727	81 2 21		41975	53	41545	985	777	81 2 21	14 44	41223	19	41204	243
	728	81 2 21	08:55	40576	23	40542	-419	778	81 2 21	14 50	40812	17	40795	-166
	729	81 2 21	200		30	49839	-122		81 2 21			16	40765	-176
	730	81 2 21			32	41147	186	780	81 2 23			24	41086	:25
882	731	81 2 21	09:14	41206	34	41172	211	761	61 2 23	09:09	41084	25	41059	78
14	732	81 2 21	09:20	41097	36	41061	:09		81 2 23			25	41462	S01
:	733	8i 2 2i			37	40994	33		81 2 23			25	41300	339
	734				39	41116	155	1	81 2 23		4.0	25	41047	88
	735	8i 2 2i			49	41032	71		Si 2 23			26	41069	108
	736	81 2 21		41113	40	41073	112	4.7	81 2 23		The second of the second	26	41226	259
	737	81 2 21		41050	42	41008	47		81 2 23		1 44 5	27	41352	491
	738	81 2 21	F 45 F 4		43	40712	-249		81 2 23			28	41328	367
	739	61 2 21		55 ( )	45	40877	-84		81 2 23			29	41362	401
11:	740	81 2 21	7.71	40712	47	40665	-296	776	81 2 23	44 4 7 7 4	5 SE SE	30	41284	323
	741	81 2 21		40806	47	10759	-202	791	81 2 23			31	41130	169
	742	81 2 21		and the second of the	48	40786	25	•	81 2 23		40923	31	40892	-50
	743	81 2 21			50	40758	203	793	81 2 23		40976	34	40942	-19
	744	81 2 21			52	40652	-309	794	81 2 23			35	40792	-169
	745	81 2 21		100	53	40521	-440		81 2 23		40763	36	40727	-234
\$100 B	746	81 2 21	A CONTRACTOR	and the second	54	40595	-366		81 2 23	1 1 1 1 1 1 1	40616	38	40578	-393
		81 2 21			55	40906	-55		81 2 23			39	40547	-414
	748				ร์ร์	40731	-230		81 2 23			40	40266	-695
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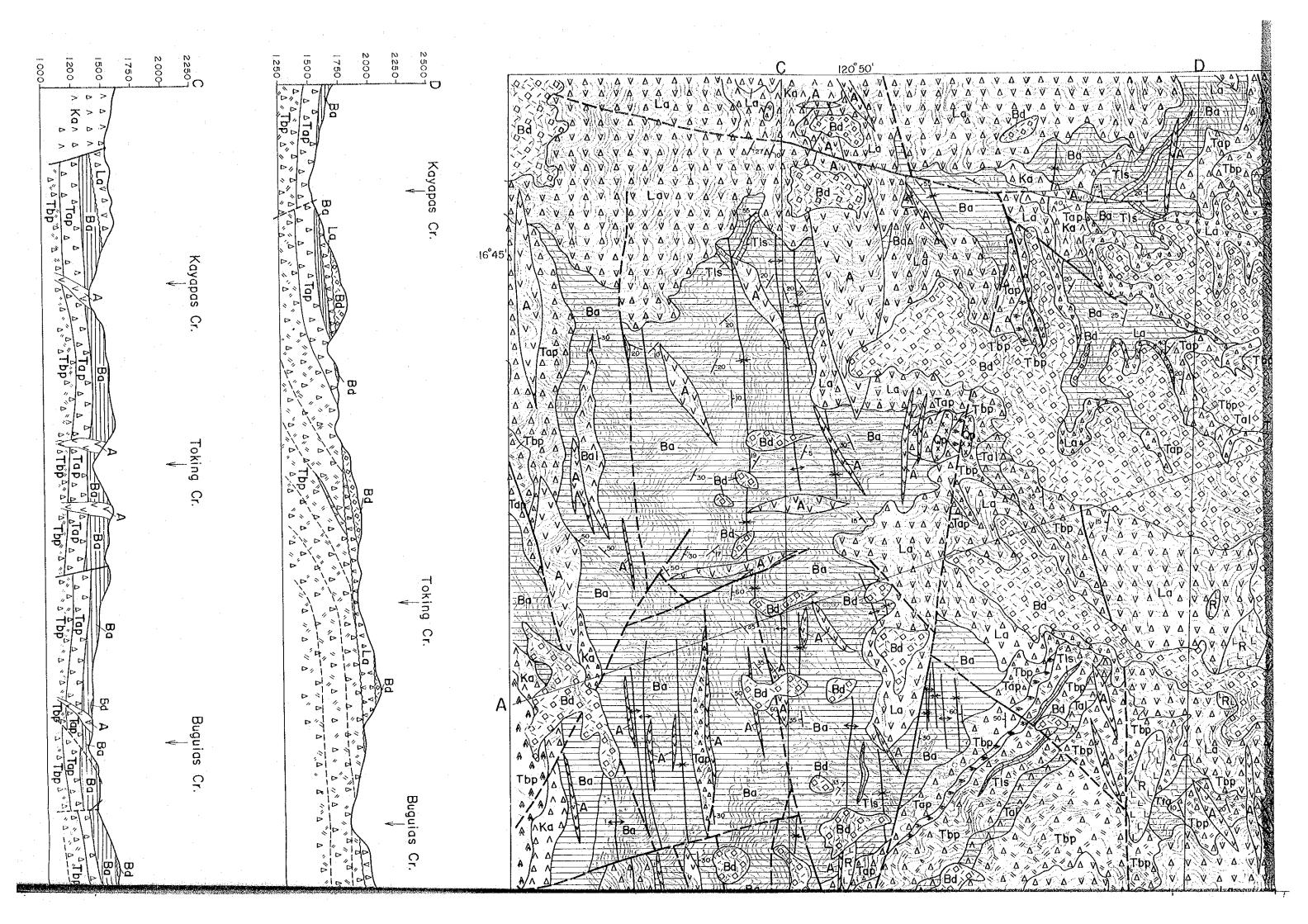
850 81 2 24 10:59

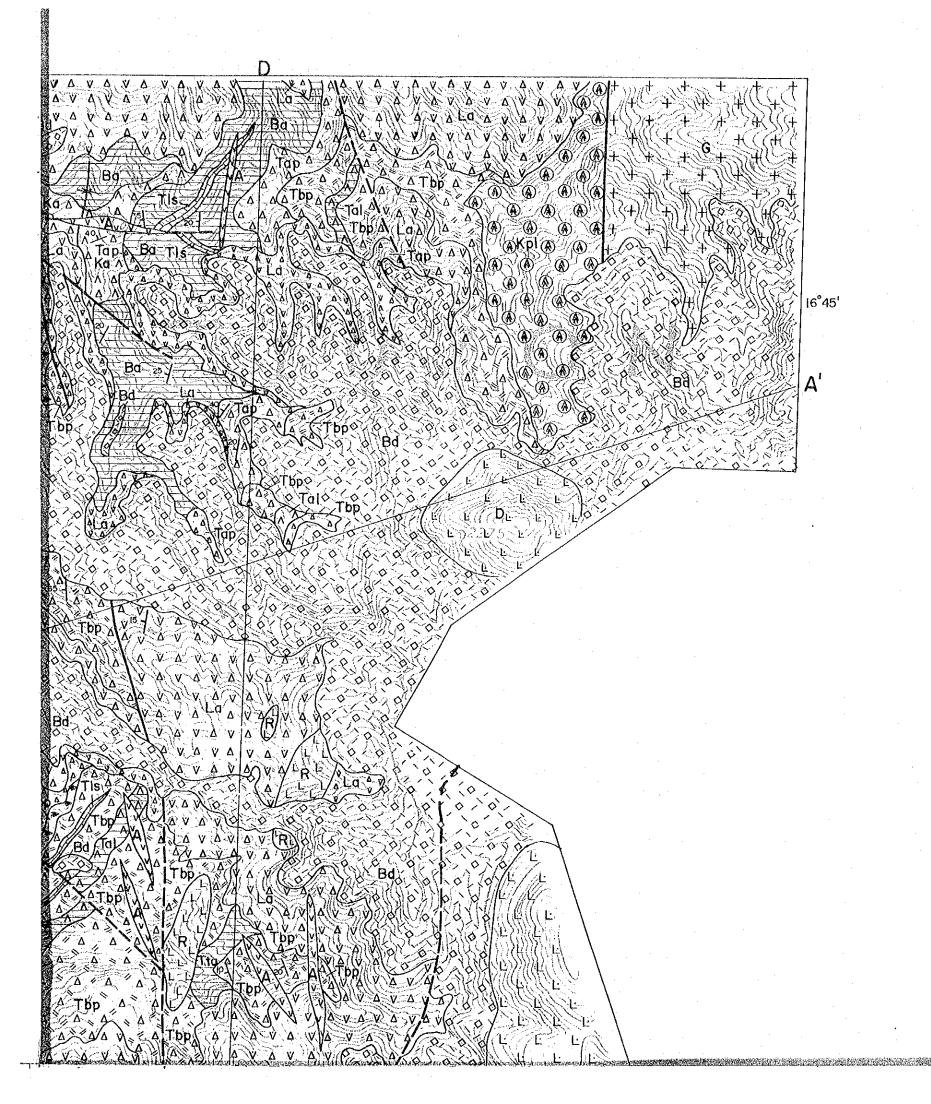
-104

900 31 2 27 11:07

-215

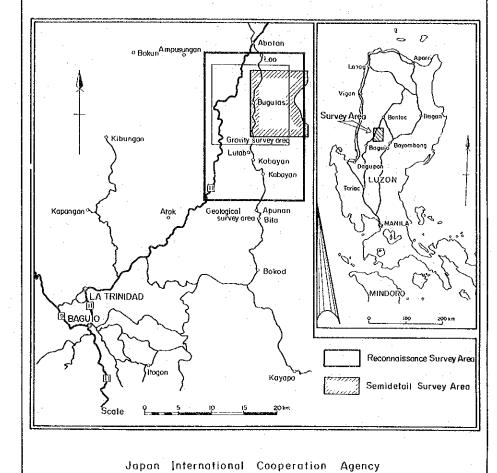
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	7.4	81	2 27	13:42	41246	-7	41253	292	764	81 3	3 15:09	40991	7	40984	23
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	919	81	2 27	14:10	42136	-1i	42147	1186	969	81 3	3 15:32	40936	4	40932	-29
	926	81	3 3	69:00	40968	- <b>i</b>	46969	8			4 08:45		-4	41322	351
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	924	81	3 3	69:21	41001	8	40993	32	974	81 3	4 07:00	The second secon	-û	40553	-398
	925	.81	3 3	09:25	40850	1.0	40791	-170	975	<b>81</b> 3			0	40668	-293
	926	81	3 3	69:27	40570	9	40661	-300	976	81 3	4 89:65	and the second second	i	40315	-146
1	727	81	3 · 3	09:30	40948	10	40738	-23	977	8i 3	4 09:08		i	40641	-526
	978	81	3: 3	09:34	40759	11	40748	-213	978	81 3	4 69:10		1	40616	-345
	929	ខ្ម	3 3	17:35	40751	12	40739	-222	979	81 3	4 09-14		2	40860	-101
	930	81	3 3	09:41	40561	13	40548	-413	930	81 3	4 09:17	and the second of	3	40972	-89
1	931	31	3 3	09:45	40768	14	40952	- 5	159		4 89:28		5	40827	- 434
ej i to	952	iS	3 3	69:47	40725	15	40719	-251	982		4 67:33		5	41636	75
	973	81	3 3	09:53	40695	16	40679	-282	783		4 09:37	And the second	7	40952	-5
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	935	81	3 3	10:00	40671	18	40653	-308			4 09 50		8	40655	-306
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	937	81	3 3	10:08	41089	20	41069	108	987		4 10:00		8	407:0	-251
1	578	13		13:39	40945	17	4û928	-33	988		4 10:04		9	40463	-626
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	941	81	. 3	13:47	41152	15	41147	186	11.1	31.3	4-10:27		10	46884	-77
		81			41368	15	41353	392			4 16:30		16	46951	-10
	943	13	3 3	13:55	41198	14	41184	223		81 3	4 10:34		16	46995	30
	744	31		13:56	41149	14	41135	174		81 3	4 10 40		11	40535	-426
	945	18	3 3	14:00	41033	13	41020	59	975	81 3	4 10 43		12	40547	-314
	946	31	3 3	14:02	41123	13	41110	147	996	4.0	4 10:45	A CONTRACTOR OF THE PARTY OF TH	13	40702	-259
				14 65	41033	13	41020	Sỹ			4 10:48		14	40509	-455
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	2.7				4.00	10 mg	1000	100							





Bugulas Geothermal Development Survey the Republic of the Philippines

Fig. II-1-6 Geological Map of Semidetail Survey



Scale (: 25,000 0 05 1.0 1.5 2.0 25<sup>km</sup>

