III. RIO TUBA MINE

CHAPTER III: RIO TUBA MINE

3.1 History and Future Prospects

The Rio Tuba Mine was developed comparatively recently by the Rio Tuba Nickel Mining Corporation which was set-up as a joint venture by an American company, UOP Co., and Philippine capital in 1969. The Rio Tuba Corp. subsequently began exploration and prospecting for nickel deposits.

In 1971 a feasiblity study on the potential for extraction of 2 million DMT/year conducted by a group of Japanese companies (Pacific Metals Corp., Ltd. Nippon Mining Co., Ltd., and Sumitomo Metal Minig Corp., Ltd.) was completed and the report for the same was finalized in the following year, 1972. As a result, application for 285 new mine lots for the Rio Tuba Corp. was conducted in addition to the 110 mine lots already settled.

In 1973 Pacific Metals Corp. acquired all stocks held by UOP Co., (40% of total stocks) becoming chief stock holder in the Rio Tuba Corp. At the same time, the Japanese Government was requested to conduct a basic design feasibility study for a development plan. Although the original objective of the plan was 1 million DMT of nickel production, this objective was reduced to 500,000 DMT, all destined for export to Japan, by the Technical Committee in response to economic conditions resulting from the Oil Crisis in 1974. In March, 1975, Nippon Steel Corp., Nisshin Steel Co., Ltd., and Nissho Iwai Corp., decided to invest in the Rio Tuba Corp., acquiring 13%, 10% and 10% of shares respectively (Pacific Metals Corp., held the remaining 67%) and promoting further development.

In 1975, with capital investment by the Export-Import Bank of Japan, construction was begun and main mining facilities were completed by December, 1976. At the same time capital for related mine facilities was provided under the JICA grant aid program with which hospital, school and gymnasium facilities for the Rio Tuba Mine employee town site were established. Mine operation commenced from January 1977 and 22,000 WMT of ore were exported to the Pacific Metals factory in Japan by April of the same year.

Operation continued smoothly for several years; however, the effects of world-wide recession caused by the second oil crisis resulted

in reduced demand for nickel. Even with the subsequent drop in international nickel prices demand failed to increase (TABLE 3-1). Accordingly, in 1979 the Rio Tuba Corp., recognizing that decreased production was unavoidable (TABLE 3-2), halted use of its diesel powered ore-drier in favor of sunlight drying and export of wet unprocessed ore in order to reduce production costs.

Shipment of wet, unprocessed ore however, entails additional shipping costs (nickel content of shipped ore is only 5%) and electric fees for processing in Japan. This has led the Rio Tuba Corp. and Pacific Metal Corp. to consider establishing a new smelting system at the mine itself with the added objective of increasing local benefits within the Philippines.

Although establishment of smelting facilities is still under study and exact power demands of the same are not yet clear, it is obvious that a large amount of power will be required for operation of the same (total peak load for the mine: about 7,500kW). Accordingly, it is desirable that as much of this power as possible be supplied by less expensive hydropower as part of the Rio Tuba Corp. cost reduction scheme.

The Rio Tuba Mine nickel reserve for potential development as of 1983 amounted to 23 million WMT at the high-quality Guintalungan ore vein alone and with the revival of the international nickel market and continued nickel scarcity, it is likely that the number of mine lots at Rio Tuba will increase and mine operation will continue for several decades hence.

3.2 Electrical Facilities and Power Demand

3.2.1 Electrical Facilities

The Rio Tuba Mine is equiped with three 700kW diesel generators at the plant site, and one 160kW and one 50kW diesel generator at the pier site. The power plant facilities at the plant site were jointly manufactured by Japanese companies in 1976 and are functioning efficiently. There are also about 6.5km of 4.16kV and 230V distribution line strung.

Operation and maintenance of the above facilities is performed by a total of 32 workers (not including managerial staff) in 3 shifts.

Overhaul of the generators takes place once in every 3,000 operation hours, and the most recent overhaul was conducted from Sept. to Oct. 1983 which makes the total operating hours to date 27,000. In general, maintenance and equipment condition is good and repairs are performed with adequate technical skill. A single line diagram for the plant and pier site is presented in FIG. 3-1. The electrical systems of the 2 sites however, are as yet unconnected.

3.2.2 Power Supply Conditions

Since Rio Tuba Mine commenced operation in 1977, efforts have been made to reduce production costs. Energy-saving sunlight drying was adopted in 1979 for example in place of the drier facility and the heat source for the latter was converted from electricity to heavy crude oil in 1982. As a result, peak load was drastically reduced from approximately 1,100kW to about 310kW, and generator operation was limited to the use of only 1 unit among the 3 existing units. In addition diesel fuel was changed from light to heavy crude oil further reducing power supply costs. Power supply conditions at the Rio Tuba Mine are presented in FIG. 3-2, while a recent example of the daily load curve is as shown in FIG. 3-3.

JAPAN INTERNATIONAL COOPERATION AGENCY

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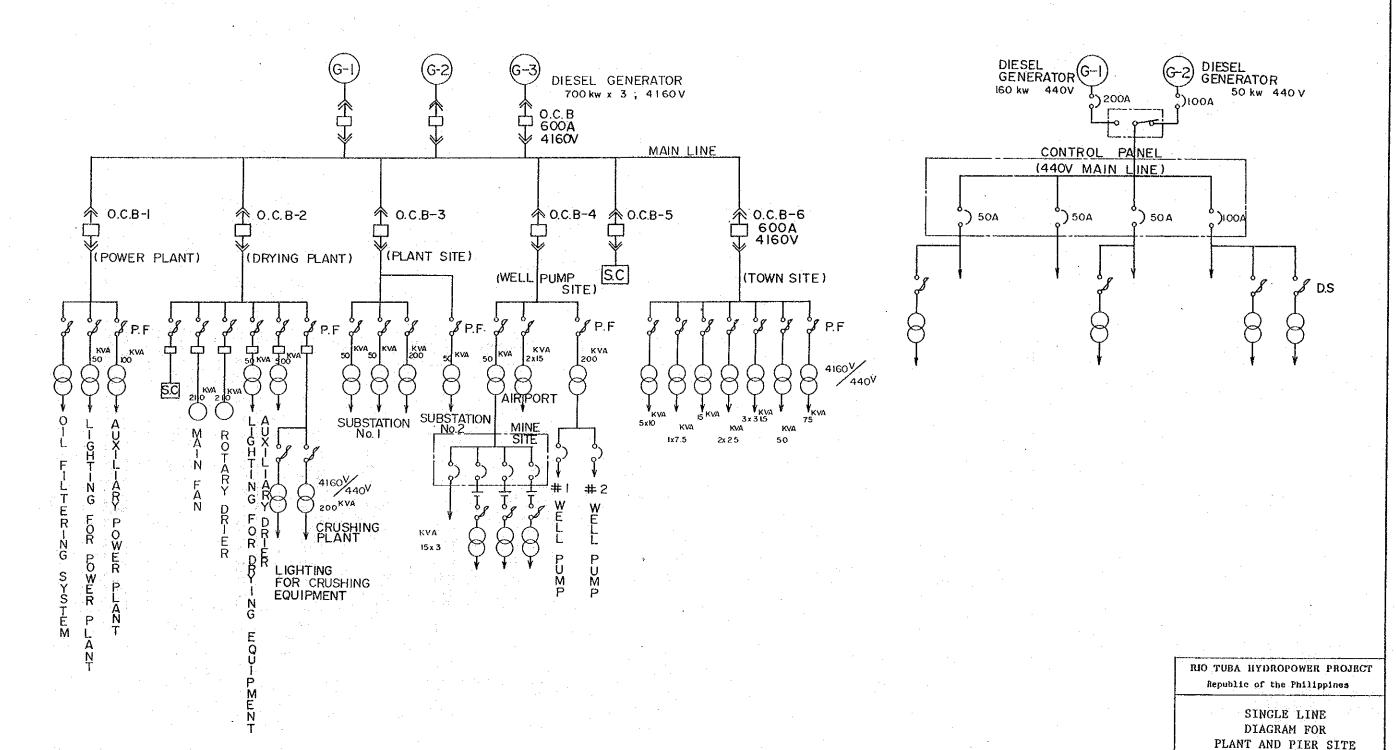
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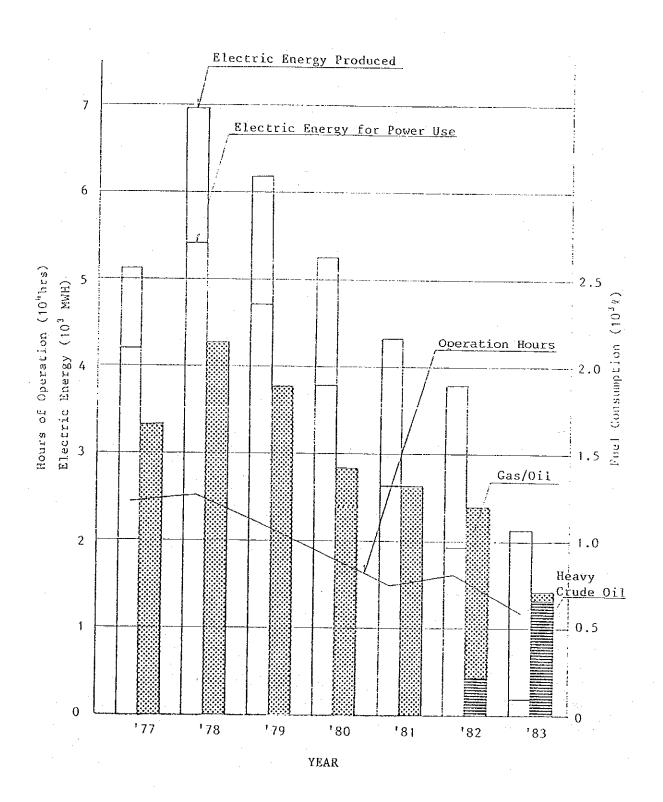
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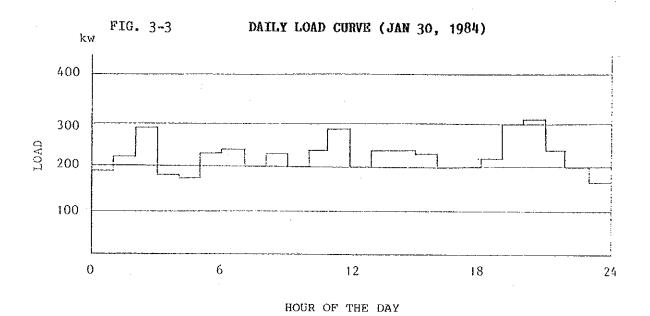
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PLANT SITE SINGLE LINE DIAGRAM

PIER SITE SINGLE LINE DIAGRAM







INTERNATIONAL NICKEL PRICE PLUCTUATIONS TABLE 3-1

Year	INCO (d/1b) (a)	Canadian Producer Price (\$/MT) (b)	Commerical Market Price (\$/MT) (c)
1975	207.3	4,570	4,155
1976	225.3	4,970	4,573
1977	241.0	5,200	4,579
1978	••	4,610	4,254
1979	280.5	5,990	5,642
1980	342.9	7,530	6,783
1981	345.0	7,560	6,736
1982	320.0	7,055	5,132
1983	320.0	7,053	4,802
1984*	-	7,273	5,510
1985*	-	7,494	6,171
1990 *		11,708	-
1995 *	500	17,965	<u></u>

Source: (a) Mining Manual 1983 (b), (c) Commodity Price, World Bank, 1984 Jan.

TABLE 3-2 CHANGES IN PRODUCTION, SALES AND FINANCIAL CONDITIONS OF RIO TUBA MINING CORP.

Year Item	1977	1978	1979	1980	1981	1982	1983
Amount Produced	472,198	644,443	759,839	675,223	542,737	474,506	421,004
Amount Sold	375,735	661,997	729,367	601,449	631,421	431,112	437,036
Turnover	8,130	9,843	13,543	17,958	16,251	9,897	6,340
Net Profit before Taxes	128	2,330	1,924	3,297	114	950	278

IV. POWER AND ENERGY
DEMAND FORECAST

CHAPTER IV POWER AND ENERGY DEMAND FORECAST

4.1 Objectives of Load Forecast

The 3,800kW maximum capacity hydropower plant to be constructed on the Tamlang River will supply the Rio Tuba Mine through a 34.5kV transmission line 44km in length. A certain portion of the same will also be used to supply electricity to rural communities along the transmission line route which are not presently electrified, thus contributing to the rural electrification program and improvement of rural life.

In consideration of the above overall objectives, load forecast was focused on the following:

- a) power demand forecast in communities to be newly electrified and determination of power distribution to PALECO and the Rio Tuba Mine;
- b) use of a few case studies regarding Rio Tuba Mine energy demand for formulation of the smelting process presently under study.

4.2 Study of Domestic Power Supply

4.2.1 Present Conditions

Brookes Point town is located about 15km northeast of the hydropower project site in Brookes Point Municipality. The population of the same is about 6,000, one of the largest population centers in the Project area. PALECO commenced supply of electricity in the area in March 1982 and a total of 11 rural communities are presently served by the same. Electrification conditions in Brookes Point Municipality are as presented in 2.4.4 above.

PALECO has 2 diesel generators supplying electricity to the above; a 300kW generator manufactured in 1945 and a 150kW generator made in 1969. In addition, connection of the PALECO power systems between Brookes Point, Naraa, Aborlan, and Quezon, is expected to be completed by 1988, the year in which the proposed Tamlang River Hydropower Project is scheduled to begin operation. All communities south of Brookes Point town to the Rio Tuba Mine are presently without electrical power supply.

4.2.2 Residential Power Demand

An interview survey was conducted in 12 rural communities (barangays) in Bataraza Municipality to determine the relationship between such factors as power demand, income, and fuel consumption among low, middle, and high income households. Survey results revealed that 1.6-18% of kerosine are consumed, and 14-158 pesos are expended monthly for lighting with an average monthly consumption of 3% at 26.4 pesos. In addition approximately 60% of households spend 15 pesos/month on dry-cell batteries for radios. The majority of people expressed the desire to become recipients of any future power supply scheme and further, as the lowest PALECO electricity rate is presently 31.1 pesos for up to 12kWh, capability of payment was deemed generally sufficient. At present, PALECO bears the cost of both wattmeter installation and line extension up to 45m from the distribution line (45m x number of household applicants). This policy greatly facilitates electrification for rural residents.

4.2.3 Load Forecast for Residential Power Supply

Load forecast for residential power demand was made for each rural community in the area according to the following conditions.

(1) Communities eligible for power supply are:

Brookes Point Municipality	Bataraza M	<u>lunicipality</u>
(South of Brookes Point Town)		
Tubtub	Inogbong	Colandanum
Oringoring	Bataraza	Rio Tuba
Tagperara	Bonobono	0cayan
Saraza	Malihod	Iwahig
Samariniana	Bulalacao	Igangigang
Salogon	Tarusan	Sarong
Malis	Sandova1	

- (2) Load forecast was made for a period of 20 years commencing with envisaged power plant start-up in April 1988.
- (3) Household power demand forecasts were made on the following premises:
 - a) Population increase was estimated for each community in consideration of past population increase rate,

- infrastructure development by PIADP, and migration trends resulting from electrification, etc.;
- b) Household number was calculated as population divided by average number of persons was per household. According to the census conducted in 1980, the average number of persons per household was 5.2 and 4.7 in Brookes Point and Bataraza municipalities respectively;
- c) Date for available of electric service in each barangay was estimated by distance from transmission lines, size of community, etc.;
- d) Initial electrification rate was estimated for each community with a 10% growth rate in the first 2 years and uniform growth thereafter. The above figures were determined in consideration of the difficulties involved in supplying individual households and small, isolated mountain communities.
- e) The number of electrified households was obtained by the multiplication of the electrification rate and the number of households;
- f) Electrical appliances were estimated for each income level, and initial average peak load of 80W per household with a 4% growth rate was assumed; and,
- g) A load factor of 30% was determined by estimation of residential power supply usage.
- (4) Demand for commercial use, public buildings, street lights, and small scale industry was estimated from number of users and peak load per user.
 - a) Number of users was assumed as 5% of number of residental user households.
 - b) Peak load per user was estimated at 170W and peak load growth rate at 5%.
 - c) Load factor was estimated as 35% based on usage conditions.
- (5) Demand for north of and including Brookes Point town will be about 800kW by the time of hydropower plant start-up according to the PALECO program, while, at the same time, the equivalent of 450kW of power output from the existing PALECO diesel generator at Brookes Point town will be supplemented by the hydropower plant to be installed by the Project. Load factor was estimated at 32% and annual output at 1,261MWH.

Demand estimate of power output for rural electrification is presented in TABLE 4-1, estimate of power demand for south of

Brookes Point twon in TABLE 4-2 and precentage of energized households for town and rural communities in TABLE 4-3.

4.3 Study of Rio Tuba Mine Power Supply

4.3.1 Present Conditions

Ore drying operations consume the largest percentage of electrical energy and costs in mine operation at Rio Tuba Mine. The Rio Tuba Mine which opened in 1977, originally used an electrical drier. In 1979 however, sunlight drying was adopted and the heat source for the drier was converted from electricity to crude oil in mid 1982 in an effort to reduce production costs. At the same time, restrictions were imposed upon electric consumption in residential use by employees. The combination of the above resulted in drastic decrease in electricity consumption, peak load dropping from about 1,100kW to 310kW while the number of generators required to fulfill demand was limited to the use of only 1 unit among the 3 existing units.

Present conditions of power supply at the Rio Tuba Mine are as illustrated in FIG. 4-1.

4.3.2 Demand Forecast of Power Supply for Mine Use

The Rio Tuba Mine is presently conducting a study to develop a plan to strengthen smelting facilities, etc. and thereby to increase values added to nickel ore production. As the above is still under study, accurate estimate of energy demand for smelting facilities at this stage is difficult to determine and accordingly energy demand forecasts were made for 3 possible cases, namely:

- Case-1 resumption of ordinary drier facility used before the present sunlight method;
- Case-2 establishment of new facilities within the maximum utilization of available energy from the hydropower plant; and.
- Case-3 installation of a new smelting system.

These cases are further detailed on the following page.

(1) Case 1

The case was assumed with the following conditions.

- 1) Demand forecast was for a 24-year period from 1984 to 2007;
- 2) Energy consumption of the drier until commencement of hydropower plant operation will be 200MWH. After start-up in 1988, the drier will be used in rainy season and sunlight drying in dry season. Energy demand for the same was designated at 3,793MWH, the 1980 standard, while the operation factor for the drier was 50%; and,
- 3) Energy consumption, excluding the drier, was estimated to have a growth rate of 4% until 1987, 8% from 1988 to 1997 and 4% thereafter. Peak load growth rate has been the same as the above.

The results of the study are presented in TABLE 4-4.

(2) <u>Case 2</u>

The case was assumed according to the following conditions:

- 1) Demand forecast period covered 20 years from 1988 to 2007;
- 2) Peak load for all facilities including employees' houses was estimated at 3,450kW, taking into account transmission line loss, and power supply of communities; and,
- 3) With a load factor of 65%, consumption of electricity was determined at 19,645MWH.

(3) Case 3

Conditions of the case were as follows:

- 1) Demand forecast period was 20 years from 1988 to 2007;
- 2) Peak load was estimated at 8,500kW with a similar approach as Case 2 above; and,
- 3) Energy consumption was determined at 59,568MWH with a load factor of 80%.

4.4 Power Distribution for Domestic and Mine Use

Residential and mine use demand forecasts to the year 2007 discussed in 4.2.3 and 4.3.2, respectively, are summarized in TABLE 4-5.

Peak demand for rural electrification 10 years after start-up of the Tamlang River Hydropower Plant is estimated at 999kW, representing 26.3% of the plant's maximum output (3,800kW) and power consumption will be 2,844MWH. As this also represents 14.9% of the annual available energy (19,087MWH), the power distribution is considered appropriate from the perspective of Project objectives. Thus, priority for use of forecast energy until 1997, and supply of 1,000kW peak demand with annual energy demand of 2,844MWH thereafter, will be given to PALECO.

4.5 Balance of Supply and Demand for Mine Use

Supply and demand balance estimation was conducted according to the following conditions:

- a) Start-up of the Tamlang River Hydropower Project was designated as April 1988;
- b) Forecast demand for rural electrification will be supplied up to 1997, while only 1,000kW of peak energy and 2,844MWH/year will be supplied for the same thereafter;
- c) Transmission line and transformer losses were considered;
- d) The Rio-Tuba Mine diesel generator installed at the pier site was not considered as a source of power supply;
- e) The existing Rio Tuba Mine diesel generators which are in good condition will be used until 1997; and,
- f) Regular inspection, overhaul etc. of diesel generators will be undertaken during the rainy season.

Estimated available hydropower energy for the Rio Tuba Mine is presented in TABLE 4-6.

4.5.1 Case Analysis

To determine the optimum development plan in light of power and energy demand several case studies were carried out; namely, Case-1, 2 and 3. A summary of the findings are presented hereinafter on the following page.

(1) <u>Case-1</u>

Supply and demand balance for Case-1 is provided in TABLE 4-7. In this case, a surplus of 2,173kW - 1,755kW occurs at peak, and 11,458MWH - 5,727MWH in electric energy from 1988-2007. In addition to developing further power demand at Rio Tuba Mine or planning new facilities, etc. for the same, a plan should also be developed to increase power supply for PALECO and create new sources of power demand.

(2) Case 2

The supply-demand balance for Case-2 is provided in TABLE 4-8. Although the hydropower plant is equipped with weekly regulation capacity via a regulating pond, it is possible that power supply to the Mine would occasionally be insufficient during the dry season as the supply to rural electrification is given priority. Simple calculations indicate that a lack of 1,350kW will occur in peak load, and accordingly, study of a coordinated operation system to compensate the peak shortage through operation of both the diesel and hydropower plants at the Rio Tuba Mine is required.

(3) Case-3

The supply-demand balance for Case-3 is shown in TABLE 4-9. In this case an insufficiency of 6,400kW in power output and 33,014MWH -34,127MWH in electric energy will occur from 1988-2007. As in Case-2, insufficiencies will be compensated, use of other power sources will be minimized and balance will be maintained by coordination of diesel generator operation with hydropower plant operation.

ENERGY DEMAND OF RIO TUBA MINING CORPORATION

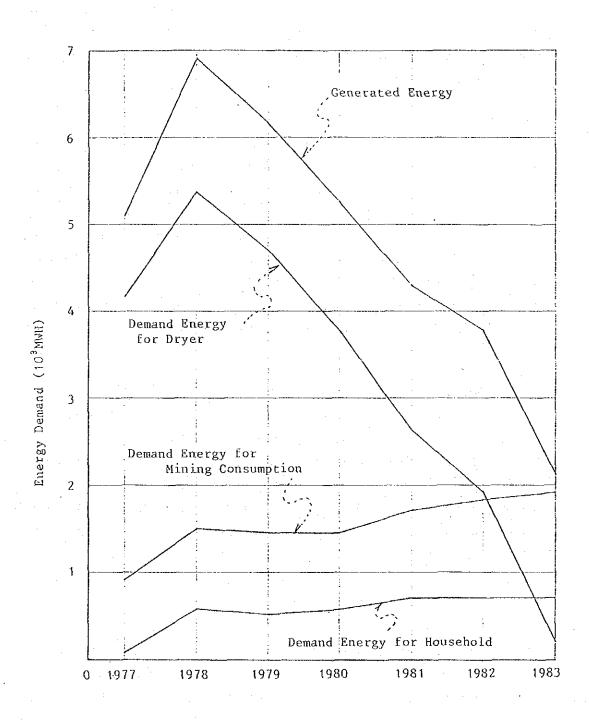


TABLE 4-1

DEMAND FORECAST FOR RURAL ELECTRIFICATION

V 0 0 0	North of B Including	Brookes Point Brookes Point Town	South of Brookes	s Point Town	Total	;al
1 0	Peak Demand (kW)	Energy Demand (MWH)	Peak Demand (kW)	Energy Demand (MWH)	Peak Demand (kW)	Energy Demand (MWH)
188	L SO	1 261	191	170	7177	1 731
1989	450	1,261	227	652	677	1, 93,
990	450	1,261	291	833	741	2,094
391	450	1,261	332	951	782	2,212
392	450	1,261	369	1,058	819	2,319
393	450	N	401	1,152	851	2,413
166	450	1,261	434	1,248	884	2,509
395	450	O	169	1,349	919	2,610
966	450	C	506	1,457	959	2,718
197	450	S	549	1,583	666	2,844
998	450	1,261	290	1,703	1,040	2,964
666	450	1,261	639	1,854	1,089	3,106
000	450	N	069	1,992	1,140	3,253
001	450	1,261	745	2,157	1,195	3,418
202	450	1,261	808	2,338	1,258	3,599
203	450	1,261	870	2,521	ന	3,782
00 ti	450	1,261	246	2,729	1,329	3,990
305	450	1,261	1,017	2,949	1,467	4,210
900	450	1,261	1,097	3,186	1,547	<u> </u>
. 200	Cu Z	, ,				

ESTIMATED MAXIMUM POWER DEMAND AND ENERGY DEMAND FOR SOUTH OF BROOKES POINT TOWN

RESIDENTIAL
INCREASE RATE OF DEMAND 4%
LOAD FACTOR 30%
COMMERCIAL, PUBLIC BUILDINGS AND STREET LIGHTS
INCREASE RATE OF DEMAND 5%
LOAD FACTOR 35%

				RES.	IDENTIAL	. *	
	-	POPULA-	HOUSE-	ENERGIZED	AVERAGE	PEAK	ENERGY
	YEAR	TIOH	HOLD	HOUSEHOLD	DEMAND	DEMAND	DEWUND
1	1988	24,802	5,047	1,984	800	159KW	418MWH
Ž	1989	25,738	5,238	2,652	8311	220KW	578MWH
3	1990	26,706	5,430	3,244	87W	282KW	741MWH
4	1991	27,718	5,632	3,562	901/	321KW	844MUH
5	1992	28,770	5,848	3,795	9411	357KW	938MWH
E	1993	29,862	6,067	3,995	97W	388KW	1,020MWH
7	1994	30,996	6,297	4,160	1016	420KW	1,104MWH
8	1995	32,179	6,536	4,319	105W	453KW	1,190MWH
9	1996	33,405	6,783	4,482	1096	489KW	1,285MWH
10	1997	34,680	7,040	4,652	1140	530KW	1,393MWH
11	1998	36,010	7,307	4,828	118W	570KW	1,498MWH
12	1999	37,387	7,586	5,014	123W		1,621MbH
13	2000	38,822	7,875	5,205	128W	666KW	1,750MWH
14	2001	40,315	8,175	5,405	133₩	719KW	1,890MWH
15	2002	41,868	8,485	5,609	1396	780KW	2,050MWH
16	2003	. 43, 483.	8,814	5,827	1446		2,205MWH
17	2004	45,159	9,149	6,050	150W	908KW	2,386MWH
18	2005	46,906	9,503	6,285	156W	980KW	2,575MWH
19	2006	48,723	9,866	6,525	162W	1,057KW	2,778MWH
20	2007	50,612	10,247	6,775	169W	1,145KW	3,009MWH

		0.00	ARACTER TOTAL			TOTOL	
		; LO	MERCIAL			TOTAL	
			HUERAGE	PERK	ENERGY		ENERGY
	YEAR	HUMBER	DEMAND	DEMAND	DEMAHD	OHAMBO	, –
1	1988	99	170W	17KW	52MWH	164KW	
2	1989	133	179W	24KW	74MWH	227KW	652MWH
3	1990	162	187W	30KW	92MJH	291KW	833MWH
4	1991	178	197W	35KW	107MWH	332KW	
5	1992	190	207W	. 39KW	120MWH	369KW	1,058MWH
6	1993	200	217W	43KW	132MWH	401KW	1,152MWH
71	1994	208	228W	47KW	144MWH	434KW	1,248MWH
8	1995	216	239₩	52KW	159MWH	469KW	1,349MWH
9	1996	224	251W	56KW	172MWH	506KW	1,457MWH
10	1997	233	264W	62KW	. 19QMWH	549KW	1,583MWH
11	1998	241	2776	67KW	205MWH	: 590KW	1,703MWH
12	1999	251	291W	73KW	224MWH	639KW	1,845MWH
13	2000	260	305₩	79KW	242MWH	690KW	1,992MWH
14	200i	270	321W	87KW	267MWH	745KW	2,157MWH
15	2002	280	337₩	:94KW	288MWH		2,338MWH
16	2003	291	353W	103KW	316МЫН	870KW	2,521MWH
17	2004	303	371W	112KW	343MWH	942KW	2,729MWH
18	2005	314	390W	- 122KW	374MWH	1,017KW	2,949MWH
19	2006	326	.409Ы	133KW	408MWH	1,097KW	3,186MWH
20	2007	339	430W	146KW	448MWH	1,189KW	3,457MWH

TAGPERARA INCREASE RATE 0F POPULATION 4.4%	PGPULR- HGUSE- ENERGIZED 1 1988 1,286 238 40% 95 2 1989 1,296 248 50% 124 1 1980 1,296 248 50% 124 1 1980 1,406 248 50% 162 1 1991 1,406 2870 60% 169 1 1995 1,570 209 60% 169 1 1995 1,671 321 60% 177 1 1996 1,901 366 60% 220 1 1 1998 1,901 366 60% 220 1 1 1998 1,901 366 60% 220 1 2 2000 2,072 398 60% 220 1 2 2001 2,163 416 60% 220 1 2 2005 2,559 446 60% 272 1 2 2005 2,570 40% 60% 284 1 2 2005 2,588 453 60% 272 1 2 2006 2,683 516 60% 310 2 2007 2,633 516 60% 310	SARAZA INCREASE RATE OF POPULATION 4.42	PUPULR- HOUSE- ENERGIZED 1 1988 2,258 434 402 174 2 1989 2,357 453 502 227 4 1991 2,461 473 602 224 1992 2,662 516 602 296 1995 2,800 538 602 296 11995 3,052 587 602 323 11 1998 3,473 652 602 323 12 2000 3,786 728 602 384 11 1998 3,473 668 602 384 11 1998 3,473 668 602 384 12 2001 3,786 728 602 418 15 2003 4,126 728 602 476 16 2003 4,508 828 602 476 17 2004 4,497 865 602 497 18 2005 4,508 828 602 497 19 2006 4,902 943 602 566 20 2007 5,117 984 602 566
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TUBTUB INCREASE RATE OF POPULATION 4.4%	PULR- HUUSE- ENERGIZED VERR TIGN	ORINGORING INCRERSE RATE OF POPULATION 4.4%	YEAR TIGN HOUSE - ENERGIZED YEAR TIGN HOLD RATE HOUSEHOLD 2990 1,313 253 40% 100 1990 1,434 2875 60% 172 145 1992 1,560 300 60% 189 1,775 9 1995 1,775 300 60% 189 1,995 1,775 80% 1995 1,955 1,955 372 60% 2,23 1,955 1,955 372 60% 2,59 1,955 2,108 405 60% 2,59 1,955 2,509 461 60% 2,59 1,955 2,509 461 60% 2,59 1,955 2,509 461 60% 2,59 1,955 2,509 461 60% 2,59 1,955 2,509 2

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TABLE 4-4

DEMAND FORECAST OF RIO TUBA MINING CORPORATION (CASE 1)

Year	Facili Excepting		Drier	System	Tot	al
	Peak Demand (kW)	Energy Demand (MWH)	Peak Demand (kW)	Energy Demand (MWH)	Peak Demand (kW)	Energy Demand (MWH)
1984 85 86 87	322 335 349 363	2,014 2,095 2,179 2,666	900 900 900 900	200 200 200 200	1,222 1,235 1,249 1,263	2,214 2,295 2,379 2,866
1988 89 90 91 92 93 94 95 96	377 392 408 424 441 459 477 496 516	2,357 2,546 2,749 2,969 3,207 3,463 3,740 4,039 4,363 4,712	900 900 900 900 900 900 900 900	3,793 3,793 3,793 3,793 3,793 3,793 3,793 3,793 3,793 3,793	1,277 1,292 1,308 1,324 1,341 1,359 1,377 1,396 1,416 1,436	6,150 6,339 6,542 6,762 7,000 7,256 7,533 7,832 8,156 8,505
1998 99 2000 01 02 03 04 05 06	558 581 604 628 653 679 706 735 764 795	4,900 5,096 5,300 5,512 5,733 5,962 6,201 6,449 6,707 6,975	900 900 900 900 900 900 900 900	3,793 3,793 3,793 3,793 3,793 3,793 3,793 3,793 3,793	1,458 1,481 1,504 1,528 1,553 1,579 1,606 1,635 1,664 1,695	8,693 8,889 9,903 9,305 9,526 9,755 9,994 10,242 10,500 10,768

TABLE 4-5

SUMMARY OF DEMAND FORECAST

Year		ral fication	Cas		lio Tuba Cas	e-2	Cas	e-3
	Peak Demand (kW)	Energy Demand (MWH)	Peak Demand (kW)	Energy Demand (MWH)	Peak Demand (kW)	Energy Demand (MWH)	Peak Demand (kW)	Energy Demand (MWH)
1988	614	1,731	1,277	6,150	3,450	19,645	8,500	59,568
89	677	1,913	1,292	6,339	3,450	19,645	8,500	59,568
90	741	2,094	1,308	6,542		19,645	8,500	59,568
91	782	2,212	1,324	6,762		19,645	8,500	59,568
92	819	2,319	1,341	7,000		19,645	8,500	59,568
93	851	2,413	1,349	7,256		19,645	8,500	59,568
94	884	2,509	1,377	7,553	3,450	19,645	8,500	59,568
95	919	2,610	1,396	7,832	3,450	19,645	8,500	59,568
96	956	2,718	1,416	8,156	3,450	19,645	8,500	59,568
97	999	2,844	1,436	8,505	3,450	19,645	8,500	59,568
1 8 1								
1998	1,040	2,964	1,458	8,693	3,450	19,645	8,500	59,568
99	1,089	3,106	1,481	8,889	3,450	19,645	8,500	59,568
2000	1,140	3,253	1,504	9.093	3,450	19,645	8,500	59,568
01	1,195	3,418	1,528	9,305	3,450	19,645	8,500	59,568
02	1,258	3,599	1,553	9,526	3,450	19,645	8,500	59,568
03	1,320	3,782	1,579	9,755	3,450	19,645	8,500	59,568
04	1,392	3,990	1,606	9.994	3,450	19,645	8,500	59,568
05	1,467	4,210	1,635	10.242	3,450	19,645	8,500	59,568
06	1,547	4,447	1,664	10,500	3,450	19,645	8,500	59,568
07	1,639	4,718	1,695	10,768	3,450	19,645	8,500	59,568

AVAILABLE HYDROPOWER ENERGY FOR RIO TUBA MINING CORPORATION

TABLE 4-6

Year	Available Energy <u>1</u> /	Energy A 2/	Demand B <u>3</u> /
	(MWH)	(HWM)	(MWH)
1988	19,087	1,731	17,356
89	19,087	1,913	17,174
90	19,087	2,094	16,993
91	19,087	2,212	16,875
92	19,087	2,319	16,768
93	19,087	2,413	16,674
94	19,087	2,509	16,578
95	19,087	2,610	16,477
96	19,087	2,718	16,369
97	19,087	2,844	16,243
1998	19,087	2,844	16,243
. 99	19,087	2,844	16,243
2000	19,087	2,844	16,243
. 01	19,087	2.844	16,243
02	19,087	2,844	16,243
03	19,087	2,844	16,243
04	19,087	2,844	16,243
05	19,087	2,844	16,243
06	19,087	2,844	16,243
07	19,087	2,844	16,243

Available Annual Produced Energy Energy Demand for Rural Electrification Available Energy for Rio Tuba Mining Corp.

BALANCE BETWEEN POWER DEMAND AND SUPPLY FOR RIO TUBA MINING CORPORATION (CASE 1)

TABLE 4-7

	Pow	er Demand		Supply	у	S	urplus
Year			Hydrop	ower	Diesel Generation	1	
	Peak	Energy	Peak	Energy		Peak	Energy
	Demand (kW)	Demand (MWH)	(kW)	(MWH)	(MWH)	(kW)	(MWH)
1988	1,277	6,150	3,450	17,356	252	2,173	11,458
89	1,292	6,339	3,450	17,174	252	2,158	11,087
90	1,308	6,542	3,450	16,993	252	2,142	10,703
91	1,324	6,762	3,450	16,875	252	2,126	10,365
92	1,341	7,000	3,450	16,768	252	2,109	10,020
93	1,359	7,256	3,450	16,674	252	2,091	9,670
94	1,377	7,533	3,450	16,578	252	2,073	9.297
95	1,396	7,832	3,450	16,477	252	2,054	8,573
96	1,416	8,156	3,450	16,369	252	2,034	8,465
97	1,436	8,505	3,450	16,243	252	2,014	7,990
1998	1,458	8,693	3,450	16,243	252	1,992	7,802
99	1,481	8,889	3,450	16,243	252	1,969	7,606
2000	1,504	9,093	3,450	16,243	252	1,946	7,402
01	1,528	9,305	3,450	16,243	252	1,922	7,190
02	1,553	9,526	3,450	16,243	252	1,897	6,969
03	1,579	9,755	3,450	16,243	252	1,871	6,740
04	1,606	9,994	3,450	16,243	252	1,844	6,501
05	1,635	10,242	3,450	16,243	252	1,815	6,253
06	1,664	10,500	3,450	16,243	252	1,786	5,995
07	1,695	10,768	3,450	16,243	252	1,755	5,727

TABLE 4-8

BALANCE BETWEEN POWER DEMAND AND SUPPLY FOR RIO TUBA MINING CORPORATION (CASE 2)

	Power Demand	d	Supply		Shortage
Year		Hydropower	Existing	Diesel Power	
	Peak Energ		Peak	Energy	Peak
	Load Demar (kW) (MWI		(kW)	(MWH)	(kW)
1988	3,450 19,6 ¹	15 17,356	2,100	2,289	1,350
89	3,450 19,6 ¹		2,100	2,471	1,350
90	3,450 19,6 ¹	15 16,993	2,100	2,650	1,350
91	3,450 19,6 ¹	45 16,875	2,100	2,770	1,350
92	3,450 19,6 ¹	45 16,768	2,100	2,877	1,350
93	3,450 19,6 ¹		2,100	2,971	1,350
94	3,450 19,6 ¹		2,100	3,067	1,350
95	3,450 19,6 ¹		2,100	3,168	1,350
96	3,450 19,64	15 16,369	2,100	3,276	1,350
97	3,450 19,64	45 16,243	2,100	3,402	1,350
1998	3,450 19,6		2,100	3,402	1,350
99	3,450 19,6 ¹	15 16,243	2,100	3,402	1,350
2000	3,450 19,6 ¹		2,100	3,402	1,350
01	3,450 19,6 ¹		2,100	3,402	1,350
02	3,450 19,64		2,100	3,402	1,350
03	3,450 19,6	15 16,243	2,100	3,402	1,350
04	3,450 19,6 ¹	15 16,243	2,100	3,402	1,350
05	3,450 19,6 ¹		2,100	3,402	1,350
06	3,450 19,6 ¹		2,100	3,402	1,350
07	3,450 19,6	15,243	2,100	3,402	1,350

TABLE 4-9

BALANCE BETWEEN POWER DEMAND AND SUPPLY
FOR RIO TUBA MINING CORPORATION (CASE 3)

	Power	Demand		Supply		S	hortage
Year		Annual Consumer of the Consume	Hydropower	Existi	ng Diesel Power		
	Peak	Energy		Peak	Energy	Peak	Energy
	Load (kW)	Demand (MWH)	(MWH)	(kW)	(MWH)	(kW)	(MWH)
1988	8,500	59,568	17,356	2,100	9,198	6,400	33,01
89	8,500	59,568	17,174	2,100	9,198	6,400	33,19
- 90	8,500	59,568	16,993	2,100	9,198	6,400	33,37
91	8,500	59,568	16,875	2,100	9,198	6,400	33,49
92	8,500	59,568	16,768	2,100	9,198	6,400	33,60
93	8,500	59,568	16,674	2,100	9,198	6,400	33,69
94	8,500	59,568	16,578	2,100	9,198	6,400	33,79
95	8,500	59,568	16,477	2,100	9,198	6,400	33,89
96	8,500	59,568	16,369	2,100	9,198	6,400	34,00
97	8,500	59,568	16,243	2,100	9,198	6,400	34,12
1998	8,500	59,568	16,243	2,100	9,198	6,400	34,12
99	8,500	59,568	16,243	2,100	9,198	6,400	34,12
2000	8,500	59,568	16,243	2,100	9,198	6,400	34,12
01	8,500	59,568	16,243	2,100	9,198	6,400	34,12
02	8,500	59,568	16,243	2,100	9,198	6,400	34,12
03	8,500	59,568	16,243	2,100	9,198	6,400	34,12
04	8,500	59,568	16,243	2,100	9,198	6,400	34,12
05	8,500	59,568	16,243	2,100	9,198	6,400	34,12
06	8,500	59,568	16,243	2,100	9,198	6,400	34,12
07	8,500	59,568	16,243	2,100	9,198	6,400	34,12

v. scheme of development

CHAPTER V SCHEME OF DEVELOPMENT

5.1 Optimum Development Plan

5.1.1 Basic Considerations in Planning

The hydro-electric power plant will supply electricity required for operation of the Rio Tuba Mine, and at the same time supply electricity to local residents for domestic use. Although an exact figure has not yet been determined, approximately 7.5MW is preferrable for mine operation. However, from the viewpoint of economic head and discharge of the Tamlang River at the optimum hydropower development site, power output will be limited to approximately 4MW. To compensate for the resultant shortage in output, use of the existing diesel generators will be continued on an the same time, development of an additional Αt auxiliary basis. hydropower site or of another electrical power source is urgently To be considered economically feasible, hydropower costs must required. be less than costs for the selected alternative energy source, namely diesel, coal or alternative power plant.

As for domestic electric supply, the Project must satisfy future demand increases, including electrification of rural communities which presently lack any electric facilities, and also supplement older PALECO diesel generators, contributing about 1MW to PALECO's demand and thus reducing fees.

From the viewpoint of immediate benefits, a plan with low preliminary capital cost is preferrable. In consideration of future increases in fuel prices and unreliable supply for energy sources other than hydropower however, the Project should be evaluated not on simple construction costs per kW and kWh of the hydropower plant alone but rather on the benefit/cost ratio where benefit is equivalent to the unit cost per kW and kWh for the alternative power plant.

Although the run-of-river type generation method is generally used for mini-hydropower, from the viewpoint of low dry season discharge and power demand characteristics, comparative study of a canal type with regulating pond is necessary for selection of the most appropriate plan. The proposed power plant is to serve both the mine and local residents and will be located approximately 44km from the mine. The power station will

have a full-time supervision system with a simple and maintenance free automatic control system.

5.1.2 Comparative Cost Analysis for Alternative Power Generation Plant and Determination of Benefit Value of kW and kWh

The Rio Tuba Mining Corporation is presently investigating new electrical smelting processes to reduce production costs and thus increase the viability of the mine. Comparative study of power sources other than hydro including diesel, coal, oil, wood, and geothermal plants, was conducted for a 10MW scale electric power generation system and a coal-fired plant was selected as the most suitable plant for the following reasons:

- a) coal has the highest overall reliability in terms of supply and efficiency;
- b) diesel generation is considered a supplementary rather than a main power source;
- c) petroleum is too expensive;
- d) combined use of coal and wood for fuel is possible, but supply of firewood is insufficient and cost is too high for economic use;
- e) geothermal power development is considered to be costly with lengthy implementation and should particularly be avoided by private enterprises; and,
- f) cost and supply of coal is likely to remain stable for a long period of time.

For the above reasons therefore, fixed cost and fuel cost (variable cost) for a 10MW coal-fired thermal plant should be selected for comparative cost analysis to determine the optimum scale of hydropower development plan However, a diesel power plant was adopted for comparative cost analysis or benefit value of kW and kWh in place of the above 10MW coal-fired theremal plant due to the following points; i) ash treatment is comparatively difficult; ii) small plant capacity results in a higher power cost; iii) power cost of diesel and coal plants in almost the same; and, iv) investment cost for the diesel plant is smaller than that for the plant.

Although use of equal scale diesel and hydropower plants in comparative analysis is generally desirable, a 10MW scale plant was selected for the diesel plant as a plant smaller than 10MW would result in higher estimated production costs and would be conservative (Detailed

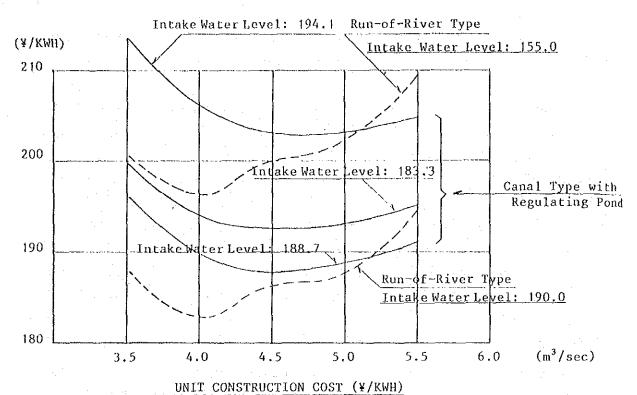
Project economic evaluation is presented in Chapters VII and VIII). The result of above study is shown in TABLE 5-1.

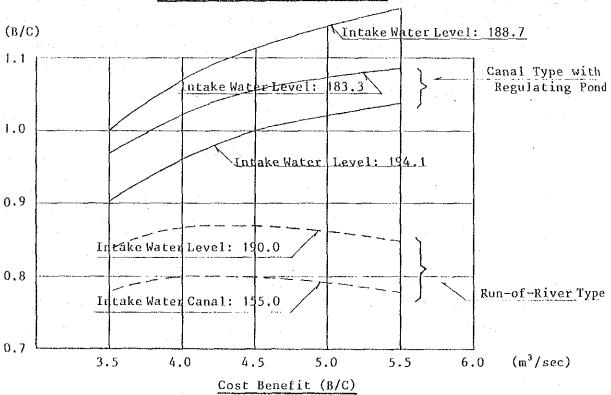
5.1.3 Optimum Development Plan

A case study was conducted to determine the optimum development scheme, comparing run-of-river and canal with regulating pond type generation methods. A total of 15 cases were compared including 3 different maximum turbine discharges with 2 intake water levels for the former, and 3 maximum turbine discharges with 3 different dam heights for the latter. On the basis of unit construction cost and benefit/cost ratio for each case, and after overall evaluation of capital cost, plant management, operation and maintenance, and effective use of the island's limited water resources, Case 5 was judged the optimum development plan (Refer to TABLE 5-2 and FIG. 5-1).

Optimum benefit/cost ratio for each case is obtained with a maximum turbine discharge of 5m³/s. However, in the event of 24-hour mine operation, the yearly period in which the said turbine discharge is available is greatly reduced while unit kWh costs correspondingly increase. For this reason, a maximum turbine discharge of less than 5m³/s was adopted. An outline of the development plan for Case-5 is presented in TABLE 5-3.

FIG. 5.1 STUDY OF SCALE





	A.	As of Feb. 1984 (1 US\$/14 E/233 E)
Description	Unit	Remarks
I. Diesel Plant		
-Plant Capacity -Standard Annual Operation -Service Life -Generator Terminal Output	5,000kW x 2 7,000Hr 15 years 70 GWH	Assumed Plant Factor 80%
-franc blergy Consumption -Annual Produced Energy -Construction Cost	70 x (1-0.18) = 57.4 GWH 2.,18 x 105 yen	Including Re-investment Cost after 15 years
Annual Cost		
II. Fixed Charge		
1) Capital Recovery Cost 2) O & M and Administrative Cost 3) Total Fixed Charge 4) Unit Fixed Charge Per kW 5) kW value	2,118 x 106 x 0.124 = 262.63 x 106 yen 2,118 x 106 x 0.03 = 63.54 x 106 yen 326.17 x 106 yen 32,620 yen 32,620 x 1.06 = 34,577 yen/kW	Interest 9%, C.V.F. = 0.124 Ratio 3.0% 1) + 2) *Revised Factor, per kW Value \$\times = 1.06\$
III. Variable Cost		
1) Fuel Cost 2) Fuel Consumption per KWH 3) Unit Cost per KWH 4) KWH Value	38.12 yen/f 0.329f/KWH 38.12 x 0.329 = 12.54 yen/KWH 12.54/(1-0.18) = 15.29 yen/KWH	*Revised Factor for KWH Value eta = 1.00
Assumption Transmission Loss Fault Station Service Use Check and Repair 2.0	Diesel 1.0% 2.0 3.0 6.0	
) x (1-0.06) = 1.06	

TABLE 5-2. COMPARISON OF DEVELOPMENT SCALE

ALTERNATIVE				CANAI	MITH I	REGULATI	CANAL WITH REGULATING POND TYPE	TYPE					RUN-OF-	RUN-OF-RIVER-IYPE	YPE	
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INTAKE EL	E		194.1			188.7			183.3			190.0			155.0	
ourler EL.	 E		85.0		-	85.0			85.0			85.0			85.0	
EFFECTIVE HEAD	£	106.6	106.9		107.2 102.0	102.3	102.6 96.4	4.96	7.96	98.0	101.0	101.0	101.0 68.0	68.0	68.0	68.0
MAXIMUM DISCHARGE	±3/s	5.0	.5	0.4	5.0	4. ت	0.4.0	0.4	2.0	સ્	O;	۲. ای	3.5	4.5	0.4	i,
MAXIMUM COTPUT	ΚW	4,390	3,960	3.530	4,200	3,790	3,380	3,970	3,380 3,970 3,580 3,230	3,230	3,740	3,320	2,910	2,520	2,240	1,950
GENERATING CAPACITY	106 KWH	21.90	21.90 21.44 20.76 20.95	20.76	20.95	20.51	19.87 19.81 19.39 18.98 17.38 17.33 16.54 12.93	19.81	19.39	18,98	17.38	17.33	16.54		12.88	12.33
CONSTRUCTION COST	106 #	'η 05h'h	4,350	4,280 4,030	4,030	3,920	3,840 3,820 3,730	3,820	3,730	3,660	3,240	3,240 3,168 3,108 2,588	3,108	2,588	2,526	2,472
CONSTRUCTION COST PER KWH	#/kwh	203.2 20	202.9	206.2	206.2 192.3 191.1	191.1	193.3	192.9 192.4	192.4	192.9	186.5	192.9 186.5 182.8 187.9	187.9	200.0	196.1	20072
BENEFIT/COST RATIO	B/C	1.020 0.	266.0		0.959 1.077 1.058	1.058	1.022	1.076	1.076 1.053 1.023 0.860 0.867 0.837 0.793	1.023	0.860	0.867	0.837	0.793	0.801 0.771	0.771

TABLE 5-3

OUTLINE OF DEVELOPMENT PLAN

ITEM	DESCRIPTION	REMARKS
Name of River Power Plant Location Catchment Area (km ²)	Tamlang River Brookes Point 39.0	
POWER PLANT SCHEME		
Generation Method	Canal Type with Regulating Pond	
Intake Water Level (m)	188.7	At Maximum Output
Tailrace Water Level(m)	85.0	n
Gross Head (m)	103.7	
Maximum Output (kW)	3,800	
Maximum Discharge (m3/s)	4.50	
Effective Head (m)	101.3	At Maximum Output
Annual Produced Energy (GWH)	20.51	
OUTLINE OF FACILITIES		
Regulating Pond		
Maximum high water level (m)	188.7	
Available depth (m) Effective capacity (103m3)	1.8 360	
Dam	500	
Туре	Concrete Gravity Dam	
Height (m)	46.0	
Crest length (m)	49.0	
Dam concrete volume (m ³)	17,000	
Headrace length (m)	1,493	Including Pressure
Tailrace Length (m)	300	Pipe

VL POWER PLANT: COST AND CONSTRUCTION IMPLEMENTATION

CHAPTER VI POWER PLANT: COST AND CONSTRUCTION IMPLEMENTATION

6.1 Power Plant

6.1.1 Main Structures

The main structures of the Project are dam, diversion tunnel, penstock and power plant. These structures are explained in brief below, while related preliminary designs are presented in APPENDIX I as FIG. 4-1, 4-3, 4-4, 4-7 and 4-9.

(1) Dam

Type : concrete gravity dam

Height : 46.0m

Length : 49.0m

Design Flood : 505m³/s

Overflow Width : 25.0m

Overflow Depth : 4.7m

An automatic inflatable rubber dam 3.7m in height will be installed at overflow crest to increase the available head. The upstream dam face will have a slope of 0.2 while the downstream face will be 0.8.

(2) Diversion Tunnel

The tunnel section will be rectangular horseshoe shaped with a bottom width of about 4.0m to allow use as an access road during construction. Approximately 70% of the total length will be unlined while 30% will be concrete lined.

Tunnel Length : 1,277m
Lined Canal Slope : 1/1,000

(3) Penstock

A 1.5m diameter FRPM (Fiberglass Reinforced Plastic Mortar Pipe) will be used for the penstock which will be embedded.

(4) Power Plant

The river side of the powerhouse building will be waterproof to ensure water tightness for the horizontal-shaft turbine during floods.

Powerhouse : 8.5m x 16.0m

6.1.2 Main Blectrical Facilities

The main electrical facilities of the Project are provided below.

(1) Dam

Type

: 1 horizontal-shaft, Francis-type turbine

Maximum Output

: 4.000kW (turbine efficiency = 91.1%)

Maximum Discharge

 $4.5 \text{ m}^3/\text{s}$

Rotation Speed

: 720RPM

Speed with

Closed Governor

: 2.5s

(2) Generator

Type

: 1 horizontal axis 3-phase alternating

current synchronized generator

Output

: 4,700 kVA

Voltage

: 4.16kV

Power Ratio

: 0.81

Frequency

: 60HZ

(3) Main Transformer

Type

: 2 outdoor, 3-phase, self-cooling type

transformers

Capacity

: 4,700kVA

Voltage:

: 4.16/34.5 + 5%kV

(4) Transmission Line

No. of Circuits

: 1

Cables

: Aluminum Cable Steel Reinforced (ACSR)

176.9MCM (89.7mm²)

Insulators

: 4 suspension insulators (250mm)

Overhead Ground Wire: 1

zinc-coated steel cable AWG 2

 (33.62mm^2)

Support

: Wood pole

Voltage.

: 34.5kV

Total Length

: 44km

6.2 Estimated Construction Cost

Estimated construction costs have been worked out in terms of the 1984 price index and are presented hereunder.

(1)	Civil Construction Costs	unit: million yen
	Dam	1,333.9
	Intake	70.3
	Diversion Tunnel	737.4
	Surge Tank	93.6
	Penstock	63.9
	Diversion Channel	65.5
	Powerhouse (building and equipment foundation)	293.7
(2)	Electrical Facilities	
٠	Power Plant Equipment (turbine, generator)	448.0
	Transmission Line	165.0
(3)	Technical Maintenance Cost	300.0
(4)	Contingency (including land compensation)	278.7
(5)	Cost Escalation	181.3
	Total	4,031.3

6.3 Annual Disbursement Schedule

The construction period required is estimated to be approximately 4 years. The annual disbursement schedule is shown in the following table and the total construction cost is about 4,000 million yen.

ANNUAL DISBURSEMENT SCHEDULE

		·azzegająjiąje-Sefrancejane na cestasty.	·	Unit: mil	lion. yen
Year Item	1st	2nd	3rd	4th	Total
Civil Construction	1,030.4	1,174.0	159.9	294.0	2,658.3
Electrical Facilities	44.8	358.4		44.8	448.0
Transmission Line	16.5	132.0		16.5	165.0
Contingency	60.6	184.0	.25.1	-	278,7
Engineering Services	120.0	120.0	60.0	-	300.0
Cost Escalation	105.7	73.8	1.8		181.3
Total	1,387.0	2,042.2	246.8	355.3	4,031.3

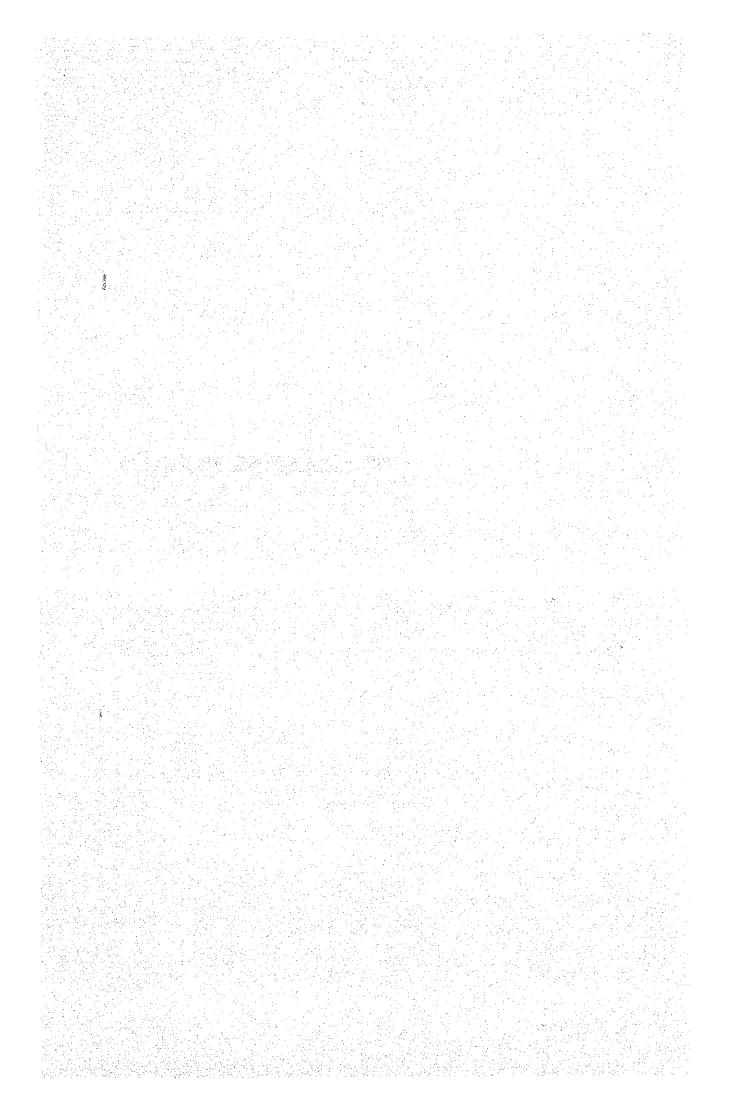
6.4 <u>Implementation Schedule</u>

The envisaged implementation schedule is presented in TABLE 6-1 and shows a period of approximately 28 months commencing upon award of contract as required for completion of the same. Approximately one year will be required prior to contract award for lining up financing, preparation of detailed design works, tender bidding and tender evaluation.

Table 6-1 Implementation Schedule

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Preparatory Works			3,565,567,567,567	0.22				-	<u></u>						Curomod			·		
Temporary Facilities		·		·	A managanan managan fe	Aggregate Plan for Tunneling	Plant Ting	3-	Concrete Placing	lacing ra	Pacilities				Telegia Telegi					
Civil Works																				
Tunnel Works	E	1,510			X253X	X89X3QXQQX	15000000000000000000000000000000000000	THE CONTRACTOR OF THE CONTRACT	ESSESSES SESSES											
Diversion Works	set	1							1205(08(38)(2)		_		· [į			
Dam	' E	Excayation 6,700 Concrete volume 17,000							5893	558 558 558 558 558 558 558 558 558 558	252753252553553555555555555555555555555		3253253553	330030033	Rubber	Dam Plug Works	8			
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Surge Tank	set								282525428	12258320000000000000000000000000000000000										
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Tailrace	ш	300												335355555555555555555555555555555555	**************************************					
Powerhouse	set	 -1									Rossessonosconoscos	2200225250	150916051		SE	Si te Deve	Bevelopment			
Electro-Mechanical Works	nical	Works																. (
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VIL FINANCIAL ANALYSIS



CHAPTER VII FINANCIAL ANALYSIS

7.1 General

The objective of project analysis, or financial and economic analysis, methods of which were developed primarily by UNIDO and OECD, is efficient allocation of scarce resources (usually potential capital for investment). These methods have been adopted by all international financing and bilateral aid agencies in implementation of feasibility studies.

Originally, both methods were developed to analyse such production sectors as industry and agriculture, etc. Evaluation of feasibility and infeasibility thus depended upon whether a certain standard of surplus benefit by production could be achieved during the project life. One indicator used to express this standard is Internal Rate of Return (IRR). Application of this approach has been expanded, mainly by the World Bank Group, to evaluate such sectors as infrastructure and utility in which neither transactions nor competitive market prices exist.

In project analysis of those sectors, for example, benefit is often measured by cost savings with other second best alternatives, while turnover of the products is regarded as project benefit in the evaluation of production sectors. Likewise, in communication projects, consumer surplus is regarded as benefit.

It should be noted that IRR is affected by identification of benefits for each project. IRR is thus often inappropriate as a standard for selection of optimum resource allocation of projects in the same sector as well as in different sectors. Most feasibility studies of power projects in Japan, for example, have adopted costs of alternative power plants using different energy sources (opportunity costs of capital) as a project benefit. In this case, different and more accurate values of IRR could be obtained as compared to internationally recognized cases where the savings in operation and maintenance (0 & M) or revenues from electric rates are regarded as benefits of power projects.

It is therefore essential not to merely compare values of benefit but to clearly identify the benefit used in the evaluation for determining whether a newly proposed project should be implemented or not.

7.2 Conditions of Financial Analysis

Financial analysis of a project compares benefit expressed as revenues, and costs expressed as expenditures from the perspective of the implementation agencies of the project. In financial analysis of a power project, investment and 0 & M costs are generally regarded as expenditures while sale of electricity is regarded as revenue. However, unlike ordinary projects, in the proposed Tamlang River Hydropower Project, electricity will be supplied by a dual system to two groups of consumers; neighbouring rural residents who are or will be served through PALECO, and the Rio Tuba Mine. Revenues for the former are equivalent to total power rates to be collected from end-users. For the latter, however, no such revenues exist; rather power production is regarded as one item of mine operation costs.

Projects are generally formulated corresponding to present and future demand. In this case, however, future demand for the Rio Tuba Mine itself has not yet been clearly determined. The primary reason for initiating the present study was to reduce power production costs by conversion to hydropower generation, and in addition, to provide an inexpensive electric supply for future expected demand for the envisioned new smelting plant. However, the smelting plant is still under study, and the present report will likely be a contributing factor in determination of scale, required electric energy, etc. Accordingly, financial analysis of this Project is necessarily different from ordinary projects and conducted assuming three possible energy demand cases as described in Chapter 4.

Based upon the premises mentioned above, it might be appropriate to consider that the benefit for the Rio Tuba Mine itself should be as follows:

(1) <u>Case-1: Substitution of Existing Diesel Generator</u>

This case substitutes hydropower generation for supply by the existing diesel generator alone. Where energy consumption is for the Mine's own use, benefit is regarded as the difference or the savings in costs between the two cases, i.e., generation by the construction of a hydropower plant and generation by the existing diesel facilities without construction of ahydro plant.

(2) Case-2: Peak Load 3,600kW

As fulfillment of power demand during the dry season is impossible with the planned hydropower plant, this case compares 0 & M costs for generation by diesel facilities alone including installation of a new diesel power plant with two 1,500kW diesel generators and by the combination of a hydropower plant and existing diesel facilities. Difference in the said costs is regarded as benefit.

(3) Case-3: Peak Load 9,500kW

In this case, installation of additional generators is required for both cases not only in the dry season but also during the rainy season. Benefit for this case is determined as for Case-2 in comparison of 0 & M costs with diesel facilities alone and combined use of the hydropower plant and existing diesel facilities.

Costs can be evaluated in the same way as benefit, the difference between construction and installation costs for the hydropower plant and for diesel plants being adopted as cost. Following the above framework in financial analysis, further considerations concerning benefit and costs for this Project are presented below, and are directly related to discussion in Chapter 4 and 5.

7.3 Benefit/Cost Calculation

7.3.1 Benefit

As stated above, Rio Tuba Mine revenues from sale of electricity to PALECO is regarded as benefit for rural electrification while the difference in cost between diesel generation only and combined use of hydro and diesel generation is regarded as benefit in the case of production by the Mine for its own consumption.

If electricity is supplied by public power corporations, the electric rate will be determined by Long-Run Marginal Costs (LRMC). In this Project, however, as electricity is supplied by a private company, the electric rate can be determined by multiplication of the capital recovery factor (CRF) and coefficients of maintenance and fair return for construction cost as practiced in Japan.

Therefore, system rates for the Project are as tabulated below.

Item	Unit	Amount
Construction Cost	Yen	4,031x10 ⁶
Available Electric Energy	kWh	19,087×10 ³
Construction Cost	kWh	$(4,031\times10^6)+(19,087\times10^3) = 211.2$ $0.045\times(1+0.045)^{45}$
CRF:		$ = 0.0522 5.2\% $ $ (1+0.045)^{45} -1 $
Maintenance Cost Coefficient		1.5%
Fair Return Coefficient	·	3.3%
		Total 10.0%
System Rate		211.2yen x 0.10 = 21.1 = 21.0yen/kWh

The above system rate is relatively inexpensive in comparison with the present PALECO system rate of 29.4 yen and that of NPC, 24.9 yen, \frac{1}{2} and consequently may be expected to contribute to reduction of present PALECO deficits. As for benefit of savings, the main component is savings resulting from reduction of diesel fuel use. According to the principles of project evaluation, increases in costs caused by inflation can be offset by the same effect on items of benefit. In cases where some specific costs of goods and/or services are expected explicitly to rise in relation to other costs and benefits, however, those costs can be allowed to escalate. According to 'Commodity Price Forecasts' by World Bank/IFC, oil-related energy prices during 1984-95 will increase by 1.8% annually in comparison with other principal items. Thus, a 1.8% annual escalation in diesel costs alone was adopted for this study \frac{2}{2}.

 $[\]underline{1}$ / Calculations based on PALECO's Annual Report and Profit and Loss Report.

^{2/} Commodity Price Forecasts (Revisions), The World Bank, Jan. 6, 1984. Calculated from P.11 Table 3 "Weighted Index of Commodity Prices".

7.3.2 Cost

As the difference in 0 & M cost was adopted as project benefit, cost was determined as the difference in costs for construction and replacement of equipment for hydropower generation (including cogeneration of hydro and diesel) and those for diesel generation alone. Moreover, residual cost of diesel generators at the end of project life was regarded as the same as removal costs.

Interest rates during the construction period have increasingly been considered in financial analysis for recent feasibility studies in Japan. The main reason seems to be facilitation of book-keeping and accounting, as well as evaluation by funding agencies after completion of the feasibility study. Project evaluation or internal rate of return in financial analysis, however, is in reality unrelated to interest rates or depreciation, evaluating only the rate of returns within the Project itself. Accordingly, interest rates during the construction period were not included within the present Report in conformity with the principles of project analysis.

Finally, project life for the hydropower generation facilities such as dam, generators, transmission lines, etc., is estimated at 45 years after completion of construction; residual costs in the last year of project implementation is estimated at zero.

In addition, a fixed depreciation method was adopted for the replaced diesel plant facilities and residual values were calculated at the final project year. However, although these residual values appear in the costs cash/flow column, these costs are minus by nature and are clearly considered as benefit.

7.4 Financial Internal Rate of Return (FIRR)

Based on the conditions outlined above, FIRR for each case were calculated as follows, details of which are presented in TABLE 7-1:

Case-1 Substitution of Existing Diesel Generator: FIRR 3.2%

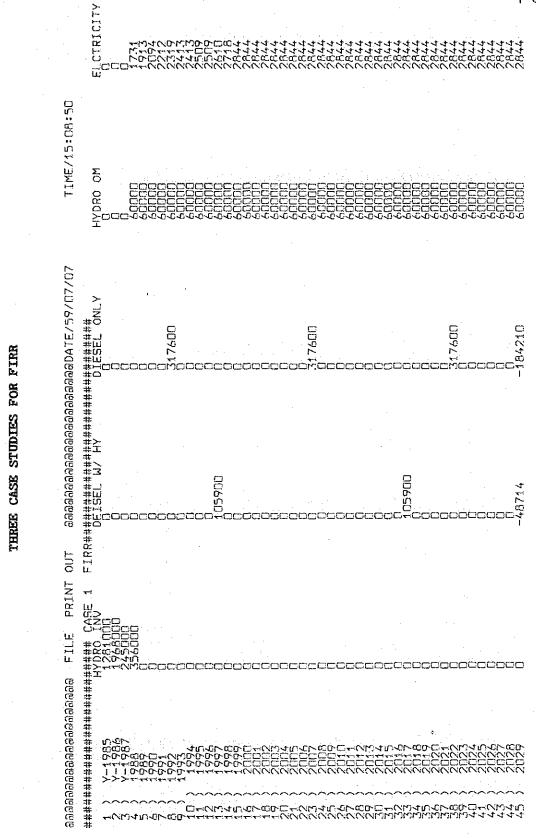
Case-2 Peak load 3,600kW : " " 7.9%

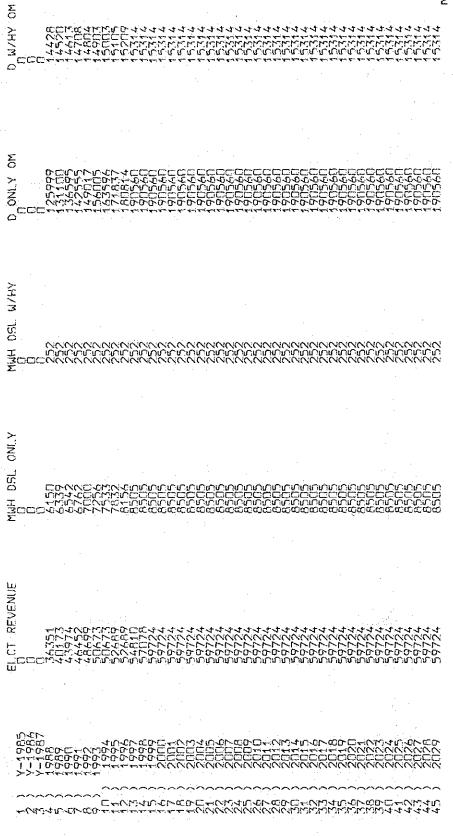
Case-3 Peak load 9,500kW : " " 9.0%

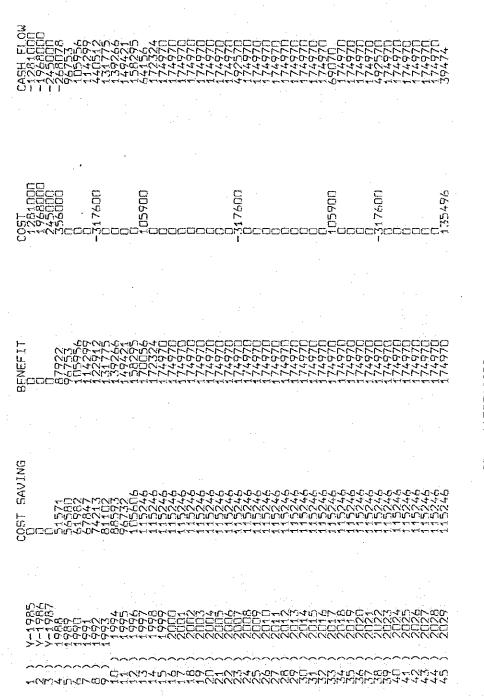
7.5 Sensitivity Analysis

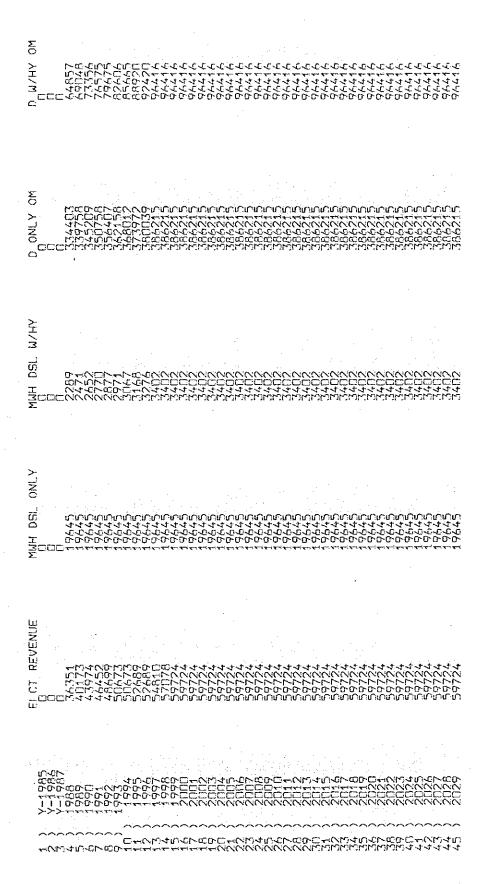
Sensitivity analysis was conducted for Case 3 (peak load 9,500kW) which would be considered most realistic and acheived the highest FIRR. The following results were obtained:

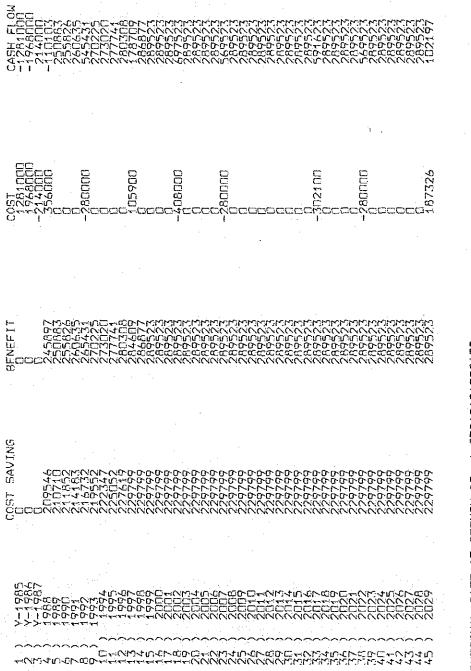
 10% increase in construction costs 20% increase in construction costs fuel prices remain constant from 1984 fuel prices increase 5% from 1984 fuel prices increase 10% from 1984 combination of first and third items above (worst case can be assumed) 	
 fuel prices remain constant from 1984 fuel prices increase 5% from 1984 fuel prices increase 10% from 1984 combination of first and third items above 	8.1%
 fuel prices increase 5% from 1984 fuel prices increase 10% from 1984 combination of first and third items above 	7.3
fuel prices increase 10% from 1984combination of first and third items above	7.8
- combination of first and third items above	11.4
	15.6
(worse case can be assumed)	6.2
- combination of first and forth items above	10.4

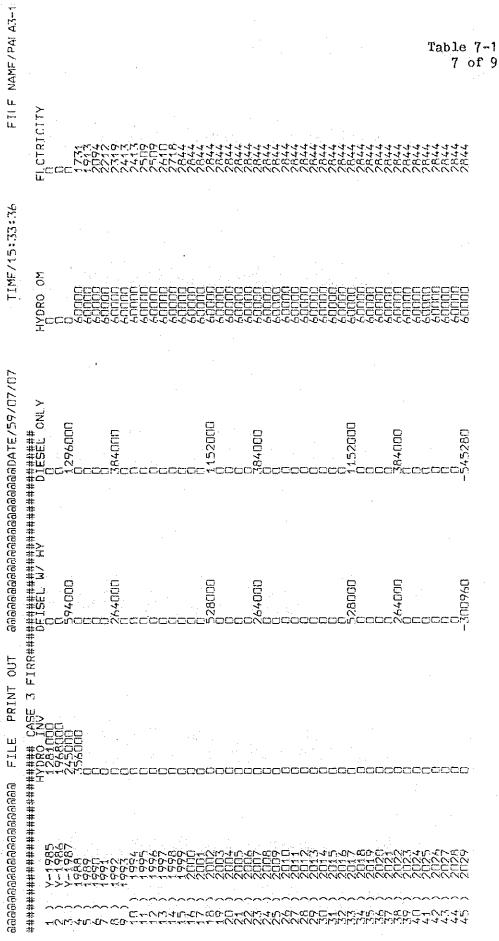


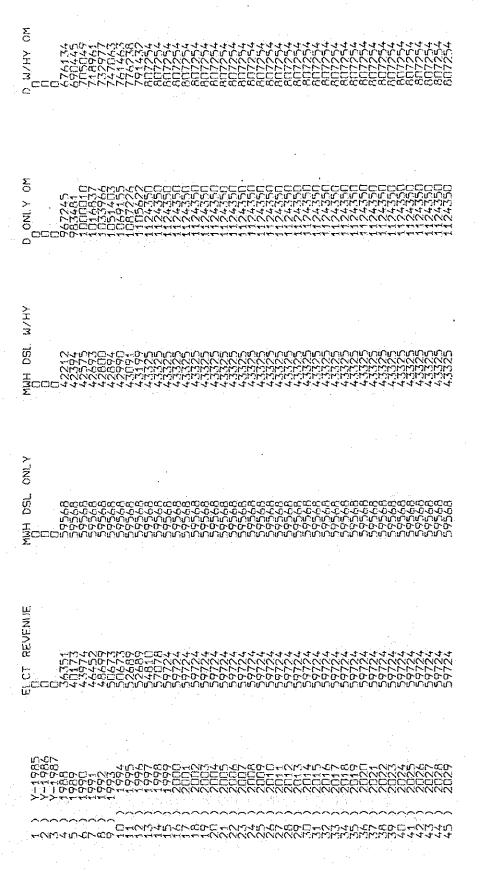


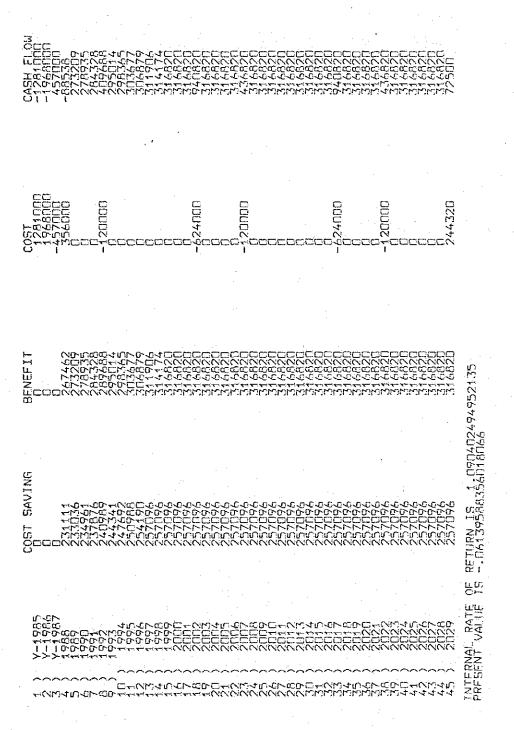












VIIL ECONOMIC ANALYSIS

CHAPTER VIII ECONOMIC ANALYSIS

8.1 Approach

Financial analysis focuses on profitability of project implementation itself while economic analysis on the other hand, studies the degree of benefit to the national economy resulting from project implementation. As in financial analysis, benefit and cost are estimated first. In financial analysis, however, the same are expressed in terms of market price while in economic analysis they are expressed in terms of economic value (shadow price).

The economic benefit of electric power projects is actually the marginal value or productivity of economic activity arising from power output and the value of efficiency. It is almost impossible however, to quantify power output benefit in such terms especially for the latter. Accordingly, in lieu of the above, the cost of the second best alternative plan is often adopted as project benefit using the so-called "alternative facilities method" in many feasibility studies in Japan. The above calculation method is an application of the opportunity cost concept in which cost input into one project can be transferred to another project, thereby obtaining a different benefit.

In this Project, for example, benefit arising from implementation of a hydropower plan (With Project) should be compared to benefit which can be obtained by investing the same costs in other different types of opportunities (Without Project). In the "alternative facilities method", however, the cost for the alternative plan is not invested in other economic activities but in the same activities, and consequently this cost can not logically be considered as economic benefit. In this economic analysis therefore, as in financial analysis, benefit was divided into two kinds, economic prices of the savings in the case of Rio Tuba Mine's own use, and PALECO revenues from sale of electricity to rural residents in the case of rural electrification as explained below.

Actual quantification of effeciency for electric power use is impossible. A common method of estimating the same is the consumer's willingness to pay (WTP). However, for accurate evaluation of WIP, an interview survey, informing people of the efficiency of electricity,

should be conducted, which is a difficult task to accomplish in a limited period of time. On the other hand, except for those households which must bear the cost of long extension lines, the majority of households within electrified areas are being served by PALECO and there is no particular problem for PALECO in collection of system rates. In Brookes Point Municipality, for example, 97% of residential consumers pay their system rates at a fixed time. From this fact it can be assumed that the current rates are equivalent to or less than the willingness to pay for the residential consumer.

In addition, areas to be covered by this Project are unelectrified excluding a part of Brookes Paint Municipality and the Rio Tuba Town Site, and almost all households use oil lamps for lighting and about 60% have transistor radios. Price of kerosene required for the lamps averages \$3.3 (\footnote{\footno

In comparison to the above, minimum PALECO system rates as of March '84 were P31.10 (up to 12kWh) and few households are paying more than the minimum rates. Conversion from present kerosene and battery consumption to electricity will thus result in real and significant savings and sufficient willingness to pay may therefore also be assumed.

8.2 Benefit Estimates

8.2.1 Benefit for Rio Tuba Mine Use

As previously stated, benefit was expressed as the economic value of the savings in 0 & M costs. The majority of 0 & M costs consist of diesel fuel and its economic value is given in border prices. The Philippines has a large petroleum refining capacity, producing for both domestic consumption and an equivalent amount on consignment for PERTAMINA, the national oil company of Indonesia. Accordingly, FOB rather

than CIF prices are most appropriate for diesel border prices. FOB diesel prices in the Philippines are approximately US\$1 less per barrel (about 159ℓ) than international prices (Singapore price) the average prices of which is US\$31.20/barrel as of February $1984\frac{1}{2}$.

Although savings also occur in cost of lubricating oil and maintenance, the above are insignificant in comparison with costs of diesel fuel and can therefore be disregarded.

8.2.2 Residential Supply Benefit

Benefit of the proposed rural electrification was generally esimated as willingness to pay reflected by revenues from PALECO system rates. As the PALECO unit rate for residential consumers in economic analysis is estimated at \$43.0/kWh (P2.59/kWh) versus the purchase rate of \$21.0/kWh (P1.27kWh) from the Rio Tuba Mining Corp., a unit rate more than twice that of the financial analysis may be obtained, indicating a substantial benefit to the national economy.

8.3 Cost Estimates

Economic costs, as stated previously, are the difference in costs between construction of the hydropower generation plant (including auxiliary diesel generation) and the alternative diesel generation plant, expressed in terms of economic prices. Construction costs are divided into those paid in foreign currencies, and those paid in domestic currencies such as labor, fuel, etc. which are procured domestically. In principle, a portion of the Project will be in Japanese yen which is assumed to reflect economic price in a free competitive market. Distortion of market prices is presumed for the domestic portion, on the other hand, and shadow prices are used to convert to economic prices as presented below.

^{1/} Platt's Oilgram Price Report, Vol. 62 No. 33, Mcgraw-Hill Inc., N.Y., P6-A.

8.3.1 Tax

In economic analysis, taxes are regarded simply as the transfer of resources within the country itself and are therefore deducted from cost. As the Rio Tuba Mining Corp. is an export oriented enterprise and as the objective of the present plan is conversion of energy generation to non-oil consuming sources, the Project is exempted from import duties on capital goods according to Presidential Decree No.1789. Taxes for the present Project are, therefore, not included within costs for financial evaluation and conversion of the same to economic price is unnecessary.

8.3.2 Exchange Rate

Due to political and economic uncertainties, fluctuation in the exchange rate within the Philippines is rather large. A shadow exchange rate rather than the official rate is therefore used to convert domestic currency to foreign currency for economic analysis. Although the shadow exchange rate is obtained by a weighted average of past import-export duties and subsidies from the past few years, statistical data during the present study period was available only up to September '83, after which period the Philippine economy underwent significant change. Consequently, the shadow exchange rate derived by the above method will naturally vary from the exchange rate of February '84. For this reason, the shadow exchange rate used by NEDA (official rate x standard conversion factor of 1.2) 1/2 was adopted for the present Study as follows: US\$1 = \$1, 4 x 1.2 = \$16.8.

8.3.3 Labor Wage

Shadow wages are also used for unskilled labor. NEDA multiplies real wages by a coefficient of 0.80 to obtain shadow wages for unskilled labor. The above coefficient however, is the average for the entire country rather than for Palawan Island where underemployment is higher than average, and a lower coefficient should be required for opportunity costs of laborers.

^{1/} As explained by NEDA in a meeting of NEDA, Economic Staff and Infrastructure Staff on February 17, 1984.

Unskilled laborers on Palawan Island also receive the minimum wage fixed by the Philippine Government when they are hired as seasonal or day labor, and the total minimum wage is equivalent to P38 per day (minimum wage P20 plus daily allowances P18 per day). The Rio Tuba Mine employs about 480 unskilled laborers on a regular basis, and a monthly average of 70 unskilled laborers are employed on a seasonal basis. A survey of seasonal employees revealed that they were employed by the Mine for an average of three months per year with a total income of approximately P1,500 per person. Income for the remaining 9 months is derived from the sale of bananas, bamboo, chickens, etc., at the market, amounting to less than P100.

Seasonal employees are still more fortunate however, than those who are not employed as the majority of able workers are engaged in low household agricultural production. Non-cash economic activities such as fishing and hunting for supplementary food supply are also common. Accordingly, opportunity cost for unskilled labor in the present Report has been determined at an average of P1,500/year, with 300 working days a year and a P5/day shadow wage. The coefficient used therefore, is 0.13 rather than the NEDA value of 0.80.

8.3.4 Land

The proposed Project dam site is located on public land with no residences in the reservoir area, while, except for an application fee to NWRC for hydropower development, no payment to the government is required for the Project. For these reasons land acquisition and compensation costs were not included in calculations for the financial analysis of the present Report.

In economic evaluation, economic price is given by the opportunity cost of land or marginal productivities of land. The total area for reservoir pondage, temporary access roads, building etc. for the present Project is approximately 100,000m². The majority of the said area is unused jungle and accordingly any losses in economic land value due to temporary roads or ponding may be disregarded. Any items other than the above, such as use of temporary roads by local residents, should be regarded as benefit rather than loss. In the present Report therefore,

economic losses related to land use were regarded as minimal, offset by potential benefits and accordingly, as in financial analysis, land costs were regarded as zero.

8.3.5 Fuel

About 17% of domestic portions or costs for civil works consist of fuel costs. As in 8.2 above, the conversion of fuels to economic costs was performed by using border prices which were equivalent to the FOB price of US\$31.20/barrel.

8.4 Economic Internal Rate of Return (EIRR)

The EIRR for each case was calculated as follows according to the basic approach discussed above while details of the same are presented in TABLE 8-1 (1 to 9):

Case-1	Substitution of	Existing	Diesel	Generator:	5.7%
Case-2	Peak Load 3,600	kW			10.1
Case-3	Peak Load 9,500	kW			11.6

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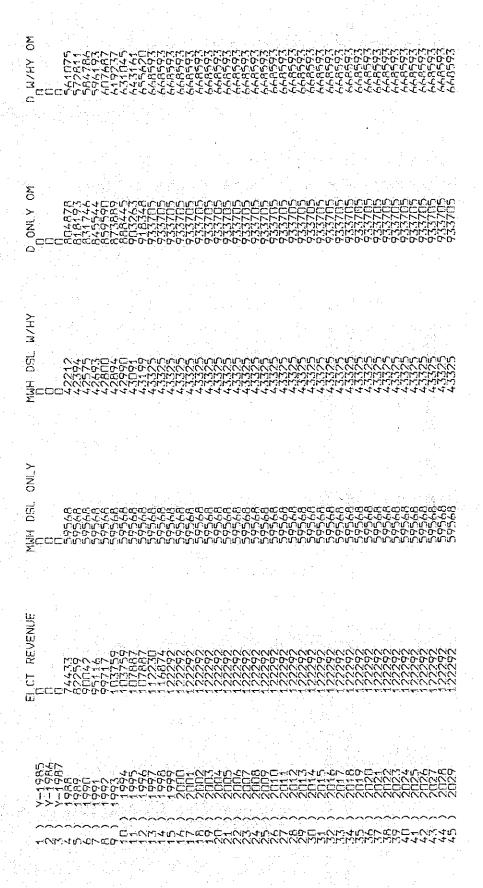
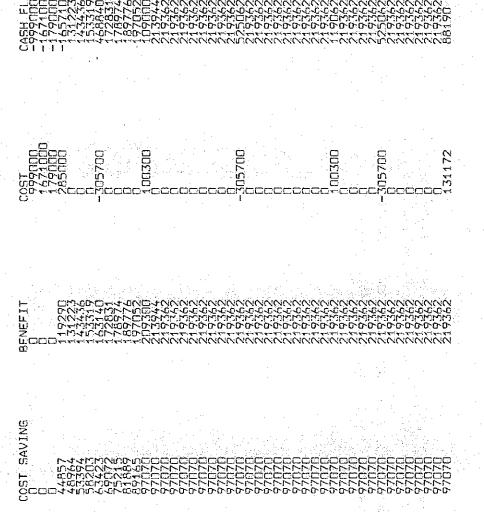
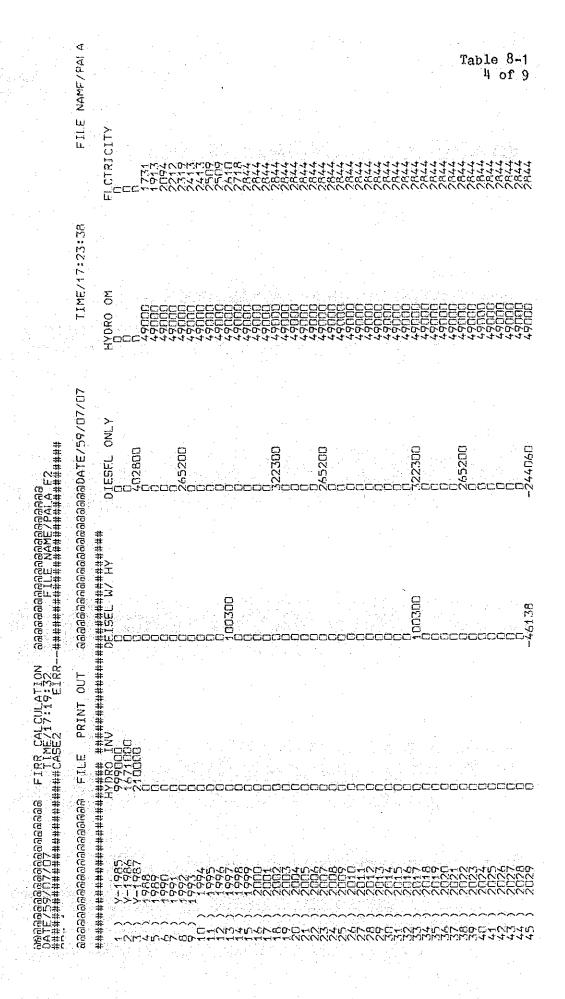
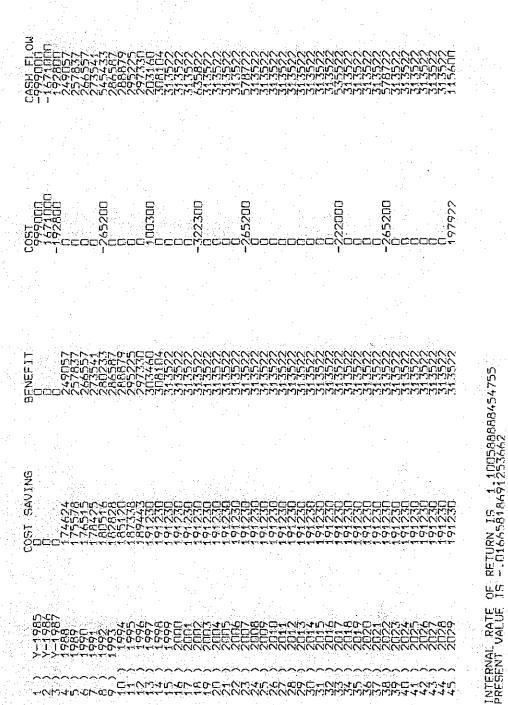


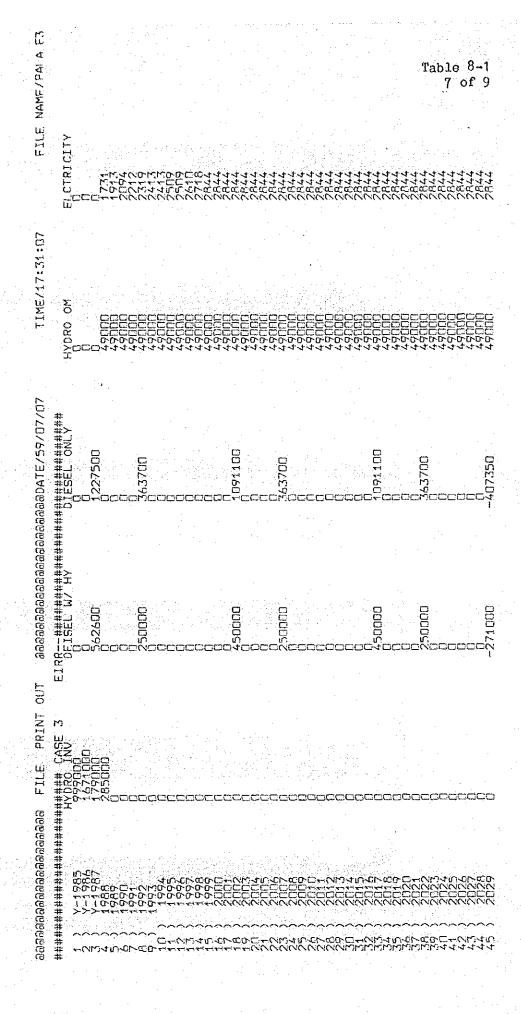
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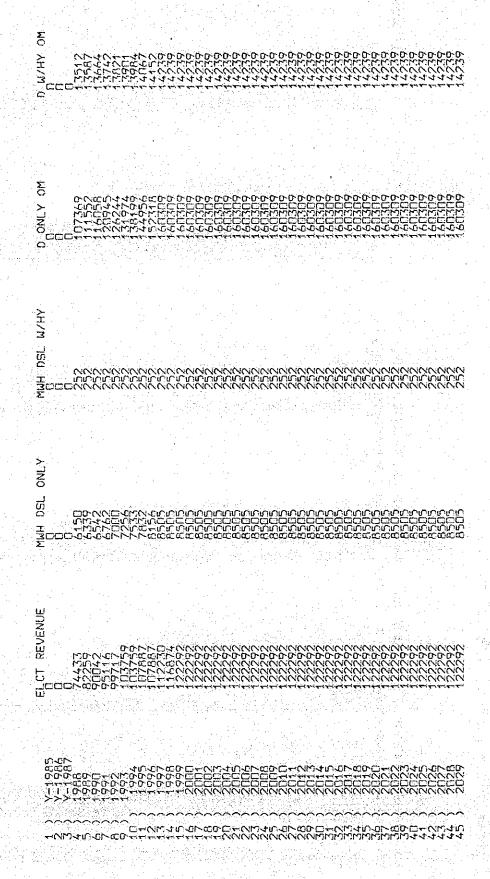


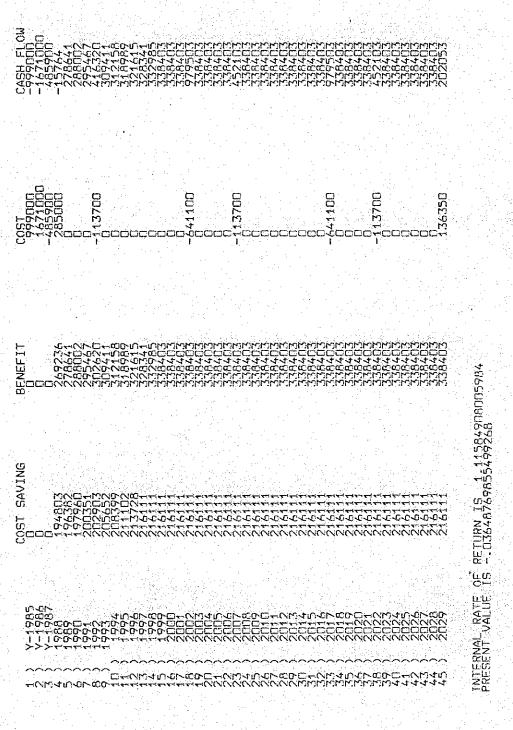












IX. INDIRECT PROJECT EFFECTS

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CHAPTER IX INDIRECT PROJECT EFFECTS

9.1 Introduction

One of the major disparities between the life styles of people in developed countries versus those in developing countries is the wide distribution of domestic electrical networks in the former which serve not only urban but rural areas as well. Electrification and rural development are closely interrelated. The Philippines however is presently highly dependent on oil as an energy source which, due to world inflation, hinders reduction in electrical utility fees and thus the spread of electrical facilities to less affluent rural areas. To reduce costs and promote rural electrification therefore, it is necessary to develop domestic energy sources such as hydropower, geothermal power, etc. The proposed Project will accordingly be designed to have substantial effects on rural communities as described below.

9.2 Effect on Productivity of Plain, Mountain and Fishing Villages

Upon review of local data and spot field survey, the possible effect on productivity of plain, mountain and fishing villages by extension of the power network can be listed as follows:

- a) overall improvement in agricultural system management through use of well and irrigation pumps;
- b) preservation of perishable agricultural produce by refrigeration;
- c) development of fish farms by installation of pump facilities;
- d) development of light industries such as lumber mills, flour mills, etc. through electricity; and,
- e) storage of catched fish by refrigeration.

The increase in income and stabilization of the rural economy resulting from the above effects will in turn contribute to increased employment opportunities.

9.3 Improvement of Non-Agricultural Sector and Socio-Economy

It is also apparent that with the provision of adequate power supply, improvement of the non-agricultural sector and socio-economy would occur in the following ways:

- a) increased development of industries and income from the same through use of electricity;
- b) increased participation of women in society and the work force as a result of electrification and consequent decrease in time required for housework, etc.; and
- c) intensification of production from light industries and commerce.

9.4 Improvement of Living Environment in Rural Areas

The following improvements in the conditions of rural areas are also expected:

- a) potential use of limited educational facilities for evening classes;
- b) increased use of audio-visual materials in educational programs, and expansion of media and information transfer;
- c) improved public sanitation and medical services through electrical illumination and refrigeration of medicines; and,
- d) reduction in crime due to electrical lighting at night.

9.5 Effect on National Economy

The effect on the national economy can be estimated as follows:

- a) increased national stability and reduction of dependency on foreign capital due to decreased oil imports;
- b) promotion of rural development and improvement of the service sector for rural residents due to strengthened rural economy and increased income; and
- c) decreased migration of rural population to urban areas.

9.6 Effect of Dam Construction on Erosion

At present, devastation of downstream lowland areas is a major problem in the Project area due to annually increasing riverbed deposits. Construction of the proposed regulating pondage dam upstream will arrest sediment deposits arising from flood discharge and result in a drop in the riverbed and increased river stabilization. This will in turn allow possible agricultural development of a larger level area downstream.

Although it is difficult to measure the above effects numerically, EIRR calculations were carried out with all figures calculated on the safe side.

APPENDIX

APPENDIX I

TECHNICAL REPORT

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