

2.4.2. Low-water Discharge

(1) General

In calculating the maximum and firm outputs and the annual energy generation for the project, the study of river discharge as well as available head which is determined by topographical conditions, one of the most important factors. To determine the riverflow at a certain catchment area, the following two methods are available: (1) using a record of discharges measured at that basin or within the same watershed; and (2) computing the discharge at the catchment basin involved from a record of precipitation measured at the watershed or observed at an adjacent gauging station. case data in a record of measured discharges, if available, covers only a short period of time or the accuracy is problematic, runoff analysis is also performed to assure the reliability. Depending on the type of power plant (reservoir, pondage, run-of-river), the kind of available hydrological materials, the interval of observation, etc., used discharges may be monthly average, 10-day average, 5-day, 24-hour, and so forth. For the case that annual regulation of the river discharge can be done in a large scale reservoir, monthly average or 10-day average discharge is applied. As for the Diduyon Damsite, low-water discharge should also be included in the study. Although the project is of reservoir type, the importance of low-water discharge cannot be neglected because it has the nature to govern the output and other characteristics of a power plant as well as the size of the reservoir, and also because there is no sufficient record of measured discharges in the vicinity of the watershed involved.

(2) Rainfall

There was no observation record of rainfalls in the watershed of the reservoir until the strat of the current feasibility study. According to the records taken at the meteorological stations around the watershed (most of them are at low altitude and 20 to 80 km apart from the damsite), the average annual rainfall varies from 600 mm to 2,800 mm, with a noticeably large record of 5,400 mm. There is no clear distinction of wet and dry seasons in the watershed of the Diduyon Reservoir, and even in a day when it is fine in the lowland vicinity there is sometimes considerable rainfall in the form of mist or showers in the highland watershed area. This will be explained by the topographic characteristics of the region, and most of the rainfall is caused by typhoons and tropical atmospheric pressures. The season of typhoons is from July to November, and heavy rainfall accompanied by thunder occurs in the same period of the year. Actual observation of maximum daily rainfall has just been commenced at the site. As stated above, the maximum daily precipitation ever recorded is 1,216 mm gauged in 1967 in Baguio located 100 km west of the Reservoir watershed. This record is helpful material to be incorporated in design computations on the Project Site. Fig. 2-4-8 shows the pattern of rainfall intensity of Baguio storms. In the course of this feasibility study, several precipitation gauge stations were set up in the direct watershed of the Project Site (see Fig. 2-4-12 and Table 2-4-6). Actual observations at the site will be useful to clarify the pattern and magnitude of precipitation in that region. Annual rainfall depth at Kamamasi in 1979, for example, is 3,256 mm as shown in Fig. 2-4-13. The daily rainfalls are listed in Table 2-4-7 (1) - (10) with illustrations in Fig. 2-4-14, while the monthly rainfalls are shown in Table 2-4-8. . A comparative chart of monthly precipitation for 1979 is presented in Fig.2-4-15. A maximum daily rainfall of 538 mm was observed at Gayan (Alayan), and a maximum monthly precipitation of 1,426 mm was recorded at Kasibu (October, 1978).

(3) Riverflow

Until the start of this feasibility study, there was no riverflow observation record of the Diduyon River, except the measurement at the Aglipay Gauging Station in the watershed of the Addalam River

on the lower reaches of the Diduyon River. Then, it was concluded that this survey should include actual observation of riverflow in the watershed of the proposed damsite. After consultation between JICA and NAPOCOR, it was agreed upon that NAPOCOR would assume charge of setting up gauging stations and processing collected data. The locations of the stream gauging stations are shown in Fig.2-4-12. Figs.2-4-16 and 2-4-17, and Table 2-4-9 show the stage discharge curve, measured river stage, and a table of sectional discharges, respectively.

(4) Evapotranspiration

i) Method of calculating evapotranspiration

On the proposed damsite, no data is available for use in the analysis of low-water runoff (calculation of daily discharge). The amount of evapotranspiration at the watershed of a natural river depends on a combination of various factors inherent to that basin, including earth covering, surface soil, topographical and geological features, and meteorological conditions such as insolation, temperature, humidity and wind velocity. Condensation must also be taken into consideration. Accordingly, it is not easy to accurately determine the amount of evapotranspiration. However, since the estimate of this amount is yet indispensable in the study of reservoir design, the following method, which seems practically appropriate, was employed for calculation.

The method of calculation is based on Thornthwaite's formula.

$$E_{p} = 0.533D_{o}(10tj/J)^{a}$$

$$a = 0.000000678J^{3} - J0.0000771J^{2} + 0.01792J + 0.49236$$

$$J = \sum_{j=1}^{12} (tj/5)^{1.514}$$

Where, $E_{\rm p}$: Monthly average evapotranspiration (mm/day)

Do : Daylight hours (12 hrs/day)

tj : Average monthly temperature for j month (°C)

ii) Dailight hours

At and around the latitude of 16° for the Diduyon region, the following correction numbers are adopted for daylight hours D_0 (12 hrs/day).

Month	Jan.	Feb.	Mar.	Apr.	May	June
Do	0.94	0.965	0.998	1.035	1.065	1.077
Month	Jul.	Aug.	Sep.	Oct.	Nov.	Dec.
Do	1.075	1.05	1.01	0.98	0.95	0.93

iii) Temperature

There was no record of temperature measurement for the Diduyon region until the start of this survey. Since observation has just been commenced during the feasibility study, data collected so far is not sufficient. Accordingly, the temperatures for the watershed of the Diduyon Reservoir are based on the measurement of annual temperatures at Magat (EL 250 m), 60 km north of the proposed site. With possible temperature drops due to the difference in the altitudes of both places taken into consideration, the following values are employed for the Diduyon Damsite.

Month	Jan.	Feb.	Mar.	Apr.	Мау	June		
Magat	21.3	21	22.3	26.2	27.3	27.3	Total	Mean
Diduyon	17.8	17.5	18.8	22.7	23.8	23.8	10001	lican
Month	Jul.	Aug.	Sep.	Oct.	Nov.	Dec.		}
Magat	27	26.4	24.9	24.5	23.3	21.7	293.2	24.4
Diduyon	23.5	22.9	21.4	21	19.8	18.2	251.2	20.9

iv) Conclusion

As a result of the study using the above values, evapotranspiration is estimated at 964 mm annually, with a monthly average of 80.3 mm. The values in the table hereunder are evapotranspiration for each month developed based on the measurements in the Magat region.

Month	Jan.	Feb.	Mar.	Apr.	May	Jun.		
Ev.Tr-n	62.4	68.6	94.9	112.5	113.9	88.1	Total	Mean
Month	Jul.	Aug.	Sep.	Oct.	Nov.	Dec.		
Ev.Tr-n	86.8	76.3	76.2	73.8	56.3	53.8	963.6	80.3

As the evapotranspiration for the Diduyon Reservoir, a daily average is obtained by 963.6 mm/365 day = 2.6 mm/day. From this value, a daily evapotranspiration of 3 mm is estimated for a day without precipitation, and this amount will be incorporated in the reservoir design.

V) Runoff analysis

(1) Outline of the tank model method

The tank model method is one of the techniques for runoff analysis, with which the runoff of a subject spot is calculated from a known amount of precipitation in the vicinity. This method can be used for both the computation of flood waveform for a short period and long-term low-water analysis. In the tank model method, a river basin is substituted by several model containers to simulate the runoff mechanism. Normally, the model consists of three to four tanks vertically arrayed in series as illustrated. The opening in the right side of each tank represents the hole for runoff, while that in the bottom is for infiltration. Rain water is poured into the uppermost container of the tank model, and the second and lower tanks receive the water from the upper tank through the infiltration hole. Part of the rain water escapes from each container through the runoff hole in the side, while the rest goes down to the lower tanks.

The river flow is the sum of discharge from the side hole of each container. Suppose the runoff qn (t) and the amount of infiltration Pn (t), then

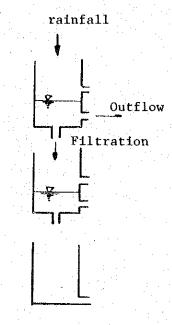
$$\begin{array}{l} qn\ (t) = 0\ \dots\ hn\ (t) \leq hn_1 \\ \\ \text{or, } qn\ (t) = \alpha n_1\ (hn\ (t) - hn_1)\ \dots\ hn_1 \leq hn\ (t) \leq hn_2, \\ \\ \text{or, } qn\ (t) = \alpha n_2\ (hn\ (t) - hn_2) + \alpha n_1\ (hn\ (t) - hn_1) \\ \\ \dots\ hn_2 \leq hn\ (t) - \dots \\ \\ \text{Pn}\ (t) = \beta n \cdot hn\ (t) - \dots \\ \\ \text{Pn}\ (t) - qn\ (t) - Pn\ (t) = \frac{dhn\ (t)}{dt} - \dots \\ \end{array}$$

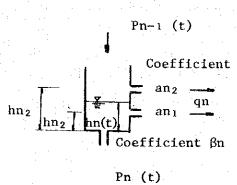
where n₁: Coefficient of runoff hole (Unit: 1/day)

n: Coefficient of infiltration hole (Unit: 1/day)

hn(t): Water depth of tank for t day (mm)

hn₁: Location of runoff hole (depth from the bottom, mm)

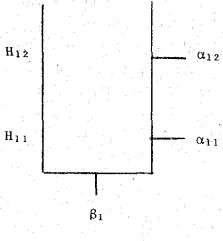




Accordingly, with the above equations (i), (ii), and (iii) set up simultaneously for each tank, $\sum_{n=1}^{n}q_n(t)$ and successively integrating, we obtain a riverflow. Though the creation of the tank model is intended to find out some constants including α , β , and h_1 , the non-linear nature precludes simple determination of these values. For this reason, it is necessary to use the method of trial and error in order to approximate the runoff qc(t) calculated with actual rainfall to the measured riverflow qo(t).

(2) Conclusion

For the purpose of runoff analysis, a 3-stage, storage-type model was created, as illustrated below.

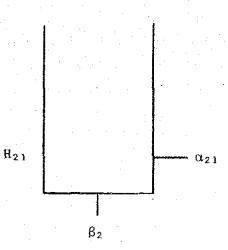


 α_{11} : 0.02

 α_{12} : 0.13

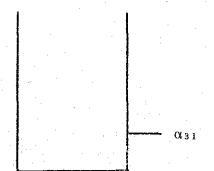
 α_{21} : 0.01

 α_{31} : 0.008



 β_1 : 0.22

 β_2 : 0.12



H₁₁ : 20

H₁₂ : 70

 H_{21} : 20

As the requirements to be met by a tank model for optimum solution, the rate of discharge, calculated by means of the above model from the precipitation recorded in the Kamamasi region with the riverflow of 1979 at Kamamasi used, must be well reproduced on the hydrograph waveform for low water period, and the mean value of the calcualted discharge during the period of calculation (1979) must equal to that of the measured discharges. Analytical study is conducted with emphasis placed on the above two conditions. As for the rainfall, examination was made for a correlation between the gauging stations located in the watershed. As shwon in Table 2-4-9 and 2-4-10, the values demonstrate a good correlation. Accordingly, together with the rate of riverflow, the rainfall measured at Kamamasi will be adopted. As evident from the hydrograph by calculation given in Fig. 2-4-17, the waveforms are adequately coincident with each other. The daily correlation coefficient between the calculated value and the measurement is 0.84, while the mean values are 30.9 m³/sec and 23.3 m³/sec for the computed and measured values, respectively. The calculated rate of discharge $30.9 \text{ m}^3/\text{sec}$ is nearly equal to the average dishcarge of 30.84 m³/sec described later.

Table 2-4-6 List of Gauging Stations Newly Established for the Diduyon Project

623m 645m 563m -do-	Name Meteorological Gauging Stations SIBU AA SIBU BAMASI CKET IGUEM)	16°18.96'N 121°17.50'E 16°18.92'N 121°17.64'E 16°15.95'N 121°25.35'E 16°18.64'N 121°25.35'E 16°18.64'N 121°20.25'E	Approx. El. 701m 685m 639m 653m 640m	Mear Mun. Hall, 500m MW of town hall 10m from weather obsr. house, fenced Beside observer's house, on top of tree At center of rice fields 5m NW from observer's house	Item of Observation Rainfall intensity - do do do -	Equipment/ Instruments g"W.B. STD Leopold Steven, Auto Rainfall, RFC g" W.B do do -	Twice daily Twice daily Twice daily Twice daily - do -	Start of Observation 7-29-1978 8-69-1978 7-19-1978 8-09-1978
16°15.84'N 563m Staff gauge 121°26.30'E support of auto. W.L. - dodo- river bank - do - W.L. recorder 16°28.62'N 95m Staff gauge 121°37.91'E 95m at river bank at river bank		121°24.30'E 16°15.70'N 121°27.26'E	623m 645m	server's house Near Consultant's bunk- house, 200m W of house	- do - Wind direction -velocity	SIAP Auto recorder	- do - Continuous	9-04-1978
Staff gauge alication 16°15.84'N 563m wooden frame support of auto. W.L. - dodo - river bank 16°28.62'N 95m Staff gauge - do - do - do - river bank 121°37.91'E Staff gauge at river bank - do - d	ations		·					
- dodo- river bank - do - W.L. recorder Continuous 16°28.62'N Staff gauge 121°37.91'E 95m at river bank - do - gauge Twice daily	~	16°15.84°N 121°26.30°E	563m	Staff gauge nailed to wooden frame support of auto. W.L.	Water level	Wooden staff gauge	Twice daily	7-20-1978
95m bolted to rock - do - Wooden staff Twice daily at river bank	щ	- op -	op			Leopold Auto W.L.recorder	Continuous	9-05-1979
		16°28.62'N 121°37.91'E	95п	Staff gauge bolted to rock at river bank			Twice daily	8-26-1979

Year 1978	78										(Unit: Ma	(10)
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15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0						0.43	8.0	26.0	20.0	50.0	4.1	6
15.6 12.0 25.0 58.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5			•			9	77.0	19.0	18.0	72.0	0.3	80
1 20.0 67.0 13.0 67.0 8.0 8.0 8.0 17.0 8.0 93.0 13.0 13.0 67.0 8.0 93.0 12.0 12.0 12.0 17.0 24.0 12.0 8.0 8.0 8.0 8.0 12.0 12.0 17.0 12.0 12.0 10.0 8.0 10.0 10.0 10.0 10.0 10.0 10.						15.0		23.0	25.0	58.0	5.0	5.2
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15.0 17.0 34.0 6.0 8.0 9.0 11.0 40.0 8.0 9.0 11.0 40.0 8.0 8.0 9.0 11.0 40.0 8.0 10.0 9.0 11.0 40.0 10.0 10.0 10.0 10.0 10.0 10	0.1					40.0	12.0	32.0	0.4	21.0	0	9
3.0 3.0 3.0 3.0 10.0 5.0 23.0 23.0 23.0 23.0 23.0 23.0 23.0 23.0 23.0 23.0 20.0 23.0 3.0								15.0	17.0	34.0	6.0	80
3.0 9.0 5.0 33.0 10.0 10.0 10.0 23.0 5.0 20.0 12.0 10.0 5.0 7.0 14.0 28.0 3.0 10.0 10.0 7.0 14.0 28.0 3.0 10.0 5.0 10.0 10.0 3.0 15.0 18.0 9.0 10.0 13.0 27.0 28.0 3.0 40.0 10.0 10.0 30.0 28.0 3.0 40.0 10.0 10.0 11.2 40.0 12.0 12.0 40.0 11.2 40.0 11.2 5.0 12.0 12.0 40.0 11.0 6.0 10.4 5.0 10.0 10.0 11.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0		-				•		0.6	11.0	0.03	0.8	9.6
10.0 5.0 27.0 37.0 12.0 5.0 5.0 23.0 5.0 20.0 5.0 10.0 10.0 3.0 3.0 60.0 5.0 10.0 10.0 3.0 15.0 15.0 18.0 10.0 12.0 15.0 28.0 3.0 40.0 12.0 40.0 12.0 40.0 12.0 12.0 40.0 12.0 50.0 15.0 6.0 13.5 8.0 10.0 10.0 11.0 11.0 10.4 5.0 8.0 10.0 13.0 20.0 11.0 11.0 5.0 8.0 10.0 13.0 20.0 11.0 5.0 8.0 6.0 10.0 10.0 5.0 5.0 8.0 46.0 10.0 10.0 11.0 5.0 8.0 10.0 13.0 20.0 11.0 6.0 8.0 6.0 6.0 6.0 6.0 8.0 46.0 11.0 6.0 6.0 8.0 46.0 11.0 6.0 6.0 8.0 6.0 6.0 6.0 6.0 8.0 4		0.0				:		0.6	5.0	33.0	10.0	6
10.0 10.0 23.0 5.0 20.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0 5.0	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \							5.0	27.0	37.0	12.0	
10.0 10.0 10.0 10.0 10.0 10.0 10.0 10.0								33.0		35.0	0.6	
10.0 5.0 7.0 14.0 28.0 3.0 3.0 3.0 10.0 10.0 10.0 3.0 3.0 3.0 3.0 15.0 15.0 15.0 13.0 13.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15					10.0			23.0	5.0	20.0		
10.0 10.0 3.0 3.0 3.0 13.0 13.0 15.0 10.0 3.0 3.0 3.0 15.0 3.0 15.0 3.0 15.0 15.0 15.0 15.0 15.0 15.0 15.0 15					5.0			7.0	14.0	28.0		
60.0 3.0 15.0 18.0 15.0 18.0 15.0 18.0 15.0 18.0 27.0 3.0 40.0 12.0 16.0 12.0 16.0 12.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0 16.0 11.0		10.0	•		10.0				10.0	10.0	3.0	
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3.0			30.0	28.0		3.0	0.04			7.0	12.4	
40.0 12.0 14.0 12.0 14.0 12.0 5.0 10.0 8.0 10.0 10.0 11.0 10.0 13.0 10.0 11.0 10.0 13.0 20.0 10.0 10.0 11.0 10.0 11.0 5.0 11.0 10.0 13.0 20.0 11.0 6.0 6.0 6.0 6.0 50.0 248.5 110				35.0		٥. ن			-	10.0	12.2	
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5.0 10.0 10.0 11.0 61.0 16.4 9 8.0 10.0 10.0 11.0 61.0 10.4 5 2 8.0 10.0 10.0 21.0 5.0 5.0 2 5.0 10.0 13.0 20.0 11.0 6.0 4 46.0 64.0 205.0 58.0 422.0 323.0 357.0 350.0 698.0 248.5 110						14.0				0.9	13.5	m
5.0 10.0 8.0 10.0 10.0 11.0 61.0 10.4 5 7.0 21.0 8.0 8.0 7.0 5.0 10.0 11.0 11.0 11.0 5.0 11.0 11.0					20.0	12.0	50.0	15.0	61.0		76.4	9.
5.0 8.0 7.0 7.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 7.0 8.0 8.0 7.0 8.0 8.0 7.0 8.0 10.0 11.0 13.0 10.0 11.0 11.0 11.0 8.0 6.0 6.0 6.0 64.0 205.0 58.0 422.0 323.0 357.0 350.0 698.0 248.5		•		. * *		3.0	10.0	11.0	61.0		10.4	រភា
8.0 10.0 11.0 5.0 11.0 5.0 11.0 5.0 11.0 5.0 11.0 11		5.0					14.0		8.0		7.0	
2 5.0 10.0 13.0 20.0 11.0 6.0 6.0 6.0 6.0 6.0 64.0 205.0 58.0 422.0 323.0 357.0 350.0 698.0 248.5		8.0	10.0			10.0	21.0		11.0		5.0	
3.0 10.0 6.0 6.0 64.0 205.0 58.0 422.0 323.0 357.0 350.0 698.0 248.5	0.5		5.0			10.0	13.0	20.0			11.0	
6.0 4 46.0 64.0 205.0 58.0 422.0 323.0 357.0 359.0 698.0 248.5						- :	3.0	10.0		\$.	0.9	1
4 46.0 64.0 205.0 58.0 422.0 323.0 357.0 350.0 698.0 248.5		·			•			0.9				
	4.0	0.94	64.0	205.0	58.0	422.0	323.0	357.0	350.0	0.869	248.5	110.
		•	?)) }) 	,			•	7,017	•

Table 2-4-7(3) Daily Rainfall at Kamamasi

. 1											~	<u> </u>												••••								••••			
	DEC.	10.80	2.60	8.00	34.80	1.40	5.20	9.60	0	0	20.00	41.60	10.80	21.00	24.60		4.60	0	15.00	20.20	19.60	24.80	18.60	24.00	23.80	19.80	ø	3.20	04.40	3.40	5-60	6.60	201 20) 1 1 1	
	NOV.	101.20	09.06	65.20	12.20	1.00	4.80	16.20	2.00	0	Φ	0	0	17.60	0	1.00	0	10.20	11.60	20.20	15.20	21.20	23.40	0	0	6.20	Z . 80	1.00	2.39	24.40	0		00.077	449.00	
	OCT.	5.60	9.00	00.6	0	3.60	8.20	12.20	57.80	108.00	62.00	13.20	0	0	0	8.20	19.40	4.00	36.80	20.80	22.20	8.00	3.20	43.40	3.20	30.60	100.40	52.20	0	51.20	86:00	100.80	0	00.4/8	
	SEP.	2.00	1.20	51.40	6.40	1.60	39.60	0	43.60	45.40	9.60	2.40	0	13.40	17.20	1.20	8.00	112.20	63.20	38.80	5.80	28.00	20.60	69.60	16.40	24.00	9.80	136.00	124.20	16.80	5.60	:		7.4.00	
	AUG.	t	ı	.	ŀ		. 1	•	4	9.90	16.80	3.40	2.20	8.40	8.60	4.40	0	0	0	5.40	30.20	11.20	13.40	68.40	52.80	33.60	2.60	0	1.40	1.60	7.20	4.40	6	262.00	
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	3.0	÷	12.2			24.0	7.2		5.0	71.6	7.4	18.4
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87	4	2.4		0.9			5.2		10.2		0.0	
19	1.2			18.2					27.0	•	23.4	12.0
20	0.0			31.8			2.0	·.	3.6	4.0	70.6	2.0
21				14.0			4.		3.6	16.4	61.6	0.
22	٠			3.0		21.6			2.4	11.6	26.0	21.8
23						13.0				7.0	18.0	21.6
24			51.2		51.0		7.0			15.6	42.4	7.67
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TOTAL	45.8	25.8	0.69	114.2	241.6	315.2	283.6	83.4	4.44.4	470.0	871.2	307.8

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9 31.0 67.2 5.0 10.2 2.4 11.2 0 10.2 15.6 1.4 4.0 6 5.0 42.0 1.0 15.0 6.2 7.0 2.2 10.4 17.6	©			٦, ٥		œ				8.2	15.2	19.0
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12.6 2.4 11.2 0 10.2 1.4 4.0 6 5.0 42.6 1.0 15.0 6.2 0 2.2 10.4 17.6 0 23.8	0		•						•	2.2	40.0	30.6
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6 5.0 42.6 1.0 15.0 6.2 18.2 2.2 10.4 17.6 0 2.2 23.8	0	10.2						1.4	•		15.0	8
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23.8	17.0							10.4			18.8	
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32 8 87 6 242.8 242.8 100.4 354.6 269.	30.8	4	44.2	,	228.6	24.2.8		100.4	354.6	269.0	450.2	221.6

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DAY	JAN.	FEB.	MAR.	APR.	MAY	JUNE	JULY	AUG.	SEP.	OCT.	NOV.	DEC.
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13	i	1	i	. 1	,	,	,	ı	20.00	24.80		6.20
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13		i	i	•			ı	,	11.20	0	4.30	17.90
91		· i	. 1	•		- 1	í	ı	57.00	8.40	10.50	20.00
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18		1	J		1		ı	1	42.40	3.70	13.70	17.90
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20	ı,		1	ļ		ı	ì	1	0	73.20	6.50	0
77		ı	•		i	i	•	3	3.80	42.40	12.80	0
22	. 1	ł	1	•		ł	1	•	37.40	65.00	10.70	0
23	1	1	i	1	Í.	i	•	1	53.60	61.72	13.00	0
24	•	•	i	i	ŧ	•	1	3	0	69.50	8.40	3.00
25	•		1	1	1	1	ŧ	1	57.8	72.91	5.50	6.40
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27	1	1	ı	ı	•	į	ŧ	1	34.60	101.24	6	6.10
28	ı		•	1	1	i	1		5.80	71.21	6.00	0
29	•		ì	1	\$	•	1	3	8.40	38.80	5.20	0
8	ı		i	i	1	ş	•	1	1.60	14.10	10.40	0
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TOTAL	•	1 -	ı	ŧ	i	. 1	. ·	•	512.80	1190.30	237.20	198.10

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SEPT.	.	6/4	*. *.	10.2	3.0	0	0	0	0	æ. €.	4.4	4.0	0	6.2	4.1	4.2	Ø.	4.2	6.3	12.5	8	3.0	2.0	0	0	0	0	50.4	0	0	0			271.8
AUG.		0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	4.2	6.3	2.0		1	TZ.5
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(Alayan)		Biyoy	(Kasibu)	Siguem	Paguet
i	ı	ı	0.1	ı	l
262.0	275.0	1	336.6	294.8	1
1	653.6	512.8	550.2	799.2	1
879.8	1404.0	1190.3	1426.3	968.4	_
449.0	352.6	237.2	238.5	128.0	
391.2	311.2	198.1	180.5	337.2	1
1982.0	2996.4	2138.4	2732.2	2527.6	
495.5	599.3	534.6	455.4	505.5	
45.8	32.8	0.0	7.0	-	1
25.8	47.4	75.3	46.0		13.0
0.69	44.2	0.0	0.49		0.69
114.2	247.6	15.8	205.0	•	98.0
241.6	228.6	51.5	58.0	-	165.0
315.2	242.8	674.7	422.0	•	302.0
283.6	1	152.1	323.0	•	358.0
83.4	100.4	12.5	357.0	1	144.0
444.4	354.6	227.8	350.0	_	373.0
470.0	269.0	114.1	698.0	_	206.0
871,2	450.2	258.0	248.5	l	292.8
307.8	221.6	33.9	110.6	•	157.0
3332.0	2239.2	1615.7	2882.5	1	2177.8
277.67	203.56	134.64	240.21	ı	197.98

Tabulation of Daily Water Level and Discharge at Kamamasi Table 2-4-9

1979

Drainage area at gaging station 462 Sq. Kms.

Day	January February	March	April	May	June	July	August	September	October	November	Decembe	er II	Day
1	22.46 1.00 14.00 0.7	2 11.28 0.62 1	13.16 0.69	16.00 0.79	16.80 0.82	22.14 0.99	31.34 1.26	22.79 1.01	37.22 1.42	23.77 1.04	43.41	1.58	1
2	21.82 0.98 13.72 0.7	1 11.55 0.63 1	12.89 0.68	14.84 0.75	19.61 0.91	20.55 0.94	25.10 1.08	33.51 1.32	67.65 2.15	24.10 1.05	44.20	1.60	2
3	21.50 0.97 13.44 0.7	0 11.55 0.63 1	12.62 0.67	13.72 0.71	27.13 1.14	33.51 1.32	23.44 1.03	29.56 1.21	73.15 2.27	26.11 1.11	42.23	1.55	3
4	21.18 0.96 13.16 0.6	9 8.52 0.51 1	12.62 0.67	14.28 0.73	28.51 1.16	37.22 1.42	34.24 1.34	24.76 1.07	78.31 2.38	22.79 1.01	39.51	1.48	4
5	20.86 0.95 12.89 0.6	8 10.51 0.59 1	12.62 0.67	14.00 0.72	24.76 1.07	28.51 1.18	29.21 1.20	27.86 1.16	62.28 2.03	24.10 1.05	37.22	1.42	5
6	20.55 0.94 12.62 0.6	7 10.51 0.59 1	12.62 0.67	13.72 0.71	20.86 0. 9 5	24.10 1.05	25.43 1.09	26.11 1.11	50.71 1.76	33.14 1.31	35.72	1.38	6
7	20.23 0.93 12.62 0.6	7 10.25 0.58 1	12.89 0.68	13.44 0.70	18.99 0.89	25.10 1.08	25.43 1.09	27.47 1.15	44.60 1.61	34.24 1.34	36.85	1.41	7
8	19.92 0.92 12.62 0.6	7 10.00 0.57 1	12.62 0.67	13.16 0.69	23.11 1.02	35.72 1.38	23.44 1.03	23.44 1.03	40.67 1.51	29.91 1.22	45.00	1.62	8
9	19.30 0.90 12.89 0.6	8 9.75 0.56 1	12.62 0.67	12.89 0.68	36.85 1.41	28.51 1.18	28.16 1.17	24,43 1.06	37.98 1.44	29.21 1.20	39.51	1.48	9
10	18.99 0.89 12.62 0.6	7 9.50 0.55 1	12.35 0.66	12.89 0.68	37.60 1.43	24.10 1.05	29.21 1.20	26.79 1.13	35.72 1.38	27.13 1.14	38.36	1.45	10
11	18.69 0.88 12.35 0.6	6 9.25 0.54 1	12.08 0.65	12.62 0.67	27.13 1.14	22.79 1.01	27.13 1.14	26.11 1.11	34.98 1.36	27.47 1.15	36.10	1.39	11
12	18.38 0.87 12.08 0.6	5 9.25 0.54 1	12.08 0 .65	12.62 0.67	22.79 1.01	22.14 0.99	24.10 1.05	22.46 1.00	38.74 1.46	26.79 1.13	33.51	1.32	12
13	18.08 0.86 11.81 0.6	4 9.00 0.53 1	11.81 0.64	14.84 0.75	19.61 0.91	21.82 0.98	23.11 1.02	22.14 0.99	33.87 1.33	26.45 1.12	33.14	1.31	13
14	17.78 0.85 11.55 0.6	3 9.00 0.53	11.81 0.64	16.00 0.79	18.08 0. 8 6	25.43 1.09	22.14 0.99	22.46 1.00	22.46 1.00	32.78 1.30	32.78	1.30	14
15	17.48 0.84 12.08 0.6	5 8.76 0.52	12.08 0.65	16.00 0.79	19.61 0.91	29.56 1.21	20.86 0.95	25.43 1.09	26.79 1.13	38.36 1.45	32.05	1.28	15
16	17.18 0.83 12.08 0.6	5 13.72 0.71	12.08 0.65	17.18 0.83	17.78 0. 8 5	24.43 1.06	20.23 0.93	24.76 1.07	32.05 1.28	35.72 1.38	31.34	1.26	16
17	16.58 0.81 12.08 0.6	5 13.72 0.71	14.56 0.74	14.84 0.75	18,08 0.86	21.18 0.96	 	31.34 1.26	30.98 1.25	33.87 1.33	30.62	1.24	17
18	16.58 0.81 12.08 0.6	5 13.44 0.70 1	14.28 0.73	24.10 1.05	18.69 0.88	19.92 0.92		28.16 1.17	29.56 1.21	32.05 1.28	29.21	1.20	18
19	16.00 0.79 12.08 0.6	5 13.16 0.69	13.72 0.71	23.44 1.03	17.78 0. 8 5	19.30 0.90	 	·	28.86 1.19	35.72 1.38	29.56	1.21	19
20	16.58 0.81 11.55 0.6			18.08 0.86	16.88 0. 8 2	19.61 0.91	18.08 0.86	33.51 1.32	28.16 1.17	37.60 1.43		1.19	20
21	16.00 0.79 11.28 0.6		30.27 1.23	16.00 0.79	16.29 0. 8 0	25.77 1.10	17.78 0.85	28.51 1.18	28.51 1.18	39.12 1.47	28.86	1.19	21
22	15.42 0.77 11.02 0.6	1 13.72 0.71	21.50 0.97	14.84 0.75	15.71 0.78	21.82 0.98	17.18 0.83	25.43 1.09	28.16 1.17	35.72 1.38	29.91	1.22	22
23	14.84 0.75 10.76 0.6	0 13.72 0.71	33.87 1.33	14.00 0.72	27.47 1.15	19.30 0.90	16.88 0.82	27.47 1.15	27.47 1.15	36.47 1.40	30.98	1.25	23
24	14.56 0.74 10.51 0.5	9 17.18 0.83	22.46 1.00	14.28 0.73	20,86 0 ,9 5	18.38 0.87	16.58 0.81	26.11 1.11	28.51 1.18	37.22 1.42	33.87	1.33	24
25	14.28 0.73 10.25 0.5		13.90 0.90	33.87 1.33	19.61 0.91	18.38 0.87	•		28.16 1.17	37.98 1.44	36.85	1.41	25
26	14.00 0.72 10.00 0.5	7 17.48 0.84	16.58 0.81	26.11 1.11	21.50 0. 9 7	31.69 1.27		23.11 1.02	26.79 1.13	49.06 1.72	38, 36	1.45	26
27	13.72 0.71 10.00 0.5		15.42 0.77	20.86 0.95	23.77 1.04	45.80 1.64	 		26.11 1.11	47.83 1.69	39.89	1.49	27
28	13.16 0.69 10.00 0.5	7 14.28 0.73	15.42 0.77	18.38 0.87	28.86 1.19	35.35 1.37	18.38 0.87	32.78 1.30	25.77 1.10	45.80 1.64	41.44	1.53	28
29	13.16 0.69	11.02 0.61	29.21 1.20	17.18 0.83	26.11 1.11	27.47 1.15	17.18 0.83	34.61 1.35	25.77 1.10	43.41 1.58	39.51	1.48	29
30	13.16 0.69	13.44 0.70	18.38 0.87	17.78 0.85	21.50 0.97	25.10 1.08	20.23 0.93	36.10 1.39	25.10 1.08	43.01 1.57	14.61	1.35	30
31	13.16 0.69	13.16 0.69		16,00 0.79		25.77 1.10	18.99 0.89		24.10 1.05		33.14	1.31	31
Total	535.60 334.14			517.96	672.41	800.47	685.83	829.90	1,129.19	1,016.93	,106.6		•
Mean	17.28 11.93		15.79	16.71	22.41	25.82	22,12	27.66	36.43	33.90	35.70		
Max.	22.46 14.00		33.87	33.87	37.60	45.80	34.24	38.36	78.31	49.06	45.00		
Min.	13.16 10.00	8.52	11.81	12.62	15.71	18.38	16.29	22.14	22.46	22.79	28.86		

REMARKS:

Discharges based on rating curve, $Q = 22.46330825 h^{1.440225614}$

Discharge measurements from May 1979 to January 1980 were used to develop the rating curve.

Total 8,483.88

Mean 23.44

78.31 Max. Min. 8.52

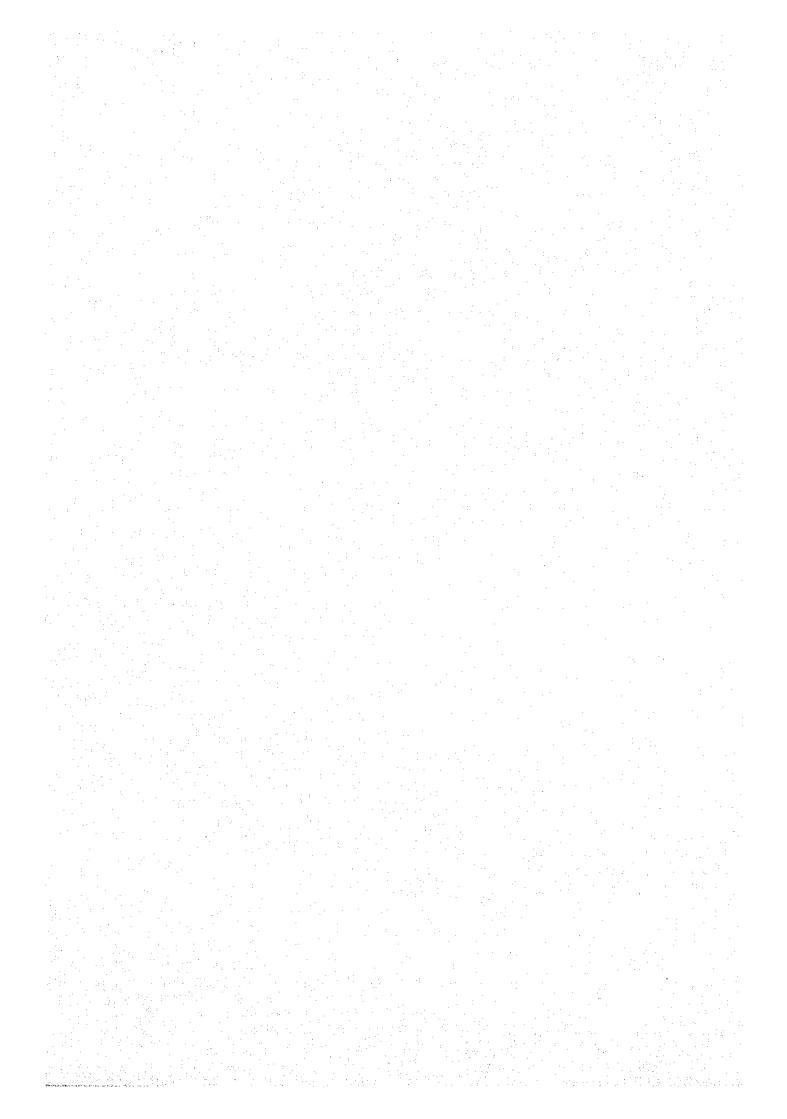


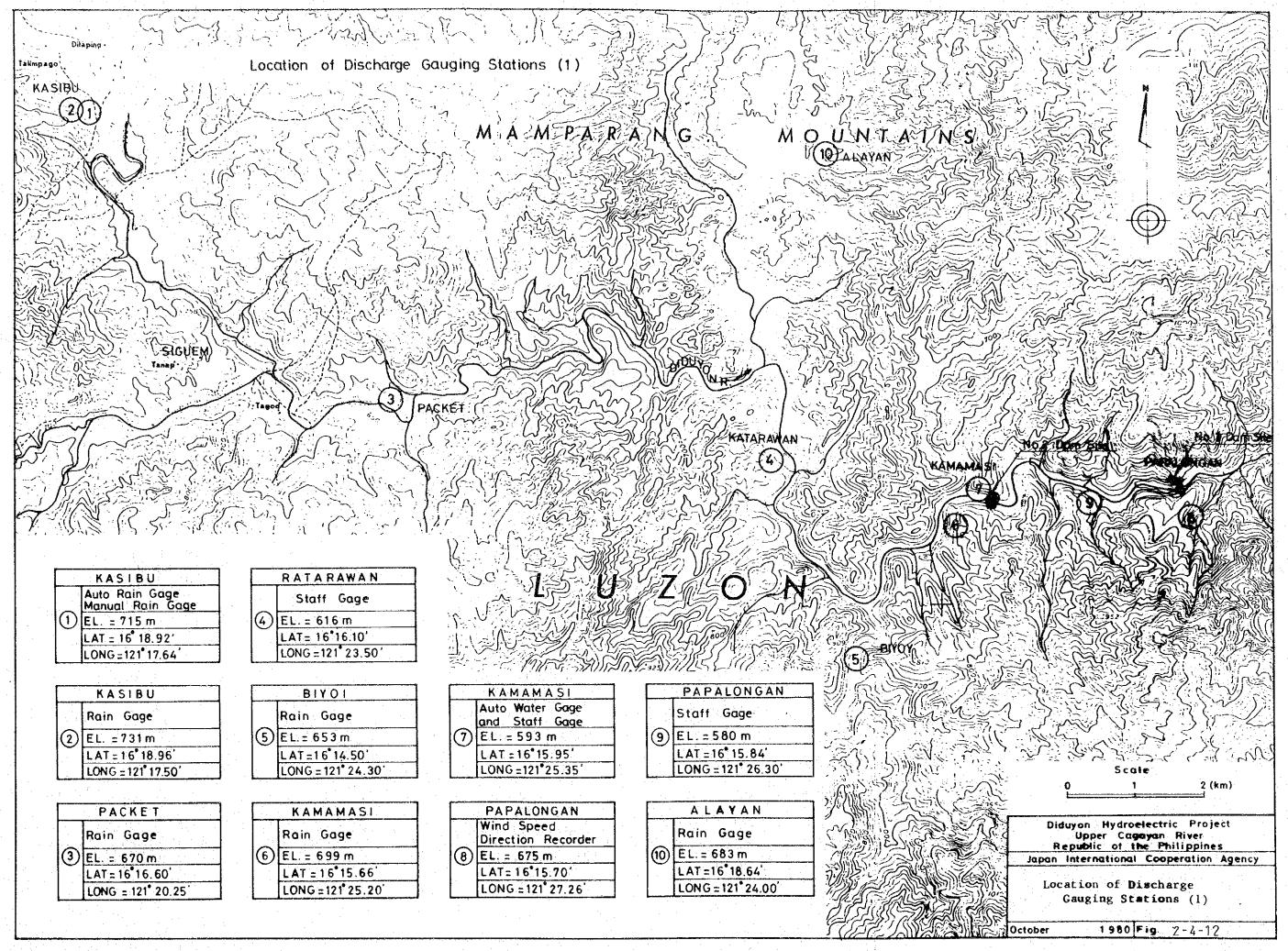
Table 2-4-10 Correlation of Daily Rainfall

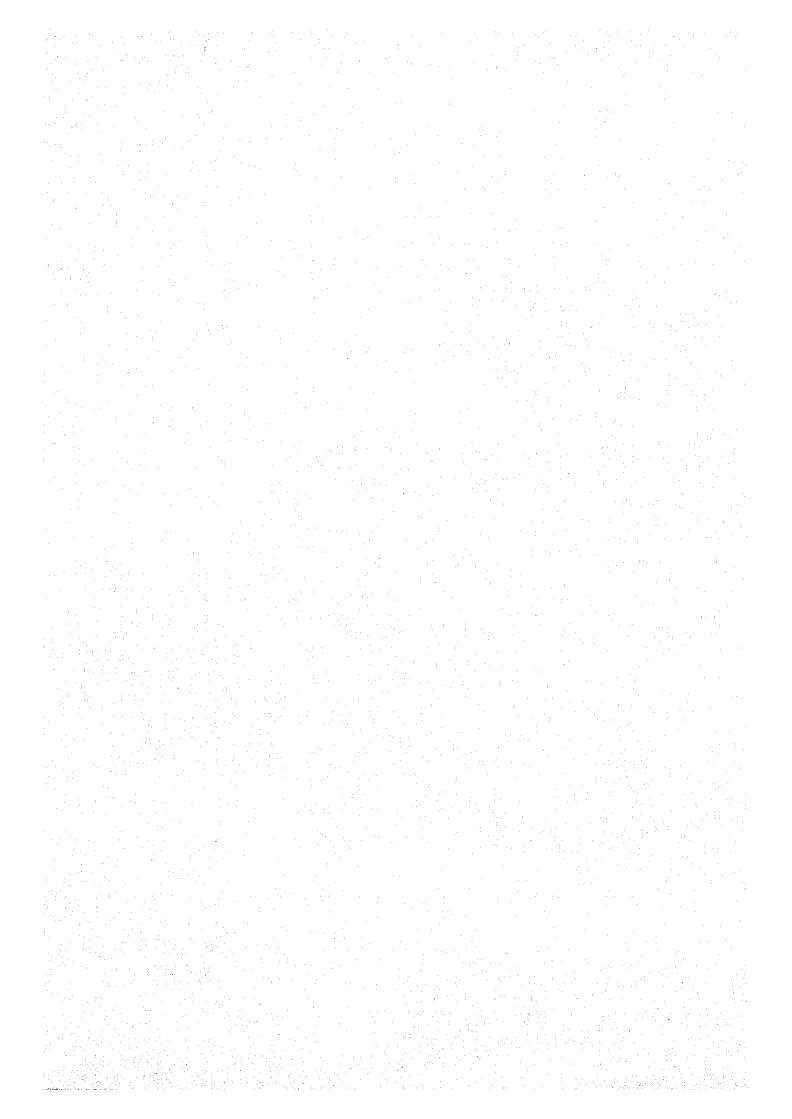
*						
/ ×	Kamamasi	Gayan Alayan	Biyoy	Poblacion Kasibu	Siguem	Paquet
Kumamasi		r=0.602 y=-0.775 +1.060x	r=0.289 y=5.087 +0.234x	r=0.536 y=4.912 +0.513x	r=0.647 y=1.351 +0.805x	r=0.445 y=3.470 +0.317x
Gayan	n=234		r=0.444 y=7.986 +0.213x	r=0.609 y=7.780 +0.350x	r=0.895 y=5.421 +0.594x	r=0.933 y=-0.532 +1.442x
Biyoy	n=484	n=209		r=0.434 y=6.988 +0.509x	r=0.406 y=7.756 +0.596x	r=0.0942 y=6.046 +0.0948x
Poblacion	n=510	n-234	n=484		r=0.604 y=3.308 +0.735x	r=0.238 y=4.841 +0.195x
Siguem	n=145	7 7∏=u	n=119	n=145		
Paquet	n=334	n=59	n=334	n=334		

Table 2-4-11

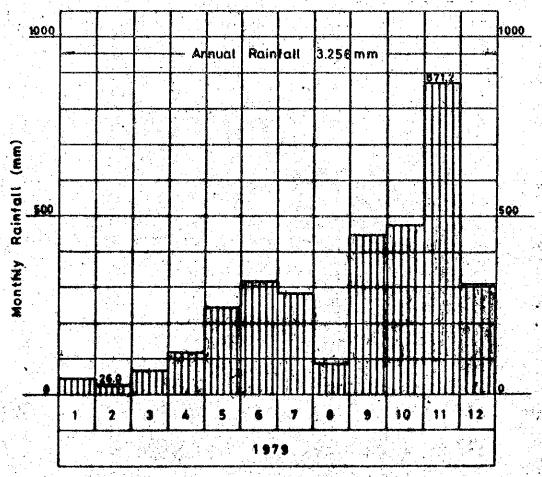
Correlation of Monthly Rainfall

y=25.62321 +0.70865x y=144.01553 +0.36741x +0.32596x y=102.38142 y=115.33820 +0.31542x r=0.81082 r=0.60156 r=0.52156 r=0.66263 Paquet y=-171.47540 +1.21811x y=164.05872 y=106.86182 +0.66523x +0.73726x +0.60217x y=176.48051 r=0.88482 r=0.87852 r=0.86400 r=0.85794 Siguem y=23.84888 +0.93781x Poblacion +0.88062x y=111.53108 +0.93058x y=27.34985 (Kasibu) r=0.88216 r=0.66344 r=0.84634 n=11 n#5 y=-53.961550 +0.81144x y=-42.10709 +0.85345x r=0.67992 r=0.88403 Biyoy 0=16 n=11 **7≖u** y=-19.30780 +0.98013x (Alayan) Geyan r=0.80171 n=15 91=u n#10 n=5 Kamamasi n=15 n=15 n*16 n=117110 Poblacion Kamamasi (Kasibu) (Alayan) Siguem Paquet Gayan Biyoy





Monthly Rainfall Record at Kamamasi



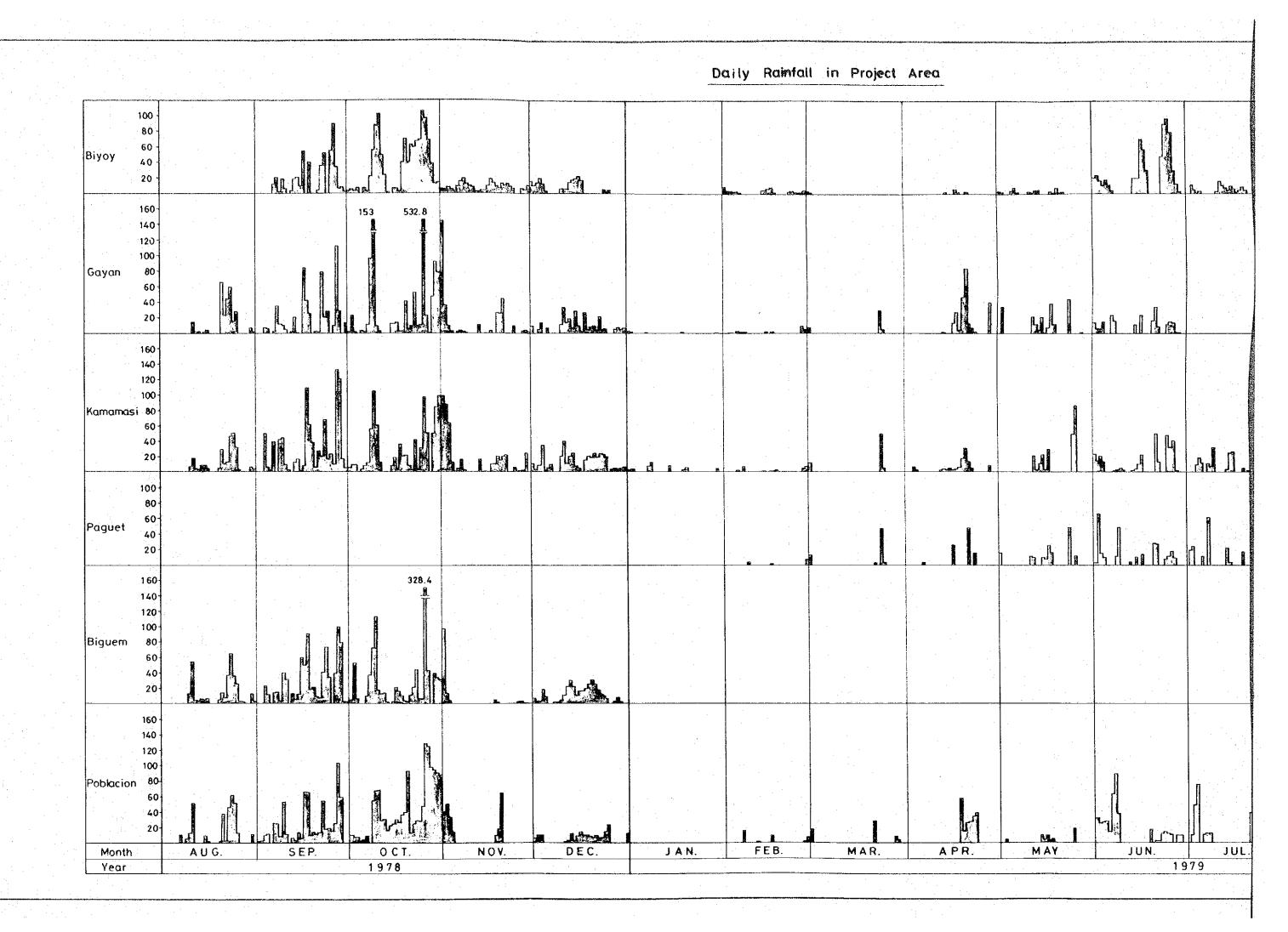
Year and Month

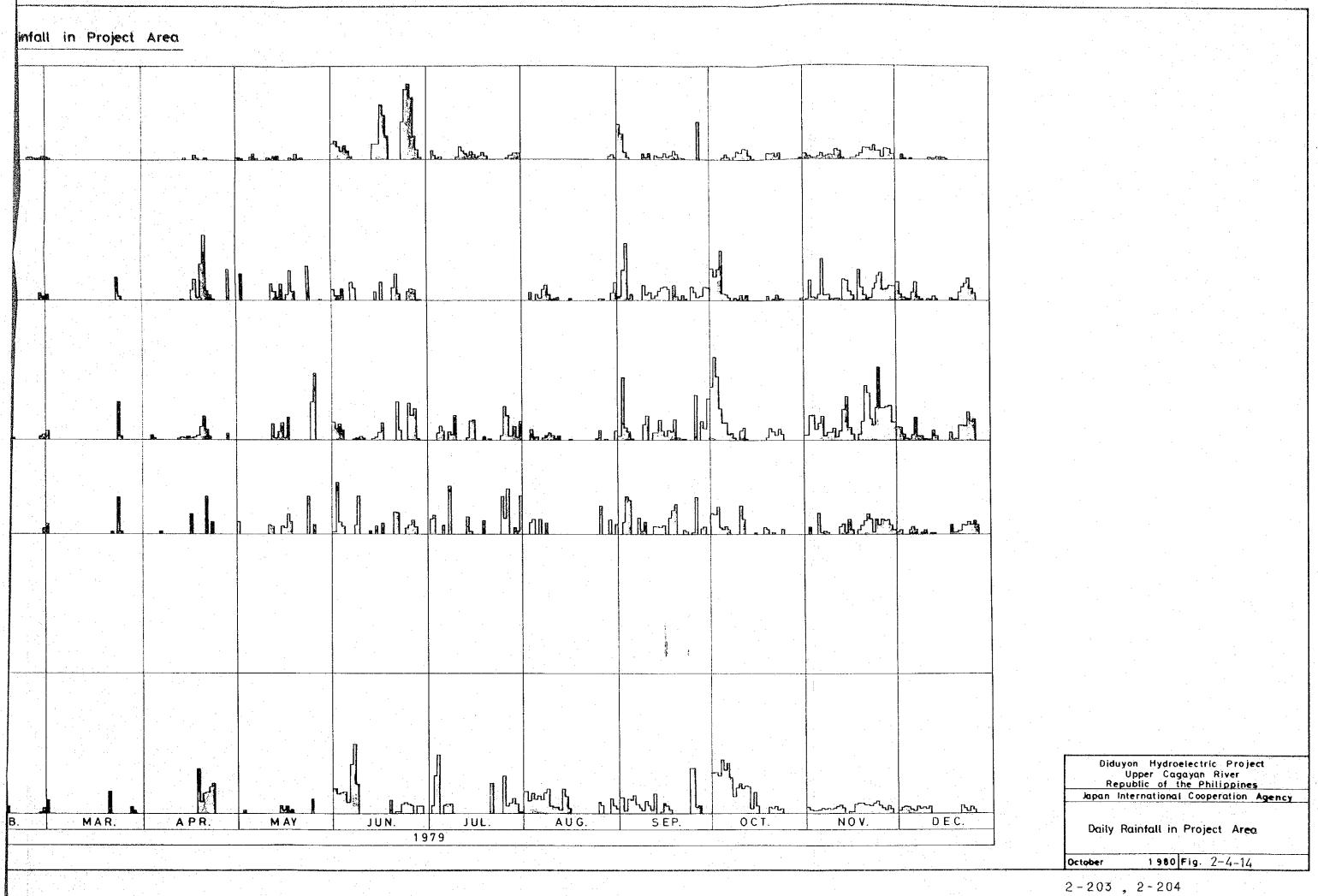
Diduyon Hydroelectris Project
Upper Gagayan River
Resublic of the Philippines

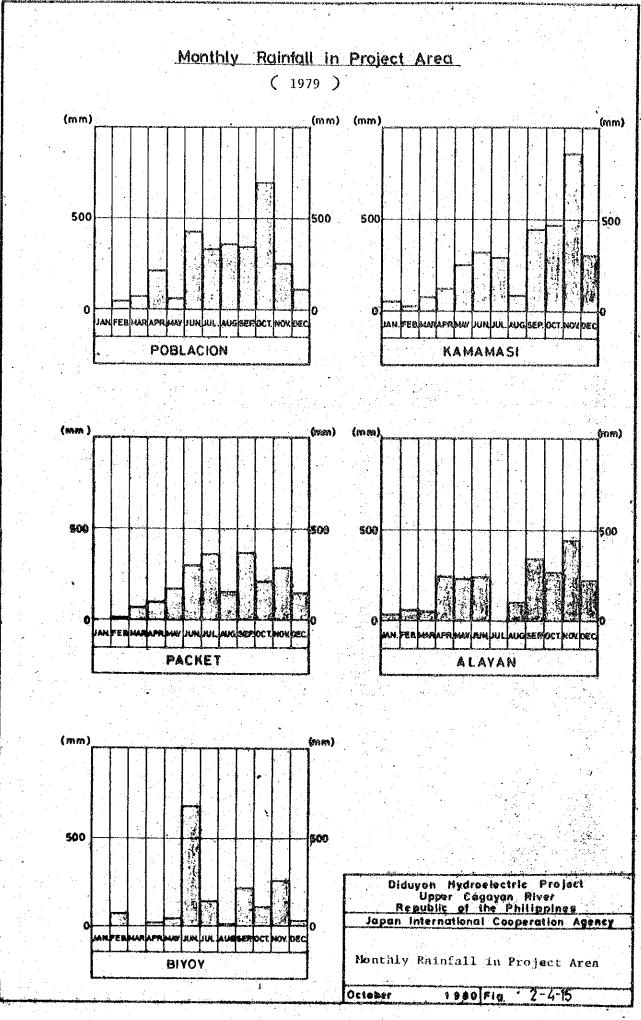
Japan International Cooperation Agency

Monthly Rainfall Record at Kamamasi

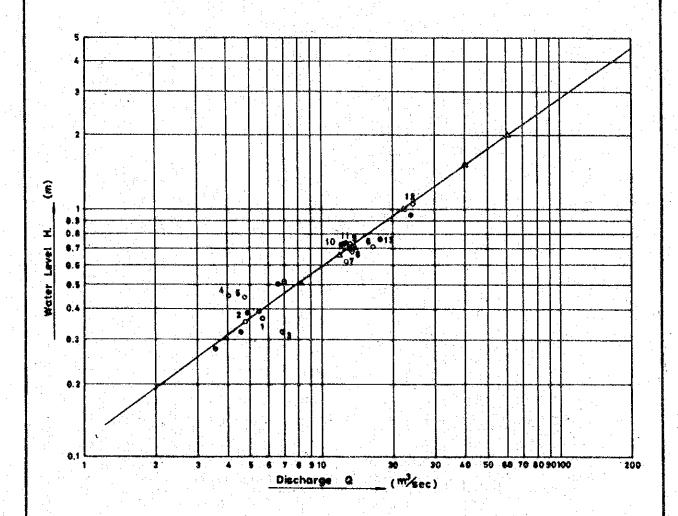
October 1 8 80 Fig. 2-4-13







Discharge Rating Curve at Kamamasi



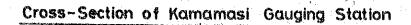
- * Note: Curve Fitted by Power Equation $Q = 22.4633H^{1.44023}$
- Δ Points Derived from Power Equation
- o Points Derived from Actual Discharge Measurements from May 1979 to January 1980
- Points Derived from Discharge Measurements for 1980

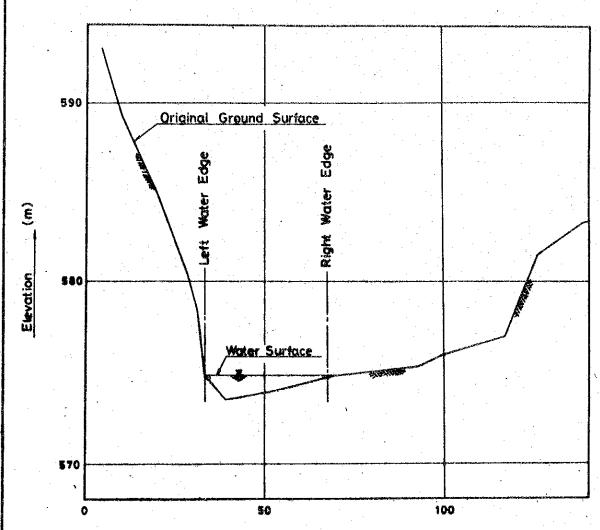
Diduyon Hydroelectric Project
Upper Cagayan River
Republic of the Philippines
Japan International Cooperation Agency

Discharge Rating Curve at Kamamasi

October

1 \$ 00 Fig. 2-4-16





Distance (m)

Note:

Gauge Height : 0.34 m

: June 23, 1980

B.M. Elevation : 578.89 m

Time : 6:00 a.m.

"O" Level of

: 574.5 m Staff Gauge

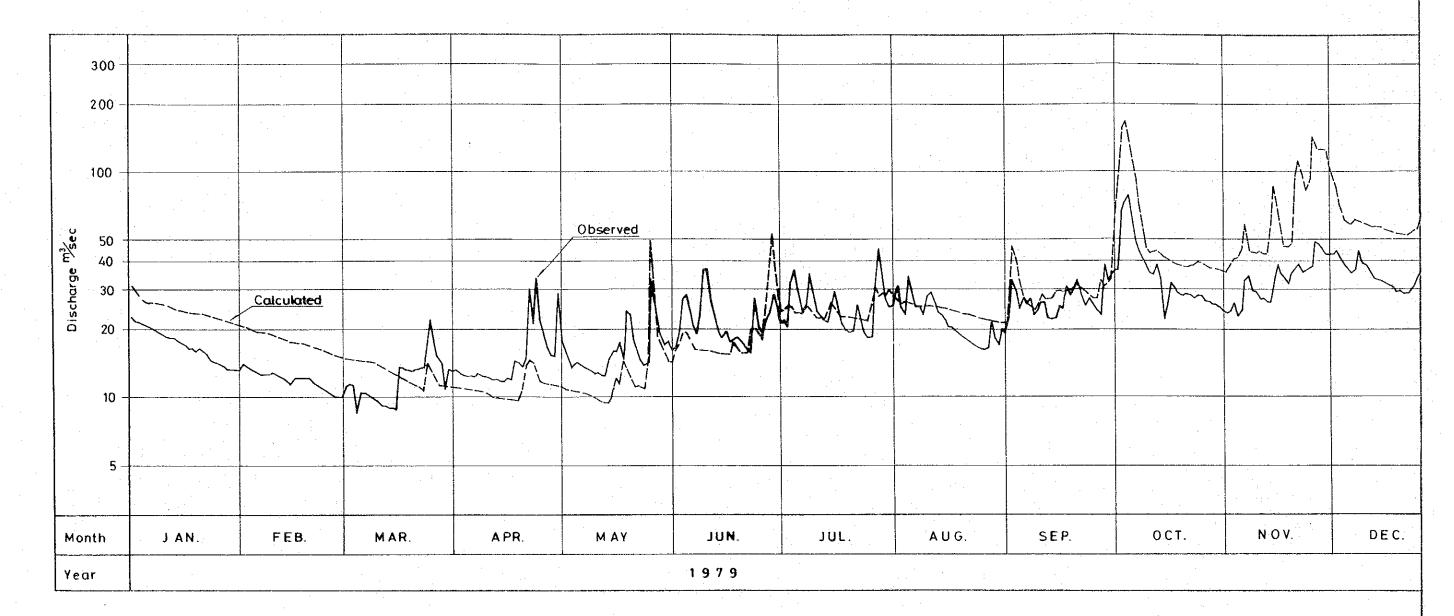
Diduyon Hydroelectric Project Upper Cogayan River Republic of the Philippines

Japan International Cooperation Agency

Cross-Section of Kamamasi Gauging Station

October 1900 Fig.

Daily Discharge at Kamamasi, Observed and Calculated



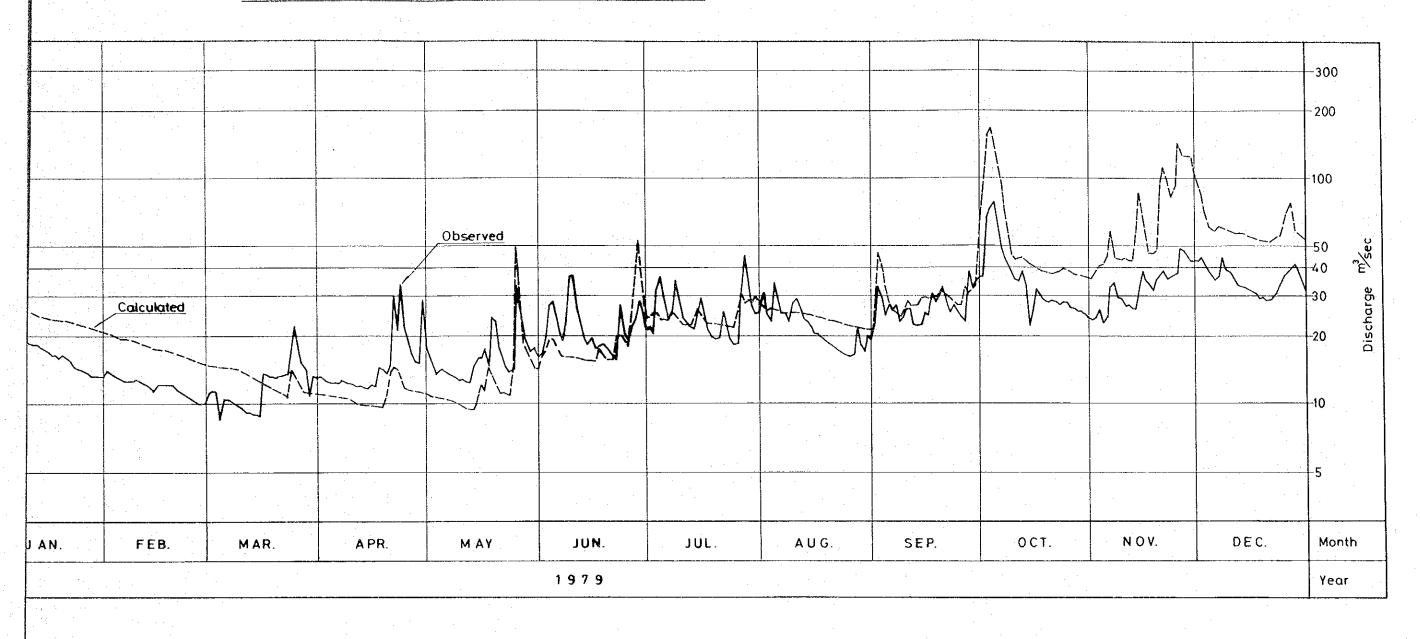
Station: Kamarnasi

Drainage area: 462 km²

Observed Daily Discharge

---- Calculated by Tank Model Method

Daily Discharge at Kamamasi, Observed and Calculated



Station : Kamamasi

Drainage area : 462 km²

Observed Daily Discharge

---- Calculated by Tank Model Method

Diduyon Hydroelectric Project
Upper Cagayan River
Republic of the Philippines
Japan International Cooperation Agency

Daily Discharge at Kamamasi

Observed and Calculated

october 1980 Fig. 2-4-18

2.4.3. <u>Hydrological Basic Discharge to be Used in the Hydroelectric</u> <u>Power Project</u>

In the project for this site, riverflow is planned to be annually regulated by means of a large-scale storage reservoir. Accordingly, management of the reservoir will be considered on a monthly basis. For more reliable simulation of output and the annually possible power generation, it is desirable to use data collected over a period of time as long as possible. However, for lack of data on precipitation in this stage, it is difficult to calculate from the amount of rainfall the rate of discharge for the site involved. In addition, data available from the gauging stations downstream on this river is considered the minimum to serve the purpose of the power project (records of riverflow actually observed for some ten years). In view of the above situation, only the measured discharges will be incorporated in the design, without attempting a longterm synthesis of riverflow variables. As stated above, there was no riverflow observation record of the Diduyon reservoir site itself until this survey was started. Table 2-4-12 shows the name and location of riverflow gauging stations in the vicinity of the project site. As shown in this table, the rate of discharge downstream on the Diduyon River has been observed at the Aglipay Gauging Station located 39 km downstream from the proposed damsite. Adding to this, river discharge relevant to the Diduyon River was measured at the Pangal Gauging Station located 17.5 km downstream of the confluences of the Cagayan River with the Diduyon (Addalam) River. The records at both stations are daily discharge measurements taken at a fixed time every day, and do not include any records on flood hydrograph. Observations at both stations are currently suspended. The periods of observation at the stream gauging stations are as follows:

Gauging Station	Observation Commenced from	Records Available for
Aglipay	June, 1964	10.5 years
Pangal	January, 1960	12 years

Since the records at both gauging stations show a good correlation as shown below, it is relatively easy to estimate the discharges in the period of suspension at one gauging station from the existing records for the corresponding period taken at the other gauging stations.

The correlation between the two stations is as follows:

Correlation coefficient by daily discharge:

 \dot{r} = 0.56, and number of data n = 2.702. Then, expressed by the Barvais-Pearson linear equation, y = 0.08602x + 22.39873 where, y = Discharge at Aglipay and x = Discharge at Pangal.

ii) Correlation coefficient by monthly discharge:

r = 0.895, and number of data n = 88. Then, expressed by the Barvais-Pearson linear equation, y = 0.16544x - 0.19141.

Thus, as values of r are larger than 0.5 in both cases, a good correlation is proved to exist.

In the course of the feasibility study on the Diduyon, a river-flow gauging station was installed at Kamamasi near the reservoir site, and thereby it has become possible to obtain river discharge directly at the proposed damsite. The name and location of the new gauging station are shown in Table 2-4-6.

Name of gauging station : Kamamasi Gauging Station

Observation commenced from : June, 1979

Method of observation : Daily observation of water stage and periodic measurement

of river section and riverflow

velocity

Data produced at these three gauging stations are processed through the method shown in Fig. 2-4-19 to prepare records for the past 16 years. Using the records, it is possible to rationally obtain the inflow to the Diduyon Reservoir. The discharges for the Diduyon No. 3 Damsite are listed in Table 2-4-13 (1) - (16), and the discharge diagram is given in Fig. 2-5-20 (1) - (4). From the tabulated annual riverflow for a period of 16 years, the average annual inflow to the reservoir is estimated at 30.8 m3/sec daily, and the rates of maximum and minimum annual riverflows to the average are calculated to be 69% and 41%, respectively (see Fig. 2-4-21). The droughty years experienced in 1969 and 1963 will inevitably have an influence on the study of reservoir planning. The types of river discharge at the Diduyon No. 3 Damsite are shown in Table 2-4-14, and the discharge duration curve for each year is given in Fig. 2-4-22 (1) - (8). Fig. 2-4-23 shows the years of the maximum and minimum riverflows, and the average river discharge. The annual average flow of 30.8 m³/sec corresponds to some one billion cubic meters per year. The droughty flow (discharge for 355 days) of 10.7 m³/sec, as compared with the high water flow of 32.0 m³/sec, signifies the discharge characteristics of this river. To determine the basic discharge for power project at the No. 3 Damsite, the average monthly riverflows shown in Table 2-4-15 are used in the calculation of reservoir management. The discharge diagram and the discharge mass curve are presented in Fig. 2-4-24.

Table 2-4-12 Location of Existing Discharge Gauging Stations

	Nam	se of Station	C.A. (km²)	Period of observation
A 1	Cagayan R.	Pangal, Echague, Isabela	4,244	1959 –
19 2	Addalam R.	Guinalvin, Aglipay, Nueva Viscaya	721	1965 -
c 3	Diduluan R.	Minuri, Jones, Isabela	272	1965 –
D 4	Dabubu R.	Dabubu, Pequino, Sen Agustin Isabela	162	1965 –
3	Cagayan R.	Dipaddiw Maddela, Nueva Viscava	2,323	1968 -

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DAY 1AN. FEB. MAR. APP. MAY JUM. JUM. AUG. 1 36.0 44.3 43.9 21.2 19.8 20.6 24.4 20.4 2 47.4 43.9 21.2 19.8 20.6 24.4 20.4 4 36.0 44.3 43.9 21.2 20.4 20.6 24.4 20.4 4 38.2 31.7 33.8 22.0 19.6 19.5 32.2 23.6 5 38.4 30.6 32.8 22.7 19.1 18.9 23.2 23.6 6 40.5 29.3 31.2 19.6 19.5 32.6 23.6 47.6 40.3 9 43.7 58.1 28.0 24.9 18.2 22.6 20.6 20.6 20.6 20.6 47.6 40.3 10 49.3 32.8 22.2 19.1 18.2 22.6 47.6 40.3 40.3 40.3													
36.0 44.3 43.9 21.2 19.8 20.8 24.4 47.4 33.9 35.9 21.2 21.3 21.5 47.0 24.4 43.5 33.9 35.8 22.2 21.3 47.6 24.6 36.5 34.7 33.8 22.6 19.6 19.5 31.2 23.6 40.5 29.3 31.2 22.7 19.1 18.9 28.9 23.6 23.6 23.6 47.6 23.6 23.6 23.6 47.6 47.6 23.6 23.6 47.6 23.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6	DAY	JAH.	reb.	MAR.	AT.	MAX	JOHN	JOLY	AUG.	SEPT.	oct.	NOV.	DEC.
47.4 37.9 39.9 21.2 21.3 21.5 47.6 24.6 24.6 34.6 34.6 35.8 22.5 20.6 20.2 47.6 24.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 34.6 44.6 34.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 44.6 <th< th=""><th>-</th><th>36.0</th><th>44.3</th><th>43.9</th><th>21.2</th><th>19.8</th><th>20.8</th><th>28.7</th><th>20.4</th><th></th><th>30.6</th><th>27.0</th><th>26.9</th></th<>	-	36.0	44.3	43.9	21.2	19.8	20.8	28.7	20.4		30.6	27.0	26.9
43.5 33.9 35.8 22.5 20.6 20.2 47.4 24.6 38.2 31.7 33.8 22.0 19.6 19.5 19.5 23.2 40.5 29.6 32.7 19.1 18.9 28.9 23.6 40.5 29.3 31.2 22.7 19.1 18.9 28.9 23.6 55.8 28.3 29.8 23.9 18.6 20.4 24.6 47.4 50.8 57.8 28.9 24.9 18.2 22.8 47.6 47.6 33.6 33.8 26.0 21.4 19.0 18.7 48.8 46.6 33.6 45.0 24.9 19.5 18.7 22.7 47.0 24.9 19.6 19.3 21.5 36.1 33.6 43.5 25.3 19.9 18.7 19.3 21.5 36.1 33.6 43.5 25.3 19.9 18.7 20.4 22.7 42.0 33.7 <th>~</th> <th>4.7.4</th> <th>37.9</th> <th>39.9</th> <th>21.2</th> <th>21.3</th> <th>21.5</th> <th>47.0</th> <th>24.4</th> <th></th> <th>30.0</th> <th>26.9</th> <th>26.1</th>	~	4.7.4	37.9	39.9	21.2	21.3	21.5	47.0	24.4		30.0	26.9	26.1
38.2 31.7 33.8 22.0 19.6 19.5 32.2 23.2 36.4 30.6 32.8 22.7 19.1 18.9 28.9 23.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.6 47.4 46.8 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33.6 33	m	43.5	33.9	35.8	22.5	20.6	20.2	47.4	24.6	1.,	28.0	26.4	25.8
34,4 30.6 32.8 22.7 19.1 18.9 28.9 23.6 55.8 28.3 29.8 22.9 18.2 28.6 28.6 28.7 55.8 28.3 29.8 23.6 18.2 22.8 47.6 47.6 59.8 57.8 28.9 24.6 18.2 22.8 46.4 46.6 47.6 43.7 58.1 28.0 23.4 18.0 22.8 28.4 46.6 40.3 33.6 49.3 22.8 46.6 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 40.3 33.4 33.4 33.4 33.4	•	38.2	31.7	33.8	22.0	19.6	19.5	32.2	23.2		26.4	25.6	25.4
40.5 29.3 31.2 23.2 18.8 19.0 26.0 28.7 55.8 28.3 23.9 18.6 20.4 47.4 57.4 57.4 46.6 47.4 56.6 47.4 46.6 47.4 46.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47.6 47	•	7.46	30.6	32.8	22.7	19.1	18.9	28.9	23.6	. :	26.3	25.0	24.9
55.8 28.3 29.8 23.9 18.6 20.4 24.6 47.4 50.8 57.8 28.9 24.6 18.2 22.8 24.6 46.6 43.7 58.1 28.0 23.4 18.2 22.8 46.6 40.3 35.8 37.5 26.6 21.9 18.2 21.8 22.7 47.0 35.8 37.5 26.6 21.9 18.2 20.4 22.7 47.0 33.6 36.8 26.0 21.4 19.0 18.7 22.1 39.9 35.8 46.4 25.6 20.6 20.2 18.7 22.1 39.9 33.4 43.5 25.3 19.9 19.4 19.5 21.9 34.4 31.5 46.4 25.6 26.0 21.4 19.6 21.5 36.1 33.4 43.5 25.3 19.9 19.4 19.5 21.9 36.1 33.4 43.5 24.9 19.5 <th>•</th> <th>40.5</th> <th>29.3</th> <th>31.2</th> <th>23.2</th> <th>1.8.8</th> <th>19.0</th> <th>26.0</th> <th>28.7</th> <th>٠.,</th> <th>29.5</th> <th>24.6</th> <th>24.5</th>	•	40.5	29.3	31.2	23.2	1.8.8	19.0	26.0	28.7	٠.,	29.5	24.6	24.5
50.8 57.8 28.9 24.0 18.2 22.8 24.4 46.6 43.7 58.1 28.0 23.4 18.0 22.9 25.4 40.3 35.8 37.5 26.6 21.9 18.2 22.7 46.8 35.8 37.5 26.6 21.9 18.5 20.4 22.7 47.0 33.6 33.8 26.0 21.4 19.0 18.7 22.7 47.0 35.8 46.4 25.6 20.6 20.2 18.7 22.1 39.9 33.4 46.3 25.3 19.9 19.4 19.5 21.9 34.4 33.4 46.4 25.6 20.6 20.2 18.7 21.9 34.4 33.4 46.4 25.3 19.9 19.4 19.5 21.9 34.4 33.4 46.4 25.3 19.9 19.4 19.5 21.9 34.4 33.4 47.0 24.9 19.5 18.7 <th>1 F</th> <th>55.8</th> <th>28.3</th> <th>29.8</th> <th>23.9</th> <th>18.6</th> <th>20.4</th> <th>24.6</th> <th>47.4</th> <th>. :</th> <th>8.99</th> <th>26.9</th> <th>25.6</th>	1 F	55.8	28.3	29.8	23.9	18.6	20.4	24.6	47.4	. :	8.99	26.9	25.6
43.7 58.1 28.0 23.4 18.0 22.0 25.4 46.3 39.9 43.1 27.4 22.5 18.2 21.8 23.4 48.8 35.8 37.5 26.6 21.9 18.7 22.1 39.9 35.8 46.4 25.6 20.6 20.2 18.7 22.1 39.9 35.8 46.4 25.6 20.6 20.2 18.7 22.1 39.9 33.4 43.5 25.3 19.9 19.2 18.7 22.1 34.1 31.5 47.0 24.9 19.5 18.7 18.7 20.9 36.1 28.6 62.7 24.4 20.1 18.7 20.9 36.1 28.6 62.7 24.4 20.1 18.7 20.9 36.1 28.6 56.2 23.6 19.5 18.9 20.6 36.1 28.6 56.2 23.9 19.5 18.2 21.5 36.8	•••	50.8	57.8	28.9	24.0	18.2	22.8	24.4	46.6		7.6.4	27.3	28.9
39.9 43.1 27.4 22.5 18.2 21.8 23.4 48.8 35.8 37.5 26.6 21.9 18.5 20.4 22.7 47.0 33.6 33.8 26.0 21.4 19.0 18.7 22.7 47.0 35.8 46.4 25.6 20.6 20.2 18.7 21.5 39.9 33.4 43.5 25.3 19.9 19.4 19.5 21.9 34.4 31.5 47.0 24.9 19.5 18.7 21.5 36.1 28.6 62.7 24.9 19.5 18.7 18.7 20.9 35.1 28.6 62.7 24.4 20.1 18.7 18.7 20.9 35.1 28.6 56.2 23.9 19.5 17.9 18.9 20.6 36.1 28.6 56.2 23.9 19.7 18.2 18.9 20.6 36.1 28.7 56.0 22.6 19.7 18.3 18.4 22.3 21.5 22.3 22.5 22.3 22.2 22.3<	6	43.7	58.1	28.0	23.4	18.0	22.0	25.4	40.3		63.4	27.6	27.4
35.8 37.5 26.6 21.9 18.5 20.4 22.7 47.0 33.6 33.8 26.0 21.4 19.0 18.7 22.1 39.9 35.8 46.4 25.6 20.6 20.6 19.7 18.7 22.1 39.9 33.4 43.5 25.3 19.9 19.4 19.5 13.7 21.5 34.4 31.5 47.0 24.9 19.5 18.9 19.3 20.9 35.1 20.9 36.2 28.6 62.7 24.9 19.2 18.7 20.9 35.1 20.6 36.7 28.6 66.2.7 24.4 20.1 18.7 18.7 20.9 36.1 28.6 56.2 23.9 19.5 17.9 18.9 20.6 36.1 28.7 24.4 20.1 18.7 18.9 20.6 36.8 28.3 25.3 22.7 20.4 19.1 17.7 22.5 53.6 26.0 61.5 22.7 20.4 19.1 17.5 22.2 59.	10	39.9	43.1	27.4	22.5	18.2	21.8	23.4	8.8	4, 1	45.0	34.1	27.0
33.6 33.8 26.0 21.4 19.0 18.7 22.1 39.9 35.8 46.4 25.6 20.6 26.2 18.7 21.5 36.1 33.4 43.5 25.3 19.9 19.4 19.5 21.9 34.4 31.5 47.0 24.9 19.5 18.9 19.3 21.5 36.1 29.8 78.0 24.9 19.2 18.7 18.7 20.9 35.1 28.6 66.7 24.9 19.2 18.7 18.7 20.9 36.7 28.6 66.7 24.9 19.7 18.4 19.3 20.6 36.1 28.6 56.2 23.9 19.7 18.2 18.9 20.6 36.1 28.6 56.2 23.9 19.7 18.3 18.4 20.5 36.1 28.7 26.0 19.7 18.3 18.4 20.5 36.1 26.0 55.3 22.5 19.6 17.4 22.3 23.6 26.0 55.3 22.5 19.6 19.6 </th <th>11</th> <th>35.8</th> <th>37.5</th> <th>26.6</th> <th>21.9</th> <th>18.5</th> <th>20.4</th> <th>22.7</th> <th>47.0</th> <th></th> <th>37.9</th> <th>30.2</th> <th>27.4</th>	11	35.8	37.5	26.6	21.9	18.5	20.4	22.7	47.0		37.9	30.2	27.4
35.8 46.4 25.6 20.6 20.2 18.7 21.5 36.1 33.4 43.5 25.3 19.9 19.4 19.5 21.9 34.4 31.5 47.0 24.9 19.5 18.9 19.3 21.5 36.1 28.6 62.7 24.9 19.2 18.7 18.7 20.9 35.1 28.6 62.7 24.4 20.1 18.4 19.3 20.6 36.7 28.6 62.7 24.4 20.1 18.2 19.3 20.6 36.1 28.6 62.7 24.1 19.7 18.2 18.9 20.6 36.1 28.6 56.2 23.6 19.7 18.2 18.6 20.6 36.1 28.6 56.0 19.7 18.2 18.6 20.5 36.8 27.1 50.4 19.7 18.3 18.4 20.5 36.1 26.0 53.2 22.5 19.6 17.6 17.9 <th>12,</th> <th>33.6</th> <th>33.8</th> <th>26.0</th> <th></th> <th>19.0</th> <th>18.7</th> <th>22.1</th> <th>39.9</th> <th></th> <th>100.7</th> <th>29.8</th> <th>28.0</th>	12,	33.6	33.8	26.0		19.0	18.7	22.1	39.9		100.7	29.8	28.0
33.4 43.5 25.3 19.9 19.4 19.5 21.9 34.4 31.5 47.0 24.9 19.5 18.9 19.3 21.5 36.2 29.8 78.0 24.9 19.2 18.7 18.7 20.9 35.1 28.6 62.7 24.4 20.1 18.4 19.3 20.6 36.7 28.6 62.7 24.4 20.1 18.4 19.0 36.7 28.7 24.4 19.7 18.2 19.1 20.6 36.1 28.3 56.2 23.9 19.7 18.2 18.6 20.5 42.6 28.3 59.2 23.6 19.7 18.3 18.4 20.5 36.8 27.1 50.4 19.7 18.3 18.4 22.3 53.4 26.0 55.3 22.7 20.4 19.1 17.5 22.5 59.0 26.0 61.5 22.1 22.5 19.6 17.4 22.2 59.0 26.0 61.5 22.1 22.5 18.1 17.5 </th <th>CH</th> <th>35.8</th> <th>4.94</th> <th>25.6</th> <th>20.6</th> <th>20.2</th> <th>18.7</th> <th>21.5</th> <th>36.1</th> <th>1.7</th> <th>233.6</th> <th>28.7</th> <th>27.1</th>	CH	35.8	4.94	25.6	20.6	20.2	18.7	21.5	36.1	1.7	233.6	28.7	27.1
31.5 47.0 24.9 19.5 18.9 19.3 21.5 36.2 29.8 78.0 24.9 19.2 18.7 18.7 20.9 35.1 28.6 62.7 24.4 20.1 18.4 19.3 20.6 36.7 28.6 55.2 24.1 19.7 18.2 19.1 20.5 42.6 28.6 56.2 23.9 19.7 18.2 18.9 20.6 36.1 28.3 59.2 23.6 19.7 18.2 18.6 21.5 36.8 27.1 50.4 23.0 19.7 18.3 18.4 22.3 36.8 27.1 50.4 19.7 18.3 18.4 22.3 36.8 26.0 55.3 22.7 20.4 19.1 17.7 22.5 59.0 26.0 61.5 22.1 22.5 19.6 17.9 17.4 22.2 59.0 26.0 61.5 22.1 22.5 19.6 17.4 22.2 59.0 36.1 55.3 22.2 </th <th>14</th> <th>33.4</th> <th>43.5</th> <th>25.3</th> <th>19.9</th> <th>19.4</th> <th>19.5</th> <th>21.9</th> <th>4. *</th> <th></th> <th>221.1</th> <th>36.5</th> <th>28.0</th>	14	33.4	43.5	25.3	19.9	19.4	19.5	21.9	4. *		221.1	36.5	28.0
29.8 78.0 24.9 19.2 18.7 18.7 20.9 35.1 28.6 62.7 24.4 20.1 18.4 19.3 20.6 36.7 28.6 53.2 24.1 19.7 18.2 19.1 20.5 42.6 28.6 56.2 23.9 19.7 18.2 18.9 20.6 36.1 28.3 59.2 23.6 19.7 18.3 18.6 21.5 36.8 27.1 50.4 23.0 19.7 18.3 18.4 22.3 33.4 26.0 55.3 22.7 20.4 19.1 17.7 22.5 57.6 26.0 61.5 22.5 19.6 17.4 22.3 53.4 26.0 61.5 22.1 22.9 19.1 17.5 21.9 40.5 26.0 61.5 22.1 22.9 19.1 17.5 21.9 40.5 36.3 60.4 21.2 18.3 18.1 21.2 21.9 22.5 36.1 22.2 18.3 18.3 21.9 20.6 36.1 36.3 22.2 21.3 22.2 21.3 22.2 21.3 22.3 21.3 <	15	31.5	47.0	24.9	19.5	18.9	19.3	21.5	38.2	٠.	91.2	38.8	29.2
28.6 62.7 24.4 20.1 18.4 19.3 20.6 36.7 28.0 53.2 24.1 19.7 18.2 19.1 20.5 42.6 28.6 56.2 23.9 19.5 17.9 18.9 20.6 36.1 28.3 59.2 23.6 19.7 18.2 18.9 20.6 36.3 27.1 50.4 23.0 19.7 18.3 18.4 22.3 36.8 26.0 55.3 22.7 20.4 19.1 17.7 22.3 53.4 26.0 61.5 22.5 19.6 17.4 22.3 53.4 26.0 61.5 22.1 22.9 19.1 17.5 22.3 53.4 26.0 61.5 22.1 22.9 19.1 17.5 22.3 53.6 26.0 61.5 22.1 22.9 19.1 17.5 21.9 40.5 36.1 53.6 21.5 22.2 18.3 25.0 20.6 36.1 36.7 49.8 21.3 22.2 18.3 21.3 24.4 36.1 45.8 21.3 22.2 21.3 22.0 20.6 36.1 <t< th=""><th>9</th><th>29.8</th><th>78.0</th><th>24.9</th><th>19.2</th><th>18.7</th><th>18.7</th><th>20.9</th><th>35.1</th><th>1.</th><th>64.8</th><th>40.7</th><th>28.6</th></t<>	9	29.8	78.0	24.9	19.2	18.7	18.7	20.9	35.1	1.	64.8	40.7	28.6
28.0 53.2 24.1 19.7 18.2 19.1 20.5 42.6 28.6 56.2 23.9 19.5 17.9 18.9 20.6 38.1 28.3 59.2 23.6 19.7 18.2 18.6 21.5 36.8 27.1 50.4 23.0 19.7 18.3 18.4 22.3 33.4 26.0 55.3 22.7 20.4 19.1 17.7 22.3 53.4 26.0 55.3 22.7 20.4 19.1 17.5 22.2 57.6 26.0 61.5 22.1 22.9 19.1 17.5 21.9 40.5 36.3 60.4 21.8 24.4 18.7 18.1 21.2 32.5 36.1 53.6 21.5 22.2 18.3 25.0 20.6 36.1 36.7 55.3 21.3 19.9 24.4 52.3 21.3 24.4 50.0 21.3 19.9 24.4 52.3 21.3 22.0 55.3 21.3 19.9 24.4 52.3 21.3 22.0 55.3 21.3 21.3 21.3 22.0 22.0 55.3 21.3 <t< th=""><th>17</th><th>28.6</th><th>62.7</th><th>24.4</th><th>20.1</th><th>#·8T</th><th>19.3</th><th>20.6</th><th>36.7</th><th></th><th>53.6</th><th>34.8</th><th>27.0</th></t<>	17	28.6	62.7	24.4	20.1	#·8T	19.3	20.6	36.7		53.6	34.8	27.0
28.6 56.2 23.9 19.5 17.9 18.9 20.6 38.1 28.3 59.2 23.6 19.7 18.2 18.6 21.5 36.8 27.1 50.4 23.0 19.7 18.4 22.3 53.4 26.0 55.3 22.7 20.4 19.1 17.7 22.5 57.6 26.0 55.3 22.7 20.4 19.1 17.7 22.3 57.6 26.0 61.5 22.1 22.9 19.1 17.5 21.9 40.5 26.0 61.5 22.1 22.9 19.1 17.5 21.9 40.5 36.3 60.4 21.8 24.4 18.7 18.1 21.2 35.5 36.1 53.6 21.5 22.2 18.3 25.0 20.6 36.1 36.7 55.3 22.2 21.3 18.5 102.4 52.3 24.4 36.1 45.8 21.9 24.4 52.3 21.3 24.4 55.3 21.3 21.3 21.3 22.0 22.0 55.3 21.3 21.3 21.3 22.0 55.3 21.3 21.3 21.3 21.3 <th>18</th> <th>28.0</th> <th>53.2</th> <th>24.1</th> <th>19.7</th> <th>18.2</th> <th>19.1</th> <th>20.5</th> <th>42.6</th> <th>ŗ.</th> <th>8.97</th> <th>31.4</th> <th>32.8</th>	18	28.0	53.2	24.1	19.7	18.2	19.1	20.5	42.6	ŗ.	8.97	31.4	32.8
28.3 59.2 23.6 19.7 18.2 18.6 21.5 36.8 27.1 50.4 23.0 19.7 18.3 18.4 22.3 53.4 26.0 55.3 22.7 20.4 19.1 17.7 22.5 57.6 25.4 53.2 22.7 20.4 19.1 17.7 22.3 57.6 26.0 61.5 22.5 19.6 17.4 22.2 59.0 26.0 61.5 22.1 22.9 19.1 17.5 21.9 40.5 36.3 60.4 21.8 24.4 18.7 18.1 21.2 36.1 36.7 55.3 22.2 18.3 25.0 20.6 36.1 36.7 55.3 22.2 21.3 18.5 102.4 21.9 24.4 36.1 45.8 21.3 19.9 24.4 52.3 21.3 24.4 50.0 20.3 21.3 21.3 21.3 22.0 22.0 55.3 21.3 21.3 21.3 21.3 22.0 55.3 21.3 21.3 21.3 22.0 55.3 21.3 21.3 21.3 22.0	13	28.6	56.2	23.9	19.5	17.9	18.9	20.6	38.1	1.0	54.5	31.4	46.6
27.1 50.4 23.0 19.7 18.3 18.4 22.3 53.4 26.0 55.3 22.7 20.4 19.1 17.7 22.5 57.6 25.4 53.2 22.5 19.6 17.4 22.2 59.0 26.0 61.5 22.1 22.9 19.1 17.5 21.9 40.5 36.3 60.4 21.8 24.4 18.7 18.1 21.2 32.5 33.1 53.6 21.5 22.2 18.3 25.0 20.6 36.1 36.7 55.3 22.2 21.3 18.2 45.0 20.8 26.9 34.9 49.8 21.9 20.9 18.5 102.4 21.9 25.7 38.1 45.8 21.3 19.9 24.4 52.3 21.3 22.0 50.0 21.3 19.9 28.6 53.9 22.0 23.6 55.3 21.5 21.3 21.3 21.3 22.9	8	28.3	59.2	23.6	19.7	18.2	18.6	21.5	36.8		44.1	30.0	\$. 44
26.0 55.3 22.7 20.4 19.1 17.7 22.5 57.6 25.4 53.2 22.5 19.6 17.4 22.2 59.0 26.0 61.5 22.1 22.9 19.1 17.5 21.9 40.5 26.0 61.5 22.1 22.9 19.1 17.5 21.9 40.5 36.3 50.6 21.8 24.4 18.7 18.1 21.2 32.5 36.7 55.3 22.2 21.3 18.2 45.0 20.8 26.9 36.7 49.8 21.9 20.9 18.5 102.4 21.9 25.7 38.1 45.8 21.3 19.9 24.4 52.3 21.3 24.4 50.0 21.3 21.3 21.3 21.3 22.0 23.6 55.3 21.3 21.3 21.3 22.0 23.6 55.3 21.3 21.3 21.3 22.0 22.9	ĸ	27.1	50.4	23.0	19.7	18.3	18.4	22.3	53.4		38.4	28.9	39.2
.4 53.2 22.5 19.6 17.4 22.2 59.0 .0 61.5 22.1 22.9 19.1 17.5 21.9 40.5 .3 60.4 21.8 24.4 18.7 18.1 21.2 32.5 .1 53.6 21.5 22.2 18.3 25.0 20.6 36.1 .7 55.3 22.2 21.3 18.2 45.0 20.8 26.9 .9 49.8 21.9 24.4 52.3 21.3 24.4 .1 45.8 21.3 19.9 28.6 53.9 22.0 .1 21.5 21.3 21.3 21.3 22.0	22	26.0	55.3	22.7	70.7	19.1	17.7	22.5	57.6		35.3	27.4	35.4
.0 61.5 22.1 22.9 19.1 17.5 21.9 40.5 .3 60.4 21.8 24.4 18.7 18.1 21.2 32.5 .3 25.6 21.5 22.2 18.3 25.0 20.6 36.1 .7 55.3 22.2 21.3 18.2 45.0 20.8 26.9 .9 49.8 21.9 20.9 18.5 102.4 21.9 25.7 .1 45.8 21.3 19.9 24.4 52.3 21.3 24.4 52.0 23.6 .3 21.5 21.5 21.5 21.5 21.3 22.0 23.6	23	25.4	53.2	22.5		19.6	17.4	22.2	59.0		36.0	26.7	33.0
.3 \$60.4 21.8 24.4 18.7 18.1 21.2 32.5 .1 \$3.6 21.5 22.2 18.3 25.0 20.6 36.1 .7 \$5.3 22.2 21.3 18.2 45.0 20.8 26.9 .9 \$21.9 \$20.9 \$18.5 \$10.9 25.7 .1 \$45.8 \$21.3 \$19.9 \$24.4 \$22.3 \$21.3 \$24.4 .0 \$21.3 \$19.9 \$28.6 \$5.3 \$21.0 \$23.6 .3 \$21.5 \$21.3 \$21.3 \$21.3 \$22.9	24	26.0	61.5	22.1		19.1	17.5	21.9	40.5		38.6	26.6	30.9
.1 53.6 21.5 22.2 18.3 25.0 20.6 36.1 .7 55.3 22.2 21.3 18.2 45.0 20.8 26.9 .9 49.8 21.9 20.9 18.5 102.4 21.9 25.7 .1 45.8 21.3 19.9 24.4 52.3 21.3 24.4 .0 21.3 19.9 28.6 53.9 22.0 23.6 .3 21.5 21.3 21.3	25	36.3	7.09	21.8		18.7	18.1	21.2	32.5		37.2	25.8	30.0
.7 55.3 22.2 21.3 18.2 45.0 20.8 26.9 .9 49.8 21.9 20.9 18.5 102.4 21.9 25.7 .1 45.8 21.3 19.9 24.4 52.3 21.3 24.4 .0 21.3 19.9 28.6 53.9 22.0 23.6 .3 21.5 21.3 21.3	56	33.1	53.6	21.5		18.3	25.0	20.6	36.1	100	33.0	25.1	29.9
.9 49.8 21.9 20.9 18.5 102.4 21.9 25.7 .1 45.8 21.3 19.9 24.4 52.3 21.3 24.4 .0 .0 21.3 19.9 28.6 53.9 22.0 23.6 .3 21.5 21.5 21.3 21.3 22.9	27	36.7	55.3	22.2		18.2	45.0	20.8	26.9	1	31.7	25.0	39.7
.1 45.8 21.3 19.9 24.4 52.3 21.3 24.4 .0 .0 21.3 19.9 28.6 53.9 22.0 23.6 .3 21.5 21.3 21.3 22.9	28	34.9	8.67	21.9		18.5	102.4	21.9	25.7		30.2	30.0	67.0
.0 21.3 19.9 28.6 53.9 22.0 23.6 .3 21.5 21.3 22.9	83	38.1	45.8	21.3		24.4	52.3	21.3	24.4		29.6	30.2	36.8
.3 21.5 21.3 21.1	8	50.0		21.3	19.9	28.6	53.9	22.0	23.6	9	29.2	28.3	32.2
	3	55.3		21.5		21.3	•	21.1	22.9	:	28.0	. ,.	31.7

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DEC.	33 6	2. C	30.5	29.5		64.3	43.9	44.8	51.4	88.6	1.46	7.09	45.0	4.5.4	9. 55	39.6	34.7	32.5	30.6	29.8	28.6	27.0	58.5	62.7	34.1	31.2	28.9	27.7	28.9	41.2	35.1	5
MOV.	35	7.0%	25.1	24.7	24.2	24.1	25.4	27.7	28.0	25.8	24.6	27.1	27.3	27.4	26.6	25.1	24.4	23.6	23.4	22.7	22.5	25.0	136.3	264.0	193.9	78.3	56.2	8.93	39.0	32.0		
oct.	3 76	20.00	30.5	27.3	24.7	23.9	23.2	27.1	33.4	29.6	36.8	30.5	49.2	68.7	43.9	37.50	34.1	53.2	62.2	47.2	39.4	36.8	35.4	m en	_	32.2	_		27.3	26.1	25.4	
SEPT.	9 77	•	24.5		24.7	27.7	24.4	22.3	21.9	22.3	22.2	22.1	30.2	22.6	20.7	20.4	22.3	23.4	21.3	23.0	25.4	4.00	62.7	38.8	34.2	28.6	25.2	4. 82	23.4	23.4		
AUG.	0 0	0.07 0.08	19.8	19.4	19.1	18.8	18.9	18.5	20.2	22.8	20.1	20.7	23.2	26.6	27.9	29.0	28.7	28.0	27.1	25.4	24.1	28.6	31.6	32.2	29.2	29.2	30.6	28.7	25.7	23.9	22.9	
JULY	ا د		33.4		•	23.2	22.3	4	34.9	6 0	0	Ŋ	. 7.	en.	pod.	Øλ	26.0	3	0	m	67	c.	ø	.7	Ö	**	, mi	'n	9.	22.1	21.4	
JUNE	10	100 100	18.2	18.2	18.3	18.2	17.8	16.8	17.4	27.4	37.8	17.4	17.1	16.9	16.9	16.8	16.7	16.6	16.8	17.1	18.2	18.5	1.81	E .	16.8	17.8	50.4	32.6	28.0	25.6		
MAY	1 2	16.7	16.6	16.3	16.5	16.4	16.4	16.5	16.3	16.2	16.2	16.5	16.9	17.6	18.0	34.6	 86.	42.8	32.2	26.7	24.0	28.9	25.0	21.5	20.7	20.3	19.6	22.9	20.8	19.9	19.0	
APR.	9) C	18.6	18.6	18.5	18.4	18.2	18.2				17.8		17.4	17.4	18.3	18.2	18.0	19.0	19.0	18.2	18.6	19.3	18.8	17.9	47.7	16.9	36.8	7.7	16.9		
MAR.		٠.	20.8			24.4	24.2	24.5	26.6	29.6	4.00	47.4	30.9	•	24.9		22.5	21.9	21.8	21.6	21.8	21.6	21.5	21.8	20.8	19.9	19.5	19.7	19.5	19.3	1.61.	
E E		4.67	24.2	24.4	27.9	30.8	28.2	25.0	23.3	22.6	22.1	23.88	21.5	21.3	21.1	20.7	20.5	20.4	20.3	20.1	19.9	19.8	19.7	19.5	20.5	90.0	21.4	20.7				
IAN	9	20.0	30.0	30.0	28.4	28.3	28.0	27.1	26.6	26.0	25.3	24.7	25.3	26.3	26.0	26.6	28.0	33.6	33.6	31.1	29.2	27.7	26.4	75.7	24.9	24.4	26.7	25.7	24.6	23.9	23.6	
λ¥		-1 r	4.67	-4	·M	90	_	Ø	σ	16	Ħ	12	13	**	15	91	17	69	19	2	77	77	23	24	22	26	23	28	53	8	31	

(Unit: cms)

DAY	JAK.	, KD	MAK.	A. D.	182	0000	700	500	VAL.		2	- 3
-1	27.1	27.9	24.1	18.6	16.8	17.5	37.9	23.0	33.9	30.5	24.4	. 1
7	26.1	28.4	23.5	18.3	16.7	17.9	35.8	22.8	33.0	29.8	24.5	
3	25.3	29.3	23.0	18.2	16.6	17.6	34.1	27.4	32.3	28.7	26.1	7.1
4	25.1	29.0	22.6	18.0	16.5	17.0	31.7	26.0	35.6	28.2	26.6	
'n	24.9	29.3	22.5	17.9	16.4	16.9	29.3	25.6	36.0	27.4	25.3	
Ś	24.2	29.8	21.9	17.7	16.3	17.0	28.4	30.6	37.0	26.3	24.5	
<u></u>	24.7	29.8	22.2	17.6	16.2	17.4	25.3	40.1	45.0	25.8	24.0	
æ	25.6	29.2	21.8	17.6	16.2	24.9	24.2	29.8	42.2	25.1	23.3	1
σ	26.0	28.0	21.2	18.2	16.1	27.4	24.7	27.1	41.1	24.6	22.8	
10	26.3	26.6	20.8	21.5	16.0	26,6	29.5	24.6	40.5	23.9	22.3	
11	25.6	25.6	20.5	21.3	16.2	23.2	32.0	23.2	38.6	23.4	22.1	1.0
12	26.9	25.0	20.3	20.4	. •	19.8	28.2	23.0	36.8	23.2	21.9	- 1
13	28.9	25.3	20.2	19.7	16.6	24.4	24.6	23.3	34.9	23.2	21.6	1
1.4	30.3	25.3	20.1	18.8		20.6	35.4	86.0	33.9	23.0	21.2	9 (
بر دی	31.7	24.7	19.9	18.4	•	19.6	33.9	151.8	32.2	23.0	21.3	
92	29.9	24.2	19.7	19.5	16.1	18.8	29.9	70.6	30.9	22.8	21.6	
17	28.5	24.1	19.4	19.3		18.3	24.5	63.8	29.9	22.7	21.4	100
18	27.6	24.2	19.5	18.4	15.8	18.4	23.4	105.9	29.0	23.7	21.1	
5	26.4	24.7	20.1	18.1		21.8	22.8	94.5	28.2	24.6	20.8	
20	26.0	26.4	19.7	17.9		20.4	23.4	68.3	27.3	24.5	20.6	
23	25.1	29.8	19.2	17.7		19.6	200	85 S	27.1	24.7	20.4	. "
22	% %	30.0	18.9	17.4	15.5	9.67	26.4	72.3	27.7	26.6	20.2	
23	29.5	31.7	18.7	17.3	15.7	21.6	24.1	57.5	28.2	35.1	19.9	
24	24.9	30.3	18.6	17.2	16.2	20.7	23.9	67.8	33.4	31.5	20.2	1.0
23	34.1	28.0	19.6	17.5	15.6	6.61	23.5	39.4	34.1	32.8	20.2	
56	33.2	26.6	19.8	17.0	15.7	19.3	22.6	37.0	44.3	29.2	19.8	. 3
27	31.9	25.3	19.4	16.9	15.6	20 0.0	22.3	35.4	39.9	27.0	20.4	
28	29.9	25.1	19.1	16.9	16.2	114.3	22.6	46.8	35.4	27.7	21.4	
53	28.6		18.9	16.9	16.6	137.4	27.6	41.8	33.0	26.4	21.6	
ဓ္က	27.3		18.8	ŝ.	16.5	56.0	24.7	38.3	31.4	25.0	26.1	100
7	77.0		0		, ' r r		000	7) i		

DAY JA									;			
	JAN. F	FE3.	MAR.	APR.	HAY	THAT	JULY	AUG.	SEPT.	oct.	MOV.	DEC.
1 28	28.6 2	23.0	25.0	19.4	16.6	17.7	215.7	24.3	17.1	60.2	7.96	155.5
2		2.7	24.9	19.1	16.6	18.3	83.0	19.8	17.1	43.2	185.6	122.8
3 23		5.3	25.0	18.9	16.6	18.2	38.7	53.9	14.5	36.1	120.1	102.0
4 27		26.4	24.5	18.8	16.6	17.2	24.8	28.8	12.9	30.2	89.3	4.06
5 26	. 7	26.3	24.9	18.7	16.8	16.8	18.7	24.8	12.2	298.8	74.8	60 60 60 60
97 9	. 2	25.1	24.5	18.6	18.5	16.5	15.4	23.2	12.6	176.8	242.2	77.7
22	۳.	24.1	22.7	18.2	18.5	16.4	15.8	53.9	12.6	109.0	232.1	46.7
ह्य 8	7.	3.7	22.6	18.0	17.6	16.5	13.7	87.2	11.2	78.7	209.5	43.8
9 28	3.9	<u>س</u>	22.5	18.2	17.0	16.8	22.6	53.0	11.9	97.8	151.8	40.6
10 36	5.5	3.2	22.0	18.4	16.7	16.6	16.7	60.2	17.1	92.5	200.7	39.3
11 44	4	2.7	21.5	18.2	16.6	18.3	13.7	58.4	12.9	77.7	139.1	39.3
12 40	~	22.8	20.7	18.0	16.4	17.6	12.2	36.1	13.2	83.0	194.4	38.7
13 35	-	26.4	21.3	18.4	16.3	17.0	16.7	29.5	18.1	53.9	239.7	40.4
14 31	•3	26.7	21.9	18.6	16.2	16.8	13.7	25.4	23.2	47.7	303.8	7.67
1.5 29	.2	27.0	22.2	18.3	16.6	16.6	17.1	24.3	30.2	39.6	413.2	94.5
16 35	9	5.7	21.1	17.8	16.9	17.0	41.4	21.5	31.7	34.6	336.5	259.5
	٠,	25.4	20.1	17.6	18.0	17.6	28.2	19.8	50.3	31.7	332.7	128.6
	-	25.7	19.4	17.4	17.9	18.2	18.1	7 80 T	60.2	29.5	263.6	83.1
		24.2	20.2	17.4	17.2	17.9	17.5	17.1	53.0	27.7	198.2	0.48
26 24		23.0	20.6	18.2	18.7	17.1	13.7	16.2	34.6	33.1	170.6	64.3
		22.5	21.1	17.8	19.7	16.6	13.2	16.2	66.0	222.1	379.2	61.3
	φ.	1.9	20.5	18.4	20.3	16.6	11.9	16.7	65.0	132.8	199.5	56.9
23 23	6.	1.6	19.8	18.0	20.6	17.8	11.6	15.4	45.9	81.9	184.4	52.5
	•	1.1	20.8	17.4	20.3	6.6	11.6	14.1	38.7	60.2	203.2	48.2
25 23	6	20.8	20.8	17.2	20.7	9.1	12.6	17.5	× .00	50.3	283.7	8.44
~	o.	3.5	20.4	17.1	21.5	8.6	14.5	16.2	36.9	51.2	229.6	63.3
	•	6.1	20.6	16.9	20.5	11.2	32.4	18.7	33.1	49.5	288.7	43.3
	1.7	ان ده.	20.8		19.8	10.6	51.2	38.7	53.9	42.3	202.0	40.7
7		9.4	21.3	16.8	19.3	19.8	31.0	30.2	65.9	56.6	311.3	39.7
23	•		20.7		18.7	273.6	35.3	19.8	68.1	86.1	207.0	39.7
	*	•	20.1		17.4		31.2	25.3		\$6.4		44.1

(Unit: cms)

Year 1965

7*****													<u> </u>			-																
DEC.	67.9	73.4	55.7	45.0	45.0	36.9	38.7	34.6	31.7	28.8	27.7	26.5	41.4	37.8	30.2	27.7	30.2	114.0	50.3	43.2	35.3	31.7	29.5	27.7	27.7	42.3	48.6	41.4	55.3	41.4	36.1	
NOV.	20.9	20.3	19.8	18.7	26.5	21.5	36.9	109.0	81.9	57.5	45.0	30.2	30.2	28.8	25.4	24.3	23.2	22.0	39.6	26.5	23.7	22.0	31.0	53.9	81.9	36.1	67.1	60.2	45.9	36.9		
OCT.	20.9	65.0	43.2	34.6	31.7	30.2	28.2	54.4	34.6	40.5	30.2	26.5	25.4	24.3	22.6	22.0	19.8	19.2	43.2	36.9	34.6	33.9	31.7	30.2	28.8	26.5	24.3	24.3	23.2	22.0	21.5	
	52.1	Ė	- 11 11						٠.	: 13.			ă.	 . i.					53.9	37.8	: print	7	00	29.5	· ·	_	×2	ເປ	~	0		
	13.4						12.6	12.6	12.6	11.9				15.4					23.2	19.8	16.7	43.2	26.0	24.3	23.2	20.9	22.0	22.0	20.9	23.7	81.9	
JULY	13.2	71.3	22.0	18.1	16.7	15.8	15.0	15.8	15.0	15.0	58.4	24.3	27.1	71.3	52,1	39.6	35.3	33.1	27.1	24.3	29.5	17.5	16.7	35.8	20.3	15.8	15.88	15.0	14.1	15.0	1.41	
JUNE	7	12.6		7	C					. :			:	12.6								6.11	15.0	15.0	13.2	12.6	6.1	1.9	1.6	12.6	,	
MAY	22.0					4.1	3.2	5.0	3.7	2.6	3.7			13.7		:						. 4.	. :			٠		. :	. :		1.2	
IPR.	7.5					8.8	5.0	5.0	4.1	4.5	4.1						5.8	5.0	4.1	4.8	σ.		~	6.5	~	0	Ö	,	~	~	=	
MAR.	5.4	4.3	3.7	4.8	3.2	2.0	0.0	3.7	5.5	5.5	5.5	1.3	3.2	2.0	. 6 (1.5	0.9	0.0	1.9.1	9.8	E 80.0	9.2 3	3.8	1.7 2	3.7	3.1	3.7	2	м	T		
FEB. M.	ri.	1.4 24	1.6	7.5).2 2	. 8 22	3.6	3.6 2	5.0	3.2	4 2	1.6	.8	1.1 22	2	v	7		~	.7	1.2 19	. 8	1.	.8	3.	.8	.7	5 2	2	7	H	
	.7 33	.7	.1 34	.3 40	.8	.6 54	.6 48	.2 48	.2. 45	.0 43	6.	.6 39	.4 37	.3	30	.9 29	\$	•	.7	7	8	.2 28	.4 27	.0 28	.7 29	.9 28	.0 27	. 4 . 26	ထ့်	.2	6	
DAY JAN	1 43	2 40	3 36	4 32		 F			9 29	e. 		12 28	28	14 50	9*7	.6. 53			. i.		1 62	ě,		59 42	7	91	27 45	8 25	9 19	13	T F	
								-		~~	e	~~		<u> </u>		277		hand	_	٠,		۲۷.	1.4	(4	e.4	4	~	C.	~	ניין	(-)	1

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DEC.	213.3	218.3	386.8	282.4	169.3	173.1	124.0	110.2	92.5	7.96	57.5	24.3	71.3	71.3	65.79	77.7	72 6	67.1	67.1	65.0	62.0	83.0	77.7	62.9	37.8	33.1	110.2	168.0	234.7	205.8	149.2	
ΔQΔ.	31.7	25.4	22.6	20.9	19.8	19.2	18.7	17.1	15.8	28.8	31.7	28.2	25.4	22.6	20.9	23.2	22.0	24.3	31.0	28.2	607.3	664.0	361.6	301.3	19.3	88.3	188.2	359.1	262.3	168.0		
t S	12.6	12.2	11.9	11.9	12.6	13.2	19.8	23.2	19.2	16.2	15.0	14.5	14.1	14.5	24.5	56.6	8.97	37.8	29.5	25.4	39.6	32.4	29.5	27.5	27.1	23.7	22.0	20.3	20.3	39.6	31.0	
SEPT.	16.7	15.8	57.5	20.9	16.7	15.8	15.4	15.0	15.0	15.0	14.5	15.8	17.1	16.7	15.8	15.8	16.2	16.7	15.4	15.0	14.1	13.2	12.9	12.6	15.8	14.5	13.2	13.7	13.2	13.2		
AUG.	20.9	27.7	25.4	24.3	31.0	40.5	52.1	57.5	49.5	55.7	8.97	33.9	28.2	29.5	26.0	24.3	22.0	8.02	20.3	18.7	17.5	17.1	16.2	17.1	23.7	41.4	26.0	19.8	20.9	18.7	17.5	
July	13.2	12.6	11.9	13.2	11.2	11.2	14.1	14.1	15.0	15.0	15.8	22.0	17.5	19.8	16.7	19.2	22.0	16.7	33.1	37.8	23.2	19.8	23.2	8.7	24.3	19.8	17.5	31.0	26.5	23.7	27.1	
2000	25.4	24.3	21.5	19.8	8.2	8.9	28.9	28.2	80.3	20.0X	23.7	19.8	17.1	15.8	15.0	15.0	15.8	14.1	14.1	19.8	17.5	18.1	16.7	1.4.1	15.0	27.7	17.1	15.4	15.0	13.7		
¥	11.2	11.2	10.6	10.6	11.2	12.6	12.2	11.2	11.2	12.6	14.1	12.2	11.2	10.6	10.6	9.9	23.2	12.2	23.2	69.2	7.9%	12.6	53.9	196	\$.06	256.0	230.9	89.3	52.1	33.1	28.00	
F.	12.6	11.9	11.2	10.6	10.6		9.9	. 7.6	4.6	7.6	6.6	9.0	9.7	4.6	9.6	4.6	9.4	1.6	4.6	4.6	4.6	9.1	6.8	60	9.7	6.6	7.6	4.0	4.6	9.1		-
MAR.	12.9	12.6	11.9	11.9	12.6	12.2	12.2	12.9	10.9	10.3	9.6	4.6	10.9	11.9	12.2	11.9	11.2	10.6	10.6	10.6	10.9	10.3	10.3	6.6	7.6	9.7	10.3	16.2	18.1	12.9	14.1	
E.	17.5	17.1	16.7	16.2	15.8	15.4	16.7	24.3	26.5	23.7	19.2	16.7	17.1	15.8	15.0	15.8	15.0	15.0	14.1	14.1	14.1	13.7	13.2	15.4	15.4	13.7	13.7	12.9				
JAN.	55.7	14.1	W. 8	31.0	31.7	8.2	28.8	27.7	28.5	24.8	24.3	22.6	22.0	21.5	20.9	20.3	19.8	17.5	16.7	16.2	24.3	25.4	20.9	18.7	18.1	17.5	17.1	26.0	18.7	18.7	18.1	
DA	~4	~	•	*	V)	•	•	•	•	19	11	12	13	14	23	7.6	P	1.8	13	20	21	22	23	24	25	56	27	28	29	ጸ	31	

1 101.0 30.2 3 106.4 28.8 5 86.1 35.3 6 70.3 27.1 26.3 10 53.9 23.7 23.7 112 46.8 26.3 14 26.8 26.3 14 26.3 14 26.3 14 26.8 26.8 14 26.8 14 26.8 14 26.8 16 26.3 17 26.3 18 26.3 18 26.3 18 26.3 18 26.3 18 26.3 18 26.3 26.3 18 26.3 26.3 26.3 26.3 26.3 26.3 26.3 26.3	22 19.2 117.8 119.2 116.7 119.2 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.9 120.	13.22 13.22 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.22.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23 11.23.23	10.6 10.6 10.3 9.9	9.9			, ,	7 17	20.3	1
n + p + m + m + m + m + m + m + m + m + m	2 1 1 2 2 3 3 3 4 4 1 8 . 7 4 8 8 8 1 8 . 7 4 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	13.2 12.2.2 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.2.6 11.6	10.6 10.3 9.9	9.7	6.3	٠	7.07	1	7.04	31.1
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8 52.1 24.3 10 53.9 23.7 11 46.8 24.3 13 46.8 25.4 14 51.2 25.4 17 88.3 23.7 18 71.3 23.7 19 61.1 20.5	2 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	11.9 12.6 11.9 11.9 11.9	6.6	9.7	7.6	12.6	32.4	92.5	180.1	39.5
9 56.3 11 66.8 12 46.8 13 46.8 14 51.2 25.4 15 88.3 23.2 18 71.3 23.2 19 61.1 20.5	2 23.7 2 23.7 3 20.9 5 20.3 18.7 17.5	16.2 12.6 11.9 11.9	6,6	11.2	6.8	32.4	24.3	37.8	104.3	38.4
10 53.9 23.2 12 46.8 24.3 13 46.8 25.4 14 51.2 25.4 15 88.3 25.4 17 880.8 24.3 18 71.3 23.2 19 61.1 20.5	2 23.7 20.9 5 20.3 20.3 18.7 17.5	11.9	7.6	14.1	10.6	21.5	36.1	27.7	105.3	37.0
12 46.8 26.3 13 46.8 25.4 14 51.2 26.5 15 88.3 23.2 17 80.8 24.3 18 71.3 22.0 19 61.1 20.9	2 2 2 2 2 2 2 2 2 2 2 3 3 3 3 3 3 3 3 3	26.69.	6.7	11.2	10.9	27.7	34.6	56.6	82.0	40.0
12 42.3 25.4 13 46.8 26.5 14 51.2 24.3 15 88.3 23.2 17 80.8 24.3 18 71.3 22.0 19 61.1 20.5	55 20.3 3 18.7 17.5	11.9	10.3	3. O	4.0	20.9	26.0	45.0	70.0	99.0
13 46.8 26.5 14 51.2 24.3 15 112.7 22.0 17 80.8 24.3 18 71.3 23.7 19 61.1 20.5	5 20.3 3 18.7 2 17.5	11.9	6.6	6	8.6	15.0	24.3	39.6	67.2	87.3
14 51.2 24.3 15 88.3 23.2 16 112.7 22.0 17 80.8 24.3 18 71.3 23.7 19 61.1 20.5	18.7	11.6	6.6	4.6	8.6	13.2	31.7	34.6	7.79	43.1
15 88.3 23.2 16 112.7 22.0 17 80.8 24.3 18 71.3 23.7 19 61.1 20.5 20.5 20.5 20.5 20.5 20.5 20.5 20.5	2 17.5		7.6	4.6	8.6	15.0	25.4	45.0	62.6	49.5
16 112.7 22.0 17 80.8 24.3 18 71.3 23.7 19 61.1 20.5 20 53.9 23.7	, , ,	11.2	7.6	4.6		14.5	24.3	36.9	66.3	43.9
17 80.8 24.3 18 71.3 23.7 19 61.1 20.5 26 53.9 23.7	17.7	11.2	11.2	9.1	. ec	1.4.1	23.7	5 67	65.4	44.7
18 71.3 23.7 19 61.1 20.9 26 53.9 23.2	3 16.7	11.9	11.9	& 6.	e0 60	52.1	34.6	124.0	72.8	46.3
19 61.1 20.9 28 53.9 23.2	7 16.2	12.6	12.9	න ග්	m 19	20.9	51.2	68.1	67.2	42.3
28 53.9 23.2	9 15.8	11.9	11.6	8.6	13.2	39.6	×.6	52.1	62.6	38.4
	15.8	11.6	11.9	e0 60	25.4	31.7	25.4	39.6	68.1	35.7
21 61.1 21.5	5 15.4	11.2	10.6	11.2	14.5	23.2	22.0	34.6	68.1	¥.
22 74.5 20.9	9 15.0	16.2	10.3	4.6	14.5	17.1	46.8	35.3	51.9	34.4
23 99.3 19.8	17.1	12.9	6.6	4.	14.1	15.0	30.5	32.4	52.7	ار ا
24 51.2 19.2	2 17.5	11.9	9.7	11.2	14.1	16.7	54.8	28.2	52.7	8
25 45.0 18.7	7 15.4	16.7	11.2	10.6	15.8	18.1	28.8	25.4	51.9	37.0
26 40.5 18.1	1 15.0	12.2	10.6	6N.	14.1	33.3	67.1	24.3	51.9	37.0
27 36.9 17.5	5 14.1	11.9	6.6	9.7	20.3	22.0	234.7	23.2	37.7	60.0
28 34.6 17.5	5 15.0	11.6		9.6	20.3	19.2	107.7	22.0	45.5	36.4
29 31.7	13.7	11.2	16.7	9.4	26.5	17.1	59.3	23.2	46.3	3.75
30 30.2	13.2	10.9	11.2	8.9	22.0	15.0	41.4	22.0	43.4	33.1
	13.2		6 6		15.8	14.1	, , , , , , , , , , , , , , , , , , ,	22.0	•••	37.7

DEC.	28.8	60	4		Ņ	0	0	*	o	o,	'n	Ŋ	1	·	'n	60	'n	60)	Fol		F-0	7	·	*	IJ.	pul.	7	Ø,	o,	O)	ø,
5	22	72	73	1	ind A	e i		#) # (का हर्म	\$ 7	₹	3.4	H	7	14	15	-4	5	77	er er			(*) pud	2 <u>4</u>	14	14	=======================================	kzd .A	***	2	H
MOV.	20.0	18.7	18.7	17.1	17.7	17.3	17.7	17.7	17.5	19.6	23.2	21.6	21.6	18.7	19.6	21.6	20.5	19.6	18.7	20.5	23.2	21.6	22.6	23.7	26.4	26.4	25.3	27.0	47.1	199.5	
5	23.2	21.0	23.2	30.6	25.8	45.0	24.2	20.5	19.6	18.7	17.7	17.7	18.7	19.6	23.7	33.1	30.0	31.2	24.7	23.2	22:1	21.0	20.8	17.8	19.6	18.7	18.7	17.7	18.7	18.7	18.7
SEPT.	20.0	18.7	17.7	20.5	21.6	16.7	18.7	17.7	16.8	16.3	19.6	21.6	22.6	6.63	62.3	31.8	27.0	23.7	22.6	20.5	0.17	20.5	22.6	18.7	17.7	16.8	16.3	26.4	30.0	28.2	
Y S	15.1	16.8	9.00	25.3	20.5	18.7	17.7	18.2	18.7	20.5	20.0	17.7	17.7	19.6	20.5	20.5	24.7	4.46	28.2	37.7	31.2	27.0	21.6	18.7	19.6	17.7	16.8	18.7	20.5	20.5	20.5
AL.	25.8	18.7	16.8	23.8	20.5	18.2	20.5	20.5	18.2	16.8	16.3	15.9	17.3	16.3	15.9	16.3	15.9	15.5	15.1	15.1	20.5	20.5	24.2	19.1	17.7	16.8	18.2	16.8	16.8	15.9	15.9
	33.1	33.1	37.0	22.6	37.0	35.1	35.1	25.3	46.3	26.4	27.0	23.2	20.0	1.8.7	17.7	16.8	15.9	17.3	17.7	22.1	17.7	18.7	22.6	19.6	17.7	17.7	17.3	16.8	21.0	24.7	
K	13.9	15.1	14.3	13.9	13.9	13.1	13.1	12.3	12.3	11.5	12.7	13.5	12.7	12.3	12.7	13.9	13.1	12.3	26.4	15.9	16.3	13.5	15.1	13.9	28.8	19.1	16.3	15.2	14.3	31.8	36.
APA.	60	6.3	7.9		9.0	8.7	5.6	9.5	9.5	9.6	9.5	5.6	9.8	. e.	9.5	9.5	9.5	9.5	9.8	9.5 S.5	9.1	9.1	9.1	9.5	10.3	9.9	6.6	6.6	22.1	16.3	
HAN.	13.9	13.5	13.5	12.7	12.7	12.3	11.9	11.9	11.5	20.5	20.0	15.1	13.5	12.3	11.5	11.5	19.1	15.9	12.3	11.5	11.1	11.1	10.7	10.3	10.3	9.1	9.1	9.1	9.1	9.1	•••
FEB.	21.0	21.6	20.5	19.1	18.7	18.2	18.2	18.2	17.7	17.3	17.7	17.3	16.8	19.6	17.3	16.8	16.3	15.9	15.1	14.7	14.7	14.7	15.1	15.5	15.5	15.3	15.5	14.7	14.3	Teat.	
JAN.	50.3	44.0	42.3	39.2	40.9	4.7	\$.0 \$	36.4	£2.3	47.9	46.3	40.0	37.7	78.4	33.1	31.8	31.8	30.6	28.2	27.0	26.4	25.3	24.7	24.2	23.2	22.6	22.1	21.6	33.1	28.2	22.6
A A	-4	~	~	*	¥'n	•	_	-	0	91	#	73	£3	14	53	2	17	8 2	19	2	য	22	23	24	22	X	27	28	82	8	31

			Table	e 2-4-13	(10)	Daily D	Discharge	at No.3 D	Damsite			(Unit: CES)	CB8)
	Year	Year 1969											
	DAY	JAN.	FEB.	MAR.	APR.	MAY	JUNE	JULY	AUG.	SEPT.	OCT.	MOV.	DEC.
	-	12.6	12.6	1.6	6.0	1.9	80	2.0	8.3	14.1	10.7	24.7	φ, φ,
	2	12.6		٠. 6	ص ت	4.1	w 00	2.0	6.7	8.9	11.1	23.7	69.1
	. m	12.6	12.6	9.1	7.3	4.4	4.1	2.2	4.6	8.6	E0.3	22.6	81.1
	7	12.6	11.9	9.	7.0	7.7	1.4	2.2	7.7	F. 6	10.3	21.6	80.2
	- L/1	12.6	12.2	8.6	6.7	4.1	6.7	2.0	N	6.6	15.1	19.6	82.0
	y ve	12.6	12.2	8.6	6.2	4.0	5.7	5.2	5.2	31.0	13.9	25.8	126.5
		13.7	11.9	8.6	6.2	4.6	6.2	8.1	5.2	86.1	12.7	27.0	52.7
	90	20.9	11.6	8.6	6.2	4.1	5.7	6.7	5.2	31.2	30.6	26.4	67.9
	.	22.6	11.6	9	6.2	80.00	5.2	5.7	5.2	20.5	28.2	22.6	63.5
	10	27.1	11.6	ာ	6.7	60 67	4.6	5.2	5.7	16.8	24.7	21.6	101.1
	=	19.8	10.9	8.1	6.5	ω. ભ	⊣.	4.4	6.4	14.7	20.0	24.2	144.5
	12	17.1		8.1	6.2	3.0	e.	3.8	4.6	13.9	18.2	25.8	1180
	.	17.1		, -i	5.7	•	3.6	3.6	6.4	13.E	21.0	22.6	87.3
	7	18.7		60	5.7	3.8	3.6	3.6	6.4	12.3	21.0	21.6	104.3
	5	17.5	10.6	7.5	5.2	4	3.6	3.6	4.9	12.3	17.3	20.5	85.2
	16	17.5		7.5	5.2	5.4	3.6	3.6	4.6	12.3	16.3	18.7	69.1
	17	20.50	10.6	7.5	5.2	4.9	6. 7	60	4	11.9	17.3	17.7	61.7
:	a 0	15.8	6.6	~. 6	5.2	4.4	9.69	N.	4	11.5	53.5	17.7	55.2
	2	60	6	8.3	5.2	6.5	en en	4.4	٠. ص	11.5	31.2	25.8	65.4
	20	15.0	Ø\	40	9.4	5.4	ም ም	4.1	4.6	11.5	4.49	44.7	73.7
	21	14.5	7.6	17	4.6	6.0	m m	4.6	6.7	11.9	53.5	74.6	65.4
	22	76.1	C &	7.3	9.4	7.0	3.0	5.7	9	13.5	45.5	61.7	75.6
	23	14.5	6.4	7.0	9.9	19. N	9	9	(B)	12.7	39.5	40.0	61.7
	24	F. 91	7.6	7.0	4.6	5.7	3.0	9.1	6.2	14.3	33.1	167.0	iol iol
	25	14.1	7.6	6.7	4.4	6.4	3.0	œ 3	5.7	12.7	9.5	133.9	63.0
: '	26	***	6	6.7	4.4	9.4	2.8	8.8	5.7	11.9	25.8	181.3	37.0
	27	13.7	9.7	6.7	4.4	4.4	2.2	6.5	5.2	11.1	24.7	101.1	37.7
	78	13.7	1.6	6.3	4.	4.4	2.2	12.9	₽	11.1	22.6	63.5	00° 00° 00°
	50	12.9		6.7	4.6	4.4	2.2	917	Ø.	- T	22.6	52.7	43.1
		12.9		6.7	4.1	7.7	2.0	7 6	6.9	10.7	33.1	54.2	46.3
	H	12.6		6.3		3.8		9.6	5.2		28.2		۳. ش
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r								7.					سنب				·····				-												
	DEC.	80.2	254.8	110.6	4.68	77.4	1.89	59.8	44.7	54.2	54.0	47.9	69.1	57.0	56.1	27.0	21.0	102.1	108.5	96.9	90.5	80.2	74.6	69.1	59.8	₹.95	55.2	54.2	52.7	51.1	50.3	49.5	
	. AON	146.7	124.4	104.3	89.4	78.3	72.8	76.5	97.9	119.1	108.5	86.3	120.1	90.5	79.3	71.8	135.0	137.1	122.3	327.7	372.9	136.0	111.7	95.8	108.5	100.0	87.3	76.5	7.76	92.6	79.3		
	8.	52.7	37.0	58.9	51.1	58.0	59.8	56.1	38.4	34.4	35.1	40.0	70.0	97.9	545.5	248.5	218.3	133.9	101.1	79.3	65.4	55.2	51.1	86.3	61.7	57.0	58.0	82.0	82.0	86.3	113.8	211.7	
	SEPT.	17.3	16.8	16.3	15.1	14.7	15.1	13.5	14.2	12.7	16.3	50.3	116.7	118.0	43.0	34.4	31.2	38.4	35.7	30.0	27.6	25.3	23.7	22.6	21.6	23.2	27.6	25.3	23.2	22.1	45.5		
	AUG.	11.9	10.7	10.3	10.3	10.3	12.3	14.3	15.5	13.5	15.1	18.7	37.0	25.3	19.6	20.5	25.8	27.6	21.6	18.2	16.8	17.3	28.2	22.6	19.6	21.0	31.8	36.4	25.8	20.5	19.1	19.1	
	JULY	12.7	12.3	11.9	7.3	w	11.5	11.5	11.5	11.1	77.7	17.7	11.9	13.9	15.1	13.9	12.7	11.5	10.7	6.6	6 6	9.5	11.9	11.1	9.5	9.1	8.7	8.7	8.3	8.7	15.5	15.5	
	THE C	11.1	15.5	19.1	23.7	21.0	19.6	22.6	21.6	19.6	19.6	18.7	19.6	20.1	29.1	18.2	17:7	16.8	16.8	19.1	17.1	15.1	16.8	18.1	17.7	15.9	15.1	14.3	13.5	13.1	13.1		
	MAY	18.5	15.9	14.3	13.5	12.7	13.9	13.9	13.9	13.5	13.1	12.7	13.1	15.5	15.9	16.8	13.5	13.5	13.5	13.9	14.3	13.9	12.7	12.3	11.9	11.5	11.9	12.7	13.5	13.5	12.7	12.3	:
	APR.	12.7	12.7	12.7	12.7	15.5	14.3	13.5	12.7	12.7	12.7	12.7	12.3	12.3	11.9	11.9	11.9	11.9	11.9	11.9	11.9	13.5	15.1	17.7	14.7	13.1	14.3	15.1	14.7	17.3	17.7		
	MAR.	16.3	17.7	16.3	15.5	15.5	16.8	15.9	15.5	15.9	15.9	15.1	14.7	14.3	14.3	13.9	13.9	13.5	13.5	13.5	13.5	13.5	13.1	13.1	13.1	13.9	13.5	13.5	13.1	12.7	12.7	12.7	*.
	FEB.	20.5	20.5	20.5	20.0	19.6	21.6	21.0	18.2	20.0	18.2	20.0	19.1	19.1	18.7	18.2	17.7	17.3	17.3	16.8	16.3	16.3	16.3	16.3	15.9	15.5	16.3	15.9	15.9				
	JAN.	52.7	49.5	58.9	60.7	52.7	51.9	53.5	51.9	52.7	44.7	58.9	47.1	4.1.5	38.4	37.0	35.7	35.1	33.7	32.4	31.2	28.2	28.8	27.0	26.4	25.8	24.7	23.7	23.2	22.6	22.1	20.5	
	MY	-	7	m		'n	ø	_	₩	0	9	1	12	13	7 4	15	16	17	2	64	20	21	22	23	24	25	56	27	58	53	9	31	

Year 1971	1971											
DAY	JAN.	FEB	MAR.	APR.	MAY	JUNE	JULY	AUG.	SEPT.	OCI.	MOV.	DEC.
	65.4	21.0	0	38.4	22.1	33.7	30.3	41.5	264.0	51.1	38.4	142.4
7	92.6	21.0	19.6	37.7	23.2	47.1	26.4	37.0	50.3	40.8	32.4	121.2
ന	95.8	20.5	19.1	34.4	24.7	8.0%	24.7	25.8	52.7	23.2	36.4	102.1
4	165.8	21.0	18.7	31.8	28.8	35.1	29.4	28.2	48.7	31.2	37.0	82.0
'n	58.9	27.6	20.0	28.2	25.3	31.8	35.1	24.2	41.5	209.5	34.4	78.3
•	55.2	28.2	19.6	30.0	28.2	28.6	28.2	23.2	47.1	144.5	35.1	67.2
7	47.1	28.8	17.7	29.4	33.1	29.4	45.5	24.7	30.6	86.3	33.1	147.9
6 0	43.1	29.4	17.7	25.3	27.0	30.6	37.0	23.7	31.8	69.1	35.7	70.0
9	39.2	31.2	17.3	30.0	28.2	30.0	35.7	23.2	37.0	200.1	44.7	97.6
10	43.1	28.8	16.8	30.6	35.1	28.8	60.7	22.6	8.0%	613.9	91.6	144.5
11	8.04	28.2	16.8	28.8	36.4	27.0	35.1	21.6	36.4	334.0	225.9	243.5
12	37.0	27.0	42.3	27.0	58.9	31.8	79.3	21.0	34.4	242.2	84.2	140.3
13	33.7	27.6	81.18	32.4	70.0	31.8	55.2	20.5	30.6	213.3	59.8	93.7
34	30.6	23.7	178.9	30.6	43.9	32.4	58.0	21.0	38.4	152.7	47.9	75.6
155	28.8	22.8	120.1	26.4	72.8	37.0	57.0	21.0	30.6	133.9	8.07	F69.1
91	28.2	21.6	79.3	25.3	62.6	59.8	60.7	20.5	33.7	120.1	35.7	60.7
17	27.0	22.6	65.4	28.8	53.5	68.1	55.2	20.0	27.6	93.7	31.2	67.2
18	27.0	30.0	53.5	28.2	55.2	8.03	109.6	19.6	23.2	81.1	82.0	79.3
51	4. 92	51.9	45.5	24.2	47.1	36.4	78.3	18.2	20.5	1.69	195.2	90.5
92	25.3	45.5	42.3	25.3	68.1	34.46	58.0	17.7	19.6	60.7	85.2	78.3
7	24.2	32.4	39.5	23.7	4.49	32.4	44.7	17.7	14.3	52.7	139.2	68.1
22	23.2	90.0c	34.4	27.0	67.2	29.6	35.1	17.3	43.1	60.7	74.6	101.1
23	22.6	27.6	33.1	27.6	36.4	28.2	33.7	17.3	24.2	68.1	87.3	90.5
77	22.1	25.3	35.7	27.0	31.2	28.2	43.1	17.3	23.7	79.3	243.5	73.7
23	21.6	23.7	33.7	27.6	28.2	31.2	37.7	17.3	24.2	86.3	6.985	62.6
23	21.0	22.6	32.4	25.8	28.2	28.2	35.7	16.3	20.0	73.7	213.3	52.7
27	22.6	21.0	30.6	24.2	30.6	30.0	31.2	16.3	26.4	67.2	165.8	47.9
58	23.7	20.5	33.1	23.7	34.4	28.2	28.2	16.3	37.7	61.7	125.4	8.04
29	28.8		32.4	21.6	57.0	35.7	27.0	15.9	47.1	57.0	111.1	35.1
<u>۾</u>			34.4	22.1	28.8	51.9	27.0	15.9	35.1	43.9	126.5	31.2
<u>ਜ</u>	23.2	÷ .	37.0		28.5		30.0	15.9		39.2		61.5

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Deily Discharge at No.3 Demsite

(Unit: cms)

	N. W.	FEB.	H.	Z X		150	1707	AGE:	SEPT.	55	NOV.	DEC:
~	95.7	14.1	6.5	5.7	5.9	4.0	1.6	22.0	11.9	6.6	7.0	55.7
7	113.9	13.7	6.5	10.9	6.2	1.8	1.6	19.8	11.6	9.7	6.7	× ×
in.	78.7	12.9	6.7	~ 6	6.2	7.3	3.6	18.7	11.6	10.9	6.5	53.0
*	₩ \$3	11.9	6.7	E 2	0.9	7.0	7.8	15.8	12.6	10.3	6.2	50.3
'n	51.2	10.9	7.0	6.5	0.9	9.7		13.7	11.9	10.3	7.3	49.5
•	47.7	9.9	6.7	6.2	9	8 .3	7.3	11.9	11.6	9.9	4.6	65.39
_	52.1	4.6	6.7	2.9	5.7	7.5	414.4	11.2	11.2	39.6	131.6	45.0
**	58.4	8.9	6.5	0.9	7.1	7.0	92.5	10.9	19.8	18.7	26.5	\$. Z\$
•	57.5	6.8	6.5	6:5	5.7	6.2	55.7	9.7	1.9.2	31.9	26.0	38.7
유	62.0	8	ه. د	7.8	5.7	0.9	23.2	34.6	18.7	11.2	34.7	37.8
===	53.9	7.9	6.2	8.1	9.9	. N	28.8	30.2	49.5	14.2	18.1	36.1
1.2	9.75	⊷ •••	6.2	9.1		5.4	23.7	28.2	43.2	10.3	16.7	35.3
£3	13	8.1	6.5	11.2	6.0	5.4	23.7	27.1	33.9	9.1	15.8	59.3
77	30.5	۳. *	7.0	9.1	5.7	5.4	19.8	24.8	22.6	9.	14.5	79.8
15	25.4	~	6.5	8.1	. 6.2	5.7	17.5	19.8	19.8	8.6	15.4	68.1
97	24.3	8. 3	6.2	8. 3	5.7	0.9	16.7	15.0	18.1	 	14.5	58.4
7	20.3	7.00	6.2	7.5	11.9	60	17.1	13.2	17.1	7.8	13.7	47.7
40	7.1		6.2	6.5	9.6	 100	47.7	12.6	16.2	7.5	16.2	45.0
6	16.2	7.3	0.9	6.5	12.2	T. 80	0.9	5 . T	15.0	7.5	13.7	43.2
20	15.4	٠, س	6.7	6.2	14.5	7.8	26.0	15.4	13.7	7.3	15.0	4.
21	15.0	7.3	6.9	0.9	13.7	7.5	17.1	14.5	12.9	7.3	14.5	37.8
22	74.5	7.0	დ ლ	0.9	19.8	7.0	17.5	13.2	12.6	7.0	24.5	39.6
23	14.5	7.0	7.0	5.7	15.4	7.0	15.4	69.2	11.9	æ 	15.8	31.7
7.	14.1	7.0	6.7	5.7	15.8	2.9	13.2	16.7	11.6	8.1	15.5	28.8
25	14.5	6.7	6.5	6.3	19.2	8.1	11.9	13.7	11.2	7.8	52.1	27.7
56	12.9	6.7	6.2	#.T	15.8	13.2	10.9	12.9	10.9	•	74.5	23.7
27	11.6	6.7	6.2	7.3	14.5	8	10.3	12.6	10.9	7.5	73.4	26.5
28	7.7	6.7	6.0	6.7	12.9	10.6	6.7	12.6	11.9	5	68.1	26.0
29	14.1	6.5	0.9	\$: 9	14.1	10.6	38.7	12.2	10.9	7.3	63.9	47.7
ጸ	18.1		0.9	4.7	13.2	9.7	62.9	11.9	10.6	7.3	60.2	24.3
3	16.2		0.9		10.9		25.4	11.9		7.0		24.3

Daily Die	
(14)	
2-4-13	
able	

		Table	le 2-4-13	(14)	Daily D	Daily Discharge	at No. 3 D	No. 3 Damsite		•		
Year 1973	973										Contra	cms)
DAY	JAN.	FEB.	MAR.	APR.	MAY	JUNE	JULY	AUG.	SEPT.	oct.	NOV.	DEC.
H	23.7	15.4	7.8	0.9	4.9	0.9	6.0	5.4	۳ 8	4.4	28.8	53.0
7	23.2	14.5	7.8	5.7	8.	6.2	5.4	6.4	80 (M	₩. M	23.2	45.9
m	22.6	14.1	75	5.4	٠. ص	6.2	5.2	6.0	9. 9		22.0	38.7
4	22.0	13.7	7.5	4:5	7.5	6.2	6.4	0.9	2.5	9.4	21.5	31.7
1	22.0	13.2	7.5	5.7	7.5	5.4	4.6	6.0	1.7	5.6	20.3	50
•	22.6	13.2	6.7	5.7	7.0	5.2		5.7	6.0	13.2	31.0	31.7
_	22.0	12.9	6.7	5.7	7.0	5.2	5.4	3.6		25.4	29.5	30.2
90	24.3	11.9	6.7	5.7	6.7	5.4	5.2	5.2	7.5	26.5	39.6	57.5
o,	24.8	11.9	6.7	5.7	6.7	5.7	6.4	7.5		17.5	29.5	60.2
10	23.2	12.6	9	5.7	7.0	N.	6.2	6.2	H. 6	16.1	28.8	67.1
11	22.0	12.2	6.5	5.4	6.7	1 2	5.2	6.5		9.11	24.8	68.6
12	22.6	10.9	ار د د	6.7	6.7	4.4	7.0	4	5.2	10.9	22.6	46.8
13	21.5	10.6	6.2	6.2	6.5	7.4	7.3	w.	6.4	9.6	22.0	45.9
14	20.9	6.6	6.2	6.0	7 6	9.5	7.0		6.7	87.2	33.9	43.2
15	21.5	4.6	6.2	6.0	ω	6.9	6.7	Ö	щ 90	180.6	17.5	39.6
16	20.9	9.7	6.5	6.0	60	4.4	6.7	2.5	6.5	212.0	57.5	34.6
17	20.3	4.6	7.0	6.0	 60	4.4	7.7	2.0	4.4	163.0	50.3	29.5
80	18.7	4.6	~: e 0	5.7	7.8	4.1		11.2	3.6	74.5	47.7	27.7
19	18.1	1006	e0	5.7	80	4.4	O.	4.7	2.00	48.6	104.1	27.1
20	17.5	Ø.	7.8	~; &)	<u>ο</u> ν	. T. 9	2.00	7.0	5.2	41.4	110.2	34.6
21	17.5	***	7.0	ed 80	7.5	124 18	2.5	19.2	4.4	27.7	262.3	52.1
22	16.2	8.9	رة ال	ත හ	٠. س	4.1	2.2	16.2	4	16.2	331.5	93.8
23	16.2	9.	6.2	ે. છ.•	7.0	တ က	•	6.2	ଟ୍ଟ	13.7	490.2	169.3
24	15.8	9.6	0.9	6.3	6.7		. •	4.4	F. 60	11.9	253.5	96.3
25	15.8	8.6	0.9	60	6.5	4.1		3.6	o. 0	13.2	114.0	61.1
5 8	15.4	9.0	5.3	T. 60	6 5	മ ന	1.7	e. C	6.3		109.0	51.2
27	15.4	.e.	۲. ا	7,00	6.2	ന	2.2	0.e	4.1	15.0	. •	60.2
28	15.0	9.00	0.9	7.8	0.9	က ဆ	2.0	e0 e0	3.6	13.7	57.5	60.2
.59	16.2		5.7	7.8	0.9	ю М	1.1	ю •	, 63 63	17.5	. *	35.3
ଛ	17.5		5.7	ੂ • •	5.7	9.0	1.7	3.6	7.8	21.5	43.2	127.8
#			Ç.				c			C (7		7 7 7

	TOPT	//T) (T-+-7 STORT	(17)			THE PARTY OF THE P					
Tear 1974							*			(Bait:	(38)
JAN.	FEB.	MAR.	APR.	XX	JUNE	JOEZ	AUG.	SEPT.	OCT.	MOV.	DEC.
1.4	11.2	11.6	3.6	7.3	90°	12.6	14.1	12.6	14.5	38.7	129.1
9.9	10.6	9.4	4.1	6.7	8.	12.2	13.7	12.2	14.1	62.9	105.2
9.2	6.6	7.6	4.6	6.2	3.8	11.9	13.2	11.9	7.37	126.7	9.99
9.9	9.7	8.3	4.4	5.6	3.6	11.6	13.2	11.2	13.7	139.1	93.5
7.5	4.0	~ · ·	4.4	5.2	3.6	11.2	13.2	10.3	13.2	134.1	87.2
7.	9.1	7.5	4.1	6.4	3.3	11.2	12.9	6.6	13.2	127.8	77.7
1.4	9.1	7.3	4.1	4.4	3.0	10.9	18.1	6.6	12.9	120.3	59.3
2.3	9.	7.0	3.8	4.1	9.°C	11.9	16.7	9.7	12.9	110.2	55.7
0.5	9:0	6.5	3.6		2.8	11.9	16.2	6.7	12.6	300.0	11.5
36.9	8.3	6.2	3.6	3.8	264.8	12.2	15.6	9.6	12.2	180.6	49.5
9	9.6	6.0	3.6	3.6	439.3	12.2	15.0	9.1	20.3	89.3	25. 6
33.1	6.6	6.0	m;	3.6	3.00.5	11.9	14.5	10.3	N.0.	67.1	117.8
32.4	4.6	5.7	3.3	4.1	105.2	11.6	16.1	14.5	25.3	63.9	115.2
•	9.1	5.7	e e	90 F7	40.5	11.2	18.7	43.2	22.6	61.1	116.0
34.6	• •	4.60	3.0	3.6	31.0	10.9	18.7	5.90	24.3	153.0	111.5
36.0	9.	5.4	3.6	3.3	20.9	10.6	16.7	31.0	27.7	86.3	175.6
25.4	8.6	4.4		м Э	12.2	10.3	25.4	25.4	6.904	47.7	155.5
24.8	8.3	5.2	9.6	D .0	11.2	15.0	26.0	21.5	186.9		153.0
22.0	.	5.2	3.3	0 ·ń	10.9	15.0	22.0	20.3	A. 99.	49.3	150.4
	₩.	6.4	M .	2.0	10.6	53.9	19.8	19.2	5.04	53.9	169.2
18.7	T. **	4.9	3.0	2.8	10.3	45.0	17.1	18.7	37.8	62.0	184.4
17.1	7.6	6.4	A.0	2.5	6.0	28.5	13.8	18.1	**	60.2	T . CO
9	7.5	9.4	***	2.5	6.6	13.7	14.1	17.5	33.0	56.6	163.0
16.7	۷.0	9.4	2.4	2.2	9.7	17.1	13.7	17.1	33.9	53.0	161.8
17.5	6.7	4.4	2.8	2.2	9.6	16.2	13.2	16.7	33.3	48.6	160.5
16.2	6.5	4.1	2.5	3.6	3.6	15.8	12.9	16.2	33.1	45.9	159.2
FS. 8	⊙	4.1	2.5	9.4	4.6	15.4	12.6	15.8	32.4	42.3	154.2
13.8	E1.9	¥.	3.3	en en	₽. #8	13.4	12.2	15.8	47.7	39.6	150.4
5.4		3.8	ю. М	3.3	6.3	15.0	13.2	15.4	40.5	215.8	147.9
13.7		3. 8	0,4	4.4	9.0	14.5	12.9	15.0	43.2	155.5	144.2
		•		1		1					

DEC.	8.44	45.6	43.6	40.8	38.4	36.9	38.0	46.5	8.03	39.6	37.3	34.6	34.2	33.8	33.1	32.4	31.6	30.2	30.5	29.8	29.8	30.9	32.0	35.0	38.0	39.6	41.2	42.8	8.07	35.7	34.2	
NOV.	24.5	24.9	27.0	23.5	24.9	34.2	35.4	30.9	30.2	28.0	28.4	27.7	27.3	33.8	39.6	36.9	35.0	33.1	36.9	38.8	7.07	36.9	37.7	38.4	39.2	50.7	49.4	47.3	8.77	44.4		
00 1.	38.4	8.69	75.5	80.9	64.3	52.4	46.0	42.0	39.2	36.9	36.1	40.0	35.0	23.2	27.7	33.1	32.0	30.5	29.8	29.1	29.4	29.1	28.4	29.4	29.I	27.7	27.0	26.6	26.6	25.9	24.9	
SEPT.	23.5	34.6	30.5	25.6	28.7	27.0	28.4	24.2	25.2	27.7	27.0	23.2	22.9	23.2	26.3	25.6	32.4	29.1	31.3	34.6	29.4	26.3	28.4	27.0	24.9	23.9	39.6	33.8	35.7	37.3		
AUG.	32.4	25.9	24.2	35.4	30.2	26.3	26.3	24.2	29.1	30.2	28.0	24.9	23.9	22.9	21.5	20.9	20.2	19.6	19.3	18.7	18.4	17.7	17.4	17.1	16.8	17.1	22.5	19.0	17.7	20.9	19.6	
JULY	22.9	21.2	34.6	38.4	29.4	24.9	25.9	36.9	29.4	24.9	23.5	22.9	22.5	26.3	30.5	25.2	21.9	20.6	19.9	20.2	26.6	22.5	19.9	19.0	19.0	32.7	47.3	36.5	28.4	25.9	26.6	
JUNE	17.4	20.2	28.0	7.67	25.6	21.5	19.6	23.9	38.0	38.8	28.0	23.5	20.2	18.7	20.2	18.4	18.7	19.3	18.4	17.4	16.8	16.2	28.4	21.5	20.5	22.2	24.5	29.8	27.0	22.2		
MAY	16.5	15.3	14.2	14.7	14.5	14.2	13.9	13.6	13.3	13.3	13.0	13.0	I.5.3	16.5	16.5	17.7	15.3	24.9	24.2	18.7	16.5	15.3	14.5	14.7	35.0	27.0	21.5	19.0	17.7	18.4	16.5	
APR.	13.6	13.3	13.0	13.0	13.0	13.0	13.3	13.0	13.0		12.5	12.5	12.2	12.2		12.5	15.0	14.7	14.2	15.6	31.3	22.2	35.0	23.2	19.9	17.1	15.9	15.9	30.2	19.0		
MAR.	11.6	11.9	11.9	හ හ	10.9	10.9	10.6		o	•	•	•	•	6.3	٠.			Τ,		13.6	~		14.2	17.7			-	14.7	•	13.9	•	
EEB.	14.5	4	13.9	m	m	m	m	6	ė	'n	2	ς.	4	ä	N	ď	2	ζ.	ä	-	_;	÷		0	0	å	ö	d.				
JAN.	20,9	•		o,	σ,	Ġ	23.2	ď	N	÷.	-		•	18.4		•		•	•				Š	'n	4	14.5	ব	n	m		C.J	
DAY	e-l	7	m	*	5	9	_	60	8	10	11	12	13	77	15	16	17	18	19	20	21	22	23	24	25	76	27	28	29	30	TE .	

Table 2-4-14 Discharge Duration at No.3 Damsite Table 2-4-1

		Maximum	95-day	185-day	275-day	355-day	Minimum	Annual Mean
	Iear	(m ³ /sec.)	(m ³ /sec.)	(m³/sec.)	Ulscharge (m³/sec.)	Ulscharge (m3/sec.)	Discharge (m ³ /sec.)	Discharge (m³/sec.)
<u>.</u> .								
	1960	233.56	35.78	27.14	21.88	18.33	17.53	32.0
	1961	264.04	29.03	24.36	19.95	16.55	16.17	28.0
	1962	330.51	30.49	25.14	20.27	17.44	16.78	29.4
	1963	298.31	29.76	24.49	19.95	16.02	15.53	28.6
	1964	413.16	43.31	23.74	17.97	12.24	9.13	8.64
	1965	137.87	33.87	24.28	14.95	11.58	10.59	28.7
:	1966	607.33	27.52	17.53	13.23	9.39	28.87	37.0
	1967	602.37	37.71	20.91	11.91	8.87	8.34	32.6
	1968	199.47	22.10	17.73	14.69	9.13	አ ራ	20.2
	1969	181.27	17.27	9.13	06.4	3.04	1.98	18.3
	1970	545.54	69.69	18.66	13.50	9.92	7.28	38.8
	1971	613.95	57.03	33.74	26.40	17.27	14.29	52.1
	1972	414.41	18.09	11.25	7.28	5.69	5.42	19.2
	1973	490.23	17.53	7.54	5.42	2.25	0.93	20.9
	1974	439.29	33.15	12.90	6.22	2.78	2.25	o. %
	1979	80.85	29.80	22.20	14.74	10.32	8.80	23.9
	Average	365.76	32.00	20.05	85 71	94	•	9

Monthly Riverflow at No.3 Damsite for 1960 ~ 1974 & 1979 Table 2-4-15 Monthly Riverflow at No.3 Damsite for 1960 ~ 1974 & 1979

		,	 	·	<u> </u>		·		r			 					·	
Mean	22.010	28.010	29.403	28.621	49.789	28.745	36.972	32.557	20.191	18.269	38.810	52.062	19.151	20.926	34.003	23.938	493.457	30.841
Tota1	384.115	336.123	352.832	343.453	597.472	344.940	443.667	390.680	242.293	219.229	465.724	624.740	229.810	251.112	408.039	287.259	5921.488	370.093
Dec.	31.223	41.815	39.134	46.487	71,081	41.895	120.853	42.580	15.752	71.412	71.683	87.467	42.759	56.244	122.145	36.856	939.381	58.711
Nov.	29.253	46.718	55.235	22.253	223.107	38.898	109.895	97.333	27.687	46.829	118.110	102.675	28.937	85,499	95.377	34.998	1162.806	72.675
Oct.	56.057	24.991	32.574	26.290	76.488	30,790	23.702	40.352	22.694	25.345	97.619	113.572	10,052	38,397	45.325	37.608	711.856	44.491
Sept.	30.179	26.369	30.914	34.425	33.071	38.444	16.650	41.329	22.853	16.076	31.242	41.170	16.814	698.4	16.816	28.561	429.782	26.861
Aug.	35.981	24.587	84.123	48.530	29.814	22.568	28.743	19.869	21,781	5.288	19.892	21.254	18,318	6.843	15.749	22.842	375.182	23.449
July	24.503	28.406	28.394	27.373	29.477	25.809	19.951	12.826	18.121	5.436	11.149	44.281	37.255	4.375	15.934	26.660	359.950	22.497
June	24.866	19.742	18,213	28.433	24.635	13.081	19.380	9.811	24.042	3.802	17.709	35.282	7.714	4.675	41.738	23.141	316.264	19.767
May	19.476	21.502	19.786	16.180	18.099	13,509	41.996	10.624	16.179	4.635	13.701	41.242	10.038	7.269	3.923	17.251	275.410	17.213
Apr.	21.311	18.093	22.501	18.228	17.985	16.555	9.778	12.487	10.01	5.619	13.534	28.888	7.302	6.642	3.440	16.487	228.064	14.254
Mar.	26.528	24.158	20.970	20.413	21.752	21.795	11.676	18.167	12,412	7.866	14.897	41.543	6.516	6.680	5.751	12.696	273.320	17.083
Feb.	28.204	22.355	23.066	27.274	24.165	36.084	16.413	23.774	17.028	10.805	18.203	27.191	8.618	10.856	8.856	12.321	335,213	20.951
Jan.	36.534	27.387	27.922	27.567	27.796	45.512	24.630	61.528	33.730	16.116	38,485	40.975	35.492	19.763	32.985	17.838	514.260 335.213	32.141 20.951
	1960	1961	1962	1963	1964	1965	1966	1961	1968	1969	1970	1971	1972	1973	1974	1979	Total	Mean

Method of Obtaining Inflow to Diduyon Reservoir

				******	***		0b:	er	vat	lon	Pe	ri	od	(Y	ear	;)		***************************************	Equation for
Location	Site	C.A. (km²)	1960	1961	1962	1963	1964	1965	1966	1967	1968	1969	1970	1271	1972	1973	1974	1979	Conversio
Cosovan R	Pangal (BPW)	4,244	•	•	•	•	•	•	•	•	•	•	•		•				y = ax + b
Haddalarni.	Aglipay (BPW)	721	- 0	i.		il O	•	•	•	•	•	•	₩	6		•	1		y = ax
	Diduyon Damsite	477	0	0	0	0	O f	0	0	0	0	0	0	0	0	0	0	0	
O O O O O O O O O O O O O O O O O O O	Kamamasi (NPC)	462																•	y – ax

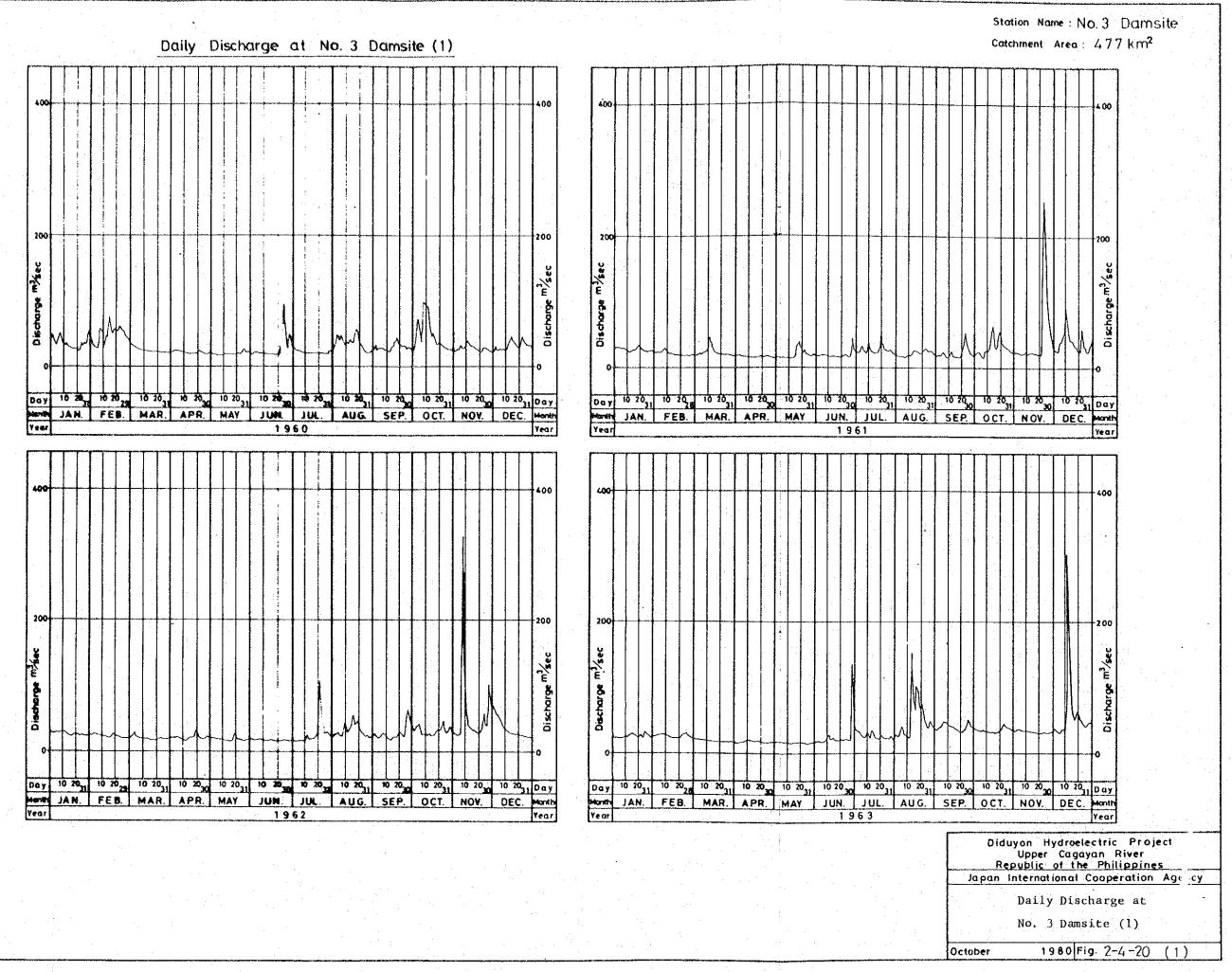
Remarks:

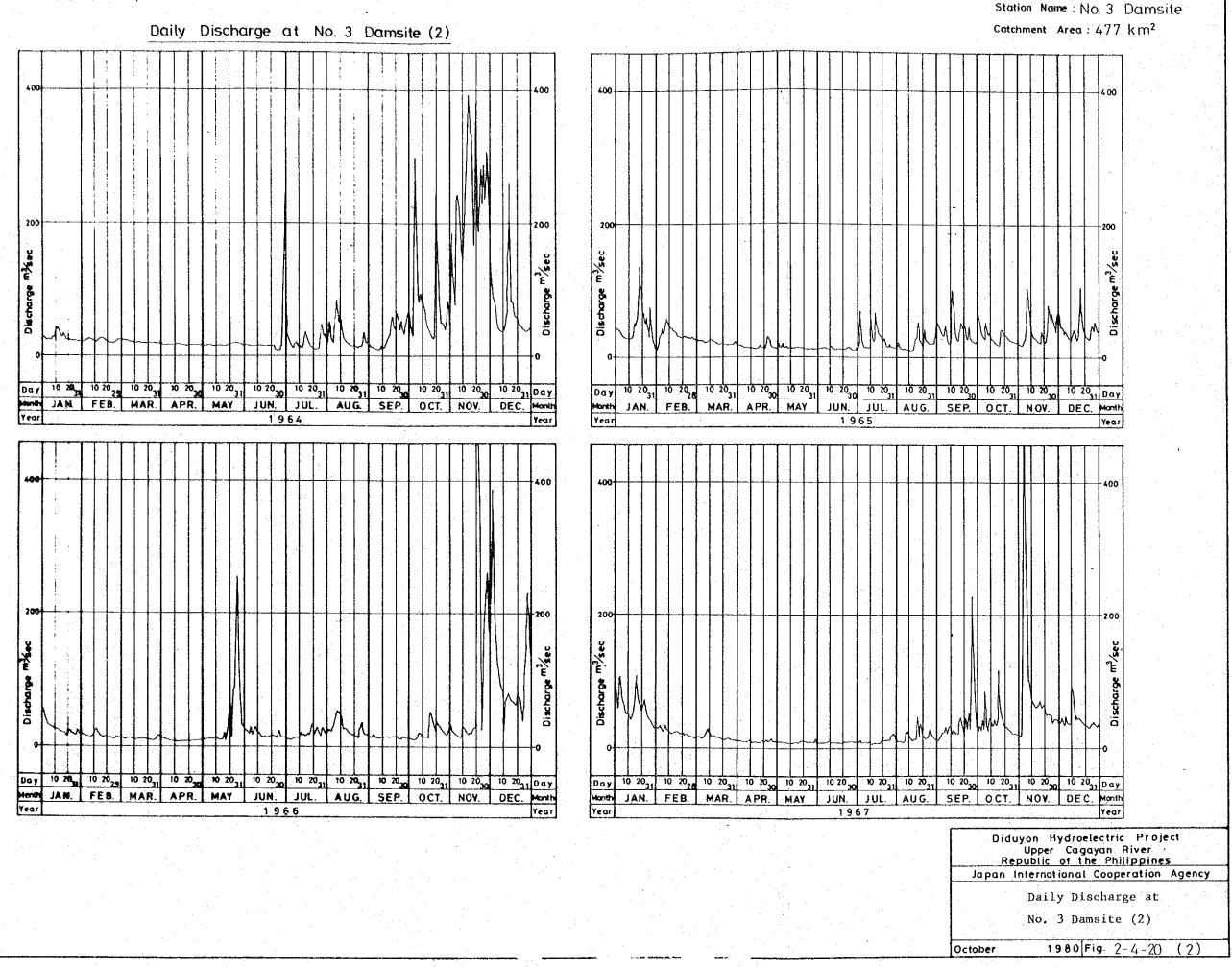
- Actually observed data
- O Arithmetically computated Data
- O Obtained inflow to reservoir
- | Way of conversion

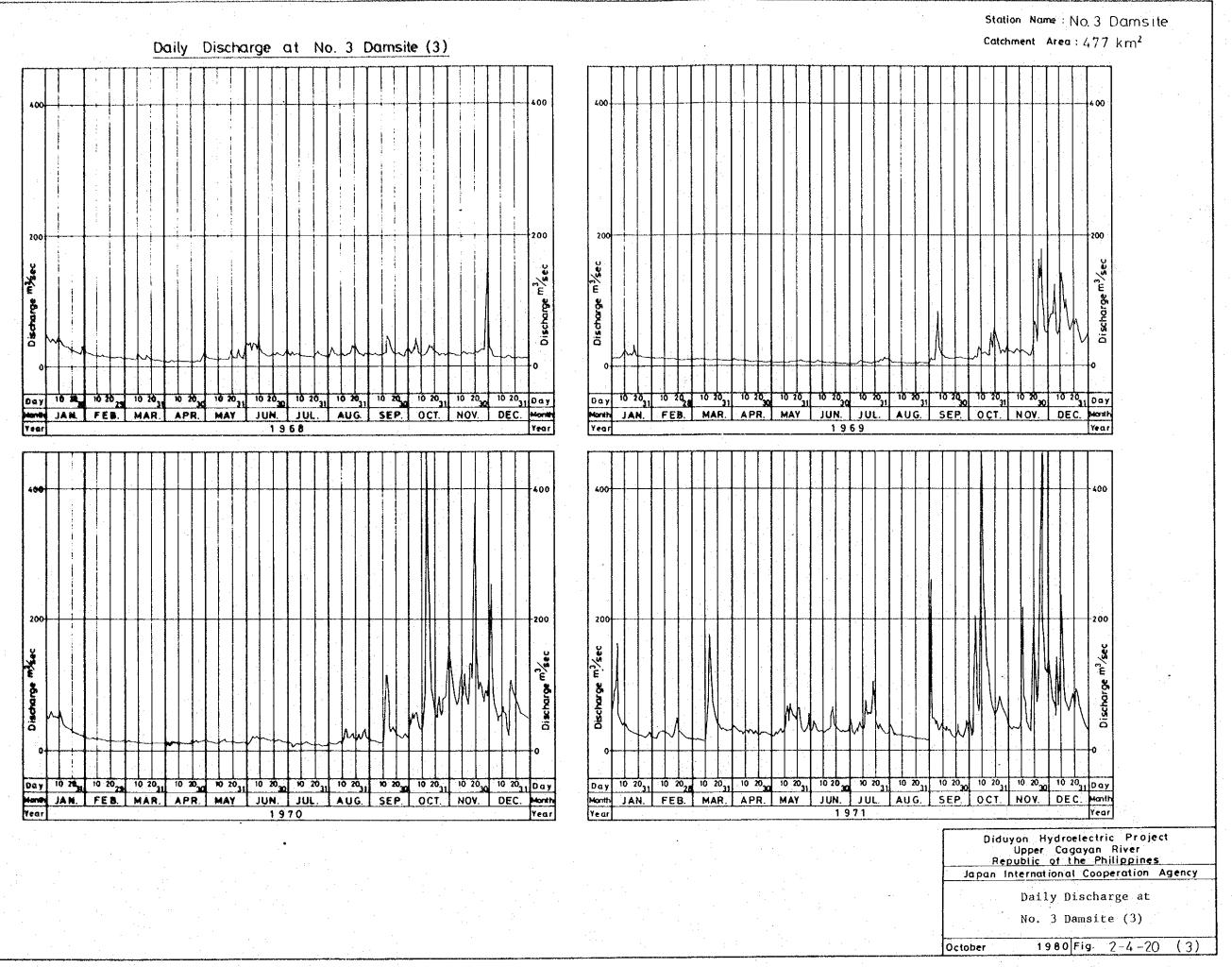
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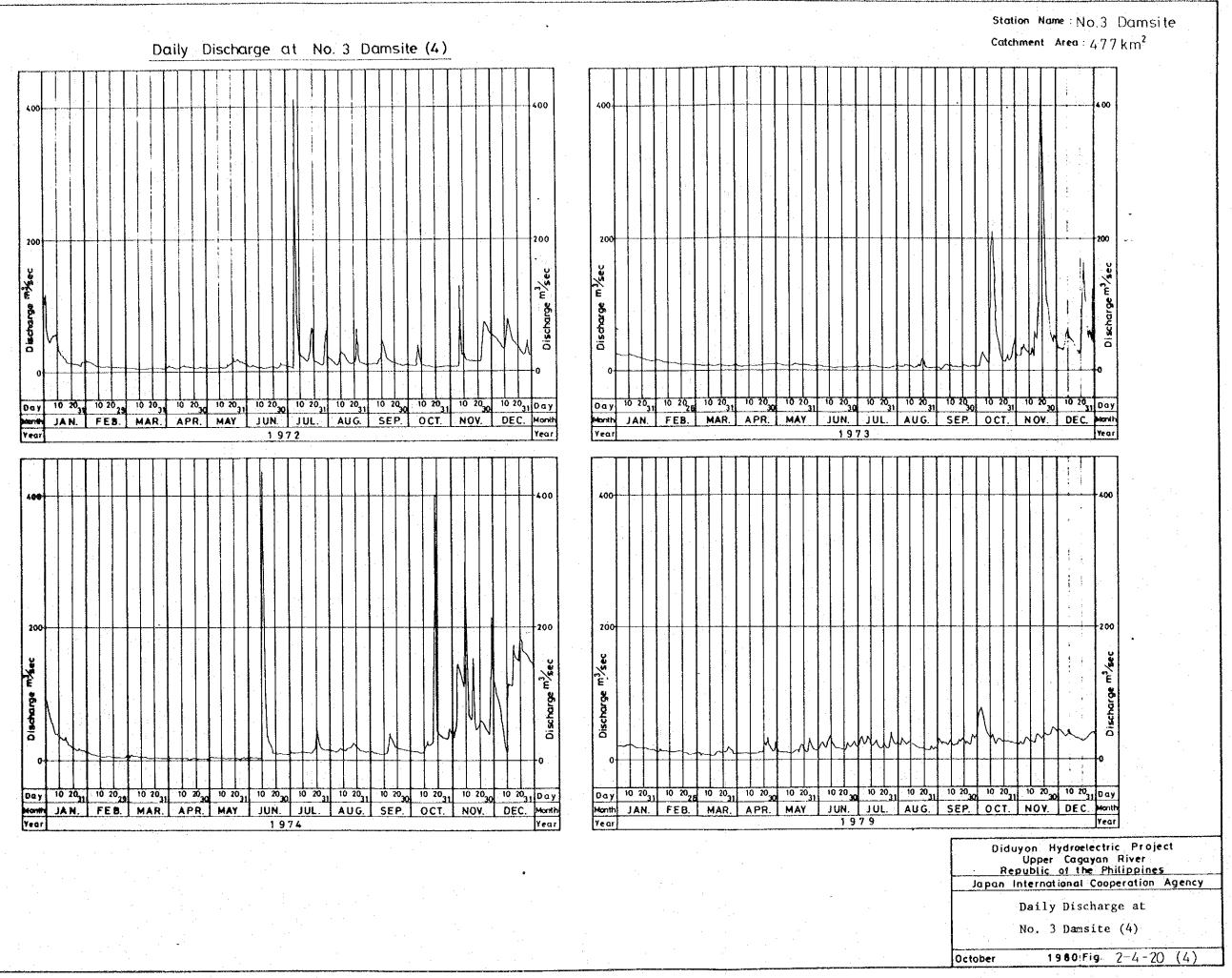
Method of Obtaining Inflow to Diduyon Reservoir

October 1 940 Fig. 2-4-19









Inflow to Diduyon Reservoir at Damsite

R	A STATE OF THE PERSON NAMED IN COLUMN TWO IS NOT THE OWNER.	-	_	THE STOCK HOME IN PRODUCTION AND ASSESSED AS A SECOND PARTY OF THE STOCK ASSESSED.	CONTRACTOR OF THE PARTY OF THE
	Q	$Q - \overline{Q}$	$Q = \overline{Q} / \overline{Q}$	Q	$(Q - \overline{Q})/\overline{Q}$
Year	Daily Average Inflow to Reservoir (m³/s - day)	Excess from Q (m ³ /s - day)	Fructu- ation from Q (%)	Inflow (m ³ /s-day)	Fluctuation from Q (%)
1960	32.009	+ 1.168	+ 3.9		
1961	28.010	- 2.831	- 9.2		
1962	29.403	- 1.438	- 4.7		
1963	28.621	- 2.220	- 7.2		
1964	49.789	+18.948	+61.4		
1965	28.745	- 2.096	- 6.8	Q Line	
1966	36.972	+ 6.131	+19.9		
1967	32.557	+ 1.716	+ 5.6		
1968	20.191	-10.650	-34.5		
1969	18.269	-12.572	-40.8		
1970	38.810	+ 7.969	+25.8		
1971	52.062	+21.221	+68.8		
1972	19.151	-11.690	-37.9	$\overline{Q} = 30.841$	
1973	20.926	- 9.915	-32.1	m³/s-day	
1974	34.003	+ 3.162	+10.3		}
1979	23.938	- 6.903	-22.4		
l6 years	$\Sigma:493.456$ Q: 30.841				<u>.</u>
				· ····································	-50 +50

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Inflow to Diduyon Reservoir at
Damsite

October 1980 Fig. 2-4-21

