IV. FLOOD RUNOFF ANALYSIS

4.1 General

The flood runoff analysis is conducted to obtain:

- a) the probable flood runoff distribution under the present river condition with and without Magat dam in order to grasp present flood phenomenon,
- b) the probable flood runoff at damsites to study flood control and to design structures,
- c) and the probable flood runoff distribution under the alternative flood control schemes for flood control planning.

The Cagayan river flows in a northerly direction from its headwaters in Nueva Vizcaya province to its mouth in the Babuyan Channel near Aparri with a total length of 522 km. The major tributaries are the Magat river $(5,113 \text{ km}^2)$, Ilagan river $(3,132 \text{ km}^2)$, Siffu-Mallig river $(2,015 \text{ km}^2)$, and Chico river $(4,551 \text{ km}^2)$. The river bed slope is 1/8,680 between the rivermouth and Tuguegarao in the main river.

The following sections describe the detail estimate of the probable flood runoff in the Cagayan river basin.

4.2 Available Data

4.2.1 Rainfall Data

Daily rainfall records are available at 10 gauges as listed below, which are used for the estimate of basin mean rainfall. The data availability at the selected gauges and the location are shown in Figs. 1.2 and 1.3.

No.	Station No.	Station Name	Basin	Recorded P	eriod
1	1	Aparri	Lower Cagayan	1951-1984	34 Yrs
2	7	Tuao	Chico	1956-1985	32 Yrs
3	8	Tuguegarao	Lower Cagayan	1949-1985	37 Yrs
4	13	Naneng, Tabuk	Chico	1956-1984	28 Yrs
5	19	Ilagan	Ilagan	1965-1984	19 Yrs
6	21	Bontoc	Chico	1963-1985	23 Yrs
7	29	Nayon, Lamut	Magat	1968-1980	13 Yrs
8	30	Echague	Upper Cagayan	1976-1985	10 Yrs
9	38	Consuelo, Santa Fe	Magat	1956-1985	28 Yrs
10	40	Dakgan	Upper Cagayan	1973-1982	10 Yrs.

Hourly rainfall record series are available at Aparri and Tuguegarao gauges, which are useful for the grasp of hourly distribution pattern. Storm records of which daily rainfall is larger than 100 mm at both gauges are shown in Fig. 4.1.

4.2.2 Flood Runoff Data

Flood hydrographs at Magat damsite are available to establish the flood runoff simulation model as shown in Table 4.1 and Fig. 4.2.

Annual maximum flood water level/runoff are available for the frequency analysis of flood runoff at the following stations:

HY-18

No.	Station No.	Station Name	Basin Area (km ²)	River Name	Recorded	Period
1	10	Calantac	907	Paret	1958-1969	11 Yrs.
2	18	Larion Alto	655	Tuguegarao	1956-1970	15 Yrs.
3 -	25	Pasonglao	1,987	Chico	1963-1969	7 Yrs.
4	41	Palattao	6,626	Cagayan	1961-1970	10 Yrs.
5	43	Minanga	1,565	Ilagan	1964-1970	7 Yrs.
6	47	Oscariz	4,150	Magat	1941-1968	25 Yrs.

4.3 Methodology

The flood runoff analysis is made in accordance with the general procedure shown in Fig. 4.3. As seen in this procedure, the flood runoff analysis is performed through three substantial works, they are:

Standard and the state of the s

- a) construction of river system model,
- b) rainfall analysis, and,
- c) flood runoff analysis.

The detailed contents of each study item are described below.

4.3.1 River System Model

The river system model is a necessary tool for the flood runoff calculation with the aid of an electronic computer. The model comprises all the elements of flood runoff mechanism such as river basins, channels and dams/reservoirs.

These elements are linked together by the subbase points. The subbase points, at which the flood runoff is calculated, are determined at locations where significant changes in peak flood runoff are expected such as:

a) junctions of main river and major tributaries,

- b) reservoir sites, and,
- c) points where the channel capacity changes.

Base points, which are selected among the subbase points, are the principal points for estimating the flood runoff and for determining the flood distribution along the river. The base points are located principally at the following points:

- a) river mouth,
- b) main river at junction of major tributary,
- c) major tributary at junction of main river, and,
- d) dams/reservoirs.

The Cagayan river basin is divided into subbasins at every base and subbase points. The channels in the model are prepared for the reach where the flood runoff is substantially influenced by the channel storage between the nodes such as subbase and base points. The dams taken into the model include the existing and proposed dams as identified.

4.3.2 Method of Rainfall Analysis

Rainfall analysis aims to estimate the basin mean probable rainfall and its hourly distribution. The results of rainfall analysis are used to the computation of the probable flood runoff.

(1) Design Storm Duration

The design rainfall duration is to be determined from the duration of recorded major storms.

(2) Basin Mean Probable Rainfall

The basin mean rainfall is estimated by either of the following two approaches depending on the number of raingauge and the availability of the recorded data.

- a) The basin mean rainfall is estimated directly from recorded rainfall by areal weight of Thiessen polygon method.
- b) The basin mean rainfall is estimated by the above areal weight and adjustment factor for basin elevation expressed in the following equation.

$$Rm = \sum_{i} fi Ri FLi$$

where,

Rm : Basin mean rainfall (mm),

f_i : Areal weight,

Ri : Point rainfall (mm),

FLi: Adjustment factor for elevation of object basin

(The relationship of FL-value with the basin average elevation which is studied in the report "Nationwide Flood Control Plan and River Dredging Program (Nov. 1982)" is applied.).

The basin mean probable rainfall is calculated by using a series of estimated annual maximum basin mean rainfall. The frequency analysis is performed by the Pearson Type III method, because the results obtained from this method fit well the rainfall data plotted by the Hazen method. The equations of the Pearson Type III and Hazen methods are described below.

a) Pearson type III method

Probable rainfall (x) at any desired return period (T) is calculated with a series of the annual maximum rainfall (X_i) by the following equations:

$$X = 10 (\bar{Y} + (\bar{V})^{0.5} k)$$
 (mm)

$$\overline{Y} = (1 / N) \sum_{i=1}^{N} Y_i$$

$$\overline{V} = (1 / (N - 1)) \sum_{i=1}^{N} (Y_i - \overline{Y})^2$$

where,

N : Total number of rainfall

i : Order of the annual maximum rainfalls in magnitude

 Y_i : Logarithm of rainfall (X_i)

k : Skew factor corresponding to (T) for the coefficients of variation (C_v) and skewness (C_s)

Y : Average of Y_i

$$C_{v} = \frac{(\overline{v})^{0.5}}{\overline{v}}$$

$$C_{s} = \frac{N \sum_{i=1}^{N} (Y_{i} - \overline{Y})^{3}}{(N-1) (N-2) \overline{V}^{3/2}}; \text{ If } C_{s} \stackrel{<}{=} 0, \text{ take } C_{s} = 0$$

b) Hazen method

The annual maximum rainfalls (X_i) are plotted on a probability paper in accordance with the following equation, and probable rainfall (X) is projected corresponding with return period (Y):

$$P(X_i) = \frac{2i - 1}{2N}$$

HY-22

where,

 $P(X_{i})$: Plotting position

i : Order of the annual maximum rainfalls in magnitude

: Total number of rainfall data

(3) Hourly Rainfall Distribution

Ŋ

The hourly rainfall distribution is assumed to have centerconcentrated pattern which is commonly applied to the estimation of design flood runoff. This pattern is derived from the rainfall intensity-duration curve using the actual hourly rainfall data of selected stations. To obtain this pattern, the hourly rainfall increments from the intensity curve are distributed in such a way that the maximum hourly rainfall increment is put at the center of total rainfall duration and the succeeding hourly rainfall increments are alternately distributed before and after the central increment so that rainfall intensity of continuous rainfall around the center could accord with the rainfall intensityduration curve of the station.

The above pattern is adopted for 24 hours in the central portion of design rainfall. For the remaining portion, the hourly rainfalls are generally distributed uniformly using the relationship between 1-day and design rainfall amounts.

4.3.3 Method of Flood Runoff Analysis

Judging from the availability of flood runoff records, the flood runoff analysis is made by applying rainfall data to flood runoff simulation model. Storage function model is applied as the simulation model, which is commonly used and judged to be suitable due to data availability. The flood runoff in a river basin is assumed to be formed by the following different functional elements:

HY-23

a) Runoff from subbasin

b) River channel flow

c) Flood regulation by reservoir

The estimation results are evaluated by comparing with recorded data to decide the final figures of probable flood runoff.

(1) Flood Runoff from Subbasin

The flood runoff calculation is performed by the storage function method. The basin factors, storage function, runoff coefficient and baseflow are provided by the following methods.

a) Basin factor

The basin factors are prepared using 1/50,000 or 1/250,000 topographic maps, they are catchment area of basin/subbasin (km^2) , river length in basin/subbasin (km), and overall slope of the longest watercourse from the point of interest to watershed divide (S).

b) Storage function

The basic equation of the storage function method is described below.

 $r - q_{f} = dS_{f}/dt$ $S_{f} = K q_{f}^{P}$ $q_{f} = q(t+T_{1})$ $Q = 0.2778 (f q_{f} + (1-f) q_{sa}) A + Q_{B}$

where,

r : Basin average hourly rainfall (mm/hr)

 q_{ℓ} : Runoff depth from a basin (mm/hr)

S₁ : Storage (mm)

q : Runoff depth from a basin with lag time, T_1 (mm/hr)

 q_{sa} : Runoff depth from a basin after saturation of rainfall, R_{sa} (mm/hr)

Q : Discharge (m^3/s)

f : Runoff coefficient

 $(r \leq R_{sa} = f = f_1, r > R_{sa} = f = 1.0)$

A : Catchment area (km^2)

 $Q_{\rm B}$: Baseflow (m³/s)

K, P: Coefficient

t : Time (hr)

c) Coefficients K and P of storage function and lag time

The coefficient of the storage function and lag time are estimated by the following formulas expressed by river length and river bed slope and are calibrated through the simulation of the flood records from the rainfall.

 $K = a*118.84*i^{0.3}$ $P = b*0.175*i^{-0.235}$ T = c*0.047*L - 0.56

where, i : River bed slope

L : River length (km)

T : Lag time (hrs)

K, P : Coefficient for a function

a,b,c: Constant for K,P,T

d) Primary runoff coefficient and saturated rainfall

Primary runoff coefficient is estimated based on the observed discharge hydrograph and corresponding rainfall records during flood. Saturated rainfall, which is the changing point of runoff coefficient, is determined based on the above hydrological records. e) Baseflow

The baseflow is estimated averaging the runoff in dry season, which is judged to be representative of the baseflow during rainy season as shown in Fig. 3.3. The baseflows at base point and in subbasin are expressed by the specific discharge derived from the relation between the baseflow and catchment area.

(2) River Channel Flow

The flood runoff from each subbasin is subject to the retardation effect due to channel storage and lag time to reach a point of interest.

a) Flood retardation by channel storage

The computational method of flood retardation is the storage function method. This method is expressed as,

 $S = KQ^{P}$

 $\frac{\mathrm{dS}}{\mathrm{dt}} = \mathbf{I} - \mathbf{Q}$

where, S : Channel storage (m^3)

Q : Outflow from the channel stretch (m^3/s)

K, P : Coefficients

dt : Unit time (sec)

- dS : Incremental channel storage corresponding to dt (m^3)
 - : Inflow to the channel stretch (m^3/s)

b) Coefficients K and P

1

The relationship between the storage and outflow is established using the non-uniform/uniform flow calculation with the aid of several data such as 1/50,000 topographic maps, surveyed cross sections and profiles, and other available topographic maps. c) Lag time of channel flow

Various empirical formulas are proposed for the estimation of the lag time of channel flow. The Kraven formula which is the simplest among them is adopted for the present study.

The Kraven formula gives the following empirical value of the flood velocity depending on the river bed slope.

River Bed Slope	More than 1/100	1/100-1/200	Less than 1/200
Flow Velocity (m/s)	3.5	3.0	2.1

(3) Flood Regulation by Reservoir

In estimating the flood runoff under the present river condition, the flood regulation by the existing Magat reservoir is assumed to be performed by the constant-ratio/constant amount outflow method. The regulation begins when the inflow to the reservoir reaches a certain amount of given discharge which is defined as the control starting discharge (QB). In this regulation method, the outflow becomes diversified at a constant ratio of the inflow, starting from QB until the peak of the inflow hydrograph. After this peak, the outflow is kept at a constant value.

The regulation method is thus, specified by the outflow rate (AA) and control starting discharge (QB). The control starting discharge is determined based on the carrying capacity of the downstream channel. The outflow rate is expressed as:

$$AA = \frac{QO}{QI_{max}} - QB$$

where,

QI max : Maximum design inflow to reservoir (m^3/s) QO max : Maximum design outflow from reservoir (m^3/s)

(4) Verification of Estimated Flood Runoff

The probable flood runoff is estimated at strategic points in the basin. This probable flood runoff estimated from probable rainfall is compared with the recorded runoff and evaluated.

(5) Flood Runoff Distribution

The distribution of the flood runoff along the river is examined under the present river condition with and without Magat dam and under the alternative flood control plans.

4.4 River System Model

The 9 points are determined principally as base points at the junctions of main river and major tributaries, Chico, Siffu, Ilagan, Magat rivers. The location of each point and its upstream basin area are tabulated below.

Base Poi	nt Location	Basin Area (km ²)	Distance from Rivermouth (km)
BP - 1	Rivermouth of Gagayan river	27,281	0.0
BP - 2	Cagayan river at junction of Chico river	21,473	51.6
BP - 3	Cagayan river at junction of Siffu river	15,334	198.7
BP - 4	Cagayan river at junction of Ilagan river	11,993	212.3
BP - 5	Cagayan river at junction of Magat river	6,633	232.8
BP - 6	Chico river at junction of Cagayan river	4,551	51.6
BP - 7	Siffu river at junction of Cagayan river	2,015	198.7

BP - 8	Ilagan river at junction of Cagayan river	3,132	212.3
BP - 9	Magat river at junction of Cagayan river	5,113	232.8

The following 15 damsites are also taken as base points.

(1)	Casecnan	(1,150 km ²)	(9)	Ilagan No.1	(1,350 km ²)
(2)	Cagayan No.2	(1,631 km ²)	(10)	Disabungan	(652 km ²)
(3)	Cagayan No.1	(2,364 km ²)	(11)	Siffu No.1 (A)	(656 km ²)
(4)	Diduyon	(477 km ²)	(12)	Mallig No.2	(362 km ²)
(5)	Addalam (A)	(864 km ²)	(13)	Chico No.2	(720 km ²)
(6)	Alimit No.1 (A)	(559 km ²)	(14)	Chico No.4	$(1,410 \text{ km}^2)$
(7)	Matuno No.1	(550 km ²)	(15)	Pinukpuk	(856 km ²)
(8)	Magat	(4,143 km ²)			

Subbase points are determined at junctions of tributaries considering the river basin scale. The Cagayan river basin is, then, divided into 50 subbasins at the selected base and subbase points. 30 river channels are prepared as the basin elements, which are regarded to influence the flood runoff substantially.

Finally, the river system model is made assembling the above base and subbase points including the following basin components:

- a) 50 subbasins
- b) 30 river channels
- c) 15 damsites

The basin division is shown including all the basin components in Fig. 4.4. The Cagayan river system model is illustrated in Fig. 4.5.

4.5 Rainfall Analysis

4.5.1 Rainfall Duration Time

The major storms recorded in Aparri and Tuguegarao show that rainfall duration is usually 4-day or less. On the other hand, the lag time of flood runoff is estimated at about 64 hours in the longest watercourse. The rainfall duration for the flood runoff analysis at base point 1 to 9 is therefore decided to be 4 days. While, the duration is determined to be 1 day for runoff analysis at damsites considering lag time.

4.5.2 Basin Mean Probable Rainfall

The Thiessen polygon method is used to estimate the basin mean rainfall from point rainfall as shown in Table 4.2 and Fig. 4.6. Although a deformed polygon appears in Fig. 4.6, basin rainfall is attested to be usable by comparing rainfalls of deformed and uniform polygons. Adjustment factor for basin mean elevation is adopted to estimate the basin mean rainfall at the damsites as shown in Table 4.3 and Fig. 4.7.

The probable basin mean rainfall is calculated from annual maximum basin mean rainfall by Pearson Type III method. The calculated probable rainfall at the base points are shown in Table 4.4 and Fig. 4.8.

4.5.3 Hourly Rainfall Distribution

A 1-day rainfall duration curve is developed using the hourly rainfall data at Aparri and Tuguegarao as given in Fig. 4.9. This 1-day rainfall duration curve is linearly extrapolated for 4 days. In this manner, the 4day duration curve is developed. A 1-day rainfall amounts to 65% of 4-day amount, in accordance with the rainfall records. The hourly rainfall distribution is assumed from records to be center-concentrated pattern. The hourly rainfall distribution of probable 4-day rainfall is, consequently, estimated as shown in Fig. 4.10. 4.5.4 Areal Rainfall Distribution

There is not enough rainfall data covering the whole basin to examine the areal distribution pattern of storm. Therefore, the areal distribution of the probable rainfall is assumed to give the intensive rainfall to each of the basins of major tributaries. Then, 5 distribution types are introduced as given in Table 4.5.

The distribution type of intensive rainfall in Upper Cagayan basin is adopted to estimate the flood runoff in the main river, because this type induces the biggest runoff. The other distribution types are used for the respective tributaries' runoff estimation.

4.6 Flood Runoff Analysis

4.6.1 Runoff from Subbasin

Flood runoff from subbasin is estimated by applying the storage function of which coefficients are based on the recorded five (5) storms at Magat damsite shown in Table 4.6.

The coefficient of the storage function and lag time for subbasins are estimated by the following formulas, which are well known as Tone River Formulas and applied for many rivers in Japan.

 $K = a \times 118.84 \times i^{0.3}$ $P = b \times 0.175 \times i^{-0.235}$ $T = c \times 0.047 \times L - 0.56$

where,	i	:	River bed slope
	L	:	River length (km)
	Т	:	Lag time (hrs)
	K, P	:	Coefficient for a function
	a,b,c	:	Constant for K,P,T ($a,b,c = 1.0$ for Tone River
			Formula)

The values a, b and c of subbasins are examined through trial and error by comparison of the flood hydrographs recorded at Magat damsite and estimated from rainfall by applying Thiessen Polygon method seen in Fig. 4.11, and determined to be 0.7, 1.0 and 1.0, respectively. Estimated coefficients of storage function K, P and T are listed in Table 4.7.

Primary runoff coefficient (f_1) and saturated rainfall (Rsa) are estimated to be 0.5 and 150 mm based on the selected storms as shown in Fig. 4.12.

The specific baseflow which is estimated using data at 23 stream gauging stations is $0.04 \text{ m}^3/\text{sec/km}^2$ as shown in Fig. 4.13.

Fig. 4.14 shows the comparison of observed flood hydrograph at Magat damsite and the calculated one with the above values. As seen in this figure, both hydrographs agree with each other. This fact implies that the above storage function is suitable to estimate flood runoff from rainfall.

4.6.2 Channel Flow

The values of the channel storage for each channel calculated under the present river condition are shown in Table 4.8 and 4.9. Under the present river condition, non-uniform flow calculation is applied to channel No. 7, 8, 11, 12, 15, 16, 17, 18, 19, 20, 21, 22, 26, 27, 28, 29 and 30 while uniform flow calculation is used for the others. The channel storage curves are shown in Fig. 4.15. The lag time of channel flow in each channel estimated by Kraven formula is shown in Table 4.9.

4.6.3 Flood Regulation by Magat Reservoir

The flood operation for Magat reservoir is performed by the constantratio/constant amount outflow method which is studied by the project "Flood Forecasting and Warning System for Dam Operation Project (May 1984)". In this project, the control starting point, constant ratio and constant amount outflow are proposed to be 1,600 m^3/s , 0.4 and 3,000 m^3/s , respectively.

4.6.4 Flood Runoff Distribution

(1) Probable Flood Estimated from Recorded Flood Runoff

The following table shows the results of frequency analysis for 100year flood on the basis of recorded flood at gauges.

Basin Area	100-Yr Flood	Specific Runoff
(km ²)	(m ³ /s)	$(m^3/s/km^2)$
907	4,900	5.40
655	4,100	6.26
1,987	7,100	3.57
6,626	17,000	2.57
1,565	5,800	3.71
4,150	13,200	3.18
	(km ²) 907 655 1,987 6,626 1,565	$\begin{array}{c c} (km^2) & (m^3/s) \\ \hline 907 & 4,900 \\ 655 & 4,100 \\ 1,987 & 7,100 \\ 6,626 & 17,000 \\ 1,565 & 5,800 \\ \end{array}$

(2) Probable Flood Runoff Estimated from Rainfall

The estimated probable flood runoff distribution along the present river and probable flood at damsites are shown in Fig. 4.16. The following table shows the 100-year probable flood peak discharges under the present river condition without Magat dam.

Base Points or Gauging Station	Basin Area (km ²)	100-Yr Flood (m ³ /s)	Specific Runoff (m ³ /s/km ²)
BP-1	27,281	21,400	0.78
BP - 2	21,473	21,000	0.98
BP - 3	15,334	25,300	1.65
BP-4	11,993	23,500	1,96
BP - 5	6,633	14,700	2.22
BP-6	4,551	8,700	1.91
BP - 7	2,015	3,300	1.64
BP-8	3,132	9,400	3,00
BP-9	5,113	10,600	2.07

Calantac	907	5,000	5.51
Larion Alto	655	4,000	6.11
Pasonglao	1,987	6,700	3.37
Palattao	6,626	14,700	2.22
Minanga	1,565	8,800	5.62
Oscariz	4,150	13,800	3.33

(3) Comparison and Evaluation

The probable 100-year floods estimated from rainfall and recorded runoff are illustrated in Fig. 4.17 for comparison. As seen in this figure, both values agree with each other. This fact implies that the flood runoff analysis method based on rainfall data is appropriate and applicable to flood control planning.

100-year flood runoff hydrographs at base points are shown in Fig. 4.18. Specific flood peak runoff for 100-year probability is illustrated in Fig. 4.19.

4.6.5 Flood Runoff under Alternative Schemes

The probable flood runoff distribution is estimated under the following flood control schemes.

For	Framework Plan	(100-year probable flood)
a)	Alternative OD	(Confining dikes without flood control dam)
b)	Alternative 5D	(Confining dikes with 5 flood control dams)
c)	Alternative 9D	(Confining dikes with 9 flood control dams)
d)	Alternative ODM	(Confining dikes without flood control dam and with
		improved narrows)
e)	Alternative 5DM	(Confining dikes with 5 flood control dams and improved
		narrows)
f)	Alternative 9DM	(Confining dikes with 9 flood control dams and improved
		narrows)

For Long Term Plan

a) with confining dikes and 5 flood control dams

b) with confining dikes, 5 flood control dams and improved narrows

c) with 5 flood control dams and improved narrows

d) with Cagayan No. 1 dam

- e) with Ilagan No. 1 dam
- f) with Siffu No. 1 (A) dam
- g) with Mallig No. 2 dam
- h) with improved narrows
- i) with Magat dam with flood control space of 200 MCM
- j) with Magat dam with flood control space of 300 MCM
- k) with Magat dam with flood control space of 400 MCM

The above flood control schemes are detailed in the sectoral study of flood control. The estimation results for the above flood control schemes are given in Fig. 4.20 and Fig. 4.21. Table 4.10 and Table 4.11 show the channel storage for confining dike condition.

V. SEDIMENT ANALYSIS

5.1 General

The sediment analysis is carried out to estimate the sediment yield in the upper river basins and the sediment transport capacity in river channels. The study results are used for the reservoir sedimentation and the river improvement plan.

5.2 Data Availability and Methodology

5.2.1 Data and Method for Sediment Yield Estimate

The sediment yield in the upper river basins is usually examined by the following records or formulas:

- a) reservoir sedimentation record,
- b) empirical formulas,
- c) sediment sampling record.

The reservoir sedimentation record does not exist in the Cagayan basin. In Luzon Island, the sediment in the reservoir is measured at Binga Dam and Ambuklao Dam in the Agno river. From this measurement, the annual sediment yield is estimated to be 4.9 mm at Binga Dam and 6.0 mm at Ambuklao Dam. These values are considerably big due to mining operations and are not representative of that in the Cagayan basin.

The empirical formula is usable for obtaining the sediment yield in the upper river basins. Dr. Tanaka and Dr. Ishige developed the following formulas on the basis of dam sedimentation records in Japan.

Tanaka Formula;

 $Y = 13.0X_1 - 6 \pm 189$, $X_1 = R_f \times E_m / 10^4$

Ishige Formula:

$$\log Y = 1.50 \log X_2 - 5.58 \pm 0.65 \sqrt{0.09 + (\log X_2 - 5.41)^2}$$

 $X_2 = R_f \times P$

where,

Y : Annual sediment yield rate $(m^3/yr/km^2)$ R_f: Mean relief of basin (m); R_f = $\sum (E_{max} - E_{min})/n$ E_m: Mean elevation of basin (m, MSL); E_m = $\sum (E_{max} + E_{min})/2n$ E_{max}, E_{min}: Maximum and minimum elevations read in a square of 4 km x 4 km on topographic maps (scale 1/50,000) (m, MSL) n : Number of squares which cover the basin

p : Mean annual major rainfall depth (mm/yr)

The suspended sediment records are collected at 25 stations in the Cagayan basin. Among these stations, 3 stations - Pasonglao, Oscariz, Dippadiw - have enough data for deriving the suspended sediment rating curves. The annual sediment yield in the upper river basin is estimated by using these rating curves and daily discharge duration curves and by adding assumed bed load.

5.2.2 Data and Method for Sediment Transport Estimate

The annual sediment transport capacity in river channels is estimated by using the sediment discharge formula and the discharge duration curves. Among 3 sediment discharge formulas, Brown Formula, Einstein-Brown Formula, and Engelund-Hansen Formula, which are commonly used and calculate the total sediment load including the suspended and bed load, one formula is selected to estimate the sediment transport capacity.

The above mentioned formulas are expressed below.

a) Brown Formula

$$Qs = 10 \left(\frac{U^2}{(W_s/W_w-1) gd} \right)^2 x Ud$$

b) Einstein-Brown Formula

$$Q_s = F_1 (g (W_s/W_w-1) d^3)^{0.5} \times 40 \times (\frac{U^2}{(W_s/W_w-1)gd})^3$$

$$F_{1} = \left(\frac{2}{3} + \frac{36 n^{2}}{gd^{3} (W_{s}/W_{w}-1)}\right)^{0.5} - \left(\frac{36 n^{2}}{gd^{3} (W_{s}/W_{w}-1)}\right)^{0.5}$$

c) Engelund-Hansen Formula

$$Q_{s} = 0.05 V^{2} \left(\frac{d}{g (W_{s}/W_{w}-1)}\right)^{0.5} \left(\frac{t_{o}}{(W_{s}-W_{w}) d}\right)^{1.5}$$

$$V = \sqrt{gR'I} \times (0.6 + 2.5 \ (n(R'/2.5d)))$$

where,

Qs	:	Sediment discharge (m ³ /s/m)
U	:	Friction velocity (m/s) ; $U = (gRI)^{0.5}$
d	:	Grain size of bed materials (m)
W _s ,W _w	:	Unit weight of sediment and water (tons/ m^3)
V	:	Mean velocity (m/s)
to	:	Tractive force of flow (tons/m ²); $t_o = W_w RI$
R		Hydraulic radius (m)
I.	: .	Energy gradient of flow
n _w	:	Kinematic viscosity of water; $n_w = 8.50 \times 10^{-7} m^2/s$
		for temperature 27°C
g	:	Acceleration of gravity, $g = 9.8 \text{ m/s}^2$

5.3 Sediment Yield

The sediment yield in the upper river basins is estimated by two empirical formulas, Tanaka Formula and Ishige Formula. 6 basins are taken for this estimation, they are Upper Cagayan, Magat, Ilagan, Lower Cagayan, Upper Chico and Lower Chico basin. The mean relief and mean elevation of Basin 1 to Basin 6 are tabulated in Table 5.1, which are based on the topographical map of 1/50,000. For Ishige Formula, the mean annual major rainfall depth is calculated as the mean of annual sum of the consecutive rainfall over 100 millimeters as shown below.

	<u>Basin 1</u>	<u>Basin 2</u>	<u>Basin 3</u>	<u>Basin 4</u>	Basin 5	<u>Basin 6</u>
Rainfall (mm)	924	945	673	753	1,703	1,146

The estimated yield by formulas is shown below.

			Sediment Yie	ld (mm/year)
Basin	Basin Name	Downst. Point	Tanaka	<u>Ishige</u>
1	Upper Cagayan	Cagayan No. 1 dam	0.7 - 1.0	0.6 - 3.4
2	Magat	Magat dam	0.7 - 1.1	0.6 - 3.3
3	Ilagan	Ilagan No. 1 dam	0.4 - 0.8	0.4 - 1.3
4	Lower Cagayan	conj. Tuguegarao R.	0.3 - 0.7	0.5 - 1.9
5	Upper Chico	Pasonglao	1.7 - 2.0	1.6 -21.5
6	Lower Chico	Pinukpuk dam	1.1 - 1.4	1.0 - 7.9

The above table shows the wide fluctuation of the yield between 0.3 mm/year and 21.5 mm/year. Then, the probable yield in the upper river basin is difficult to be determined by the empirical formulas.

The sediment yield in the upper river basins is therefore estimated by applying the sediment rating curve. The suspended sediment rating curves are developed at Pasonglao in the Chico river, Oscariz in the Magat river and Dippadiw in the Upper Cagayan river as shown in Fig. 5.1. The suspended sediment yield is estimated at long term and reliable runoff gauges, Ampawilen, Oscariz and Guinalvin, which is shown in Table 5.2. The bedload is assumed to be 20% of the estimated suspended load considering the sediment material and concentration. The estimated sediment yield is summarized below.

		Unit:	m ³ /km ² /year
Runoff	Suspended	Bed	Total
Gauge	Load	Load	Sediment
*.		고 문제가 가지 않았다.	· · ·
Ampawilen	880	180	1,060
Oscariz	1,270	250	1,520
Guinalvin	1,070	210	1,280
	Gauge Ampawilen Oscariz	GaugeLoadAmpawilen880Oscariz1,270	GaugeLoadLoadAmpawilen880180Oscariz1,270250

Among the above values, the biggest one of $1,520 \text{ m}^3/\text{km}^2/\text{year}$ or 1.5 mm/year is selected as the sediment yield for the whole basin on the safe side.

5.4 Sediment Transport

The sediment transport capacity of the present river channel is calculated at the selected 26 points on the Cagayan river and the tributaries. Einstein-Brown Formula is applied to the sediment transport capacity estimation, since Brown Formula, Einstein-Brown Formula and Engelund-Hansen Formula lead near results and the Einstein-Brown Formula is simple.

The specific gravity and the mean diameter of the riverbed material are determined to be 2.61 and 0.04 cm on the basis of the investigation result, and are applied to Einstein-Brown Formula. Ten days mean simulated runoff is used for this Einstein-Brown Formula, then the adjustment factor of 2.0 is introduced, which is the ratio between the estimate based on the daily runoff and that based on 10 days mean runoff derived at Palattao. The computed sediment transport capacity in the present river channel is shown in Fig. 5.2.

HY-40

VI. WATER QUALITY

6.1 Evaluation of Water Quality

Water quality analysis aims to evaluate the appropriateness of river water quality for irrigation, municipal and industrial uses.

The water quality test results are tabulated in Table 6.1 for the Gagayan basin. According to the water quality criteria by NPCC shown in Table 6.2, water in the Cagayan basin is judged to be usable for irrigation, municipal and industrial purposes though Calcium is much contained.

			Drainage	Anni	ial_ru	noff coef	ficie	nt	- Remarks	
	Station	Stream	area (km ²)	Runoff	(mm)	Rainfall	(mm)	Coeff.	Kemarks	
5	Simay	Zinundungan	189	165-171	2,421		2,268	1.07		
7	Calaoagan	Dummon	308	'68-'71	2,019		2,710	0.75		
10	Calantac	Paret	907	163-164	3,221		4,110	0.78		
12	Escolta	Matalag	655	'65 -'7 1	1,656		2,430	0.68		
18	Larion Alto	Tuguegarao	655	'65-'71	3,067		4,000	0.77		
19	Pinukpuk	Saltan	856	'65-'71	1,740		2,500	0.70	4. *	
24	Abbot	Chico	3,349	'63- <u>'</u> 64	3,287	:	2,770	1.19		
25	Pasonglao	Chico	1,987	'66-'69	2,676		2,960	0.90		
29	Antagan	Tumauini	170	'65-'71	3,405		4,330	0.79		
30	Ampawilen	Chico	751	'65-'71	2,639		3,400	0.78		
34	Taed	Chico	391	'65-'71	2,511	· · ·	3,300	0.76		
37	Casile	Casile	195	'66-'69	457		1,800	0.25		
38	Maligaya	Mallig	563	'68'71	1,070		2,260	0.47		
39	Munoz	Siffu	686	'66-'69	1,049		2,220	0.47		
40	Malalam	Ilagan	3,123	'63-'64	2,496		3,170	0.79		
41	Palattao	Cagayan	6,626	'65-'71	1,594	:	2,370	0.67		
42	Supang	Sabangan	57	'65-'71	2,464		3,200	0.77		
43	Minanga	Ilagan	1,565	166-169	1,646	:	2,580	0.64		
45	Caipilan	Taotao	430	¹ 61- ¹ 62	381		1,800	0.21		
46	Dipalin	Di sabungan	198	'66-'69	1,640	:	2,770	0.59		
47	Oscaríz	Magat	4,150	'63-'64	1,534		2,250	0.68		
48	Dulao	Alimit	573	168-171	2,244	:	2,900	0.77		
50	Hapid	Ibulao	606	'66 <u>-</u> '69	2,672		3,350	0,80		
51	Camandag	Cadaclan	261	'69	1,196	:	2,400	0.50		
52	Pangal	Cagayan	4,244	'65-'71	2,188	:	2,750	0.80		
53	Panang	Cagayan	2,392	'61-'62	1,707		2,880	0.59		
54	Guinalvin	Addalam	921	'65-'71	1,676		2,400	0.70		
55	Bante	Matuno	558	'63-'64	2,701		3,200	0.84		
57	Kamamasi	Diduyon	462	179-180	846	:	2,700	0.31		
61	Bato	Magat	1,649	'65-'71	1,377	:	2,710	0.51		
62	Dippadiw	Cagayan	2,380	'68'71	2,435	:	2,850	0.85		

Table 1.2 Mean Monthly Water Level at Aparri

(Daily Mean)

Unit; m

Year	Jan	Feb	Mar	Apr	May	June	July	Aug	Sept	Oct	Nov	Dec	Mean
1961 1962	0.03 0.16	0.04 0.19	0.16 0.19	0.16 0.20	0.22 0.21	0.31 0.16 0.28 0.29	0.37 0.32	0.31 0.38	0.34 0.39	0.34	0.30	0.17 0.21	0.22 0.25

Mean= 0.24

(Daily Maximum)													it; m
Year	Jan	Feb	Mar	Apr	Мау	June	July	Aug	Sept	0ct	Nov	Dec	Mean
1961 1962	0.50	0.54	0.66	0.66 0.75	0.68	0.83 0.90 0.80 0.90	0.72	1.05 0.78	0.74 0.88	0.72	0.88	0.76 0.75	1.05

Maximum= 1.05

(Daily Minimum) Unit; m Year Jan Feb Mar Apr May June July Aug Sept Oct Nov Dec Mean 1960 -0.48-0.52-0.44-0.42-0.42 -0.25 -0.34-0.38 -0.40-0.38-0.34-0.32 -0.52 1961 -0.44-0.34-0.34-0.42-0.31 -0.34 -0.28-0.24 -0.22-0.26-0.33-0.39 -0.44 1962 -0.32-0.24-0.28-0.32-0.32 -0.28 -0.26-0.18 -0.28 - - - -0.36 -0.36 1963 -0.35-0.42-0.41-0.31-0.41 -0.37 -0.39-0.39 -0.36-0.39-0.39-0.39-0.33 -0.42

Minimum= -0.52

HY-43

Table 2.1

Summary of Meteorological Record

Rainfall (mm)

Station	Period	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug	Sept.	Oct.	Nov.	Dec.	Annua!
Aparri	1951 - 85	134.4	75.2	45.4	35. <u>3</u>	99.4	175.2	183.5	226.5	286.8	345.2	397.6	210.8	2,215.3
Lal-lo	1972 ~ 84	125.0	56.1	29.5	55.5	162.3	145.9	171.2	275.0	197.7	310.3	349.1	197.2	2,074.8
Bitag Grande	1975 - 80	85.5	21.0	28.9	27.4	212.6	118.3	313.0	199.9	548.7	214.2	286.3	141.2	2,197.0
Tuao	1956 - 85	29.4	24.3	31.2	63.3	171.0	195.4	214.8	232.2	175.1	246.7	230.8	96.9	1,711.1
Tuguegarao	1949 - 85	18.7	14.5	30.2	49.1	113.1	155.2	195.5	234.5	202.2	248.5	276.4	94.7	1,632.6
Pinukpuk	1970 - 81	83.7	26.0	58.4	75.8	203.8	233.6	263.2	322.3	212.7	365.5	364.2	189.2	2,398.4
Naneng	1956 - 85	38.3	28.1	51.4	72.9	208.0	271.8	285.4	337.8	288.7	298.2	299.2	94.9	2,274.7
Guilguila	1963 - 80	122.7	56.1	61.7	77.0	215.4	321.8	329.1	284 . 7	312.9	318.5	375.9	237.2	2,713.0
Lubuagan	1969 - 78	62.6	32.8	65.2	51.2	147 7	224.6	213.1	236.5	210.8	237.2	275.0	155.4	1,912.1
Basao	1963 ~ 75	95.6	27.2	70.6	114.8	288.8	422.0	382.0	341.4	314.9	312.6	439.8	271.5	3,081.2
Ilagan	1965 - 84	59.1	20.9	32.3	62.6	155.4	172.8	144.7	186.0	172.2	291.1	315.9	191.1	1,804.1
Banga-an	1963 - 78	27.2	7.6	22.0	78.8	218.7	274.8	302.4	375.6	274.5	148.8	115.3	26.4	1,872.1
Bontoe	1963 - 85	17.9	11.9	46.6	127.6	263.8	294.5	390.5	267.9	302.8	204.8	152.5	54.4	2,135.2
Barlig	1963 - 85	134.4	41.0	92.9	95.2	309.7	402.6	394.7	411.6	372.1	407.8	499.5	326.3	3,487.8
Bauko	1963 - 80	6.5	7.5	43.8	169.1	284.5	304.8	371.0	421.4	313.4	188.7	67.9	54.4	2,233.0
Mt. Polis	1963 - 80	160 4	134.0	110.1	157.7	337.3	457.1	516.8	553.5	453.0	378.1	370.9	246.6	3,875.5
Mt. Data	1950 - 78	27.2	25.0	74.6	187.9	357.0	413.5	619.4	563.3	465.2	296.3	220.4	78.2	3,328.0
Lagawe	1968 - 82	176.0	88.5	65.2	190.1	171.3	265.0	.362.0	319.9	341.4	331.6	394.3	146.3	2,851.6
Nayon	1968 - 80	63.4	25.5	69.9	89.5	217.2	200.4	207.8	243.6	220.4	240.2	185.7	99.3	1,862.9
Echague	1976 - 85	17.5	9.1	18.2	91.7	114.5	97.1	148.8	259.9	189.6	272.8	128.0	142.3	1,489.5
Diadi	1968 - 71	54.2	16.3	49.9	54.4	173.0	239.2	275.8	192.4	211.4	399.6	280.0	153.3	2,099.5
Barat	1968 - 80	23.8	10.1	35.8	90.0	226.7	224.8	271.4	323.1	302.7	337.8	156.4	104.9	2,107.5
Consuelo	1956 - 85	33.5	18.0	44.0	70.9	221.5	252.6	380.4	331.0	325.5	263.9	211.8	60.5	2,213.6
Gabong	1973 - 82	38.6	13.0	25.5	33.4	128.5	179.9	251.5	216.7	-229.0	230.0	284.9	90.3	1,721.3
Dakgan	1973 - 82	18.4	11.3	29.8	23.1	134.5	158.8	234.2	176.5	216.5	273.1	274.6	68.9	1,619.7
Casiguran	1961 - 84	234.2	113.8	176.5	136.3	242.3	229.4	284.7	251.9	592.5	421.7	628.8	402:9	3,715.0
Wacal	1980 - 85	36.8	19.6	112.2	160.7	174.1	107.5	255.5	201.4	183.2	259.9	141.4	50.4	1,702.7
Banti	1980 - 85	33.7	12.4	17.9	71.4	102.7	86.6	133.0	169.9	224.6	177.9	78.9	34.7	1,143.7
Dippadiw	1980 - 83	185.8	19.7	53.2	27.2	190.1	59.7	245.8	239.2	181.1	249.7	458.1	299.5	2,209.1
San Francisco	1975 - 80	122.8	138.2	47.0	41.8	146.3	82.3	143.1	143.4	153.9	328.3	209.8	171.7	1,728.6
NIA, Cabarroguis	1982 - 85	54.2	7.7	52.0	95.5	170 3	185.8	96.0	187 8	124.2	159.2	121 0	117.5	1.371.2
•	1976 - 85	15.4								241.4				1,562.7
Baretbet	1977 - 85	21.1								254.4				1,774.0
Baligatan	1976 - 85	29.4							:					1,652.5
Poblacion	1010 00		10	31.03	,	20010	21110	23444				10012		2,05205
Lagawe	1976 - 85	44.9	37.5	62.7	117.9	240.1	183.3	284.8	267.4	230.1	250.7	136.3	64.3	1,920.0
Sto Domingo	1976 - 85	28.6	14.6			· .				232.7	1 A 2			1,453.7
Kasibu	1978 - 85	52.5	44.4	86.0	189.8	260.1	221.3	223.1	234.9	259.6	555.6	398.4	132.1	2,657.8
Kamamasi	1978 - 85	183.1	55.5 3	111.5	158.7	279.0	187.7	325.4	216.4	401.2	521.3	505.7	306.7	3,252.2
Alayan	1978 - 85	112.1	42.4	60.1	191.4	229.6	170.4	253.8	200.3	375.2	535.9	475.1	268.3	2,914.6
Packet	1979 - 84	45.4	30.5	75.2	126.2	261.3	171.9	259.5	187.3	335.8	231.5	277.7	201.8	2,204.1

(to be continued)

HY-44

(Continuation)

Mean air temperature (°C)

Station	Period	Jan.	Feb.	Mar.	Ápr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	Mean
Aparri	1951 - 85	23.1	23.8	25.3	27.1	28.3	28.5	28.3	27.9	27.6	26.8	25.4	23.8	26.3
Tuguegarao	1951 - 83	23.1	24.1	26.1	28.2	29.0	28.6	28.0	27.7	27.3	26.3	24.8	23.5	26.4
Echague	1981 - 84	21.5	22.7	24.5	26.1	26.9	27.6	26.8	26.6	26.3	25.3	24.2	22.2	25.1

Mean max air temperature (°C)

Station	Period	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	itean
Aparri	1951 - 85	26.3	27.6	29.6	31.6	33.3	33.5	32.9	32.4	31.6	30.2	28.3	26.8	30.3
Tuguegarao	1951 - 83	29.2	31.2	33.8	35.9	36.8	35.7	34.9	34.2	33.6	32.2	30.1	28.3	33.0
Malasin	1976 - 80	27.2	27.4	30.2	32.8	32.9	31.9	31.5	31.3	30.9	29.0	27.0	26.0	30.0
San Isidro	1976 - 80	27.3	28.2	30.6	33.1	33.0	31.9	31.7	31.6	31.3	29.2	27.3	26.2	30.1
Lagawe	1981 - 84	29.1	29.0	28.9	28.8	29.7	30.2	29.7	29.9	29.7	29.7	29.6	28.4	29.4
Hapid	1981 - 84	23.7	24.6	25.7	27.3	28.5	28.2	27.7	26.8	28.2	26.7	25.5	23.0	26.3
Baretbet	1981 - 84	26.1	28.2	31.2	31.0	30.1	29.9	29.1	28.8	29.8	28.4	27.8	25.9	28.9
Consuelo	1981 - 84	25.5	28.7	30.3	30.9	31.7	31.1	29.2	27.6	28.6	27.4	27.1	24.8	28.6
Sto Domingo	1981 ~ 84	27.7	29.1	28.9	31.0	32.2	32.7	31.9	30.1	30.0	29.4	30.1	27.2	30.0

Mean min air temperature (°C)

Station	Period	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	$0 \operatorname{ct}$	Nov.	Dec.	Mean
Aparri	1951 - 85	20.4	20.7	22.0	23.6	24.5	24.9	24.8	24.6	24.3	23.8	22.8	21.4	23.2
Tuguegarao	1951 - 83	19.3	19.4	20.9	22.6	23.7	23.8	23.6	23.6	23.3	22.5	21.6	20.3	22.1
Malasin	1976 - 80	21.8	21.9	23.6	24.6	24.8	25.3	25.1	25.3	25.4	24.7	23.2	22.3	24.0
San Isidro	1976 - 80	21.3	21.1	23.0	24.9	25.4	25.7	25.6	25.5	24.6	24.1	22.8	21.6	23.8
Lagawe	1981 - 84	20.5	19.0	2210	21.7	21.2	22.1	20.6	21.8	21.5	21.8	22,0	21.1	21.3
Hapid	1981 - 84	21.2	20.5	21.1	22.7	23.3	24.1	23.8	23.2	23.0	23.4	22.0	20.5	22.4
Baretbet	1981 - 84	21.7	23.1	23.3	24.3	24.5	24.4	24.2	24.8	25.0	24.0	23.8	22.5	23.8
Consuelo	1981 - 84	20.4	21.5	23.7	24.2	25.4	25.2	24.0	23.4	23.6	22.9	22.0	21.1	23.1
Sto Domingo	1981 - 84	19.6	20.1	19.5	20.2	22.2	22.0	21.2	20.4	20.1	18.7	19.1	18.9	20.2

Relative humidity (%)

Station	Period	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov,	Dec.	Mean
Aparri	1951 - 85	85	83	82	81	80	80	81	83	84	84	86	87	83
Tuguegarao	1949 - 85	81	76	72	68	69	73	75	78	79	80	83	83	76
Echague	1981 - 84	88	86	81	79	83	84	84	87	86	85	90	92	85
Malasin	1976 - 80	85	81	78	70	72	80	81	80	85	83	88	86	81
San Isidro	1976 - 80	86	82	78	74	73	80	82	81	83	86	90	88	82

(to be continued)

(Continuation)

Daily evaporation, A-pan (nm)

Station	Period	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	Mean
Tuguegarao	1974 - 85	2.6	4.2	5.2	5.8	5.8	5.2	5.1	4.2	3.3	3.3	2.6	2.0	4.1
Alimanao reservoir	1957 - 67	4.9	5.5	6.6	7.8	7.5	6.4	6.0	5.5	5.8	5.3	4.5	4.4	5.9
Talictic (Baligatan)	1957 - 84	3.7	4.6	6.0	7.3	7.1	6.1	5.6	5.1	5.1	4.6	3.7	3.3	5.2
Bontoc	1969 - 74	3.9	4.4	4.2	4.3	3.0	3.5	2.5	3.1	3.6	3.2	2.9	3.0	3.5
Echague	1977 - 85	3.0	3.9	5.3	5.6	5.4	4.7	4.8	4.2	4.3	3.5	3.2	2.9	4.2
Lagawe	1980 - 83	3.9	3.7	4.3	5.4	5.7	4.8	4.9	5.7	4.9	6.4	5.5	3.9	4.9
Consuelo	1980 - 84	3.5	4.6	5.2	6.0	6.1	5.4	5.1	3.7	4.7	3.3	3.3	3.1	4.5
Sto Domingo	1979 - 84	4.3	5.3	6.3	7.3	6.3	6.4	5.8	5.6	6.0	5.3	4.7	4.7	5.7
Baretbet	1980 - 84	3.4	3.3	5.7	6.2	6.2	5.8	5.6	5.3	5.0	4.3	3.6	3.2	4.8
Wacal	1980 - 84	3.0	4.2	5.2	5.6	5.8	6.6	5.7	5.4	4.8	4.7	3.5	3.0	4.8
Malasin	1976 - 80	3.5	4.4	6.2	8.3	7.5	6.2	6.0	5.5	4.3	3.8	3.1	2.6	5.1
San Isidro	1976 - 80	3.5	4.4	5.8	7.3	7.1	6.4	6.1	5.4	4.9	3.8	3.1	2.6	5.0
										÷	÷	• •	· · · ·	1
Wind speed (km/hr)					. • •				1 - E.	÷.,	1.4	1) 	· · · ·
Station	Period	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	Mean
Aparri	1951 - 85	12	10	10	10	8	8	9	8	8	11	14	12	10
Tuguegarao	1958 - 85	5	4	5	5	5	5	5	-4	4	5	5	5	5
												1 1 L		
<u>Daily sunshi</u>	ne duration	(hr)								· . ·	۰.	an a		· · ·
Station	Period	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	Mean
Tuguegarao	1978 - 85	4.4	6.5	7.4	8.0	7.5	7.8	6.8	5.2	6.0	4.7	3.6	2.7	5.9
Echague	1981 - 84	2.2	5.6	6.1	6,8	6.7	6.4	5.9	3.9	5.0	3.8	.3.3	1.8	4.8
														· .

Table 3.1

Selection of Runoff Gauge for Tank Model

$\frac{/1}{Runoff}$	Stream	Drainage Area	Selection	Reason for
Gauge		(km ²)	Dercotron	Selection
Palattao	Cagayan	6,626		.appropriate
Pangal	Cagayan	4,244		drainage area
Panang	Cagayan	2,392		.long record period
Guinalvin	Addalam	921	Selected	
Dippadiw	Cagayan	2,380		
Oscariz	Magat	4,150		.appropriate
Dulao	Alimit	573	Selected	drainage area
Hapid	Ibulao	606		.less missing
Camandag	Cadaclan	261		2
	Matuno	558	·	
Bato	Magat	1,649	·	
Malalam	Ilagan	3,123		.appropriate
Minanga	Ilagan	1,565	Selected	drainage area
Dipalin	Disabungan	198		
Calaoagan	Dummon	308		.appropriate
Calantac	Paret	907		drainage area
Larion Alto		655	Selected	.long record period
Antagan	Tumauini	170		• •
Ampawilen	Chico	751	Selected	.appropriate
Taed	Chico	391		drainage area
Supang	Sabangan	57		.less missing
Escolta	Matalag	655	· · · · · · · · · · · · · · · · · · ·	.less missing
Pinukpuk	Saltan	856	Selected	
	Runoff Gauge Palattao Pangal Panang Guinalvin Dippadiw Oscariz Dulao Hapid Camandag Bante Bato Malalam Minanga Dipalin Calaoagan Calantac Larion Alto Antagan Ampawilen Taed Supang	RunoffStreamGaugePalattaoCagayanPangalCagayanPanangCagayanGuinalvinAddalamDippadiwCagayanOscarizMagatDulaoAlimitHapidIbulaoCamandagCadaclanBanteMatunoBatoMagatMalalamIlaganDipalinDisabunganCalaoaganDummonCalantacParetLarionAltoAntaganTuguegaraoAntaganSabanganEscoltaMatalag	RunoffStreamArea (km²)PalattaoCagayan6,626PangalCagayan4,244PanangCagayan2,392GuinalvinAddalam921DippadiwCagayan2,380OscarizMagat4,150DulaoAlimit573HapidIbulao606CamandagCadaclan261BanteMatuno558BatoMagat1,649MalalamIlagan3,123MinangaIlagan1,565DipalinDisabungan198CalaoaganDummon308CalaoaganTuguegarao655AntaganTuguegarao655AntaganChico391SupangSabangan57EscoltaMatalag655	Runoff GaugeStream (km2)Area (km2)SelectionPalattao Pangal Cagayan Cagayan DippadiwCagayan Calaclan Calanada Calantac Calantac Calantac Calantac Calantac Calantac Calantac Calantac Calantac Calantac Calantac Calantac Calantac Calantac

Note; <u>/1</u>: Runoffs at these gauges are examined by double mass curve and runoff coefficient, and judged to be reliable.

Table	3.2	
	J . L	

.

		IAUIC	J · 2		10 - 0		N/ALL =======	(117)					
* 51	ATION		ILAGAN							0	055	2 19	
			ISABEL/						REGION	****	~~ REG	ION 11	
				******			******						******
YEAI	{	JAN	FEE	MAR	APR	MAY	34UL	JUL Y	AUG	SEPT	001	NOV	DEC
196	3 (F)	0.	27.5	Ŭ.	13.2	0.	29.4	180.0	164 4	31.8	42.2	17.5	95.0
	(٢)	0.	54.5	7.	18.7		244.6	67+1	83.9	74.2	77 8	18 7	117.3
	(L)	26.3	31.6	22.8	0	90.8		76.9	191.4	124+4	51.8	61.0	
1964		19.9	14.9	23.8	0.	32.8	79.8	82.1	98.3	71.2	129 2	137.8	42.9
	(٢)	7.5	33.1	21.7	26.1	36.0	88.9	69.7		135.9	34+8	446.1	194.8
	(L)	15.5	63.0	13.8 ა.	10.8	156.1	117.0 63.0	139.6	50.5 34.8	138.5	92.Z 0.	171.8	29.1 16.5
1965	5 (F) (M)	3.8 4.3	C. 2.5	G.	0. 21.1	9.4	27.2	167.6	60.8	16.3	109.7	0.	47.8
	(1.)	0.	С.	0.	28.4	49.3	110.1	0.	35.1		0.		40.4
1966		ŏ.	2.3	5.8	0.	154.7	62.4	60 1	44.4	19.3	67.5	67.3	93.9
	(м)	1.5	0.	ð.	28.4	30.2	95.5	30.5	0.	31.1	53.0	176.2	57.5
	(L)	7.4	8.7	1.5	12.7	98.4	50.8	51.9	48.0	7.4	58.3	382.8	
1967		16.3	15.0	17.7	67.1	0.	76.7	93.C	66.1			101 8	
	(٢)	19.3	27,9	8.1	15.2	12.7	35.2	31.8	39.4	10.3	19+2	20.4	5.0
		20.3	0. 15.5	0. 0.9	34.0	46.9 49.5	221.1	81.9 34.0	46.5 127.2	31 4 29 5	0. 14.0	5.0 9.9	17.2
1968	5 (F) (M)	5.0 12.4	0.	J.	0.	7.1	66.5	69.2	224.8	79.4			
	(1)	1.0	6.3	ΰ.	85.9	16.3		45.4	21.5	126.3	10.8	67.9	
1969		23.4	č.0	ΰ.	29.6	7.1	67.8	18.2		92.5	223.4	5.6	105.9
	(8)	4.8	2.8	54.7	0.	28.2	38.1	1.9	105.8	17.8	43.2	164.1	108.5
	(1)	.0.0	0.0	Û.	0.	96.6	1.0	4.1			7.6	139.9	107.7
1970		79.2	28.0	25.4	22.9	0.	19,2	38.1	124.5	55.9	182 8	114.4	
	(M)	0.	0.	Ũ.	13.2	12.0	97.9	33.0	83.8	112.6	112.0	98.2	147.0
4074		10.7	25.6	14.5 12.7	78.8 C.	5.1 76.0	66.0 99.5	27.9	20.3	33.0 81.8	313.0	79.7	281.9
1971	(F) (∀)	76.1 0.	55.9	181.2	0.	99.6	205.7	199.3		258.4		227.7	101.6
	(1)	51.0	с.	ΰ.	0.	38.1	40.6	-	116 8	18 4	162.6	373.6	124 8
1977		111.7	ö.	ΰ.	٥Č 9	43 1	25.4	96 3	58.5	48.2	35 5		35.6
	(٢)	ο,	15.2	<u>ئ</u>	88.93	139 1	5.1	17.8	15 2	15.8	5 1	0.	7.6
	(1)	37.1	0.	20.3	6.30		106.7		43.2	40.7	17.7	149.8	0.
1973		2.5	7.6	Э.	0.	0		27 9	83.8	15.2	104 1	129.5	127.0
	(M)	0.	0.	15.2	0.		99.1	25.3	127.0	106.6	264 1	254.0	
107/	(1)	12.7	C. 20.3	7.6 J.	0. 12.7	45.7 38.1	102.2	101.6	17.7	0. 58.4	50.5 304.8	357.2	5.1 53.3
1974	(子) (四)	5.1	0.	ö.	5.1	89.8	12.7	96.5	104.1	58.4	279.4	137.2	223.5
	(L)	41.9	2.5	ΰ.	Ċ.	15.2		2.5	0.	63.5	337.8	35.6	
1975		22.8	2.5	J.	10.2	0.	30.4	35.5	45.6	40.6	5.1		132.1
	(M)	7.6	2,5	2.5	с.	55.9	45.7	20.3	2.5	71.1	128.8		66.0
	(L)	48.2	0.	2.5	25.4	99.0	73.7	79.4	38.0		157.5		101.6
1976		76.2	14.9	5.1	63.5	48.2	68.5	25.4		25.4	66 1		35-5
	(٢)	15.2	0.	38.1	25.4	56.2	30.5	6.		149 8	2.5		165 1
1017		7.6	7.6	0.	C 204	177.8 2.5	122.3	81.3 0.	5 1 68.6	17 8 35 5	106.6	266.7	27.9
1977	' (F) (M)	17.8	17.7	0. 7.6	Č,	27.9	2.5	48.2	0.	101.5	20.3	200.6	
	(L)	30.5	5.1	0.	õ.	152.3	38,1	40.6	40.6	119 4		15.2	12.7
1978		2.5	Ο.	ŏ.	7.6	2.5		15.2	106.6	106.6	63.5	20.2	3.3
	(M)	Ο.	2.5	υ.	с.	45.7	12.7	34.3	40.6		27.9	185.4	56.0
	(L)	0.	5.0				12.7			96.5			
1979		3.0	3,4	11.7	14.9	0.	126.3	129.9	25.8	219.4	98 1	90.7	
	(M)	0.	2.0	0.0	15.2	73.8 219.2	20.5	173.9 192.1	109.6	72.5	17.4	26.2 29.2	5.6 19.7
1980	(L) (f)	0. 17.7	8.1 2.5	0.3 25.4	0.	0.	4.2	44.4	5 0	70.8	68.4	279.0	51.8
,,,,,	(٣)	.6.7	10.6	0.	53.4	20.7	0	66.9	23.0	34.2	7.2	44.0	110.6
	(L)	17.8	5.1	12.7	G.	89.7	4.6	55.9	9.8	10.4	231.0	33.8	18.4
1981		9.6	1.1	1.6	C.	6.0	123.8	58.0	87.4	40.2	33.4	130 6	30.2
	(M)	27.8	0.7	1.8	3.8	58.6	94.8	133.6	\$7.2	73.2	36.8		25.4
	(L)	13.6	1.2	U .	16.0	17.2	32.1	0.	29.4		172 0	64.0	8.2
1982		15.0	0.	Û.	25.5	13.6	0.	4.2	48.8	128.0	12 2	40.0	70.4
	(M)	0.	10.8	<u>0</u> .	4.0	.46.4	84.6	30.0	51.2	84.2	73.0	81,2	42.4
1983	(L) 5 (F)	6.4 40.5	С. С.	6.6 13.2	5C.0 49.4	51.2 C.	52.4	1.6 0.	86.4 32.6	0. 21.8	40.2 114.4	35.0	12.0
1403	(M)	60.8 54.8	14.8	0.	49.4 C.	78.6	36.6	40.0	20.4	0.	17.2	50.2	15.0
	(L)	0.	Ċ.	Û.	č.	66.4	20.2	11.2	63.0	105.2		7.6	8 4
1984		· Š . Z	6.2	28.6	0.	111.4		120.4	89.2	24.8		3.2	95.0
	(M)	34.4	3.6	51.6	168.8	54.2	36.0	0.	16+0	3.4	102.0	9.8	13.2
	(L)	3.4	ć.4	45.2	48,2	128.0	183.4	146.4	110.0	7.6	335.2	4.6	41.8
*****			*******		*****		******				~~~~		

	ATION						*244322	(MM) 4995555					
		******				• •		•	CODE A		GSS REC		
YEAR	****	JAN.	FEB	MAR	APR	MAY	JUNE	JULY	AUG	SEPT	007	 ۷ 0 א	- D E C
1963	• • •	0.	24.8	ι.	11.9	• 0.	26.6	162.6	148.7	28.8	38.2	15.8	85.
	(州)	0.	49.03	6.4	16.9	10.7	551.5	60.6	75.9	67.1	70.4	16.9	
1964		23.8 18.0		20.7		82.1	152.9	69.5	.173.1	112.5	46.9	55 1	21
1704	(M)	3.6	13.4	21.5 19.7	0.0 23.6	29.7 27.1	72.2	74.3	9.33	64.3	116.8	124.6	38.
۰.		14.0	57.0			141.1	80.4	03.Ū		122.9	31.5	403.4	176.
1965		8.7	20.0	10.5	19.5	42.7			45.7	125.3	83.4	155.4 41.0	56.
	(M)	10519	0.0	3.8			58.3	82.6	55.0	31.4	50.5	1 2	23.
1044	(L)	69.9	11.7	22.4	45.5	42.2	54.4	162.9	31.8	107.2	5.9	23.0	36.
1966	(F) (M) .	8.5 5.0	7.6		23.5		56.4	54.4	7ć.0	3.8	20.2	85.4	77.
÷.	(L)	12.4	5.2	0.0	8.7	67.7	86.4	27.5	53.5	14.6	14.2	117.5	32.
1967		50.2	.9.8	13.8	26.1	146.8 0.0	45.9 69.4	46.9	102.9	4.2	25.2	258.2	
	(11)	68.5		5.5	31.8	43.2	31.8	50.2 36.0	57.2 81.2	86.4 99.8	141 S 115 4	149.9	60.
	(L) -	22.4	3.2	0.U	32.8	49.8	101.0	149.8	110.6	69.4	8.4	20.7 18.1	·25. 32.
1968	(F)	0.	C.	51.1	с.		122.3	70.1	165.1	135.6	37.9	18.1	0.
	(M)	0.		υ.	0.	8.4	67.1	21.9	185.1	Ο.	41.2	14.5	14,
1040		0.	1:+5	U. U.	369.9	47.2	197.1	170.7	108,8	33.9	19.8	16.7	0.
1707	(M)	18.3	11.9	35.6	21.3 0.	1.3	28.5	24.4	7.9	72.7	5.68	0.8	26.
	(L)	0.	Ċ.	1.3	6.6	6.9	65.5 0.	0. 79.0	11.4 95.2	0.	12.2	0.	45.
1970	(7)	184.4	č.	90.2	21.6	25.9	158.2	0.	21.4	69.9 33.3	1.8 42.9	93.7 57.9	110.
· · ·	(٣)	24.9	C.	Ú.	Ο.	23.6	80.1	54.0	11.2	171.8	288.3	80.5	
	(L) -	0.	6.5	24.9	6.1	62.0	с.	103.4	111.0	26.7	109.2	177.3	C.
1971	(F)	78.3		15.0	С.	107.7		98.5	16.5	181.1	314 6	66 3	27
	(K) (L):	8.4		6.28	3.3	308.1	55.9	164.7	0.		56.2	34.3	57.
1972	(F)	0. 63.2	73.4	11.1 J.	0. 47.8	22.1	33.6	155.2	134.1	95.6	29.9	215.3	73.
1775	(M)	7.9	0.	. č. 9.	35.8	127.6	45.2	118.1 104.4	118.3 212.2	82.5	18.0	96.1	2.
	(L)	68.c	5.3	10.4	C.	96.5	18.5	55.4	10.4	25.2 0.	C. 13.4	10.4	0.
1973	(F)	0.	42.3	ij,	0.	5.1	Ċ.	45.7	48.3		134.9	29.8 29.7	1.
	(2)	0.	G,	0.	0.	101.6	163.1	G.	183.7	9.4	148.2	9.4	14,
1974		2.3	Ç.	69.2	Q.	52.8	8.80	3:52	302.4	59.0	60.5	212.6	о.
1979		14.3 33.3	0.	9.9	.2.	Ç.	69.1	76.6	2.8	77.2	0.	98.4	27,
	(L)	28.0	5.4 Q.	Ú. 1Ű.7	57.7	32.9	161.3	38.6	83.5	с.	177.7	24.9	137
1975	(D)	23.2	G.	14.2	8.7 C.	0. 48.1	37.3 57.7	21.5	34.3	112.0	225:5	94.7	11.
	(8)	107.2	45.0	5.2	ŏ.	12.9	14.0	56.4	5.8	103.4	14 0 85 9	73.7	52.
	(L) .	40.6	4.1	15.9	4,9	64.6	10.5			97	34.2	31.3	130.
1976	(\mathbf{r})	0.	6.2		103.6	133.5	96.5	41.9	117.2		113.2	25.2	19.
	(M)	0.	7.6	30.5		45.2	Ο.	15.0	94.4		51.1	41.4	49.
1977	(1)	0.	16.2	¥,,	0.	316.8		78.8	46.8	95.5	26.9	26.4	8.
1771	(Y)	19.3 27.1	12.0	3.3	60.3	25.9		69.4	162.0	52.4	35.9	29.6	13.8
	(L)	.38.2	.0.	13.5	С.З Л.	12.9 246.9	75.2	76.2	25.6	109.2	29.5	168.3	2.
1978	(1)	2.6	3.1	3.4	16.0	6,1	4C.9 δ4.0	2.5	20.5	26.6 59.5	2.0	34.8	
	(٢)	0.	5.3	17,5	30.0	0	77 3	75.0	19.8	128.9	112.1 65.8	112.0	31.
• •	(L)	1.3	28.5	2.0	102.6	126.6	23.1	\$5.3	236 2	125.7	207.4	9.9	15. 53.
1979	(F)	22.6	с.	19.3		5.4	214.6	57.7	100.6	75.2	175.0	\$3.0	17.
	()	0.5	с.	3.6	25.5	153.8	28.7	50.5	61.2	66.1	70.6	69.9	4.0
1980	(L) (T)	8.7 0.	C. 11.7	10.8	120.0	80.6	115.3	105.4	16.0	137.3	13.8	73.2	32.3
.,		0.	23.2	25.9 5.3	. C. 89.1	5.1	0.0	50.0 116.9	94.4	-39.9	47.9	241.5	12.4
	(L)	ò.		151.6	2.0		24.1	74.7	22.3 60.1	123.3	05.9	29.0	42.
1981	(1)	7.0	22.3	0.0	0.0	7.5		159.4	113.6	52.5 158.2	255.2	18.3 54.9	2.1
	(8)	4.5	4.1	0.0	48.6	134.7	-	243.2	59.6	100.6	30.8	33.6	6.9 1.4
	(L)	10.2	16.8	U.O	193.2	296.1		59.0	8,9	56.0	213.7	87.1	9.5
1982		4.0	0.0	26.3	71.0	28.7	51.6	57.2	63.0	101,4	4,5	55.7	29
•	(₩) (()	11.3	C.S	29.6	128.2	46.9		130.1	12.7	62,8	75.0	23.0	6.0
1983	(L) (F)		0.0	144.0	90.8	267.1	55.5	73.4	173.5	38.0	3.0	41.8	15.9
	(M)	30.2	0.0	0.0 ŭ.0	9.4 0.0	2.1 49.6	14 5	26.0	61.2	3.5	63.6	1.9	0,0
Ε.	(L)	8.3	0.0		0.0	14.8	54.6	49.4 29.5	45.5 39.0	27.6	81.5	4.9	7.1
1984		0.0		20.7		209.7		114.5	59.6	153.2 0.0	165.3 26.8	1.4	1.9
	(M)	2.1	C.C.	109.2		45.6	99.7	97.2	65.2	51.0	20.0 82.3	3.2. 2.6	59.5 0.0
	(L)	7.8	2.6	7.1		112.5	23.1		110.0	20.1	262.9	12.6	4.0

Continuation

				2 % E #	10 - 0		SESSES NFALL		122 2				
				ARAQ			******		CODE N REGION		055 REG		an th Attack an an
* DIS ********* YEAR		 JAN	CAGAYA FEB	*AR	APR	MAY	JUNE	JULY	AUG	SEPT	0CT	NOV	0 E C
										نه ده دو ب به بر			
1963	(f) (K)	0.5	0. 10.1	0. 1.6	C. 1.0	1.0 C.3	18.1	110.4	20+8 23+5	66 1 122 6	0.10.6		139.5
	(L)	0.	2.3	4.3	0.	6.4	114.5	33.2	10.9	59.5	5.1	14.6	0.8
1964	(1)	4.8	с.	35.5	0.3	18.5	65.9	29.8	323.5	99.0		155.0	52.4
	(#)	0.	3.3	1.0	4.1	1.3	56.7	75.4	100.9	10.8		444.4	65.1
10/1	(L)	0.	41.0	0. 1.8	2.7	58.6 15.7	34.4	81.2	23.2	71.4	54-8 0-	359.4 98.7	3.8
1965	(F) (M)	4.6 10.3	0.	Ð.	0.0	3.0	65.6	358.0	67.9	3.9	70.5	4.9	9.7
	(L)	20.7	ο.	7.2	9.2	107.7	47.4	57.6		111.3	3.1	22.4	4.9
1966	(1)	0.	7.9	9.2	4.1	153.3	64.1	24.4	70.9	12.0	7.1	74.4	48.7
	(*)	1:5	C.S 12.7	1.3	32.1	56.9 197.7	29.2 59.2	115.8 66.9	117.1	31.3 0.		117.3	43.2
1967	(L) (F)	3.6	· · · ·	3.9	225.1	0.	62.5	00.7 G.	5.83	55.4		101.9	4.6
	(8).	3.8	2.6	J.	8.1	36.0	0.	0.	147.1	36 1	337.9		1.5
	(L)	6.4	Ç.	J.	5.6	38.1			226.9	17+7	1.5	7.9	
1968	(1)	7.9	C. 1,1	8.9 0.	0. 21.4	25.9 6.4	82.8 64.5	25.2	162.3	32.2	25.7 9.9	1.3 11.2	0.3
	(M) (L)	0.3 0.	C.		53.9		56.5	106.8	56.8	290.9	2.9	5.9	0.
1969	(1)	0.8	Ő.	ΰ.	51.6	Ğ.	138.7	133.5	28.6	73.1	79 1	5.2	30.9
	(#)	0.	0.	1.5	0.	29.4	25.22	30.7	2.6	64.4	3.2	150.4	29.9
4070	(L)	0.	0.	,) ,	1.3	54.0	0.	353.3	40.1	65.3 38,5	13.2 49.9	31.9	7.7
1970	(f) (8)	41.4	0. 0.	11.1	4.1 6.5	96.2 47.4	71.7 17.9	156.8	44.7	49.6	122.4	69.0	
	(L)	3.0	1.8	123.6	24.2	42.1	1.6	9.6	72.7	76.6	261.2	79.3	
1971	(F)	5.5	8.1	6.	0.	39.5	83.6	60.4	28.2	36.6	303.7	179.9	113.8
	(4)	0.8	38.8	9.3	10.0	35.6	53.1	209.8		114.3	127+3	190-2	70.0
1972	(L) (f)	0.5 52.7	0. 4.8	1.0 3.1	0.	27.4	9.1 79.1	42.3	1.0 55.7	91.3 86.5	136_4 0	483.1	36.7 24.3
1712	(#)	0.	5.1	28.7	14.5	5.38	14.7	62.1	69.3	5.0	0		
	(1)	27.4	C.3	4.5	10.7	21.3	77.8	90.3	92.6	59.4	26.2	55.6	9.6
1973	(f)	8.8	7.1	0.	0.	44.2	27.5	25.2	92.7 52.3	28.6 35.5	147.6 281.4	47.8	53.1 2.6
	(M). (L)	0. 6.6	с. 0.3	0. 25.7	0. 0.	12.5	42.7	16.7	131.3	20.1	63,7	538.9	2.2
1974	(1)	0.	1,5	Ű.	10.1	51.7	108.5	20.5	46.5	16.5	199,1	320.4	19.3
	(٢)	۵.	С.3	û.	7.1	14.2	12.2	20.5	67.0	100.5	90,8	160.3	98.5
	(1)	.3.5	C.	Õ.	37.3	29.7	29.2 33.3	18.3	31.2	139.9	208.0 199.1	11.5	38.0 13.1
1975	(f) (M)	0. 0.	C. G.	Ū. 7.6	С. С.	50.0 27.2	82.5	26.5	28.8	38.9	90.8	34.4	56.5
	(1)	0.	č.	24.0	c.	3.33	34.8	4.5	118.4	4.6	207.6	1.3	
1976	°(F)	12.5	0.5	2.8	48.7	δ.1	18.3	7.1	53.6	0.5	42.1	125,8	2.5
		7.6	C.	4.0	0.	41.4	112.3	0.5	39.8	98.5	19.0	131.8	39.0
1977	(L) (F)	4.9 6.1	0.5	35.0 0.1	0. 6.5	133.8	78÷6 52.8	93.0 37.2	97.1 98.4	8.6 162.0	153.5 38.1	20.3 29.4	13.2
1991	(4)	3.1	1.1	0.2	0.	3.5	44.0	46.6	46.8		21.2	108.9	4 C
	(L)	9.0	C .	1.0	12:5	70.8	31.8	265.8	42.6	107.2	0.9	10.0	11.8
1978	(F) (N)	0.	1.6	2.2	0.4	Ç	51.1	1.8		58.7	75.4	47.8	32.2
	(א) (L)	0. 2.8	4.8 2.1	10.C 8.5	41.6 31.0	6.6 127.4	. 0. 21.5	97.6	267.2	122.0	46.0 158.4	137.9	57.0 10.0
1979	(F)	2.2	10.4	4.0	5.0	6.8	18.9	198.3	24.2	53.6	179.4	141.2	1.0
	(8)	1.4	5.9	0.	10.2	85.0		55.1	49.4	31.0	104.5	45.5	4.7
10 d 0	(1)	6.0	0.	0.	29.9	65.3	13.2	58.1	5.8	29.4	1.8	17.1	66.3
1980	(M) (L)	0. 0.	2.5 26.5	1.0 0.	C. 18.2	C. 134.4	3.8	122.3	35.8 80.4	36.4 65.0	38.1 17.0	180.8	22.5 60.6
	(1)	ο.	Ċ.	53.3	0,	8.15	12.7	134.9	23.9		277.9	13.3	9.0
1981	(F)	0.4	1.2	0.4	0.	2.0	112.0	21.4	171+1	6.8	80.0	195.5	4.8
	(*)	3.6	8.0	3.6	1.0		133.0	11.0	97.2	159.6	66.6	17.0	3.6
1982	(L) (F)	1.0 3.0	1.4 C.2	1.0	0,02 28,8	127.8	29.6 49.2	1.0 14.4	22.0	0. 79.2	124.2	69.4 34.2	30 812
1764	(8)	3.8	3.3	0.	45.8	96,8	8.0	14.0	38.0	52.7	173.5	129.0	10.4
	(1)	1.6	0.	Ů.	9.6	51.4	25.2	30,3	84.0	65.9	0.4	98 2	22.6
1983	(F)	17.2	С.	6.2	7.6	6.	4.6	с.		156.2	151.8	6.4	1.0
	(⊬) (į)	48.0 3.2	1.4	. 3 . 4	с. 0.	34.C 26.8	30.4	21.4	22.9	1.4 30.2	61.0 123.4	7.8 41.6	3.0
1984	·(f)	3.2 0.	0.	6.6	0.	58.1	18.0	24.0	117,5	10.4	14.7	8.4	0.2
	(E)	õ.	ċ.	2.1	46.6	19.3	44.8	29.2	33.4	0.	0.4	53,0	Ο.
	(L)	0.	0.	Ú.Ż	67.2	113,0	117.2	51.4	422.2	6.7	187,6	18.8	0.
					******			******					********

Continuation

.

þ

	TION. TRICT	*****	BONTOC	IN					CCDE N REGION	ب ه بد ده		1 21 10N I	
YEAR	هه نان ويو سه مه	JAN	FEB	PAR	APR	MAY	JUNE	JULY	AUG	SEPT	OCT	NOV	DEC
1963	18)	0.		0.		0.	142.3	203.4	104.9	79.5	0.	0.	21.
	(M)	0.	9.6	ΰ.	0.	145.3	68.3	191.8	105.7	62.7	0.	34.3	63.
	(L)	0.	5.1	14.0		81.7	190.2	111.0	81.3	69.8	0.	73.6	88.9
1964	-(F) -(M)-	0. 0.	0. 0.	5*0	0. 8.8	99.4 48.7	104.7	70.2	297.2 147.0	158.2	206.4	70.0	12.0
	(1)	0.	0.	0. 29.5		134.9	177.5	98.3	58.5	100.8 50.8	30.2 12.9	111.3	206.
1965	(F)	ŏ.	Č.	0.	59.4	112.1	120.6	64.7	8.9	74.5	8.6	7.3	ò.
	(4)	11.4	0.	3.8	24.1	96.7	91.4	195.2	106.9	8.7	7.1	0.	31.
	(E)	13.2	0.	26.6	139.0	113.2	34.3	296.3	59.5	72.1	73.7	4.3	7.
1966	(F)	1.0	2.5	12.5	10.2	81.47	114.3	44.5	227.8	74.2	23.1	17.2	129.
	(M) (L)	0. 2.8	9.4 5.8	1.0 16.2	24.9 118.9	145.9 168.8	24.5 53.4	55.9 96.8	104.4	1G.2 0.	48.1 86.1	56.9 313.8	3. 6.
1967	(1)	1.8	Ċ.	10.2	7.3	0.	120.9	13.0	157.2	128.6	146.1	301.8	1.
	(2)	7.1	0.	. Ö,	0.5	107.5	51.4		144.5	139.1	273.0	0.	0.
	ŝ	6.1	0.	0.	70.1	26.7	185.4	453.5	267.3	260.5	0.	0.	0.
1968	(F)	1.3	C.	37.6	3.1	56.9	96.8	72.3	111.1	207.2	67.3	- 3.8	0.
	(8)	.0,	0.	31.3	49.0	197.8 65.8	225.1	160.2	219.2	134.4	25.4	0. 47.3	0.
1969	(L) (F)	13.2	0. 0.	62.8 0.	59.1	89.4	189.0	131.8	76.3	69.5	75.2		0. 15.
	(M)	9.2	Ċ.	15.2	81.8	111.4	96.3	167.5	76.4	61.2	3.0	11.4	2.
	(L)	0.	С.	U.	3.0	124.9	35.8	821.1	85.8	62.1	12.6	89.1	15.
1970	-(1)	97.7	0.	12.7	28.7	169.0	162.0	32.2	78.3.		168.0	100.6	41.
	(M) (L)	0.	0. 4.8	0. 73.4	0. 138.1	140.9 140.3	157.8 39.1	93.3	189.9	266.7 72.6	154 8 175 3	72.0 14.5	31.
1971	(E)	34.7	3.6	.0.	22.8	21.0		81.4	55.1	92.9	303.4	50.0	1.
••••	(M)	0.	49.1	11.0	0.	34.0	82.9	225.1	100.8	64.0	53.6	47.9	9.
5	(L)	0.	6.4	49.5	17.7	77.4	44.9	180.6	131.1	186.4	35.4	99.6	29.
1972	(F)	9.7	0.	1.8	23.8	155.5	189,1	120.0	39.6	24.4	0.7	18.8	55.
· •	(M). (L)	0.	0.	25.1	131.4 88.5	80.1 175.7	57.1 71.6	390.6 201.9	66.1 60.8	21.8	1.6 1.2	3.8	1.
1973	(4)	0.	2.3	۰ <u>۵</u> ,	32.6	207.5	53.6	93.7	83.2	194.1	247.2	26.9	11.
	(M).	٥.	1.5	2.3	3.8	171.0	33.4	78.4	104.3	73.9	243.1	25.7	1.
107/	(1)	0.	Ç.	Ş.1	75.2	92.5	78.3	55.6	98.3	67.4	16.3	189.0	- ş.
1974	(F) (M)	1.8 0.8	°G. 5.1	0. 0.	82.6 49.6	43.9 39.3	233.0	47.4 85.4	\$6.5 186.7	48.5 27.0	65.3 352.0	274.3	1. 92.
	(L)	20.5	0.	22.3	187.1	106.0	16.2	120.7	166.5	117.6	215.0	30.5	12
1975	(1)	0.	č.	25.9	79.4	220.2	119.7	91.1	87.4	187.1	62.4	44.9	24.
	(K)	0.	4.3	2.5	0.	48.5	94.7	133.4	60,1	95.1	5Z.S	4.4	50°
	(1)	13.7	с.	5.1	13.3	77.7	11.7	93.6	129.6	0.1	46.7	2.5	55*
1976	(F) (M)	7.1	0. 0.	8.8 0.55	45.4	42.7 33.0	23.1 224.9	120.1	39.5 26.8	80.8 148.1	170.5	21.6	5. ∵18.
	ά	0.	е.	65.4	0.	231.2	278.9	113.3	79.0	88.1	7. 6	3,3	0.
1977	(E)	2.5	Ö.	0.	493	G.	70.2	150.5	165.2	66.8	38.8	17.0	ō.
	(٢)	12.7	C,	Ŭ.	. 77.8	8.6	74.6	122.9	20.0	399.6	18.2	186.2	0.
1070	(L) (F)	7.8	0.	26.1	0.		-106.5	146.7	78.5	-64,1 1/5 (1	1.0	0.	0.
1978	(E) '(M)	0.	0.	17.3	24.6	47.2	31.3	193.5	0.	145.9	0. 0.	0 75.9	0. 21.
	(L)	0.	0.	41.4	31.7	90.2	39.4	144.3	11.4	240.5	7.1	0.	0
1979	(1).	5 8	0.6	28.0	.0.	67.6	167.5		54.9	47.6	36.0	25.1	10
	(M)	1.0	0.0	0.4	10.6	73.1	19.6	94.9	11.2	25.9	78.8	42.2	25.
*	(L)	11.6	1.4	0.0	159.0	42.2	67.0	78.3	3.6	30.7	27.4	59.3	38.
1980	(F) (M)	4.1 0.	0. C.	21.4	0. 18.8	270.2	6.9	147.3	45.5 87.5	37.2	37.8	171.9	13.
• •	(1)	27.9	0.	21.0	35.8	150.6	1.3	331.0	101.7	57.2	261.2	12.6	0.
	(F)	6.4	Ö.	Ū.	C.	43.2	248.9	104.1	53.5	42.9	58.3	185.9	õ,
	(M)	2.0	Ο.	Ο.		197.7	146.3	42.3	72.8	176.0	7.1	16.2	Ο.
· .		Ŭ •	C.	0.	7 • 4	133.5	55.3	34.3	70.1	0.	91.2	66.0	5.
	(F) (K)	0.	с. З.С	0.	43.2	56.2	37.9	83.8 J.	91.0	193.0	0. 9/1	68.6 55.9	53.
сі і і і 1	- (£) ∋(L)	0. 0.	5.0 0.	0. 46.5	61.3	50.2 50.3	124.5	0. 82.3	120.9	50.8 201.5	94.1	55.9 12.2	. 65 18.
1983	(F) -	10.2	0	15.5	18.3	13.7	33.1	38.1	88.1	35.8	75.4	0.	0.
	(*)	17.0	20.0	υ.	C.	25.4	59.5	94.5	83.2	43.8	111.8	23.0	Õ.
1. a.e. e.	(É/) -	0.	C.	Ü.	0.	128.0	27.4	242.2	70.2	17+8	44.9	1.8	2
1984	(f) (M)	0.	: 0. 0.	0. 110.8:	<u> </u> .	55.3 18.4	58.2	66.8	111.7	0.	14.0	δ.	98.
					70.5		39.4	44.5	31.8	64.4	0.4	50.4	σ.

Continuation

- TC - DAY RAINFALL (MM) =

				# 2 = 1 = 1			INFALL ¤×=¤¤¤¤:	(MM) Xereate:	2 222	··			
	ATION STRICT		TUAO CAGAYA				*******		* CODE N • REGIO			52 07 510N 11	
YEAR		JAN	fEb	MAR	APR	MAY	JUNE	JUEY	AUG	SEPT	OCT	NOV	DEC
1963	(1)	1.1	12.8	U.	C . 5	0.5	65.8	166.8	43.4	58.2	19.2	3.8	101.7
	(M)	11.5	34.8	Ú.	11.7	41.1	155.9	112.6	22.2		14.7	<u>0</u> .	
10//	(L)	0.8	8.1	7.6	Ç.	20.3	162.8	1.3	41.4	32.8	12.0	9.7	3.6
1964	(T) (K)	9.9	1.C 3.6	89.4	4.6	5·1 2+6	8.63 0.58	34-2	180.4	68.0	115.5		32.2
	(L)	θ.	8.0	0.	0.3	75.9	52.1	82.8	80.3 78,5	84.7 107.4	47.4 73.9	437.5	52.9
1965	(F)	ŭ.3	17.8	4.2	Ŭ.	195.0	78.3	28.2		207.7	0.	72.4	11.1.8
	(٢)	26.9	с.	ŭ.3	10.9	0.8	97.6	198.9	52.4	14.0	51.1	1.3	10.0
	(L)	12.6	5 - 1	5.9	117.7	96.4	24.7	185.2		35.0	3.1	39.9	17.3
1966	(F)	1.0	1.3	20.6	5.9	80.3	50.9	56.0	15.5	22.2	28.0	87.5	17.0
	(M) (L)	0. 0.6	5.7 2.0	ŭ. 1.3	117 9	108+1	32.1	79.4	105.6	55.3	59.2	113.4	30.0
1967	(F)	-3,3	0.8	0.9	124.8	0.	55.1 124.0	111.1	110 . 7 78.7	13.3 50.4	.89.2 238.2	340.9	85.0
	(4)	3.7	4.3	2.8	Ū.8	53.9	0.6	6.2	126.7	82.9	225.4	104.0	30.7 3.1
	(1)	4.6	1.0	ù.	46.1	51.6	224.9	106.6	99.9		2.3	24.1	9.1
1968	(F)	31.5	5.6	4.1	С.	17.3	68.9	54.0	181.4	44.1	1.5	0.	
	(*)	. 1.3	2.8	ί.	23.9		55.4	23.1	291.9	0.5	31.0	1.3	0.5
10/0	(L)	Q.	0.	1.3	59.3	71.1	37.4		40.7	219.8	13.1	4.3	0.2
1969	(F) (P)	2.8	1,5	J.	55.8	1.0	106.1	136.1	21.8	102.8	113.1	14.7	
	(L)	7.1 0.	с.	3.0 C.	G. 1.5	68.4 30.7	32,5	31.3	Ç.	72.5	24.9	61.4	22.7
1970	(F)	48.9	4.5	33	17.3	44.4	0. 60.2	360.1	11.9	53.6 52.9	11.6 74.6	72.7	19±0 43±4
	(™)	2.6	0	J.	2 8	174.5	20.7	50.8	49.2		113.2	139.8	89.6
	(L)	2.3	Ċ.	35.7	21.3	92.4	2.8	38.4	125.0	41.5	173.0	64.5	21.1
1971	(1)	29.7	11.3	3.8	Ο.	61.0	140.0	52.2	13.3	84.9	294.8	106.0	76.3
	(M)	6.4	39.8	31.8	0	34.2	31.4	174.4	73.8		98.8	63,2	82.5
1972	(L)	1.5	4.3	c • 5	0.	17.7	29.3	39.6	3.3	45.1	55.6		29.5
1972	(F) (%)	47.0	1.5 2.0	6.6 34.1	5.6 20.8	64.3	42.4	93.8	82.9	30.4	6.9	54.9	38.0
	(L).	11.8	4.4	14.5	20.8	76.7	24.6	102.7	140.2	14.8 32.9	0.2	0	1.5
1973	(ii)	13.0	11.4	U.	1.0	, C.,	96.9	72.2	107.5	98.5	13.6	54 8 59 4	3.3 56.0
	(٢)	12.7	6.	J.	C	34.5	181,2		63.8	40.6	317.2	109.2	9.8
	(L)	4.8	1.8	20.4	3.6	22.3	37.6	53.7	216.0	39.3	40.9	399.5	14.7
1974	(1)	6.9	3.8	J.S	7.8	94.1	64.2	3.3	61.9	1.6	183.8	247.9	26.1
	(M) (L)	8.0	C.5	2.0	11.2	41-1	. 6.9	31.8	138.3	89.7	78.0	134.1	122,6
1975	(F)	14+2 10+3	2.2 0.	ປ. ປີ	75.0 43.6	96.8 115.6	15.2 93.4	7.1 98.3	29.6	137.4	212.2	17.0	34.4
	(M)	5.5	2.6	3.7	0.	43.5	169.4	55.9	88.5 32.0	5.0 36.3	28.4 73.5	15.2	15.2
	(L)	29.0	1.0	2 J C	3.0	92.2	24.0		214.9	. 0.	293.8	22.5	43.2 78.0
1976	(F)	30.7	1.0	24.6	11.9	14.7	52.5	71.3	50.6	12.2	96.2	95.5	50 1
	(⊵)	12.1	0.5	15.2	0.	54.3	82.8	Ο.	56.1	72.9	3.6	132 7	17.0
	(L)	12.0	1.3	20.0	0.	162.0	119.6	130.8	134.1	19.9	92.0	73.8	9.6
1977	(₹) (∀)	14.2	3.1	1.5	9.6	0.	44.9	13.4	161.4	70.8	1.2	27.6	8.0
	(t)	12.9	3.4	1.5 10.0	2.2 0.	14.7 93.0	103.9	36.1	9.5	135.5	7.6	92.7	1.8
1978	(1)	9.4	ί.ε	3.3	6.	19.6	52.0	200.0	34.5 87.7	99.6 112.3	5.9 195.5	13.1	12.4
	(*)	3.0	2.0	23.4	15.5	47.7	58,9	168,9			59.9	18.1	36.0 52.8
	(1)	0.2	2.5	2.3	21.6	100.4	27.5	56.1	282.8	87.0	129.7	6.6	15.1
1979	(1)	1.5	35.1	3.0	11.9	6.9	7.6	104.0	30.4	96.5	114.0	117 1	5.7
	(*)	0.8	C.4	ຸວ.	16.3	86.6	4.9	66.0	8.9	41.8	105.5	70.7	19.5
1920	(L) (D)	0.2	0. 1./	Ú. 15 4	26.7	66.6	29.7	93.2	4.3	14.1	3.1	28.7	83.2
1700	(F) (M)	5.1 5.2	1.4 10.2	15.6 0.7	0. 25:18	5.4 249.6	29.C	118.8	2.2	83.6	25.2	166.2	12.0
•	(1)	17.1	0.	25.2	0.8	39.4	0. 58-2-	93.8 104.0	37.2	40.4 12 A	18.2	51.4	59 4
1981	(7)		6.1	Ů.	ö.	0.8	234.4	-35.4	61.4	12.6	378.9 102.6	9 0 169 2	94 34
	(4)	10,9	C.2	19.3	2.1	99.9	81.8	124.7	166.0	150.1	40.9	31.2	1.5
	(L)	5.2	0.5	U.	42.0	105.8	10.2	6.9	3.5	13.2	112.2	49.8	7.1
1982	(F)	11.9	C.5	Ū.	42.9	10.7	88.2	81.8	25.9	120.7	8.9	10.2	47.9
	(*)	2.7	11,9	Ú.	18.8	111.1	1.3		30,7	50.3	186.0	104.9	39.9
1983	(1)	0.7	с.	Ú.	84.3	164.1	79,9	19.0	131.6	34.7	1.0	109.9	40.7
1767	(F) (M)	3.0 59.5	С. 2.С	1.0	6.1 0.	6. 43.4	23.8	0.	107.8	87.0	115.4	28.7	115.8
	(1)	6.8	C.	33.3	ΰ.	43.4 8.4	61.4	37.6 115.5	44.3	68. <u>3</u>	43.1	7.4	43.1
1984	(1)	5.6		9.2	5.1	114.4	32.3	77.1	38,1 84.7	35.8	106.4	48.1	106.4
									V 1 # 1		ų j	35.6	86.2
	(*)	0.2	с.	0.3	168.1	16.0	126.5	45.5	6.9	2.3	36.8		
	()) (L)	0.2 4.3	C. 5.‡7	0.3 1.3	168.1 84.9	16.0 142.0	126.5	45.5	6.9 321.8	2.3 18.8	36,8 100.2	71.0	0. 3.6

Continuation

.

		*****	APARRI CAGAYA	N	н 			د ب	CODE N REGION	20 - 20 - 20	REG	ION II	
YEAR	· · · · · · · · · · · · · · · · · ·	JAN	FEB		APR		JUNE	JULY		SEPT	ÓCT	NOV	DEC
1963	(F)	46.0	14.0		49.3	1.3		81.6		185.4	19.4	0.	73.4
	(11)		88.9	0.8	0.	0.		87.5	8.2	19.5	56.1	0.	184.4
1964	(L) (F)	74.0	5.6 36.4	·0. 4.0	0.	0. 0.	47.8 36.3	0.3	28.9	29.1	60.0	. 0.	54.3
1704	(M)-	0	13.8	0.5	0.	8.3		1.5	88.5	227.8 27.2	212.0 79.5	420.2	85.8 278.1
	(L)	7.3	7.4	1.2	0.	128.5	9.5	6.9		139.5	113 2		
1965	(F)	139.2	9.1	0.4	0.	42.2	138.7	36.8	53.7	227.3	38	89_2	17,9
	(M)	177.3	0.	18.0	0.	0.	95.6	108.6	44.4		143.9	1.8	46.6
1966	(L) (F)	102.0	0.6	0.5	6.7	71.9	42.0	87.1	14.8	10 5	0.	67.6	78.5
1700	(M)	6.7 0.	7.4	0. 0.1	0. 50.8	126.0	52.1 1.8	1.3	32.4	17.3 205.6	18.1 119.3	174.8 149.3	62.2
	- äõ	6.7	22.6	33.4	0.		12.4	24.8	29.8		200.6	375.4	95.7
1967	(F).	37.5	35.8	31.5	84.6	0.	123.4		121.2	65.8	235.1		123.9
	(H)	54.9	23.5	1.3	0.	3.6	52.8	1.8		151.3	296.8	15.9	91.5
4040	(L)	1.0	7.6	2.0	0.	7.1	244.2	43.6	203.6	139.6	2.8	32.8	87.4
1968	(F) (M)	37.3	14.0 16.8	51.5	0. 0.		48.5	124.0	205.7	44.9	4.0	4.5	0.
	(L)	18.2	14.5	0. 0.	65.1	0.	40.9 76.3	74.5	182.1 20.1	44.3 354.6	74.9	3.3	30.4
1969	(F)		23.5	0	5.2	.0.	67.1	79.5	15.9	249.0	4.3 295.4	25.7 26.2	3.5 97.8
	(M)	28.1	0.	33.4	0.	17.8	62.5	1.1	1 1	94.5	22.1		89.5
	(L)	0.	0.1	0.3	0.	28.1	0.	204.7	0.5	50.1		181.1	30.9
1970	(F)	61.5	26.2	2.3	0.2	18.5	68.7	20.3	64.4	30.8	42.2		
	(M) (L)	186.9	0.9	0.	0.7	65.3	98.1	39.9	56.5	17.5	105.1		.112.6
1971	(7)	20.5	45.6	140.6	40.6 21.5	13.8 13.1	28.9	23.7	97.9 91.9	77.4 10.2	247.3	100.6	3.6
	(8)	0.	57.1	109.4	5.0	0.2	38.3	376.7	66.6	58.4	165.9		49.1
	(L)	153.7	0.	0.	0.	2.5	49.9	16.3	0.	74.9			117.3
1972	(F)	77.7	47.3	58.2	20.1	17.9	31.8		116.3		37.6	56.6	26.0
	(M)	53.6	25.0		11.1	106.8	5.1	91.0	22.3		0.5	13.9	5.7
1973	(L) (F)	4.5	108.1	48.5	0.2 0.1	56.7	26+6	45.1	65.9	116.1		112.0	
1713	(M)	61.5 26.8	-0.2	0. 0.	0.	0. 16.8	27.0 197.5	19_3 38_3	67.7 7.8		229.7	196.7	51.7
	(L)	22.7	0.	36.7	0.	0.	21.3		159.4			580.3 565.3	
1974	(F) '	33.2	37.0	0.	1,6	1.1	25.6	23.3	30.2	14.2	151.4		41.1
	(M)	46.4	4.4	0.9	0.6	2.5	1.6	16.2	175.2	47.9	89.5		79.5
4075	(L)	66+0	25.9	0.	8.0	4.3	0.2	1.1		178.4	228.4	65.5	54.5
1975	(F) (N)	24.9 119.3	36.8 13.3	3.0 4.4	33.0	1.1 49.5	43.2	55.6	53.4	2.7	31.5	15.6	59.7
	(L)	63.0	9.5	10.2	0.5	53.3	61.6	18.9	57.6 105.8	34.8 3.1	148.4 147.7	25.0	79.2 34.6
1976	(F)	5.4	0.4	2.7	3.4	12.8	27.8		110.8	2.1	185.4	57.9 197.0	31.8
	(M)	10.5	0.	0.5	1.3	27.6	7.7	27.1		74 Z	16.5		4.1
	(Ĺ)	1.6	1.6	1,1	0.	93.3	115.8		100.1	110.6	102.0	53.3	54.6
1977	(F)	21.6	17.3	4.0	V BO	0.	44.5	6.5	26.5	58.7	34.7	71.0	7.6
· · ·	(M) (L)	87.9	45.3		6.3	0.	46.7	9+8		159.4		184.5	0.
1978	(F)	41.3 21.3	2.5	0.1 25.8	0. 6.6	36.2 0.	18±9 2.0	222.0		143.9 146.0	22.8 138.5	54.9 50.5	9.5 26.5
	(M)	12.6	67.8	20.1	Ū.	64.7	23.0		103 0	67.0		145.5	64.0
	(L)	0.	21.2	0.6	1,1	95.8	78.5	45.1	157+5	132.7	301.7	44.0	34.7
1979	(F)		72.5	0.	9.5	1.0	11.5	99.5	125.0	28.0	150.0	110.2	1.5
	(M)	1.2	33.7	0.	3.0	188.7	5.0	25.0	284.4	4.5	182.5	141.4	3.0
1980	(L) (D)	1.0:. 2.0	0. 5.0	0.	4.0	34.8 0.		126.5 204.5	C.	44.0	49.5	215.7	61.5
1700	(M)	30.5	3.8	0.	12.6	160.5	0. 0.	160.5	0. 13.2	68.0 153.5	83.5 3.5	65.0 332.0	197.5 126.2
	(L)	48.5	1.1	38.2	0.	10.0	3.5	44.0	24.0	39.0	319.5	52.5	32.0
1981	(F)	42,0	11.0	31.0	0.3	1.5	89.0	28.5	108.0	0.	33.7	63.0	57.0
		13.5	Ο.	3.0	32.5	446.0	212.5		110.8	573.0	12.0	11.0	64.6
4000	(L)	12.0	0.	2,5	5.0	23.5	13.2	0.5	9.0	7.0	76.5	108.5	30.1
1982	(F) (M)	32.1	0. 15.0	0. 0.	77.9	0.	6,5	97°7		. 44.5	45.2	36.0	113.5
· ·	(L)	39.5	0.	1.7	4.0 5.5	4.0 9.2	31.3 157.5	27.0 79.1	48.0 36.5	22.5 18.0	99.5 0.	84.5	228.8
1983	(F)	20.0	0.	10.5	3.5	0.	29.5	0.	0.	221+0	130.1	60.0 106.6	85.8 21.5
	CH)	227.2		35,5	Ο.	2.0	23.0	2.0	68.0	0,	38.8	95.3	67.9
	(L)	117.1	0.	5.0	0.	4.0	37.0	10.0	2.2	59.9	301.1		180.6
1984	(F)	62 5	7.5	136.7	Ο.		91.0	127.5	50.5	0.1	50.0	34.0	249.0
	(H) (H)	0.	1.5	0.		4.0		16.0	25.2	7.5	44.8	176.2	0.
	(L) -	54.0	31.2	4+D.	129.5	90.0	67.5	0/sU	166.5	44.0	150.0	225.8	123.6

to be Continued

Continuation

* STA	TION		NANENG		*****	포학드드고학학	NFALL 39=====	*	CODE N				
* 015	TRICT		KALING			*****	******	* 	REGION	****	REG	ION II	****
YEAR		JAN	FEB	MAR	APR	MAY	JUNE	JULY	AUG				DEC
1963	(F)	3.8	27.6	0.	10.1	·1.0	61.0	194.7	118.9	44.6	14 7	24 9	116+6
	(H)	3.8			0.		86.4		47.6			0.3	72.9
1964	(L) (F)	7 .7 21.4	10_6 0_8	6∎5 31∎9	0. 4.1	20+1 74+2		51.9 77.∎8	141.6		26.6	68 8 172 1	
1704	(8)	0.5	9.7	24.7	17.3	11.0	191.8	115.9	77.8	193.0	96.1	262.2	
	(L)	6.1	1.8	0.5		217.9		111.7			67.7		
1965	())	. 9.1	34.0	17.8	21.6	73.4 6.9	57.2	67.5 309.4		133.1	47.3	40.9	
	(*) (L)	55.3 34.6	0.5 28.7	0.5 31.8	44.4 95.1	82.3	18.1			174.3		22 .6	
1966	(F)	3.6	18.1	11.2	17.8	182.6	163.4	101.4	237.9	50.6	14.7	85.5	
	(M)	46.0	5.4	0.		222.8	39.4	176.9	26.7	57.7	71.3		48.
	(L)	22.1	29.8	68.4	42.2	309.6		147.4	131.5 84.8	24.3	92.5 210.3	329.5	
1967	(주) (변)	74.5 101.5	14.5 3C.8	20.5	61.2 47.2	64.1		53.4	120.4		171.2		
	(L)	33.2	4.7	0.0	48.6	73.8				103.0	12.5	26.9	48
1968	(E)	9.4	0.	56.0	0.	59.9	101.4	61.4	178.6		35.9	7.2	0.
	(M)	6.4	с.	8.0		57.7 152.6		81.1 95.3	298.6 130.5	112.3		12.1 41.3	
1969	(L) (F)	9.3 13.8	C. 1.4	38.7 0.	85.1 115.8	22.3		120.2	81.5		211.7		47.
1707	(M)	1.2	0.	25.6	Ő.	74.0		101.0	115.1		83.9	4 4	21.
	(L)	0.	0.	0.5		160.2		223.1	76.3			104.8	
1970	(F)	37.2	8.3	27.9	33.6	63.1	68.8	44.3	70.4	42.5	87.3 208.9	139.5	
	(M) (L)	14.0 0.	0.3 1.1	7.9 139.3	0.8 5.4	260.5		68.6	0.		223.4	137.4	
1971	(1)	83.0	39.5	2.3	0.	43.2	187.1	85.9	71.2		258.2	32.4	72
	(M)	5.8	54.3	45.1	0.3	115.2	156.4	229.3			114.9	152.9	
	(ι.)	7.1	0.	1.3	20.3	58.4		72.9	29.7	97:6	74 4		38.
1972	(E) (M)	22.2 0.3	7.3	4.0 9.0	20.9 66.8	43.1 164.8	128.8	88.6	27.8 158.0	32.7 39.7	0.3	64.3 18.3	56
	(L)	20,5	0. 2.6	20.7		236.6	54.7	57.3	96.9			6.5	0.
1973	(F)	7.1	4 9	0.	18.6	32.0	186.3	78.9	93.1	96.1	114.5	84.4	20.
	(M)	0.	0.	15.3	47.0	13.2	178.0			140.6		41.7	
	(L)	0.6	. 0.	52.4	G. 52.9	15.5	143.8 148⊾6	58.2 79.3	166.8 113.6	134.9	42.2	199.7 183.2	20.
1974	(F) (M)	2.0 1.6	8.ć 1.8	9.7	38.9	40.2	4.3		214.3		136.5	77.4	93.
	(L)	98.7	0.8	0.	38.9	43.9	30.9	75.2	41.4	140.8	206.1	115.4	55 .
1975	(F)	55.5	0.3	0.8	44.5	53.7		194.0		140.3	139.0	60.9	111.
	(8)	28.0	1.4	0.5	0.	77.4		218.3	34.7	54±6 0±8	66.6 79.8	21.3 2.5	7.
1976	(L) (F)	59.5 18.2	0. 0.8	19.3 97.9	42.6 0.3	151.1	55.7		62.1	9.7	67.9	20.5	41
	(M)	46.8	0.	8.1	0.	26.5	139.8		107.2			63.6	39
	(L)	16.6	0.	0.	0.	159.4	204.3	162.2	170.3	58.9		56.5	4
1977	(F)	10.0	1.1	0.5	36.8	6.9 72.5		100.3 39.0	153.5	14.2	5.9	46.5 75.8	0. 11.
	(M) (L)	2.1 18.8	28.5 1.0	0. 41.0	26.2 0.		54.7 134.2	77.7	106.6		0.		
1978	(F)	3.8	Ο.	11.7	0.	6.9	22.1	88.7	167.8	117.5	218.2	6.4	23
		0.		0.3		39.9				202.8			7.
1070	(L) (D)	0.	2.1	0. 36 3	15.9	99.8 3.5	9.2 83.1	149.0 53.9	190.0 62.7	130.6	133.3 118.0	2.4	3. 14.
1979	(F) (M)	7.5 1.3	0.8	36.3	- 8.7 5.7	48.0		123.3	49.9	13.6	48.8	138.8	35
	(1)	15.0	1.8	0.	8.9	2.1		101.7	27.4		7.9	75.0	70.
1980	(F)	7.2	6.2	12.3	2.5	0.	74.7	28.5	50.3	17.0	36.3	53.7	21.
	(M)	5.7	9.0	11.8	0.9	36.8	53.8	120.4 99.8	15.2		130.0	217.0	37.
1981	(L) (F)	8.0 3.2	18.2 1.6	0. 8.7	0. 2.1	156.2	79.8	62.5	52°2 35°7		197.6 138.8	134 1	18.
	(M)	17.0	0.3	0.	3.8	72.7	24.4	99.4	87.8		138.1	368.0	29.
	(L)	8.4	0.6	9.4	0.	100.3	148.4	177.2	144.0	19.8	47 .4	571.0	2.
1982	(F)	2.9	0.	0.	70.7	48.5	85.8	133.3	193.8	393.0	0.	180.4	47.
	(M) (E)	21.1	6.9	1.5	90.3 33.0	59.0 175.5	95.3 241.0	13.2	103.4		791.0 236.2	9 • 7 206 • 3	5. 0.
1983	(E) (F)	4.6 5.9	3.5 0.3	0. 4.5	33.U 19.1	0.	85.9	10.9	49.6		200.2	200+3	0.
	(8)	11.9	1.8	0.	ċ.	31.5	22.4	66.0	218.2		115.3	222.0	
	(L)	3.5	0.3	35.1	0.	63.5	0.	91.7	19-8	136.2	92.5	519.9	ż.
1984	(F)	0.	0.		.0.	32.8 14.3	0.	15.1	30.0	0.		41.5	
	(#) (L)	2.3	0. 2.1	7.9 13.2	20.0	14.3	39.8	35.9 27:2	19±1 45±3	3.3	42.9 186.6	82.7 34.6	0 4
		. EeJ 999999999		129C	.050 160.	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			ل ع لا ا مور شاه ها ها ها		100.00		

to be Continued

1. y

Continuation

				=====		AY RAL							
	TION TRICT	******	CONSUEI NUEVA	LO VIZCAYA				tt.	CODE N REGION	****	055 Reg		
YEAR		JAN	FEB	MAR	APR	MAY	JUNE	JULY	AUG	SEPT	001	RÖV	DEC
1963	(1)	11.7	20.0	0.	0.	3.8			33.1	197,1	11.2	9.6	10.4
	(M)		17.7	0.		104.9	73.6	83.8		113.1	4.9		138.4
	(L)	9.2	5.6	5.3	2.5		172.5	39.7	52.5		9.7	21.6	2.5
1964	(f)	1.2	0.0	13.8	10.3		127.9		201.1		146.2	84.8	6.5
	(M)	10.6	. 0.0	10.3	69.1	67.6	76.7		155 - 8	69.1			120.5
1965	(L) (F)	0.7 0.0	7.6 0.0	21.1	27.2	62.7	160.7	64.2 77.1	94.0 17.9	65.6	39.5	59.6 50.8	19.3 9.6
	(M)	8.7	C.C	0.0	33.0	53.0		162.3	69.9		27.4	5.0	3.1
	(L)	13.8	4.5	41.5	90.0	123.0		63.4	42.0	19.0		5.5	1.9
1966	(7)	4.1	10.4	44.9	23.4	85.0	17.3	65.0		178.1	8.6	70.4	23.8
	(٣)	15.5	Ð.	Ο.	5.6	339.7	48.3	72.0	114.6	103.6	40.4	204.4	24.2
	(L)	10.7	10.6	30.8	3.8	233.4	79.8	54.6	65.2	33.0	15.3	165.9	42.4
1967	(F)	0.9	1.7	2.7	28.4	0.	15.7	58.3	181.8	98.7	145.3	329.5	17.8
	(M) (L)	4.8 1.6	6.4 1.9	1.4	16.2 36.3	48.3 1.9	05	71.1 152.4	144.2	124.8	168.6 0.3	4.6	1.3
1968	(F)	8.0	0.	25.5	1.5	29.0	39 4	39.1	89 9		11.5	5.6	12.0
1700	(M)	5.1	ΰ.	0.	9.7	108.9	43.9	76.1	97.1	185.1	20.3	11.0	1.2
	(L)	16.5	8.0	0.8		40.4	19.6	272.2			1.0	103.3	1.5
1969	(Ŧ)	1.8	4.8	6.	30.8	.13.7	49.0	65.5	179.4	252.5	73.7	Ο.	16 0
	(M)	2.0	0.	0.	0.	113.2	47.3	72.2	51.3	71.3	89.2	45.4	3.6
	(1)	<u>.</u>	0.	Ū.	8.6	56+3	41.0	361.1	92.3	10.4	36.0	71.9	-31.2
1970	(F)	93.3	1.7	18.1	31.3	12.9	160.0	31.6	88.8	99.0	99.2	68.5	49.6
	(M) (E)	3.5	0. 2.5	0.	0. 113.5	86.3 60.7	182.7 66.0	83.7 104.0	83.8 94.0		182.8	86.2	55.8
1971		0. 2.5	0.	28.1 0.		114.2		167.5	74.7	106.7	346.8	45.7	0. 29.2
1711	(M)	ō.	15.2	12.7	10.2	114.2			60.9	41.9	123.2		30.4
• •	(L)	0.	15.2	12.7	30.4	96.4	71.4	139.6	106.6			148.5	92.7
1972	(F)	30.4	5.1	2.5	8.9	46.9		581.5	132.6	31.5	0.	124 5	24.0
	(M)	2.5	2.5	22.3	12.7	81.3	19.1	649.0	253.1	219.2	0.	5.0	15.2
	(L)	38.1	0.	28.0	26.6	80.0	93.9	816.7	69.0	37.8	0.	3.8	0.
1973	(F)	22.9	14.0	0.	0.		33.1	89.1	82.5	76.2	339.1	50.7	
	(M)	0. 3.9	0.	0.	2.5		139.7 38.1	35.5	31.9 79.9	180.7	235.0	58.4 92.7	14.0
1974	(L) (F)	8.9	3.8	22.9 57.1	71.1 0.	39.4 30.4	220.8	33.1	0.	71.2	48.2	302.3	8.9 22.8
	(M)	2.5	C.	19.0	ő.	59.7	77.4	238.6	ŏ.	38.1	475.5		123.2
	(L)	19.0	3.8	8.9		88.8	22.9	40.7	0.	96.6	458.6	134.7	53,4
1975	(F)	7.7	0.	1.3	25.4	24.3	52.1	26.7	116.9		33.1	19.0	31.8
	(≜)	-30-5	0.	6.4	0.	125.8	43.3	39.3	104.2	124.6	152.4	19.2	69.8
	(L)	66.0	0.	21.6	2.5	113.1	40.6	71.1	63.5	48.4	68.5	3.8	45.7
1976	(F) (W)	59.6	6.4	1.3	63.0 21.5	34-3	25.4	38.3	46.6 51.5	62.6	71.1	2.3	2.0
	(M) (L)	16.5 19.2	1.3	36.9 5.0		44.4	116.9 742.2	92.8 139.3	194.4	68.0	27.9 111.4	38.3 4.0	0.
1977	(F)	1.5	0.	0.	1.5	7.1	62.3	48.3	57.9	32.8	16.3	18.9	13.8
	ČMÓ	2.0	7.1	7.6	0.	74.7	37.4	140.2	112.1			255.4	2.5
•	(L)	3.0	0.	40.7	0.	102.3	59.0	75.7	90.2	97.3	0.	1.0	0.
1978	(F)	5.0	1,5	14.7	0.5	7.6	80.4	26.2	111.6	65.9	185.9	111.3	32.7
	(M)	0.	. 0.	8.4	С.	1.5	43.2	118.3	60.8	140.7	83.0	13.2	54.1
1979	(L) (T)	0.	1.5	3.6	35.2	88.3	29.9	101 4	471.5	253.4	291.6	6.6	10.0
1979	(f) (M)	4.3	0. 0.	1 ⊾ 5	0.5 9.2	23.1 58.8	157.7 120-1	148.2	117.5 57.5	49.2 108.5	239.2	22.2 32.6	17.2
	(L)	0. 0.	0.	0. 44.2	73.4	50+0 59+4	81.8	48.6	46.7	1.14.0	11.6	32.0	2.0 16.8
1980	(8)	5.0	0.	44.z Q.	0.	47.0	81.0	94.4	8.6	214.2	20.7	982.9	25.1
	(M)	14.0	11.6	1.0	90.4	63.6	37.2	209.3	29.3	168.5	22.0	29.2	29
•	(L)	3,5	0	29.5	0.	93.1	34.0	471.1	126.5	144.8	96.1	25.1	0.
1981	(F)	24.5	8.6	0.	0	45.2	51.5	451.0	122.7	139.8	40.2	20.3	13.2
	(M)	6.6	10.7	0.	5.1	71.4	274.4	174.2	187.3	165.8	30.7	61.9	15.
4000	(L)	5.5	3.5	0.	80.4	50.1	92.7	14.7	48.9	125.5	140.1	223.5	5.
1982	(F) /#\	1.5	0.	5.1	36.4	4.5	14.8	202.1	107.8	96.3	20.9	65.0	9.0
	(M)	2.5	. 8.9	0.	33.5	7.5	21.6	149.9	21.3	31.2	124.0	16.3	16.0
1983	(L) (E)	2.5 36.3	0. 0.	64.0 6.1	8. 1.0	73.3	67.4	93.8 99.6	181.1	46.7 46.4	21.2	25.6 6.9	20.9
1705	(1)	30.4	0.5	0.1 U.	0.	0.	37.6	150.4	264.4	39.5	104.4	67.8	0. 0.
	(L)	5,2	5.3	5.1	0.8	35.0	4.0	123.7	29.7	70.7	125.3	0.	0.
1984	(F)	0.	8.9	22.9	õ.	68.6	50.4	62.2	25.4	65.1	155.7	13.2	7.
	(M)	0.	0.	64.8	141-1	205.6	53.1	4.8	175.3	57.0	64.5	17.7	Ο.
	(L)	10,4	2.5	23.1	41.4	74.2	66.5	67.1	343.8	58.2	317.3	3.6	0.

Table 3.3 Conditions and Results of Tank Coefficient Calibration

Runoff Gauge Raingauge	Basin 1 (Upper Cagayan) Guinalvin Ilagan	Basin 2 (Magat) Dulao Nayon	Basin 3 (Ilagan) Minanga Ilagan
Drainage	921	573	1,565
Area (km2)			
Calibration	1965 71,74	1968 70	1966, 68 69
Period			
<u>/1</u>			
Rainfall	1.35	1.60	1.20
Ratio			
<u>/2</u>			
Evaporation	0.7	0.7	0.7
Ratio			
Rainfall (mm)	2,808	2,845	2,153
Loss (mm)	1,255	1,221	1,152
LOOD (man)	1/200	.,	2/200
Estimated	1,553	1,624	1,001
Runoff (mm)			
Observed	1,686	1,497	915
Runoff (mm)		· ·	a a an

Runoff Gauge Raingauge	Basin 4 (Lower Cagayan) Larion Alto Tuguegarao	Basin 5 (Upper Chico) Ampawilen Bontoc	Basin 6 (Lower Chico) Pinukpuk Tuao
Drainage Area (km2)	655	751	856
Calibration Period	1957 73	1963 76	1968 71
<u>/1</u> Rainfall Ratio	2.20	1.40	1.70
<u>/2</u> Evaporation Ratio	0.7	0.6	0.7
Rainfall(mm)	3,707	3,379	2,913
Loss (mm) Estimated	1,244	1,037	1,143
Runoff (mm)	2,463	2,342	1,770
Observed Runoff (mm)	2,427	2,383	1,890

Notes;

<u>/1</u> ;Ratio of basin rainfall to rainfall at applied gauge.

/2 ;Ratio of evapotranspiration to evaporation by A-pan. HY-56 Table 3.4

8

*************** SIMULATED 10-DAY MEAN RUNOFF

(L) (F) (<u>N)</u> (L) (F)	30.7 12.6 12.1 10.1 19.8 15.9 11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	29,9 18,4 18,6 39,9 25,2 21,0 24,3 11,9 10,6 12,5 28,5 26,0 27,6 10,5 9,2 10,6 11,3 10,1 11,3 22,2	11.9 19.7 16.8 13.1 17.4 15.5 12.4 9.1 9.0 8.1 10.5 15.7 12.7 6.2 0.1 7.3 7.8 14.5 0.9 15.1	8.9 12.7 12.0 10.6 11.8 11.9 16.6 8.8 6.2 5.6 17.5 13.3 12.8 8.0 7.9 22.4 7.5 7.4 7.4 10.5	22.3 10.4 10.1 65.1 10.4 16.3 10.1 71.4 16.5 45.0 11.3 10.2 9.6 16.6 8.5 7.1 7.3 7.2 25.2 6.9 7.9 6.5	133.6 53.3 57.4 79.2 18.0 12.6 54.2 37.5 58.6 33.7 26.0 14.6 59.7 118.2 54.2 45.4 31.9 14.7 8.8 7.1 32.4 31.8 56.1 139.8 48.0 40.1	63.1 52.1 87.7 96.0 124.5 22.8 36.4 21.3 20.8 62.3 22.5 42.3 21.0 32.0 22.3 7.8 6.8 6.1 15.2 13.8 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7		97.8 51.2 99.0 112.9 67.7 24.0 20.8 14.2 14.0 11.4 24.9 23.7 21.8 26.0 51.4 91.5 56.8 18.0 22.0 25.7 70.8 27.3 74.1 192.2 56.3 26.6	43.6 113.2 49.7 66.5 16.4 55.8 16.0 22.1 28.9 30.3 86.2 26.4 17.7 28.8 39.6 20.7 147.9 55.1 19.3 123.0 98.0 127.4 231.0 203.0 150.5 23.6 19.4 16.0 0,0	37.7 113.3 336.2 204.1 73.6 21.0 25.0 45.0 123.7 286.9 54.9 23.8 18.5 19.6 17.4 29.8 17.7	87.5 154.3 141.7 45.9 288.0 161.0 133.7 41.5
(K) (L) (F) (M) (L) (F) (F) (F) (F) (F) (F) (F) (F) (F) (F	$\begin{array}{c} 25 \cdot 3 \\ 20 \cdot 7 \\ 28 \cdot 6 \\ 23 \cdot 8 \\ 19 \cdot 2 \\ 44 \cdot 1 \\ 37 \cdot 4 \\ 28 \cdot 0 \\ 17 \cdot 7 \\ 14 \cdot 5 \\ 11 \cdot 6 \\ 62 \cdot 6 \\ 39 \cdot 4 \\ 30 \cdot 7 \\ 12 \cdot 6 \\ 12 \cdot 1 \\ 10 \cdot 1 \\ 19 \cdot 8 \\ 15 \cdot 9 \\ 11 \cdot 4 \\ 77 \cdot 1 \\ 29 \cdot 5 \\ 22 \cdot 5 \\ 69 \cdot 0 \\ 32 \cdot 5 \\ 31 \cdot 1 \\ 133 \cdot 1 \\ 58 \cdot 6 \\ 49 \cdot 1 \\ 16 \cdot 4 \\ 15 \cdot 4 \\ 13 \cdot 3 \\ 38 \cdot 4 \\ \end{array}$	24.7 29.9 18.4 18.6 39.9 25.2 21.0 24.3 11.9 10.6 12.5 28.5 26.0 27.0 10.5 9.2 10.6 11.3 10.1 11.3 22.2 10.6 11.3 26.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	$ \begin{array}{c} 15.8 \\ 11.9 \\ 19.7 \\ 16.8 \\ 13.1 \\ 17.4 \\ 15.5 \\ 12.4 \\ 9.1 \\ 9.0 \\ 5.1 \\ 10.5 \\ 15.7 \\ 12.7 \\ 6.2 \\ 6.1 \\ 7.3 \\ 7.8 \\ 10.5 \\ 15.1 \\ 12.6 \\ 10.3 \\ 10.4 \\ 102.7 \\ 20.5 \\ 20.7 \\ 20.4 \\ 11.9 \\ 11.7 \\ \end{array} $	10.7 8.9 12.7 12.0 10.6 11.8 11.9 16.6 8.8 8.2 8.6 17.5 13.3 12.8 8.0 7.9 22.4 7.5 7.4 7.5 7.4 7.5 18.9 16.6 14.0 12.0 24.5 49.5 49.5 15.1 11.8	7.9 22.3 10.4 10.1 65.1 10.4 16.3 10.1 71.4 16.5 45.0 11.3 10.2 9.6 16.6 8.5 7.1 7.3 7.2 25.2 8.9 7.9 6.5 20.7 53.3 17.3 28.5 91.2 112.9 11.1		71.4 55.3 63.1 52.1 87.7 96.0 124.5 22.8 36.4 21.3 20.6 62.3 22.5 42.3 21.0 32.5 42.3 21.0 32.0 22.3 7.8 6.8 6.1 15.2 13.6 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	21.6 132.3 82.7 4C.4 33.0 23.5 32.6 21.6 24.3 15.7 15.5 44.9 26.8 23.5 81.4 162.9 39.0 51.4 66.6 28.6 16.7 47.8 81.2 84.2 28.4 23.4 22.2			26.5 37.7 113.3 336.2 204.1 73.6 21.0 25.0 45.0 123.7 286.9 54.9 23.8 18.5 19.6 17.4 29.8 17.7 96.1 112.3 110.2 93.9 78.1 141.4 202.4 318.5 22.5 .57.4 .87.8 108.4	97.5 35.3 91.3 169.5 66.0 20.7 27.6 25.8 133.2 76.6 133.7 43.0 16.7 16.7 17.7 16.7 16.7 17.7 16.7 16.7 17.7 17.7 16.7 17.
(L) (F) (M) (L) (F) (F) (L) (F) (F) (C) (F) (F) (C) (F) (F) (F) (F) (F) (F) (F) (F) (F) (F	20.7 28.8 23.8 19.2 44.1 37.4 28.0 17.7 14.5 11.8 62.6 39.4 30.7 12.6 12.1 10.1 19.8 15.9 11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 38.4	29,9 18.4 18.6 39.9 25.2 21.0 24.3 11.9 15.6 12.5 28.8 26.0 27.6 10.5 9.2 10.6 11.3 10.1 11.3 22.2 17.5 20.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	$ \begin{array}{c} 11.9 \\ 19.7 \\ 16.8 \\ 13.1 \\ 17.4 \\ 15.5 \\ 12.4 \\ 9.1 \\ 9.6 \\ 5.1 \\ 10.5 \\ 15.7 \\ 12.7 \\ 6.2 \\ 0.1 \\ 7.3 \\ 7.8 \\ 10.5 \\ 10.5 \\ 10.5 \\ 10.4 \\ 102.7 \\ 20.5 \\ 20.7 \\ 20.4 \\ 11.9 \\ 11.7 \\ \end{array} $	8.9 12.7 12.0 10.6 11.8 11.9 10.6 8.8 6.2 5.6 17.5 13.3 12.6 8.0 7.9 22.4 7.5 7.4 7.5 7.4 7.5 12.5 8.0 7.9 22.4 7.5 7.4 7.5 16.6 17.5 12.5 11.5 11.5 11.5 11.5	22.3 10.4 10.1 65.1 10.4 16.3 10.1 71.4 16.5 45.0 11.3 10.2 9.6 16.6 8.5 7.1 7.3 7.2 25.2 5.9 7.9 6.5 20.7 53.3 17.3 26.5 21.2 112.9 11.1 11.0	133.6 53.3 57.4 79.2 18.0 12.6 54.2 37.5 58.6 33.7 26.0 14.6 59.7 118.2 54.2 45.4 31.9 14.7 8.8 7.1 32.4 31.8 56.1 139.8 48.0 40.1 28.2 59.3 140.2	55.3 63.1 52.1 87.7 96.0 124.5 22.8 36.4 21.3 20.6 62.3 22.5 42.3 21.0 32.5 42.3 21.0 32.5 42.3 7.8 6.8 6.1 15.2 13.6 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	132.3 82.7 4C.4 33.0 23.5 32.6 21.6 24.3 15.7 15.5 44.9 26.8 23.5 81.4 162.9 39.0 51.4 66.6 28.6 16.7 47.8 81.2 84.2 28.4 22.2	97.8 51.2 99.0 112.9 67.7 24.0 20.8 14.2 14.0 11.4 24.9 23.7 21.8 26.0 51.4 91.5 56.8 18.0 22.0 25.7 70.8 27.3 74.1 192.2 56.3 26.6 22.0 23.3	43.6 113.2 49.7 66.5 16.4 55.8 16.0 22.1 28.9 30.3 86.2 26.4 17.7 28.8 39.6 20.7 147.9 55.1 19.3 123.0 98.0 127.4 231.0 203.0 150.5 23.6 19.4 16.0 0,0	37.7 113.3 336.2 204.1 73.6 21.0 25.0 45.0 123.7 286.9 54.9 23.8 18.5 19.6 17.4 29.8 17.7 96.1 112.3 110.2 93.9 78.1 141.4 202.4 318.5 22.5 17.4 87.8 108.4	35.2 91.3 169.5 66.0 20.1 27.6 25.8 133.2 76.2 175.1 20.1 16.4 13.7 43.0 19.5 96.7 87.5 154.3 141.7 45.9 288.0 161.0 133.7 41.5 23.2 17.5 169.4
(M) (L) (F) (P) (L) (F) (M) (L) (F) (M) (L) (F) (M) (L) (F) (M) (L) (F) (M) (L) (F) (M) (L) (F) (M) (L)	23.8 19.2 44.1 37.4 28.0 17.7 14.5 11.8 62.6 39.4 30.7 12.8 12.1 10.1 19.8 15.9 11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	18.0 39.9 25.2 21.0 24.3 11.9 10.6 12.5 28.8 26.0 27.6 10.5 9.2 10.6 11.3 10.1 11.3 22.2 10.6 11.3 10.1 11.3 22.2 17.5 20.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	$ \begin{array}{c} 16.8 \\ 13.1 \\ \hline 17.4 \\ 15.5 \\ 12.4 \\ 9.1 \\ 9.0 \\ 5.1 \\ 16.5 \\ 15.7 \\ 12.7 \\ \hline 6.2 \\ 0.1 \\ 7.3 \\ 7.8 \\ 10.5 \\ 15.1 \\ 12.6 \\ 19.3 \\ 10.4 \\ 102.7 \\ 20.5 \\ 20.7 \\ 20.4 \\ 11.9 \\ 11.7 \\ \end{array} $	12.7 12.0 10.6 11.8 11.9 16.6 8.8 8.7 5.7 5.7 12.8 8.0 7.9 22.4 7.5 7.4 7.5 9.2 16.6 14.0 12.0 24.5 49.5 45.1 11.5 11.4	10.4 10.1 65.1 10.4 16.3 10.1 71.4 16.5 45.0 11.3 10.2 9.6 16.6 8.5 7.1 7.3 7.2 25.2 8.9 7.9 6.5 20.7 53.3 17.3 26.5 21.2 112.9 11.1	53.3 57.4 79.2 18.0 12.6 54.2 37.5 58.6 33.7 26.0 14.6 59.7 118.2 54.2 45.4 31.9 14.7 8.8 7.1 32.4 31.3 56.1 139.8 43.0 40.1 22.2 59.3 140.2	63.1 52.1 87.7 96.0 124.5 22.8 36.4 21.3 20.6 62.3 22.5 42.3 21.0 32.0 22.3 7.8 6.8 6.1 15.2 13.6 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	82.7 4C.4 33.0 23.5 32.6 24.3 15.7 15.7 15.7 44.9 26.8 23.5 81.4 162.9 39.0 51.4 66.6 28.6 63.9 57.6 16.7 47.8 81.2 28.4 23.4 22.2	51.2 99.0 112.9 67.7 24.0 20.8 14.2 14.0 11.4 84.9 23.7 21.8 26.0 51.4 91.5 56.8 18.0 25.7 70.8 27.3 74.1 192.2 56.6 23.3	113.2 49.7 66.5 16.4 55.8 16.0 22.1 28.9 30.3 86.2 26.4 17.7 28.8 39.6 20.7 147.9 55.1 19.3 123.0 98.0 127.4 231.0 203.0 150.5 23.6 19.4 16.0 0,0	113.3 336.2 204.1 73.6 21.0 25.0 45.0 123.7 286.9 54.9 23.8 18.5 19.6 17.4 29.8 17.7 96.1 112.3 110.2 93.9 78.1 141.4 202.4 318.5 22.5 17.4 87.8 108.4	91.3 169.9 66.0 20.7 27.6 25.8 133.2 76.6 175.1 20.1 16.4 13.7 16.7 43.0 19.5 96.7 96.7 87.5 154.3 141.7 45.9 288.0 161.0 133.7 41.5 23.2 17.5 169.4
(M) (L) (F) (P) (L) (F) (M) (L) (F) (M) (L) (F) (M) (L) (F) (M) (L) (F) (M) (L) (F) (M) (L) (F) (M) (L)	23.8 19.2 44.1 37.4 28.0 17.7 14.5 11.8 62.6 39.4 30.7 12.8 12.1 10.1 19.8 15.9 11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	18.0 39.9 25.2 21.0 24.3 11.9 10.6 12.5 28.8 26.0 27.6 10.5 9.2 10.6 11.3 10.1 11.3 22.2 10.6 11.3 10.1 11.3 22.2 17.5 20.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	$ \begin{array}{c} 16.8 \\ 13.1 \\ \hline 17.4 \\ 15.5 \\ 12.4 \\ 9.1 \\ 9.0 \\ 5.1 \\ 16.5 \\ 15.7 \\ 12.7 \\ \hline 6.2 \\ 0.1 \\ 7.3 \\ 7.8 \\ 10.5 \\ 15.1 \\ 12.6 \\ 19.3 \\ 10.4 \\ 102.7 \\ 20.5 \\ 20.7 \\ 20.4 \\ 11.9 \\ 11.7 \\ \end{array} $	12.0 10.6 11.8 11.9 16.6 8.8 6.7 5.7 12.5 12.3 12.8 8.0 7.9 22.4 7.5 7.4 7.5 7.4 7.5 7.4 7.5 7.4 7.5 7.4 7.5 7.4 7.5 7.4 7.5 16.6 14.0 12.0 24.5 49.5 49.5 49.5 45.1 11.5 11.4	10.1 65.1 10.4 16.3 10.1 71.4 16.5 45.0 11.3 10.2 9.6 16.6 8.5 7.1 7.3 7.2 25.2 6.9 7.9 6.5 20.7 53.3 17.3 26.5 91.2 112.9 11.1 11.0	57.4 79.2 18.0 12.6 54.2 37.5 58.6 33.7 26.0 14.6 59.7 118.2 54.2 45.4 31.9 14.7 8.8 7.1 32.4 31.3 56.1 139.8 48.0 40.1 28.2 59.3 140.2	52.1 87.7 96.0 124.5 22.8 36.4 21.3 20.6 62.3 22.5 42.3 21.0 32.0 22.3 7.8 6.8 6.1 15.2 13.6 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	4C.4 33.0 23.5 32.6 21.6 24.3 15.7 15.5 44.9 26.8 23.5 81.4 162.9 39.0 51.4 66.6 28.6 16.7 47.8 81.2 84.2 28.4 23.4 28.4 23.4	99.0 112.9 67.7 24.0 20.8 14.2 14.0 11.4 84.9 23.7 21.8 26.0 51.4 91.5 56.8 18.0 22.0 25.7 70.8 27.3 74.1 192.2 56.3 26.6 22.0 23.3	49.7 66.5 16.4 55.8 16.0 22.1 28.9 30.3 86.2 26.4 17.7 28.8 39.6 20.7 147.9 55.1 19.3 123.0 58.0 127.4 231.0 203.0 150.5 23.6 -19.4 16.0 0,0	336.2 204.1 73.6 21.0 25.0 45.0 123.7 286.9 54.9 23.8 18.5 79.6 17.4 29.8 17.7 96.1 112.3 110.2 93.9 78.1 141.4 202.4 318.5 22.5 57.4 87.8 108.4	169.5 66.0 20.7 27.6 25.7 133.2 76.6 133.7 16.7 16.7 43.0 19.5 96.7 96.7 96.7 96.7 96.7 96.7 96.7 96.7
(F) (F) (F) (F) (F) (F) (F) (F) (F) (F)	44.1 37.4 28.0 17.7 14.5 11.8 62.6 39.4 30.7 12.6 12.1 10.1 19.8 15.9 11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	25.2 21.0 24.3 11.9 15.6 12.5 28.8 26.0 27.6 10.5 9.2 10.6 11.3 10.1 11.3 22.2 17.5 20.4 26.1 28.5 27.9 44.3 26.1 28.5 27.9 44.3	17.4 15.5 12.4 9.1 9.0 8.1 10.5 15.7 12.7 0.2 0.1 7.3 7.8 10.5 12.7 0.9 15.1 12.6 10.3 16.4 102.7 20.5 70.7 23.0 20.4 11.7	11.8 11.9 16.6 8.8 6.7 5.6 17.5 12.5 12.5 8.0 7.9 22.4 7.5 7.4 7.5 7.4 7.4 10.5 9.2 18.9 16.6 14.0 12.0 24.5 49.5 45.1 11.5 11.4	10.4 16.3 10.1 71.4 16.5 45.0 11.3 10.2 9.6 16.6 8.5 7.1 7.3 7.2 25.2 8.9 7.9 6.5 20.7 \$2.3 17.3 26.5 21.2 112.9 11.1 11.0	18.0 12.6 54.2 37.5 58.6 33.7 26.0 14.6 59.7 118.2 54.2 45.4 31.9 14.7 8.8 7.1 32.4 31.3 56.1 139.8 43.0 40.1 22.2 59.3 140.2	96.0 124.5 22.8 36.4 21.3 20.8 62.3 22.5 42.3 21.0 32.0 22.3 7.8 6.8 6.1 15.2 13.8 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	23.5 32.6 21.6 24.3 15.7 15.5 44.9 26.8 23.5 81.4 162.9 39.0 51.4 66.6 28.6 63.9 57.6 16.7 47.8 81.2 47.8 81.2 28.4 23.4 23.4	67.7 24.0 20.8 14.2 14.0 11.4 23.7 21.8 26.0 51.4 91.5 56.8 18.0 22.0 25.7 70.8 27.3 74.1 192.2 56.6 22.0 23.3	16.4 55.8 16.0 22.1 28.9 30.3 86.2 26.4 17.7 28.8 39.6 20.7 147.9 55.1 19.3 123.0 98.0 127.4 231.0 203.0 150.5 23.6 19.4 16.0 0,0	73.6 21.0 25.0 45.0 123.7 286.9 54.9 23.8 18.5 19.6 17.4 29.8 17.7 96.1 112.3 110.2 93.9 78.1 141.4 202.4 318.5 22.5 17.4 87.8 108.4	20.7 27.6 25.8 133.2 76.2 175.1 20.1 16.4 13.7 16.7 43.0 19.5 96.7 96.7 87.5 154.3 141.7 45.9 288.0 161.0 133.7 41.5 23.2 17.5
(P) (L) (F) (E) (E) (E) (E) (E) (E) (E) (E) (E) (E	37.4 28.0 17.7 14.15 11.6 62.6 39.4 30.7 12.6 12.1 10.1 19.8 15.9 11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	21.0 24.3 11.9 12.5 28.5 26.0 27.6 10.5 9.2 10.6 11.3 10.1 11.3 22.2 17.5 20.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	$ \begin{array}{c} 1 > . \\ 5 \\ 12 . \\ 4 \\ 9.1 \\ 9.0 \\ 5.1 \\ 10 . \\ 5 \\ 15 . \\ 7 \\ 2. \\ 7 \\ $	11.9 16.6 8.8 6.7 5.6 17.5 13.3 12.8 8.0 7.9 22.4 7.5 7.4 7.5 7.4 7.5 9.2 16.6 14.0 12.0 24.5 49.5 49.5 11.5 11.5 11.5	1G.3 10.1 71.4 16.5 45.0 11.3 10.2 9.6 16.6 8.5 7.1 7.3 7.2 25.2 8.9 7.9 6.5 20.7 53.3 17.3 28.5 91.2 112.9 11.1	12.6 54.2 37.5 58.6 33.7 26.0 14.6 59.7 118.2 54.2 45.4 31.9 14.7 8.8 7.1 32.4 31.3 56.1 139.8 48.0 40.1 28.2 59.3 140.2	124.5 22.8 36.4 21.3 20.6 62.3 22.5 42.3 21.0 32.0 22.3 7.8 6.8 6.1 15.2 13.6 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	32.6 21.6 24.3 15.7 15.5 44.9 26.8 23.5 81.4 162.9 39.0 51.4 66.6 28.6 63.9 57.6 16.7 47.8 81.2 84.2 28.4 23.4 22.2	24.0 20.8 14.2 14.0 11.4 24.9 23.7 21.8 26.0 51.4 91.5 56.8 18.0 22.0 25.7 70.8 27.3 74.1 192.2 56.3 26.6 22.0 23.3	55.8 16.0 22.1 28.9 30.3 86.2 26.4 17.7 28.8 39.6 20.7 147.9 55.1 19.3 123.0 98.0 127.4 231.0 203.0 150.5 23.6 -19.4 16.0 60.0	21.0 25.0 45.0 123.7 286.9 54.9 23.8 18.5 19.6 17.4 29.8 17.7 .96.1 112.3 110.2 93.9 78.1 141.4 202.4 318.5 22.5 .57.4 .87.8 108.4	27.6 25.8 133.2 76.2 175.1 20.1 16.4 13.7 16.7 43.0 19.5 96.7 96.7 96.7 96.7 96.7 96.7 97.5 154.3 141.7 45.9 288.0 161.0 133.7 41.5 23.2 17.5
(L) (F) (L) (E) (E) (E) (E) (E) (E) (E) (E) (E) (E	28.0 17.7 14.5 11.8 62.6 39.4 30.7 12.6 12.1 10.1 19.8 15.9 11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	24.3 11.9 15.6 12.5 28.8 26.0 27.0 10.5 9.2 10.6 11.3 10.1 11.3 22.2 17.5 20.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	12.4 9.1 9.0 8.1 10.5 15.7 12.7 0.2 0.1 7.3 7.8 10.5 0.9 15.1 12.6 10.3 10.4 102.7 20.5 20.7 21.4 11.9 11.7	10.6 8.8 6.7 5.6 17.5 13.3 12.8 8.0 7.9 22.4 7.9 22.4 7.9 22.4 7.5 7.4 7.4 10.5 9.2 18.9 16.6 14.0 12.0 24.5 49.5 49.5 45.1 11.5 11.4	10.1 71.4 16.5 45.0 11.3 10.2 9.6 16.6 8.5 7.1 7.3 7.2 25.2 8.9 7.9 6.5 20.7 53.3 17.3 26.5 21.2 112.9 11.1	54.2 37.5 58.6 33.7 26.0 14.6 59.7 118.2 54.2 45.4 31.9 14.7 8.8 7.1 32.4 31.8 56.1 139.8 48.0 40.1 28.2 59.3 140.2	22.8 36.4 21.3 20.8 62.3 22.5 42.3 21.0 38.0 22.3 7.8 6.1 15.2 13.8 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	21.6 24.3 15.7 15.5 44.9 26.8 23.5 81.4 162.9 39.0 51.4 66.6 28.6 63.9 57.6 16.7 47.8 81.2 84.2 28.4 23.4 22.2	20.8 14.2 14.0 11.4 24.9 23.7 21.8 26.0 51.4 91.5 56.8 18.0 22.0 25.7 70.8 27.3 74.1 192.2 56.3 26.6 22.0 23.3	16.0 22.1 28.9 30.3 86.2 26.4 17.7 28.8 39.6 20.7 147.9 55.1 19.3 123.0 98.0 127.4 231.0 203.0 150.5 23.6 -19.4 16.0 60.0	25.0 45.0 123.7 286.9 54.9 23.8 18.5 19.6 17.4 29.8 17.7 96.1 112.3 110.2 93.9 78.1 141.4 202.4 318.5 22.5 17.4 87.8 108.4	25.2 133.2 76.2 175.1 20.1 16.4 13.7 16.7 43.0 19.5 96.7 97.7 96.7 96.7 97.7 96.7 97.7
(F) (L) (F) (K) (F) (K) (L) (F) (K) (K) (K) (K)	$ \begin{array}{c} 14.5 \\ 11.8 \\ 62.6 \\ 39.4 \\ 30.7 \\ \hline 12.8 \\ 12.1 \\ 10.1 \\ 19.8 \\ 15.9 \\ 11.4 \\ 77.1 \\ 29.5 \\ 22.5 \\ \hline 69.0 \\ 32.5 \\ 31.1 \\ 133.1 \\ 58.6 \\ 49.1 \\ \hline 16.4 \\ 15.4 \\ 13.3 \\ 38.4 \\ \end{array} $	1 C + 6 1 2 + 5 2 8 + 5 2 6 + 0 2 7 + 6 1 0 + 5 9 + 2 1 0 + 6 1 1 + 3 1 0 + 1 1 1 + 3 2 2 + 2 1 7 + 5 2 0 + 4 2 6 + 1 2 8 + 5 2 7 + 9 4 4 + 3 3 8 + 7 4 1 + 1 1 3 + 7 1 2 + 4 1 3 + 7 1 4 + 7 1 3 + 7 1 4 + 7 1 3 +	$\begin{array}{c} 9.6 \\ 8.1 \\ 10.5 \\ 15.7 \\ 12.7 \\ \hline \\ 6.2 \\ 0.1 \\ 7.3 \\ 7.8 \\ 10.5 \\ 10.4 \\ 102.7 \\ 20.5 \\ 20.7 \\ 20.4 \\ 10.7 \\ 20.4 \\ 11.9 \\ 11.7 \end{array}$	8.7 8.6 17.5 13.3 12.8 8.0 7.9 22.4 7.5 7.4 7.5 7.4 7.4 7.5 18.9 16.6 14.0 12.0 24.5 45.1 11.5 11.4	16.5 45.0 11.3 10.2 9.6 16.6 8.5 7.1 7.3 7.2 25.2 5.9 7.9 6.5 20.7 53.3 17.3 26.5 21.2 112.9 11.1 11.0	58.6 33.7 26.0 14.6 59.7 118.2 54.2 45.4 31.9 14.7 8.8 7.1 32.4 31.3 56.1 139.8 48.0 40.1 28.2 59.3 140.2	21.3 20.8 62.3 22.5 42.3 21.0 38.0 22.3 7.8 6.1 15.2 13.6 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	15.7. 15.5 44.9 26.8 23.5 81.4 162.9 39.0 51.4 66.6 28.6 63.9 57.6 16.7 47.8 81.2 84.2 28.4 23.4 22.2	14.0 11.4 24.9 23.7 21.8 28.0 51.4 91.5 56.8 18.0 22.0 25.7 70.8 27.3 74.1 192.2 54.3 26.6 22.0 23.3	22.1 28.9 30.3 86.2 26.4 17.7 28.8 39.6 20.7 147.9 55.1 19.3 123.0 98.0 127.4 231.0 203.0 150.5 23.6 19.4 16.0 60.0	123.7 286.9 54.9 23.8 18.5 19.6 17.4 29.8 17.7 96.1 112.3 110.2 93.9 78.1 141.4 202.4 318.5 22.5 17.4 87.8 108.4	133 76 175 20 16 13 16 13 96 96 96 96 96 96 1542 1417 455 288.0 161.0 1337 415 23.2 175
(F) (L) (F) (K) (F) (K) (L) (F) (K) (K) (K) (K)	$ \begin{array}{c} 14.5 \\ 11.8 \\ 62.6 \\ 39.4 \\ 30.7 \\ \hline 12.8 \\ 12.1 \\ 10.1 \\ 19.8 \\ 15.9 \\ 11.4 \\ 77.1 \\ 29.5 \\ 22.5 \\ \hline 69.0 \\ 32.5 \\ 31.1 \\ 133.1 \\ 58.6 \\ 49.1 \\ \hline 16.4 \\ 15.4 \\ 13.3 \\ 38.4 \\ \end{array} $	1 C + 6 1 2 + 5 2 8 + 5 2 6 + 0 2 7 + 6 1 0 + 5 9 + 2 1 0 + 6 1 1 + 3 1 0 + 1 1 1 + 3 2 2 + 2 1 7 + 5 2 0 + 4 2 6 + 1 2 8 + 5 2 7 + 9 4 4 + 3 3 8 + 7 4 1 + 1 1 3 + 7 1 2 + 4 1 3 + 7 1 4 + 7 1 3 + 7 1 4 + 7 1 3 +	$\begin{array}{c} 9.6 \\ 8.1 \\ 10.5 \\ 15.7 \\ 12.7 \\ \hline \\ 6.2 \\ 0.1 \\ 7.3 \\ 7.8 \\ 10.5 \\ 10.4 \\ 102.7 \\ 20.5 \\ 20.7 \\ 20.4 \\ 10.7 \\ 20.4 \\ 11.9 \\ 11.7 \end{array}$	8.7 8.6 17.5 13.3 12.8 8.0 7.9 22.4 7.5 7.4 7.5 7.4 7.4 7.5 18.9 16.6 14.0 12.0 24.5 45.1 11.5 11.4	16.5 45.0 11.3 10.2 9.6 16.6 8.5 7.1 7.3 7.2 25.2 5.9 7.9 6.5 20.7 53.3 17.3 26.5 21.2 112.9 11.1 11.0	58.6 33.7 26.0 14.6 59.7 118.2 54.2 45.4 31.9 14.7 8.8 7.1 32.4 31.3 56.1 139.8 48.0 40.1 28.2 59.3 140.2	21.3 20.8 62.3 22.5 42.3 21.0 38.0 22.3 7.8 6.1 15.2 13.6 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	15.7. 15.5 44.9 26.8 23.5 81.4 162.9 39.0 51.4 66.6 28.6 63.9 57.6 16.7 47.8 81.2 84.2 28.4 23.4 22.2	14.0 11.4 24.9 23.7 21.8 28.0 51.4 91.5 56.8 18.0 22.0 25.7 70.8 27.3 74.1 192.2 56.3 26.6 22.0 23.3	28.9 30.3 86.2 26.4 17.7 28.8 39.6 20.7 147.9 	123.7 286.9 54.9 23.8 18.5 19.6 17.4 29.8 17.7 96.1 112.3 110.2 93.9 78.1 141.4 202.4 318.5 22.5 17.4 87.8 108.4	76.2 175.1 20.1 16.4 13.1 16.4 43.0 19.5 96.1 96.1 96.1 96.1 96.2 154.2 141.7 45.5 288.0 161.0 133.7 41.5 23.2 17.5
(F) (K) (L) (F) (K) (L) (F) (K) (L) (F) (K) (L) (F) (K) (L) (F) (K) (L)	62.6 39.4 30.7 12.6 12.1 10.1 19.8 15.9 11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	22.5 26.0 27.0 10.5 9.2 10.6 11.3 10.1 11.3 22.2 17.5 20.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	10.5 15.7 12.7 6.2 0.1 7.3 7.8 14.5 0.9 15.1 12.6 10.3 10.4 102.7 24.5 20.7 24.4 11.9 11.7	17.5 13.3 12.8 8.0 7.9 22.4 7.5 7.4 7.5 7.4 7.4 10.5 9.2 18.9 16.6 14.0 12.0 24.5 49.5 49.5 11.5 11.4	11.3 10.2 9.6 16.6 8.5 7.1 7.3 7.2 25.2 8.9 7.9 6.5 20.7 53.3 17.3 28.5 21.2 112.9 11.1 11.0	26.0 14.6 59.7 118.2 54.2 45.4 31.9 14.7 8.8 7.1 32.4 31.3 56.1 139.8 48.0 40.1 28.2 59.3 140.2	62.3 22.5 42.3 21.0 38.0 22.3 7.8 6.1 15.2 13.6 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	44.9 26.8 23.5 81.4 162.9 39.0 51.4 66.6 28.6 63.9 57.6 16.7 47.8 81.2 84.2 28.4 23.4 22.2	24.9 23.7 21.8 26.0 51.4 91.5 56.8 18.0 22.0 25.7 70.8 27.3 74.1 192.2 56.3 26.6 22.0 23.3	86.2 26.4 17.7 28.8 39.6 20.7 147.9 55.1 19.3 123.0 98.0 127.4 231.0 203.0 150.5 23.6 19.4 16.0 60.0	54.9 23.8 18.5 19.6 17.4 29.8 17.7 96.1 112.3 110.2 93.9 78.1 141.4 202.4 318.5 22.5 17.4 87.8 108.4	20. 16. 13. 16. 13. 16. 96. 96. 87. 154. 154. 288.0 161.0 133.7 41.5 23.2 17.5 169.4
(F) (F) (F) (F) (F) (F) (F) (F) (F) (F)	39.4 30.7 12.6 12.1 10.1 19.8 15.9 11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	26.0 27.0 10.5 9.2 10.6 11.3 10.1 11.3 22.2 17.5 20.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	$ \begin{array}{c} 15.7 \\ 12.7 \\ \hline 2.4 \\ 0.1 \\ 7.3 \\ 7.5 \\ 10.5 \\ 0.9 \\ 15.1 \\ 12.6 \\ 10.3 \\ 10.4 \\ 102.7 \\ 20.5 \\ 20.7 \\ 21.4 \\ 10.4 \\ 11.9 \\ 11.7 \\ \end{array} $	13,3 12,8 8.0 7.9 22.4 7.5 7.4 7.4 10.5 9.2 18.9 16.6 14.0 12.0 24.5 49.5 49.5 49.5 49.5	10.2 9.6 16.6 8.5 7.1 7.3 7.2 25.2 5.9 7.9 6.5 20.7 53.3 17.3 26.5 21.2 112.9 11.1 11.0	14.6 59.7 118.2 54.2 45.4 31.9 14.7 8.8 7.1 32.4 31.3 56.1 139.8 48.0 40.1 28.2 59.3 140.2	22.5 42.3 21.0 38.0 22.3 7.8 6.1 15.2 13.6 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	26.8 23.5 81.4 162.9 39.0 51.4 66.6 28.6 63.9 57.6 16.7 47.8 81.2 84.2 28.4 23.4 22.2	23.7 21.8 26.0 51.4 91.5 56.8 18.0 22.0 25.7 70.8 27.3 74.1 192.2 56.3 26.6 23.3	26.4 17.7 28.8 39.6 20.7 147.9 	23.8 18.5 19.6 17.4 29.8 17.7 96.1 112.3 110.2 93.9 78.1 141.4 202.4 318.5 22.5 17.4 87.8 108.4	16. 13. 16. 43. 19. 96. 96. 87. 154. 141. 45. 288. 161. 161. 23.2 17.5 169.4
(L) (F) (K) (L) (F) (L) (F) (K) (L) (F) (K) (L) (F) (K) (L) (F) (F) (F) (F) (F)	30.7 12.6 12.1 10.1 19.8 15.9 11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	27.0 10.5 9.2 10.6 11.3 10.1 11.3 22.2 17.5 20.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	12.7 6.2 6.1 7.3 7.8 14.5 0.9 15.1 12.6 10.3 16.4 102.7 24.5 20.7 24.4 11.9 11.7	12.8 8.0 7.9 22.4 7.5 7.4 7.4 10.5 9.2 18.9 16.6 14.0 12.0 24.5 49.5 49.5 49.5 45.1 11.5 11.4	9.6 16.6 8.5 7.1 7.3 7.2 25.2 8.9 7.9 6.5 20.7 53.3 17.3 26.5 21.2 112.9 11.1 11.0	59.7 118.2 54.2 45.4 31.9 1.4.7 8.8 7.1 32.4 31.8 56.1 139.8 48.0 40.1 22.2 59.3 140.2	42.3 21.0 32.0 22.3 7.8 6.8 6.1 15.2 13.6 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	23.5 81.4 162.9 39.0 51.4 66.6 28.6 63.9 57.6 16.7 47.8 81.2 84.2 28.4 23.4 22.2	21.8 26.0 51.4 91.5 56.8 18.0 22.0 25.7 70.8 27.3 74.1 192.2 56.3 26.6 22.0 23.3	17.7 28.8 39.6 20.7 147.9 	18.5 19.6 17.4 29.8 17.7 96.1 112.3 110.2 93.9 78.1 141.4 202.4 318.5 22.5 17.4 87.8 108.4	13.; 16.; 19.; 96.; 96.; 96.; 87.; 154.; 141.; 288.; 161.; 288.; 161.; 23.; 23.; 169.; 49.; 169.; 164.; 179.; 164.; 19.; 154.; 19.; 154.; 19.; 154.; 19.; 154.; 19.; 154.; 19.; 154.; 19.; 154.; 19.; 154.; 19.; 154.; 19.; 10.;
(M) (L) (F) (K) (L) (F) (M) (L) (F) (M) (L) (F) (M) (L) (F) (M) (L)	12.1 10.1 19.8 15.9 11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	9.2 10.6 11.3 10.1 11.3 22.2 17.5 20.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	$\begin{array}{c} 0.1 \\ 7.3 \\ 7.6 \\ 10.5 \\ 0.9 \\ 15.1 \\ 12.6 \\ 10.3 \\ 10.4 \\ 102.7 \\ 20.5 \\ 20.7 \\ 20.4 \\ 11.9 \\ 11.7 \end{array}$	7.9 22.4 7.5 7.4 7.4 10.5 9.2 18.9 16.6 14.0 12.0 24.5 49.5 49.5 45.1 11.5 11.4	8.5 7.1 7.3 7.2 25.2 5.9 7.9 6.5 20.7 53.3 17.3 26.5 21.2 112.9 11.1 11.0	54.2 45.4 31.9 14.7 8.8 7.1 32.4 31.3 56.1 139.8 48.0 40.1 28.2 59.3 140.2	3 & 0 2 2 . 3 7 . 8 6 . 1 1 5 . 2 1 3 . 6 1 0 . 4 6 1 . 3 1 4 2 . 7 4 7 . 4 7 4 . 4 3 1 . 1 1 2 2 . 9 2 7 . 7	162.9 39.0 51.4 66.6 28.6 63.9 57.6 16.7 47.8 81.2 84.2 28.4 23.4 22.2	51.4 91.5 56.8 18.0 22.0 25.7 70.8 27.3 74.1 192.2 56.6 22.0 23.3	39.6 20.7 147.9 	17 . 4 29 . 8 17 . 7 . 96 . 1 112 . 3 110 . 2 93 . 9 73 . 1 141 . 4 202 . 4 318 . 5 22 . 5 	43.0 19.5 96.7 87.5 154.3 141.7 45.9 288.0 161.0 133.7 41.5 23.2 17.5
(M) (L) (F) (K) (L) (F) (M) (L) (F) (M) (L) (F) (M) (L) (F) (M) (L)	12.1 10.1 19.8 15.9 11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	9.2 10.6 11.3 10.1 11.3 22.2 17.5 20.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	$\begin{array}{c} 0.1 \\ 7.3 \\ 7.6 \\ 10.5 \\ 0.9 \\ 15.1 \\ 12.6 \\ 10.3 \\ 10.4 \\ 102.7 \\ 20.5 \\ 20.7 \\ 20.4 \\ 11.9 \\ 11.7 \end{array}$	7.9 22.4 7.5 7.4 7.4 10.5 9.2 18.9 16.6 14.0 12.0 24.5 49.5 49.5 45.1 11.5 11.4	8.5 7.1 7.3 7.2 25.2 5.9 7.9 6.5 20.7 53.3 17.3 26.5 21.2 112.9 11.1 11.0	54.2 45.4 31.9 14.7 8.8 7.1 32.4 31.3 56.1 139.8 48.0 40.1 28.2 59.3 140.2	3 & 0 2 2 . 3 7 . 8 6 . 1 1 5 . 2 1 3 . 6 1 0 . 4 6 1 . 3 1 4 2 . 7 4 7 . 4 7 4 . 4 3 1 . 1 1 2 2 . 9 2 7 . 7	162.9 39.0 51.4 66.6 28.6 63.9 57.6 16.7 47.8 81.2 84.2 28.4 23.4 22.2	51.4 91.5 56.8 18.0 22.0 25.7 70.8 27.3 74.1 192.2 56.6 22.0 23.3	39.6 20.7 147.9 	17 . 4 29 . 8 17 . 7 . 96 . 1 112 . 3 110 . 2 93 . 9 73 . 1 141 . 4 202 . 4 318 . 5 22 . 5 	43.0 19.5 96.7 87.5 154.3 141.7 45.9 288.0 161.0 133.7 41.5 23.2 17.5
(F) (K) (L) (F) (K) (L) (F) (K) (L) (F) (K) (L) (F) (K) (L)	19.8 15.9 11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	11.3 10.1 11.3 22.2 17.5 20.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	7.8 10.5 0.9 15.1 12.6 10.3 16.4 102.7 20.5 20.7 20.4 11.9 11.7	7.5 7.4 7.4 10.5 9.2 18.9 16.6 14.0 12.0 24.5 49.5 45.1 11.5 11.4	7.3 7.2 25.2 8.9 7.9 6.5 20.7 52.3 17.3 28.5 21.2 112.9 11.1 11.0	31.9 14.7 8.8 7.1 32.4 31.3 56.1 139.8 48.0 40.1 22.2 59.3 140.2	7.8 6.1 15.2 13.8 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	51.4 66.6 28.6 63.9 57.6 16.7 47.8 81.2 84.2 28.4 23.4 22.2	56.8 18.0 22.0 25.7 70.8 27.3 74.1 192.2 56.3 26.6 22.0 23.3	147.9 	17,7 96,1 112,3 110,2 93,9 78,1 141,4 202,4 318,5 22,5 17,4 87,8 108,4	96.7 87.5 154.3 141.7 45.9 288.0 161.0 133.7 41.5 23.2 17.5 169.4
(F) (F) (F) (F) (C) (F) (C) (F) (C) (F) (F) (F) (F)	15.9 11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	10.1 11.3 22.2 17.5 20.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	10.5 0.9 15.1 12.6 10.3 16.4 102.7 20.5 26.7 24.0 20.4 11.9 11.7	7.4 7.4 10.5 9.2 18.9 16.6 14.0 12.0 24.5 49.5 45.1 11.5 11.4	7.2 25.2 5.9 7.9 6.5 20.7 53.3 17.3 26.5 21.2 112.9 11.1 11.0		6.8. 6.1 15.2 13.6 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	66.6. 28.6 57.6 16.7 47.3 81.2 84.2 28.4 23.4 22.2	18.0 22.0 25.7 70.8 27.3 74.1 192.2 56.6 22.0 23.3		96.1 112.3 110.2 93.9 78.1 141.4 202.4 318.5 22.5 	96.7 87.5 154.3 141.7 45.9 288.0 161.0 133.7 41.5 23.2 17.5 169.4
(L) (F) (K) (L) (E) (K) (L) (F) (K) (L) (F) (H)	11.4 77.1 29.5 22.5 69.0 32.5 31.1 133.1 .58.6 49.1 16.4 15.4 13.3 38.4	11.3 22.2 17.5 20.4 26.1 28.5 27.9 44.3 .38.7 41.1 13.7 12.4	0.9 15.1 12.6 10.3 16.4 102.7 20.5 20.7 20.4 11.9 11.7	7.4 10.5 9.2 18.9 16.6 14.0 12.0 24.5 49.5 49.5 45.1 11.5 11.4	25,2 8,9 7,9 6,5 20,7 53,3 17,3 26,5 21,2 112,9 11,1 11,0	8.8 7.1 32.4 31.3 56.1 139.8 48.0 40.1 -22.2 59.3 140.2	6.1 15.2 13.6 10.4 61.3 142.7 47.4 74.4 31.1 22.9 27.7	28.6 63.9 57.6 16.7 47.8 81.2 84.2 28.4 -23.4 22.2	22.0 25.7 70.8 27.3 74.1 192.2 56.3 26.6 	19.3 123.0 98.0 127.4 231.0 203.0 150.5 23.6 -19.4 16.0 60.0	112.3 110.2 93.9 78.1 141.4 202.4 318.5 22.5 .17.4 87.8 108.4	87.5 154.3 141.7 45.5 288.0 161.0 133.7 41.5 23.2 17.5 169.4
(F) (L) (F) (K) (C) (F) (K) (C) (F) (F) (F) (F)	29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	17.5 20.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	12.6 10.3 10.4 102.7 20.5 20.7 23.0 20.4 11.9 11.7	9.2 18.9 14.0 12.0 24.5 49.5 45.1 11.5 11.4	7,9 6.5 20.7 53.3 17.3 26.5 	32.4. 31.8 56.1 139.8 48.0 40.1 28.2 59.3 140.2		57.6 16.7 47.8 81.2 84.2 28.4 - 23.4 - 23.2	70.8 27.3 74.1 192.2 56.3 26.6 	98.0 127.4 231.0 203.0 150.5 23.6 -19.4. 16.0 60.0	93.9 78.1 141.4 202.4 318.5 22.5 17.4 87.8 108.4	141.7 45.5 288.0 161.0 133.7 41.5 23.2 17.5
(F) (L) (F) (K) (C) (F) (K) (C) (F) (F) (F) (F)	29.5 22.5 69.0 32.5 31.1 133.1 58.6 49.1 16.4 15.4 13.3 38.4	17.5 20.4 26.1 28.5 27.9 44.3 38.7 41.1 13.7 12.4	12.6 10.3 10.4 102.7 20.5 20.7 23.0 20.4 11.9 11.7	9.2 18.9 14.0 12.0 24.5 49.5 45.1 11.5 11.4	7,9 6.5 20.7 53.3 17.3 26.5 	32.4. 31.8 56.1 139.8 48.0 40.1 28.2 59.3 140.2		57.6 16.7 47.8 81.2 84.2 28.4 - 23.4 - 23.2	70.8 27.3 74.1 192.2 56.3 26.6 	98.0 127.4 231.0 203.0 150.5 23.6 -19.4. 16.0 60.0	93.9 78.1 141.4 202.4 318.5 22.5 17.4 87.8 108.4	141.7 45.5 288.0 161.0 133.7 41.5 23.2 17.5
(F) (M) (L) (F) (K) (L) (F) (N) (L) (F) (M)	69.0 32.5 31.1 133.1 	26.1 28,5 27.9 44.3 38.7 41.1 13.7 12.4	10.4 102.7 20.5 20.7 20.4 20.4 11.9 11.7	16.6 14.0 12.0 24.5 49.5 45.1 11.5 11.4	20.7 53.3 17.3 28.5 91.2 112.9 11.1 11.0	56.1 139.8 48.0 40.1 -28.2 59.3 140.2	61.3 142.7 47.4 74.4 	47.8 81.2 84.2 28.4 23.4 22.2	74.1 192.2 56.3 26.6 22.0 23.3	231.0 203.0 150.5 23.6 	141.4 202.4 318.5 22.5 .17.4 87.8 108.4	288.0 161.0 133.7 41.5 23.2 17.5
(M) (L) (F) (K) (L) (F) (L) (F) (F) (M)	32.5 31.1 133.1 58.6. 49.1 16.4 15.4 13.3 38.4	28.5 27.9 44.3 	102.7 20.5 20.7 23.0 20.4 11.9 11.7	14.0 12.0 24.5 49.0 45.1 11.5 11.4	53.3 17.3 28.5 	139.8 48.0 40.1 	142.7 47.4 74.4 31.1_ 22.9 27.7	81.2 84.2 28.4 	192.2 56.3 26.6 22.0 23.3	203.0 150.5 23.6 	202.4 318.5 22.5 	161.0 133.7 41.5 23.2 17.5 169.4
(L) (F) (C) (C) (F) (U) (F) (M)	31.1 133.1 	27.9 44.3 	20.5 20.7 23.0 20.4 11.9 11.7	12.0 24.5 49.0 45.1 11.5 11.4	17.3 28.5 	48.0 40.1 	47.4 74.4 31.1_ 22.9 27.7	28.4 28.4 23.4 22.2	56,3 26,6 22,0 23,3	150.5 23.6 	318 + 5 22 + 5 	133.7 41.5 23.2 17.5 169.4
(E) (E) (M) (L) (E) (E) (M)	58.6 49.1 16.4 15.4 13.3 38.4		20.4 11.9 11.7	49.0 45.1 11.5 11.4	21.+2 1129 111 11.0	28.2. 59.3 140.2		22.2	23.3	19.4. 16.0 60.0	17.4. 87.8 108.4	23.2
(L) (F) (N) (L) (F) (R)	58.6 49.1 16.4 15.4 13.3 38.4		20.4 11.9 11.7	49.0 45.1 11.5 11.4	21.+2 1129 111 11.0	28.2. 59.3 140.2		22.2	23.3	19.4. 16.0 60.0	17.4. 87.8 108.4	23.2
(f) (N) (L) (F) (F)	16.4 15.4 13.3 38.4	13.7	11.9 11.7	11.5 11.4	11.1 11.0	140.2	27.7			0.00	108.4	169.4
(N) (L) (F) (N)	15.4 13.3 38.4	12.4	11.7	11.4	11.0			62.2	23.5			
(L) (F) (N)	13.3 38.4						23.4	94.1	61.3	190.3		
(4)						77.3	51.0	26.5	25.9	68.0	298.8	41.0
		27.9	16.5	13.2	11,1	112.1	11.8	11.7	18,1	209.1	253.9	70.2
(())	31.9	23.2	10.3	11.6	1,9	21.8	38,5	45.6	30.3	235.1	166.6	183.4
	28.9	25.1	13.1	11.2	10.0	15.3	11.6	12+3	58.1	200.0	78.1	94,1
(<u>1)</u>	51.8 40.9	27.6	20.2 15.3_	14.8	11.2	17.0 18.1	20.2	27.1	17.3	13.2	55.2	77.3
(L)	37.5	29.0	14.9	2.3	39.6	37.4	30.9	14.3		101.7	18.9	73.1
(1)	68.5	20.1	13.0	14.5	11.1	53.7	23.9	133.8	18.7	42.2	111.4	82.2
(N) (L)	28.6	15.6	13.0 14 3	11.4	14.0 02.1	21.4		30.2	83.7	19.9	169.3	140.6
												53.4
												19.2
(L)	31.2	25.6	12.3	9.7	02.20	9.7	10,3	9.8	79.4	12.0	28.8	12.0
(1)	11.0	7.9	7.0	7.4	7.1	8.4	6.7	40.8	77.3	52.2	38.5	26.3
		7.2	7.+5 68		8.U 35.3							35.4 54.1
						~ •						
		11.1	9.1 7.0	6.8				31.7	82.3	71.2 31.0	28.3	22.4
(L).	13.2	12.2	0.2	12.1	116.8	36.4	136.6	36.8	33.9	22.8	24.5	15.8
(F)	16.0	11.9	9.6	7.6	7.3	7.5	8.3	8.7	17.5	21.2	213.5	44.0
												. 85.1 27.4
			•···· ••		···				-			
	221						81.8_					32.0 5.65
							14.4	20.0	40.0	101.6	53.8	18.7
(F)	18.4	10.8	7.2	6.5	6.2	6.0	7.4	8.1	80.4	12.5	21.6	47.4
		10.9	5.9	7.6	7.2 8.0	19.1	5.3	37.7	61.4 15.0	17.6	26.3	33.5
(;)	31.3	11.6	7.9	6.8	5.4	7.4	5.2					11.5
. (#)	. Jó 8	9.9		5.5	16.1.	. 7.9.	_ 5.9	4.9	.4.8	.14.7	33.4	10.0
(L)			5.1	5.12	20.5	6.4	4.5	8.3	38.6	48.5	14+8	7.1
(1)	6.9	5.* 6	4.5	4.4			91.6	69.5	24.2	14.7	50.4	52.6
(L)	5,9	5.7	7.0	15.1	65.0	103.2	75.0	59.0	13.4	209.6	20.6	22,4
					ΗY	-57	.	*****		to	be Coi	ntinu
-	(N) (L) (F) (K) (L) (F) (M) (L) (F) (F) (F) (F) (F) (F) (F) (F		$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	(N) 28.6 15.6 13.0 (L) 20.9 17.8 10.3 (F) 38.7 24.1 15.5 (L) 31.2 25.6 12.3 (F) 11.0 7.9 7.6 (M) 10.1 7.2 7.5 (L) 8.1 9.6 $c.8$ (F) 23.7 12.2 9.1 (L) 8.1 9.6 $c.8$ (F) 23.7 12.2 9.1 (L) 13.2 12.2 9.2 (F) 13.7 11.0 6.2 (L) 13.7 11.0 6.2 (L) 13.7 11.0 6.2 (L) 14.4 9.9 $c.6$ (K) 23.4 14.3 9.0 (K) 13.7 11.6 7.2 (K) 14.4 9.9 $c.4$ (L) 14.2 <	(N) 28.6 15.6 13.0 11.4 (L) 20.9 17.8 10.5 10.0 (F) 38.4 28.9 10.9 12.6 (K) 38.7 24.1 15.5 10.8 (L) 31.2 25.6 12.3 9.7 (F) 11.0 7.9 7.6 7.4 (M) 10.1 7.8 7.5 7.3 (L) 8.1 9.6 $c.8$ 7.2 (F) 23.7 12.2 9.1 6.7 (L) 8.1 9.6 $c.8$ 7.2 (F) 13.7 12.2 9.1 6.7 (L) 13.2 12.4 0.2 12.1 (F) 16.0 11.9 9.6 7.6 (H) 13.7 11.0 6.2 9.3 (L) 11.9 12.6 7.0 7.4 (F) 18.4 10.8 7.2 6.5 (L) 16.9 <	(N) 28.6 15.6 13.0 11.4 14.0 (L) 20.9 17.6 10.5 10.0 92.1 (F) 38.4 25.9 10.9 12.6 9.6 (K) 38.7 24.1 15.5 10.6 9.5 (L) 31.2 25.6 12.3 9.7 $o2.2$ (F) 11.0 7.9 7.6 7.4 7.1 (M) 10.1 7.2 7.5 7.3 8.0 (L) 8.1 9.6 6.8 7.2 35.3 (F) 23.7 12.2 9.1 6.8 6.6 (Y) 18.9 11.1 7.6 6.7 14.2 (L) 13.7 11.0 6.2 9.3 7.3 (L) 13.7 11.6 6.6 6.3 6.3 (K) 13.7 11.6 7.2 6.5 6.2 (L) 14.4 9.9 6.6 6.3	(N) 28.6 15.6 13.0 11.4 14.0 21.4 (L) 20.9 17.8 10.5 10.0 92.1 73.0 (F) 38.7 24.1 15.5 10.6 9.6 11.9 (R) 38.7 24.1 15.5 10.8 9.5 9.6 (L) 31.2 25.6 12.3 9.7 $o2.2$ 9.7 (F) 11.0 7.9 7.6 7.4 7.1 8.4 (M) 10.1 7.2 7.5 7.3 8.0 7.2 (L) 8.1 9.6 $c.8$ 7.2 35.3 6.3 (F) 23.7 12.2 9.1 6.8 6.6 98.0 (F) 16.0 11.9 9.6 7.6 7.4 7.4 (L) 13.2 12.2 9.3 7.3 7.5 (L) 13.7 11.0 $b.2$ 9.3 7.3 7.0 (L) 11.9 12.6 7.0 7.4 21.1 7.0 (F) 23.4 14.3 9.0 $c.6$ 6.3 50.0 (K) 22.1 11.5 7.6 6.5 9.1 55.2 (L) 16.9 13.2 $c.0$ 6.4 7.2 22.5 (L) 16.9 13.2 $c.0$ 6.4 7.2 22.5 (L) 16.9 9.9 $c.6$ 6.4 7.2 22.5 (L) 16.9 9.9 $c.6$ 6.4 7.2 22.5	(N) 28.6 15.6 13.0 11.4 14.0 21.4 17.0 (L) 20.9 17.8 10.5 10.0 92.1 73.0 28.2 (F) 38.7 24.1 15.5 10.6 9.6 11.9 9.0 (K) 38.7 24.1 15.5 10.8 9.5 9.6 10.9 (L) 31.2 25.6 12.3 9.7 $o2.2$ 9.7 10.3 (F) 11.0 7.9 7.0 7.4 7.1 8.4 $o.7$ (M) 10.1 7.2 7.5 7.3 8.0 7.2 (L) 8.1 9.6 $c.8$ 7.2 35.3 6.8 6.0 (F) 23.7 12.2 9.1 6.8 6.6 98.0 84.7 (K) 18.9 11.1 7.6 6.7 14.2 22.5 127.4 (L) 13.7 11.0 6.2 9.3 7.3 7.0 19.8 (L) 13.7 11.6 6.2 9.3 7.3 7.0 19.8 (L) 11.9 12.6 7.0 7.4 21.1 7.0 19.5 (F) 23.4 14.3 9.0 $c.6$ 6.3 50.0 26.5 (K) 22.1 11.5 7.6 6.5 9.1 55.2 81.8 (L) 13.7 10.8 7.2 6.5 6.2 6.0 7.4 (H) 14.4 9.9 6.6 6.5 9.1 <td>$\begin{array}{c c c c c c c c c c c c c c c c c c c$</td> <td>$\begin{array}{c c c c c c c c c c c c c c c c c c c$</td> <td>$\begin{array}{c c c c c c c c c c c c c c c c c c c$</td> <td>$\begin{array}{c c c c c c c c c c c c c c c c c c c$</td>	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $

SIMULATED 10-DAY MEAN RUNUFF

	tinua				ATTOG			73, (50				UNIT	сн
YEAR		NAL	FEU	MAR	APR	YAH	JUNE	10LY	AUG	SEPT	ÚC T	110 V	DEC
1963	(F) (た) (し)	13.7 	11,2 12.6 17,8	10+4 3+9 7+0	7.7 7.0 5.8	5.3 5.2 13.4		101+1 56+8- 41+5	81.5 59.9- 89.1	44.6 44.9 66.4	39,7 45,9- 32,6	20.5 18.6 27.8	49.
1964	(F) (F) (U)	19.7 16.9 13.8	14.C 13.6 26.5	14+6 14+6 14+9 10+2	9.3 8.9 7.9		39.3	46.7 39.0 59.5	59.4 35.9 26.0	36.1 66.4 78.2	80.0 40.9 40.7	76.6 217.5 150.2	75. 115. 52.
1965	(1) (M) (L)	29.4 64.6 53.2	31.7 23.0 26.3	10.7 10.0 13.4	13.3 12.3 12.8	13.6 14.0 13.9	37.6 32.9 29.8	33.0 44.4 77.8	40.0 36.2 20.8	36.8 24.0 55.4	19.1 27.6 15.0	17.7 14.6 14.3	14. 15. 15.
1966	(E) _(E)_ (L)	13.6 <u>11.9</u> 10.0	8.8 2.5	9.9 4 7.0	7.3 0.4 6.5	13.7 24.4 58.9		28.4 157 17.7	36.4 31.2 47.9	16.1 13.9 11.8	11.1 10.2_ 8.8	29.1 60.8 138,9	82.
1987	(E) (P) (L)	46.1 48.2 24.0	18.4 16.9 18.6	13+1 13+5 6+6	9.7 7.4 9.2	7.9 8.5 8.8	23.8 13.0 42,4	29.7 19.1 62.3	44.0 47.7 56.6	57.6 62.8 50.7	82.2 81.0 27.0	81,4 38,0 22,2	37. 25. 22.
1968	(F) (N) (L)	17.0 14.8 11.5	10.4 9.8 11.2	10.4 0.4 0.5	5.9 5.6 123.3	71.8 18.7 16.5	55.8 42.9 100.6	61.9 20.7 70.5	103.4 120.4 82.1	94.8 32.7 27.4	27.9 29.0 19.1	19,3 17,5 16,1	14. 13. 10.
1969	(E) (E) (E)	10.4 10.0 8.4	8.6 7.6 	5.8 	5.6 5.5_ 5.5	5.4 4E.1 7.9	8.4 19.2 7.3	7∍0 5.8 14.7	7.2 	34+3 9+4 23+3	41.7 13.5 9.2	8.5 6.9 28.8	16. 22. 49.
1970		101.0 42.0 13.7	12.3 . 10.0 . 11.0	0,55 7,7 0,5	8.1 6.3 5.7		63.6 48.5 10.4	7.8 9.9 38.2	15.4 9.9 37.4	22.2 81.6	27.1 140.9 86.7	59.1 58.0 103.6	122. 98. 33.
1971	(F) (M) (L)	52.0 24.1 18.1	17.5 14.9 33.5	15.0 35.4 15.9	12.0 _9.8 _5.6	31.0 145.5 45.1	23.7 27.8 18.6	46.9 82.0 88.4	37.8 16.1 53.6	102.7 61.4 64.4	170.4 .85.6 40.4	49.6 35.8 116.3	56. 50. 50.
1972	(f) (<u>K)</u> (L)	51.4 24.5 37.9	21.9 18.6 20.8	13+9 12+2 10+4		10.4 46.8_ 45.8	30,4 <u>13,7</u> 12,0	45+1 <u>57+9_</u> 35+1	64+2 117+9_ 37+1	50.8 26.8 17.4		-35-2 15-2- 15-4	
1973	(F) (K) (L)	9.2 8.3 6.8	8.7 7.1 8.1	5,9 5,9 10,0	5.8 5.7 5.6	5.6 25.3 18.0	6.7 .00.0 42.8	27.7 10.6 11.0	18.0 85.7 149.8	93.4 33.6 37.0	7458 94.2 53.8	35.2 21.0 105.0	37. 22. 16.
1974	(F) (E) (L)	16.8 17.2 15.4	14.1 12.2 13.1	9.8 8.5 7.0	6.4 8.2 6.2	5.4 5.4 4.8	11.1 68.1 30.0	34.4 21.3 10.5	9.1 23.6 12.8	33.9 11.2 44.4	12.8 80.1 116.5	88.1 40.9 58.2	33, 77, 29,
1975	(F) _ <u>(F)</u> (L)	21.9 57.8 _ 34.4	18.0 12.5_ 20.1	14.2 12.0 5	9.0 	7.6 6.2 7.9	18.2 5 6.6	9.0 15.2_ 9.2	10.5 .0.3 9.2	42.8 17.5 10.1	8.8 28.2_ 16.6	35.9 22.2 12.5	22. 65. 33.
1976	(1) (7) (1)	14.0 11.5 8.7	8.1 7.2 8.7	43,4 19,1 7,3	30.4 9.0 5.8	42.3 24.4 132.8	87.2 23.2 69.8	38,5 17,4 39,7	65.9 63.1 35.5	52.9 112.0 81.1	60.8 51.8 27.0	23 1 27 9 22 0	19, 28, 16,
1977	(f) (F) (L)	16.4 16.2 15.8	14.6 13.2 14.4	9.7 9.2 7.5	10.2 7.7 6.4	6.2 5.6 84.4	24.9 34.3 21.7	32.0 39.0 48.9	88.8 37.1 37.3	34.4 59.1 28.7	23.9 19.0 12.9	15.5 79.6 41.2	19. 15. 11.
1978	(F) _(K) (L)	11.2 9.5_ 7.8	7.8 	υ.5 α.1 4.7	5.0 	6.2 4.9 32.1	40.1 39.3. 14.1	8.3 20.2- 38.0	16.1 11.4. 94.4	57.1 75.0 81.8	78.1 	7+ 59 	21. 19. 26,
1979	(f) (f) (L)	19.8 10.1 13.2	12.1 10.1 11.7	0.8 7.7 6.4	5.9 5.6 33.5		107.5 42.0 61.6	42.3 35.5 50.3	62.0 46.0 17.1	38.0 40.3 74.9	106.0 68.1 25.6	35.Q 45.0 49.9	26. 18. 16.
1980	(F) (M) (L)	15.4 13.5 10.4	16.2 9.3 11.5	6.6 6.0 46.9	10.5 30.9 9.9	8.0 35.0 49.3	12.6 9.6 9.0	11.4 49.1 38.9	52.5 22.3 26.4	23.1 60.6 40.3	32.6 38.6 117.8	33.6	22. 27. 17.
1981	(f) (出) (L)	16.8 14.9 12.2	12.6 11.£ 13.0	9.5 ; <u></u> 	5.5 	17.2 58.5 134.9	104.4 76.3 73.5	97.0 145.5- 68.2	29.5 	81.3 75.1 52.2	27.0 24.4. 98.7	64 -6 40 •1 56 •9	25. 20. 16.
1982	(f) (M) (L)	16.6 15.1 12.1	11.6 10.6 12.C	9.3 7.1 46.9	40.3 64.2 55.5	24.5	61.3 48.7 38.4	36.5 70.3 49.2	46.0 20.9 76.9	74.8 53.8 35.1	20.4 36.4 17.2	26.9 19.5 25.4	22. 16. 14.
1983	.(M) (L)	13.9 14.1 11.4	10.7 9.9 11.2	6.7	6.2 6.2 6.1	6.0 7.4 5.4	5.7		13.4	6051	47.4 88.5		7.
	(F) {23} (23) (し)	7.5 6.9 5.8	k .9 6 . 1	4.3		98.9 52.1 HY	52.0, 21.3			17-1	38.2) is. 11.

.

SIMULATED 16-DAY NEAR PUROFF

	Cor	tinu	ation			LT 1 0 11			LILANGA .					
						ATHAGE								: CHS
	YEAR		JAN	FE0	** A R	4 F K	M A Y		10CY	AUG	S E P T	0 ¢ T	NOV	080
	1963	(F) (P)	38,3 34.9	31.1	2019		15+4		182.0		83.3 . 85.5_	76.5 	50.7	95.1 127.8
		(L)	29.9		14.9					100.1	120.2	63.3	51.0	57.6
	1964	(T) (H)	48.4 43.9	36.9 35.1	34.0 32.3	24.9. 23.1	19.5 18.6	65.1 70.6	81.1 67.8	107.5	65.8 123.0	149.3	146.1	146.7
		(1)	37.0	49 9	23.7	50.5	70.0		107.3	45.1	145.1	88.9	283.6	106.6
	1965	(1)	74.3	53.6	30.5	25.0	21.2	23.0	113.5	36.0	6.03	31.0	83,4	33.0
		(E) (L)	. 68.6 55.3	.47.4. 52.6	26.3	23±1 2159	20.9	20.8 57.1	153.7	41.7	37.8 34.6	64.7 28.8	34.5 38.0	37.5 34.6
÷.	1966	(1)	31.8	23.0	12.5	16.7	76.2	44.9	44.5	32.0	24.5	25.0	\$3.7	189.1
	•	_(Ľ)	28.4 22.9	20.4	17.2.	16.4 16.2	24`Q_ 50.1	42.9	8.0 <u>7</u> 29.0	26.7_	23.5_		147.1	-113.S 218.0
	40.0										98.8	101.3	63.5	31,1
	1967	(T) (7)	99.4 61.5	50.6 47.1	37.3	27.6	20.9 18.5	23.3	74.1	54.6	35.5	40.3	36.8	29,4
		(1)	49.5	52.2	24.9	24.3	16.4	64.1	49.0	31.2	32.3	30.1	32.1	25.0
	1968	(E) (M)	24.1	19.0 16.4	15-1	14.4	18 9	129.1	28.9	93.5 195.3	41.1	44.3 52.6	34.7	30.1 50,3
		(1)	15.7	19.2	15.3	19.4	12.3	56.3	28.1	60.9	112.1	34.0	36.3	30.9
	1969		30.4	3.95	14.2	13.6	13.0	33.1	13-1	51.5		169.7	29.3	127.0
		- <u>(E)</u> (L)	28.2 21.8	15-13 9.05		13,2	21,6	14.5	10•6	35.5	27.3	28.7	139,5	115.5
	1970	(13-	105.3	19 E	29.8	20.0	16.4	13.1	20.5	66.5	29.5	145.1	146.5	194.0
. •		(h.) (L.)			- 24,1 19,9	20.6	14,0	30,2 34.1	17.9.	23.3	81.7 36.6	126.1	126.6	188.0
	1971	(F)	95,9	48.0	37.2	34.2	27.1	65.0	79.8	66.5	101.1	205.5	198.4	389.1
	1471	(內)	\$4.3	47.0	121.9	.27.7	60.0	166.8	174.2	103.5	237.7	269.8	266.7	243.8
		(1)	\$0.6	53.0	35.8	24.5	26.7	70.8	71.0	109.1	93.0	207.8	408.5	195.7
	1972	(1) _(2)	194.9	25.0 	61.3 557	47.4	50.9 _115.2.	68.7 51.7	99.6 53.6	48.Z 45.0.	43.9 41.1_		36.5 .33.2	59.7 _ 38.1
		(L)	86.7	87.2	44.5	62.5.	145.8	76.0	44.0	39.6	40.0	31.1	102.3	32.7
	1973	(T) (M)	32.3 29.8	36.6	23.5 23.5	22.8 22.4	21,8 21,4	155.1 109.3	41.7	78.5	39.6 74.9	74.5 230.2	143.2 255.0	242.7
		(L)	26.1	24.5 30.2	21.0	22.1	19 Z	100.1	61.5	41.5		101.4	378.1	67.2
	1974	(1)	1.33	54.0	20.9	26.6	51.8	126,1	55.2	22.2	50.0	245.9	336.5	104.8
		(٢) (L)	60.9 52.3	48.1 53.5	23.7 20.9	23.3	31.3 19.9	33.4 27.0	41.7 21.5	49,5 21,8	32.8 45.1	295.9 330.9	235+6 124+6	233,4 138,9
	1975	(E) ⁻	0.83	62.7	42.8	30.4	22.4	25.8	29.8	33.6	20.3	24.1	77.0	89.7
		<u>(۲)</u>						26.\$_ 40.5	26.5_ 32.7	27.15.		73.9	34.7. 32.8	78.4
										155.0	31.4		136.0	128.0
	1976	(F) (K)	91.8 45.1	36.4 31.2	24.7	20.9 20.4	17.5	67.0 29.9	34.0	47.8	95.5	33.2	210.9	183.8
		(L)	35.7	35,1	19.3	17.8	98.9	84.1	30.1	10.3	37.8	05.5	282.3	83.8
	1977	(f) (K)	61.2	50.3 45.5	34.4 30.1	24.4	18.2 17.9	20.0	16.7 16.5	21.9 16.8	16.9	30.6 24.9	20.5 130.6	28.1 25.8
		ίÛ	50.5	C.9	24.4	18.5	66.5	17.6	14.9	15.2	91.7	20,3	42.8	21.4
	1978	(T)	20.1	13.9	13.2	12.6	12,1	12.7	11.1 10.9.	38.4	93.1 88.3.	66.9	57.0	40.1
		(Ľ) (L)	<u>17.9_</u> 14.6	16.8	11.7	12.5_ 12.3	<u>119</u> 30.8	11.6. 11.3	9.8	82.8	88.9	133.0	75.3	68.5
	1979	(F)	37.9	24.8	17.4	12.1	11.6	120.5	59.0	72.9	188.0	92.8	68,3	38.4
		(h) (L)	34.5	21.0 24.6	14.2 11.2	11.9	14.4.	. 32.9	154.2	103.9	115.0 53.1	49.6 39.8	46.0 42,4	35.6
	1980	(1)	30.7	22.6	17.7		13.6	13.6	12.0	13.9	16.3	18.3	256.9	57.3
	1700	(2)	27.2	20.2	14.9	14.2	13.6	13.0	17.3	13.2	14.4	13.8	110.0 57.2	104.5
		(L)	3,55	23.5					17.7	11.1				41.3
	1981	(F) (K)	37.0 35.0	27,7 21.0	17.4	11.9 11.8	11.4 	48.8 	27.3 	46.7 76.4_		30.9	137.y	45.7 40.1
		(U)	29.7	24.9	11.0	11.6	10.1	21.6	20.4	28.2	48.0	116.5	71.9	31,1
	1982	(F) (M) [32.6	26.4 19.0	13.5 12.3	11.9 11.8	11.4 11.2	10.9 17.7	12.0 11.6	10.1	90.4 74.6	19.6 25.5	25.4 56.5	56.5
		(L)	22.0	20.8	11:0	11.6	10.1	17.7	9.3	35.3	21.0	22.2	35.8	23.0
	1983		36.7	22.0	14.8	10.0	9.5	10.8	8.3	δ.4	8.4	78.0	46.7	18.
		(l.) (l.)	23.5	19.3 20.2	11.7 7.2	9.8 9.6	13.5	10.8 10.0	8.7 7.8	8.3 8.9	7.9 35.0	19.1	39.6 20.5	17.1
	1984	(1)	12.0	9.5	7.4	7.1	59.1	12.6	111.8	87.5	35.9	23.9	84.0	63.0
		(N) (L)		7.7	7.•4 6.9		31.0	12.0.						
					******			HY-59						

to be Continued

.

************* SIRULATED 10-DAY HEAN RUNOFF

.

.. -

 					ATTAGE			LARION/ 555. (SC	\LTO }.KM)				г : сн
YEAR	******	JAN	FEL	PAR	APR	MAY	1086	JULY	AUG -	SEPT	001	NOV	DEC
	(F) (K)	24 8 21_2	12.9	ə.ö 						101.1.		15.0	92.4 114.4
1964	(L) (F)	15.3	12.6	5.6 20.6	5.2	4.5		59.4	19.5	75.8		10.8	35.4 198.1
	(n) (L)	17 7 12 4	8.4	7.2 0.0	4.6	4 . S 1 5 . 7	42.0 28.1	52.9 61.1	157.0	46.8	78-5	375.8 400.8	142.0
 1965	(F) (M) (L)	57.5 49.6 41.0	38.7 32.1 33.4	21.4 10.5 13.3	12.7 10.7 9.4	8.8 7.4 50.0	16.5 42.8 39.4	16.8 255.1 113.2		119.8 46.7 99.0	38.1 67.7 27.8	83.3 35.9 32.1	25.1 22.1 17.4
 1966	(f) (K) (L)	15.4 	10.1 8.9 10.7	7.8 4.4 6.5	6.2 7.4 5.5	87.5 58.2 136.6	91.4 48.9 56.5		77.4 _111.4 114.4	55.4 45.4_ 28.2	33.1.	86.6 117.0 348.6	166.0 104.3 129.0
1967	(F) (M) (L)	65.6 44.5 34.4	31.2 25.8 26.5	17.0 13.5 10.8	144.4 46.3 20.1	15.1 16.7 18.7	44.4 16.0 208.9	68.6 28.2 34.8	61.7 126.4 187.5	115.3 72.7 44.7		136.3 82.5 51.7	43.1 37.4 29.4
 1968	(F) (M) (L)	28.3 23.5 17.5	15.4 14.2 15.9	11.6 10.0 7.6	6.8 6.7 17.3	11.2 6.9 7.3	46.0 51.4 49.0	27.8 75.1 87.0	146.7 261.3 122.0	77.7 40.6 226.9	105.5 54.4 34.7	32.2 28.4 24.3	20.1
 1969	(F) (N) (L)	12.0 10.9 8.8	7.8	0.0 <u></u>	14.6 5_8 5.7	5.7 	93.8 			70.7 		24.1 	
 1970	(F) (N) (U)	38.7 23.0 17.4	14.9 11.2 12.8	9.0 .0.6 .53	14.5 10.5 	53.8 42.1 	55.6 25.1 15.6	14.2 102.6 31.9		45.9 49.0 69.6	108.3	206.4 131.2 114.5	
 1971		41.0 . 34.3 25.0	24.1 27.4 26.1	10.3 15.6 10.7	9 8 8 7 7 0	9.5 14.0 9.9	52.1 45.9 15.8	39.5 157.1 71.4	46.2 50.3 21.2	27.0 89.1 94.4	251.7 182.9 153.9		258.2 169.2 103.4
 1972	(7) _(8)	103.6 	47.5 	20.4 27.4 20.5	17.2 16.0 14.8	17.1 	59.7 25.6 59.8	60.9 	68.4 74.0 83.6	96.0 	29.5 	41.2 22.2 43.9	
1973	(f) (K) (L)	16.7 13.4 10.0	10.8 9;8 10.9	7.3 0.7 6.3	6.5 6.4	10.7 27.0 8.5	10.5 61.2 42.5	25 2 33 4 15 8	65.3 54.8 98.5	43.5	115.4 242.4 120.7	89.6 184.0 461.8	216.4 101.7 56.4
 1974	(F) (P) (L)	51.8 43.4 33.3	30.3 24.8 25.7	15.9 14.2 11.1	11.0 9.6 11.3	26.3 12.0 11.6	70.5 24.4 21.9	17.5 16.3 13.2			164.4 131.6 161.5		72.4 114.4 75.3
 1975	(F) (E) (L)	46.9 <u>39.2</u> 29.5	24.5	14.5 14.4 11.0	11.2 7.7		27.5		73.8 39.6 84.1	45.8	145.5 115.5 173.4	89.6 64.4 35.7	31.7 53.5 68.7
1976	(F) (K) (L)	39.4 27.8 21.4	18.8 14.7 14.9	10∓8 9∓4 10∓0	22.3	6.7 9.5 76.2	31.3 82.6 77.4	26.9 .17.8 52.1	54.0 43.7 73.3	25,9 77:9 31:3	40.8 27.0 107.0	132.3 144.1 70.5	35.6 46.6 28.5
1977	(L) (K) (F)	26.2 22.2 17.5	15.1 11.7 . 13.2	9.0 	5.5 5.5 5.4	5.4 5.3 24.1	34.1 31.6 23,1	25.6 33.6 175.7	133.2 79.5 53.0	138.1 268.2 176.1	59.8 61.8 36.4	38.7 98.8 48.2	31.9 27.4 22.1
 1978	(F) (81) (L)	19.9 16.1 11.9	11.4 10.4 11.7	5.0 7.2 5.6	5.3 	5.3 5.1 60.9			65.2_	115.1 131.0 122.6		94 • 1 - 141 • 5 - 61 • 8	55.9
1979	(F) (M) . .(L)	30.7 25.9 20.0	19.2 16.0 16.0	11.4 y.7 7.2	6.6 5.8 6.5	5.3 .38.2. 40.8			35.6 44.9 19.1	31,8	136.0 120.8 39.5	120.1 78.2 44.4	28.4 24.3 44.9
1980	(F) (N) (L)	23.6 _19.2 13.7	11.7 12.9 12.7	5.8 7.3 10.3	7.0 6.7 5.3	73.1. 23.5		179-3	76.3 84.6 42.0		38.0 25.5 187.9	204.0 119.2 60.6	48.0 69.2 34.2
 1981		28.9 24.7 18.1	15.8 1.2.1 13.5	9.4 	5.0 4.9 5.6	77.6	98.8 121.3_ 57.5	32.2		25.2 1.18.9 40.2			42.5
 1982		22.7 19.0 13.8	11.5 10.6 12.1	ឋ - 1 ៤ - 7 4 - 7	5.7 13.6 5.6	5.0 47.1 34.8	37.7 13.2 13.1	11.0 9.6 9.9	41.2 33.2 57.5			42.1 108.9 110.4	101.5 48.8 35.1
 1983	(F) (K) (L)	3011 .4810 2311	20.2	1U.U 6.9 7.4	6.9 5.3 4.6	4.5 6.1 5.6	4 . 4 5 . 7 4 . 4	4.2 4.2 4.5	41.0 19.3 8.3	102.3 28.2 25.1	79.0	44.9 26.0 37.9	21.6 18.0 12.8
 1984	(F) .(<u>K</u>) (L)	10.6 7.9 6.4	5.8 4.7 	ن د د 	3.7 <u>9.0</u> 35.0	39.4 14.5 65.9	_32.9		_55.6.	121.0 49.4 36.0		55.3 61.2 38.4	92.2

****** SINULATED 10-DAY KEAN RUNDEF

Con	tinu	ation			1110H			MPANILE					
		****		DR	ALUAGE	AREA :	7	51. (SO	«KH)				: CH
YEAD		јлн 	FEN	•	AP8		JUNE	JULY	λUG	SEPT	001	NOV	D 8 C
1963	(F) (II) (L)			o.1 u.4_		5+8 54+7-	86.1 55.2		95.7 		28.0 23.9.	16.2 16.0.	
1964	(1)		12.5	5.5 0.0	5.9 5.5	27.1	120.0	99.4 72.7	69.3 196.9	60.6 120.4	17.8	36.4	56.
	(M)	16.2	.9.7 10.4	5.6 5.0	5.4 5.4	20.4	93.0	73.8	146.4	99.0	66.6 31.2	86.9 153.0	147.4
1965		32.1	21.6	12.7	12.5	72.7	86.9	44.8	68,9	64.2	28.9	22.5	13.4
	(N) (L)	28.0	18.5	10.81 9.3			74.0 36.3	125_1 190_7	85.9 55.8	30.2 48.4	22.8 32.5	19.1 16.5	13.1 11.4
1966	(†) (8)	11.0 10.1	7.4	5.8 5.8	5.6	43.8	92.1		148.8	65.5	20.5	23.7	138.
		7.9	7,4	5,2	38.0	101.5	34.6	54.8	67.5	22.5		197.1	25.
1967	(*)	23.8 21.1	14.6 11.7	9.3 7.4		5.4 33.4			174.6	142.8	157.6 221.1	216.9 79.3	38. 33.
	(L)	16.4	13.3	5 . 1	9.5	9.7	109,3	252.0	184.5	202.1	70.5	44.1	25.
1968	(1) (3) (1) 1	24.2	15.2 13.7 14.9	11.3 11.4 17.4	10.4 12.0 54.2	37.6 117.6 	69.3 148.7 178.4	124.8	123.9	170.1 139.7 292.9	141.4 71.7 39.5	38.5	28.
1969		18.1	12.7	7.7	9.3	30.5	126.3		205.0	79.5	71.6	33.3 28.0	19. 27.
	(N) (L)	<u> 16.2</u> 13.1	10.9 11.9		30.5_ 7.3	61_4 71.3				68.7_ 64.8		25.2. 46.4	
1970			1513	1.0.8	11.6	103.1	121.4	35.0	66.9	94.5	138.1	116.6	48.
	(L)	21.9_ 16.8	15.0	16.9	53.1		58.1	6319 6417		190.0. 104.6	159.8	88.6	28 (
1971		31.5	19.3	14.8	12.4	9.4	27.8	47.4	72.4	84 8 54 1	223.0	54.4	33.
	(L)	20.7	21.9	13.0		17.8	28.9	128.9	90.4	130.7	52.5		25.
1972	(1) (2)	21.4		10.3	7.9	95.0 <u>54.9</u>	139.8	90.9 258.5	88.7 			21,1 · 	
1973	(L) (L)	17.5	15.3 6.7	7.6 0.4	51.7 6.2	102.5	6C.2	180.3 63.3	56.0 58.5	92.6	20.9	15.7	10. 51.
	(N) (L)	9,3 7,2	6.6 8.1	. U.4 5.7		_121.5 71.6	26.3	59.7 40.1	75.7 69.7	84.1 65.3	193.7	35.3	30. 24.
1974		23.2	15.0	9.7	18.5	43.7	147.1	24.5	77.5	70.0	76.6	233.5	38,
	(H) (L)	19 5	12.9	7.8	101.6	24.8 52.5	22.1	73.0	13124 12355	37.7 81.5	234.8 183.9	96 • 4 58 • 9	69. 33.
1975	(F) (M)	30.3		13.5			75.8	53.3	71.7		49.0	40.9	19 .18
· ·	(L)	21.8	17.9	9.3	9., 1	42.7	22.2	69.2	81.8	1 A	37.7	21.2	16.
					_ 11.4	7.5	134.7	127.5	29,3	62.1	.86.9		22
1977	(L) (L)	10.5	9.3 10.7	9.0 0.0	6.7	105.0 5.5	32.9	71.8 97.6	47.9	83.3 54.6	29.7 61.7	25.6 24.6	23.
		13.8 10_8			23.1.	5.4. 20.1		93.0 97.3	46.9	252.7		107.0	21. 15,
	(7)	14.5	9.0	5.3	5.2	12.0	12.8	116.6	24,3	69.1	50.2	17.5	14.
	(Ľ).	<u>11.9</u> 9.8	7.8	4.9	<u>15-0</u> 9-1	23.7	838 36.7	62.8_ 87.9		170.3	24.3 19.2	31.5 16.9	10.
1979	(F) (K)	9.9	6.8 5.4	4.7		41.9	94.0	27.3	42.2	16.3	16.2	17.5 23.8	17. 16.
	(L)	7.5	6.0	4.2	60.8	19.6	38.4	49.0	13.7	15.1	19.1	37.2	18.
1980	(8)	13.7	9.1 7.4		4.0		27.7		85.9 75.2		36.4	153.5	28.
1981	(L) (L)	10.0	8.1 10.3	3.8	4.0 4.4	104.9	10,7 163,2	191.5 76.5	72.4	52.9 36.7	149.1	36.3	19.
				<u>4.5</u> 4.0			_1.2.7.1_ 64.4						
	(1)	14.2	8.3	4.5	6.9	8.4	-13.1	52.7	56.3	117.0		42.6	36.
	(M) (L)	11.4	6.9 7.1	4.4 4.8	15.8 5.1	12.5	64.4 44.5	14.4 32.3	81.1 24.5	60.5 134.3	66.6 22.1	45.3 23.4	26.1
1983		17.5 15.8	10.6	5.Ú 6.1	4.3	4.1	16.0 25.2	12.3	88.1 49.8	33.4	42.1 74.8	19.6 18.5	12.
		12.5	10.7	4 Ŭ	4.2		11.4	132.3	51.0	20.2	40.2	15.6	10.
1984	(F) (ሸ)		4.5	5.9 14.0	110							30.7 	62.
	(L)	5+4	4,9	11.2		41.9	14.6	25.8	218.2	13.9	63.6	22,5	15

******* SIMULATED IG-DAY HEAN PUNOFF

	Con	tinua	ition	· • ••• •••• ••••		λεμλος	AREA :	8	290° (20	(KM)		••• · ••	דנאט	: (115
	 Y[∧R	*-)	JAN	FEH	PAR	APR	на у	JUHE	JULY	AUG	SEPT	001	NOV	DEC
	1963	(1) (!')		12.7 14.5_	10.8 	9.3 9.2	१∎२ 1С∎4.	23.3 6.301 _	160.3 _130.9	45.8 31.3.	49.0 27.0	22.5	12 2 10 9	56.9
	1964	(L) (I) (I) (L)	12.6 21.9 16.1 10.1	15,4 9,8 5,6 19,5	8.0 39.0 9.9 7.3	9.0 7.9 7.5 7.7	7.6 7.5 22.3	145.4 57.9 65.9 48.4	40.5 17.5 17.6 45.3	30.1 140.9 101.0 78.6	26.3 76.2 85.2 105.4	14.1 120.8 76.7 72.5	10,2 170,6 386,9 330,2	33.7 156.7 125.8 88.7
	1965	(F) (K) (L)	50.9	22*0 23*0 23*0 23*0	10.1 14.0 11.2	واجدا المالمانين	149.8 41.0 66.9	75.4 91.1	30.6 151.5 167.0		134.0 76.0 54.2	32.S 39.5 23.8	51.5 25.4 30.0	23.8
•••••••••	1966	(F) _(E)	۱۶۰۶ اع، ۹ ۱۱۰3	11.3 11.1_ 13.7	10.6 10.6. 10.6.	10.3 <u>59.0</u> 99.2	81.0	95.0	56:5 73.7 92:3	43.9 90.4 97.1	52.6 57.4 31.4	29.1 48.3 70.9	90.8 115.7 294.6	123.3 75.5 88.3
	1967	(1) (ř) (Ľ)	43.5 33.7 24.5	19.5 16.6 19.1	13.8 12.2 10.7	65.5 15.9 19.0	12.4 17.0 24.5	88.5 23.4 162.1	86.1 32.0 74.0	82.5 119.1 101.6		203.6 241.1 63.1		45.9 32.3 24.7
<u></u>	1968	(†) (K) (L)	27.0 21.6 15.4	15.7 14.2 16.1	12+1 11+9 10+7	11.6 11.4 17.6	12+5 11-3 	46.2 44.5 31.5	41.0	136.5 257.9 107.1	75.7 37.0 168.6	01.4 46.1 29.1	24.6 18.2 15.2	13.9 12.0 10.4
	1969	(1) _(と) (と)	10.6 	10.2 	4.7 	9.3 9.1 9.0	8.9 22.4 11.9		81.7 40.8 245.3	106.5 38.5 26.4		102.5 52.1 26.5	24,4 43.8 65.9	52.3 34.1 23.5
	1970	(F) (P) (L)	40.5 21.4 14.8	12.7 11.3 12.6	A*0 - A*5 - A*2	8.9 8.8. 8.6	10.7 - 110.1 81.4	64.7 .28.0 18.4		79.5 54.7 92.7	68.2 72.7 50.9	49.3 104.4 146.2	157.6 162.6 110.1	78.(100.0 50.1
	1971	(f) (光) (L)	44,6 30,6 21,3	18,9 21,1 20,9	13.7 13.6 14.9	10.1 9.9 9.3	18+1 14+5 9-8	84.0 39.5 23.7	36.5 131.7 59.5	28.9 57.2 21.4		230.3 152.6 86.9	116.4 91.9 265.5	158.1 127. 69.2
•	1972	(1) _(<u>4)</u> (L)	69.3 38.0 38.7	23.8 17.7 20.2	14.6 	11.9 19.1 13.5	30.3 48.9 49.0	39.2	70.0 91.9 85.9	89.9 131.8 63.6	45.5 30.6 29.0		26.2 14.5 30.0	34.1 -17.8 13.0
	1973	(†) (Å) (L)	13.0 12.4 10.4	10.7 10.0 12.3	9.7 9.5 5.5	9.2 9.1 9.0	8 52 78	44.7 134.5 02.6	60.5 47.1 42.2	68.8 72.0 162.1	132.5 75.9 55.0	166.7 294.5 125.2	101.8 124.9 347.6	176.3 84.7 49.0
	1974	(f) (M) (L)	42.5 33.2 25.4	21.2 17.6 20.1	14.1 12.4 10.0	11.5 11.3 28,5	63.6 38.4 59.8	60.1 23,4 18,9	12.9 13.4 10.6	24.4 99.1 41.4	19.7 57.1 114.0	171.8 116.8 179.9	258 .1 198 .8 93 .5	64.6 122.6 68.1
	1975	(E) <u>(片)</u> (L)	42.2]3.4 28.6	23.9 17.9 20.3	14.2 12.6 10.9	13.7 1.1.3 11.2		81.0 144.4 61.3	89.6 68.2 26.2	63.2 40.9 151.9	59.4 45.9 27.3	25.3 	93.4 53.1 34.1	29.2
	1976	(1) (2) (L)	46.3 28.2 21.2	17.5 14.6 16.7	13.0 12.2 10.9	11.0 10.3 10.7	10.5 14.5 100.2	64.7 73.5 105.1	83.0 29.6 86.1	65.8 60.3 1C4.3	46+0 67+1 34+7	80.9 30.8 66.2	95 1 131 5 102 3	77.1
	1977	(F) (M) (L)	20.5 24.5 18.8	15.8 14.3 16.5	11.7 1u.9 ¥.7	10.5 10.4 10.2	10.1 9.9 35.0	31.9 74.4 78.4	28.1 27.6 133.7	165.1 62.1 39.8	64.8 119.5 113.0	40.5 29.5 20.6	21.6 55.6 29.0	20.1 16.1 12.1
	1978	(f) (<u>r)</u> (L)	13.0 12.0 9.7	9.3 9.7 	9.4 	9,0 8,9 8,7	8.6 <u>11.3</u> 49.8	42.6 44.9. 23.3	14.8 102.0 60.9	80.9 97.3 215.4	-106.4.	184.3 	68.6 76.8. 38.8	41. -56. 29.
	1979	(f) (A) (L)	24.6 18.8 13.5	16.5 13.7 15.5	10.8 10.3 7.2	10.0 9.9 9.7	۹.5 ۹.35 39.2	14.9 16.3 10.3	57.3 54.2 69.1	40.6 21.0 13.3	54.1 4G.2 20.3	80.4 99.8 28.2	95.0 83.5 49.3	27.5 24.6 57.0
	1980	(T) (h) (L)	25.4 19.5 15.0	12.6 11.5 13.6	9.0 6.5 7.9	5.5 5.4 8.3	E.1 155.5 60.3	33.7 17.7 24.9	85.7 29.5 89.5	3C.7 32.2 76.0	85.1 54.5 27.8	25.8	219.2 120.2 55.3	39 58 29
	1981	(f) _(K) (L)	25.5 21.8 15.0	13.7 12.3 13.8	9.6 9.5 0.5	9.2 9.0 10.5		186.8 	35.6 98.4 28.9	51.2 135.2 			160.5 .81.4 68.3	34.0 26.9 19,9
	1982	(f) (N) (L)	18.1 14.4 11.8	11.4 10.7 12.3	9.7 9.0 0.0	11.0 9.2 35.1	12.0 63.6 115.5	99.2 29.5 59.4	73.8 51.2 24.5	24.0 22.9 84.7	47.1		28.8 81.6 108.5	57.
	1983	(f) (g) (L)	27.7 46.3 22.7	18.3 13.3 15.6	10.7 7.0 7.2	9,5 9,4 9,2	9.1 11.0 8.0	8.7 19.0 10.1	8.3 9.9 59.0	90.1 54.2 33.5	69.1 67.0 43.0	95.3 60.7 86.2	53.0 27.8 38.8	97.1 65. 91,5
	1984	(F) _(M) (L)	38 +8 24 +8, 17 +4		4.3 	8+3 	91.2 30.5 92.3	49.5 101-9. 158.5	108.0 68.4_ 40.9	218.5	30.4	26.3. 108.9	47.9	

Sub- basin	Basin/1	Drainage area (km ²)	Basin rainfall (mm)		
1	1	1,150	3,300		
2	1	481	3,600		
3	1 .	733	3,400		
4	1	298	2,900		
5	1	351	2,800		
6	1	142	2,300		
7	1	477	2,750		
8	1	387	2,650		
9	1	193	2,500		
10	1	264	2,150		
11	1	1,106	2,080		
12	1	1,051	2,060		
13	2	620	2,500		
14	2	292	3,100		
15	2	550	3,500		
16	2	1,228	2,500		
17	2	628	4,000		
18	2	559	3,000		

Sub- basin	Basin/ <u>1</u>	Drainage area	Basin/2 rainfall
		(km ²)	(nun)
19	2	266	2,070
20	2	970	1,910
21	- 3	247	2,100
22	3	876	2,500
23		474	2,300
24	3 3 3	215	2,400
25	3	652	3,800
26	3	915	3,900
27	4	209	2,960
28	- 2	656	2,850
29	2	408	1,820
30	2	362	2,500
31	2	589	1,820
32	4	225	3,530
33	4	739	2,180
34	4	327	3,690
35	4	92	2,250
36	4	657	3,880

Notes:	/1	;	1 =	Upper Cagayan,	2 =	Magat,
			3 ⇒	Ilagan,	4 =	Lower Cagayan
			5 =	Upper Chico,	6 =	Lower Chico

12 ; Basin rainfall is assumed on the basis

of the isohyetal map for the period

from 1963 to 1978.

Sub- basin	Basin ^{/1}	Drainage area (km ²)	Basin/2 rainfall (mm)
			2,000
. 37	6	1,042	2,000
38	. 4	969	3,100
39	6	73	2,100
40 .	5	386	3,100
41	5	334	3,500
42	5	157	2,950
43	5	533	2,950
44	5	372	3,340
45	5	612	2,200
46	6	856	3,090
47	6	366	1,900
48	6	775	2,900
49	6	160	1,900
50	6	169	2,080
51	4	417	2,000
52	6	393	2,500
53	6	278	2,300

Basin	Runoff gauge	Drainage area (km ²)	Basin rainfall (mm)		Basin	Runoff gauge	Drainage area (km ²)	Basin rainfall (mm)
l. Upper Cagayan	Guinalvin	921	2,700	4.	Lower Cagayan	Larion Alto	655	3,880
2. Magat	Dulao	573	3,000	5.	Upper Chico	Ampawilen	751	3,270
3, llagan	Minanga	1,565	2,400	6.	Lower Chico	Pinukpuk	856	3,090

Table 3.6 Runoff Estimation

• •

Year	Jan,	per Cagâyan June → Dec. Annual	Nagat Jan. June → May → Dec. Annual	llagan Jan. June → May → Dec. Annual
1963	16.6	100.2 116.8	10.5 80.0 90.5	8.5 48.0 56.5
1964	20.3	128.4 148.7	16.1 102.8 118.9	11.9 61.2 73.1
1965	18.2	50.7 68.9	25.5 44.8 70.3	13.1 24.2 37,3
1966	16.8	78.3 95.2	15.1 55.8 71.0	9.1 36.2 45.4
1967	21.0	46.4 67.4	18.3 66.6 84.8	13.3 21.6 34.8
1968	10.1	62.7 72.7	24.3 71.4 95.7	5.9 29.0 34.9
1969	10.6	66.7 77.3	10.5 26.3 36.9	6.1 30.0 36.1
1970	18.1	85.6 103.7	19.4 79,4 98.8	10.8 39.2 50.1
1971	30,8	182.0 212.8	33.7 92.4 126.2	16.9 87.4 104.3
1972	50.2	42.5 92.8	25.1 46.4 71.5	29,5 24,4 53.9
1973	11.8	120.3 132.0	9.7 74.8 84.5	8.3 57.2 65.5
1974	19.6	122.6 142.2	10.6 60.9 71.6	13.1 58.1 71.3
1975	23.9	48.6 72.5	17.9 29.5 47.3	15.5 22.9 38.4
1976	23.3	90.1 113.4	27.4 70.2 97.6	12.4 42.2 54.6
1977	22.0	32.0 54.0	17.3 51.9 69.2	13.1 15.2 28.3
1978	9.5	59.6 69.1	10.6 70.1 80.7	5.2 27.0 32.2
1979	18.1	78.7 96.8	18.5 72.0 90.5	9.4 38.0 47.4
1980	10.3	49.1 59.4	20.3 62.9 83.2	6.4 22.3 28.7
1981	10.3	58.3 68.6	29.2 93.7 122.9	6.5 26.1 32.6
1982	8.6	34 0 42.5	33.8 58.3 92.2	5.6 14.4 20.0
1983	12.3	22.7 35.0	9.1 31.3 40.4	6.2 10.2 16.3
1984	16.7	64.9 81.5	23.8 54.2 78.1	6.9 30.0 36.9
Average	18.1	73.8 91.9	19.4 63.4 82.8	10.6 34.8 45.4
Sub-basin	$\overline{1}$	7 12/	137~ 20/	22/~ 26
Drainage Area (km ²)	\sim	6,633	5,113	3,132

	Si Jan,	ffu-Ma Jun	•	Jan.	Chico Jun		Ућ Jan,	ole Bas June	
Year	→ May	🥪 Dec	. Annual	-> May	→ Dec	. Annual	-> May	→ Bec.	Annua
1963	3.4	26,1	29.6	9.2	56.2	65.4	56.7	369.4	426.1
1964	5.3	33.6	38.9	9.5	95.8	105.3	72.7	552.4	625.1
1965	8.3	14.6	23.0	23.1	54.5	77.6	111.9	257.1	369.0
1966	4.9.	18,2	23.2	20.9	66.0	87.0	91.0	353.1	444.1
1967	6.0	21.8	27.7	11.5	97.0	108.5	95.1	358.1	453.1
1968	7.9	23,3	31.3	15.4	79.6	95.0	74.6	342.2	416.7
1969	3.4	8.6	12.1	11.0	71.5	82.6	49.0	275.1	324.1
1970	6.3	26.0	32.3	20.9	79.5	100,4	94.9	395.8	490.7
1971	11.0	30.2	41.2	11.4	77,8	89.1	118.6	601.8	720.4
1972	8.2	15.2	23.4	20.7	52.0	72.7	162.4	232.8	395.3
1973	3.2	24.4	27.6	12.8	85.9	98.7	54.1	479.2	533.3
1974	3.5	19.9	23.4	17.6	82.6	100.2	83.1	443.1	526.2
1975	5.8	9.6	15.5	17.6	57,3	74.9	98.9	238.0	336,8
1976	8.9	2Ż.9	31.9	12.9	63,7	76.7	101,8	358.2	460.0
1977	5.7	17.0	22.6	8.4	58,7	67,1	77.1	253.6	330.7
1978	3.5	22.9	26.4	7.4	60,4	67.8	46.6	330.9	377.5
1979	6.0	23.5	29.6	10.5	34.2	44.8	76.2	304.1	380.3
1980	6.6	20.6	27.2	15.9	63.4	79.3	74.4	297.9	372.2
981	9.6	30.6	40.2	12.6	60,1	72.6	82.4	347.4	429.9
1982	11.0	19.1	30.1	10.3	50.8	61.1	82.9	235.4	318.4
1983	3.0	10,2	13.2	8.3	41.2	49.5	50.1	158.0	208.2
984	7.8	17.7	25.5	14.8	\$3.5	68.3	85.4	298,5	383,9
lverage	6.3	20.7	27.0	13.8	65,5	79.3	83.6	340.1	423.1
Sub-basin	72	8. 3	77	40	1~"	49/	· .		
Drainage Area (km ²)		2,01	, ;		4,55	1		27,281	

Table 3.	7 Mean	Monthly	Runoff
----------	--------	---------	--------

						:						(Unit:	m³/s
POINT	JAN	FEB	MAR	APR	MAY	JUNE	JULY	AUG	SEPT	OCT	NOV	DEC	ANNU MEAI
1	42.5	28.2	20.1	18.3	36.4	63.3	58.4	64.1	68.7	103.2	134.4	96.3	61
2	19.4	12.9.	9.2	8.4	16.6	28.9	26.6	29.2	31.4	47.1	61.3	43.9	28
3	27.9	18.5	13.2	12.0	23.9	41.6	38.3	42.1	45.1	67.8	88.2	63.2	40
4	9.7	6.4	4.6	4.2	8.3	14.4	13.3	14.6	15.7	23,5	30.6	21.9	14
5	11.0	7.3	5.2	4.7	9.4	16.4	15.1	16.6	17.8	26.7	34.8	24.9	15
6	3.7	2.4	i.7	1.6	3.1	5.4	5.0	5.5	5.9	8.9	11.6	8.3	s
7	14.7	9.8	7.0	6.3	12.6	21.9	20.2	22.2	23.8	35.7	46.4	33.3	21
8	11.5	7.6	5.4	5.0	9.8	17.1	15.8	17.3	18.6	27.9	36.3	26.0	16
9	5.4	3.6	2.6	2.3	4.6	8.1	7.4	8.1	8.7	13.1	17.1	12.2	7
10	6.4	4.2	3.0	2.7	5.4	9.5	8.7	9.6	10.3	15.4	20.1	14.4	9
11	25.8	17.1	12.2	11.1	22.1	38.4	35.4	38.9	41.7	62.5	81.5	58.3	37
12	24.3	16.1	11.5	10.5	20.8	36.1	33.3	36.6	39.2	58.9	76.7	54.9	35
13	18.4	11.9	10.8	13.1	27.2	34.0	35.5	40.2	41.6	43.6	41.6	28.7	29
14	10.8	δ.9	6.3	7.6	15.9	19.9	20.7	23.5	24.3	25.5	24.3	16.8	16
15	22.9	14.8	13.4	16.2	33.8	42.2	44.1	50.0	51.6	54.2	51.7	35.7	36
16	36.5	23.5	21.4	25.9	53.9	67.3	70.3	79.7	82.3	86.4	82.4	58.9	57
17	29.9	19.3	17.5	21.2	44.1	55.1	57.5	65.2	67.3	70.7	67.4	45.5	47
18	19.9	12.9	11.7	14.1	29.5	36.8	38.4	43.5	45.0	47.2	45.0	31.1	31
19	6.5	4.2	3.8	4.6	9.7	12.1	12.6	14.3	14.8	15.5	14.8	10.2	10
20	22.0	14.2	12.9	15.6	32.6	40.6	42.4	48.1	49.7	52.2	49.7	34.3	34
21	6.3	4.8	3.4	2.8	4.2	7.0	6.8	7.4	8.1	11.9	15.9	12.2	7
22	26.6	20.2	14.2	11.8	17.6	29.7	28.8	31.4	34.0	50.3	67.3	51.6	32
23	13.3	10.1	7.0	5.9	8.8	14.8	14.3	15.6	16.9	25.0	33.5	25.7	15
24	6.3	4.8	3.3	2.8	4.1	7.0	6.8	7.4	8.0	11.9	15.9	12.2	1.
25	30.1	22.9	16.0	13.4	19.9	33.6	32.5	35.5	38.5	56.9	76.1	58.4	36
26	43.4	32.9	23.1	19.3	28.7	48.3	46.8	51.2	55.4		109.7	84.1	52
27	6.6	4.2	2.7	2.8	6.1	10.1	14.4	19.0	17.4	23.0	27.8	15.2	12
28	22.2	14.3	13.0	15.8	32.8	41.0	42.8	48.5	50.1	52.6	50.2	34.6	
29	8.8	5.7	5.2	6.3	13.0	16.3	17.0	19.3	19.9	20.9	19.9	13.8	34 13
30	10.8	6.9	6.3	7.6	15.9	19.9	20.7	23.5	24.3	25.5			
31	12.8	8.2	7.5	9.0	18.8	23.5	24.5	27.8	28.7	30.2	24.3 28.8	16.8	16.
32	8.5	5.4	3.5	3.6	7.8	13.0	18.4	24.4	22.4	29.5	35.7	19.9	20.
33	17.3	11.0	7.0	7.3	15.9	26.3	37.4	49.6	45.4	59.9		19.5	16
34	13.0	8.2	5.3	5.5	11.9	19.7	28.0	37.1		44.9	72.5	39.6	32.
35	2.2	1.4	0.9	0.9	2.0	3.4	4.8		34.0		54.3	29.7	24.
36	27.4	17.4	11.1	11.5		41.6		6.4 78.4	5.8 · 71.9	7.7	.9.3	5.1	4.
37	19.2	11.9	8.7	12.7	31.8	46.4	50.0	62.3	53.1	94.8 67.4	114.7 75.5	62.6 44.1	51. 40.
38	32.3	20.5	13.1	13.6	29.6	40.4	50.0 69.7	92.4	55.1 84.7				
39	1.4	0.9	0.6	0.9	23.0	49.0 3.4	3.7	4.6		111.7	135.2	73.8	60
40,	8.1	5.6	3.9						3.9	5.0	5.6	3.2	3.
41	7.9		3.8	7.5	23.6	32.5	43.1	41.0	41.1	33.3	26.3	14.5	23
42	3.1	5.4		7.3	23.1	31.7	42.1	40.1	40.1	32.6	25.7	14.1	22
42	10.6	2.2	1.5	2.9	9.1	12.6	16.7	15.9	15.9	12.9	10.2	5.6	9.
43		7.3	5.1	9.8	31.1	42.7	56.6	53.9	54.0	43.8	34.6	19.0	30.
	8.4	5.8	4.0	7.8	24.5	33.7	44.7	42.6	42.7	34.6	27.3	15.0	24.

(to be continued)

(Continuation)

(oone ne	wation)											(Unit:	ia'/s)
POINT	JAN	FEB	MAR	APR	МЛҮ	JUNE	JULY	AUC	SEPT	OCT	NOV	DEC	ANNUAI MEAN
46	24.3	15.1	11.0	16.1	40.4	58.9	63.5	79.0	67.4	85.5	95.9	56.0	51.3
47	6.4	4.0	29	4.2	10.6	15.5	16.7	20.8	17.7	22.5	25.2	14.7	13.
48	20.7	12.9	9.3	13.7	34.3	50.0	53.9	67.1	57.2	72.7	81.5	47.6	43.
49	2.8	1.7	1.3	1.8	4.6	6.8	7.3	9.1	7.7	9.8	11.0	6.4	5.
50	3.2	2.0	1.5	2.1	5.4	7.8	8.4	10.5	9.0	11.4	12.7	7.4	6.1
51	9.0	5.7	3.6	3.8	8.2	13.6	19.3	25.7	23.5	31.0	37.5	20.5	16.
52	9.0	5.6	4.1	6.0	15.0	21.9	23.6	29.4	25.0	31.8	35.6	20.8	19.
53	5.9	3.7	2.7	3.9	9.8	14.2	15.3	19.1	16.3	20.7	23.2	13.5	12.
101	61.9	41.1	29.3	26.7	53.0	92.2	85.0	93.4	100.1	. 150.2	195.7	140.2	89.
102	89.9	59.6	42.5	38.7	76.9	133.8	123.3	135.4	145.2	218.0	283.9	203.4	129.
103	110.6	73.4	52.3	47.6	94.6	164-6	151.7	166.6	178.7	268.2	349.3	250.2	159.4
104	26.2	17.4	12.4	11.3	22.4	39.0	35.9	39.5	42.3	63.5	82.8	59.3	37.4
105	31.6	21.0	15.0	13.6	27.0	47.1	43.4	47.6	51.1	76.7	99.8	71.5	45.0
106	145.8	96.8	69.0	62.8	124.7	217.1	200.1	219.8	235.7	353.8	460.7	330.0	210
107	177.9	118.1.	84.2	76.7	152.2	265.0	244.2	268.2	287.6	431.7	562.3	402.8	256.
108	29.2	18.8	17.1	20.7	43.1	53.9	56.2	63.7	65.8	69.1	65.9	45.5	45.
109	52.1	33.6	30.5	37.0	77.0	96.1	100.3	113.7	117.4	123.3	117.6	81.1	81.
110	118.5	76.4	69.5	84.0	175.0	218.5	228.1	258.7	267.1	280.5	267.4	184.5	186,
m	138.4	89.2	81.2	98.2	204.5	255.3	266.5	302.2	312.1	327.7	312.4	215.6	217.
112	145.0	93.4	85.0	102.8	214.2	267.4	279.1	316.5	326.8	343.3	327.2	225.8	228,
113	167.0	107.6	97.9	118.5	246.7	308.0	321.5	364.6	376.5	395.4	376.9	260.L	262.
114	369.2	241.9	193.6	205.6	419.7	609.2	599.0	669.4	703.3	886.0	1,015.9	717.8	556.
แร	39.9	30.3	21.2	17.7	26.4	44.4	43.1	47.0	51.0	75.3	100.8	77.3	47.
116	76.3	57.9	40.5	33.9	50.4	85.0	82.4	89.9	97.5	144.1	192.8	147.9	<u>,</u> 91.
117	119.7	90.8	63.6	53.2	79.1	133.4	129.2	141.L	152.9	226.1	302.4	232.1	143.
118	495.3	337.4	260.6	261.6	502.9	749.5	735.0	817.9	864.3	1,124.0	1,334.2	962.2	705.
119	31.1	20.0	18.2	22.0	45.9	57.3	59.8	67.8	70.0	73.6	70.1	48.4	48.
120	23.5	15.2	13.8	16.7	34.7	43.4	45.3	51.3	53.0	55.7	53.1	36.6	37.
121	54.6	35.2	32.0	38.7	80.6	100.7	105.1	119.2	123.0	129.2	123.2	85.0	85.
122	556.5	376.8	295.3	303.1	589,7	860.3	854.4	956.1	1,004.8	1,276.2	1,485.3	1,062.4	804.
123	565.0	382.3	298.8	306.7	597.5	873.3	872.9	980.6	1,027.2	1,305.8	1,521.0	1,081.9	820.
124	595.3	401.5	311.1	319.4	625.3	919.2			1,106.6				877.
125	624.9	420.3	323.1	331.9	652.5		1,002.2	1,152.1	1,184.3	1,513.1	1,771.8	1,218.9	932.
126	676.4	452.8	344.9	358.2		1,059.6					1		1,033.
127	16.0	11.0	7.7	14.8	46.7	64.2	85.2	81.1	. 81.2			28.6	46.
128	19.1	13.1	9.2	17.7	55.9	76.7	101.9		97.1	78.8		34.2	55.
129	29.7	20.4	14.3	27.5	86.9	119.4	158.5	150.9	151.1	122.6			85.
130	38.1	26.2	18.4	35.2	.111.5	153.1	203.2	193.5	193.8	157.2		68.2	110.
131	71.5	47.6	33.7	59.7	· 178.4	248.5	315.2	318.7				140.4	138.
132	98.6	64.4	46.0	. 77.6	223.4	314.0	385.8	406.6	382.4	375.4		202.8	245.
133	101.4	66.2	40.0	79.5	228.0	320.7	393.1	415.7	390.1	385.2		202.0	251.
						1,383.8							
134	779.2	519.8	392.8	438.6		1,405.2							
135	791.4	527.5	397.9	444.5		1,405.2							
136	800.4	533.1	401.9	450.5									
137	806.3	536.8	404.6	454.3	982.6	1,441.3	1,585.3	1,811.6	1,789.9	2,1//.2	2,484.5	1,011.0	1,343.

Table 3.8

Comparison of Calculated Monthly Runoff with Observed or Studied One (Unit: m^3/s)

Basin 1 at P	and the second s						J.			7, 196		_	
Calculated: Observed :	J 223 211	F 155 154	M 124 162	A 83 83	M 144 206	J 353 224	J 370 331	A 367 341	5 394 430	0 554 690	N 784 1095	D 675 732	Ave. 353 389
Basin 1 at C	asecna	n Dams	site (1	150 kr	n ²)					196	3-79		
_	J	, F	M	Α	M	J	J	А	S	0	N	D	Ave.
Calculated: Studied :	48 67	32 36	23 32	20 26	39 33	72 44	64 62	72 65	77 89	110 125	149 136	$\frac{111}{113}$	68 69
Basin 2 at H						_			65~66	, 196		,	
Calculated:	Ј 27	F 21	M 14	A 20	м 31	J	J FO	A	S	0	N	D	Ave.
Observed :	25	18	14	11	32	61 43	59 77	71 90	56 78	40 47	69 63	58 34	44 45
Basin 2 at M			-		·	· •			_	-	3-84		
Calculated:	J 145	F 93	м 85	A 103	м 214	J 267	J 279	A 317	S 327	0 343	N 327	D 226	Ave. 228
Studied :	134	122	78	81	175	210	305	338	399	408	329	200	232
Basin 2 at S											372		
Calculated:	J 28	F 16	м 12	A 13	M 26	J 38	J	A 50	S 17	0	N	D	Ave.
Studied :	20	14	12	15	20 24	-30 40	45 57	50 54	47 62	45 61	53 62	44 38	35 38
Basin 2 at M	atuno 1	Damsit	e (550	km ²)	•					196	3-76		
······	J	F	M	A	Μ	J	Ĵ	A ·	S	0	N	D	Ave.
Calculated:	2.8	17	14	13	28	41	41	52	51	52	54	44	36
Studied :	30	19	16	15	27	39	52	55	58	61	52	37	38
Basin 3 at D											6-68		
Coloulanais	J	F	M	A	M	J	J	A	S	0	N	D	Ave.
Calculated: Observed :	8 9	6	4 6	4 6	6 7	12 7	8 6	12 7	10 9	9 12	17 17	16 20	9
observed ;			0	U	1	1	0		9	1.Z.	11	20	10
Basin 4 at C	alaoag	an (30	8 km ²)							196	5-70		
	J	F	M	A	M	J	J	A	S	0	N	D	Ave.
Calculated:	7	4 5	3 3	5 6	8 4	13	19	23	18	22	23	14	13
Observed	7	J	. .	0	4	10	19	29	13	34	22	10	14
Basin 4 at C			-							196	366		
	J	F	М	A	M	J	J	Α	S	0	N	D	Ave.
Calculated:	27	19	12	8	37	51	93	95	77	56	153	102	61
Observed :	60	31	12	8	46	21	72	30	72	114	77	194	62
Basin 4 at A		(170 F	km∠) M	٨		т	т	,	Ċ		5-71	D	
Calculated:	J 7	5	3	A 4	M 7	J 12	J 19	A 21	S 18	0 25	N 29	D 17	Ave. 14
Observed	18	9	9	5	8	10	12	16	9	26	37	36	14
Basin 5 at C							~		_		3-84		
0-1-41-44-44	J	F	M	A	M	J	J	A	S	0	N	D	Ave.
Calculated: Studied :	30 34	20 21	14 16	28 26	87 83	119 129	159 168	151 154	151 131	123 106	97. 113	53 57	86 86
Basin 6 at E	1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 -					~~~		× 2 4				ا مر	
Dasin v at g	$\frac{\text{scorea}}{\text{J}}$	(655 F	Km ⁻) M	Α	М	J	J	A	S	.0	5-72 N	D	Ave,
Calculated:	20	12	8	16	34	38	53	62	49	57	60	37	37
Observed :	25	19	15	17	25	28	48	41	42	65	57	45	36
and the second													

Table 4.1 Storm Records in the Cagayan River Basin

	Tropical	Cyclone	Flood Hyd	lrograph	Hourly Rainfall	· .
Code	Name	Period	Avail ability	Peak (m ³ /s)	Availability	Remarks
(1) <u>Ma</u>	igat damsi	te (C.A. = $4,143$	<u>km²)</u>			
T6718	Welming	Nov. 1 - 5'67	x	8,281	x	
T6811	Nitang	Sep. 24 - 29 '68	x	1,790	x	
T6905	Elang	Jul. 24 - 27 '69	х	1,242	x	
T7013	Pitang	Sep. 8 - 12 '70	x	9,540	x	
T7311	Narsing	Oct. 12 - 16 '73	x	6,128	x	
T7416	Tering	Oct. 14 - 17 '74	x	5,658	x	
T7604	Didang	May 15 - 26 '76	x	4,900	x	
T7717	Uding	Nov. 10 - 17 '77	0	1,449	ο	
T7810	MIDING	Aug. 23 - 26 '78	ο	3,060	0	1997) 1997
T7818	WELING	Sep. 26 - 30 '78	· 0	3,100	0	
T7822	Kading	0ct. 25 - 27 '78	0	7,906	0	
rs7922	Krising	Dec. 21 - 24 '79	x	2,537	x	· · · ·
T8011	Nitang	Jul. 18 - 22 '80	O	3,101	0	
T8012	Osang	Jul. 22 - 27 '80	x	1,650	x	
S8019	Yoning	Oct. 28 - 30 '80	0	3,297	• •	
T8020	Aring	Nov. $1 - 7$ '80	о	7,637	o	
S8105	Elang	Jul. 3 - 5 '81	0	3,996	0	
T8120	Anding	Nov. 21 - 27 '81	о	5,440	ο	
S8410	Maring	Aug. 28 - Sep. 5	184 o	2,140	0	· · · ·
D8415	Seniang	Oct. 28 - Nov. 3	'84 o	4,440	0	
S8510	Miling	Sep. 2 - 11 '85	o	3,192	0	
T8516	Tasing	Oct. 18 - 26'85	0	6,300	0	
2) <u>Mat</u>	tuno dams;	ite (C.A. <u>= 550 km</u>	2)			
T8011	Nitang	Jul. 18 - 22 '80	0	852	0 2	brs. rainfall
-						
3) <u>Pal</u>	lattao G/S	5 (C.A. = 6,626 km)	2)			
	•	Nov. 22 - 23 '61	0	5,978	x	
		Nov. 6 - 7 '62	0	4,786	· X	ta a secondaria de se Secondaria de secondaria de
		Jun. 27 - 28 '63	o	3,290	X	· :
4) <u>Cab</u>	oulay G/S	$(C.A. = 196 \text{ km}^2)$				
_	· .	Sep. 18 - 19 '65	0	105	x	
5) <u>Ibu</u>	lao G/S ($C.A. = 606 \text{ km}^2$				1. ·· .
		Sep. 23 '71	0	445	x	
6) <u>Gab</u>	oong G/S ($C.A. = 586 \text{ km}^2$				
		Jul. 19 - 25 '80	0	441	x	

Table 4.2 Thiessen Weight for Base Point Basin

Basin				Rai	nfall Gau	ging Stat	ion			
	Aparri	Tuao	Tuguegarao	Naneng	Ilagan	Bontoc	Nayon	Echague	Consuelo	Dakgar
Casecnan		-	-	_	_	· _	-	~	1.00	-
Cagayan No.2	-	_ .	-		-	-	-	-	1.00	-
Cagayan No.1	~		-	-	-	-	-	~	1.00	•-
Diduyon	-		· _		-			-	1.00	-
Addalam (A)	-	-	-	-	-	-	-	~	1.00	-
Matuno No.1	→	-	-	-		-	-	-	1.00	
Alimit No.l (A)	-	-		1.00	-	-	_	-		-
Magat	-	-	-	0.27	-	~	-		0.73	
Ilagan No.1	-	-	0.64	-	-	-	-	-	0.36	-
Disabungan	~		1.00	-	-	-			<u> </u>	-
Siffu No.1 (A)	~ .	-	-	1.00	_ ·		-	-	_	-
fallig No.2	.	-		1.00	-		-	-		
Chico No.2	-			1.00		-	-	-	-	
Chico No.4	••	-	÷	1.00	-	-	-	~	-	
?inukpuk	-	0.23	. –	0.77	-	-	-	-		-
ase Point No.1	0.04	0.09	0.29	0.28	-	_	-	-	0.30	-
" 2	-	0.02	0.36	0.22	-	· -	-	-	0.40	-
" 3		- '	0.23	0.21	-	-		-	0.56	-
н 4	-	-	0.06	0.27	-	-	-	-	0.67	-
" 5	**	-	0.09	0.16	-		-		0.75	-
ч - 6	-	0.36	0.02	0.62	-	-	-		-	-
"7	~	-	0.23	0.77	-	-	-	-	-	~
"8		-	0.85	-	-	-	-		0.15	-
	-	. .	0.02	0.38	-	-	-	-	0.60	-

Case 1 (Period 1956 - 1963)

Case 2 (Period 1964 - 1967)

Basin				Rai	nfall Gau	ging Stat:	lon			
£881N	Aparri	Tuao	Tuguegarao	Naneng	Ilagan	Bontoc	Nayon	Echague	Consuelo	Dakgar
Casecnan	_	-	~	-	-	1.00	-	-	- ·	_
Cagayan No.2	-	-	-	-	-	1.00	-	-		-
Cagayan No.1	-	-	-	-	-	1.00			-	-
liduyon	-	-	-	- ·	-	1.00	-	-	-	-
ddalam (A)	-	· -	-	-	-	1.00	-	~	-	-
latuno No.l	-	-	-		-	1.00	-	~	-	-
limit No.1 (A)		-	-		-	1.00	-	-	-	
lagat		-	-	-	-	1.00	-	-	-	-
lagan No.1	-		0.78	-		0.22	-	-		
isabungan	-	-	1.00		-	· -	-		-	-
iffu No.1 (A)	-	-		0.72		0.28	· 🛶	-	-	
allig No.2	-		· 🕳	1.00	-	••	-	-	-	-
hico No.2	-	-	-	~	-	1.00	~		-	
hico No.4		~	-	0.31		0.69	-		-	_
inukpuk	-	0.23	-		0.77	-	-		-	-
ase Point No.1	0.04	0.09	0.30	0.14	-	0.43	-	-		-
. 2	-	0.02	0.38	0.10	-	0.50	-	÷-	-	-
" 3	-	-	0.26	0.05	_	0.69	-	-	-	-
н. 4	-	-	0.08	0.07		0.85		-		-
" 5	-	-	0.09	0.06		0.85	-		-	
" 6	-	0.36	0.01	0.38	-	0.25	-	-	_	
" 7		-	0.23	0.68		0.09	-	-	-	-
" 8	-	•	0.91	-		0.09	-	-	<u></u>	-
1) g	~	-	0.02	0.09		0.89	-	-		-

to be Continued

Basin		Rainfall Gauging Station												
	Aparri	Tuao	Tuguegarao	Naneng	Ilagan	Bontoc	Nayon	Echague	Consuelo	Dakgan				
Casecoan	-	-	-	-	-		-	_	1.00	·				
Cagayan No.2	-			-		i	-	-	1.00	~				
agayan No.1	-	· •••	-	-	~	-	0.23	-	0.77	-				
iduyon	-		-	-	-	-	0.21	-	0.79	-				
ddalam (A)	-	⊷ ,	-	-	-	-	0.51	-	0.49	· م				
atuno No.1	-	-	-	-	-		0.83		0.17	-				
limit No.1 (A)) -	-	-	-	· •	0.28	0.72	-						
agat	-	-	-		<u> </u>	0.07	0.66		0.27	м. ¹				
lagan No.1	-	-	-	. –	1.00	-	•-	-	-	-				
isabungan	-	-	-		1.00	-	-	-		-				
iffu No.l (A)	-	-	-	0.66	0.06	0.25	0.03			-				
allig No.2		-		1.00	 .		-	-	-	-				
nico No.2	-		-		-	1.00	-		-	- -1.				
nico No.4	••	-		0.31	· –	0.69	-	÷		- -				
inukpuk	-	0.23	-	0.77	-	-	-		. –	: 🛥 · · ·				
ase Point No.1	0.03	0.09	0.12	0.10	0.26	0.06	0.22	-	0.12	÷.				
" 2	~	0.01	0.15	0.04	0.34	0.02	0.28	-	0.16	-				
" 3	-	-	-		0.37	0.02	0.39	-	0.22					
" 4	. 🕶	-	-	<u>``</u>	0.20	0.03	0.49	-	0.28	-				
" 5	-		-	-	0.26	-	0.40	-	0.34	ъ ·				
" 6	-	0.36	0.02	0.38	-	0.24			-	-				
" " T		-	0.02	0.47	0.42	0.08	0.01	_ ·	-					
" 8	-	-	-	- ·	1.00	i	-	-		-				
יי 9	-		-	0.01	0.08	0.06	0.63		0.22	· _				

Case	3	(Period	1968	1976)
------	---	---------	------	-------

Case 4 (Period 1977 - 1984)

Rainfall Gauging Station Basin Aparri Tuao Tuguegarao Naneng Ilagan Bontoc Nayon Echague Consuelo Dakgan 1 1 ... -0.19 0.81 -_ _ Casecnan _ •• ----_ ----0.13 0.87 Cagayan No.2 -----_ ---0.01 0.09 0.90 ~ Cagayan No.1 ----** ---0.04 ~ 0.12 0.84 ---Diduyon ------0.01 0.12 0.07 0.79 --Addalam (A) --------+ (0.83 0.17 -_ _ Matuno No.1 -1 --_ 0.28 0.72 ~ Alimit No.1 (A) -----0.07 0.65 0.27 0.01 ---_ Hagat -----_ ~ 0.05 --•• 0.95 -Ilagan No.1 _ _ •• --1.00 ----Disabungan ---' -0.03 ----~ ** 0.66 0.06 0.25 Siffu No.1 (A) Mallig No.2 Chico No.2 ------1.00 ц. ••• ---_ -------1.00 --_ 0.31 -------**-** . ' 0.69 Chico No.4 -0.23 0.77 -----_ · __ Pinukpuk --0.15 0.06 0,11 0.18 0.05 0.11 0.03 0.12 0.10 Base Point No.1 0.09 0.20 0.02 0.14 0.23 0.07 0.14 0.04 0.02 0.14 2 -H 0.20 0.32 0.09 0.19 _ 0.18 0.02 3 ----.. 0.25 0.30 0.25 _ --_ --0.06 0.02 0.12 4 H, ~ 0.04 0.44 ---0.04 0.02 0.46 _ ---5 11 --0,38 0.25 0.35 0.02 -6 ---_ н 0.47 0.41 0.01 ---_ 0.07 7 ---0.02 ... _ 0.41 8 9 0.59 . 13 _ --0.01 0.06 0.58 0.09 0.22 0.04

Dam Basin					all Gau	iging St	ation			
	Aparri	Tuao	Tugue- garao	Naneng	Ilagan	Bontoc	Nayon	Echague	Con- suelo	Dakgan
Casecnan	1.52	1.48	1.50	1.15	1.47	0.85	1.22	1.45	1.00	1.14
Cagayan No.2	1.47	1.44	1.45	1.11	1.42	0.82	1.18	1.41	0.96	1.11
Cagayan No.l	1.44	1.41	1.42	1.09	1.40	0.81	1.16	1.38	0.94	1.08
Diduyon	1.55	1.52	1.53	1.17	1.50	0.87	1.25	1.48	1.10	1.27
Addalam (A)	1.27	1.25	1.26	0.96	1.24	0.72	1.03	1.22	0.91	1.04
Matuno No.1	1.50	1.46	1.48	1.13	1.45	0.84	1.21	1.43	1.07	1.22
Alimit No.1 (A)	1.27	1.25	1.26	0.96	1.24	0.72	1.03	1.22	0.91	1.04
Magat	1.22	1.20	1.21	0.92	1.19	0.69	0.99	1.17	0.87	1.00
Ilagan No.1	1.25	1.22	1.23	0.94	1.21	0.70	1.01	1.20	0.89	1.02
Disabungan	1.17	1.14	1.15	0.88	1 13	0.66	0.94	1.12	0.83	0.95
Siffu No.1 (A)	1.17	1.15	1.16	0.89	1.14	0.66	0.95	1.12	0.84	0.96
Mallig No.2	1.18	1.16	1.17	0.89	1.15	0.66	0.95	1.13	0.84	0.97
Chico No.2	1.81	1.77	1.79	1.37	1.76	1.02	1.46	1.73	1.29	1.48
Chico No.4	1.52	1.49	1.51	1.15	1.48	0.86	1.23	1.46	1.09	1.25
Pinukpuk	1.29	1.26	1.28	0.97	1.25	0.73	1.04	1.24	0.92	1.06

Table 4.3 Adjustment Factor for Basin Mean Elevation

Table 4.4 Probable Rainfall in the Base Point Basin

						·			•	Ŭ	nit: mm
	Basin		1/2	1/5	1/10	1/25	1/50	1/100	1/200	1/1,000	1/10,000/1
	Casecnan		155	248	328	400	480	560	650	900	1,250
	Cagayan No.2	2	150	241	321	390	470	550	640	890	1,250
	Cagayan No.1	<u>L</u>	138	223	298	360	440	510	620	840	1,200
	Diduyon		149	239	316	420	510	600	700	980	1,400
	Addalam (A)		115	183	236	315	382	457	539	768	1,209
r-4	Matuno No.1		117	153	176	205	226	247	267	316	386
Rainfall	Alimit No.1	(A)	83	114	137	168	193	219	247	319	44.3
a i n	Magat		91	123	144	169	188	207	227	272	339
A N N	Ilagan No.l		135	201	247	310	358	408	461	591	804
-Day	Disabungan		135	201	251	321	377	439	505	681	998
,	Siffu No.1 ((A)	68	103	128	161	187	214	242	312	426
	Mallig No.2		76	111	136	169	194	221	248	316	427
	Chico No.2		124	171	202	242	271	301	331	403	511
	Chico No.4		97	144	177	220	253	287	323	410	549
	Pinukpuk		88	127	153	188	215	242	270	337	444
	Base Point 1	.1	168	217	248	286	314	341	· <u> </u>		
		10.2	170	229	267	315	351	386	-	-	-
Ē		No.3	178	244	288	344	385	427		-	-
Rainfall		lo.4	188	261	310	372	419	466	· _	· 	-
Rai		lo . 5	204	285	340	409	462	515	· _	÷	
ਨਿਚ		10.6	169	233	276	330	371	412	_	_	
4-Day		No.7	165	220	256	301	335	367	-	-	**
,		lo.8	191	264	313	375	421	468	_	· ••	
		No.9	177	241	283	336	376	416	-	-	

Note: 1/1; Probability

	•	······	Re	turn Pe	riod (y	ear)	
Distribution	· · ·	2	5	10	25	50	100
Type	Area		Ar	ea Rain	fall (m	m)	
	u <u>/*</u>	204	285	340	409	462	515
	<u>/**</u> BP-4	168	231	273	326	366	40
Intensive rainfall	<u>/***</u> BP-3	142	183	209	244	263	28
in Upper Cagayan Dasin	BP-2	150	192	215	243	266	284
	BP-1	161	173	178	179	180	18
	М	177	241	283	336	376	41
	BP-4	196	276	330	399	451	50
Intensive rainfall in Magat basin	BP-3	142	183	209	244	263	28
in nagat basin	BP-2	150	192	215	243	266	284
	BP-1	161	173	178	179	180	181
	I	191	264	313	375	421	468
Intensive rainfall	BP-3	175	239	282	336	376	41
n Ilagan basin	BP-2	150	192	215	243	266	2.84
· · ·	BP-1	161	173	178	179	180	181
	S	165	220	256	301	335	367
ntensive rainfall n Siffu basin	BP-2	171	230	268	316	353	388
	BP-1	161	173	178	179	180	181
ntensive rainfall	С	169	233	276	330	371	412
n Chico basin	BP-1	168	214	242	277	303	327

Table 4.5 Areal Rainfall Distribution

Remarks:

/*; U = Upper Cagayan basin, M = Magat basin, I = Ilagan basin, S = Siffu basin, C = Chico basin /**; BP-4 means the area upstream BP-4 except U. /***; BP-3 means the area between BP-3 and BP-4.

				Rainfa	11		Runoff		Co	efficie	ent
No.	Stor	m 	l-hr Max (mm)	24-hr Max (mm)	Total (3-day) (mm)	1-hr Max (m ³ /s)	Total (3-day) (mm)	Direct Runoff (mm)	Peak	Total	Direct
* 1.	T7717	Uding	38.0	81.0	125.1	1,440	52.7	43.3	0.03	0.42	0.35
* 2.	T7810 I	Miding	32.9	96.5	135.3	3,060	87.7	78.3	0.08	0.65	0.58
3.	T7818	Weling	26.1	66.2	89.1	3,100	100.1	90.7	0.10	1.12	1.02
* 4.	т7822 н	Kading	95.2	193.8	203.9	7,906	125.3	115.9	0.07	0.61	0.57
5.	T8011 I	Nitang	42.0	55.0	55.5	3,101	69.0	59.6	0.06	1.24	1.07
* 6.	т8019	Yoning	55.7	87.8	141.8	3,297	64.5	55.1	0.05	0.45	0.39
7.	T8020	Aring	83.0	244.2	284.9	7,637	220.9	211.5	0.08	0.78	0.74
8.	TS8105 I	Elang	73.4	130.1	132.9	3,996	73.3	63.9	0,05	0.55	0.48
9.	T8120	Anding	45.2	101.5	114.4	5,440	110.1	100.7	0.10	0.96	0.88
*10.	TS8410 1	Maring	23.1	62.7	115.6	2,140	56.3	46.9	0.08	0.49	0.41
11.	TD8415	Seniang	28.3	67.7	102.9	4,440	100.3	90.4	0.14	0.97	0.88
12.	TS8510 1	Miling	24.8	52.1	86.0	3,192	58.0	48.6	0.11	0.67	0.57
13.	T8516	lasing	38.8	86.4	113.5	6,300	113.1	103.7	0.14	1.00	0.91

Table 4.6 Runoff Coefficient of the Selected Storms at Magat Damsite

Note: * Storm selected for simulation study. The others are not selected due to unreliability of runoff coefficient value and unreliable response between hourly rainfall and runoff data.

Table 4.7

Storage Function of Subbasin

Basin No.	A (km2)	L (km)	Ĩ	ĸ	р	Tl (hr)
· · ·		$(1,1) \in \mathbb{R}^{n \times n}$	- 100	00.5	0 11 2	
1	1,150 481	$92.1 \\ 25.0$	1/20 1/90	$27.5 \\ 21.6$	0.416	3.8
2 3	733	37.5	1/50	25.7	0.504 0.439	0.6 1.2
4 · ·	298	35.0	1/260	15.7	0.646	1.1
5	351	62.5	1/330	14.6	0.684	2.4
6	142	30.0	1/740	11.5	0.827	0.9
7	477	42.5	1/200	17.0	0.608	1.4
8	387	56.0	1/40	27.5	0.416	2.1
9	193	22.5	1/560	12.5	0.774	0.5
10	264	45.0	1/1,730	8.9	1,009	1.6
11	1,106	65.0	1/1,040	10.4	0,895	2.5
12	1,051	55.0	1/1,000	10.5	0,887	2.0
13	620	26.0	1/190	17.2	0.601	0.7
14	292	44.0	1/80	22.3	0.490	1.5
15	550	41.0	1/90	21.6	0.504	1.4
16 17	1,228 628	45.0 53.0	1/390 1/80	13.9	0.711	1.6
18	559	53.0	1/240	22.3 16.1	0.490	$1.9 \\ 2.1$
19	266	42.5	1/480	13.1	0.747	1.4
20	970	112.0	1/560	12.5	0.774	4.7
21	247	30.0	1/390	13,9	0.711	0.9
22	876	82.0	1/190	17.2	0.601	.3,3
.23	474	50.0	1/220	16.5	0.622	1.8
24	215	38.0	1/680	11.8	0.810	1.2
25	652	48.0	1/120	19.8	0.539	1.7
26	915	63.0	1/120	19.8	0.539	2.4
27	209	35.0	1/150	18.5	0.568	1.1
28 29	656 408	48.0 88.0	1/150 1/1,910	18.5 8.6	0.568	1.7 3.6
30	362	51.0	1/150	18.5	1.033 0.568	1.8
31	589	82.0	1/1,390	9.5	0.959	3.3
32	964	55.0	1/220	16.5	0.622	2,0
33	327	39.0	1/120	19.8	0.539	1.3
34	92	19.0	1/3,940	6.9	1.225	0.3
35	657	74.0	1/70	23.3	0,475	3.0
36	1,042	76.5	1/5,000	6.5	1.295	3.0
37	969	70.0	1/140	18.9	0.559	2.7
38	73	13.5	1/5,000	6.5	1.295	0.1
39	386	26.0	1/70	23.3	0.475	0.7
40	334	42.5	1/90	21.6	0.504	1.4 0.6
41 42	157 533	25.0 36.0	1/30 1/40	30.0 27.5	0.389 0.416	1.1
43	372	44.0	1/70	23.3	0.475	1.5
44	612	53.5	1/230	16.3	0.628	2.0
45	856	58.0	1/60	24.4	0.458	2.2
46	1,301	70.0	1/120	19.8	0.539	2.7
47	169	30.0	1/240	16.1	0.634	0.9
48	417	19.0	1/350	14.4	0.693	0.3
49	393	69.0	1/480	13.1	0.747	2.7
50	278	29.5	1/5,670	6.2	1.334	0.8
		1. A.	Notes;		1. A.	

A; Catchment Area L; River Length I; Basin Slope K, P; Storage Function Tl; Lag Time (hr) (km2) (km)

Table 4.8 Relationship of Discharge and Channel Storage (Present River Condition)

Νо.	Chann Caga - S			Channel-2 Cagayan S Q		el-J yan Q	Chann Caga S		Channel-5 Addalam S D	
	(x10 ⁶ m ³)	(m^{3}/s)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)
1	6.0	228	5.8	204	21.7	1,265	19.3	1,265	3.3	200
2	12.0	719	11.5	645	43.4	3,990	38.5	3,990	13.6	636
3	18.0	1,404	17.3	1,262	65.1	7,788	57.8	7,788	20.4	1,250
4	24.0	2,252	23.Ò	2,026					27.3	2,019
5	30.0	3,249	28.8	2,929					34.1	2,929
6	42.0	5,622	40.3	5,066						• • • • •
7	60.0	10,004	57.5	9,041						
8										
9							. ·			
10										
u										
12								÷ .		
13			<u> </u>							

					·					• :
No.	Chann Adda	lam	Channe Cagay		Channe Caga		Channe Naga		Channe Nag	
	<u> </u>	<u>q</u> :	<u>s</u>	<u>Q</u>	<u> </u>	Q	<u>s</u>	Q	S	<u> </u>
	$(x10^{6}m^{3})$	(m ⁾ /s)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m^{3}/s)	(x10 ⁶ m ³)	(m ³ /s)
1	1.3	200	19.7	580	46.2	580		•	12.0	331
2	5.6	636	29.2	1,160	70.5	1,160	14.3	681	24.0	1,048
3	8.4	1,250	38.5	1,740	91.4	1,740	21.4	1,331	36.0	-2,053
4	11.1	2,019	53.5	2,900	128.7	2,900	28.5	2,136	48.0	3,299
5	13.9	2,929	68.9	4,060	166.0	4,060	35.6	3,082	60.0	4,765
6			88 6	5,800	228.7	5,800	49.9	5,325	84.0	8,281
7			121.2	8,700	352.6	8,700		•		
8			163.1	11,600	489.5	11,600		1. 1		
9			210.0	14,500		•				
10			256.3	17,400			÷ •			
11			357.4	23,200						
12			482.2	29,000						
13										

				· · ·			N	1. 1 1. 1		
No.	Channe Maga		Channe Cagaya		Channe Iløg:		Channe I Ilaga		Channe 11ag	
no.	<u> </u>	Q	S	<u> </u>	<u> </u>	<u> </u>	S	Q	S S	9
	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)	$(x10^{6}m^{3})$	(m ³ /s)
1	14.1	300	20.0	490			. * *		10.9	300
2	21.4	500	28.3	980			13.3	400	14.8	500
3	38.5	1,000	43.8	1,960	5.8	800	15.9	800	23.0	1,000
4	72.6	2,000	61.7	2,940	8.5	1,700	23.2	1,700	36.4	2,000
5	L08.8	3,000	91.8	4,900	10.6	2,500	28.9	2,500	48.1	3,000
6	144.7	4,000	119.7	6,860	14.5	4,200	39.6	4,200	58.7	4,000
7	181.4	5,000	163.0	9,800	17.4	5,400	47.4	5,400	69.9	5,000
8	252.9	7,000	229.5	14,700					92.8	7,000
9	354.9	10,000	312.3	19,600			÷		133.8	10,000
10			391.5	24,500						
11			474.2	29,400						
12									. · · ·	
13										

HY-76

to be Continued

.

No.	Channe Cagay		Channel-17 Siffu			Channel~18 Hallig		1-19 an	Channe 1-20 Cagayan	
60,	<u> </u>	<u> </u>	S	<u>Q</u>	<u> </u>	Q	S	Q	รั	Q
· · ·	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(u3/s)	(x10 ⁶ m ³)	(10 ³ /s)	(x10 ⁶ m ³)	(m ³ /s)
· 1	16.0	1,000	11.1	300	9.0	300	26.4	500	17.6	500
2	25.2	2,000	19.5	500	11.8	500	41.3	1,000	28:9	1,000
Э	33.7	3,000	79.9	1,000	58.9	1,000	65.2	2,000	48.2	2,000
4	49.8	5,000	211.2	2,000	110.5	2,000	87.8	3,000	65,4	3,000
5	62.7	7,000	325.2	3,000	382.4	3,000	180.0	5,000	123.0	5,000
6	91 1	10,000					262.1	7,000	167.5	7,000
7	155.9	15,000					406.5	10,000	247.1	10,000
8	224.8	20,000			· .				380.5	15,000
9	285.2	25,000							527.9	20,000
10	342.5	30,000								
11	467.7	40,000								
12										
13			1 - A							

No.	Channe Caga		Coga	Channe 1 – 22 Cogayan		1-23 co	Channe Chi		Channel-25 Chico	
	\$	Q	<u> </u>	Q	<u> </u>	Q	S	Q	5	Q
	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m³/s)
1	49.9	500	40.2	2,000						
2	78.8	1,000	48.1	3,000	5.4	740				
3	129.7	2,000	60.8	5,000	7.2	1,180			6.8	940
4	175.0	3,000	74.0	7,000	9.0	1,710			9.6	1,650
5	360.8	5,000	98.8	10,000	10.8	2,300	6.1	1,530	11.1	2,060
6	557.7	7,000	137.0	15,000	12.7	2,950	7.5	2,080	14.1	2,990
7			175.8	20,000	16.3	4,430	9.8	3,050	17.2	4,050
8			212.8	25,000	20.0	6,110	12.3	4,190	20.4	5,230
9			245.5	30,000	23.8	7,980	15.8	5,960	22.1	5,880
10			305.2	40,000	27.5	10,010	18.7	7,500	27.1	7,980
11			359.5	50,000						
12										
13										

:		•								
No.				Channel-27 Chico S Q		Channel-28 Cagayan S O		1-29 yan 0	Channel-30 Cagayan S D	
	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(m ³ /s)
ι	7.0	300	25.2	300	19.6	1,000	39.0	2,000	121.3	2,000
2	10.5	500	34.7	500	30.2	2,000	45.3	3,000	134.0	3,000
3	18.0	1,000	58.1	1,000	39.0	3,000	57.0	5,000	161.4	5,000
4	33.0	2,000	97.5	2,000	58.4	5,000	74.0	7,000	209.6	7,000
5	41.0	3,000	144.3	3,000	73.6	7,000	101.4	10,000	274.2	10,000
6	79.8	5,000	183.2	4,000	99.1	10,000	148.4	15,000	378.5	15,000
7			217.9	5,000	147 2	15,000	193.4	20,000	500.0	20,000
8			282.2	7,000	199.6	20,000	239.2	25,000	14	
9			372.9	10,000	245.3	25,000	279.6	30,000		
10					286.1	30,000	352.3	40,000		
11					357.4	40,000	415.3	50,000		
12					419.3	50,000				
13										

Table	4.	9	

Storage Function of Channel (Present River Condition)

Channel	L	I	K	Р	TI
No.	(km)				(hr)
1	25.0	1/330	68.9	0.593	3.3
2	31.0	1/560	69.2	0.595	4.1
3	19.3	1/790	65.8	0.629	2.6
4	17.2	1/980	68.4	0.610	2.3
5	56.0	1/40	50.9	0.648	4.4
6	22.5	1/560	3.6	0.894	3.0
7	45.0	1/1,730	22.6	0.824	6.0
8	58.0	1/2,900	82.7	0.774	. 7.7
. 9	45.0	1/390	.66.6	0.623	6.0
10	42.5	1/480	145.4	0.557	5.6
11	63.5	1/870	15.7	0.948	8.4
12	20.5	1/6,410		0.810	2.7
13	14.0	1/260	59.4	0,502	1.9
14	38.0	1/680	178.1	0.492	5.0
15	40.0	1/2,470	27.5	0.780	5.3
16	18.5	1/3,850		0.946	2.4
17	88.0	1/1,910	0.6	1.499	11.6
18	82.0	1/1,390		1.685	10.8
19	35.5	1/3,940		0 944	4.7
20	19.0	1/19,00		0.930	2,5
21	76.5	1/5,000		0,938	10.1
22	13.5	1/5,000	47.3	0.701	1.8
23	20.0	1/110	22.9	0.631	1.9
24	20.0	1/120	11.4	0.683	1.9
25	25,5	1/120	25.8	0.629	2,4
26	53.5	1/230	16.3	0.834	7.1
27	61.0	1/1,030		0.787	8.1
28	10.0	1/50,000		0.809	1.3
29	11.5	1/19,170		0.775	1.5
30	29.5	1/5,670		0.626	3.9
50	h. I & .I	2757070	2,00 . 0	0.000	~···

Notes;

L; River Length (km) I; River Slope K,P; Storage Function Tl; Lag Time (hr)

Table 4.10 Relationship of Discharge and Channel Storage

(Confining dike condition)

No.	. C.a.	nel −7 µayan Q	Chann Cag S	el-8 ayan · Q·		nel~11 Igat Q		nel-12 agayan	τ	nel~15 lagan
	(x10 ⁶ m ¹		(x106m]			3) (m ³ /s)		Q (m ³ /s)	<u> </u>	Q 1 ³) (m ³ /s
	······································			· · · · ·			(A10 ta	, (m-121	1210~1	-/ (m-//
1	0.5	10	2.3	10	0.9	10	0.9	10	1.0	10
2	17.6	580	47.5	580	13.8.	300	19.3	500	10.8	300
3	26.2	1,160	71.6	1,160	20.7	500	27.5	1,000	14.8	500
4	34.4	1,740	92.3	1,740	36.2	1,000	43.1	2,000	23.0	1,000
5	48.0	2,900	130.0	2,900	61.5	2,000	61.2	3,000	36.4	2,000
6	62.0	4,060	168.5	4.060	89.3	3,000	93.4	5,000	47.4	3,000
7	78.0	5,800	226.7	5,800	109.2	4,000	124.6	7,000	56.6	4,000
8	106.6	8,700	329.9	8,700	130.9	5,000	163.5	10,000	66.6	5,000
9	143.5	11,600	431.5	11,600	166.7	7,000	216.6	15,000	87.5	7,000
10	181.5	14,500			214.9	10,000	269.4	20,000	115.1	10,000
11	222.1	17,400					321.3	25,000		
12	306.4	23,200					368.8	30,000		
13	413.4	29,000								
14										
			:							
		nel÷16		nel-19		nne 1 - 20		nne1~21		nnel-22 gayan
No.	S	ayen ' Q	Cag S	ayan Q	s s	gayan Q	S S	gayan Q	. S	gayan Q
	(x10 ⁶ m ³) (m ³ /s)	(x10 ⁶ m ³) (m ³ /s)	(x10 ⁶ m	³) (m ³ /s)	(x10 ⁶ m	(m^{3}/s)	(x10 ⁶ m	3) (m ³ /
1	0.8	10	1.5	10	.0.8	10	3.6	10	2.0	10
2	16.9	500	31.3	500	17.9	500	58.5	500	25.0	500
3	21.9	1,000	48.2	1,000	28.7	1,000	83.7	1,000	31.8	1,000
,	32.3	2,000	17.1	2,000	47.7	2,000	131.3	2,000	41.4	2,000
4				1	65.3	3,000	172.6	3,000	49.7	3,000
4 5	41.8	3,000	104.8	3,000	4245	21000		-		F 000
	41.8 59.6	3,000 5,000	104.8	3,000 5,000	99.7	5,000	261.4	5,000	63.2	5,000
5		en l'hanne		-				5,000 7,000	63.2 74.8	7,000
5 6	59.6	5,000	159.6	5,000	99.7	5,000	261.4	-		•
5 6 7	59.6 74.0	5,000 7,000	159.6	5,000 7,000	99.7 132.8	5,000 7,000	261.4	-	74.8	7,000 10,000
5 6 7 8	59.6 74.0 86.7	5,000 7,000 10,000	159.6 205.5 275.9	5,000 7,000 10,000	99.7 132.8 183.0	5,000 7,000 10,000	261.4	-	74.8 90.1	7,000
5 6 7 8 9	59.6 74.0 86.7 134.6	5,000 7,000 10,000 15,000	159.6 205.5 275.9 384.6	5,000 7,000 10,000 15,000	99.7 132.8 183.0 260.2	5,000 7,000 10,000 15,000	261.4	-	74.8 90.1 116.7	7,000 10,000 15,000
5 6 7 8 9	59.6 74.0 86.7 134.6 171.5	5,000 7,000 10,000 15,000 20,000	159.6 205.5 275.9 384.6	5,000 7,000 10,000 15,000	99.7 132.8 183.0 260.2	5,000 7,000 10,000 15,000	261.4	7,000	74.8 90.1 116.7 143.1	7,000 10,000 15,000 20,000 25,000
5 7 8 9	59.6 74.0 86.7 134.6 171.5 209.3	5,000 7,000 10,000 15,000 20,000 25,000	159.6 205.5 275.9 384.6	5,000 7,000 10,000 15,000	99.7 132.8 183.0 260.2	5,000 7,000 10,000 15,000	261.4	7,000	74.8 90.1 116.7 143.1 167.9	7,000 10,000 15,000 20,000

	Chann Caga		Chann Caga		Channel-30 Cagayan		
No.	S ·	Q	S	Q	. S	0	
<u>-</u> -	(x10 ⁶ m ³)	(m ³ / ₃)	(x10 ⁶ m ³)	(m ³ /s)	(x10 ⁶ m ³)	(a ³ /s)	
1	0.7	10	1.1	10	13.0	10	
2	17.2	500	29.0	500	118.1	500	
3	21.8	1,000	30.6	1,000	120.9	1,000	
4	31.4	2,000	35.2	2,000	129.5	2,000	
5	39.6	3,000	39.8	3,000	140.1	3,000	
6	54.5	5,000	49.1	\$,000	164.3	5,000	
7	67.9	7,000	59.1	7,000	189.7	7,000	
8	93.2	10,000	75.4	10,000	227.6	10,000	
9	136.5	15,000	101.7	15,000	286.4	15,000	
10	173.7	20,000	125.3	20,000	337.7	20,000	
11	206.8	25,000	146.0	25,000	383.6	25,000	
12.	235.2	30,000	164.8	30,000	427.7	30,000	
13	285.4	40,000	195.5	40,000			
14	329.4	50,000	226.0	50,000			
14				-			

Channel No.	L (km)	I	K	Р	Tl (hr)	Channel No.	L (km)	I	K	P	T1 (hr)
1	25.0	1/330	68.9	0.593	3.3	16	18.5	1/3,850	42.5	0.711	2.4
2	31.0	1/560	69.2	0.595	4.1	17	88.0	1/1,910	0.6	1.499	11.6
3	19.3	1/790	65.8	0.629	2.6	18	82.0	1/1,390	0.1	1,685	10.8
4	17.2	1/980	68.4	0.610	2.3	19	35.5	1/3,940	73.9	0.753	4.7
5	56.0	1/40	50.9	0.648	4.4	20	19.0	1/19,000	33.3	0.794	2.5
6	22.5	1/560	3.6	0.894	3.0	21	76.5	1/5,000	205.1	0.690	10.1
7	45.0	1/1,730	21.1	0.817	6.0	22	13.5	1/5,000	173.1	0.552	1.8
8	58.0	1/2,900	118.1	0.728	7.7	23	20.0	1/110	22.9	0.631	1.9
9	45.0	1/390	66.6	0.623	6.0	24	20.0	1/120	11.4	0.683	1.9
10	42.5	1/480	145.4	0.557	5.6	25	25.5	1/120	25.8	0.629	2.4
11	63.5	1/870	40.5	0.797	8.4	26	53.5	1/230	16.3	0.834	7.1
12	20.5	1/6,410	44.4	0.750	2.7	27	61.0	1/1,030	73.2	0.787	8.1
13	14.0	1/260	59.4	0.502	1.9	28	10.0	1/50,000	41.7	0.709	1.3
14	38.0	1/680	178.1	0.492	5.0	29	11.5	1/19,170	109.3	0.586	1.5
15	40.0	1/2,470	59.6	0.677	5.3	30	29.5	1/5,670		0.402	3.9

Table 4.11 Storage Function of Channel (Confining dike condition)

Note: L; River Length (km)

I; River Slope

K,P; Storage Function

T1; Lag Time (hr)

Table 5.1 Mean Relief and Elevation of Basin

		Ba	asin 1	Ba	isin 2	Ba	nsin 3	Ba	sin 4	Ba	isin 5	Ba	sin 6
Mean Reli	ef, Rf' ((100 n	n)				alle a faith ann an Anna an				i r a httariaith an Alaciana)	*******	
EL.(m)	Xi (100m)	$f_{\mathbf{i}}$	Xi Ji	fi	Xi Ji	f_{i}	xi fi	f_{i}	xi.fi	fi	Xi.fi	$f_{\rm i}$	Xi.f
0~ 99	1	2	2	7		0	0	1		1	l	0	
100~199	2	2	4	13	26	6	12	4	8	0	0	ĩ	
200~299	3	.3	9	18	54	6	18	2	6	2	6	1	
300~399	4	. 9	36	19	76	5	20	7	28	1	4	4	1
400~499	5	16	80	33	165	13	65	3	15	0 0	4	1	L
500~599	6	20	120	25	150	15	90	2	12	3	18	5	3
600~699	7	2.5	175	23	161	14	98	3	21	9	63	4	2
700~799	8	27	216	26	208	12	96	2	16	22	176	3	2
800~899	9	21	189	33	297	8	72	5	45	20	180	10	9
900~ 999		13	130	25	250	5	50	2	20	14	140	5	5
1000~1099	11	13	143	18	198	2	22	5	55	19	209	7	7
1100~1199	12	5	60	14	168	1	12	4	48	21	252	6	7
1200~1299	13	2	26	8	104	-		1	13	7	91	5	6
1300~1399	14	-		ĩ	14				2.4	5	70	2	2
1400~1499	15			4	60					5	75	1	1
1500~1599	16			:1	16					2	1.5	-	
	Total	158	1,190	268	1,954	87	555	41	288	129	1,285	-55	50
$\frac{1}{f} = Xi$			7.53		7.29		6.38		7.02		9.96		9.1
EL.(m)	Xi (100m)	f_{i}	Xi.fi	fi	Xi.fi	fi	Xi.fi	fi	Xi <i>f</i> i	fi	Xi∙∮i	fi	xi.J
0~ 99	1	0	0	0	0	0	0	3	3	0	0	0	
100~ 199	2	2	4	0	0	3	6	5	10	0	0	1	
200~ 299	. 3	4	.6	16	48	8	-24	8	24	1	3	4	1
300~ 399	4	7	28	22	88	7	28	1	4	1	4	3	1
400~ 499	5	12	60	23	115	8	40	6	30	2	10	4	2
500~ 599	6	13	78	32	192	8	48	3	18	3	- 18	3	.1
600~ 699	7	12	84	22	154	11	77	2	14	4	28	2	1
700~ 799	8	20	160	20	160	17	136	3	24	6	48	3	2
800~ 899	9	25	225	19	171	19	81	3	27	4	36	3	2
900~ 999	10	17	170	22	220	6	60	3	30	5	50	2	2
000~1099	11	14	264	24	264	6	66	- 3	- 33	6	66	6	6
100~1199	12	10	120	11	132	3	36	1	12	9	108	2	2
200~1299	13	9	117	8	104	0	0			6	78	5	6
300~1399	14	2	28	9	126	1	14			15	210	3	4
400~1499	15	1	15	14	210					9	135	4	6
500~1599	16			4	64					13	208	4	6
600~1699	17			7	119					11	187	4	6
700~1799	18			3	54					9	162	2	3
800~1899	19			6	114					8	152		
900~1999	20			2	40					10	200		
000~2099	21			3	63					4	84		
1.00~2199	22			. 0	0		:			3	66		
200~2299	23			0	0								
300~2399	24	÷.,		1	24								
	Total	158	1,359	268	2,462	87	616	41	229	129	1,853	55	57
$m' = Xi \cdot J$			8.60		9.19		7.08		5.59	·····	14.36		10.4

fi : frequency

Table 5.2	Suspended	Sediment	Estimation	

Basin		Basi	<u>n 1</u>	Basi	n 2	Basi	<u>n 5</u>	
Runoff gau	ıge	Guinal	vin	Oscari	Z	Ampawi	len	
Runoff rec	cord	1965 -	1971	1958 -	1964	1963 -	1976	
Drainage a	irea	921 km	2	4,150	km²	751 km²	2	
Rating cur	ve	Dippad	iw	Oscari	Z	Pasonglao		
<u></u>			· .					
Limits (%)	Interval (%)	Water discharge (m³/s)	Sediment discharge (tons/day)	Water discharge (m³/s)	Sediment discharge (tons/day)	Water discharge (m ³ /s)	Sediment discharge (tons/day)	
$0.0 \sim 0.1$	0.1	925.3	1,263,259	3,601.5	3,550,901	1,045.4	538,468	
$0.1 \sim 0.5$	0.4	627.8	352,578	2,278.8	1,256,361	653.2	147,051	
$0.5 \sim 1.5$	1.0	354.7	53,885	1,363.1	391,290	490.3	66,622	
1.5~ 5.0	3.5	172.1	4,990	663.0	76,200	227.8	8,031	
5.0~10.0	5.0	114.2	1,295	433.0	28,970	155.3	2,790	
10.0~20.0	10.0	77.2	357	285.0	11,210	103.6	913	
20.0~30.0	10.0	52.0	97	204.0	5,248	69.7	306	
30.0~40.0	10.0	40.8	44	147.5	2,514	51.8	135	
0.0~50.0	10.0	33.3	22	108.0	1,239	35.7	48	
50.0~60.0	10.0	28.2	13	76.0	558	26.9	22	
50.0~70.0	10.0	23.9	8	54.0	257	20.5	10	
0.0∼80.0	10.0	20.0	4	44.0	161	13.7	3	
80.0~90.0	10.0	16.8	. 2	32.9	83	7.6	. 1	
0.0~95.0	5.0	13.2	- 1	25.2	46	4.7	0	
5.0~98.5	3,5	7.4	0	11.8	8	3.4	0	
8.5~99.5	1.0	5.4	0	4.5	· I	2.0	. 0	
9.5~99.9	0.4	3.4	0	1.3	0	1.6	0	
9.9~100.0	0.1	3.0	0	0.3	0	1.6	0 0	
	(1)	(2)	(3)	(2)	(3)	(2)	(3)	
nnual suspe ediment,(1)		3,506 to	ons/day	18,734	tons/day	2,357 t	ons/day	
		1,070 m ³ /km	1²/year	1,270 m ³ /		880 m ³ /k	-	

		· · · · · · · · · · · · · · · · · · ·			EC		HARDNES	s	c	ALKALINITY		
 2	LOCATION	TURBIDITY	COLOR	pH	ℓ ^{mhos} ∕cm	Ca ppm	Mg ppm	Total ppm		Bicarb ppm	Carb ppm	CaCo3 ppm
:	Larion Alto, Tuguegarao	nil Z nil	nil' {5	7.20 7.70	157 2 191	65 130	15.79 ک 15.80	130 2 145	70 { 120	134.2 2 164.7	0 20	110 2 135
	Casile, Nallig	11 107	55 1,000	6.92 7.29	190 201	80 } 110	0, 4.86	100 2 100	70 2 115	94.5 122	0 1 0	77.5 100
	Malalam (Alinguigan)	nil 7	ni 1 30	6,94 2 7.15	85 1 115	60 200	0 2 8.50	70 l 135	70 2 115	97.6 134.3	0 2 0	80 110
	Palattao, Naguilian	nil ? 9	nil { 120	6,92 { 7.45	128 201	65 90	7.29 8.51	100 2 120	80 2 100	88.45 195.2	0 20	72.5 2 160
	Cabulay, Santiago	ni l Z 140	nil 530	6.93 2 7.47	280 302	100 160	21.87 26.73	210 250	80 2 135	207.4 269.4	0~0	170 220
	Hapid, Lamut (Tupaya)	nil { nil	nil (5	7.12 7.58	178 240	60 2 80	4.86 4.86	80 100	70 2 150	97.6 122	0 2 0	80 2 100
	Dabubu, Pequino	nil ? nil	nil } 10	7.05 { 7.38	108 2 128	60 2 110	2,43 { 4.86	100 2 120	70 2 100	97.6 231.8	0 2 0	80 2 190
	Dippadiw, Madella	nil ł nil	níl ? 75	7.07 7.59	154 197	70 2 100	7.29 12.15	120 2. 130	80 2 110	76.25 195.2	0 2 0	62.5 { 160
	Pingkian, Kayapa	nil { 34	0 2 900	6.81 { 7.94	260 280	85 2 160	9 32.81	160 220	70 2 110	173.85 { 183	0 2 0	142.5 { 150
	Bangag	nil { 4	nil 260	6.83 7.67	150 2 172	70 { 120	9.11 2.43	100 { 107.5	70 { 275	134.2 183	0 2 0	110 150
	Baybayog	10.5 12	10 { 280	7.22 { 7.86	240 2 350	130 180	12,75 17.01	182.5 200	65 2 125	183 256.2	0 ~ 0	150 210
	Rosario	nil } nil	ni1 75	7.40 2 7.94	310 2 320	120 } 180	0 14.58	160 230	75 2 90	256.2 280.6	0 ~ 0	210 230
	Tungngod	nil ? nil	nil (10	7.16 (7.50	250 300	60 { 140	9.75 { 14.58	140 200	50 1 80	158.6 244	0 2 0	130 200
	Careb	nil l nil	nil { 7	7.33	250 1 380	140 2 190	24.3 27.95	240 280	60 1 70	256.2 { 292.8	0 2 0	210 240
	Baliling	nil 1 nil	nil } 65	6.91 7.87	200 { 290	130 200	0 1 21.87	140 290	60 { 120	170.8 256.2	0	140 1 210
: .	Beti	nil { 1	ni 1 2 10	6.77 7.70	112 { 280	60 2 105	2,43 { 8.51	70 2 140	65 2 100	146.4 231.8	0~0	120 190
	Ilut	nil l nil	ni1 } 10	7.10 1 7.30	220 250	70 { 110	.5	120 1 150	70 2 100	183 250.1	0 2 0	150 205
÷	Aurora East	nil ł nil	nil { 15	7.59 7.83	260 210	100 160	12.15 } 36,45	210 280	70 2 100	219.6	0 ~ 0	180
	Gamis	nil 1 nil	nil 2 15	6.64 7.58	340 420	130 180	18,22	250 200	70 ₹ 90	195.2 451.1	. 0 ~ 0	160 370
	Jones	nil 'S	0 . 2 50	6.74 7.30	132 195	60 2 160	0 1 2,43	70 2 160	60 ₹ 75	97.6 2 146.4	0 ≀ 0	80 { 120

Table 6.1 Water Quality in Cagayan River

Observed in June to August, 1985 by NWRC

.

_	Quality	Critoria	itoria Unit		CLASS					
[Parameter			<u>AA</u>	<u>A</u>	В	C	D	<u> </u>	
1. Ce	olor	not less	units		75	50	50	_	L-0	
	emperature	not exceed	00	<i>~</i>	30	30	3(e).	3(e)	_	
	ransparency	-	~	-	-	(c)	(c)	(c)		
4. Di	issolved									
	Oxygen	not less	mg/1	-	5	5	5	3	2	
5. 5.	-day BOD		0.							
	at 20°C	not exceed	mg/1		10	15	20		-	
6. To	otal Dis.									
	Solids	not exceed	mg/l		·	-	1000	1000	-	
7. Te	otal Solids	not exceed	mg/1	500(a)	500(a)	 '	2000	2000	~	
8. Pł	i -	within	-	6.5-8.5	6.5-8.5	6.5-8.5	6.5-8.5	6.5-8.5	5.0-9.	
9. Co	oliform	not exceed	MPN/100 ml	50	5000	1000	5000	-	-	
0. Ph	nenolic Subs.	not exceed	mg/1	0.001	0.001	0.002	0.02		-	
1. Ra	dicactive		-							
	Subs.:									
Gr	coss Alpha	not exceed	pCi/1	3	3	-	-		-	
Gr	ross Beta	not exceed	pCi/l	30	30	-		-		
2. Tr	ace Elements									
. A1	แก่เกมจ	not exceed	mg/1	. —	-			5		
Ar	senic	not exceed	mg/1	0.05	0.05	0.05	0.05	0.1	· ••	
Ba	rium	not exceed	mg/l	1.0	1.0	-	0.5	- 1	-	
	ryllium	not exceed	mg/l	+	· _	-	-	0.1		
	ron	not exceed	mg/1	-	· _	 ·		0.75	-	
Ca	dmium	not exceed	mg/l	0.01	0.01	0.01	0.01	0.01	-	
Ch	romium	not exceed	mg/1	0.05	0.05	0.05	0.05	0.10		
Col	balt	not exceed	mg/1	-	-	<u> </u>	****	0.05		
Co	pper	not exceed	mg/l	1.0	1.0		0.02	0.02		
Cya	anide	not exceed	mg/l	0.05	0.05	0.05	0.05	_	· _	
P1 0	ouride	not exceed	mg/l	0.6	0.6		••• ·	· 1	_	
Ire	on	not exceed	mg/1	1.0(a)	1.0(a)	-	_	5		
Lea	ad	not exceed	mg/1	0.05	0.05	0.05	0.05	5		
Li	thium	not exceed	mg/1	-	-			2.5(d)		
Mai	nganese	not exceed	mg/l	0.5	0.5	_ ·	-	0.2	_	
Meı	reury	not exceed	mg/1	0.002	0.002	0.002	0.002	÷.	_	
Mel	lyboenum	not exceed	mg/l			_	_	0.01	_	
Nic	ckel	not exceed	mg/l		_	· _	-	0.2	_	
Sel	lenium	not exceed	mg/l	0.05	0.05	0.05	0.05	0.2	_	
Sil	lver	not exceed	mg/1	0.05	0.05	0.05	0.05	-	-	
Ver	adium	not exceed	mg/1	_		-	-	0.1	_	
Zin	10	not exceed	mg/1	5(S)	5(S)	-	2	2	-	
. Sod	lium Absorp-			,	2(4)			5		
t	tion Ratio	within	(SAR)	-			-	8-18	_ ·	
. Org	anic		(•	0-10	. 7	
Che	micals									
Syn	nthetic									
	ergents	not exceed	mg/l	NII,	0.5	0.5	0.5			
0i1	& Grease	not exceed	mg/1	NIL	2	2	5	5 .	10	
Per	sistent					14	,	,	10	
P	Pesticides									
Ald	lrin	not exceed	mg/l	0.001	0.001	0,001	0.01			
DDT	•	not exceed	mg/l	0.05	0.05	0.05	0.02		~	
Die	ldrin	not exceed	mg/l	0.001	0.001	0.001	0.005	-	-	
	ordane	not exceed	mg/1	0.003	0.003	0.003	0.00	-	-	
	rin	not exceed	mg/1	0.0002	0.0002	0.0002	0.002	-	-	
	tachlor	not exceed	$\frac{mg}{1}$	0.0001	0.0002	0.0002	0.002		-	
	dane	not exceed	mg/1	0.004	0.004	0.004	0.02	. –	-	
	aphane	not exceed	mg/1	0.005	0.005	0.004	0.02	-	~	
	hexychlor	not exceed	mg/1	0.1	0.005	0.1	0.005	-	-	
	4 - D	not exceed	mg/1	0.1	0.1	0.1		· · · ·	-	
	4, 5 – TP	not exceed	mg/1	0.01	0.01	0.01	4.0	-	-	
РСВ		not exceed	mg/1	NIL	0.001		••• ·		-	
Oth		HAA ONGCOU	11/K/ I	1111	0.001	0.001		-	-	
	hemicals									
	onia	not exceed	տg/1		0.01					
	cium	not exceed		75	0.01		-	-	-	
	oride		mg/1		-75	-	••	-	-	
	nriae nesium	not exceed	mg/1	200(a)	200(a)	-	-	-	-	
	rate	not exceed	mg/1	50(a)	50(a)	-	-	-	••	
	rate fate	not exceed	mg/1	30	30	. •	-	-		
	rients	not exceed not exceed	mg/l	200(a)	200(a)	(b) ·	<i></i>		-	
Nut:		non evened .	-	-	(b)	161	(Ъ)	(b)		

Water Quality Criteria for Fresh Surface Water by NPCC (1978) Table 6.2

NOTES:

(a) Secondary Standards; compliance with the standard analysis are not obligatory.
(b) Shall not be present in concentrations to cause deleterious or abnormal biotic growth.
(c) Secchi disk shall be visible at a min. depth of 1 M.
(d) Recommended max. concentration for irrigating is .075 mg/1.
(e) The maximum rise above natural temperature

Fig. 1.1 LIST OF CLIMATOLOGICAL STATION	Imperature Imperature Imperature <th>III III IIII III III III III III IIII IIIIIII IIIIIIII IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII</th> <th>66 66 66 66 66 7 7 7 7 7 7 7 7 7 7 7 7</th> <th>alion</th> <th>mperature il6°35' 121°15' 10100 112°15' 121°</th> <th>meeriure 16°10 120°37 600 10°1 10°1 10°1 10°1 10°1 01ion 16°48 121°27 200 10°1 10°1 10°1 10°1 10°1</th> <th>mperature 16°48 121°07' 400 Ition Ition Ition Ition Ition</th> <th></th> <th>mperoture 16° 42 121°15 280</th> <th>mperoture</th> <th></th>	III IIII III III III III III IIII IIIIIII IIIIIIII IIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIIII	66 66 66 66 66 7 7 7 7 7 7 7 7 7 7 7 7	alion	mperature il6°35' 121°15' 10100 112°15' 121°	meeriure 16°10 120°37 600 10°1 10°1 10°1 10°1 10°1 01ion 16°48 121°27 200 10°1 10°1 10°1 10°1 10°1	mperature 16°48 121°07' 400 Ition Ition Ition Ition Ition		mperoture 16° 42 121°15 280	mperoture	
Fig. 1.1	ldity	-38, 12°39	16°42'		Air Temperature Evaporation 16°35'		Air Temperature 16°48'121 Evaporation Evaporation Sunshine Mours	Evaporation Sunshine Hours	16° 42'	Air Temperature Relative Humidity Evaporation Air Temoerature	Relative Humidity Evoporation
	No. Station 1 Aparri	2 Tuguegarao	3 Echogue	4 Santo Domingo	5 Baretbet	 7 Consuelo, Santa Fe Baligatan (Taliata)	9 Lagawe 10 Wasol	11 Bontoc 12 NIA - PIO Bovembono	13 Hopid	14 Malasin	15 San Isidro

No. Station	ω	0
Aporri	1 atitude Longitude (m)	
	18° 12' 121° 40' B	
3 Agguneton, Gattoron	-	
4 Bitog Grande		
Imurung	17°55'121°56	
6 Bouan, Peñoblanca	121° 43	
Tuco	17°45/121°28' 35	
8 Tuquegorgo	121044	
_	10107	
Pinukouk	101000	
Ļ	1000101	
Tominoon		
38.	07-17	
Noneng,	121°14	
Guilgulla, Tanudan	17° 18 121° 14 500	
Tumauini	121°49	
Cabagan	121-46	
Lubuadan	120 222 11 210 021	
Baroo Ticalouat	ł	
11		
10001	1/4 50,12 60,11	
Sanga - An	17°07 120°54 1,600	
Bontoc	17° 05 120°58 855	
Barlig	17°03 121°06 1,500	
Bauko	16°59'120°52' 1.200	
Reina Mercedes	21°50	
Mt Polis, Banaue	21.00	
	116.51 1120.52 1 500	
ind iten	10000	
	5	
Nayon, Lamut		
Echague	16° 42 121°401 66	
Diadi	_	
Solono	1.010	
	1 - 1 -	
~	121°09	
Barat, Bambang	16°23 121°06 610	
Dupax	121005	-÷-
Matico	16 11 120 51 1 250	
Imunan Santa Fa		
01110 · 0	12.021	
6uoaba	16° 01' 121°21'	
Uakaan	16.05(121.30)	

HY-86

and the standard standard with the standard standard standard and the standard and the standard standard standard

No.	Station	Location	Elevotion	946	64 84 74 84	15 056	24 23 25	29 22	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	19	29 29 19	99 92 99	29	12 02 69 89	12	57 74 73	92	62 82 22	08 18 58	84	58	Applied
4	Casiauron		100 (W)			51				51 51			_	51			-		61	-	5	Study
	Toan				-	1	+		+	4			╞									*
43	Upper Casecnan				ŀ	F	<u> </u> 		+	[1	╋	-		╞	+						
-	Aurora				 -	-								1					╞			
10	Aritao						-		-			+-				+					-	
46	Kayapa											ŀ					1		+-			
	Wacał		-	+		-						+		Ī	+-	+					-	
1-	Banti					†		1	+	Ţ.		╞			╞					Ī		. *
1	Солжар					1			+	Ţ		+				-					. -	<
50	Dippodiw					<u></u> 	╞		-						+	+-					+-	*
	Tabayong						-											ŀ			-	
-	Lios, Barlig	17°05'121°	08,												+	-						
	San Francisco	18° 10' 121°	39							[1			-	*
	NiA-PIO, Cabarroguis	16° 30' 121° 32'	32' 129		F		-		-		ŀ	+-				╞						*
	Hopid, Lamut	16°42'121°	1			-	 	\vdash				-	F				ļ					*
56.	Barethet, Bagabag	16°35' 121°				+			-		+-				-							*
	Baligatan	16°48' 121º	· ·		 	+			-					1	+							: *
	Poblacion Lagawe	16°48 121°	1						-										┿			: *
		16°25 121°					<u> </u>			-			F	+	+-							
	Kesibu	16° 19' 121°				-	<u> </u>		<u> </u>		+	-	-	†	+							*
19	Kamamasi	16°16 121°25	25 639								+	╞			-							*
-	Biyoy	16°15'121°				 									-	-			ł			
_	Alayon	16°19' 121°						 			1-	╞		-					╢			*
64	Packet	16°17' 121°														ļ				1		 *
								F					Ē		-			<u> </u>				
-+					-									-							-	
-+						_									 							Γ
		-																				
												 		+-			-	-				Γ
											 	-		ŀ		.			-			
									┝	E	-	╞		ŀ			F					Γ
						-					- -		-	-					-			
									╞		+	+	F	╞	+	F	1	+	╞	İ		Γ
											\vdash	╞		$\frac{1}{1}$	╞	E	╞	+	+			
										E	╞	╞	F	╞	ŀ	F	+	+	╞	-	-	Ĩ
											-	╞		 		-					 	
-						-						╞		-	L	Ē	F	<u> </u>				Γ
									-	E			F		ŀ	E	╞				 	T
							_	-		Ē		-		-	╞	F	-	-	-			ſ

per est

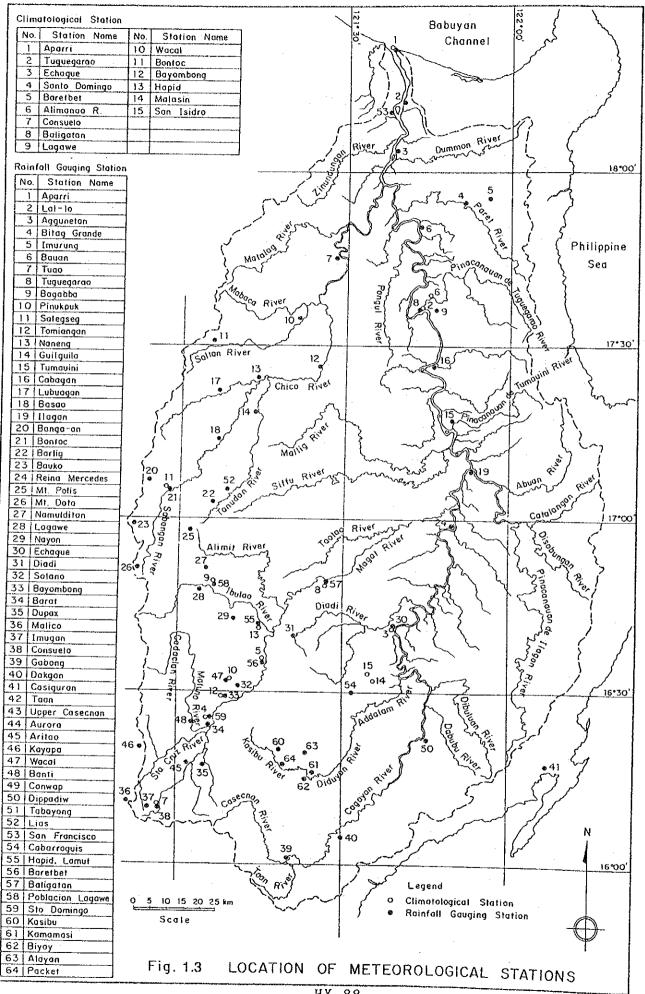
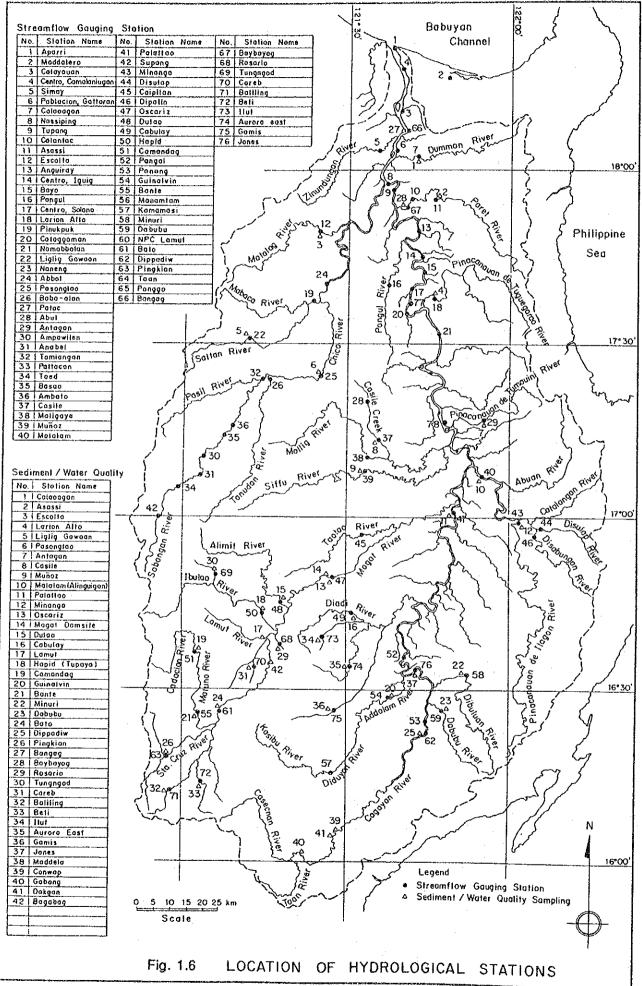


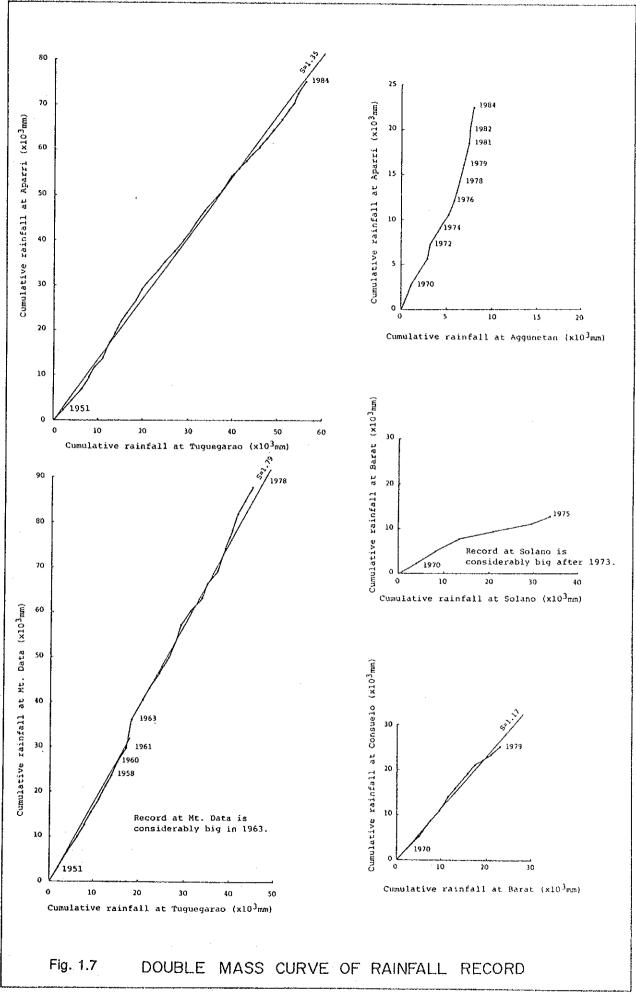
	Fig. 1.4	LIST	ОF S	STREAMFLOW		GAUGING	STATION (1/2)	Uaily Gauge Height
No. Station	River	Location Latitude Londitude	Drainage Area km 2 1	Discho	Irge Zero of Guge O	25 25 21 21	22 22 22 22 22 22 22 22 22 22 22 22 22	74 75 76 77 77 77 77 78 82 82 82 82 82 82 82 82 77 77
Aparri	Cagayan	18°22' 121	121-37 27.281		000			
	Banurbor	18°16'121	.50 112	Avoilable	-0.574			
+		18° 18' 121° 39'	121°39 27,081	1	0.0			
-+			2	0	0.0			
\dashv		18° 04' 121	121°35 189	Available				
-+		18°04' 121	121°38' 26,615	10	0.0			
Calaoagan,	Dummon	18°03'121		8 Avoilable		 		
	Cogoyan	17*58'121	3		0.0			
9 Tupong, Alcalo	Cogayan	17°57' 121°38'	121° 38' 21,436		0.0			
Calanta	Paret	17*55 121	°41 90	7 Available	3.341			
Asassi, Baggoo	Pore1	17°55' 121	121°47 730	0				
Escolto, Rizoi	Matolog	17*50'121	°25 65	5 Available				
Anguiray, Amulong	Cagayan	17°49 121	43 20.21	5	0,0			
-+	Cagayon	17.45/121	*44' 19,68;	3	0.0			
15 Baya, Iguig	Cagayan	12.42 121	•44 19,62		0.0			
16 Pangui, Solana	Pangul	17.40 121.38	•38 312	2 Available	20.399			
	Caaovan	17°39' 121°41	41 19 54		00			
			121°46 655	Available	18.184			
Pinukpi	Γ	17°37'121	.24 856	Availab				
		17°35 121	121°40 19,494		0.0			
· · ·		17°32'121°47	47 18 68		0.0			
22 Liglig Gawaan, Balbalan	T		.12 255	1				
				Available			1	
<u> </u>	Chico	17°42'121			43,497			
Pasongloo, Tabuk	Chico	17°24 121	121°25 1.987	7 Available				
Baba-Alan, Tabuk	Tanudan	17°23'121°16	16 365	Availab				
Paloc, Bobaalan	Tanudan		÷					
Abut, Quezon	Casile Creek	17°20	35 29		113.719			
Antagan, Tumauini	Pina de Tumauini	17° 17' 121°56	56 170	Available				
Ampowiten	Chice		751	Availabl				
Anobel	Chico		605	Avoilabl				
Tomiangan	Chico	17°24'121°14	-					
Pattacan, Tomlangon	Chico							
Taed	Chico	17.05 120.59		Availabl				
Basao	Chico	17-14 121	08 891	i.		┼┈		
Ambato, Tinglayan	Chico	17°16 121°09	-	Availabl				
	Cosile Creek	17°13		Availabt	49.119			
Matigaya, Mallig	Mollig	17-11-1121	<u> </u>	Available	41 716			
Muñoz, Roxas		Siffu 17°09'121°34'	34 686	Available	50.520			a
Matata (Atta ant to)		1 2000 1 2 10	1	A. allable	269.1 5 1 2 2 2			

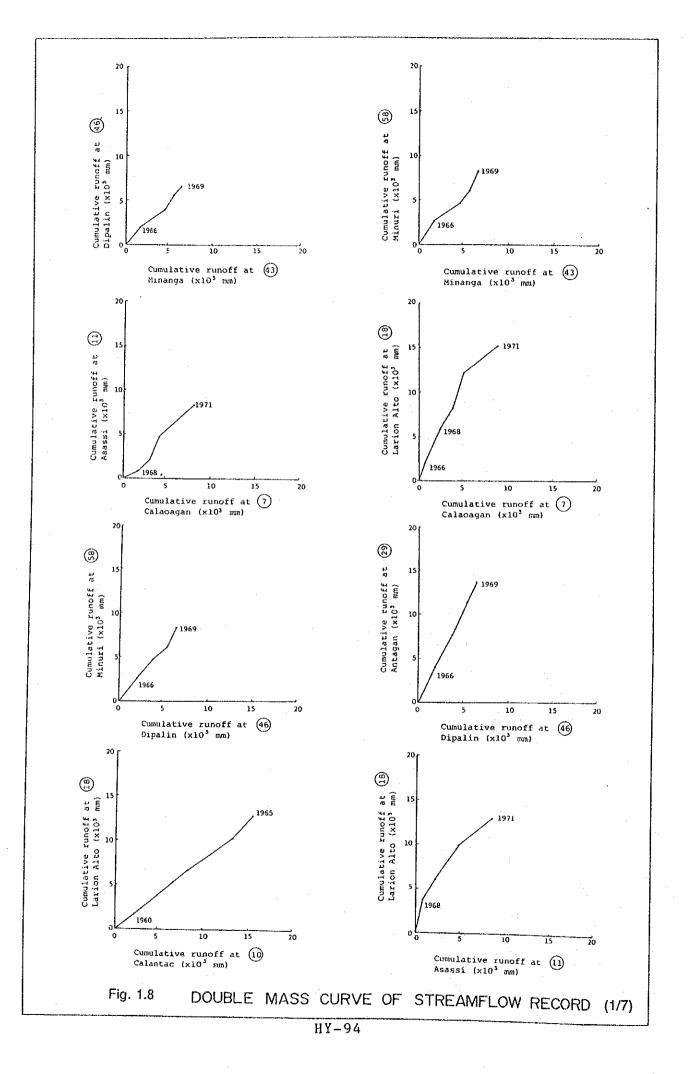
(a) A set of a set of the set of the probability of the set of

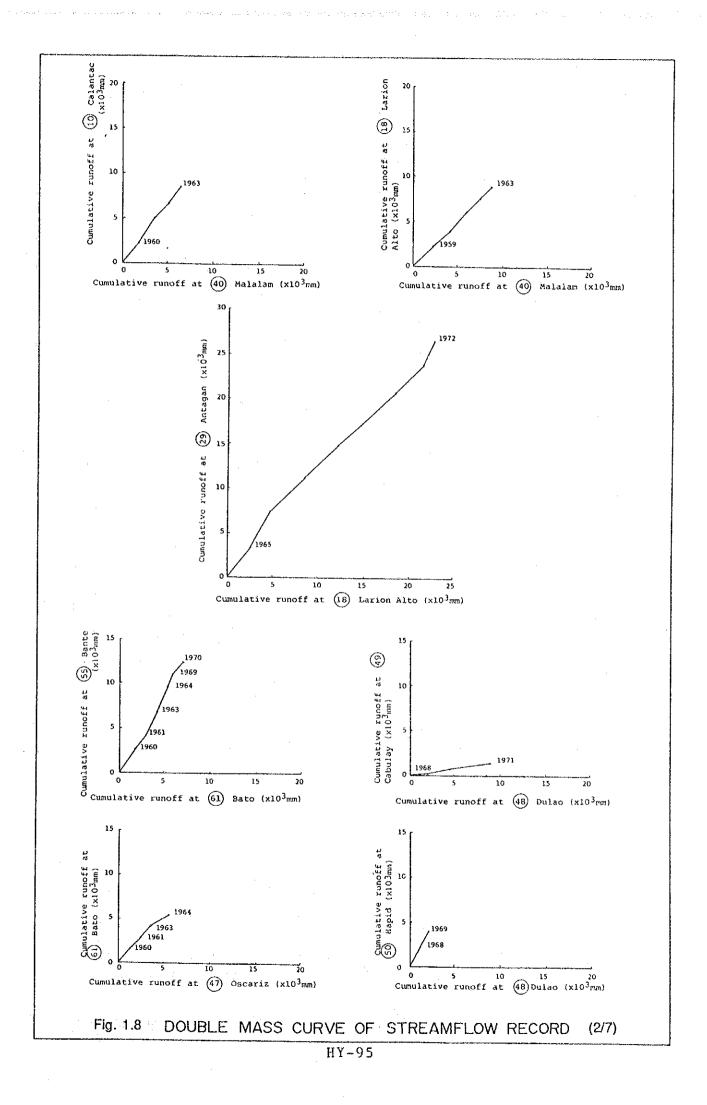
╞																				Doily Discharas	schorop
	Station	River	Lotitud	Location atitude Longitude	Areo	al Discharge Measuremer	Discharge Zero of Gouge	096	5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	29 99 99	69	19 19 19	67 66 65 66 66 67 66 67 66 66 67 67 67 67 67 67	89 29 99	12 02 69 89	57 73	92 52	62 82 22	80 80	92 94	2512120
14 14	Palattao, Naguitian	f I	17°01	121-50	1 6 62E	Available	27 227	7 181-							61		-		1.		
	Supang, Sabangan	Sabangan	17.00	120-54	57	Available			+			 	╞				or AL	n	_		
-	Minanga, SN Mariano	agai	17°00	122.01	***				-				1						-+		
-	<u>Disulap, SN Mariano</u>		16°58	122°05	Í	1									1 1						
	Calpilan, Aurora	- F	16°57	121°33	4 30		62 416	0					8] -			<u>a</u>		-+		
40		uggu	16°57	16°57' 122°04	196	Available				╹┤╴											
_ _	<u> Uscariz (Maris Dam)</u>		16°47	121°30	150		89.747			1 							+				
	Dulao, Lagawe	Alimit	16°44	121°20	573	Avoilable	1		-	4_						 [- - -		
-+	Cobulay, Santiago	Diadi	16°44	16°44'121°29	196	Available	79 487	182-								+			_		
	<u>Hapid, Lamut (Tupaya)</u>	Ibulao	16°43	127°15		Available	1	184 654								Ì	Ĩ		_]	
	Camandag, Klangan	Cadaclan	16°36	16°36'121°03'		Available				<u> </u>				Į́∏ -							
52 Po	Pangai, Echaque		16°36	121°41	4.244			+		+-				 	1	┦				6	
	Ponang, SN Agustin	Cagayan	16°25	16°25'121°45	2 392											1			, 	Ť	
_	<u>Guinalvin, Aglipay</u>		16°29	121°39		Avoilohla					 -										
	Bante, Bambang	Matuno	16°27'	121004	α 3 2	Avoitable							1			I -+)- 	
÷.,	Manamtam, Bambang	Matuno												I			I				
57 Ko	Kamamasi, Kasibu	Diduyon	16°16	121027		Aunitohla			-							-+	-+-				
	Minuri, Jones	Dibuluan														+	+				
	Dabubu, Peguiño	Dobubu	16°27	121047	101	Aunito				$\frac{1}{1}$			 		Ţ	-+-					
	NPC Lamut	Magat								$\frac{1}{1}$						╞┼				<u>}</u>	
61 80	Bato, Bayombong		16°26	121°07		Available	294 057									-#					
-+	Dippadiw, Madelta	Ģ	16°23	121°44	2,380	Available					Ц 						1.				
	Pingkian, Kayapa	N	16.19	16° 19' 120°57'		Available								-	u				+		
	Taon									<u> </u> 											
+	Ponggo, Maddela															+		10			
-+	Bangag	đ	18°07	121°41		Available	-1.52				-					-					
-+-	Baybayog		17°54	17.54 121.41	996		1.98											1		-0 -0	
	Rosario		16°39	121°18	ĺ		225.37			-						╞			-		
69 Tu	Tungngod		16°48	121.07	95							+-				 -				- { {	
	Coreb		16°34	121012																	
	Baliling	a	16°14	120°58	96	Available	487 32		1										-+-		
	ti.	Ę.	16°15	121-03	.	Available										+			+]	
73 11ut	1		16.40	16.40 1121.26		Available	145 489									-			_	Ó	
74 Aur	Aurora East	Ganano				Available					 							1		a 	
ġ	Gamis	9	16.40	121020							$\frac{1}{1}$					-			-	₿	
Jones	es	Τ	16.33	10100101		Avoitable			+		$\overline{+}$	+	+				-			0	
1.0	Tuguegorao	Γ	2	1		HVUIDDIE														a	
L L		Casavan		Ţ				+		_ _ +	$\frac{1}{1}$	+							Ö-		
			T													-			0- 	 -	
									-					-							
								_				_		- 	-	-		-			

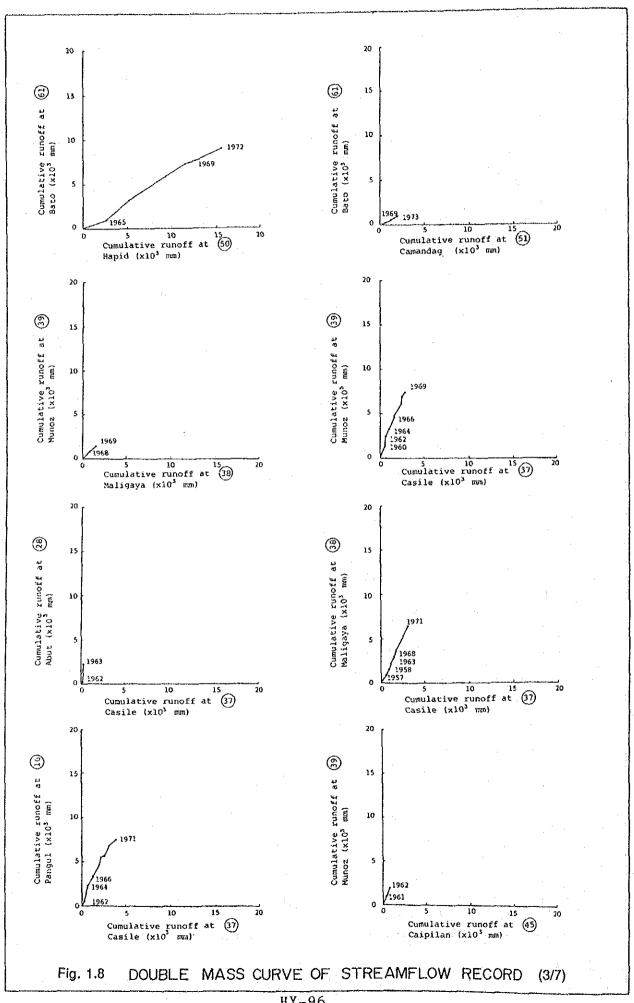
医普里耳氏 计分词分词 化分子分子分子分子分子分子 机动力的 法公共法律法 化乙基乙基乙基乙基乙基乙基乙基

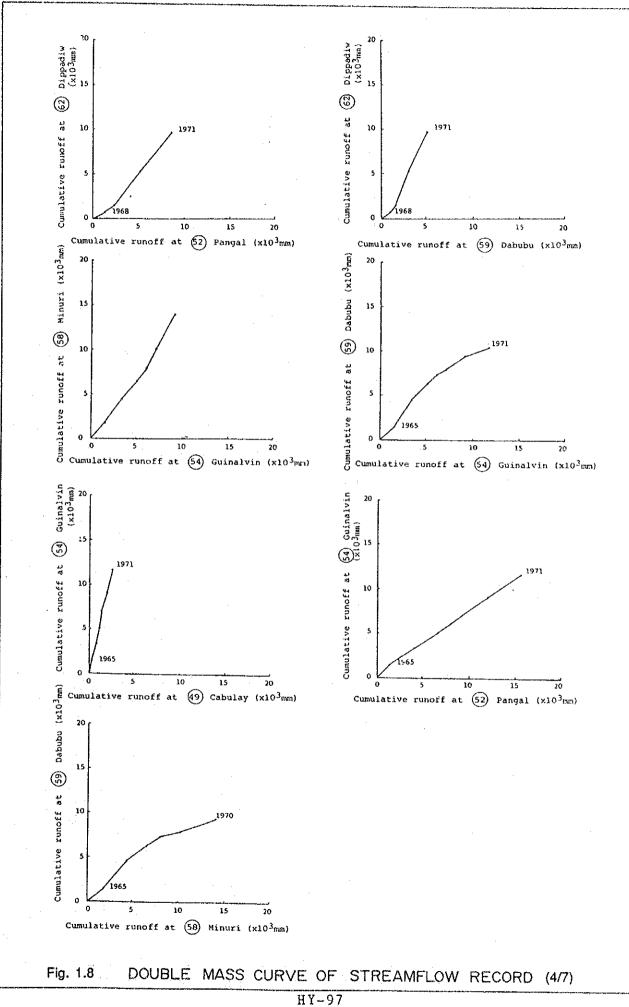


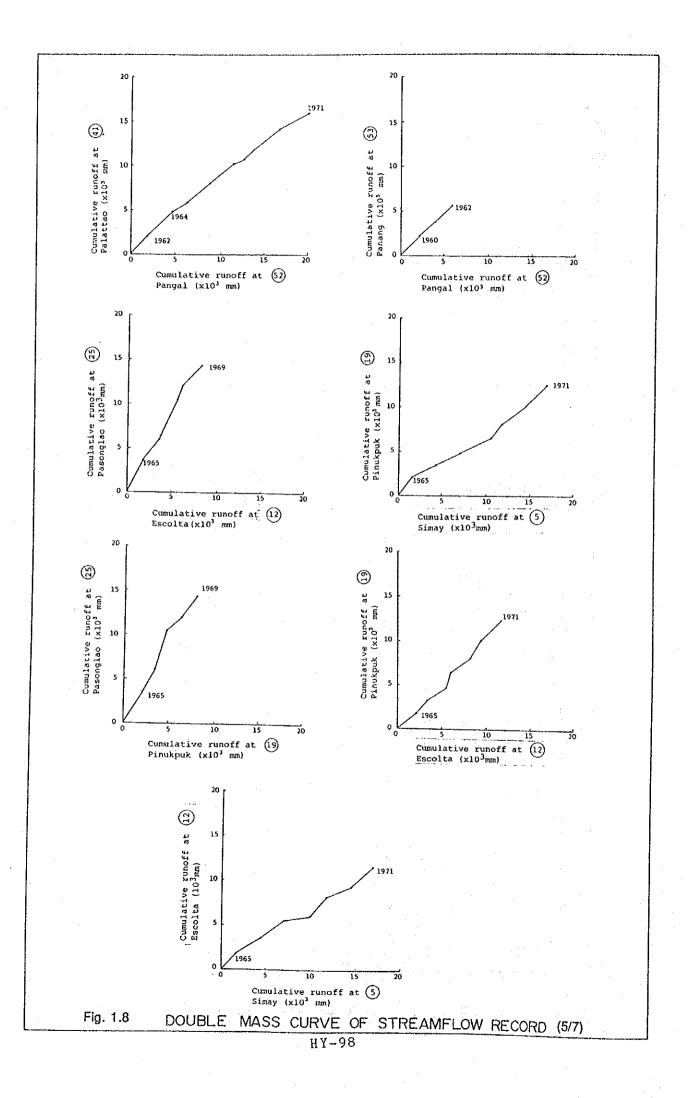


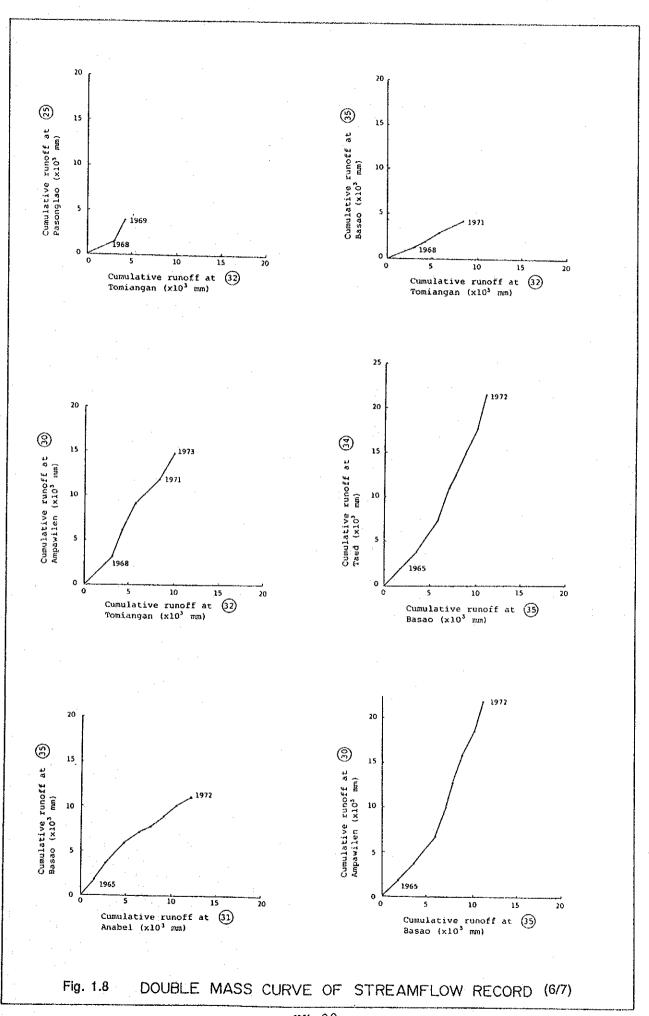


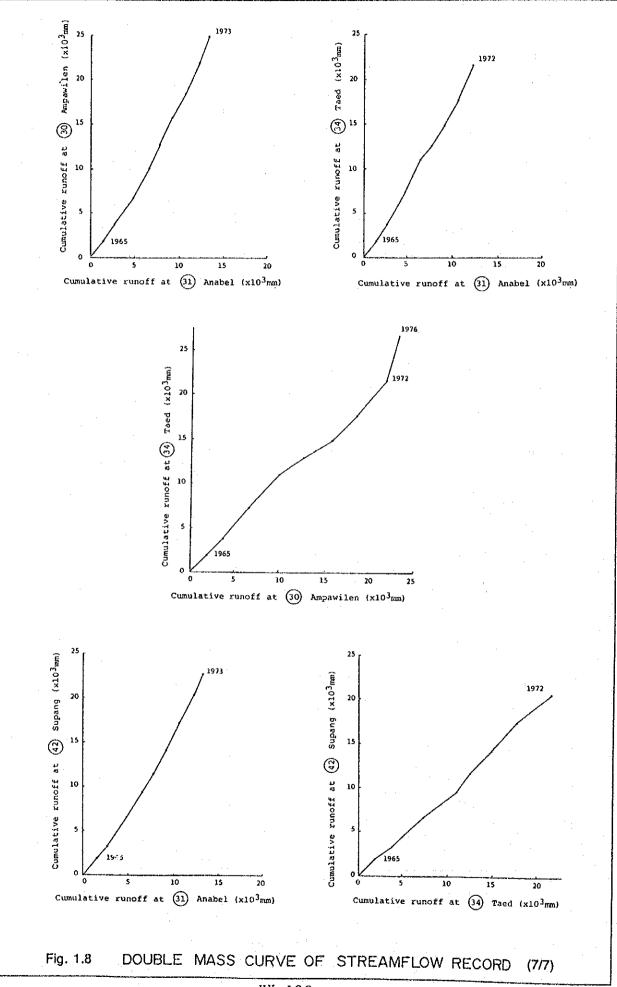


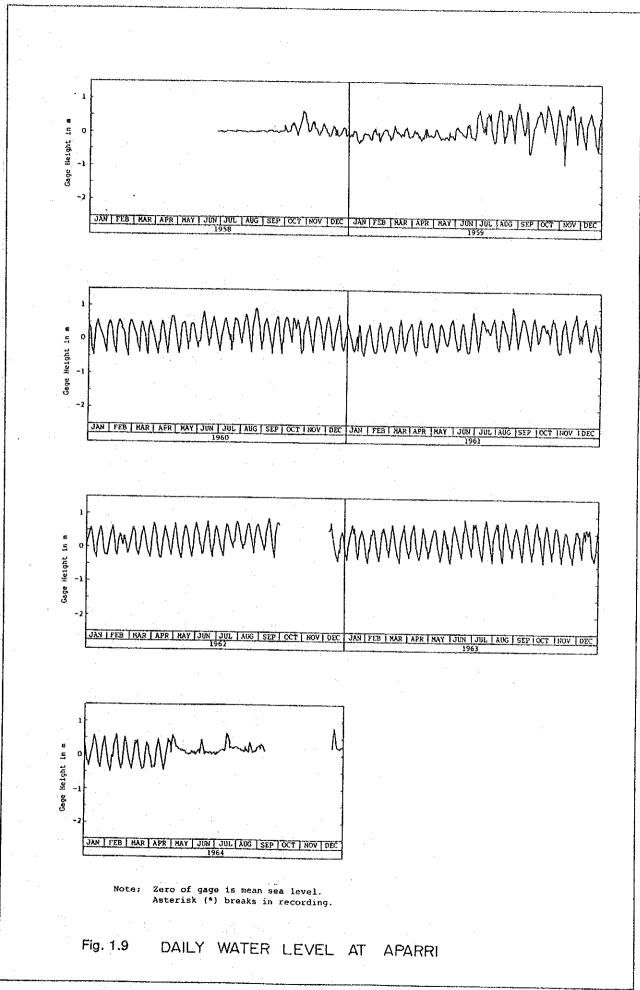


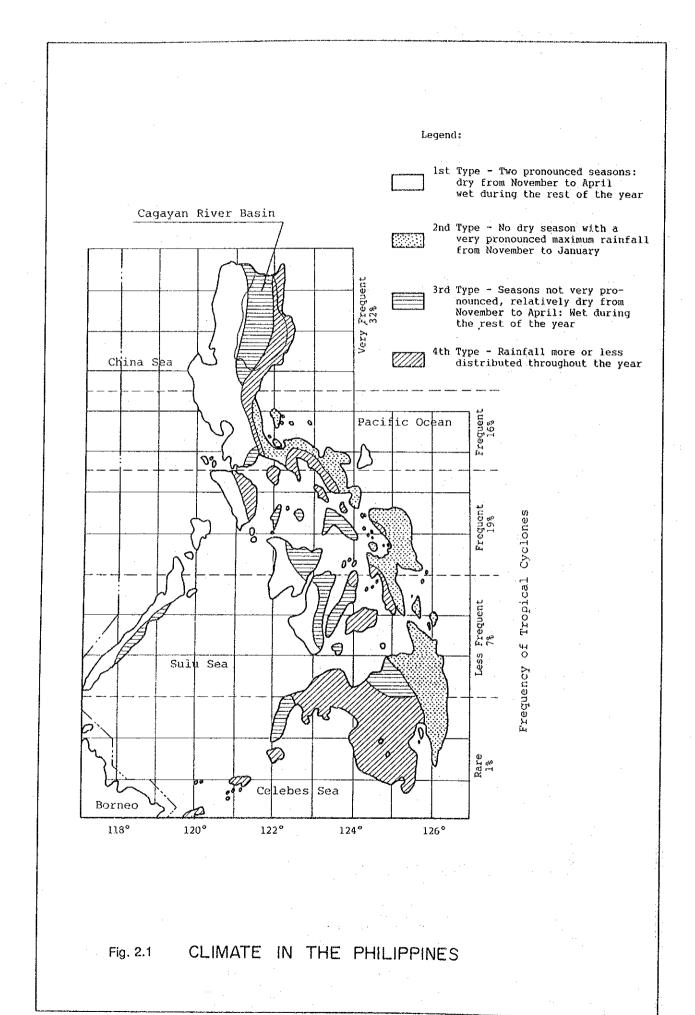












. The Carlos of the Carlos and a constant strength of the Alexandra Strength and the Carlos
