APPENDIX 6

PHASING OF PROPOSED BRIDGES

Sheet 1 of 9		2000				7	8	p≈t	god
Shee	DECIEM AND CONCIDION DECYMENTS	descend Color	. No topographic survey data	. No topographic survey data	. No picture , No topographic survey data	. Topographic and geological surveys are required Study on flood control is necessary Use of cofferdam for deep water (h=3.5 m) is required Long span bridge is advisable because of deep water	. Topographic and geological survey are required. . Use of cofferdam for deep water {h~2.0m} is required.	. No difficulty in construction because of ordinary types of abutments (2) and pier (1).	. No special difficulty in construction . Use of cofferdam in water (h*1.0m) is required.
	PROPOSED BRIDGE	TYPE				Continuous steel girder Pile foundation	. H-beam girder . Pile foun- dation	. H-beam gfrder . Pile foun- dation	. H-beam girder . Pile foun- dation
	PROPOSE	СЕМОТН ІМ Э				з @ 30≖9С ш	17417=34 m	23+23=46 m	25+25×50 m
	ы	LOAD LIMIT (TONS)	10	ហ	ស	•	ស	દ	ıs
	EXISTING BRIDGE	CONDITION	Bailey Fair Steel	Timber . Oilapi- dated timber trestle	Steel Struss	Timber . Dilapi- dated timber trestle	Bailey . Oilapi- dated timber trestle	Balley Ollapi- dated Elmber trestle	Timber . Serfously dilapi- dated
	EX	LENGTH (m)	24.40	30.00	48.80	90.06	30.00	39.63	48.00
•	TRAFFIC VO: 11MF	(ADT)	53		237	281.	261	ţ	281
Š	NAME	BRIDGE	Ellet Bridge Benguet	Birmilog 8 Br. Hocos Sur	Malaya Br. Ilocos Sur	Sta. Cruz Bridge Cagayan	Dumadata Br. Quirino	Baan Br. No. 2 Nueva Vizcaya	Diora Br. Cagàyan
	BRIDGE	Š.	10.10	01.02	01.03	02.01	02.02	02.03	02.04
	Ş			2	•	Ħ	rð.	φ.	

Sheet 2 of 9	0110	הוצעוול	N	y di silanda kunininda kungsangan pengunjungka dalah dalah 44	na na manana ing kalangan na manana na m	and the second s		2	
	CTREMENT OF THE PROPERTY OF TH	DESIGN AND CONSTRUCTION REGUREMENTS	. Study of flood area and control is required. . Bridge length should be studied		. Topographic survey does not show the alignment of existing road and river			. Flood water level shall be studied . Topographic and geological survey is required Alignment of road shall be studied in order to avoid demolision of existing houses.	. Proposed widening with concrete girder is recommended
מחסתואם חייסר	D BRIDGE	TYPE						. H-Beam Girder Spread Footing	
	PROPOSED BRIDGE	LENGTH (m)	:					3 @ 25~75m	
	ı	LOAD LIMIT (TONS)			e	j	•	и	in ed
	EXISTING BRIDGE	CENSTH AND	Timber (Washed- Out)	Timber . Destroyed	Timber Dilapi- dated	Timber • Destroyed	Timber · . Destroyed	Spillway Over- flow meter	A.C.D.G. Defect- Ive super- structure
	EX	LENGTH (m)	30.00	34.00	12.00	12.00	36.00	80.00	
	THAFFIC	(ADT)	797	1	•				
	NAME	BRIDGE	Olduyon Br.	Segum Br. Nusva Ecija	Calabasa Br. Rueva Ecija	Malinao Br. Nueva Ecija	Asam Br. Nueva Ecija	Binambang Bridge Batangas	Mango Br. Rizal
	BRIDGE	o O	50.20	8 6	03.02	63.03	03.04	04.018	94. æa
,	Ş	į	æ	Ø	P	e-1	13	es es	I.

SES	
O BRIDGES	
PROPOSED BE	
020	
2002	
PHASING	
:	

	TRAFFIC	Market	EXISTING BRIDGE	tu	PROPOSE	PROPOSED BRIDGE	CANDRIDGE NORTH INCOME TO SEE MAINTENANT SEE MAINTE	
	(ADT)	LENGTH (m)	LENGTH AND CONDITION	LOAD LIMIT (TONS)	LENGTH (m)	TYPE	DESIGN AND CONSTRUCTION REQUIREMENTS	PHASING
Leviste II Br Batangas	520	40.00	Timber (washed- out)	•	20+20+20 +20 = 80 m	. H-Beam girder . Spread foundation	. Maximum high flood water level shall be reviewed	~
Lumang Bayan Br. Mindoro Occ.	208	60.00	Balley Fair Steil Offapi- dated timber trestle	ka	3 @30 1 30 m	. Continuous steel girder . Pile foun-	. Study on flood area and elevation is required	
Olengoan Br. Palawan		36.00	Bailey Fair Steel Timber	w	20+20 = 40 m	. H-Beam Girder . Pile foun- dation	. Geological survey is required . Use of cofferdam for water is required	2
, <u>, , , , , , , , , , , , , , , , , , </u>	8r. 153	351.00	Bailey Fair Steel Permanent sub-	8	. Depend on existing span length	. Depend on existing pier	. Stability of existing substructure shall be checked	N
•	Ofpulao Br. 50 Palawan	30.00	Bailey Fair Steel Dilapi- dated timber	IC	25 h	. Skewed H-Beam girder Pile foun- dation	. No difficulty in construction	po#
, cn i	Cogon Bridge Romblon	20.00	Bailey Fair Steel Dilapi- dated timber	ĸ	23 m	. H-Beam girder . Spread founda- tion	. No difficulty in construction	p-4
Ouguit Br. Camarines Norte	1561	30.00	. Sted F-Sed Fair	50			. Urgent replacement is not recommended . Coping of piers shall be remedied	-Andrews and Anthony and A

4 04 9	SAN SALIO		1	2	10 10 10 10 10 10 10 10 10 10 10 10 10 1	~	2	• ••	
20043	SECTION OF THE STATE OF THE SECTION		. Mo difficulty in construction	. Bridge length shall be examined considering river bank	. Steel of baily is fair and substructure is permanent . Construction of bridge approach is recommended	. No difficulty in construction	. Geological survey is required because of swampy and soft ground condition . Use of cofferdam for deep water (h=2.0m) is required	. No difficulty in construction	. Urgent replacement of superstructure might not be recommended . Stability of substructure shall be checked
	PROPOSED BRIDGE	TYPE	. H-Beam girder . Spread type foun- dation	. Conti- nuous steel girder . File foun- dation		. H-Beam girder . Pile foun- dation	. Steel plate girder . Pile foun- dation	. H-Beam girder . Pile foun- dation	
	PROPOSE	LENGTH (M)	20-m	2 @ 35-/0 м		20+20 - 40 m	28 3	21+21+42 m	
	Lt)	LOAD LIMIT (TOWS)	2	est	07	- m	50 60	•	r
	EXISTING BRIDGE	LENGTH AND CONDITION	Balley	. Bailey . Dilapi- dated timber trestle	Bailey No bridge approach	Bailey Fair Steel Timber trestle	Timber Oflapi- dated	Bailey . Des- troyed	Baidey Stair Steel Perma- nedt subs
	EX	LENGTH (m)	20.00	45:00	40.00	39.00	25.00	20.00	30.00
	TRAFFIC	(ADT)	624		2420	390	526	03	92
	NAME	BRIDGE	Patitinan Br. Camarines Sur	Narangasan i Bridge Nasbate	Talus Bridge Negros Occ.	Cataan Br. Iloilo	Iyang Sr.	Guintas Br. Capiz	Tumalalud Br. Capiz
	BRIDGE	2	05.02	05.03	10.00	20.30	£0.40	06.04	06.05
	Ş		22	8	Ž.	\$2	26	2	28

PHASING OF PROPOSED BRIDGES

Sheet 5 of 9		radoline	8	8	gard .			elappas programa, seria de la composição	
		DESIGN AND CONSTRUCTION ACCORDENENTS	. Geological survey is required . Study of flood area is required	. Geological survey is required . Maximum high flood water level shall be reviewed	. No difficulty in construction	. No difficulty in construction	. No difficulty in construction	. No difficulty in construction	. No difficulty in construction
PHASING OF PROPOSED BRIDGES	PROPOSED BRIDGE	有文章	. Steel plate girder . Pile foun-	. H-beam girder . Pile foun- dation	. H-beam girder Pile foun- dation	. H-beam girder . Pile foun- dation	H-beam glrder Pile foun- dation	. H-beam girder . Pile foun- dation	. H-beam girder . Pile foun- dation
NG OF PROP	PROPOSE	LENGTH (m)	30, m	24°м	12 m	18+18 = 36 m	19+19 и 38 и	22° m	23.m
PHAS	ш	LOAD LIMIT (TONS)	រភ	. Lo	m	10	S	LC	
	EXISTING BRIDG	LENGTH AND CONDITION	Timber . Dilapi- dated	Balley Fair Steel Ollapi- dated trestle	Balley . Dilapi- dated timber trestle	. Timber	. Timber. . Bad condi- tion	. Timber . Bad condition	Balley Unpass- able due to dila- pidated steel member
	Ŋ	LENGTH (m)	25.38	20.83	12.6	35.00	33.78	18.00	21.65
	TRAFFIC	(ADT)	25	\$	66	207	50	96	. 1
	NAME	BRIDGE	Banban Br. Cebu	Campa cas Bridge Cebu	Campanga Bridge Cebu	Camachiles Bridge Toledo City	Lagnason Br. Cebu	Poray Br. E. Samar	Iba Bridge Samar
	BRIDGE	o S	0.70	07.02	07.03	07.04	07.05	08.01	08.02
	Ş	·	58	8	eri eri	25	671 F7	Ħ	88

Sheet 6 of 9

	PHASING	2	2	***	***	.	~ *	rd
	DESIGN AND CONSTRUCTION REQUIREMENTS	. Geological survey is required . Study of flood area is required	. Topographic and geological surveys are required . Study flood area and control is required	. No difficulty in construction	. No difficulty in construction	. No difficulty in construction	. No difficulty in construction	. No difficulty in construction
D BRIDGE	7 7 P.E	. H-beam girder . Pile foun- dation	. H-beam girder . Pile foun- dation	. H-beam girder . Pile foun- dation	. H-beam girder . Pile foun- dation	. H-beam glrder Pile foun- dation	. H-beam gfrder . Pile foun- dation	H-beam girder Pile foun- dation
PROPOSED BRIDGE	LENGTH (m)	22+22+22=66m	27+27 = 54 m	. 16. 28.	23°m	17+17 = 34 m	19+19 p 38 m	20+20 # 40 m
ы	LOAD LIMIT (TONS)	7			m	3	ហ	
EXISTING BRIDGE	LENGTH AND CONDITION	Bailey Good Timber trestle	River Crossing . No exis- ting bridge	Timber Bad condi-	Timber Bad condi- tion	Timber . Deterio- rated condi-	Bailey Fair steel Timber trestle	Balley : Fair steel : Timber trestle
EX.	LENGTH (m)	61.45	51.40	13.70	15.40	45.00	35.50	25.00
TRAFFIC	(ADT)		•	B	340	290	290	21.9
NAME	вяюсе	Habay Br. S. Leyte	Talisayan River Crossing Leyte	Pinucawan Br. Leyte	Batungal Br. Basilan	Mangop Br. Zamboanga del Norte	Canawan Br. Zambanga del Norte	Piangon Br. Zamboanga del Norte
BRIDGE	og .	08.03	08.04	96.95	09.01	20°60	20-50	09.04
2	į	Ş	37	es es	S E	40	\$	\$

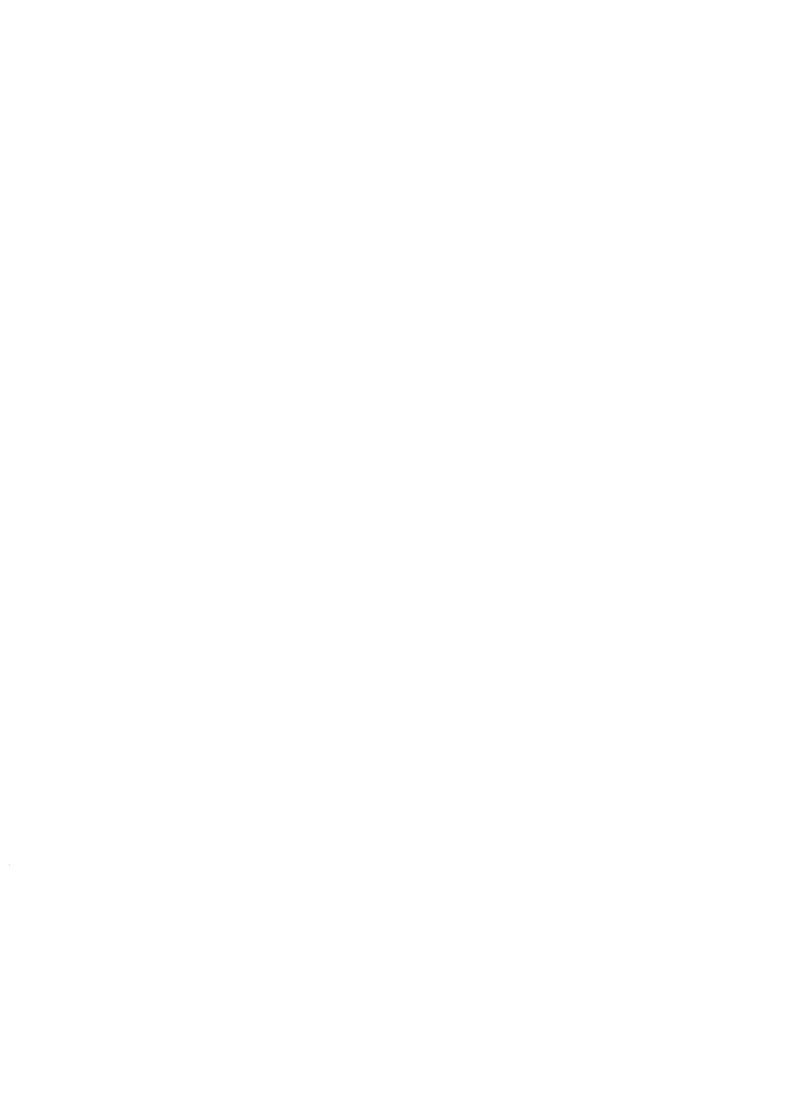
H-beam Stability of existing permanent substructures girder shall be examined and incorporated in design effector. Stability of existing permanent substructures girder Geological survey is required dation. Use of cofferdam for deep water is required foundation. No difficulty in construction girder. Spread foundation. No difficulty in construction dation. H-beam girder Spread foundation. No difficulty in construction dation. H-beam girder. Spread foundation. No difficulty in construction dation. No difficulty in construction dation. H-beam girder with the dation. No difficulty in construction dation. Hebeam girder with dation. No difficulty in construction dation. Hebeam girder with dation. No difficulty in construction dation.	TRAFFIC EXISTING BRIDGE	NAME TRAFFIC EXISTING BRIDGE	EXISTING BRIDGE	EXISTING BRIDGE	546	546		PROPOSE	PROPOSED BRIDGE	DESIGN AND CONSTRUCTION REQUIREMENTS	PHASING
H-beam Stability of existing permanent substructures girder shall be examined and incorporated in design elicity from the examined and incorporated in design elicity from the end of cofferdam for deep water.is required dation H-beam Girder No difficulty in construction H-beam H-beam girder Spread foundation H-beam girder Spread foundation H-beam girder Spread foundation H-beam girder Spread foundation will dation will difficulty in construction dation H-beam girder girder will difficulty in construction dation dation will defice the foundation will define the dation will defice the foundation will define the foundation will define the foundation will define the foundation will be will be foundation will be foundation will be foundation will be	BRIDGE	BRIDGE (ADT) LENGTH (m)	LENGTH (m)		CONDITION CONDITION	_	LOAD LIMIT (TONS)	CENOTH (m)	TYPE		
H-beam girder H-beam girder H-beam girder H-beam girder H-beam girder Spread foundation H-beam girder Spread foundation H-beam girder Spread foundation H-beam girder Spread foundation H-beam girder	Patunan Br. 667 25.00 timber trestle	667 25.00	25.00		Balley Fair steel Permanent pler timber trestle			25° m	. H-beam girder	. Stability of existing permanent substructures shall be examined and incorporated in design	N
H-beam girder Spread foundation H-beam girder Spread foun- Spread foun- Spread foun- H-beam girder H-beam girder H-beam girder H-beam girder H-beam girder H-beam girder Gation H-beam girder H-beam girder Gation H-beam girder Gation H-beam girder Gation H-beam girder Gation	Hayangabon I Timber 10.01 Bridge 55 40.00 dated condition	55 40.00	40.00	F.	Timber . Dilapi- dated conditio	<u> </u>	ឆ	21+23·m 42 m	. H-beam girder . Pile foun- dation		2
. H-beam girder Pile foun- Albeam girder Spread foun- A-beam girder H-beam girder Pile foun- Aation H-beam girder H-beam girder H-beam girder Relief foun- Aation Aation Aation Abeam Abea	Maradugao Br. 1319 21.00 . Bilapi- Bukidnon 1319 21.00 . Dilapi- chted timber trestle	1319 21.00	1319 21.00		Dailey Fair stee Ollapi dated timber trestle		ភេ	25.≄	. H-beam girder . Spread foundation		**4
. H-beam girder . Spread foun- dation . H-beam girder . Pile foun- dation . H-beam girder . H-beam girder . H-beam dation . Mo difficulty in construction dation . dation . Adation	Maundo Br 18.00 . Dilapi- 10.03 Agusan del 18.00 dated Sur timber	Maundo Br. Agusan del 18.00 · Sur	18.00 ·		Bailey Fair steel Oflapi- dated timber trestle		ى	£			p-1
. H-beam girder . No difficulty in construction dation . H-beam girder . No difficulty in construction dation . Pile four . No difficulty in construction dation	Sta. Irene Br. 20.00 . Unpass-Sur	Sta. Irene Br. Agusan del - 20.00 Sur	- 20.00		Log Bridge . Unpass- able		3	E	. H-beam girder Spread foun- dation		p=d
. H-beam girder m . Pile foun- dation	Timber Timber 10.05 Malubog Br. 362 25.00 ' Dilabi-dated condition	Malubog Br. 362 25.00 '	7 25.00	}~- _*	Timber , Dilapi- dated conditio	E	L/s			. No difficulty in construction	pr-¢
	Lambunao Br. 40.00 Balley Sur Sur	Lambunao Br. Surigao del - 40.00 Sur	40.00		Bafley		ř		. H-beam girder . Pile foun- dation		pod

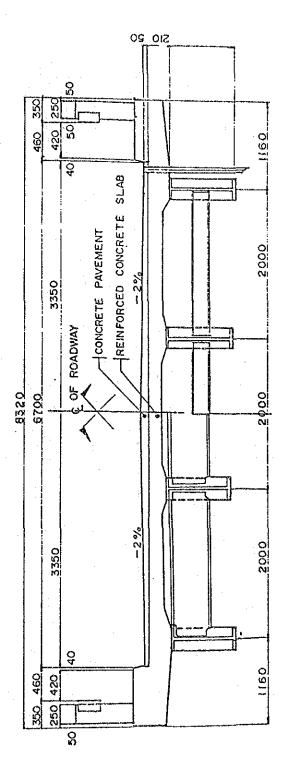
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Sheet 6 of	0380	0300000	. "	•	2		2	0	••
	DECIEN AND PONCTEMENTON DECHEORMENTS		. Mo data	. No difficulty in construction	. Stability of permanent substructure shall be checked	. No data	. Maximum high water leyel shall be checked	. Stability of permanent substructure shall be checked	. Midifficulty in construction
	PROPOSED BRIDGE	TYPE		H-beam ringer pile feundation	. Depend on existing pier. condition		. H-beam girder . Pile foun- dation	. Depend on existing pler condition	. H-beam girder Spread foundation
	PROPOSE	LENGTH (m)		20~20 = 40 교	. Demand on existing span [*] length		EE [2	. Depend on existing span length	25-25 = 50 m
	bi .	LOAD LIMIT (TONS)	ı	ພ	ហ	5	es	L O	G
	EXISTING BRIDGE	LENGTH AND CONDITION	Timber	Timber Deterfora- tion steel and timber trestle	Balley Fair Steel Permanent sub- structure	Balley	Bailey	Bailey Fair steel Permanent Sub- structure	"Bailley "Dilapi- dated condition
***************************************	ω	LENGTH (m)	36.00	36.80	42.67	72.00	20.00	40.00	45.00
	TRAFFIC	(ADT)		0.22	450	•	9,4	•	758
, i.e.,	NAME	BRIDGE	Balibadon Br. Surigao del Sur	Calabanit Br. South Cotabat	Manay Bridge Davao Oriental	Culaman I Br. Davao del Sur	Pikinit Br. Lando del Norte	Durugao Br. Magufndanso	Uplan Bridge North-Cota- bato
	BRIDGE	20	11.02	11.03	11.04	11.05	12.01	12.02	12.03
	Š		င္အ	51	ß	୧୨	<mark>ቖ</mark>	₩.	55

CHESTER	rapsing	N	N		TO MAKE AND	Militah (pagyikusin kecintah paku pagyangan
DECISION AND CONCEDITION DESIGNATIVE	DESIGN AND CONSTRUCTION REGULARINGS	. Birection of river stream was changed . Study of flood is required	 Stability of existing permanent substructure shall be checked. 			
BRIDGE	TYPE	. H-beam girder . Pile foun- dation	. Depend on exis- ting pier			•
PROPOSED BRIDGE	LENGTH (M.)	24 m	. Depend on existing span. length			
ឃ	LOAD LIMIT (TONS)	o	10			
EXISTING BRIDGE	LENGTH AND CONDITION	ī faber	Bafley Fair Steel Perma- nent sub- structure			
EX	LENGTH (m)	25.00	100.00			
TRAFFIC	(ADT)	9.2	989 •			
NAME OF	BRIDGE	Dangolaan Bridge Lanao del Norte	Sapakan Br. Maguindanao	:		
BRIDGE	ġ	12.04	8.2.2			
Ş	:	57.	58			,



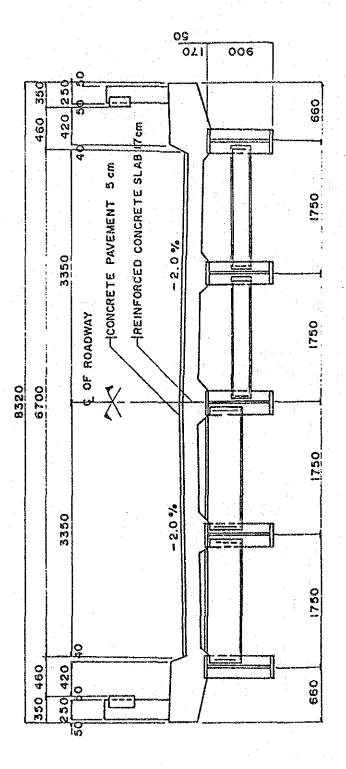
APPENDIX 7 DESIGN ANALYSIS OF SUPERSTRUCTURES





SUPERSTRUCTURE CROSS SECTION scale: SPAN L = 12,16,17,18,19,20,21,22,23 M

FIGURE 1 SUPERSTRUCTURE CROSS SECTION (L=12 - 23)



SUPERSTRUCTURE CROSS SECTION SPAN L = 25 m.

FIGURE 2 SUPERSTRUCTURE CROSS SECTION (L=25)

2. MAIN GIRDERS SECTION AND STRESS

Main girder sections are determined at G.1.

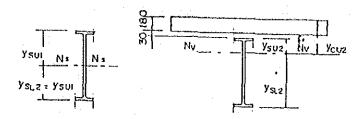


FIGURE 3

TABLE 1 STRESS OF GIRDER (L=12,16,17,18,19)

	pan L)	12	16	17	18	19
	rder ize	H790x300	H700×300	H700×300	H792×300	H800×300
Before Composite Sec	Is As Ysu Ysu	201.000 235.500 35.000 35.000	same to L = 12 m	same to L = 12 m	254.000 243.400 39.600 39.600	292.000 267.400 40.000 40.000
After Composite Sec.	Iv Av Yeuz Ysuz Ysez	580.100 785.500 23.090 2.090 67.910			717.700 791.100 24.880 3.880 75.320	793.400 816.700 26.030 5.030 74.970
	σc	23.100	46.200	53.100	49.800	52.100
Stress	gze	425.000 1007.000	749.000 1689.000	843.000 1886.000	872.000 1875.000	870.000 1835.000

TABLE 2 STRESS OF GIRDER (L=20,21,22,23,25)

Span (L)		20	21	22	23	25
	rder ize	H890x299	н900х300	H900x300	H912x300	H900x300
e Sec	Is	345.000	411.000		493.000	411.000
Before posite	As	270.900	309.800	Same to	364.000	309.800
Bef(Compos	Ysu	44.500	45.000	L = 21 m	45.600	45.000
Š	Ys L	44.500	45.000		45.600	45.000
After Composite Sec.	Iv Av Yeuz Ysu Ys1	939.500 821.200 27.640 6.640 82.360	1069.800 860.100 29.530 8.530 81.470		1239.700 914.000 31.940 10.940 80.260	957.500 678.900 34.280 14.280 75.720
Stress	σc	49.800	50.200	53.200	54.300	67.500
St	์ ซรน	918.000	882.000	967.000	916.000	1025.000
	0se	1878.000	1758.000	1910.000	1744.000	1872.000

Notice: The bridges of which span length are from 12 m to 23 m consist of 4 main girders. The bridge $L=25\,\mathrm{m}$ have 5 main girders.

3. REACTION OF SUPERSTRUCTURE FOR ONE ABUTMENT

TABLE 3 REACTION OF SUPERSTRUCTURE

R: ton

				Earthquake				
Span	Vei	rtical Reac	tion	Longit	udinal	Lateral		
	Dead Load	Live Load	Total	Vertical	Hori- zontal	Vertical	Hori- zontal	
12	45.0	51.4	96.4	45.0	10.8	45.0	5:4	
16	60.0	55.8	115.8	60.0	14.4	60.0	7.2	
17	63.6	56.6	120.2	63.6	15.3	63.6	7.6	
18	67.6	57.4	125.0	67.5	16.2	67.6	8.1	
19	71.4	58.2	129.6	71.4	17.1	71.4	8.6	
20	75.0	59.0	134.0	75.0	18.0	75.0	9.0	
21	78.8	59.4	138.2	78.8	18.9	78.8	9.5	
22	82.4	60.0	142.4	82.4	19.8	82.4	9.9	
23	86.4	60.4	146.8	86.4	20.7	86.4	10.4	
25	86.2	61.3	147.5	86.2	20.7	86.2	10.3	

- 4. MOMENTS AND SHEARING FORCES OF MAIN GIRDER (Span Length $L = 12 \sim 23 \text{ m}$)
- 4.1 Loads

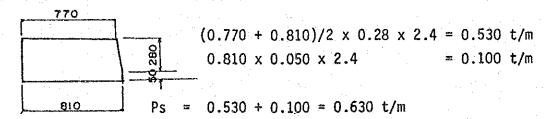
4.1-1 Dead Loads

(1) Hand Rail

Post
$$0.250 \times 0.250 \times 0.8 \times 2.4 = 0.120 \text{ t}$$

Beam $0.150 \times 0.300 \times 1.85 \times 2.4 = 0.200 \text{ t}$
 $P_{H} = (0.12 + 0.200)/1.85 = 0.175 \text{ t/m}$

(2) Side Walk



(3) Concrete Pavement

$$0.05 \times 2.4 = 0.120 \text{ t/m}^2$$

(4) Concrete Slab

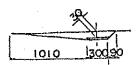
$$0.180 \times 2.4 = 0.432 \text{ t/m}^2$$

(5) Girder Weight

(6) Haunch

G.1
$$(1.4 + 0.3)/2 \times 0.03 \times 2.4 = 0.061 \text{ t/m}$$

G.2 $(0.72 + 0.3)/2 \times 0.07 \times 2.4 = 0.086 \text{ t/m}$





4.1-2 Live Loads

4.1-3 Impact Fraction

$$I = \frac{50}{\frac{L}{0.305} + 125}$$

$$L = Length of Meter$$

$$I : Impact Fraction$$

$$(But \le 0.3)$$

TABLE 4 IMPACT FRACTION

•		
Span (L)	Impact (I)	
12	0.300	
16°	0.282	
17	0.277	
18	0.272	
19	0.267	
20	0.262	
21	0.258	
22	0.254	
23	0.249	
25	0.242	

4.2 Bending Moment

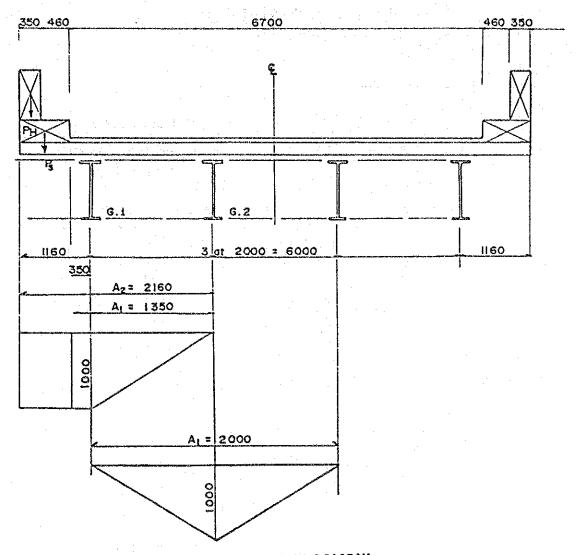


FIGURE 4 LOAD DISTRIBUTION DIAGRAM

4.2-1 Dead Load

G. I

Sidewalk Live Load Ww = $0.293 \times 0.460 = 0.135 \text{ t/m}$ Amount of the dead load and the sidewalk load moments are determined by the formula:

$$Md = 1/8.Wd.L^2 (t \cdot m)$$

Amount of the live load moments are determined by AASHTO (Appendix A)

TABLE 5 BENDING MOMENT OF G1

г		SCHOTHO HONCH!	01 01			M: t⋅m	
	Span	Before	Before After Composition				
	(m)	Composition	Dead Load	Live Load	Impact Load	Total	
				2.4			
-	12	23.3	17.4	24.4	7.3	51.5	
				4.3			
-	16	41.4	30.9	37.2	10.5	82.9	
				4.9	Ì		
-	17	46.7	34.9	40.8	11.3	91.9	
-				5.5			
 	18	52.4	39.2	44.1	12.0	100.8	
				6.1			
L	19	58.4	43.6	47.3	12.6	109.6	
				6.8			
L	20	64.7	48.4	50.6	13.3	119.1	
	·			7.4			
-	21	71.3	53.3	53.8	13.9	128.4	
				8.2			
_	22	78.3	58.5	57.1	14.5	138.3	
			•	8.9]		
	23	85.6	63.9	60.4	15.0	148.2	
				10.5			
L	25	101.1	75.5	66.9	16.2	169.1	

 $0.432 \times 2.0 = 0.864 \text{ t/m}$ Slab 0.086 t/mHaunch Girder 0.300 t/mWd1 = 1.250 t/m

Pavement $0.120 \times 2.0 =$ 0.240 t/mWd2 = 0.240 t/m

TABLE 6 BENDING MOMENT OF G2

M; t·m After Composition Before Span Dead Live Impact Total Composition (m)Load Load Load 51.2 4.3 22.5 36.1 10.8 12 55.1 15.5 78.3 16 40.0 7.7 45.2 16.7 17 8.7 60.4 85.8 17.8 92.8 18 50.6 9.7 65.3 99.5 10.8 70.0 18.7 19 56.4 62.5 12.0 74.9 19.6 106.5 20 20.6 113.6 21 68.9 13.2 79.8 14.5 120.7 84.7 21.5 22 75.6 127.8 82.7 15.9 22.3 23 89.6 97.7 99.2 24.0 142.0 25 18.8

4.2-3 Shearing Force

TABLE 7 SHEARING OF G1,G2

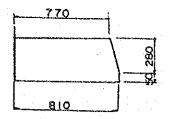
	OHLANIA.	MG OL 61'95	-			S: to	
Girder	Span	Before		After Comp			
	(m)	Composition	Dead Load	Live Load	Impact Load	Tota	
				0.8			
:	12	7.8	5.8	10.0	3.0	19.6	
				1.1			
	16	10.4	7.7	10.8	3.0	22.6	
				1.1			
	17	11.0	8.2	11.0	3.0	23.3	
				1.2			
	18	11.6	8.7	11.1	3.0	24.0	
G.1				1.3			
	19	12.3	9.2	11.2	3.0	24.7	
				1.4			
	20	12.9	9.7	11.3	3.0	25.4	
			-	1.4			
	21	13.6	10.2	11.4	2.9	25.9	
•				1.5			
	22	14.2	10.6	11.5	2.9	26.5	
				1.6			
	23	14.9	11.1	11.5	2.9	27.1	
	12	7.5	1.4	14.9	4.5	20.8	
	16	10.0	1.9	16.0	4.5	22.4	
	17	10.6	2.0	16.2	4.5	22.7	
	18	11.3	2.2	16.4	4.5	23.1	
G.2	19	11.9	2.3	16.6	4.4	23.3	
•	20	12.5	2.4	16.8	4.4	23.6	
	21	13.1	2.5	16.9	4,4	23.8	
	22	13.8	2.6	17.0	4.3	23.9	
	23	14.4	2.8	17.1	4.3	24.2	

- 5. MOMENT AND SHEARING FORCE OF MAIN GIRDER
- 5.1 Loads Span Length L = 25 m
- 5.1-1 Dead Loads
 - (1) Hand Rail

Post
$$0.250 \times 0.250 \times 0.8 \times 2.4 = 0.120 \text{ t}$$

Beam $0.150 \times 0.300 \times 1.85 \times 2.4 = 0.200 \text{ t}$
 $P_{H} = (0.12 + 0.200)/1.85 = 0.175 \text{ t/m}$

(2) Sidewalk



 $(0.770 + 0.810)/2 \times 0.28 \times 2.4 = 0.530 \text{ t/m}$ $0.810 \times 0.050 \times 2.4 = 0.100$

Ps = 0.530 + 0.100 = 0.630 t/m

(3) Concrete Pavement

$$0.05 \times 2.4 = 0.120 \text{ t/m}^2$$

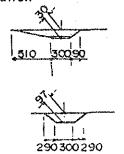
(4) Concrete Slab

$$0.170 \times 2.4 = 0.408 \text{ t/m}^2$$

(5) Girder Weight

0.300 t/m

(6) Haunch



G-1 $(0.9+0.3)/2 \times 0.03 \times 2.4 = 0.043 \text{ t/m}$ G₇₂ $(0.67+0.3)/2 \times 0.062 \times 2.4 = 0.072 \text{ t/m}$ G-3 $(0.88+0.3)/2 \times 0.097 \times 2.4 = 0.137 \text{ t/m}$

5.1-2 Bending Moment

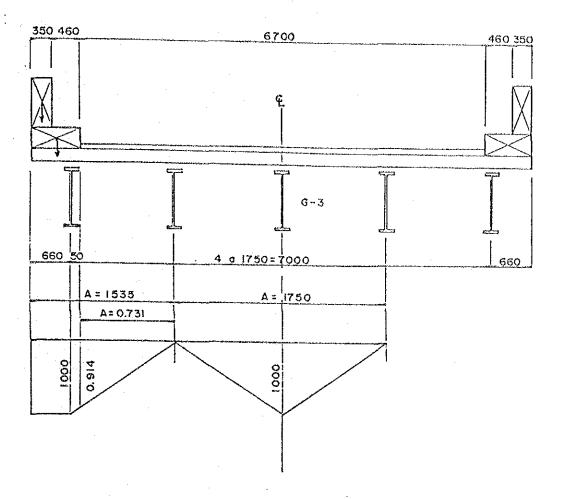


FIGURE 5 LOAD DISTRIBUTION DIAGRAMN

(1) Dead Load

<u>G-1</u>							
Slab	0.408 x	1.535	æ	0.626	t/m		
Haunch	•		#	0.043	t∕m		
Girder			æ	0.300	t/m		
**************************************		Wdl	==	0,969	1/ m		

Sidewalk Live Load Ww = $0.293 \times 0.46 = 0.135 \text{ t/m}$ Amount of the dead load and the sidewalk load moments are determined by the formula:

$$Md = 1/8 \cdot Wd \cdot L^2 (t \cdot m)$$

Amount of the live load moments are determined by AASHTO (Appendix A)

TABLE 8 BENDING MOMENT OF GI

(M: t-m)

Span	Before	Before After Composition				
(m)	Composition	Dead Load	Live Load	Impact Load	Total	
			10.5	anne e menemen promete une e e e e e e e e e e e e e e e e e		
25	75.7	69.8	41.6	10.1	132.0	

Note:

Before Composition

$$M = 1/8 \times 0.969 \times 25.0^2 = 75.7 \text{ t·m}$$

After Composition

M (D.L.) =
$$1/8 \times 0.893 \times 25.0^2$$
 = 69.8 t·m
M (L.L.) = $(166.2 \times 2)/7.0 \times 0.875$ = 41.6 t·m
M (L.W.) = $1/8 \times 0.135 \times 25.0^2$ = 10.5 t·m
M (L.I.) = 41.6×0.242 = 10.1 t·m

G.3

Slab = 0.408 t/m Haunch = 0.137 t/m Girder = 0.300 t/m Wd1 = 0.845 t/m

Pavement $0.120 \times 1.75 = 0.210 \text{ t/m}$ Wd2 = 0.210 t/m

TABLE 9 BENDING MOMENT OF G2

	Span	Before	After Composition					
ļ	(m)	Composition	Dead Load	Live Load	Impact Load	Total		
	25	66.0	16.4	83.1	20.1	119.6		

5.2 SHEARING FORCE

G.1

Before Composition

 $Sd1 = 1/2 \times 0.969 \times 25.0 = 12.1 t$

After Composition

$$Sd2 = 1/2 \times 0.893 \times 25.0 = 11.1$$
 $SW = 1/2 \times 0.135 \times 25.0 = 1.7$
 $SL = (28.96 \times 2)/7 \times 0.875 = 7.2$
 $Si = 7.2 \times 0.242 = 1.8$
 $S2 = 21.9 \text{ t}$

<u>G.3</u>

Before Composition

 $Sd1 = 1/2 \times 0.845 \times 25.0 = 10.6 t$

After Composition

Sd2 =
$$1/2 \times 0.210 \times 25.0$$
 = 2.6 t
SL = $(28.96 \times 2)/7 \times 1.75$ = 14.5 t
Si = 14.5×0.242 = 3.5 t
S2 = 20.6 t

NOTE: Table of Maximum M.S.R., Loading HS 20-44 (MS18)

from AASHTO APPENDIX A

TABLE OF MAXIMUM MOMENTS, SHEARS AND REACTIONS-SIMPLE SPANS, ONE LANE

Impact not included

Span (m)	Moment (kNm)	(t·m)	Reaction (kN)	(t)
12	593.1	(60.52)	244.3	(24.93)
16	904.3	(92.28)	263.4	(26.88)
17	991.8	(101.20)	266.7	(27.21)
18	1071.7	(109.40)	269.6	(27.51)
19	1149.4	(117.30)	272.4	(27.80)
20	1229.5	(125.50)	275.0	(28.06)
21	1309.5	(133.60)	276.8	(28.24)
22	1389.7	(141.80)	278.9	(28.46)
23	1469.8	(150.00)	280.9	(28.66)
25	1628.6	(166.20)	283.8	(28.96)

APPENDIX 8
GUIDELINE FOR DESIGN OF SUBSTRUCTURES



1. Earth Pressure

As Rankine's formula specified by AASHTO specification does not take into account effect due to seismic horizontal force, Coulomb's formula which is modified to include the effects is adoptable.

1.1 Active Earth Pressure of Sandy Soil

Coulomb's formula for active earth pressure of sandy soil, is expressed as follows:

$$pa = (q + r x) KA$$

where:

pa: active earth pressure at x

KA: Coulomb's active earth pressure coefficient

KA =
$$\frac{\cos^2 (\emptyset - 0 - 0)}{\cos 0 \cos^2 \cos (0 +) \circ + 8} \Big|_{1} + \frac{\sin (\emptyset +) \sin (\emptyset - 0 \circ)^2}{\cos (0 +) \circ + \cos (0 - d)}$$

when \emptyset -a-Oz 0, adopt \emptyset - -Oo = 0

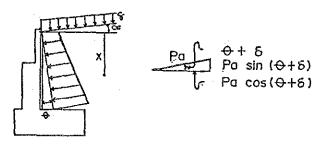


FIGURE 1 EARTH PRESSURE

ø: angle of backfill

 θ o: θ o = $tan^{-1} k$

k: seismic horizontal coefficient

θ: angle between back of wall and vertical plane

ά: angle between ground surface and horizontal plane

8: friction angle along wall boundary

: surcharge

r: unit weight of backfill

x: depth of point under construction

1.2 Ø and r

It is recommended to use the following angle of repose Ø and unit weight of backfill r, unless selected backfill is used.

$$0 = 30^{\circ}$$

$$r = 1.8 t/m^3$$

1.3 6

There are two types of failure wedge, for stability of a structure and for design of a wall member.

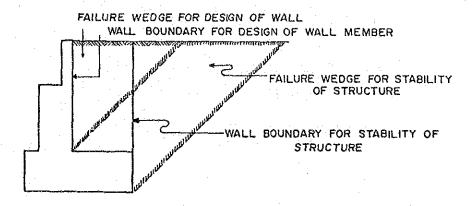


FIGURE 2 FAILURE WEDGE AND WALL BOUNDARY

The friction along the wall boundary is different for each wedge.

It is recommended to use the following table of friction angle.

TABLE I FRICTION ANGLE

	Friction Between	Group I L.	Group VII L.
Stability	Fill and fill	Ø	Ø/2
Design of Members	Fill and concrete wall	Ø/3	0

Ø: angle of repose of backfill

1.4 Earth Pressure Coefficient KA

The earth pressure coefficient KA is tabulated in Table 2 varying \emptyset from 25° to 40°, k from 1.0 to 0.25 and k = 0 (group I loading) with combinatin of &

1.5 Surcharge q

Live load surcharge q for HS-20 on backfill is obtained as follows:

Weight of a rear axle load
$$w = 32000 \text{ lbs.}$$
 $= 14.5 \text{ tons}$
Distance of rear axles $L = 14 \text{ ft.}$
 $= 4.267 \text{ m}$
Width of truck $B = 10 \text{ ft.}$
 $= 3.048 \text{ m}$

$$q = \frac{w}{L.B.} = 1.17^{t/m^2}$$

1.6 Earth Pressure for Design Footing

A footing shall be designed taking account of vertical component of earth pressure. The component is assumed to be distributed as an equivalent triangle on the footing, as shown in Figure 3.

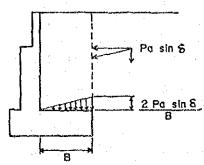


FIGURE 3 VERTICAL COMPONENT OF EARTH PRESSURE FOR DESIGN OF FOOTING

2. Horizontal Seismic Force due to Superstructure

Substructures shall be designed taking account of horizontal seismic force due to superstructures as follows: (refer Figure 4).

AL (Expansion Bearing)
 Horizontal seismic force at AL, HAL

Ral x fall
HAL = smallest of $\frac{1}{2}$ k WA

(2) P_1 (Fixed and Expansion Bearing) k WA

HaR + HbL = largest of or 1/2 KWA + RoL fbL

(3) AR (Fixed Bearing)

HbR = kWb

Where:

fal: friction coefficient of expansion bearing AL

An equivalent friction coefficient of an elastomeric bearing is obtained as follows:

Using relation of shearing force and strain of an elastomeric bearing due to horizontal force H.

H = GrA

G: Modulus of shearing elasticity (6.2 kg/cm^2)

r: shearing strain (maximum r = 0.5)

A: area of elastomeric bearing

Assuming the normal stress of bearing of 30 kg/cm² under dead load

 $N/A = 30 \text{ kg/cm}^2$

then:

H = GrN/30

H/N = Gr/30

 $= 6.2 \times 0.5/30 = 0.10 = f$

fbL: friction coefficient of expansion bearing BL

Hal: horizontal seismic force on AL due to span A

HaR: horizontal seismic force on P1 due to span A

HbL: horizontal seismic force on P1 due to span B

HbR: horizontal seismic force on AR due to span B

ks : horizontal seismic coefficient

Ral: reaction on AL due to WA

RaR: reaction on P1 due to WA

RbL: reaction on P1 due to WB

WA: dead weight of span A

WB : dead weight of span B

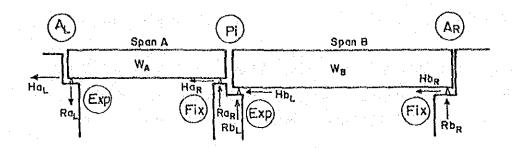


FIGURE 4 HORIZONTAL SEISMIC FORCE

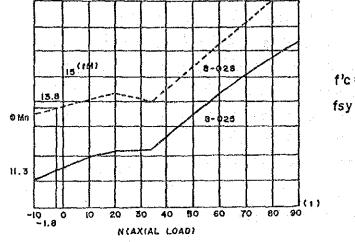
3. Pile

3.1 Ultimate Strength of Precast RC Pile

Required number and arrangement of piles is governed not only by capacity of the ground to support the load delivered by the pile, but also by the strength of the pile itself subjected combinations of bending moment and axial load.

It is recommended to use Load Factor Design for design of a pile under Group Loading VII.

Figure 5 gives the interaction diagram of standard RC pile



 $f'c = 210 \text{ kg/cm}^2 (3000 \text{ psi})$ $fsy = 2800 \text{ kg/cm}^2 (Grade)$

FIGURE 5 INTERACTION DIAGRAM OF STANDARD RC PILE (0. M4 x 0. M4)

Example

Select type of a pile subjected M = 10.1 tm/pile and N = -1.8 t/pile

Try pile provided 8-\$25

$$\phi M = 11.3^{\text{tm}}$$

 $1.3M = 1.3 \times 10.1 = 13.1$ $\phi M = 11.3 \text{ No}$

Try pile (8-\$28)

3.2 Spacing, clearance and Embedment

It is recommended to use following minimum spacing, clearance and embedment of piles considering accuracy of pile driving on the position, firm connection with a footing and reduction of load carrying capacity as group pile, though AASHTO specifies otherwise.

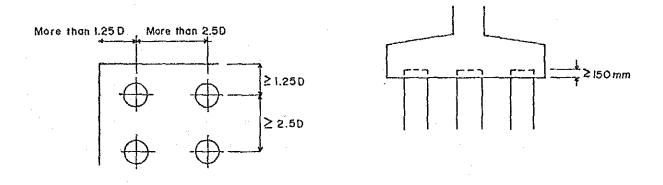


FIGURE 6 SPACING, CLEARANCE AND EMBEDMENT OF PILE

3.3 Design of Pile Embedment in Embankment

Piles in an open type of abutment are often used being extended from original ground, a-d embedded in embankment adjacent to a slope.

In this case, it is very difficult to expect subgrade lateral reaction to the piles as well as in original ground, even though the embankment is well compacted. And also, the embankment has a tendency to move toward the slope.

Taking these facts into consideration, it is recommended to analyze the pile assuming that one is extended from the original ground and no lateral resistance to the pile is expected in the embankment.

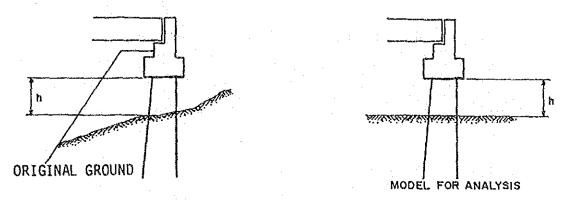


FIGURE 7 PILE EMBEDDED IN EMBANKMENT

4. Design of Backwall

A backwall is greatly affected by wheel loads as surcharge. Assuming that a wheel load is distributed depending on the depth from the load surcharged.

$$Px = \frac{T}{(a+x)}$$

$$Py = \frac{T}{(a+x)}$$

FIGURE 8 EARTH PRESSURE ON BACKWALL

where:

T = distributed axle load (t/m)

a = longitudinal distribution of wheel load (m)

x = depth (m)

Ka = earth pressure coefficient

integrating PY from 0 to h

then, bending moment and shearing force of backwall can be obtained by the following equation in the case of h 1^{m} , substituting

a =
$$0.2^{m}$$
, T = 14.5 t/3.05^{m}
= 4.75 t/m (9.81)
Mw = $8.5 \text{ Ka x (h-0.24)}$ (tm/m)
Sw = 8.5 Ka (t/m)

5. Wing Wall

5.1 Dimensions

Dimensions of a wing wall are determined by slope of backfill and retaining height of an abutment, as shown in Figure 9.

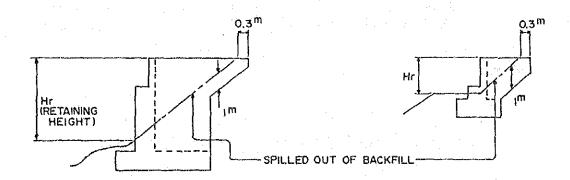


FIGURE 9 DIMENSIONS OF WING WALL

5.2 Design of Wing Wall

A wing wall is analytically a two-way slab subjected earth pressure. However, it is recommended to use the following simplified concepts for the design:

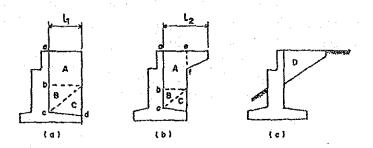


FIGURE 10 TYPE OF WING WALL

- Part A and D are supported along ab and ef respectively, as a cantilever beam, and it is assumed that bending moment and shearing force caused by the earth pressure on part A and D, is equivalently distributed along ab and ef.
- 2. Part B and C are supported along bc and cd respectively, as a cantilever beam, as shown in Figure 11.

Bending moment can be obtained as follows.

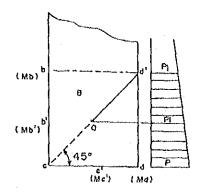


FIGURE 11 DESIGN OF WING WALL

for b-b'
$$M_b = 1/2 \times pi \times \overline{bd'}^2$$

b-C $M'_b = 1/2 \times pi \times \overline{b'0}^2$
d-C' $Md = 1/6 \times (2pi + pk) \times \overline{dd'}^2$
C'-C $M'c = 1/6 \times (2pi + pk) \times \overline{C'0}^2$

5.3 Connection of Wing Wall With Backwall

A backwall has to sustain a part of horizontal bending moment transmitted from part A and D.

It is recommended to provide a haunch and increase thickness of backwall in order to secure frim connection with backwall, when it is relatively thin comparing thickness of wingwall as shown below:

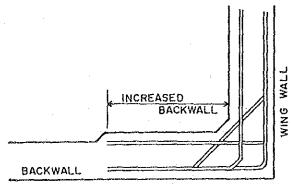
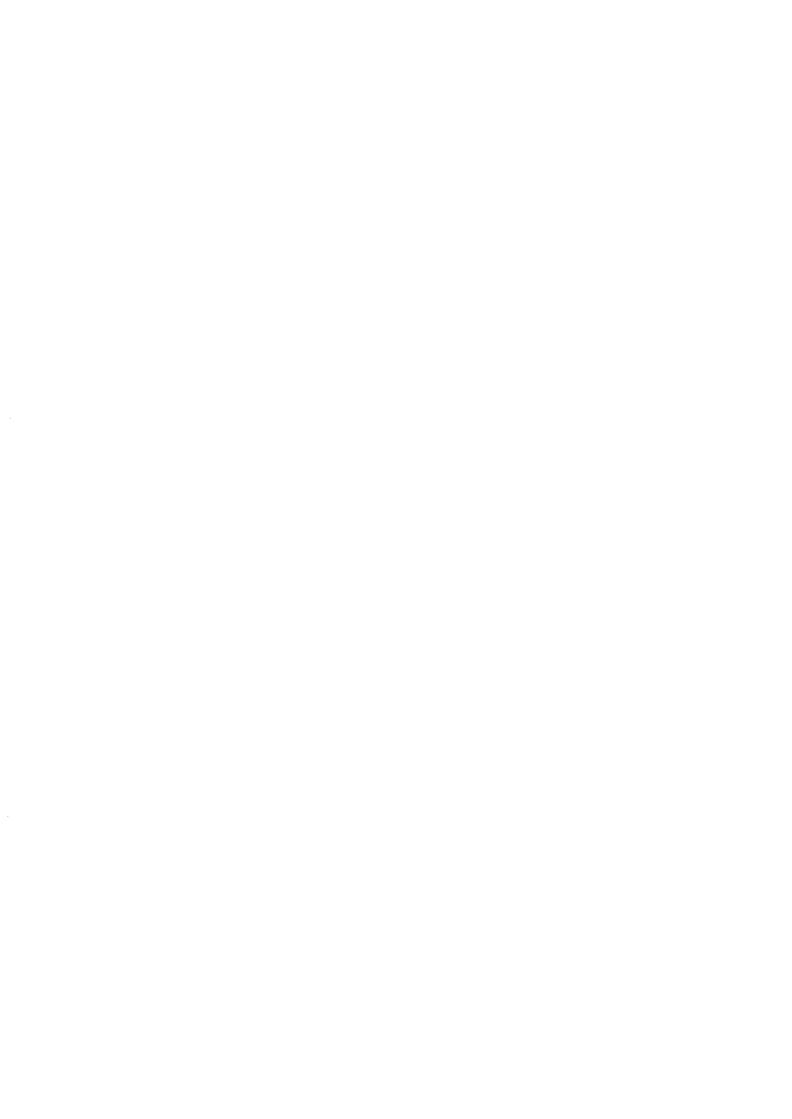


FIGURE 12 CONNECTION OF WING WALL WITH BACK WALL



APPENDIX 9
BENEFIT CALCULATION



BENEFIT CALCULATION

1. General

The quantified traffic benefits are savings in road traffic costs, maintenance costs, restoration cost and salvage value. These direct benefits were studied as follows:

2. Traffic Benefits

1) Savings in Road Traffic Costs.

Basic vehicle operating cost (BVOC) of owning and operating road vehicles is composed of the following cost.

Running Cost: That portion of the vehicle operating cost which is calculated in units of distance (Kilometers) travelled.

Basic Fixed Cost: That portion of the vehicle operating cost which is calculated in units of time travelled.

Passenger Time Cost: Passenger time value including the time of the car driver.

Accidents Cost: The implementation of this Project will reduce the number of traffic accident caused by detouring or bridge failures.

The above mentioned basic costs, which are used as a basis for this study, were updated by the Planning Service of the Department of Public Works and Highways (DPWH) to 1988 prices in accordance with the procedure outlined in DPWH's Highway Planning Manual. Such costs were assumed to be incurred by vehicles operating under the basic ideal Philippines condition:

2) Savings in Maintenance/Restoration Costs

Without the project, maintenance restoration expenditures will be required. With the project, such expenditures will become unnecessary and they can be added as project benefit. Basic conditions considered are as follows:

The costs of Maintenance/restoration were assumed by applying EMIC (Equivalent Maintenance Kilometer) method being used by DPWH.

3) Salvage Value

The allowance in the economic analysis of a net salvage value at the end of the economic life of the project is beset with uncertainties. Whether road construction consisting of land molded to road geometrics would have a positive salvage value at some Fardistant year is uncertainly. Practically none of the road construction would be beneficial to any alternatives use without considerable cost expanded to make it suitable. Likewise, most bridges have no value except as a part of a road. Therefore, this benefit was considered negligible.

3. Saving in Road Traffic Costs

Road Condition and Future Traffic Volume

The road conditions of the road section including the subject bridge and the alternative routes are estimated as follows:

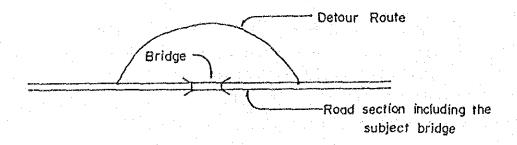


TABLE 1 Road Condition (Average)

	Road including Subject Bridge	Alternative Route
Length of Section	10 Km	35 Km
Surface Type	Grave1	Gravel
Surface Condition	Bad	Bad
Traffic Volume	See Table 10-2	

TABLE 2 Future Traffic Volume (AADT)

Vehicle Type	1988	1990	2000	2010
Car/Van	2,544	2,658	4,128	6,411
Jeepney	2,459	2,570	3,990	6,192
Bus	863	902	1,400	2,175
Truck	2,368	2,474	3,843	5,968
Total	8,234	8,604	13,361	20,751

Traffic Growth Rate

Growth in Traffic is calculated on the basis of population growth, growth in per capita income and transport demand-income elasticities, possibly by income group. The formula for the Traffic growth rates (TGR) is as follows:

TGR (in percent) =
$$\left[\left(\frac{I \times E}{100} + 1\right) CP - \overline{1}\right] - 100$$
,

Where: TGR is the traffic growth rate per annum;

- E is the transport demand-income elasticity for the respective vehicle type;
- I is the growth rate (in percent) for per capita income in constant prices; and

CP is the compound population growth rate per annum (e.g. 3 percent population growth becomes 1.03 compounded).

Given Data:

E = 1.0 (corresponding to the per capita income)

I = 2.0 percent

CP = 1.025

TGR =
$$\left[\left(\frac{2.0 \times 1.0}{100} + 1 \right) 1.025 - 1 \right] \times 100$$

= 4.5 %

TABLE 3 TRAFFIC VOLUME (AADT), 1987

Bridge No. (Location)	Car/Van	Jeepney	Bus	Truck	Total
02.03	100	90	23	37	250
02.04	112	101	25	43	281
04.07	20	18	. 4	8	50
04.08	24	22	.5	9	60
05.02	250	225	56	93	624
06.02	156	140	35	59	390
06.04	24	22	5	9	60
07.03	36	32	8	13	89
07.04	107	96	24	40	267
07.05	20	18	4	6	50
08.01	38	35	9	14	96
08.02	46	35	9	17	107
08.05	52	47	12	19	130
09.01	68	200	=	72	340
09.02	169	127	116	178	590
09.03	169	127	116	176	590
09.04	179	182	128	178	667
10.02	165	224	€	930	1,319
10.03	252	227	57	94	630
10.04	232	209	52	87	580
10.05	78	51	123	110	362
11.01	90	89	17	112	308
11.03	108	97	24	41	270
12.03	49	45	11	19	124
The Local	2,544	2,459	863	2,368	8,234

TABLE 4 (P/KM., EXCLUDING TAXES, DECEMBER 1986 PRICES) ECONOMIC BASIC VEHICLE OPERATING COST AND PASSENGER TIME COST

Sur Type	face Condition	Vehicle Type	Running Costs (P/Km)	Fixed Costs (P/Km)	Time Costs (P/Km)	Total Costs (P/Km)
	Very Bad	Car/Van	1.711	.096	.377	2.184
. e		Jeepney	1.266	.729	.457	2.452
. 1		Bus	4.199	1.015	2.193	7.407
		Truck	4.495	1.087	0	5.582
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Bad	Car/Van	1.497	.072	.283	1.852
**	• •	Jeepney	1.108	.547	.342	1.997
•		Bus	3.536	.761	1.645	5.942
	<i>₹</i>	Truck	3.785	.815	0	4.600
Paved	Fair	Car/Van	1.283	.048	.188	1.519
. *	$x^{(i)}$	Jeepney	.949	.364	.228	1.541
÷		Bus	2.873	.609	1.316	4.798
	.*	Truck	3.075	.652	0	3.727
	Good	Car/Van	1.069	.041	.161	1.271
		Jeepney	.791	.312	.195	1.298
		Bus	2.210	.507	1.096	3.813
£ .		Truck	2.366	.543	0	2.909
	Very Bad	Car/Van	2.032	.096	.377	2.505
		Jeepney	1.503	.729	.457	2.689
÷	•	Bus	5.083	1.015	2.193	8.291
		Truck	5.441	1.087	0	6.528
	Bad	Car/Van	1.711	.072	.283	2.066
		Jeepney	1.266	.547	.342	2.155
		Bus	4.199	1.015	2.193	7.407
		Truck	4.495	1.087	0	5.582
Gravel	Fair	Car/Van	1.390	.057	.226	1.673
		Jeepney	1.029	.437	.274	1.740
		Bus	3.315	.761	1.645	5.721
		Truck	3.548	.815	0	4.363
	Good	Car/Van	1.230	.048	.168	1.466
		Jeepney	.910	.364	.228	1.502
		Bus	2.763	.609	1.316	4.688
		Truck	2.957	652	0	3.609

TABLE 5 SAVING IN TRAFFIC COSTS

	Vehicle Type	Traffic Volume (Veh. Day)	Add. Cost (P/Veh.)	No. of Days	Saving in Detour (M 9)
-	Car	2,544	58.78	20	2.99
	Jeepney	2,459	56.00	20	2.75
1988	Bus	863	153.60	20	2.65
	Truck	2,368	139.75	20	6.61
	Total	8,234	and the state of t		15.00
	Car	2,658	58.78	20	3.12
	Jeepney	2,570	56.00	20	2.88
1990	Bus	902	153.60	20	2.77
	Truck	2,474	139.75	20	6.92
	Total	8,604			15.69
	Car	4,128	58.78	20	4.85
2000	Jeepney	3,990	56.00	20	4.46
2000	Bus	1,400	153.60	20	4.29
	Truck	3,848	139.75	20	10.75
	Total	13,361			24.35
	Car	6,411	58.78	20	7 . 53
2010	Jeepney	6,197	56.00	20	6.95
CATA	Bus	2,175	153.60	20	6.68
÷	Truck	5,968	139.75	20	16.68
<u></u>	Total	20,751			37.73

4. Calculation of Economic Cost-Benefit Streams

TABLE 6 ADDITIONAL TRAFFIC COST

		Car	Jeepney	Bus	Truck
Add. Length	Km	25	25	25	25
Add. Time	hour	0.34	0.43	0.55	0.89
B. R. C.	P/km	1.71	1.26	4.20	4.50
B. F. C.	P/hour	0.07	0.55	1.02	1.09
P. T. C.	P/hour	42.00	25.00	42.00	••
Running Cost	P/Veh.	42.75	31.50	105.00	112.50
Fixed Cost	P/Veh.	1.75	13.75	25.50	27.25
Time Cost	//Veh.	14.28	10.75	23.10	_
Total	P/Veh.	58.78	56.00	153.60	139.75

TABLE 7 ECONOMIC COST-BENEFIT STREAMS

(Unit: MP at 1988 Prices) Before Discount After Discount (15%) Year Cost Saving in Saving in Total Traffic Cost Maintenance Cost Cost Benefit 93.60 1988 ... 93.60 10.40 1989 3.93 0.02 3.95 9.04 3.43 1990 15.69 0.08 15.77 11.92 1991 16.47 0.08 16.55 10.88 1992 17.33 0.08 17.41 9.95 1993 18.20 80.0 18.28 9.09 1994 19.07 0.08 19.15 8.28 19.93 1995 0.08 20.01 7.52 1996 20.80 0.08 20.88 6.83 1997 21.67 0.08 21.75 6.18 1998 22.53 0.08 22.61 5,50 23.40 0.08 23.48 5,05 1999 24.35 4.57 0.08 24.43 2000 25.79 4.21 25.71 0.08 2001 27.13 3.83 27.05 0.08 2002 3.50 28.48 28.40 0.08 2003 3.14 29.83 29.75 0.08 2004 2.90 0.08 31.17 31.09 2005 2.63 32.52 0.08 2006 32.44 0.08 33.88 2.37 33.80 2007 2.15 35.23 0.08 35.15 2008 1.45 27.42 0.06 27.36 2009 114.94 102.60 Total 104.0

NPV = 12.34 MP

B/C = 1.12

IRR = 17.0%

APPENDIX 10

COUNTRY DATA

I. Land and Population

(1) Land

The Philippines consist of 7,100 islands that were formed by repeated orogenic movements and volcanic activities. The islands are divided into the three (3) main groups of Luzon, Visayas and Mindanao. Luzon is the largest island and is located furthest north. Visayas, composed of Samar, Leyte and other islands, is situated between the other two, and Mindanao, the second largest island, is located furthest south.

The area of the major islands is as follows:

Island	Area (km2)
Luzon Mindanao Samar Negros Palawan Others	104,687 94,630 13,079 12,704 11,784 43,541
Total	280,415

(2) Climate

The Philippines is located in the tropics. The climate in the Philippines is due to its grographical location and the different winds system that prevails over the locality. The condition of the climate has been described in term of the characteristics of the distribution of rainfall received in a locality during the different month of the year. There are four climate types in the Philippines.

Over 50% of the rainfall is associated with tropical cyclones. The frequency of tropical cyclones in the Philippine Area of Responsibility (PAR) has an average of 20 times a year, while the frequency crossing in the Philippines has an average of 8.8 times a year.

The average annual rainfall in the Philippines is 2416.3 mm The largest average annual rainfall are 4316 mm and 4360 mm at Borongan in Samar and Hinatuan in Surigao del Sur, respectively, both of which face the Pacific Ocean and belong to the 2nd type of climate. The highest daily rainfall was 979.4 mm recorded in Baguio City on October 17,1967. In Samar and Leyet islands, the highest daily rainfall of 387.9 mm was recorded in Catbalogan City, whereas in Mindanao Island, 564.7 mm in Surigao City.

(3) Population

The National Capital Region, an integrated community composed of 4 cities and 13 municipalities, holds a population density of 9,317.4 persons per each square kilometer, as compared to 160.3 for the whole country. Its population has being growing at a much higher rate.

Table 1 shows comparative figures of the population, and density of each region.

II. Economy

(1) National Economy

The decade of the 1970's witnessed substantial growth in the Philippine economy. Real Gross National Product (GNP) increased at an average yearly rate of 6.2 percent from 1972 to 1980. However, the early 1980's was a period of relatively slower growth in the Philippine economy as an effect of the worldwide economic recession precipitated by the oil crisis.

This moreover, continued to pose difficulties for the Philippine economy until the early part of 1983. As a result of this tight financial situation, the maturities of Philippine borrowings became shorter while interest rates became higher. The declining pace of the economy continued until it reached the lowest fall in GNP in 1984 which gave a negative growth of 5.3%. The negative growth of 2.5% in 1985 showed a gradual recovery of the economy, which was actually the start of the Philippine economic recovery, from a negative growth to a positive growth of 1.2% in 1986 to a rapid growth until the early part of 1987 which was estimated at 5.4%.

The relatively higher growth the country is currently experiencing is expected to continue as the necessary structual reforms within the economy are currently being instituted under the new leadership.

(2) Regional Economy

A review of past regional economic performance reveals that different regions of the country showed wide variations in growth and development as exhibited in Table 2 Overall, more than half of the country's domestic output was contributed by only 3 regions: Metro Manila (NCR), Southern Tagalog (R-III) and Western Visayas (R-VI). The depressed regions are Regions II, VIII, IX and XII.

Poverty has been identified as a critical problem in all of the country's regions. Despite various government assistance and programs directed toward low-income groups, the situation has worsened in recent years.

Larger number of poor families and higher poverty incidences have been observed in both developed and poorer regions, pointing to the uneven distribution of incomes within the regions.

As shown in Table 3 regional poverty incidence in 1985 ranged from 44.1 percent in the National Capital Region to a high 73.2 percent in Region V. Nine of the country's thirteen regions had poverty incidences higher than the national average. The Visayas area, covering three regions, had a generally higher proportion of poor families in the Philippines. Poverty in the rural sector is more severe than in the urban areas. Rural poverty incidence were highest in Regions V, VI, VII and VIII, with more than 70 percent of families falling below the poverty line.

In urban areas, the proportion of poor families was highest in Eastern (R-VIII) and Western (R-VII) Visayas and Northern Mindanao (R-IX).

(3) Industrial Structure

By industrial sector, the service sector consistently dominated the country's economy throughout the years from 1970 to 1985, contributing 38% to 42% to the national economy. Industry was next with contributions from 30% to 37%. Agriculture had the least contribution, ranging from 25% to 29% during the same period.

The economy of the country is basically agricultural and its total land area is predominantly rural. The total arable land of the Philippines is 1,333,258 hectares. In 1986, total agricultural crop production of the country reached to 28.5 million metric tons planted to 12.2 million hectars and valued at 77.9 million. Of total production about 80% was contributed by food crops made up of palay, corn and fruits, and only 20% by commercial crops with coconuts and sugarcane as the leading commercial crops.

The largest crop producing region of the country is Region XI (Southern Mindanao) contributing about 18 percent of the country's total crop production. The next largest crop producing region are Central Mindanao (R-XII) and Western Visays (R-VI) contributing 12 percent, respectively.

These different regions of the country consists of different soil types suitable to different types of crops, thus different regions each advantages to different types of crops. The major producers of palay are Regions X, XI and XII, all in Mindanao while the major producers of coconuts are Southern Tagalog (R-IV) and Southern Mindanao (R-XI). Sugaarcane is predominantly grown in Western Visayas (R-VI) while abaca is the major crop of Bicol Region (R-V).

Table 4 shows crop production and the value of production by region.

我们们还是不是"我的人的。""我们们我们的我们就是我们的,我们就是要你们,我会们就是我们的人们都是不是什么。"

III. National Development Plan

The Medium-Term Philippine Development Plan for 1987 to 1992 was formulated to guide development efforts in both the public and private sector as follows:

The plan address the fundamental problems of people: persistence of poverty and income inequality, high unemployment and underemployment, and urban/rural and regional disparities. These have been brought about bу continued structural inefficiencies in the economy. Moreover, the external debt crisis experienced in 1983 set back whatever gains had been attained in the past.

The Philippines experienced the worst economic and financial crisis in its postwar history starting in late 1983. The roots of these problems can be traced to structural weaknesses in the foundation of the economy, errors in economic management, and abuse of power by the previous regime.

Philippines devedlopment efforts in 1987-92 shall be principally directed towards the following goals: (a) alleviation of poverty, (b) generation of more productive employment, (c) promotion of equity and social justice, and (d) the attainment of sustainaable economic growth.

Table 2.1-2 shows the gross national product and per capita GNP, for 1986-92.

TABLE 1 POPULATION DENSITY BY REGION AND RANK 1980, 1975, 1970

			1 9	1980		1 9	975		1 9	1970	
		(Sq. Km.)	Population (In Thousand)	Density	Rank	Population (In Thousand)	Density	Rank	Population (In Thousand)	Density	Rank
Philippines	sə	300000	48099	160.3		42071	140.2		36685	122.3	
National	National Capital Region	636	5926	9317.4	-	4971	7814.5	tana	3967	6236.9	rd
Region I	Region III-Central Luzon	18230.8	4803	263.4	~	4210	230.9	2	3616	198.3	m
Region V	VII-Central Visayas	14951.4	3787	253.3	က	3387	226.6	ണ	3033	202.8	2
Region	VI-Western Visayas	20223.1	4526	223.8	⋖Ϯ	4146	205.0	4	3618	178.9	₹
Region	V-Bicol	17632.5	3477	197.2	ഹ	3194	181.1	S	2967	168.3	ເດ
Region	I-Ilocos	21568.4	3541	164.2	9	3269	151.6	9	2991	138.7	9
Region	IX-Western Mindanao	18685.1	2529	135.3	~	2048	109.6	5	1869	100.0	00
Region VI	Region VIII-Eastern Visayas	21431.7	2800	130.6	00	2600	121.3	7	2381	had bad bad t	~
Region	IV-Southern Tagalog	46924.2	6119	130.4	თ	5214		_, ω	4456	95.0	ത
Region	XI-Southern Mindanao	31692.8	3347	105.6	. 21	2715	85.6	6-mi	2201	69.4	
Region X	XII-Central Mindanao	23293.2	2271	97.5	p-ref	2070	88.9	10	1942	83.3	01
Region	X-Northern Mindanao	28327.7	2759	97.4	12	2314	81.7	12	1953	68.9	12
Region	II-Cagayan Valley	36403.0	2216	6.09	13	1933	53.1	13	1692	46.5	13

GROSS DOMESTIC PRODUCT AND GROWTH RATE BY REGION: 1971 TO 1985 (AT CONSTANT 1972 PRICES) TABLE 2

	Region/Year	1971	1971 1975	Million Pesos 1980	1985	1971-1975	Growth Rate 1975-1980 198	Rate 1980-1985	1971-1985
	Philippines	53528	67455	92706	90469	6.0	6.6	9.5	3.8
	N C R	16182	20976	29959	27026	6.7	7.4	8.0	3,7
• ⊭-1	Ilocos Region	2691	3144	3315	3859	4.0	1.1	3.1	2.6
p4	Cagayan Valley	1421	1809	2437	2472	6.2	6.1	0.3	4.0
} } }! }:		4664	5556	7500	7996	4.5	6.2	۳. ا	3.9
IV.	Southern Tagalog	6434	9617	12935	12905	9.0	6.1	-0.05	5. 3.
>	Bicol Region	2032	2554	3277	3069	5.9	5.1	8.7	3.0
VI.	Western Visayas	5988	5837	7331	7241	9.4	4.7	9.8	***
VII.	Central Visayas	3137	4754	6794	6332	1.0	7.4	8.6	ω. •••
VIII.	Eastern Visayas	1766	2094	2272	2205	4.4	1.6	9.4	ω
IX.	Western Mindanao	1589	1834	3248	3235	3.6	2.1	9.6	5.2
×	Northern Mindanao	2304	2731	4267	4349	4.3	හ ් ග	0.4	4.6
XI.	Southern Mindanao	3552	4587	6292	6157	6.6	6.5	9.6	4.0
XII.	Central Mindanao	1768	1962	3079	3623	2.6	9.4	3.3	ກ. ສຸງ

TABLE 3 REGIONAL POVERTY INDICATORS: 1985

		Total			Urban			Rural	
Region	Total Poverty Threshold (In P)	Magnitude of Poverty (000 Families)**	Incidence of Poverty (In %) ***	Total Poverty Threshold (In P)*	Magnitude of Poverty (000 Families)**	Incidence of Poverty (In %)***	Total Poverty Threshold (In P)*	Magnitude of Poverty (000 Families)**	Incidence of Povert (In%) ***
Philippines	2,382	5,676.6	59.3	3,021	1,875.9	52.1	2,066	3,800.7	63.7
N C R	3,282	550.5	44.1	3,282	550.5	44.1			
Outs, NCR	2,285	5,126.1	61.6	2,912	1,325.4	56.3	2,066	3,800.7	63.7
	2,374	364.9	52.3	3,093	89.7	56.2	2,139	275.2	51.
II	2,194	246.3	54.6	2,897	31.3	48.6	2,092	215.0	55.6
III	2,550	420.0	44.4	3,153	178.5	45.2	2,104	241.5	43.8
ΛI	2,471	712.2	55.9	3,048	241.7	50.6	2,174	470.5	59.1
^	2,148	464.0	73.2	2,625	81.2	62.3	2,047	382.7	76.0
IA	2,449	632.4	73.1	3,069	154.1	65.0	2,249	478.3	76.2
IIA	1,982	530.6	8.89	2,426	142.7	58.9	1,819	387.9	73.4
IIIA	2,016	385.4	70.4	2,733	81.9	70.1	1,822	303.5	70.5
XI	2,118	316.5	65.3	2,650	47.2	61.6	2,025	269.3	0.99
×	2,262	355.4	66.2	2,952	91.7	65.7	2,022	263.7	66.3
×	2,388	426.0	61.7	2,998	143.1	59.6	2,079	282.9	62.8
⊢ ×	2,233	272.4	65.2	2,624	42.2	56.8	2,161	230.2	0.79

* The monthly income required to satisfy 100 percent of nutritional requirements and other needs of a family of 6.

** The total number of families below the poverty line or threshold in 1985.

*** Out of the total number of families, the proportion of families that fall below the povertyline in 1985.

SOURCE: Inter-agency Working Group on Poverty Determination - NEDA, FNRI, NCSO.

TABLE 4(1) CROP PRODUCTION BY REGION, 1986 (IN METRIC TONS)

	Ilocos	Cagayan Valley	Central Luzon	Southern Tagalog	Bicol	Western Visayas	Centnal Visayas	Eastern Visayas	Western Mindanao
All Crops	1,713,726	1,760,242	2,001,026	2,753,156	1,741,385	3,038,775	1,157,011	1,594,719	1,511,66
Food Crops	1,582,284	1,710,079	1,789,876	1,824,165	1,485,439	1,769,198	815,986	1,266,609	1,122,547
Palay (Rough Rice)	871,740	1,172,110	1,525,355	985,765	683,090	1,121,920	148,180	469,440	353,37
Corn (Shelled)	64,530	374,835	8,370	242,305	133,975	43,740	243,645	273,020	216,700
Fruit and nuts except Citrus	265,868	73,754	101,881	330,135	118,420	430,622	137,106	254,842	191,75
Others	241,280	67,985	121,495	262,570	83,810	392,469	119,110	247,207	185,54
Commercial Crops	131,442	50,163	211,150	928,991	255,946	1,269,577	341,025	328,110	389,12%
Coconut (Products)	84,961	23,393	10,913	624,397	212,533	116,617	133,123	245,035	295,67:
Sugarcane	7,576	16,615	197,127	303,218	13,536	1,149,153	205,072	61,519	~
Abaca			i	594	29,860	1,185	930	21,462	360 6
Tobacco	35,855	10,122	3,105	695	13	412	583	39	95
Coffee	1,846	4,969	230	32,971	1,215	4,793	1,445	390	17,261
Cacao	114	09	# -	133	113	186	2,174	66	300
Peanut	11,117	17,394	1,954	3,051	1,118	676	19,119	844	1,661
Root.crops	85,378	22,590	38,364	95,247	466,930	82,291	242,079	285,208	301,211
Vegetables	147,067	9,433	35,130	54,954	17,484	25,658	10,482	5,184	3,074
Others	102,446	100,790	79,251	310,751	50,347	57,425	23,089	10,702	142,968

TABLE 4(2) CROP PRODUCTION BY REGION, 1986 (IN METRIC TONS)

Sdoro	Northern Mindanao	Southern Mindanao	Central Mindanao	Philippines
All Crops	2,673,185	5,040,157	3,544,782	28,529,828
Food Crops	2,351,905	3,995,652	3,207,726	22,921,461
Palay (Rough Rice)	342,095	653,195	770,720	086,980,6
Corn (Shelled)	252,850	1,203,315	900,735	3,922,020
Fruits and Nuts Except Citrus	1,469,021	1,927,076	729,846	6,030,326
Others	550,159	1,320,388	725,915	4,286,357
Commercial Crops	321,280	1,044,505	337,056	5,608,367
Coconut Product	177,555	983,362	254,827	3,162,389
Sugarcane	122,711	34,590	24,091	2,135,316
Abaca	5,474	9,653	4,409	82,665
Tobacco	652	99	4,405	56,002
Coffee	40,457	26,058	4,880	136,515
Cacao	846	3,070	246	6,235
Peanut	563	688	2,163	43,907
Rootcrops	184,054	101,547	763,577	2,668,476
Vegetables	20,603	18,845	9,246	357,060
Others	49,017	50,927	288,812	729,768

TABLE 5 CHARACTARISTIC OF THE PHILIPPINES ECONOMY

्रांत क्षेत्र क्षेत्र त्यात क्षेत्र क्षेत्र क्षेत्र क्षेत्र क्ष्म क्ष्म क्ष्म क्ष्म क्ष्म क्ष्म क्ष्म क्ष्म क्ष		*****				6 No 45 44 44 48 48 48 48	
	1970	1975	1980 -	1982	1983	1984	1985
大學 大狗 CH (10) 100 400 400 400 100 100 100 100 100 100							3 (30 en e n en en en en en
Population (thousands)3	6,850	42,070	48,320	50,740	51,960	53,170	54,380
GNP (billion pesos)	42	114	265	335	379	539	607
GDP (billion pesos)	143	195	265	279	282	268	257
GNP Growth rate (%)					1.1	-6.8	-3.8
GNP Per Capital (Pesos)		375		769	635	660	
Consumer Price Increase				ı			
Rate (%)		***		10.2	10.0	50.4	23.1
Exchange Rate on US\$							
(Pesos) 5	9,044	72,479	75,114	85,400	111,127	166,987	186,073
External Accounts							
(US\$ mil.)	• .						
Current Account	-48	~923	-1,917	-3,212	-2,751	-1,268	8
Trade Account	-26	-1,196	-1,939	-2,646	-2,485	-679	-482
Exports	1,064	2,263	5,788	5,021	5,005	5,391	4,629
Imports	1,090	3,459	7,727	7,667	7,490	6,070	-5,111
Invisible trade							
Account	-141	-46	-412	-1,040	-738	-975	
Capital Account	271	1,094	2,684	2,846	-394	750	301
Total External Accour	ıt 75	-11	891	-730	-3,501	-403	952
Gold, Foreign Current	:A						
Reserves	251	1,359	3,140	1,711	864	890	1,116
Commercial Banking							
(mil.Rupiah)	1.						
Total Asset	12	47	123	164	201	224	
Deposit liabilities	7	15	45	66	76	88	100
Public Finance	•				•		
(mil.Pesos)							
Revenues	4,849	16,838	34,373	37,993	45,606	56,851	68,961
Expendi tures	4,790	18,198	37,758	52,407	53,074	66,689	80,102
Accounts		-1,360			-7,468	-9,828	-11,141
External Debt(US\$mil.)	1,562	2,043	17,390	24,166	23,871	24,381	
External Deht/GNP(%)	22.1	12.9	49.4	61.5	69.9		
Debt Service (US\$mil.)	258	404	1,576	2,930	2,659	2,802	2,774
Debt Service/Exports(%))	12.7	19.7	36.6	32.7	35.0	35.0

Source: IMF, International Monetary Statistics yearbook, 1986 Philippines Central Bank Data

FUNCTIONAL CLASSIFICATION OF NATIONAL GOVERNMENT EXPENDITURES, 1987-1992 (Percentage Distribution) TABLE 6

	Actual	100 co			Proje	Projections			Annual
	1976-85	1986	1987	1988	1989	1990	1991	1992	1987-92
Economic Sarvices	33.8	17.3	19.9	21.6	23.0	26.3	28.4	30.3	25.1
Agriculture	7.3	3,2	3.9	5.7	9,51	7.4	8.2	9.1	8.8
industry, trade and tourism	ઌ૽	0.7	6.		2.4	2.8	3.0	က	2,5
Utilities and infrastructure	23.5	13.4	14.6	14.0	15.0	16.1	17.2	17.9	15.8
Social Services	20.2	18,3	21.5	24.5	28.4	31.4	35.7	39,2	30.1
Education	12.3	10.2	ដ	13.2	14.1	14.9	17.1	18.7	15.0
Health	800	3.0	3.4	4.2	5.9	6.6	8.2	9.6	က
Social security and welfare	2.1	4.7	6.2	6.2	6.2	60	6.4	6.4	6.2
Housing and community development	Gi Gi	0.4	0.4	6.0	2.2	3.6	4.0	4,5	2.7
Defense	14.0	8.8	7.3	7.4	8.0	8.4	8.5	83	8
General Public Services	20.0	10.0	11.3	15.7	14.7	13.7	12.3	9.6	12.9
Dabt Service Fund and Net Lending ^a	11.9	47.5	40.0	30.8	25.0	20.2	15.1	12.0	23.9
Total	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0	100.0

For 1857 onwards, this item includes a portion of the external liabilities of government financial institutions to be assumed by the national government. Excludes
debt service on liabilities of the Philippine Nuclear Power Plant.
 Sources of Basic Date: MSM and NEDA.

TABLE 7(1) EXISTING ROAD LENGTH, 1985

			Nationa attona		•	÷	Ü	こったく	
	Concrete	Asphalt	15 1	Earth	Total	Concrete	Asphalt	Gravel	Total
Philippines	6132.90	5714.75	13601.18	810.29	26259.12	637.44	2016.48	1166.85	3820.77
м С	440.47	421.64	14.04	1	876.15	281.87	832.78	159.09	1273.74
}1	447.90	943.16	904.49	98.19	2393,74	8.25	183.42	118.05	309.72
}1 1	607.02	107.95	1530.31	61.95	2307.23	t	ı	•,	ŧ
prod brod	810.59	501.19	378.08	1	1689.86	56.52	115.83	40.95	213.30
IV-A	507.04	973.72	854.66	16.30	10351.72	37.28	120.17	47.26	204.71
IV-8	23.47	265.89	1343,49	73.10	1705.95	0.64	7.46	54.91	63.01
>	624.42	401.32	961.39	47.45	2034.58	20.34	81.14	125.77	227.25
VI	314.73	590,39	1637.44	52.80	2595,36	79.80	163.05	51.31	294.16
IIA	159.48	648.51	859.77	9.40	1677.16	32,43	236.68	. 24.10	293.21
VIII	664.81	58.84	1161.16	100.30	1985,11	39.09	2.81	20.02	61.92
IX	50.99	338,17	651.03	ı	1040,19	8.22	76.89	36.31	121.42
×	639.07	311,62	1251.06	5.70	2207.45	36.10	71.20	98.91	206.21
×	458.22	123.64	1234.97	142.95	1959.78	15.10	92.45	319.06	426.61
IIX	384.69	28.72	819.31	202.14	1434.86	21.71	32.61	71.11	125.43

TABLE 7(2) EXISTING ROAD LENGTH, 1985

, s		:	Municipal				-	Provincial		
Neg Ion	Concrete	Asphalt	Gravel	Earth	Total	Concrete	Asphalt	Gravel	Earth	[ota]
Philippines	11706.25	1579.03	6318.79	3220.75	12990,63	711.57	2739.52	19443.45	5524.74	28419.28
z C R	351.18	162.02	29.36	11.78	554.34	•	. 1	t	* , 1	1
b=-4	40.44	286.70	667.64	409.74	1404,52	48.84	483,32	1578.65	659.69	2870.51
port port	21.09	56.45	827.99	236.41	1141.94	8.44	159.04	1416.70	388.23	1972.41
	202.22	213.60	465.88	155.21	1082,09	302.75	360.87	1534.95	185.66	2384.23
IV.A	279.98	217.12	252.22	114.97	885,65	132.36	498.75	954.66	308.24	1894,01
IV-B	50.03	22,16	342.84	103.87	472.55	11.47	50,30	1667.75	351.90	2081.42
>	107.07	192.40	360.93	121.16	799,68	35.02	318.15	1089,53	361,05	1803.75
>	197.95	87.52	345.14	59.01	695,28	61.92	94.29	1966.89	106.20	2229.30
	97.56	137.24	445.53	228.19	930.47	13.69	169.93	1906.53	266.51	2356.66
VIII	246.93	18.12	305,44	137.95	717.13	65.39	327.39	865.55	185.12	1443.45
X	3.31	25.58	518,10	253.71	800,80	1.68	184.36	1563.86	278.35	2028.25
×	38.25	91,72	556,34	523.88	1221.26	14.09	87.97	1907.97	663.34	2673.37
ï×	39.57	33.56	753.77	429.50	1283,37	10.74	4.50	2018.59	783.61	2817.44
XII	30.58	34.84	447.61	435.37	951.50	5.17	79.0	876.83	986.85	1869,52

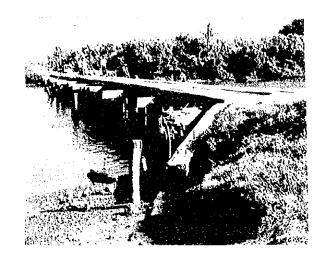
TABLE 7(3) EXISTING ROAD LENGTH, 1985

\$ \$ \$ \$			Barangay				-	Total	
E 0 . D	Concrete	Asphalt	Gravel	Earth	Total	Concrete	Asphalt	Gravel	Earth Total
Philippines	ı	i	90213.83	1	90213,83	9188.15	12049.78	130749.11	9721.59161708.63
ω υ ν		1	234.71	1	234.71	1073.52	1416.43	437.20	11.78 2938.93
þ····	ı		11011.23	ı	11011.23	545.44	1896.59	14380.08	1157.62 17989.73
jeret jevel	ı	ı	7745.80	1	7745.80	636.55	323.44	11520.80	686.59 13167.38
	ı	1	7943.06	1	7943.06	1372.08	1191.48	10362.91	386,05 13312.52
IV-A	•	ı	5428.89	,1	5428.89	956.66	1809.76	7537.69	460.87 10764.98
IV-B	ı	t	3782.27		3728.27	85.61	345.82	7191.26	532,56 8155,25
>	t	1	4012.86	8	4012.86	786.85	993.01	6550.47	547.78 8878.11
₩ >	1	ı	7486.82		7486.82	654.41	935.25	11487.60	223.67 13300.93
IIA	ı	ŧ	5854.05	ĭ	5854,05	303.66	1192.36	9089.97	526.04 11112.03
IIA	1	g	5113.86	1	5113.86	1016.22	407.12	7466.02	432.05 9321.44
XI	3	ı	5210.93	1	5210.93	64.20	625.00	7980.22	532.16 9201.58
×	1	ı	9675.19	1	9675.19	727.60	562.51	13489.47	1204.00 15983.58
ïx	ŧ	ŧ	9306.09	1	9306.09	523.72	254.15	13631.48	1382.98 15792.33
IIX	1	1	7408.08	1	7408.08	442.14	96.84	9623,94	1627.46 11790.38

APPENDIX II

PHOTOGRAPHS OF BRIDGES

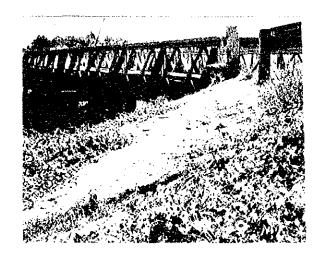




BRIDGE NO. 02.01

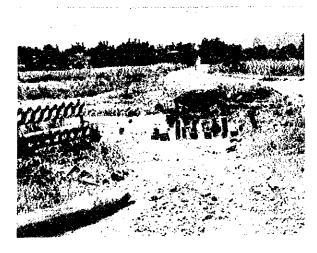
NAME OF BRIDGE: STA. CRUZ BRIDGE





BRIDGE NO. 02.02

NAME OF BRIDGE: DUMADATA BRIDGE:





BRIDGE NO. 02.05 NAME OF BRIDGE : DIDUYON BRIDGE





BRIDGE NO. 04.010

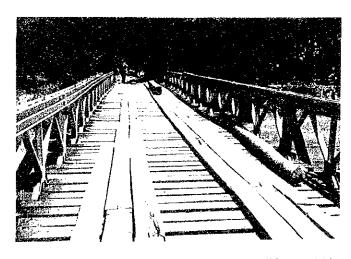
NAME OF BRIDGE: BINAMBANG BRIDGE





BRIDGE NO. 04,03a

NAME OF BRIDGE: LEVISTE IL BRIDGE





BRIDGE NO. 04.04b

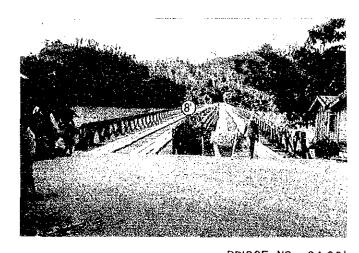
NAME OF BRIDGE: LUMANG BAYAN BRIDGE

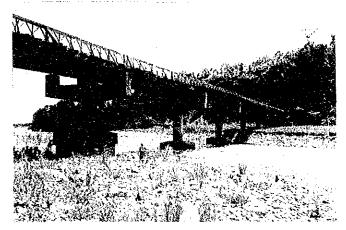




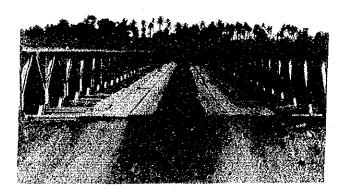
BRIDGE NO. 04.05b NAME OF BRIDGE: OLANGOAN

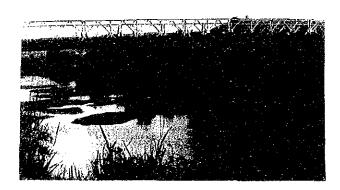
BRIDGE





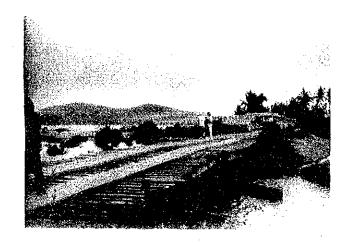
BRIDGE NO. 04.06b NAME OF BRIDGE: BONGABON BRIDGE

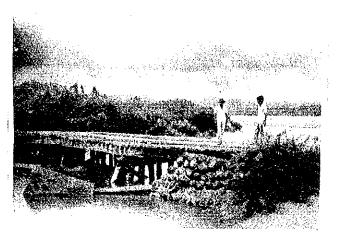




BRIDGE NO. 05.03

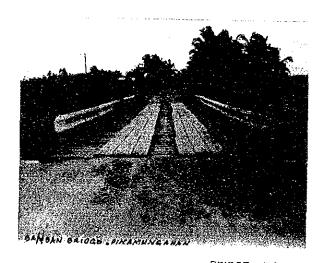
NAME OF BRIDGE: NARANGASAN I BRIDGE





BRIDGE NO. 06.03

NAME OF BRIDGE: IYANG BRIDGE

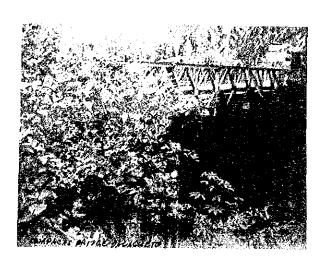




BRIDGE NO. 07.01

NAME OF BRIDGE BANBAN BRIDGE

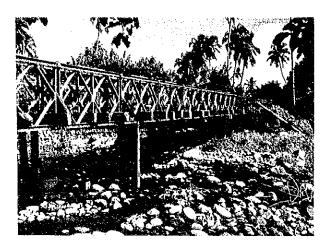




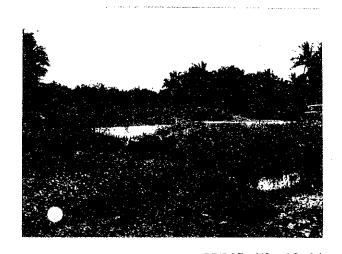
BRIDGE NO. 07.02

NAME OF BRIDGE: CAMPACAS BRIDGE





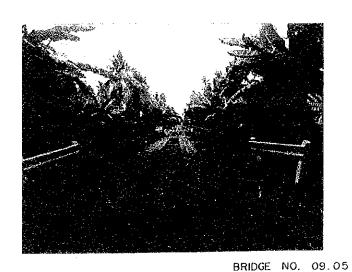
BRIDGE NO. 08.03 NAME OF BRIDGE: HABAY BRIDGE





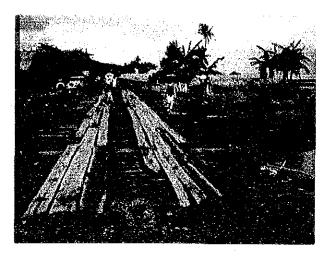
BRIDGE NO. 08.04

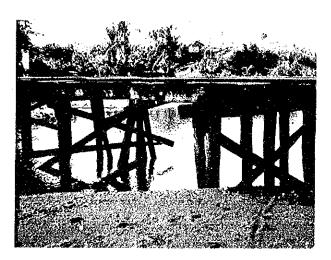
NAME OF BRIDGE TALISAYAN RIVER CROSSING





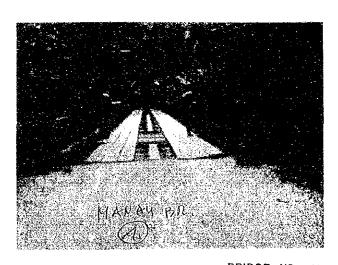
NAME OF BRIDGE: PATUNAN BRIDGE





BRIDGE NO. IO.OI

NAME OF BRIDGE: HAYANGABON BRIDGE





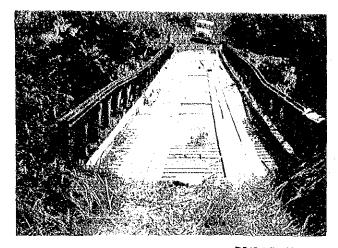
BRIDGE NO. 11.04

NAME OF BRIDGE: MANAY BRIDGE



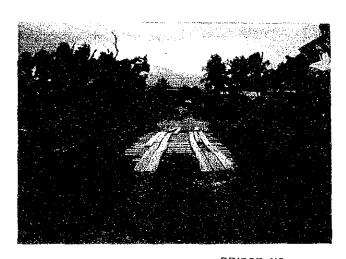


BRIDGE NO. 12:01 NAME OF BRIDGE; PİKINIT BRIDGE



BRIDGE NO. 12.02

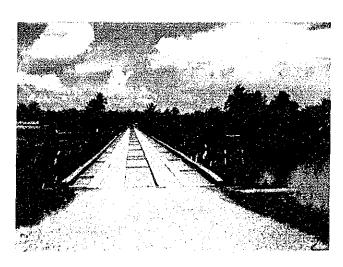
NAME OF BRIDGE: DURUGAO BRIDGE





BRIDGE NO. 12.04

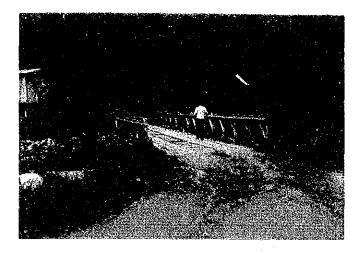
NAME OF BRIDGE : DANGOLAAN BRIDGE

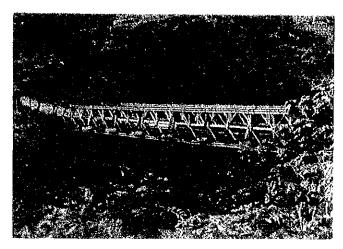




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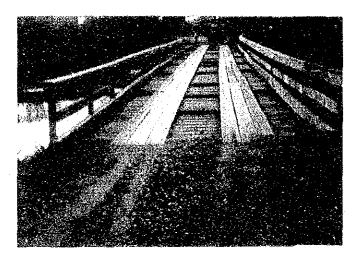
NAME OF BRIDGE: SAPAKAN BRIDGE

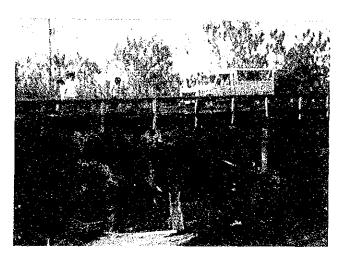




BRIDGE NO. 01.01

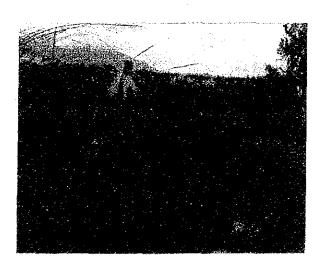
NAME OF BRIDGE: ELLET BRIDGE





BRIDGE NO. 01.02

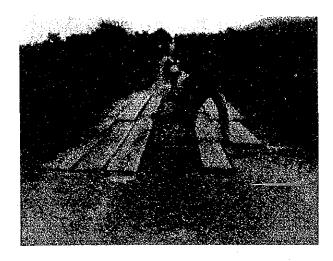
NAME OF BRIDGE BIMMILOG BRIDGE





BRIDGE NO. 03.01

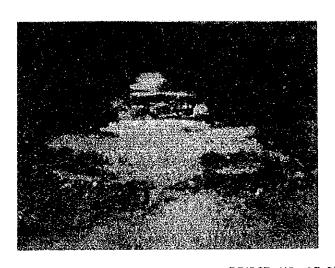
NAME OF BRIDGE: SEGUM BRIDGE





BRIDGE NO. 03.02

NAME OF BRIDGE: CALABASA BRIDGE





BRIDGE NO. 03.03

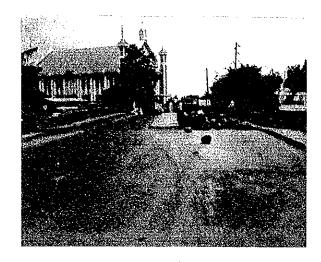
NAME OF BRIDGE! MALINAO BRIDGE

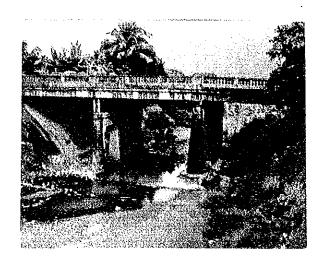




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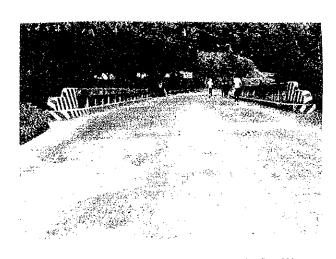
NAME OF BRIDGE: ASAM BRIDGE





BRIDGE NO. 04.020

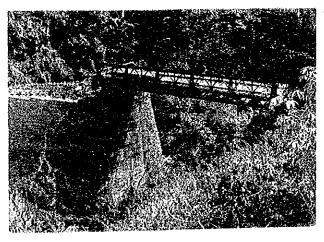
NAME OF BRIDGE: MANGO BRIDGE

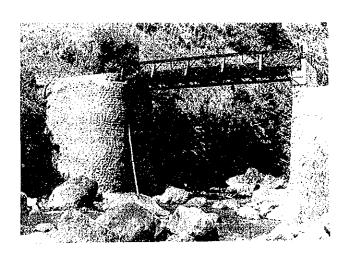




BRIDGE NO. 05.01

NAME OF BRIDGE : DAGUIT BRIDGE

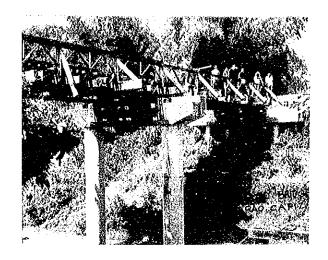




BRIDGE NO. 06.01

NAME OF BRIDGE: TALUS BRIDGE





BRIDGE NO. 06.05

NAME OF BRIDGE: TUMALALUD BRIDGE

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