

(MPPENDIX)

BERTEMBER 1974

CODESTATION ASSETTEN



THE REPUBLIC OF THE PHILIPPINES

REPORT ON

CAGAYAN VALLEY ELECTRIFICATION PROJECT

(APPENDIX)



SEPTEMBER 1974

JAPAN
INTERNATIONAL
COOPERATION AGENCY

国際協力事業団
| 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 | 108 |

CONTENTS

			Page	
A-1	Tempor	rary Electrification Scheme for Irrigation	• A-	1
	A-1-1	Objectives	· A-	1
	A-1-2	Outline of Equipment and Facilities	• A-	2
	A-1-3	Construction Cost	- A-	2
	A-1-4	Power Cost of Diesel Power Plants (for Temporary Purpose) and Salable Energy Rate at the Consumer's End		3
	A-1-5	Construction Schedule		
	A-1-6	Comments		
A-2	Demand	l Forecast	· A-	7
	A-2-1	Forecast on Power Demand by Sabstations	· A- '	7
	A-2-2	Area and Power Demand of Proposed Irrigation Pump Projects by Substations	• A-1	0
A-3	Cagaya	n Transmission Line and Substation Scheme	• A-2	1
A-4	Analyse	es of Electric Power Systems	- A-3	5
	A-4-1	Outline	· A-3	5
	A-4-2	Voltage Regulation	· A-3	5
	A-4-3	Transient Stability	· A-3	7
	A-4-4	Short-Circuit Capacity	· A-38	8
A- 5	Protect	ive Relay System of Transmission Lines	• A-5	5
	A-5-1	Basic Principle of Preliminary Design	• A-5	5
	A-5-2	Outline of Preliminary Design		
•	A-5-3	Outline of Facilities	• A-5	7
A-6	Distrib	ution Line Scheme	· A-6	1
A-7		llocation of 230 kV Transmission Line		2

APPENDIX A-1 TEMPORARY ELECTRIFICATION SCHEME FOR IRRIGATION

Appendix

A-1 Temporary Electrification Scheme for Irrigation

A-1-1 Objectives

The Government of the Philippines has been exerting its utmost to self-reliance in production of rice which is a staple food for Philippine people as one of its highest priority policies in order to depart from the present situation of depending upon foreign countries for a considerable quantity of rice and for the purpose of coping with demand for this food due to annual increase in her population which is exceeding one million.

Because of the above background, it is the ardent desire of NEA that electrification of the Cagayan Valley for irrigation be materialized as soon as practicable. Bearing this necessity in mind, the Team has studied the Cagayan Valley Electrification Project with a view to minimization of a construction period which will be allowable from a technical point of view.

During the stay of the Team in Manila, NEA expressed its desire to erect large diesel power plants whose manufacture and delivery can be made in a short period of time, at three site and to construct 69 kV transmission lines and receiving substations as well as distribution lines as a temporary measure for acceleration of electrification for irrigation in the Valley up to the beginning of 1978 when the Cagayan Transmission Line and Substation Scheme is scheduled to be commissioned.

The temporary electrification scheme pivoted on erection of the above-mentioned diesel power plants has been worked out lest useless investment should be made to construction of transmission lines, substations and distribution lines prior to completion of the Cagayan Valley Electrification Project although the above-mentioned diesel power plants will be used for temporary purpose. Elaborate consideration was also bestowed on effective utilization of the transmission lines, substations and distribution lines to be constructed under this temporary scheme even after completion of the Cagayan Valley Electrification Project with a view to prevention of possible double investment.

A-1-2 Outline of Equipment and Facilities

A large-scale generating complex composed of many diesel power plants is to be erected in Solano, Santiago and Tuguegarao. And 69 kV transmission lines and receiving substations that are the same as those described in this report will be constructed. If the transformation facilities given in 5-2-2, i.e. 13.2 kV/69 kV step-up equipment is to be installed in Solano, Santiago and Tuguegarao while equipment at Ilagan, Cauayan and Camalaniugan Substations is to be the same as that stated in this report, the temporary diesel power plants for this temporary scheme are given hereunder.

2 units of diesel power plants with an installed capacity of 3 MW each	At Solano
5 units of diesel power plants with an installed capacity of 3 MW each	At Santiago
4 units of diesel power plants with an installed capacity of 3 MW each	At Tuguegarao

Relation between the Cagayan Transmission Line and Substation Scheme and the temporary electrification scheme is as given in Fig. A-1-1.

A-1-3 Construction Cost

The breakdown of the construction cost of this temporary electrification scheme in the respective currency portions is as follows:

(In Thousand U.S. Dollars)

Items	Foreign Currency	Domestic Currency	Total
Diesel Power Plants (11 un	its) 8,760	1,800	10,560
69 Transmission Lines (140 k	m) 1,430	1,220	2,650
Substations (6 site	s) 2,670	360	3,030
Distribution Lines	3,700	1,940	5,640
Total	16,560	5,320	21,880

Refer to Table 5-10 in the report for the particulars of the construction cost of diesel power plants described in the report. The total construction cost of the 69 kV transmission lines has been tabulated by adding their indirect costs to their direct costs given in Table 5-3.

That of the distribution lines is as shown in Table 6-2.

A-1-4 Power Cost of Diesel Power Plants (for Temporary Purpose) and Salable Energy Rate at the Consumer's End

Power cost and salable energy rate at the consumer's end under the temporary electrification scheme have been obtained by multiplication of the construction cost by the annual cost rate given in Table 5-9. As a result, 51.9 mills per kWh and 59.2 mills per kWh have been tabulated as power cost and salable energy rate at the consumer's end. The latter is approximately two times as expensive as the salable energy rate of 29.3 mills per kWh at the consumer's end which will be made available in 1978 upon the commissioning of the Cagayan Valley Electrification Project.

A-1-5 Constrution Schedule

The period required for order and delivery of the diesel power plants is estimated to be 10 months. In addition, if the period of their erection at the site is to be 4 months and that of constructing the transmission lines, receiving substations and distribution lines under this scheme is assumed to be the same as those given in Fig. A-1-2, it is estimated that this temporary electrification scheme will be completed at the end of 1976, which is one year earlier than the completion date of the proposed Cagayan Valley Electrification Project. The construction schedule of this scheme is as shown in Fig. A-1-2.

A-1-6 Comments

As stated before, power transmission by erection of the diesel power plants is to be commenced only one year before completion of the Cagayan Valley Electrification Project.

It will be considered possible to transfer such diesel power plants to other places. Nevertheless, various expenditures will be required from their disassembly, transport, installation and foundation construction at new sites which will amount to about 30% of the total construction cost of the diesel power plants shown in A-1-3. It is believed that investment for this purpose is not sound.

For the above reasons, after careful evaluation of merits and demerits of this temporary electrification scheme to hasten the commencement date of electrification for irrigation in the Valley by one year, compared with the commissioning of the Cagayan Valley Electrification Project, it is essential that the Government of the Philippines decide on its policy concerning electrification measures for irrigation in the Valley.

Scheme in Cagayan Valley. Electrification Fig. A-1-1 Temporary

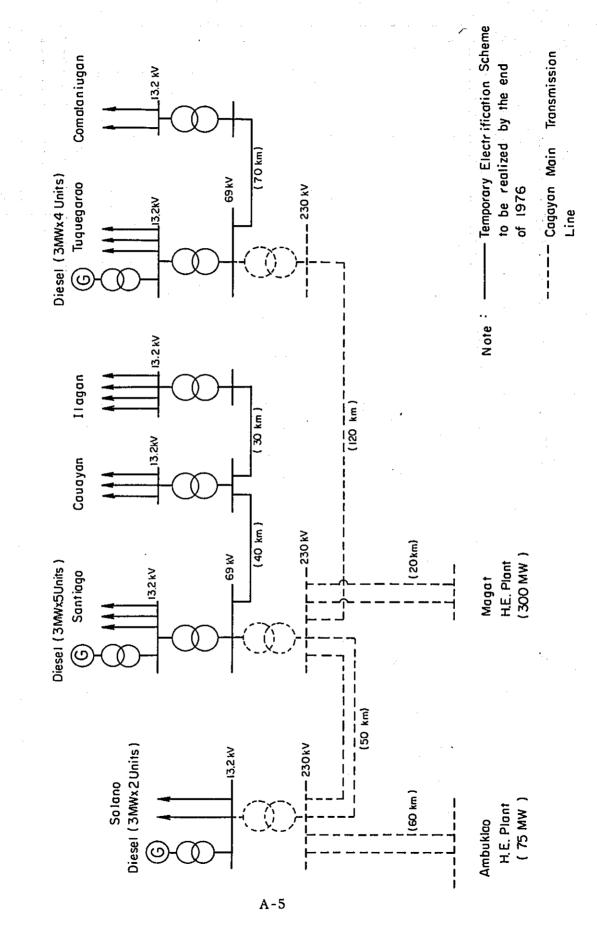
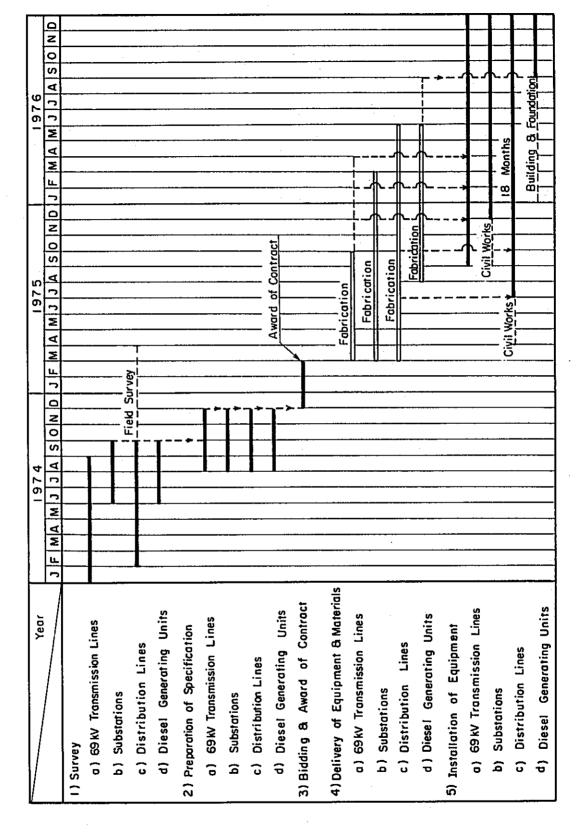


Fig. A-1-2 Temporary Electrification Scheme in Cagayan Valley



APPENDIX A-2

DEMAND FORECAST

A-2-1 Forecast on Power Demand by Sabstations

Table A-2-1 Forecast on Power Demand by Substations

			1978	1979	1980	1981	1982	1983	1984	1985	1986	1987
Ξ	Solano											
	Urban Rural	(MWh) (MWh)	3,386 0	3, 832 1, 272	4,338	4,911	5,559 3,180	6, 349 4, 109	6, 856 5, 038		7,997 6,896	8, 627
	Non-utility Irrigation Total	(MWh)	6, 528 3, 850 13, 764	6, 998 3, 916 16, 018	7,500 3,960 17,706	8, 035 4, 026 19, 516	8, 622 4, 092 21, 453	9, 237 4, 180 23, 875	9, 902 4, 224 26, 020	10, 621 4, 290 28, 283	11,384 4,356 30,633	12, 206 4, 400 33, 060
	Energy requirement at substation end (MWh) Load factor (%) Max. demand (MW)	ment at (MWh) (%) (MW)	15, 293 52 3.4	17, 797 52 3.9	19, 673 51 4.4	21, 684 51 4. 9	23, 836 50 5.4	26, 527 50 6.1	28, 911 49 6. 7	31, 425 49 7.3	34, 036 48 8.1	36, 733 48 8. 7
(2)	Santiago									•		
	Urban Rural Non-utility Irrigation Total	(MWh) (MWh) (MWh) (MWh)	4, 024 0 9, 123 5, 500 18, 647	4,788 1,929 9,779 5,588 22,084	5, 698 2, 894 10, 482 5, 720 24, 794	6, 781 3, 859 11, 230 5, 764 27, 634	8, 069 4, 824 12, 048 5, 874 30, 815	9, 593 6, 244 12, 909 5, 940 34, 686	10, 389 7, 664 13, 839 6, 050 37, 942	11, 251 9, 084 14, 861 6, 160 41, 356	12, 185 10, 504 15, 910 6, 248 44, 847	13,212 11,924 17,056 6,314 48,506
	Energy requirement at substation end (MWh) Load factor (%) Max. demand (MW)	(MWh) (%) (MW)	20,718 52 4.5	24, 537 51 5.5	27,548 50 6.3	30, 704 50 7.0	34,238 49 8.0	38,540 48 9.2	42, 157 48 10.0	45, 951 47 11.2	49, 830 47 12.1	53, 895 47 13.1
(3)	Cauayan											
	Urban Rural Non-utility Irrigation Total	(MWh) (MWh) (MWh) (MWh)	1,360 0 5,404 5,610 12,374	1, 672 742 5, 793 5, 676 13, 883	2, 057 1, 114 6, 209 5, 786 15, 166	2, 530 1, 486 6, 652 5, 852 16, 520	3, 112 1, 857 7, 137 5, 940 18, 046	3, 703 2, 431 7, 646 6, 050 19, 830	4, 039 3, 005 8, 197 6, 160 21, 401	4, 407 3, 579 8, 786 6, 248 23, 020	4, 808 4, 153 9, 424 6, 314 24, 699	5, 231 4, 727 10, 104 6, 380 26, 442

(continued)

<u>_</u> ;	380 49 6.8	22 44 8 48 8 8	40 50 9.6	32 32 08 01	78 49 12.3
1987	29,	7, 922 7, 144 12, 206 10, 384 37, 656	41,8	12, 195 11, 032 14, 308 9, 966 47, 501	52,7
1986	27, 443 49 6.	7,316 6,289 11,384 10,274 35,263	39, 181 50 8.9	11, 314 9, 728 13, 341 9, 878 44, 261	49, 178 49 11.5
1985	25, 577 50 5.8	6, 755 5, 437 10, 634 10, 120 32, 946	36, 606 50 8.4	10, 495 8, 427 12, 441 9, 812 41, 175	45,750 50 10.4
1984	23,778 50 5.4	6, 238 4, 585 9, 902 10, 010 30, 735	34,150 51 7.6	9, 736 7, 126 11, 612 9, 746 38, 220	42,466 50 9.7
1983	22, 033 51 4.9	5, 760 3, 733 9, 237 9, 856 28, 586	31, 762 51 7.1	9, 032 5, 825 10, 834 9, 658 35, 349	39,276 50 8.9
1982	20,051 51 4.5	5, 423 2, 881 8, 622 9, 724 26, 650	29, 611 52 6. 5	7,761 4,524 10,107 9,570 31,962	35,513 51 7.9
1981	18,355 52 4.0	4, 373 2, 304 8, 035 9, 592 24, 304	27,00 4 52 5.9	6, 713 3, 619 9, 420 9, 482 29, 234	32,482 51
1980	16, 851 52 3.7	3, 527 1, 728 7, 500 9, 504 22, 259	24, 732 53 5.3	5, 807 2, 714 8, 793 9, 438 26, 752	29, 724 52 6.5
1979	15, 425 53 3.3	2, 844 1, 152 6, 998 9, 328 20, 322	22,580 53 4.9	5, 023 1, 809 8, 204 9, 350 24, 386	27, 095 52 5, 9
1978	13,748 53 3.0	2, 294 0 6, 528 9, 240 18, 062	20, 068 53 4.3	4, 346 0 7, 653 9, 240 21, 239	23, 598
	ment at (MWh) (%) (MW)	(MWh) (MWh) (MWh) (MWh)	ment at (MWh) (%) (MW)	(MWh) (MWh) (MWh) (MWh)	ment at (MWh) (%) (MW)
	Energy requirement at substation end (MWh) Load factor (%) Max. demand (MW)	llagan Urban Rural Non-utility Irrigation Total	Energy requirement at substation end (MWh) Load factor (%) Max. demand (MW)	(5) Tuguegarao Urban Rural Non-utility Irrigation Total	Energy requirement at substation end (MWh) Load factor (%)
		(4)		(5)	

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			1978	1979	1980	1981	1982	1983	1984	1985	1986	1987
(9)	(6) Camalaniugan											
	Urban Rural	(MWh)	1, 183	3, 149	3,999	5,079	6,450	8, 105	8, 729	9,401	10, 125	10,914 9.876
•	Non-utility Irrigation	(MWh)	7,999	8, 574 3, 124	9, 190	9,846	10, 563	11, 318 3, 322	12, 134 3, 366	13,006	13, 950	14,955
	Total	·	12, 262	16, 477	18, 802	21, 397	24, 324	27, 981	30,624	33,393	36, 264	39, 375
	Energy requirement at substation end (MWh) Load factor (%) Max. demand (MW)	ment at (MWh) (%) (MW)	13, 624 50 ⁻ 3, 1	18,307 50 4.2	20, 891 50 4.8	23,774 49 5.5	27,026 48 6.4	31, 090 47 7. 6	34, 026 47 8.3	37, 103 46 9.2	40, 293 46 10.0	43,750 46 10.9
(2	(7) Cagayan Valley											
	Max. demand (MW Energy requirement (MW	(MW) ment (MWh)	23.5 107,049 1	27.7 125,741	31.0 34.5 38.7 43.8 47.7 52.3 56.9 61.4 139,419 154,003 170,275 189,228 205,488 222,412 239,961 258,376	34.5 154,003	38.7 170,275	43.8 189, 228	47.7	52.3 222, 412	56.9 239,961	61.4

Note: Annual energy requirement for irrigation has been tabulated on the assumption that the operation hours of pumps are to be 2,200 hours per year.

1-2-2 Area and Power Demand of Proposed Irrigation Pump Projects by Substations

Table A-2-2 Area and Power Demand of Proposed Irrigation Pump Projects by Substations

(As of 1978)

MM	Sav 16.6 MW	Sav						
16, 600	2,557	11,473(481)	2,570 ⁽¹³⁾	38,800	5,580	25, 490 (128)	7,730 ⁽³⁾	Tota1
1,400	256	1, 144 (48)	1	3,100	530	2,570 ⁽¹³⁾		Camalaniugan
4,200	380	1,770(90)	2,050(9)	11,000	973	4, 297 (28)	$\frac{3}{5}$, $7\overline{30}$ (2)	Tuguegarao
4,200	929	3,004(112)	520(4)	9,700	1,410	6, 290 ⁽²⁴⁾	$\frac{2}{2},0\overline{00}^{(1)}$	Ilagan
2,550	468	2,082(81)	ŧ	5,000	860	4, 140 ⁽¹⁷⁾	1, 6	Cauayan
2,500	454	2,046 ⁽⁷⁹⁾	•	5,400	982	4,418(22)	•	Santiago
1,750	323	1, 427 (71)	t	4, 600	825	3, 775 (24)	t	Solano
Total	Private I. P. $1/\sqrt{1}$	Communal I. P.	National I.P.	Total	Private I.P.1/	Irrigation Area in na. (Number of projects) National Communal Private I. P. I. P. I. P. I. P. I. P. I.	National I. P.	Substation

implies the project area and power demand of private irrigation projects which are estimated to be approximately 20% of those of communal irrigation projects. Note:

 $\frac{2}{}$ indicates Magsaysay Pump Irrigation Froject.

indicates Solana - Tuguegarao and Pared River Pump Irrigation Projects, 3/

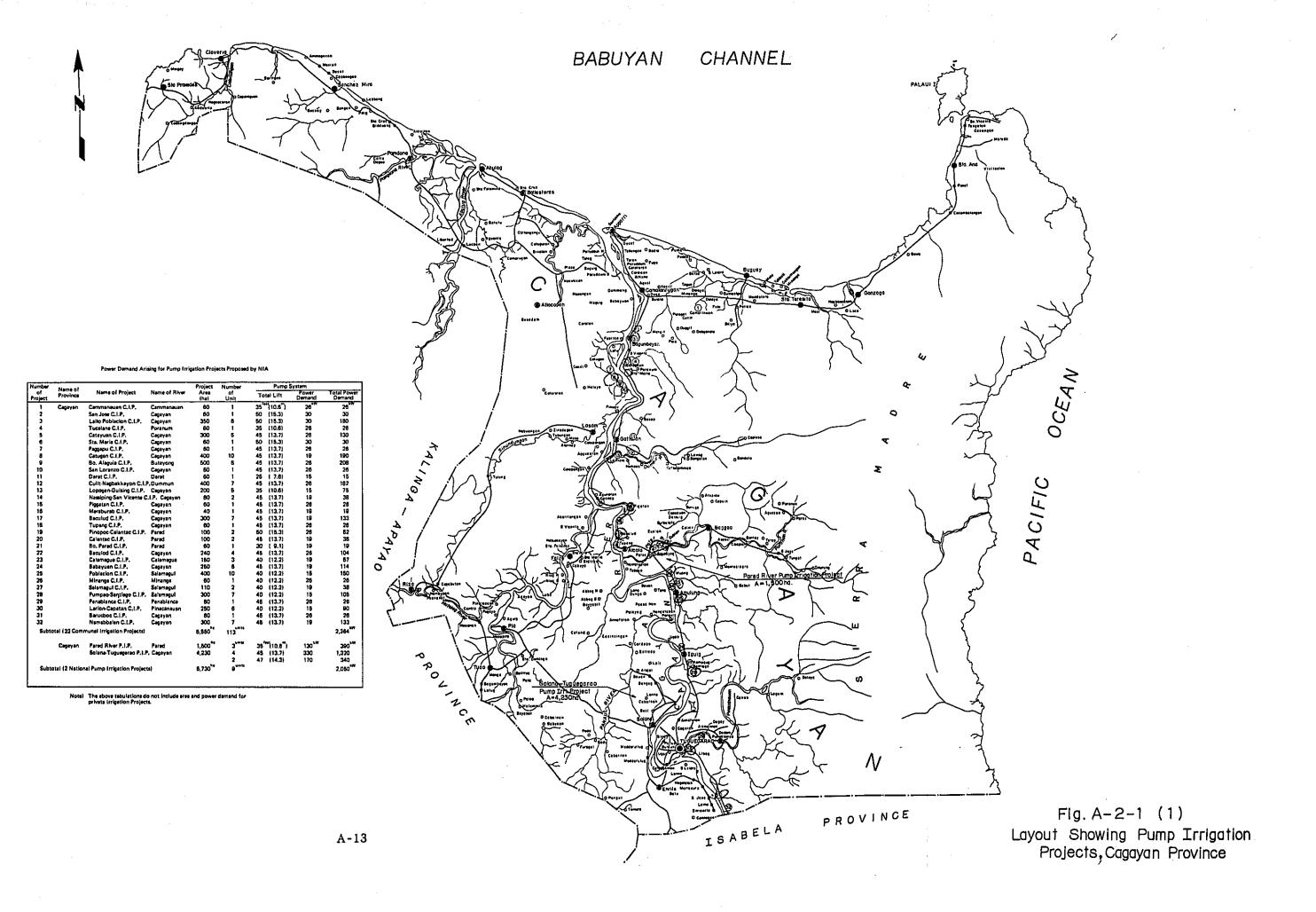
Say 17.5 MW 1,860 2,670 2,700 4,350 1,470 11, 473 (481) 3, 427 17, 470 4,420 Total Power Demand in kW (Number of units) Communal Private I.P. $\frac{1}{2}$ 968 326 618 530 433 624 3,004(112) 1, 144 (48) 2, 082 (81) 1,770(90) 2,046⁽⁷⁹⁾ 1, 427⁽⁷¹⁾ 2,570(13) 520(4) 2,050⁽⁹⁾ National Irrigation Area in ha. (Number of projects) 7,580 40,800 5, 700 5,400 3,300 4,900 1,273 11,300 1,910 10,200 Total Private I.P. 1/ 1,282 1,260 1, 125 730 25, 490 (128) 2,570⁽¹³⁾ 4, 140⁽¹⁷⁾ 6, 290⁽²⁴⁾ 4,297⁽²⁸⁾ 4, 418(22) 3,775⁽²⁴⁾ Communal 7,730⁽³⁾ 2,000(1) 5, 730⁽²⁾ National Camalaniugan Tuguegarao Substation Santiago Cauayan Solano Ilagan Total

Note: 1/implies the project area and power demand of private irrigation projects, which are estimated to be approximately 30% of those of communal irrigation projects.

(As of 1987)

	Irrigation	Irrigation Area in ha. (Number of projects)	Number o	f projects)	Power Den	Power Demand in kW (Number of units)	Number of	units)
Substation	National I.P.	Communal Private I.P. 1/	Private I.P. 1/	Tota1	National I. P.	Communal I. P.	Private I. P. $1/$	Total
Solano	1	3, 775(24)	1, 525	5,300	ı	1, 427 ⁽⁷¹⁾	573	2,000
Santiago	1	4,418(22)	1,782	6,200	•	2,046(79)	824	2,870
Cauayan	1	4,140(17)	1,660	5,800	•	2,082(81)	818	2,900
Ilagan	2,000(1)	6, 290 (24)	2,510	10,800	520 ⁽⁴⁾	3,004(112)	1, 196	4,720
Tuguegarao	5, 730 ⁽²⁾	4, 297(28)	1,773	11,800	2,050(9)	1,770(90)	710	4,530
Camalaniugan	ı	2,570 ⁽¹³⁾	1,030	3,600	1	1, 144 (48)	506	1,650
T otal	7,730 ⁽³⁾	25, 490 ^{(128),} 10, 280	10,280	43,500	2,570 ⁽¹³⁾	11,473(481)	4,627	18, 670
							Say 18	Say 18.7 MW
							- 1	

Note: $\underline{1}/$ implies the project area and power demand of private irrigation projects, which are estimated to be approximately 40% of those of communal irrigation projects.



Power Damand Arising for Pump Irrigation Projects Proposed by Na

umber	Name of			Project	Number	Pump S	ystem	
of roject	Province	Name of Project	Name of Filver	Area (ha)	of Unit	Total Lift	Power Demand	Total Pos Deman
1	Isabela	Sen Jose C.I.P.	Cagayan	180	3	40'" 12.2")	26 ^{1W}	78
2		Ugad C.I.P.	Pinacanauan	80	2	35 (10.7)	15	30
3		Angecesillan C.j.P.	Belluto	140	3	35 (10.7)	18	45
4		Pakulago C.I.P.	Pakulago	50	1	30 (9.1)	15	16
5		Baguecay C.J.P.	Baguebay Lake	200	4	30 (9.1)	15	60
6 7		Malasi Grande C.I.P. Cansan C.I.P.	M. Grande Cagayan	350 117	8 2	50 (15.2) 40 (12.2)	30	180
É		Batasig No. 1 C.J.P.	Balasia	100	2	40 (12.2) 50 (15.2)	26 26	52 52
ğ		Balasig No. 2 C.I.P.	Balasig	100	â	40 (12.2)	19	38
10		Lanna C.I.P.	Седауал	60	ī	40 (12.2)	26	26
11		Uged C.I.P.	Cagayan	60	i	40 (12.2)	20	26
12		Silio Bato C.I.P.	Pinacanauan	60	1	40 (12.2)	- 28	26
13		Arcon C.I.P.	Pinecanauan	500	8	40 (12.2)	26	208
14		San Antonio C.I.P.	Cagayan	1,200	21	60 (18.3)	30	630
15 18		Pete Lake C.I.P. Belog Pacey C.I.P.	Pata Lake Batog	100 100	2 2	50 (15.2) 40 (12.2)	26	52
17		Sto. Nino C.I.P.	Cagayan	115	2	40 (12.2) 50 (15.2)	19 26	36 52
18		Pilitan C.I.P.	Cagayan	200	i	40 (12.2)	19	78
10		Lepogen C.I.P.	Cegeyan	900	15	40 (12.2)	26	390
50		Sta. Isabela C.I.P.	Cegayan	350	7	70 (21.3)	30	210
21		Canapi C.I.P.	Cagayan	70	2	35 (10.7)	16	30
55		Sen Juan C.I.P.	Rugao	120	3	60 (18.3)	30	90
23		Rugeo C.I.P.	Rugao	50	1	60 (15.2)	26	26
24 25		Teba C.I.P. Atlangigan C.I.P.	Cagayan	120	2 2	40 (12,2)	26	52
28		Maislam C.I.P.	Hagart Hagari	120 60	1	40 (12.2) 50 (15.2)	26 30	82 30
27		Bos. of Gamu C.I.P.	Cagayan	460	i	40 (12.2)	26	208
28		Upl C.I.P.	Capayan	125	ž	80 (24.4)	30	90
29		Barrios of Gamu C.I.P.	Cegayen	1,000	18	48 (13.7)	28	416
30		Minanga C.I.P.	Caunayan	220	4	60 (18.3)	30	120
31		Pablicion C.I.P.	Cageyan	100	2	60 (18.3)	26	52
32 33		Sen Manuel C.I.P.	Anips	100	2	50 (15.2)	26	62
34		Anips C.I.P. Ba. Aningsn C.I.P.	Anipa Caunayan	100 60	2 7	50 (15.2) 50 (15.2)	26 19	52
35		Caunayan C.I.P.	Caunayan	400	÷	40 (12.2)	26	38 182
36		Palatteo C.I.P.	Caunayan	120	ź	40 (12.2)	26	62
37		Turod C.I.P.	Megat	350	7	70 (21.3)	30	210
38		Puzzer C.I.P.	Puzzer	200	4	70 (21.2)	26	104
39		Maceneo C.I.P.	Mecanao	300	8	40 (12.2)	19	114
40 41		Bo. #3 Lune C.I.P. Sitlo Tunggi C.I.P.	Macanao Macanao	180 200	3	40 (12.2)	26	78
42		Sta. Lucia C.I.P.	Cagayan	200	•	30 (9.1) 30 (9.1)	15 18	60 60
43		Sillawit C.I.P.	Nungnungan	150	3	50 (15.2)	26	75
44		San Antonio C.I.P.	Cagayan	200	ä	35 (10.7)	15	80
45		Sitio San Antonio C.I.P.	Alinom	60	1	40 (12.2)	26	26
46		Rizal C.I.P.	Makeokaoayen	400	8	80 (24.4)	30	240
47		Burgos C.I.P.	Paddad	300	6	80 (24.4)	30	180
48 49		Rizelune C.I.P.	Padded	400	8	80 (24.4)	30	240
49 50		Paddad C.I.P. Bo. Burges C.I.P.	Paddad Paddad	400 200	8 4	80 (24.4) 80 (24.4)	30 30	240
51		Bo. Victoria C.I.P.				14.7.,		120
52		Sta. Maria C.I.P.	Ganano Ganano	120 250	2	50 {15.2} 60 (15.2)	30	50
53		Gumbaoan C.I.P.	Ganano	290 500	à	60 (15.2) 60 (15.2)	30 30	120 240
54		Fuga C.I.P.	Ganano	200	ä	50 (15.2)	26	104
55		Buneg C.I.P.	Ganano	178	ž	50 (15.2)	30	90
56		Meligays C.I.P.	Cagayan	300	6	50 (15.2)	26	158
57 58		Ipil C.I.P.	Ganano	200	4	50 (15.2)	26	104
58		Sta. Monice C.I.P. Belwarte C.I.P.	Ganano Ganano	100 200	2	50 (15.2) 50 (15.2)	26	52
60		Nabbuan C.I.P.	Dumatata	200 60	1	50 (15.2) 50 (15.2)	26 30	104
61		Malini C.I.P.	Ganano	300	ė	50 (15.2)	30 26	30 158
62		Sinili C.I.P.	Ganago	300	ě	50 (15.2)	26	156
63		Patul Bayog C.I.P.	Ganano	500	8	60 (16.2)	30	240
64		Sen Andres C.I.P.	Diadi	60	ī	50 (15.2)	30	30
65		Ambalatungan C.I.P.	Diadi	350	6	50 (15.2)	30	180
66		Sagat C.I.P.	Sagat	100	2	BO (15.2)	26	52
Subtat	al (66 Comr	nunal Irrigation Projects)		15,465 ^{he}	285			7,510
	Isabala	Magsaysay P.I.P.	Cagayan	2,000	4	35 ^{*ee} (10.6 ^m)	130***	520

Note) The above tabulations do not include area and power demand in Private Impation Projects

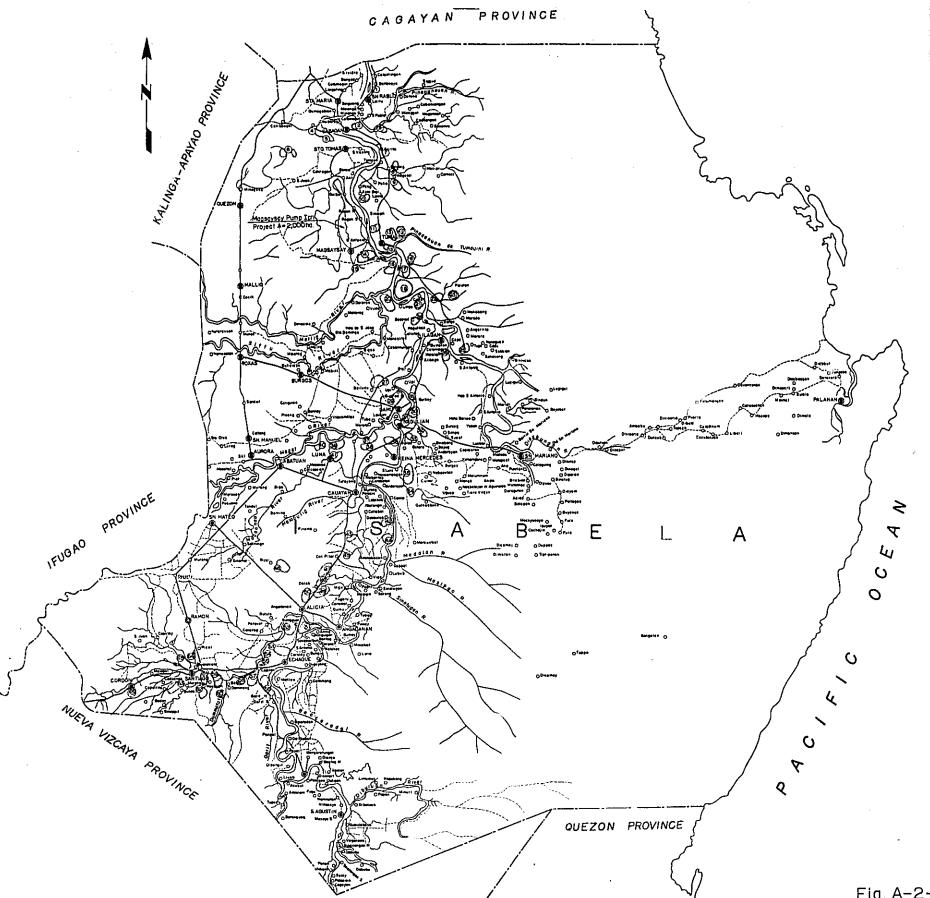
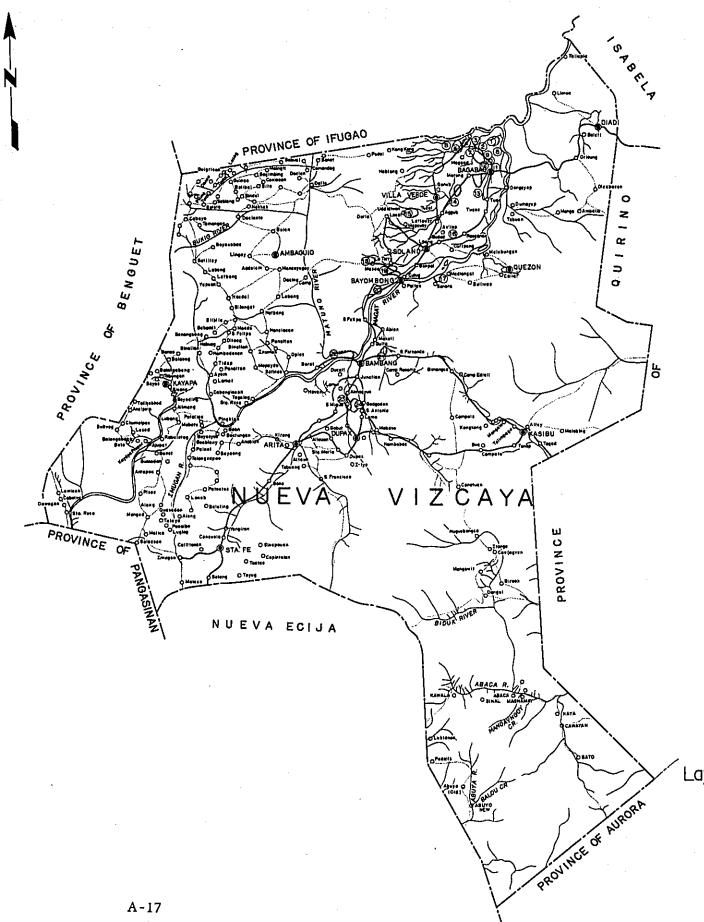


Fig. A-2-1 (2)
Layout Showing Pump Irrigation Projects
Isabela Province



Power Demand Arising for Pump Irrigation Projects Proposed by NIA

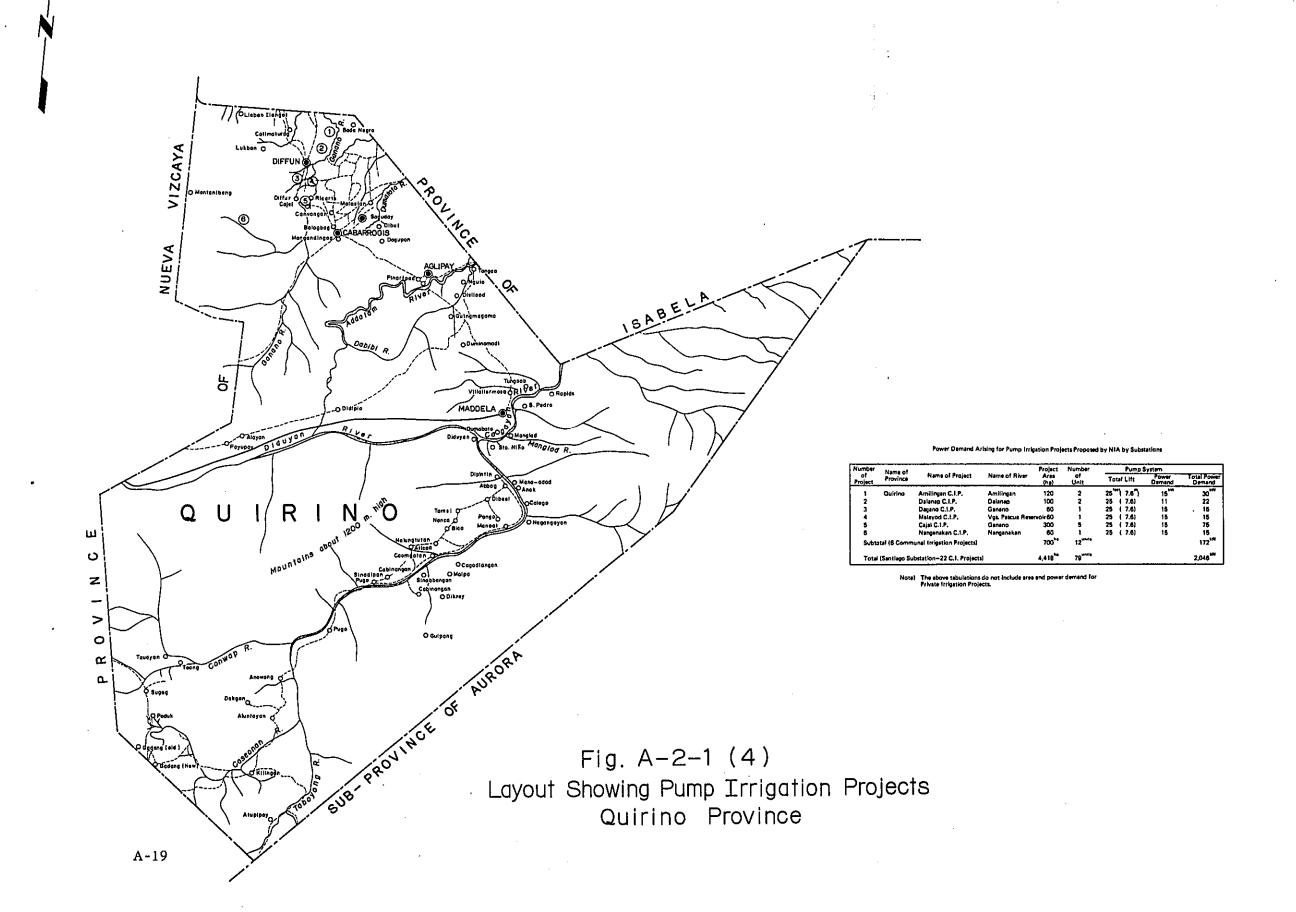
of umber	Nama of Province	Name of Project	Name of River	Project Area	Number of	Total Lift	Pump System Power Demend	Total Power
roject				(hs)	Unit			Demand
1	Nueve Vizceve	Sta. Lucis #1 C.I.P.	Ste. Lucia	100	2	35***(10.7*)	15 ^{1W}	30 ^{kW}
2	-	Sta. Lucie #2 C.I.P.	Zamore	75	2	40 (12.2)	15	30
3		Saranay-Malasin C.I.P.	Lanog	220	4	48 {13.7}	26	104
4		Bekir C.I.P.	Lanog	50	1	25 (7.8)	11	11
5		Paniki C.I.P.	Paniki	135	3	30 [9.1]	15	45
6		Mangelisen C.I.P.	Lamut	100	2	30 (9.1)	16	30
7		Calutiutan C.I.P.	Lanog	500	6	45 (13.7)	28	208
6		Sitio Tabanganay C.I.P.	Unaon	83	2	40 (12.2)	15	30
9		Villa Reina #1 C.t.P.	Villa Reina	70	2	30 (9.1)	11	22
10		Villa Reina #2 C.J.P.	Geuan Reservoir	75	2	35 (10.7)	15	30
11		Useon C.I.P.	Unson	60	1	35 (10.7)	26	26
12		Sitio Unaon C.I.P.	Uneon	130	3	40 (12.2)	15	45
13		Tuliag Lake C.I.P.	Tutleg Lake	400	7	35 (10.7)	19	133
14		Murana C.I.P.	Lanog	300	5	35 (10.7)	26	130
15		Uddiswan C.I.P.	Uddlawen	100	2	40 (12.2)	19	38
16		Besceren C.I.P.	Don Doro Lake	100	2	30 (9.1)	15	30
17		Medjangat C.I.P.	Magat	120	2	45 (13.7)	26	52
18		Masoc C.I.P.	Pappapa Spring	100	2	25 (7.6)	11	22
19		Page C.I.P.	Pagac	120	2	25 (7.6)	15	30
20		Ballwawang C.I.P.	Baliwawang	150	3	30 { 9.1}	15	45
21		Domang C.I.P.	Nambunakan	250	4	35 {10.7}	26	104
22		Batungao C.I.P.	Matuno	120	2	30 { 9.1}	19	38
23		Mabessar C.I.P.	Banay	120	2	30 (0.1)	19	38
24		Almaguer C.1.P.	Banay	300	8	60 (18.3)	26	156
Subt	otal (15 Com	munal Irrigation Projects)		3,775**	71****			1,427***

Note) The above tabulations do not include area and power demand for

Fig. A-2-1 (3)

Layout Showing Pump Irrigation Projects

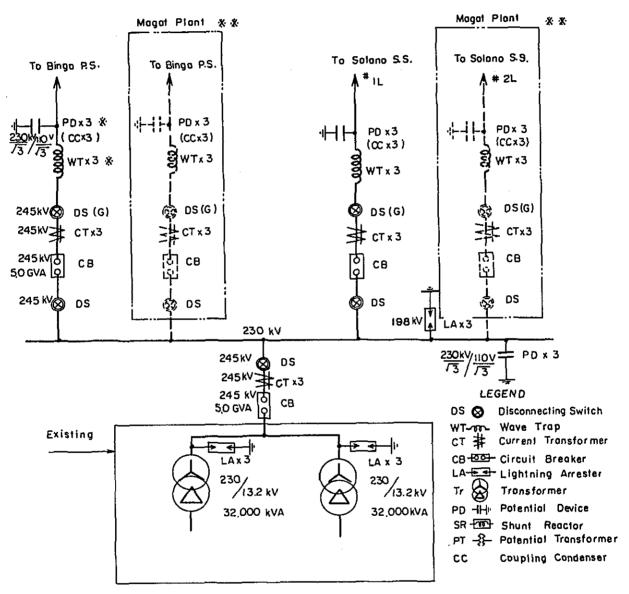
Nueva Vizcaya Province



APPENDIX A-3

CAGAYAN TRANSMISSION LINE AND SUBSTATION SCHEME

Fig.A-3-1 Skelton Diagram of Ambuklao Power Station.



Note

- 1. The Dott Line Indicating lines to be linked with Bingo and Solana Power Stations, respectively upon completion of Magat Power Station are not included in the proposed Project.
- 2. * Implies existing equipment which will be transferred to this power station
- 3, ** Implies upon completion of Magat Power Plant this line is to be connected with Binga Power Station and or Solono Substation

Fig.A-3-2 Skelton Diagram of Solano Substation

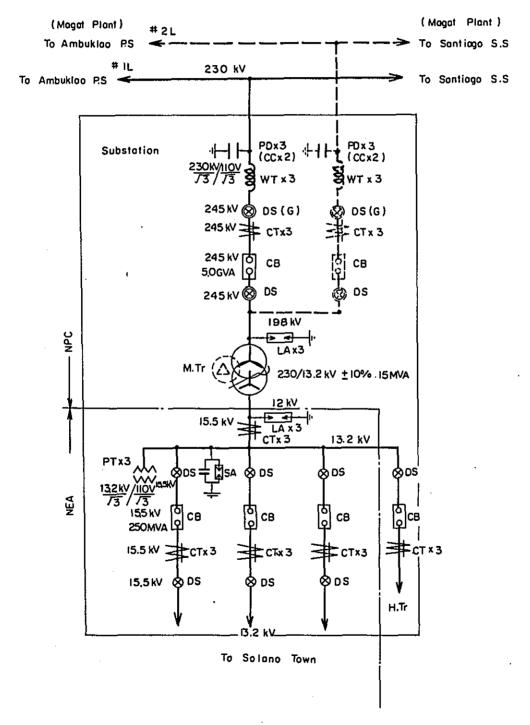
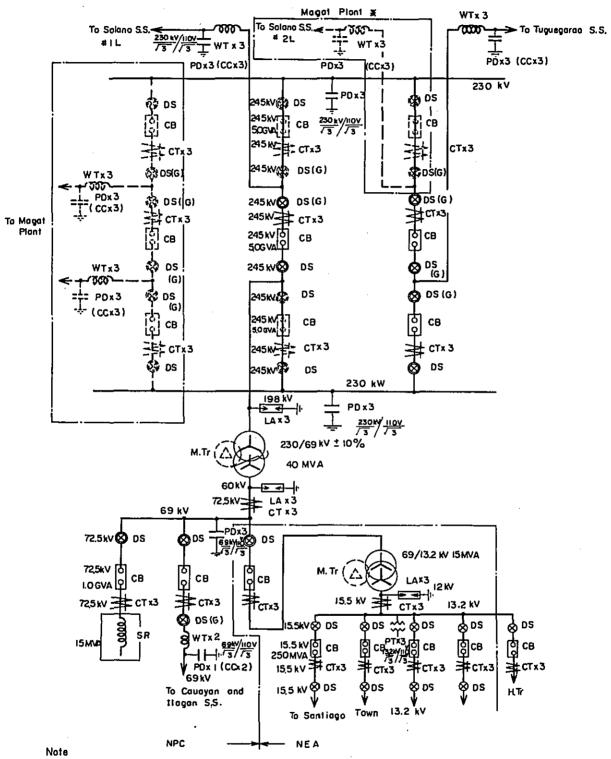


Fig.A-3-3 Skelton Diagram of Santiago Substation.



* Implies upon completion of Magat Power Plant this line is to be connected with Solano Substation.

Fig.A-3-4 Skelton Diagram of Tuguegarao Substation.

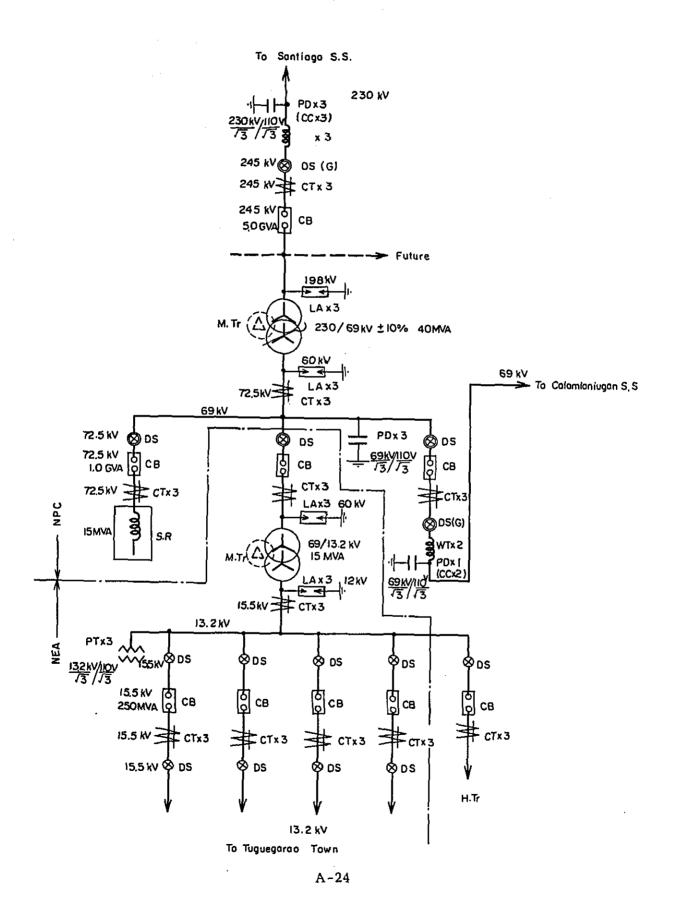


Fig.A-3-5 Skelton Diagram of Cauayan Substation.

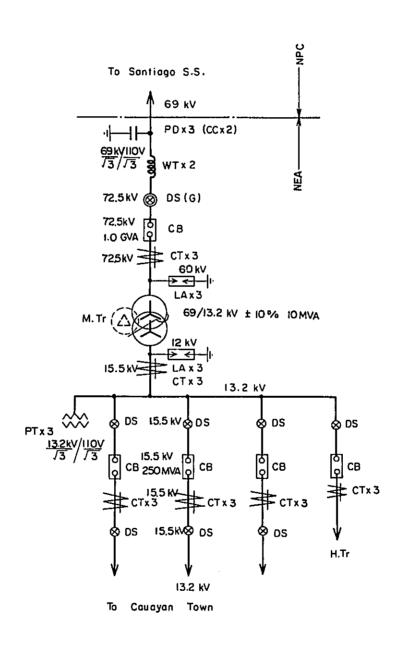


Fig.A-3-6 Skelton Diagram of Camalaniugan Substation or Ilagan Substation

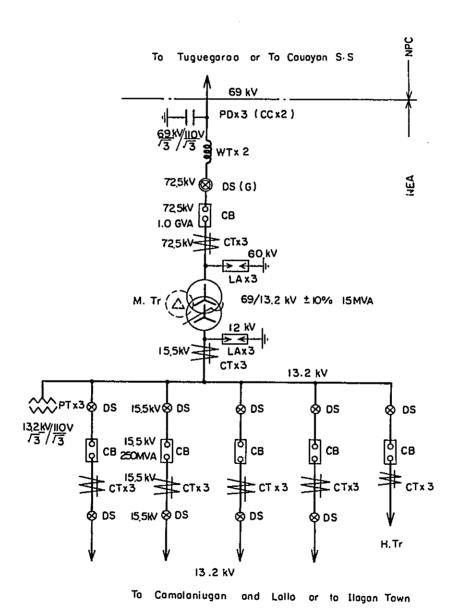


Fig.A-3-7 Layout of Ambuklao Switching Station

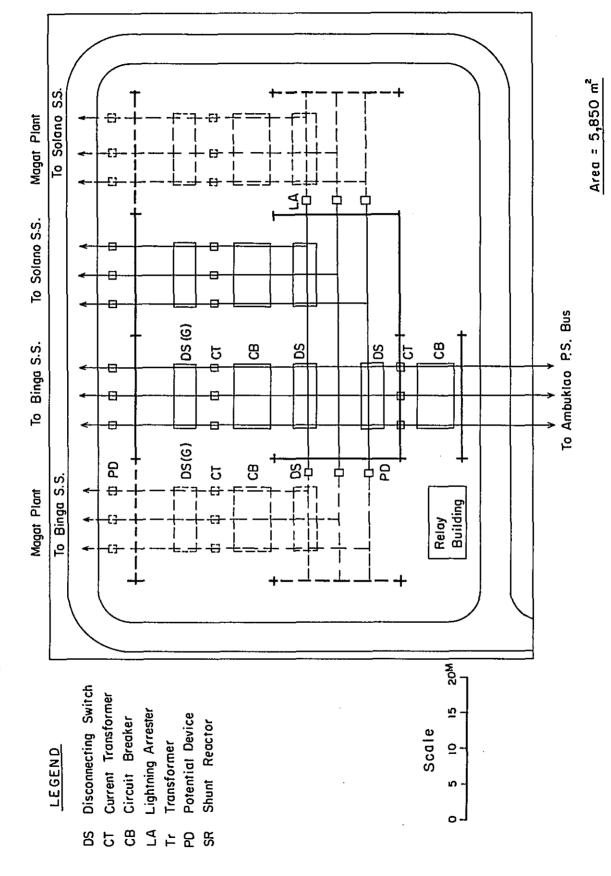
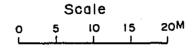
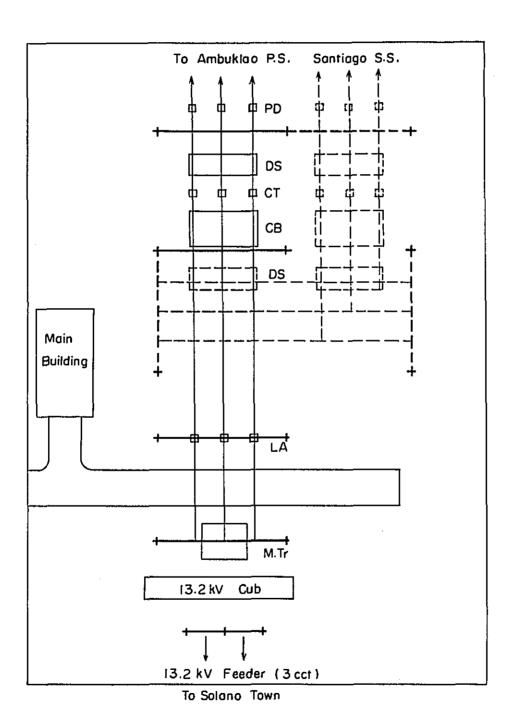


Fig.A-3-8 Layout of Solano Substation





A-28

Fig.A-3-9 Layout of Santiago Substation.

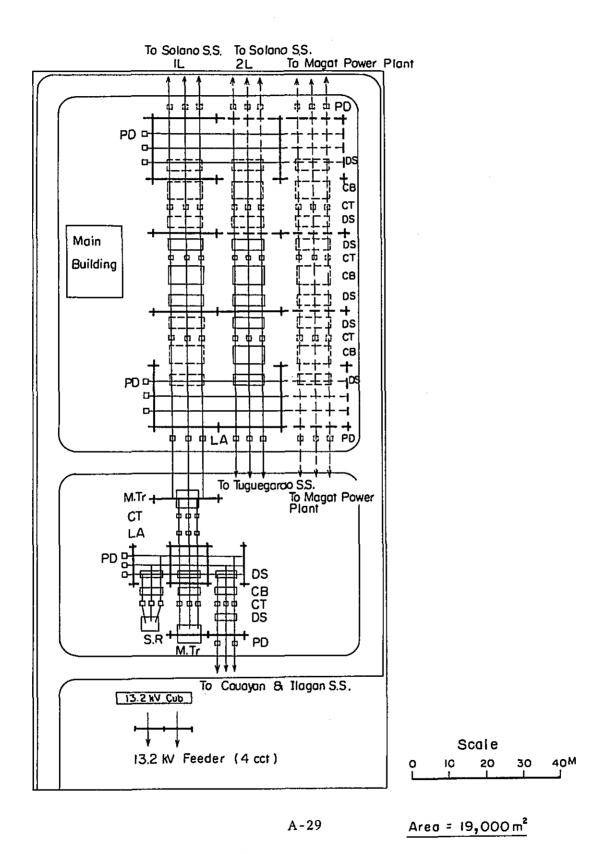


Fig.A-3-10 Layout of Tuguegarao Substation

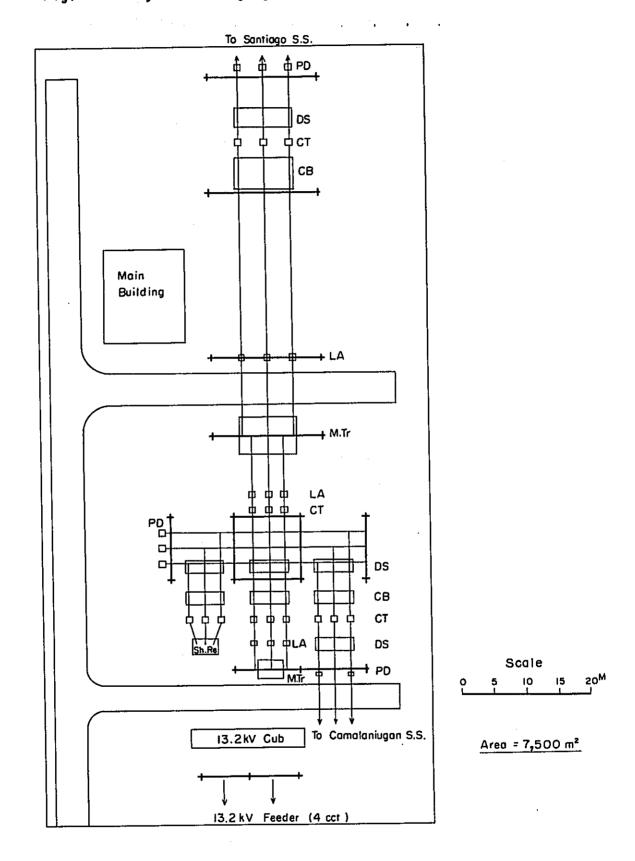
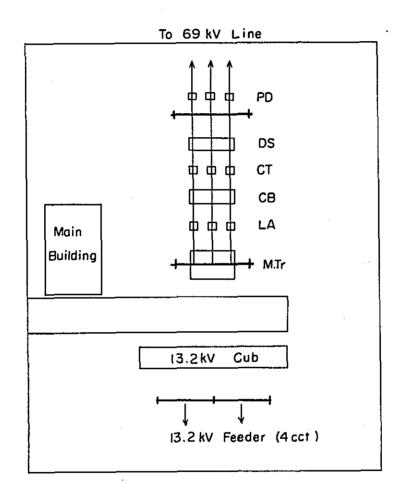


Fig.A-3-11 Layout of Ilagan, Cauayan and Camalaniugan Substation

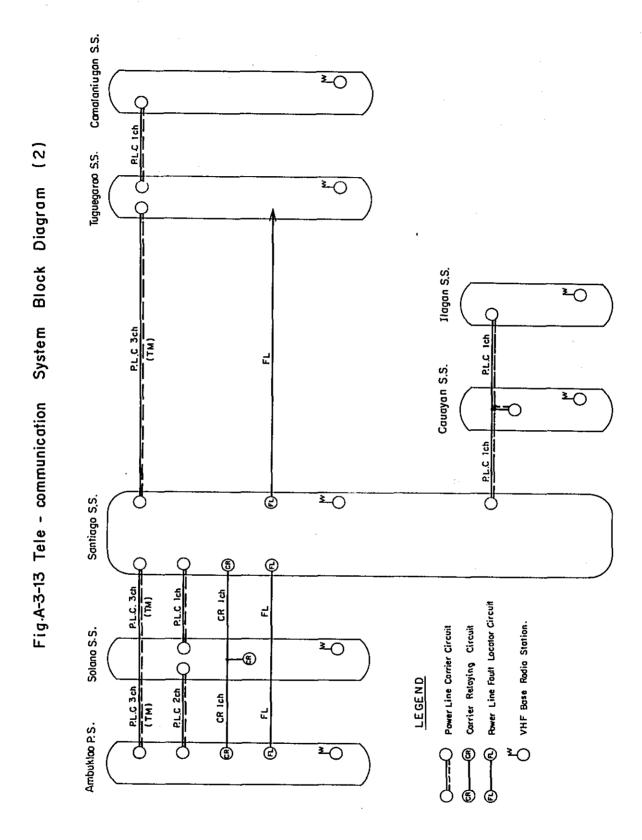


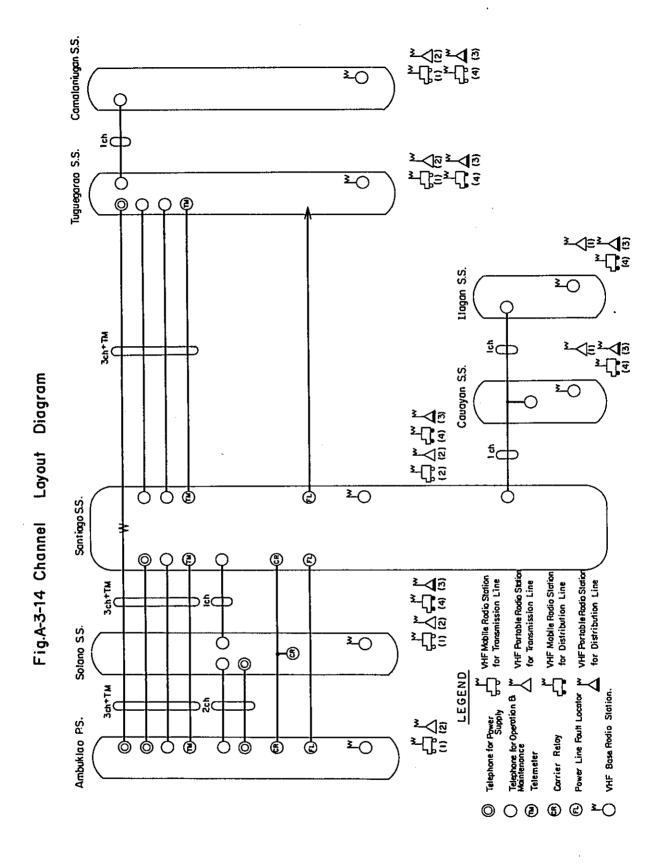
Scale 0 5 10 15 M

Area = 2,880 m²

Camalaniugan S.S. Hagan S.S. **⋈**-<u>श</u>-ख - 15 - 15 E \$ [] 4 Fig.A-3-12 Tele-communication System Block Diagram (1) -(];= <u>}-(];</u>= -(];= <u>}-(];</u> Tuguegarao S.S. Cauayan S.S. N TIME Ð **≟**_O Santiago S.S. VHF Pertable Radio Station for Distribution Line. VHF Mette Radio Statio for Distribution Line. <u>²</u>√3 ²√6 ²-(}3 ²-(}3 3<u></u> W VMF Base Radio Station Solano S.S. VHF Mobile Rodio W Sotion for Transmission Line, VMF Pertable Radio V Station for Transmission Line. 26 T ***-**[]; <u>³</u>-⊲ LEGEND Cyclic Digital Telemeter ≟Ū°≘ Power Line Foult tocote Power Line Carner <u>-</u>-O Coupling Filter Ambuklao P.S. Dividing Filter Telephone Set Corrier Relay ALE Wove Trap 9 ⋈ 🗓 € **5**] 5 Ü

A-32





APPENDIX A-4

ANALYSES OF ELECTRIC POWER SYSTEMS

Appendix

A-4 Analyses of Electric Power Systems

A-4-1 Outline

Northern Luzon Power System is presently interconnected with the Central Luzon Power System up to Ambuklao Power Station approximately 150 km north of Manila, and in 1978 it is planned for the Cagayan Valley to become interconnected with the Luzon System by the 230 kV transmission lines (See Fig. A-4-1).

The objectives of this system analysis are to study a possibility of interconnection of the trunk transmission lines with the Central Luzon Power System from a technical standpoint with respect to voltage regulation, transient stability, short-circuit capacity, etc. Moreover, in conducting this analysis, careful attention was paid to future power development plans in the Cagayan Valley and its vicinities.

A-4-2 Voltage Regulation

(1) Voltage Regulation Criteria

Voltage regulation concerns how balance of reactive power of the system is to be taken and is performed through generators, voltage regulating equipment and transformer taps. In calculation of the voltage regulations, the Mexico bus voltage has been assumed to be 102% (234.6 kV) according to the IECO Report.

a. The ranges of voltage regulation were taken to be 100±5% for 230 kV system voltages, 105 to 90% for 69 kV system voltages, 105% for peak times and 95% (100±5% at 13.2 kV) for off-peak times for 13.2 kV system considering voltage drop of distribution systems, and 100±3% for generator terminal voltages (provided that this is within the range of generator power factor). It is necessary that at the time of interconnection due consideration be given to the tap voltage of transformers of Ambuklao Power Station.

- b. Load power factors are to be 90% for peak times and 95% for off-peak times.
- c. Regarding transformer taps, all except for the 69/13.2 kV transformers of Santiago and Tuguegarao Substations are to be with OLTC in view of the fact that voltage fluctuations on the load sides during peak and off-peak times are large.
- d. The points of time for consideration are to be peak and off-peak time in 1978, 1982 and 1987 with system structure to be parts north of Mexico. The number of circuits, length of lines, capacity of transformers and their impedance are as shown in Impedance Map (See Fig. A-4-2).
- e. The number of generators in parallel is to be full output during peak time and I unit in parallel as a rule during offpeak time.

(2) On-Load Tap Changer

Regarding tap range of OLTC, from the results of analyses of voltage regulation (See Table A-4-1), if the maximum range is about 15%, it would be possible to maintain target voltages on the 13.2 kV side at 105% for peak times and 95% for off-peak times, and if allowances for "on-load tap changer" are to be made, it would be adequate if a range of 20% is to be provided.

It should be noted that if OLTC is to be provided at the primary side, over-excitation of more than 5% may occur, depending on the tap location, and if this is to be allowed, it would be necessary to strengthen insulation of transformers.

If the taps are to be provided at secondary sides, the problem of over-excitation would disappear, and based on the fact that voltage fluctuation would be greater on the secondary sides than the primary sides, it was considered that OLTC would all be installed at secondary sides.

(3) Shunt Reactor

Since line currents are small during off-peak times and there is much reactive power produced from the lines, system voltage will be raised up to 110%. Transformers (taps 242 kV - 236.5 kV - 231 kV - 225.5 kV - 220 kV) of the existing Ambuklao Power Station will become over-excited. Accordingly, there is a necessity to bring the voltage of the 230 kV system to 105% or lower, and in order to achieve this, a total shunt reactor capacity of 30 MVA is required for the system. Therefore, it was planned for reactors of 15 MVA capacity each to be installed at the 69 kV sides of Santiago and Tuguegarao Substations.

(4) Shunt Capacitor

Through tap adjustment of OLTC it will be possible to maintain system voltage at the target value even in 1987 and shunt capacitors will be, therefore, unnecessary.

(5) Power Flow Diagram

The power flow diagrams for peak times and off-peak times in 1978, 1982 and 1987 are shown in Fig. A-4-3 through Fig. A-4-8.

A-4-3 Transient Stability

Transient stability calculations were made of single-circuit, 3 LG, 0 - CO for the cases tabulated below for peak times in 1982 and 1987, and the results indicated stability as shown by the swing curves in Fig. A-4-9 through Fig. A-4-13.

Year	Fault Location	Type of Fault	Breaker Acting time	Judgment
1982	Magat - Santiago	1 cct 3LG 0-CO	0.1S-0.5S-0.6S	Stable
11	Santiago - Ambuklao	н	0.1S-0.5S-0.6S	Unstable
11	Santiago - Ambuklao	u ,	0.1S-0.7S-0.8S	Stable
1987	Magat - Santiago	11	0.1S-0.5S-0.6S	Stable
- 11	Sadanga - Beckel	п	0.1S-05S-0.6S	Stable

However, if the reclosing time should be about 0.5 sec (30 Hz), a fault between Santiago and Ambuklao (length: 110 km) would cause a shock at a point of large swing to result in instability, but if the said time is made loger to around 0.8 sec (48Hz), the line will be stable. Consequently, it is thought advisable to provide reclosing apparatus with which it would be possible to adjust the reclosing time between 0.4 sec and 1.0 sec in three-phase reclosure and to set it for the time being at around 0.8 sec.

A-4-4 Short-Circuit Capacity

The short-circuit power distribution at peak time in 1987 is shown in Fig. A-4-14. The short-circuit capacity of the various stations are as indicated in Table A-4-2, and it will suffice for breaking capacities to be 5,000 MVA on the 230 kV sides, 1,000 MVA on the 69 kV side and 250 MVA on the 13.2 kV sides.

It is noted here that the generator constant was taken to be xd'.

Table A-4-1 Appropriate OLTC Tap Voltage (Max. Min.)

7.7.0	C I	19	1978	19	1982	T	1987
Substations	128	Peak	Off-Peak	Peak	Off-Peak	Peak	Off-Peak
Salano	230/13.2 kV	104.0 (103.0)	91.0 (103.9).	106.0 (101.8)	90.5 (104.9)	106.0 (103.4)	91.0 (104.9)
Santiago	230/69 kV	101.5 (103.6)	94.0 (103.7)	105.0	94.0 (104.8)	107.0 (104.5)	93.5 (104.6)
u.	69/13.2 кV	103.0 (103.6)	103.0 (92.5)	102.0 (105.0)	102.0 (93.3)	103.5 (105.0)	103.5 (92.2)
Cauayan	66/13.2 kV	101.0 (101.2)	98.5 (92.2)	102.5 (100.1)	97.5 (92.5)	105.5 (98.1)	100.0 (90.9)
Ilagan	66/13.2 kV	102.0 (100.1)	98.5 (92.0)	102.5 (98.3)	97.5 (92.1)	108.5 (95.1)	100.5 (90.3)
Tuguegarao	230/69 kV	100.0 (104.3)	94.0 (103.1)	104.0 (103.4)	94.5 (104.1)	106.5 (103.4)	93.5 (103.9)
=	69/13.2 kV	103.0 (103.4)	103.0 (92.1)	102.0 (105.0)	102.0 (93.4)	103.5 (105.0)	103.5 (92.2)
Camalaniugan	66/13.2 kV	100.0	98.5 (92.0)	101.0 (101.2)	98.5 (92.7)	107.5 (96.7)	98.5 (91.5)
Claveria	66/13.2 kV	•	. 1	1	1	106.5 (95.5)	99.5 (91.8)
Note: 1. 2. 3.	Figures i All OLTC Voltages	parenthesis aps are to b aploy the pe	n parenthesis indicate primary side voltage in $\%$. Taps are to be installed at secondary sides. employ the percent values corresponding to 230 kV, 69 kV and 13.2 kV.	ary side vol secondary s orrespondir	tage in %. ides. ig to 230 kV, (69 kV and 1	3. 2 kV.
4	. Target volta	ages on 13.	Target voltages on 13.2 kV side are to be 105% during peak times and 95% during	to be 105% d	luring peak ti	mes and 95	% during

66 kV taps are to be used at receiving substations. For 69/13.2 kV transformers at Santiago and Tuguegarao, no-load tap changers have

off-peak times, respectively.

been employed.

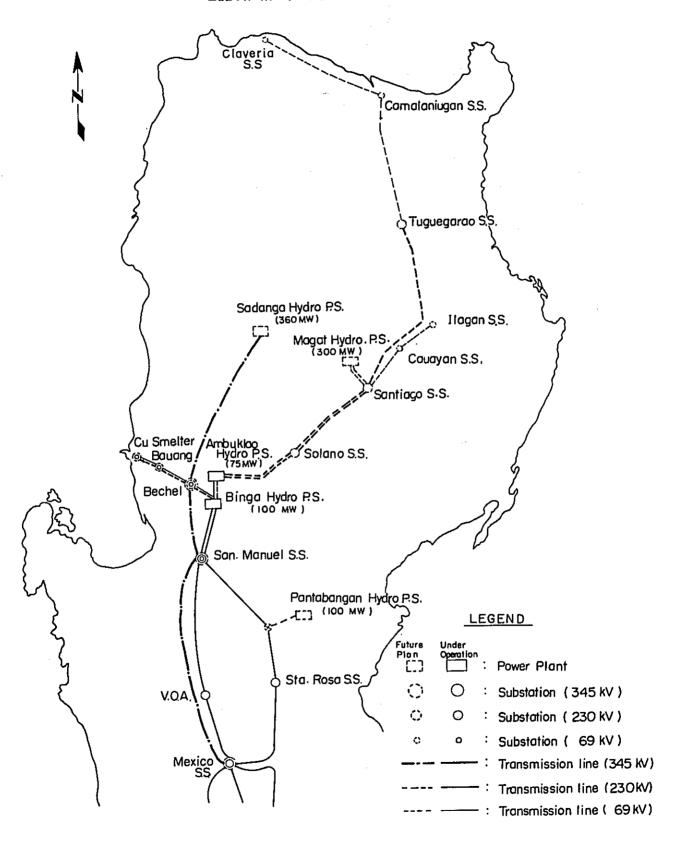
6.5

Table A-4-2 Short-Circuit Capacity

(Peak Time in 1987)

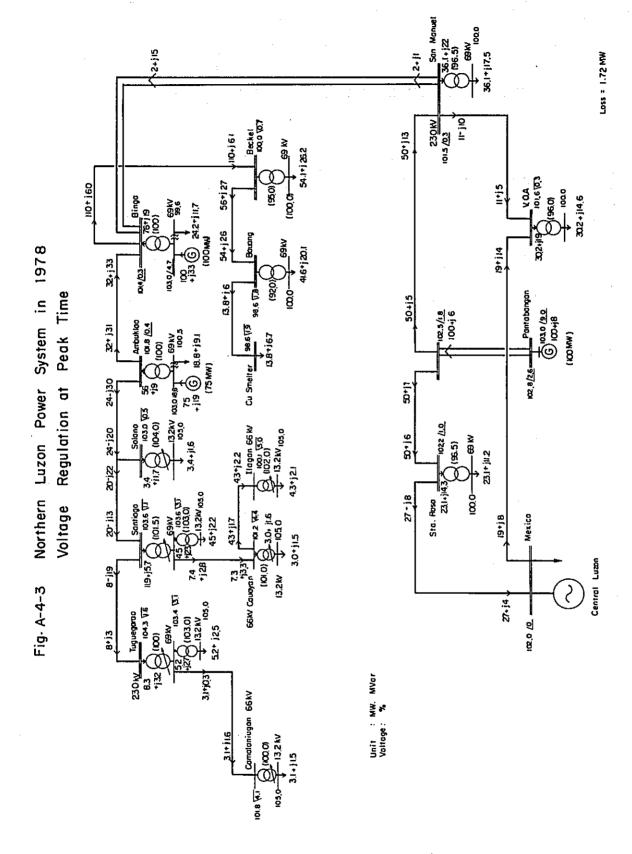
Stati	on .	Breaking Capacity (MVA)	Remarks
Ambuklao	230 kV 69 kV	2,828 246	xd' is used as generator constant.
п	13.2 kV	709	generator constant.
Solano	230 kV 13.2 kV	1,521 107	
Santiago "	230 kV 69 kV 13.2 kV	1,630 201 100	
Tuguegarao	230 kV 69 kV 13.2 kV	549 160 89	
Magat	230 kV Generator Terminal	1,591 1,581	
Cauayan	69 kV 13.2 kV	110 60	
Ilagan	69 kV 13.2 kV	81 51	
Camalaniugan ''	69 kV 13.2 kV	72 53	
Claveria	69.kV 13.2 kV	41 35	

Fig. A-4-1 Power System Diagram for Northern Luzon in 1987



2,=0295+|1,88(|6,5112) San Monuel 100 MVA 0. 21 25 MVA 10.4 Favors L Beckel Map, 100 MVA, 345 kV, 230 kV Base. Z, 1.54+j8 23 (j 7.16212) Northern Luzon Power System in 1987 Z,sQ.08+jQ48[Q42x2] Z,zQ.6+j3.86 (j3392x2) 40 km 150 MAR 150 121.7 V.84 269 | 2,10,09+10.55 ()195612) Zi= 0.997+| 5.82 (|4.75x2) 2,*02491|1455[]5.06(2) 15 MVA 117.4 Pantabangar 120 km [10004W] [110004W] [1114VA 1114VA 100 km Cu Smelter 22 km Zi = 1,65+j10,62 (39.33x2) 110 km Z. + 0.165+J1585[|50,84 x 2] Z1 = 0,2 + 1 19 (161.02 x 2) Zir 0.498 + | 2.91 (| 2.54 = 2) 1 m pedance E OS 2=12.11+329.57() 0263-23 Z1 + 0.52 + 13.09 (12.968x2) 60 MVA A SX Z,* 1.22* | 68 (| 5.98 x 2) Cougyon A 65km Sta. Resa Fig. A-4-2 Z, =1.8+j11.58 (jiQJ8x2) 15 km 120 km 2, r 0, 113 + j 0,725 [|254x2} 40 M/R 122.5 69 IV Central Luzon 5 300MA (360 MW) 55 1,=38,35+j93,6(j0.832=2) <u>2, = 28,26+j68,98(j0.6) +2)70lim</u> Comotoniugan (300uw) 333 uva 16 * jii.i 1394 175.0

A-42



-69tV 100.0\24 San Manue! 103.8\0.9 34.9 5117 Northern Luzon Power System in 1978 Regulation at Off Peak Time. 121,12 TOPESOI -. 11.0 12-30 Cu Smeller 0i - 7 5-115 Voltage 69KV 1000\22 5-120 1.4 -i -9 Fig. A-4-4 12-118 61,10 09+103 66W Cauayan 9.9 25- j6 22 192 25116 Unit : MW, MVar Voltage: % 69 - 10.3

(WUT OO!) 10400 Mexico 12-130 **= 07**0°201

Loss = 0,26 MW

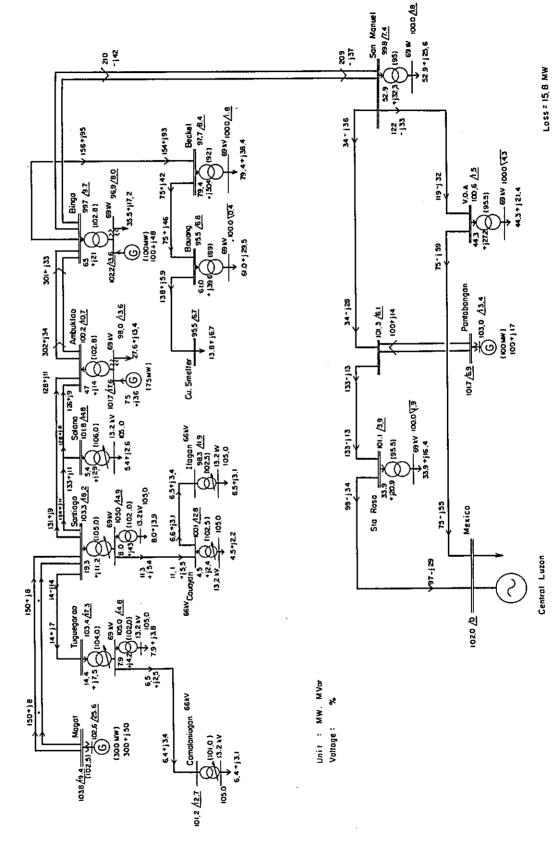
- 1000/20

Central Luzon

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Fig. A-4-5 Northern Luzon Power System in 1982

Voltage Regulation at Peak Time.



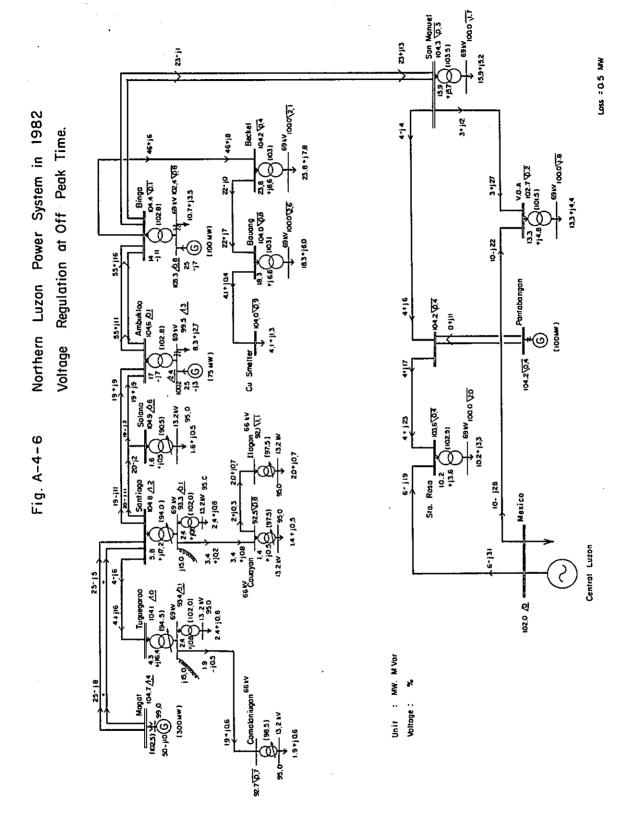
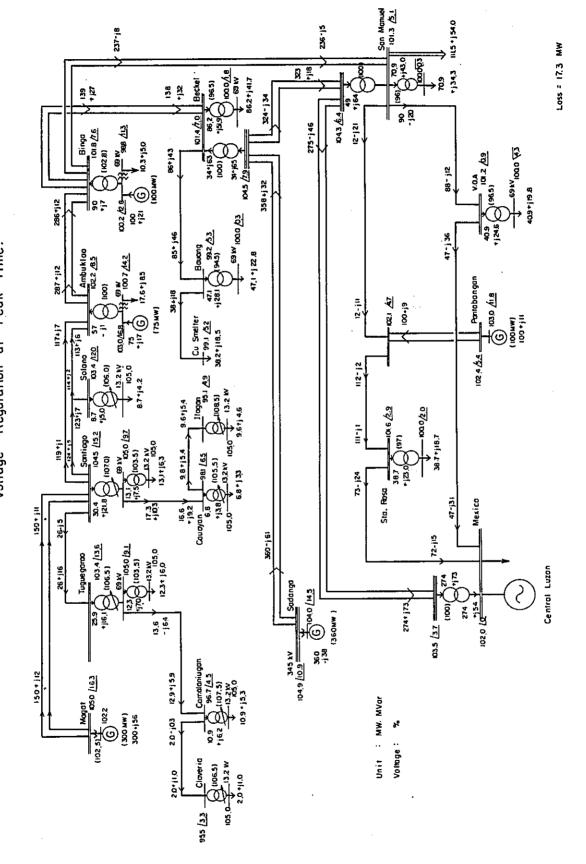
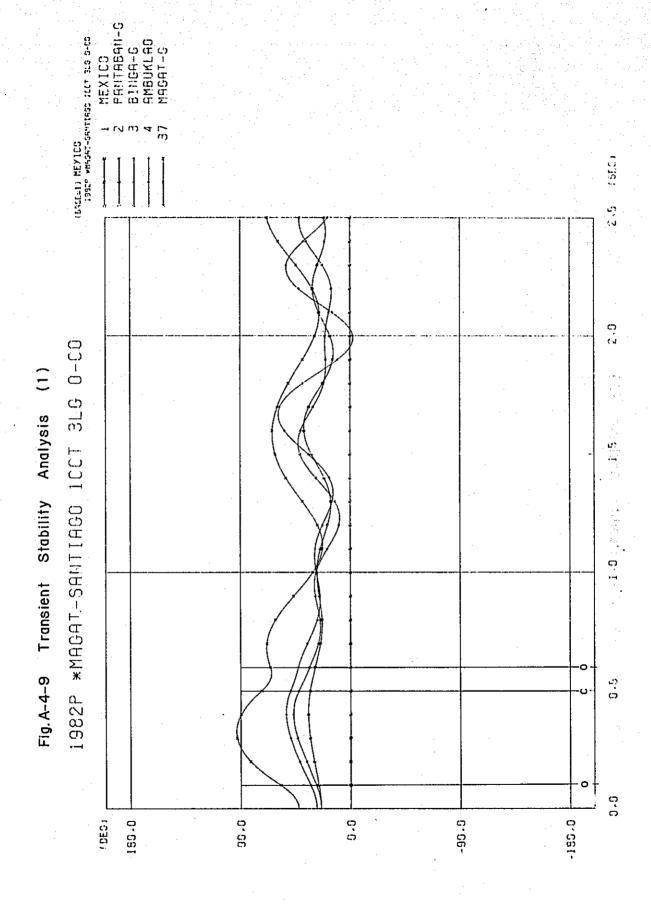


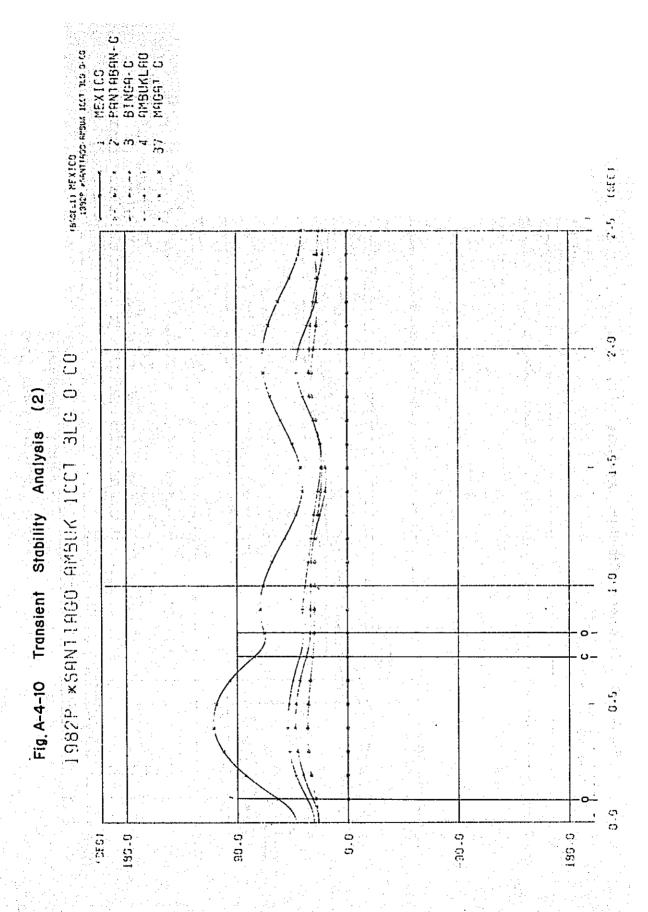
Fig. A-4—7 Northern Luzon Power System in 1987 Voltage Regulation at Peak Time.

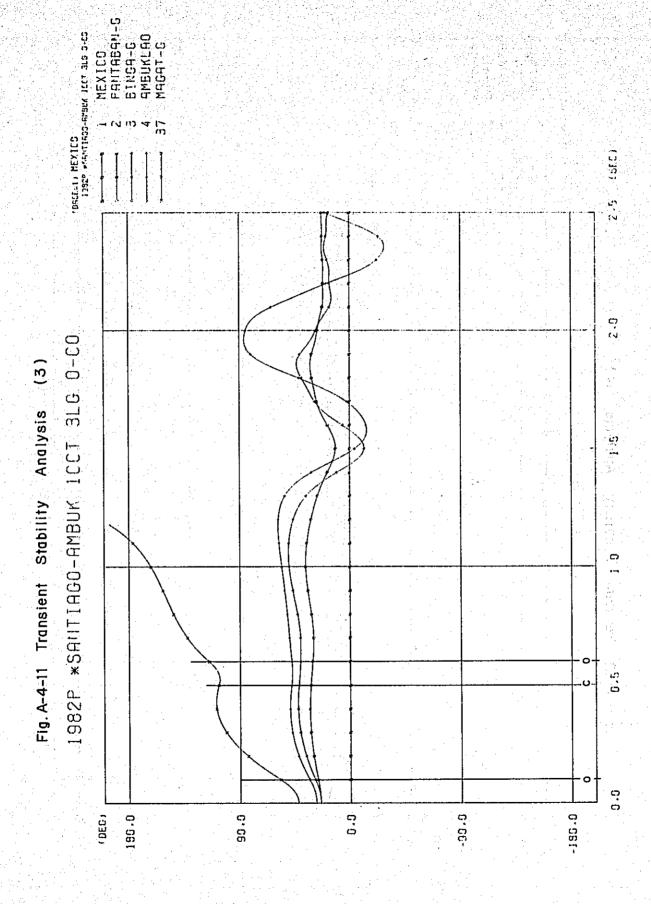


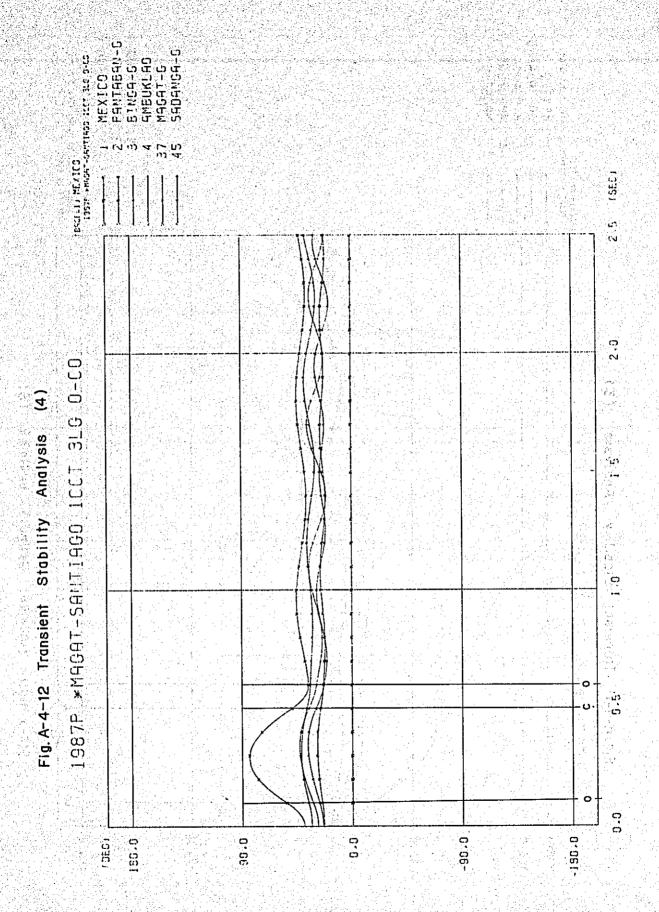
21-144 Northern Luzon Power System in 1987 Voltage Regulation at Off Peak Time. 0+156 50+110 11.5+j29 B.O. U.O. 161,8 3-;18 3-12 Fig. A-4-8 61-51 20-129 25-15 Sadanga 105,4 (2.7 22 - 189 104.1 \Q3 🚞 1020

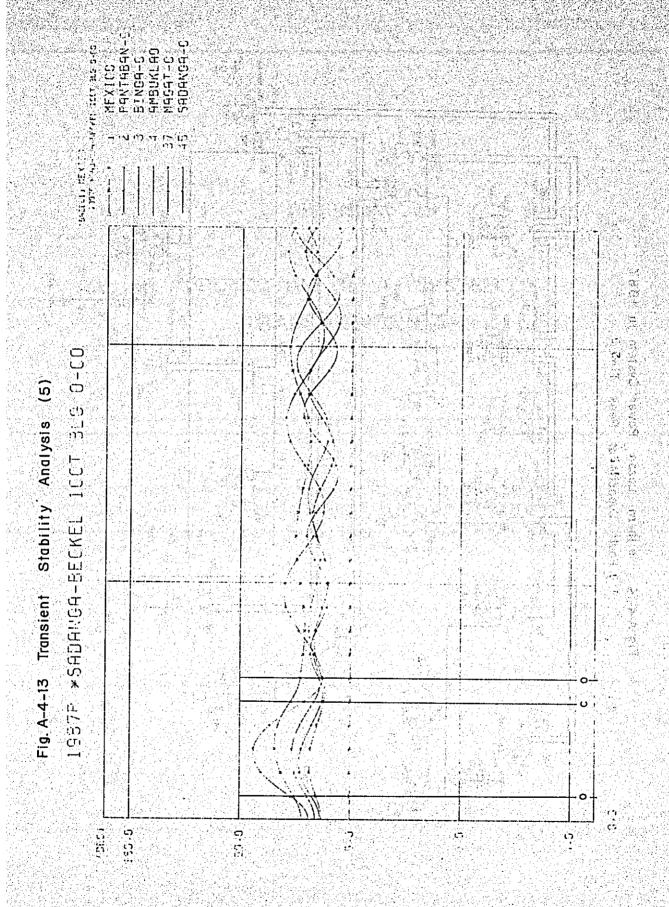
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Fig. A-4-14 Northern Luzon Power System in 1987 Fault Capacity at Peak Time.

APPENDIX A-5

PROTECTIVE RELAY SYSTEM OF TRANSMISSION LINES

Appendix

A-5 Protective Relay System of Transmission Lines

A-5-1 Basic Principle of Preliminary Design

The protective relay system of the transmission lines including the reclosing system has been designed in consideration of the conditions and forms of transmission systems, such as conditions of system interconnection, neutral grounding systems, etc. as well as frequency of lightning tripouts and future plans in the Valley.

(1) Santiago to Solano to Ambuklao (230 kV, 1cct)

Initially, this will be a single-circuit transmission line with a power source only at the Ambuklao end, but in the future (1982) with putting into service equipment of Magat Power Station at Santiago, it will become a double-circuit transmission line. Consequently, this will be an important interconnecting transmission line, and regarding the protective relaying system and reclosing system, design work has been carried out in anticipation of stringing another circuit in the future.

(2) Santiago to Tuguegarao (230 kV, 1 cct)

Until interconnection of the Chico Hydro Power Complex with Tuguegarao Substation, the Santiago end will be a power source and Tuguegarao will be a receiving substation. Therefore, in the way of a protective relaying system, there is to be a distance relaying system at the Santiago end and a combination of an overcurrent relaying system and an undervoltage relaying system at the Tuguegarao end. Further, at the Santiago end, a low-speed reclosing system is to be provided in order to facilitate quick fault clearance. After realization of interconnection of the Chico Hydro Power Complex with Tuguegarao, the line will become an interconnecting transmission line and the protective relaying system is to be replaced by a power line carrier relaying system.

(3) Ilagan to Cauayan to Santiago (69 kV, 1 cct)

The Santiago end will be the power source with Ilagan and Cauayan being receiving substations. Therefore, the protective relaying system is to consist of a distance relaying system at the Santiago end. At each receiving end, combination of an overcurrent relaying system and an undervoltage relaying system should be equipped. Further, in order to facilitate quick fault clearance, a low-speed reclosing system is to be provided at Santiago.

(4) Camalaniugan to Tuguegarao (69 kV, 1 cct)

The Tuguegarao end will be the power source with Camalaniugan being the receiving substation. Therefore, the protective
relaying system is to consist of a distance relaying system at the
Tuguegarao end. As for the Camalaniugan end, a combination of
an overcurrent relaying system and an undervoltage relaying
system is to be equipped. Further, in order to facilitate quick
fault clearance, a low-speed reclosing system is to be provided
at Tuguegarao.

A-5-2 Outline of Preliminary Design

(1) Santiago to Solano to Ambuklao (230 kV, 1 cct) Santiago and Ambuklao

Protective Relaying System

Main Protection:

, , ,

Distance directional comparison systems combined with power line

carrier relaying system

Back-up Protection: Distance relaying system

Reclosing System

Three-phase low-speed reclosing (only Ambuklao)

Single-phase and three-phase high-speed reclosing

Solano

Protective Relaying System

Main Protection: Distance directional comparison

system combined with line carrier relaying system

Back-up Protection: Overcurrent and undervoltage relaying systems

(2) Santiago to Tuguegarao (230 kV, 1 cct)
Santiago

Protective Relaying System

Distance relaying system

Reclosing System

Three-phase low-speed reclosing

Tuguegarao

Protective Relaying System

Overcurrent and undervoltage relaying systems

(3) Santiago to Cauayan to Ilagan (69 kV, 1 cct)
Santiago

Protective Relaying System

Distance relaying system

Reclosing System

Three-phase low-speed reclosing

Cauayan and Ilagan

Protective Relaying System

Overcurrent and undervoltage relaying systems

(4) Camalaniugan to Tuguegarao (69 kV, 1 cct)

Tuguegarao

Protective Relaying System

Distance relaying system

Reclosing System

Three-phase low-speed reclosing

Camalaniugan

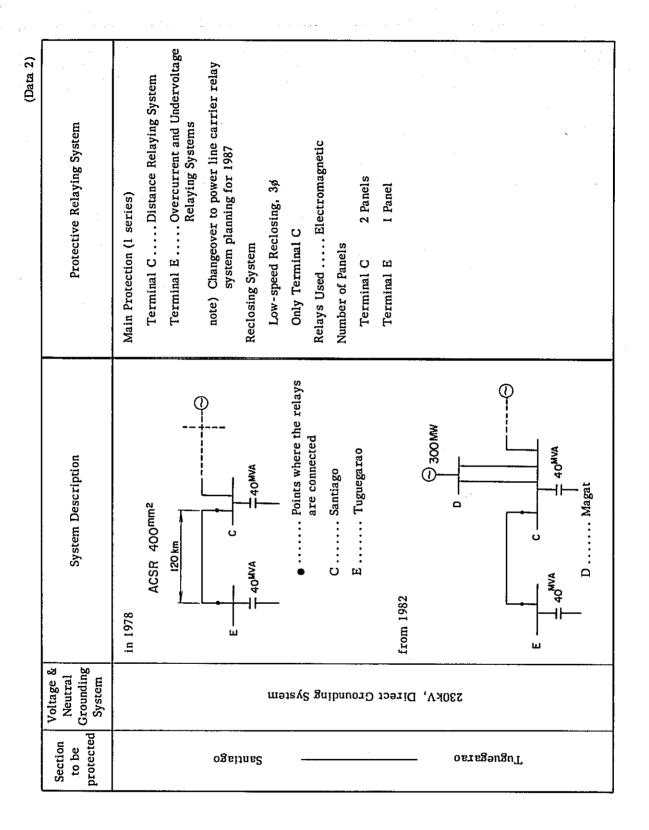
Protective Relaying System

Overcurrent and undervoltage relaying Systems

A-5-3 Outline of Facilities

See Data 1 - 3.

(Data 1)	Protective Relaying System	Main Protection (1 series)	System	Terminal AOnly power source	Terminal BOnly load	Terminal C Variable both for power source and load	Backup Protection (1 series)	Distance relaying System (Terminals A, C)	Overcurrent and Undervoltage relaying System (Terminal B)	Reclosing System	High-speed reclosing, 16, 36	Applicable to terminals A, C	3¢ to be used from 1982	Low-speed reclosing, 3¢	Only Terminal A	Relays Used Electromagnetic	Number of Panels	Terminal A, C 3 panels	Terminal B I panel
	Signal Transmission System		шәз	r Sys	. Lie	rad enid	19/	woq	u	ster	ág S	guibi	Sen	rier	TEO	ше	iT y	ren	ib¤O
	System Description	in 1978	Sokm 60km	Load		C B A A A A A A A A A A A A A A A A A A		Hydro Points where the relays	are connected A Ambuklao				from 1982			B A————————————————————————————————————		Load Load Θ_{75} MV	© 300МW D Magat
Voltage &	Neutral Grounding System					ше	yste	2 gaibr	Groun	rect	' בוי)KA'	23(
	Section to be protected			01	ıkla	udmA —			onsic	s -				· 03	sita	s2			



(Caraci)	Protective Relaying System	Main Protection Terminal D Distance Relaying System Terminal F Overcurrent and Undervoltage Relaying System Reclosing System Reclosing System Low-speed Reclosing, 3¢ Only Terminal D Relays Used Electromagnetic Number of Panels Terminal D Terminal D Relays Used Electromagnetic	Main Protection Terminal E Distance Relaying System Terminal H Overcurrent and Undervoltage Reclosing Systems Low-speed Reclosing, 3¢ Only Terminal E Relays Used Electromagetic Number of Panels Terminal E Terminal H I Panels
	System Description	until 1987 — Points where the 230kV — relays are connected 40kV — D Santiago F Cauayan 13.2kV — 40km G Ilagan F — G — Load Load	until 1982 230 ^{kV} E Location protected by relay E Tuguegarao 40 ^{kVA} E Camalaniugan 13.2kV H Camalaniugan H Camalaniugan
	Voltage & Neutral Grounding System	Direct Grounding System	Direct Grounding System
	Section to be protected	Ilagan —— Cauayan ——Santiago	Camalaniugan ——— Tuguegarao

APPENDIX A-6

DISTRIBUTION LINE SCHEME

Fig.A-6-1 Distribution System- 7.62/13.2 kV, 3 Phase, 4 Wire, Common Neutral Multiple Grounding System.

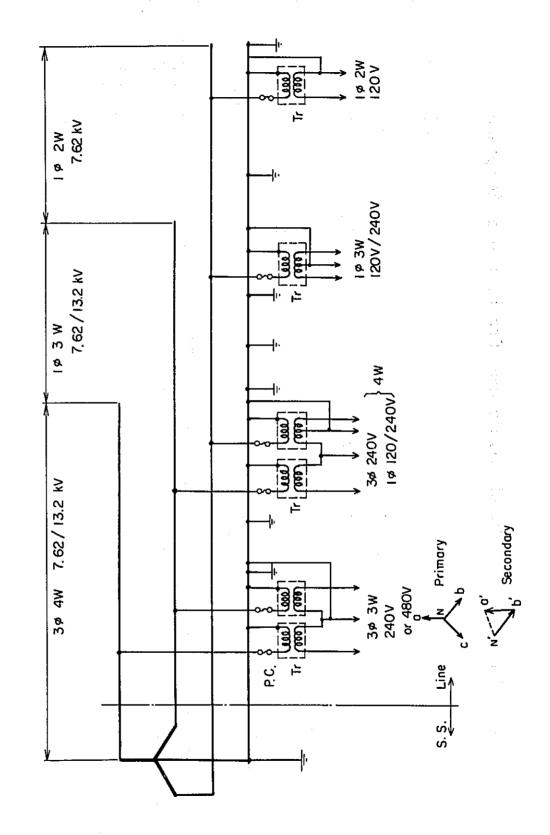


Fig.A-6-2 Layout of Model Distribution Facilities and Equipment.

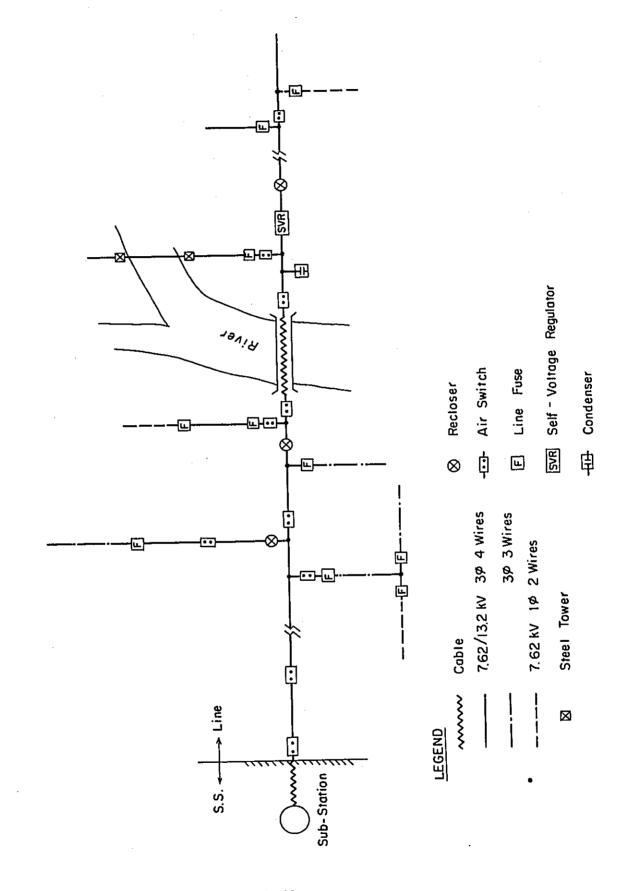
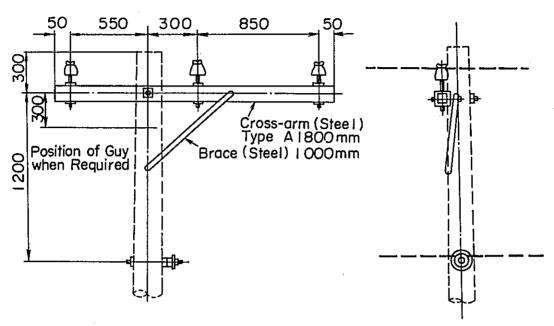


Fig.A-6-3 Details of Pole Dimension Diagram. (7.62/13.2 kV, 3-phase)



O° to 5° Angle, Single Primary Support

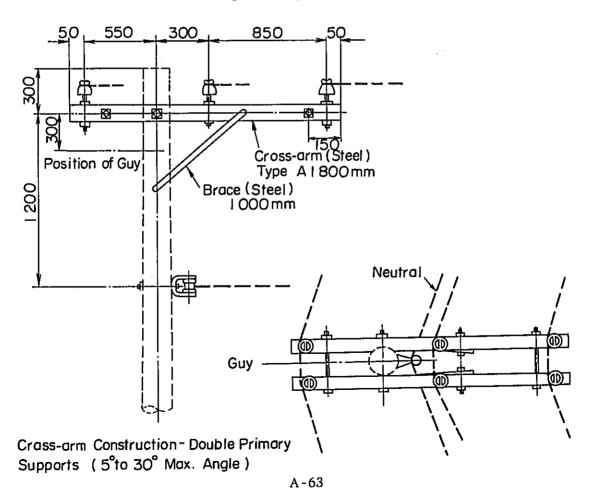
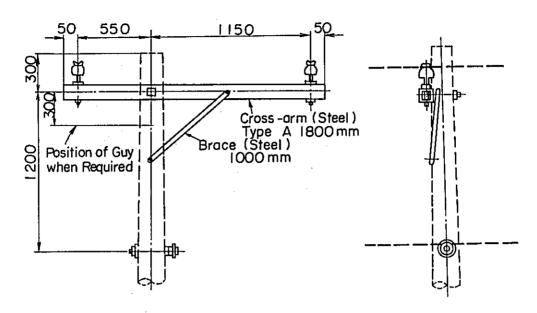
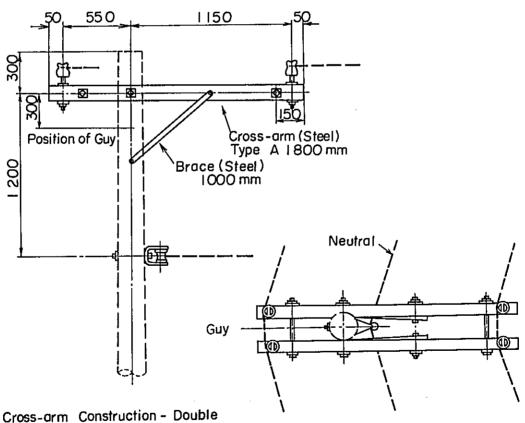


Fig.A-6-4 Details of Pole Dimension Diagran.

(7.62 / 13.2 kV, 3- phase.)



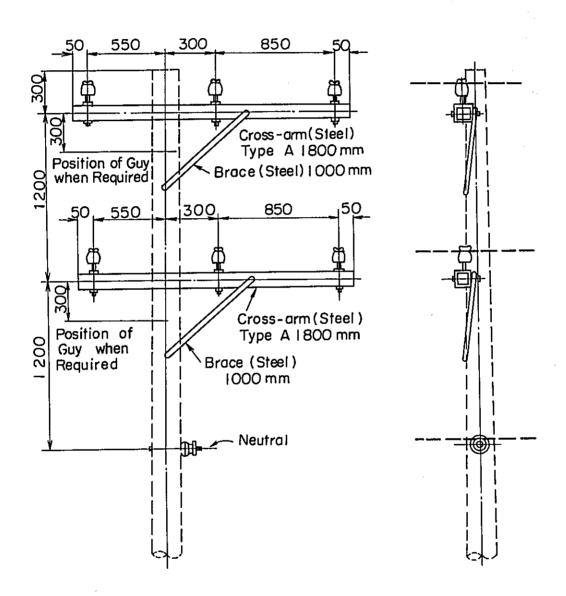
O° to 5° Angle, Single Primary Support



Cross-arm Construction - Double Primary Supports

(5°to 30° Max. Angle)

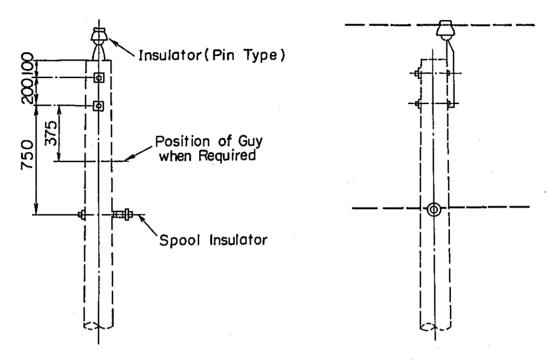
Fig.A-6-5 Details of Pole Dimension Diagram . (7.62 / 13.2 kV, 3 - phase)



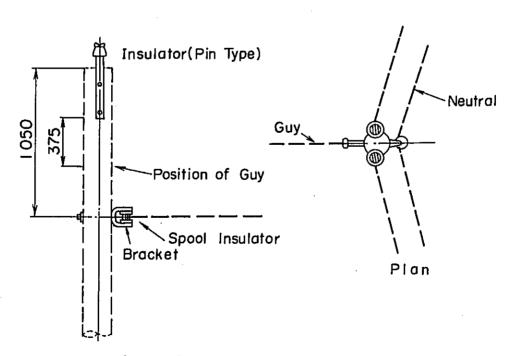
Cross-arm Construction - Double Circuit Single Primary Support at O°to 5°Angle.

Fig.A-6-6 Details of Pole Dimension Diagram.

(7.62/13.2 kV, Single phase.)



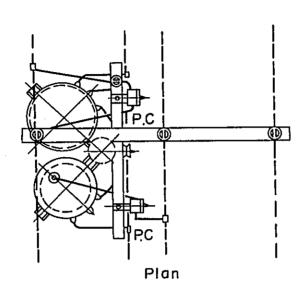
O° to 5° Angle , Single Primary Support



5° to 30° Maximum Angle, Double Primary Supports

Fig.A-6-7 Details of Pole Dimension Diagram.

(7.62 / 13.2 kV, Two Transformers on 3-phase.)



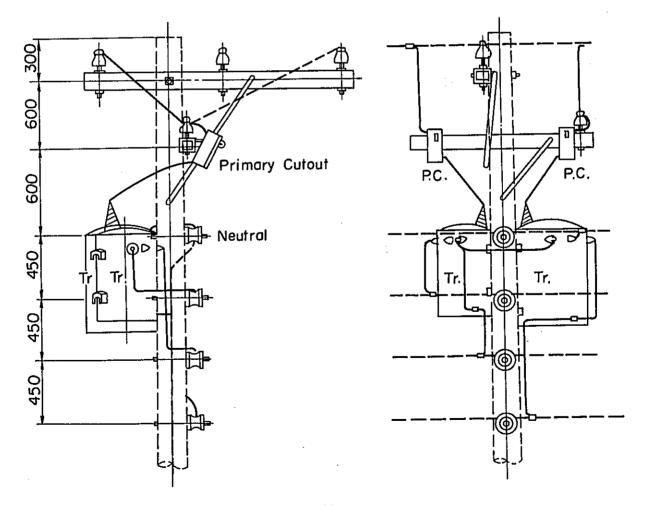
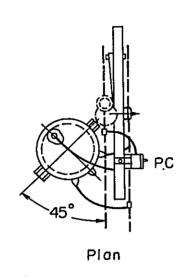
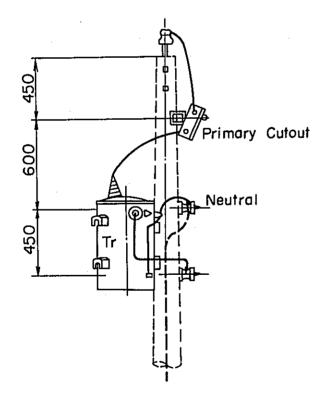
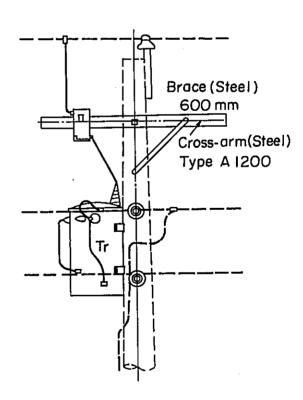


Fig.A-6-8 Details of Pole Dimension Diagram

(7.62/13.2 kV, Single Phase Transformer)







APPENDIX A-7

COST ALLOCATION OF 230kV TRANSMISSION LINE BETWEEN AMBUKLAO AND SANTIAGO

Appendix

A-7 Cost Allocation of 230 kV Transmission Line between Ambuklao and Santiago

(1) Upon interconnection of the Magat Power Plant with the Cagayan Power System in 1981, most of power will be transmitted to the Central Manila Power System. Therefore, it is not appropriate that the proposed transmission facilities under this Project only bear all costs to be incurred in its construction, but in measuring the economy of the transmission line the cost should be allocated to the Magat Hydro Power Plant according to a suitable ratio commensurate with the benefits to be derived by the said power plant and the transmission line.

The "benefit" of the power plant has been obtained by multiplying the kW value and kWh value of an alternative thermal power plant shown in Table A-7-2 with the power requirement (kW) and energy requirement (kWh) of power transmittable to Manila through the Central Luzon Power System. Benefits of the Cagaya Valley transmission line have also been obtained by multiplying the abovementioned values of the standard thermal power plant with the kW and kWh values obtained on the basis of the forecasted power demand in the Valley described in this study.

(2) As seen in Table A-7-1, in order to obtain a ratio of costs to be allocated between the Magat Hydro Power Plant and the transmission line, the benefits to be accrued in the respective years during the serviceable life of the facilities are converted into values in the beginning of 1978 at a discount rate of 12%. As a result of these tabulations, the allocation ratio to the Magat Hydro Power Plant is 75.3%.

Table A-7-1 Cost Allocation of Transmission Line between Ambuklao and Santiago

Items	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987	1
Magat P.S. Available power (MW) Available energy (GWh)	1 1		t t	200	300 991	300 991	300 991	300 991	300 991	300 991	
Cagayan Valley Power requirement (MW) Energy requirement (GWh)	23.5	27.7	31.0 139	34.5 154	38.7	43.8 189	47.7	52.3 222	56.9	61.4 258	
Transmittable power and energy to Manila Power (MW)	1	1	i	165.5	261.3	256.2	252.3	247.7	243.1	238.6	
Energy (GWh) kW value 1/ (US\$/kW) kWh value (mills/kWh)	31.7	31.7 16.9	31.7 16.9	768 31.7 16.9	821 31.7 16.9	31.7 16.9	786 31.7 16.9	31.7 16.9	751 31.7 16.9	31.7 16.9	
(1) Cagayan Valley kW value (10 ³ US\$/kW) kWh value (10 ³ US\$/kWh)	744 1,808	878 2, 129	982 2,349	1,093	1,226	1,388 3,194	1, 512 3, 464	1, 657 3, 751	1,803 4,056	1,946	
(2) Power and energy to ManilakW value (10³US\$/kW)kWh value (10³US\$/kWh)	1 1	t t	1 1	5, 246 12, 979	8, 283 13, 874	8, 121 13, 553	7, 997	7, 852 12, 996	7, 706	7, 563	

Note: 1/ implies the figures derived from an alternative thermal power plant to Magat Power Station.

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	Items	1978	1979	1980	1981	1982	1983	1984	1985	1986	1987
Ξ)	(1) Cagayan Valley										
	Total value (10 ³ US\$)	2,552	3,007	3, 331	3, 695	4,099	4, 582	4,976	5, 408	5, 859	6,306
(2)	(2) Manila Grid										
	Total value (10 ³ US\$)	1	ı	1	18, 225	22, 157	21,674	21, 280	20,848	20,397	19,950
	Discount rate (12%)	0.892	0.797	0.711	0.635	0.567	0.506	0.452	0.403	0.360	0.321
(3)	(3) Present value $(10^3 US\$)$:		•	· .
	Cagayan Valley	2,276	2,396	2,368	2,346	2, 324	2,318	2,249	2, 179	2,109	2,024
	Manila Grid	ı	•	ı	11, 572	12, 563	10,967	9,618	8, 401	7,342	6, 403
(4)	(4) Total present value (103US\$)										
	Cagayan Valley		22, 589	+ (6, 306	x 8.244	x 0.321)	= 22, 589	+ 16, 687	22, 589 + (6, 306 x 8.244 x 0.321) = 22, 589 + 16, 687 = 39, 276	.0	
	Manila Grid		66, 866	66, 866 + (19, 950 x		8.244×0.321) = 66, 866 +	= 66, 86	6 + 52, 79	52, 794 = 119, 660	099	•
		Constru	Construction cost to be allocated to the Project=	st to be a	llocated	to the Pr		39,276 39,276 + 119,660		× 100	

A-71

Table A-7-2 Alternative Thermal Power Plant

Plant capacity (MW)		200
Plant factor (%)		70
Annual energy production (GWh)		1,230
Station service use (%)		5.0
Annual available energy (GWh)		1,170
Thermal efficienty at sending end (%)		35.7
Construction cost (thousand US\$)		52,100
Foreign currency	·	42,700
Domestic currency	•	9,400
Serviceable life (years)		30
Annual cost (thousand US\$)		
Fixed cost		
Amortization		5,210
Repair and maintenance		830
Annual salary		110
Miscellaneous cost		100
Administration cost		90
Subtotal		6,340
Variable cost		
Fuel cost		19,500
Repair and maintenance		210
Subtotal		19,710
Total		26,050
Fixed cost (US\$/kW)		31.7
Variable cost (mills/kWh)		16.9
Total cost (mills/kWh)		22.3
	•	

Note: 9,650 BTU/kWh

