## BOUND OF THE CHAPTER 6 CONCLUSIONS

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As a result of the geological survey and the geochemical survey of the soil in the 30 km<sup>2</sup> area of 8 km long in the east-west direction and 4 km long in the south-north direction from the Pagar Gunung deposit to the Patahajang (Baruté) mineralization zone, the relationship between the deposit and geology, geological structure and igneous activities has been clarified. The survey results of this area are summarized in the following.

- (1) Geologically, this area consists of the Huara Botung Formation and Patahajang Formation formed of andesite, dacite, sandstone, mudstone and limestone, and these Formation are correlative with Silungkang Formation of Peusangan Group, Permian-Carboniferous System in Sumatra Island.

  These Formations are further divided into 7 Members.
- (2) The muscovite granodiorite that is widely distributed in the northern part of the survey area has undergone mylonitization, and shows banded texture and has become mylonite. Also, it has been intrued by Juraic tonalitic porphyry and quartz diorite porphyry.
- (3) There is a synclinal structure, having an synclinal axis of N 60° W in the central part of survey area, that is, from the Summit of T. Pagar Gunung to the ridge of T. Mandagang, and the arrangement of tonalite and quartz diorite stocks are also regulated to this direction.
- (4) There are the following ore deposits or mineralized zones in the survey area.
  - (a) Silver-bearing lead-zinc deposit (Skarn deposit)

    Pagar Gunung West deposit

    Pagar Gunung East deposit (Outcrop B)
  - (b) Disseminated sphalerite mineralized zone

    Barute mineralized zone
  - (c) Pyrite mineralized zone

    Pagar Gunung East deposit (Outcrop A)

    A. Sambak pyrite disseminated zone
  - (d) Others

    Quartz vein containing molybdenite

- (5) The Pagar Gunung West deposit is embedded in the alternated Member of Clastic rock and volcanic rock of the Patahajang Formation. It's strike and dip are about N 90° B and 30° S and has a maximum vein width of 2.50 m, and it's strike length is about 200 m while it's width changes from thick to thin along the extension. Purthermore, together with Pagar Gunung West deposit (Outcrop A) situating 650 m east of it, it is classified into silver-bearing lead-zinc skarn deposit, replacing muddy limes stone and accompanied by calcic skarn minerals like clinopyroxene, epidote and calcite. Further in the east by 6 km, there is the Barute mineralized area accompanied by sphalerite emplaced in the same stratigraphical horizon of Pagar Gunung ore deposit.
- (6) In the muscovite granodiorite and dacitic tuffaceous rock that are distributed in the northern marginal part of the survey area, there is a silicification zone accompanied by pyrite dissemination. Especially on Outcrop A of the Pagar Gunung East deposit there is a pyrite dissemination zone of about 20 m width in the dacitic tuffaceous sandstone, and bedded or banded pyrite deposit is distributed.
- (7) Through the geochemical survey of the soil, it is found that anomalous areas overlapping with path-finder elements of Au, Ag, Cu, Pb, Zn co-incides with outcrop lines of Pagar Gunung ore deposits and the Barute-Patahajang mineralized area. Also, an anomalous area of gold, silver, copper, lead and zinc overlapping each other was discovered 3 km long and 1 km wide from the A. Mandagan upstream to the Barute mineralized area. This anomalous area is situated in the same horizon and Alternated Member of Clastic rock and Volcanic rock of Patahajang Formation as the Pagar Gunung ore deposit and Barute mineralized zone.

In addition, an anomalous area of silver (and gold) is recognized in the neighborhood of stecks of tonalite and quartz diorite, which have intruded into limestone, in the A. Sabul upstream in the west of Simpang Pining. While there are other anomalous areas of silver (and gold) in places such as the north ridge of the A. Salidi in the limestone area and the ridge of T. Pagar Gunung in the south of Pagar Gunung mineralized area, but in these places no quartz diorite or tonalite are exposed. When it is considered that silver (gold) shows the aureale margin of quartz diorite and the like, there is a possibility of quartz diorite latently existing in these areas. Also, distribution of skarn deposits could be conceivable.

# Fig. 11-3-33 Microscopic Photograph of Thin Section and Ore Sample, Muara Sipongi Area B

### Abbreviation

q : Quartz

pl : Plagioclase

bí : Biotite

nu : Miścovite

hy : Hypersthene

au : Augite

fe : Ferric mineral

ca : Calcite

chl : Chlorite

se : Sericite

ep : Epidote

cp : Chalcopyrite

sp : Sphalerite

ga : Galena

po : Pyrrhotite

py : Pyrite

c.f.and: Rock fragment (andesite)



Sample No.: L-29

Location : T. Pagar

Gunung

Pyroxène Rock name :

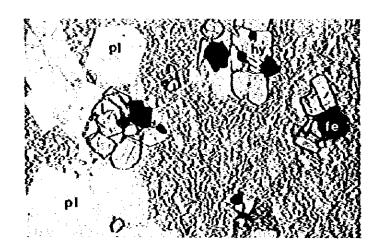
andesite

Tertiary Pormation:

volcanic

rock

only lower polar 0.5 as



Sample No.: Location : L-100

T. Simpang

Opat

Pyroxene Rock name :

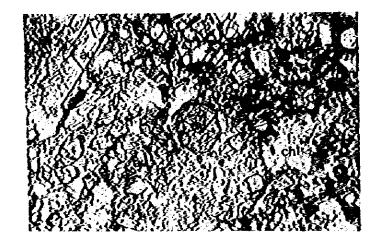
andesite

Formation: Tertiary

volcanic

rock

only lower polar 0.5 \*\*



Sample No.: L-2

West of Location :

T. Handagang

Pyroxenite Rock name : Basic Formation:

volcanic rock Hember Patahajang Pormation .

only lower polar 05 aa

Sample No : L-3 Location : West of

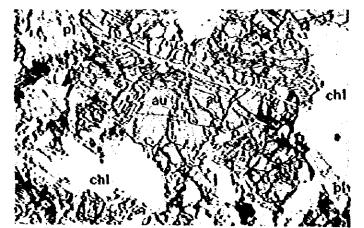
T. Mandagang

Rock name: Pyroxenite Basic

Pormation:

volcánic rock Hember Patahajang **Formation** 

only lower polar Q5 az



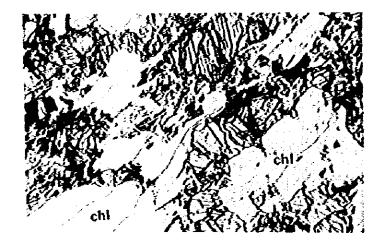
Sample No.: L-113 T. Pagar Location : Gunung

Rock name: Basaltic tuff

Formation: Basic

volcanic rock Member Patahajang Formation

only lower polar 0,5 AR



Sample No.: L-125 Location : T. Pagar

Gunung

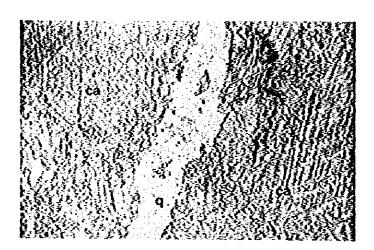
Rock name : Basaltic

tuff

Formation: Basic

volcanic rock Member Patahajang **Formation** 

only lower polar 0.5 ar



Sample No.: L-1 Location :

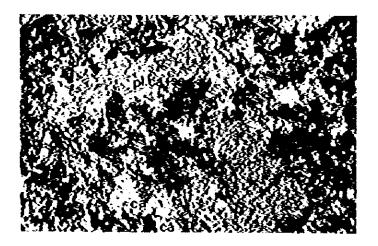
West of T. Mandagang

Forwation:

Rock name : Limestone Lover

> limestone Kember Patahajang **Formation**

only lower polar 0,5 ≈≈



Sample No.: L-19

Location : Tributary of

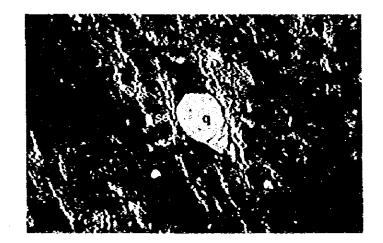
A. Sabul

Rock name: Meta andesite

Formation: Andesite

Hember Patahajang **Formation** 

cross polars О\_\_\_\_\_ О.5 лл



Sample No.: M-2

Location : A. Mandagang

Rock name : Phyllitic

mudstone

Formation: Alternated

Hember of clastic rock and volcanic

rock

Pátahájáng Formátión

cross polars

) 0,5 a n



Sample No.: KR-21

Location: A. Sambak Rock name: Sandstone

Pormation: Alternated Member of

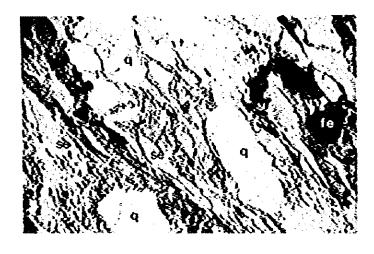
clastic rock and volcanic

rock

Patahajang Portation

cross polars

0.5 a



Sample No.: L-138

Location : A. Palelo Rock name : Dasitic

Rock name: Dasitic sandy tuff

Formation: Alternated

Hember of

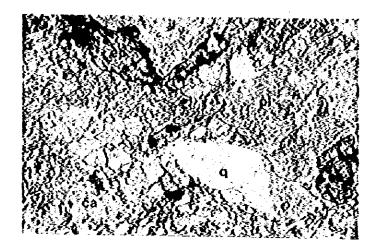
clastic rock and volcanic

rock

Patahajang Formation

only lower polar

0,5 \*\*



Sample No.: L-147

Location: Tributary of

A. Sambak

Rock name: Andesitic

tuḟf

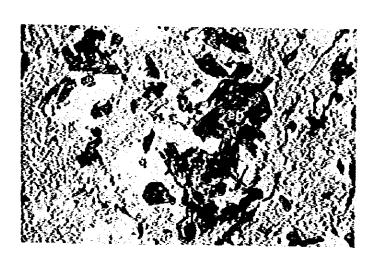
Formation: Alternated

Hember of clastic rock and volcanic

róck

Patahajang Pomation

only lower polar O O,5 mm



Sample No.: L-156

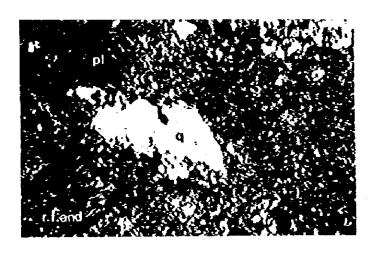
Location : A. Palelo Rock name : Dacitic to

Rock name: Dacitic tuff Formation: Alternated

Member of clastic rock and volcanic

rock Patahajang Formation

only lower polar
0 05 nm



Sample No.: K-10

Location : B. Pungkut Rock name : Dacitic tuff

Formation: Alternated

Member of clastic rock and volcanic

rock

Patahajang Formation

cross polars O O5An



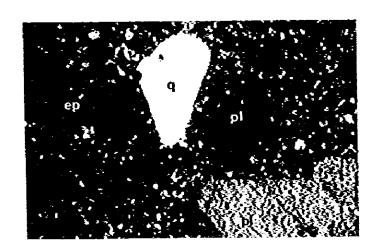
Sample No.: L-132 Location: A. Palelo Rock name: Andesite Formation: Alternated

Member of clastic rock and volcanic

rock

Patahajang **Formation** 

cross polars 0.5 aa



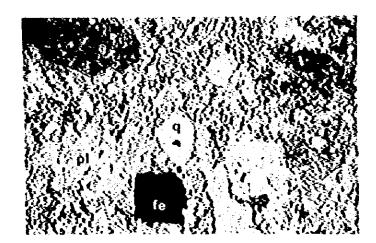
Sample No.: K-18
Location : A. Mabobar
Rock name : Dacite
Formation : Dacite

Hember

Patahajang **Formation** 

cross polars

O.5 a 4



Sample No.: M-21

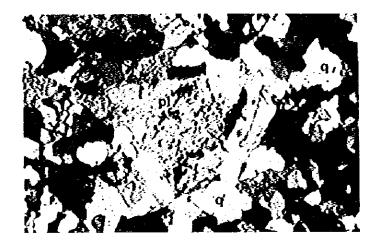
Location : A. Habobar Rock name : Dacitic tuff

Formation: Dacite

Hember Patahajang Formation

only lower polar

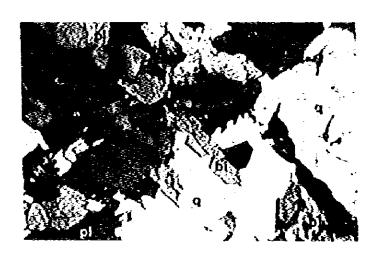
G.5 a =



Sample No.: K-15
Location : A. Matimba
Rock name : Tonalite
Dorphyry

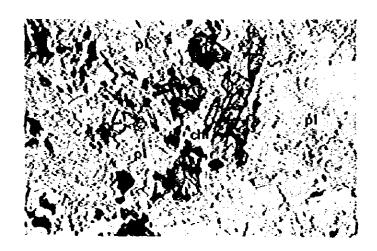
porphyry

cross polar



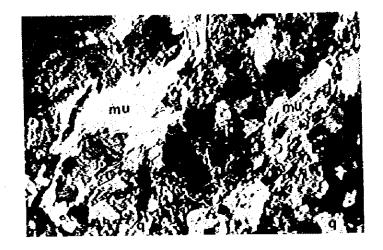
Sample No.: K-28
Location : B. Pungkut
Rock name : Tonalite

cross polar



Sample No.: L-41 Location : A. Sabul Rock name : Diorite porphyry

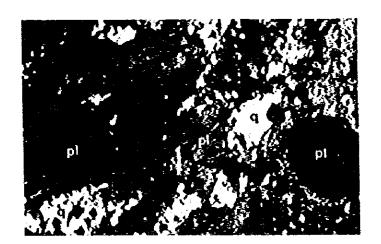
> only lower polar 0 05 ил



Sample No.: L-131 Location : A. Palelo Rock name : Muscovite

granodiorite (mylonite)

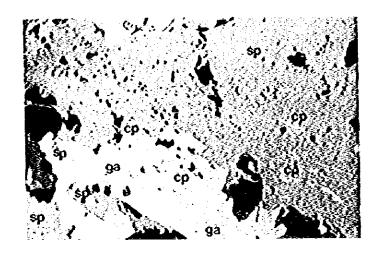
cross polars O 0.5 mm



Sample No.: X-40 Location : A. Karlan Rock name : Muscovite

granodiorite (mylonite)

cross polars 0,5 au



Sample No.: KR-37

Location : Pagar Gunung

West ore deposit Adit No. 2

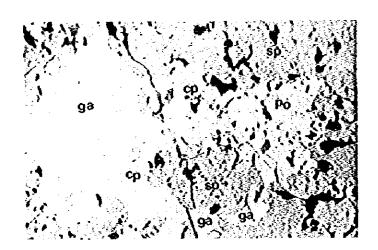
Adit No. 2 Ore name : Kassivė

chalcopyrite-

gålenasphålerite

ore

пя \$.0



Sample No.: KR-52

Location : Pagar Gunung

West ore deposit Adit No. 6

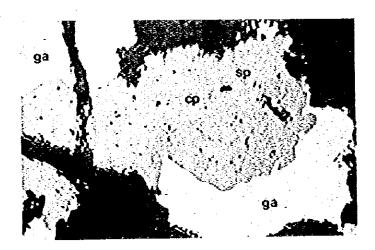
Ore name : Massive

pyrrhotitechalcopyrite-

galenasphalerite

ore

2 S S O



Sample No.: ZH-3.5

Location : A. Palelo

Pagar Gunung East ore deposit

Outcrop B

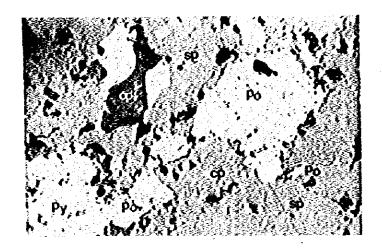
Ore name : Massive

chalcopyrite-

galenasphalerite

ore

0.2ma



Sample No.: 28-3.5

Location : A. Palelo

Pagar Gunung
East ore
deposit
Outcrop B
Massive

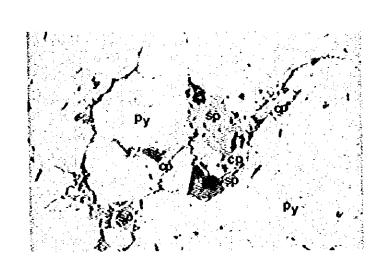
Ore name : Massive

pyrrhôtité chalcopyrite-

galenasphalerite-

ore

0.2 mm



Sample No.: L-139

Location : A. Palelo

Pagar Gunung

East ore deposit Outcrop A

Ore name : Massive

pyritė orė

0 02 ==

Table II-3-9 Assay Result of Geochemical Survey, Kuara Sipongi Area B

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	Sample Ho.	Coord	inàtes	ត់ប	Áα	Ċu	ያ b	75
		X,	Y	ppb	ppn	\$ p m	ត្តព	P 1: 13
	K\$1	0505	-1010	4	0.4	70	240	5.45
4 4	1.52	6530	-1365	i	0.4	59	39	130
	KS3	6880	-1590	4	0.1	38	14	4.6
	ľ,Š i	7020	- 1910	20	Ó. L	4.8	17	68.
	K\$5	7585	-2050	75	0.1	62	1 4	112
	K\$6	6150	-535	1.1	0.4	108	280	309
	K\$7	6369	-1275	4	0.2	5 1	46	131
	KSS	1335	-1770	2	4.1	45	17	95
	<b>1.53</b>	7620	-1760	5	0.1	3.7	24	31
	KS10	6190	-1175	4	0.1	5.5	25	535
	KSII	5030	-210	άO	0.6	134	51	350
	8812	4120	5/0	24	0.9	7.4	25	33
	KS13	4435	-815	85	1.0	9.4	22	145
	KS 14	5165	-770	21	0.5	71	23	36
	Ř\$15	5340	-540	21	0.6	112	33	440
	E\$16	5710	-280	24	1.1	72	550	1000
	K\$17	4775	-2010	2	6.1	¥3	16	124
	F\$18	4820	-1410	5	0.1	35	12	82
	K\$ 19	5150	-1520	45	0.4	65	42 -	148
	K\$20	5035	-1140	65	0.4	35	33	151
	K\$21	4260	-1815	E	0.1	70	11	73
_	K\$22	3900	-1800	12	0.1	75	8	102
	K\$23	4140	-1310	30	0.3	128	21	139
	K\$24	4120	-1090	12	1.5	130	3 9	265
	<b>FS25</b>	4475	1235	52	0.6	75	-13	105
	K\$26	6375	-1740	3	0.3	48	35	171
	K\$27	6675	-1970	16	0.2	5.4	22	103
	K\$23	5275	-2020	4	0.1	58	9	88
	1.529	5120	210	21	0.9	660	70	270
	1:530	310	1135	12	1.7	3.8	93	2500
	K\$31	340	1705	33	1.1	83	33	220
	K\$32	^ <b>&gt; 5</b>	2130	19	0 I	15	4.4	171
	K\$33	-50	1865	95	2.0	3.4	4.4	250
	1.534	490	1930	3	0.7	4.1	3 (	199
	1:535	745	1800	11	0.4	124	3.1	139
	KS36	640	1390	3	0.1	35	47	210
	KS37	615	830	3	0.1	19	3	130
	U\$1	560	35	3.9	0.1	123	1	93
	182	770	- 80	4.6	0.1	125	A	105
	LS3	1220	210	4	0.1	£ 1	1	56
	L\$4	1260	-115	4	0.1	54	3	53
	F.2.2	1535	- 739	51	9.9	104	ŀŷ	\$4
	1.56	1270	-975	43	0.1	74	22	94
•	£51	345	-235	37	0.2	€8	19	100
	188	790	2,50	4	0.1	155	4	113
	133	1015	4.40	4	0.1	25	1	40
	1.510	\$ 6 6	650	5	0.1	23	7	58
	1.511	385	330	29	0.1	78	16	131
	1.512	580	790	11	0.1	21	10	2.8
	1.813	95	740	7	0.1	14	13	40

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8 6.		u s ko		منفعاله عادا	er <b>a</b> Albasia.		. <b></b>	he (276 of	. 5:
* & A	nplet	ROT	SeCoordi X	nates,∴ Y	չասը - բթե	रें रहेंगि≑े स्वेवे	rCu: (t≥	ppm ppm	1, -
	1514		700	-655	15	1.3	8.5	26 137	
	1.5.15		380	- 320	105	0.1	12	21 66	
	LS16		- 1380	-, 4 4 0	5	0.1	21	6 51	
	1517	÷	1030	-640	.24	0.1	89	16 95	
	1,513 1,519		970 100	-945 -170	230	0.6 3.9	67 115	30 112 14 102	•
	1520	. 1	110	60	1	0.1	93	2 83	
	1.521		- 80	125	5	0.1	23	8 40	•
	1 \$22	1	165	110	, 15	0.1	3.8	5 93	
	LS23		155	- 1 £ 0	4 &	2.4	73	19 142	
÷	LSŽ4.		- 6 2 5	20	8.2	1.3	53	11 99	
	US 25	7	+35 550	- 390	53	0 . 1	58	35 109	
	1826	1.5	550 390	-400 -755	38 3	0.2	72	15 110 13 54	
	125	- 1	2460	-2070	2	0.1	22	14 61	
	1,\$29	3 ·	2710	-1780	14	0.1	43	6 80	
	1830	Ç +	2540	-1380	- , <b>21</b>	0 - 1	88	21 136	
	1,831	1.1	2850	-1285	7	0.1	6.4	25 105	
	1.532	; .	2300	-895	35	0.1	3.3	8 39	
	F833	-	2320 2200	-1640 -1910	100	0.4	120 62	26 113 10 36	
	1335	7 € 1 ⊑	1340	-1290	8	0.1	32	9 56	
	1836	1 1	1840	-1740	3	0.1	20	8 41	
	1.537		2060	-1500	. j. j.	0.1	3.6	3 11	
	F238		2230	-1250	21	0.1	64	37 176	
	1 \$39 LS40	t	2145 1340	-920 -620	43 43	0.4	110	22 125 31 109	
	1.541	1.1	2450	-855	61	0.1	84	21 116	
	1842		1680	-1330	7	0.1	4.8	13 78	
	1.543		1654	-1040	3 /	0.1	70	14 123	
	1544		3465	-1880		0.3	6.3	10 .103	
	1845		3105	-1570		0.2	76	11	
	LS46 LS47		2830 -640	-2020 465		0.1 0.5	73 44	8 97 8 50	
	1548		- 1020	530		1.3	54	32 73	
	1.349		-2430	1645		0.1	64	3 192	
	1850		-2315	2080	· 1	0.1	22	20 94	•
	L\$51			2130		0.1	2.2	21 18	
	US52		-1850	1850	1	0.1	21	17 72	
	LS53		- 2020 - 2310	1580 1350		0.1 0.1	38 30	11 67 11 66	
	1.855		-1520		56	0.1	63	26 72	
	1.856		~1180			0.5	32	7 . 55	
	1,857	1	-1205	1945	1	0.1	19	15 35	
	1359			1205		0.1	80	5 86	
	1.559		-1630			0.1	3.6	9 74	
	1 860 1 861		~1155 ~1500			0.1	30 19		
	1.862		-1800				13	20 59 14 47	
	1863		- 1500		8		\$6	23 120	•
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	200	X	Y	pet	¢ p a	្រស់ ក្នុង	ទូសូម	p p in
1,564		1420	2440	3 3 1	,0.1	50	46	122
1,565	****	-1740	2445	/ / 2	0.1	15	16	43
1.868			2625	7 ( <b>2</b>	0.3	15	27	46
1,567	-1 -1	1150	2545 2305	: 1	0.1	13 29	15	:57
1 S 6 8 1 R S 1	2.5	-1110 5740	-520	: 6 :31	- 0 ; 1 2 ; 7	250	10 3000	111
KKS2		5686	-675	3	0.5	60	240	1600
KRS3		5720	-1005	28	2.0	88	700	2000
KRS4		5810	-1220	13	675	74	350	800
KRS5		5540	-1305	13	0.1	95	23	124
KRS6		5900	-1570	24	0.1	62		96
KR\$7		5/35	-1800	3	0.1	74	11	120
KRSS			-2030	5	0.1	81	10	103
KRSO		5425	-1770	16	0.1	107	38	152
KRSI		4600	1725	3	0.1	72	15	109
KRSI		4205	-1600	11	0.1	64-	18	8.8
ERST		3895	-1530	44	0.3	48	59	154
KRS1		3510	-1400	2	0.1	18	26	33
KRSI		3155	-1140	8	0.8	41	15	54
KEST		3575	-1059	13	0.1	78	18	110
KRSI		-840	2105	15	0.7	3.2	20	73
KESI		-550	2300	: 15	0.8	50	91	275
KRSI	8	-130	2040	8	0,3	57	23	125
KRSI	9	-270	2280	1	0 . 1	- 17	1.4	. 72
HS 1	-	3570	-90	- 16	0.5	31	35	66
HS2	÷ .	3210	35	53	0.8	12	15	7.4
H23		2760	180	- 5	0.1	. 24	1 1	38
H S 4		3660	180	43	1.0	103	1000	270
828		4395	405	23	0 . 6	600	38	164
สรุธ		2440	30	1	0.1	53	16	51
HS7		2270	580	4	0.1	. 32	1.3	57
HS8	٠.	1730	-175	1	0.1	51	3	63
HSS		2160	- 10	3 0	0.1	100		101
8810		2520	-260	8.8	1.0	60	6.9	147
H\$1		2770	-125	3.4	1.0	75	51	250
ns 1:		2445	-515	171	0.8	30	32	75
HS13		2105	-365	74	6.7	85	62	146
H\$34	_	2785	-710	140	0.3	55	37	550
8515		2960	- 325	9.8	0.2	78	73	176
HS 1		3310	-380	45	1:6	44	25	34
#\$ # 1 # \$ 1 \$	5 - 5	3600 4480	-300 155	64	0.5	103		184 560
88.J		4685	155 -170	74	2.7	190 84	1200 205	585
#873 # <b>\$</b> 20		4205	- 90	3 Ô	0 4	96	41	178
#85 1987	-		-300		0.6	117		<b>215</b>
HS2:				58	0.3	100		153
482			-760	73	0.5	45		
#\$ <i>2</i>		1200	680		0.2	203		
852	<b>5</b>	3870	680	1.3	1.3	. 63	8/	295

+ 4				-	1	* -	
Sample Ho.	- Coördi		Λu	ាក់ថ្ងៃការ	Cu	- <b>ይ</b> ዮ - 2	5 <b>76</b> 50 6
	X	Υ :	ը թ թ	<b>b</b> b a	ppn	t t a	ti o ta
8327	3430	800	9.3	1.2	81	1	1200
H\$28	3220	1130	113	1.3	40	86	3147
8529	2820	600	132	2.0	44	425	176
B\$30	3060	800	38	1.1	41	265	225
HS31	2980	1170	14	6.5	31	3 2	180
H\$32	2€30	910	20	0.3	5.2	2.3	67
HS33	4270	-470	-241	0.4	90	25	9.8
8834	3850	-830	<b>' 5 1</b>	2 9	38	23	6759
H\$35	3380	- 750	270	9.8	60	. 123	210
8536	4489	760	26	0.2	43	57	- ¢\$
H\$37	3630	1040	52	0.3	44	161	123
N\$38	3360	1385	19	9124	39	44	50
HS39	3055	1575	28	6.7	9 ž	176	295
H\$40	3500	1750	23	0.2	33	10	123
Ř\$41	3590	1640	113	6 3	30		110
HS42	4775	500	10	0.5	350		445
H\$43	1430	1550	10	0.3	6.8	5.5	150
HS44	1100	1630	1	0.2	45	13	8.3
NS 45	038	1045	2	0.1	87	3	80
HSAG	1215	1345	: 1	0.1	42	16	119
HS 47	2045	1630	16	0.3	6.0	270	285
HS48	2150	1355	5	0.2	24	89	132
HS49	1385	1105	5	0.2	72	78	235
H\$50	1200	800	3	0.1	62	6	13
K\$51	1455	640	4	0.1	78	- <b>È</b>	87
H\$52	1635	410	. · · · · · · · · · · · · · · · · · · ·	0.3	86	11	3.8
8553	1365	265	3	0.1	106	5	78
8854	1630	90	<b>, 3</b>	Ò.1	73	8	11
8855	1300	190	8	<b>0</b> . 1	81	8	52
8\$5€	2049	470	4	0.1	111	: 13	73
B\$57	1880	815	ð	0.1	80	9.4	181
H\$58	1730	1100	25	0.5	100	91	570
H\$59	1600	1420	4	0.3	5.4	4.4	390
KS 60	2260	1000	2	0.1	35	5	33
HŚĠI	2475	1225	5	0.2	3 1	10	35
H\$62	2460	1590	15	0.2	85	<b>£ 3</b>	171
HS63	2375	2010	10	0.3	53	3.9	168
8864	1150	1895	12	0.5	6.4	83	235
8865	1425	1950		0.7	23	12	104
HS66	2810	1395	?	0.1	22	8	30
HS67	2685	1830	9	0.6	50	31	134
HS68	3030	1930		0.1	51	15	55
6324	2810	2170		9. i	46	43	
HS70	2525	2440	1	0.1	37	23	113
8571	2220	2500		0.1 0.3	31	110	8.3
H\$72	1830	2515	7	0.3	21	60	75
ns73	1530	2205		0.7	21	14	71 193
H\$74	2060	2160		0.1	28	20	193 375
7A0.0 7A0.5	-720 -750	2065 2020		0.2	83	48 14	310
484.5	- 190	2029	7.0	4.9	3 (	14	3 2 11

Sample Ro.   Coordinates   Nu   Ng   Cu   Pb   7n   X   Y   Pph   Ppn   Ppm				•					_
X		Sample Ro.	Coord	inates	ĤΨ	· Na	Cu	Քե	7 n
761.0770 1970 1 0.4 22 15 81 701.5 -790 1930 1 0.1 30 10 45 702.0 -810 1885 1 0.1 16 10 35 702.5 -830 1840 1 0.5 15 10 40 763.0 -850 1800 1 0.4 16 26 56 703.5 -875 1750 1 0.3 13 23 47 704.0 -900 1700 2 1.1 17 20 46 705.0 -935 1815 1 0.1 17 20 46 705.5 -960 1560 1 0.1 17 20 46 705.5 -960 1565 1 0.2 19 7 49 706.0 -935 1815 1 0.3 18 12 63 705.5 -960 1565 1 0.2 19 7 49 706.0 -930 1520 1 0.1 23 7 56 706.5 -1010 1490 3 0.1 41 6 81 707.0 -1030 1435 1 0.1 33 7 51 707.0 -1030 1435 1 0.1 33 7 51 707.0 -1030 1435 1 0.1 33 7 51 707.0 -1030 1435 1 0.1 33 7 51 707.0 -1030 1436 1 0.1 35 7 47 708.0 -1080 1340 3 0.1 18 7 47 708.0 -1080 1340 3 0.1 18 7 47 708.0 -1080 1340 3 0.1 86 3 115 709.0 -1120 1250 5 0.1 86 3 115 709.0 -1120 1250 5 0.1 86 3 115 709.0 -1140 1200 5 0.1 86 3 115 7011.0 -1205 1070 147 0.5 39 18 57 7011.0 -1205 1070 147 0.5 39 18 57 7011.0 -1205 1070 147 0.5 39 18 57 7011.0 -1205 1070 147 0.5 39 18 57 7011.0 -1205 1070 147 0.5 39 18 57 7011.0 -1205 1070 147 0.5 39 18 57 7011.0 -640 1305 6 0.4 20 24 109 781.5 -660 1865 4 1.1 19 30 119 782.5 -700 1775 10 1.0 40 365 480 783.0 -720 1730 8 0.2 22 19 103 783.5 -740 1835 4 0.1 39 18 106 784.5 -720 1730 8 0.2 22 19 103 785.5 -825 1500 3 0.1 34 19 36 787.5 -825 1500 3 0.1 34 19 30 18 787.5 -825 1500 3 0.1 34 19 30 19 787.5 -825 1400 7 0.2 15 9 36 787.5 -825 1400 7 0.2 15 9 36 788.0 -845 1460 4 0.2 24 199 781.5 -860 1865 4 1.1 19 30 119 782.5 -740 1835 4 0.1 39 18 106 784.5 -720 1730 8 0.2 22 19 103 787.5 -825 1500 3 0.1 34 10 46 788.0 -845 1460 4 0.2 22 19 03 787.5 -825 1500 3 0.1 34 10 46 788.0 -845 1460 4 0.2 22 19 03 787.5 -825 1400 7 0.2 15 9 36 787.5 -930 1320 7 0.2 22 7 7 57 781.0 -890 1370 7 0.1 132 9 7 56 781.5 -930 1320 7 0.2 22 7 7 57 781.0 -800 1320 7 0.2 22 7 7 57 781.0 -800 1320 7 0.2 22 7 7 57 781.0 -800 1320 7 0.2 22 7 7 57 781.0 -800 1320 7 0.2 22 7 7 57 781.0 -800 1320 7 0.2 22 7 7 57 781.0 -800 1320 7 0.2 22 7 7 57 781.0 -800 1320 7 0.2 22 7 7 57 781.0 -800 1320 7 0.2 2 22 7 7 57 781.0 -1025 1000 21 1.2 26 30 72 7811.5 -1020 1320 7 0.2 2 2 2 3 38 781						=			
Z01.5									
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ZANIO.5       -1180       1115       9       1.7       19       7       36         ZANII.0       -1205       1670       142       0.5       39       18       57         ZANII.5       -1220       1020       22       1.4       25       9       50         ZANII.5       -1245       970       6       0.2       84       4       82         ZBO.0       -595       2000       20       0.2       39       33       410         ZBO.5       -615       1955       7       2.4       19       10       74         ZBI.0       -640       1905       6       0.4       20       24       109         ZBO.5       -660       1865       4       1.1       19       30       119         ZBO.0       -675       1820       8       0.3       29       64       158         ZBO.0       -720       1730       2       0.2       22       19       103         ZBO.0       -740       1635       4       0.1       70       41       174         ZBO.0       -740       1635       4       0.1       30       13								=	
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7011.5       -1320       1020       22       1.4       25       9       50         7012.0       -1245       970       6       0.2       84       4       82         780.0       -595       2000       20       0.2       39       33       410         780.5       -615       1955       7       2.4       19       10       74         781.0       -640       1905       6       0.4       20       24       109         781.5       -660       1865       4       1.1       19       30       119         782.0       -675       1820       8       0.3       29       64       158         783.5       -700       1775       10       1.0       40       365       480         783.5       -740       1685       4       0.1       70       41       174         784.5       -740       1685       4       0.1       70       41       174         784.5       -720       1590       5       0.6       62       143       295         785.5       -825       1500       3       0.1       34       10 <t< td=""><td></td><td>•</td><td></td><td>: 1115</td><td>3</td><td>· 1:1</td><td>13</td><td>7</td><td>3 &amp;</td></t<>		•		: 1115	3	· 1:1	13	7	3 &
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780.0		2011.5	-1320	1020	2.2	1.4	25	9	50
780.5		7012.0	-1245	970	. 6	0.2	84	4	8.3
780.5		780.0	-595	2000	20	9.2	39	33	410
781.0		760.5	-615	1955	. 7	2.4	13	10	. 74
761.5			-840		3		•		
782.0       -675       1820       8       0.3       29       64       158         782.5       -700       1775       10       1.0       40       365       480         783.5       -740       1635       4       0.1       70       41       174         784.6       -760       1640       13       0.1       39       18       106         784.5       -720       1590       5       0.6       62       143       295         785.0       -300       1515       2       0.1       136       9       138         785.5       -825       1500       3       0.1       34       10       46         786.0       -845       1460       4       0.2       24       3       65         787.0       -890       1370       1       0.1       32       8       73         787.0       -890       1370       1       0.1       32       8       73         787.5       -910       1320       2       0.2       27       7       57         788.0       -930       1275       3       0.1       24       5       46			-660		4				
782.5       -700       1775       10       1.0       40       365       480         783.5       -740       1635       4       0.1       70       41       174         784.0       -760       1640       13       0.1       39       18       106         784.5       -720       1590       5       0.6       62       143       295         285.0       -300       1515       2       0.1       136       9       138         785.5       -825       1500       3       0.1       34       10       46         286.0       -845       1460       4       0.2       24       3       65         786.5       -885       1410       7       0.2       15       9       36         787.0       -890       1370       1       0.1       32       8       73         787.5       -910       1320       2       0.2       27       7       57         788.0       +930       1275       3       0.1       24       5       46         789.5       -1000       1140       8       0.1       30       4       5					. 8				
763.0       -120       1730       2       0.2       22       19       103         763.5       -740       1635       4       0.1       70       41       174         764.9       -760       1640       13       0.1       39       18       106         764.5       -720       1590       5       0.6       63       143       295         285.0       -300       1515       2       0.1       136       9       138         785.5       -825       1500       3       0.1       34       10       46         286.0       -945       1460       4       0.2       24       3       65         786.5       -945       1410       7       0.2       15       9       36         787.0       -890       1370       1       0.1       32       8       73         787.0       -890       1370       1       0.1       32       8       73         767.5       -910       1320       2       0.2       27       7       57         768.0       -930       1275       3       0.1       24       5       46									
783.5		· -							
764.9760 1640 13 0.1 39 18 106 764.5720 1590 5 0.6 62 143 295 285.0 -800 1515 2 0.1 136 9 138 285.5 -825 1500 3 0.1 34 10 46 286.0 -845 1460 4 0.2 24 9 65 786.5 -885 1410 7 0.2 15 9 36 787.0 -890 1370 1 0.1 32 8 73 787.5 -910 1320 2 0.2 27 7 57 788.0 -930 1275 3 0.1 24 5 46 788.5 -950 1230 1 0.1 37 2 57 289.0 -970 1190 4 0.1 31 5 69 789.5 -1000 1140 8 0.1 40 4 56 2810.0 -1625 1095 23 0.1 20 4 91 7810.5 -1045 1050 68 0.8 64 61 177 7811.0 -1970 1000 21 1.2 26 39 72 7811.5 -1090 950 23 0.8 28 10 52 2812.0 -1110 910 31 0.6 46 31 245 76-7.0 -370 2110 2 2.5 38 38 162		The second secon						=	
784.5       -720       1590       5       0.6       63       143       295         285.0       -800       1515       2       0.1       136       9       138         285.5       -825       1500       3       0.1       34       1e       46         286.0       -845       1460       4       0.2       24       3       65         716.5       -825       1410       7       0.2       15       9       36         787.0       -890       1370       1       0.1       38       8       73         787.5       -910       1320       2       0.2       27       7       57         788.0       -930       1275       3       0.1       24       5       46         788.5       -950       1230       1       0.1       37       2       57         289.0       -970       1190       4       0.1       31       5       63         789.5       -1000       1140       8       0.1       40       4       56         269.0       -970       1000       21       1.2       26       39       72 <td></td> <td></td> <td></td> <td></td> <td></td> <td>and the state of t</td> <td></td> <td></td> <td></td>						and the state of t			
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7811.5 -1000 950 23 0.8 28 10 52 2812.0: -1110 910 31 0.6 46 31 245 70-2.0 -370 2110 2 2.5 38 38 162		and the second s							
7812.0: -1110 910 31 0.6 46 31 245 70-2.0 -370 2110 2 2.5 38 38 162		·							
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76-1.5 -390 2070 5 0.6 58 24 100									
		20-1.5	-390	2070	5	0.6	5.8	2.4	100

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Sample II	n. Conrd	inates Y	Ոս Էլե	e A a d d	Cu pps	PFM PFM	76 ·	
70-1.0		2025	2	0.5	· 500		89	
76-0.5	-430	1980		1.0	6.3	42	260	
20.0	-455	1935	7.4	1.0	6.3	143	350	
700.5	415	1890	8	0.7	18	3.3	162	
701.0 701.5	-500 -520	1845	. 42 39	0.2 0.8	3 Ø	83 157	159 250	
7(2.0	-540	1760	24	7.2	30		1600	
202.5	- 560	1710	10	1.3	3 0	150	370	
703.0	-529	1665	1 7	6.7	3 32	73	163	
Ž(3.5	- 600	1620	4	0.6	40		182	
764.0	-625	1575	5	0.5	60		350	
ŽC4.5 (7C5.6)	-645 -670	1530	· 1	0.4	116	43 9500	325 3900	
7.05.5		1440	- 1	0.1	49	13	-391 -391	
705.0	- 710	1390	2	<b>8 ∂</b> . 1	41	7	101	
206.5	· 725	1350	2 -	6.1	54	5	103	
767.0	-750	1300	15	0.1	104	6	171	
201.5		1260	?	0.1	-51	4	73	
: /// 2 / 2 / 2 / 2 / 2 / 2 / 2 / 2 / 2	2790 2815	1210 1165	1	0.1 0.1	- 66 50	4 · ·	330	
2(3.0	-815	1120	3	0.1	37	21	78	
209.5	-860	1075	12	0 1	60	7	62	
·7010.		1030	23	0.3	37	7	70	
*ŽČ10.	-900	975	32	0 : 1	32	10	46	
7¢11.		930	4.3	0.4	27	24	75	
7011.		890	18	0.1	26	20	33	
2012.	) - 360 - 320	840 1870	77	0.5	65 38	43 38	162 210	
200.5	-340	1825	163	2.1	61	170	980	
261.0	- 360	1780	175	7.4	55	300	1350	
701.5	-380	1740	41	2.1	37	138	2050	
702.0	-405	1690	155	2.1	88	460	3100	
702.5	-425	1650	2	0.2	13	36	112	
703.0 703.5	-450 -470	1600 1555	- 23	0.1	36 40	13 120	121	
704.0	-490	1510	- 9	1.0	90	330	1050	
704.5		1465	3.4	4.4	300	1400	590	
705.0	- 530	1420	25	0.1	6.4	1	115	
ž65.5		1375	1	0.1	8 2	1	80	
706.0		1330	2	0.1	78 78	2	150 115	
706.5 707.9		1280 1235	3	0.1	64	5	200	
707.5		1190			58	i	280	
708.0					51	1	158	
708.5	-680	1100		0.1	4.8		72	
269.0				0.1	11		3.4	
709.5				0.l	€ € 5 8		120	
7010. 2010.					58 104	10 3	104	
7010. 7011.					72	21	137	
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, -117 f	X		ppb.	ppm	p p 14	ppn	ppn	
7011.5	-805	820	1	0 , L	70,	2	96	
70.12.0	-225	780	2	0.1	10/	1	110	
780.0	-180	1810	<b>95</b>	4.0	3.2	230	270	
760.5 761.0	-205 -225	1760 1720	53 37	1.8	36 33	319 190	420 1300	
ZE1.5	-245	1670	90	1.1	33	300	1000	
7 F 2 . 0	-270	1630	21 -	9.8	23	134	150	
7F.2.5	-230	1580	17	2.1	36	249	535	
7 F 3 . G	- 310	1540	6	0.9	45	180	265	
763.5	- 330	1435	25	2.1	410	3050	1750	•
764.0 764.5	-350 -375	1445	40 16	2.8 0.4	415	4650 460	4900 1450	
7 E 5 . 0	-400	1350	10	0.1	67	11	, 31	
265.5	- 415	1310	. 1	0.1	30	13	197	
7 6 . 0	-440	1265	2.	0.1	106	2	190	
256.5	- 460	1215	2	0.1	37	6	5.4	
7E7.0	-420	1170	4	0.1	7.3	13	60	
7E7.5	-505	1130	3	0.1	33	12	4.7	
768.0 269.5	-525 -545	- 1080 1646	: 4 2	0.3 0.1	32 162	10	4.4 7.3	
7E 9.0	-565	390	2	0.1	34	3	112	
289.5	- 590	940	80	0.8	91	1 8	136	
ZF10.0	-610	895	7.0	2.2	32	10	57	
ZE10.5	- 630	345	3	0.1	3 4	2	127	
7E11.0	-650	305	2	0.4	44	4	-51	
ZE 11.5 ZE 12.0	-670 -695	760 715	7	0.1 0.2	65 36	· 4	78 131	
750.0	- 45	1745	30	2.8	33	190	250	
7F0.5	-70		29	2.9	27	146	170	
Z£ 1.0	- 30		8	1.7	22	102	<b>\$ 2</b>	
7F1.5	-110		27	1.3	24	28	45	
7F2.0	- 135		3	0.7	21		45	
7f2.5 2f3.0	155 - 170		.4	0.9	22 25		37 51	
ZF3.5	-195		3	2.0	33	33	41	
2F4.0	-215		5	0.7-	3.4	15	47	
7F4.5	-240		. 1	0.6	49	12	6.0	
Z£5.0	-260		. 1	0.2		\$	71	
75.5	- 280		3	0.1	74	1 4 &	35	
266.0 766.5	-305 -325		1 2	0.1 0.1	30 67	7	235 139	
7, Q 9 7, 7, Q	-345		2	0.1	31	6	57	
767.5	-370		2	9.1	40	8	47	
288.0	- 330	1015	3	0.1	59	3	5.8	
788.5	- 4 1 0		, <b>6</b>	0.1	57	3		
783.0	-130		8	0.2	23	\$	33	
7 <b>59.</b> 5	- 450 - 175		6 3	1.6	24 20		50 31	
2519.0 2519.5	-1/5 -495			1.0 0.1	29		5 f	
2F11.0	- 5 1 5		1	0.1	10	5	90	

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	Sample Ho.	Coordi	nates	Ĥu	Ŋа	( u	ք ե	7 6
		Х	Y	թթե	<b>Ե</b> Ն ա	pps	թթա	ស្ស្រា
	7811.5	-265	570	1	0.1	38	5	58
	71112.0	-285	520	2	9.1	30	2.2	193
	710.0	360	1555	13	0.1	66	13	106
	210.5	340	1505	11	1.0	6.0	2.8	182
	711.0	320	1460	13	0.1	46	Ê	37
	211.5	295	1415	S.	6.0	26	5.3	300
	712.0	275	1370	12	0.2	33	51	134
	712.5	255	1325	6	Ó.5	30	52	3.6
	713.0	230	1275	6	1.0	43	7.4	195
	213.5	210	1230	13	8.6	360	3000	2000
	734.0	130	1185	6	0.4	45	33	205
	214.5	170	1140	1	0.1	102	3	205
•	715.0	150	1095	1	0.1	6.8	3	76
	215.5	130	1050	3 1	9.1	112	7	3.8
	7.16.0	195	1010	Ĭ.	0.4	78	\$	130
	216.5	85	950	3	9.1	6.6	5	6.2
	217.9	60	910	3	Ó.1	5.8	13	66
	711.5	40	855	Ź	0.1	48	6	97
	713.0	20	820	2	0.1	76	7	143
	718.5	9	780	Ż.	0.1	67	1.4	14
	719.0	-20	735	5	0.1	39	5	48
	713.5	- 45	685	3	0.1	30	14	3 /
	7110.0	-65	640	3	0.1	128	5	37
	2110.5	-9 <b>0</b>	595	2	Q. 1	99	2	3.4
	7111.0	-110	550	4	0.1	23	- 10	3 /
	2111.5	-130	500	4	0.1	2.8	14	5 1
	Ž112 0	-155	460	3	0.1	4.5	46	148

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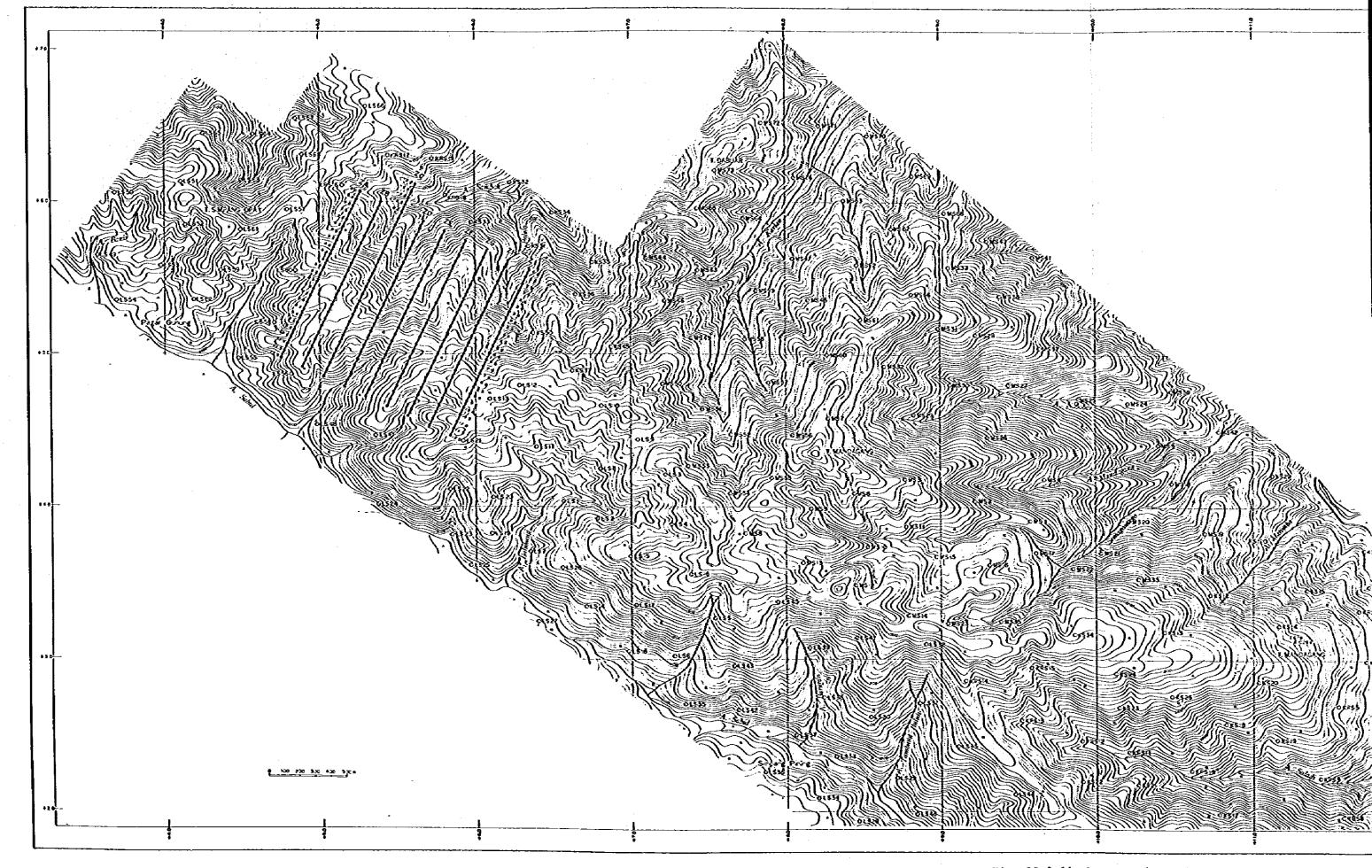


Fig. 11-3-34 Location Hap of Geochemical Samples in Mus

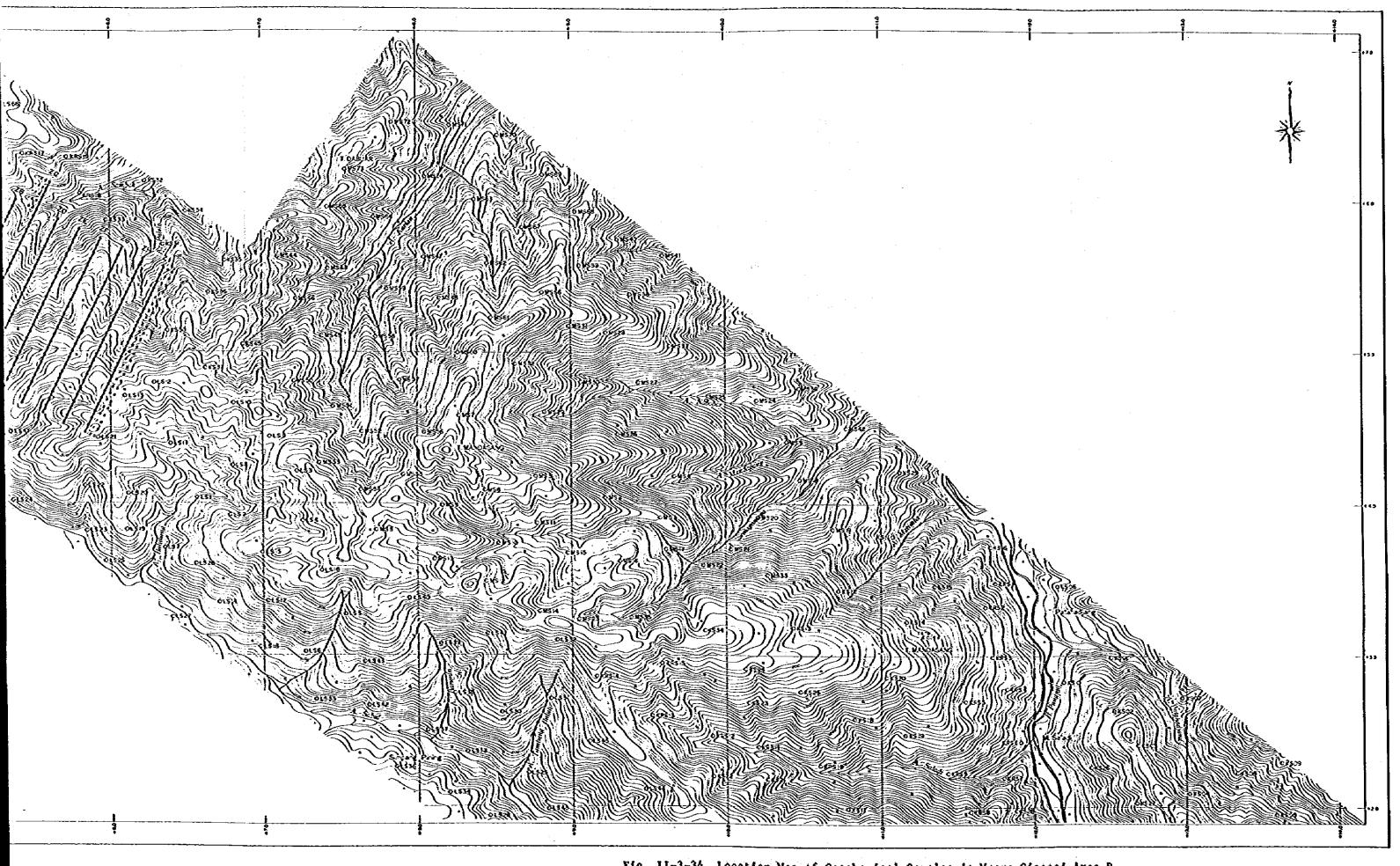


Fig. 11-3-34 Location Hap of Geochemical Samples in Huara Sipongi Area B

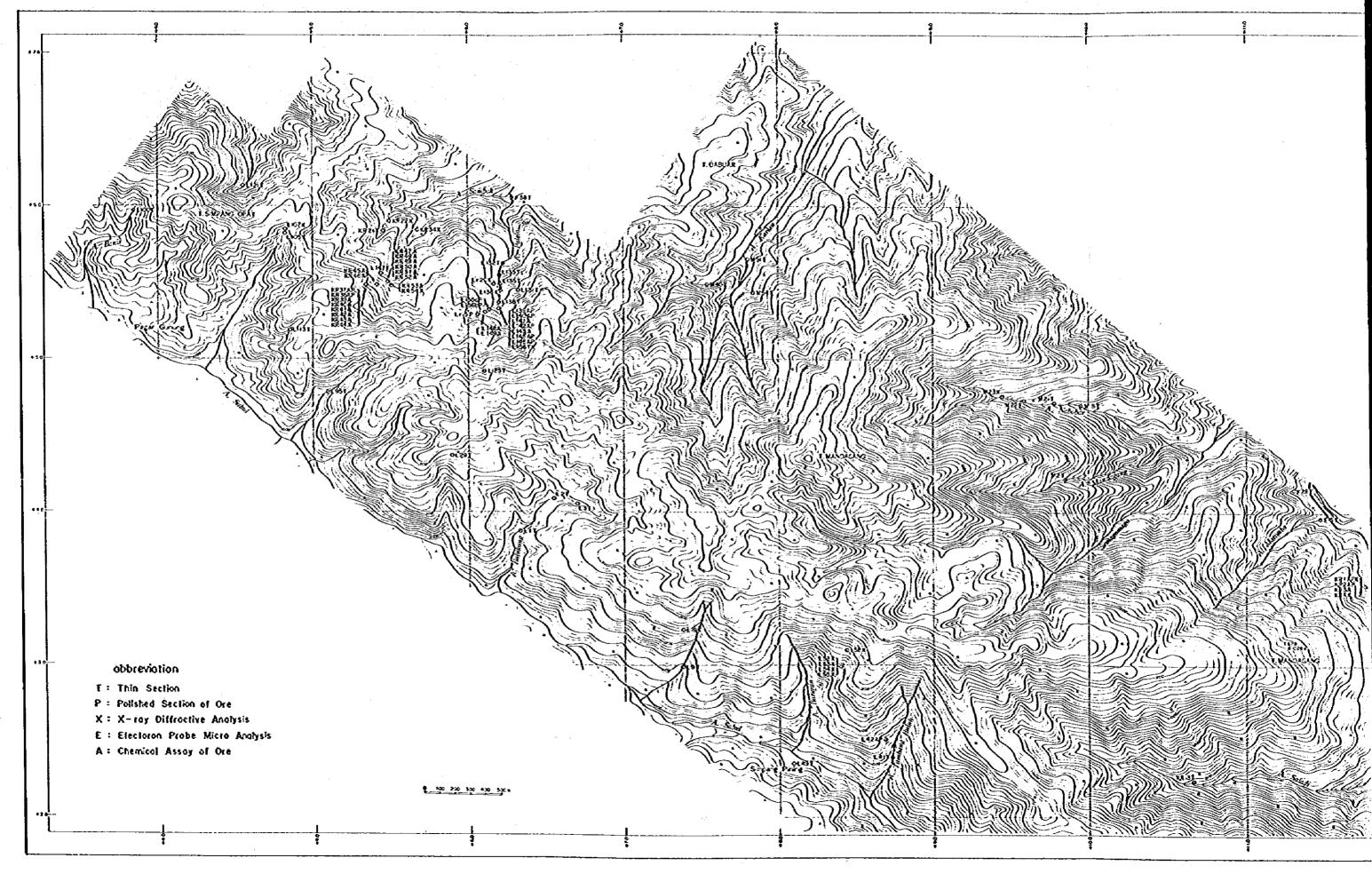


Fig. 11-3-35 Location Hap of Rock and Ore Samples Tested in

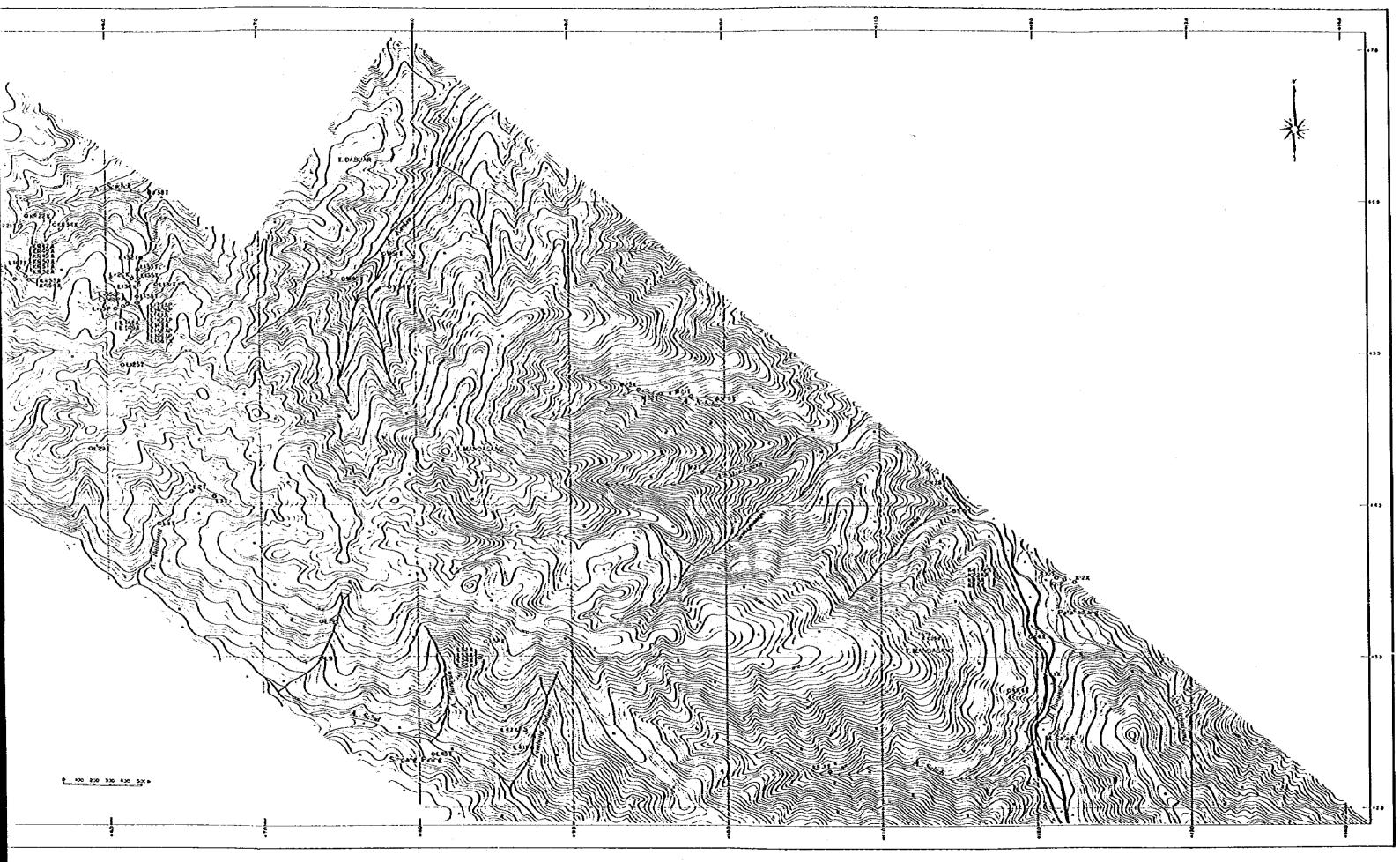


Fig. 11-3-35 Location Hap of Rock and Ore Samples Tested in Kuara Sipongi Area B

# PART III GEOPHYSICAL SURVEY (SPECTRAL INDUCED POLARIZATION METHOD)

### CHAPTER 1 GENERAL DISCUSSION

### 1-1 THE PURPOSE OF THE SURVEY

In the first phase survey (1982), a reconnaissance survey consisting of geological and geochemical survey was conducted in the Muara Sipongi area, (extending over a 400 km<sup>2</sup> area). The distribution of several outcrops containing copper, lead and zinc sulphides were confirmed in Pagar Gunung. These deposits are of a contact metasomatic skarn type.

The outcrops can be sporadically found in a 200 meter elongated zone, extending in an East-West direction, however, the continuous extent of the deposits at the surface could not be traced due to the dense growth of the tropical rain forest.

In order to conduct a geophysical survey which would give clear results, the Spectral IP method was used. This method makes it possible to identify the kind of mineral, or type of deposit which exists, by means of the spectral responses to magnitude and phase. This method is the most modern method which is used for ore deposit surveys, as it allows for reliable acquisition of deep, low resistivity zones, by de-coupling the electro-magnetic phenomena, which was difficult to achieve by using the conventional IP method.

### 1-2 AREA OF THE SURVEY

The area of the survey is located to the south-east of Kotanopan, 9 kilometers away. The terrain has generally steep slopes, which are covered with dense tropical rain forest. However, the mountain tops are generally smoother and the vegetation is less dense than that of the sides (Fig. III-1-1).

### 1-3 THE QUANTITY OF WORK AND THE SURVEY PERIOD

There were a total of 9 survey lines, with a total length of 11,000 meters. The individual line lengths, and their results are shown below, in Table III-1-1:

Table III-1-1 List of Survey Lines

No.	Name of Line	Length of Line (m)	Measurement Value (point)
. 1	Line A	1,200	40
2.3 3	Line B Line C	1,200 1,400	(1) vivina <mark>39</mark> seq (1941) visar
4 99		1,200	times in 40 si thi Louisia
. 5 6	Line E Line F	1,200 1,200	. 1 19 1 40 372 3 4 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
- 7 ·	Line G	3 3 1 1 1 200 x 1 2 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	1 5 5 6 40 5 M , 6 3 6 6
8	Line H	1,200	40
9	Line I	1,200	40
. 77 : 1	Total	11,000 (m)	368 (point)

### Survey Period as a section of the control of the co

Hobilization and Preparation
Line Brushing and Survey
SIP Data Acquisition
Data Processing at Site
Demobilization
Data Processing, Physical
Property Measurement and
Interpretation
Submittal of Report

From 30 May 1983 to 13 June 1983
From 11 June 1983 to 9 July 1983
From 14 June 1983 to 18 July 1983
From 19 July 1983 to 12 August 1983
13 August 1983

From 15 August to 31 December 1983

Markett Transport

1 4-14 -15 1

10 February 1984

### **Specifications**

(1)	Total Line Length	11,000 m
(2)	Number of Lines	9 lines
(3)		368 points
(4)	Line Interval	150 m
(5)	Station Interval	100 m
(6)	Electrode Separation Factor	$n_1 = 1 - 5$
(7)	Electrode Configuration	Dipole-Dipole Array

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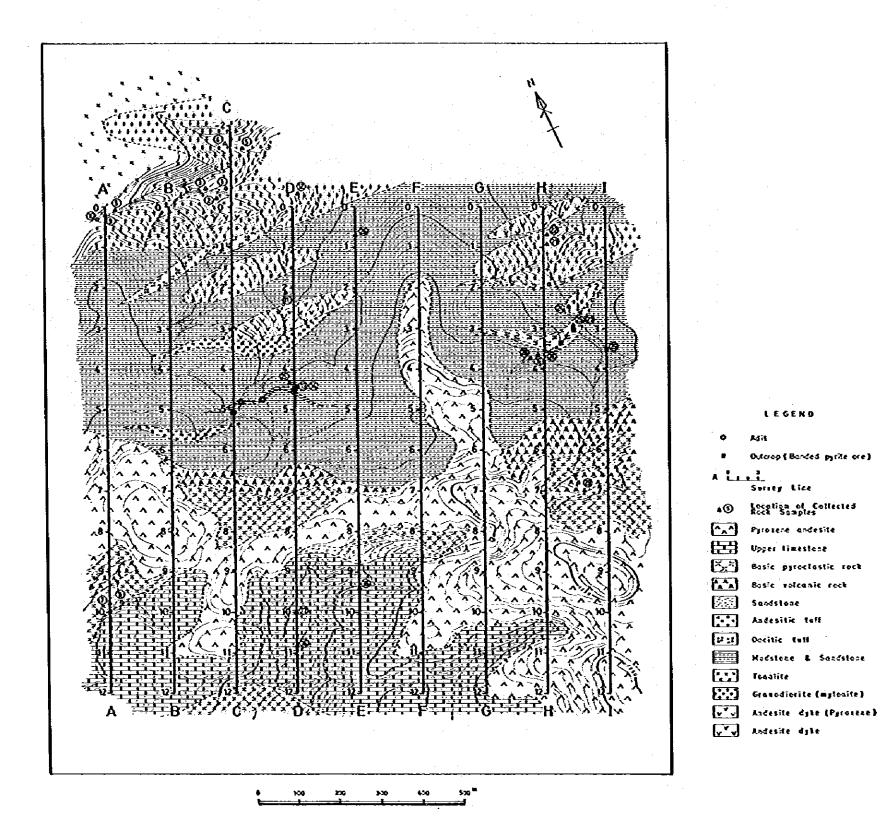


Fig. III-1-1 Location Map of Spectral IP Survey Lines

### CHAPTER 2 SURVEY METHOD

The Spectral IP method gives the ability to survey the magnitude and phase, using a wide variety of frequencies from 0.001 to 1,000 Hz. This method has the advantage over the former method, as it has the ability to discriminate between the anomalous IP source from the frequency responses (spectral responses) of the stratum and the ore body. On the other hand, the conventional IP method only surveys the resistivity of the two frequencies. The frequency range most often used is from 0.1 to 100 Hz for all practical reasons. In this present survey a system of the Zonge Engineering & Research Organization, which is the manufacturer of the equipment were used whose frequency range is from 0.125 - 88 Hz. In this survey, three fundamental frequencies of 0.125 Hz, 1 Hz, and 8 Hz were adopted. A Fourier analysis of these frequencies, and also their third, fifth, seventh, ninth and eleventh harmonics were surveyed, to check the IP responses.

### 2-1 SURVEY METHOD

The survey technique for the Spectral IP method is basically not so different than the technique for the conventional IP method, in that they both use dipole-dipole electrode configurations in the frequency domain. However, in the Spectral IP method it is necessary to record the same period in time of the signals, in both the transmitter and receiver, as the Spectral IP survey uses the magnitude and phase in higher frequencies. In order to accomplish this timing of the signals, a "communication wire" connecting the transmitter and receiver, is laid parallel to the survey line. The layout of these lines is shown in Figure 111-2-1.

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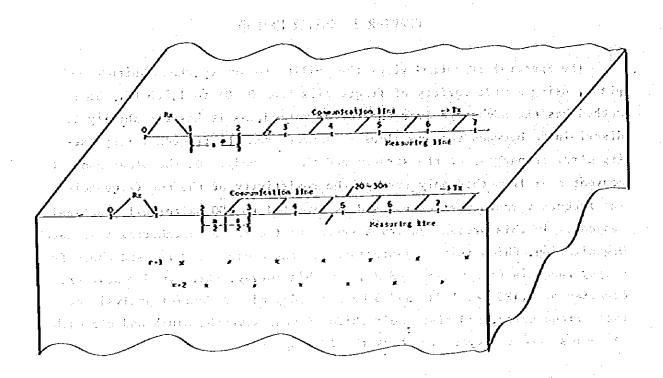


Fig. III-2-1 Spectral IP Survey Lines

The Layout of the Potential Electrodes

In this survey, non-polarizable potential electrodes were used. These electrodes consist of a saturated copper sulphate solution, contained in a porous pot with a copper conductor. Three electrodes are placed together, this is different from the ordinary IP method. (see Figure III-2-2).

This arrangement enables better noise rejection in the differential preamplifier, as a zero electric potential point is established at point (B), exactly the same distance between points (A) and (C).

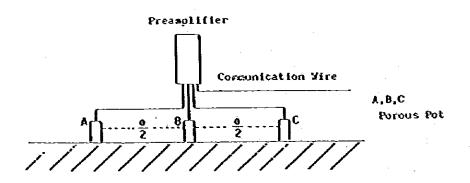


Fig. III-2-2 Arrangement of Potential Electrodes & Preamplifier

The Layout of the Current Electrodes

When the current electrodes are laid out, the future mobility and operational efficiency of the electrodes are taken into consideration. Normally, 7 or 9 electrodes are placed ahead of time, and the connections are changed at the transmitter, as required. In this survey a 9 electrode configuration was used. This arrangement is shown in Figure III-2-3.

The electrodes consist of 8 Stainless Steel wires, with a diameter of 5 mm, they are 0.60 meters long. If the resistance to earth is very high, the number of electrodes is doubled, to give a total of 16.



Fig. III-2-3 Arrangement of Current Blectrode & Wires

### 2-2 MEASURING EQUIPMENT

The equipment used in this survey is manufactured by Zonge Engineering and Research Organization Co., from Tucson, Arizona, U.S.A. The component parts of this equipment are described in Table III-2-1, and a typical measurement configuration is shown in Figure III-2-4.

Data processor	CDP-12/2G	1
Pre-amplifier	FP-12	2
Isolation amplifier	1S0/1	2
Cassette-printer	CAP-12	1
Oscilloscope	Tektronix 212	1
Transmitter	FT-1 Geotronics	1
Engine generator	ZHG-5	ī
Voltage regulator	VR-1	ŧ

Table III-2-1 Survey Equipments

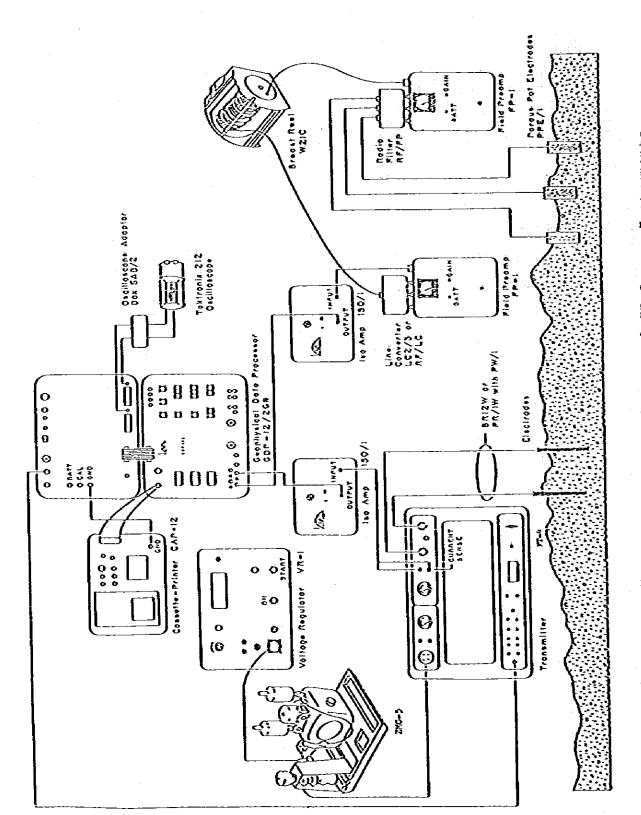


Fig. III-2-4 Block Diagram of Spectral IP Survey Instruments

responded to the first of the contract of the

In the Spectral IP method, the magnitude and the phase of the signal are measured, the results are plotted as the spectrum versus the frequency, or the Cole-Cole diagram, as it is called. Apparent resistivity, 3 point decoupled phase, and so on are shown as a pseudo-section, which is the same as the former IP method.

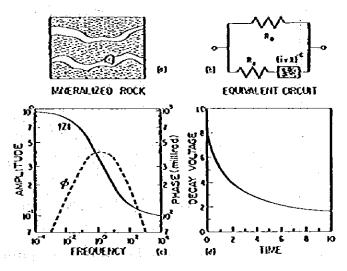
# The Conception of Spectral IP

And result of Daniel the artist the first

The conception of spectral IP is shown in Figure III-3-1, where (a), shows a small section of a mineralized rock, which has both blocked and unblocked pore pasages. If this is depicted in an equivalent

is depicted in an equivalent circuit, then it appears like (b). (c) shows the time domain responses, while (|Z|) and (\$\phi\$) are the measuring value in spectral IP.

In Figure III-3-2, the concept of in-phase and out-of-phase are shown. When the arbitrary amplitude rectangular waveforms are transmitted, the signals, which phase-shift, are (\$\phi\$),



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Fig. III-3-1 Spectral IP Effect

with an amplitude of (V) obtained at the receiver.

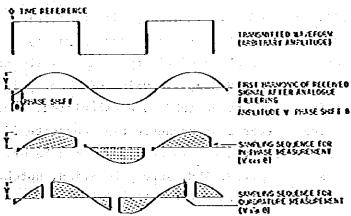


Fig. III-3-2 Transmitting & Receiving Wave-forms

The sampling sequences for in-phase and quadrature measurement are shown in the graphs in the lower part of Figure III-3-2. The relation between frequency effect and phase angle is shown in Figure III-3-3, in this figure the Cole-Cole diagram is adopted, with the Vertical axis showing negative out-of-phase factors, and the horizontal axis showing positive in-phase factors. The magnitude (Mi) is at 0.1 Hz, and (M2) is at 1 Hz, the phase angle is (\$\phi\_1\$) and (\$\phi\_2\$). Frequency effects and in-phase factors are approximately directly proportional to each other, and the phase angle and out-of-phase factors are directly proportional to each other. The black dotted line in the figure shows the results of the measurement, with the lower frequencies occurring to the left.

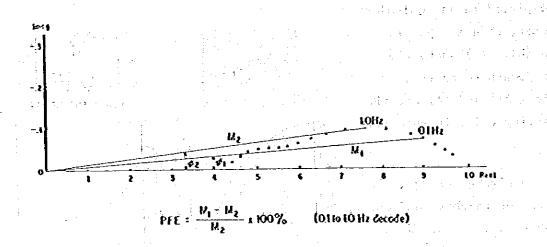


Fig. III-3-3 Relation between Frequency Effect & Phase Shift

## 3-1 DATA MANIPULATION

Data from field measurements give phase shift and amplitude of eighteen frequencies, from 0.125 Hz to 88 Hz. These signals are recorded and inputted to the data Processor (GDP-12G), where the real and imaginary part of each frequency are calculated, as are the resistivity values of the three fundamental frequencies (0.125, 1, and 8 Hz), the value of three point de-coupled phase and the percent frequency effect (PFE) are calculated. The results are printed out, and can also be stored on magnetic tape cassette if necessary. Other data relevant to the survey are also stored and can be printed out, these include; the current supplied, SEH, survey location, notch filter setting, and stacking number, (see Figure III-3-4).

23.23 2002 818 2212 824 2 CH CR YELL GAING 88 SEFFLIER BY STRS 85127 7 8.22 SHI 8.13 R-SP 5.822 · KI +,91735E18 11 +,5561964E41-2 KI 1,98865E18 II 1,120192X18 E 1. 142622E+8.3 द्वा १.६६५११६४ । १.४५११६६६ SE9 1.8177553E18 19 1.3917183E18 Z 在江川湖流出 17、4、34%17年18至 60 1.1783245E4 PR 1.594375E-173 37 1.1643353E-1 FEELETTSSZELE BI LITTIKA BUNINGSAS 如 4.从对策略 如此复复数的 \*\*\*8042 

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#### Index

RCVR; Receiver position XMTR : Transmitter position 2 CH CR; 2channel Spectral IP Gains; Gain of channel 1,2 Filter O1; Notch filter "ON" STKS; Number of stucking 8.0 Hz; Transmitted frequency SHNT; Shunt resistor N-SP; Electrode spacing factor RE11 ; Real part (left side) II; Imaginary part (right side) RHO; Apparent resistivity PH ; Raw phase 3PT; 3 point decoupled phase MG1, MG2; Magnitude of channel 1,2 CRT; Transmitted current SEM; Standard error mean

Fig. III-3-4 Example of field data print out

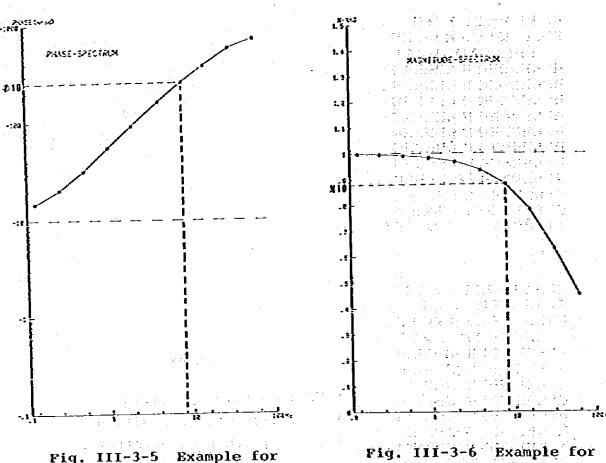


Fig. III-3-5 Example for

Phase Spectrum

Magnitude Spectrum

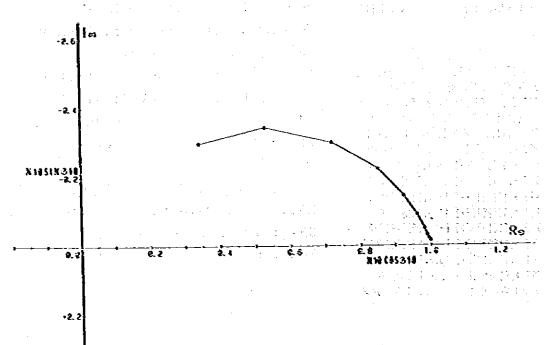


Fig. III-3-7 Example for Cole-Cole Diagram

As data manipulation occurs, a pseudo-section is normalized, also a calibration correction and any topographic corrections are applied if necessary, to the resistivity curves.

# 

A daily calibration measurement was taken, prior to any field measurements, the values received in this measurement were then removed from subsequent signal measurements at each point, in order to be sure that only the correct earth signal was being calculated. Phase spectrum (Figure III-3-5), magnitude spectrum (Figure III-3-6), and a Cole-Cole diagrams (Figure III-3-7), were made for the surveyed values, after the calibration.

### 3-2 TOPOGRAPHIC CORRECTIONS

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Generally, when a dipole-dipole electrode array is used, then the topography strongly effects the apparent resistivity values. The tendency is that topographic highs produce correspondingly higher apparent resistivity values, and topographic lows produce correspondingly lower apparent resistivity values. As this survey was in a mountainous region, then corrections for these elevation changes were made, especially to the south, on survey lines B, D, E and G. The topographical section was measured for each of these survey lines, these measurements were inputted in the computer, which then calculated the effects of the topography to the apparent resistivity. These calculated effects were then used to correct the observed results from the survey lines.

# 3-3 ROCK SAMPLE MEASUREMENT of the property of the property of the first of the batch of the bat

In order to evaluate the observed results of the resistivities and spectral responses of magnitude and phase of the rocks which are found in the survey area, a total of 29 rocks and ore samples were collected from the surface of the survey area. These samples were sent to Japan to be analyzed for their properties, Figure III-3-8 shows the test measurement installation.

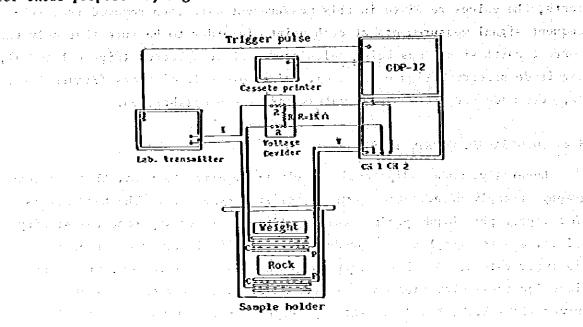


Fig. 111-3-8 Block Diagram for Sample Measurement

It seems dangerous and limited to try to represent the resistivity and spectral responses for phase and magnitude of these surface samples as being the same as the sub-surface rocks in the same area; however, it is important to know the types and qualities of the local rocks, and especially for the anormalous rocks by Spectral IP method.

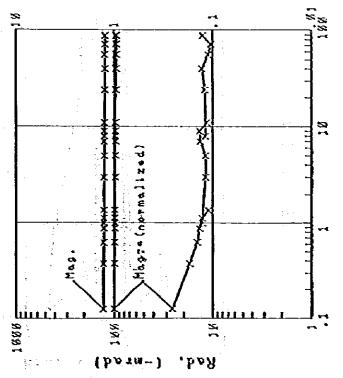
The results from these samples can be categorized by their spectrum which fall into four groups, as follows:

- Type A: The spectrum which decreases slowly as the frequency decreases.
- Type B: The spectrum which shows the minimum value in the 3 5 Hz range, and increases in the low and high frequencies.
- Type C: The spectrum which shows almost a horizontal line.
- Type D: The spectrum which increases as the frequency increases.

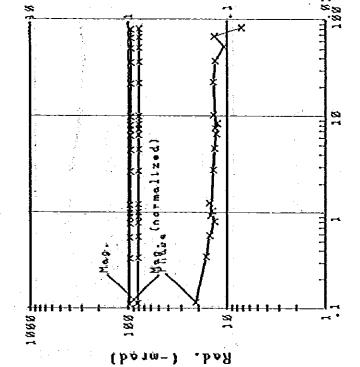
Table III-3-1 Results of Rock Sample Measurement

<del></del> 1				<u> </u>	) point		Spectral	
Sarrie Fo.	Rock Name	Slock So. of Saist Out	Resistivity (U-m)	Pav Fbase (-zro3)	Pecosples  [hase [-mas]	(1)	Die of	Estarks
3	Musicovité granciforite (Hylonite)	69474	\$42	26.0	32.8	2.03	A	Py-diss
2	Muscovite granodioxite (Mylónite)	58*63	457	21.3	25.0	2.10	8	
3	Muscovite granodicrite Divionite)	527-57	1845	17.7	18.0	2.23	D	ty-diss
4	Miscorite granoficrite (Mylocite)	81 > 85	414	27.2	39.4	2.83	à	fice by veta
5	Priscovite granodiorite (Bytonite)	33541	722	17.9	20.6	1.61	8	
6	Courts velu	63769	2590	20.5	29.5	2.51	С	By setvort
7	fice grain Andesite	201-75	2200	4.93	4.87	0.67	D	
. 8	Easic tollacious sandstone	33 - 38	5020	16.2	16.3	2.01	D	
9	Riscorlite gracodiocite	21 ~ 26	1090	25.6	27.1	3.07		Fy network
10	Meta ändesite	8548)	3310	10.2	10.3	1.43	D	ly-izp
,11	Silicious audstone	154 20	6360	6.17	6.99	0.73	c	
12	Biscorite granodiorite	87 ~ 90	644	15.4	17.3	1.62	c	by network
13	Black ore (Fb + Zn + Fy)	31.33	130	33.0	111	9.28	A.	
14	Black ore {!lacultizes} (Fb + Ea)	137-19	163	133	150	13.2	λ	
15	Black cre (fb + 2n + fy)	53.4.35	61.0	436	456	69.5	A	
16	&n≫sitic telf	31 ~ 33	2320	9.50	11.3	0.92	В	
17	White limestone	176	7630	5.24	4.8)	0.75	D	
18	White limestone	53 > 62	21300	4.90	4.93	0.53	0	
19	Sandstone	254, 6.7	1230	16.0	29.1	1.34	В	
20	Sabistone	75 4 8 1	1530	10.5	17.4	0.82	٨	Quite vein
21	Muscovite granodiorite	9114	2340	15.4	16.0	1.58	D	
22	Siliclous andesite	25 \$ 30	7730	29.3	24.7	4.47	D	Py-120
23	Altered assessite	45 ~ 51	45.9	90.3	133	4.65	A	
24	Muscovite gramodicrite	45 > 50	433	33.8	19.5	3.23	λ	
25	Bankel pyrite cce	€4∿63	45.3	429	437	75.3	A	
<b>76</b>	Limmite gussan	7712	631	20.0	31.9	2.99	С	Porous, Py-1s
27	Bardol fyrite cre	18 ~ 24	168	4%	129	€1.7	λ	
28	Docttic telfactors sandstone	\$13.56	2550	€9.7	67.6	7.63	٨	Fy. 1b + En-Imp
23	Dacitic tellacious substace	15 \ €)	1819	11.2	31.9	1.29	С	





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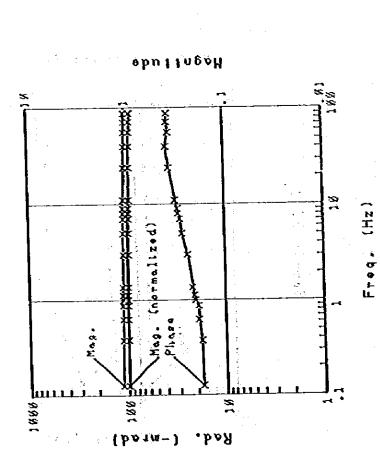
Freq. (Hz)
Fig.III-3-9.2 Spectrum of phase & Magnitude (Sample No.2)

Pig.III-3-9.1 Spectrum of phase & Magnitude

Frag. (Hz)

(Sample No.1)





Sample NO. 4

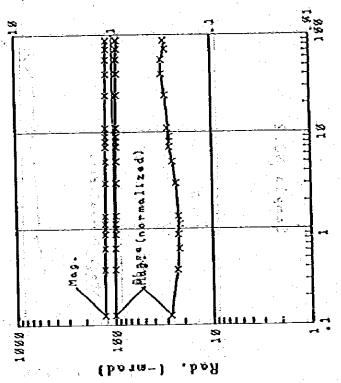
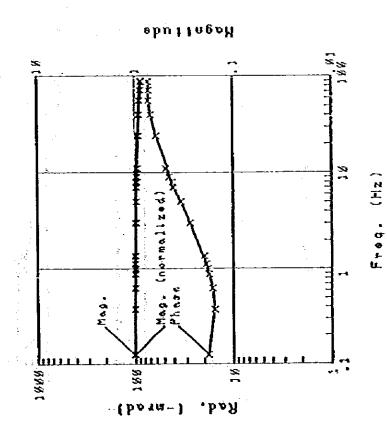


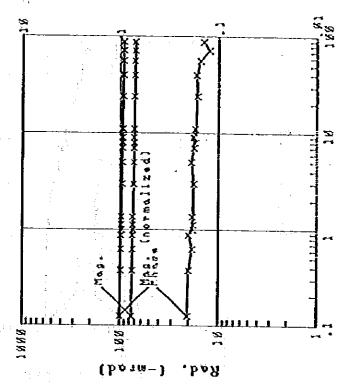
Fig. III-3-9.4 Spectrum of phase & Magnitude (Sample No.4)

Fig.III-3-9.3 Spectrum of phase & Magnitude

(Sample No.3)







Sample NO. 5

Fig.III-3-9.6 Spectrum of phase & Magnitude

Fig. III-3-9.5 Spectrum of phase & Magnitude

(Sample No.5)

(Sample No.6)



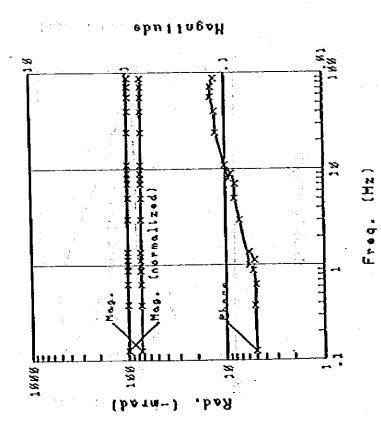


Fig.III-3-9.7 Spectrum of phase & Magnitude (Sample No.7)

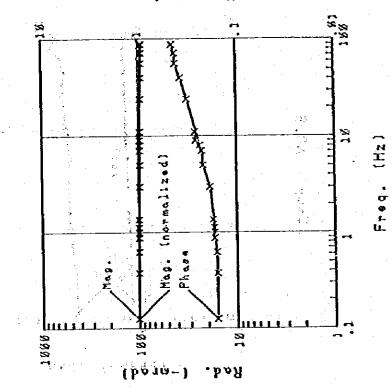
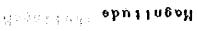
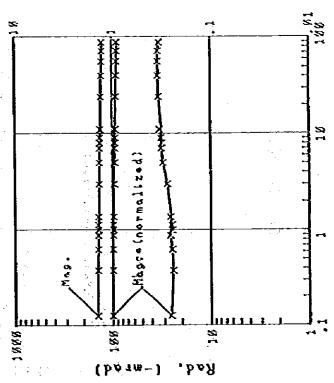
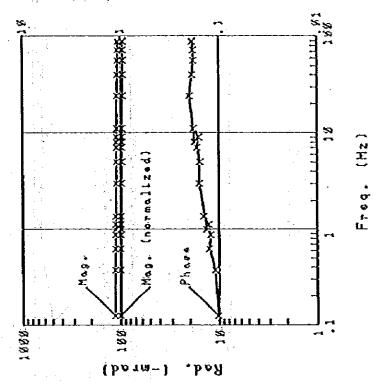


Fig.III-3-9.8 Spectrum of phase & Magnitude (Sample No.8)





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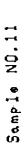


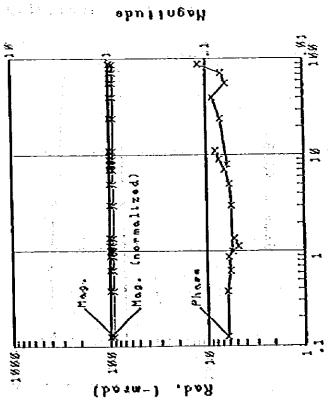
Sample NO.9

Fig. III-3-9.10 Spectrum of phase & Magnitude (Sample No.10)

Fig. III-3-9.9 Spectrum of phase & Magnitude (Sample No.9)

Freq. (Hz)



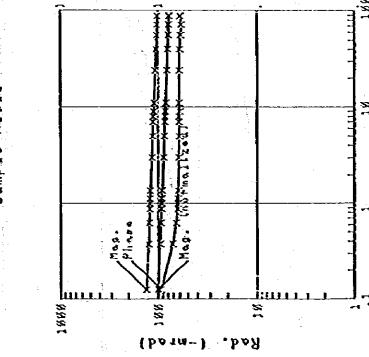


Freq. (Hz)

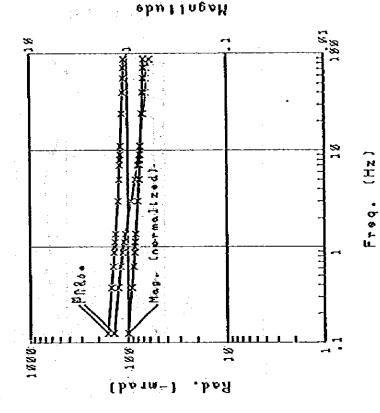
Fig. III-3-9.11 Spectrum of phase & Magnitude

(Sample No.11)

Fig.III-3-9.12 Spectrum of phase & Magnitude (Sample No.12) Freq. (Hz) (bo1m-)

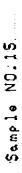


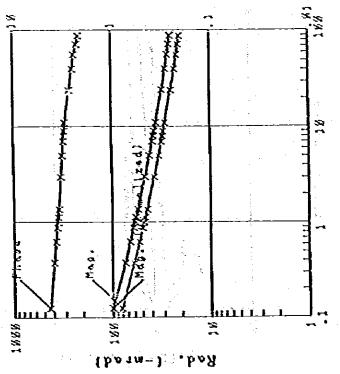
Freq. (Hz]
Fig.III-3-9.13 Spectrum of phase & Magnitude
(Sample No.13)



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Fig. III-3-9.14 Spectrum of phase & Magnitude (Sample No.14)





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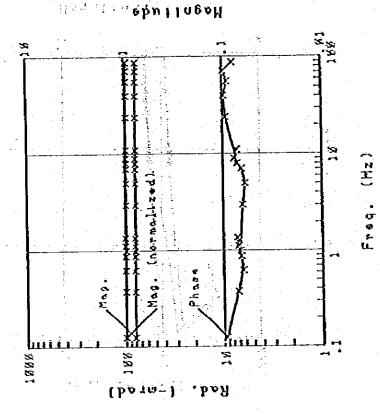


Fig. III-3-9.16 Spectrum of phase & Magnitude (Sample No.16)

Fig. III-3-9.15 Spectrum of phase & Magnitude

Freq. (Hz)

(Sample No.15)

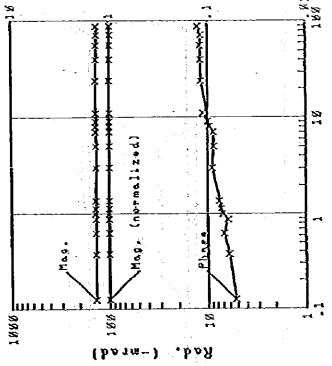
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Sample NO.18



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Freq. (Hz.)

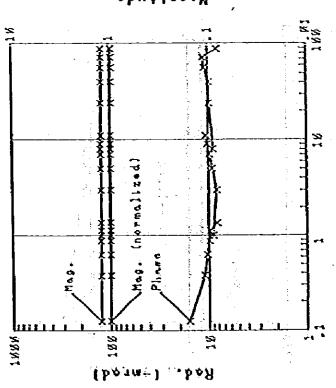
Fig. III-3-9.18 Spectrum of phase & Magnitude (Sample No.18)

Fig. III-3-9.17 Spectrum of phase & Magnitude

Freq. (Mz)

(Sample No.17)





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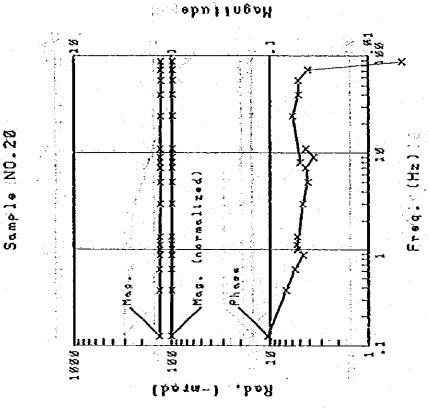


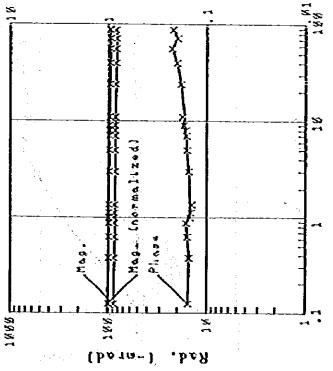
Fig. III-3-9.20 Spectrum of phase & Magnitude (Sample No.20)

Fig. III-3-9-19 Spectrum of phase & Magnitude

Freq. (Hz)

(St.on oldmas)





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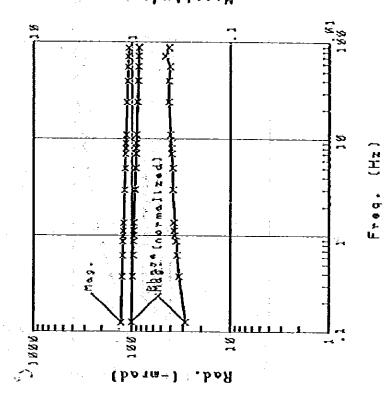
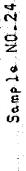


Fig. III-3-9.22 Spectrum of phase & Magnitude (Sample No.22)

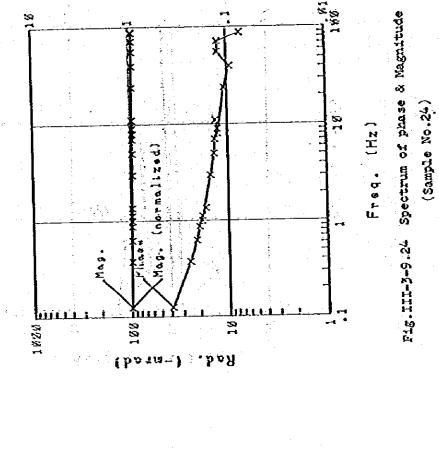
Pig. III-3-9.21 Spectrum of phase & Magnitude

Freq. (Hz)

(Sample No.21)

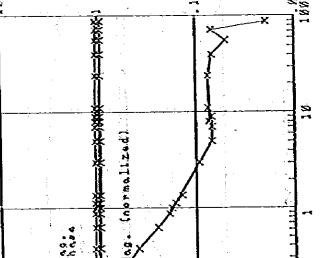


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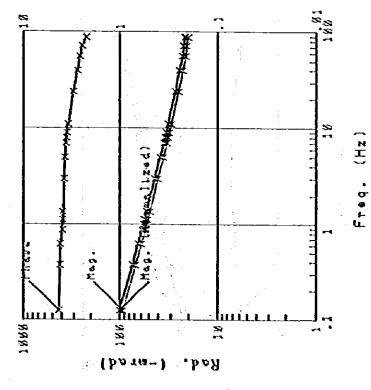


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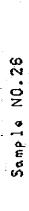
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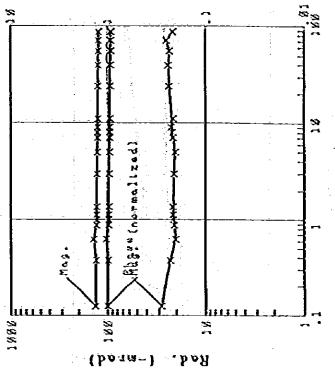
Freq. (Hz)
Fig.III-7-9.23 Spectrum of phase & Magnitude (Sample No.23)





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Pig. III-3-9.26 Spectrum of phase & Magnitude

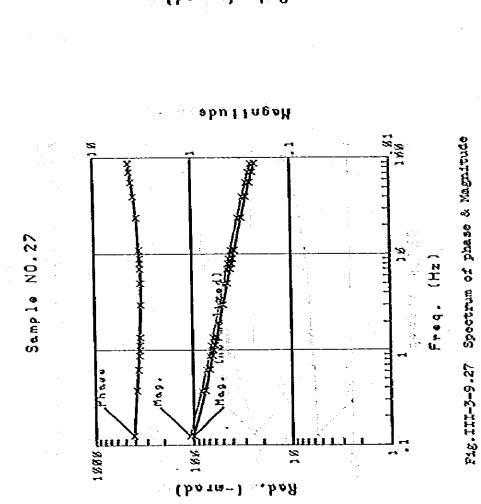
Fig. III-3-9.25 Spectrum of phase & Magnitude

(Sample No.25)

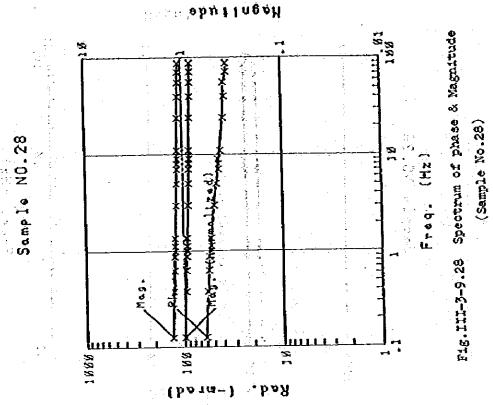
Freq. (Hz)

(Sample No.26)

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(Sample No.27)



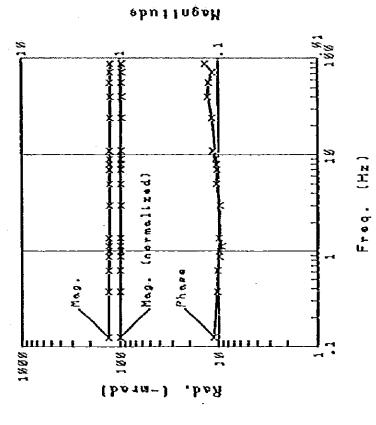


Fig.III-3-9.29 Spectrum of phase & Magnitude (Sample No.29)



The resistivity (0.125 Hz), phase (0.125 Hz), 3 point decoupled phase, and PFE (0.125 - 1 Hz), are classified of these four types in Table III-3-2. The mean values in this table were obtained by excluding the maximum and minimum values. Resistivity in the table is shown when the frequencies were at 0.125 Hz:

Table III-3-2 Classification of Phase Spectrum

	Туре	Maximum	Minimum	Average
	·A	2,650	45.3	356
Resistivity	В	2,370	414	876
(Ω-a)	С	6,360	644	1,870
e de la Seconda	D	24,300	1,840	4,710
	A - 5	436	10.5	172
Phase	В	27.2	9.50	20.8
(-arad)	С	28.0	6.17	15.8
	D	28.3	4.90	11.7
	A	466	13.4	175
3 point	В	30.4	11.3	22.6
decoupled phase	С	31.9	6.0	16.5
(-arad)	D	24.7	4.87	11.7
	A	75.3	0.82	22.5
PFE	В	3.07	0.92	1.99
(%) (0.1 - 1.0 Hz)	C	2.99	0.73	1.82
(3.1	D	4.47	0.59	1.52

The Type A rocks show the lowest resistivity, then come B, C, and D, the reason for the low resistivity of the Type A rock is the presence of large amounts of disseminated pyrite. The phase (0.125 Hz), 3 point decoupled phase, and PFE (0.125 - 1 Hz), a Type A spectrum shows that a large value makes a big difference to the mean values of the B, C and D Types. A conclusion from these facts assumes that if ore or pyrite dissemination exists, the resistivity value becomes approximately  $300 \sim 400 \,\Omega$ -meters, and the phase spectrum decreases as the frequency increases, this is what was observed with the Type A.

When samples with phase spectrum characteristics of a Type A (10 samples), and Type B (6 samples), were examined with the naked eye, they were seen to contain a large quantity of pyrite. There are no differences of the spectra,

between the samples which contain galena, and zinc-blend (sample numbers 13, 14 and 15) and those samples containing pyrite dissemination only. This is because sample number 13, 14 and 15 also contain quite a bit of pyrite. The difference between the spectra of the samples containing pyrite dissemination and banded pyrite ore is as follows; if there is a large amount of pyrite, then it is a Type A rock, if it is low, then it is a Type B or C.

### 3-4 THE ANALYSIS METHOD

Topographic and calibration corrections were applied to the field data, then section, plane and spectrum diagrams were drawn, and the results analyzed for IP anormalies, as follows;

- (1) Plane and section map of apparent resistivity (0.125 Hz).
- (2) Plane and section map of PFE (0.125 1 Hz, and 0.375 3 Hz).
- (3) Section diagram of Phase (15 frequencies).
- (4) Cole-Cole diagram.
- (5) Phase spectral response diagram.
- (6) Magnitude spectral response diagram.
- (7) Three point decoupled phase diagram.

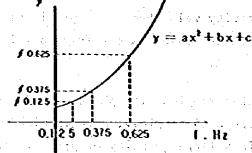
Ordinary method of analyses were used for (1) and (2), as these are the same kind of apparent resistivity and PFE by the conventional IP method. The (3 ~ 7) are the special case of spectral IP, and can be identified through their abnormal spectral response.

The (7) is the method through which we can require the phase in direct current, using 0.125, 0.375 and 0.625 Hz. If we assume that frequency and phase have quadratic relationship, and let phase ( $\phi$ ) be an ordinate, frequency (f) be an abscissa, it then becomes a quadratic function  $y = ax^2 + bx + C$ , this "C" is the phase which can become a frequency close to a direct current, and it is called the three point decoupled phase. To solve "C", 0.125, 0375 and 0.625 Hz are put in for frequency (x), and phase (y) becomes  $\phi_{2.125}$ ,  $\phi_{3.375}$ ,  $\phi_{3.575}$ ,  $\phi_{3.625}$ .

#### where:

 $\phi_{0.125} = a(0.125)^2 + b(0.125) + C$  $\phi_{0.375} = a(0.375)^2 + b(0.375) + C$ 

 $\phi_{0.625} = a(0.625)^2 + b(0.625) + C$ 



From this, "C" can be driven by the following equation.

$$C = \frac{15}{8} \phi_{0.125} - \frac{10}{8} \phi_{0.375} + \frac{3}{8} \phi_{0.625}$$

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## CHAPTER 4 RESULTS OF INTERPRETATION AND CONSIDERATION

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#### 4-1 RESULTS OF INTERPRETATION

## 4-1-1 Cole-Cole, Phase and Magnitude Spectrums

Cole-Cole diagram was proposed by Cole and Cole in 1941 with the purpose to examine the measurement results of rock samples. The measurement results are plotted with every frequency by setting the negative out-of-phase (imaginary) on vertical axis and the positive in-phase (real) on horizontal axis (Fig. III-3-3). Frequency effect is very proportional to in-phase, while phase angle is proporitional to out-of-phase.

Cole-Cole diagram is expressed on the sections of survey lines A ~ I and is shown in Figure III-4-1. Cole-Cole diagram generally shows a simple ascent to the left; however, in south of survey lines G ~ I, there is small out-of-phase with small anomaly. Southern end of survey lines A ~ P with no IP phenomenon shows perpendicular pattern, and northern part of survey lines indicates the pattern of the ascent to the left.

Concerning the phase spectral, steady increase caused by electro magnetic coupling can be seen at high frequency range (harmonic of 8 Hz), and some patterns reflecting characteristics of the anomaly source can be seen at low resistivity range (harmonic of 0.125 Hz).

First one of the patterns is the anomaly which is recognized at n = 3 ~ 5 at northern end of survey lines A, B, D and E. There is the anomaly of flat and of more than -50 milliradian at harmonic of 0.125 Hz. This can be considered as the effect of disseminated sulfide.

Second one of characteristic patterns is the V-shape spectral in the center of survey line C. This spectral is the one whose harmonic of 0.125 Hz decreases as frequency increases. This type of spectral can be observed at survey lines B and D. This anomaly has the value of less than -40 milliradian at 0.125 Hz is not much remarkable than the above-mentioned one. This pattern is normally seen for big mineral grain size. For a case as this, it is probably caused by massive sulfide.

Furthermore, as for the third pattern, there is steady increasing spectral with the ascent to the right as seen at southern end of survey line A, where there is anomaly caused only by electro magnetic coupling without any phase in low frequency range.

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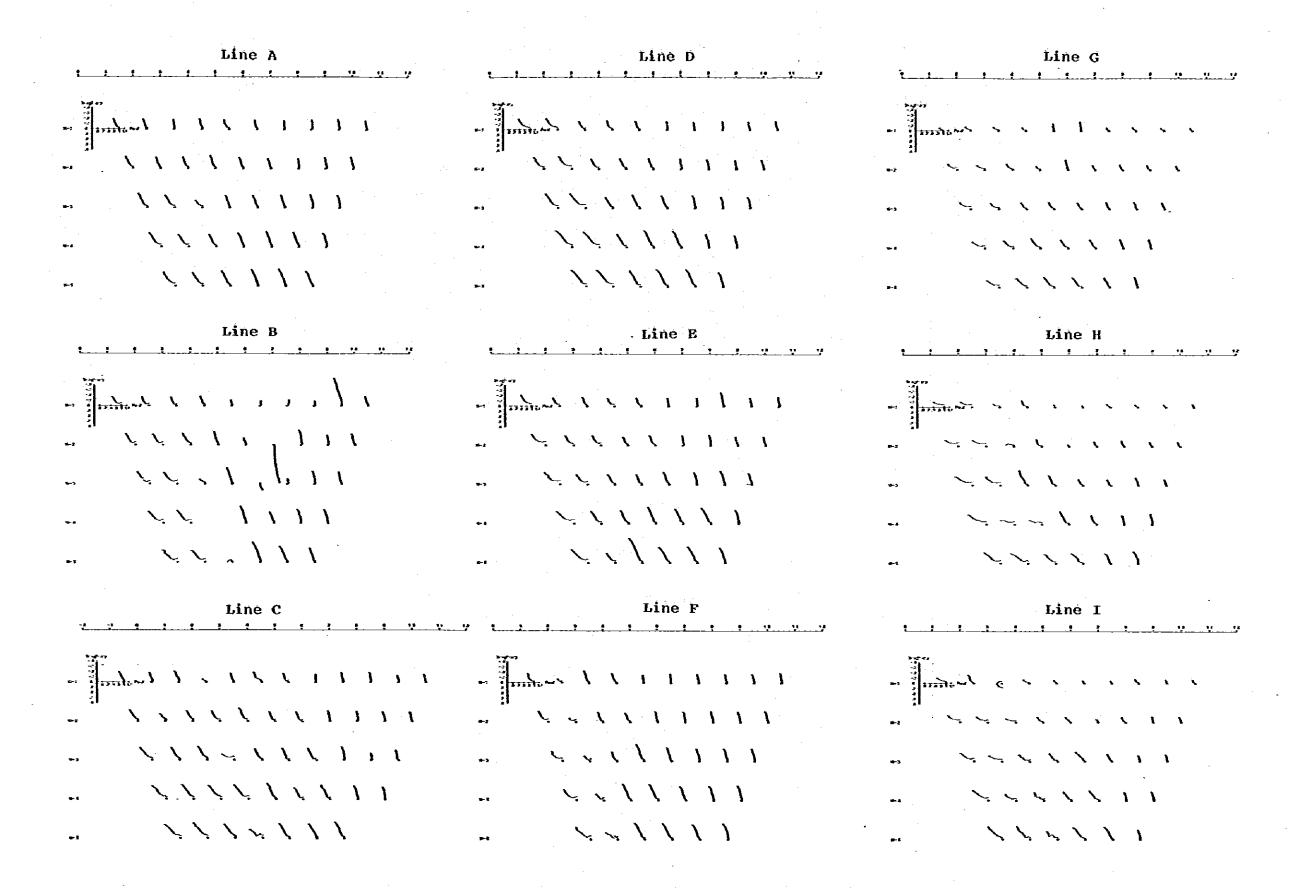
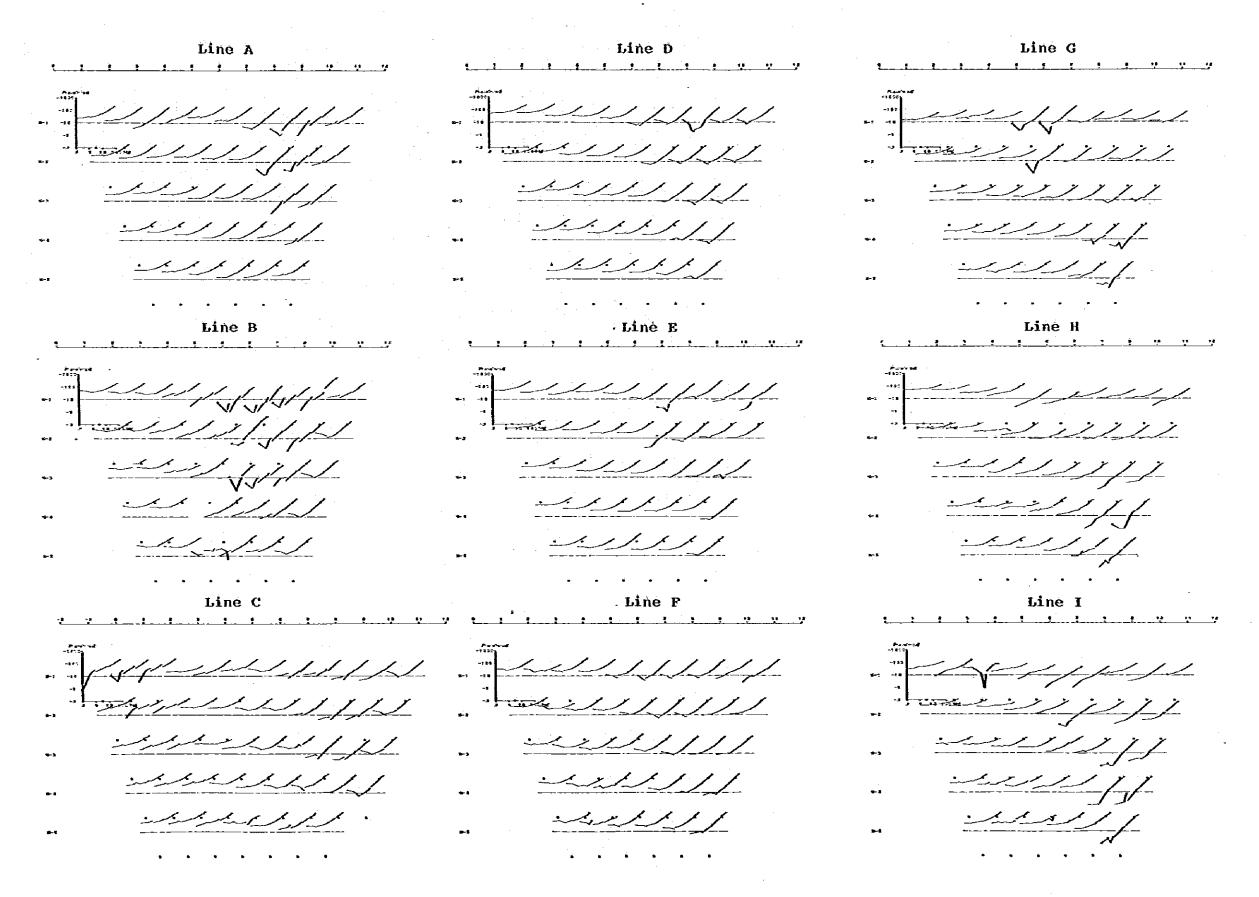


Fig. III-4-1 Cole-Cole Diagram



Pig. III-4-2 Phase Spectrum

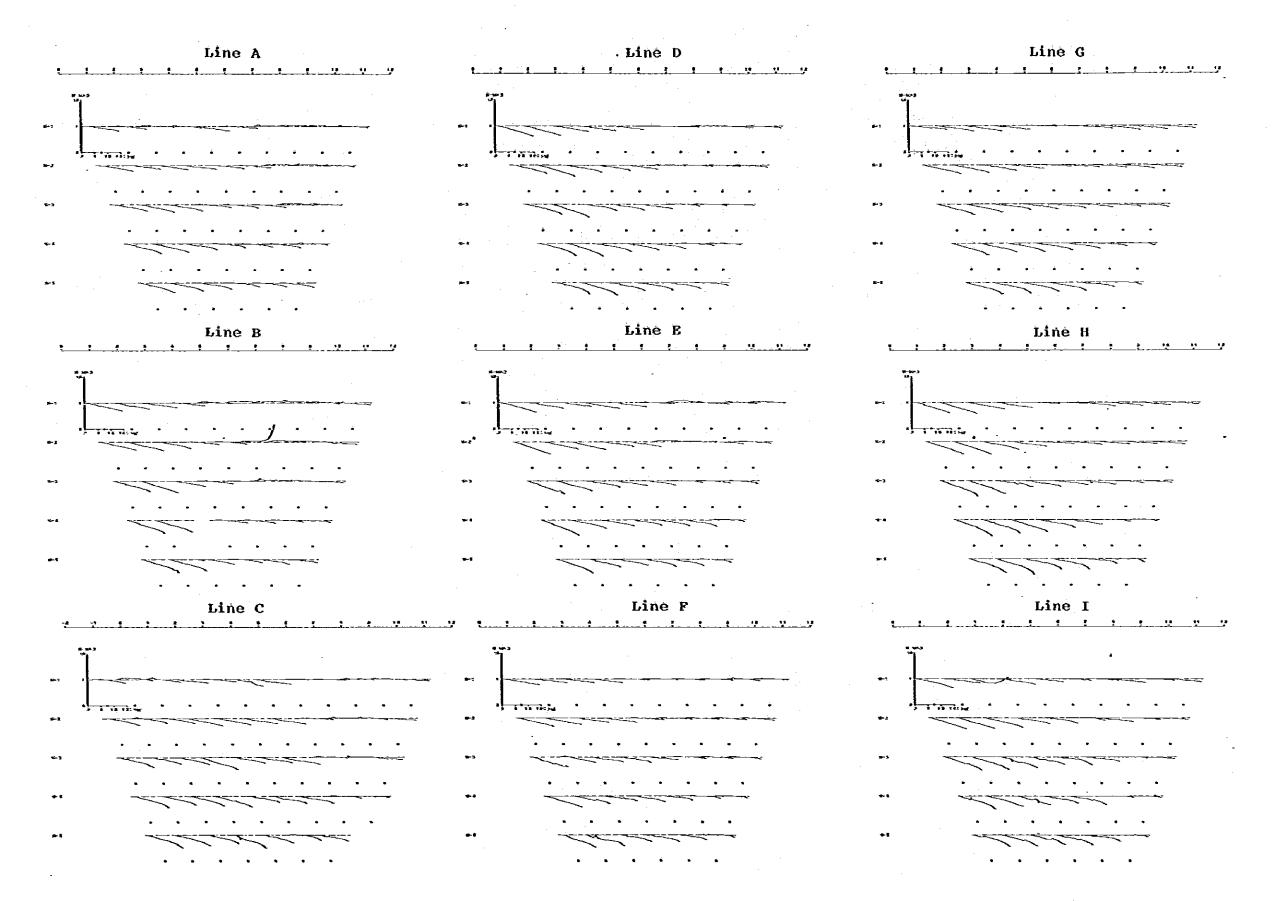


Fig. III-4-3 Magnitude Spectrum

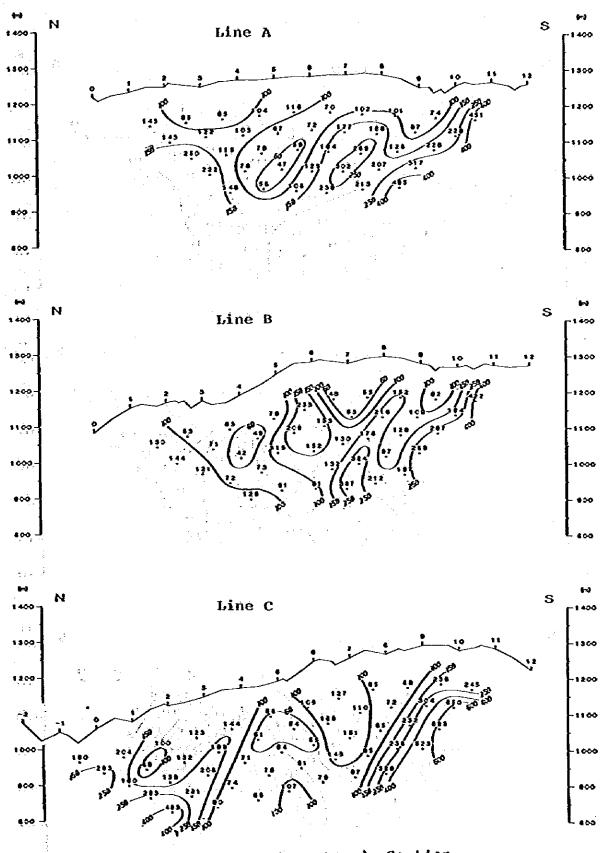


Fig. III-5-1.1 Spectral IP Pseudo-Section
Apparent Resistivity (Line A, B, C)

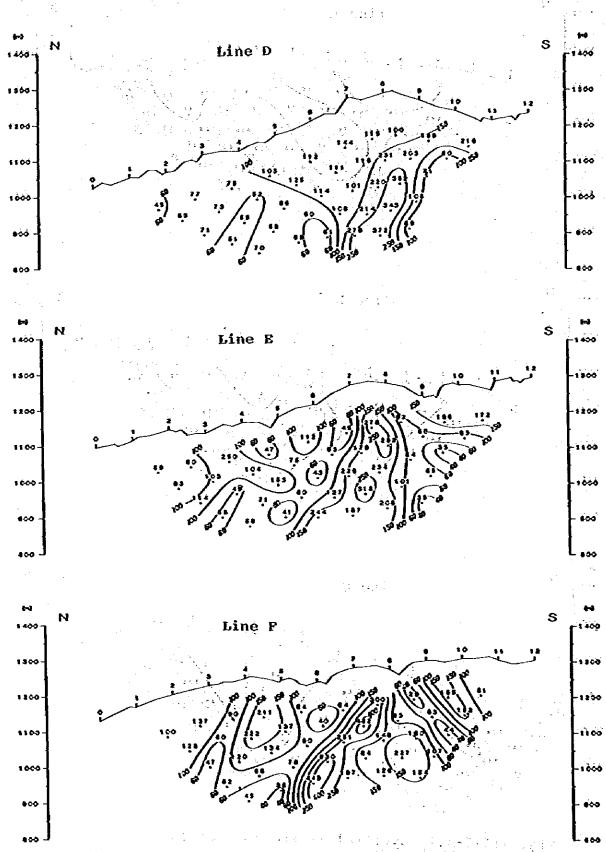


Fig. III-5-1.2 Spectral IP Pseudo-Section
Apparent Resistivity (Line D, E, F)

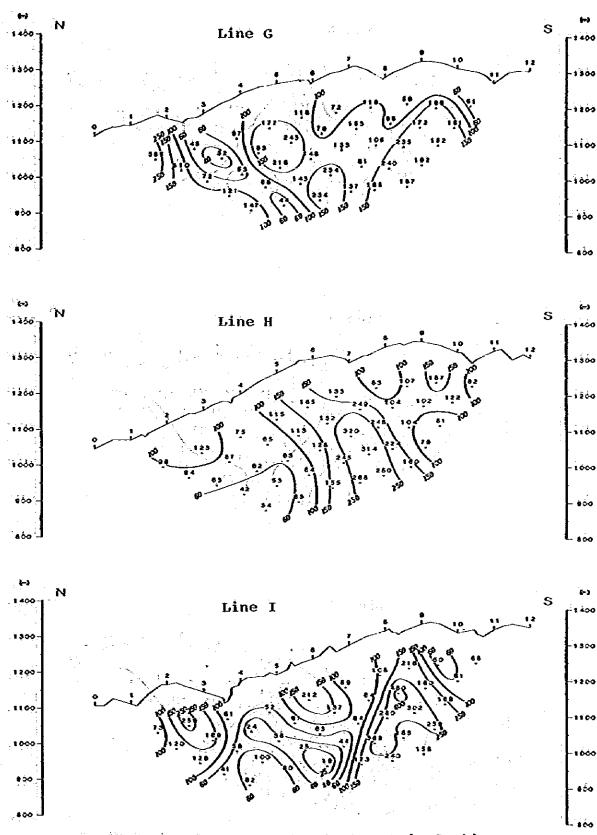


Fig. 111-5-1.3 Spectral IP Pseudo-Section

Apparent Resistivity (Line G. H. I)

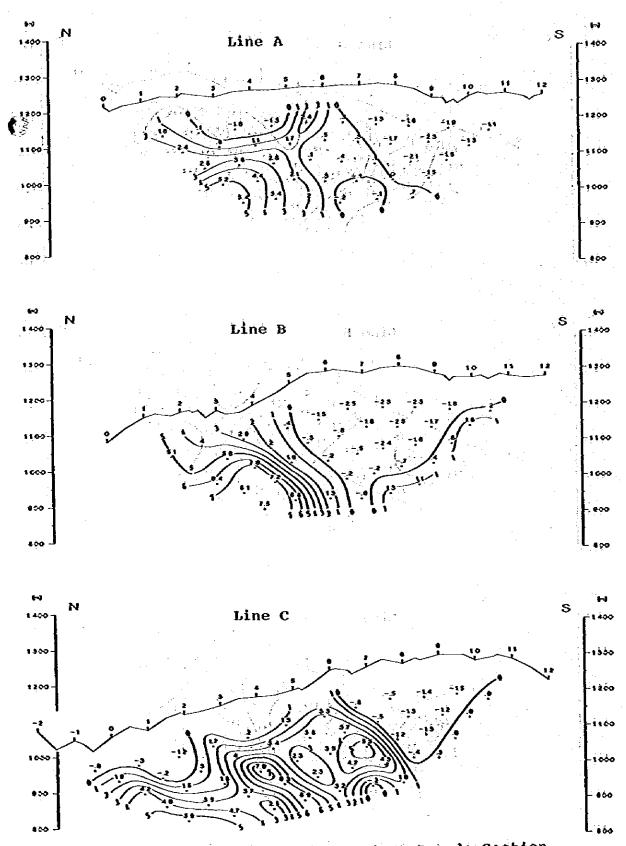


Fig. 111-6-1.1 Spectral IP Pseudo-Section Percent Predency Effect [0.125 ~ 1.0 Hz] (Line A, B, C)

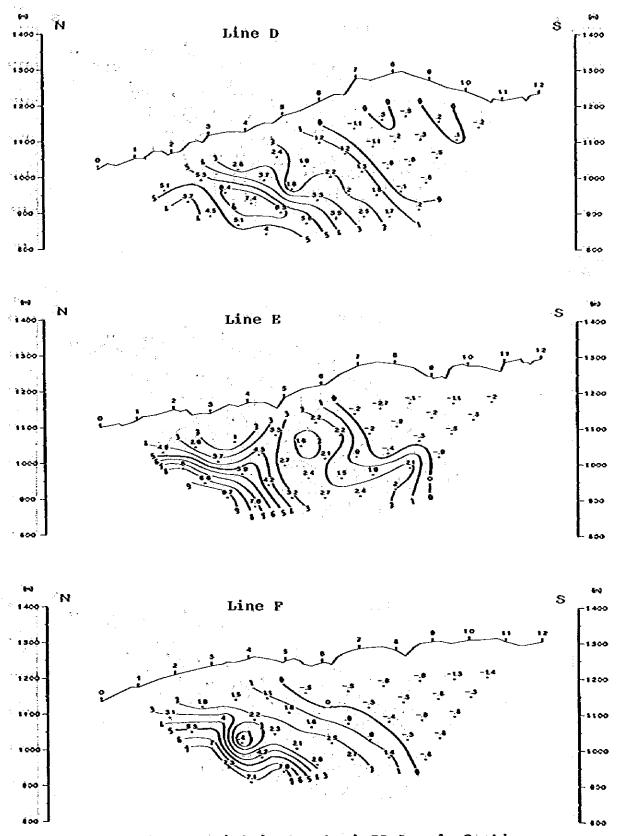


Fig. III-6-1.2 Spectral IP Pseudo-Section Percent Pregency Effect [0.125 ~ 1.0 Hz] (Line D, E, F)

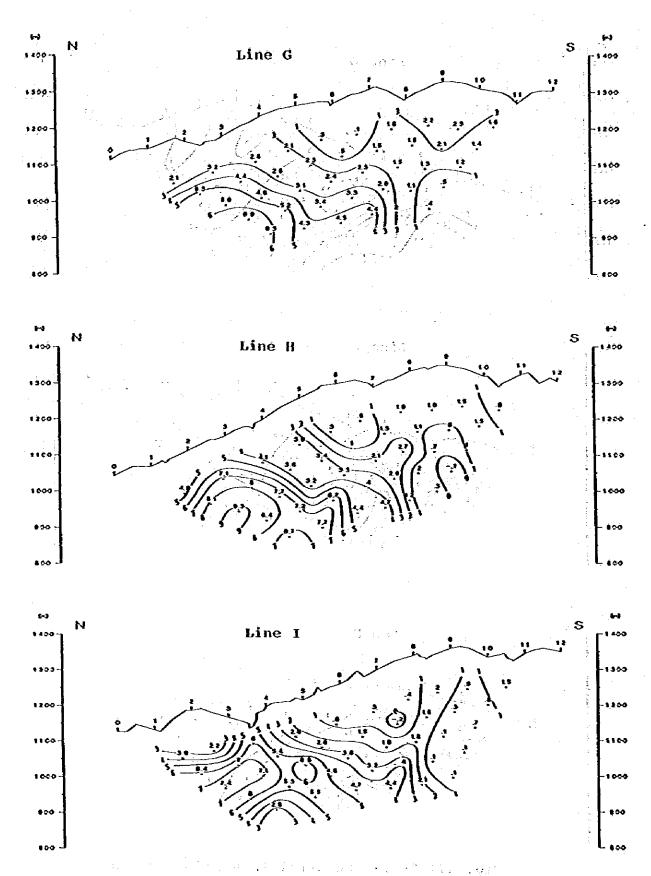


Fig. III-6-1.3 Spectral IP Pseudo-Section Percent Frequency Effect [0.125 ~ 1.0 Hz] (Line G, H, I)

Magnitude Spectral is normalized at 0.125 Hz and its magnitude decreases as frequency increases. It shows the pattern with descent to the right when IP effect is large. This kind of pattern seen in northern half of every survey line has the same significance with one of the Cole-Cole diagram ascending to the left; that means, in-phase decreases (frequency effect increases) as the frequency increases.

## 4-1-2 Apparent Resistivity

The geographical effects are accumulated in measured apparent resistivity. In order to remove them, two dimensional topographic correction was carried out by means of the computer with finite element method (Fig. II-5-1.1 - 1.3).

The correction is effective when the survey lines (such as A, D and so on) intersect at the right angle with topographic contour and/or when two dimensional geological change has taken its place. However, the correction may not be able to cover all of the effects along the mountain ridge (like as survey line F). For such case, distribution of resistivity is qualitatively considered by examining the surrounding topography.

Resistivity of this area generally shows low value of change within 40  $^{\circ}$  200  $\Omega$ -m. As for resistivity change, it is understood that value with less than 100  $\Omega$ -m is as the low resistivity zone, and one with more than 200  $\Omega$ -m as high resistivity zone. Especially low resistivity shown at center part of survey line C with some outcrops around No. 5 shows the same anomaly zone with IP anomaly. Furthermore, high resistivity is shown at non-altered andesite dike and limestone.

It is needed to pay attention for spectral IP since the coupling phenomenon occurs in the area with low resistivity. By the calculation of electro magnetic coupling against two-layered structure model, phase change of 10  $\Omega$ -m with 10 m thickness of overburden and 100  $\Omega$ -m 2nd-layered models shows a value of -1 ~ -200 milliradian.

## 4-1-3 Frequency Effect

Besides 0.125 - 1 Hz frequency effect, 0.375 - 3 Hz frequency effect, which is the closest frequency effect to the conventional IP method, is calculated and shown as pseudo-section in Fig. III-6-1 - Fig. III-6-6. Both 0.125 - 1 Hz and 0.375 - 3 Hz FE show the same anomaly pattern with no predominant differences.

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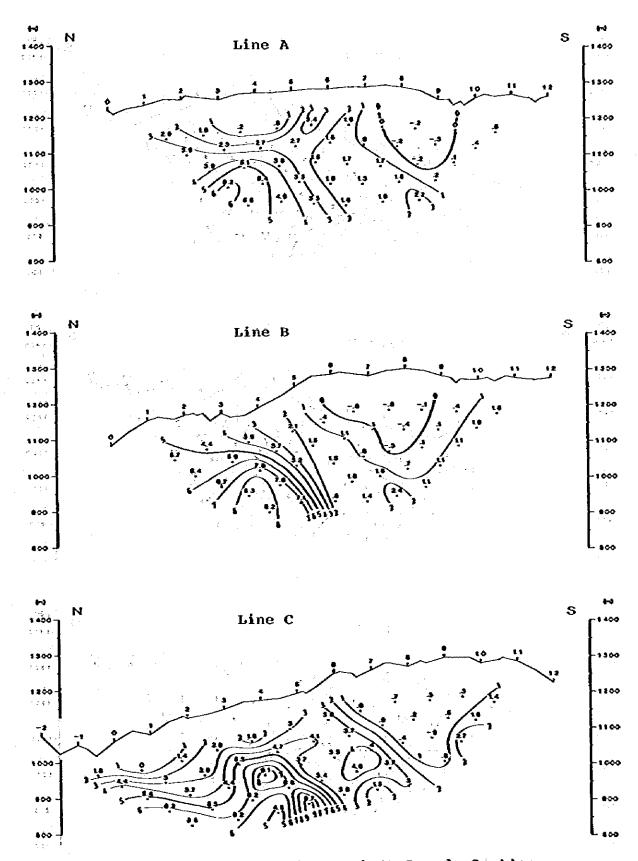


Fig. III-6-2.1 Spectral IP Pseudo-Section
Percent Prequency Effect (0.375 % 3.0 Hz) (Line A, B, C)

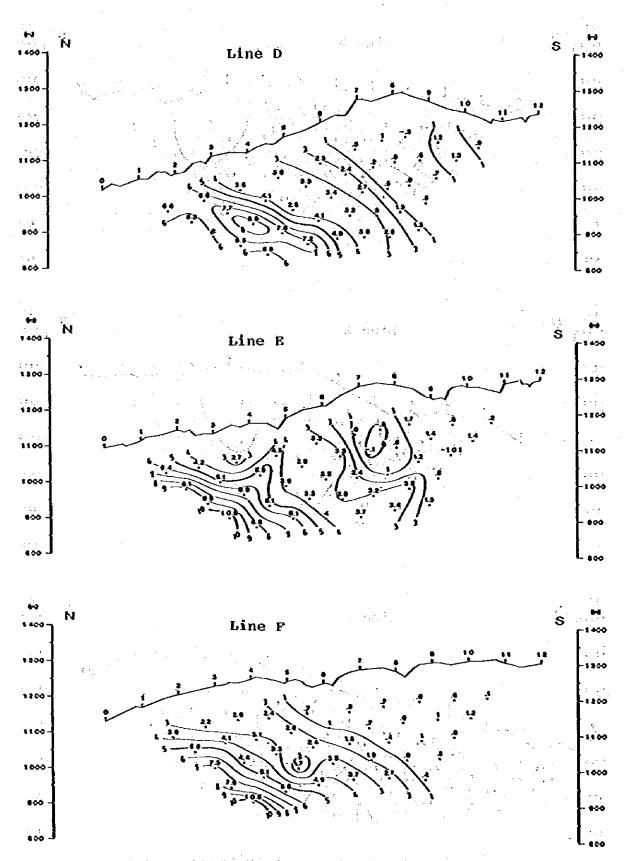


Fig. III-6-2.2 Spectral IP Pseudo-Section Percent Frequency Effect [0.375 \ 3.0 Hz] (Line D, B, F)

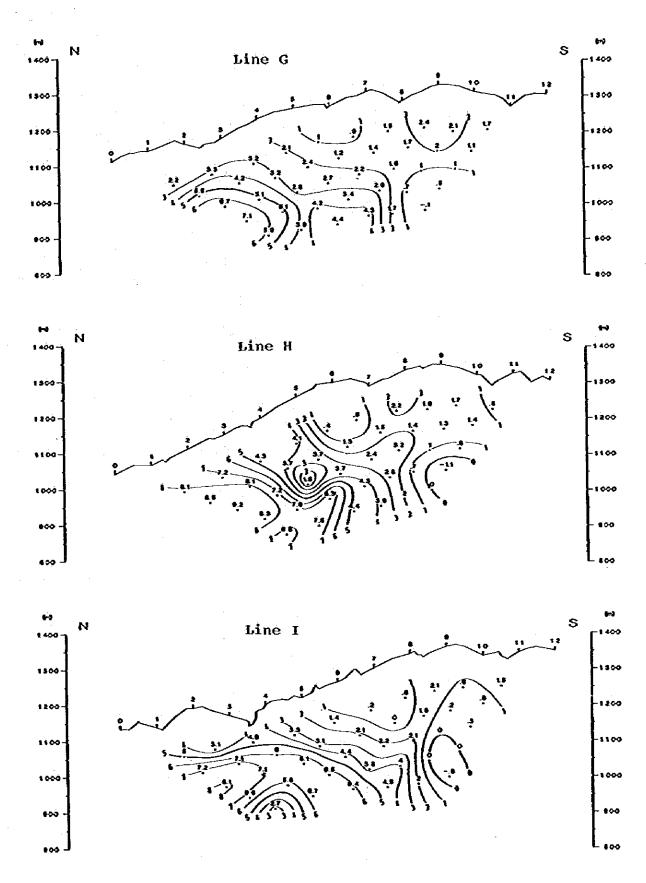


Fig. III-6-2.3 Spectral IP Pseudo-Section Percent Frequency Effect [0.375 & 3.0 Hz] (Line G. H. I)

Moreover, these anomalies shows good correlation with phase. Taking the correlation between phase and FE with total of 54 pairs of IP anomalies for A  $\sim$  P sections, they show the arrangement as shown in Fig. III-6-3, and its coefficient of correlation is calculated as  $\gamma = 0.945$ .

FE of each survey line indicates anomalous zone if more than 3% is anomalous. (This is equivalent to phase anomaly with value of more than -30 milliradian)

Northern end of survey line A at around 200 m deep has 3 ~ 6% of anomatous source. There is shallower anomatous source for survey line B.

About survey line C, FE anomalies are detected in the wide range. Especially the anomaly of the south dipping source of more than 4% caused by anomalous source, spreading from No. 5 ~ 6, is considered to be due to the effect of massive sulfide even though its value of anomalies are less than the ones detected at the northern end of the line.

Generally FE anomaly of

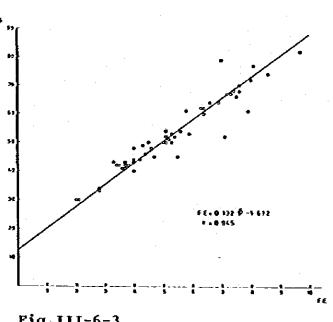


Fig.III-6-3
Correlation of Phase (\$) & PFE

the disseminated sulfide is normally larger than that of the massive sulfide, but it is needed to note that the strong IP anomaly might be caused by pyrite for some of the cases.

Anomaly zone at the northern end of survey lines D, E, P and G successive—
ly distributes toward East-West with gentle south dipping. It is understood
as that disseminated sulfide is latent in souther side of the boundary of
andesite and sedimentary rocks.

For survey line H, this type of anomaly is recognized near the ground surface, and width of dissemination widely distributes toward north of No. 3 ~4. In addition, the biggest value of FE anomaly is 9.3% detected at deep part of No. 3.

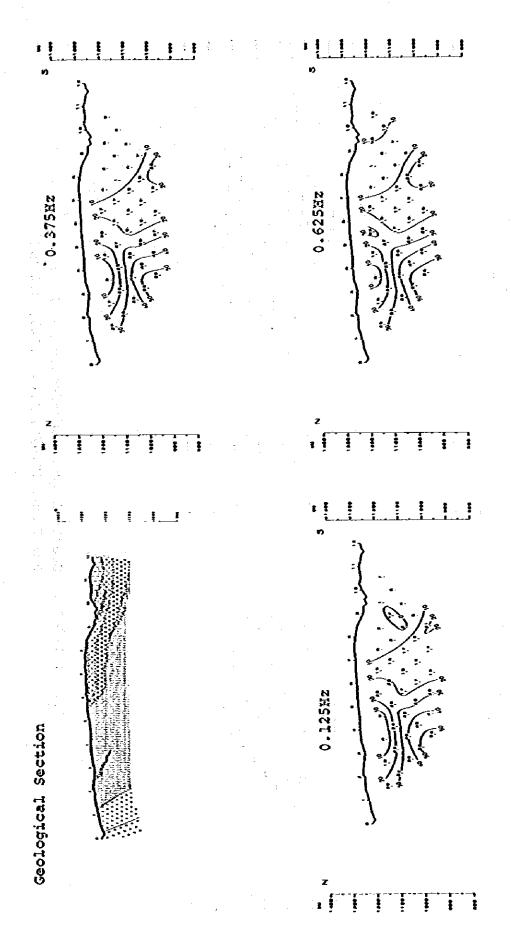


Fig. III-7-1.1 Spectral IP Pseudo-Section of Line A Raw Phase (G. Sec., 0.125, 0.375, 0.625 Hz)

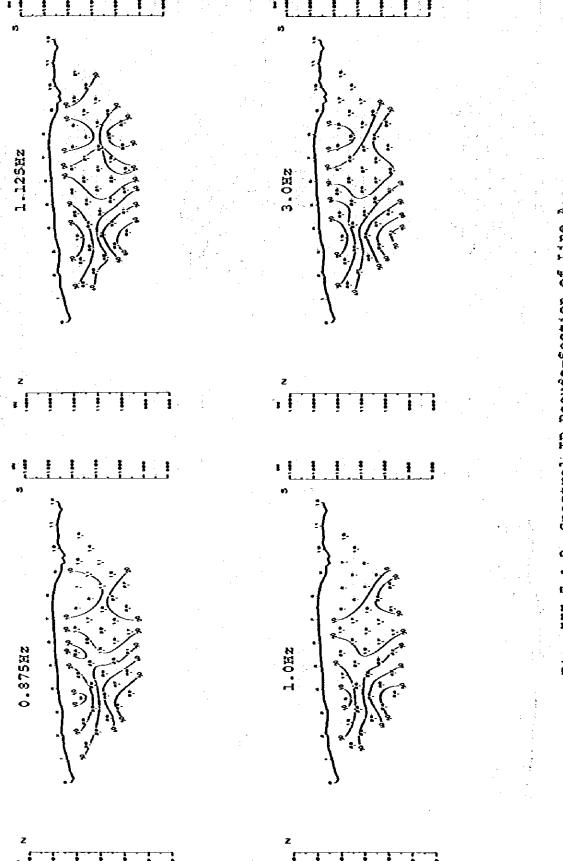


Fig. III-7-1.2 Spectral IP Pseudo-Section of Line A. Raw Phase (0.875, 1.0, 1.125, 3.0 Hz)

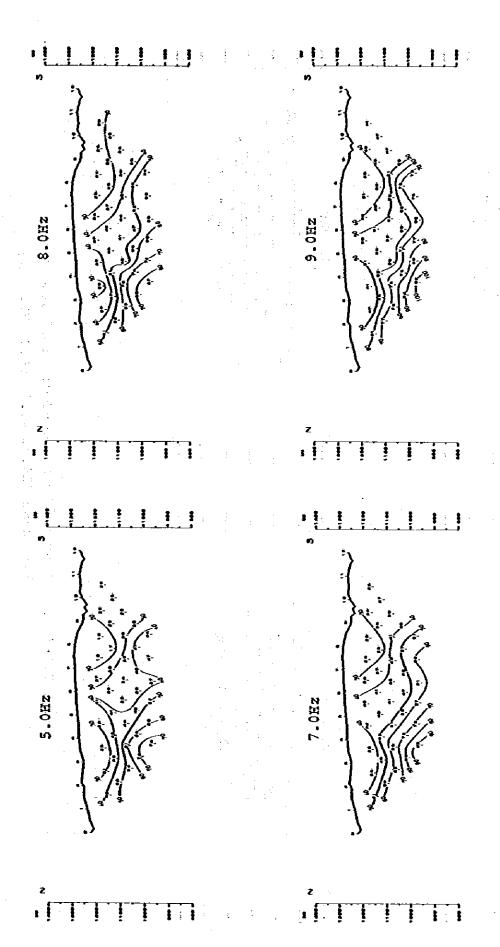
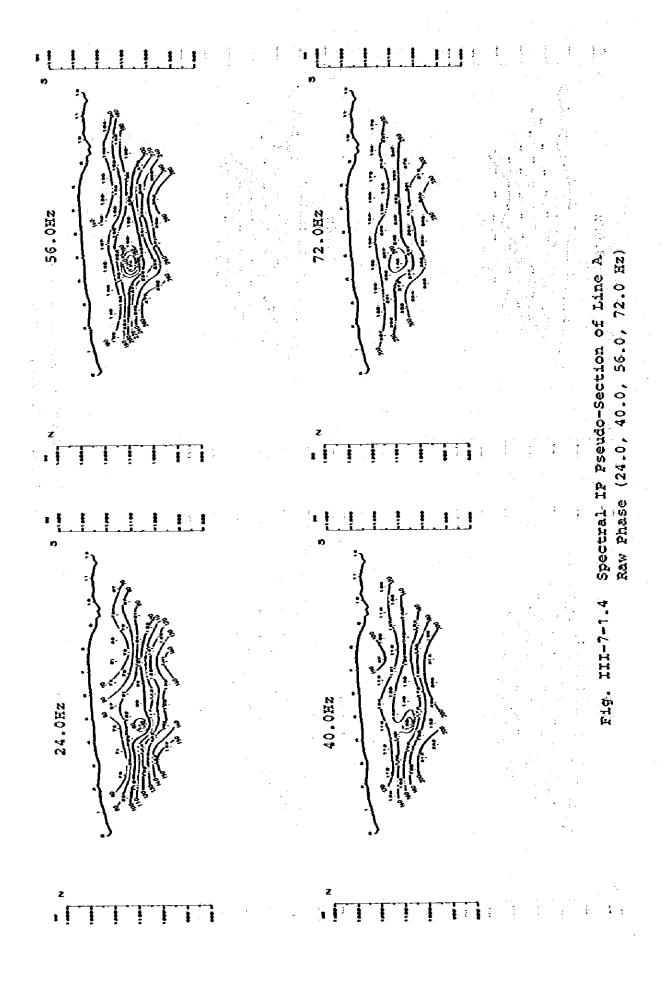
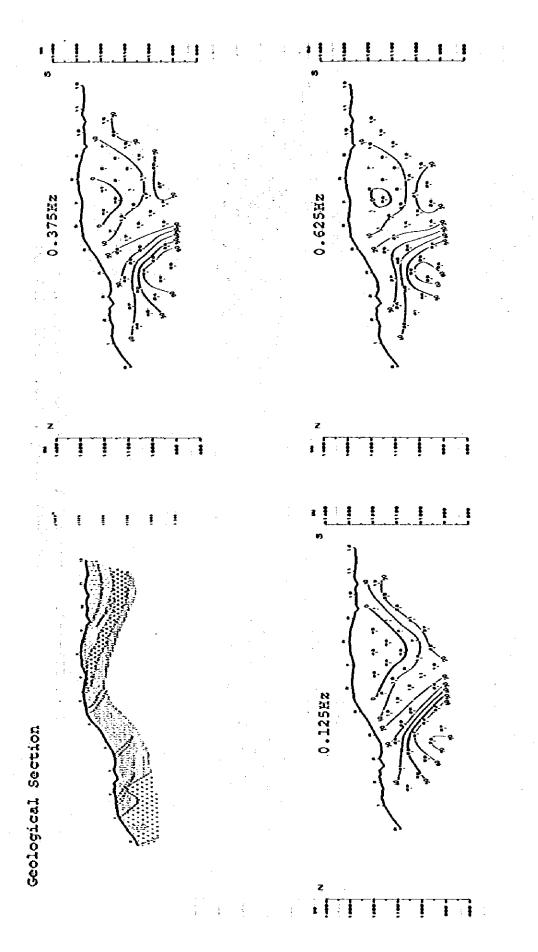


Fig. III-7-1.3 Spectral IP Pseudo-Section of Line A Raw Phase (5,0, 7.0, 8.0, 9.0 Hz)





Raw Phase (G. Sec., 0.125, 0.375, 0.625 Hz) Fig. III-7-2.1 Spectral IP Pseudo-Section of Line B

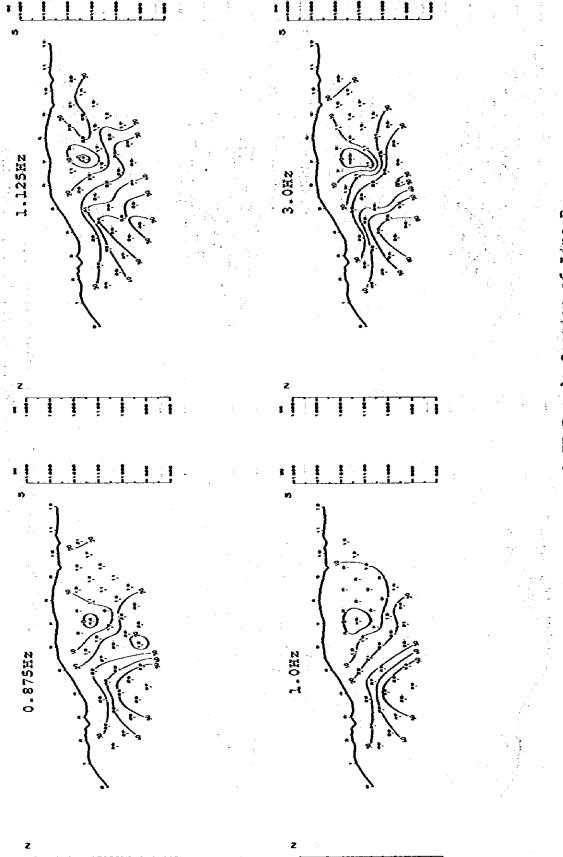
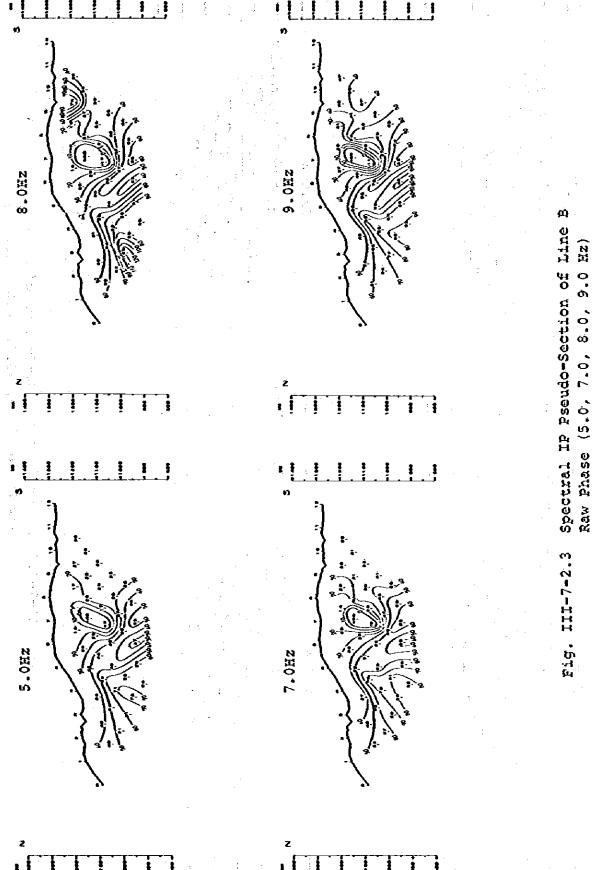
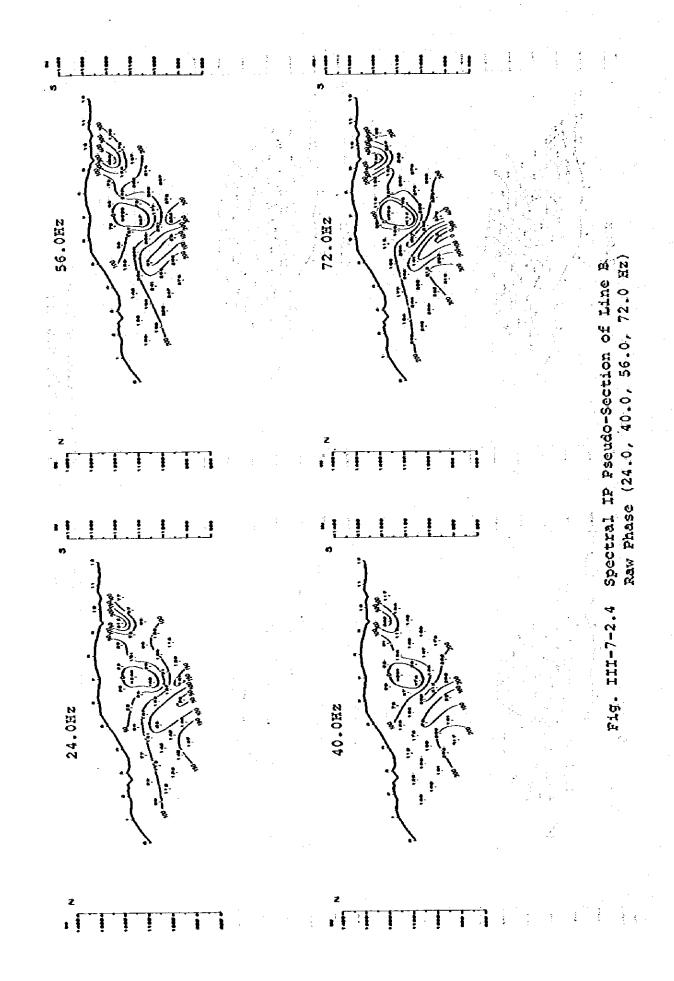


Fig. III-7-2.2 Spectral IP Pseudo-Section of Line B. Raw Phase (0.875, 1.0, 1.125, 3.0 Hz)





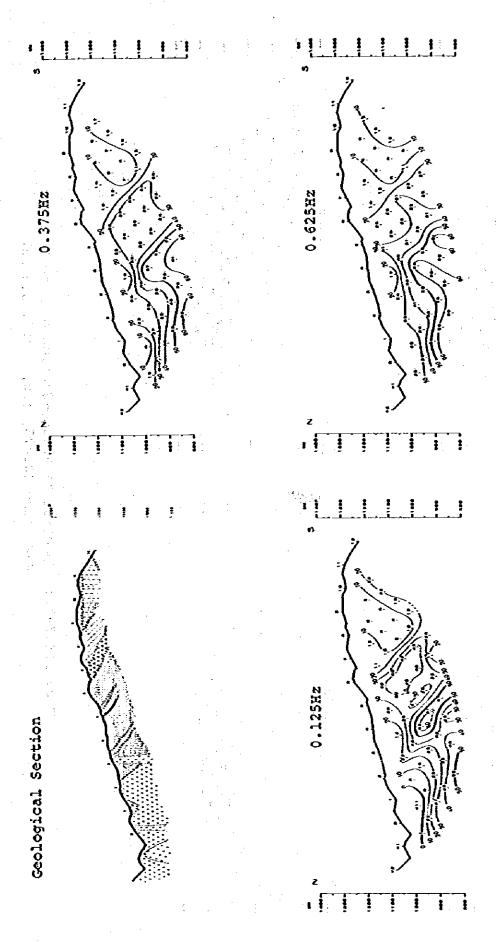
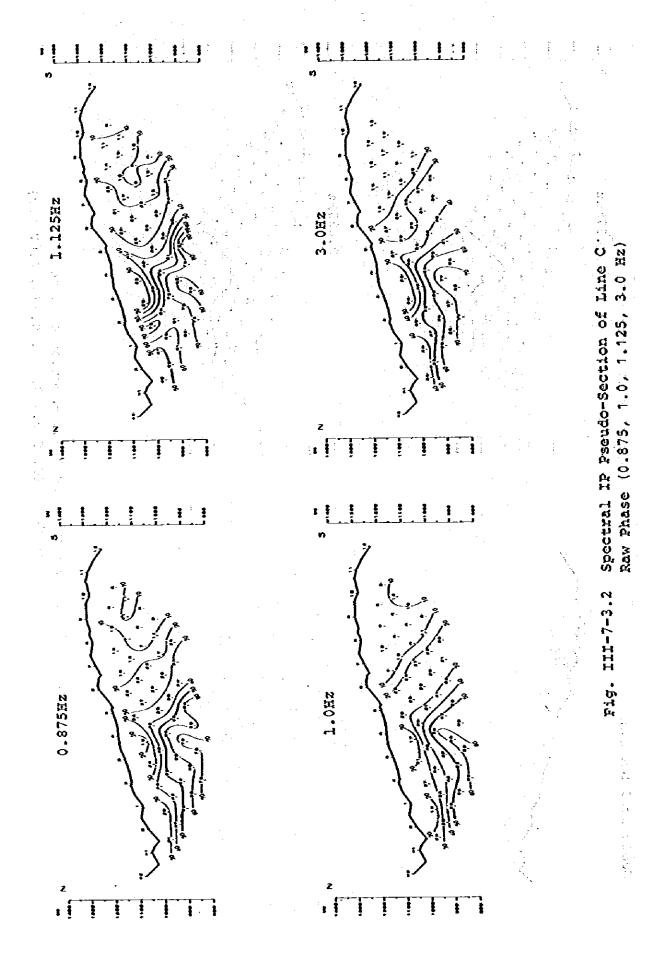


Fig. III-7-3.1 Spectral IP Pseudo-Section of Line C Raw Phase (G. Sec., 0.125, 0.375, 0.625 Hz)



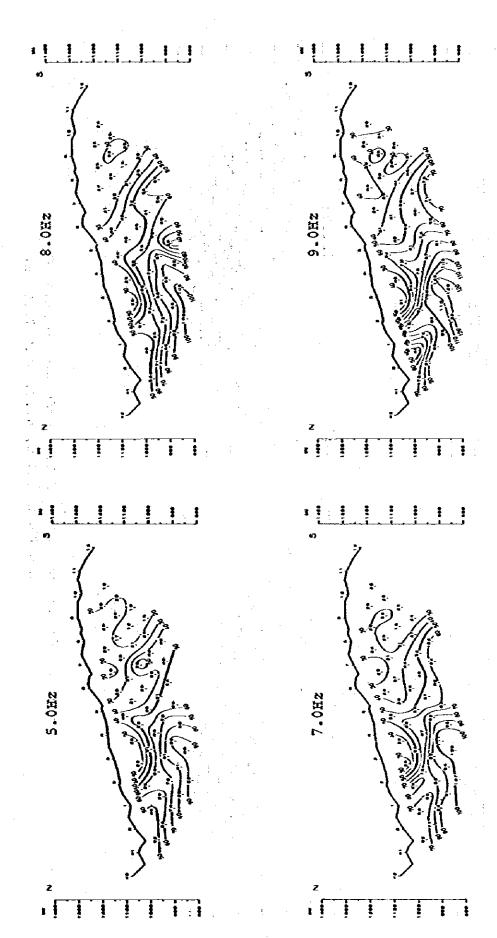
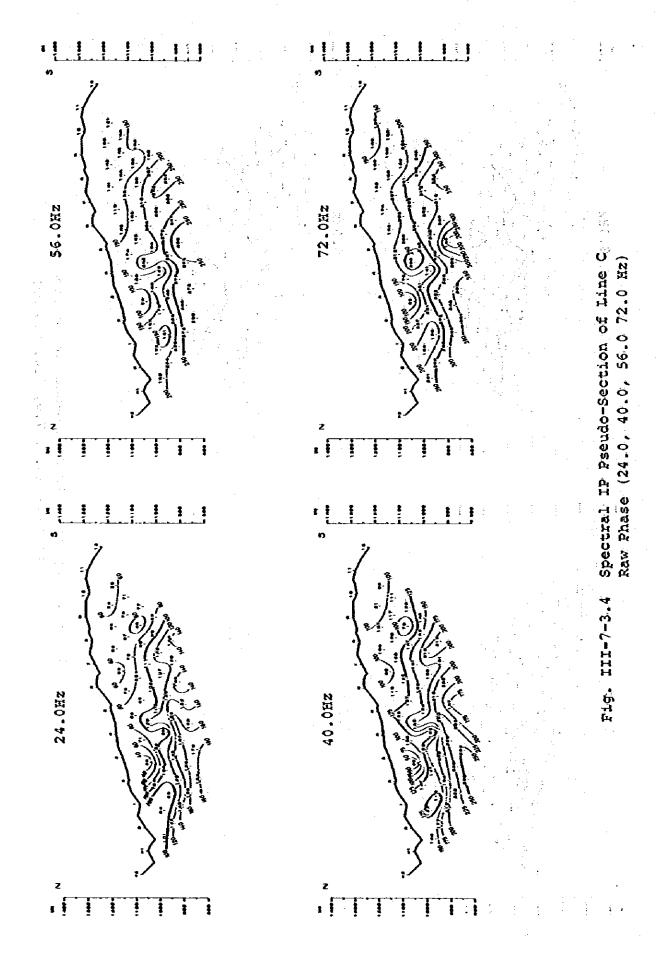


Fig. III-7-3.3 Spectral IP Pseudo-Section of Line C Raw Phase (5.0, 7.0, 8.0, 9.0 Hz)



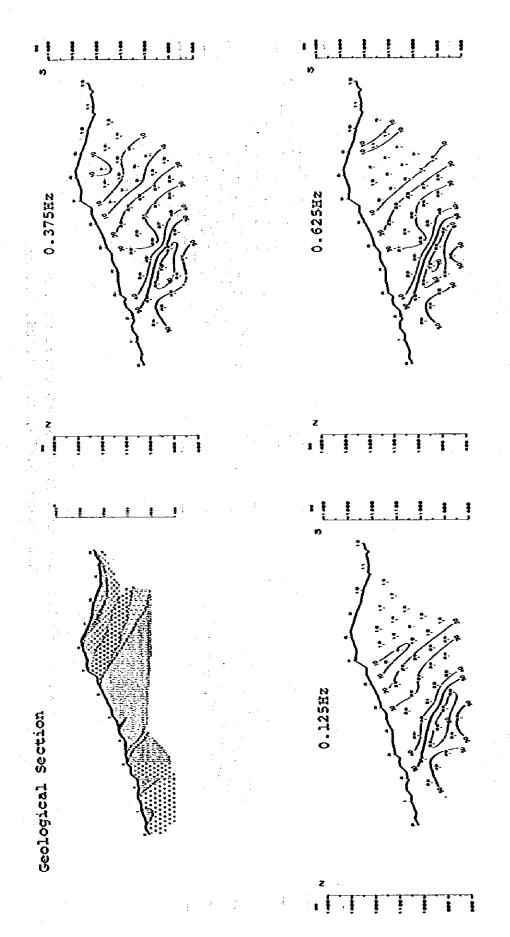


Fig. III-7-4.1 Spectral IP Pseudo-Section of Line D Raw Phase (G. Sec., 0.125, 0.375, 0.625 Hz)

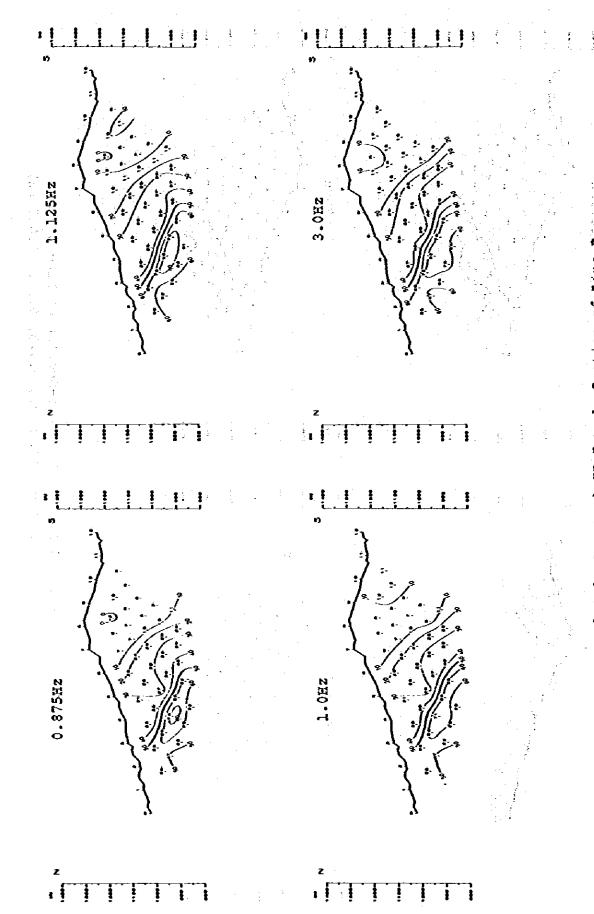


Fig. III-7-4.2 Spectral IP Pseudo-Section of Line D Raw Phase (0.875, 1.0, 1.125, 3.0 Hz)

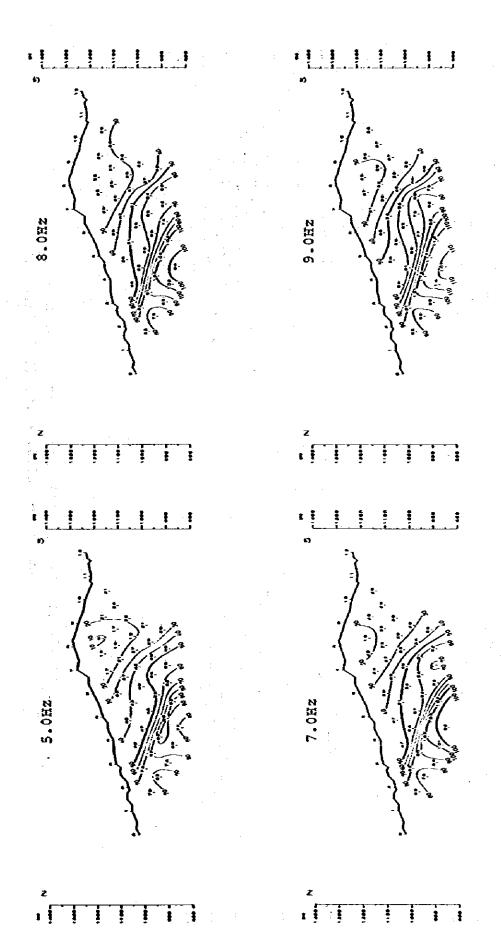
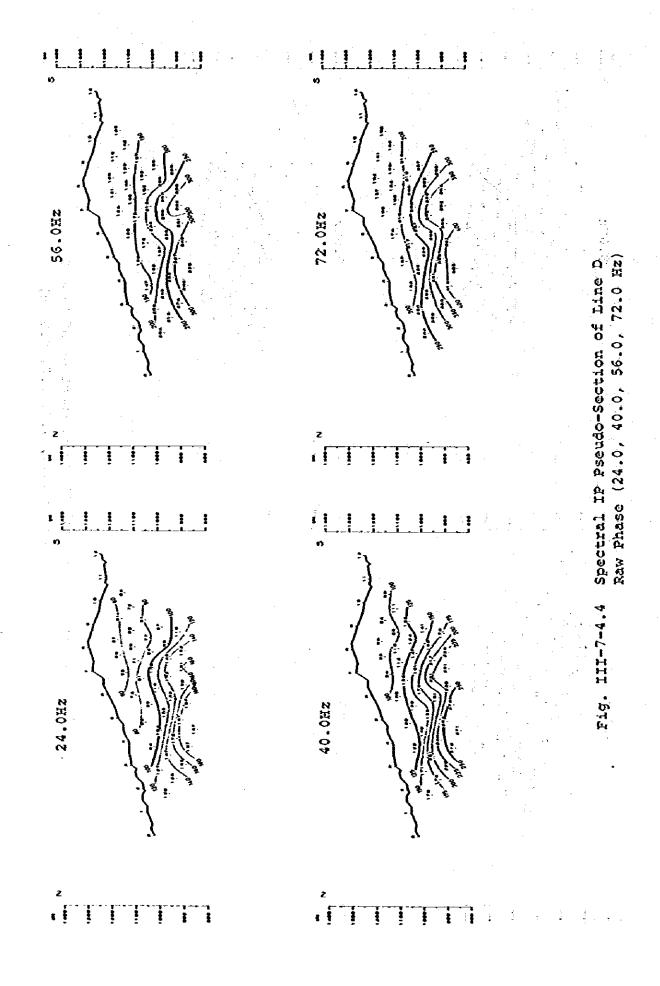


Fig. III-7-4.3 Spectral IP Pseudo-Section of Line D Raw Phase (5.0, 7.0, 8.0, 9.0 Hz)



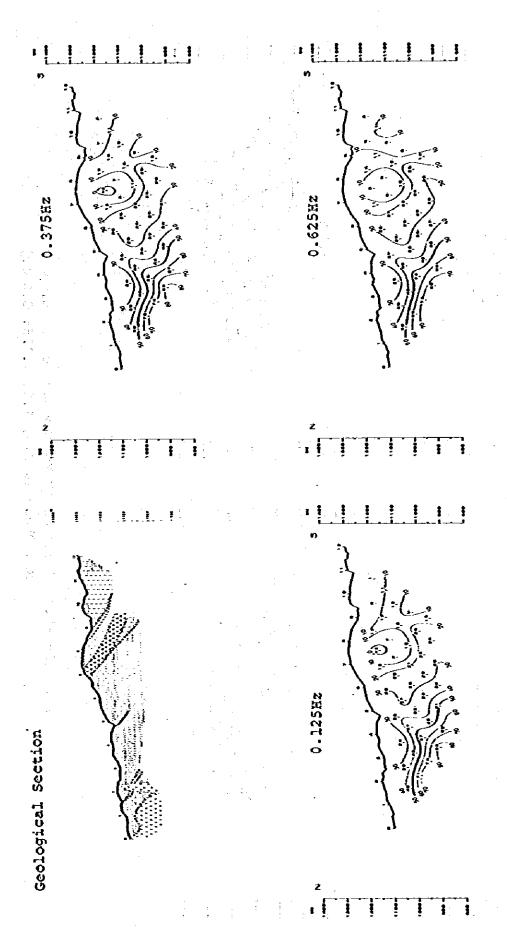


Fig. III-7-5.1 Spectral IP Pseudo-Section of Line E Raw Phase (G. Sec., 0.125, 0.375, 0.625 Hz)

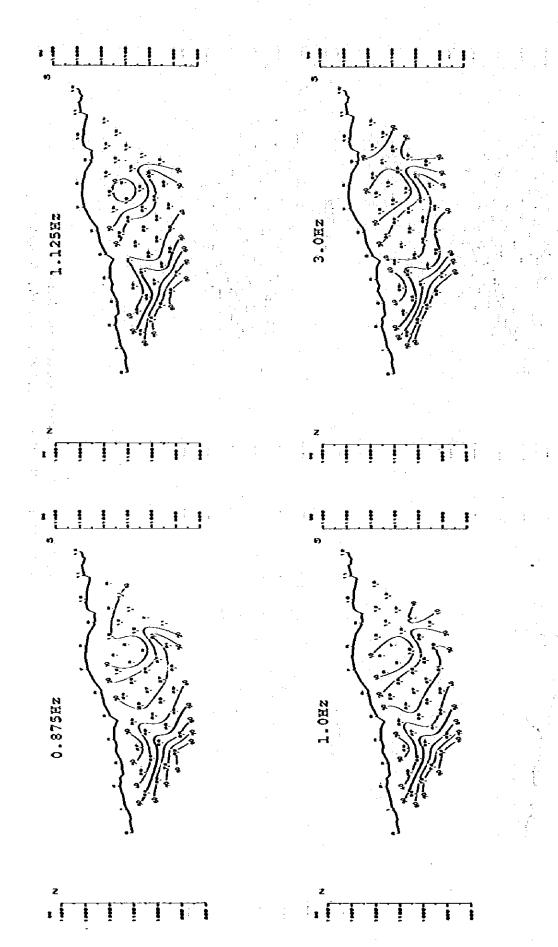


Fig. III-7-5.2 Spectral IP Pseudo-Section of Line E. Raw Phase (0.875, 1.0, 1.125, 3.0 Hz)

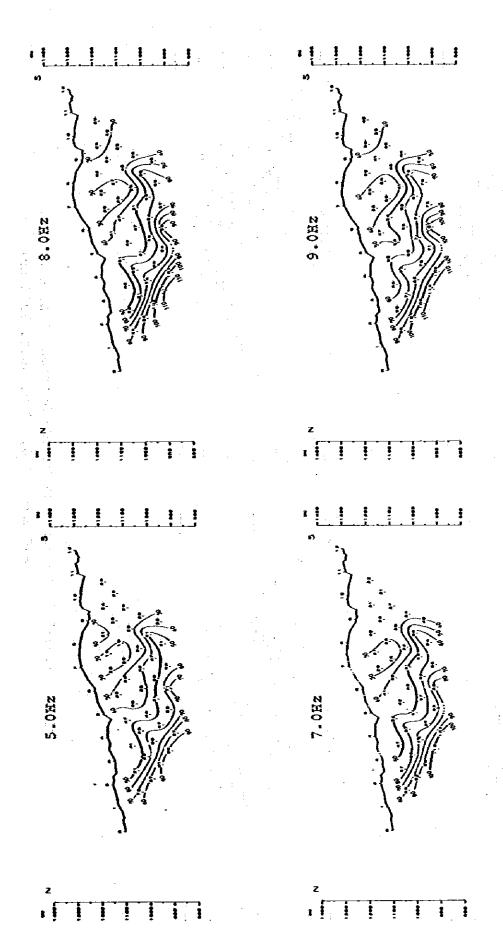
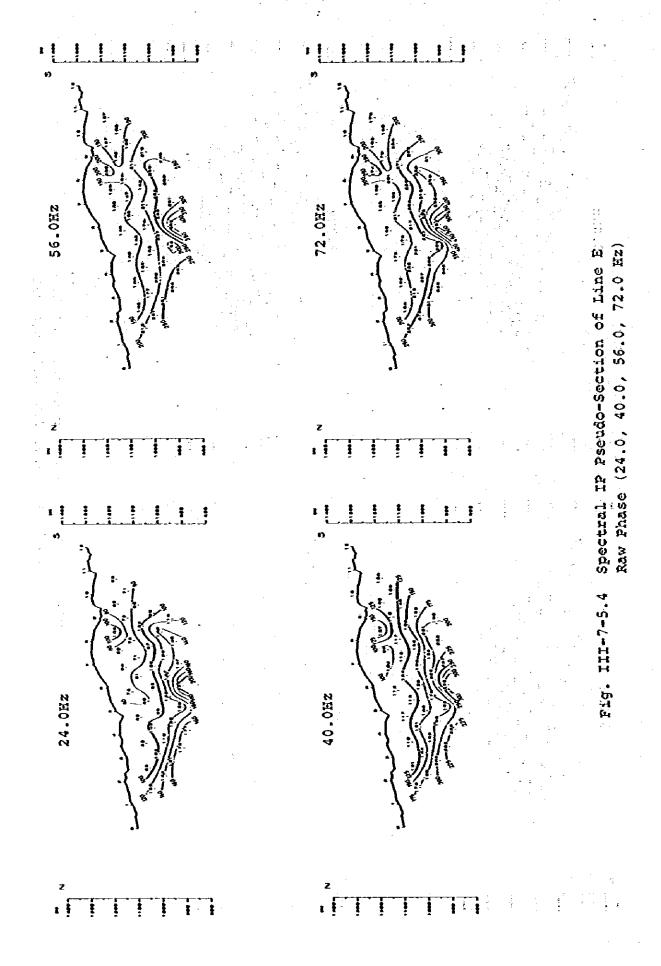


Fig. III-7-5.3 Spectral IP Pseudo-Section of Line E Raw Phase (5.0, 7.0, 8.0, 9.0 Hz)



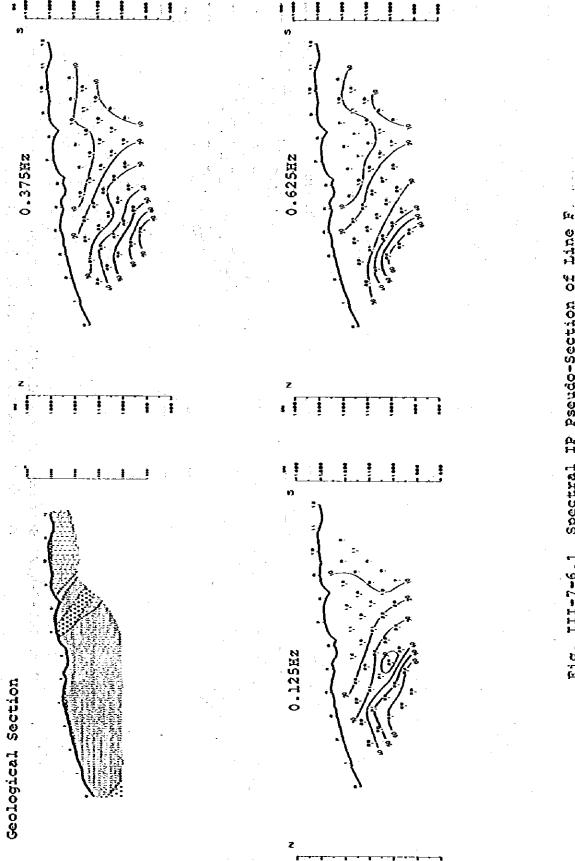
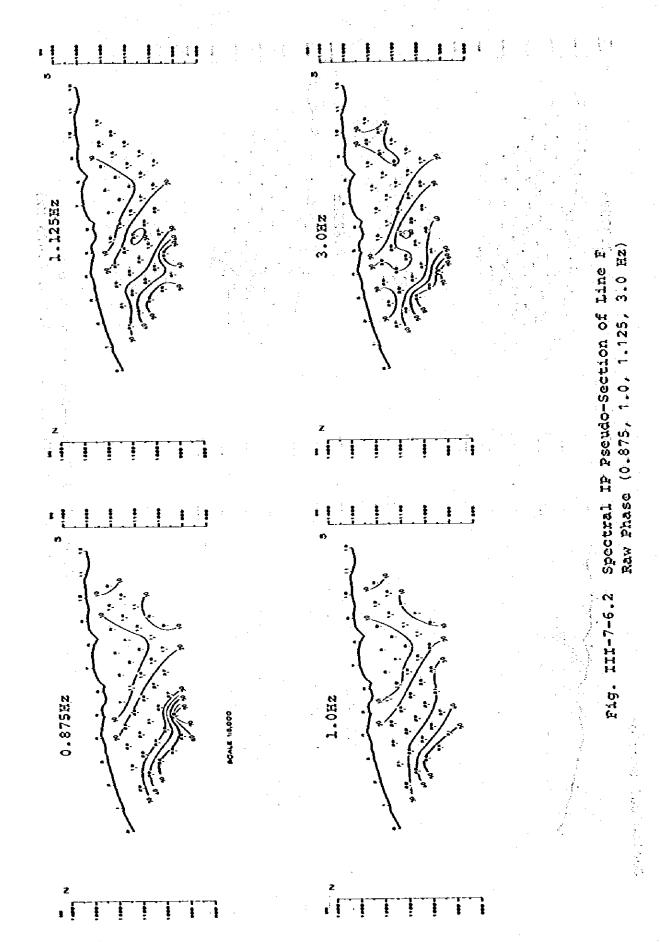


Fig. III-7-6.1 Spectral IP Pseudo-Section of Line F. Raw Phase (G. Sec., 0.125, 0.375, 0.625 Hz)



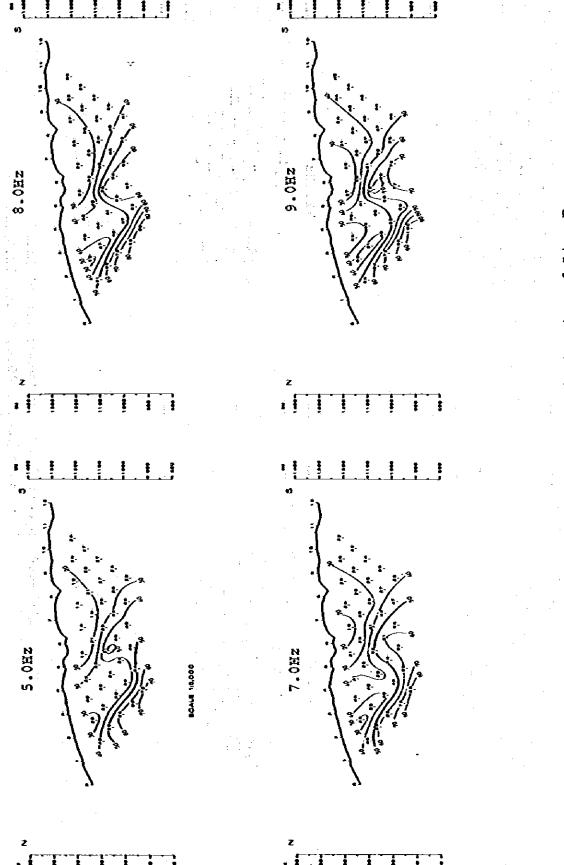
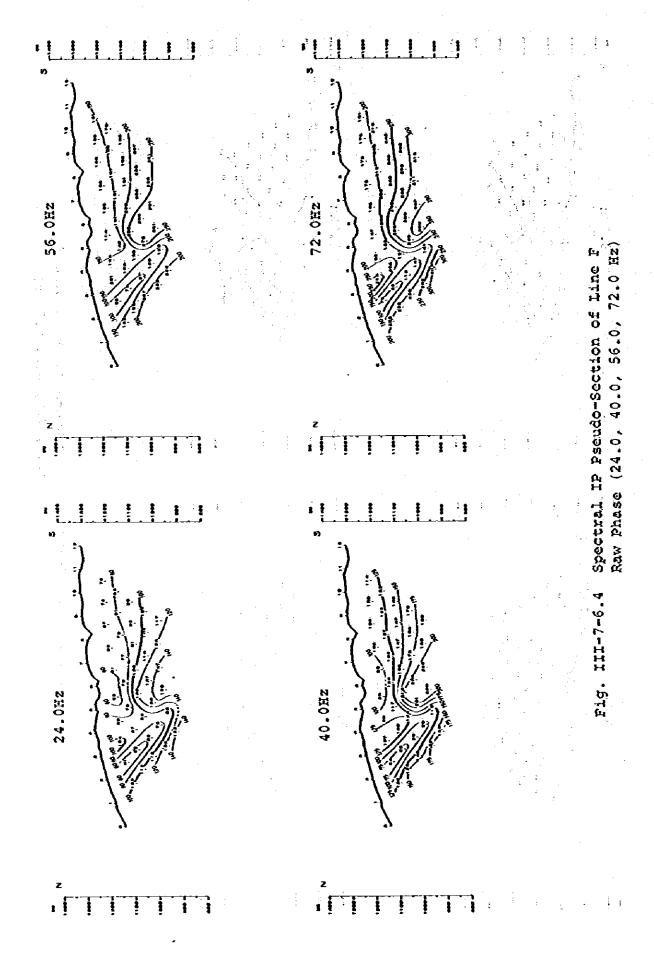


Fig. III-7-6.3 Spectral IP Pseudo-Section of Line F Raw Phase (5.0, 7.0, 8.0, 9.0 Hz)



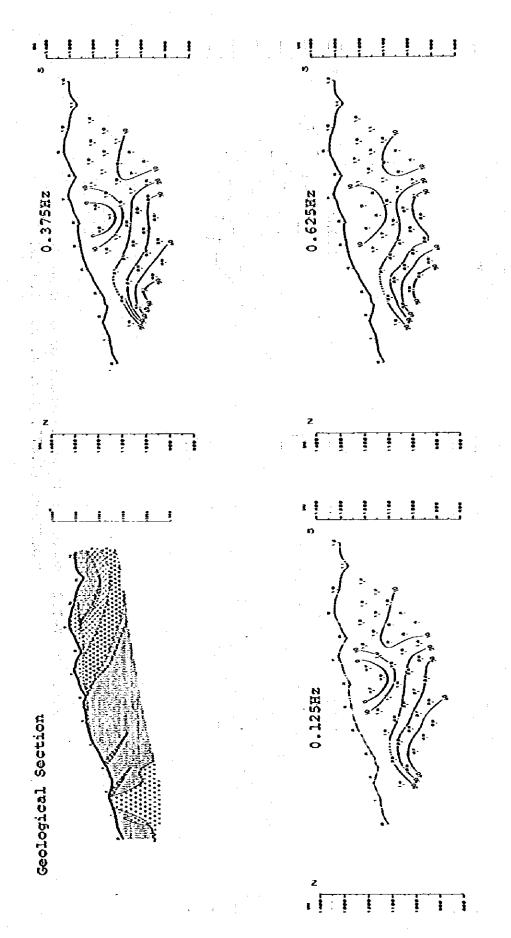
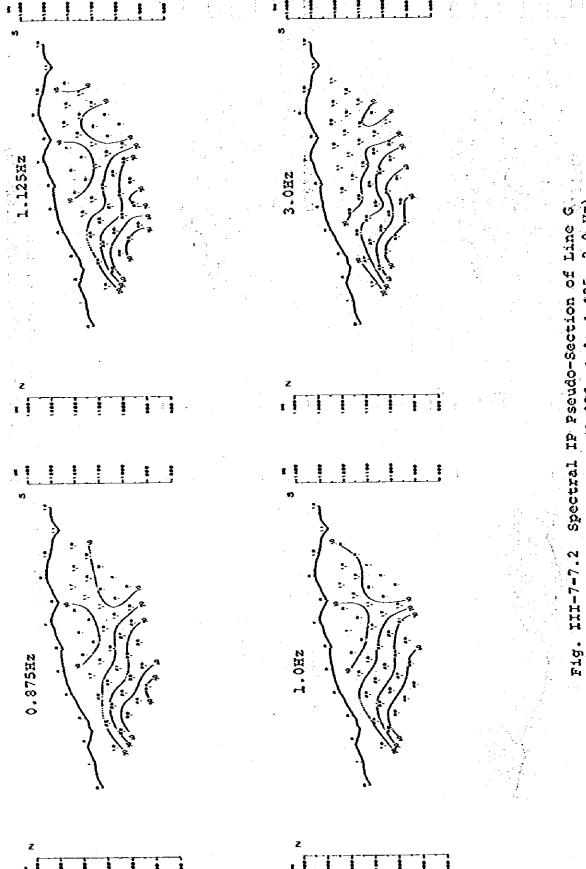


Fig. III-7-7.1 Spectral IP Pseudo-Section of Line G. Raw Phase (G. Sec., 0.125, 0.375, 0.625 Hz)



Raw Phase (0.875, 1.0,

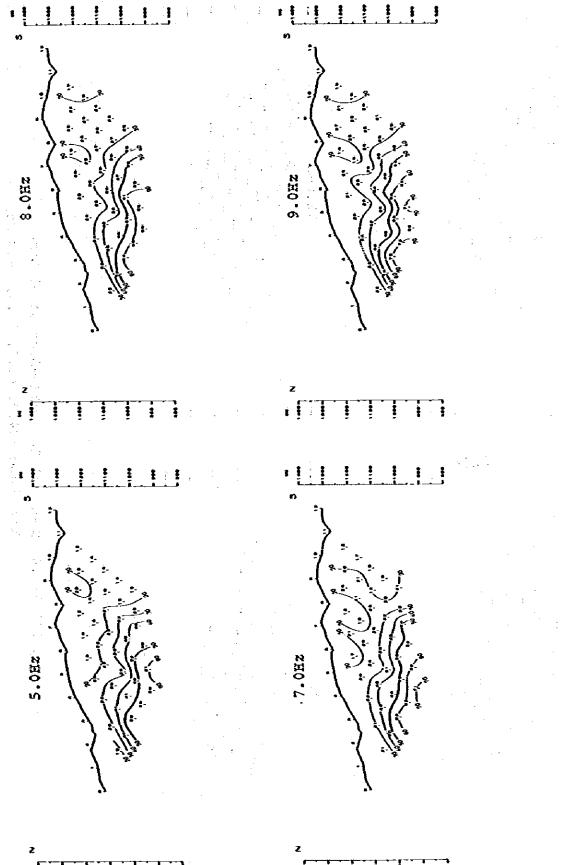
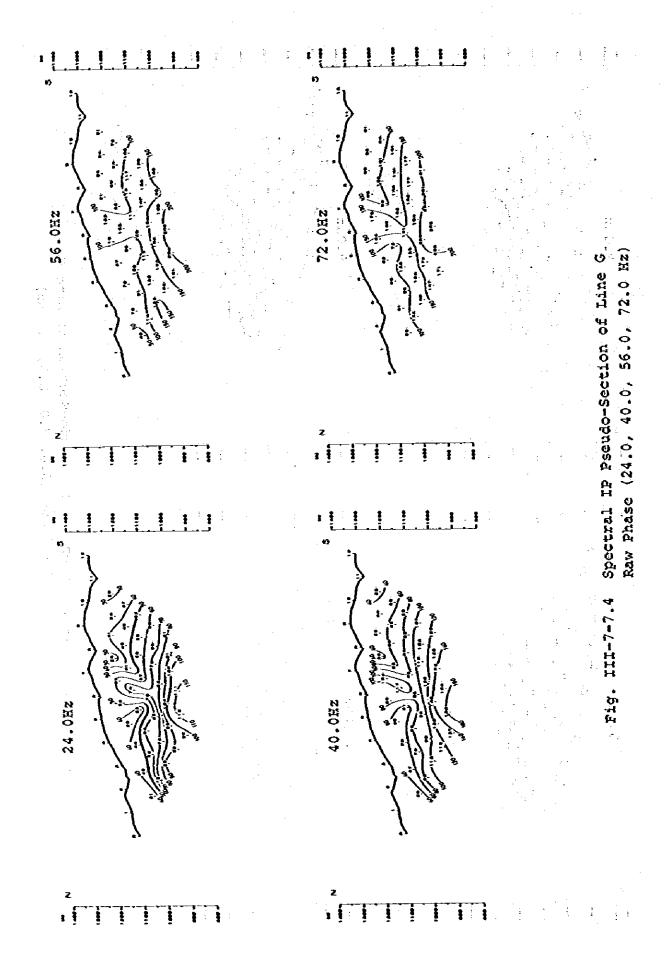


Fig. III-7-7.3 Spectral IP Pseudo-Section of Line G Raw Phase (5.0, 7.0, 8.0, 9.0 Hz)



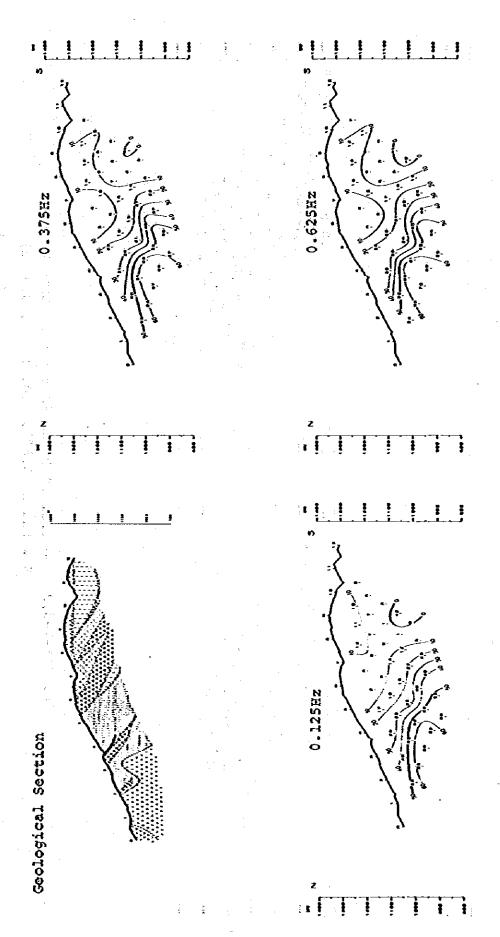


Fig. III-7-8.1 Spectral IP Pseudo-Section of Line H Raw Phase (G. Sec., 0.125, 0.375, 0.625 Hz)

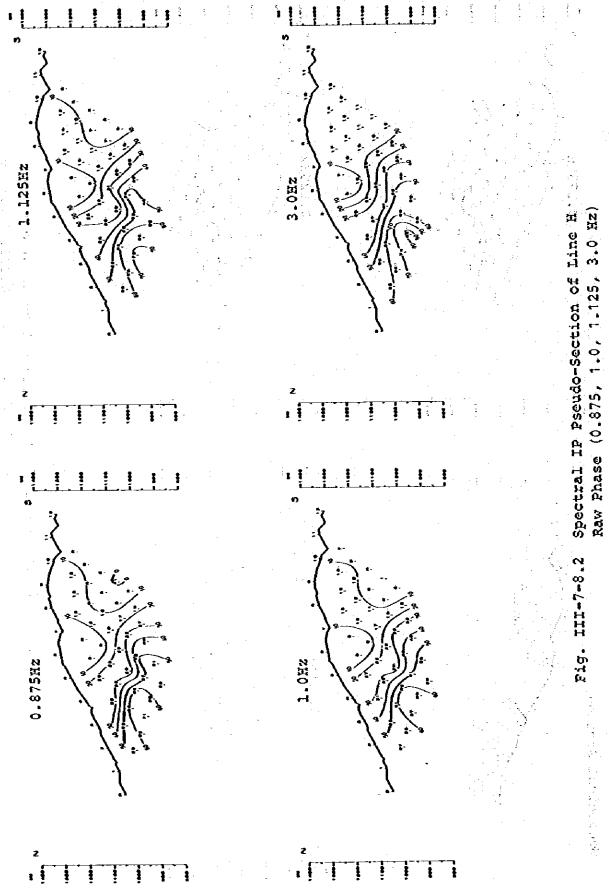


Fig. III-7-8.2

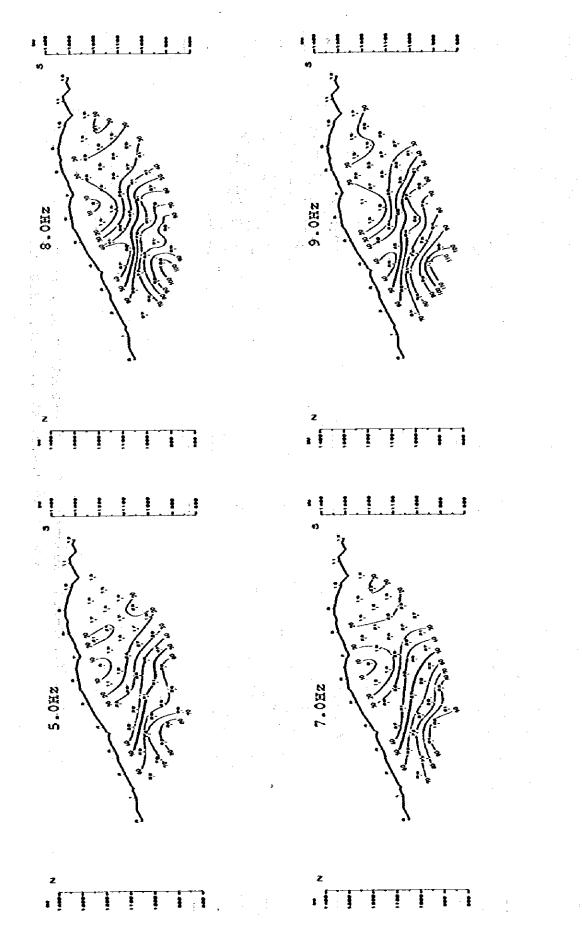
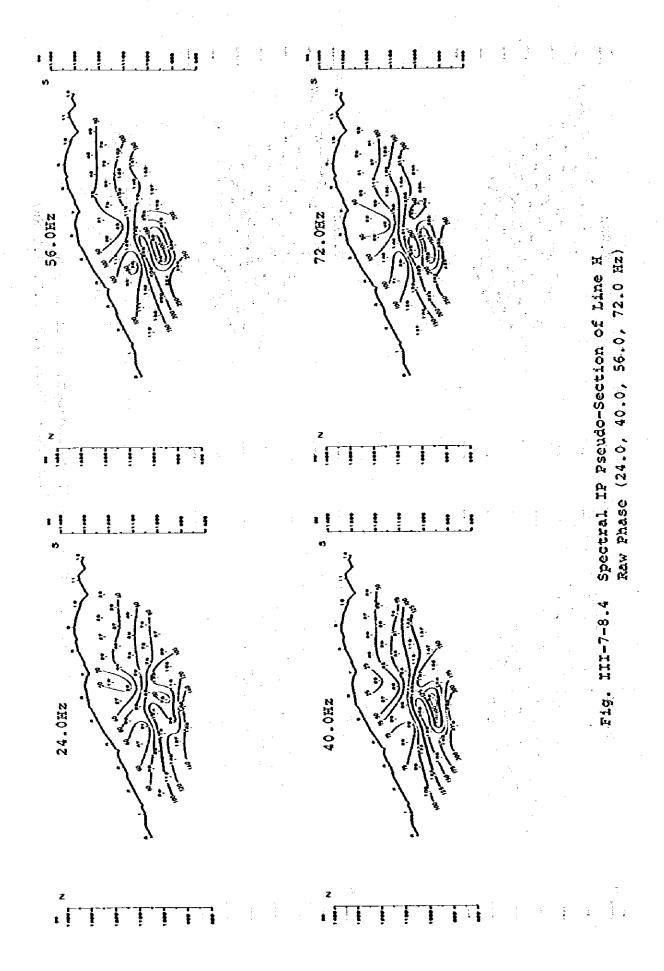
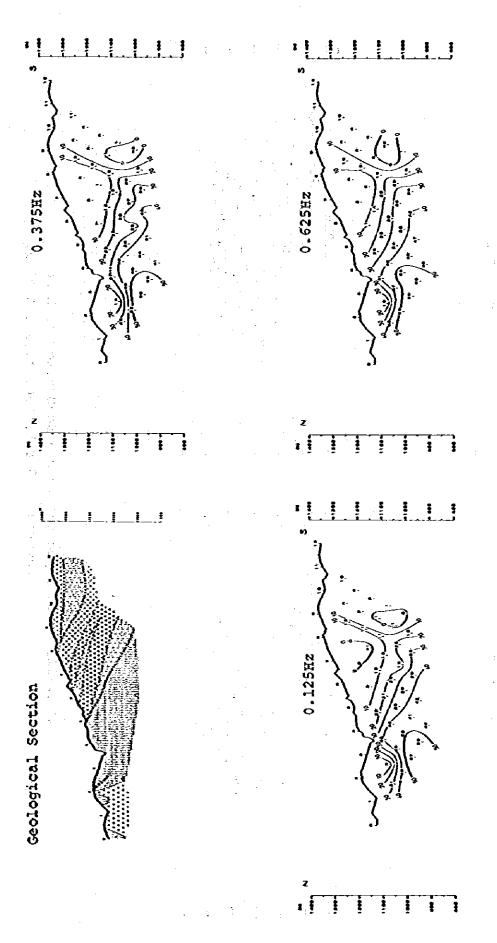
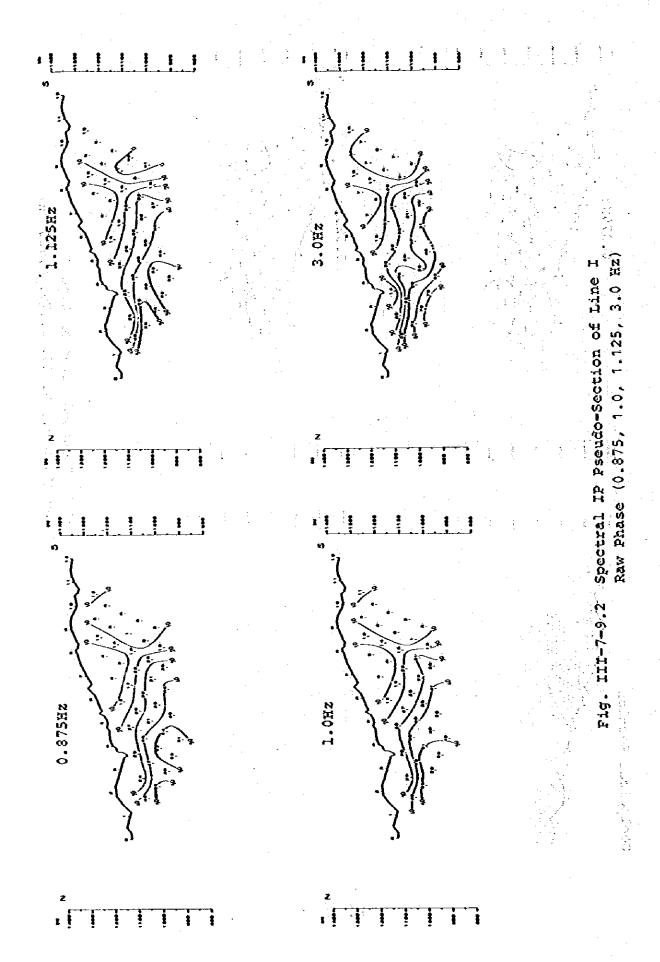


Fig. III-7-8.3 Spectral IP Pseudo-Section of Line H Raw Phase (5.0, 7.0, 8.0, 9.0 Hz)





Spectral IP Pseudo-Section of Line I Raw Phase (G. Sec., 0.125, 0.375, 0.625 Hz) Fig. III-7-9.1



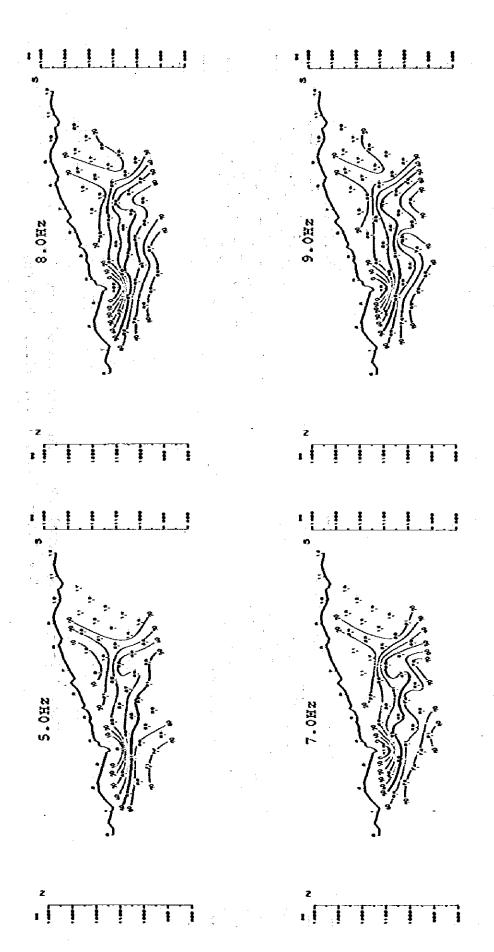
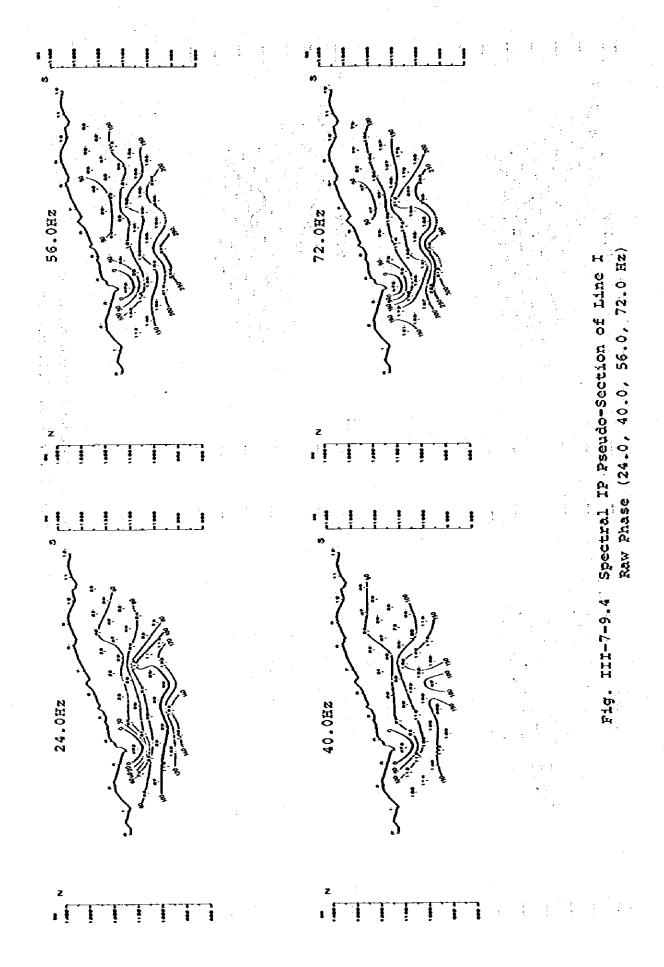


Fig. III-7-9.3 Spectral IP Pseudo-Section of Line I Raw Phase (5.0, 7.0, 8.0, 9.0 Hz)



For survey line I, there is large FB anomaly locating in the valley at 1000 No.  $3 \sim 4$  with the depth of shallower than 100 m.

## 4-1-4 Raw Phase and 3-point Decoupled Phase

For each survey line, pseudo-sections of Raw Phase with frequency of more than 15 kinds are shown in Fig. III-7-1 ~ Fig. III-7-9. 3-point decoupling diagrams done with 0.375 Hz ~ 0.625 Hz are shown in Fig. III-8-1 ~ Fig. III-8-3.

Since these sections are considered to reflect the spectral IP anomaly very clearly, geological sections are attached to the upper part of each survey line. Phase anomaly of each survey line is constructed as follows:

# Survey Line A:

The top of the anomalous source is present at the depth of 200 m at No. 3 ~ 5, and anomalous value with more than ~50 milliradian is detected. This anomaly in north is in almost same anomaly pattern at 0.125 Hz harmonic (range of 0.125 ~ 1 Hz), and shows constant phase value disregarding to frequency increase in the spectral.

For frequency range of 3 ~ 7 Hz, there is no anomaly recognized at No. 6 ~ 8 covered with pyroxene andesite, even though northern limit of anomaly gradually spreads towards south with a weak dissemination spread. About section with value of more than 24 Hz, contour is almost horizontal and phase increases as depth caused by electro magnetic coupling.

### Survey Line B:

As same as line A, top of the anomalous source is considered to be at the depth of about 150 m at No. 4 and stronger anomaly of -70 milliradian is detected. This anomaly seems to be successive to the depth with south dipping at No. 3, even though no anomalies seen at No. 4 - 10. Especially at shallow parts of No. 6 - 8, there is no anomaly recognized; however, negative coupling can be partially observed since it is adjacent to remarkable anomaly.

At low frequency range, weak anomaly with value of -20 ~ -30 milliradian at the northern end of survey line shows spectral decreasing with frequency increase at the harmonic of 0.125 Hz. This spectral is similar to the one of which detected at center part of survey line C.

#### Survey Line C:

For this survey line, the most eminent anomaly of all in this area is

detected. There are three anomalies for 0.125 Hz phase section and deep anomaly in northern end of the line seem to successive to survey lines A and B.

At the depth of 150 m in the center part of survey line, anomaly with the Value of more than -60 milliradian are detected, and it is combined with the central anomaly at the higher frequency range than 0.125 Hz.

As it can be seen in phase of 0.125 Hz, above-mentioned anomaly is considered to be caused by two south dipping sources, which are caused by disseminated sulfide, since no phase change is shown as frequency increases.

Meanwhile, at No. 5 ~ 6, -40 milliradian phase which is considered to originated with south dipping anomaly source from the depth of about 100 m, is massive even though it is a weak anomalies and phase is weakend rapidly at 0.125 ~ 0.625 Hz. This is considered to be different anomaly source from the one detected in the northern part of the survey line judging from its spectral, and seems to be caused by massive sulfide by its rapid decrease.

### Survey line D:

South dipping anomaly from shallow part of No. 2 ~ 3 has value of more than -70 milliradian. Since there is no phase change at low frequency range of 0.125 ~ 3 Hz, it is considered to be due to the same anomalous source as one spreading from northern end of survey line A. By its anomaly pattern, it is believed to be caused by disseminated sulfide with gentle dipping towards south.

#### Survey line E:

Phase anomaly with value of -50 ~ -80 milliradian is detected at the north half of the survey line. It is considered as that the anomaly is caused by one which is deeper than 100 m, but weak dissemination is believed to be at the ground surface around No. 5 ~ 6.

The anomaly is considered to be the same with one found in northern part of each survey line, since no phase change is noted with frequency increase.

### Survey line F:

At the depth of about 150 m at No. 3, there is phase with value of -50 -60 milliradian constructing the anomaly zone at northern end of the survey line. This is similar to the one in the center part of survey line C since slight phase decrease can be seen at low frequency range.

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Weak anomaly can be perceived at the depth of 200 m at No.  $5 \sim 6$  with increasing tendency at frequency range of more than 1 Hz. There is no anomaly recognized in southern half of the survey line.

### Survey Line G:

Like as survey line F, weak anomaly zone with value of -40 ~ -50 m milliradian is detected at the depth of about 150 m. This is considered as weak anomaly caused by disseminated sulfide and no phase change at low frequency range has occurred.

No anomaly is detected at thick andesite overlain area in northern part of the survey line.

# Survey Line H:

As same as survey line G, anomaly zone is detected at northern end of the survey line, but anomaly source is shallow so that phase indicate large value of  $-60 \sim -70$  milliradian.

At A.Palelo, northern end of survey line, there is sulfide mineralization on the surface with gentle south dipping dissemination seemingly successive to the depth of about 150 m at No. 3 ~ 4.

### Survey Line I:

At creek between No.  $3 \sim 4$ , there is mineralization in the shallow part with value of  $-40 \sim -50$  milliradian.

This is also a gentle south dipping considered to be successive to the north.

No anomaly can be detected in the shallow part in the northern half of the survey line.