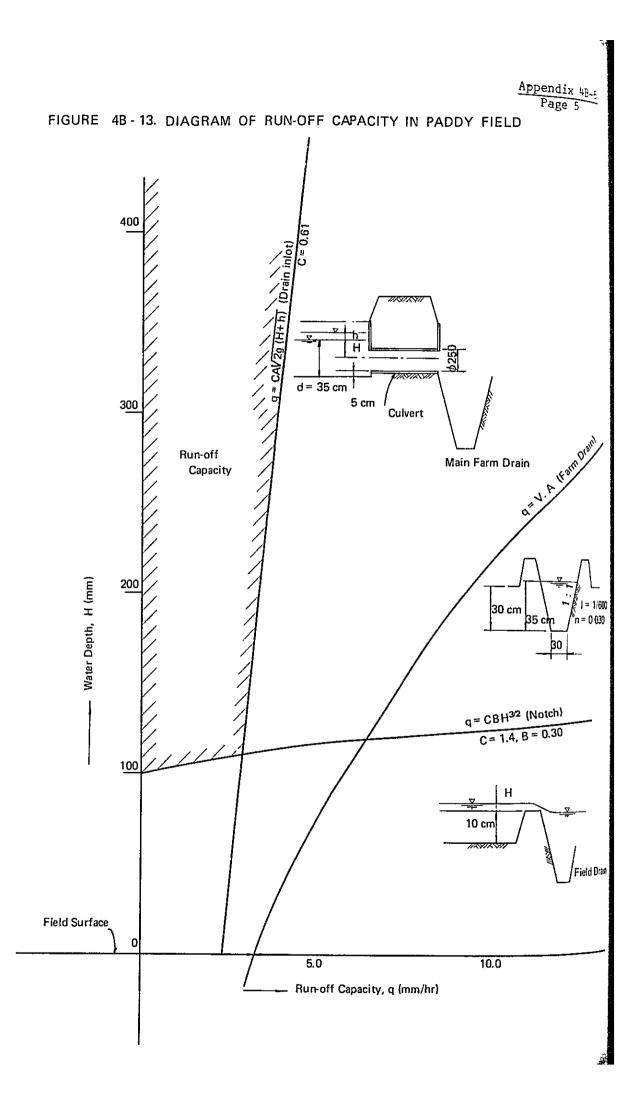
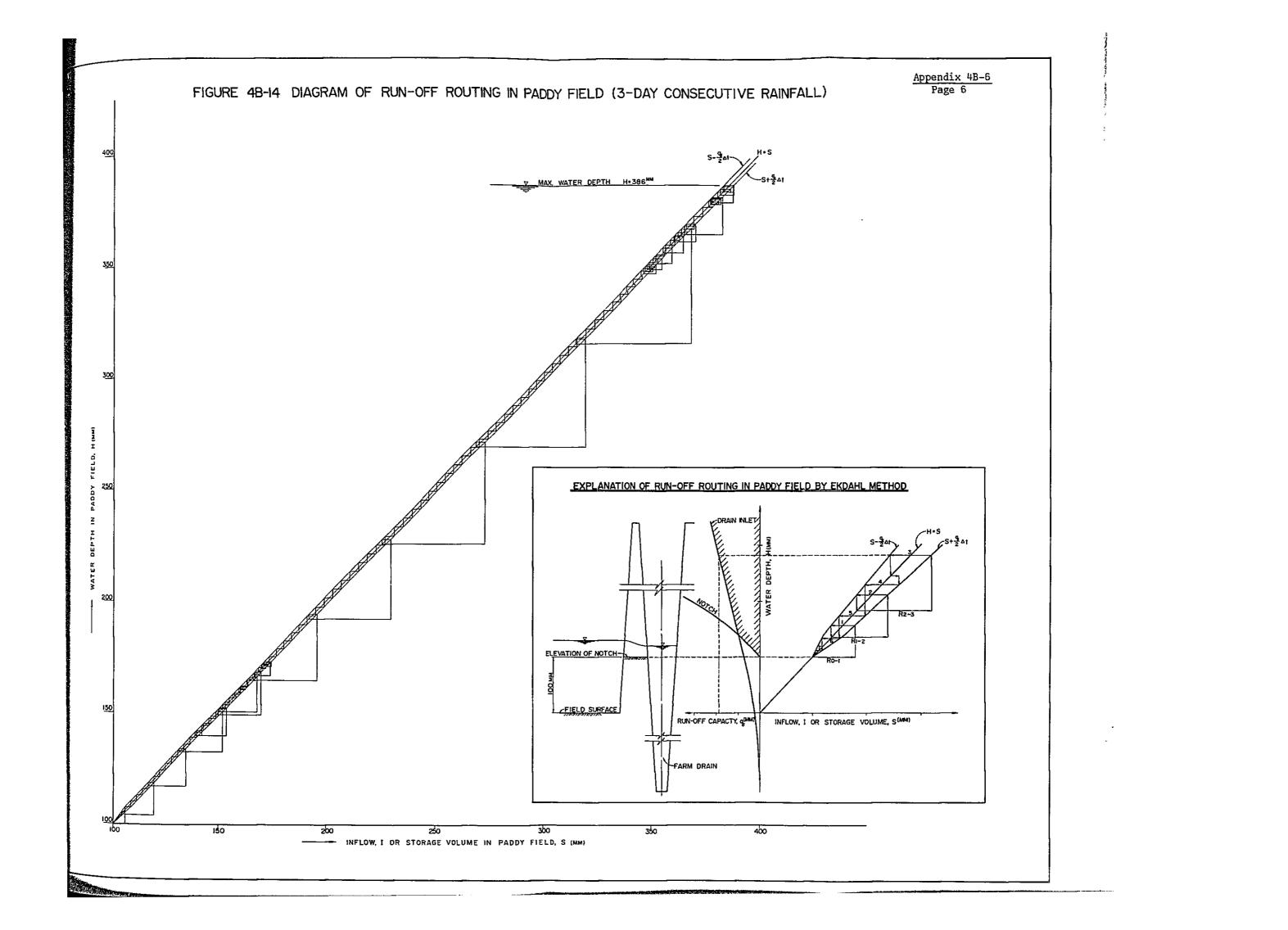
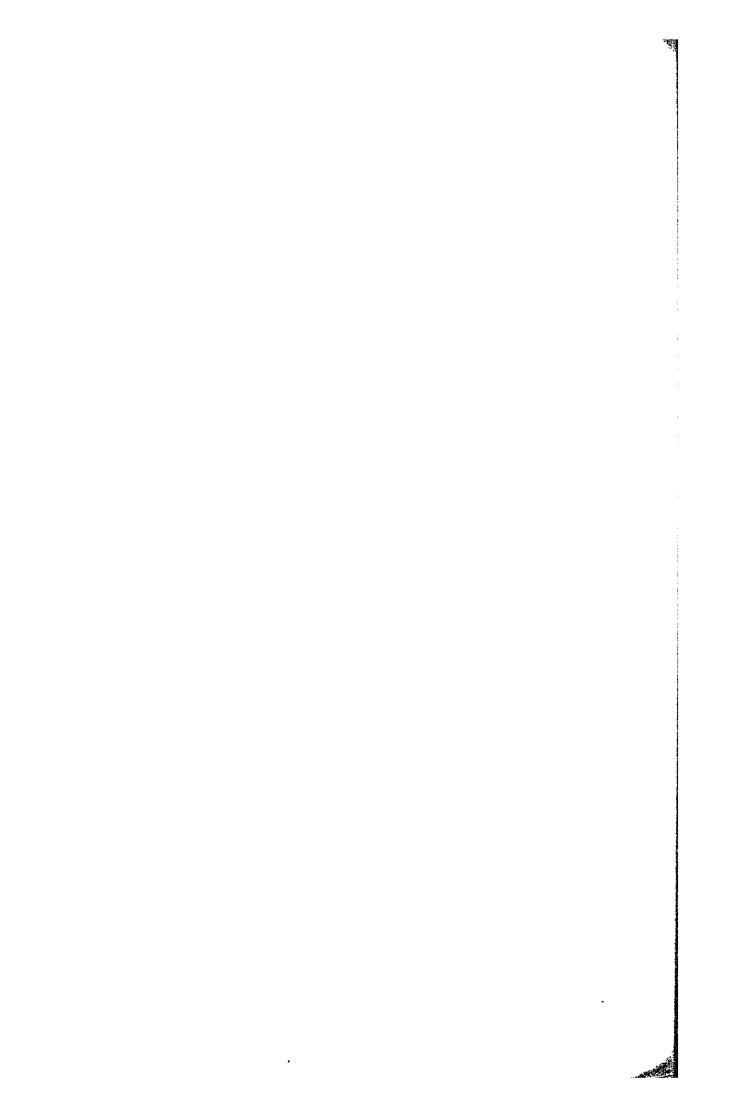


### FIGURE 48-12. DRAINAGE SYSTEM IN THE PADDY FIELD



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Run-off Discharge mm3/ cu.m/sec/sq.km	4.43 1.231												4.25 1.1B1															4.21 I.169		4.17 1.15B	4.15 1.153	4.12 1.144	~	-1	4.07 1.131
LUN LUN	 +	3	77, 44	1	÷	Ŧ	÷	÷,	Ŧ	<b>1</b>	=	<b>.</b>	3		÷	4	а.	÷	3	Ŧ	4	4	Ŧ	÷	Ξ.	±.	<b>a</b>	3	=	2	±.	±.	Ŧ	4	4
Lffective Water Depth Rainfall in Paddy Field2/ (mm)	385.5	384.3	386.0	383.0	380.0	380.1	379.0	376.3	372.0	367.7	363.5	359.2	354.8	351.5	349.7	348.8	350.4	353.2	357.9	363.0	368.5	367.9	364.8	361.5	358.0	354 .4	351.5	347.6	0.446	340.6	337.2	333.7	329.7	325.8	321.6
Lffective Rainfall (mm)	4.7	3.1	6.3	1.6	1.6	4.7	3.1	1.6	0	a	0	Ō	0	0.6	2,6	3.2	5.7	6.9	8.5	9.2	9.7	3°4	1.7	6.0	6'0	0.6	1.1	0.3	0.3	0.9	0.6	0.3	0	0	0
Hourly Rainfall (mm)	4.7	3.1	6.3	1.6	1.6	4.7	3.1	1.6	Ð	c	0	¢,	0	9.0	2.6	3.2	5,7	6,9	8.6	9.2	9.7	а. С	1.7	6.0	0.9	0.6	1.1	0.3	0.3	6.0	0.6	0.3	0	Ð	0
Time	12	E T	1	15	16	17	18	61	20	21	22	23	24	Ч	7	സ്	7	ŝ	Ð	7	8	თ	10	Ħ	12	13	14	15	16	17	18	19	20	21	22
t A E						0	_		_											-	г		-												
Run-off Discharg- mm <sup>3</sup> / cu.m/sec/99.km	0		0	.70																3.11 0.864						3.10 0.861	3.16 0.878	3.35 0.931	3.52 0.978	3.80 1.056				Η	4.43 I.23I
Water Depth in Paddy Field2/ (mm)	0		0	1.70	2.90	3.00	3.09	3.19	3.20		3.19	3,18	3.18	3.18	3.17		3.14	3.15	3.14	3.11	3.10	3.08	3.05	3.04	3,04	3,10	3.16	3.35	3.52	3.80		4,33	1 011 1	E 4.4	
, <u>spi</u>	/ 81.2 0	86.7 0	93.4 0	1.70	118.6 2.90	134.0 3.00	3.09	168.2 3.19	172.8 3.20	173.1 3.20	171.6 3.19	170.0 3.18	168.2 3.18	167.4 3.1B	164.8 3.17	3.15	160.8 3.14	159.0 3.15	156,7 3.14	153.6 3.11	150.5 3.10	147.5 3.08	144,5 3.05	141.2 3.04	141.5 3.04	152.2 3.10	166.0 3.16	194.2 3.35	227.5 3.52	271.0 3.80	00 h 2 LTE	366.5 4.33 1	380.8 4.40 1	385.5 4.43 1	H.43 1
Water Depth in Paddy Field2/ (mm)	0 <u>1</u> / 81.2 0	0 86.7 0	0 93.4 0	105.0 I.70	14.7 118.6 2.90	18.4 134.0 3.00	19.6 150.5 3.09	20.8 168.2 3.19	7.4 172.8 3.20	3.7 173.1 3.20	1.9 171.5 3.19	1.9 170.0 3.18	1.2 168.2 3.18	2.5 167.4 3.1B	0.6 164.8 3.17	0.6 162.2 3.15	1.8 160.8 3.14	1.2 159.0 3.15	0.6 I56.7 3.14	0 153.6 3.11	0 150.5 3.10	0 147.5 3.08	0 I44,5 3.05	0 141.2 3.04	3.1 141.5 3.04	14.1 152.2 3.10	17.2 166.0 3.15	31.4 194.2 3.35	37.6 227.5 3.52	47.0 271.0 3.80	50.2 317.2 H.00	53.3 366.5 4.33 1	380.8 4.40 1	9.4 385.5 4.43 1	4.7 385.5 4.43 1

Talle 40 11 Recut of Run-off Routing in Luddy IIcid (1)

Rainfail of 20 mm is neglected as initial losses in paddy fields height of notch : 100 m above field surface Water level : 80 mm 귀 Note:

2/: Obtained from Figure 3/: Obtained from Figure

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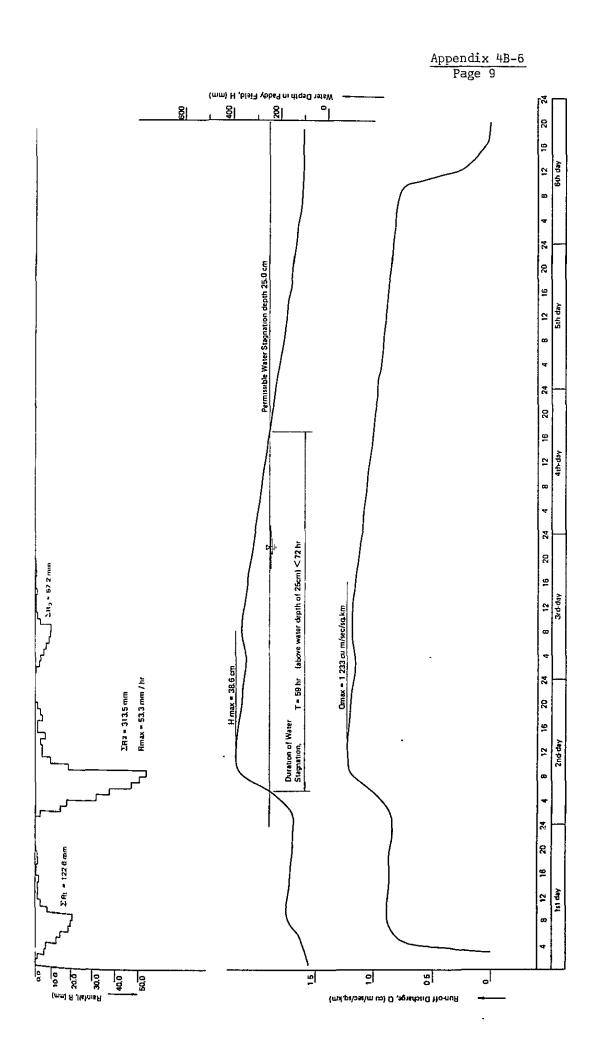
arge	/sq.km	416.	.906	006	897	889	886	378	.875	367	.861	358	358	353	34.7	.842	833	131	128	122	.817	811	806	806				٩g	e	8	_		5	
Run-off Discharge	cu.m/sec/sq.km	5°0	0.9	0.9	0.8	•	•	0.878	0.8	9.0	3.0	3.0	9.0	3.0	0.6	0.5	0.8		0.6	0.6	0.8	0.8		0.8	0,8	0.7		0.4	0.278	0.2	0.139	0.033	50.0	
Run-c	uu uu	3.29	3,26	3.24	3.23	3.20	3.19	3.16	3.15	3.12	3.10	3.10	3.09	3.07	3.05	3.03	3.00	2.99	2.98	2.96	•	2,92	2.90		•	2.86	2.30	1.60	1.00	0.90	0.50	0.30	0. 20	· · · ·
in Paddy Field	( <u>um</u> )	185.6	-	-	175.0		-		161.5		154.8		148.4	145.0	143.8	139.O	135.8	133.0	130.3	127.2	124.3	121.3	118.6	115.7	113.0	110.2	107.3	105.4	103.7	192.7	102.0	5.101	2.111	
Rdinfall	( tum )	ı	,	ı	ı	ł	ſ	ı	ł	ı	ı	ı	ı	ı	ı	ı	ı	1	I	ı	1	1	ı	ı	ı	ı	ł	I	I	I	ı	ı	ı	+ I
Rainfall	( uu )	1	ı	ı	ı	ı	ł	1	ı	ı	I	1	ı	ı	ı	ı	I	ı	ı	ł	ı	,	ı	ł	t	,	ı	ı	ï	1	ı	ł	ţ	I
Tîme		6	10	11	12	13	14	15	16	17	1.8	19	20	21	22	23	24	~1	2	ო	t,	ы	g	٢	æ	ဇာ	10	11	12	13	14	1.1	14.	
[ Discharge	cu.m/sec/sq.km	1.125	1.113	1.108	1.100	1.097	1.089	1.083	1.081	1.077	1.066	1.061	1.055	1.053	1.042	1.039	1.028	1.025	1.019	1.014	1.005	1.000	-	•	٠		0.972	•	•	0.944	0.442		•	 
Run-off		4.05	4.01	3,99	3.96	3.95	3.92	3.90	3.89	3.88	3.84	3.82	3.80	3.79	3.75	3.74	3.70	3.69	3.67	3.65	3.62	3.60	3.60	3.55	3.54	3.51	3.50	3.50	3.48	3.40	3,39	3.37	3,36	1. 1. 1.
Water in Pad	( mm )	317,6	313.8	310.0	306 4	302.4	298.5	294.8		287.4		279.8	276.0	٠	268.5	264.7	260.9	257.0	253.0	249.9	245.0	241.0	237.0	233.0	229.0		221.0	217.1	213.3	209.1	205.2	201.2	197.7	1931
Effective Rainfall		0	Q	ı	1	t	t	ı	I	I	ı	ı	t	1	ı	I	ı	ł	ł	ı	I	ı	t	ı	r	ı	ı	ł	ł	ı	ı	I	ı	1 -
Hourly Rainfall	(	0	0	ł	ı	ı	I	I	ı	I	1	1	1	1	1	1	ı	ı	1	I	I	ł	ı	ı	ł	ı	1	1	ŀ	ŧ	i	ł	,	<b>+</b> 1
Time		23	24	1	2	<b>თ</b> .	ב <del>ו</del> ו	ມ ເ	ιο		ω (	ה ה י	01:	11	21	<u>5</u> 1	H T	15	16	Т7	18	19	20	21	22	23	24	Ч	2	ო	7	ç	ى	<b>.</b> 2

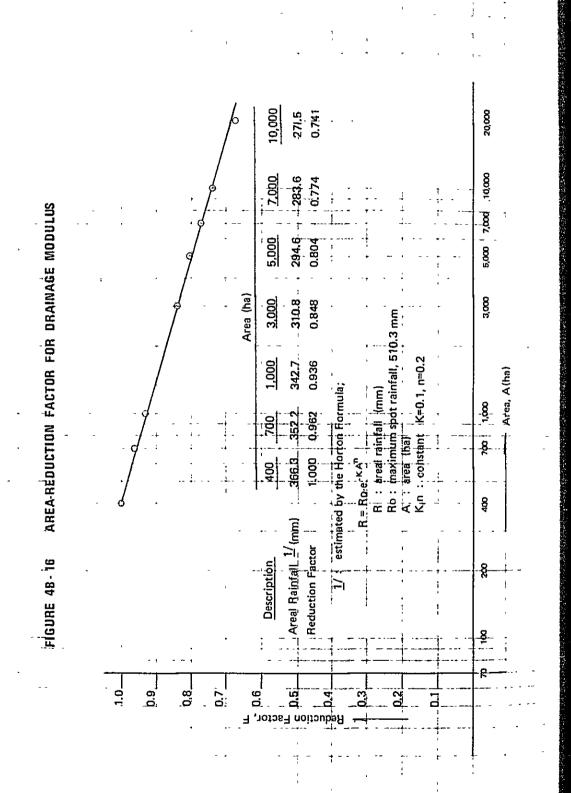
Table 4B-11. Result of Run-off Routing in Paddy Field (2)

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## E. Drainage Discharge from Hilly Land $\frac{1}{}$

Drainage areas located in the hilly land are mostly less than 10 - 4.4m. The flood time of concentration for such a small drainage area will be less than one hour. Only hourly peak rainfall, theretore, was considered for drainage discharge analysis. Relationships -etween observed peak discharges from drainage areas less than 100 1.4.4m and hourly peak rainfall intensity was plotted as shown in 1.1gure 4B-17. This shows the peak discharge and hourly rainfall increase in a rather constant rate. So, the run-off coefficient was et = 1.14m and f = 0.269 from the figure. This run-off coefficient 1.14m adopted to estimate the peak discharge from hourly rainfall.

The obtained run-off coefficient might be on a high side, recause the available peak discharges are mostly in the mountainous area. Normally run-off coefficient for small areas in hilly land ranges from 0.1 to 0.3. So, the obtained value of 0.269 is considered to be acceptable.

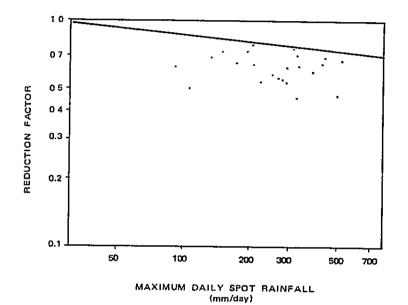
The estimation of peak discharge was made based upon the Rational formula;

Q = 0.2778.f.r<sub>t</sub>.A
where f : run-off coefficient of 0.269
r<sub>t</sub>: areal hourly peak rainfall intensity (mm/hr)
A : catchment area (sq.km)

In order to estimate the peak discharge, the peak rainfall as Ltained from the reduction factor of daily rainfall (see figure -5-18), was considered as average rainfall in the Project Area, and used in the Rational formula for areas smaller than 100 hectares. The areal hourly rainfall obtained from the relationship of spot "ourly rainfall to areal hourly rainfall (see Figure 4B-19) was adopted to estimate the peak discharge for large areas up to 20,000 rectares using as basis for estimation of areal hourly rainfall "Ltained from Laoag and Vigan. The results are shown as follows;

<sup>27:</sup> reference was made to the study of NISIS-I, prepared by NIA, 1976.

### Figure 4B-18. Reduction Factor of Areal Rainfall to Maximum Daily Spot Rainfall



Note: Arithmetic mean method was adopted to estimate a reduction factor of spot rainfall to the areal rainfall. The maximum rainfall and the reduction rate to the areal rainfall was plotted on the logarithmic paper.

#### Areal Hourly Rainfall of Each Return Period

Return Period	Spot Peak Hourly Rainfall (mm)	Areal Hourl (1) (mm)	y Rainfall (2) (mm)
5-year	53.3	41.0	35.5
10-year	66.2	49.7	40.0

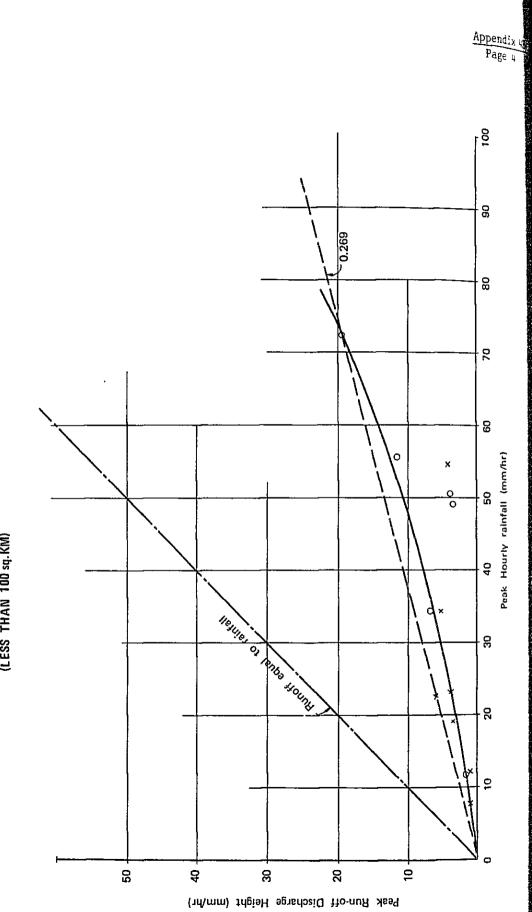
(1) : Obtained from the reduction factor of areal daily rainfall. (Fig. 4B-18)

(2): Obtained from the relation ship of spot hourly rainfall and(Fig. 4B-1:) areal hourly rainfall.

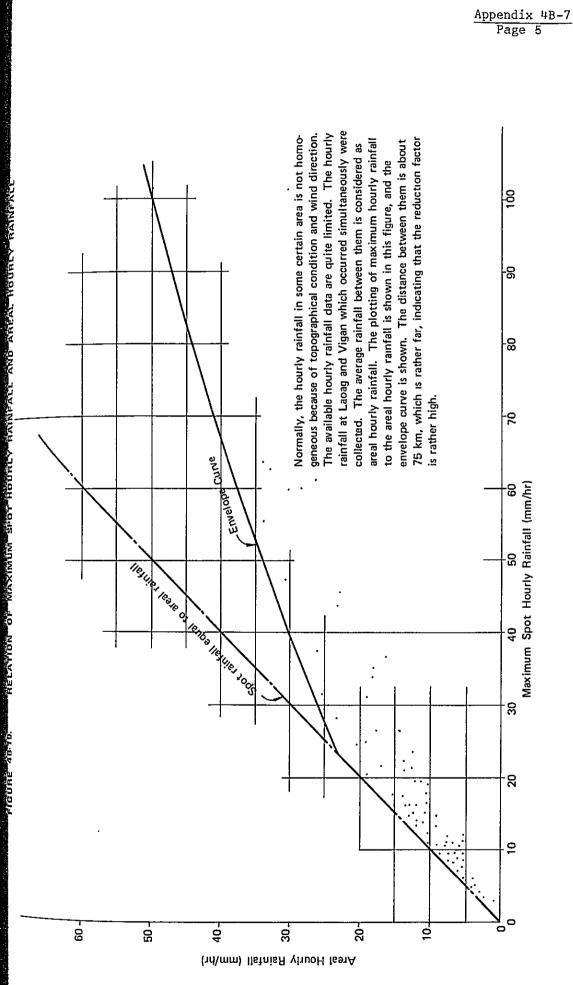
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	<u>Peak</u> Dis	charge of Hi	lly Land Area	
Ieriod	Drainage Area (sq.km)	Hourly Rainfall (mm/hr)	Peak Discharge (cu.m/sec)	Specific <u>Discharge</u> (cu.m/sec/ha)
1,5	1.0	41.0	3.1	3.064
	200.0	35.5	530.5	2.653
1,10	1.0	49.7	3.7	3.714
	200.0	40.0	597.8	2.989
	,			

Peak Discharge of Hilly Land Area



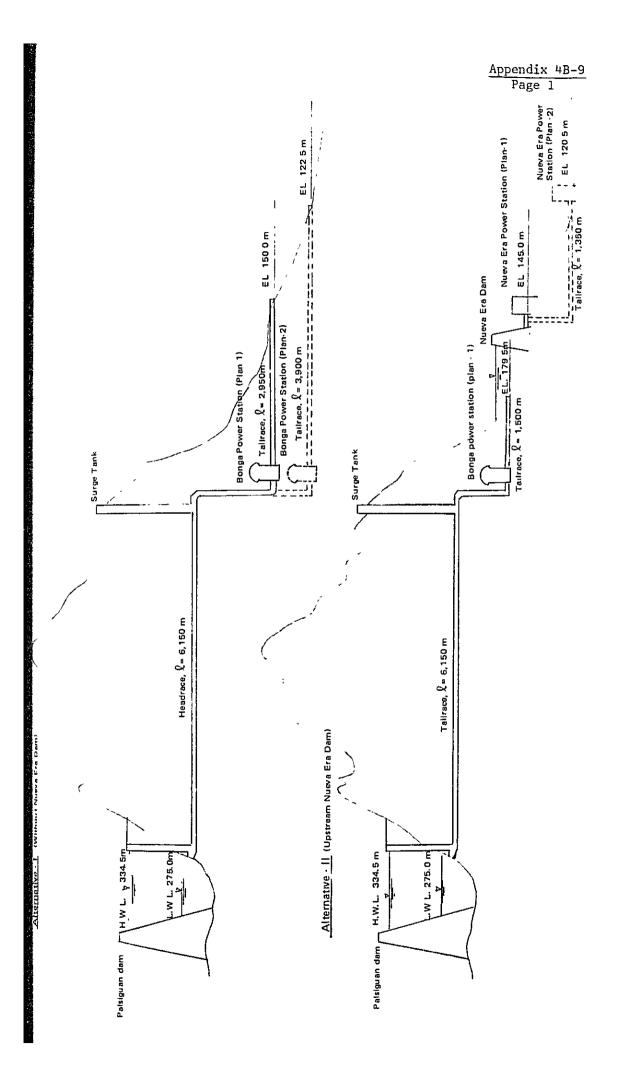




Description	Unit	FL 265.00 m	Low Water Level Et 275.00 m EL 2	Level EL 285.00 m	EL 295.00 m
Max. Discharge at Bonga P/S	D a	28,225	28,225	28,225	28,225
Design Effective Head	£	146.26	150.82	155.40	161.22
Installed Capacity	ΧW	35,200	36,000	37,400	38,800
Annual Generation	GWh	154.83	159.66	164.51	170.67
Effective Output	КW	32,586	33,776	35,198	36,718
Construction_Cost Bonga P/S_	P10 <sup>3</sup>	527 <b>,</b> 241	538,325	566,564	584,127
Palsiguan Dam <sup>2/</sup>	₽10 <sup>3</sup>	798,963	844,483	889,080	954,738
Tunnel	P10 <sup>3</sup>	160,140	140,330	138,330	138,330
Power Plant	₽10 <sup>3</sup>	143,600	144,400	145,600	146,900
Annual Cost Ratio	0 <sup>0</sup> 0	15.43	15.43	15.43	15.43
Annual Cost Value of Bonga P/S (C)	₽10 <sup>3</sup> /Year	81,353	83,064	87,421	90,131
Annual Unit Capacity Value	₽/KW	700.0	700.0	700.0	700.0
Annual Unit Energy Value	₽/KWh	0.429	0.429	0,429	0.429
Annual Capacity Value (B)	₽l0 <sup>3</sup> /Year	82,599	85,288	88,156	91,599
Annual KW Value <sup>3/</sup>	₽l0 <sup>3</sup> /Year	22,810	23,643	24,639	25,703
Annual KWh Value <sup>±/</sup>	Pl0 <sup>3</sup> /Year	59,780	61,645	63,517	65,896
(C) - (B)		- 1,246	- 2,224	- 735	- 1,468
Note: <u>1</u> /: (Palsiguan dam cost	dam cost + Tunnel cost) x	+ +	Power plant cost		

Table 4B-12. Comparison of Low Water Level

Appendix 48-8



### Table 4B-13

### Comparison of Alternative Plans

					Appendi: Page	
Table 4B-13 Compari	<u>son of</u>	Alternat	ive Plan	5		
1. Major Dimension						
ltem	Unit	Proposed Plan	Alterna Plan-1	Plan-2	Altern Plan-l	ative-11 Plan-1
a. Bonga Power Station						
Full Water Level	m	334.50	334.50	334.50	334.50	<b>334</b> .50
Tail Water Level	m	150.00	150.00	122.50	179.50	179.50
Tailrace Length	km	2,95	2.95	3.90	1.50	1.50
Effective Head	m	150.82	150.82	177.32	119.82	119.82
Installed Capacity	KW	36,000	36,000	42,000	29,000	<b>29,0</b> 00
Firm Peak Capacity	KW	30,510	-	-	24,600	24,600
Annual Generation	MWh	159.660	159.660	185.300	123.400	123.400
Turbine	type	Deriaz	Francis	Francis	Deriaz	Deria:
	set	1	1	1	1	1
b. Nueva Era Power Station						
lligh Water Level	m	150.00	-	-	179.50	179 50
Lower Water Level	m	148.50	-	-	177.50	177.50
Tail Water Level	m	120.50	-	-	145.00	120.50
Tailrace Length	km	-	_	-	-	1 35
Effective Head	т	27.92	_	-	32,32	55 tai
Installed Capacity	KW	6,800	-	-	7,900	13,600
Annual Generation	MWh	39,540	-	_	54,700	73,200
Turbine	type	Kaplan	-	-	Kaplan	Kaplan
	set	1			1	1
c. Nueva Era Dam						
Catchment Area	sq.km	52.40	_	-	45.10	45.10
Dam Height		45.50	_	_	47.10	47.10
Crest Length	m	220.00	_	-	187.00	187.00
Dam Volume		141,000	_	_	130,000	
Diversion Channel		Open Channel 10mx7m	-	-	Tunnel Ø8m	Tunnel ø8m
d. Diversion Dam		No Provision	Provided	Provide	ed Provid	ted No Provisi

## 2 Evaluation of Alternative Plans

Item	Unit	Proposed Plan	Alterna Plan-l	ntive-1 Plan-2	Alterna Plan-1	Plan-2
Luctabled Canacity						<u>1 1011-2</u>
Bonga Power Station	KW	36,000	36,000	42,000	29,000	29,000
Nueva Era Power Station	KW	6,800	-		7,900	13,600
Jotal		42,000	36,000	42,000		-
h Annual Generation		-	•	,		,
Bonga Power Station	MWh	159.660	159.660	185.300	123.400	123.400
Mueva Era Power Station	M₩h	39.540	-	-	45.700	73.200
Total		199.200	159.660	185.300	169.100	196.600
Effective Output						
Bonga Power Station	KW	33,780	14,720	17,490	26,690	26,690
Nueva Lra Power Station	KW	4,510	-	-	5,210	8,410
Tota1		38,290	14,720	17,490	31,900	35,100
5 Construction Cost						
Bonga Power Station	10 <sup>3</sup> ₽	144,400	171,700	198,000	113,600	113,600
Nueva Era Power Station	10 <sup>3</sup> ₽	40,900	-	-	46,000	75,200
Nueva Era Dam	10 <sup>3</sup> ₽	121,600	-	-	119,500	119,500
Diversion Dam	10³₽	-	10,000	10,000	10,000	-
lotal		306,900	181,700	208,000	289,100	298,300
n. Unit Valve						
Annual Cost Ratio	00	15.43	15.43	15.43	15.43	15.43
Annual Unit Capacity Value	₽/KW	700	700	700	700	700
Annual Unit Energy Value	₽/KWh	0.429	0.429	0.429	0.429	0.429
7. Annual Value						
kh Value <sup>1</sup> /	10 <sup>3</sup> ₽	26,803	10,304	12,243	22,330	24,570
Wh Value <sup>2</sup> /	10 <sup>3</sup> ₽	76,911	61,645	71,544	65,290	75,907
Total (B)	10³₽	103,714	71,949	83,787	87,620	100,477
8 Annual Cost Value (C)	10 <sup>3</sup> P	47,355	28,036	32,094	44,608	46,027
<sup>9</sup> . (B) - (C)	10 <sup>3</sup> ₽	56,359	43,913	51,693	43,012	54,450
<sup>10</sup> . Use Ratio of Effective Output <sup>3</sup> /	0) 0	0.281	0.134	0.138	0.275	0.261
Note: 1/: Effective out		700₽/KW				

Note: <u>1</u>/: Effective output x 700 $\mathbb{P}/KW$ <u>2</u>/: Annual generation (KWh) x 0.90 x 0.429  $\mathbb{P}/KWh$ <u>3</u>/: Effective output x 4hr x 365days/Annual Generation (KWh)

Table 4B-14 Hydro Power Operation Study for 10 Year (1960 – 1969) - Bonga Power Station	Table 4B 15 Hydro-Power Operation Study for 10 Year (1960 – 1969) - Nucva Era Power Station	Note Bonga Power Station	Max Loss 13 B5 m (28 225 m <sup>3</sup> /s) Mini Loss , 4 23 ( 9 5 m <sup>3</sup> /s)	Turbin Efficiency $d = H W L$ , $-W.L$ .	Efficiency (1) = 0 000454 × d + 0 865 (28 225 m³/s) Efficiency (2) = 0.00134 + d + 0 700 ( 9 50 m³/s)	Generator Efficiency 0.975	Nucva Era Power Station Loss = 0 0015 x Q <sup>2</sup> + 0 30	Turbine Efficiency Discharge Efficiency	2	m <sup>3</sup> /s m <sup>3</sup> /s 27.273 ~ 25.00 0.890 24.99 _ 20.00 0.895	- 17 50	- 12 50	12.49 - 10.00 0.872 9.99 - 9.00 0.850 8.99 - 0.800	iciency. 0 965	H W.L. : High Water Level (m)	-	Losses Losses (m)			Paak Kw Prak Duitput (Kw) Detroversee SWH see Studiet Grugerstick/SWH)
Table	Table																			

Appendix 4B-10 Page 1

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-	GROSS (M)	184.500	81.54	177.537 177.537 172.266	167.513 162.875 159.152	157.066 154.952 153.757	152 - 778	51.4×	150.307 150.307 149.386	148.420 147.527 141.969	146.193 149.072 152.643	156.709 160.914 165.737	168-830 170-576 172-337	176*930 182•061 183•165	183.500 184.008 184.500
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11	377	49,402	49.828	149.736	49.857	101 07	760.02	149.840 I		49.560 40 430	149.456		49°2	149.250 1	7 ° 7	9.250	49.2	49 <b>.</b> 250	052.64	149.250 1	49.355	000 00	149.411	17	200	47 47 40 474	149,908		9,609	49.635	000	150.000 1	0000.0	0,000	49	49.680			
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NVFR F.	(CM/S)		0.0	2	0.0	0.0	0.0			0.0	0-0	0.0	0.0	0.0		0.0	0-0	0.0		0.0	<b>0</b> .0	0.0		0.0	0.0	0.0	5		0.0		0.0	0*0	0.0		0.0	0.0	0.0	1	0.0		0,0	0-0	0.0
T.D.15.	(CN/S)	<15.71	54.243	)   	29.273	29.273	29.273	f	272.62	512.62	24.213	27.273	29.273	29.122		28.921	28.871	28.806		28.713	28.684	29.273	1	£72.95	29.273	29.27}	626 06	24.27	29.273		29.273	29.273	29.273		29.273	29.273	29.273		512.62		214.22	16.4P7	11.411 H. 100
F . HF AD	(M)	27.015	27.915	, ,	5	16.7	27.915	3	C16.12	16.7	· ·	27.91F	27.915	27.937		· ·	27.972	~		· · ·	27.998	r .	1	16.1	27.915	· ·	-	516.75	16.7		27.915	r.	27.915		5	16-7	r.		214-72 22 115		128-82	2c * 4 6 1	24,481 30,263
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1.DIS.	8.000	31	1. (2	5 6	99	5	4.30	8.78	24.706	5	15 437	3.36	1	30.	4 8 4	5	c6.	4.815 4.015		f. • 96 l	7 442	612.0	47	ŝ	-15	4.4	7.715	5	00 6	22.207	6.70	5.73	15.072	• 76	¢,	6.739	45			
f .HF ∆[ [ 4 ]	0.264	9 594	9.406	411	6 790 	106.	8.586	7.984	27.995	150.0	29.600	9.8U3		5°0	50.400		°.0	30.616 20.605		30.345	m * • •	2°.	4.167		•	0.1	30.301	0.2	0.844	28 847 2	o.470	12.9.6	29.636	1.0	2 2 2	014.05	44.0			
	.396	0 :		.287		•	• 186	543	• 536	410	0.657	568		6 E E •	996	1	335		5	373	• 383 • • • •	+ 40 0	569	0.565	400	.435	0.389	• 396	055	1.040	.718	648	0.641	° 443	212	0.468	£9F.			
(W)		°, °	*	29 <b>-</b> 69H	<b>.</b>		6	9.52	29.531	00.0	30.257	0.37	-	2 2 2	30.945	•	6°0	30,947	;	30.75U	l 2 n	+ 0 + 5	਼	30.374	0	0.5	30.640	0.6	0.30	29,837	0.1 P	0.2	30.277	۰°	- 0	30.778	8			
	585	9.260		0.175	. 006 °6		053	456	449	9.686	19.255	9,068		0 - 2 C C	18.305	•	8,307	18.308		402		061.0	9.518	19.063	8•599	8.718	18.560	8.585	9,027	19.864	9.369	9.236	19.222	B. 744	8. 657	8.472	8.447		<u>.</u> •	
3.1.	49.250 1	49.514 1 49.734 1		50	49. ( 05 40 - 080		49.825 1	49.483 1	49.980 1	49-681 1	49.512 1	49.439 1		49.250 1 49.250 1	49.250 1		49.250 I	49.250 l		49.250 1	1 052464		49.054 1	49.437 1	1 662.64	49.302 1	49.250 1	49.250 1	49.423 1	49.751 1	49 <b>.</b> 557 l	49.505 1	49.499 1	49°312 1	9.278	11 052 01	9.250			
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LWI	1)24 a60.	160540.	2709120.	040040°	1004784	2817744.	1020480.	1096 920.	3197160.	723360.	046840. 1526329.	2396488.	43968C.	4306AC.	443648. 	13030U8. 43769C.	439680	439680.	1319040.	439680.	443648.	1363005	1104260.	1561440.	3c30Fr0.	1519440.	1706760.	4858200. 5 2014 0	535200.	o35184.	170.0544	674160. A 314 80	934840.	20956J0.	1632000.	1214634
X X	3854.	3109. 4265.		- E F H 4	3806.	777	4 374	4155.		3014. 3106	2133 <b>.</b>		1432.	1532.	1832.	1832.	1432.	1832.	1 4 3 3	Ld32.	1832.	7 00 7	4 60 J -	6 506.	000 7	6331.	6465.	. 000 0	2230.	2406.		2407	3916.	1.847	6.00	* \$ ] \$
FFFICF.	0.885	0.889		0 892	0.889	600 0	0.842	0.889		210-0	0-850		0.800	•	0.800	0.600	0.800	0.800	0.900	0.800	0.800	6 00 0	0.892	0.890	ere o	0.890	0. F90	0.850	0.850	0.850		217.0	0.889	<del>.</del> Н 4	0.843	2
OVER F. (CM/S)	0.0	0.0		0.0	0.0	0,1	0.0	0.0	0		0-0		0.0	0.0	0.0	0.0	0.0	•••	0.4	0.0	0.0		0.0	0.0	2.158	0.0	0.0	0.0	0.0	0.0	0		<b>C</b> •C	0.0	0.0	
T.DIS.	L5.489	17.247	243 10	19.877	15.280	17.364	17.654	16.774	166 61	10.884	9.036		8,01U	н, 000	8.000	в.000	8.000	8.030	8.000	6 000	А.000	19.752	6	~	29.273	26.593	27.239	9.107	6 [ J ]	0+0-6	1		5	24.075	29.273	101-11
F.H <sup>r</sup> An ( M)		29 412	d	29.122	<b>a</b> 0	5	29,369	<b>6</b> .4	0		30.146		30,269	<u>`</u>	¥.	0.2	30.269	0.2	~ C	30.269	0.2	1.1	29.261	B.1	7.9	28.286	4 <b>.</b> 1		30.172	σ.	0 0	• •	5	8.6	27.915	•
LUSSES (M)	0.660	0.746	0.474	0.893	0.450	. 76	0.707	. 72	ŝ	15	0.422		0.396		065.0	90	0.396	ŝ	30	0.396	33				. 58	1.361	41	0.424		- 4-	707 0		0.672	- 16	1.585	
25	30。255 30。407		0.5	30.015	0.26	30.135	30.130	30.184	7	30.507	ð (	:	30.665 30.655	0 4 0 4	3	0.66	30.665	0.00	30.665	30.665	30-65	30.021	30.082	29.600		29.647	•		30.594		4 4	30.622	÷ 2 4	9.78	29.500	
Т. Ч. (М)		19.41	18.83	6	19.24	9.45	119.454	9.37	4 1 1	118 845	8-07		110-545			10.50	18.545	20.01	8.585	118.585	8.585	9-64	119.543	0.33	20.50	20.259	20.31	18.68	18.	18.76	8.88	18.656	19.28	20.03	.20.500	
Н.Ч.L. (М)	149.514 1 149.417 1	49.576	49.348		9.507	49.591	49.590	49 <b>.</b> 559	945.94	49.352	49.287		162.64	022-07	2	49.250 1	49.250 I	1 002.44	49.250	49.250	49.250	49.664	49.025	49 <b>.</b> 935	50.000 1	49*906 1	49.928 I	49°289 I	49.292 1	49.318 l	49.368	149.278	49.523	49.817	150-000 1	
			S.TDTAL DEC 1 1		DEC 3 1		JAN 2 1				-			• -	4	-	-	-	٦	-		JUN 1 1	-	-	-		-		-	-			-			
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HMX .	669840.	1074000. 1314240.	305806	1339680.	116028	3595080	01141	1705170.	396125		1560432.	373771	439680. A 10-40	48364	1363004. 230540	439684	39, 65	1319040.	80.64	549280	147864	87144	1209840	3152880.	70512	84792	2877264.	75848	141040	2507104	071606	1632000	0267920	1632000. 1280140.	14057	375321	33921206	
х х	2791.	5476.	•	5582. 4423	4395.	0.40		459		2000.	242.	•	1832.	1832.	6 5 0 1	1412.	132	( C )		2270.		3631.	5041.	+ + 0 7 *	2438.	3533. 5014	• 310 6	5327.	3476.		, 10G.	6800.		6800. 5336.	3184.			
I FF TCE .	0.472	568.0		0 895	0 892	a	6 9	0.840	2000	0.942	0.450		0.800	0.800	0.04.0	0.800	00+0	0.000	0.800	0.850		<u>ب</u>	0.895	•	0.872	0.862		0.842	0.882		0.850	0.863		0.855	.8.			
TVER F	0.0 			0.0	0.0	0.0		0.0			0.0	•		0 0	0.0	0.0	0.0	0 - 0		0.0		0 0			0.0	0.0			0.0	0		0.0	1 360	0.0	° 0°0			
T_DIS. (CM/S)		52.449		22.434 18.474	1.747	15, 494	10-844	21.208	6.211 1.6	12.472	0,245		8.000	8.000	8 - 000	8,000	8.000	0.000	8.000	9.304		14.668 20.200	20,503		11.898	[4.253 20.39]		13.305 13.366	14.010	16 300	10	29.273	c	21.817	÷.			
H7 A7 4 ]	5°044	6.817		PC1 - B2	9.359	543.0	9.010	28.203	0 77.4	9-745	169	2	~~	20	400	30.264	20			30.158	i	0,676 , 2,2			9.939	9.717 9.062		9.801 6.413	9 742	264.0	141-0	7.915	7 014	6.742 P.A94	9.858			
N	104.	050	0	0.812	772	679	95.2	10 1	400	203	0.428	101	90.106	340	. 346	0.396	.396	404	306	0.432	i	623	154-0		512	0.605 2		569 566	0.594 2	547	110	1.585 2	5 a 5	1.014 2	• 545			
РОSS.н (м)	•	9.6	2	20.09L	13	52.4	29.962	19		0.138	30.597	377 0	30.665	0.665	0.665	30.665	0.465	0.065	0.065	30.540		°¦ ′	006-02	4 6	0.45	0.922 9.936		7 2 0	0.336	5		29.507	d	9.908	•			
T.H.L.	8 ° 8	9.886	010	528	463	296	741		010.4	9 123	A. 697	202	585	585	. 585	8.585	.585	8.585	8.585	8.708		.186	111		d.936 0.110	9.701 2.		9.070 9.058		762.0	8.727	0.5.0	. 500	9. 429 2'	•016			
M.W.C. (M)	9°9	9.759 I		49.619 119.		528 1	49.703 11	.927	1 087.	49.461 11	.294 1	G	49-250 116	õ	250 1	49.250 11	250 1	20	.0	49.298 11			49.604 119.		9.387	9.687 11		49.435 11 49.435 11	462	1 905	305 1	8	0-000 1	9.737 11	9.419 I			
		14	-			1		٦			-	-	•	-	-	-	-		. –	-	•		•	•	4 - 1 -	4 4	• •		-	-		-	េះ		14		TOTAL	
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	·		נ		)		ر		-			)		С		2		5	)		Э		3	)		)		D		)		)		נ		2		

MURA FRA P/S         MURA FRA P/S         1000           MULL         TAUL         TAUL         TAUL         TAUL         TAUL         TAUL           MULL         TAUL         TAUL         TAUL         TAUL         TAUL         TAUL         TAUL           MULL         TAUL         T	3												1
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C       C			н ( м) ( м)	1.H.L [3]	GRUSS.H (M)	LUSSFS (M)	•••	T.DIS. (CM/S)	UCK F.	EFFICF.	X	Кин	,
C         C	)	NOV 1 NOV 2	149。674 149。975	19.0620.43	30 <b>.</b> 007 29.540	0.901 1.523	29.106	20.017	0.0	- 89 - 88	4 43 L. 6680.	1143440. 14032002	
0       0	Э	NDV 3 S.TOTAL	149.876	20.18	29.692	1.296	28.396	25.764	0°C	. я	6158.	1477920.	
C         C	)	DEC	6,4	20.25	- 0 - 0 - 0	.35	N	5.57	0.0	0.890	0327.	1518430.	
<ul> <li></li></ul>	c	DEC 3 DEC 3 S.TOTAL	64	19.81	66°	÷8	÷ °.	1.67		0.F83 0.895	6506. 5303.	1561440. 1399922.	ł
<ul> <li></li></ul>			64	20.24	- e -		2		0*0	0.850	6340.	4479912. 1521600.	
FINIX       Finix <td< th=""><th>2</th><th>JAN 2 JAN 3</th><th>- 0 - 4 - 4</th><th>19.92 20.34</th><th>o o</th><th></th><th>8.7 8.1</th><th>~ ~</th><th>0.0</th><th>0.895 0.883</th><th>5575. ¢478.</th><th>1338000. 1713192.</th><th></th></td<>	2	JAN 2 JAN 3	- 0 - 4 - 4	19.92 20.34	o o		8.7 8.1	~ ~	0.0	0.895 0.883	5575. ¢478.	1338000. 1713192.	
TFBS       149.450       119.070       00.192       79.770       11.703       0.00       0.882       100.1         STDTAL       149.450       119.070       00.192       79.770       11.716       0.00       128.2       111.20         STDTAL       149.450       119.070       00.192       0.318       00.314       0.318       0.0194       141.452         STDTAL       149.250       118.319       00.134       0.318       00.591       5.000       0.100       110.2       0.1172       141.452         STDTAL       149.250       118.319       00.131       0.318       00.591       5.000       0.000       111.2       141.452         STDTAL       149.250       118.319       00.311       0.0131       0.300       111.2       141.452         STDTAL       149.250       118.317       00.511       0.0131       0.000       111.2       141.453         STDTAL       149.250       118.413       00.511       0.0131       0.010       111.2       141.453         STDTAL       149.250       118.413       00.311       0.0131       0.010       111.2       141.453         STDTAL       149.250       118.413       00.511	2	S.TOTAL FEB L	_	119.402	• 1 ¢	7.57.0	- 7		0-0	0 - RH 4	4774	4564792	
0       5.7001       1.14.50       0.0101       0.0102       3.27.       2.31592         1.44.720       119.720       119.121       0.0131       0.0131       0.0131       0.0131       0.0147		FE8 2 5 20 3	49.451 20.223	119.099		U. 582	0.		0.0		1403	816723.	,
MAR 1       149-250       18-315       30.345       0.354       30.551       5.441       3.3       149-250       18-315       30.314       0.355       5.645       0.0       0.000       1124       27722         MAR 3       149-250       18-316       30.31       0.355       5.645       0.0       0.000       1114       27722         MAR 3       149-250       18.312       30.31       0.357       5.045       0.0       0.000       1114       27722         MAR 1       149-250       118.312       30.31       0.357       0.353       5.045       0.0       0.000       1141       24121         MAR 2       149-250       118.413       30.475       0.357       0.302       0.301       19.446       0.410       1144         MAR 2       149-250       118.413       30.747       0.346       30.727       5.602       0.0       0.000       1141       77440         MAR 2       149-250       118.413       30.747       0.346       30.727       5.602       0.0       0.000       1141       77440         MAR 2       149-250       118.47       30.747       0.346       30.747       0.346       30.741       119.750	)	S.TOTAL	0++•	010.411	-	696.0	ž –	<b>n</b> -	n•n	88.	-1327.	2315592。 4146552	
<ul> <li></li></ul>		HAR I MAC 2	49°2	18.35	30.845	16	5°0	144*5	0•0	0.800	1258.	101925. 101923.	•
<pre>     TOTAL     FPR 2     FPR 3     FPR 3     FPR 3     FPR 3     FPR 3     FPR 4     FPR 4</pre>	c	MAR 3	49.2	16.31	30, 931	2.2	 		0.0	0.800	1160	277920.	
<pre>C FFF 2 149-250 118-319 30-37 0-338 30-99 5-105 0-0 0-00 11012 201240 HAY 1 149-250 118-319 30-37 0-338 30-99 5-102 0-0 0-00 1191. 241400 HAY 1 149-250 118-319 30-37 0-348 30-52 5-102 0-0 0-00 1191. 241400 HAY 2 149-250 118-473 30-47 0-348 30-52 5-102 0-0 0-00 1191. 241720. HAY 2 149-250 118-473 30-47 0-348 30-52 5-102 0-0 0-00 1170. 241720. JUN 2 149-290 118-473 30-517 0-348 30-421 5-102 0-0 0-00 1170. 241720. JUN 2 149-290 118-473 30-517 0-348 30-421 5-102 0-0 0-00 1170. 11710. JUN 2 149-290 118-473 30-517 0-438 30-470 30-04 0-0 0-672 2-559. 0-31240. JUN 2 149-290 118-570 30-050 0-038 2-4228 18-945 0-0 0-090 2-326. 0-31770. JUN 2 149-290 118-567 30-019 0-019 9-633 0-0 0-090 2-326. 131740. JUL 1 149-280 118-567 30-010 0-018 2-428 18-945 0-0 0-080 2-759. 131740. JUL 1 149-280 118-567 30-102 0-018 2-429 18-944 0-0 0-080 2-075. 49700. JUL 2 149-280 118-567 30-105 0-091 2-418 30-197 0-0 0-080 2-259. 54710. JUL 2 149-280 118-567 30-105 0-901 2-418 30-197 2-000 0-080 2-259. 54710. JUL 2 149-280 118-961 30-192 2-102 2-0.047 0-0 0-080 2-259. 547100. JUL 2 149-280 118-941 30-401 0-114 29-194 11-973 0-080 2-259. 54710. JUL 2 149-280 118-941 30-401 0-114 29-194 11-973 0-00 0-080 2-259. 54710. JUL 2 149-280 118-941 30-401 0-114 29-194 11-973 0-00 0-0805 2-593. 130742. JUL 2 149-280 118-941 30-401 0-114 29-194 11-973 0-00 0-0805 2-593. 130742. JUL 2 149-280 118-941 30-401 0-114 29-194 11-973 0-00 0-0805 2-593. 130742. JUL 2 149-280 118-941 30-401 0-114 29-194 11-973 0-00 0-0472 2-951. 170740. JUL 2 149-280 118-941 30-401 0-114 29-194 11-973 0-00 0-0472 2-953. 170740. JUL 2 149-280 118-941 30-401 0-114 29-194 11-973 0-00 0-0472 2-953. 170740. JUL 2 149-280 118-941 30-401 0-114 29-194 11-973 0-00 0-0472 2-953. 170740. JUL 2 149-280 118-941 0-114 11-913 0-114 29-194 11-973 0-100 0-1072 2-953. 170740. JUL 2 149-280 118-981 29-041 0-114 29-194 11-973 0-100 0-1972 2-553. 170740. JUL 2 149-280 118-981 29-041 0-114 20-194 11-973 0-100 0-1972 2-553. 170740. JUL 2 149-240 119-914 0-114 0-114 0-114 0-1</pre>		5. TUTAL	36 07	CL 01	000 00	2							• *
APR 3       149.250       118.255       30.925       0.349       30.515       5.102       0.0       0.000       1111       73340         MAY 1       149.250       118.453       30.475       0.346       30.527       5.002       0.0       0.000       11750       11750         MAY 1       149.250       118.453       30.717       0.346       30.527       5.002       0.0       0.000       1319       11750         MAY 2       149.250       118.453       30.717       0.346       30.527       5.002       0.0       0.000       1319       11750         MAY 2       149.250       118.473       30.717       0.346       30.527       5.023       0.0       0.000       1319       11750         JUN 2       149.250       118.750       30.517       0.3463       30.1249       0.0       0.400       1314       131720         JUN 2       149.250       118.750       30.517       0.319       30.143       0.000       0.300       0.300       0.300       0.300       0.3134       0.3134         JUN 1       149.267       118.750       30.147       0.3193       0.00       0.400       1314       0.3146         J	ر	2 PR 2	49.25	18.31	30.931	n m m	30.593	5,045 5,045		• •	11/2	25	:
WAY 1       147.250       118.470       0.347       30.571       5.112       0.0       0.800       119.       11760.         WAY 2       149.250       118.475       30.475       0.346       30.577       5.662       0.0       0.800       139.       11760.         WAY 2       149.250       118.475       30.475       0.346       30.577       5.662       0.0       0.800       139.57         UNN 1       149.260       118.473       30.517       0.470       30.472       10.470       30.472       5.662       0.0       0.800       139.57         UNN 1       149.260       118.473       30.517       0.470       30.473       90.470       30.474       30.474       30.474       147.643       143.75       143.75       149.570       5.93.647       0.0       0.892       453.651       143.645       456.76       5.662       0.0       0.892       453.651       143.75       143.645       456.77       5.662       0.0       0.893       5.837       5.837       5.837       5.837       5.846.75       5.837       5.837       5.837       5.837       5.846.75       5.847.65       5.847.65       5.847.65       5.847.65       5.847.65       5.847.65       5.8		APR 3	49 <b>.</b> 25	18.32	30.925	33	30.5 Bh	5.102	0.0	0.000	1411	2+3440.	>
WAY 2       149.250       118.375       30.475       0.346       30.527       5.662       0.0       0.400       15.61       403372         WAY 3       149.250       118.473       30.747       0.346       30.421       6.638       0.0       0.400       15.61       403372         UNN 1       149.250       118.770       30.747       0.346       30.421       6.638       0.0       0.400       15.61       403372         UNN 2       149.630       118.770       30.517       0.470       30.139       9.643       0.0       0.490       133472         UNN 2       149.630       119.670       30.0617       0.418       30.113       9.643       0.0       0.490       133472         UN 1       1       149.264       119.643       30.0174       0.470       30.019       9.643       0.0       0.3922       46714       1121642         JUL 1       149.265       119.670       30.063       0.017       0.418       30.173       7.069       9.643       0.0       2055       46714       1121642         JUL 1       149.265       118.704       30.173       0.418       30.173       0.00       2075       46704 <t< th=""><th>C</th><th>PATUTAL</th><th>49.2</th><th>18.18</th><th>30.870</th><th>34</th><th>0.52</th><th>5,712</th><th>0-0</th><th>0.800</th><th></th><th>H45040. 212550</th><th></th></t<>	C	PATUTAL	49.2	18.18	30.870	34	0.52	5,712	0-0	0.800		H45040. 212550	
MAY 3       149.250       118.443       30.7131       0.3421       6.638       0.0       0.800       15/6.       403392.         JUN 1       149.347       118.424       30.577       0.470       30.471       0.0       0.472       2637.       0.33300.         JUN 2       1490.347       118.730       30.577       0.438       30.139       9.603       0.0       0.892       4571.       112.1347.         JUN 2       1490.250       119.577       30.617       0.418       30.139       9.603       0.0       0.892       4671.       112.1347.         JUL 1       1490.250       119.457       30.617       0.418       30.197       8.863       0.0       0.892       4671.       112.1347.         JUL 1       1490.250       119.457       30.617       0.418       30.177       7.069       0.0       0.892       4671.       112.1347.         JUL 2       1490.675       119.4670       30.177       7.069       0.00       0.892       467000.       487000.         JUL 3       1490.675       119.4703       30.177       7.0697       0.00       0.0950       217597.       217597.         JUL 3       1490.675       119.4703	)	MAY 2	49.2	18.37	30.475	1	0.52	5.062	0.0	0.800	1305.	13720. J13720.	2
JUN I       149-343       110.824       30.517       0.470       30.449       10.648       0.0       0.572       2637       133300         JUN Z       149-367       116.730       30.577       0.470       30.139       9.603       0.0       0.350       558240         JUN Z       149-530       110.570       30.577       0.438       30.1139       9.603       0.392       4671       112.1043         S-107AL       149-250       119.670       30.617       0.418       30.1137       7.069       0.0       0.3972       4671       112.1043         JUL Z       149-250       119.670       30.617       0.418       30.1137       7.069       0.0       0.3972       4671       112.1043         JUL Z       149-250       119.670       30.617       0.418       30.173       7.069       0.0       0.3972       4671       3103640         JUL Z       149.250       119.670       30.743       30.7162       20.007       0.0       215492       54.150         JUL Z       149.250       119.670       30.743       30.7452       0.0       0.00       219740       215470         JUL Z       149.250       118.641       30.462	ç	МАҮ 3 с.тота)	4 <b>9</b> •2	18.46	30,747	36	0.42	6.638	0.0	0.800	15/8.	403342.	
JUN 2       149.307       118.730       30.577       0.438       30.139       9.603       0.0       0.890       2326.       558240.         JUL 1       149.250       119.570       30.617       0.418       30.139       9.603       0.0       0.892       4071.       11216443.         JUL 1       149.250       118.653       30.617       0.418       30.173       7.069       9.03       4403       10.7       2175462.       446003.         JUL 2       149.250       118.502       30.617       0.418       30.173       7.069       9.03       29.102.       10.416.       10.75.       446003.         JUL 2       149.250       118.670       30.052       0.903       29.102       20.047       0.0       0.809       10.75.       457150.         JUL 2       149.256       118.704       30.505       0.903       29.264       8.000       0.1932.       547150.       275470.         JUL 3       149.256       118.585       30.505       0.356       30.264       8.000       0.1375       27916.       547150.       275470.       275470.       275470.       275470.       275470.       275470.       275470.       275470.       275470.       275470.	)		49.3	18.82	30.519	0.470	40.0	ം	0.0	0.672	2639.	[]33672° 533360.	2
S-107AL JUL 1 [49-250 [18.663 30.617 0.418 30.199 8.863 0.0 0.800 2075, 486000, JUL 2 [49-250 [18.502 30.448 0.375 30.173 7.069 0.0 0.800 1024, 98765, JUL 2 [49-250 [18.502 30.468 0.375 30.173 7.069 0.0 0.895 4.934, 1303632, JUL 3 [49-250 [18.567 30.093 294102 20.047 0.0 0.895 4.934, 1303632, AUG 1 [49-250 [18.585 30.465 0.396 29.269 8.000 0.0 0.893 4.934, 1307632, AUG 3 [50:000 [20:500 29.500 [1585 27:915 29.273 1.357 0.893 6.800, 1795,00, AUG 3 [50:000 [20:500 29.500 [1585 27:915 29.273 1.357 0.893 6.800, 1795,00, AUG 3 [50:000 [20:500 29.500 [1585 27:915 29.273 1.357 0.893 6.800, 1795,00, AUG 3 [50:000 [20:500 29.500 [1585 27:915 29.273 1.357 0.893 6.800, 1795,00, AUG 3 [50:000 [20:500 29.500 [1585 27:915 29.273 1.357 0.893 6.800, 1795,00, AUG 3 [19.611 30.094 0.805 29.294 11.473 0.0 0.472 2941, 777764 SEP 3 [49:443 30.094 0.552 29.4442 12.975 0.0 0.0 0.472 2941, 777764, SEP 3 [49:443 30.394 0.552 29.4442 12.975 0.0 0.0 0.472 2951, 104792, SEP 3 [49:443 30.394 0.552 29.4442 12.975 0.0 0.0 0.472 2951, 104792, SEP 3 [49:443 30.394 0.552 29.4442 12.975 0.0 0.0 0.472 2951, 104792, SEP 3 [49:443 30.394 0.552 29.4442 12.975 0.0 0.0 0.492 4.553, 104792, SEP 3 [49:443 119.631 30.394 0.552 29.4442 12.975 0.0 0.0 0.492 4.553, 104792, SEP 3 [49:443 119.631 30.394 0.552 29.4442 12.975 0.0 0.0 0.495 4.652, 1157440, SEP 3 [49:443 119.455 1.90,114 0.4771 30.377 1.4071, 0.0 0.492 4.573 1.57440, SEP 3 [49:455 119.656 29.455 1.0,114 0.4771 30.377 1.4071, 0.0 0.492 4.573 1.57440, SEP 3 [49:455 119.656 29.451 0.4711 0.5140 0.0 0.0 0.492 4.573 1.57440, SEP 4 [19:656 20,114 0.556 20,114 0.5744 0.0 0.0 0.0 0.495 4.672, 115440, SEP 4 [19:656 20,114 0.556 20,114 0.5344 0.0 0.0 0.00 0.00 0.00 0.00 0.00 0.0	C	2 NUL E NUL	9 64 64	18.73 19.57	30.577 30.066	0.433	0.L3 9.23	• •	n.0	048.0	2326.	558240. 1121063	
ULL       149.250       119.675       30.749       0.375       30.177       9.665       0.375       30.177       9.665       0.375       30.177       9.665       0.3165       130762       466000         ULL       149.675       119.670       30.076       0.903       29.102       20.047       0.0       0.895       491761         AUG       1       149.675       119.670       30.065       0.903       29.102       20.047       0.0       0.895       4130752         AUG       1       149.256       118.704       30.592       0.430       30.162       9.316       0.0       0.0800       1003762       54/150         AUG       2       149.250       118.585       30.043       0.305       9.0162       9.010       0.0800       1003762         AUG       2       149.250       118.585       30.0443       0.0       0.0800       1432       54/150         AUG       2       150.0000       120.5500       29.590       11.453       0.0792       20.9440       7696443         AUG       2       149.4615       119.611       30.0443       0.0       0.0472       29543       769745         SFP       149.4615 <th></th> <th>S. TOTAL</th> <th>5 07</th> <th></th> <th>617 QE</th> <th></th> <th></th> <th></th> <th></th> <th></th> <th></th> <th>2312640.</th> <th>)</th>		S. TOTAL	5 07		617 QE							2312640.	)
UL 3 149-675 119-670 30.005 0.903 29-102 20.047 0.0 0.895 4/34. S.TOTAL 149-296 118-704 30-592 0.430 30-162 9.316 9.0 0.450 2259. AUG 2 149-250 118-585 30.465 0.396 30.269 8.000 0.0 0.490 1432. AUG 3 150-000 120.500 29.500 1.585 27.915 29.273 1.357 0.893 6400. S.TOTAL 149-389 118-941 30.443 0.514 29.934 11.953 0.0 0.472 2951. SEP 2 149.615 119.517 30.094 0.605 29.293 18.346 0.0 0.472 2533. S.TOTAL 149-389 118.941 30.443 0.552 29.4442 12.955 0.0 0.472 2533. S.TOTAL 149.426 119.031 30.394 0.552 29.4442 12.955 0.0 0.472 2533. S.TOTAL 149.426 119.031 30.394 0.552 29.4442 12.955 0.0 0.472 2533. S.TOTAL 149.428 119.631 30.394 0.552 29.4442 12.955 0.0 0.472 2533. S.TOTAL 149.428 119.631 30.394 0.552 29.4442 12.955 0.0 0.472 2533. S.TOTAL 149.428 119.631 30.394 0.552 29.4442 12.955 0.0 0.472 2533. S.TOTAL 149.428 119.631 30.394 0.552 29.4442 12.955 0.0 0.495 2525. S.TOTAL 149.428 119.631 30.394 0.552 29.4442 12.955 0.0 0.495 2555. S.TOTAL 149.428 119.631 30.394 0.552 29.4442 12.955 0.0 0.0 0.495 2555. S.TOTAL 149.428 119.651 30.314 0.5719 23.255 0.0 0.0 0.495 2555. S.TOTAL 149.428 119.651 30.314 0.5719 23.255 0.0 0.0 0.495 2555. S.TOTAL 149.428 119.651 30.314 0.5719 23.255 0.0 0.0 0.495 2555. S.TOTAL 249.428 119.651 30.414 0.771 20.0555 0.0 0.0 0.495 2555. S.TOTAL 249.455 119.051 30.314 0.771 20.555 0.0 0.0 0.495 2555. S.TOTAL 249.455 119.651 30.414 0.771 20.555 0.0 0.0 0.495 2555. S.TOTAL 249.455 119.655 30.451 0.555 0.555 0.555 0.0 0.0 0.495 0.555 0	2		49.2	18.50	30. 148	31	• •	7.069		0.800		4 8 6 0 0 0 <b>.</b> 5 8 7 7 6 <b>) .</b>	
O       AUG I       149.295       118.704       30.592       0.430       30.162       9.316       0.3       0.450       2259.         AUG Z       149.250       118.585       30.465       0.396       30.269       8.000       0.0       0.403       2490.         AUG Z       150.000       120.500       29.500       1.585       27.915       29.273       1.357       0.803       6400.         AUG S       150.000       120.500       29.500       1.585       27.915       29.273       1.357       0.893       6400.         AUG SEP I       149.389       118.941       30.443       0.514       29.434       11.473       0.0       0.472       2941.         ASEP 2       149.615       119.9517       30.394       0.552       29.4442       12.9456       0.0       0.0       0.472       2953.         ASEP 2       149.4261       119.031       30.394       0.552       29.4442       12.9456       0.0       0.472       2953.         ASEP 3       1449.428       119.031       30.394       0.552       29.4442       12.9455       0.0       0.472       2953.         ASEP 3       1449.428       119.031       30.344 <t< th=""><th></th><th>JUL 3 S.TOTAL</th><th>44°D</th><th>19.6/</th><th>3005</th><th>6</th><th>-</th><th>20.047</th><th>0.0</th><th>C-845</th><th>ם אולו א</th><th>1303632. 3576303</th><th></th></t<>		JUL 3 S.TOTAL	44°D	19.6/	3005	6	-	20.047	0.0	C-845	ם אולו א	1303632. 3576303	
AUG 2       149.629       30.605       0.396       30.269       8.000       0.0       0.400       1432.         AUG 3       150.000       120.500       29.500       1.545       27.915       29.273       1.357       0.493       6400.         SFP11       149.389       118.941       30.443       0.514       29.934       11.453       0.0       0.472       2941.         SEP 1       149.489       118.941       30.443       0.514       29.934       11.453       0.0       0.472       2941.         SEP 2       149.615       119.517       30.034       0.552       29.4442       12.955       0.0       0.472       2753.         SEP 3       149.4755       119.031       30.334       0.552       29.4442       12.955       9.273       10.922       29.253.         STOPA       30.349       0.552       29.4442       12.955       9.29.33.       4537.       4547.       4547. <th>С</th> <th></th> <th>49.2</th> <th>18.70</th> <th>ം</th> <th>4</th> <th></th> <th>٠</th> <th>0°0</th> <th>• 45</th> <th>2259.</th> <th>542150.</th> <th>F J</th>	С		49.2	18.70	ം	4		٠	0°0	• 45	2259.	542150.	F J
<ul> <li>S.TOTAL</li> <li>S.TOTAL</li> <li>S.FP L</li> <li>I.49-389</li> <li>I.8-340</li> <li>0.443</li> <li>0.514</li> <li>29,934</li> <li>I.453</li> <li>0.0</li> <li>0.472</li> <li>2941.</li> <li>SEP 2</li> <li>149.615</li> <li>119.517</li> <li>0.00</li> <li>0.605</li> <li>29,434</li> <li>18.346</li> <li>0.0</li> <li>0.472</li> <li>29,517</li> <li>0.615</li> <li>29,434</li> <li>119.517</li> <li>0.036</li> <li>0.605</li> <li>29,434</li> <li>119.615</li> <li>119.611</li> <li>0.552</li> <li>29,442</li> <li>119.631</li> <li>30,394</li> <li>0.552</li> <li>29,442</li> <li>12,955</li> <li>0.0</li> <li0.0< li=""> <li>0.0</li> <li>0.0</li> <li>0.0</li></li0.0<></ul>		AUG 3	50.0	20.50	ာင်	÷3	N P		<u>د</u>	.80 .89	1432. c800.	434480. 179520J.	age
SEP 2     149.615     119.517     30.094     0.805     29.243     18.346     0.0     0.802     45.33       C SEP 3     149.475     119.031     30.394     0.552     29.4442     12.955     0.0     0.802     45.33       C SEP 3     149.475     119.031     30.394     0.552     29.4442     12.955     0.0     0.802     45.355       OCT 1     149.493     119.453     30.114     0.177     23.254     0.0     0.495     457.5       O     0CT 1     149.492     119.453     30.114     0.177     23.264     17.472     0.0     0.495       O     0CT 1     149.492     110.4653     30.114     0.177     23.264     17.472     0.0     0.495       O     0CT 2     149.494     110.4653     30.114     0.177     23.264     17.472     0.0     0.495	כ	S.TOTAL SEP 1	49	94 °E	30.443	3	6°6	_	0-0	0.472	7461	277704C。 764240	ix 2 2
S.TOTAL         S.TOTAL <t< th=""><th>-</th><th>SEP 2</th><th>40.4</th><th>9.51</th><th>30.094</th><th>1084</th><th></th><th>1.00 10</th><th></th><th>0.992</th><th>4523</th><th></th><th>4<u>8</u>.</th></t<>	-	SEP 2	40.4	9.51	30.094	1084		1.00 10		0.992	4523		4 <u>8</u> .
(11.1 149-592 119-458 30,134 0.1710 21.14 17.0.2 0.0 0.492 4572 11.1 11.1 149-458 30,134 0.471 30,364 17.0.2 0.0 0.492 4572 11.1 10.1 10.0 0.471 30,347 130,347 130,347 130,347 130,0 0.472 4547	)	S. TOTAL	0 7			: :					• • • • • • •	-cato242	- <u>10</u>
	)	1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	- 0 7 - 4	19.45 18.87				10. 11. 11.			~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	1 5 5 5 4 4 0 <b>.</b> 1 5 4 1 6 4 0 <b>.</b>	ا ر
	)	5. TUTAL			•								)

, , , , starility Forecast of the Selected Major Crops

# . Method of Forecasing

Paddy rice, garlic and mungbean together with virginia tobacco and cotton have been selected as the major crops in the Project. In order to analyze their demand-supply balance at the three levels of the whole country, Ilocos region and Ilocos Norte province during erroreried of 1975 to 1979, the demand of these crops has been estirated base on the NEDA data on the projected population and food erroumption per capita whereas the supply capacity estimation has been rade hased on the production data of BAEcon and the other government agencies.

The data of the projected population applied in forecasting are

#### Projected Population

				( 0)	nit: '(	000)
Year	Whe	ole Country	Ilocos Regio	on <u>Ilocos</u>	Norte	Province
1375		42,517	3,310		371	
1376		43,841	3,374		380	
1977		45,165	3,438		389	
1978		45,500	3,499		397	
1979		46,700	3,565		405	
1980		49,137	3,631		414	
1990		65,041	4,445		497	
	Source:	Population	Dimension of	Planning,	NEDA,	1975

(Medium Assumption)

To compute the demand of the selected major crops in from 1975 to -379 and 1990, the food consumption per capita shown in the following table has been applied in the computation.

#### Consumption per Capita

		ilippin		Iloco	s Regio	n
Crop	1975-1979	<u>1/</u> 1.Q.E.	$\frac{2}{1990}\frac{3}{}$	1975-1979	<u>1/</u> _I.Q.E.	$\frac{2}{1990^{3/}}$
Rice & rice product Garlic Mungbean	106.1kg 0.4 1.3	0.13% 0.48 0.48	112.9kg 6.5 1.6	133.8kg 0.3 1.8	0.02% 0.23 0.34	135.1kg 0.4 2.1

Note: 1/ The data on the consumption per capita for the year from 1974 to 1976 in "the Regional Consumption Pattern for Major Foods" prepared by DA in 1976.

2/ Income-quantity elasticity in the report mentioned in 1/

3/ Forecast from the assumed income increase rate at 50% From 1974-1976 to 1990, applysing the above-mentioned I.Q.E.

### B. Forecast of Marketability

#### 1. Rice

The Philippines was an importer of rice for a long time although some surplus of rice was recorded in 1979 (See Table 4C-1) It is presumed that the average rice consumption per capita will continuously increase in future, too, juding from the small average consumption per capita at present as well as from the fact that reportedly about 20 percent of the total popultaion lives on corn.

The Five-year Development Plan of the Government indicates that the total demand for rice in the year 1990 will increase to 140 percent of that as of 1978. This estimate has been made based on such a small consumption per capita as about 95 kg. Therefore, it is well anticipated that the actual demand for paddy rice will be more than the above-estimated in 1990.

In 1979 rice equivalent to 20 percent of the total demand in Ilocos region was short. The demand for rice in the region as of 1990 is forecast at 604 thousand tons. To meet the above-mentioned demand, the yield per unit area of paddy should increase to 3.1 ton/ ha if the paddy cropping area is not expanded. In fact, the paddy cropping area in the region has not been expanded these 10 years:

							1
It	Item	1975	1976	Actual 1977	1978	1979	forecasted 1990
Philippines	Supply (Paddy)	5,660.0	6,159.5	6,456.l	6,894.9	7,199.0	1
	(Rice)	3,396.0	3,695.7	3,873.7	4,136.9	4,319.4	<i>*7</i> ,329
	Demand (Rice)	4,506.0	4,647.0	4,787.0	4,140.0	4,260.0	*5,766
	Balance (Rice)	(-)1,110.0	(-)951.0	(-)913.0	(-)3.0	59.0	*1,563
Ferion I	Supply (Paddy)	422.0	577.5	511.0	575.8	638:7	ł
	(Rice)	253.2	346.5	306.6	345.5	383.2	ł
	Demand (Rice)	443,5	452.1	460.7	468.9	477.7	596
	Balance (Rice)	(-)190.3	(-)105.6	T.#31(-)	(-)123.4	(-)94.5	I
Ilocos Norte	Supply (Paddy)	50.9	72.4	83.6	83.3	92.4	I
	(Rice)	30.5	43.4	50.2	50.0	55.4	I
	Demand (Rice)	49.7	50.9	52.1	53.2	54.3	67
	Balance (Rice)	(-) 19.2	(-) 7.5	(-) 1.9	(-) 3.2	(-) 1.1	I

-

Source; Supply ---- BAEcon \* ------- Five-year Philippine Development Plan (1978-1982) Note: Conversion rate from paddy to rice : 60%

Appendix 4C-1 Page 3

On the countrary, it is the tendency that the paddy cropping area is decreasing in the region recently. It might be difficult to increase in a short time the present yield per unit area to the above-mentioned 3.1 ton/ha. Under the situations, Ilocos region will remain as one of the rice digicit area in the year of 1990.

Ilocos Norte province recorded some surplus production of rice in 1979, however, the production trend indicates that the production in the province has a great yearly variation.

The demand for rice in the province as of 1990 has been forecast at 67 thousand tons. To meet the forecast demand plus the buffer stock equivalent to 15 percent of this forecast demand, the target production of rice in 1990 should be set up at 77 thousand tons, which is converted to the unhulled rice of 130 thousand tons. This volume of unhulled rice is equivalent to 150% of the averaged production in the province during the three year-period from 1977 to 1979. (The difference between the forecasted demand for the year of 1990 and the said present production is some 44 thousand tons.)

At least an area of about 10 thousand hectares of paddy harvesting area would be newly developed under on-going irrigation projects inclusive this Project. Under the situations, the above-mentioned target could be easily achieved if the yield per unit area slightly increases.

#### 2. Virginia Tobacco

É,

PVTA data shows that the average production of virginia tobacco at the whole country level was about 42 thousand tons during 1975 to 1978. Out of this production, about 10 thousand tons were exported as one of the major export goods obtaining foreign currencies. In the Five-year Development Plan of the Government the annual increase rate of virginia tobacco production is projected at 2.4 percent during 1978 to 1987. Inocos region and Ilocos Norte province produced virginia tobacco quive ent to 94% and 10% of the national production in 1977, respectively. The Presidential Degree on the zonification of virginia + paceo production area suggests that the cropping area of virginia to.a.c will be continueously concentrated to Ilocos region.

The virginia tobacco production in the Project Area could increase at least up to 130 percent of the total production as of 1978 if 2.4 percent of annual increase rate is applied.

#### 3. Gariic

The BAEcon data indicate that the garlic production in Ilocos ...glon maintained its share of more than 75 percent of the total roduction in the whole country for the past ten years from 1970 to ...79. Garlic production area in the region concentrates in the Project Area and its neighborhood.

At the national level, the domestic demand of garlic in each of the last five years appears larger than the supply capacity as shown in the following table.

					(Unit	thousa:	nd ton)
				Actual			Forecasted
Item		1975	1976	1977	1978	1979	1990
Pilippines	Supply Demand Balance	16.0 17.0 (-)1.0	15.2 17.5 (-)2.3	16.0 18.1 (-)2.1	16.8 18.2 (-)1.4	14.0 18.7	32.0
tigion I	Supply Demand Balance	11.8 1.0 10.8	11.9 1.0 10.9	12.4 1.0 11.4	13.6 1.0 12.6	9.6 1.1 8.5	1.8
llocos Norte	Supply Demand Balance	9.9 0.1 9.8	10.0 0.1 9.9	10.5 0.1 10.4	11.5 0.1 11.4	7.4 0.1 7.3	0.2

Table 4C-2 Demand and Supply Balance, Garlic

Source: Supply---BAEcon

However, the "Garlic Projection and Marketing, Ilocos Region" prepared by DA in 1978 suggests that the Philippines has been an exporter of garlic these years, specially in 1978. A considerably large amount of demand than the supply capacity as previously described may be derived from the underestimate of the garlic production in the production data.

The demand of garlic at national level for the year of 1990 is forecast as much as 32 thousand tons, which corresponds to about 176 percent of the total demand in 1978. The production target in the Project Area for the year 1990 could be set up at 176 percent of the total production in 1978 since the marketing share of garlic in the Project Area will be easily maintained, at least, at present level.

#### 4. Mungbean

A marked increase of mungbean production in the whole country has been registered since 1973 according to the BAEcon production data. The production share of mungbean in Ilocos region was expanded to a great extent from seven percent in 1973 to 45 percent in 1977 due to the increase of harvested area by five times. This sharp increase in mungbean production of the region made almost 100 percent contribution to the nation-wide increase of this crop during the said period.

The mungbean production data in the Ilocos Norte province also show a moderately large increase in production and harvested area as well since 1973. The harvested area was expanded in 1979 to 1.9 times of that in 1973 whereas the production in 1979 increased only to 1.4 times of that in 1973. That is, the increse of production per unit area is not observed during the period.

As seen in the following table 4C-3, a tremendous amount of deficit is found in the demant-supply balance of mungbean at the national level.

(Unit: thousand ton)

					• • • • • •		
			_	Actual			Forecasted
Item	<u></u>	1975	1976	1977	1978	1979	1990
philincines	Supply	21.7	24.4	25.3	26.2	29.0	
-	Demand	55.3	57.0	58.7	59.2	60.7	104.1
	Balance(-	)33.6	(-)32.6	(-)33.4	(-)33.0	(-)31.7	
Region I	Supply	6.0	10.8	11.3	N.A.	N.A.	
	Demand	6.0	6.1	6.2	6.3	6.4	9.3
	Balance	0.0	4.7	5.1	N.A.	N.A.	
Ilocos Norte	Supply	0.8	0.9	0.9	1.0	1.0	
	Demand	0.7	0.7	0.7	0.7	0.7	1.0
	Balance	0.1	0.2	0.2	0.3	0.3	

Table 4C-3 Demand and Supply Balance, Mungbean

Source; Supply --- BAEcon

The "Commodity Situation Report, Mungbean" prepared by BAEcon in 1979 indicates that the Philippines'imported mungbean of about 9 thrusand tons during the 10 years from 1967 to 1976 whereas the country exported the product of less than one thousand tons during the same period. The report recommends to export mungbean since it is free from tariff duties.

Its production target to meet the forecast demand in the year 1990 at the national level should be set up so much as 3.9 times of it tital production in 1978. In this connection, the production in the Project Area could be at least as much as to 3.9 times of the production in 1978.

#### 5. Cotton

Philippine Cotton Cooperation (PCC) is responsible for the Development of cotton production in this country. The "National Option Production Development Program, 1979 to 1987" prepared by this organization aims to attain the self-sufficiency of cotton by 1987. The target production for this purpose is 138 thousand tons. The said program also suggests that some 146 thousand hectares are

Appendix . Page 9

identified as potential cotton production area, of which 32 thousand hectares (22 per cent of the total) and 4 thousand hectares (two %) belong to Ilocos region and Ilocos Norte province, respectively. For the identified area in Ilocos Norte, three thousand hectares are assumed to be located in paddy fields. Then, the potential cotton area in the Ptoject Area is estimated at 1.3 thousand hectares based on the proportion of paddy field area in the Project Area to the total paddy field area in Ilocos Norte province.

							(Unit:ha)	ha J	
Cropping Pattern (Wet Season + Dry Season)	Cura	Nueve Era	Sub-total	Madupayas	Batac- Paoay	Pinili	Badoc- Sinait	Sub-total	Total
l Paddy + Paddy	1,270	600	1,870	60	2,130	80	830	3,100	4,970
2 Paddy + Upland Crops									
<pre>(1) Paddy + Tobacco</pre>	40	30	70	80	1,150	280	550	2,060	2,130
(2) Paddy + Garlic	100	0 11	140	I	700	450	915	2,065	2,205
(3) Paddy + Garlic + Mungbean	ans -	I	ł	I	700	450	915	2,605	2,065
(4) Paddy + Cotton	ł	i	ı	20	510	140	360	1,030	1,030 1,030
(Sub-total)	(140)	(10)	(510)	Ū	(100) (3,060)	(1,320)	(2,740)	(1,220)	(7,220)(7,430)
Total (Physical Area)	1,410	670	2,080	160	2,190	1,400	3,570	10,320 12,400	12,400
(Cropping Area)	2,820	1,340	4,160	320	11,080	3,250	8,055	23,245	26,865
Cropping Intensity (%)	200	200	200	200	213	232	226	225	217

Tuble 4C-4. "Nouting Acta by Cropping Patters, Sub-project Mrs. (With Project, In Future)

# Result of Field Survey on Farmers' Intension for Improvement of Farm Management

#### A. Purpose and Method of the Survey

The prupose of the survey is to know the needs of irrigation project for farm management in the Project Area and the field survey by interviewing some 70 sample farmers was made with prepared questionary in the Project Area, exclusive of Cura and Nueva Era Sub-project Areas from 18th to 28th, January, 1980.

The selected sample Barangays and sample farmers were, as a general rule, the same as those of the Farm Management Survey conducted by NIA in 1978. But some interviewees were unavoidably different from there of the NIA survey. The sample Barangays and number of farmers by Barangays are listed as follows;

No.	Municipality	Barangay	Nos. of Sample Farmers
l	Batac	San Pedro	9
2	Paoay	Cabaguan	7
3	Paoay	San Roque	5
4	Paoay	Sideg	3
5	Paoay	Bacsil	3
6	Pinili	Dart	5
7	Pinili	Puritac	6
8	Pinili	Tartarabang	9
9	Badoc	Ar-arusip (A)	6
10	Sinait	Battog	4
11	Sinait	Duy-yayat	7
12	Sinait	Barikir	6
Total			70

### Sample Barangays and Nos. of Sample Farmers

# 3. Result of Survey

Farmers' responses to each question in the questionary are tabulated in Table 4C-5. Based on the Table 4C-5, farmers' intention for the improvement of their farm management and also the recessity of irrigation project are summarized as follows;

# . (utline of Farm Management of Sample Farmers

Average farm size per farm household is 1.2 hectares, including introduces of paddy field and 0.1 hectare of upland field. Out of introduces os paddy field, 0.2 hectares are irrigated by Communal irrigation Systems and the remaining 0.9 hectares are rainfed. As for land tenure of the cultivated land, each half of 1.2 hectares i paned and tenanted.

The average cropping area by crops per farm household in this curve? are as follows;

Cropping Area by Crop per Farm Household

<u>Cro;</u>	Area (ha)	Percentage (%)
Paddy (Wet season)	1.1	52.4
Tollacco	0.3	14.3
Garlie	0.4	19.0
Mungo	0.1	4.8
Corn	0.1	4.8
Others	0.1	4.7
<u>Iotal</u>	2.1	100.0

 $\mathbb{T}^{t_{\rm of}}$  main cropping pattern by each sample farmer is shown as  $fo_{\rm lows};$ 

# Main Cropping Pattern of Sample Farmers

	<u>C</u> 1	ropj	bing Pattern	Nos. of Farmers	Percentage
1.	Pá	addy	/ (P) only	3	(%)
2.	Ρ	t	Tobacco (T)	3	4.3
3.	Ρ	+	Garlic (G)	13	18.6
4.	₽	+	Corn (C)	1	1.4
5.	Ρ	+	T / G	17	24.4
6.	Ρ	+	T / G	1	1.4
7.	Ρ	+	T / Mung Bean (M)	1	1.4
8.	Ρ	+	G / M	4	5.7
9.	Ρ	+	G / O	1	1.4
10.	Ρ	+	G / C	3	4.3
11.	Р	+	М / С	1	1.4
12.	Ρ	+	Т/С/М	1	1.4
13.	Ρ	+	Т/G/С	9	12.9
14.	Р	+	Τ/G/Ο	3	4.3
15.	Р	+	Т / М / С	1	1.4
16.	Ρ	+	G / M / C	1	1.4
17.	Ρ	+	Τ/G/C/Ο	6	8.6
18.	Ρ	+	Т/G/М/С/О	1	1.4
		-	fotal	70	100.0

# 2. Major Source of Family Income in Future

All of sample farmers responded that they would continue their present farm management in future as well and the major source of their family income would come from their farm mamangement.

# 3. Present Irrigation Condition

Seventy-seven percent of interviewees can not have enough irrigation water, especially during the dry season.

# . If oding Damages in Past Five Years

Sixty percent of sample farmers have been suffered from flood damages two or three times on an average within past five years. imong the flood damages, the biggest damage experienced was such damage do scale of 0.3 hectares in the area with 1.7 meters flood intr and 3.3 days in duration.

#### -. Main Cropping Pattern in Future

Seventy-eight percent of sample farmers chose the cropping tattern of three croppings a year, for example, "Paddy + Garlic + "ung Bean", as the main cropping if they can have enough irrigation water throughout the year.

On the other hand, thirty two percent of sample farmers responded that they would choose such cropping pattern as "Paddy + Paddy" or "Faddy + Tobacco or Garlic + Paddy", both of which have two croppings of paddy. It may be one of the reason why so many farmers as thirty two percent of interviewees desire to plant paddy twice a year that trose farmers want to increase rice production because their rice rodu tion is limitted under small farm size at present. Table 4C-5. Farmers' Response to Questionary

1. General Information       1-1. Cultivated area: - Pady land, Owned ha 36.6       0.5         on Their Farm Management       - Upland, Owned ha 6.6       0.1         1-2. Irruigated area by: - Wet season       ha 12.6       0.2         1-3. Irruigated area by: - Wet season       ha 12.6       0.2         1-3. Irruigated area by: - Wet season       ha 12.6       0.2         1-3. Irruigated area by: - Wet season       ha 12.6       0.2         1-4. Pumps       - Dry season       ha 51.8       0.1         1-4. Pumps       - Pady, Wet       ha 29.0       0.4         1-4. Planted area by: - Paddy, Wet       ha 19.4       0.3         1-4. Planted area by: - Protecco       ha 19.4       0.1         1-4. Planted area by: - Protecco       ha 19.4       0.1         1-4. Planted area by: - Protecco       ha 19.4       0.1         1-4. Planted area by: - Protecco       ha 19.4       0.1         1-4. Planted area by: - Paddy, Wet       ha 19.4       0.1         1-4. Planted area by: - Protecco       ha 19.4       0.1         1-4. Planted area by: - Protecco       ha 19.4       0.1         1-4. Planted area by: - Paddy, Wet       ha 29.0       0.1         1-4. Planted area by: - Paddy for       ha 29.6       0.1 </th <th>Main Item</th> <th>Sub-Item</th> <th>Unit</th> <th>Total</th> <th>Per Farm Household</th>	Main Item	Sub-Item	Unit	Total	Per Farm Household
Irrigated area by: - Wet season Communal irri.systems - Dry season Pumps - Wet season Pumps - Wet season Pumps - Dry season Planted area by: - Paddy, Wet - Dry season Planted area by: - Paddy, Dry - Paddy - Paddy, Dry - Paddy - P		- Paddy land, - Upland,	ted	36.6 43.5 6.6 3.4	0.000
Irrigated area by: - Wet season ha - Pumps - Dry season ha 51.8 Planted area by: - Paddy, Wet ha 80.1 crop - Paddy, Dry ha 19.4 - Tobacco ha 19.4 - Garlic ha 29.0 - Mungo ha 4.8 - Corn ha 11.1 - Others ha 2.5 Total Nos. of family members 420 Nos. of farm lavor within family 200		- Wet ems - Dry	ha ha	12.6 -	0.2
Planted area by: - Paddy, Wet ha 80.1 crop - Paddy, Dry ha 80.1 - Tobacco ha 19.4 - Garlic ha 29.0 - Mungo ha 4.8 - Corn ha 11.1 - Corn ha 11.1 - Corn ha 2.5 Total ha 2.5 Total Nos. of family members 420 Nos. of farm lavor within family 200		1-1	ha ha	- 51.8	- 0.7
- Others ha 2.5 Total Total ha <u>146.9</u> Nos. of family members 420 Nos. of farm lavor within family 200		ced area by:	н н н н н н н н н н н н н н н н н н н	80.1 19.4 1.8 1.1	
Nos. of family members Nos. of farm lavor within family 200			ha ha	2.5 146.9	0.1 2.1
Nos. of farm lavor within family		. of family members		420	6.0
		. of farm lavor within family		200	2.9

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Main ltem		Sub-ltem		Unit	lotal	Percent
II. Source of Farmily Income in Future	II-1.	To continue farm management in future	; - Farm income only n - Farm income + Others - Others/No r-sonse		0 7 8	60 0
	II-2.	To stop farm management in future			0	0
	II-3.	No response/other reply			0	σ
III. Present Irrigation	III-l.	Sufficient			16	23
Condition (Availability of Irrigation Water)	<b>III-2.</b>	Deficient	<ul> <li>In both wet &amp; dry season</li> <li>In wet season only</li> <li>In dry season only</li> </ul>	Pason	ფიფ ₽	6 C 8 9
	III-3.	No response/other reply			0	o
IV. Flooding Damages	IV-1.	Not suffered			28	011
in Past Five Years	IV-2.	Suffered	•••		42	60
			- Nos. of times	time	0 1 1	
			- Damaged area	вh	0.3	
			<pre>/Diggest itous) / Flood depth</pre>	E	1.7	
			(biggest flood) - Flood duration	day	ຕ <b>.</b> ຕ	
			(biggest flood)		-	

TARE 50 . A DECRET PERSON FOR THE DATE (CONTER)

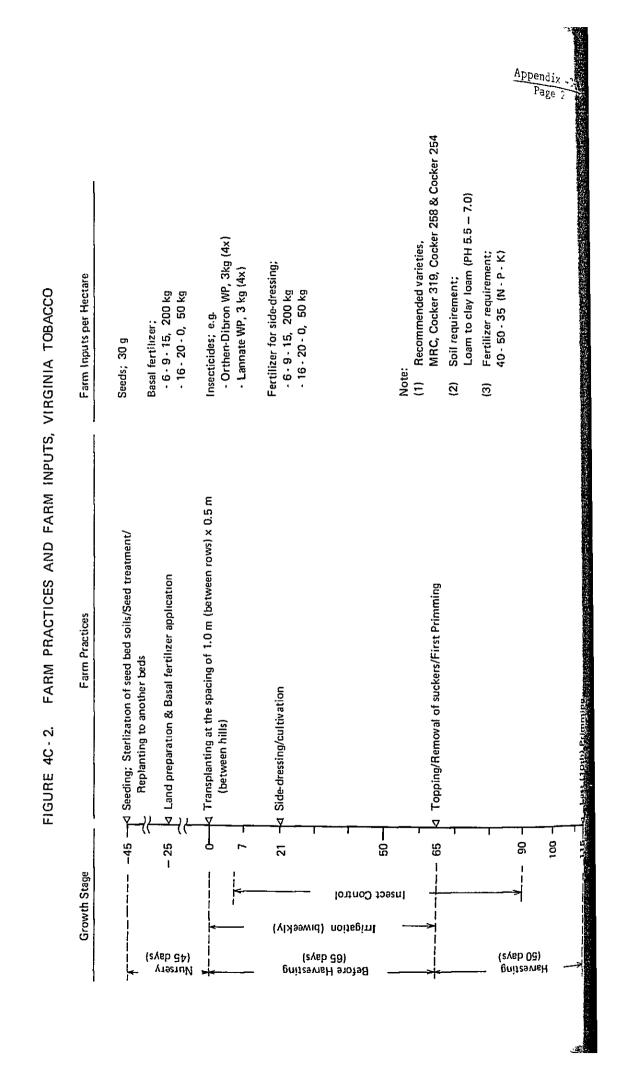
(Cont'd)

Table 4C-5. Farmers' Response to Questionary (Cont'd)

Main Item	1	Sub-Item	Unit	Total	Percent
	V-1.	One cropping a year;		0	o
fattern in futre (In case of	V-2.	÷		ω,	11
c		- Paddy + Garlic (G) - Paddv + Tobacco(T)		υC	ထင
		+	្រល្	0	9 m
	V-3.	Three cropping a year; - P + T/G + P		<b>15</b>	21
		- P + T/G + Corn/Others	hers	18	26
		-P + T/G + Mungo (N	(W	15	21
		- Others (EX. P+P+M)	<u> </u>		0T
VI. Needs of Agricultural Development Project	VI-1.	Construction/improvement of irrigation facilities	o%	70	100
	VI-2.	Construction of drainage facilities	0 <sup>10</sup>	70	100
	VI-3.	Construction/improvement of farm roads	0 <sup>,0</sup>	70	100
	.μ-IV	Strengthening of extension activities	0%D	70	00T
	VI-5.	Expansion of farm credits such as M-99	0/0	70	100
	VI-6.	Land exchange for grouping dispersed parcels	0%)	70	100

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	FIGURE 4C . 1 FARM PRA	ARM PRACTICES AND FARM INPUTS, PADDY RICE	NPUTS, PADDY RICE
Growth Stage	Farm Practices		Farm Inputs per Hectare
(\$	-25 - 7 Land preparation/Seed bedding (400 m <sup>2</sup> , wet seedbed)	et seedbed)	Seeds, 50 kg
edaing -sqp34 b (25 day	20		Fertilizer for seedbeds; 14 - 14 - 14, 10 kg
ne 1 8	-10 - 0 0-4 Transplanting in the straight rows (20cm x 20cm)	20cm)	Insecticide for seedbeds; e.g. Azodrin 20.2% EC, 0.12 qts
(s/	Application of pre-emergence herbicides		Basal fertulizer; 16 - 20 - 0, 150 kg
161909V	20		Insecticide for treatment of Seedings; e.g. Furadan 22% Flowabie, 0.75 qts
(13x)	40 -		Herbicıdes (Ex.); e.g. Hednal 40% EC 2.0 qts.
re   	50		Insecticides; e.g. - Hopcin 50% EC, 1.25 qts (2x) - Hytox 50% WP, 1.5 kg (1x)
Asproduction (sysb 03)	70 - Second top-dressing		Fertilizer for top-dressing; - First; Urea, 35 kg (Wet) 45 kg (Dry)
	80 -		kg (Wet) kg (Dry )
	90 4 Drainage Note:	(1) Recommended varieties; IR • 36, 38, 40 & 42	Pa
	100 - Harvesting	(2) Fertilizer requirement; 50 - 30 - 0 65 - 30 - 0	(Wet) (Dry)



Jre	P	0 bulbs) ; (1×) qts (2×)			varıeties,	it; ity loam )	rement - P - K)
Farm Inputs per Hectare	Fertulizer: • 46 • 0 • 0, 50 kg • 0 • 0 • 60, 55 kg • 16 • 20 • 0, 325 kg	Seeds: 420 kg (25,000 bulbs) Insecticides; e.g. - Lannate EC, 1 qts {1×} - Malathion EC, 2 qts (2x)		Note:	(1) Recommended varieties, llocos White	<ul> <li>(2) Soil requirement;</li> <li>Clay loam to silty loam</li> <li>(PH: 5.5 - 7.0)</li> </ul>	(3) Fertilizer requirement 75 - 65 - 35 (N - P - K)
Farm Practices	Land preparation/Basat fertilizer application, Mulching	Start of irrigation	Weeding				

FIGURE 4C - 3 FARM PRACTICES AND FARM INPUTS, GARLIC

ļ							Арр	Page - P
Farm Input per Hectare	Basal fertılızer; - 14 - 14 - 14, 150 kg	Seeds; 25 kg	Insecticides; e.g. - Thiodam 35%, EC, 3 qts. (3x) - Furadam 3G, 16 kg	Note; (1)		<ul> <li>(2) Soil requirement;</li> <li>Clay loam to silty loam</li> <li>(PH 5 8 - 6.5)</li> </ul>	(3) Fertilizer requirement; 20 · 20 · 20 (N · P · K)	r dge .
Farm Practices	Land preparation/Basal fertilizer application	Drilling moculated seeds at the spacing of 50 cm between rows	Thinning/Off-baring, Hilling-up/Weeding		First Harvest		Last Harvest	
Growth Stage		(20 9	(xc) uc	Before Harvesti (65 days) Insect Control 2 8 8	<u> </u>	,	4	

FIGURE 4C - 4. FARM PRACTICES AND FARM INPUTS, MUNGBEAN

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FARM PRACTICES AND FARM INPUTS, COTTON Farm Input per Hectare	Basal fertilizer, - 14 - 14, 200 kg - 46 - 0 - 0, 50 kg	Seeds; 25 kg Pesticides for seed treatment; e.g.; orthocide 50% WP, 0.75kg	Insecticides; e.g • Thiodan 35%, EC, 6 qts (4x) • Metasystoc 25% EC, 4 qys (3x)	- Kani, wr, okg (ox)	Note;	(1) Recommended varieties; Deltapine 16		(3) Fertilizer requirement; 50 - 25 - 25 (N - P - K)				endix 4C- Page 5	4
FIGURE 4C 5. FARM PRACTICES Farm Practices	Land preparation/Basaf fertilizer application	Sowing three to four seeds at the spacing of 1.00 m (major rows) x 0.75m {minor rows}	Start of insect control/cultivating & spot weeding	Off-baring	Side-dressing/Hilling-up							First Harvesting (Three to four days - interval, four times)	Last Harvesting
	50	• - <del>7</del>	یں ۲	<u>7</u>	<u>₹</u>	1	50	- 19	┙╱᠇ ᢩᢩ	110 -	120 -	130 - 4 140 - 4	145
Growth Stage	1	Lation (20 d		 -	on (5x) Iour	itegi	ן וו זיי	ore Hays 10 days ect &				ן (sveb פ ראפאני	jui

Tobacco Garlic Mung Bean cotton (2,130 ha) (4,270 ha) (2,065 ha) (1,030 ha) Ground Per ha Total Per ha Total Per ha Total	kg 0 420 kg 1,793 25 kg 52 25 kg 26 Paddy 869	Tobacco 0	Garlic 1,793	, Mung Bean 52	Cotton 26		- 50 kg 214 50 kg 52 924	kg 213 1,640	- 55 kg 235 235		- 325 kg 1,388 3,994	150 kg 310 200 kg 206 640	kg 852 852	8,285		128 3.0 qt. 128 30 qt. 62 10.0 qt. 103 785	б 5.8kg б 36	` - 17 kg 35 35		антана и антана анта
249 0.03 kg							224	497 100 kg 213	i L		746	•	- 400 kg 852			104 6.0 128	7 3.0 6	, ,	1 5	1
1. 110 1010T LET. 100 1010T	50 kg 620 50 kg 3				·		35 kg 434 45 kg	75 kg 930 100 kg <sup>t</sup>	1		150 kg 1,860 150 kg	10 kg 124 -	, ,			2.1 qt. 260 2.1 qt.	1.5 kg 19 1.5 kg	•	2.0 gt. 248 20 dt.	,
Per ha Tota	ton 5						ton 3	2			15	4				×400 2.	ton 1.	kg	*100 2.	kg X
STOT.JACK MARK	1. Seeds					2. Fertilizer	- Urea (45-0-0)	- Ammosul (21-0-0)	- Potassium (0-0-60)	Chloride	- Compound (16-20-0)	- Compound (14-14-)	- Compound (6-9-15)	Total	3. Insecticides	- Liquid	- Water Soluble Powder	- Granular	4. Herbicides - Liquid	- Water Soluble Powder

Total Amount of Input Materials, with Project, In Future Table 4C-6.

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Filet field of Major Crops, "With Project"

: Paldy

\_\_\_\_Esperimental Yield

Following experimental data on paddy yield at each amount of rithogen were used to have the quadratic equation for the regression priver yield (Y) and amount of applied nitrogen (X).

Daddy Viold at Fach Lawsl of Applied Nitrogen

raddy i	ieid at Lach	Tever	or Appile	<u>a Nitro</u>	gen	
				(un	it:ton/h	a)
		Nitroge	n Appli <u>c</u> a	tion (k	g/ha)	
Season	0	30	90	120	150	
Wet	3.3	3.9	4.5	4,2	-	
Dry	3.5	-	4.7	5.3	5.4	

Source: BPI, Average yield of the latest 6 HYVs at three national experiment stations (Maligaya Rice Research and Training Center, Bicol Rice and Corn Experiment Station and Visaya Rice Experiment Station)

... quadratic equations for above data are shown as follows; Wet season crop:  $y = 3.28 + 0.025x - 0.00014x^2$ Dry season crop:  $y = 3.50 + 0.029x - 0.00011x^2$ 

(The curves for both equations are shown in Figure 4C-6.)

The attained yield under Masagana 99 (1976-1979) in the Project Twichpalities is 3.6 ton/ha for wet season crop and 3.5 ton/ha for In Stason as shown in Table 3D-16, Appendix 3D-1.

Almost all the same level of average yields are attained in the Almost all the same level of attained in the Almost all the same level of average yields are attained in the Almost all the same level of attained in the Almost all the same level of attained in the Almost all the same level of attained in the Almost all the same level of attained in the Almost all the same level of attained in the Almost all the same level of attained in the Almost all the same level of attained in the Almost all the same level of attained in the Almost

#### Attained Yield in Existing National Irrigation System Areas (1977)

<u>Area</u>	Yield (cavan/ha)	Area Coverage of HYVs
Laoag-Vintar	70	more than 70%
Dingras	70	more than 75%
Cura	40	less than 50%
Bonga Bump #2	73	more than 70%
Mean	<u>71</u> (3.6 ton,	/ha)

Note: (1) The yields refer to the average yields for wet and dry season crops

(2) The mean yield is exclusive of the yield in Cura area because of small area coverage of HYVs.

The attained yield in the foundation seed farm at BPI Dingras Experimental Station (1977) was 3.8 ton/ha for wet season crop and 3.5 ton/ha for dry season crop. But the station has attained more high yield of 4.4 ton/ha for wet season crop a few years ago.

The irrigation conditions in the existing national irrigation system areas need rehabilitation under NISIP because of the inadequate irrigation water amount and on-farm facilities. Also, at BPI Dingras experiment station, the irrigation water supply during dry season is limitted very much because the irrigation water supply to the station is made by one of the existing national irrigation systems. These unfavorable irrigation conditions are considered to be the main reason why the comparatively low yield in the existing national irritation system areas and also at BPI Dingras Experimental Station.

On the other hand, the yield of 4.41 ton/ha was attained at 70 kg of applied nitrogen according to the yield record of FAO/NFAC/ JICA Fertilizer Trial (1978-1979) in three Project municipalities (See Table 3D-18, Appendix 3D-1).

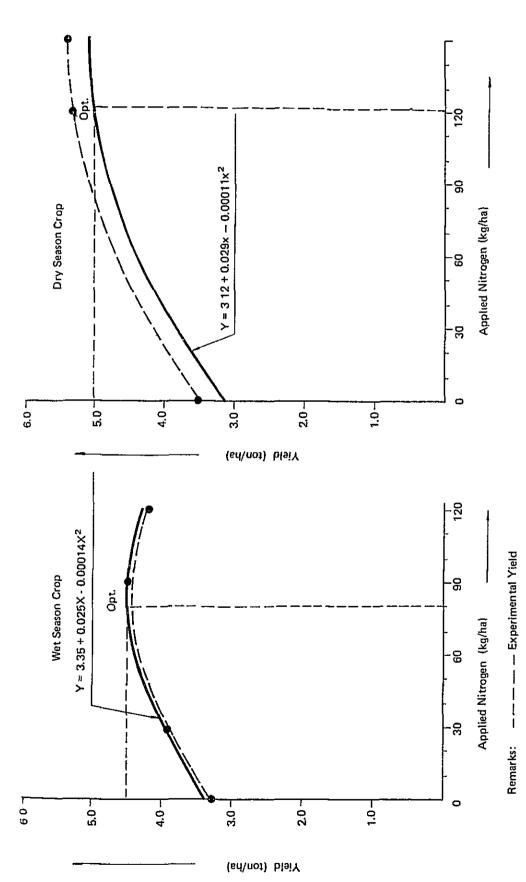


FIGURE 4C . 6. EXPERIMFNIAL AND PREDICTED YIELD OF PADDY

Appendix 4C-6 Page 3 It is considered that the proposed irrigation development of the Project will improve the irrigation conditions to attain high yield, at least such level of attained yield of 4.41 ton/ha at 70 kg of applied nitrogen for wet season paddy rice by FAO/HFAC/JICA Fertilizer Trial in the Project municipalities, as shown previously. The following equation is assumed to represent the quadratic equation for the regression between potential yield (y) and amount of applied nitrogen (x) in the Project, which is produced by substituting the above yield data into the said equation for the experimental yield data of wet season crop:

 $y = 3.35 + 0.025x - 0.00014x^2$ 

For dry season crop, such kind of yield data for the substitution is not available. Therefore, the assumed potential yield of 4.78 ton/ha at 70 kg of applied nitrogen is used to have the equation as follows:

The assumed potential yield for dry season crop:

4.41 ton/ha (potential yield of the wet season crop) x 4.7 ton/4.5 ton = 4.61 ton/ha

where; 4.7 tons and 4.5 tons are the above-mentioned experimental yields at 90 kg of applied nitrogen for wet season crop.

Thus the new equation with regard to potential yield for dry season crop in the Project Area is as follows:

 $y = 3.12 + 0.029x - 0.00011x^2$ 

3. Yield at Optimum Amount of Nitrogen Application

Optimum amount of nitrogen application and their yields are computed as follows:

Wet season crop: Opt. nitrogen (kg/ha) =  $\frac{0.025Py - Pn}{2(0.00014 \times Py)}$  = 82 kg Yield at 82 kg of the nitrogen application = 4.5 ton/ha Dry season crop: Opt. nitrogen (kg/ha) =  $\frac{0.029Py - Pn}{2(0.00011 \times Py)}$  = 122 kg Yield at 122 kg of the nitrogen application = 5.0 ton/ha Where Py = F 2,090 (Paddy price per ton) Pn = F 4.5 (Nitrogen price per kg) (Projected prices for the year of 1990 at the values in

1980)

4. Estimated Yield at Different Land Class

The yields at optimum amount of nitrogen application are regarded as the potential yield after Project. Hence, the yield at different land classes are estimated as follows:

	Range of	Average Productivity	Target Yield	l (ton/ha)
Land Class	Productivity (%)	Rating (%)	Wet Season	Dry Season
Potential	100	100	4.5	5.0
lR	90 - 100	95	4.3	4.7
2R	80 - 90	85	3.8	4.2
3R	70 - 80	75	3.4	3.8

#### Target Yield of Paddy

#### B. Upland Crops

#### 1. Tobacco

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The potential yiels of virginia tobacco varieties to be intro-duced in the Project are estimated at 2.0 ton/ha, based on the following Table.

Variety	$\frac{\text{Growth}^{1/}}{\text{Period}}$	No. of Harvested Leaves	Potential <sup>2/</sup> <u>Yield</u> (ton/ha)
NC Blight Yellow	80 - 90	29	2.08
Coker 254	90 - 100	26	2.27
Coker P-11-1	N.A.	N.A.	2.05
MRS-3	90 - 100	25	1.89
Golden Harvest	80 - 90	26	1.91
Average			2.04

### Potential Yields of Selected Varieties

Note: 1/: From transplanting to flowering

2/ : Data source : "Three Years of Cooperative Research on Philippine Virginia Tobacco, UFord. PVTA Research & Training Program, 1973"

The PVTA compact farm that was organized in San Pedro, Batac by the farmer paticipants to the "UPLB-PVTA applied package technology commercial trials for virginia tobacco" attained about 1.6 tons of average yield in 1977-78, according to "the Philippine Virginia Tobacco Industry : In Search for Effective Technology for Development and Transfer in the Farmland prepared by Adolf C. Necesito in 1979"

The yield was attained by applying the PVTA-UPLB and Taiwan technology having the fertilizer recommendations of 30-60-90 and 54-54-128 (N-P-K in kg per hectare) respectivery. Reffering to

the relationship between the attained yield and the soil conditions in the compact farm, the target yield for second class land is set up at 1.7 tons per hectare.

The target yields by land class are decided in the basis of above id\_\_.tential yield and the target yield for second class land as follows;

Land Class	Range of Productivity (%)	Average Productivity <u>Rating</u> (%)	Target Yield (ton/ha)
Potential	100	100	2.0
First	90 - 100	95	1.9
Second	80 - 90	85	1.7
Third	70 – 80	75	1.5

#### Target Yield of Virginia Tobacco

#### 2. Carlie

Potential yield of garlic is estimated at 3.0 ton/ha from to experimental data on the garlic planted in October and November at ETI Dingras Experimental Station.

The high-yield farmers, one third of sample farmers in "the Ca. 1. Production and Marketing, Ilocos Region prepared by DA" had about 2.3 tons of average yield per hectare.

Following target yields by land class are decided in the basis of the above-mentioned potential yield and the yield of high-yield farmers.

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#### Target Yield of Garlic

Land Class	Range of Productivity (%)	Average Productivity <u>Rating</u> (%)	Target Yield (ton/ha)
Potential	100	100	3.0
First	90 - 100	95	2.9
Second	80 - 90	85	2.6
Third	70 – 80	75	2.3

#### 3. Mungbeans

I var

The potential yield of mungbeans is estimated at 1.3 tob/ha from the following studied yield of improved varieties.

### Studied Yield of Mungbeans

. .

Variety	Studied Yield (ton/ha)	Maturity to days to lst Priming (day)
MG 50-10A(G)	1.0 - 1.3	60 - 65
MD 15-2	1.0 - 1.3	60 - 65
E.G. Glabrous	1.0 - 1.3	60 - 65
CES 55	1.0 - 1.5	65 - 68
CES 87	1.0 - 1.5	65 - 68
CES 1D-21	1.0 - 1.2	65 - 68

# Source: Philippine Recommendation on Mungbeans, PCARR

According to the yield data taken from "the Angat-Magat Integrated Agricultural Development Project Applied Research Phase one Report", the yield of about 1.2 ton/ha was attained for the wet season crop in 1974 on farmers' field of Magat Project Area. (used variety; CES-55) The target yields by land class are decided as shown in the following Table, assuming the potential yield and the yield for the first class land as 1.3 ton and 1.2 ton per hectare respectively.

#### Target Yield of Mungbean

Land Class	Range of Productivity (%)	Average Productivity Rating (%)	Target Yield (ton/ha)
Potential	100	100	1.3
First	90 - 100	95	1.2
Second	80 - 90	85	1.1
Third	70 - 80	75	1.0

#### 4. Cotton

The estimated potntial yield is 2.9 tons/ha (seed cotton) from the following experimental data.

	Experimental Yiel		ton/ha, seed cotton)
	Plant Density		<pre>&amp; Planting Time</pre>
Fertiliaer Level (kg/ha)	83,882 (Oct. 1st)	93,393 (Nov. 1st)	Mean
120 - 25 - 25	2.4	2.4	2.4
90 - 25 - 25	2.9	2.9	2.9
90 - 0 - 0	1.8	1.0	1.4
50 - 25 - 25	1.2	2.0	1.6
Control	1.1	1.5	1.3

Source: PCC Annual Report (1977 - 1978) Philippine Cotton Cooperation through Cotton Development and Research Institute

Nots: (1) Experimental location : Pangasinan (Irrigated) (2) Variety : Deltapine

The target yields by land class are decided as shown in the following Table, based on the above mentioned potential.

Land Class	Range of Productivity (%)	Average Productivity Rating (%)	Target Yield (ton/ha)
Potential	100	100	2.9
First	90 - 100	95	2.8
Second	80 - 90	85	2.5
Third	70 - 80	75	2.2

### Target Yield of Cotton

# C. Projected Total Production with Project

#### 1. Paddy

The aggregate projected production after full implementation of the Project is 74,492 ton, 51,916 tons of which are wet season harvest and the balance of 22,576 tons are dry season harvest. The weighted average yield at each area of different land class is 4.2tons/ha and 4.5 tons/ha for wet and dry season crop respectively. (See Table 4C-7)

### 2. Upland Crops

The total projected production and the weighted average yield at each area of different land class for each selected upland crops are as follows;

Crop	Weighted Average Yield (ton/ha)
Tobacco Garlic Murch	1.7 2.6
Mungbean Cotton	1.1 2.5

### Total Projected Upland Crops Production

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Product For	
and Upland Crops f, Future	
Paddy Nice With In Tee	
lable 40-7.	

l. Paddy

Product- ion (ton)	1,394 12,400 (4.2) 51,916	22,576
Total Product Area Yield ion (ha)(ton/ha) (ton)	(4.2)	1,254 4,970 (4.5)
Area (ha)(t	12,400	4,970
<u>3R or 3R(3)</u> Product- Area <u>Yield</u> ion (ha)(ton/ha) (ton)	1,394	1,254
3R or 3 Yield on/ha)	3.4	Э•8
Area (ha)(to	h10 3.4	330
2R or 2R(2) Product- Area Yield ion A: (ha)(ton/ha) (ton) (1	7,866	4,116
2R or 7 Yield on/ha)	3.8	4.2
Area (ha)(t	2,070 3.8	086
Product- ion (ton)	42,656	17,202
<u>IR or IR(1</u> Pro <u>Pro</u> (ton/ha) (1	4.3	4.7
<u>Area Yield</u> (ha)(ton/ha)	9,920 4.3	3,660 4.7
Season	Wet	Dry

2. Upland Crops

		1R(2) or	2R(2)		3R(3)			Total	
Crop	Area (ha)	<u>Yield</u> (ton/ha)	Area Yield Production (ha) (ton/ha) (ton)	Area (ha)	<u>Yield H</u> (ton/ha)	Area Yield Production (ha) (ton/ha) (ton)	Area (ha)	<u>Yield</u> (ton/ha)	on Area Yield Production (ha) (ton/ha) (ton)
(1) Tobacco	2,130	2,130 1.7	3,621	i	ı	I	2,130	(1.7)	2,130 (1.7) 3,621
(2) Garlic	4,190	2.6	10 <b>,</b> 894	80	2.3	184	4,170	(3.6)	11,078
(3) Mungbean	2,065	1.1	2,272	I	I	1	2,065	2,065 (1.1)	2,272
(4) Cotton	1,030	2.5	2,575	1	1	I	1,030	(2.5)	2,575
Total	9,415			80			9,495		



# Page ]

#### Farm Mechanization and Land Requirement

## A. Proposed Farm Mechanization Plan

The farm operation systems as shown in Figure 4C-7 will be applied for the scheduled farming after completion of the Project. These systems require mechanization in such major operations as land preparation, threshing and drying. The selected machines and the assumed area coverages of mechanization area by selected machine are as follows;

## Selected Farm Machinery and Assumed Area Coverage of Farm Mechanization

Operation	Selected Machine	Area Coverage
Land preparation	- Hand tractor (7-8 HP diesel)	(%) 40
Threshing	- Powered thresher (7-8 HP diesel, throw-in type)	50
	- Pedal thresher	50
Drying	- Dryer (flat-bed type, 2.0 ton bin)	50

As for all selected machines, the Philippines-made or the imported ones are available in the Philippines. The traditional way of operation for land preparation by draft animal and drying by sunshine will be employed in the areas where the above-mentioned mechanization will not cover. The farm operation efficiency are calculated for the operation of land preparation, threshing, drying and transportation in both cases of using machineries and draft animals as shown in Table 4C-8. LIGUEL W. C. TEOLOSED FARM OFTRATION POTEM

Trans-	portation
	Drying
	<u>Threshing</u>
Harvest-	ing
	Weeding
	Spraying
Trans-	<u>planting</u>
Final Harrowing	Furrowing
Plowing &	Harrowing

a) Paddy Rice

Draft Animal	W/Cart
Sunshine	<pre>&amp; Dryer W/Cart</pre>
Powered &	Pedal Thre
Man-	Power
Rotary Weeder Man- Powered & Sunshine Draft Animal	5 Man-power
Hand	Sprayer
Man-power	Straight-row Sprayer
Draft Animal	W/Harrow & Leveler
Hand Tractor	W/Rotary

b) Diversified Crops

Sunshine Draft Animal	W/Cart
Sunshine	
Man-	Power
Power	
Man	
Hand	Sprayer
Man-power Hand	Sprayer
	W/Harrow Sprayer

- Area coverage of mechanization for the operations of plowing and harrowing by hand tractor is estimated at 40 percent of cultivated area in both cases of paddy rice and diversified crops. (1) Note:
- Area coverage of mechanization for threshing by the powered thresher and pedal thresher is estimated at 50 percent of cultivated area respectively. (2)

Appendix	40-2
D	

Page 3

										-	
(12)= (10)+(11)	Days <u>per day</u> (day/ha)	7.0	2.4	2.4	1.8	з.4	6'0	6.0	0° †	0.7	
	Hours per day (hr./day)	æ	æ	60	Ø	80	8	۵	Q	16	•
(9) (10)=(8)x(9) (11) 0pe.	Hours <u>per ha</u> (hr./ha)	\$5.6	18.9	19.2	14.3	27.4	7.4	5.6	24.0	10.5	ı
(6)	Ope. Times (time)	Ţ	-	2	г	~	N	~	-1	1	1
(8)	Hours per ha (ha/hr.)	55,6	6 . 18	9°6	14.3	13.7	3.7	5,6	24.0	10.5	ı
(7)=(5)x(6) Actual	Ope. <u>Capacity</u> (ha/hr.)	0.019	0.053	0,104	0.070	0.073	0.269	0.179	0.042 (0.19ton)	0.095 (0.4ton/hr.)	0.1 ton
(9)	Ope. Lfficiency (%)	90	08	65	80	65	80	75	75	80	BC
(5)=(3)×(4) Ope.	city hr.)	0.022	0.066	0.160	0.088	0.112	0.336	0.238	0.056 (0.25ton)	1	0.]6 tan
(†)	Efficiency in Field (%)	Bu	BO	80	80	80	90	80	BO	_	80
(3)= Theoretic	Ope. Capacity (ha/hr.)	0.026	0.083	0.200	011.0	0.140	0.420	0.298 (1.25ton/hr.)	0.070 (0.32ton/hr.)	0.119 (0.5ton/hr.)	0.2 t n
(2)	Ope. Speed (km/hr.)	2.2	1.5	2.0	2.0	2.0	3.0	ŗ	,	ı	2.5
(1)	Ope. Width (m)	0.12	0.55	1.0	0.55	0.7	1.4	ı	ı	I	I
	Machinery/ Animal	-Carabao w/plow	-Hand tractor w/rotary	-Carabao w/harrow	-Hand tractor w/rotary	-Carabao w/harrow & leveler	-Hand tractor w/ harrow & leveler	-Powered thresher	-Pedal thresher	-Dryer (Flat-bed type, 2.0 tons bin)	-Carabao w/ cart
	Operation	a) Plowing		b) Harrowing		c) Final Harrowing		d) Threshing		e) Drying	f) Transportation

Table 40-8. Efficiency of Farm Operation

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5. Number of Required Machinery per Compact Farm

It is considered that the required units of machinery will be introduced in each compact farm or in each two compact farms for the collective use of machinery in order to minimize the machinery costs. The required units of the machinery per compact farm (average size (s 40 hs) are computed as follows;

#### Hani tractor

The type of hand tractor having P.T.O. for the attachment of rotary will be chosen in most of the Project Area because of big area coverage of upland crops. One unit of the hand tractor is required for land preparation work in 16 ha (40 percent of compact farm area) in each compact farm in this chase as follows;

Efficiency: 4.2 (2.4 + 1.8) days/ha/unit (see Table 4C-8)

Possible operation days per crop season: 67 days (Lag period + land praparation period + Overtime work)

Number of required units: 4.2 days/ha x 16 ha ÷ 67 days ‡ one unit

#### - Thresher

One unit of powered thresher and five units of pedal threshers

#### Etwered Thresher

Efficiency: 0.9 days/ha/unit (See Table 4C-8) <sup>1</sup>Esumed possible operation days per crop season: 35 days x  $0.8^{1/2}$ = 28 days

Amber of required units: 0.9 days/ha x 20 ha ÷ 28 days ÷ one unit

#### Pedal Thresher

Dfficiency: 4.0 days/ha/unit (See Table 4C-8)

Recipie operation days per crop season: 28 days

Number of required units: 4.0 days/ha x 20 ÷ 28 days ÷  $0.6^{2/}$  = five up.

Remarks  $\underline{1}/:$  assumed rate of possible operation days to full operation days

2/: assumed reduction rate of operation efficiency

3. Dryer

One unit of the selected drier has the capacity of drying up 2.0 tons of threshed paddy in moisture content from 26% to 14% and will take eight hours. But it is considered that the traditional way of sunshine-drying will be employed at least in the half stage of drying in moisture content from 26% to 14%. In this case, the dryer has the capacity to dry up 2.0 ton with four hours of the drying time. Then, one unit of the drier is able to cover two compact farms as follows;

Efficiency: 4.2 ton/ha (unit yield of wet season crop) ÷ 2.0 tons/ unit x three rotations = 0.7 days/ha/unit (See Table 4C-8) Possible operation days per crop season: 28 days<sup>1/</sup> Number of required units: 0.7 day/ha/unit x 40 ha ÷ 28 days ≑ one unit Remarks <u>1</u>/: 35 x 0.8 (assumed rate of possible operation days)

4. Working Carabao

The operation of land preparation in non-mechanization area (24 per compact farm ha) will be performed by animal power (carabao or cattle). The required heads of draft animal per compact farm is computed as follows:

Efficiency:	Plowing:		7.0	animal-days/ha
	lst	harrowing:	2.4	animal-days/ha
	2nd	harrowing:	2.4	animal-days/ha
	3rd	harrowing:	3.4	animal-days/ha
		Total	15.2	animal-days/ha

Estimated possible operation days per crop season = 55 days Required heads of working carabao: 15.3 animal-days/ha x 24 ha  $\div$  67 days  $\doteqdot$  6 heads

## 2. Labor Requirement and Machinery Cost

The labor requirements for paddy rice and concerned diversified crops are estimated as follows:

	Labor Require	
Crop	Man-day	Machinery or animal day
Paddy Rice	103.1	20.2
Tobacco	273.5	28.8
Garlic	165.0	22.5
Mung Beans	86.3	22.3
Cotton	139.3	37.3

Remarks: The detailed labor requirements by crop and operation are indicated in Table 4C-9 to 4C-13.

The machinery cost of paddy rice cultivation is calculated at 569 per ha. The cost for the diversified crops is computed at 395 per ta because of no machinery cost for threshing and drying. (See Table +C-14). Table 4C-9. Labor Requirement of Paddy Cultivation with Project in Future

(Unit: day/ma.

		Machinery	
Operation	Man-day	or Animal-day	Remarks
1. Seed-bedding			
a) Land preparation/Sowing b) Care of seedlings Sub-total	1.5 1.5 (3.0)	0.5 (0.5)	Same as the item 2
2. Land Preparation			
a) Plowing b) Harrowing c) Final harrowing/Leveling d) Repair of dikes Sub-total	5.2 3.6 2.6 2.7 (14.1)	5.2 3.6 2.6 (11.4)	Animal(60%), Machine(-,) -do- Animal(100%)
3. Transplanting			
a) Pulling/Delivery of seedli b) Transplanting Sub-total	ngs 7.5 20.0 (27.5)	0.5 (0.5)	
4. Fertilizer Application			
a) Basal fertilizer b) Top iressing (2x) Sub-total	1.0 1.0 (2.0)	0.2 0.2 (0.4)	
5. Spraying			
a) Insecticides (3x) b) Herbicides (1x) Sub-total	3.0 1.0 (4.0)		
6. Weeding			
a) lst weeding (2x) b) 2nd weeding Sub-total	7.0 6.0 (13.0)		
7. Irrigation/Drainage	5.0		
8. Harvesting			
a) Cutting/Bundling b) Hauling/Piling c) Threshing Sub-total	16.0 3.0 8.5 (27.5)	2.0 2.6 (4.6)	Powered Thresher(50%) & Pedal Thresher (50°)
9. Post Harvesting			
a) Drying b) Sacking c) Piling/Delivery sub-total	3.5 2.0 1.5 (7.0)	2.5 0.3 (2.8)	Drier(50%) & sunshine (50%)
Total	103.1	20.2	

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Table 4.-10. Labor Requirement of Tobacco Cultivation with Project in Future

		Machinery	
Operation	Man-day	or Animal-day	Remarks
Seed-bedding			
a) Land preparation/Sowing r) Care of seedling Sub-total	4.0 22.2 (26.2)	0.5 (0.5)	
2. Land Preparation			
<ul> <li>a) Plowing</li> <li>b) Harrowing</li> <li>c) Leveling/Furrowing</li> <li>Sub-total</li> </ul>	9.4 4.2 2.7 (16.3)	9.4 4.2 2.7 (16.3)	Animal(60%), Machine(40%) -do- Animal(100%)
3. Transplanting			
a) Preparing of seedijgs b) Transplanting/Replanting Sub-total	5.0 30.0 35.0		
Fertilizer Application			
a) Basal fertilizer p) ^ide-dressing	4.0 4.0 8.0		
5. Weeding/Hilling-up	8.8	8.0	Animal(100%)
<pre>c. 4rajing (8x)</pre>	8.0		
<pre> Irrigation (5x)</pre>	10.0		
<ul> <li>Topping/Sucker control</li> </ul>	10.0		
<pre> darvesting (8x)</pre>			
<ul> <li>a) Printing/Hauling</li> <li>c) Sorting/Sticking</li> <li>Sub-total</li> </ul>	60.0 40.0 (100.0)	4.0 (4.0)	Animal(100%)
1. Fost darvesting			
a: Curing z) Grading/Bundling T) Packing/Storing Sub-total	30.0 20.0 2.0 (52.0)		
Total	273.5	28.8	

## Table 4C-11. Labor Requirement of Garlic Cultivation with Project in Future

		Machinery or		
Operation	<u>Man-day</u>	Animal-day	Remarks	
1. Land Preparation				
a) Plowing b) Harrowing c) Leveling/Furrowing d) Mulching Sub-total	9,4 4.2 2.7 8.7 (25.0)		Animal(60%), -do- Animal(100%) Animal(100%)	Machine(up
2. Planting				
a) Preparing of seeds b) Planting Sub-total	10.0 35.0 45.0			
3. Fertilizer Application	2.0	0.2	Animal(100%)	
4. Thinning	2.0			
5. Spraying (3x)	8.0			
6. Irrigation (4x)	8.0			
7. Harvesting				
a) Pulling/Gathering b) Hauling Sub-total	23.0 2.0 (25.0)	2.0 (2.0)	Animal(100%)	
8. Post Harvesting				
<ul> <li>a) Drying</li> <li>b) Cleaning/Cutting of roots</li> <li>c) Classifying/Grading</li> <li>d) Bundling/Trimming Sub-total</li> </ul>	5.0 15.0 10.0 10.0 (40.0)			
9. Removal of hay (rice straw)	10.0			
Total	165.0	22.5		

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# Table 4C-12. Labor Requirement of Mungbeans Cultivation with Project in Future

		Machinery or		
Operation	Man-day	Animal-day	Remarks	
1. Land Preparation				
a) Plowing b) Harrowing c) Leveling/Furrowing Sub-total	9.4 4.2 2.7 (16.3)	9.4 4.2 2.7 (16.3)	Animal(60%), -do- Animal(100%)	Machine(40%)
2. Planting				
a) Seeding/Covering b) Thinning Sub-total	4.0 1.0 (5.0)			
3. Fertilizing	2.0			
<ol> <li>Cultivation/Weeding</li> </ol>				
a) Off-baring b) Hilling-up c) Weeding Sub-total	2.0 2.0 10.0 (14.0)	2.0 2.0 (4.0)	Animal(100%) Animal(100%)	
5. Spraying (3x)	4.0			
6. Irrigation (3x)	6.0			
7. Harvesting				
a) Picking (4x) t) Hauling	25.0 2.0	2.0	Animal(100%)	
. Threshing/Drying/Others	12.0			
Total	86.3	22.3		

# Table 4C-13. Labor Requirement of Cotton Cultivation with Project in Future

Operation	Man-day	Machinery or Animal-day	Remarks	
1. Land Preparation				
a) Plowing	9.4	9.4	Animal(60%),	Machine(4
b) Harrowing	4.2 2.7	4.2 2.7	-do-	
c) Leveling/Furrowing Sub-total	(16.3)		Animal(100%)	
	(1000)	(2010)		
2. Planting/Thinning				
a) Seeding/Covering	20.0			
b) Re-planting	2.0			
c) Thinning	1.0			
Sub-total	(23.0)			
3. Fertilizing				
a) Basal fertilizer	4.0			
b) Side dressing	4.0			
Sub-total	(8.0)			
4. Cultivation				
a) Off-baring/Hilling-up	18.0	18.0	Animal(100%)	
5. Spraying (10x)	20.0			
<pre>6. Irrigation (5x)</pre>	10.0			
7. Harvesting/Drying				
a) Picking (4x)	30.0			Ĭ
b) Hauling	3.0	3.0	Animal(100%)	
c) Cleaning	3.0			
d) Drying	4.0			
Sub-total	(40.0)			
8. Packaging/Deliverying	4.0			2 2
Total	139.3	37.3		

•

Farm Machinery Cost Table 4C-14. •

Fixed Cost

Total cost per hectare (P)	L77	ю Б	26	27	323
Coverage per unit (ha)	Wet 16 Dry 19	Wet 20 Dry 12	Wet 4 Dry O	Wet 40 Dry 12	
Total Cost (P/year)	6,210	2,962	105	1,423	
Other Fixeg/ Cost2/ (P/year)	230	194	2	83	
Repair Cost (₱/year)	1,840 (8%)	583 (3%)	ŝ	412 (5%)	
Depreci- ation/ Cost <sup>-</sup> / (P/year)	041,4	2,185	86	928	
Durable Period (Year)	വ	ω	ß	ω	
Purchasing Price (P)	23,000	19,425 <u>3</u> /	650	8,250	
Machinery	Hand tractor	Thresher	Pedal thresher	Dryer	<u>Total</u>

- Computed as (1) x 0.9 + (2) 10 IN IN Note:
  - Computed as (1) x 0.01
- Price without engine because the engine of hand tractor can be used for thresher.

Appendix " Page 13

Cost	
Variable	
N	

Note: G: Gasoline, L: Lubricant Oil, K: Kerosin

3. Machinery Cost per Hectare

Paddy : P323 (fixed cost) + P346 (variable cost) = 669
Diversified Crops: P177 (fixed cost) + P218 (variable cost) = P395

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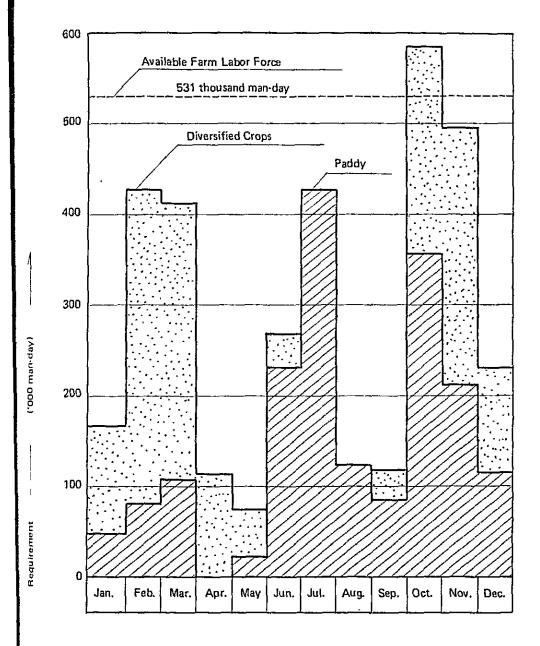
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建自己进行的 的第三人称单数 化基化合金 化分配分子 化合合合合合合合合合合合合合合合合合

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Appendix 4C-7 Page 14

## FIGURE 4C - 8. FARM LABOR BALANCE (WITH PROJECT, IN FUTURE)



	Remarks	Siniot(1,770ha), Nueva Era(670ha) only	Whole service area								F l,540,000/year x l.75(lst to 3rd year)	P 70,000/year x 3 years			
	Cost (₱ 1000)	78	272	(350)	150	770	20	150	1,440		r 2,690	210	2,900	4,340	
1	Unit Price (F)	32	22		1,400	7,200	20,000				14,500/year 2,690				
ł	Amount	2,440 ha	12,400.ha		s 106	106	r-4				106	lump sum			
	Items 1. Preparation of cadastral maps	(a) Production of cadastral maps	(b) Preparation of cadastres	(sub-total)	2. Arrangement for establishment of FIAs	3. Construction of FAI Offices	4. Extension of FIA Federation offices	5. Others	Total	6. Operation Cost	(a) FIA Officeş	(b) FIA Federation Offices	Total	Ground Total	

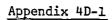
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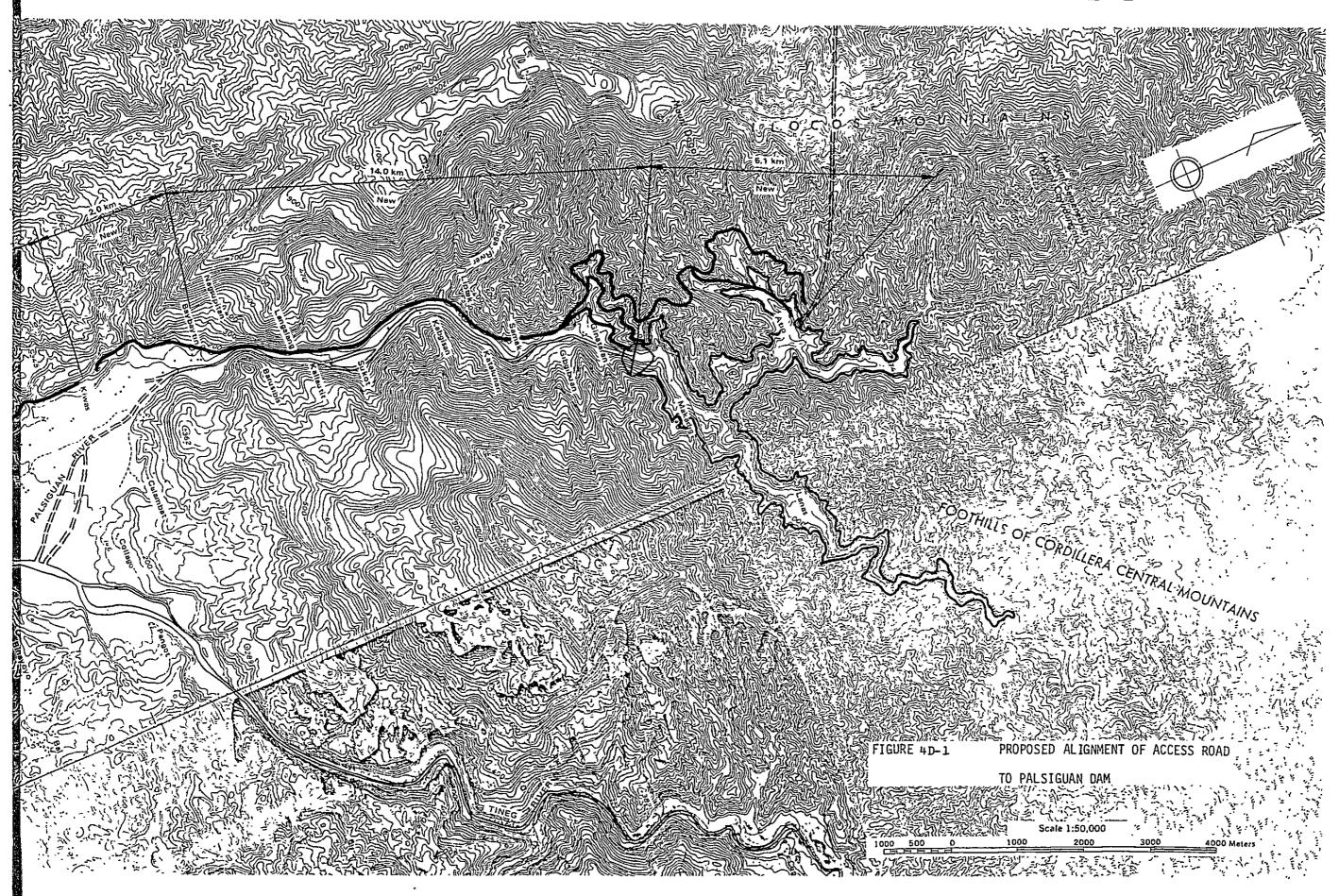
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Table 4C-15. Agricultural Development Cost

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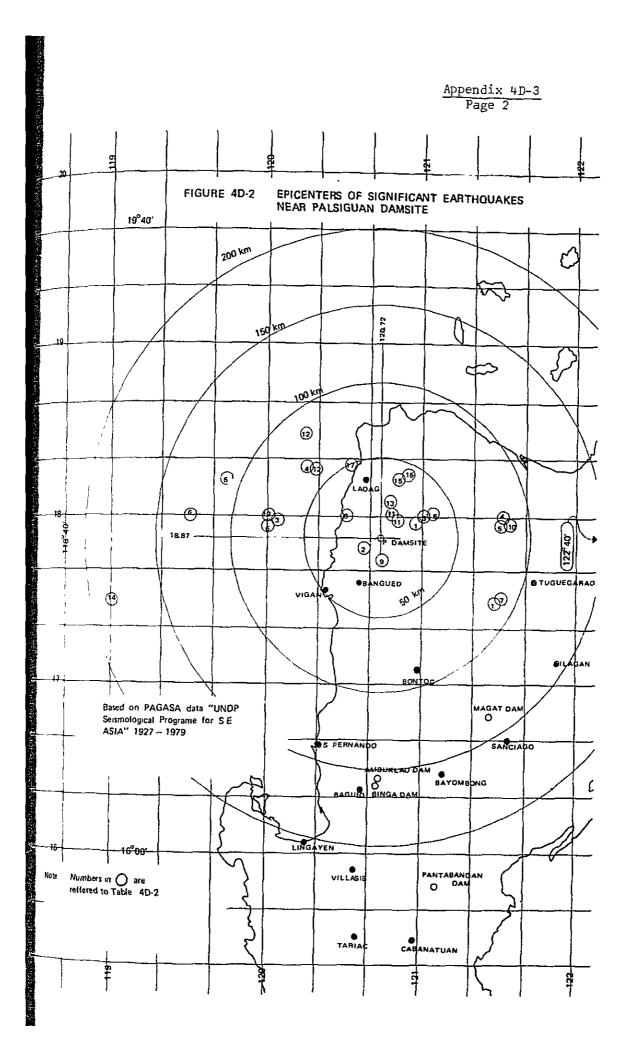
iguan Dam	Concrete Gravity Concrete Arch		$2,100,000^{\pm/}$ $500,000^{\pm/}$ $600,000^{\pm/}$	24 6 - 7	600 L,500	14,400 9,000 - 10,500	350 ~ 600 ~	600 (average 418)	need more excavation impossible	3 ~ tt	2.5 ~ 3.4	need more excavation impossible	gravel;exist gravel;exist	huge big	not economical impossible	
on Chart for Pals	Fill	140 ~			0	0	250 ~	300 ~ 6		- 1	2.0 ~ 2			1		
Dam Type Comparison Chart for Palsiguan Dam	Earth and Rock		8,900,000	JOO	n 100	10,000		rock .cm)	good	ed rock c)	d rock c)	good	earth and rock; exist	small	suitable	al condition, ,Dome type ,Constant angle type
Table 4D-1	Dam Type	l) Dam height (m)	<pre>2) Dam volume (cu.m)</pre>	3) -ditto- (ratio)	4) Unit cost ratio for Dam construction	5) Cost index 3) x 4)	<li>6) Required compressive strength of bed rock (kg/sq.cm)</li>	<ol> <li>Present compressive strength of bed rock (kg/sq.cm)</li> </ol>	8) Judgement 6) < 7)	<ol> <li>Required elastic wave velocity of bed rock (km/sec)</li> </ol>	<ol> <li>Present elastic wave velocity of bed rock (km/sec)</li> </ol>	11) Judgement 9) < 10)	12) Construction material	13) Concrete mixing plant	Final judgement	Note 1/ estimated at nomal condition, $\overline{2}/$ -ditto- , Dome type $\overline{3}/$ -ditto- , Constant ang.

Appendix 4D-2

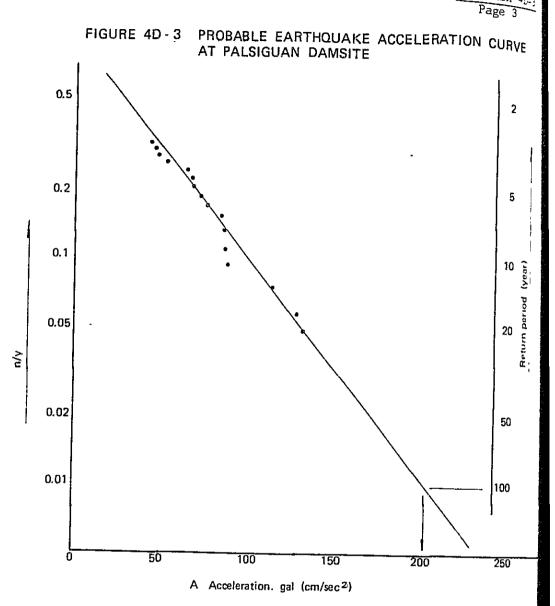
			-				
Ranl	king Date		center Longitude	Inten- sity	Distance fr Palsiguan D		/
				(m)	(km)	(001)	Averag-
4	3-19-31	18.3 18.0	120.2 121.5	6.9 6.9	72.9 83.7	121.8 104.0	112.9
7	10-28-31	17.5	121.5	6.25	98.1	84.1	84.1
12	1-14-32	18.3 18.0 18.5	120.2 120.0 120.25	6.5 6.0	72.9 77.5	85.9 44.1	66.0
14	2-14-34	17.5	119.0	6.5 7.6	86.0 186.4	68.1 51.7	E1 7
3	3-16-37	1810 18.0	121.0 120.0	6.5	33.0	174.9	51.7 127.j
		18.2	119.7	6.5 7.0	77.5 113.9	79.2 73.8	<b>⊥</b> £;.J
6	3-23-38	18.0 18.0	119.5 120.0	7.0	129.8 77.5	59.1 123.1	85.3
1	12-29-49	17.5 18.0	121.5 121.0	7.2 7.2	92.2 33.0	116.8 250.3	183.5
10	1-3-50	18.0	121.5	6.5	83.7	70.9	7J
5	6-11-57	18.0	121.5	6.7	83.7	86.9	θo.
16	9-30-62	18.0	121.0	5.0	32.9	45.7	45,'
17	3-14-63	18.3	120.5	5.5	53.3	43.4	43,4
8	8-26-70	18.02	120.5	5.5	30.4	83.9	83.9
15	4-29-71	18.21 18.25	120.85 120.72	5.3 5.2	40.3 42.2	50.4 42.0	46.2
9	5-22-72	17.7	120.7	5.0	19.1	75.5	<b>75.</b> E
2	2-29-72	17.8	120.6	5.5	14.9	131.3	131.3
13	3-6-73	18.1	120.71	5.1	27.0	62.9	62.9
11	9-21-76	17.98 17.95		5.1 4.2	16.2 14.2	91.4 41.6	66.5
				_			

Table 4D-2 Probable Earthquake Accelerations at Palsiguan Damsite

<u>1</u>/ Okamoto's Formula:  $\log_{10} \frac{\text{Galmax}}{640} = \frac{D + 40}{100} (-7.604 + 1.7244M - 0.1(3i))$ 



Appendix 4D-3



Based on PAGASA data "UNDP Seismological Programe for Southeast ASIA" 1927 – 1979, and Okamoto's Formula;

$$\log_{10} \frac{\text{gal max}}{640} = \frac{D+40}{100} (-7.604 + 1.7224\text{M} - 0.1036 \text{ M}^2)$$

- gal: Acceleration at the damsite
- D: Distance between damsite and epicenter
- M: Magnitude at epicenter
- n: Chronological order according to acceleration
- y: Number of years of records = 53

Seismic forth, K = gal/980

Appendix 4D-4 Page 1

Tesian of Dam and Appurtemant Structures

. Freeboard and Crest Elevation of Dam

Freeboard is the difference between the crest elevation and the full water surface level in a reservoir and is shown in the following equation in consideration of various factors according to the Design hit-ria for Dams which was published (and revised on July 1978) by latanese National Committee on Large Dams.

Hf≧ hw + he + ha + hi

WLEIL,

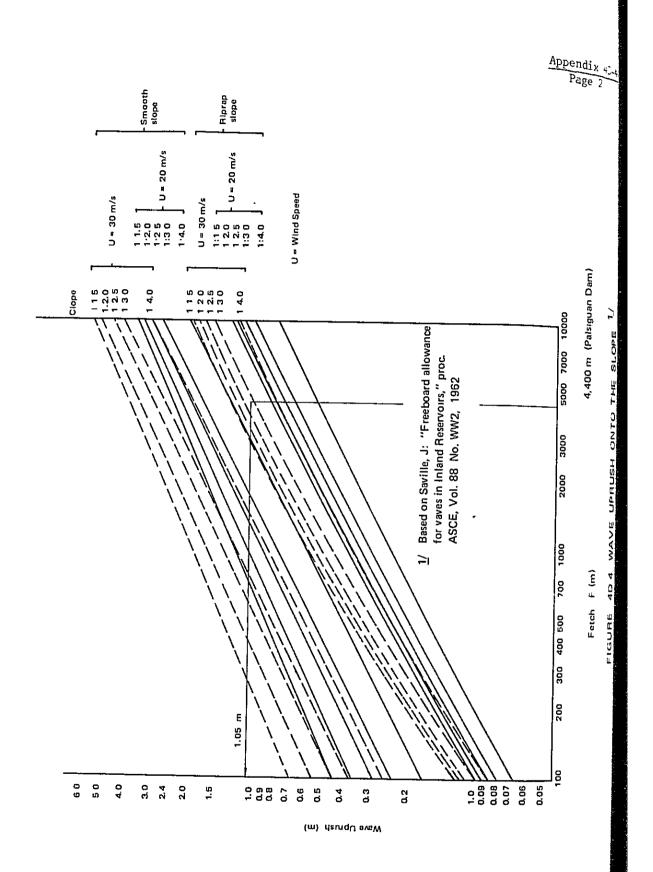
Hf: freeboard of dam (m)

- hw: height of wave due to wind (m)
- he: height of wave due to earthquake (m)
- ha: rise of water level due to unexpected accident in operating spillway gates, standard value ha=0.5 m is adopted
- hi: addition of allowance according to type and importance of dam, standard value hi=1.0 m is adopted for fill type and zero for concrete type.

Height of Wave dur to Wind

h ight of wave due to the wind is considered to be caused by 1 -Jwater wave, and then, the height of significant wave is adopted based on S.M.B. (Sherdrup-Munk-Breschneider) method which is derived thom factors such as fetch and wind speed. On the other hand, since 4 rathing height varies considerably with embankment slope and chapteress of slope, height of significant wave should be adjusted ad-quately with Saville method to obtain height of wave due to the 4 and with consideration of uprushing height as well.

The calculation results with various slope, fetch and wind Teed are shown in the Figures 4D-4.



In order to obtain the height of wave due to wind in the "il.iguan damsite, the wind speed of 30 meters per second in 10 minutes on an average is to be adopted taking into account the .Derved data of maximum instantaneous wind speed in Laoag (observed raximum value is 40 m/sec in July 1965) and the following conditions.

- The maximum instantaneous wind speed does not last for the blow time (usually 10 minutes) which is required for bringing about the wave due to wind.
- In many case, the wind direction does not accord with the maximum fetch direction.
- The wind speed in the Palsiguan damsite decrease by the topographical and vegetative conditions.

#### z) Height of Wave due to Earthquake

The height of wave due to earthquake can be obtained by Sato's formula, as follows;

he = 
$$\frac{K\tau}{2\pi} \cdot \sqrt{g.Ho}$$

- , the isotropy of the height of wave at upstream face of the dam due to the earthquake.
  - K : horizontal seismic coefficient. (K=0.2)
  - $\tau$  : period of seismic wave in second. (usually,  $\tau$  is 1.0 second adopted)
  - g : gravitational acceleration (g=9.8 m/sec<sup>2</sup>)
  - Ho: depth of reservoir water (m)

## c) Freeboad

Estimated freeboard of the Palsiguan dam is shown in the following table. The upstream surface of Palsiguan dam is formed with fockzone by the materials obtained from quarry site, therefore, the "tiprar slope" was adopted as the height of wave due to wind.

F	hw	Ho	he	ha	hi	<u>Hf</u> (m)
(m)	(m)	(m)	<u>(m)</u>	(m)	(m)	(m)
4,400	1.05	130	1.15	0.50	1.00	3.70 ≦ 4.00

#### d) Dam Crest Elevation

The Palsiguan dam will be constructed not only for irrigation the also for hydro-electric power, and its corresponding water surface elevation are tabulated as follows;

Water level	Storage capacity	Water surface elevation	Area of water surtate
	(x 10 <sup>3</sup> cu.m)	(EL m)	(x 10 <sup>3</sup> sq.")
Full water Dead water	232,000 43,000	334.5 275.0	5,040 1,560

From the above table, the Palsiguan dam crest elevation without extra bank can be obtained by adding the freeboard to full water surface;

Dam crest elevation EL. 334.50 + 4.00 = EL. 338.50 m

## 2. Surface slope stability

In case that the dam body will be constructed by the material with less cohesion, the critical slip circle approaches to the surface of dam body. In this case, the factor of safety<sup>1/</sup> can be obtained from the following formula;

For upstream slope 
$$F.S = \frac{(1-K.\frac{\gamma_{sat}}{\gamma_{sub}}.tan\alpha)}{K.\frac{\gamma_{sat}}{\gamma_{sub}} + tan\alpha} \cdot tan\phi$$

For downstream slope  $F.S = \frac{1 - K.tan\alpha}{K + tan\alpha} \cdot tan\phi$ 

where, F.S : factor of safety

К	:	seismic coefficient	(K=0.2	see	Figure	4D-3,
		Appendix 4D-3 )			_	

- $\gamma$ sat: saturated density of outer shell material ( $\gamma$ sat=2.21 ton/cu.m  $\frac{2}{}$ )
- ysub: submerged density of outer shell material (ysub=ysat - l= 1.21 ton/cu.m)
- α : tangential value of slope
- φ : angle of internal friction of outer shell material (φ=45, see Appendix 3B-4)
- 1/ The factor of safety is in conformity with the Design for Dams established by Japanese National Committee on Large Dams is to say, it must not be less than 1.2 in any case.

2/ 
$$\gamma \text{sat} = \frac{\text{Gs} + e}{1 + e} = 2.21$$
  
where, Gs(Specific gravity of the rock material) = 2.7  
reduced as 10% allowance from the Test result;  
2.95, See Appendix 3B-4.

e(Void ratio of the rock embankment) = 0.4

3. Spillway

a) Design Flood Discharge

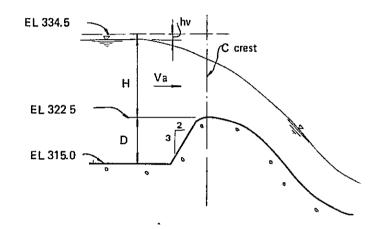
The peak discharge (inflow) and design flood discharge of the Falsiguan dam are shown in the following table.

	Catchment	Max. Peak	Design Flood
<u>Dam type</u>	area	Discharge	Discharge
	(sq.km)	(cu.m/sec)	(cu.m/sec)
Earth and rockfil	.1 153	3,070	3,070

Note; (See Chapter III.B.2)

## b) Overflow Head and Width

In general, open type spillway should be adopted to the fill type dam from view points of nonresistance against overtopping from unexpected flood and hydraulic characteristic of itself. It is considered that the gate type spillway is more suitable to be adopted than the ungated spillway from the view points of design discharge and topographical feature. In the gated spillway, at least two gates or more should be provided for the purpose of diversification of risk by gate control.



The discharge coefficient of complete overflow on the weir has a close relation with a shape of weir. On assumption that D/H is 0.61., the most effective upstream slope of weir is 3 vertical to 2 horizontal and coefficient of discharge is 2.14. Length of weir, ...g. width of spillway can be obtained from the following equation, considering the contraction by piers.

$$L = \frac{Qd}{CH^{3/2}} + N.b + 2N.Kp.H = \frac{Qd}{2.14.H^{3/2}} + (b+2Kp.H)N$$

where,

- L : length of weir (width of spillway) (m)
  - H : overflow head (m)
  - b : width of peir (b=2.50m, place for lifting unit)
  - Kp : coefficient of contraction on pier. (Kp=0 at the design discharge)
  - N : number of pier

The length of weir for various overflow heads in case of the Palsiguan dam spillway is estimated in the following table.

Qđ Number 2N.Kp.H Length overflow CH 3 12 of weir Gate size head of pier (m) (m) (m) (m)  $3 - 11.5 \times 13.1$ 44.3 39.3 H = 11.0 N = 23'- 12.5 x 11.5 3 - 13.5 x 10.2 34.5 39.5 H = 12.0 N = 2'N =2 30.6 35.6 H = 13.0

Note: (a) height of gate leaf (b) width of gate leaf

21 Hydraulic Dimensions

The water depth on chute section for the Palsiguan dam is shown in the following table.

$\frac{\text{Water Depth}^{1/2}}{d(m)}$	Velocity V(m/sec)	Froude <u>Number</u> Fr
8.0	11.1	1.3
3.2	24.5	4.4
2.5	31.4	6.4
2.2	35.1	7.5
2.2	35.9	7.8
	d (m) 8.0 3.2 2.5 2.2	d (m)V(m/sec)8.011.13.224.52.531.42.235.1

1/ calculated by Manning's roughness : n=0.014

From the flip-bucket which is installed at EL 230 m  $_{\rm V}$  235 m. Length for the shall fly through following points.

Distance from the Flip (m)	$\frac{\text{Elevation}^{1/2}}{(\text{EL-m})}$
0	235.0
20	244.3
40	249.0
60	249.1
80	244.7
100	235.7
140	204.0 = river bed

1/ calculated by energy loss of 10%

#### 4. Diversion Works

The tunnel type diversion facilities are planned for the Palsiguan dam due to the topographical condition and the diversion facilities will be used for the outlet facilities from the reservoir after completion of the dam.

a) Design Flood Discharge

The design flood discharge for diversion facilities is as follows.

Dam type	Catchment Area (sq.km)	Design Flood Discharge for Diversion Facilities (cu.m/sec)
Earth and rockfill	153	950

The open flow type tunnel has been proposed so that the dam construction will not hinder the transportation of pulpwood by the Palsiguan river flow.

Necessary tunnel sizes according to the ration of water dept to tunnel diameter is as follow;

Depth/Diameter	Tunnel Diameter 1/	Clearance (m)	$\frac{\text{Velocity}^{1/}}{(\text{m/sec})}$
0.70	10.16	3.05	14.6
0.75	9.86	2.47	14.5
0.80	9.62	1.92	14.3
0.85	9.45	1.42	14.1
0.90	9.34	0.93	13.8

1/ conditions : Q = 950 cu.m/sec Slope = 7/740Manning's n = 0.014  $_{\rm Siges}$  of pulpwood, which is measured at Baybaytin on February  $_{\rm eth},$  1980 are varied as follows;

	Normal	Longest	Thickest		
	(cm)	(cm)	(cm)		
Diameter	40	25	85		
Length	150	180	145		

In order to keep the pulpwood transportation, the tunnel clearance should be nearly two meters, so the tunnel diameter of 9.6 meters is adopted with the following hydraulic dimensions:

Tunnel		Manning's		
Diameter	Slope	Roughness	Depth	<u>Velocity</u>
(m)			(m)	(m/sec)
9.60	7/740	0.014	7.74	14.3

## b) drest Elevation of Coffer Dam

The necessary elevation of coffer dam can be obtained from the recessary head for tunnel flow as shown belows;

	el flow	Necessary Head at Tunnel Front <u></u>
	Velocity Head	at Tunnel Front <sup>±/</sup>
(m/sec)	(m)	(m)
14.3	10.4	15.6

Necessary Elevation,		
Necessary Elevation 2/ at Tunnel Front 2/	Free board	Top of Coffer dam
(m)	(m)	(EL-m)
222.6	2.4	225.0

1/150% of tunnel velocity head 2/ Invert of tunnel entrance = EL 207.0 m

stability Analysis of Gravity Dam Table 4D-3 •

		2	8, 625 7, 423 5, 606 5, 477 5, 477		N 41.879 23.746 16.458 10.656 9.303 8.319 7.558 7.558		N 359, 904 255, 593 14, 595 11, 611 9, 797 7, 592 8, 528 7, 592		N 239.740 58.373 28.292 18.924 18.623 10.427 10.427 10.427 9.204		N 160.488 128.149 105.210 79.286 71.601 65.157 71.601 59.829	:	*
		00-00 00-00 00-00	52, 559 62, 898 72, 459 81, 985 91, 505		SD 10, 661 16, 398 16, 398 24, 545 33, 456 33, 456 54, 135 58, 135 58, 319 56, 214		50 5.7392 5.7392 8.7395 16.7396 16.7395 23.137 23.137 23.137 23.137 23.137 23.137 53.428 53.428 53.428		SD 1.565 3.915 3.915 10.030 17.608 34.955 34.955 34.955 51.303		80 -5.160 -5.769 -5.875 -1.703 -10.875 -10.875 -10.875 -10.875 -10.875 -10.875	ł	50 0. 367 1. 475 1. 8356 1. 8356 1. 8356 5. 029 9. 5356 12. 6329
			2.758 2.758 3.946 5.430 7.084		su 17. 498 19. 739 20. 922 21. 898 23. 521 26. 084 295 32. 374		SU 25, 758 29, 734 31, 736 32, 758 32, 758 32, 559 33, 175 35, 175 37, 242		50 23.585 34.618 37.526 39.648 40.894 40.894 45.381 48.334		su 35.779 47.576 47.576 47.576 70.898 70.898 77.301 83.274 90.595 98.732	i	50 54,051 54,051 54,054,054 55,054 76,350 83,095 90,504 90,504
Н=0.88 Nl=0.0 HF=27.00 N2=0.20		-106.06 -369.06 -964.76	2013,042 -3001,125 -6194,941 -9377,719 -13459,426		SM 48.649 51.809 -98.253 -98.253 -98.979 -1176.438 -2191.448 -3395.230		SM 144.904 324.524 409.524 409.528 287.998 -161.443 -979.735 -2235.391 -2235.391		SM 199. 361 476. 052 745. 697 924. 859 917. 478 710. 729 710. 729 710. 729 710. 729		5M 277.047 827.067 1789.781 3298.316 5174.844 7610.523 10849.355 15022.941		SH 224, 002 693, 921 1516, 435 2805, 936 4362, 995 6358, 492 9011, 992 12431, 316
Fillet		5H -79.72 185.16 338.82	-350, 272 -789, 643 -1087, 983 -1435, 213 -1831, 206		8H -42.821 -113.771 -222.221 -366.170 -351.620 -772.570 -1031.020 -1326.970		SH -20.100 -77.231 -177.231 -177.231 -177.231 -735.99 -735.972 -735.972 -735.972 -1324.031		SH -7.538 -49.988 -129.938 -247.387 -402.337 -402.337 -824.787 -1092.187		SH 11. 302 21. 384 35. 343 53. 179 75. 109 101. 758 103. 166 133. 166 133. 166	i	
ning Point of	0. 150		521.074 904.081 1258.380 1675.730 2156.131	0.0	8N 130.094 246.454 410.114 621.074 904.081 1258.380 1675.730 1675.730 2156.131	0.075	SN 143.911 262.779 428.947 642.415 926.333 1280.861 1598.439 2179.067	D. O	6N 143.911 262.779 428.947 642.415 926.333 1280.861 1280.861 1598.439 2179.067	0.075	5N 150.698 285.118 471.238 709.058 1001.457 1356.777 1775.547 2257,767	0.0	150.698 285.118 2709.698 201.238 1001.457 1356.777 1356.777 1775.547 2257.767
est to Beginn	KG*1 K= 0	00 N	22, 440 27, 540 32, 940 38, 340 43, 740	KC=2 K= (	T 9.240 13.640 18.040 22.440 22.440 32.940 38.340 38.340 43.740	KC#1 KH	T 9,240 13,540 18,640 18,040 18,040 22,440 32,540 32,540 32,540 32,540 32,740	KC=2 K= 1	T 9.240 13.640 13.640 18.040 22.440 22.440 332.940 332.940 332.340	KC=1 K= -	T 9.240 13.640 18.040 22.440 22.440 32.940 332.940 38.340 43.740	¥ "	13.240 13.540 13.540 18.040 22.440 22.540 32.940 33.940 53.740
Downstream Slope Upstream Slope Distance from Cre Slope of Fillet	KA-1 KB-1	ពេលពេរ ភ្នំពេំដំ	23, 500 30, 500 40, 500 45, 500	KA=1 KB=1	× 10.500 10.500 10.500 20.500 25.5000 25.500 25.500 25.500 25.500 25	KA≖1' KB⊭2	× × 15.500 20.500 25.500 25.500 40.500 40.500 40.500	KA=1 KB=2	x 15.500 20.500 25.5000 25.5000 25.5000 25.5000 25.5000 25.5000 25.5000 25.5000 25.5000 25.5000 25.5000 25.5000 25.50000 25.50000000000	KA=1 KB=3	x 10.500 25.5000 25.5000 25.5000 25.5000 25.5000 25.50000 25.50000000000	KA≖1 KB=3	4 4 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
S D U D	-	K=0,15			K=0.0	-		_		- 920 920		K=0.0	
	Condition Full water	Earthquake,		Full water	carthquake,							Empty Earthquake, 1	

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2.000	7.700	7.700	2.350	1.000	0.500	0.200	1.000	180,000
HIGH-WATER-LEVEL	LOW-WATER-LEVEL	ELEVATION OF SEDIMENT	UNIT-WEIGHT OF CONCRETE	UNIT-WEIGHT OF SEDIMENT	ő	COEFFICIENT OF UP-LIFT	COEFFICIENT OF SLIDE	ALLOWABLE SHEARING-STRESS

- Note:

- :: Dam height (m)
  : Bottom width of dam (m)
  : Vartical force (ton)
  : Horizontal force (ton)
  : Moment (ton.m)
  : Vartical stress at upstream toe (ton/sq.m)
  : Vartical stress at downstream toe (ton/sq.m)
  : Safety factor for sliding shearing friction

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# B. Fiversion Dams

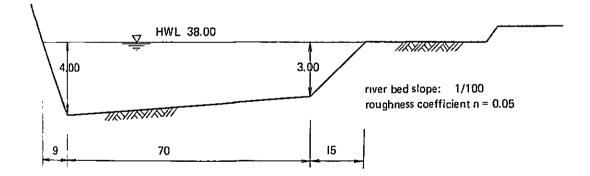
The diversion dams, Madupayas and Tibangran diversion dams, are hoppsed in the project. The subsequent paragraph gives the hydraulic disculation for determining major dimensions of the facilities in case of Tibangran diversion dam.

. De Lan Conditions

Intake discharge:	Q = 7.71 cu.m/sec
High-water discharge:	Qf = 950  cu.m/sec
Intake water surface:	NWS. 36.50 m
Dam bed elevation:	EL. 34.15 m
Dam crest elevation:	NWS. 36.50 + 0.15 = 36.65 m
Weir type:	Floating type

### ... Fresent High-Water Level

Frecent high-water level can be estimated depending on the prepert typical cross section of river at the proposed site as shown whom:



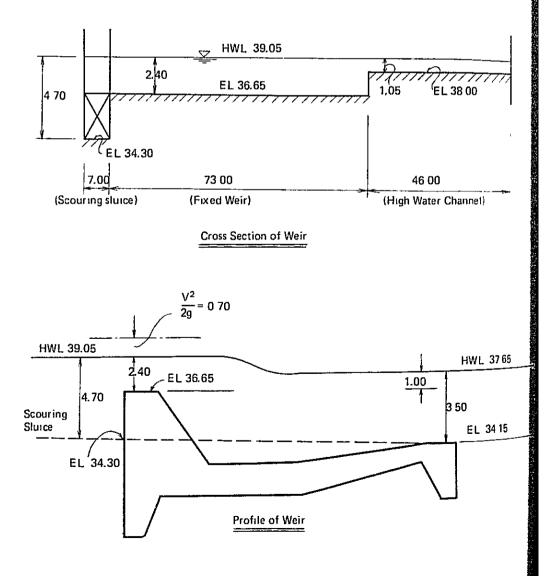
acw, when high-water level is assumed at WL 38.0 m, total distrange of the section is estimated at 1,188 cu.m/sec, by applying the "anning's formula.

 $A_1 = 4 \times 9 \times 1/2 = 18 \text{ sq.m}$   $A_2 = (4 + 3) \times 1/2 \times 70 = 245$   $A_3 = 3 \times 15 \times 1/2 = 22.5$   $\Sigma A = 285.5 \text{ sq.m}$ 

P = 9.8 + 70 + 15.3 = 95.1 m  $R = 285.5/95.1 = 3.00, R^{2/3} = 2.08$   $V = \frac{1}{0.05} \times 2.08 \times \left(\frac{1}{100}\right)^{1/2} = 4.16 \text{ m/sec}$   $Q = 285.5 \times 4.16 = 1,188 > 950 \text{ cu.m/sec}$ So, high-water level is decided at WL. 38.0 m.

## 3. Future High Water Level

Future high water level after completion of the diversion  $da_{n_i}$  can be estimated by using the proposed section of weir.



Appendix 4D-6 Page 3

Approaching velocity:

$$A_{1} = 7.00 \times 4.70 = 32.9 \text{ sq.m}$$

$$A_{2} = 73.00 \times 2.40 = 175.2$$

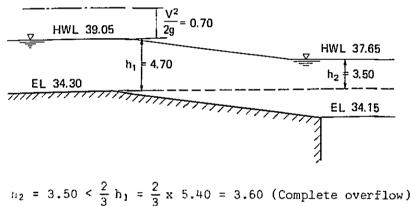
$$A_{3} = 46.00 \times 1.05 = 48.3$$

$$\Sigma A = 256.4 \text{ sq.m}$$

$$V = \frac{0.50}{256.4} = 3.71 \text{ m/sec} \qquad \frac{V^{2}}{2g} = \frac{3.71^{2}}{19.6} = 0.70 \text{ m}$$

oming Sluice

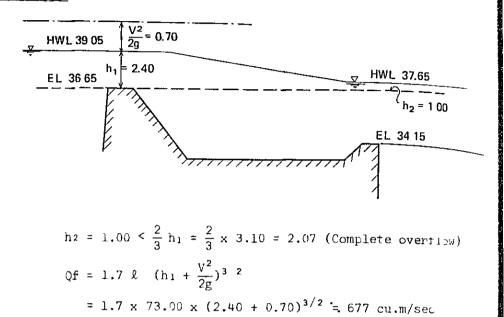
whe



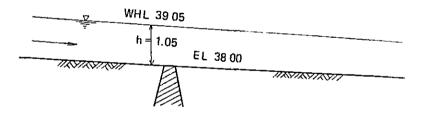
$$v_{n} = 1.70 \text{ Lm } (h_{1} + \frac{V^{2}}{2g})^{3/2}$$
  
= 1.70 x 6.62 x (4.70 + 0.70)^{3/2}  
`= 141 cu.m/sec  
re; bo = 6 - 0.04 nh\_1

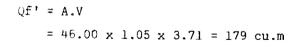
 $= 7.00 - 0.04 \times 2 \times 4.70 = 6.62$ 

Fixed Weir



High-Water Channel



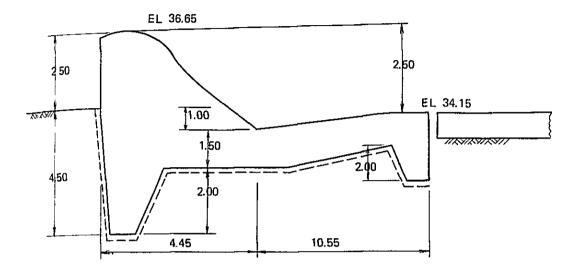


Total discharge;

 $\Sigma Q = Qm + Qf + Ff' = 141 + 677 + 179 = 997 > 950 cu.m/sec$ 

Therefore, back water shall be determined at HWL 39.05  $\ensuremath{\texttt{m}}$  assumed.

4. Lesign of Fixed Weir



```
=) length of Fore-apron

Fy Bligh Method;

lf_1 = 0.6 \cdot C \sqrt{D_1}

= 0.6 \times 9 \times \sqrt{2.50} = 8.53 < 10.55 \text{ m}

Length = 10.55 m
```

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.) rling (Creep Length)
```

By Bligh Method;

 $S = C \cdot \Delta h$ = 9.0 x 2.50 = 22.50 m S' = 4.50 + 2.00 + 15.00 + 2.00 = 23.50 mS < S' - 0.K

By Lane Method;

L =  $C \cdot \Delta h$ = 3.5 x 2.50 = 8.75 L' = (4.50 + 2.00 + 2.00) + 1/3 x 15.00 = 13.50 m L < L' 0.K c) Thickness of Fore-apron

$$T_{a} = \frac{4}{3} \times \frac{\Delta h - hf}{r - 1}$$
$$= \frac{4}{3} \times \frac{2.50 - 1.16}{2.3 - 1} = 1.37 < 1.50 m$$
$$hf = \frac{\Delta h}{S} \times 5^{+} = \frac{2.50}{23.50} \times (4.50 + 2.00 + 4.45) = 1.16 m$$
Thickness = 1.50 m

d) Apron Protection Works

By Bligh Method;  $l = 0.67 \text{ C } \sqrt{D_1 q}$   $l \text{fr} = l - l \text{f}_1$   $l = 0.67 \times 9 \times \sqrt{2.50 \times 9.3} = 46.22 \text{ m}$ where;  $q = \frac{677}{73} = 9.3$  l fr = 29.08 - 10.55 = 18.53 mLength = 20.00 m

- 5. Design of Scouring Sluice
- a) Elevation

Elevation of scouring sluice shall be determined based on teaveraged river bed slope of the stream center line after construction diversion dam. Accordingly, the elevation was calculated at EL 5-... based on the averaged river bed slope derived from the elevation of the 100 m upstream point and the 150 m lowerstream point of the famsite.

b) Design Discharge for Flushing Sediment

In order to flush away sediment even during irrigation period, the normal water discharge in irrigation periods (Qo = 13.0 cu.m/cc.', is adopted.

```
3) Feculired Water Velocity for Flushing Sediment
Vc = 1.5 C √d
where; Vc: required velocity (m/sec)
C: coefficient by sand/gravel condition 4.5
d: max. particle size of sediment (m)
Vc = 1.5 x 4.5 x √0.15 = 2.61 m/sec
```

## ) Lith

Lunc = 
$$\frac{Q_0}{q}$$
  
 $q = \frac{Vc^3}{g}$   
where; Lunc: width (m)  
 $q$ : traction discharge per unit width (cu.m/sec/m)  
 $g$ : acceleration of gravity (m/sq.sec)  
 $Q_0$ : design discharge for flushing away sediment  
(cu.m/sec)  
Vc: required water velocity for flushing away  
sediment (m/sec)  
 $q = \frac{2.61^3}{9.8} = 1.81$  cu.m/sec/m  
Lunc =  $\frac{13}{1.81} = 7.18$  m  
width = 7.00 m x 1 set

#### -† Nope

The slope is determined to secure the critical velocity in the "ouring sluice canal, setting the control point on the upstream end i this canal as follows:

$$Ic \ge \frac{n^2g}{hc^{1/3}}$$