Fig. 2-2-36 (3) GEOLOGIC LOG OF UPH-01

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Fig. 2 - 2-36 (4) GEOLOGIC LOG OF UPH-01

anal	EHOL	WAREGUEEN	Control to be designed in the last	-	ELEV	*******				-				_		Oi Toos	TOTAL DEPTH 400 m
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DEPTH	SYM- BOL	NAME	WEATH	JOINT	HARD-	8	Ŕ.	Q.	Ď. (%)		V A	λĽ	ŲΕ	m	CLASSI	REMARKS
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										60	Ι.						
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	17.73									N. S.							
	拉汉									X	P						165.7 ∼ 165.9m
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	133		• •							1						:	oriented at 25°
		:	:)	1 }					166.2 ~ 168.3m
	133							•									few calcite filled thick
-170-	(1)				<u> </u>			÷		,		į			; ;		few calcite filled thick joints (max.100mm) observed oriented at 20 to 35.
	分割		+ 2							Ç) —						1716 - 1717M
	ZZZZZZ									ė		:	Ì				171.6 ~ 171.7 m
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BORE	HOL	E No.			ELEV	ATI	ON		******	- Checker	IN	ČLI	NΑ	TIC	NC	908	UPH - OI TOTAL DEPTH 4
DEPTH	SYM-	G E C NAME	L O MEATH	G Y	HARD-		R.	REC Q.I	XXXI D.	FY (%)	1	Ü	31.7	JE JE		ROCK CLASSI- FICATION	REMARKS
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Fig. 2-2-36(6) GEOLOGIC LOG OF UPH-01

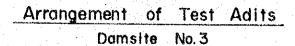
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	HOL	ENO.	UPH L. O	-01	ELEV	112	<u>Ş</u>	X ^	Υ λ .Α.	, VQ	IN	CL	N/	AT I	ON	90°	TOTAL DEPTH 400 ^m
DEPTH	SYM- BOL	NAME	L. O WEATH- ERING	JOINT	HARD- NESS	8	R,	0 e), (° 0, (° 0 80	(A) (C)		ν A		ON UE 2	0	ROCK CLASSI- FICATION	
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										2							joints are rare.
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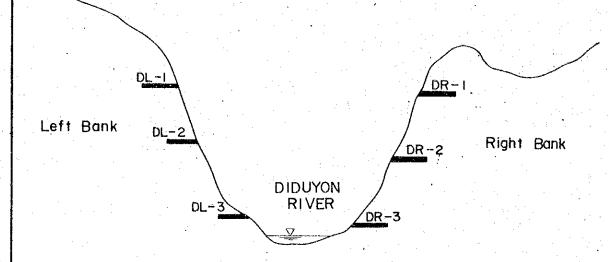
BORE HOLE No. UPH - O G E O L O G OEPTH SYM NAME WEATH JOIN A d Por A d Por Agg A d 330 A gg Por A gg Por A gg		ION	HNCL	NOTTANI.	190*1	TOTAL DEPTH 400
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Por Ad ? ? ?						no return water.
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Por						porphyrite.
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**** Por			Y			
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x*x*x Por						infilling white minerals
* *			13			weathered.
X X X X X			{ 1 4. }	1 1 1	1	
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To be continued

Fig. 2-2-36(8) GEOLOGIC LOG OF UPH-01

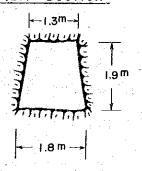
	BORE	HOL		и VPH				<u> </u>	<u> </u>			سنست					TOTAL DEPTH 400 M
	DEPTH		G. F. C	10	GY		COR	FRE	ΩVE	ŔŶĺ		UĆ	Ēί	NC		ROCK	
			NAME	MEATH- ERING	TOINT	NE.SS	. 20	40	60 8C	ico		VA	L () E 5 2	2	CLASSI- FICATION	REWARKS
	350														·		clarts are pebbly to cobbly
		定的												1.1	:	Сн	joints filled with calcite.
															٠.		dark grayish with reddish tints.
										1						CL	fractured
																_	357~ 361.5 m
			Agg	: :								i				CH (CM)	highly altered and slightly swelled.
									P			i					dark grayish with
	-360-	シス														CL	greenish tints.
											-					См	
					e e												363 ~ 365m
54 1		沙尔	10.00	1.11				***	e a								highly fractured.
						`		4			**		į			CL	redrilled after
			Αd						P				1				cementation light grayish
										$oldsymbol{\sqcup}$						Сн	porphyritic and coarse
										V			ļ				grained textune.
	-370-		^ - -						1	4	_	- j					
			Agg					: 1					1				dark gray with purplish
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Location	Test Adit	Length (m)	Remarks
Right Bank	DR - 1	50	
	DR - 2	50	
	DR- 3	50	
	Total	150	
Left Bank	DL-I	50	
	DL-2	50	
	DL - 3	50	
	Total	150	
Grand	Total	300	

Adit Section



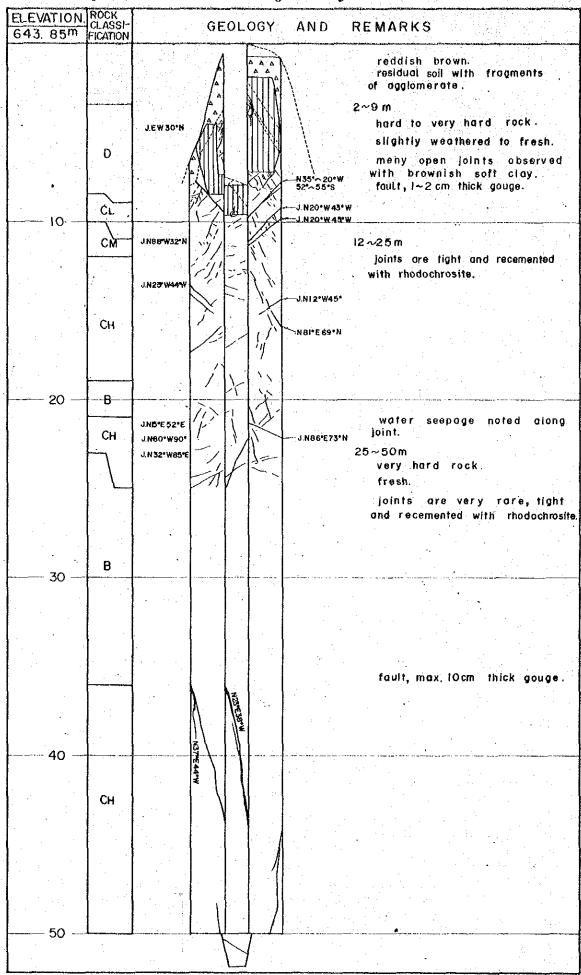
Diduyon Hydroelectric Project
Upper Cagayan River
Republic of the Philippines
Japan International Cooperation Agency

Geologic Logs of Test Adits

October 1980 Fig. 2-2-37

Legend Geology Residuat Soil / Talus Deposits Agglomerate Symbols Timbered Section Q Water Seepage Method of Drawing the Log Rock classification MALL Geology Diduyon Hydroelectric Project Upper Cagayan River Republic of the Philippines Japan International Cooperation Agency Geologic Logs of Test Adits 1980 Fig. 2-2-38 Oc to ber

Fig. 2-2-39 Geologic Log of DR-I



ELEVATION 595.56m	ROCK CLASSI- FICATION		GEOLOGY	AND REMARKS
	СМ			0~5m hard to very hard rock, joints slightly open. j.N25°E52°E
Table Towns And Annual Control of the Control of th	СН	1.H30+#38+W		joints are rare to very rare tight and recemented with rhodochrosite.
10				
20 —				
	В			
30				
30				
40				
50 —	L]		

Fig. 2-2-41 Geologic Log of DR-3

í		IBAA		- cooreg	ic Log of DR 3
	ELEVATION 557, 34m	CLASSI- FICATION		GEOLOGY	AND REMARKS
		D CL	WE GAN		open joint. O~8 m moderatoly weathered. low angle fault, with brownish gouge max. 20cm thick. fault with max. 30cm thick brownish gouge.
	10	CM			8~11m
		Сн			altered and weathered along joints. LI~50 m hand to very hand rock. sLightLy weathered to fresh.
					joints are rare, tight and recemented with modochrosite.
	20				
		• В			
	30				
					fault? with weathered
	40	Сн			N32*W54*W white veinlet max locm thick, N32*W52*W 38 m water seepage noted at upstream wall
	40	См			N36°W49°W fault. Water seepage noted along the fault. NI6°W82°E moderately weathered and
					slightly fractured.
	 50	8			
	50				

Fig. 2-2-42 Geologic Log of DL-1

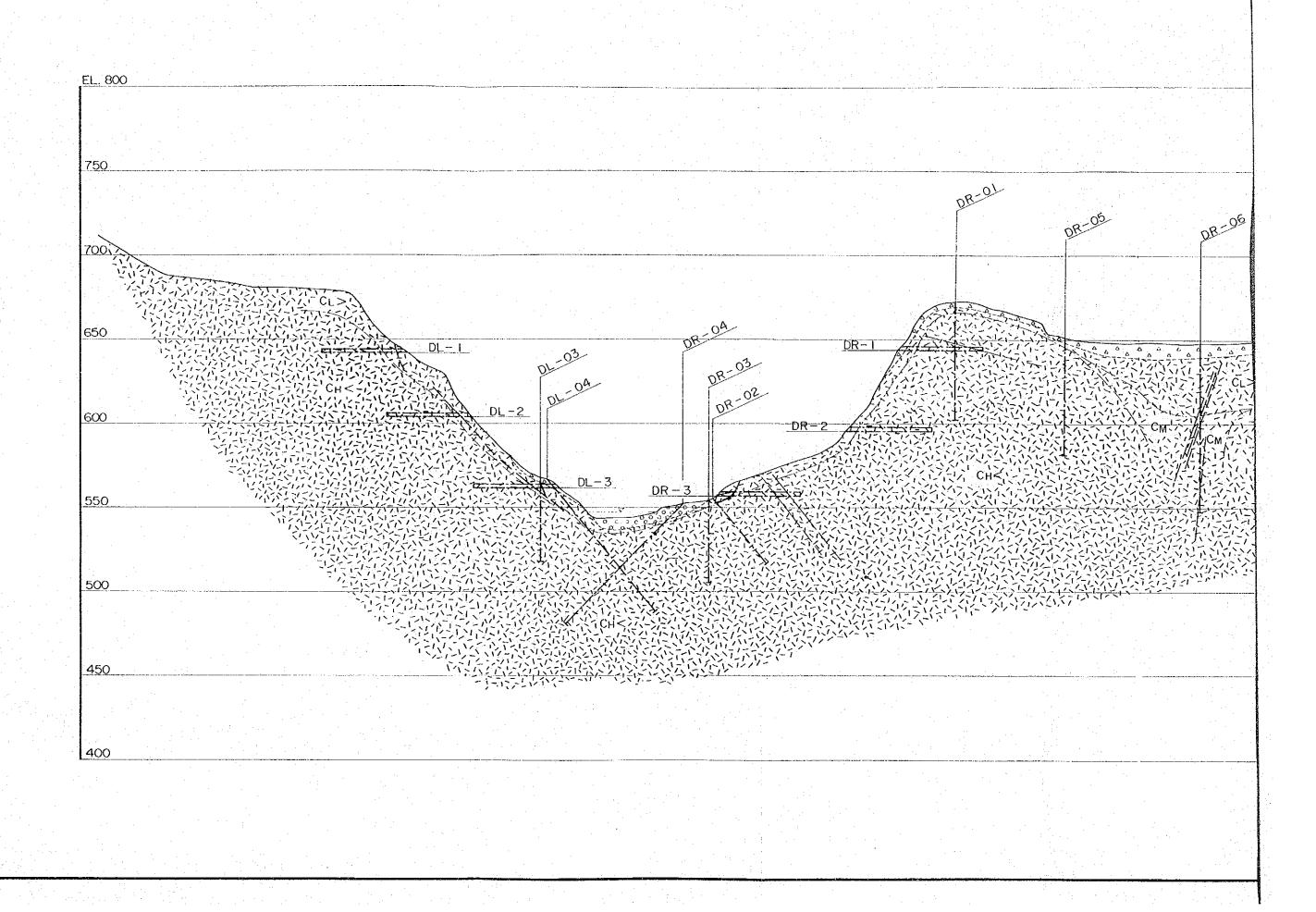
643	VATION 2.59m	ROCK CLASSI- FICATION		GEOL	.OGY	AND	REMARKS
		D		1/1	2 2 2 2	J.N62°W84°N	0 \sim 4 m moderately weathered. open joints observed. 4 \sim 10.5 m
		См					hard rock slightly weathered
	- 10				\ \ \		10.5∼ 50m very hard rock joints are rare, tight and
					, L		recemented with rhodochrosite.
	- 20	Сн					
	•					J.H40*W76°E	
	30	В	- 1	<u> </u>			
				,			
	- 40 -	* ***					
	- 40	СН					
							slightly weathereed along
	- 50				1		joints

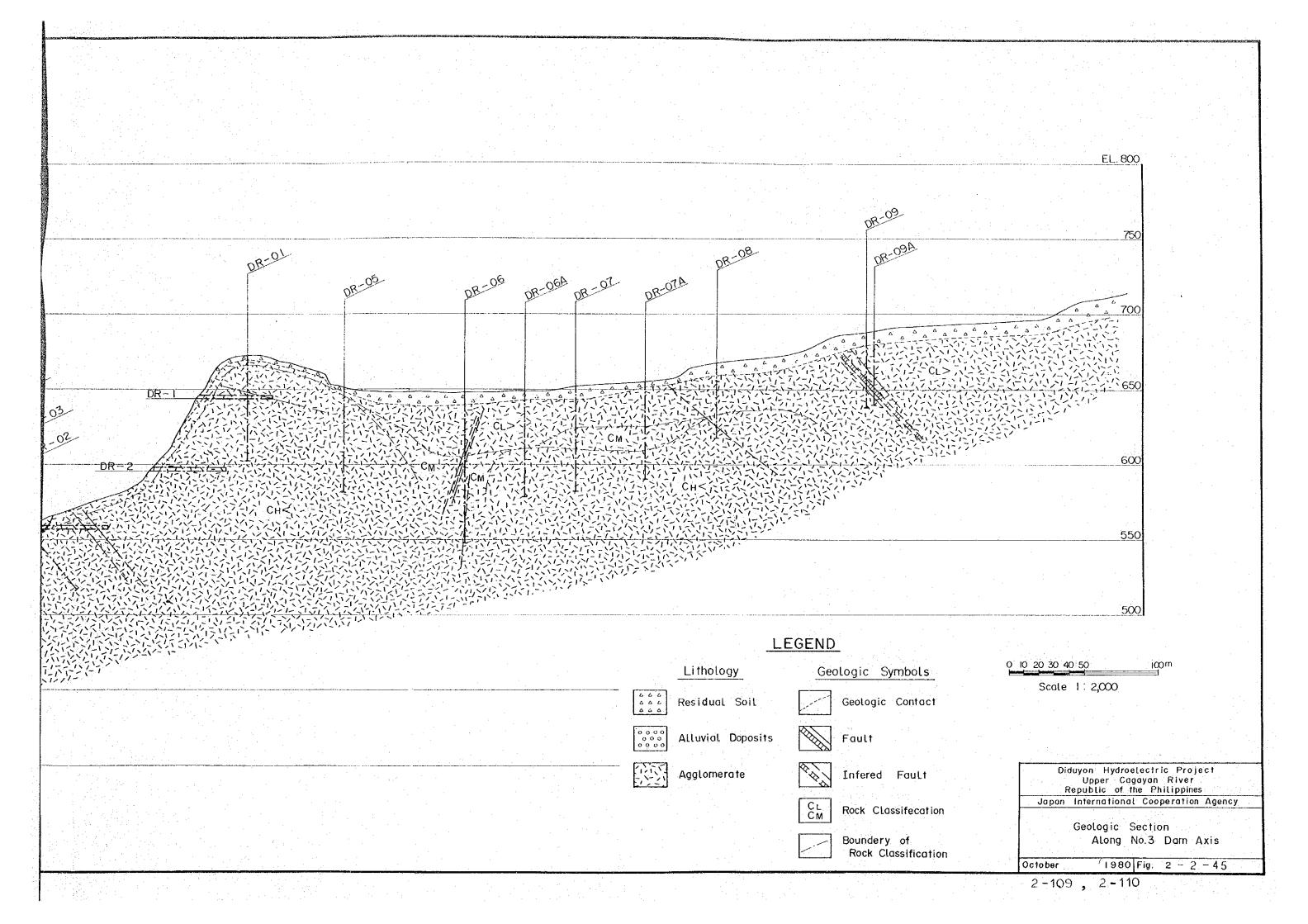
Fig. 2-2-43 Geologic Log of DL-2

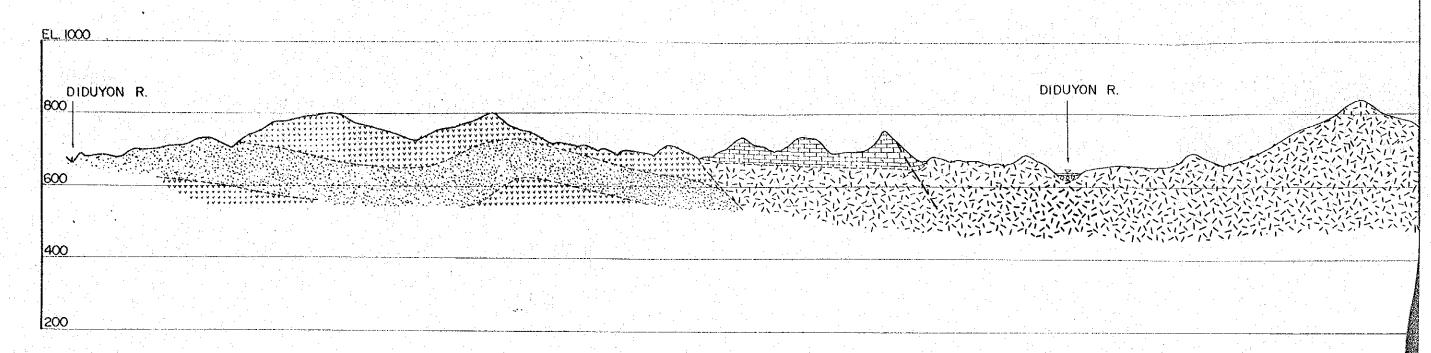
		and the second s	Georog	IC LOG OF DL-2
ELEVATION 604.79m	ROCK CLASSI- FICATION	G	EOLOGY	AND REMARKS
				O∼9 m hard rock moderately to slighly weathered.
	Cı	12/		
	O.			N54*W40*S fault with brownsih gouge.
				9∼.50m
10				very hard rock. stightly weathered to fresh. joints are rare, tight and
	Сн			recemented with rhodochrosite.
20 —				unes weers stained along joint
	-			
	В			
				J N85°W75°N
40				40 ~ 50m very hard and sound rock.
				fresh and massive.
50				

Fig. 2-2-44 Geologic Log of DL-3

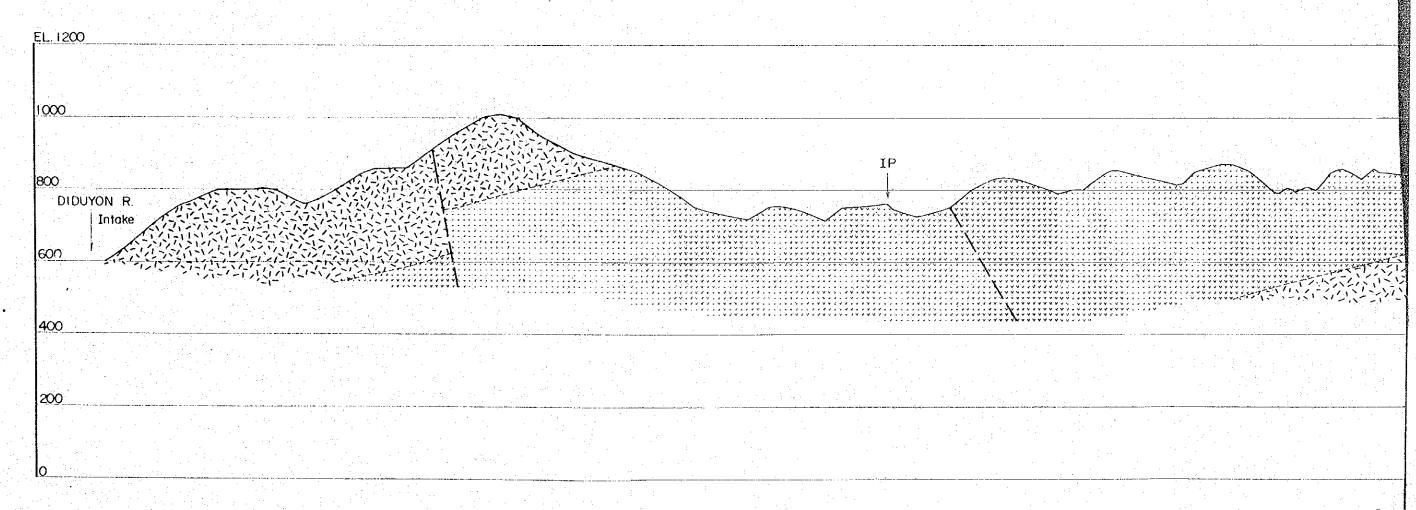
. [ELEVATION 562,46m		the second second	***			REMARKS
-	562,46m	FICATION	ga parimunitin dan ali day embala errepi basabuat per		<u> </u>		
:		D		,,,,,,,			open joint, 10~15am wide, fitled with residual soil.
		CL	Ī/	9/11			O~4m hard rock, moderately weathered.
					\		4~14.5 m hard to very hard rock.
-		См		Y		N22"W72"W N65"W72"W	slightly weathered. fault with brownish gouge
		Oill					and white vein max. 10cm thick.
ŀ	—— 10 —					N76'W72'S	fault with gouge and weathered along fault plane
			•				max 10cm wide.
		1 1 + 1 / / /	K		1	N65°W34°S	fanit, water seepage noted along fault
						J 70*W40*N	145 ~ 30m very hard rock
		СН				JNIO*E70*W	slightly weathered to fresh joints are rare and tight.
	20						
							calcite filled joint observed, max. 15cm thick.
	•	В					max 13 cm thick.
					\.		
		Сн			·		
-					Y	N38°W40°W	fault.
H	30						30 ~ 50m
						**	very hard rock. fresh and massive.
					\setminus		joint are very rare and tight.
ŀ							
		В					
-	40	·					
	· · · · ·						
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$\ \cdot\ $	50 <u></u>	<u> </u>	L L		/		
L		<u> </u>		<u> </u>			

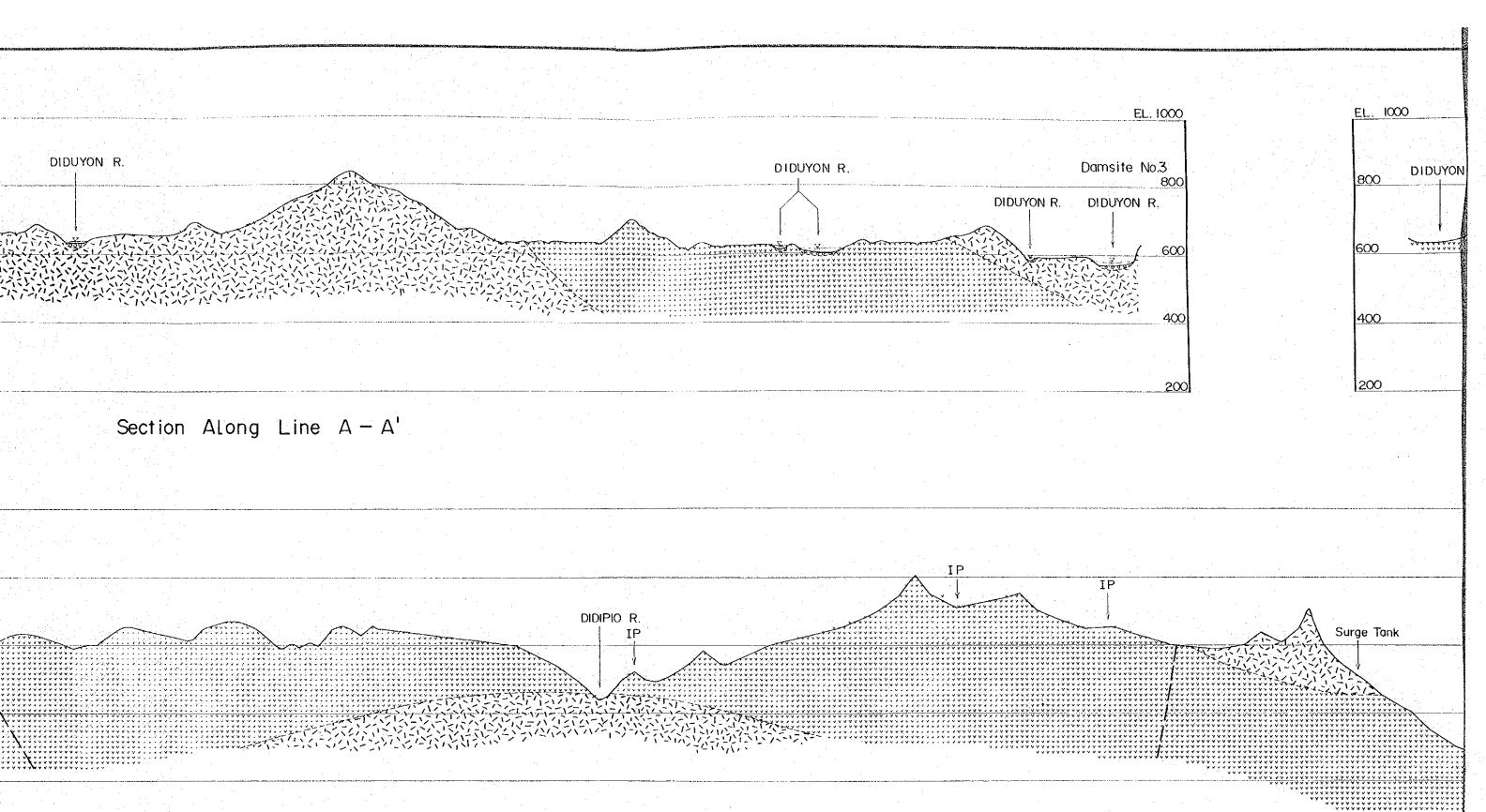




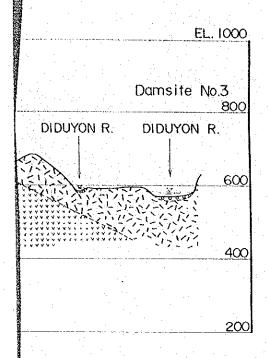


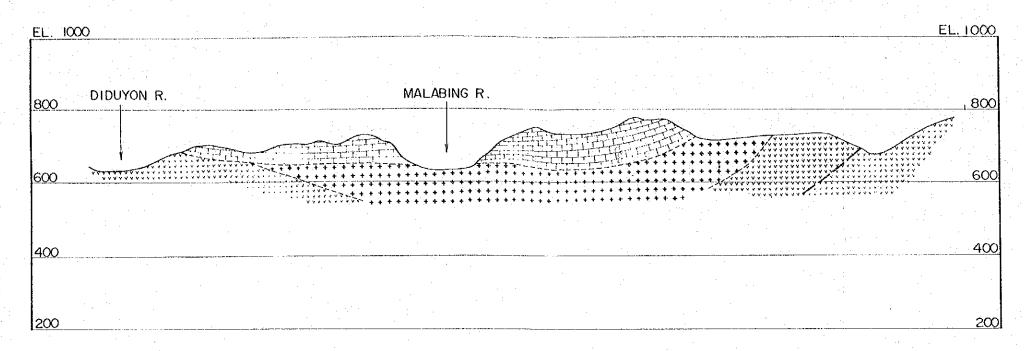
Section Along Line A - A



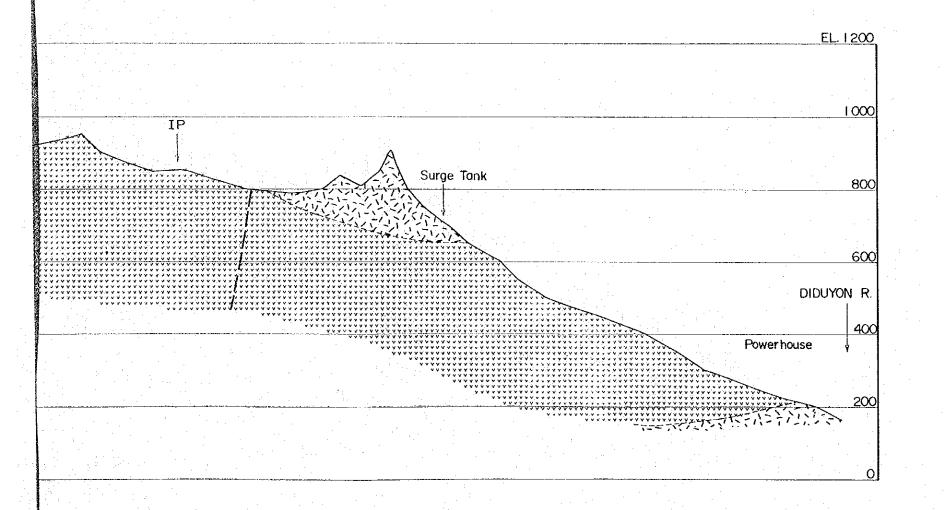


Section Along Waterway

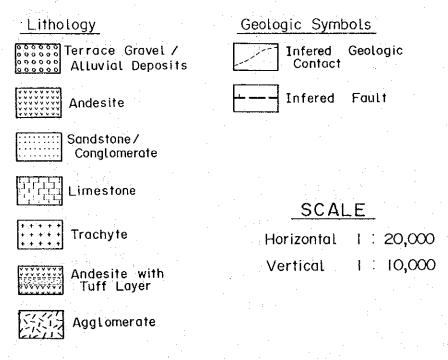




Section Along Line B-B'



LEGEND



Diduyon Hydroelectric Project
Upper Cagayan River
Republic of the Phllippines
Japan International Cooperation Agency Geologic Section

1980 Fig. 2 - 2 - 46

2-111, 2-112

2.3. Earthquake

2.3.1. Data on Past Earthquakes

For the purpose of computing a design seismicity that may act on the planned damsites, records of past earthquakes on Luzon and vicinity were investigated. Earthquake records were provided by the Geology and Geotechnics Division of NAPOCOR. They indicate the location of epicenters and magnitudes of earthquakes that have occurred during the 77 years between 1901 and 1977.

A total of 1,167 earthquakes have been observed. Observation results of past earthquakes are given in Fig. 2-3-1 and Table 2-3-1. These earthquake data are used as basis for calculating the design ground acceleration.

2.3.2. Seismic Analysis

(1) Magnitude and Seismic Intensity

The magnitude indicates the scale of an earthquake, while the seismic intensity indicates the violence of ground motion during an earthquake at the observation point. Consequently, it is not possible to discuss the seismic intensity and the magnitude on the same level. According to the Gutemberg-Richter system, the following relative equation exists between A/T and magnitude M:

log 10 A/T = 0.76 + 0.71M - 0.027M²
where A: maximum amplitude (in microns)
T: cycle (in seconds).

The acceleration at the epicenter is $\alpha_0 = 4\pi^2 \quad A/T \ .$

Therefore, the following equation exists between α_0 and M: $\log~10~\alpha_0~=-2.1~+~0.81M~-~0.027M^2$

In general the seismic intensity decreases when the epicenter is farther away. Dr. Kanai proposes these equations as shown below on the basis of large number of observation results. For earthquake dynamic spectra applicable to the earthquake bed from near the epicenter to a distance of about 200 km,

$$A = 10(0.61M - Plog_{10} X + Q') \times T$$

$$V = 10(0.61M - Plog_{10} X + Q'')$$

$$a = 10(0.61M - Plog_{10} X + Q) 1T$$

where

M: magnitude of past earthquake

A: subsurface displacement acting on the planned damsite

V: subsurface velocity acting on the planned damsite

a: subsurface acceleration(gal.) acting on the planned damsite

X : epicenter distance - from the epicenters of past earthquakes to the projected damsite.

P:
$$1.66 - \frac{3.60}{X}$$

Q: $0.167 - \frac{1.83}{X}$

Q': $-(1.43 + \frac{1.83}{X})$

Q": $-(0.631 + \frac{1.83}{X})$

By T is represented the predominant period of the seismic waves. From the magnitude and the distance from the epicenter, T is obtained as shown in Table 2-3-2 using the Seed diagram shown in Fig.2-3-2.

The seismic intensity that acts on the projected damsite can be calculated using the above equations on the basis of data on past eqrthquakes that have occurred on Luzon Island. The maximum accelerations by year taken out of the calculated accelerations are given in Table 2-3-3.

(2) Calculation of Probable Acceleration

From results of the foregoing studies, probable accelerations at 100, 200, 300 and 500 years returns were estimated on the basis of the maximum accelerations by various methods such as the Thomas plotting method. As a result, probable accelerations were obtained and shown in Table 2-3-4.

Under the Thomas plotting method, 88 gals were obtained as the probable acceleration at the 200th year return. This agrees well with Table 2-3-3 in which year-by-year maximum accelerations are plotted.

(3) Design ground acceleration

In Figs. 2-3-4 and 2-3-5 earthquake energy of the Philippines and that of Japan are shown. In the figures, the contour lines show the degree of seismic energy accumulated in a year in units of $erg/km^2/year$.

Comparison of these figures shows Japan's seismic energy to be greater than that of the Philippines, though there are differences in the accuracy of the two sets of data.

In Japan, incidentally, 120-200 gals are adopted as the design seismic intensity for gravity dams. Also, in consideration of the 128-gal probable acceleration for the 500th year calculated under the Thomas plotting method, 120-gal design ground acceleration for the Diduyon Dam will be safe enough (the seismic intensity for general structures in the Philippines is 0.18 * 100 gals). When an earthquake of 120-gal acceleration occurs directly below, the magnitude will be about M = 6.6.

(4) Design Seismicity for design of dam body

In the case of a gravity dam, the seismicity acting at right angles on the dam axis can generally be designed for the same value as the ground acceleration. But as the proposed dam is a high dam of 100-meter class, the following examinations were made.

(a) Natural period of frequency of the gravity dam

If the dam is assumed to be of triangular wedge shape and subject to flexural vibration, the natural period of frequency of the dam To is derived from the quation:

To = 1.65
$$\frac{H^2}{B} \sqrt{\frac{12\gamma}{Eg}}$$

where

H: height of the dam (m)

B: width of the dam base (m)

E: Young's modulus of elasticity of the dam

 $(2 \times 16^6 \text{ t/m}^2)$

Y: volumetric weight per unit of dam material

 (2.5 t/m^3)

g: acceleration of gravity (9.8 m/sec²)

when H = 110 m and B = 90 m are assumed for the Diduyon Dam, calculations result in To = 0.27 sec.

(b) Design seismicity

G.W. Housner obtained response spectra against typical severe earthquake records in the United States and produced Fig.2-3-6 by averaging them. From this figure,

the average response coefficient of $\beta 0$ =1 is obtained when the natural period of frequency is 0.27 sec. and the recession constant h of the gravity dam is assumed to be h = 0.1 - 0.2. Consequently, 120 gals, the same as for sub-surface acceleration, will be safely adopted for the dam body acceleration.

Table 2-3-1 (1) Past Earthquake Records in North Luzon 1901 - 1977

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7.196	- KIN- SEC		05-35-03	05-35-03	26-36-67	17-28-64	72-43-67	20-2/-32	05-59-38	11-20-10	050205	12-10-32	02-35-01	8-14-18	02-19-48	02-28-22	2-2-E	17-16-46	21-55-32	3	87 - 50 - CD	17-14-11	17-28-02	10-76-61	14-99-41	04-63-62	13-45-46	21-66-11	09-53-10	04-21-53	17-09-07	15-68-52	05-32-37	15-40-31	X-60-8	19-13-40
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1114	RE-MIN-SEC. LATITUDE LONGITUDE NAC DEPTHS INTE	22-57-00 14*00' 122*00' 7.8 25	20-39-48 14.00	23-52-64 13-00	00-16-12 14-30'	05-01-32 13*30*	.81.91 92-90-00	16-25-64 17-30	80-03-53 15°18°	03-00-05 17-00	21-47-46 19.06	14-49-44 19-00.	.B. X .1-1-1-1	20 00 00 00 00 00 00 00 00 00 00 00 00 0	17-30-10 16-00, 120-00, 6.75	13-21-42 18708* 120°09*	15-13-26 13-62.	04-57-65 119-30"	06-01-62 16.30	14-41-56 16'00' 119'EF	21-11-06 13*361	17-00-19 16'06'	17-25-48 16-38"	15-15-25 14"B"		01-33-47 18-24			00 of 00 of	Of 61 97-17-10				.00-91 21-61-60	16-38-21 15-06"	01-25-52 15-06.
	MAC DEPTHS INTE	22-57-00 14*00' 122*00' 7.8 25	20-39-48 14.00	23-52-64 13-00	14.36	13.30	16.18.	17.30	15.18	13.00	. 19.00.	.00.61	174-14 X°88'	16.00° 120°10° 6.24	17-30-10 16-00, 120-00, 6.75	13-21-42 18708* 120°09*	13*62*	04-57-65 119-30"	1 16.30'	16.00, 119.38	136361	17-00-19 K.C.	17-25-40 16-30	15-15-25 14"B"		01-33-44 18-24	00 61		00 of 00 of	Of 61 97-17-10				.00-91 21-61-60	16-38-21 15-06"	12.08.

Table 2-3-1 (2) Past Earthquake Records in North Luzon 1901 - 1977

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Jiga	1 ATTTION		15,30,	18.00.	15°18°	18,30	18.30	18,30	18 30	.06.77	13.30	13,30	15*36	17*30	15*54	16.24	18,00	16.24	16.56	19.10.	17.39	18.42	12.30	18.30	18,30	9.1	19,00,	19.00	38°18°	19.54.	36.71	17.48	17.36	18.06	14.00.	14.42	15.00.	
TIME	HP-MIN-SEC		11-52-23	06-41-29	01-07-39	10-26-33	15-13-16	02-44-34	18-09-00	04-03-38	21-45-48	21-45-48	10-27-41	10-32-65	22-32-12	11-16-06	21-29-02	17-29-20	23-64-12	22-36-00	22-27-15	10-36-15	18-65-19	12-52-34	13-01-13	23-17-53	07-50-55	04-02-36	20-54-15	07-14-29	22-55-36	10-04-41	16-12-54	19-22-58	06-29-24	19-16-14	00-52-54	
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	2	TODE	17.00.	8	2	2		2	3,	2	2	2	17.00.	3	*	10.34	*	.00.51	17.44	17.42	78.87	36.91	1.0 4.4	17°12'	.07.71	16.18	19.30.	.00.87	19.00	14.42	13.54	***		, 8 7	15-24	18.42	15.30	
		4	17	18.00	17.00	17.00	17.00	17.00	14.12	18.00	13.36	18.30	1	75.57	X.X	91	18.34	13	~	1		*	18	- 13	- -	Ä	=	7	P.	4		1	15.18	15.48	2	=	1.5	
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Table 2-3-1 (3) Past Earthquake Records in North Luzon 1901 - 1977

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11-740-CI	Me-Kinexac	LATITUM	LATITUM LONGITUM			THE REAL PROPERTY.	-			P-DAY-TR	NA-MIN-SEC	LATITUDE	LATITUDE LONGITUDE	MAG	(km)	INTERSITY
4-05-55	02-36-05	13,00	119.00.	2	-				176	7-01-57	16-41-26	16°00°	120°54	:		
-14-55	06-26-25	18.36	123"06"					- द्व ै	177	7-25-57	22-16-32	18.00	121 00.	٠.		
S-11-53	11-34-36	19.60	121.36					- 	178	9-27-53	14-22-37	17°36°	121.42	i.		
6-14-55	15-59-48	13.36	120.00						179	11-20-57	16-14-59	.89°	121°36'			
7-02-55	16-03-52	. 30.61	121"36"						28.	11-26-57	19-06-19	.00.67	121 00.			
P-20-55	15-44-61	18.00	116.48						183	12-30-57	13-58-29	18, 36,	120,30	4		
11-15-55	15-22-46	15.36	120.11,						182	1-20-56	07-13-06	. 50. 97	120.00			
11-14-55	06-41-35	12. 常	120-12					-	183	1-20-58	07-13-22	.09.91	120.60			
11-24-55	04-52-36	. 76. 26.	121.667						1.84	1-20-56	09-11-50	15.86	120-60	•		:
12-05-55	62-32-36	17.00	121.410						165	2-14-58	17-56-16	15.80	119 48			
12-05-55	18-13-11	17.18	121 36.					red.	186	2-19-58	14-31-03	15,30,	121-00,			
12-29-55	26-35-20	14.06	120.48					F44	181	3-11-5	21-22-00	× 91	121*62	•	:	
2-12-56	21-49-20	13.60	119.30	. •			•	с-1	E 250	3-19-56	14-15-07	. 89 BT	121°36°	:	1	
4-30-55	16-63-12	16 20	121.00,					, =~4		3-23-58	10-15-66	.83	120.00			
5-04-56	18-46-49	25.62	122.00.					;=4	2	\$17.78	28-59-55	15.00	120.00			
8-6-	18-44-36	18.00	121.36	٠.				M	I O I	4-16-58	12-36-26	.80.91	120,30	٠.		
7.5.7	09-15-02	13,30,	124.000					:-4	192	4-20-38	12-57-36	19.00	121.30.			
7-19-56	20-61-23	15.18	119 18					4	193	5-01-56	07-13-06	, S. S.	120.00			
10-23-56	175	14.03.	120.25					e4	194	8-01-58	12-28-28	13,30,	120,30			
10-27-56	12-15-25	14.12.	123°%					, _F -4	•	8-24-58	16-5/-25	36.08	121.00			
10-28-56	10-45-44	. 27. 91	123.38.		•			, sed		9-23-58	19-07-50	15.00	119.48			
10-28-56	13-20-44	14.13	123°36'	٠				. व्य	P4	20-02-02 02-02-02	61-57-60	14 62	123*00			
10-28-56	14-00-34	34.30	123°36'					r4		11-12-56	03-58-38	18.42	121.36	: .		
10-26-56	15-23-33	16.18	123,36		٠.			• ~ 1	100	11-11-18	05-25-54	15.30	122.0%			
10-23-X	03-17-02	14,18,	123.36					2	200	11-13-58	8-8-8	15.40	122,15	·. ··.		
19-29-56	03-22-22	14.18.	123 36					2	102	11-19-56	21-54-02	15°36'	119°36			
11-02-36	20-21-CE	14.18	123*36					**	202 I	12-03-58	09-48-26	. 60.	121.30	•		
11-10-56	14-40-23	15.62.	130.13,						203	12-18-58	07-27-15	18.00	120°30			
11-17-24	62-66-91	16.18	123"36"					~	707	1-21-59	11-08-10	.00.61	120.00	5.5		
11-14-26	12-42-48	15.45	120-12					~	202	2-21-59	06-27-67	16.18	120.18			
7. *	14-37-14	74.57	120.12						508	2-21-59	11-06-10	16.00.	120.00	5.5		
3-12-57	19-20-35	. X. 4.	123°30'					κģ	207	7-13-59	19-59-57	15,30	120°30	6.75	. :	1,
¥12-57	19-22-35	14.30	123,30						208	6-10-39	£5-69-40	13,30,	120,00			
7-14-37	16-61-00	. M. 77	123°30°			-		Ø	508	9-06-59	14-18-04	36.71		5.0		
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Table 2-3-1 (4) Past Earthquake Records in North Luzon 1901 - 1977

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*	EPICENTER	LONGITUDE	76.000	130.14	122.00	121.24	121.43	120-54	119.56	120°26	121.061	119°54	120,36	121.68	121.41	121.42	119.42	122*30°	120°30	120 36	119*36	122°18°	122.42.	121.48	121.18	119.48	121.56	119-62	120.06	119.30	121 18	139*627	121.48	122-10	119.42	1.20*30	120*42*	
7777	27.43	LATITUDE	176471	* C	24.41	18.5%	18°36	.8.	14.48	15,30	19*18*	75.97	13.54	15.26	15.18.	15.18	15.26	15.18	15.06	14.00	27.72	17.42	15.00	19,30	15,30	17.30.	26.92	36.18	15.42	16.00	19.06	16.34	19,00,	16,10	. 90. 91	13,36	18*68	
- 1261 110		HR-MIN-SEC		20.13.45	19-26-51	18-16-47	13-07-57.8	21-57-26.8	12-06-21.5	21-57-17.5	11-03-36.8	12-07-12.7	13-55-03	03-28-35.3	18-20-44.7	10-21-55.3	07-07-10.5	18-28-24	04-19-27.8	05-56-54.	17-36-52.8	61-92-00	04-49-51.5	19-21-49.6	23-45-16.8	10-53-59.	03-55-01	95-90-90	06-09-18	16-43-12.2	09-08-04.1	20-08-34.4	15-49-57.4	01-01-00	13-09-09.6	15-06-35	20-38-16.5	
מי רוו דתק	DATE	MO-DAY-YR	,	70-07-4	, 49 V2 - 4	7-12-62	9-27-62	- W-62	10-28-62	11-07-62	11-10-62	11-27-62	12-01-62	12-21-62	12-21-62	12-23-62	12-30-62	12-31-62	1-12-63	1-17-63	2-07-63	2-17-63	2-25-63	2-25-63	2-25-63	Y 15-63	127 153	3-25-63	5-17-63	718-63	5-20-63	6-01-63	6-07-63	10-22-63	12-21-63	1-14-64	1-20-64	
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		LATITUDE LONGITUDE	120°30'	120.00	120,001	120,30	120,00	120.00.	121.00	120.001	121.30.	121.12	120.42	120.18	119.30	120-42	120.42	121742	121,00,	120.39	121.36	121.24	120°24	121 "06"	119.18	120.00	119"42'	119*42	121-12	120.54	120*36'	120.36	120.26	,81.021	121,121	120.36	120-12	
4	EF 1LEN IER	LATITUDE	. R.	17.40	19.00	13,30,	.00.41	14.86	13.30	18.00	15,36	16.18	14.13	16.48	78.61	13,36	13.36	15.42	.06.61	13.30	16.06	16.34	16°36°	16.12	.00.51	13.34	12.X.	15.34	16.48	13.48	13.30	13°54	16.34	13.44	19.18	13.42	14.38	
		H-HIP SEC	02-51-07	01-22-00	04-24-44	21-12-07	05-23-16	05-22-53	16-00-05	22-43-40	16-06-09	10-51-35	27-12-20.5	06-40-12	28-23	13-48-00	14-01-08	19-30-61.6	13-52-37.6	02-31-07	27-01-04-8	11-27-65.4	16-88-40.4	01-21-57.4	10-37-40.7	17-27-44.9	22-38-X-1	22-36-34.1	16-21-53.3	00-06-52.5	00-17-53.5	21-14-32.5	23-43-34.4	05-31-03.4	16-66-27.2	11-35-21.1	11-09-13.5	
		MY-YA	1-11-60	1-13-60	1-23-60	1-24-60	1-29-60	2-29-60	7-23-60	4-27-60	3-30-40	10-27-60	10-23-60	11-06-40	12-10-60	12-13-60	12-13-40	12-23-60	1-01-61	1-11-61	2-X-6	7727	3-23-61	7.56	4-13-61	19-80	\$-23- 61	5-27-61	1757	7-10-61	7-15-61	13-12-61	13-22-61	777-1	7-03-62	4-15-62	\$-03 -6 2	
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TRIENSITY 128 60 7 LONGITUDE 121 12 179.36 121.121 120,00 120 06 120,00 120.00 122°30' 122 54 120.00 122,06 121*48 121 36 121 06 121.54 122.12 122-12 119 42 119 30 120.001 120.00 121°54° 120001 120.00 120.00 122,00 122.26 120°36 119"42 120-42 199.30 122.30 119,30 EPICEMTER. LATITUDE 15.18 Table 2-3-1 (5) Past Earthquake Records in North Luzon 1901 - 1977 13.48 25.30 13.88 14.30 15.36 15.30 13,36 16. X 16.54 13.24 14.24 13.54 14. 26 16.48 16.48 15.08 25.88 80.71 14.24 15,18 16.42 74.54 14.12 HE-NIN-SEC 80-00-80 11-13-27 01 - 19 - 1280-80-8 20-00-00 8-69-60 15-16-46 11-58-35 20-00-00 8-8-8 00-00-00 8 8 20-00-00 2000 8-8-8 20-00-80 00-00-00 8-8-8 20-00-00 00-00-00 00-00-00 00-00-00 20-00-00 8-8-8 8-00-00 18-22-14 20-20-20 9-45-00 8-8-8 00-00-00 20-00-00 20-00-00 00-00-00 20-00-00 00-00-00 HO-DAY-YE -16-66 79-10-1 99-10-1-10-66 2-26-66 2-17-66 2-17-66 203 3-12-66 3-12-66 1-12-66 3-14-66 3-22-66 3-26-66 4-12-66 4-21-66 99-92-1 2-03-66 100 2-12-66 2-20-66 100 4 3-8-3-25-66 4-21-66 104.46 4-29-66 101-66 5-03-66 -28-66 -23-66 99-90-9 99-80-9 117-66 9 INTENSITY (test) 3.5 ** s. O 2 .. LATITUDE LONGITUDE 120 % 122"24" 120.001 20.48 .00.02 120.24 119.36 19.42 120-42 139.54 126°00° 19°54 . 9€ .6TT 120.00 120 36 119 30 120,38 120.30 119*62 119.48 120°30 121.00 119,36 120 54 121,30 120,36 120-36 29.6ET 120 30 121 48 122 24 EP ICENTER 13.48 15.30 19.18 13.42 13068 13,30, 24.30 16.30 15.56 16,12 13,30 13.42 13,36 15.18 13.42 15 32 14.42 15.42 13.42 16.24 13,68 15.12 ET 97 14.48 21-23-35.5 21-17-46.1 12-28-45.6 37.15 45.7 X-25-16.3 13-13-22.7 20-34-21.6 21-17-72.7 15-00-27.E 16-01-18.4 22-38-26.5 22-53-33.9 1-14.1 H-46-25.3 32-53-26.2 26-30-51.1 IN-YIX-SEC 14-28-23 20-37-07 2-33-00 11-10-59 35-47-05 307070 20-12-08 22-06-00 00-19-10 13-17-00 80-80-8 05-35-10 00-00-0X 14-13-49 8000 80-00-00 00-00-00 02-51-00 80-80-60 C-DAY-YE 7-12-64 1-22-64 1-03-65 1-07-65 1-03-65 7-34-65 1-25-65 0-02-65 2-18-64 717-6-22-04 1-13-65 1-23-65 1-23-63 -10-65 -17-65 118-65 1-23-65 0-02-65 0-26-65 9-25-63 1-01-65 2-13-65 12-26-63 3-8-1 1-30-6 2-01-64 71755 71765 1-25-65 29-60-2-01-65 7272 79-92-6 1-01-64

Table 2-3-1 (6) Past Earthquake Records in North Luzon 1901 - 1977

	INTENSITY																																ě	į			
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EPICENTER	LONGITUDE		120.24	121.00	122°06°	120°30'	120.06	119.30	120.30	121.42	121°54	122 24	120-12	120-12	122.06	123°18	122.30	122.12	119.36	122,30	120.30	122 30	122.06	120*18	120.62	120.42	119.46	120.36	121.18	122"18"	121.84	119.48	120,36	121.36	120°48°	119.36.	119.48
EPIC	LATITUDE		15°30'	15,30,	16.48	13.42.	13.45	12.50	15°36	14.18	15°36'	15,00	13.54	13.48	16°18'	13.48	16.42	15.24	14.68	16.36	13°56	16.42	13,18,	13,26	13.68,	13.54	16.54	13.36	15,30,	105.91	15.18	14.45	14.54	16*18	13.48.	15"12"	14"12"
3614	HR-MIN-SEC			20-09-36											18-20-66											06-13-36		13-24-55	ŧ		23-03-23		:		13-24-26		
PATE.	NO-DAY-YR		10-26-66	10-26-66	10-27-66	10-29-66	10-31-66	10-31-66	11-05-66	11-21-66	11-30-66	12-02-66	12-20-66	12-20-66	12-20-66	12-22-64	12-23-66	12-23-66	12-26-66	12-26-45	12-24-46	12-24-66	12-26-66	1-02-67	1-05-67	1-05-67	1-14-67	1-16-67	1-19-67	1-24-67	1-24-67	1-25-67	1-25-67	1-31-67	1-31-67	2-17-67	2-18-67
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EP 1 CHAILTEA	LONGITUDE		121 12'	119.48	120-42	120,12,	121*54	119.54	120*30	119*42'	122.00.	120.06	121*54	119.56	120.06	122-12	122.10*	121.48	119.30.	130-30	130.45.	120.00	121°12'	. 9€,611	.95,611	121.00.	121.00	120-12	119.54	120°42'	120.34	120*30	119°36'	120.36	121*62	119.48	120"00'
0143	LATITUDE		15.48	15,30,	16.30	13,36	13.24	15.00.	13.8	16.42	15.18	13.24	15,30	14.42	16.10	14.34	13.24	13.46	14.36	16.18	13.42	15.16	15.42	14.00	.00. 17	15.36	13.36.	13.24	15°30'	16.42	14.54	13°54'	13.06	14.46	16.48	16.12	13°42'
2114	- FIF-		90-00 -8 0	00-00-00	00-00-00	00-00-00	00-00-00	00-00-00	15-30-21		1) 4),										24-34-33	15-62-13.0	80-00-90	00-00-00		21-50-53						12-06-16.0					
17.7	NO-DAY-YE		F-19-E	6-19-66	6-20-66	6-22-66	6-22-66	€-29-€6	7-01-66	7-06-66	7-06-46	7-13-66	7-13-66	7-15-66	7-19-66	7-22-66	7-27-66	\$-10- 6	33-90-	**-22-4	P-28-66	1-31-66	9-02-66	3-60-6	130 ES	9-26-66	9-28-66	10-01-6	10-01-66	10-01-66	10-09-66	10-11-66	10-16-66	10-18-66	10-18-66	10-21-66	10-13-66
	2		351	352	353	¥	355	×	357	35	359	3	7	38.2	X	Ž	× ×	¥	Ã	*	¥	37.0	17.0	22	373	374	375	3%	377	376	*	3	ī	18 2	Î	¥	Ñ

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ក្	191		13.06	120,00				***			4		:	9	
623	3-03-63		1,90.30	.90.121					70-2	20-1-10	S. 97	122°26	Ø.	33	
423	2-10-67		13.48	119.62				\S*	8-01-68	20-57-18	16.00	122"12"	6	33	
4.24	3-19-67	5-35-3.0	13.42	120'36'	•	*		3	89-10-8 8	21-15-3.0	15.42	121.48	5.7	33	
623	4-03-67		15.42	121,18	:		•	459	8-01-58	23-16-26.0	16.00	122-18	4.7	33	
Ą	4-05-67		16.36	121-129				997	8-01-68	23-45-10	15.24	122°26'	4	es es	· · · · · ·
623	4-07-67		16.918	101*AAB				794	\$-05-68	90-40-36	16.12	122°30	6.4	33	
×	4-08-47		\$ 4 4 8 9	1070141			•	462	8-02-68	01-05-49	. 90. 91	122°12'	5.0	ä	
2	5-02-67		B 17	9 4 4 6 7				463	8-02-68	01-55-36	16.18	121.54	4	33	
7	101			144 540	•			\$99.9	2-05-68	01-55-38	16.18"	121 54	99,	m	
4		1 6 - 50 - 54	20.031	11.7 No.			-	999	6-02-68	02-10-18	16.48	122.24"			
42.4	6		91 61	119 est				994	8-02-68	63-48-21	15°36	121.48	6.7	63	
(P)	5-16-62	4 14 67	200	. 20 . AZ T		:		467	8-03-68	04-24-60	16.00.	122 24			:
4		9 1 4	70 5		æ :	37.2		8999	8-02-69	04-58-29	16.12	122°06'			
¥	6-12-63	75 L			v1 ≈0	를 영		604	6-02-65	05-20-56	15.48	122"18"			
*	*** **********************************	:	200	171 68.				470	8-02-68	05-64-27	15.68	122°30°			
, ,			E .	130.00.				471	6-02-68	06-23-06	16°06	122*18*			
3	A THE			119.54.				472	6-02-68	07-11-51	18.56	132018			
9 3	\ 91 TO\			219*300				473	8-82-68	67-38-34	16.42	1270127			
	10-7		-	119*54.				676	6-02-68	2746	16198	1 2000			
3	7-05-67	21-09-08	73.46	22013	8	3		4	B-02-68	07-56-36	37 97	77.777			
3	7-14-67		14.46	119.42					8 - 2 - 2	9 7 6	7 7 6 7 6	27 777			
244	7-30-67	20-29-18	15.54	121 12	4	14	:	673	9 69	97-17-60	. S	122~30	-		
3	8-06-67	09-13-5.6	13.30	1.20°54				80.49	80-20-8	10-60 CF	. 24. 67	122.26			
} 	12-67	19-54-4.0	.R.91	120-121	en en	4	: .	\$ 7.5 \$ 7.5	89-20-8	13-09-40	26.41	.27.721			÷
3	9-10-67	13-49-16	16.48	121.121	ه. ه	22		087	0 0 0	73-30-43	.00-77	122.30.			
3	9-12-67	11-8-11	13.56	120.001) (4)	8-03-68	12-43-11	25 25	97.727			
£	10-17-67	11-00-11	74.00	121°54				682	8-02-68	18-27-23	. PC 77	. 777		,	
7		17-170	. 97. 97	119 54	85 89	2	•	1 PM	8-03-68	00-13 G	201.451	ØT 777			
\$	6-12-6E	23-26-3	13.40	120.43	5.0		· .	486	35.00	27-35-00 17-35-00	******	. MC 771			
2	7-05-68	11-11-49	36.97	119.48	4	78		587	# 10-F	01-50-34	16.7.91	20000			
3	77-10-4	11-03-32.0	16.30	122.30				4.84	8-03-E	01-55-28	1 40 %	1770300			
*25	7	11-50-55		122.26.				487	8-03-68	02-01-23	174.71	10000			
	7-10-1	11-44-21		122.24.				488	8-03-68	02-08-33	16.00	1226201		:.	
\$:	**-TO-*	18-27-36	15.24	122*12*		:		489	8-03-64	02-10-18	10.00	77.701.02			:
ŝ	*9-10-	20-19-21	.08	122,30, 7	7.3	ж	,	90	8-03-68	1	, 75 . ST	1224121			
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Table 2-3-1 (8) Past Earthquake Records in North Luzon 1901 - 1977

	DATE	TUE	141	EPICENTER						1.70	11.16	SOLUTION.	8040			
2	HO-DAT-YE	SHEW TOWN	LATITUM.	TATITUDE LONGITUDE	200	DETTER	THERMSTITE				CBC REA AN	20124141	PORC L	U O N		TENTEN STATE
					1	9				11 107 14	The state of the s		200		<u> </u>	
164	8-03-68	04-47-23	13.87	122.24	٠.,				526	20-03	22-32-12	15.54	122*18			
492	8-0.7-6	06-23-05	16.30	122*10'	8	37			\$27	3	23-36-17	15.30	122*12*			1
493	8-03-64	09-34-01	15.42	122*30*					526	90-90-8	01-18-45	15.42	121°42'			
*	8-03-68	10-00-11	15°44	122.30	4				\$25	99	02-12-44	15*36*	122*12*			
\$	8-03-68	11-50-50	76.36	122.121					83	-00-	03-06-27	16.36	122.24	5.1	33	
\$	#-60-	14-17-35	15.30	131 54	4.7	33			531	103	03-16-29	16*12*	121.54	4.3	43	
(\$	8-03-E	15-36-35	15,30,	122*30'	•	33			. 233	\$	04-53-04	15.42	121*54'	5.2	2	
*		15-51-48	16.00	122"24"	4.7	33			533	\$	05-53-52	15.42	171.27			
664	1	19-19-01	16"18"	122 30					534	\$	06-07-48	.81.91	122*06*			
8	\$	22-16-58	15°30	122*30"			į		535	- op-	07-21-57	15.42	121 *54	,		
ğ	‡	23-04-34	15 36	122.30					536	1	08-05-33	15"24"	122*30*			
302	89-10-8	02-04-44	16"42"	122*30'					537	-op	12-36-32	15*54	122.00			
ĝ	10-10-1	02-39-41	15.42	121.54					1	ģ	12-57-34	16.06	122*30*		•	
ğ	8-0-10	02-39-41	15.62	122.30	. ,	٠.			539	ş	13-25-39	15.42	122*26*		-	
ş	‡	03-13-41	15.34	122.30					240	4	14-22-00	15.54	122.24.			
\$	‡	85-66-76	16*18	121.48					¥3	-op	15-02-59	15.30	122.24			
ĝ	ł	03-08-42	15°36'	122*30'					54.2	þ	15-43-53	16.18	122.26			
Ş	‡	45-18-30	15°54	122*06					4	•	15-49-41	15.18	122°30'		:	
ğ	†	85-30-48	15.42	1122.06					264	4	21-48-29	15,36,	121.24			
240	‡	05-41-22	15.34	122°06'					25.	: -	22-11-47	15.24	122.06	,		
116	ŧ	61-95-90	16*18*	121.42.					246	ģ	23-39-27	15.30	122°30°			
213	ļ	07-16-36	13.36	122°30'					K	ę P	23-64-35	15*30*	121°48°	5.1	33	
25	į	07-56-16	15.30	122"18"					***	\$9-70-	01-29-16	15.30	122 30			
314	‡	06-05-14	16.30	132°24	5.1	81			848	89-07-6	03-53-25	15.42	121 *54	8.4	*	
\$18	-	15-22-38	16.13	122*30	5.0	33			550	e e	05-57-11	15.48	122*301			
978	- CO	02-19-43	16.00	121.54					551	-op	05-57-11	15.48	122"30"		:	
51,7	\$-02- 68	05-27-06	76.32	122°24'			•		552	9	10-58-02	16.00	122*24*		-	
\$18	ļ	06-31-04	× .9.	122.24					553	-dp	16-08-43	15.24	122°12*			
ž	\$	54-04-80	. %0. 9 1	121.48.		`			55.	ş	18-23-35	16.12,	122-12			
200	1	8-11-80	15*42*	121-68				٠	555	8-08-68	01-66-26	16°36'	122 24		1	
521	o d	10-48-46	16.18	122°12°					556	8-08-68	03-00-12	16,00,	122*00*			
\$22	-9	12-53-33	15°54"	122*24*					557	8-08-68	08-90-80	16°18°	122*30'			
523	#	16-51-09	16.00	122,00	4.6	£3			558	89-08-68	14-00-45	16.00	122.00.	5.1	17	
\$2\$	- op	19-64-33	16.12,	122*18"		:	ē.		559	8-08-68	20-35-19	15.54	122.221	·		
\$25		19-46-41	16-12	122.00			- !		260	8-08-68	21-10-06	16 00	122*24			
l																

Table 2-3-1 (9) Past Earthquake Records in North Luzon 1901 - 1977

	E A	111		EN ICENTER							DATE	工工版	EPICENTER	CNTER				
8	AY-YAI	MA MIN SEC		LATITUDE LONGITUDE	2	(NA)	LALEMS LLL			8	MO-DAY-YE	HR-MIN-SEC	LATITUDE	LONGITUDE	EAG.	DEPTHS	INTERSITY	
. 3	2	11.56.11	, A-100 t	. 71 - 66 1		Ì				,	,							
Į.		77-96-77	95	97 771						296	8-16-68	20-44-19	15,30	122.00.				-
%	99-60-g	02-22-57	8. 9.	122.06						297	8-17-68	11-00-11	15.48	122-18				
7	89-60-8	02-30-68	15 36	122 26						5.98	5-17-63	11-11-18	15.24	121.42				
Ź	89-60-9	02-47-48	16°36"	122.06						599	8-17-68	20-02-18	16.90	122.00°				
868	89-60-9	67-65-33	16.80	122.24				•		9	8-18-68	04-16-31	15.36	122.18				
200	(日本) (AC) - (B)	17-32-17	12° %	122.00						601	8-18-68	07-00-00	15.48	121°54°				
267	8-04-48 8-04-48	15-13-66	15.12	121°00'	4	8				602	8-20-8	24-17-05	72.27	122,00	-			
3	89-60-6	20-00-0Z	16.12	122,26	-					509	8-20-68	13-13-13	15.54	121.42				
S	89-60-8	24-33-56	15.42	121°56'	Ø.	3				Š	2-20-62	13-41-07	15°36°	122"24"				
510	8-10-68	57-88-78	16.54	122.24					٠	603	8-21-68	13-21-39	15.54	122°24°		•		
571	9-10-68	09-32-26	16,00	122*12						\$0.9 \$0.9	8-21-68	15-23-05	15.48	121.54				
572	3-10-68	10-03-10	15.42	121.38,		٠				. 409	8-11-8	15-31-53	16.00	122.00	-	-		
573	8-10-68	16-41-25	13.38	177.38	4	es es				603	6-22-68	16-42-13	15.24	121*30	5.5	25		
\$78	8-10-68	27-29-39	35.51	122°26						Ş	\$-22-58	19-29-55	16.24	121.54			٠	
\$75	8-10-68	19-49-58	17.00	122°24	.3	8.3				610	8-22-6B	21-24-43	16.36	122°24°				
96.0	6-11-6	SE-03-50	15.56	122"06"						51.i	8-23-68	05-19-36	15.54	122*26"				
C KA	6-11-66	17-21-69	16.34	122.24						612	8-23-6¢	14-06-26	15.68	122.00	*			
578	8-12-68	04-37-53	15.30	132°26						623	8-25-68	07-58-38	15.36	122 12				
2,5	\$-12-66	12-59-23	17.00	122"24"		92				\$18	8-25-68	23-11-35	15°42°	122.06"				
	8-12-68	17-69-10	16°48	122°30'		ę				61.5	3-26-58	23-08-05	15,36	122.42				
X	\$-12-68	18-09-26	15.36	121.48						616	8-27-68	04-24-45	15*12*	122.00	:			
7	8-13-68	0-14-59	13.36	121.42.	e.	Ą				613	5-25-68	02-15-16	15.18,	322"18"				
2	B-13-68	01-21-13	15.34	321°56						919	\$-20-66	20-42-16	15-36	122.00	•			
*	₽-13-6®	17-19-16	15.12.	122.00	÷					619	8-25-68	01-36-18	12.48	121.54	ις Ε.	1.7		
¥	#-13-48	19-05-03	16,00	122.24						620	8-29-68	02-11-24	15.24	122*30		. *		-
*	2-13-68	22-53-25	16.06	122*24						621	8-29-68	04-15-13	16.06	122*30				
3	8-13-63	23-64-18	16.00	122°24'	-					622	8-29-62	04-52-30	13.48	121.54		,		
9	6-14-68	03-55-23	13,18	122-12				٠		623	8-29-68	05-34-07	16.06	121.48				
ş	8-14-68	07-36-55	12,0%	122*30*	×. 4	a			-	624	8-29-68	06-18-05	15.42	122.00.				
2	8-14-68	11-47-28	15.30	122*30						625	8-29-68	06-19-49	1.5 30	122*06"				:
Ź	8-14-68	17-00-16	13,36	122,18,			÷.			626	8-29-62	06-32-07	16.06	121.36	:	:		··
2	#-12- 4	04-14-01	15.42	122"06"		:				627	8-29-68	08-05-30	15,30,	122.06	S.2	22		
2	8-15-68	09-17-57	15.48	122"18"		:				628	8-29-68	08-37-21	15.48	122"18"				-
£	B-15-68	11-11-05	15.42.	122"06"						629	8-29-68	12-26-03	15.48	121 30'				
ř	8-15-68	11-15-14.0	15.36	122"24"				•		6.30	8-29-68	15-13-05	15*30	122.06	-	ē		
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Table 2-3-1 (10) Past Earthquake Records in North Luzon 1901 - 1977

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| ZONCI TUDE | 122"12" | 122*18' | 122.18 | 122*24* | 122°12 | 121-42
 | 122-12 | 122.18 | 122.24 | 122"18" | 122*18' | 122°18' | 121-48
 | 121.48 | 122.24 | 121.48 | 122°24 | 122*18
 | 122.00. | 122.06 | 122*18" | 122-12 | 122-18' | 122.18
 | 122*18 | 122,00, | 122-12. | 122°00 | 122.12
 | 122*12 | 122*12* | 122*18 | 122°24° | 122,18
 |
| LATITUDE | 15*54 | 15°24' | 15,30 | 16*18 | 15.30 | 15.24
 | 15.30. | 15.36 | 15.43. | 15,30 | 15 26 | .87.91 | 15.26
 | 16.00 | 15.48 | 15,36 | 15.24 | 15°30
 | 15-42" | 15.42 | 15,30 | 15.36 | 15.12 | 15.12
 | 16.24 | 16.00 | 15*42* | 15.48 | 15.42
 | 15.42 | 15.42 | 15.42 | 15.42 | 15.42
 |
| IR-MIN-SEC | 10-54-30 | 13-00-04 | 17-02-38 | 05-00-05 | 10-17-04 | 07-32-09
 | 04-10-47 | 05-47-45 | 07-91-80 | 15-09-51 | 17-05-26 | 03-67-19 | 06-02-21
 | 11-07-33 | 05-25-23 | 14-33-10 | 04-11-48 | 04-53-24
 | 09-23-01 | 14-02-30 | 14-04-51 | 14-33-11 | 65-36-90 | 65-66-60
 | 20-37-23 | 06-23-12 | 17-21-14 | 12-15-52 | 16-08-06
 | 17-21-14 | 17-21-16 | 18-05-30 | 21-20-42 | 23-10-01
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| | 906 | 39 -30-6 | 89-90-6 | \$ 9 -80-6 | 89-90-6 | 890168
 | 89-90-6 | 9-11-68 | 9-11-68 | 9-13-64 | 9-13-66 | \$\$-17-d | P-14-68
 | 9-14-6 | 7-16-68 | 9-17-68 | 9-16-68 | 9-11-6
 | 89-81-6 | 9-18-68 | 9-18-68 | 8-13-60 | 89-67-6 | 9-11-6
 | 9-20-68 | 9-22-6 | 9-22-6 | 9-22-6 | 9-22-6
 | 9-22-68 | 9-22-68 | 9-22-68 | 9-22-68 | 9-22-68
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 | 672 | 673 | 674 | 878 | 676 | | 678
 | 679 | 089 | 683 | . 289 | 6.83
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| LONGITUDE | 122.24 | 122°18' | 122-12 | 122.18 | 122.18 | 121°42
 | 122.06 | 122.18 | 122.30 | 122-12" | 122.24 | 122*24 | 122.00
 | 122,12, | 122.06 | 122.12, | 122.06 | 122.18
 | 122.26 | 122.34 | 122°12 | 132.18 | 122°24 | 122°12"
 | 122°18° | 122"18" | 122.00. | 122*12". | 122-12'
 | 122°12' | 122*18* | 122.12 | 121 48 | 122°12'
 |
| LATITUDE | 15°30 | 15.36 | 15,18, | 15.24 | 13.36 | 15°54
 | 16.00 | 15,30 | 16.00 | 15.54 | 15.12 | ,21,51 | 16.00
 | 15.36 | 12.00 | 15,36 | 15.18 | 15.49
 | 12,36. | 13,30 | 15°36° | 15,30 | 13.36 | 15.30
 | 15.42 | 15.36 | 15.48 | 15,34. | 15.36
 | 15.24 | 15.30 | 15.36 | 15*42 | 15,10,
 |
| M-MIN-SEC | 15-28-15 | 15-53-49 | 16-04-12 | 17-22-38 | 18-05-53 | 21-04-07
 | 21-20-02 | 22-19-43 | 00-34-13 | 02-24-57 | 05-22-23 | 11-03-05 | 11-35-33
 | 20-20-14 | 22-28-17 | 23-44-32 | 04-44-18 | 07-X-14
 | 19-54-18 | 01-51-36 | 01-51-56 | 07-28-45 | 10-49-57 | 13-12-57
 | 18-08-18 | 22-19-43 | 23-24-45 | 07-28-45 | 01-29-46
 | 02-18-14 | 06-12-26 | 07-53-49 | 14-18-27 | 19-36-41
 |
| W-X21 | 8-22-68 | 123-61 | 1-39-48 | P-29-60 | 8-29-68 | 8-29-68
 | \$-53-6B | 8-53-6E | \$-30-6s | ₽ -30-6 2 | 8-30-68 | ₩-30-4 | #3-0K-4
 | 8-30-68 | -30-6 | 130-68 | 8-m-68 | 6-31-68
 | F-31-68 | 8-31-68 | \$-01- 61 | 3-10- | 3-10-4 | \$-01 -68
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| | NA-MIN-SEC LATITUDE LONGITUDE NAG DEPTME INTERSITY NO. NO-DAY-YE HE-MIN-SEC LATITUDE LONGITUDE NAG | NATIONAL MAILTONE LAW LONGITUDE MAG DEFTING NO. NO | HEALTHDE LONGITUDE MAG DEFINE HATERSITY HO. | No. NO. | No. NO. | 15-28-15 15°30' 122°24' (km) 666 9-04-68 10-54-30 15°54' 122°12' (km) 15-38-12 13°30' 122°12' (km) 15-38-12 13°34' 122°12' (km) 15-38-12 13°18' 122°12' (km) 15-38-12 13°18' 122°12' (km) 15°24' 122°12' (km) 15°24' 122°12' (km) 15°24' 122°12' (km) 15°34' 122°12' (km) 12°24' 12°24' 12°24' 12°24' 12°218' (km) 12°24' 12°24' 12°218' (km) 12°24' 12°24' 12°24' 12°218' 12°218' 12°218' 12°218' 12°218' 12°218' (km) 12°218' (km) 12°218' 12°218' (km) 12°218'
(km) 12°218' (km) | 15-28-15 15°30' 122°24' (km) (km) 666 9-06-68 10-54-30 15°54' 122°12' (km) 15-58-12 15°34' 122°12' (km) 15-58-12 15°34' 122°12' (km) 15-53-49 15°34' 122°12' (km) 15°54' 122°12' (km) 15°54' 122°12' (km) 15°34' 122°12' (km) 15°34' 122°12' (km) 15°34' 122°12' (km) 15°34' 122°12' (km) 15°34' 122°12' (km) 15°34' 122°12' (km) 15°34' 122°12' (km) 15°34' 122°12' (km) 15°34' 122°12' (km) 15°34' 122°12' (km) 15°34' 121°42' (km) 15°34' 121°42' (km) 15°34' 121°42' (km) 15°34' 121°42' (km) 15°34' 121°42' (km) 15°34' 121°42' (km) 15°34' 121°42' (km) 15°34' 121°42' (km) 15°34' 121°42' (km) 15°34' 121°42' (km) 15°34' (km) | 15-28-15 13°30' 122°24' (km) | 15-28-15 15°30' 122°24' (km) | 15-26-15 15'26' 122'24' 122'12' 15'26' | 15-26-15 15°30' 122°24' (km) | 15-28-15 15°30° 122°24° | 15-26-15 15'20' 122'24' 122'18' 666 9-06-66 10-54-30 15'54' 122'12' (ka) 15-31-49 15'34' 122'18' 666 9-06-66 13-00'-04 15'24' 122'18' (ka) 15-31-49 15'34' 122'18' 669 9-06-66 13-00'-04 15'30' 122'18' (ka) 15-31-49 15'34' 122'18' (ka) 15'34' 122'18' (ka) 15'34' 122'18' (ka) 15'34' 122'18' (ka) 15'34' 122'18' (ka) 15'34' 122'18' (ka) 15'34' 122'18' (ka) 15'34' 122'18' (ka) 15'34' 122'18' (ka) 15'34' 122'18' (ka) 15'34' 122'18' (ka) 15'34' 122'18' (ka) 15'34' 122'12' (ka) 15'34' 122'12' (ka) 15'34' 122'12' (ka) 122'18' (ka) 15'34' 122'18' (ka) 15'34' 122'18' (ka) 15'34' 122'18' (ka) (ka) 122'18' (ka)
(ka) (ka) | 15-26-15 15'90' 122'24' 122'12' 15-36-15 15'94' 122'12' 122' | 13-24-15 13-36 122-24 122-12 13-36 122-24 122-12 13-36 122-12 13-36 122-12 13-36 122-12 13-36 122-12 13-36 122-12 13-36 122-12 13-36 122-12 13-36 122-12 13-36 122-12 13-36 122-12 13-36 122-12 13-36 122-12 13-36 122-12 13-36 122-12 13-36 122-12 13-36 122-12 13-36 | 14-28-15 15-30 1327.24 127.18 MAG DEFTIGE PAG DEFTIGE DEFT | 15-23-15 113-30 122-72 | 15-21-13 13'30' 122'24' 122'12' 15-31-49 15'34' 122'12' 122'12' 15-31-49 15'34' 122'12' 122'12' 15-31-49 15'34' 122'12'
122'12' 122' | 15-28-13 13'30' 122'72' (ba) (ba) (ca) | 14-28-15 15'70' 122'74' | 15-28-15 15'70' 122'24' (ba) | 15-28-15 13'70' 122'74' 122' | 15-28-15 13'70' 122'24' 122'18' 666 9-06-66 15-06-10 15'24' 122'12' 122'12' 16-06-12 13'74' 122'18' 669 9-06-66 15-06-03 15'34' 122'18 | 15-26-15 117-107 1006/11708 Mag 000744 100745
100745 100745 | 13-28-15 117-105 1080 1 | 13-28-13 13-28 13-218 13-28 | 11-23-13 113'70' 122'73' (ba) (ca) | 13-23-13 117-05 1006/1702 1006/170 | 1.24-11 17.9 127.11 18.0 18.0 19.0
19.0 19 | 13-23-13 13-34 13213 48.0 12213 48.0 | 1.22-1.1 1.11 1.12 1.1 | 1.2.2.1.1 1.1.1.1.2 1.1.1.1.2 1.1.1.2 1.1.1.2 1.1. | 15-26-15 13-78 1 | 1-22-14 17.70 1.066.1108 1.066 1.07 1.066.1109
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Table 2-3-1 (11) Past Earthquake Records in North Luzon 1901 - 1977

		INTENSITY									,				-									:				1				٠.			: -		
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		DEPTHS	•			75	•	•								•	61		118	75	37	35		22	•	: .!					. 51		29	20		٠	
		X	80	6.3	3	7 7		4	v	, ,		4 6	,	5.2	4	. s.	5.2	4.6	S. 3	5.4	3.0	5:1		5.7	5.5	6.4	80.4	į.	4.7	4.3	. 00	4.9	8	6.4	4.5	8.4	3
	EP I CENTER	LOWCITUDE	120*30'	119.18	119.24	120.16	20.36	120*18	1318131	71 774	133,00	25 777	120.57	121,12,	121-00	100,36	120.54	120.54	120-42	120*12*	121 42	121-48	121°42"	121.54	121°54	121.42	121 54	121 042	121°42°	121.54	121 48	121.43	121.48	121.48	121"36"	121.48	121 36'
		LATITUDE	19*12	15.42	15,30,	13.16	13.48	1 1 2 2 %	10013	77 64	17.00	12.00	75.51	19"12"	19*12	13,36	13*30	18*42*	13.54	13.24	15.48'	15.48	15.24	15.42	15,30,	15.24	15,36	15.18	15,18	15,30,	15.24	15*36'	15.18	15.24	15.18	15*18	15°18'
1		HR-KIN-SEC	23-04-59.7	16-06-03.6	16-16-56.6	05-06-27.9	14-06-00.5	22-67-18 2	29-39-15	10-57-46 7	16-60-00	02-21-16 1	16-30-32 9	20-48-17.8	06-22-34 4	15-50-11	01-17-44.5	15-38-34.4	02-18-01	00-54-30.8	05-34-05.6	05-53-40.1	0.96-06-36	06-11-52.3	06-34-13.6	07-45-16.7	07-58-57.4	07-59-57	08-25-31.2	09-13-26.1	09-24-27	09-39-09.2	10-31-35.8	10-63-29.6	13-03-30.7	13-10-12.7	13-28-54.2
	DATE	MO-DAY-YR	11-05-69	11-11-69	11-11-69	32-22-69	12-23-69	12-28-69	1-06-70	1-21-75	1-24-70	07-82-1	2-12-70	2-23-70	2-24-70	2-26-70	3-04-70	3-13-70	3-29-70	6-06-70	4-07-70	4-07-70	-019-	100	93	6-07-70	ģ	-69	-op-	-09-	9	op)	þ	-60-	-op-	-op-	-op-
		2	736	737	7.7	736	740	74.1	14.7	3.4.2	777	745	7,46	747	768	749	750	751	752	753	754	755	7.25	757	758	759	760	191	762	763	764	765	992	767	768	769	770
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	3								1						5.1	5.2	5.8	5.1	5.0	9.0	ท	4.7	N.	5.0	•	1	4.7	2.5	5.1	5.0	4.7	\$.1	6.3	5.1	5.6		•
PICOTTE	LATITUM LOMESTUME		122.06	122*12	122-12	132.06	122*00*	122°24	122*00*	122.06	122*12	121 30	122.06'	121.48	121 54'	120.24	122*18	122"18"	122.06'	122"12"	120,38	121.5%	122.16	120.36°	121,42	122 12	119.36	121 54	122*14	119 36	120-42	120*18	121,121	119.36	120 06	119°36'	122*12*
EPI	LATITUM		15.18.	15.18,	15.24	12.84	16.18	15,30	16.06	15.48	15.36	15.42	15,30,	16.00	16.061	13°30'	16°18'	16.18	16.24	16.24	13,36,	15,30,	16.18	13.42	15*48	16.12	14.42	. 90. 91	15.12	75. 57	15.42	13.30	16.00	16.18	12,00,	14.24.	16.18
TIME	HR-MIM-SEC		18-06-43	19-51-01	04-51-22	12-12-10	09-49-61	14-50-50	14-59-46	19-05-42	\$ -60-B	04-03-48	09-24-24	08-51-35	09-34-57	22-21-19	04-59-23	09-41-16	08-03-18	16-00-30	07-15-50	92-20-90	17-11-29	05-37-30	07-41-31	15-27-40.6	02-10-21	07-53-03	20-17-25	17-05-17	11-06-37	86-89-08	13-12-55	18-10-36	12-48-05	08-48-47.1	07-19-08
TTAG	MO-24Y-YR		9-23-68	1-23-6	9-24-68	9-24-61	9-24-68	9-24-68	9-24-68	9-24-68	9-25-68	89-20-6	9-28-68	9-30-68	11-02-68	11-04-68	11-22-68	11-22-68	11-28-68	12-12-63	12-29-68	1-04-69	1-11-69	1-13-69	3-06-69	3-06-69	8-60-6	5-15-69	69-40-9	6-21-69	6-23-69	6-25-69	8-25-69	69-04-6	10-06-69	10-20-69	10-28-69
	9	-1	701	702	703	ğ	202	70%	707	2	\$	710	1112	71.2	713	714	71.5	716	7117	718	71.0	750	721	722	723	7.24	725	726	727	728	27	8	731	732	733	7.7%	735

Table 2-3-1 (12) Past Earthquake Records in North Luzon 1901 - 1977

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RPICENTER	CONCRETE	CONCILEDE	121.48	121,45,	122*06"	121.34	122.00	122.06	122.06	122.00	122*00*	122.12.	122*12	121 \$6	121.54	122.00	122-24	122.00,	121*48	122°24°	122.12	122*00*	122.00	121 56	122.18	122°30°	121*54"	121.54	121.54	122*24	122.12"	121°36°	121.18	122.42.	.750661
0.2		TAILTUDE	15.48	15.36	12.00,	12.06	15,12,	12.06	15.00	15.06	15.06	15.00	15.00	15.06	13.06	15.06	15.06	15°06'	15.06	12.06	15.06	12.061	15.061	15.06	15.88	15.06	14.48.	15.06	12.00.	13.06	15.12	15.18	14.56	.90.51	1 5.06
ERIL	200	HR-MIN-SEC	16-19-03.1	23-32-57.4	77-10-70	04-15-32.5	04-16-57.1	04-26-38.5	05-10-37.1	05-27-52.4	05-27-52.4	05-34-53	06-03-48.7	06-23-31.7	06-29-56.4	06-36-52.6	8.10-15-90	06-58-26.0	07-03-48.4	07-16-03.2	08-33-18	9-91-46.6	10-48-42.8	12-11-37.9	13-55-61.3	14-22-38.9	15-33-47.0	17-02-01.8	22-36-52.3	23-52-07.6	08-28-21.8	12-52-11.3	12-02-30.4	13-14-21.4	13-24-30.2
PATE	ייין קר איראפון ארראפון	MO-UM - I K	04-11-70	04-11-70	04-12-70	04-12-10	04-12-70	04-12-70	04-12-70	04-12-70	04-12-70	04-12-70	04-12-70	04-12-70	04-12-70	04-12-70	04-12-70	04-12-70	04-12-70	04-12-79	04-12-70	06-12-70	04-12-70	04-12-70	04-12-70	04-12-70	04-12-70	04-12-70	04-12-70	04-12-70	04-13-70	04-13-70	Q-15-70	04-15-70	04-15-70
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	T ONC LTON	SCIPLI TOMOT	121.43,	121 42	121°36'	121.54	121.42	121.42	121-42	121.54	121.36	121.36	121.42	121.48	121.36	122*00*	121.42	121*42'	121.44	121.42	121.54	121.43	121.44	121.7	121*42	122.00	121.40.	121.48	121.42.	121°36°	121.48	121*48	121.42	121.30,	122000
CENTER	7 .	∌ l	•		15.54	15.14	15.18	15,13,	15.18	12.48	15,18	15.18	15.40	15.30	15.48	15.30	115.36	15.11	15.24	15,30,	15.54	15,18	15.30	15.24	16.00	38.SE	13,30,	15,30	15°24'	15,18,	15.24	15.30.	15.42	15,30,	149626
EP ICENTER	I ATT THE	1111	15.54	13.48	1.5	H			100			٠		7.	22.5	-31.3	-39.S	20-13-17.7	21-23-56.6	71-33-52.3	03-#-12	22-67-39	22-33-44.3	22-47-10.2	24 K-25.6	28-32-35	8-2-3	26 43-27	10-08-05	10-18-49	11-39-35.2	17-59-52.9	00-01-15.4	00-23-15.2	12-17-57 2
TIME IPICENTER	14917	4	15-05-50.5 15*2	-	_			22-27-47.2	05-13-40.	07-22-47.4	20-06-90	8 + Y 16.	09-52-XE	09-58-30.2	14-38-22.5	16-14-31	17-54-23.	Š	==	Ľ	N	74	2	N 6	1 17	8	క	*	9	育	7	17	Ş	Š	1
	TALL SECTION AND THE SECTION A	THE LATEL WILL						-40- 22-27-47.2	4-04-70 05-13-40.8	-do- 07-22-47.	-ep-		-do- 09-52-54	-do- 09-38-3	-do- 14-38-	-do-	4-71	29-1	-12	04-04-70 22	04-04-70 22		<u>.</u>	04-04-70 22 04-04-30		ine Sant	04-09-70	95 02-50-10	04-09-70 IO	04-09-70 10-	04-09-70 11-	04-09-70 17-	04-10-70 00-	04-10-70 00-	24 00 01 12

Past Earthquake Records in North Luzon 1901 - 1977 Table 2-3-1 (13)

				ET ICENTER	•					DY II	1116	31 31	EP ICENTER			
ei —	P-DAY-YE	385 - ATM - AND	LATITUDE	LOMCI TUDE	20	(and	INTERSTITE		No.	MD-DAY-YR	RR-MIN-SEC	LATITUDE	CONCITUDE	MAG	DEPTHS	INTERSITY
**	24-15-70	17-21-04.5	15.06'	122°36'	₩			٠.	876	10-26-70	11-46-55.6	18.24	120 48	6.3)	
7	84-15-78	17-33-46.6	13.06	122.48				:	877	11-01-13	15-12-11.6	18.24	120.54	\$ 5		
24 3	04-17-70	GB-31-06.4	15.00.	122.36			-		878	11-07-70	23-18-24.0	18,30	120 34	5.4		
1	04-17-70	12-37-23.6	15°36	121.48	4.4				878	11-21-70	12-19-39.2	15.00,	120.06	5.5		
588	04-17-70	13-14-55.8	15.06	122-18	39		:			11-27-70	22-46-33.8	12.00	122*48	4.7		
974	04-17-70	14-33-39.2		122°24'	4.1				3.91	01-02-10	07-08-24.7	18.48	120.48	4.6		
ì	04-12-70	13-46-53.5	13.18	121°48°	œ.				388.2	02-24-71	19-20-16.8	19.12	151,06	\$		
3	04-23-70	13-26-23.4	15°16'	122°26'	4				883	03-04-71	04-59-51.6	75.91	120 36	6.9	÷	
5	06-25-70	17-53-26.1	15*16'	122*18*	4		,		988	07-10-71	11-50-18.9	14.06	119.54			
8	04-24-78	22-14-54.8	15-12	122"36"	-37 609				885	03-12-71	22-32-51.0	18,48	119.48	5.0	:	
955	04-27-70	2-43-08-5	15°06°	122.06	9 4				3	03-26-71	14-51-22.9	19.12.	120.24			
\$\$2	04-28-70	04-12-30.9	15.18	121.30	4.4				567	56-27-71	10-04-06.3	19.12.	121,12,	5.0		
653	04-28-70	14-29-12.5	15.36	122°30°	.F.				888	06-29-71	00-46-45.4	18.12	120.42	5.2		
***	05-01-70	03-22-13.4	15.42	121°48°	w)		-		68 3	77-10-90	00-26-13.6	18,00	120.18	2.0		
\$68	05-02-70	17-49-04.9	13.00	122*30	8				890	86-15-71	05-27-34.9	18 00	119.30	5.1		
***	05-04-70	02-33-17.2	15°42°	121.42	ις 10		:		831	07-02-71	01-21-38	15°54	120.12	6.9		
2	05-09-70	01-16-59.6	14.34	123.54	6.6				8	07-04-71	11-30-51:5	15°36'	121.54	2.5		
95	05-16-70	03-17-05.2	14.18	119.12	8.8	•			68	67-06-72	06-35-43.5	17.12	120,18	6.3		
\$	2-17-50	06-62-23.3	13.00	122 26	w.	٠			894	07-20-71	10-34-11.5		120.18	νς 49		
2	04-12-70	12-53-55.5	18°42'	122"16"	8				898	08-20-71	11-19-51.9		120.42	8.9		
ž	G-16-70	06-08-15.6	15.06	122.08"					969	09-03-71	02-17-26.2		120*36			
3	36-28-78	13-03-13.L	15.68	122°18'	ю. 0			•	8	09-04-71	14-11-31.5	1	121*42*	60 - 19		
*	24-27-76	16-22-66.5	18.24	120.00.	C-				896	10-07-71	09-39-21.6	ri p	121.48			
*	04-24-70	14-30-37.9	10.42	121.24	e .				\$	10-11-11	15-56-14.6	13,36,	122°30'			
*	04-23-70	20-36-53.4	15.48.	122.00.	4.7				8	10-15-71	02-33-16.1	.00 67	121.06			
1	07-10-70	14-11-08.1	15.30	121,30	.: .: 1.				401	11-03-71	01-38-52.4	17.48	122"24"	5.0		
ŝ	08-20-70	14-11-00-1	15.30	121.30					905	11-09-11	01-39-27.7	. 75 . 61	121*18	5.2		
7	04-23-70	09-04-13:3	14.42	120.12	**				903	01-14-72	00-01-32.8			 		
*	04-26-70	15-11-34.6	8.2	120.30	3.4				ğ	02-01-72	02-13-21.1		:	~ ~		
2	06-28-70	18-22-02.9	18.36	121-00.	5.1				905	02-05-72	68-32-31.0	."	121.30	**		
871	10-22-70	23-55-35.9	1.9.00	130.021					906	02-08-72	08-37-52.4		122*00	<u>ب</u>	·:	
872	10-04-70	23-38-02.5	.9.20	122°12*	•				907	02-14-72	00-39-20.8	. 1	122-18'	5-2		
873	10-06-70	17-08-38.2	19*54	122*18'	3.5				906	02-24-72	11-32-00.2		119.48	6.7		
27.8	10-04-70	20-157 W.S.	19-62	122*06*	*			:	606	02-29-72	13-00-45.0	4.5	120.27	~ ~		
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Table 2-3-1 (14) Past Earthquake Records in North Luzon 1901. - 1977

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	, 17°		4	4.5	4	9.4	5.1	5.2	4.3		9	4.5	4 .	5.3		4.1	5.7	4.7	**	- 1	5.1	9 .		5.1	2.4	6.	4:3	5.2	6.3	· ;	3	9.4	5.0	4.6	5.2	4.3	4.4	
EPICERTE2	ATTENDE LONGITURE		120.48	120*12	120.00	120,48	120.72	120-24	122.48	119.36	120.62.	120.54	119.36.	120*48	120.48	121,00,	121.12	121.18.	122.24	120°30'	119.24	120.48	122.00.	121.36	120,30,	119°42°	121.18	120.42	121.00	120°36'	122*12*	122.24	122°18'	122.24	122*26	121.06	121*12*	
ZPI(1 ATTTIME	200	13,30,	13.00.	17.18	13,48	.90.81	13,24	13,36	15.54	13,36	19*42	T2.24,	13,38,	13.42	18,30,	19.06	.87.61	16.24	13.48	14.24	18*18*	16.24	19.30	15.24	15.06	19.06	18.48	18.18	18.18	16.12.	16.12	16.18,	,90,91	15.18.	14.15	19.12.	
7,1962	Jan-Myw. co.	20 M	04-10-04.5	12-23-45.8	12-42-11.1	08-27-32.7	03-58-40.2	17-58-39.4	06-22-06.5	16-56-41.9	09-34-05.7	02-03-56.1	13-44-38.5	12-55-42.6	20-32-34.4	21-10-23.1	07-19-46.3	2 00-90-80	15-12-50.5	08-17-17.7	03-53-41.2	09-15-29.0	17-25-37.7	21-50-01.4	09-11-57.7	09-29-01.8	02-44-24.5	13-48-32.2	22-02-55.9	02-24-34.9	11-11-26.2	11-42-08.2	12-20-37.2	21-17-52.0	01-44-57.5	15-53-07.9	11-58-10.2	
PALTE.		- TO - TO - TO - TO - TO - TO - TO - TO	01-03-73	01-04-73	01-07-73	02-14-73	03-06-73	03-15-73	03-23-73	04-03-73	04-07-73	04-29-73	05-10-73	95-13-73	95-23-73	06-14-73	06-25-73	06-25-73	06-25-73	#-24-73	07-10-73	08-06-73	08-23-73	08-25-73	04-31-73	09-10-73	09-15-73	09-21-73	09-23-73	04-25-73	10-01-13	10-07-73	10-07-73	10-07-73	10-09-73	10-29-73	EL-09-73	
	Ş	i	*	947	276	496	980	951	952	933	954	955	356	957	954	\$8.60 60.00	3	198	%	X	ž	\$	*	2	3	698	9,0	971	972	973	974	975	9.26	977	82.6	626	930	
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		(III)	`. 																			•			•													
			4.5		8.0	5.4	9.4	5.1	5.0	5.1	5.3	6.0	4.7	4.7	•	S. S.	5.3	5.7	8.3	6.8	4.7	4.0	5.0	8.0	2.1			5.1	8.0	9.4	6.9			5.2		. 12	4.7	
		LONGITUM	120.48	120.18	119.42	120.30	120.24	120*30	120"36"	120 36	120.10	120-36	120,30,	120*30	120*42	120.021	120.30	122°18'	122.30	122°36'	122.18	122.24	122-12	122*24	122-12	122°18'	122.30	122-24	122°24°	122-24'	122.24	122-12'	X.021	121 30	121*34'	121.54	122.18	
	F 10 F 13 F	LATITUDE LONGITUME	13*30*	18.06	14.24	13.30	13.30	13.30	13.30	13,30,	13.30	13.30	13,30,	13.30	. m.	13,30	13.36	16.36	16*36	16.30	16.26	16.24	16.24	16.48	16.42	16.36	16.34	16°24°	16°36'	16.36	16.36	16.48	18.12	15.30	14.48	30.62	16.34	
		HR-MIN-SEC	08-29-20.6	05-03-46	12-44-13.2	20-46-35.9	04-16-40.5	04-30-19.5	04-10-44.9	04-49-42.9	08-34-34.6	06-69-42.9	04-X-X-0	14-17-45.1	01-29-36.2	15-15-34.3	16-07-08.6	24-20.1	04-11-13.0	1.9 -97-80	07-29-22.3	10-44-21.1	20-24-46.9	08-19-28.6	17-51-27.6	08-11-26.6	04-47-28.9	05-31-51.4	04-31-15.5	19-09-16.3	11-19-44.4	23-27-45.5	01-36-55.0	14-31-13.3	02-30-29.6	17-04-39.9	22-54-38.4	
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Table 2-3-1 (15) Past Earthquake Records in North Luzon 1901 - 1977

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Table 2-3-1 (17) Past Earthquake Records in North Luzon 1901 - 1977

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Table 2-3-2 Maximum Amplitude of Earthquake

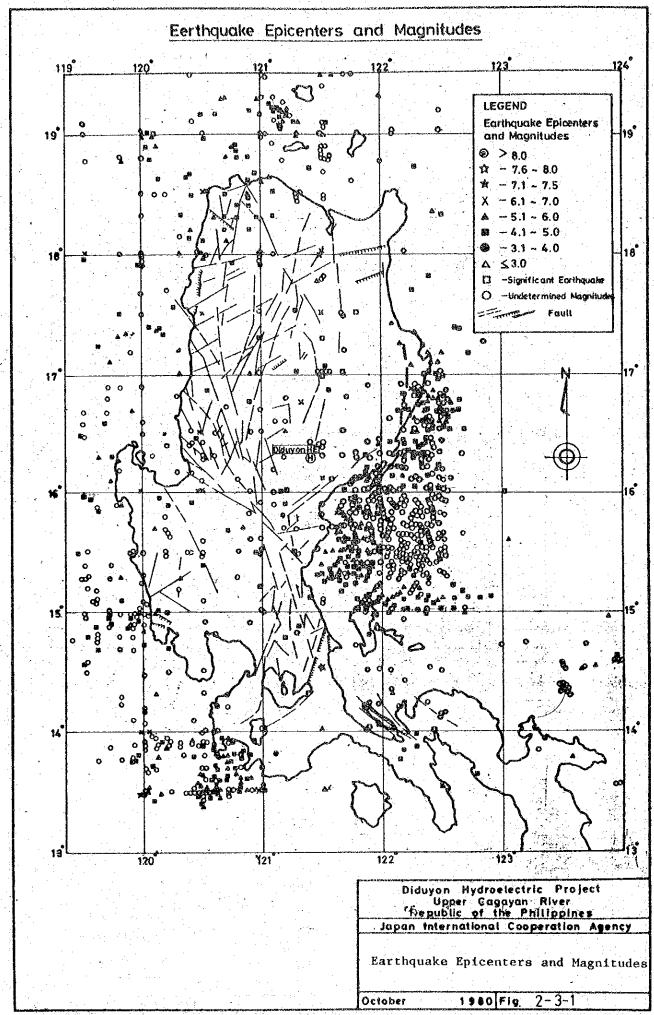
with Magnitude 5.5 ∿ 8.5

T(sec)M = 7.6 v 8.50.5 9.0 8 6.0 0.4 $T(sec)M = 6.6 \circ 7.5$ 0.5 9.0 0.3 4.0 0.7 $T(sec)M = 5.5 \sim 6.5$ 0.25 0.3 4.0 0.5 9.0 ∿ 100 ∿ 200 201 ∿ 250 0 ~ 50 101 ∿ 150 x (km) 151

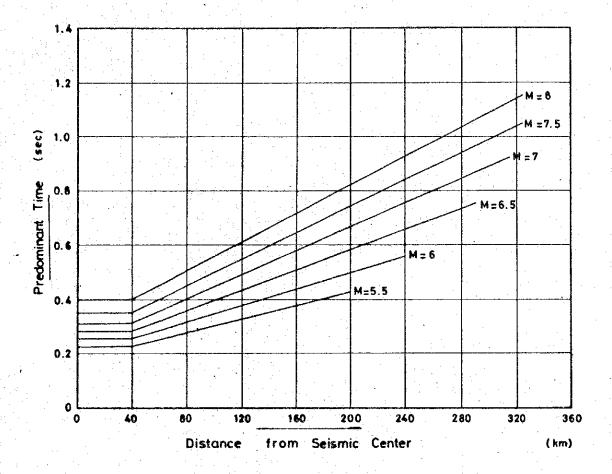
	Tab1e	2-3-3	Maximu	m Acceleration		
	Date of rthquakes		enter <u>E</u>	Magnitude	Acceleration at Diduyon	<u>Order</u>
190	l 12 14	14.000	122,000	7.80	(gal) 8.42	9
1907	4 18	14.000	123.000	7.60	4.93	16
192	7 4 19	16.000	120.000	6.75	4.62	18
192	8 8 5	16.000	119.500	6.25	1.87	- 28
193.	1 10 28	3 17.500	121.500	6.25	5.64	. 13
193	2 8 24	16.500	120.500	6.25	8.13	10
193	3 6 6	14.000	120.000	6.25	1.15	32
193	4 2 14	17.500	119.000	7.60	4.88	17
193	5 2 7	13,500	122,500	6.00	0.69	36
193	6 5 20	13.500	121.500	6.00	0.64	37
193	7 8 20	14.500	121.500	7.50	12.95	5
193	8 5 23	18.000	119.500	7.00	2.92	23
193	9 5 6	13.500	121.500	6.50	1.42	31
194	3 28	14.500	120.000	6.75	1.75	29
194	1 5. 9	14,000	123,000	6.75	1.92	27
194	2 4 8	13,500	121.000	7:80	6.29	11
194	8 3 3	3 18,500	119,000	7, 20	2.64	24
194	9 12 29	18.000	121.000	7.40	9.10	8
195	0 1 3	3 17.000	121.600	6.50	22.33	4
195	8 12 3	3 19.000	121.500	6.00	0.77	34
195	9 7 18	3 15.500	120.500	6.75	9.58	7
196	0 5 30	15.500	121.500	6.50	5.37	14
196	1 2 26	16.100	121.600	6.10	44.09	1
196	2 10 28	3 14.800	119,900	5.00 =	0.27	39
196	3 5 17	15.700	120.100	5.50	1.05	33
196	4 2 18	3 17.500	121.300	4,50	0.48	38
196	5 10 25	17.000	120.900	5,20	0.75	35
196	6 1 26	16.500	120.000	5.80	1.65	30
196	7 7 30	15.900	121.200	4.70	4.45	19
196	8 8 1	16.000	122.500	7.30	23.12	. 3
196	9 5 15	5 16.100	121.900	5.20	4.10	21
197	0 4 7	15.800	121,700	6.40	26.72	. 2
197	1 7 4	15.600	121.900	5.50	5.22	15
197	2 5 22	2 16.600	122.300	5,70	4.15	20
197	3 11 21	**	121.000	5.10	2.56	.25
197	4 9 18		122.100	4.80	2,50	26
197			121.900	4.60	3.18	22
197	6 2 13		121.700	5,40	6.25	12
197	7 4 20) 16.367	121.900	5.40	9.67	6

Table 2-3-4 Probability Acceleration

Probability Probability Metho	flity	Thomas Plot Method	Logarithmic Normal Method	Iwai Method	Gumble Method
Probability 10 Strength	100 years	64 8al.	51 gal.	53 gal.	37 gal.
Probability 20 Strength	200 years	88	69	71	67
Probability 30	300 years	104	80	78	97
Probability 500 Strength	500 years	128	26	101	50



Predominant Time of Maximum Earthquake Acceleration



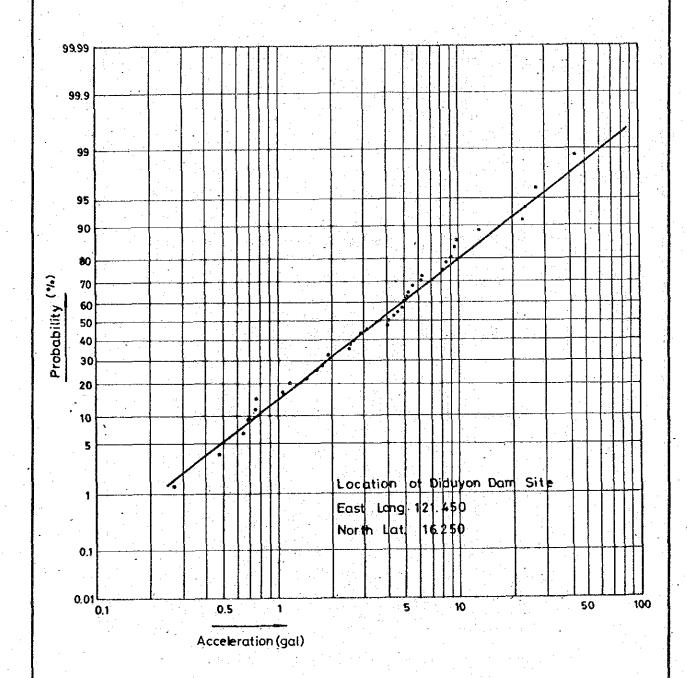
Diduyon Hydroelectric Project Upper Cagayan River Republic of the Philippines Japan International Cooperation Agency

Predominant Time of Maximum

Earthquake Acceleration

October 1980 Fig 2-3-2

Probability Diagram of Anticipated Seismic Intensity at Diduyon Damsite (1901–1977)

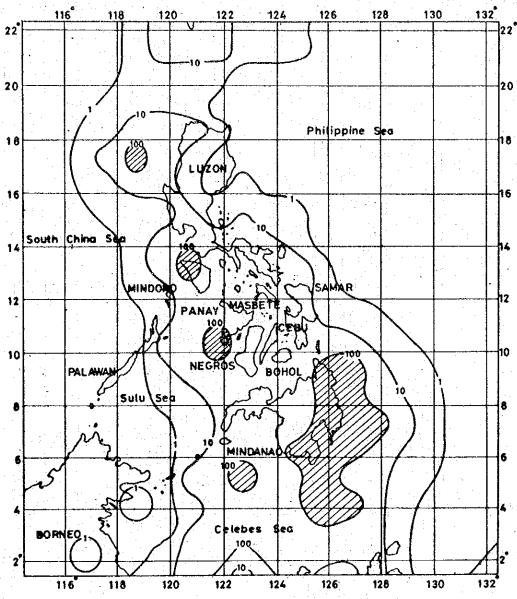


Diduyon Hydroelectric Project , Upper Cagayan River Republic of the Philippines Japan International Cooperation Agency

Probability Diagram of Anticipated Seismic Intensity at Diduyon Damsite

October 1980 Fig. 2-3-3

Seismicity of the Philippines



Seismicity Contours are numbered in $10^{15}\,\mathrm{ergs}~\mathrm{km}^{-2}~\mathrm{year}^{-1}$

Legend

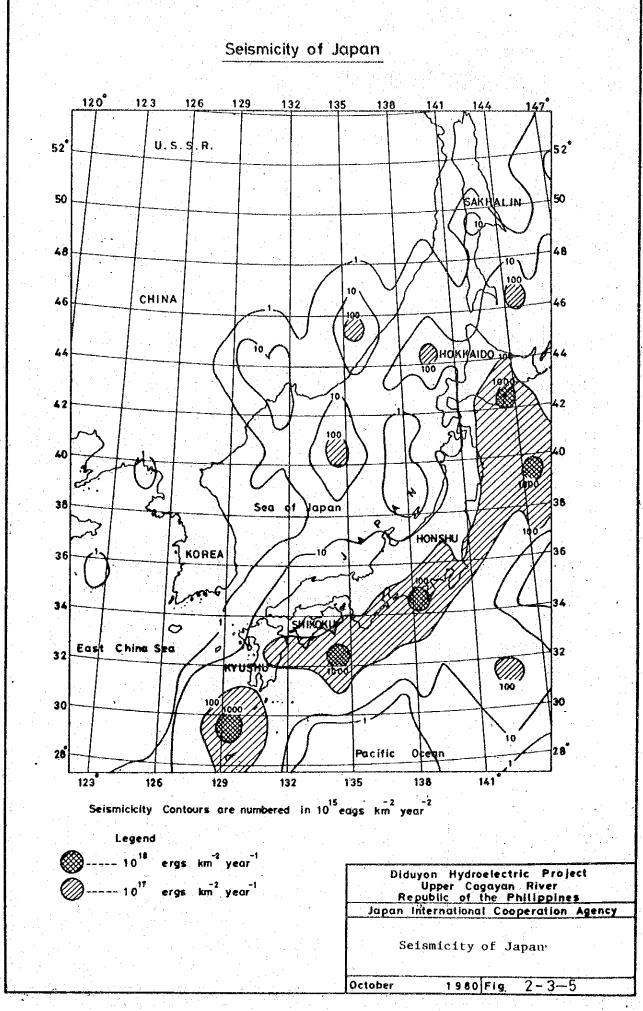
O se

-Seismicity of 10¹⁷ ergs km² year¹

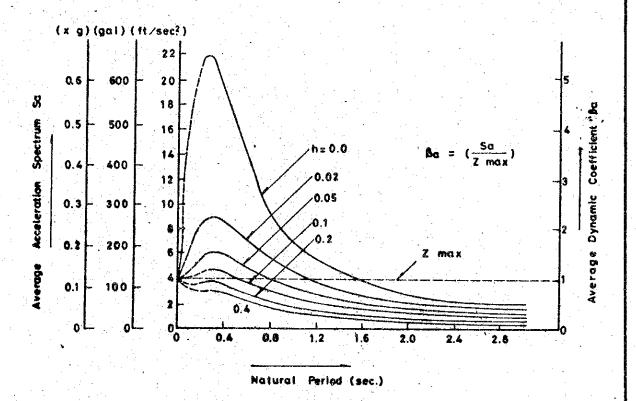
Diduyon Hydroelectric Project
Upper Cagayan River
Republic of the Philippines
Japan International Cooperation Agency

Seismicity of the Philippines

October 1980 Fig. 2-3-4



Relation between Average Acceleration Spectrum and Average Dynamic Coefficient



Diduyon Hydroelectric Project
Upper Cagayan River
Republic of the Philippines
Japan International Cooperation Agency

Relation between Average Acceleration Spectrum and Average Dynamic Coefficient

October 1,980 Fig. 2-3-6

2.4. Hydrology

2.4.1. Highwater Discharge

(1) Outline

In designing a dam, it is necessary to calculate the design flood volume needed for planning the capacities of spillway and diversion tunnels. Depending on the type of dam, a design spillway flood of 200-year return period for a concrete dam, and 1.2 times thereof for a fill dam, will be adopted. For the diversion tunnel, a design flood of 2-year to 20-year return period will be adopted. Here will be given the result of estimating the highwater discharge from study of the measurements of past floods and the run-off hydrographs derived by the kinematic wave method.

(2) Estimate from measured flood volumes in the entire Cagayan River Basin

Peak flood flows measured in the various rivers of the Cagayan River basin are given in Table 2-4-1. All of 23 gauging sites in the table have more than $100~{\rm km}^2$ of the catchment area. The minimum is $162~{\rm km}^2$ and the maximum is $6,266~{\rm km}^2$. The data made available as of 1965 cover from 2 to 25 years.

From the given values, the relation of unit discharge $q (m^3/s/km^2)$ to basin area A (km^2) was approximated in $q = C \cdot A^P$, and constants C and P were determined so as to form a envelope curve. Thus we obtain : $q = 137A^{-0.41}$ (Fig. 2-4-1).

In table 2-4-2 is given a tabulation of the annual maximum discharges over the period of 12 years between 1959 and 1970 at the Pangal gauging station (C.A. = $4,244~\rm km^2$) on the lower reaches of the project site, available from the BPW flow data. The probable highest discharges for the corresponding return periods of T = 2 to 200 years, are obtained using these values. From the logarithmic normal distribution equation based on the moment method and the ex-

treme value distribution equation based on the Gumble method, the following values were obtained (see also Fig. 2-4-2):

	Probable floo	d discharge
Return period	logarithmic normal distribution	Gumbel distribution
T (year)	Qp(m ³ /S)	Qp (m ³ /S)
1,000		40,000
200	27,500	32,200
100	24,500	28,600
20	17,600	20,300
10	14,500	16,600
2	6,700	7,000

As these are values for the catchment area = 4,244 km², it is necessary to convert them to the probable flood volume at a point having optional catchment area. The Creager equation $q = C \cdot A^P$ form is assumed between the unit discharge $q = (m^3/s/km^2)$ of the flood and the catchment area $A (km^2)$. Where the value P = 0.41 calculated from the flood peak values actually measured at the 23 points in the Cagauan River basin was used, then C_T , the value of C corresponding to each return period T, was obtained as in the table below from Qp obtained in the above. For the value of Qp, a value by the Gumble distribution was adopted, allowing for safety.

	*		
Т	$Q_{\mathbf{PT}}$	$Q_{PT} = Q_{PT/A}$	$C_{\rm T} = q_{\rm PT/A} - 0.41$
Year	r (m ³ /s)	(m ³ /s)	(m ³ /s)
1,000	0 40,400	9,519	292
200	32,200	7,587	233
100	28,600	6,739	207
20	20,300	4,783	147
10	16,600	3,911	120
	7,000	1,649	51

Probable flood discharges for the various return periods obtained using this C_T for No. 2 damsite ($C \cdot A = 462 \text{ km}^2$) and for No. 3 damsite ($C \cdot A = 477 \text{ km}^2$) result in the values shown on Table 2-4-3. And the 200-year probable flood for No. 3 damsite (concrete gravity dam) would be 8,900 m³/s, and that for No. 2 damsite (fill dam) would be 10,500 m³/s.

(3) Estimates from Rainfall

Normally, riverflow analysis of a site under investigation requires a hyetograph representing the basin in question and actually measured hydrological values corresponding thereto.

In other words, various constants showing the runoff characteristics of the basin are determined on the basis of several typical hyetographs and hydrographs actually measured in the basin. Probable flood corelating to probable rainfall can be obtained using these constants. With regard to the upper basin of the Cagayan River now udner investigation, no actually measured rainfall records that can be referred to are available, as the observation equipment has been very recently installed and measured data is insufficient. At the Pangal gauging station on the lower reaches, too, observations have been made merely by periodical reading of the water stages; no flood hydrograph data and available. Consequently, in developing the estimates at this time, average values (without verification of actual measurements) that can be empirically proved from past investigations were used as the constants for riverflow analysis. The procedure given below was applied for rainfall analysis.

- i) As no long-range data were available at the observation stations around the basin, records of maximum daily rainfalls over a period of 28 years for the entire territory of the Philippines were used as basic data.
- ii) Verification was made using actually measured rainfalls for October 16 17, 1967, which were taken out of the hyetographs observed in Baguio as giving the maximum values.

As these methods were considered to produce the value on the adequately safe side at least as far as the point in question was concerned, that is, as they should give flood discharge on the higher magnitude they may be considered compatible with the purpose of estimating the desing floods for the project.

(4) Method of Runoff Analysis

There are several methods available for calculating the runoff from the rainfall in the basin. Here runoff calculation was made under the kinematic wave method that permits direct incorporation of the topographical characteristics of the basin into the computation. Under this method, the basin is assumed as a combination of a number of square slopes and flow channels, and the flow of rain water down these sloped channels is hydraulically traced by means of the equation of motion and the equation of continuity. The basic equations are as given below.

For river channel

$$Q = AR^{2/3} j^{1/2}/n$$
 (1)

$$\frac{\partial A}{\partial t} + \frac{\partial Q}{\partial x} = q(t) \dots$$
 (2)

For basin slopes

$$h = KqP \qquad (3)$$

$$\frac{\partial h}{\partial t} + \frac{\partial q}{\partial x} = \alpha \gamma_e \dots$$
 (4)

where j: water surface slope

h: depth

A: Flow section area

Q: Flow volume in the river channel

n: Manning's roughness coefficient

q: unit flow on the slope

 $K : \sqrt{N/\sin\theta} P (P = 3/5)$

Ya: Effective rainfall

N: Equivalent slope roughness

 α : Unit conversion constant

 θ : Slope angle

With equation (1), (2), (3), and (4) set up simultaneously, numerical integration is performed to obtain a solution. Of the parameters in the above equations, equivalent slope roughness N and effective rainfall γ_e are of particular importance in practical calculation. Generally, such values should be those measured at appropriate gauging points in the basin area. In this case, however, 1.0 is employed as an emprically feasible value for N. While the effective rainfall γ_e is, for simplicity, assumed to be 70 % the actual amount of rainfall, taking into consideration the runoff coefficient to be incorporated in rational equations with respect to possible runoff into the rivers in mountainous regions. Topographic features of the watershed are modeled based on 1/250,000 and 1/50,000 topographic maps.

Figure 2-4-3 shows a model topography in the basin and constants applied.

(5) Analysis of runoff based on daily rainfall in the vicinity of the watershed

i) Daily rainfall

During a period of 28 years from 1948 to 1975, a total of 112 typhoons (cyclones) hit the Philippine Archipelago. Table 2-4-4 lists how much the 24-hour rainfalls were and where they were gauged at the time of 28 typhoons that caused the heaviest 24-hour precipitation in each year. As evident from this table, maximum daily rainfalls were recorded 9 times in the Baguio City, 100 km west of the upper watershed of the Cagayan River System. Of those, 9 belong to the first 7 of the 28 cases listed. Accordingly, it might be good to use this data, which was collected

In the survey covering the entire territory of the Philippines as basic material for computing the probable daily precipitation in the upper basin of the Cagayan River, though the resultant figures could be somewhat inflated. From these 28 pieces of data, probable rainfalls were worked out through the equation of extreme value distribution with Gumbel's method. The table below presents the results for the return periods of 2, 10, 20, 100, and 200 years.

Return Period	Probable	Daily Rainfall
T (Year)	R ₂₄	(mm/24 hrs)
200		1,345
100		1,212
20		901
10		763
5		404

ii) Hyetograph

Based on the probable daily rainfall for a 200-year return period obtained from the above table, a rainfall pattern was composed as shown in Fig. 2-4-4, which is necessary for computing flood wave. Using this hyetograph, runoff is calculated for three patterns. In composing the rainfall patterns, the following assumptions and conditions were incorporated.

- a) The unit period of time for rainfall patterns must be a duration within which peak flood is reached. Based on the results of some trial computations, the unit is set at 6 hours.
- b) For the conversion of daily rainfall into rainfall intensity, it is convenient to use the well-known equation $R = \alpha T^{\beta}$, which expresses the relationship between the rainfall duration T (hr) and the total rainfall depth R(mm). In this expression, $\beta = 1/2$ is employed for the coefficient β . This value is determined by measurement at the basin of the Chico River, one of the tributaries of the Cagayan

River (according to the design data on the Chico River). The value of α is then obtained by $\alpha = R_{24}/24^{1/2}$.

- c) The duration of rainfall is taken as long as 48 hours. For credibility's sake, preparation of the hyetograph is such that the peak rainfall appears in the latter 24 hours preceded by the first half period of antecedent rainfall.
- d) The aforementioned probable daily rainfall is the amount of spot rainfall. The conversion into the average precipitation for the watershed is carried out according to the Depth-Area-Duration Cuve presented in Figure 2-4-5, which was created with data from the Lower Agno Report.

As s a result of calculations, it was found that no conspicuous difference exists in the values of flood peak (Qp) due to the variation in the amount of rainfall as read from the prepared hyetograph, and 8,652 m³/s was obtained for the Diduyon No.3 Damsite. Figures 2-4-6 and 2-4-7 show the hyeto-hydrographs for the Diduyon No.3 Damsite and the Diduyon No.2 Damsite, respectively.

(6) Analysis of runoff based on the record of storm rainfalls in Baguio City

NAPOCOR provided us the record of Baguio Storm on the amount of rainfall (record of precipitation taken every 6 hours) observed in the past. According to this material, a maximum value of precipitation appears during the period shown in Table 2-4-5. The hyetograph is presented on a day basis in Figure 2-4-8. As generally said, extreme values are given by the data for the two consecutive days, 16th and 17th of October, 1967 (maximum daily rainfall 1,216 mm). Based on this data, analytical study was conducted under the same conditions as those for the preceding runoff analysis by daily rainfall in the vicinity of the watershed.

Figure 2-4-9 shows a hydrograph prepared in this way for the Diduyon No.2 and No.3 damsites. For the damsite No. 3, the runoff is estimated at $6,753 \text{ m}^3/\text{sec}$.

(7) Design-flood discharge

As stated in the preceding paragraphs, the probable flood discharge for a given return period was calculated from known flood discharges in the past in the watershed of the Cagayan River, Aside from this, the runoff in the river basin was studied from the amount of rainfall in the area by analytical means. The results of these computations are listed in the following table. (For information, the past highest flood as computed for the damsite is 614 m³/sec.)

200-year Probable Flood Discharge for Diduyon Damsite (m³/sec)

Damsite	Estimate from Peak Flood Discharges in the Entire Cagayan Watershed	Estimate from Rainfall	
	Buttle Vagayan watershed	Estimate from 200-year probable rainfall	Estimate from Baguio Storm
No.2 Damsite (Fill type)	10,500	10,100	7,900
No.3 Damsite (Concrete gravity	8,900	8,652	6,753

For the design flood discharge of a concrete dam, a flood discharge of 200-year return period is generally adopted. As seen in the above table, no basic inconsistency exists between the values worked out from peak flood discharges of adjacent rivers and those calculated from the amount of rainfall through runoff analysis. Rather, it might be concluded that these two figures are well corelated with each other. Accordingly, flood discharges of 8,900 m³/sec and 10,500 m³/sec are adopted for the design of spillways at the Diduyon

damsites No. 3 (concrete dam) and No. 2 (fill dam), respectivly. In case of the fill dam, the design flood discharge is usually taken 20% more than that of the concrete dam.

Fig. 2-4-10 presents an envelope curve plotting unit discharges (q) and drainage agrees (A) of past floods recorded at the watershed of the Cagayan River, q and A for each of the return periods of 2 through 1,000 years, and design values computed for other projects in the neighboring areas. As for typhoons and runoff, refer to Figs.2-4-11(1) through 2-4-11(3), which provide corellations with the measurements at the Pangal district.

Table 2-4-1
Observed Peak Flows in Cagayan River Basi

No.	River	Station	Drinage Area (km²)	Maximum Discharge (m ³ /sec)	Specific Discharge (m ³ /sec/km ²)	Period of Observation	Number of Year
1	Cagayan	Dippaddiw	2,323	13,071	5.626	1959-65	7
2	Dabubu	Dabubupequino	162	344	2.123	64-65	2
3	Olbulan	Minuri	272	666	2.448	64-65	2
4	Addalam	Guinalvin	721	1,420	1.969	64-65	2
5	Diadi	Cabulay	196	663	3.382	55-65	11
6	Cagayan	Pangal	4,244	17,550	4,135	58-65	8
7	n	Palattao	6,266	8,063	1.286	61-65	5
8	Matuno	Bante	558	790	1.415	56~65	10
9	Magat	Bats	1,784	1,540	0.863	58 -6 5	8.
10	Ibulad	Hap io	606	645	0.899	64-65	2
11	Magat	Oscariz	4,150	6,795	1.637	41-65	25
12	Taotao	Caipilan	430	531	1.234	55-65	11
13	Pin. De. Ilagan	Mananga	1,565	1,800	1.150	64-65	2
14	Casile Creek	Casile	195	241	1.235	49-65	17
15	Siffu	Munoz	686	997	1.453	48-65	18
16	Pin. De. Tumauni	Antagan	170	1,004	5.905	64-65	2
17	Pinacauan	Larionalts	655	2,775	4.236	55 - 65	11
18	Panga1	Pangal	312	4,014	12.865	55 - 65	11
19	Paret	Calantac	907	2,476	2.729	57 - 65	9
20	Chico	Pasonglao	1,987	4,040	2.033	63-65	3
21	Matalag	Escolta	655	1,195	1.824	64~65	2
22	Dummon	Calaoagan	308	1,238	4.019	64-65	2
23	Sinunouogan	Simay	189	1,265	6.693	59-65	7

Source: Technical Series No. 18
Envelope Curve for Peak
Discharges in the Republic
of the Philippines
Jan., 1973

Table 2-4-2

Annual Maximum Discharge at Pangal (C.A. = 4,244 km²)

Year	Discharge (m ³ /sec.)
1959	17,550
60	4,810
61	5,270
62	7,560
63	6,790
64	4,300
65	1,460
66	12,320
67	16,010
68	5,030
69	1,460
70	9,710

Source: Chico River

Hydrology Report No. 2 Flood Studies Feb., 1975

Table 2-4-3 Design Flood Discharge

			· ·· · · · · · · · · · · · · · · · · ·		· · · · · · · · · · · · · · · · · · ·	
scharge)	120%	13,300	10,700	9,500	6,700	2,300
Flood Di	100%	11,100	8,900	7,900	5,600	1.900
Specific Discharge	$(m^3/s/km^2)$	23.29	18.59	16.51	11.73	4.07
tharge	120%	13,100	10,500	9,300	6,600	2,300
Flood Disc (m³/s).	1,00%	10,900	8,700	7,700	5,500	1,900
Specific Discharge	$(m^3/s/km^2)$	23.60	18.83	16.73	11.88	4.12
E	year	1,000	200	100	20	2
	Flood Discharge (m³/s)	Specific Flood Discharge Specific Flood Discharge Discharge (m^3/s). Discharge (m^3/s) $(m^3/s/km^2)$ 100% $(m^3/s/km^2)$ 100%	Specific Discharge (m³/s) Flood Discharge (m³/s) Specific (m³/s) Flood Discharge (m³/s) (m³/s/km²) 100% 120% (m³/s/km²) 100% 23.60 10,900 13,100 23.29 11,100	Specific Discharge (m³/s) Flood Discharge (m³/s) Specific (m³/s) Flood Discharge (m³/s) (m³/s/km²) 100% 120% (m³/s/km²) 100% 23.60 10,900 13,100 23.29 11,100 18.83 8,700 10,500 18.59 8,900	Specific Discharge (m³/s) Specific (m³/s) Flood Discharge (m³/s) Flood Discharge (m³/s) (m³/s/km²) 100% 120% (m³/s/km²) 100% 23.60 10,900 13,100 23.29 11,100 18.83 8,700 10,500 18.59 8,900 16.73 7,700 9,300 16.51 7,900	Specific Discharge Flood Discharge (m³/s) Specific (m³/s) Flood Discharge (m³/s) Discharge (m³/s) 100% 120% (m³/s/km²) 100% 23.60 10,900 13,100 23.29 11,100 18.83 8,700 10,500 18.59 8,900 16.73 7,700 9,300 16.51 7,900 11.88 5,500 6,600 11.73 5,600

Table 2-4-4 Annual Highest 24-hr. Rainfalls

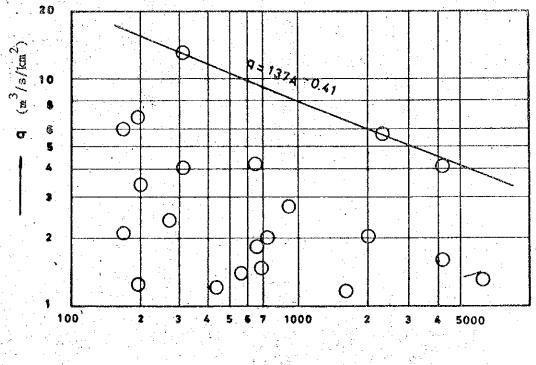
No.	Year	Rainfall (mm)	Location
1	1948	530	Clarian
2	9	391	Daet
3	1950	418	Balatoc Mr. Province
4	1	754	Atoc
5	2	432	Valderama, Antique
6	3	214	Lacag
. 7	4	368	
8	5	389	Ilagan, Isabela
9	6	283	Baguio
10	7	1	Casiguran
•	1	423	Baler
11	8	459	Virac
12	9	388	Catbalagan
13	1960	356	Iba
14	1	288	Laoag
15	2	409	Laoag
16	3	320	Baguio
17	4	417	Virac
18	5	368	Baguio
19	6	316	Roxas
20	7	1,216	Baguio
21	8	650	Baguio
22	9	546	Baguio
23	1970	235	Catbalagan
24	1	121	Legaspi
25	2	480	Baguio
26	3	331	Baguio
27	4	818	Baguio
28	5	278	Legaspi

Table 2-4-5 Six-hr Maximum B

Six-hr Maximum Rainfall Data at Baguio City

DATE	2:00 P.M.	8:00 P.M.	2:00 A.M.	8:00 A.M.	TOTAL
May 25, 1976	171.7	141.2	162.1	130.3	605.3
June 30, 1976	57.7	132.4	95.5	8.66	385.4
October 11, 1974	157.0	390.2	151.4	82.8	781.4
July 17, 1972	57.7	128.3	142.2	151.4	479.6
June 6, 1967	22.4	80.0	53.3	57.2	212.9
October 16, 1967	0.3	10.2	96.3	268.0	374.8
October 17, 1967	445.8	334.5	167.4	31.7	979.4

Envelope Curve for Observed Peak Flows
In Cagayan River Basin

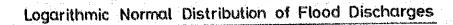


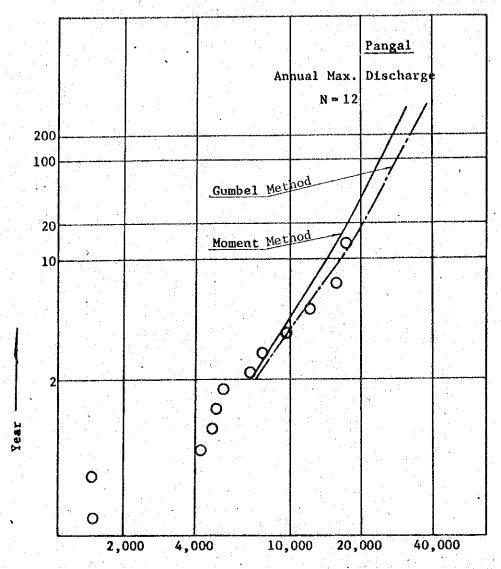
A (km²)

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Envelope Curve for observed Peak Flows in Cagayan River Basin

October 1980 Fig. 2-4-1





Discharge (m³/sec.)

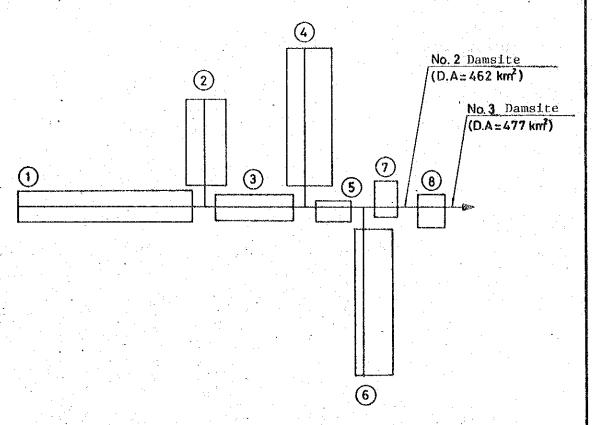
Period	Flood Disch	ISTRE (M)
(year)	Moment Method	Gumbel Method
200	27,500	32,200
100	24,500	28,600
20	17,600	20,300
10	14,500	16,600
2	6,700	7,000

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Japan International Cooperation Agency

Logarithmic Normal Distribution of Flood Discharges

October 1980 Fig. 2-4-7

Hydrological Model of Diduyon Drainage Area for Kinematic Wave Method



	River Cl	nannet	Left B	onk Ar	ea	Right	Bank	Area	Orainage Area
• •	L	ı	L	1	A	L	: 1	A	δA
Block	km	10 ⁻³	km	10-3	km²	km	10-3	km²	km²
1	24.45	64.4	2.25	158	55.01	2.22	123	54.28	109.29
2	11.9	29.8	2.96	152	35.22	2.4	100	26.56	63.70
3	11.15	1.8	1 67	109	18.62	1.82	110	20.29	38.91
4	18.85	7.5	3.7	68	69.75	2.39	105	45.05	114.80
5	4.95	1.1	0.85	155	4.21	2.12	110	10.49	14.70
6	20.15	33.7	1.31	118	26.40	3.91	105	78,79	105.19
7	3.15	4.8	3 71	129	11.69	1.21	1535	3.81	15.5
8	3.80	4.8	1 18	160	4.48	2.79	110	10.60	15.08
Total		*		·*····································				1.	477.25

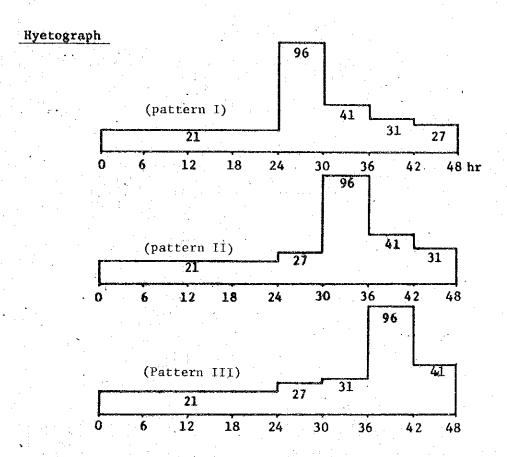
L : Length I : Slope A : Aren

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Hydrological Model of Diduyon Drainage Area for Kinematic Wave Method

October 1980 Fig. 2-4-

Rainfall Patterns for Computation of Flood Waves



- 1. 200-year probable daily rainfall (spot rainfall) R_{24} = 1345 mm 2. 6-hour continuous rainfall R_t = $R_{24}(t/24)^{1/2}$ = $K_t^{1/2}$ $(K = 1,345/24^{1/2} = 275)$

•	t (hr)	Rt (mm)	Δ Rt (mm)	rt (mm/hr)	P∗∗	r (mm/hr)
Ŀ	6	673	673	112	0.86	96
	12	953	280	47	0.87	41
ļ	18	1167	214	35	0.88	31
Į.	24	1345	178	30	0.89	27
L	48	1905	560	23	0.91	21

Diduyon No. 3 Dam

$$D.A. = 477 \text{ km}^2$$

*
$$R_t = \alpha t^{1/2}$$
 } $\frac{R_t}{R_{24}} = (\frac{t}{24})^{1/2}$

** Refer to Fig. 2-4-5

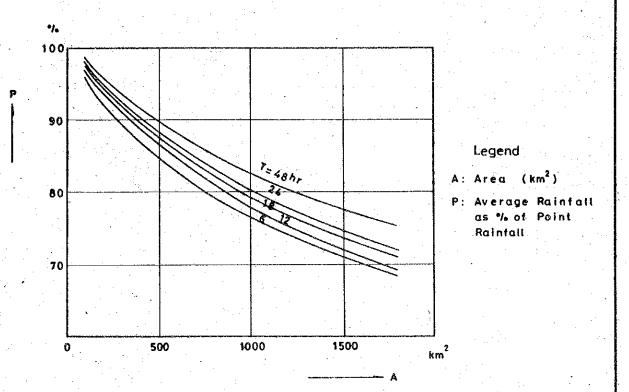
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Rainfall Patterns for

Computation of Flood Waves

October 1980 Fig. 2-4-4

<u>Depth - Area - Duration Curve</u>



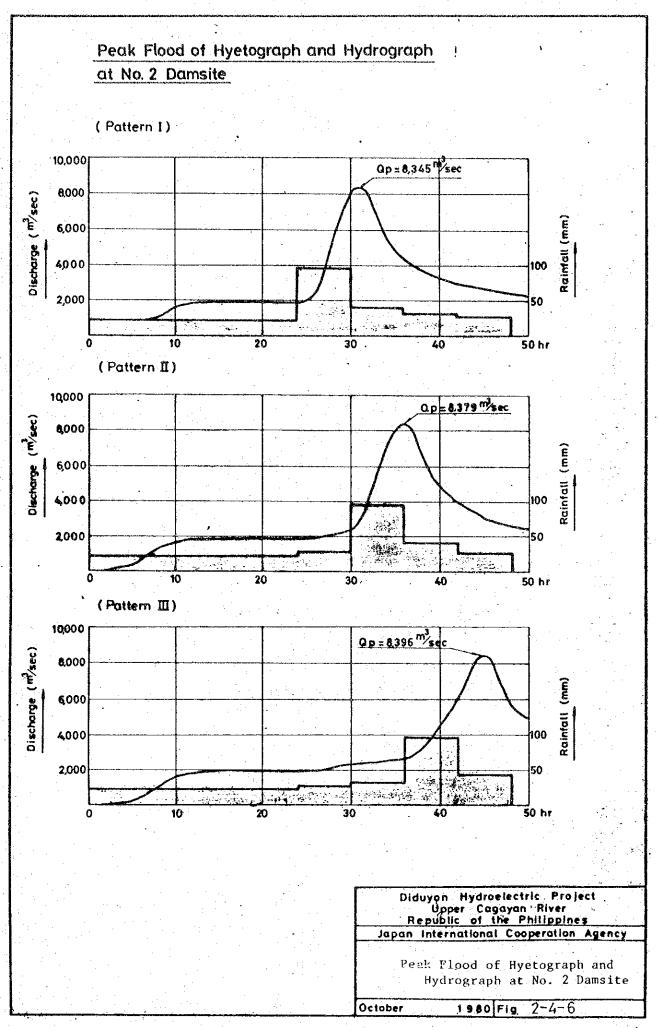
Lower Agno Dev. Plan By Electroconsult, July, 1976

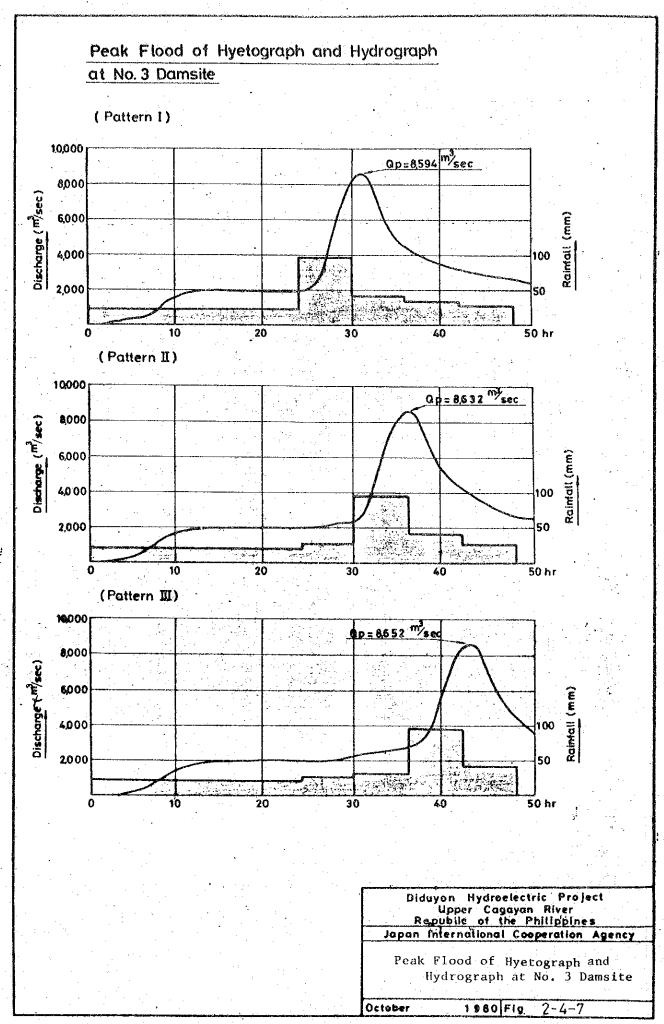
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Depth-Area-Duration Curve

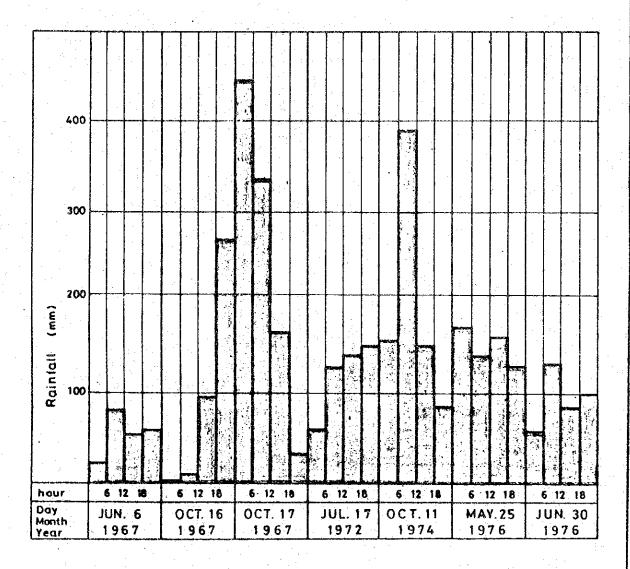
October

1980 FIg. 2-4-5





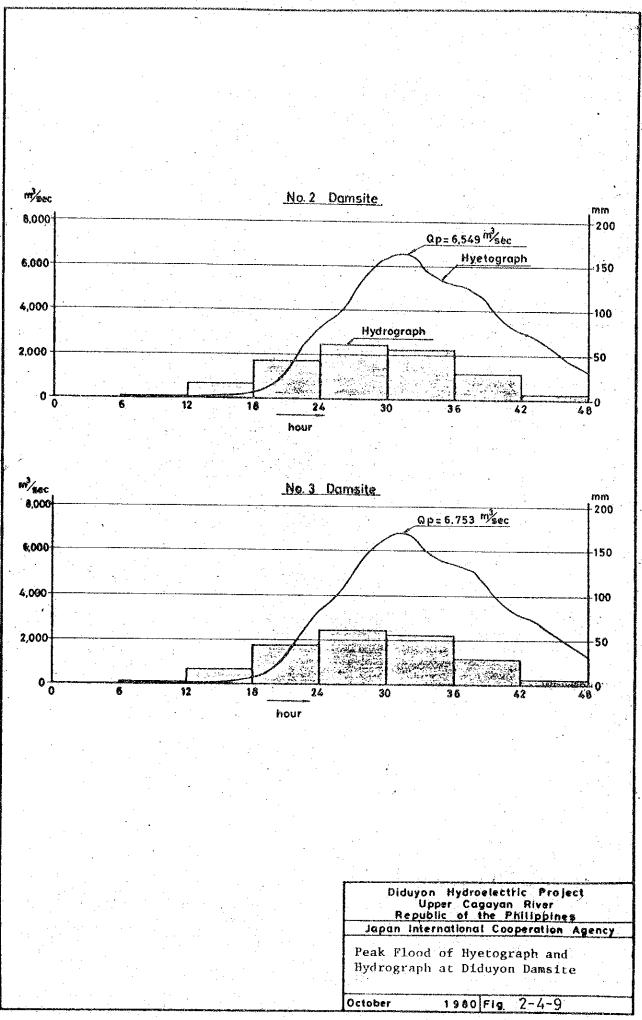
Rainfall Intensity at Baguio City



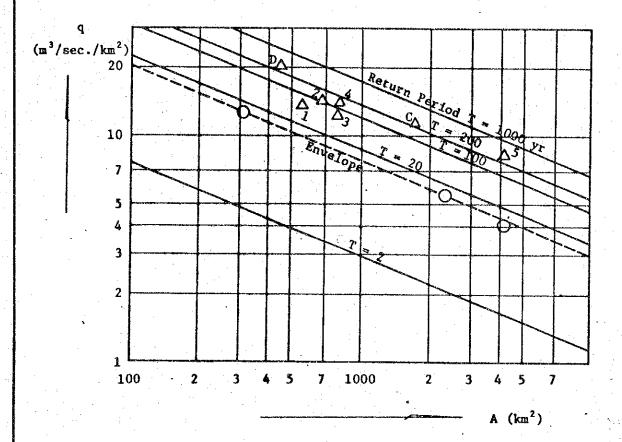
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Rainfall Intensity at Baguio City

October 1 940 Fig. 2-4-8



Relation between Specific Discharge and Catchment Area (North Luzon)



- 1: Angat
- C: Cabingatan
- 2:
 - Ambuklao D: Diduyon
- ·3: Binga
- 4: UPRP
- Magat

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Relation between Specific Discharge and Catchment Area (North Luzon)

October

1980 Fig.

