# APPENDIX 12-1 SPECIFICATION FOR CONCRETE PAVEMENT

## TABLE 1 STANDARD SPECIFICATION FOR CONCRETE PAVEMENT REVISED 1972

Specification Item		Description
1. Aggregate Subbase Materials	1)	Proportion of the filler passing N 200 sieve to that passing N 040 sieve is less than 2/3 and not to exceed of total
	. 2)	Liquid limit = less than 25
		Plasticity index = less than 6
Compaction	1)	More than 95% of maximum density as determined by AASHTO T-180, C or D.
2. Concrete Slab Materials	1)	Cement = the requirement of AASHTO M 85 shall be conformed.
	2)	Fine Aggregate =
		Sieve Size Percent Passing
		3/8 inch 100 # 4 95-100 # 16 45-80
		# 50 10- 30
		#100 2- 10
·	3)	Coarse Aggregate
		Passing (40) Grading A Grading B Grading C
		2-1/2" 100%
		2" 100% 95-100
		1-1/2" 95-100 100% 1" 35- 70 95-100
		3/4" 35- 70 1/2" 10- 30 25- 60
		3/8" 10- 30 No. 4 0- 5 0- 5 0- 10
		- Abrasion loss = less than 45
Concrete Strength		- Not specified
Measuring of Materials		<ul> <li>In principal, measured by weight but by equivalent volume will be permitted in special case.</li> </ul>
		- Water shall be measured for each batch by accurate measure device.
Mixing		- Mixer with capacity at least 27 cubic feet
		- Maximum net water content per bag of cement is 23 liters.
		- Amount of cement is $7.85\ \mathrm{bag}\ \mathrm{per}\ \mathrm{cubic}\ \mathrm{meter}.$
		- Slump is within ranging from 5 cm to 7.5 cm.
Finishing and Compaction		<ul> <li>In principal, a mechanical concrete spreader and a finishing machine with vibrating, screeding and trowelling functions shall be use but hand finishing will be permitted in specia case.</li> </ul>

## TABLE 2 BPH MEMO CIRCULAR FOR CONCRETE PAVEMENT

Item 316 - Portland Cement Concrete Pavement

Cement - Type I, Portland Cement ASTM C-150 or AASHO M-85, Fine Aggregate:

Sieve Designation	% Passing
3/8" No. 4 No. 16 No. 50 No. 100 No. 200 (by Washing) Mortar Strength - 90% min. at 7 days	100 95 - 100 45 - 80 10 - 30 2 - 10 0 - 3

## Coarse Aggregate

Sieve Designation	Grading A	Grading B	Grading C
2- 1/2"	•	100	
2 <sup>n</sup>	100	95 - 100	100
1-1/2"	95 - 100		100
1"		35 - 70	95 - 100
3/4" 1/2"	35 - 70		
1/2"		10 - 30	25 - 60
3/8"	10 - 30		*
No. 4	0 - 5	0 - 5	0 - 10
o. 200 (By washing)			

Abrasion Loss: 45% max.

Water - Odorless, colorless, tasteless

Proportioning of Concrete: -

At least 4.5 bags/cu.yd (8.5 bags/m<sup>3</sup>) based on 94-1b bags of cement. (BPH Mens. Circular No. 48 dated April 25, 1973)

Water - 6 gallons (23 L) max. per 94-lb. bag.

Slump -2 to 3 inches (5 to 7.5 cm)

Flexural Strength at 14 - days (BPH, Memo. Circular No. 48): 525 psi by third-point method 600 psi by mid-point method

## GENERAL SPECIFICATIONS FOR CONCRETE PAVEMENT

1976

#### ITEM 301 GRANULAR SUB-BASE

#### 301.1 DESCRIPTION

- This item shall consist of furnishing, spreading and compacting granular sub-base in accordance with the Specification and the Drawings. Granular sub-base shall consist of natural or processed aggregates such as gravel, sand or stone fragments which shall conform to the following requirements.
- 2. Sub-base material shall be either Class A or Class B as shown on the Drawings.
- 3. Where sub-base is required to be placed on a subgrade consisting of an existing cement concrete pavement prepared in a accordance with Clause 205.2.6 and where the surface levels of the resulting subgrade level are outside the permitted tolerance given in Table a levelling course of sub-base material shall be laid as shown on the Drawings. This work shall comply with the requirements of this Item.

## 301.2 MATERIAL REQUIREMENTS

- The granular sub-base material shall be clean and free from organic matter and other deleterious substances and shall be of such nature that it can be compacted readily under watering and rolling to form a firm, stable base.
- 2. The material shall comply to the following grading and quality requirements.
  - (a) The sub-base material shall have a grading curve within the limits of either Class A or Class B given in Table The Coefficient of Uniformity  $D_{60}/D_{10}$  shall be not less than 3, where  $D_{60}$  and  $D_{10}$  are the particle diameters corresponding, respectively, to 60% and 10% passing (by weight) in a grain size analysis.

TABLE 3 SUB-BASE MATERIAL GRADING

US Standa	rd Sieve	Percent Passing By Weight
nun	Alternative	Class A Class E
75	(3")	100
37.5	(1 1/2")	80 - 100 100
9.5	(3/8")	45 - 100 -
4.75	(No. 4)	30 - 85 60 - 100
2.00	(No. 10)	15 - 65 40 - 90
0.425	(No. 40)	5 - 35 15 - 50
0.075	(No. 200)	0 - 15 2 - 15

- (b) The material shall have a soaked CBR-value of not less than 25%, determined according to ASTM D1883. The CBR-value shall be obtained at a density corresponding to 98% of the maximum dry density determined according to AASHTO T180 Method D.
- (c) The coarse aggregate material retained on a 4.75 mm (No. 4) sieve shall have a percentage of wear by the Los Angeles Abrasion test (AASHTO T96) of not more than 50.
- (d) The maximum dimension of any particle shall be not greater than two-thirds of the required thickness of the layer in which it is to be placed. Oversize material if present shall be removed at the pit by screens or grizzlies or by hand picking.
- (e) In order to avoid intrusion in the sub-base of silty and clayey material from the subgrade, it will be required that the ratio  $D_{15}$  (Sub-base)/ $D_{85}$  (Subgrade) is less than 5, where  $D_{15}$  and  $D_{85}$  are the particle diameters corresponding, respectively, to 15% and 85% passing (by weight) in a grain size analysis.
- 3. The portion passing the 0.425 mm (No. 40) sieve shall have a liquid limit not greater than 35 and a plasticity index not greater than 11 as determined by AASHTO T89 and T90 respectively.

#### ITEM 406 CEMENT CONCRETE PAVEMENT

### 406.1 DESCRIPTION

This work shall consist of constructing a pavement of portland cement concrete on a prepared base in accordance with the Specification and the Drawings.

### 406.2 CLASSES OF CONCRETE

The classes of concrete for cement concrete pavement shall be Class E and Class F. The concrete shall satisfy the requirements of Table 4.

TABLE 4 REQUIREMENTS FOR CEMENT CONCRETE

Class	of C	Size oarse egate	28 day Con Stre	ength	28 day l Stren	
	mm	<u>in</u>	kgf/cm~	N/mm	kgf/cm	N/mm
E	75	(3)	280	(28)	43	(4.3)
F	50	(2)	280	(28)	43	(4.3)

#### 406.3 MATERIAL REQUIREMENTS

### 406.3.1 Portland Cement

Portland Cement shall conform to the requirements of clause 501.3.1.

### 406.3.2 Fine Aggregate

Fine aggregate shall conform to the requirements of Clause 501.3.2.

### 406.3.3 Coarse Aggregate

The coarse aggregate shall conform to the requirements of Clause 501.3.3.

## 406.3.4 Combined Aggregate

The aggregate shall unless otherwise ordered by the Engineer be combined in proportions to produce a mixture within the grading limits for combined aggregates shown in Table 5.

TABLE 5 GRADING OF COMBINED AGGREGATES

US Star	ndard Sieve	Percent Passi	
nm	Alternative	Class E	Class F
75	(3")	100	7 ( <del>-</del>
63	$(2\frac{1}{2}^{1})$	95 - 100	
50	(2")	80 - 95	100
37.5	$(1\frac{1}{2}")$	65 - 87	80 - 100
25	(1")	50 - 75	50 - 86
19	(3/4")	45 - 66	45 - 75
9.5	(3/8")	38 - 55	38 - 55
4.75	(No. 4)	30 - 45	30 - 45
2.36	(No. 8)	23 - 35	23 - 38
1.18	(No. 16)	17 - 27	17 - 33
0.600	(No. 30)	10 - 17	10 - 22
0.300	(No. 50)	4 - 9	4 - 10
0.150	(No. 100)	1 - 3	3 1 - 3
0.075	(No. 200)	0 - 2	0 - 2

# APPENDIX 12-2 PRESENT STATE OF ASPHALT PAVEMENT

#### PRESENT STATE OF ASPHALT PAVEMENT

#### 1 Material

## 1-1 Petroleum Asphalt

Crude Oil materials are mainly imported from the Middle East of varying types namely: the Arab Heavy, Arab Medium, and Kuwait types. Recently, crude oil has been produced from Philippine oil wells namely: the Minas, Tapis, Matinloc, Nido, Cadlao, etc.

## 1-1-1 Present Quantity of Production

Various petroleum companies have put up their refinery plants using crude oil or raw materials. Importation of crude oil are shown in Table 1 decreasing by year in thousand barrel as a result of inventory draw down.

TABLE 1
CRUDE OIL IMPORTATION (MB)

	1980	1981	1982	1983	1984	1985
Crude Oil	68,014	60,761	57,003	59,827	49,453	48,843

MB = Volume in Thousand Barrels
DATA SOURCE: Bureau of Energy

Total refinery production indicating percentage share of each By Products are shown in Table 1-1-1B.

TABLE 2 % SHARES OF REFINERY PRODUCTION 1980 - 1985

		4				
	1980	1981	1982	1983	1984	1985
AVGAS	-4	-0.01	ښـ	-0.01	-0.01	0.02
AVTURBO	3.5	3.3	4.4	11.9	7.0	6.2
Premium Gasoline	9.3	9.5	11.4	26.3	11.3	13.7
Regular Gasoline	8.6	6.9	4.9	11.6	4.4	5.2
Diesel	5.5	6.8	6.5	6.1	4.2	4.4
Fuel Oil	26.2	26.7	27.2	28.7	31.4	32.0
Kerosene	41.7	41.7	39.4	36.1	34.7	32.0
PG	0.4	0.3	0.3	0.3	0.3	
LPG	2.8	2.1	2.1	2.6	2.8	3.2
Asphalt	0.5	0.6	0.7	1.0	0.6	0.5
Solvents	0.4	0.3	0.8	0.6	0.3	0.4
Naphtha	1.2	1.6	2.3	4.0	3.0	2.2
Others		•	· · · · · · · · · · · · · · · · · · ·		<b>*-</b>	hed .
Total Refinery Products	100.0	100.0	100.0	100.0	100.0	100.0

DATA SOURCE: Bureau of Energy

The total petroleum asphalt of production is shown in Table below.

TABLE 3
PETROLEUM ASPHALT PRODUCT

Name of Company	1984	1 9 8 5
Petrophil. Corporation	47,180 m. ton	38,830 m. ton

DATA SOURCE: Petrophil. Corporation

## 1-1-2 Productive Capacity

There are only three major companies that produce asphalt. Their capacity are shown in Table

TABLE 4
PLANT REFINERY CAPACITY

Capacity Per Day		
150,000 Barrel/day		
70,000 Barrel/day		
65,000 Barrel/day		
285,000 Barrel/day		

DATA SOURCE: Bureau of Energy

## 1-1-3 Quality

The quality of Asphalt produced are shown in Table 5 below.

TABLE 5
ASPHALT GRADE PRODUCED

Asphalt Type	Grade	%
Asphalt Cement	60/70, 85/100, 150/200	80%
Emulsified Asphalt	SS-1	10%
Cutback Asphalt	MC-70, MC-250, RC-800	10%
Oxidize Asphalt		

DATA SOURCE: Petrophil. Corporation

## 1-2 Aggregates

There are two ingredients in asphalt construction - aggregate, including mineral filler if it is used, and asphalt. The performance of asphalt structure can be influence by the properties of the aggregate and of the asphalt used.

Aggregate is the most important ingredient in asphalt paving. It is 92 to 96 percent of the weight of mixture. The aggregate fraction consist of coarse aggregate, fine aggregate and mineral filler. The dividing size between coarse and fine aggregate is 2.36 mm.

Coarse aggregate maybe obtained from gravel deposits or stone quarries. The source of fine aggregate are natural deposits of bank, river sand or screening from aggregate crushing plants.

Sand includes natural sand, artificial sand, crushed stone, dust, etc. Natural sand is classified by source of product into river sand, pit sand and sea sand. The most common source of sand used for road pavements originates from the rivers.

## 1-3 Filler

Mineral filler may consists of finely ground limestone, rock powder, naturally-occuring silt, portland cement, hydrated lime or similar clean non-plastic finely divided mineral matter. It may occur naturally in the fine and coarse aggregate as mineral dust or it maybe added as a separate ingredient.

## 2. <u>Asphalt Concrete</u>

Bituminous mixture is a proportioned combination of bituminous material and aggregate with or without mineral filler. The common practice is without mineral filler. The Asphalt Penetration Grade is 85 - 100.

A bituminous paving mixture is called "Plant Mix" if it is prepared in a central mixing plant. Depending on the grade of

aggregate, the mixture maybe classified into dense graded and open graded. Both types maybe road or plant mix designed as base or surface courses. All types of bituminous materials maybe used except the rapid-curing cutbacks and the rapid-breaking emulsions.

### 3. Paving Operation

Paving Operation includes the preparation of the paving equipment and inspection of the Binder and the base. Check the paving equipment since the breaking down would affect the paving operation. The surface must be cleaned of loose and foreign material.

A Tack Coating is applied to the surface of an underlying course by spraying emulsified asphalt. The most common use is the Asphalt Sprayer or Asphalt Distributor. The rate of application of emulsified asphalt used in tack coating is within the range from 0.4 to 0.8 liters per square meter.

The most common use equipment is the Baber Greene and Blawknox for spreading. The paving width of the equipment is 3 meters. The spreading and finishing equipment in operation leaves in the new surface course tracks or indented areas that are not corrected by the scheduled operations or if other blemishes are produced, the use of such equipment shall be discontinued.

After spreading the material shall be thoroughly compacted to the required lines, grades and cross section by means of pneumatic tampers, or with other compacting equipment which consistently obtain the degree of compaction required. The compacting equipments use are the Macadam Roller, Pneumatic Self Propelled Roller and Tandem Static Smooth Drum Roller.

Joint shall be formed by cutting back on the previous days run so as to expose the full length of the course. The exposed edge shall be painted with a thin coat of hot asphalt cement or asphalt cement thinned with naptha, or emulsified asphalt. The fresh mixture shall be raked against the joint, thoroughly tamped with hot tampers and rolled.

## 4. Quality Control and Inspection

A higher degree of quality control is necessary in asphalt construction, compared to concrete construction. The temperature control is important since the asphalt is semi-solid under normal temperatures. Control of asphalt is also critical, since too much or too little of asphalt in the mixture will make it unstable. The quality control measures should be strictly followed in order to expect satisfactory performance of the asphalt structures.

Inspection involves investigation of the work done and material quality of the finished pavement, to check whether all aspects of pavement quality satisfy the requirements of contract plans and specification.

APPENDIX 12-3
TRAFFIC REGULATIONS

TABLE 1 COMPARATIVE TABLE OF VEHICLE WEIGHTS BY VARIOUS ACTS, LETTERS OF INSTRUCTIONS AND MEMORANDA

Type of Wheel/Axle/	RA 4136	101 112	101.874	Menorandum	Memorandum	Menorandum	Mrwh Memorandum	Memorandum of
ITUCK	1904	19/3	13/3	25 July 1977	or 8 Jan. 1979	18 Dec. 1979	11 Nov. 1981	13 May 1983 <u>d</u> /
Per most heavily loaded wheel	3,600 kg							
Per most heavily loaded axle	8,000 kg							-
Per most heavily loaded								
being at least I m & less	14,500 kg							
Iruck with two axles		- 1	14 tons b/	14,700 kg to	15.000 kg	16.000 kg	15.000 kg	15,000 kg
wheels   Iruck with tandem rear		15 tons	25 tonsb/	19,000 kg-/	21 000 10	64 000 36	21 000 1.0	21 000 10
axles (3 axles/10 wheel)		15 tons a/	net weight	20,000 kgc/	21,000 kg	25,000 Kg	21,000 xg	21,000 xg
five axles (18 wheels,		27 tons a/			33,000 kg		33,000 kg	33,000 kg
Code 12-2)					:			
fruck semi-trailer with four axles (14 wheels,	* -	27 tons <sup>a</sup> /					27,000 kg	27,000 kg
code 11-2 or 12-1)								
inuck semi-tralier with three axles (10 wheels, Code 11-1)		27 tons <sup>a</sup> /					20,000 kg	29,000 kg
Truck trailer with two								
axies at motor vehicle and two axies at trailer (Code 11-11)							28,000 kg	28,000 kg
Truck trailer with two								
axles at motor vehicle			-				34,000 kg	34,000 kg
and three axles at trailer (Code 11-12)								
Truck trailer with three								
axles at motor vehicle						ć	35 000 40	35,000 %g
and two axles at trailer							\$4 000 for	fu 200 to 2
(code 12-11)								
iruck trailer with three axles at motor vehicle							-	
and three axles at				-			41,000 kg	41,000 kg
trailer (Code 12-12)				:				

P/The net load (metric tons) allowed by LOI No. 874 relates to palay, rice and corn only. The net limits were subsequently changed to gross weights of 19,000 kg for 6-wheelers and 30,000 kg for 10 wheelers, vide MPWH Memorandum date 7 May 1981. The LOI is still in force.

d/The weights were limited to specific truck models, and did not include all truck models.

Between the Ministry of Public Works and Highways, the Ministry of Transportation and Communications and Ministry of Defense. This Memorandum of Agreement has been signed by the respective Ministries but the implementing guidelines have yet to be introduced and it is not inforce.

## PROPOSED TRAFFIC REGULATIONS

## CHAPTER III. PERMITTED WEIGHTS AND OVERALL DIMENSIONS OF VEHICLES

## Article 5. Permitted Axle Loads

- (a) The weight transmitted to the road surface by all the wheels of a single two tire axle shall not exceed 8,000 kg. A tandem axle shall be regarded as two single axles in this respect.
- (b) The weight transmitted to the road surface by all the wheels of a single four tire axle shall not exceed 13,000 kg. A tandem axle shall be regarded as two single axles in this respect.
- (c) The weight transmitted to the road surface by all the wheels of a three axle bogie (12 wheels) shall not exceed 30,000 kg.
- (d) The weight transmitted to the road surface by all the wheels of a three axle bogie (6 wheels) shall not exceed 23,000 kg.

## Article 6. Permitted Gross Weights For Trucks -

- (a) The sum of the weights transmitted to the road surface by all the wheels of a truck with two axles (6 wheels) shall not exceed 18,000 kg.
- (b) The sum of the weights transmitted to the road surface by all the wheels of a truck with three axles (10 wheels) of which two form a tandem with a single motive axle shall not exceed 28,000 kg.
- (c) The sum of the weights transmitted to the road surface by all the wheels of a truck with three axles (10 wheels) of which two form a tandem with two motive axles shall not exceed 31,000 kg.
- (d) The sum of the weights transmitted to the road surface by all the wheels of a truck with three axles (8 wheels) of which two axles are steering axles shall not exceed 26,000 kg.
- (e) The sum of the weights transmitted to the road surface by all the wheels of a truck with four axles (12 wheels) shall not exceed 38,000 kgs.
- (f) The sum of the weights transmitted to the road surface by all the wheels of a truck other than those specified in 6(a),

6(b), 6(c), 6(d), and 6(e) <u>supra</u> shall not exceed 90 (ninety) percent of the sum of the maxium permitted loads on the individual axles of the truck.

## Article 7. <u>Permitted Gross Combination Weights</u> For Articulated Vehicles

- (a) The sum of the weights transmitted to the road surface by all the wheels of an articulated vehicle with three axles (10 wheels) shall not exceed 31,000 kg.
- (b) The sum of the weights transmitted to the road surface by all the wheels of an articulated vehicle with four axles (14 wheels) shall not exceed 41,000 kg.
- (c) The sum of the weights transmitted to the road surface by all the wheels of an articulated vehicle with five axles (18 wheels) shall not exceed 50,000 kg.
- (d) The sum of the weights transmitted to the road surface by all the wheels of an articulated vehicle with six axles (22 wheels) shall not exceed 50,000 kg where the length of the vehicle, not including projecting load, is less than 14 (fourteen) meters and shall not exceed 54,000 kg where the length of the vehicle, not including projecting load, is 14 (fourteen) meters or more but less than 15.5 (fifteen and a half) meters and shall not exceed 58,000 kg where the length of the vehicle, not including projecting load, is more than 15.5 (fifteen and a half) meters.
- (e) The sum of the weights transmitted to the road surface by all the wheels of an articulated vehicle other than those specified in 7(a), 7(b), and 7(c) and 7(d) supra shall not exceed 90 (ninety) per cent of the sum of the maximum permitted loads on the individual axles of the vehicle.

## Article 8. Permitted Gross Weights for Drawbar Trailers

- (a) The sum of the weights transmitted to the road surface by all the wheels of a drawbar trailer with three axles (12 wheels) or more (12 wheels or more) shall not exceed 33,000 kg.
- (b) The sum of the weights transmitted to the road surface by all the wheels of a drawbar trailer other than those specified in 8(a) supra shall not exceed 90 (ninety) percent of the sum of the

maximum permitted loads on the individual axles of the trailer.

Article 9. Permitted Gross Combination Weights For Truck-Trailers

The sum of the weights transmitted to the road surface by all the wheels of a truck-trailer shall not exceed 50,000 kg where the length of the truck-trailer, not including projecting load, is less than 14 (fourteen) meters and shall not exceed 54,000 kg where the length of the truck-trailer, not including projecting load, is 14 (fourteen) meters or more but less than 15.5 (fifteen and a half) meters and shall not exceed 58,000 kg where the length of the truck-trailer, not including projecting load, is more than 15.5 (fifteen and a half) meters.

## APPENDICES FOR CHAPTER 13

# APPENDIX 13-1 FORMATS FOR PAVEMENT CONDITION SURVEY

## TABLE 1 INDIVIDUAL PRESENT SERVICEABILITY RATING

BOUND:	DATE:
ROAD SECTION:	RATER:
	VEHICLE:

1/41	s	urface	Cor	ndition		A	ceptal	ole
KM.	VG	G	, F	Р	VΡ	YES	NO	Un- decided
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				•				
				-				
	·							·
		,						
						·		

POINTS		SURI	FACE CONDITION
5 ~ 4	-	Very Good	(VG)-Very Comfortable
4 ~ 3		Good	(G) - Comförtable
3 ~ 2		Fair	(F) -Satisfactory
2 ~ 1		Poor	(P) - Uncomfortable
1 ~ 0		Very Poor	(VP)-Very Uncomfortable

# TABLE 2 INDIVIDUAL REHABILITATION REQUIREMENT RATING

ROAD SECTION:			alada ayad Püyl marma qayad bibib	R			
		Surfac	e Con		EHICLE		cceptable
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Color of the Color	**************************************						
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	_	-					
			7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7				
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	-						

POINTS	SURFACE CONDITION	REMARKS
5 ~ 4 -	- No Deficiencies	A - Sealing
4 ~ 3 -	- Little Deficiencies	B - Patching
3 ~ 2 ~	<ul> <li>Considerable Deficiencies but Immediate treatment is not required.</li> </ul>	Association of the second
2 ~ 1 -	Considerable severe deficiencies, immediate treatment is required	7 13
1 ~ 0 -	Reconstruction is immediately required.	. W.

TABLE 3 OCULAR SURVEY OF PAVEMENT DEFICIENCIES AND GENERAL INFORMATIONS

Bound ...

Date : .\_\_

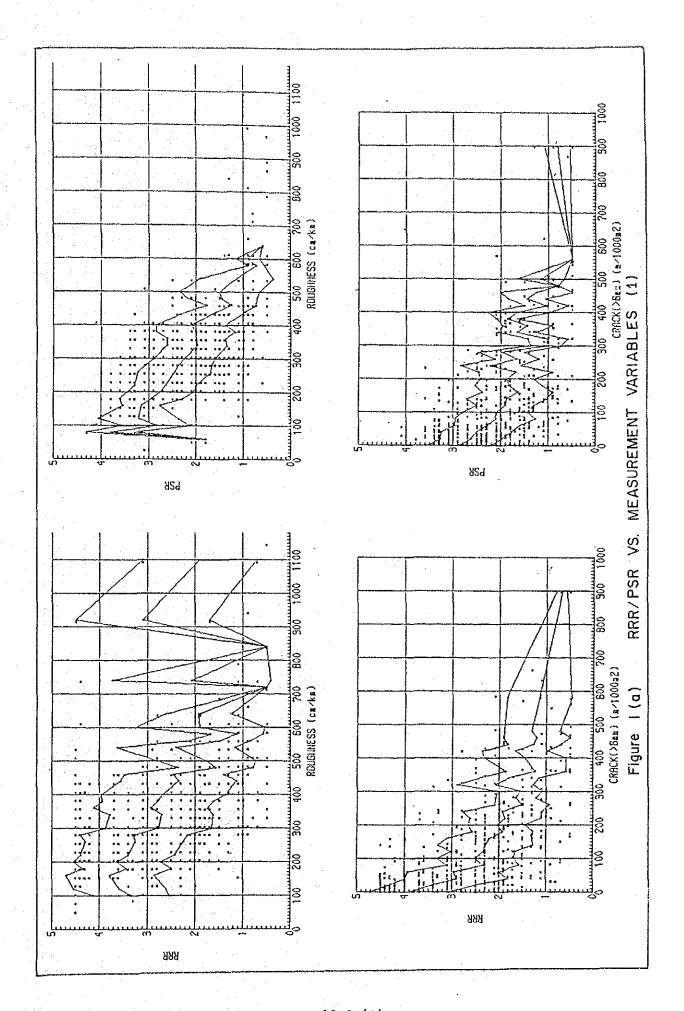
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			4		Forest (F)									4;		/Rando	Block / Random Cracking (A)	dng (A)		
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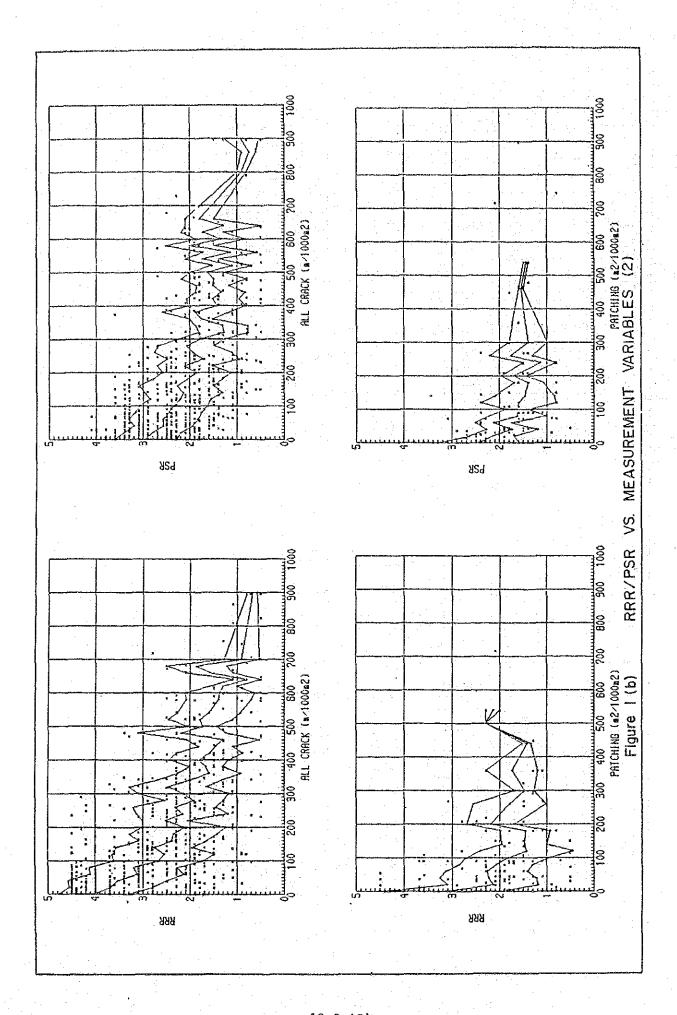
## TABLE 4 ROUGHNESS SURVEY

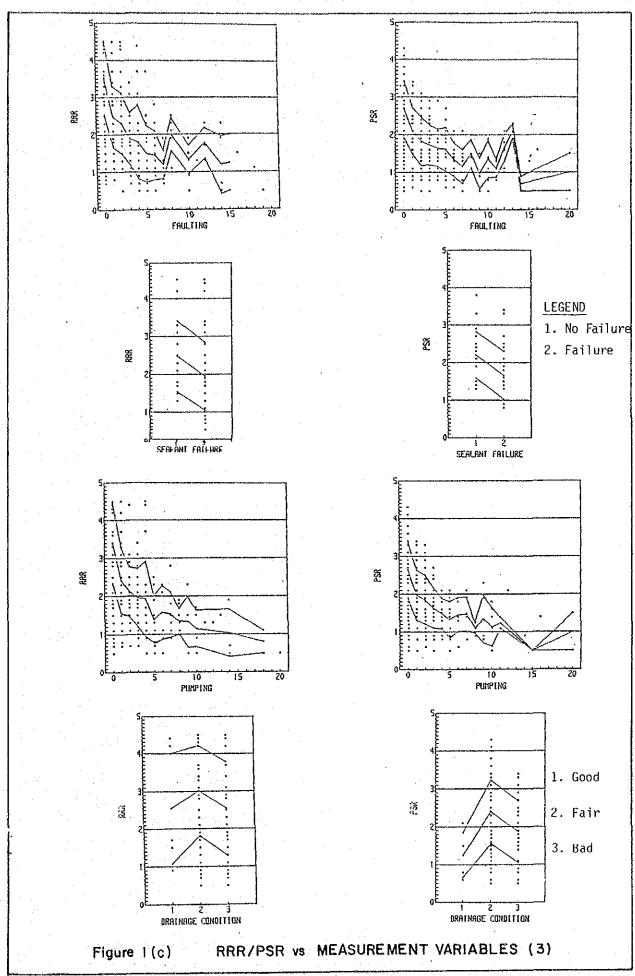
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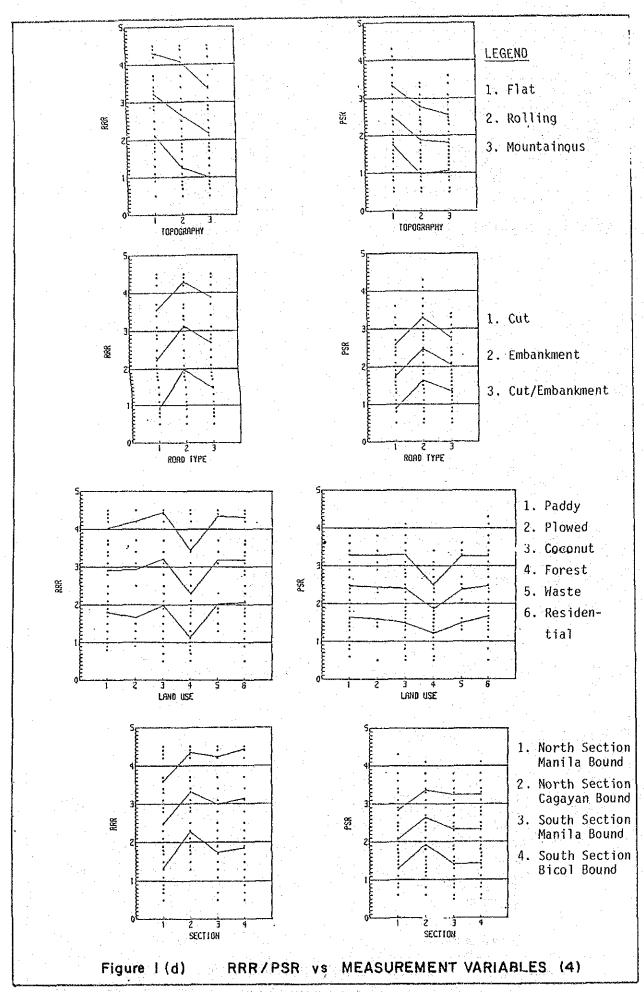
## APPENDIX 13-2

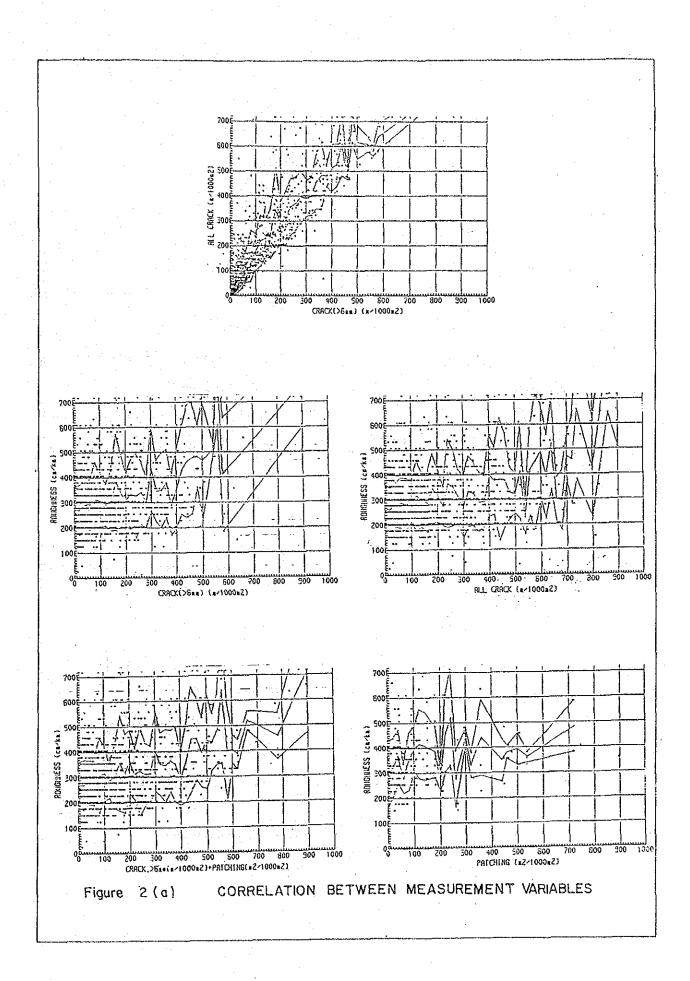
## CORRELATION ON MEASUREMENT VARIABLES ON PAVEMENT CONDITIONS

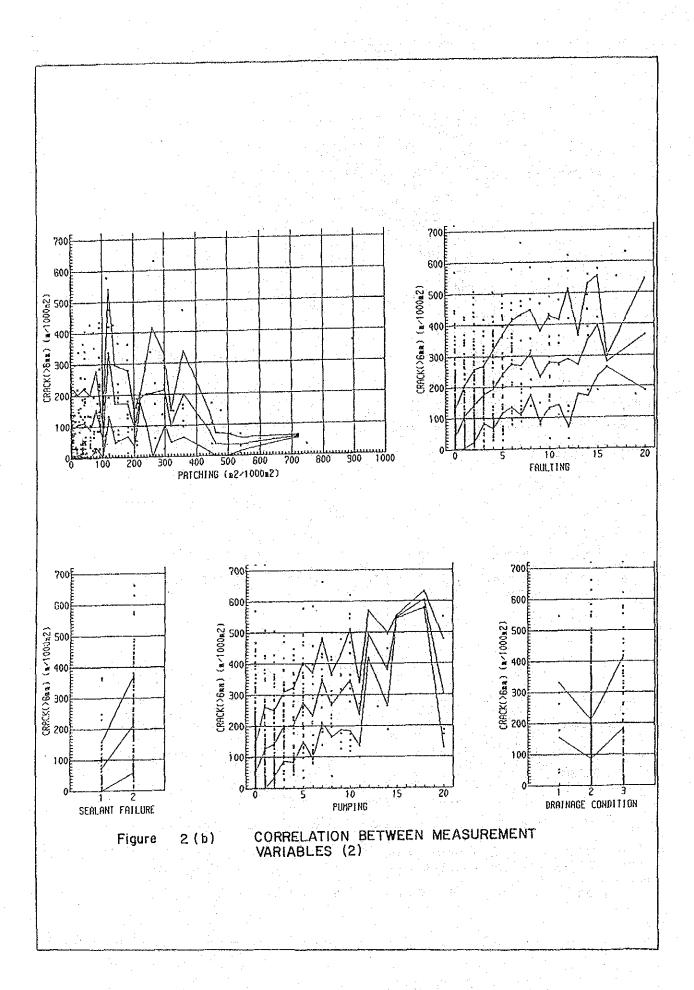












# APPENDIX 13-3 COMPARISON BETWEEN RRI IN THE STUDY AND PSI IN AASHO

#### 1. Conversion of AASHTO'S PSI Formula

1) Symbols

R' = roughness in the AASHTO's formula (in/mile)

C' = cracking in the AASHTO's formula (ft/1,000 sq. ft.)

P' = patching in the AASHTO's formula (sq. ft/1,000 sq.ft.)

R = roughness measured in this Study (cm/km)

 $C = \text{cracking measured in this Study (m/1,1000 m}^2)$ 

P = patching measured in this Study  $(m^2/1,000 m^2)$ 

R1 = roughness measured with the British standard bump integrator (in/mile)

2) AASHTO's PSI Formula for Rigid Pavement

PSI = 5.41 - 1.80 log (0.40 R<sup>+</sup> - 33) - 0.09 
$$\sqrt{C^{T}+P^{T}}$$

3) Relationships between R1 and R2 and between R2 and R

$$R1 = \frac{0.394}{0.621} \quad R2 = 0.634 \quad R2 \quad ---- \quad (1)$$

$$R2 = 100 + 0.75 R$$
 ---- (2)

Source: Philippine Island Road Feasibility Study Final Report, 1980

4) Relationship between R1 and R'

Source: Fig. 22.3 of "The Design and Performance of Road Pavements". TRRL, 1977 (See Figure 1)

By the least squares regression method, the relationship between R' and R2 is expressed as follows (see Figure 2)

$$R^{+} = 1.08 R1 - 61$$
 (3)

5) Relationship between R' and R

By substituting the equations (1) and (2) into (3),

$$R^{1} = 0.51 R + 7.5$$

6) Relationships between C' and C and between P' and P

$$C' = 0.30 C$$

$$P_1 = P$$

7) AASHTO's PSI Formula for Rigid Pavement Expressed by R, C and P

PSI = 5.41-1.80 log (0.40R' - 33) - 0.09 
$$\sqrt{C'+P'}$$
  
= 5.41-1.80 log (0.40 (0.51R + 7.5) - 33 $\frac{1}{2}$  - 0.09  $\sqrt{0.30 C+P}$   
= 5.41-1.80 log (0.20 R-30) - 0.05  $\sqrt{C+3.3 P}$ 

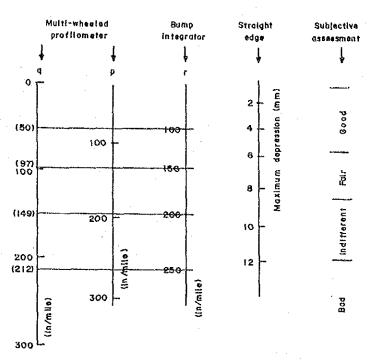


Fig. 22-3. Comparison between surface trregularity and riding quality.

Fig. I Relationship of roughness values

Source: The Design and Performance of Road Pavements, TRRL, 1977

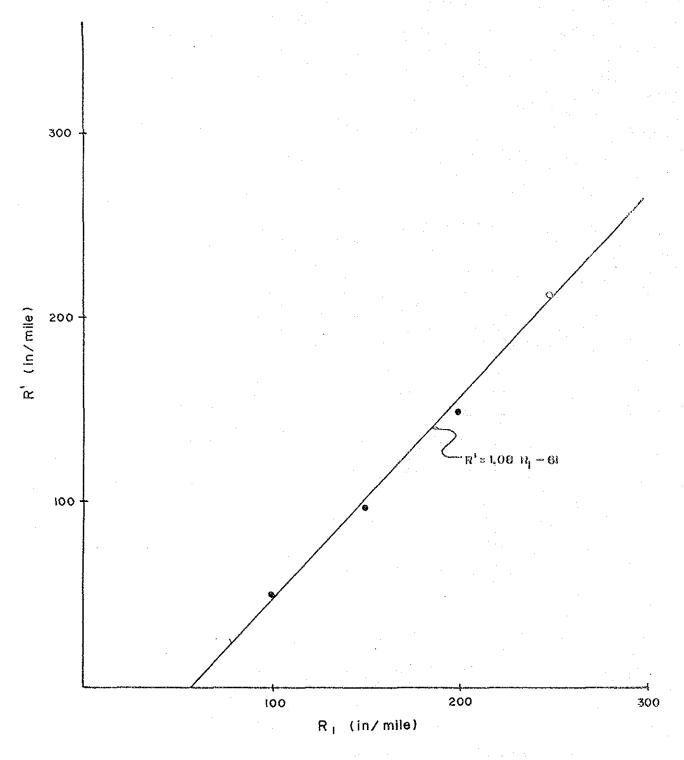


Figure 2 Relationship between R<sub>1</sub> and R'

#### Roughness and Cracking in AASHO's Road Test

Figure 3 based on AASHO Road Test shows the mean relationship between total length of cracking (projected in either the longitudinal or transverse directions) per 100 ft. of traffic lane and PSI derived from equation of AASHO's PSI formula.

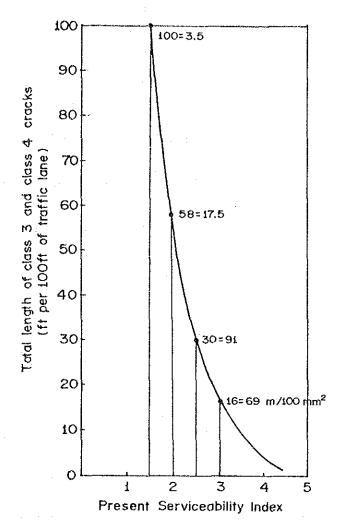


FIG. 3 RELATIONSHIP BETWEEN DEGREE OF CRACKING AND PRESENT SERVICEABILITY INDEX

Using Figure 3, cracking was estimated, at each level of PSI. And then, roughness was calculated using AASHO's PSI formula. The result is shown in Table 1.

TABLE 1 AVERAGE CONDITION IN AASHO ROAD TEST

AASHO¹s PSI	Cracking <sub>2</sub> (m/1000 m <sup>2</sup> )	Roughness (cm/km)
4.0	12	180
3.5	28	200
3.0	50	220
2.5	110	260
2.0	220	300
1.5	350	340

#### 3. Roughness and Cracking in the Study Section

Based on pavement surface condition survey and RRI and PSI analysis, the average roughness and cracking at each level of index is the Study Section were estimated as follows.

TABLE 2 AVERAGE CONDITION IN THE STUDY SECTION

RRI	Cracking	Roughness	PSI
4.0	5	155	3.2
3.5	12	270	2.7
3.0	58	289	2.4
2.5	136	315	2.1
2.0	248	340	1.7
1.5	393	368	1.4
1.0	. 000		

RRI	Cracking	Roughness PSI
4.0	0	75 4.7
3.5	0	133
3.0	4	207 3.8
2.5	34	282 3.2
2.0	153	319 2.4
1.5	356	362 1.6

#### 4. Comparison between AASHO's PSI and RRI in the Study

Table 3 shows average cracking and roughness under each serviceability index of AASHO Road Test and in the Study Section.

Table 4 shows the difference of AASHO's PSI and RRI and PSI in the Study.

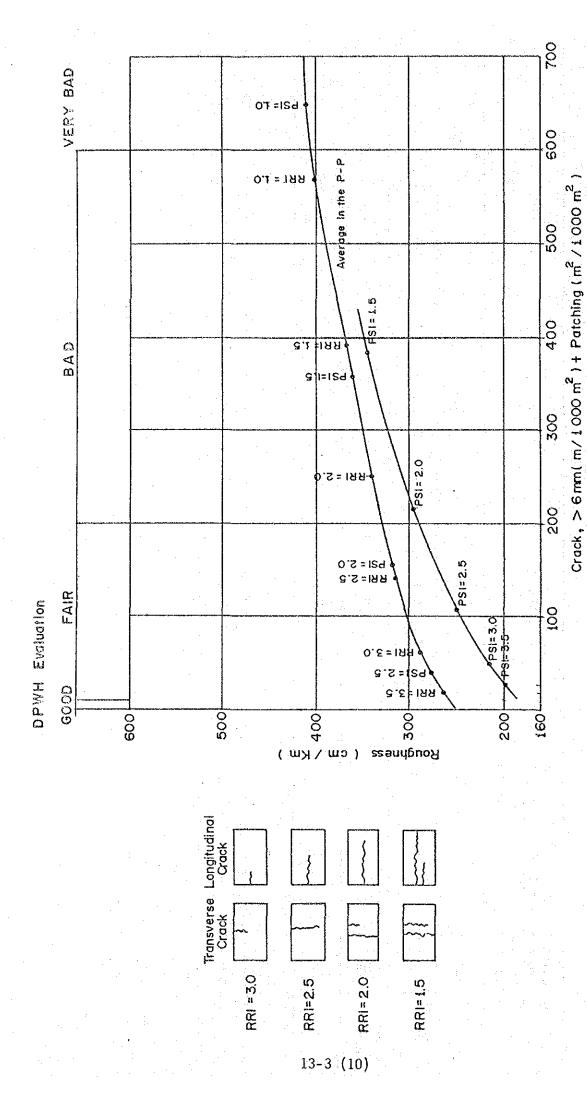
Figure 4 summarizes these comparisons.

TABLE 3 AVERAGE CRACKING AND ROUGHNESS CONDITION

Roughness (Cm/Km)         RRI         Cracking Roughness         The Study in the Philippines           175         4.0         5         160         4.0         0           190         3.5         12         270         3.5         0           220         3.0         60         290         3.0         4           260         2.0         140         320         2.5         35           360         2.0         250         340         2.0         150           360         1.5         400         370         1.5         360		AASHO Road Test				-			
12         4.0         5         160         4.0         0           28         190         3.5         12         270         3.5         0           50         220         3.0         60         290         3.0         4           110         260         2.0         140         320         2.5         35           220         300         2.0         250         340         2.0         150           390         360         1.5         400         370         1.5         360	PSI	Cracking <sub>2</sub> (m/1000 m <sup>2</sup> )		RRI	Cracking	The Study in the Roughness	he Philippi PSI	nes Cracking	Roughness
28         190         3.5         12         270         3.5         0           50         220         3.0         60         290         3.0         4           110         260         2.0         140         320         2.5         35           220         300         2.0         250         340         2.0         150           390         360         1.5         400         370         1.5         360	4.0	12	175	4.0	5	160	4.0	0	80
50         220         3.0         60         290         3.0         4           110         260         2.0         140         320         2.5         35           220         300         2.0         250         340         2.0         150           390         360         1.5         400         370         1.5         360	3.5	28	190		12	270	3,55	0	130
110         260         2.0         140         320         2.5         35           220         300         2.0         250         340         2.0         150           390         360         1.5         400         370         1.5         360	3.0	50	220	3.0	09	290	3.0	4	210
220     300     2.0     250     340     2.0     150       390     360     1.5     400     370     1.5     360	2.5	110	260	2.0	140	320	.s	35	280
390 360 1.5 400 370 1.5 360	2.0	220	300	2.0	250	340	2.0	150	320
	1.5	390	360	5	400	370	ω.	360	360

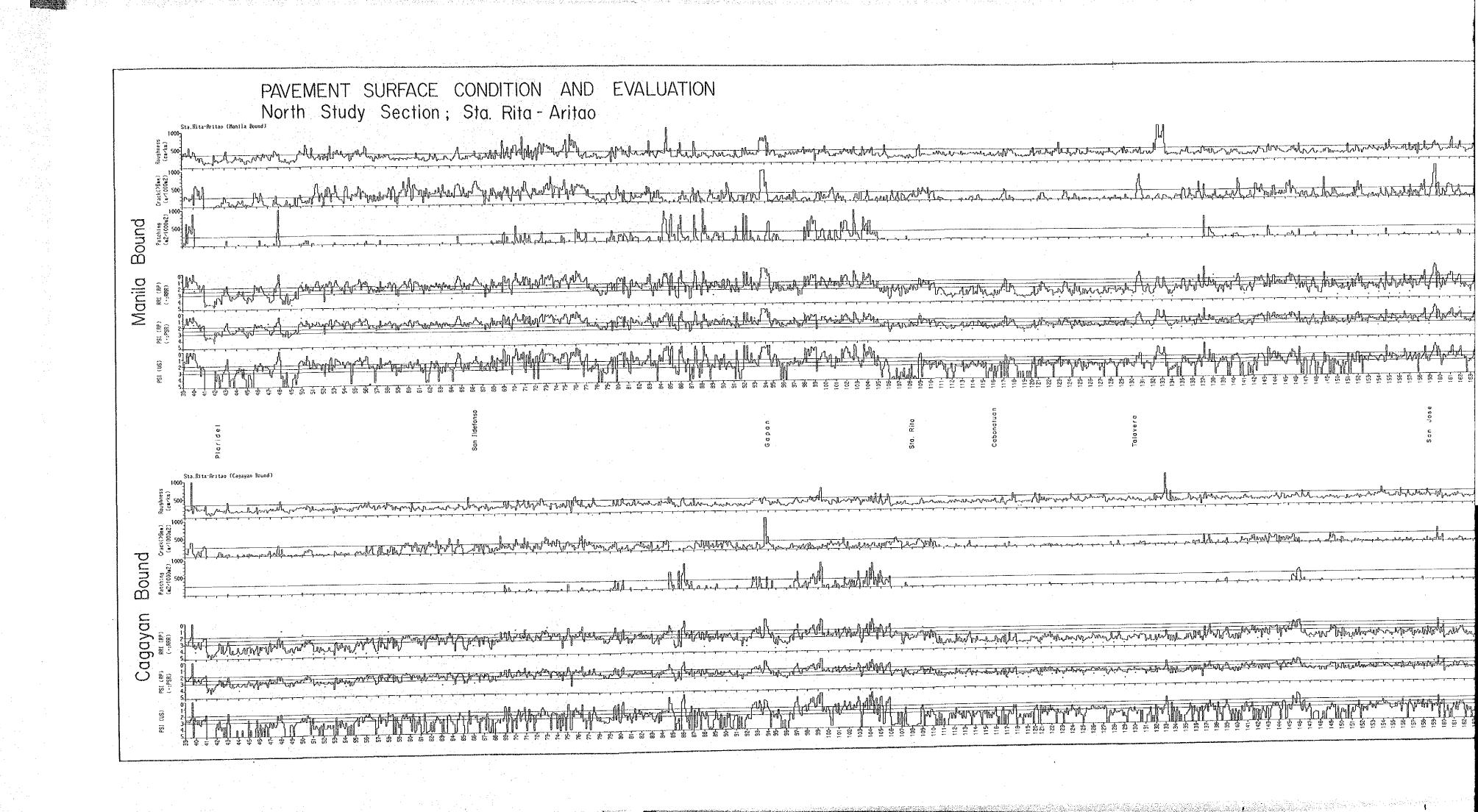
TABLE 4: COMPARISON OF SERVICEABILITY INDEX BETWEEN AASHO AND THE STUDY

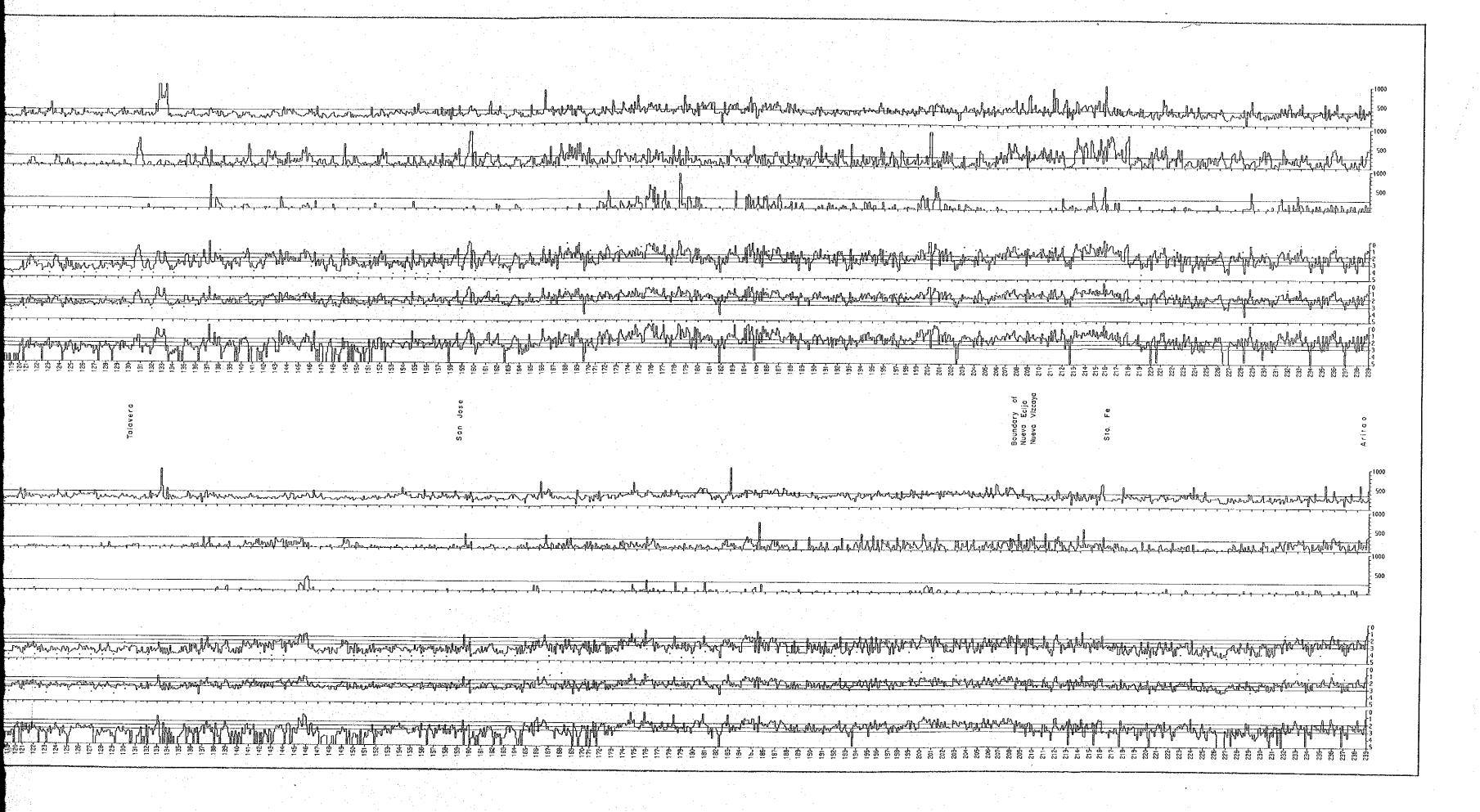
In the Study PSI	3.1	2.9	2.6	2.3	1.9	3.
In the Study RRI	3.8	3.5	3.2	2.8	2.2	1.5
AASHO's PSI	4.0	3.5	3.0	2.5	2.0	1.5
ss Condition s Road Test) Roughness (cm/km)	175	190	220	260	300	360
Cracking and Roughness Condition (Average in AASHO's Road Test) Cracking2 (m/1000 m²) (cm/km)	12	28	50	110	220	390

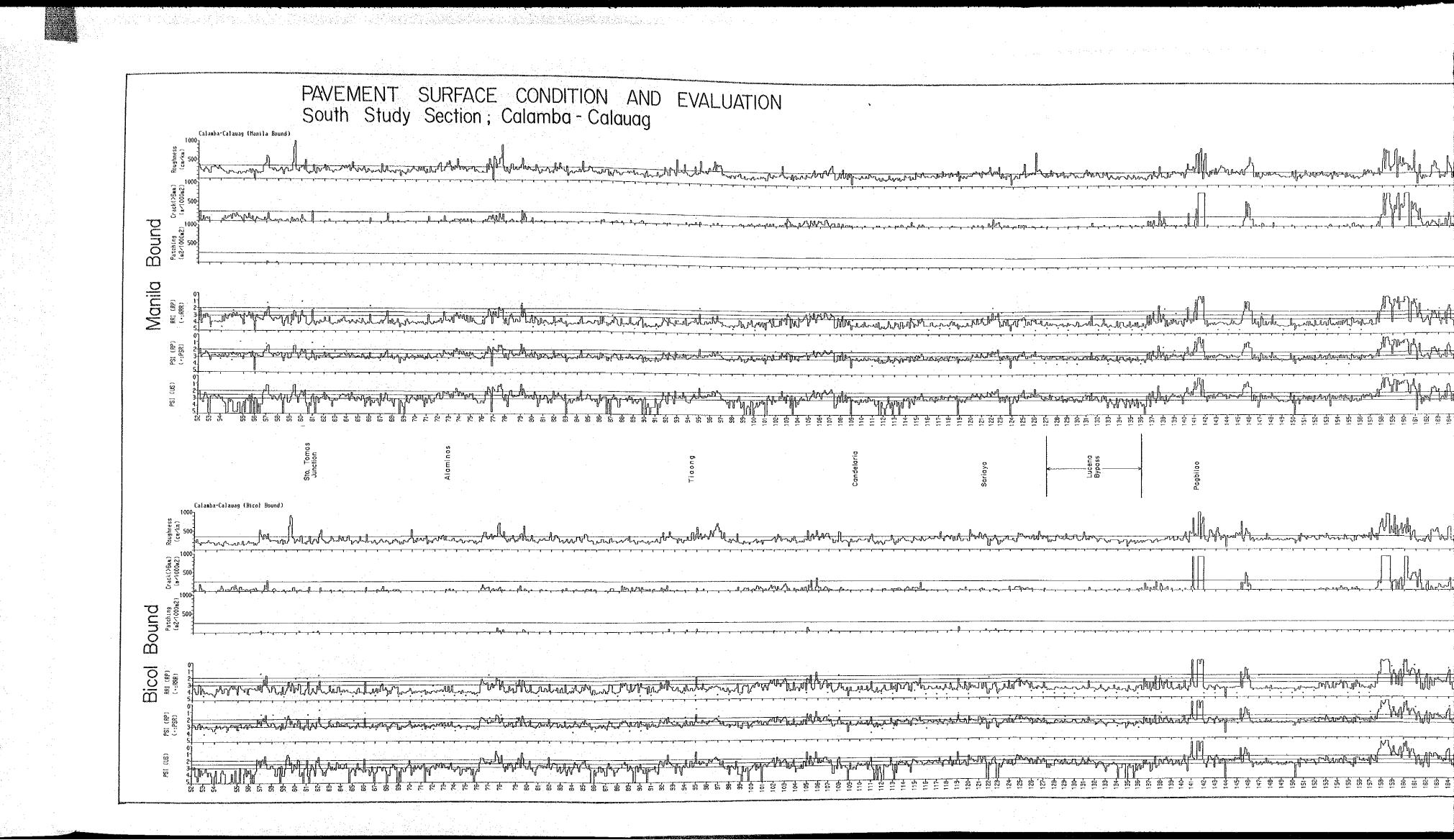


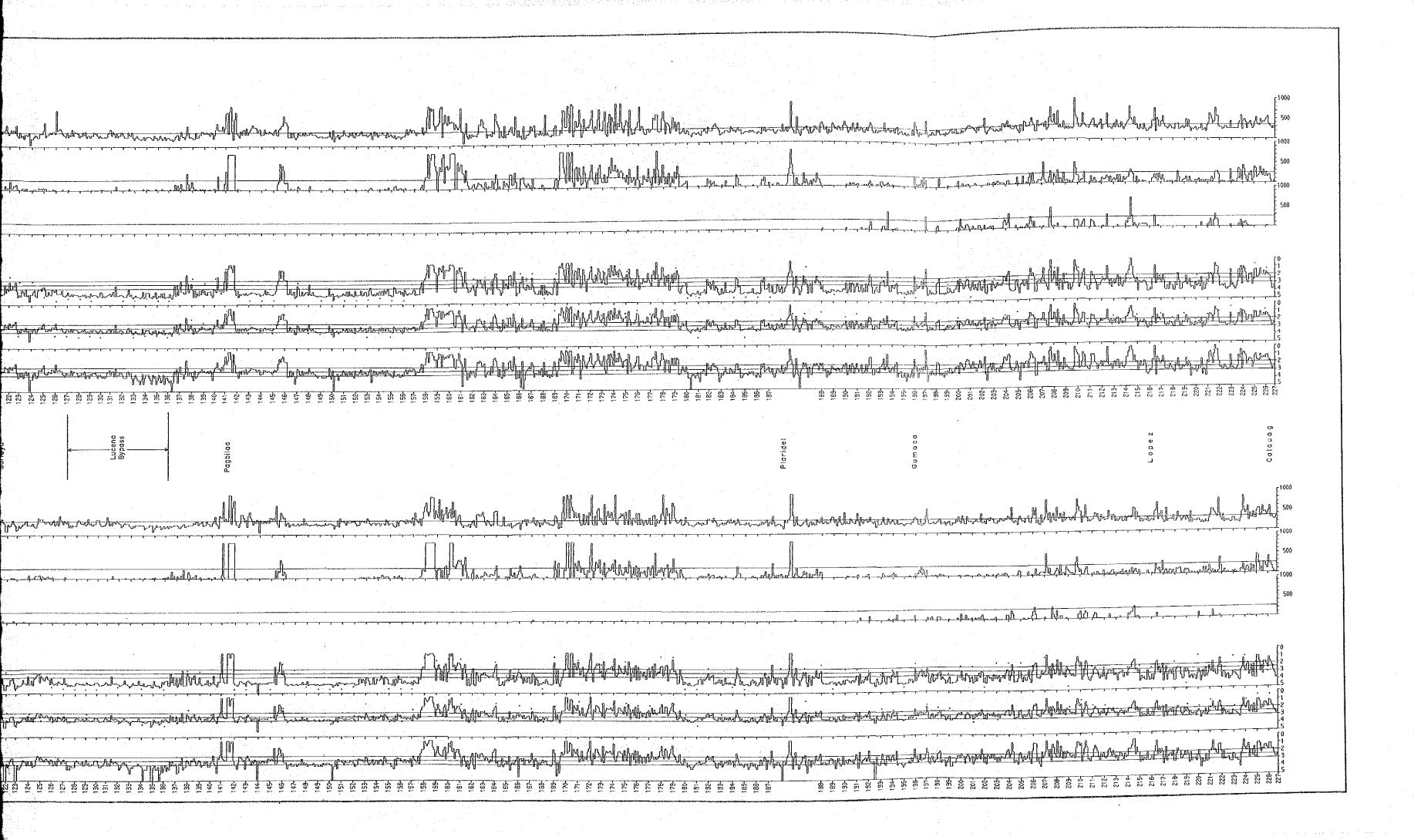
AVERAGE RELATIONSHIP BETWEEN RRI AND ROUGHNESS, CRACKING, PATCHING な <del>ار</del> 10

## APPENDIX 13-4 PAVEMENT SURFACE CONDITION AND EVALUATION



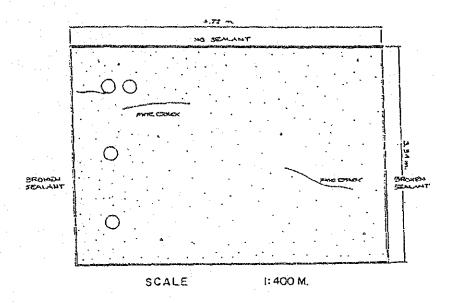






#### APPENDICES FOR CHAPTER 14

### APPENDIX 14-1 DETERIORATION CONDITION OF SURVEY SLABS



- 1. Cracking No wide crack. Few fine crack.
- Sealant Failure \* No sealant at longitudinal joint. Broken sealant at contract joints.

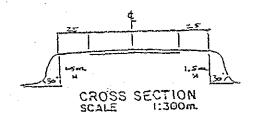
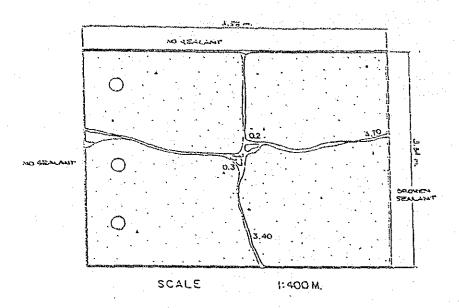
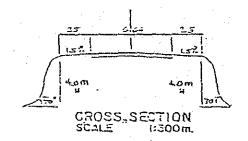




FIGURE 8.2-1 (1) DETERIORATION CONDITION OF  $N_1$ -G SLAB



- 1. Cracking = Wide crack total length = 8.bu m. Few fine crack.
- Sealant Failure \* No sealant in most part of joints.
   Broken sealant in some part.
- Spalling \* Observed at some part of cracks.



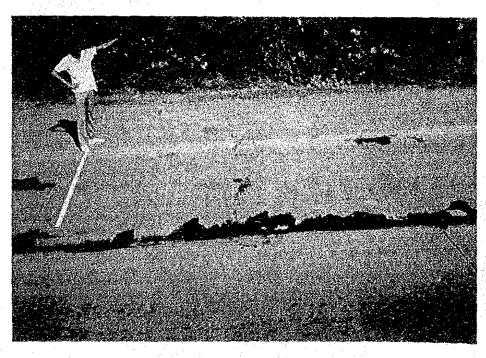
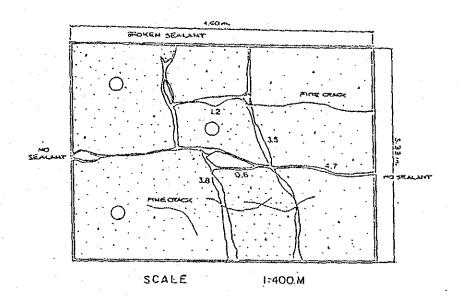
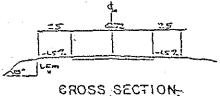


FIGURE 8.2-1 (2) DETERIORATION CONDITION OF  $N_1$ -F SLAB



- Wide crack (total length) = 13.801m Fine crack (total length) = 1.90 m
- Settlement = Observed at (1) and (2)
- Sealant Failure = No sealant at contract joints. Broken sealant at longitudinal joint.
- 4. Spalling = Observed in almost part of cracks.



GROSS SECTION-SCALE -= 1:300m

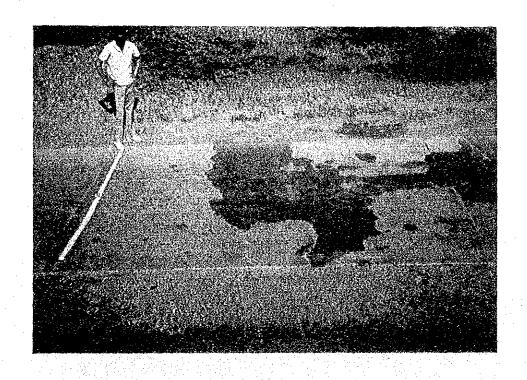
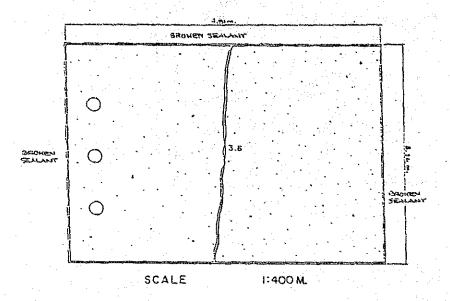
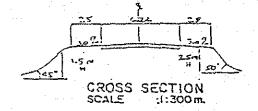


FIGURE 8.2-1 (3) DETERIORATION CONDITION OF  $\mathrm{N}_1\mathrm{-B}$  SLAB



- Cracking = Wide crack total length = 3.60 m
   No fine crack.
- Sealant Failure = Broken sealant at all joints.



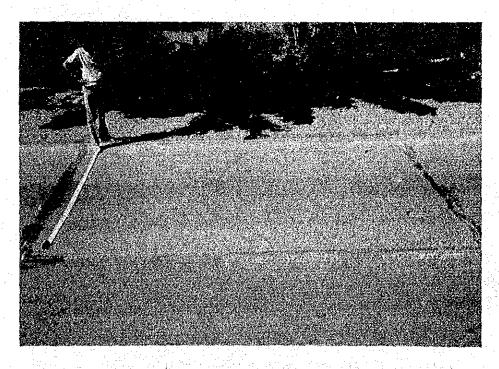
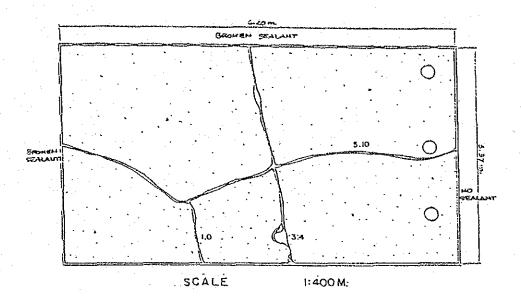
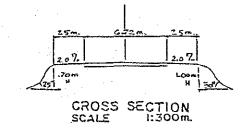


FIGURE 8.2-2 (1) DETERIORATION CONDITION OF N<sub>2</sub>-G SLAB



- Cracking \* Wide crack (total length) \* 10.90 m
   No fine crack.
- Sealant Failure \* Broken sealant at all joints.
- Spalling = Observed at (1).



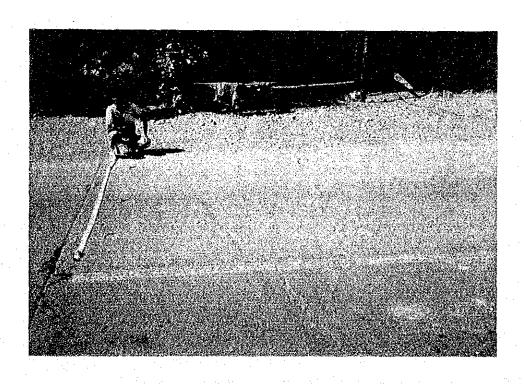
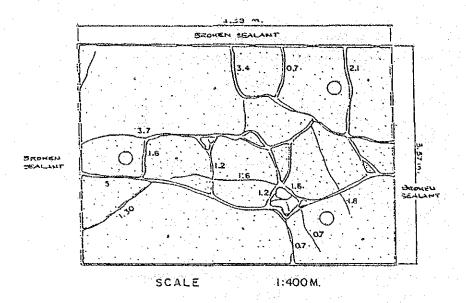
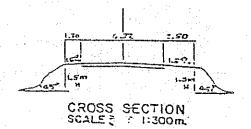


FIGURE 8.2-2 (2) DETERIORATION CONDITION OF N<sub>2</sub>-F SLAB



- 2. Sealant Failure = Broken sealant at all joints.
- Spalling = Observed at some cracks.
- 4. Patching \* Observed in most part of cracks.



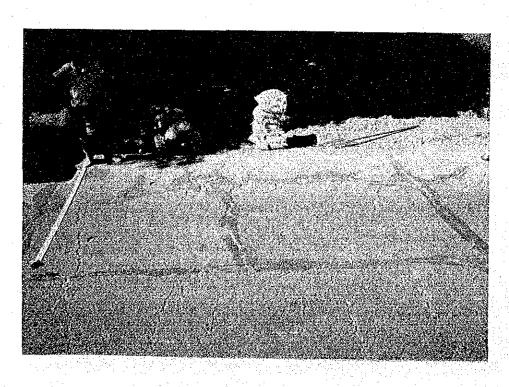
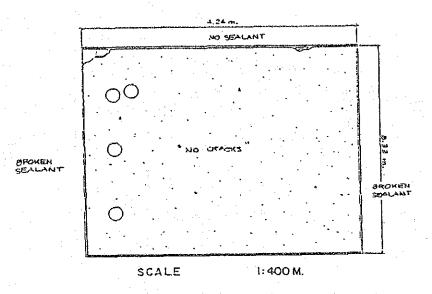


FIGURE 8.2-2 (3) DETERIORATION CONDITION OF  $N_2$ -B SLAB



- 1. Cracking \* Few fine crack.
- Sealant Failure \* Broken sealant in all joints. Lack of sealant at longitudinal joint.

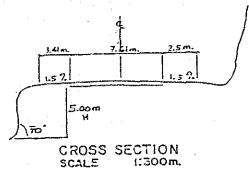
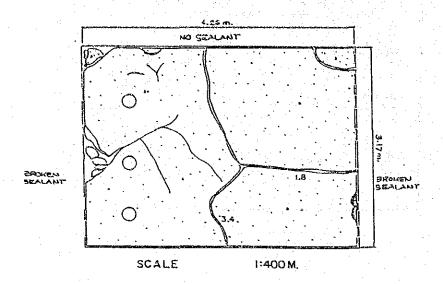
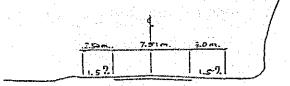




FIGURE 8.2-3 (1) DETERIORATION CONDITION OF  $\mathrm{N}_3\mathrm{-G}$  SLAB



- 1. Cracking = Wide crack (total length) = 8.10 m Fine crack (total length) = 3.40 m
- Sealant failure = 8roken sealant at contract joints.
   No sealant at longitudinal joint.
- Pumping \* Observed at (1) crack.
- 4. Spalling = Observed at (2) crack.



CROSS SECTION SCALE 1:300m.

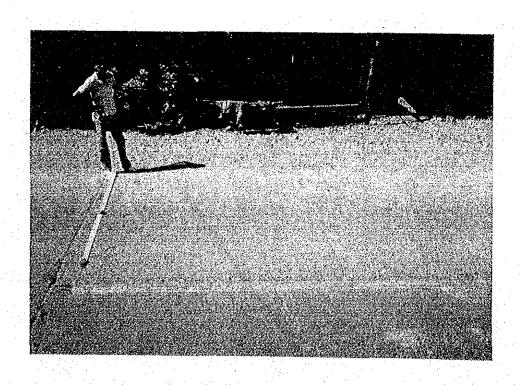
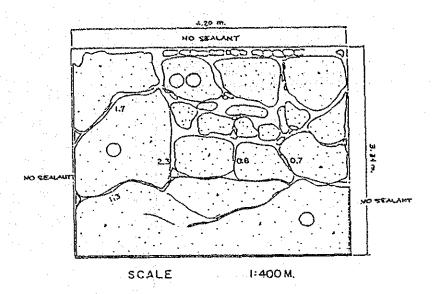
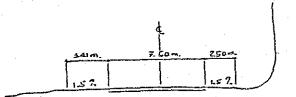


FIGURE 8.2-3 (2) DETERIORATION CONDITION OF  $N_3$ -F SLAB



- 1. Cracking \* Wide crack(total length) \* 22.10 m Fine crack(total length) \* 3.30 m
- 2. Settlement \* Observed at (1), (2) and (3) cracks.
- 3. Pumping = Observed between (2) and (3) cracks.
- 4. Sealant Failure \* No sealant in all joints.
- 5. Joint Shattering \* Observed at longitudinal joint.



CROSS SECTION SCALE 1:300m.

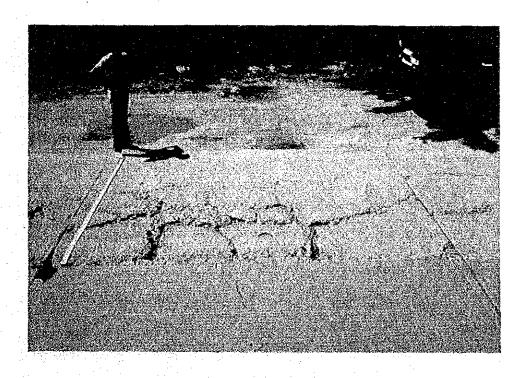
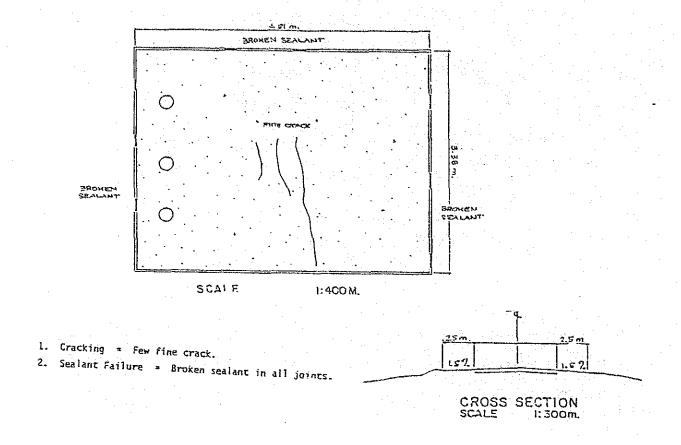


FIGURE 8.2-3 (3) DETERIORATION CONDITION OF N<sub>3</sub>-B SLAB



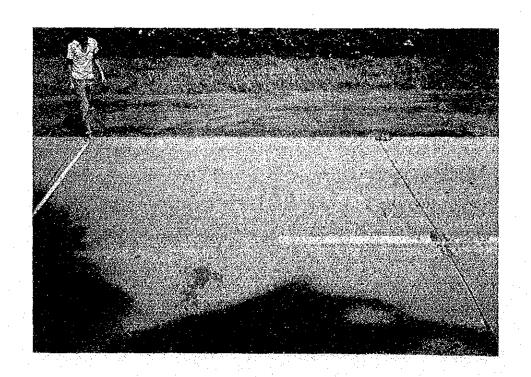
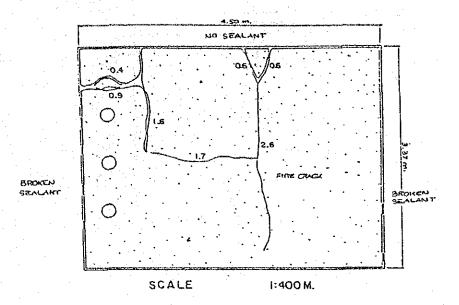


FIGURE 8.2-4 (1) DETERIORATION CONDITION OF  $s_1$ -G SLAB

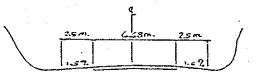


CORNER CRACK

 Cracking = Wide crack (total length) = 4.10 m Fine crack (total length) = 4.30 m

Sealant Failure \* Broken sealant in both contract joints.
 No sealant at longiducinal joint.

3. Pop-outs - Minor pop-outs was observed.



CROSS SECTION SCALE 1:300m.

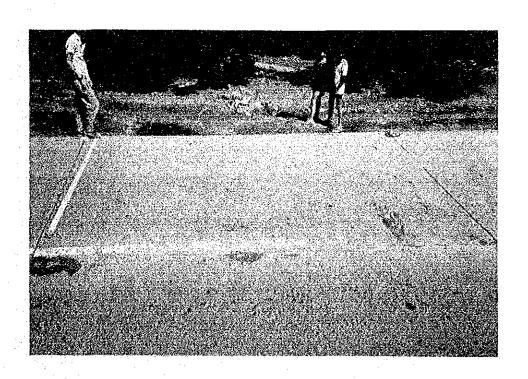
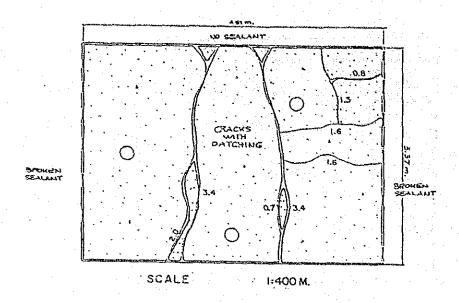


FIGURE 8.2-4 (2) DETERIORATION CONDITION OF  $\mathbf{S}_1$ -F SLAB



TRANSVERSE CRACK

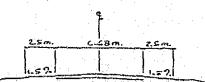
1. Cracking = Wide crack (total length) \* 9.50 m Fine crack (total length) \* 5.30 m

2. Sectlement = Observed at (1)

Sealant Failure \* Broken sealant in both expansion joints.
 No sealant at longitudinal joint.

4. Pop-outs \* Minor pop-outs was observed.

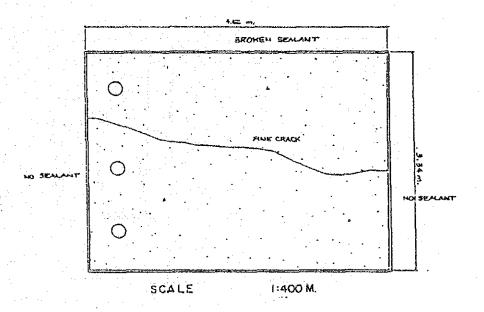
5. Patching \* Most cracks were patched.



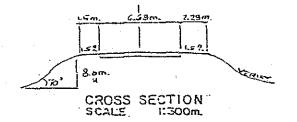
CROSS SECTION SCALE 1:300m.



FIGURE 8.2-4 (3) DETERIORATION CONDITION OF  $\mathbf{S}_1\mathbf{-B}$  SLAB



- 1. Cracking = No wide crack.
  Fine crack (total length) = 4.50 m
- 2. Sealanc Failure = No sealant on both contract joints\_ Broken sealant on longitudinal joint...



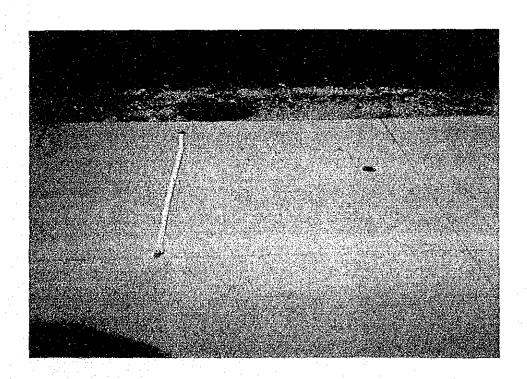
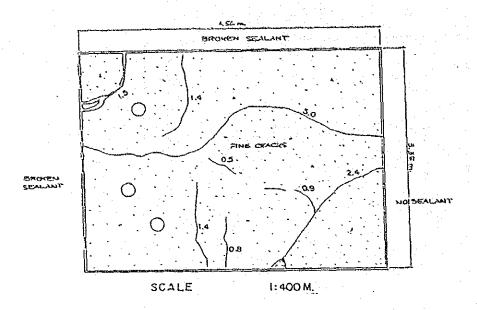
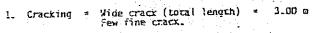
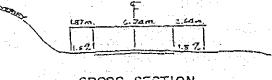


FIGURE 8.2-5 (1) DETERIORATION CONDITION OF  $\mathrm{S}_2\mathrm{-G}$  SLAB





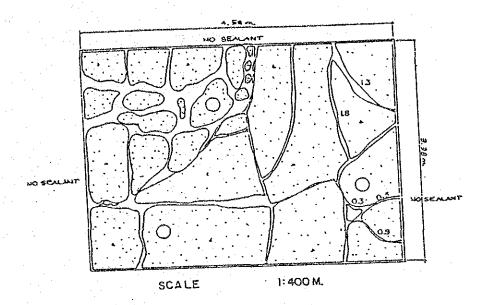
- 2. Sertlement = Observed in most of the cracks.
- 3. Pumping = Observed at cracks (5)-(6)
- Slab Rocking = Observed at cracks (5)-(δ)
- S. Spalling = Observed in some cracks.
- 5. Sealant Failure = No sealant in all joints.



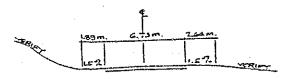
CROSS SECTION SCALE 1:300m.



FIGURE 8.2-5 (2) DETERIORATION CONDITION OF  $S_2$ -F SLAB



- 1. Cracking \* Wide crack (total length) = 6.70 mFine crack (total length) = 7.20 m
- 2. Settlement = Observed at (1)
- Sealant Failure \* Broken sealant most part of joints.
   No sealant in some part.



CROSS SECTION SCALE 1:300 m.



FIGURE 8.2-5 (3) DETERIORATION CONDITION OF  $\mathrm{S}_2\mathrm{-B}$  SLAB