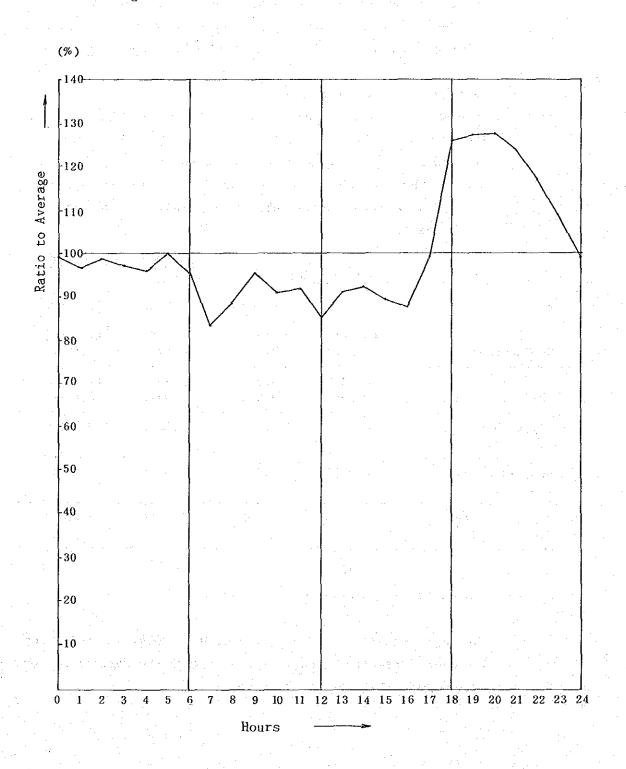
Fig. A-3 Standard Weekday Load Curve in East Java System



iv) to compare this load curve with the given system load curve and revise every assumed curves in order to decrease the differences at each hour under the condition that each daily sold energy should be fixed.

is required as the next procedure.

An example of this procedure is illustrated on Supplement B.

The results of this approach are shown on Fig. A-4; and the final result is highly precise as shown on Fig. A-5(3).

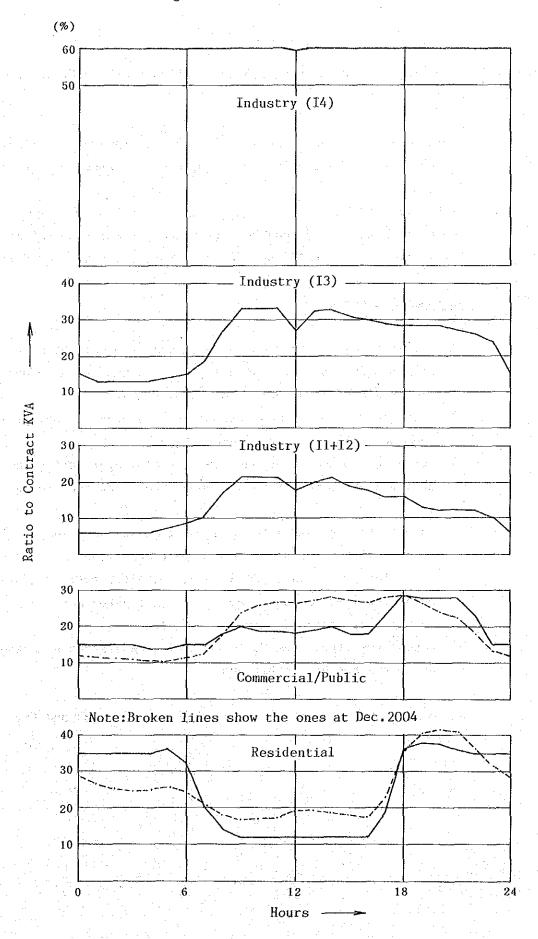
Hereby, the following demand conversion factors which contain no losses should be applicable at the middle of 1983/84 (September).

	for Contra	ct kVA	for Weekday Average Demand			
	14 hours	19 hours	14 hours	19 hours		
Residential	(0.1819) 0.1200	(0.4010) 0.3800	(0.7153) 0.4720	(1.5768) 1.4940		
Commercial/Public	(0.2806) 0.2000	(0.2639) 0.2800	(1.3915) 1.0410	(1.3096) 1.4580		
Light Industry (II + I2)	0.2100	0.1300	1.5650	0.9690		
Heavy Industry (13)	0.3250	0.2850	1.3340	1.1700		
Heavy Industry (I4)	0.6000	0.6000	1.0000	1.0000		

# (3) Future Transfiguration of Load Curves

In the remote future, for instance, Dec. 2004, the following changes of electric uses will transfigure the residential or commercial/public use load curves.

Fig. A-4 Standard Load Curves by Use



Supplement B Illustration for Decision Process of Standard Load Curves by Use

Table A-3(1)~(3) and Fig. A-5(1)~(3) are prepared for illustration; they show the iterative approaching aspect over three (3) stages.

After prepared Table A-2, the ratios of weekday average demand to contract kVA can be determined for each use category. Hereafter, we will call them "Load factor to contract capacity"

## Approach Procedure

- Assume trial load curves for each use category, so as to each one has the daily quantity which equals twenty-four (24) times of load factor to contract kVA.
- 2) Convert this load curves into MW base by means of multplying contract capacity of each use category.
- 3) Obtain a tentative weekday load curve by aggregating those MW for every categories, and normalize it on the average value.
- 4) Compare this curve with the normalized standard weekday load curve which are obtained in a manner described in the foregoing paragraph and shown on Fig.A-3; alter every tentatively estimated load curves so as to the aggregated curve approaches to the standard curve mentioned.
- 5) Repeat the steps from 2) to 4) until the difference mentioned above reaches negligible one.

As for the concrete method, refer Table A-3(1)~(3) and Fig. A-5(1)~(3).

Table. A-3(1) Approach to Standard Load Curves by Use

<del></del>			-				
	Residential % per contract/MW	% per	11+12 % per contract/MW	I3 %per contract/MW	I 4 % per contract/MW	Total MW /% per ave	System L.C.( % per ave.)
1	30 / 95.84	15 / 26.01	8 / 7.69	15 / 30.83	49 / 46.16	206.53/ 88.2	97
2	"   "	"   "	6 / 5.77	11 / 22.61	"   "	196.39/ 83.9	9 7
3	"   "	"/"	"   ".	"/"	"   "	196.39/ 83.9	9 7
4	"/"	14 / 24.28	"   "	"   "	"   "	194.66/ 83.2	96
5		15 / 26.01	"   "	"   "	/	196.39/ 83.9	99
6	25 / 79.87	14 / 24.28	"   "	"/ "	" / "	178.69/ 76.4	95
7	21 / 67.09	15 / 26.01	12 / 11.53	19 / 39.05	"   "	189.84/ 81.1	83
8	18.4 / 58.78	19 / 32.95	17 / 16.34	29 / 59.61	59 / 55.58	223.26/ 95.4	88
9	19.0 / 60.70	18 / 31.21	19 / 18.26	32 / 65.78	70 / 65.94	241.89/103.4	9 3
10	<i>"   "</i>		"   "	"   ""	"   "	"   "	9 2
.11	"   "	11 / 11	"   "	/	".   "	"   "	9 2
12	" / "	"   "	18 / 17.30	30 / 61.67	68.7 / 64.72	235.60/100.6	8 5
13	"   "	"   "	19 / 18.26	32 / 65.78	64 / 60.29	236.24/100.9	9 1
. 14	"   "	"   "	"   "	"   "	70 / 65.94	241.89/103.4	9 2
15	"   "	"   "	"   "	"   "	69 / 65.00	240.95/103.0	8 9
16	" / "	. " / "	18 / 17.30	31 / 63.72	"   "	237.93/101.7	88
17	23 / 73.48	23 / 39.88	17 / 16.34	30 / 61.67	"   "	256.37/109.5	99
18	32 /10223	29 / 50.29	16 / 15.38	29.6 / 60.84	64 / 60.29	289.03/123.5	126
19	33 /105.42	28 / 48.55	12 / 11.53	29 / 59.61	59 / 55.58	280.69/119.9	127
20	" / "	" / "	"   "	"   "	11 / 11	280.69/119.9	127
21	32 /102.23	"   "	"   "	28 / 57.55	"   "	275.44/117.7	123
22	31 / 99.03	23 / 39.88	11 / 11	26 / 53.44	"   "	259.46/110.9	117
23	30 / 95.84	20 / 34.68	"   "	23 / 47.28	"   "	244.91/104.6	108
24	"/"	16 / 27.75	"   "	19 / 39.05	"   "	229.75/ 98.2	99
total	610.4/1,950.03	461.0 /799.37	322.0 /309.47	584.6/1,201.66	1,430.7/1,356.24	5,616.77/2,400.0 (234.032)	2,4 0 0
contract MVA	(319.46)	(17341)	(96.10)	(205.55)	(94.20)		

Fig. A-5(1) Approach to Standard Load Curves by Use

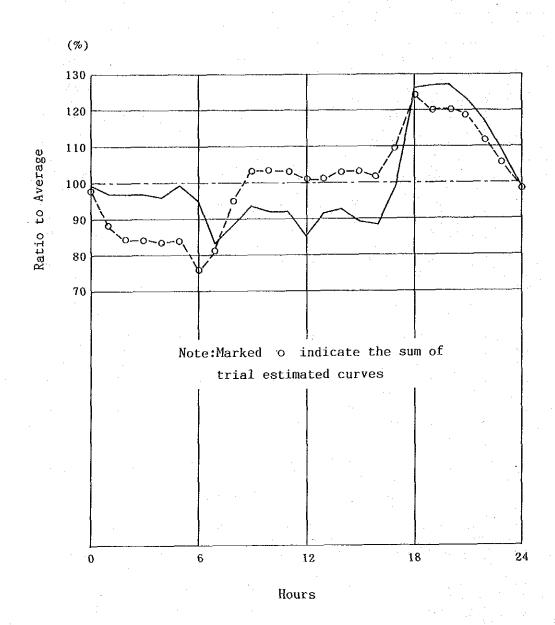


Table. A-3(2) Approach to Standard Load Curves by Use

<del></del>			·	<del>,</del>	<del></del>		
	Residential % per contract/MW	Comm/Pub % per contract/MW	I1+I2 % per contract/MW	I 3 % per contract/MW	I4 % per contract/MW	Total MW / % per ave.	System L.C.( % per ave.)
1	35 /111.8	15 / 26.01	8 / 7.69	16 / 32.89	60 / 56.52	234.91/100.4	97
2	" / "	"   "	6. / 5.77	13.4 / 27.54	"   "	227.64/ 97.3	9 7
3	"   "	" / "	"   "	11 / 11	" / "	227.64/ 97.3	9 7
4	"   "	14 / 24.28	" / "	"   "	"   "	225.91/ 96.5	9 6
5		15 / 26.01	/ "	/	"   "	227.64/ 97.3	9 9
6	28 / 89.45	14 / 24.28	"   "	"   "	"   "	203.56/ 87.0	9 5
7	21 / 67.09	15 / 26.01	12 / 11.53	19 / 39.05	"/"	200.2 / 85.5	8 3
8	17.4 / 55.59	19 / 32.95	17 / 16.34	28 / 57.55	"   "	219.0 / 93.6	88
9	12 / 38.34	18 / 31.21	19 / 1826	31 / 63.72	"   "	208.1 / 88.9	93
10	"   "	"   "	"   "	"   "	"   "	/	9 2
11	"   "	"/"	"   "	"   "	"   "	"   "	9 2
12	"/"	"/"	18 / 1730	29 / 59.61	59.7 / 56.24	202.7 / 86.6	85
1 3	"/"	"/"	19 / 18.26	31 / 63.72	60 / 56.52	208.1 / 88.9	9 1
14	"   "	"   "	"   "	"   "	"   "	"   "	92
1 5	"   "	"   "	"   "	"   "	"   "	"   "	8 9
16	"   "	"   "	18 / 17.30	30 / 61.67	"   "	205.0 / 87.6	88
17	23 / 73.45	23 / 39.88	17 / 16,34	29.6 / 60.84	"   "	247.0 /105.6	9 9
18	35 /111.80	29 / 50.29	16 / 15.38	28 / 57.55	"   "	291.5 /124.6	126
19	37 /118.2	28 / 48.55	12 / 11.53	"   "	"   "	292.4 /124.9	1 2 7
20	"   "	"   "	"   "	"   "	"   "	"   "	127
21	36 /115.0	"   "	"   "	"   "	"   "	289.2 /123.6	123
22	35 /111.82	23 / 39.88	"   "	26 / 5344	"   "	273.2 /116.7	117
2 3	"   "	20 / 34.68	"   "	23 / 47.28	"   "	261.8 /111.9	108
24	"   "	16 / 27.75	"   "	19 / 39.05	"1"	246.7 /105.4	9 9
total	6104/1,949.9	461.0 /799.37	3220 /309.47	584.6/1,201.6	1,439.7/1,356.20	5,617.00/2,400.1 (234,032)	2,4 0 0
contract MVA	(319,46)	(17341)	(9610)	(205.55)	(94.20)		

Fig. A-5(2) Approach to Standard Load Curves by Use

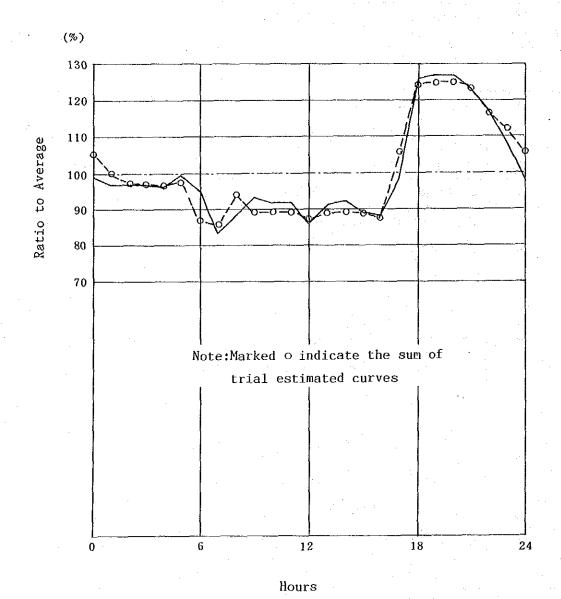


Table. A-3(3) Approach to Standard Load Curves by Use

		·			·		
	Residential % per contract/MW	Comm/Pub % per contract/MW	11+12 % per contract/MW	I 3 % per contract/MW	I 4 % per contract/MW	Total MW /% per ave.	System L.C.( % per ave.)
1	35 /111.81	15 / 26.01	6 / 5.77	13 / 26.72	60 / 56.52	226.83/ 96.9	97
2	"/"	"/"	"   "	"/"	"/"	" / "	9 7
3	"   "	"   "	"   "	"   "	"   "	" / "	9 7
4	"   "	14 / 2428	"   "	"   "	"   "	225.10/ 96.2	9 6
5	36 /115.01	" / "	7 / 6.73	14 / 28.78	"   "	231.32/ 98.8	99
6	32 /102.23	15 / 26.01	8 / 7.69	15 / 30.83	"   "	223.28/ 9541	9 5
7	20 / 63.89	"/"	10 / 9.61	19 / 39.05	"   "	195.08/ 83.36	8 3
8	14.4 / 46.00	18 / 31.21	17 / 16.34	27 / 55.50	"   "	205.57/ 87.8	88
9	12 / 38.34	20 / 34.68	21 / 20.18	33 / 67.83	"   "	217.55/ 93.0	9 3
10	"   "	19 / 32.95	"   "	"   "	"   "	215.82/ 92.2	9 2
11	n / n	"   "	"   "	"   "	11 1 11	"   "	92
12	" / "	18 / 31.21	18 / 17.30	27 / 55.50	59.7 / 56.24	198.59/ 84.9	8 5
13	"   "	19 / 32.95	20 / 19.22	32 / 65.78	60 / 56.52	212.81/ 909	9 1
14	"   "	20 / 34.68	21 / 20.18	32.5 / 66.80	"   "	216.52/ 92.5	9 2
15	" / "	18 / 31,21	19 / 18.26	31 / 63.72	"   "	208.05/ 88.9	8 9
16	n / n	"   "	18 / 17.30	30 / 61.67	" 1 "	205.04/ 87.6	88
17	19 / 60.70	23 / 39.88	16 / 15.38	28.6 / 58.79	"   "	231.27/ 98.8	9 9
18	36 /115.01	29 / 50.29	"   "	28.5 / 58.58	"   "	295.78/1264	126
19	38 /121.39	28 / 48.55	13 / 12.49	"   "	"   "	297.53/127.1	127
20	"/"	"   "	12 / 11.53	"   "	"   "	296,57/126.7	127
21	36 /115.01	" / "	" / "	27 / 55.50	" / "	287.11/122.7	123
22	35 /111.82	23 / 39.88	"   "	26 / 53.44	"/"	237.19/116.7	117
23	"   "	15 / 26.01	10 / 9.61	24 / 49.33	"/"	253.29/108.2	108
24	"   "	"   "	6 / 5.77	15 / 30.83	"   "	230.95/ 98.7	99
total	610.4 /1,950.05	461.0 /799.38	322.0 /309.47	584.6 /1,201.63	1,439.7/1,356.20	5,616,73/2,399.8 (234,032)	2,4 0 0
contract KVA	(31946)	(173.41)	(96.10)	(205.55)	(94.20)		

Fig. A-5(3) Approach to Standard Load Curves by Use

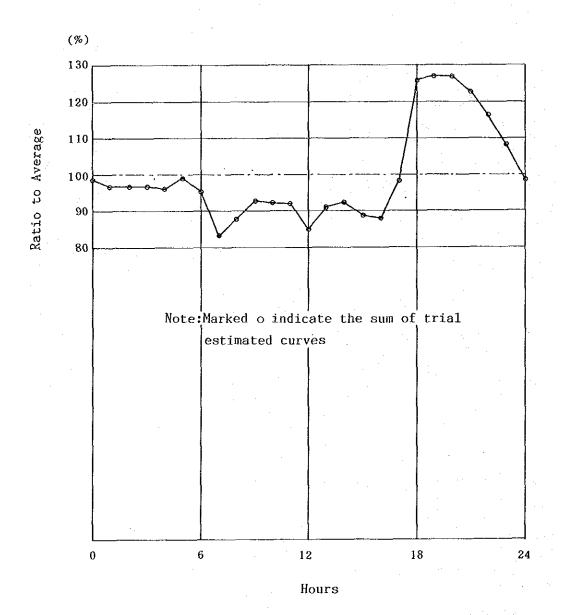


Table. A-4(1) Residential Load Curve in Summer

[Present Status in a Developed Country for Reference to Forecast Future Status in East Java

	Developed (	Country	East Java		f East Java
<u> </u>	% to ave.	% to ave.	1983/84 % to ave.	% beverop	ed Country % to contract
time	(integrated)	(indicated)	(do)	(do)	(do)
1	79.8	71.7	137.61	104.66	26.62
2	63.6	60.4	11	99.01	25,18
3	57.2	57.25	n	97.43	24.78
4	57.3	58.6	11	98.11	24.95
5	59.9	59.4	141.55	100.48	25.56
6	58.9	67.3	125.82	96.56	24.56
7.	75.7	82.7	78.64	80.67	20.52
8	89.7	86.95	56.62	71.79	18.26
9	84.2	83.95	47.18	65.57	16.68
10	83.7	84.4	11	65.79	16.73
11	85.1	88.7	11	67.94	17.28
12	92.3	101.15	ti .	74.17	18.86
13	110.0	105.5	tt .	76.34	19.42
14	101.0	97.7	II .	72.44	18.42
15	94.4	94.0	11	70.59	17.95
16	93.6	93.0	**	70.09	17.83
17	92.4	104.6	74.71	89.66	22.80
18	116.8	136.65	141.55	139.1	35.38
19	156.5	166.55	149.41	157.98	40.18
20	176.6	177.75	n	163.58	*41.60
21	178.9	175.95	141.55	158.75	40.38
22	173.0	150.65	137.61	144.13	36.66
23	128.3	109.7	n n	123.66	31.45
24	91.1	85.45	TI .	111.53	28.37

<sup>\*</sup> This percentage to contract kVA is calculated on the supposition that it is in inverse proportion to the load factor. Namely, 38%x163.58/149.41=41.6%.

Table. A-4(2) Commercial/Public Load Curve in Summer

Present Status in a Developed Country for Reference to
Forecast Future Status in East Java

East Java Halving of East Java							
	Developed Country		East Java 1983/84	& Develor	ed country		
time	% to ave.	% to ave.	% to ave.	% to ave.	% to contract		
CIME	(integrated)	(indicated)	(do)	(do)	(do)		
1	36.1	36.0	78.09	57.0	11.51		
2	35.9	34.7	tt	56.35	11.38		
3	33.5	33.05	tt	55.57	11.22		
4	32.6	32.55	72.89	52.22	10.54		
5	32.5	32.45	11	52.67	10.64		
6	32.4	35.65	78.09	56.87	11.48		
7.	38.9	49.15	rr	63.62	12.85		
8	59.4	82.55	93.71	88.13	17.80		
9	105.7	129.1	104.12	116.61	23,55		
12	152.5	159.5	98.92	129.21	26.09		
11	166.5	168.9	ıı	133.91	27.04		
12	171.3	170.5	93.71	132.11	26.68		
13	169.7	173.25	98.92	136.09	27,48		
14	176.8	176.65	104.12	140.39	28.35		
15	176.5	176.5	93.71	135.11	27.28		
16	11	173.7	11	133.71	27.00		
17	170.9	159.7	119.74	139,72	28.21		
18	148.5	136.25	150.98	143.62	*29.00		
19	124.0	115.0	145.77	130,39	26.33		
20	106.0	96.35	tt	121.06	24.44		
21	86.7	78.35	τr	112.06	22.63		
22	70.0	61.6	119.74	90.67	18.31		
23	53,2	48.55	78.09	63.32	12.79		
24	43.9	40.0	TF.	59.05	11.92		

<sup>\*</sup> Present value in East Java is applied.

#### Domestic Uses

Various uses other than minimum lighting, including television, refrigerator, cooking and air conditioning will grow remarkably; so it will bring more higher demand which accompanies people's activity and make the share in midnight lowered.

#### Commercial Uses

The demand for office building should be expected to make remarkable growth; so it will bring higher demand in the working hours of offices, consequently the share in the other hours will be lowered.

The load curves for residential or commercial/public uses in Dec. 2004 shown on Fig. A-4 using broken lines are obtained by halving present statuses for East Java and for KEPCO in Japan in summer. (Refer Table A-4(1),(2)) Consequently, those demand conversion factors at Dec. 2004 which contain no losses should be changed into the values which given in parentheses on the table mentioned. For all of the other future time points, simple interpolation have been applied.

(4) Formulation of Distribution Loss Rate for Every Cabangs

According to PLN's data and targets of distribution line loss rate which obtained by the following expression,

$$1oss rate = \frac{Esub - Ecus}{Esub} * 100 (%)$$

where Esub: energy sent out of substations

Ecus: energy supplied to customers,

it in general decreases monotonously year by year  $^{1)}$  and approaches a final saturation value ten (10.0) percent. (Refer Table A-5)

A trend curve which called "modified exponential curve" and expressed by the formula shown on Table A-6 is adequate to express such trend.

Note 1) As a particular case, in Cabang Banyuwangi most of whose customers are supplied by tariff S1 at present, it is considered that the loss rate will increase year by year and will infinitely approach to ten (10.0) percent; because many S1 customers whose consumption time in a month is calculated but any measurement so long as five hundred (500) hours per month because of without meters.

This estimation results too much apparent energy sales and too less loss evaluation that is 8.31%, 1983/84.

On the other hand, the increase of number of customers with meter will lead to decrease of such an error; as the results the apparent loss rate will increase year by year in such a case.

The coefficients of the modified exponential functions which obtained by means of regressive analysis for each Cabang are shown on Table A-6.

These formulas are used when convert each demand into the one at substation.

Table. A-5 Target of Distribution Losses by Cabang [%]

								-		·		
1993/94	10	10	10	10	10	10	10	.01	10	10	10	10
1992/93	10	10	10	10	10	10	10	10	10	10	10	10
1991/92	10	01	10	10	10	10	01	10	10	10	10	10
1990/91	10	01	10	10	10	10	10	10	01	10	10	10
1989/90	10	11	11	11	TT	IT	11	10	10	10	11	10
1988/89	1.1	12	12	12	12	1.2	12	11	11	10	12	10
1987/88	12	13	13	13	13	13	13	12	12	10	13	10
1986/87	13	15	16	15	15	14	14	13	13	10	14	10
1985/86	14	17	18	17	18	16	15	14	14	10	1.5	10
1984/85	15	19	20	19	20	17	17	15	15	6	91	10
1983/84	15.93	20.97	40.05	21.87	23.33	19.03	18.66	16.71	16.09	8.31	17.28	10.95
F Y Cabang	Surabaya Utara	Surabaya Selacan	Bojonegoro	Malang	Pasuruan	Kediri	Mojokerto	Madiun	Jember	Banyuwangi	Situbondo	Pamekasan

Table. A-6 Distribution Loss Formulas for Each Cabang

$$(loss rate) = K+S*(exp A)*(exp B)**t$$
 [%];

where k=10.0

S=-1 for Cabang Banyuwangi

S=+1 for all of the other Cabangs

t is expressed by dominical years considered t = 0.0 in Dec.1900.

The values of exp A and exp B are determined by applying regressive analysis to the data of PLN for each Cabang. Those results obtained are shown on the following table.

			<del>,</del>	<del>_</del>
Cabang	K	S	A	В
Surabaya Utara	10.0	+ 1	27.04162	-0.3040436
Surabaya Selatan	10.0	+ 1	31.00065	-0.3443655
Bojonegoro	10.0	+ 1	49.48337	-0.5582369
Malang	10.0	+ 1	32.17167	-0.3579769
Pasuruan	10.0	+ 1	34.25163	-0.3815969
Kediri	10.0	+ 1	28.06051	-0.3116261
Mojokerto	10.0	+ 1	27.57348	-0.3064051
Madiun	10.0	+ 1	29.14473	-0.3285625
Jember	10.0	+ 1	27.47745	-0.3091248
Banynwangi	10.0	- 1	61.03855	-0.7307686
Situbondo	10.0	+ 1	24.25191	-0.2680974
Pamekasan	10.0	+ 1	59.77571	-0.7241021

## A.4 Demand Forecast for Each Substation

In East Java, each Cabang is divided into ten(10) and less zones, and those locations are roughly shown on Table A-7.

If the demand at a specified time is forecasted for every zones by means of the procedure mentioned in the preceding paragraph, the demand at a substation could be forecasted by combining these ones for all zones which fed from this substation.

The present supply areas of each substation in East Java have been estimated as a set of zones mentioned above with reference to maps which roughly show the locations of every substations and distribution lines and to the latest actual load of each substation and so on. Further, for a zone which seems to be fed by several substations, the supply area has been set up as a combination of one tenth of a zone.

Next, considering the yearly increasing feature of the demand of each substation, alterations of supply area have been planned yearly so as to transfer demand from heavy loaded substations to newly installed or light loaded substations. These contents are shown on Table A-8.

## (1) Computerized Calculation

Basing on the method mentioned in the preceeding paragraph, we have developed a computer program including vast itterative calculations of trend analysis and executed a series of computerized calculation which use a large sized computer.

A part of the many outcomes obtained will be described as an extraction.

#### a. Demand Conversion Factors.

Table A-9 shows the demand conversion factors which are used to convert contract kVA or weekday average demand into peak demand by year, by use category and by time (nineteen hours or fourteen hours).

The meanings of figures in the columns of M,K,L are as follows;

Table. A-7 Major Towns Included in Each Zone

_		$\frac{(1/3)}{1}$
Cabang	zone code	Major Towns/Villages
	0.1	Genteng
	0 2	Bubutan, Tandes
Surabaya	03	Pabean, Cantian
Darabaya	0 4	Semampir, Simokerto, Tambaksari
	0.5	Sukolilo
	0 6	Gresik, Bungoh
**	0 8	Krembangan
	1 0	Krian, Wonoayu, Wringìnanom
	1 1	Sawahan, Tegalsari
<b>.</b>	1 2	Menganti, Kademean, Driyorejo, Karangpilang
Surabaya	1 3	Wonokromo, Wonocolo
Selatan	1 4	Gubeng
peratan	1 5	Rungkut, Waru
	1 6	Taman
	1 7	Lakor
ļ	1 8	Sidoarjo, Tanggulangin, Krembung
	1 1	Bojonegoro
	1 2	u .
	1 3	• н
Podemones	1 4	rr ( )
Bojonegoro	1.5	<b>u</b> the state of t
	16	Tuban, Semanding, Tasikmadu
<u>;</u>	1.7	Lamongan, Babad
·	1 8	Tuban
· · · · · · · · · · · · · · · · · · ·	1 1	North-East Part of Malang City
·	1 2	East "
	1 3	North "
	1 4	North-West "
Malang	15	South "
- · · · <b>O</b>	1 6	West "
	1 7	Lawang, Bedali, Bululawang, Batu, Selekta
!	1 8	Singosari, Tumpang, Poncokusumo
	1 9	Turen, Dampit, Sukorejo, Ngantang

(	2	/	4	)

Cahana	zone code	(2   Major Towns/Villages
Cabang		
	1 0	Pasuruan, Plered
	11	Probolingo, Leces
	1 2	Kraksaan, Pajarakan
Pasuruan	1 3	Bangil, Beji
	1 4	Pandaan
	1 5	Tretes
	1 6	Porong, Gempol,
	1 0	Trenggalek, Pogalan
	1 1	South Part of Kediri City
	1 2	East
	1 3	West
12.	1.4	North "
Kediri	1 5	Blitar, Sanankulon,
	1 6	Tulungagung, Karangrejo, Gandekan
	1 7	Nganjuk, Berbek, Loceret, Sidokare, Sukomero
	1 8	Kertosono
	1 9	Pare, Kandangan
	11	South Part of Mojokerto City
	1 2	North "
	1 3	Bangsal, Dellangn, Pacet
	1 4	
Mojokerto	1	Jombang, Peterongan, Diwek
	1 5	Ngoro, Kandangan
	1 6	Ploso, Sentul, Tembelang
	1 7	Mojosari, Wonokusumo, Sidorejo
	1 8	Mojosari
	1 0	Caruban, Bancong
	1 1	North Part of Madium City
	1 2	East "
	1 3	South "
	1 4	West
Madiun	1 5	Dolopo, Ponorogo, Sarangan
	1 6	Magetan, Sarangan, Plaosan
	1.7	Ngawi, Geneng, Paron
	18	Maospati, Tebon
	1 9	Pacitan, Kebonagang

		(3/3).
Cabang	zone code	Major Towns/Villages
	1 1	Jember City
	1 2	Lumajang, Sukodono
Jember	1 3	Bondowoso, Wonosari
	1 4	Kalisat
	1 5	Kalisat
	1 7	Jember City
	1 1	Banyuwangi City
	1 2	n
Banyuwangi	1 6	Rogojampi, Kabat, Singojuruh
	1 7	Genteng
	18	Muncar
<u></u>	1 1	Situbondo City
Situbondo	1 2	Panarukan
Dicapondo	1 3	Besuki
	1.4	Asembagus
	1 0	Kamal, Ambunten, Sepulu, Waru, Batu Marmer, Tanjung Bumi, Banyu Atas, Sapudi, Omben,Kwanyar
	1 1	Pamekasan City
	1 2	Gading, Guluk-Guluk, Sumenep
	1 3	Sampang
	1 4	Bangkalan
Pamekasan	1 5	Ketapang
	1 6	Pasongsongan
	1 7	Modung, Blega
	18	Pakong
	1 9	Prenduan

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ZONE CNO. \* RATIOS

YEAR

NAME

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	- 0				0.	* *	00			16*0.5.						11. 0. 0. 0. 0.			• •	15*0.2			18*0.2							
٠	6*1.0. 8*1.0.	* * *	0.0.4 0.0.4 0.0.4		•	14*0.0	14*0.3	14*0.3	• .	11*0	٠ *	o.	* *	0	0 *	15*0.6	*	0 *	٠ *	17*1.0.	0	, 0 *	* *		0	0	*	0 C	11 *0.5	
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SURABAYA UTARA	JUNG REMBA REMBA	SAWAHAN TANDES SEGGROMADU	1000 1000 1000 1000	SURABAYA SELATAN	4	OLIL OLIL	CKOL.	טרור סרור	GAG	ה. ה	RIYORE	RIYORE JO	BUDURAN (SIDDARJU)	ENJERAN	ENJER		UNGKU	UNGKU	IMPANG	DARMO GRAND	ABATAN	ABATA	A 4	ב ב	EMANBUN	EMANB	ALANG P	TINTAN	1001	
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SUBSTATION	
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ZONE	
SUPPLY	

BOJONEGORO BABAT BABAT	750	C	* * *	13*1.0.	14*1.0.	15*1.0.
BABAT LAMONGAN LAMONGAN TUBAN MALANG	1988/ 1988/ 1988/ 3 8 8 8	17*0.03 17*1.0 17*0.5	16*0.6.	18 * 0 . 6 . 18 * 0 . 4 ,		
KEBUNGGUNG POLEHAN BLIMBING BLIMBING SENGKALING SENGKALING	1983/12 1983/12 1983/12 1986/13 1983/12 1983/12	1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	15*1.0, 16*0.3, 16*1.0, 16*0.7, 18*0.3,	11*1.0.		
SUKOREJO TUREN TUREN SENGGURUH SENGGURUH SELGREJO KEPANJEN PASURUAN	1983/12 1983/12 1983/12 1983/12 1983/12 1983/12 1993/12	000000	17*0.3, 17*0.2, 17*0.1,			
PROBOLINGO PROBOLINGO PLERED BANGIL PANDAAN PORONG KRAKSAAN PAITON	1983/12 1983/12 1983/12 1983/12 1983/12 1988/ 3	113 10.4 10.4 10.4 10.4 10.4 10.4 10.4 10.4	12*1.0, 10*0.6, 15*1.0,	10*0.6		
KEDIRI KEDIRI TULUNGAGUNG BLITAR PLIA WLINGI KERTOSONO KERTOSONO TRENGGALEK	1983/12 1983/12 1983/12 1986/ 3 1986/ 3	16 * 1 . 0	12*1.0, 17*1.0. 17*0.7,		19*1.0.	11*1.0.

SUPPLY ZONE OF SUBSTATION

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									17*1 0.											٠.				٠.								-						
		18*1.0.		· ·					14*1		0.					-		٠		13*1.0.						18*1.0.												:
		17*1.0.						•	14*1.0.		14*1.0.				4					17*1.0.	*	· O · I * C ·				17*1.0.				14*1.0.						10.40.3.		
RATIOS		13*1.0.			-				13*0 5	Ģ	13*0.5.			4	10.0*0				. ,	*		10.1.		:		16*1.0.	16*1.0.		-	13*1.0.	13*1.0.				-	17*1.0,	10*0.7	
(NO. * RAT		12*1.0.	15*1.0;			15*0.3			17*0	0	12*0.5	•		· 1	* n • O * V	-				<del>-</del>	*	, o . L * + L	*	:	-	12*1.0,	12*1.0.	*		12*1.0,	12*1.0,	٠.			10*0.2,	*	19*1	<del>-</del>
ZONE (N		11*1.0.	14*1.0	٠,	16*1.0.	14*1.0.			11*1.0.	11*1.0.	11*1.0.	10*1.0.	15*0.0	•	10 * 0 . 0 .				•	11*1.0.	o,		13*1.0.	11*0.5		11*1.0.	11*1.0	> - *		11*1.0.	<del>-</del> ;	**		•	14*1.0	13*1.0.	11*1.0	¥-
YEAR		1983/12	1983/12	2004/ 3	4	1990/ 3			1083/12	1988/ 3	19897 3	1983/12	1983/12	1985/12	10001	1988/ 3				-	1986/ 3		1986/ 3	_		*	1990/ 3			_	2004/ 3				1983/12	1983/12	1983/12	3 - /00/1
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Σ «	MOJOKERTO	MOJOKERTO	PLIA MENDALAN	PLTA MENDALAN	PLOSO	COMBANG		MADIUN	MAN TO HAY IN AM	AANISREJOSNEK	MANISREJO: NEW	CARUBAN	PONOROGO	PACITAN OCTOR	MALON MALAN	NGAET AN		JEMBER		JEMBER	JEMBER		BONDOMOSO	TANGGUL	BANYUWANGI	BANYUWANGI	SANYUWANGI	GEN-ENG GEN-ENG	SITUBONDO	SITUBONDO	SITUBONDO	4 SEMBAGOS	PAMEKASAN		BANGKALAN	SAMPANG	PAMEKASAN	รายเกา
Q	~				1.1	44		ω	_			٠	٠.	<b>.</b>			•	٥					u M	7	O	<del>ب</del>	,- (	y.	<del>-</del>	·		T.	12		- W			

column M 1: contract capacity

2: weekday average demand

column K 1: residential

2: commercial/publc

3: industry (Low Volt.)

4 : industry (Medium Volt.)

5: industry (High Volt.)

column L 1: fourteen (14) hours on a weekday

2: nineteen (19) hours on a weekday

#### b. Distribution Loss Rate

The distributon loss rates by year, by Cabang are shown on Table A-10.

The figures at the first column of the table mean the following Cabangs;

1 : Surabaya Utara 2 : Surabaya Selatan

3 : Bojonegoro 4 : Malang

5 : Pasuruan 6 : Kediri

7: Mojokerto 8: Madiun

9 : Jember 10 : Banyuwangi

11 : Situbondo 12 : Pamekasan

## c. Editing of Input Data

In accordance with various purposes, it is easily possible to edit the input data mentioned or some files of output; here, the results edited the historical input data by Cabang by category will be illustrated for Cabang 1 to 3 on Table A-11 as an example.

Besides, various historical statistics are available because the number of customers are also stored monthly. (Refer "Regional Load Forecast Programming" mentioned)

## d. Establishment of Target Data

Based upon the manner described in the preceding paragraph, the following tables were obtained.

As for residential and commercial/public uses, the multipliers which obtained as the ratios of connected capacities at March in 1989,1994 and 2004 divided by the one at Mar.1983 were applied for each Cabang.

As for industrial uses, the trend analysis including some control technique was applied to the total connected capacities of I1,I2 and I3 by each Cabang at the first place. Then the results were divided into small industries(I1+I2) and medium industries(I3) under some adequate estimation concerning the component ratios of I3. And further, using the forecasted total energy sales shown on the table and the developed forecast by Cabang, the connected capacity of I4 was forecasted by Cabang.

The further mentions will be given in the item(3).

- e. Forecasting Peak Hours Femand by Substations in a Time Series
  The demand of each substation at the weekday peak hours which was
  obtained as a final output are shown on the Table.A-12(1)~(14)
  in the form of time series.
- (2) Demand Forecasted by Substation at Nineteen (19) Hours in Mar.1994, 1999,2004

As for mentioned above, the results extracted from Table.A-12(1)~(14) are shown on Table.A-13(1)~(6) together with forecasted demand of big customers which supplied by 70 kV or 150 kV.

(3) Demand Forecast for High Voltage Big Customers

As for annual energy sales for big customers so called 14 are introduced as the energy sales of industry minus the sum of energy sales of I1~I3 for each Cabang.(Refer Table.A-14)

On this procedure, a minute modification was applied for some Cabangs so that it could obtain I4 energy stay in a reasonable range. Next, referring this results and individual information which concern I4 customers, we established a long term demand forecast concerning big sustomers. (Refer Table.  $\Lambda$ -15(1)~(7))

In order to supplement the information deficiencies concerning remote future and to make total system demand reasonable, we temporarily assumed some unknown customers called X as if they are scheduled. The results are shown on Table.A-13(1)-(6) together with demands of distribution transformers using double and single parentheses for 150 kV and 70kV customers respectively.

	1984/ 5	12.20	38.07	20.26	27.95	21.00	13.00	32.50	28.50	60.00	60.00	47.99	155.25	105.24	145.32	156.50	96.96	133.40 133.40	117.00	100.00	100.00
	1984/ 4	12.18	38.06	25.33	26.95	21.00	13.00	32.50	28 20 20 20 20 20 20 20 20 20 20 20 20 20	60.00	00.09	47.89	149.64	105.10	145.38 136.03	156.50 156.50	96.90	133.40	117.00	100.00	100.00
	1984/ 3	12.15	38.05	20.20	27.96	21.00	13.00	32.50	28.50 28.50	60.00	00.09	47.79	149.60	104.95	145.44	156.50	96.90	133,40	117.00	100.00	100.00
	994/ 2	12.13	38.04	20.16	27.97	21.00	13.00	32.50	28.50	60.00	00.09 00.09	47.69	149.57	104.81	145.50	156.50 156.50	96.90	133.40	117.00	100.00	100.00
	1984/ 1-1 1994/ 3-1	12.10	38.03	20.13	27.97	21.00	13.00	32.50	28.50	60.00	00.09 00.09	47.60	153.64	122.05	145.56	156.50	96.90	133.40	117.00	100.00	100.00
	1983/12 1	12.08	38.03	20.10	27.98	21.00	13.00	32.50	28.50	60.00	00.09	58.47	149.50	120.34	145.62	156.50	06.96	133.40	117.00	100.00	100.00
	1983/11	12.05	38.02	23.34	27.99	21.00	13.00	32.50	28.50	00:09	00.09	47.40	149.47	104.38	145.68	156.50	96.90	133.40	117.00	100.00	100.00
	1983/10 1	12.03	38.01	20.03	27.99	21.00	13.00	32.50	28.50	60.00	60.00	47.30	149.43	104.24	145.74	156.50	96.90	133.40	117.00	100.00	100.00
	1983/ 9	12.00	38.00	20.00	28.00	21.00	13.00	32.50	288 500 500	80.00	60.00	54.91	149.40	104.10	145.80	156.50	96.96	133.40	117.00	100.00	100.00
	983/ 8 989/ 3	11.97	37.99	19.97	28.01	21.00	13.00	32.50	28.50	00.09	60.09 60.09	47.10 53.73	149.37	103.96	145.86	156.50	96.90	133.40	117.00	100.00	100.00
	1983/ 7 1	11.95	37.98	19.93	28.01	21.00	13.00	32.50	28.50 28.50	60.00	\$0.00 \$0:00	47.00	149.33	103.82	145.92	156.50	96.90	133.40	117.00	100.00	100.00
(2)	983/ 6	11.92	37.97	19.90	28.02	21.00	13.00	32.50	28.50 28.50	60.00	60.00	51:35	149.30	103.67	145.98	156.50	96.90	133.40	117.00	100.00	100.00
ST TATE	983/ 5	11.90	37.97	19.87	28.03	21.00	13.00	32.50	28.50	60.00	60.00	46:80	149.27	103.53	146.04	156.50	96.90	133.40	117.00	100.00	100.00
	9837 4 9857 3 0047 3	. W.		. w ru e	000	100	- n n	0 W W	2000 2000 2000 2000	000		. 6	1001 1001	- M - O - O	446	0.00	0000	10000	400	000	0000
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Table A-10 Distribution Loss Rate

	um Ja	.36	0.73	3.49	50.08	1.25	7.89	4,4	5.68	5.43	8.92	6,61	0,00	
	1984 1998	 70	6.0	7.8	10	∪ <del>-</del> -		10	en en e	- <del></del>	<b>-</b>	'e- e-	Arr Arr	
	1984/ 4	15.50	20.01	10.01	20.38	21.61	18.10	17.69	15.84	15.57	8.85 10.00	16.76	10.57	
	984/3	15.64	20.30	10.29	10,15	10.12	10.31	17.89	10.12	15.71	8.78 10.00	16.91	10.60	
	984/21	15.79	20.60	31.26	21.02	10.18	10.27	18.09	16.17	15.86	10.00	10.36	10.64	
-	994/ 3 1	15.93	10.33	32.27	21.36	22.77	10.75	18.30	16.34	16.02	8.62	17.22	10.68	
	993/12 1	16.09	21.23	33.33 10.13	10.43	10.39	10.98	18.52	10.31	10.37	8.53	10.62	10.00	
	983/11 1	16.24	21.55	34.44	10.05	10.57	19.22	18.74	16.70	10.48	30.00	10.81	10.77	
	983/10 1	16.40	21.89	35.60	10.87	10.83	19.46	18.96	16.88	16.50	90.00	17.73	10.82	
	983/ 9 1 990/ 3 1	16.57	11.30	36.82	11.25	11.21	19.71	11.25	10.84	16.67	48 6.6 86.6	17.90	10.01	
	983/81	16.74	11.84	38.10	23.18	11.78	19.97	19.43	11.16	11.22	86. 9.7 1.7	18.08	10.92	
	983/ 7 1	16.91	22.96 12.60	39.44 12.18	12.58	12.60	12.39	12.32	17.47	17.02	9.03	18.26	10.98	
	983/ 6 1	12.27	23,34	40.84 13.80	13.66	13.81	13.26	19.93	12.24	12.26	7.88	13.09	10.07	· · · · · ·
'n	983/ 5 1 986/ 3 1	13.07	23.72	16.64	15.23	15.59	20.78	20.18	13.11	13.08	9.75	18.64	10.14	
LOSS RAT	983/ 4 1 985/ 3 1	14.16	24.12 17.30 10.01	21.61	17.48	27.00 18.18 10.01	21.06 16.09 10.02	15.81	14.32	14.19	V 0 0	8 % N N % N	~~~	
	984/ 6 1 999/ 3 2	15.23	19.45	45.46 27.65 10.00	25.30 19.78 10.05	27.55 20.89 10.04	21.35 17.69 10.08	20.72 17.31 10.08	15.34 15.34 15.534	15.29	7.46 10.00	W 9 7	2.24	
	*- <del>(-</del> *-	-	N	ю	4	ιń	<b>v</b>	~	∞	•	0	÷.	<u>~</u>	

LE A-11 (1) HISTORICAL DATA FOR LOAG FORECAST BY USE CATEGORIES IN EACH CABANG

	SURABAYA UTA	RA NUM	MBER OF ZON	E: 7		÷	
YEAR	RESIDENT	COM/PU	IND. 1,2	IND. 3	TOTAL		
				\ \frac{1}{2}			
CONNEC	TED CAPACITY	MVA				-	
(M)	2.63	2.06	4.16	9.93	8.79		
1983/ 4	63.184	62.608	24.527	O.	170.258		
83/	3.88	2.68	4.59	1.32	72.49		
983/	4.06	3.70	5.16	1.32	74.25		
983/	4.48	3.93	5.14	1.32	4.88		
7586	4.76	3.78	5.53	1.32	75.40		
983/	5.08	4.03	5.83	1.32	76.28		
83/1	5.48	4.20	5.92	1.32	76.93		
983/1	5.64	4.23	6.11	2.01	78.01		
983/1	5.95	4.33	6.13	2.91	79.33		
784/	6.39	4.44	6.21	2.91	95.62		
/ 78	8.00	4.66	6.13	2.91	81.71		
148	8.53	5.01	6.13	2.94	82.62		-
847	8.45	5.37	6.34	2.94	3.13		
847	8.96	5.35	6.22	2.94	3.48		
24/	0.35	6.66	5.91	3.55	6.48		
AVERAG	E DEMAND	3					
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983/	5.10	67	i N	82	9.15		
85/	5.57	.90	23	. 17	1.89	١.	
983/1	5.31	.42	.94	. 23	2.41		
983/1	5.83	.68	.65	90.	0.23		
983/1	4.51	86.	.01	. 60	0.11	:	
1786	5.99	0.0	.81	7	1.06		
7786	6.67	80	. 12	<u>.                                    </u>			
786	5.02	. 19	03		0.42		
84/	5.05	72	.02	ŭ	1.11		
841	4.9	78	. 43	. 54	3.67	•	
84/	49	.06	80	. 74	3.28		
			•				

USE CATEGORIES IN EACH CABANG Table A-11 (2)

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9 1 - 4 -	10 1	TOTAL
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'n	0.	m,
HISTORICAL DATA FOR LOSD FORECAST BY OVE CATEGORIES	 ພ	IND.
T	0F 20	1,2
ב ה	NUMBER OF ZONE:	IND. 1,2
- X	-	COM/PU
1 ( ) [	SELATA	ດວ
20 0 1 2	SURABAYA SELATAN	RESIDENT
		YEAR

CONNECTED CAPACITY MVA

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.72	.258	20	.92	73	.03	. 21	. 76	.33	00.	7.0	67.	.28	.12	.36	0.			5.546	۲,	.43	17	700	58	М	. 45	.82	٠,	. 26	. 9	66.	93	33	77
0	308	<b>~</b>	*~	٠	3	(1)	3	M	M	4	4	ហ	Ŋ	Ø	v			6.5	62	62	67	ស	67	2	9	7	7.1	7.7	52	76	7	78	7.
9,00	9.960	5.74	2.54	6.82	5.37	5.37	5.37	8.97	0.78	1.40	3.68	9.57	0.20	2.05	2.09			2	8.36	8.09	2.74	4.33	2.22	4.51	3.37	6.10	6.56	6.06	0.48	2.49	4.01	7.82	4.03
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Table A-11 (3)

Table A-11 (3)  Table A-11 (3)  Table A-11 (3)  TEAR  RESIDENT  CONNECTED CAPACITY  NUMBER OF IONE:  8 11 - 18  TOTAL  CONNECTED CAPACITY  NVA  1983 / 4  1983 / 4  1983 / 4  1983 / 4  1983 / 4  1984 / 2  1984 / 2  1985 / 4  19	### ### ##############################
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able A-11 (3)  HISTORICAL DATA FOR LOAD F  S BOJONEGORO  YEAR  RESIDENT  CONNECTED CAPACITY  983/4  983/4  7.550  2.275  9.406  983/12  8.577  2.297  0.406  983/12  8.577  2.297  0.406  983/12  8.689  2.400  0.449  983/12  8.689  2.400  0.449  983/12  8.689  2.400  0.449  983/12  8.689  2.400  0.449  983/12  8.689  2.400  0.449  983/12  8.689  2.400  0.449  983/12  8.689  2.400  0.449  983/12  8.689  2.693  0.032  983/13  1.860  0.516  0.032  983/14  1.800  0.516  0.032  983/17  1.908  0.509  0.034  983/17  1.931  0.509  0.035  984/17  1.931  0.509  0.035  984/17  1.931  0.509  0.035  984/17  1.931  0.509  0.035  984/17  1.931  0.509  0.035  984/17  2.153  0.526  0.040  984/17  2.153  0.526  0.040	able A-11 (3)  HISTORICAL DATA FOR LOAD F  S BOJONEGORO  YEAR  RESIDENT  CONNECTED CAPACITY  WAS  9837 4 7.580  9837 5 7.455  9837 6 7.825  2.297  0.416  9837 7 8.689  9847 2 8.689  9847 2 8.689  9847 2 8.689  9847 2 8.689  9847 3 8.067  9857 6 0.449  9857 6 7.825  0.449  9857 7 8.081  9857 7 8.081  9857 8 8.689  9857 8 8.689  9857 9 8.469  9857 9 8.469  9857 9 8.689  9858 9 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
able A-11 (3)  HISTORICAL DATA FO  HISTORICAL DATA FO  S BOJONEGGRO  NUMB  YEAR  RESIDENT  CONNECTED CAPACITY  983/ 3  983/ 4  7.255  2.178  983/ 5  983/ 6  7.850  2.295  983/ 6  983/ 6  983/ 6  984/ 2  8.689  984/ 1  8.965  984/ 3  985/ 6  986/ 4  985/ 6  985/ 6  986/ 7  1.908  986/ 8  986	able A-11 (3)  HISTORICAL DATA FO  HISTORICAL DATA FO  S BOJONEGGRO  NUMB  YEAR  RESIDENT  CONNECTED CAPACITY  983/4  983/4  7.255  2.178  983/4  7.850  2.295  983/4  8.689  2.408  983/6  984/2  984/2  985/5  984/2  985/5  986/6  986
able A-11 (3)  HISTORIC  TEAR  BOJONEGGRO  TEAR  RESIDENT  CONNECTED CAPACITY  983/ 3 7.255  983/ 4 7.405  983/ 4 7.405  983/ 4 7.405  983/ 6 7.825  983/ 6 7.825  984/ 2 8.687  984/ 2 8.687  984/ 2 8.687  984/ 3 9.663  985/ 4 9.159  984/ 5 7.1008  985/ 6 9.663  985/ 6 1.906  985/ 7 1.908	able A-11 (3)  HISTORIC  TEAR  S BOJONEGGRO  CONNECTED CAPACITY  983/ 5 7.255  983/ 5 7.825  983/ 5 7.825  983/ 5 7.825  983/ 6 7.825  984/ 2 8.887  984/ 2 8.887  984/ 2 9.653  984/ 5 9.653  984/ 5 9.653  984/ 5 9.653  984/ 5 9.653  984/ 5 9.653  984/ 6 9.653  984/ 6 9.653  985/ 6 1.808  983/ 6 1.808  983/ 6 1.908  983/ 7 1.808  983/ 7 1.808  983/ 7 1.808  983/ 7 1.908  983/ 7 1.908  983/ 7 2.003  983/ 7 2.003  983/ 7 2.003  983/ 7 2.003  983/ 7 2.003  983/ 7 2.003  983/ 7 2.003  983/ 7 2.003  983/ 7 2.003  983/ 7 2.003  983/ 7 2.003  983/ 7 2.003  983/ 7 2.003  983/ 7 2.003  983/ 7 2.003  983/ 7 2.003
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SUMMARY OF SUBSTATION LOAD FORECAST

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SUMMARY OF SUBSTATION LOAD FORECAST

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	٠	4 69	13.94 12.
101.10 100.20 44.11 101.10 100.20 410.	.20 41.9	3.87	5.30 52
99/ 3 41.25 49.63 80.88 81.26 * 57.65 47.	2.87	90.00	5.0157

SUMMARY OF SUBSTATION LOAD FORECAST

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	KRIAN		03150		SMAMANA		A ANG P	TI ANG	KETINTANG	
	-	EVENING	DAYTIME	EVENING		EVENING	TIME	EVENING	IME	EVENING
1984/ 3	0.0	0.0		0.0	0.0	0.0	0.0	ċ	0	0.0
841		0.0		0.0	•	0.0				
178	•	0.0	0.0	0.0		0.0			•	0.0
1984/ 6	0.0	0.0		0.0	0.0	•	0.0	0.0	0.0	
85/	•	0.0	0.0	0.0	0.0	0.0			•	•
86/	۳.	•	0.0	0.0	0.0	0.0	•	•		
728	*	ø	0.0	0.0	0.0		•	•	٠	•
88/	.0	~	0.0	0,0	0.0		0.0			
897	2.9	0	0.0	0.0	0.0	0.0	•		•	
106	5.3	W	0.0	0.0	•	0.0	'n	•		- 4
91/	7.6	M	0.0	0.0	M		٥.	12.71	•	
92/	0.4	N	0.0	0.0	38.95	38.20	13.82	•		•
93/	3.5	m	0.0	0.0		4.2	ω	N	•	
146	6.9	~	0.0	•	52.12	0	W	ъ.		•
/566	0.6	<del>~-</del>	0.0	0.0	59.61			o		
196	4.7	~~		• •	•	65.20	24.70	N		•
1266	9.2	-3	0.0	0.0				7	0.0	
1866	4.9	*		ิณ	٥.	- 6	3.7	1		• •
1666	9	O	0	7.	0		39,50	7		
/700	35.06	37.35		94.52	103.41	'n	4.0	63.20	М	
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	TROSORIO TROSORIO			1	₹ 200	אר בי				
	XIL.X	-	AYTI	EVENING	Σ	EVENING	•			
84/	0.0		0.0	0.0	104.00					
8	0.0		٠.	0.0	•	÷				
1986	0.0		0.0	0.0		133.05				
984/	0.0	•	0.0	0.0	105.00	133.34				
985/	0.0	•	0.0	0.0						
7986	0.0	•	0.0	0.0	131.53	164.55 *		*		
7286	0.0	٠	٠,	0.0	151.13				-	
988/	0		-	0	0.72	212.52 *				
1989/ 3	•	0	0.0	Ţ.,	•	9		٠		
/066			•	0	м -	74.3				
991/	0.0	٠	,	0	Ø	-				
992/			•	0.0	05.7	ŝ				
993/			٠	0.0	20.7	397.71				
1566		•	0	0.0	01.4	4				
7566	•	•	٠	0.0	S	0				
1966		•	-	0.0	22.1	4				٠
1266	•	0	•	0.0	92.9					
7866	ĸ	5.0	٠	0.0		* 42.902				
/666	19.20	17.57	。	0.0		786.69 *				
1700	ស	8	32.02	34.89 *	1295.95	1275.33 *				

Table A-12(4)  SUMMARY OF SUBSTATION LOAD FORECAST  BOJONEGORO  BOJONE  BOJONEGORO  BOJONE  BOJONEGORO  BOJONE  BOJONEGORO  BOJONEGORO  BOJONEGORO  BOJONEGORO  BOJONEGORO  BO								1			
BOJONEGORO  BOJONEGORO  BOJONEGORO  BOJONEGORO  BOJONEGORO  BABAT  LAMDNGAN  BOJONEGORO  BOJONEGORO  BOJONEGORO  BABAT  LAMDNGAN  BOJONEGORO  BAYTIME  DAYTIME  EVENING  DAYTIME  BOJONEGORO  BAYTIME  BOJONEGORO  BAYTIME  BOJONEGORO  BAYTIME  BOJONEGORO  BAYTIME  BOJONE  BOJO	Table A-12	(4)			· .						
BOJONEGORO		SUMI	9	LOAD	RECAST	:	3 1			٠	
BOJONEGORO  BABAT  BOJONEGORO  BARAT  LAMONGAN  DAYTINE  EVENING  BOJONEGORO  BABAT  LAMONGAN  TUBAN  TUBAN  TUBAN  TUBAN  TUBAN  TUBAN  BOJONEGORO  BABAT  LAMONGAN  TUBAN  TUBAN  TUBAN  BOJONEGORO  BABAT  LAMONGAN  TUBAN  TUBAN  BOJONEGORO  BABAT  LAMONGAN  TUBAN  TUBAN  BOJONEGORO  BATTINE  EVENING  DAYTINE  EVENING  DAYTINE  EVENING  DAYTINE  DAYTINE  EVENING  DAYTINE  DAYTINE  EVENING  DAYTINE  DAYTING  DAYTONG  DAYTING  DAYTING  DAYTING  DAYTING  DAYTING  DAYTING  DAYTONG  DAYTING  DAYTONG  DAYTING  DAYTING  DAYTING  DAYTING  DAYTING  DAYTING  DAYTONG  DAYTING  DAYTING  DAYTING  DAYTING  DAYTING  DAYTING  DAYTONG  DAYTING  DAYTING  DAYTING  DAYTING  DAYTING  DAYTING  DAYTIN											
BOJONEGORO BAYTIME EVENING DAYTIME EVENING DAY	100	NEGORO					- N.	. :			
DATING PAYTINE EVENING DAYTING		L TO		• • •		- X	-	11004		000	C C C C
1.19       2.79       0.81       2.00       0.048       1.28       0.0		DAYTIME	EVENI	Σ	VENIN	DAYTIME	VENIN	Σ	_	DAYTIME	JUNEGORD IE EVENING
1.19       2.79       0.80       1.99       0.48       1.28       0.0       0.0         1.18       2.77       0.81       2.01       1.51       2.28       0.0	1984/ 3	7	N	80	2	0.48	1.2	0	0.0	2.47	20.9
3       ***       1.18       2.77       0.80       2.00       1.52       2.28       0.0       <	ė		-	00	٥.	*	ú	. •	· •	4.	90.9
3     ***     1.18     2.76     0.80     1.96     0.58     1.49     0.0     0.0       3     1.40     2.84     0.82     1.97     0.70     1.70     0.0     0.0       3     1.69     2.03     0.87     1.79     0.0     0.0       3     2.72     4.00     1.29     2.26     0.60     1.21     0.70       3     2.72     4.00     1.29     2.26     0.60     1.21     0.70     1.34     4       3     2.72     4.00     1.29     2.26     0.60     1.21     0.70     1.34     4       3     2.72     4.00     1.29     2.26     1.36     1.36     1.36     1.36       3     3.93     5.17     1.76     2.77     0.77     1.38     1.48     1.88       3     4.40     4.76     5.77     0.94     1.60     1.42     2.15     3.23       4     4.76     6.17     2.13     3.23     0.94     1.60     1.42     2.43       3     5.33     7.05     2.27     3.44     1.05     1.73     2.43     1.73       3     5.33     7.05     2.55     3.64     1.05     1.76     2.73<	1984/ 5	1:1	8 2.7		٥.		ú	. •	. •	ī	7.06
3 **     1.23     2.73     0.82     1.97     0.70     1.70     0.0     0.0       3 1.40     2.84     0.89     1.97     0.70     1.70     0.0     0.0       3 2.72     4.00     1.05     2.01     0.52     1.11     0.70     1.34     4.4       3 3.55     4.57     1.29     0.60     1.21     0.86     1.50     1.34       3 3.55     4.57     1.24     0.60     1.21     0.86     1.53       3 3.93     5.17     1.74     2.77     0.77     1.38     1.68     1.68       3 4.40     5.72     1.96     3.01     0.94     1.46     1.42     2.15     3.23     0.94     1.46     1.50     2.15     3.23       3 5.6     6.61     2.27     3.44     1.05     1.73     2.43     1.50     2.55       3 5.3     7.05     2.41     3.65     1.16     2.43     1.70     2.56     1.7       3 5.8     8.00     2.27     1.48     2.69     1.78     2.69     1.7       3 5.4     1.29     2.11     2.85     2.74     1.95     2.92     1.6       3 5.2     1.48     2.27     1.48     2.27     1.5     2.	Ę	_	2.7	œ	٥.		•			ń	7.06
3     1.40     2.84     0.89     1.97     0.70     1.70     0.0     0.0       3     1.69     3.09     1.01     2.03     0.87     1.98     0.0     0.0       3     2.14     3.48     1.05     2.20     0.60     1.34     4       3     2.72     4.00     1.29     2.26     0.60     1.30     1.34     4       3     3.35     4.57     1.54     2.53     0.69     1.30     1.02     1.58     5       3     4.40     5.72     0.69     1.30     1.40     1.68     1.50       3     4.40     5.72     0.94     1.60     1.42     2.15       3     4.40     5.72     0.94     1.60     1.42     2.15       3     5.06     6.61     2.27     3.44     1.05     1.73     1.52     2.15       3     5.06     6.61     2.27     3.44     1.05     1.73     1.52     2.50       3     5.37     2.64     1.75     2.43     1.52     2.56     11       3     5.87     6.15     2.92     1.44     1.27     2.14     1.73     2.92       3     6.47     2.92     4.39	1985/ 3 **	N	2.7	0.82		Ŋ	4	. •		ø	6.19
3     1.69     3.09     1.01     2.03     0.87     1.98     0.0     0.0       3     2.14     3.48     1.05     2.01     0.52     1.11     0.70     1.34     4       3     2.72     4.00     1.29     2.26     0.60     1.21     0.86     1.50     5       3     3.93     5.17     1.76     2.77     0.69     1.02     1.08     1.08       3     4.40     5.72     1.96     3.01     0.85     1.46     1.30     2.01     8       3     4.76     6.17     2.13     3.23     0.94     1.60     1.42     2.15     9       3     5.06     6.17     2.27     1.05     1.73     1.52     2.30     9       3     5.05     6.17     2.44     1.05     1.73     1.51     2.43     10       3     5.05     6.61     2.27     1.73     1.70     2.56     11       3     5.59     4.05     1.48     2.27     1.78     2.92     11       3     5.27     1.29     4.39     1.59     2.40     1.95     2.92     16       3     5.29     1.29     4.37     2.11     2.28 <td< td=""><td>1986/ 3</td><td>7. T</td><td>œ</td><td>0.89</td><td>1.97</td><td>۲-</td><td>~</td><td></td><td>· •</td><td>οį</td><td>6.51</td></td<>	1986/ 3	7. T	œ	0.89	1.97	۲-	~		· •	οį	6.51
2.14     3.48     1.05     2.01 *     0.52     1.11 *     0.70     1.34 *     4       3.35     4.00     1.29     2.26     0.60     1.21     0.86     1.50     5       3.35     4.57     1.54     2.53     0.69     1.30     1.02     1.68     6       3.93     5.17     1.76     2.77     0.77     1.38     1.18     7     1.68       3.93     5.72     1.96     3.01     0.85     1.46     1.30     2.01     8       4.40     5.72     2.13     3.23     0.94     1.60     1.42     2.15     9       3     5.06     6.61     2.27     1.05     1.73     1.52     2.30     9       3     5.33     7.51     2.55     4.04     1.57     2.43     10       3     5.59     7.51     2.68     4.04     1.78     2.27     1.78       3     5.51     2.93     4.39     1.59     2.40     1.95     2.92     16       3     5.47     9.11     2.92     1.78     2.92     1.5       3     5.47     4.39     1.59     2.40     1.95     2.92     16       3     5.47     5.	1987/ 3	ø	3.0	1.01	0	ထ	ø	•	•	'n	7 11
3     2.72     4.00     1.29     2.26     0.60     1.21     0.86     1.50     1.68     1.50     1.68     1.68     1.68     1.68     1.68     1.68     1.68     1.68     1.68     1.68     1.68     1.68     1.85     7       3     4.40     5.72     1.96     3.01     0.85     1.46     1.30     2.01     8       3     4.76     6.17     2.27     3.23     0.94     1.60     1.42     2.15     9       3     5.06     6.61     2.27     1.73     1.52     2.30     1       3     5.53     7.51     2.41     3.44     1.15     1.87     2.43     1       3     5.59     7.51     2.58     4.04     1.78     2.69     11       3     6.15     8.56     1.29     1.59     2.40     1.78     2.92     1       3     6.47     9.11     2.92     1.59     2.92     1     2.92     1       3     5.42     4.39     4.37     2.11     2.85     2.92     1       3     2.92     2.11     2.85     2.92     1     2.92     1       4     3.42     4.37     2.11     2.8	1988/ 3	٣.	3.4	1.05	٠	'n	4.11 *	۲.	M	•	7.94
3.35     4.57     1.56     2.53     0.69     1.30     1.02     1.68       3.93     5.17     1.76     2.77     0.85     1.18     1.85     7       3.93     5.17     1.76     2.77     0.85     1.18     1.85     7       3.01     0.85     1.46     1.30     2.01     8       3.02     0.94     1.60     1.42     2.01     8       3.02     6.61     2.27     3.44     1.05     1.73     1.52     2.30       3.02     6.61     2.68     4.06     1.26     2.00     1.70     2.56     11       3.25     6.15     8.50     2.68     4.04     1.57     2.27     1.78     2.69     11       3.25     1.29     4.39     4.39     2.40     1.95     2.92     16       3.25     1.29     2.11     2.85     2.27     2.92     16	1989/ 3	~	0.7	1.29	'n	'n	1.21	œ	S	27.5	8.97
3.93     5.17     1.76     2.77     0.85     1.46     1.30     2.01     8       4.40     5.72     1.96     3.01     0.94     1.46     1.30     2.01     8       3.23     6.17     2.27     3.44     1.05     1.73     2.30     2.30       3.33     7.05     2.27     3.44     1.05     1.73     1.52     2.30       3.59     7.05     2.55     3.85     1.26     2.00     1.70     2.56     11       3.59     6.15     8.50     2.68     4.04     1.37     2.90     1.78     2.95     1.48       3.50     1.29     4.39     1.59     2.40     1.95     2.92     16       3.25     1.29     2.40     2.85     2.25     16	1990/ 3	M	4.5	1,54	'n	÷	1 30		v	9.60	10.08
6.17     2.01     0.85     1.46     1.30     2.01     8       7.56     6.17     2.13     3.23     0.94     1.60     1.42     2.15     9       7.50     6.61     2.27     3.44     1.05     1.73     1.52     2.30     9       3     5.33     7.51     2.55     3.85     1.26     2.00     1.70     2.43     10       3     5.59     7.51     2.55     3.85     1.25     2.90     1.78     2.56     11       3     6.15     8.53     2.80     4.22     1.48     2.27     1.87     2.91     12       3     6.47     9.11     2.93     4.39     1.59     2.40     1.95     2.92     16       3     8.54     12.90     3.42     4.87     2.11     2.85     3.25     16	1991/ 3	ς.		1.76	Ļ	7	1.38	*-	ထ	79.2	11.17
4.76     6.17     2.13     3.23     0.94     1.60     1.42     2.15     9       5.06     6.61     2.27     3.44     1.05     1.73     1.52     2.30     9       3     5.33     7.05     2.41     3.42     1.15     1.26     2.00     1.70     2.43     10       3     5.87     8.00     2.68     4.04     1.37     2.14     1.78     2.56     11       3     6.15     8.53     2.26     1.48     2.27     1.87     2.92     12       4.39     1.59     2.40     1.95     2.92     16       3     8.54     12.90     3.42     4.87     2.11     2.85     3.25     16	1	*	5.7		0	æ	1.46	M	٥.	8.51	12.20
5.06     6.61     2.27     3.64     1.05     1.73     1.52     2.30     9       7.3     7.05     2.41     3.65     1.15     1.87     1.61     2.43     10       3     5.59     7.51     2.55     3.85     1.26     2.00     1.70     2.56     11       3     5.87     8.00     2.68     4.04     1.37     2.14     1.78     2.69     11       13     6.15     8.53     2.80     4.22     1.48     2.27     1.87     2.91     12       13     6.47     9.11     2.93     4.39     1.59     2.40     1.95     2.92     16       13     8.54     12.90     3.42     4.87     2.11     2.85     3.25     16	1993/. 3	٠.	6.1	2.13	ď	o.	1.60	4	-	9.25	13,15
3     5.33     7.05     2.41     3.65     1.15     1.87     1.61     2.43     10       3     5.59     7.51     2.55     3.85     1.26     2.00     1.70     2.56     11       3     5.87     8.00     2.68     4.04     1.37     2.14     1.78     2.69     11       13     6.15     8.53     2.80     4.22     1.48     2.27     1.87     2.81     12       13     6.47     9.11     2.93     4.39     1.59     2.40     1.95     2.92     16       13     8.54     12.90     3.42     4.87     2.11     2.85     2.28     3.25     16	1994/ 3	•	9	N	4.	0	1.73	S	M	06.6	14.08
3     5.59     7.51     2.55     3.85     1.26     2.00     1.70     2.56     11       3     5.87     8.00     2.68     4.04     1.37     2.14     1.78     2.69     11       5     6.15     8.53     2.80     4.22     1.48     2.27     1.87     2.81     12       6     3     6.47     9.11     2.93     4.39     1.59     2.40     1.95     2.92     12       7     3     4.87     2.11     2.85     2.28     3.25     16	1995/ 3	M	3 7.0	٧.	٧	₩	œ	1.61	4	10.50	0
3     5.87     8.00     2.68     4.04     1.37     2.14     1.78     2.69     11       7     6.15     8.53     2.80     4.22     1.48     2.27     1.87     2.81     12       6     6.47     9.11     2.93     4.39     1.59     2.40     1.95     2.92     12       7     3     4.87     2.11     2.85     2.28     3.25     16	Ŀ	'n	6	ń	œ	S	٥,		M.	11.09	15.93
7.3 6.15 8.53 2.80 4.22 1.48 2.27 1.87 2.81 12 7.3 6.47 9.11 2.93 4.39 1.59 2.40 1.95 2.92 12 7.3 8.54 12.90 3.42 4.87 2.11 2.85 2.28 3.25 14	1	ω	8.0	Ó	0		٠.		ø	11.69	007
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	2004/ 3	'n	12	,	٠	. • .	∞	Ņ	2	M	23.87

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KEBONAGUNG  DAYTIME  S.41  11.86  4.29  6.16  5.47  11.86  4.29  6.16  5.47  11.96  4.29  6.16  5.21  11.96  4.29  6.16  5.21  5.47  11.96  4.30  6.25  5.25  6.25  5.45  11.96  4.30  6.25  5.25  6.25  5.45  11.26  6.25  5.45  11.26  6.25  5.45  6.25  5.45  6.25  5.45  6.25  5.45  6.25  5.45  6.25  5.45  6.25  5.45  6.25  5.45  6.25  6	NATION   Continue
KEBONAGUNG  KEBONAGUNG  KEBONAGUNG  KEBONAGUNG  KEBONAGUNG  KEBONAGUNG  KEBONAGUNG  KEBONAGUNG  KERNING  KERNIN	KEBÜNAGUNG  KEBÜNAGUNG  KEBÜNAGUNG  KATINE  KVANING  KVAN
FEBDNAGUNIG	REBONAGUNG POLEHAN BLIMBING FURING ANTIME FU
KEBONAGUNG KEBONAGUNG KEBONAGUNG KATTHE KVENING KATTHE K	KEBONAGUNG KEBONAGUNG  KEBONAGUNG  KEBONAGUNG  KEBONAGUNG  KEBONAGUNG  KERNING  KATTINE  KATT
KEBONAGUNG  BOATIME  FYATIME	KEBDUAGUNG  DAYTIME  EVENING  DAYTIME  DAYTIME  EVENING  DAYTIME  C. 29  C. 16  S. 27  T. 19  C. 29  C. 11  C. 29  C. 20
KERDNAGUNG  POLEHAN	KEBONAGUNG  POLEHAN  BLIMBING  DATIME EVENING  044, 5  5.41  11.86  4.29  6.16  5.23  5.25  5.45  11.96  4.70  6.16  5.29  5.70  5.89  5.90  5.9
KEBONAGUNG  POLEHAN  KEBONAGUNG  A-29  A-30  A-29  A-31  A-29  A-30  A-31  A-32  A-31  A-32  A-31  A-32  A-39  A-3	KEBDAAGUNG  DAYTIME EVENING DAYTIME  4,29 6,16 5,41 11,86 4,29 6,16 5,20 8,47 8,62 11,96 4,76 6,29 8,22 11,96 4,76 6,29 8,22 11,96 6,19 8,22 11,96 8,22 11,97 8,23 8,23 8,33 8,33 8,33 8,34 8,36 8,36 8,36 8,36 8,36 8,36 8,36 8,36
KEBONAGUNG  AYTIME  5.41  11.86  4.29  6.16  5.42  11.86  4.29  6.18  6.18  6.19  6.19  6.18  6.19  6.	REBONAGUNG  BAYTIME  S.47  11.86  4.29  6.16  984/ 5  984/ 5  986/ 6  986/ 6  986/ 7  986/ 7  986/ 7  986/ 8
KEBONAGUNG  AVTINE  BAYTINE  CVF 11.86  CVF 11.87  CVF 11.88  CVF 11.88  CVF 11.88  CVF 11.88  CVF 11.88  CVF 11.89  CVF	KEBONAGUNG DAYTINE DAY
KEBONAGUNG  PAYTIME EVENING  PAYTIME EVE	XEBONAGUNG DAYTIME EVENING 984/ 3 9864/ 5 9864/ 5 9864/ 5 9886/ 5 9886/ 3 9886/ 3 9886/ 3 9986/ 3 9886
KEBONAGUN  AYTIME  AYTIME  AYTIME  BAYTIME  BAYTIME  BAYTIME  A 11.25  BAYTIME  BAYTIME  BAYTIME  BAYTIME  BAYTIME  BAYTIME  CO.50  CO.	XEBONAGUN 984/ 3 984/ 4 984/ 5 984/ 5 984/ 5 986/ 5 988/ 3 988/ 3 999/ 3 999/ 3 999/ 3 999/ 3 998/ 3 988/ 3
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KERT	VENING DAYT	.82	.83	.86	. 87	.01	. 22	50	.83	.23	. 72	. 32	. 03	. 60	.18	52	. 42	. 09	7.76 5	. 42	. 10		4								-		:											
3	AYTIME	7	7	7.	4	Ŋ	9	~	0	τ-	1.43	7	•	7	^	Τ	'n	0.		æ		-			:					*														
1	EVENING	1 24	1.25	1 29		•	- •			. 4				•	•	•	- •				. •			Z	5.6	~	0. 9	9	α (1)	,	25.12	٠ ص	φ. Ω	7	S	~	8	5.1	4	2.6	1 4	0	0	
α:	AYTIM	9	ò	۷,	Ś	۲-	c,	ς-	4	۲-	Τ.	٧	٠.	٥	-	۲.	'n	Ò	6.62	7	۲,	- 2	¥	Σ	O	~	N	M	<b>7</b>	M	13.50	9	ο\ ( α) (	7	8.0	0.2	8	8	5.6	7	٨	5	2	. (
	N N N N	٥	O,	0	0	ó	7	0	ø	N	٥	Ý	M	٧,	8.6	8	3 4	6.1	29.02	2.0	7 6						•	•		7	75.0	ø	۲.	œ,	o.	Ò	ú	М	S	œ	2.07	M	^	•
ULUNGA		ø	V	۲.	٧.	0	Ŋ	٧	٥.	œ		Ø	٥	٨	9.0	-	œ	5	7 7	٥	3		Ž	AYTIM	0	0.0	0	0	0	N	0.28	~	M.	4	s	٥	٧-	œ	٥	-	N	7	^	٠,
	EVENIN	9.9	6.7	8 8	8.9	2.6	8	10.0	11.4	13.1	15.0	17.1	19.4	22.2	25.3	28.8	32.0	35.4	38.88	2 2	0		LEK	EVENIN	1.7	1.7	<b>~</b>	1.7		2 0	2 14	2.2	2	2	2.4	2.5	2.6	2.8	2.9	0 10	-	N	1	•
IRI	AYTIM	ø	9	7	۲-	N	o	5.8	∞	0	9.38	9	Ý	9.7	٥	7 6	2	4	27.74	ö	7.6		RENGGA	YTIM	9	٧	9	9	^	ω	0.0	٥.	0	•	1.27	M)	1.51	1.63	1.77	1 91	0	2 2 3	۳,	
		/ 58	٠.	178	84/	857	198	877	7886	989/	106	991/	1266	1866	1766	1566	1966	126	1998/ 3	/66	/ 50				847	847	7 986	7 8 6	9857	7986	1987/ 3	988/	7686	/066	9917	992/	1866	1766	95/	1966	1266	7866	/ 60	1111

SUMMARY OF SUBSTATION LOAD FORECAST

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Table A-12(9)

ž.	MOJOKERTO			MENDALAN	PL050		JOMBANG		MOJOKERTO	CERTO
	DAYTIME	EVENIN	DAYTIME	EVENING	DAYTIME	EVENING	DAYTIME	EVENING	DAYTIME	EVENING
1984/ 3	4.92	7.0	1.25	2.57	0.09	0.23	0.0	0.0	6.26	9.83
1984/ 4	7.96		1.25	2.57	0.09	0.23	0.0	0.0	6.30	9.96
14	86.4	7.22	1.28	5.64	0.09	0.24	0.0	0.0	6.35	10.10
178	66.4		1.30	2.67	0.10	0.24	0.0	0.0	6.39	10.18
1985/ 3 **	5.72	8.48	1.42	2.79	0.10	0.25	0.0	0.0	7.24	11.52
	6.86	m	1.58	2.95	0.11	0.26	0.0	0.0	8.56	13.55
1987/ 3	8.21	'n	1.77	3.12	0.12	0.27	0.0	0.0	10.10	15.93
	9.77	15.01	1.98	3.31	0.13	0.28	0.0	0.0	11.89	18.60
	11,55	ω	2.21	3.51	0.14	0.29	0.0	0.0	13.91	21:60
1990/ 3	13.55	0.9	•	0.75 *	0.15	0.29	2.05	2.95 *	16.14	24.90
	15.75	24.28	95.0	0.82	0.16	0.30	2.18	3.03	18.55	28.43
	ú	8.0	0.55	0.91	0.16	0,30	2.28	3.08	21.21	32.33
1993/ 3	21.03	2.2	99:0	1.03	0.16	0.30	2.40	3.13	24.25	36.69
	Š	36.85	0.80	1.17	0.17	0.29	2.53	3.20	27.70	41.52
19957. 3	27.76	٥.	0.99	1.36	0.17	0:30	2.67	3.28	31.59	46.85
2	1 7	4	1.22	1.59	0.17	0.30	5.84	3.37	35.96	52.67
	36.11	H)	1.52	1.89	0.17	0.30	3.03	3.47	40.83	58.98
1998/ 3	٥.	ò	1.90	2.25	0.18	0.30	3.27	3.64	46.26	65.84
1999/ 3	46.21	4	2.37	2.70	0.18	0.31	3,63	3.91	52.39	73,34
2004/ 3	78.39	104.25	4.71	4.62 *	0.24	0.35	7.56	7.20 *	90.90	116.42

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	FVENING	2.4	U	٠,	2.64	ò	7	ο,	ò	W	٠,	6		'n	4	M	•	0	00	'n	ò															•								
טפט זטט	) Σ	C		4-	1.15	М	S	ω	Ŋ	Ÿ.	٩.	Ŋ	4.02	'n	Τ,	۲.	7	٥.		w	M																			-	-			
	EVENING	0	Ś	'n	0.55	٧.	۲.	ω,	0	•	1.25	1.41	ហ	<b>~</b> -	œ	.0	Τ.	M	7	'n	Ġ		-	٠																				
ACTTA	· F	0	0	N	0.21	N	2	£-3	7	7	5	ò	۵.	7	∞,	6.	٥.	۲.		$\omega$	S	 -																						
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	EVENING	-	-	₹-	1.13	ď	4	φ	¢.	N	'n	۰	3.15	7	œ	_	Ŋ	ω.	N	5	æ	-	1	Z :	31	S	ω	S	6.5	œ	7	1.U.	٠ د		kJ N	7.1	0	8.4	8	3.0	7.4	61.87	7.9	9
ONORO	Σ	7 0	٠,	Ŋ	0.51	S	٥	١	0	0	1.19	М	1.51		∞.	-	'n	v	2.87	•-	v	•	7042	ΞΙ	•	×	^	٥.	٩.	7	0	Ò	9	ω ω	0	S.	۰. در	7	3	6.9	0.8	45.08	ς. N	75.41
	EVENING	7 0	7	7	97.0	'n	Ś	Ý	άĐ	ø.	1.04	1.17	1.31	1.44	1.57						7		4	⊸ ં		•	٠	0.0	٠	•	Ο.							œ	O.	O	٥	2.00		0
401194	DAYTIME	C		Υ.	0.19	Ŋ	N	K)	M	7	7	S	6	ø	۲-	œ	6	Ò	1 02	0		-		- - (	•	٠	•	٠	٠	0	0		۲.	ထ	٥.	Ò	0	•		S	S	1.30		
Σ	EVENING	0	٥	_	10.25	5	3	0.7	4.0	3.6	7 .	7		7.	3.9	7.9	0.6	9	6.7	 	6.7			<b>⊸</b> a '	ė	٠	٠	٠		0.0		٥.	0	Τ.	Τ.	v	ú	Ġ	₩,	М	м	2,42	7	٥.
SREID	N I WI	80	•	٥	5.96	٥	Ŷ	æ	9 34	۲,	•	Ø	Ÿ	6.0	^	-	23.71	6 5	29.53	2	2 2	E U C	25.000	AYILM	٠	٠.				٠		0	o.	0	~~	τ-	ď	S	m	m	М	•	S	M
		2 /7861	ιœ	84/		85/	1986/ 3	877	88/	168	706	911	927	93/	1766	95/	196	126	786	/666	/70				7	V + 70	84/	847	985/	7986	7286	988/	7886	/066	9917	1266	1266	1766	7566	1966	1266	1998/ 3	1666	/500

Table A-12(11)

9 JEMBER

	JEMBER		LUMAJANG	·	BONDOWGSO		TANGGUL		JEMBER	<b>6</b> %
	DAYTIME	EVENING	DAYTIME	EVENING	DAYTIME	EVENING	DAYTIME	EVENING	DAYTIME	EVENING
19847.3	3.25	7.08	1.06	2.21	0.0	0.0	0.0	0.0	4.32	9.29
1984/ 4	3.30	7.19	1.07		0.0	0.0	0.0	0.0	4.38	77.6
1984/ 5	3.36	7.32	1.10	2.32	0.0	0.0	0.0	0.0	•	49.6
1984/ 6	3.47	7.48	1.12	2.36	0.0	0.0	0.0	0.0	4.59	9.84
1985/ 3 **	3.86	8.10	1.22	2.54	0.0	0.0	0.0	0.0	5.08	10.65
1986/ 3	3.61	4.35	1.43	2.87	0.80	1.67 *	0.0	0.0	5.85	11.90 *
1987/ 3	4.13	8.19	1.66	3.22	0.95	1.91	0.0	0.0	6.73	13,32
1988/ 3	4.71	9.12	1.91	3.61	1,13	2.19	0.0	0.0	7.76	14.93
1989/ 3	5.37	10.15	2,21	40.4	1.35	2.52	0.0	0.0	8.93	16.72
1990/ 3	3.40	6.32 *	2.54	4.53	1.62	2.90	2.71	* 96.7	10.26	18.71 *
1991/ 3	3.84	7.00	2.93	5.08	1.94	3.35	3.07	5.49	11.78	20.93
1992/ 3	4.33	7.73	3.39	5.70	2.33	3.87	3.46	20.9	13.50	23.38
1993/ 3	4.85	8.50	3.91	9.40	2.81	87.5	3.88	6,68	15.45	26.06
1994/ 3	5.39	9.31	4.52	7.18	3,38	5.19	4.33	7.33	17.63	29.01
1995/ 3	5.97	10.14	5.23	8.06	4.07	6.03	4.81	8,00	20.08	32.23
1996/ 3	25.9	11.03	6.03	40.6	06.4	6.95	5.31	8.72	22.82	35.74
1997/ 3	7.25	12.00	26.9	10.14	5.78	7.91	5.88	9.50	25.89	39.55
19987 3	8.02	13.05	8.05	11.36	6.71	8.90	6.53	10.36	29.31	43.67
1999/ 3	8.88	14.20	9.29	12.73	7.68	06.6	7.26	11.30	33,11	48.13
2004/ 3	15.06	21.51	18.88	22.42	12.92	14.97	12.61	17.40	29.47	76.30
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SUMMARY OF SUBSTATION LOAD FORECAST BANYUWANGI

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		DAYTIME	EVENING	DAYTIME	EVENING	DAYTIME	EVENT
1984/ 3		1.68	3.86	0.0	0.0	1.68	m
1984/ 4	:	1.71	3.94	0.0	0.0	1.71	M
1984/ 5		1.75	70.7	0.0	0.0	1.75	4.
1984/ 6	•	 	4.18	0.0	0.0	1.83	4.
1985/ 3 *	#	2.11	4.66	0.0	0.0	2.11	4
1986/ 3		2.56	5.38	0.0	0.0	2.56	'n
1987/ 3		3.12	6.24	0.0	0.0	3,12	9
1988/ 3		3,85	7.25	0.0	0.0	3.85	~
1989/ 3		08.4	8,48	0.0	0.0	4.80	80
1990/ 3		4.29	7.25 *	1.76	2.73 *	6.05	8
1991/ 3		5.30	8.37	2.40	3.47	7.70	11.
1992/ 3	٠.	6.61	9.72	3.25	4.42	9.86	14.
1993/ 3		8.28	11.35	4.39	5.62	12.67	16.
1994/ 3		10.38	13.31	5.87	7.13	16.25	20.
1995/ 3		13.00	15.65	7.74	8.99	20.73	24.
19861		16.17	18.41	10.06	11.23	26.23	29.
1997/ 3		19.95	21.63	12.83	13.83	32.78	35
1998/ 3	ÿ.	24.34	25.33	16.02	16.78	92.07	42.
1999/ 3		29.25	29.43	19.60	20.05	ω̈́	69
2004/ 3		56.45	52.62	41.11	39.52	94.56	92.
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	SUMMARY	OF SUBSTATION	LOAD	FORECAST		35
SITUBONDO	OUND					
	ITU		ASEMBAGUS		1	5
	DAYTIME	EVENING	DAYTIME	EVENING	DAYTIME	EVENING
м	0.86	2.06		0.0	ω.	5.06
4	ω,	0	0.0			5.09
vn	06.0	۲,	0.0		٥.	2.16
9	٥.	N	0.0		0.92	N
* *	0.98	2.32	0.0	0.0		2.32
m	1.08	'n	•	0.0		S
m	1.20	۰,	•	0.0		Ø
m	1.32	2.90	0.0		1.32	
m	1.46	۲.	•	0.0		
23	1.62	M		0.0	1.62	М
m	1.79		•	0.0		3.67
m			•	•	1.99	
m	ď	4.29	0.0	0.0	ď	4.29
m	2.43	79.7	0.0	0.0	2.43	4.64
m	ý	5.01	0.0	0.0	Š	5.01
Ŋ	2.95	5.40	0.0	0.0	2.95	4.
M	3.24	5.81		0.0	ď	æ
m	3.54	6.25	0.0	0.0	'n	6.25
ĸ	3.87	6.71	0.0	0.0	3.87	۲.
m	5.48	* 28.8	0.26	* 07.0	5.74	9.27 *

SUMMARY OF SUBSTATION LOAD FORECAST

1 2	PAMEKASAN								
	CANDIHC	GILI TIMUR)	BANGKALAN		AMPAN		AMEKA		SUMENEP
	ш	EVENING	Σ	Z	DAYTIME	Z	TIME	EVENIN	DAYTIME
1984/ 3	0.02		0.35	0.7	0.5	9.0	0.61		97.0
1984/ 4	0.03		m	٧.	Ġ	۲.	٠	1.28	87.0
1984/ 5	0.03		m	۲.	w	۲.	Š	N)	67.0
1984/ 6	0.03	0.0	W	۲-	'n	7	٧.	1.31	67.0
1985/ 3	**	60.0	14.0	0.88	0.35	0.85	0.72	4	0.56
1986/ 3	70.0	: • ;	0.48	0	7.	1.01	φ,	1.70	99.0
1987/ 3	0.05	0.1	۷;	1.18	ň	1.19			0.78
1988/ 3	0.0	0.1	٠.	M	۰,	1.41	1.17	ú	0.91
_	20.0	0.1		1.55	۲.	Ý	1.36	'n	1.06
	0.0	•	06.0	~	ď	•	1.57	2.88	1.23
1991/ 3	0.10	0.2	1.04	ď.	۲-	2.33	1.79	4	1.43
1992/ 3	0.13	м. О	1.18	2.25	1.36	~	0	ó	1.65
1993/ 3	0.15	0.3	1.34	4	ø	۳.	W	٥.	1.90
1994/ 3	0.19	7.0	1.52	. •	æ	'n	v		2.19
1995/ 3	0.22	0.5	1.72	0	٠.	٥.	ç	æ	2.52
1996/ 3	0.27	9.0		4	4	ĸ	ĸ,	M	2.88
1997/. 3	0.32	0.7	Τ,	œ	~	۲.	0	ω	3.29
1998/ 3	0.36	8.0	٠,		3.04	۲.	٥.		3.71
1999/ 3	17.0	0.91	2.71	'n	•	ý		96.90	4.17
2 /7006	59.0	72 1			T U	0	0		4 00

즈	۲.	٥.	o.	?	'n	Ġ	٦.	٥.	۲.	Ŋ	0	2.0	5.5	5.2	7.0	8.9	6.0	3.0	25.22	6.9
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PAMEKASAN

Table. A-13(1) Long Term Demand Forecast of Distribution Substations

Cabaugs	Sudstations	Ordinar	y Peak Demar	ıd on Weekday	s (MW)
Cavaugs	SHOTJEJUE	1989/3	1994/3	1999/3	2004/3
Surabaya	Ujung	(8.4) 10.4	( 8.4) 16.4	( 8.4) 25.5	( 8.4) 38.8
Utara	Krembangan	23.2	39.3	32.0	50.3
& Selatan	Sawahan	36.3	54.2	(10.5) 77.8	(10.5) 105.1
	Tandes	22.9	36.9	(18.0) 61.0	(18.0) 98.0
	Segoromadu	((21.0)) (21.0) 20.8	((27.3)) (28.5) 26.7	((27.3)) (31.5) 43.0	((27.3)) (31.5) 59.9
ļ	Simokerto			35.0	57.5
	Benowo		17.8	28.7	40.0
	PLTU Gresik			((22.8))	((97.6))
	Simpang	16.4	27.6	48.0	73.2
	Waru	(34.5) 28.8	(51.3) 47.7	(51.3) 83.3	(51.3) 133.6
į	Sukolilo	43.2	85.8	64.7	99.9
	Ngage1	9.8	15.3	23.8	34.9
	Driyore jo	6.8	12.9	26.4	46.3
	Buduran	16.4	29.2	52.7	85.4
	Kenjeran	16.4	27.9	49.6	81.2
	Rungkut	57.6	66.3	81.3	94.5
	Darmo Grand	25.6	27.1	49.9	82.0

Table. A-13(2) Long Term Demand Forecast of Distribution Substations

Cahanaa	Substations	Ordina	ry Peak Dema	ind on Weekda	ys (MW)
Cabangs	Substactous	1989/3	1994/3	1999/3	2004/3
	Babatan	4.5 (( 3.5))	8.6	66.2	110.0
	Krian	16.0	((47.2))	((151.1)) 22.9	((382.5)) 37.4
	Ngiwo			57.4	94.5
	Semanbung		51.0	57.4	94.5
	Kalang Pilang		18.3	36.7	63.2
	Ketintang			57.4	94.5
	Trosobo			17.6	30.8
	Sidosermo			er en	34.9
Bojonegoro	Bojonegoro	4.0 ((18.0))	6.6	9.1	12.9
	Babat	((18.0)) 2.3	((18.0)) 3.4	((18.0)) 4.4	((18.0)) 4.9
	Lamongan	((13,9)) 1.2	((23.4)) 1.7	((23.4)) 2.4	((23.4)) 2.9
	Tuban	1.5	2.3	2.9	3.3
Malang	Kebonagung	19.1	27.5	38.0	50.3
	Polehan	11.0	19.2	32.0	50.4
	Blimbing	10.6	21.4	33.9	48.1
	Sengkaling	7.0	13.0	21.1	31.2
	Lawang	9.8	18.1	29.1	42.5

Table. A-13(3) Long Term Demand Forecast of Distribution Substations

		0	n District		(MLI)
Cabangs	Substations -	1989/3	1994/3	and on Weekda 1999/3	2004/3
		1909/3	1774/3	1999/3	20047.3
	Sukorejo	·	4.4		8.6
:	<u> </u>	2.4	4.4	6.6	0.0
	Turen			11.0	17.0
·		6.6	7.3	11.8	17.3
	Sengguruh				
		1.1	2.1	3.3	4.6
	Karangkates				
		1.1	2.1	3.3	4.6
	PLTA Selorejo				
	Berorejo	1.2	2.2	3.2	4.3
	Kepanjen				
			4.8	7.6	10.8
Pasuruan	Probolingo				
		10.5	20.1	34.0	51.5
	Plered				
Į		4.3	8.2	13.8	20.7
	Bangi1				
	20811	2,6	5.2	8.7	12.9
•	Pandaan			.e i	
	randan	7.2	14.3	25.3	40.1
Ì	Porong				
.	Torong	2.9	5.5	9.1	13.2
	Lacos				
	Leces	6.1	11.7	20.0	30.6
	Vnolan-				e in public
	Kralsaan	2.1	4.2	7.9	13.6
	D. I.				
	Paiton	( 1.8) 0.9	1.8	3.4	5.8
				((15.4))	((44.1))
Kediri	Kediri	(9.1) 13.2	(20.7) 25.4	(21.6) 42.4	(21.6) 60.3
ļ					
	Tulungagung	9.2	18.6	32.0	47.7
	Blitar	2 2	7.8	12.6	16.7
	DITERL	3.3	7.8	12.0	10.7

Table. A-13(4) Long Term Demand Forecast of Distribution Substations

Cabangs	Substations	Ordina	ry Peak Dema	ınd on Weekda	ys (MW)
Garango	040044010110	1989/3	1994/3	1999/3	2004/3
	PLTA Wlingi	2.2	5.2	8.4	11.1
	Kertosono	3.2	5.1	8.7	15.2
	Trenggalek	2.3	2.8	3.3	3.5
	Nganjúk	0.7	1.4	2.7	5.3
Mojokerto	Mojokerto	(7.5) 17.8	((10.5)) (12.0) 36.9	((41.9)) (12.0) 66.4	((105.8)) (12.0) 104.3
	PLTA Mendalan	3.5	1.2	2.7	4.6
	Ploso	0.3	0.3	0.3	0.4
	Jombang	0	3.2	3.9	7.2
Madiun	Manisrejo	13.7	23.9	38.2	56.7
	Caruban	0.9	1.6	2.1	2.5
	Ponorogo	2.2	3.8	5.6	6.9
	Pacitan	1.1	1.9	2.5	3.0
	Dolopo	5,4	9.4	13.6	16.7
	Magetan	2.1	2.3	2.5	2.9
	Ngawi	1.6	1.9	2.0	2.0

Table. A-13(5) Long Term Demand Forecast of Distribution Substations

Cabangs	Substations	Ordira	ry Peak Dema	ind on Weekda	ys (MW)
Cavaligs	Dubscations	1989/3	1994/3	1999/3	2004/3
		((13.7))	((25.3))	((38.2))	((69.3))
Jember	Jember	10.2	9.3	14.2	21.5
	Lumajang				
		4.0	7.2	12.7	22.4
	Bondowoso	0.7	r 0	9.9	15.0
		2.5	5.2	9.9	15.0
	Tanggul	·	7.3	11.3	17.4
	<b>.</b>				
Banyu- wangi	Banyuwangi	8.5	13.3	29.4	52.6
			-	-	
	Genteng		7.1	20.1	39.5
Situbondo	Situbondo				
STUDONIO	2110001100	3.1	4.6	6.7	9.3
	Asembagus	÷.			0.4
		((36.0))	((36.0))	((36.0))	((36.0))
Pamekasan	Candih	0.2	0.5	0.9	1.3
	D 1 1				5 6
į.	Bangkalan	1.6	2.8	4.5	6.5
	Sampang	1.7	3.6	5.7	8.0
·	Pamekasan	2.6	4,4	6.9	9.5
·.	Sumenep	2.2	4.0	7.2	11.6

Note: o Each figure means forecasted average demand at 19:00 hours on weekdays.

- o Double parenthesized figures mean big customers demand fed by  $150 \mathrm{kV}$ .
- o Single parenthesized ones mean those of 70kV or special use for construction (Paiton).
- o The rest mean those of distribution transformers.

Table. A-14 Forecast of I4 Energy Sales by Cabang

			e de la companya del companya de la companya del companya de la co					·
	loss	(11+12)	(11+12)	(13)	(13)	(11+12 +13)	Total	14
Cabang	rate	MWsub	GWh cus	MW sub	GWh cus	GWh cus	GWh cus	GWh cus
01 Surabaya Utara	0.1 1 2 3 0.1 0 2 7 0.1 0 0 6 0.1 0 0 1	1 1.8 4 2 2.6 0 4 0.2 5 6 3.9 4	5 6.0 3 1 0 8.1 1 1 9 2.9 8 3 0 6.7 4	1 9.5 2 4 4.3 3 9 5.4 8 1 8 3.5 4	1 0 8.3 7 24 8.7 7 5 3 7.0 6 1,0 3 2.9 6	1 6 4.4 0 3 5 6.8 8 7 3 0.0 4 1,3 3 9.7 0	5 9 2.7 9 3 0.2 1,7 1 9.0 2,9 5 2.6	4 2 8.3 5 7 3.3 9 8 9.0 1,6 1 2.9
02 Surabaya Selatan	0.1 1 8 4 0.1 0 3 3 0.1 0 0 6 0.1 0 0 1	1 8.7 0 3 7.2 4 7 1.4 7 1 2 6.5 5	8 7.8 8 1 7 8.0 2 3 4 2.6 7 6 0 7.1 0	1 2 6.4 7 2 6 6.5 9 5 3 3.5 1 9 5 5.2 0	6 9 7.3 0 1,4 9 5.0 3 3,0 0 0.9 2 5,3 7 5.8 5	78518 1,673.05 3,343.59 5,982.95	1,1 0 2.3 2,4 9 4.7 5,0 3 1.9 9,6 0 2.4	3 1 7.1 8 2 1.6 1,6 8 8.3 3,6 1 9.4
03 Bojoneg- oro	0.1124 0.1008 0.1000 0.1000	2.1 7 4.5 4 4.7 4 4.7 5	1 0.2 7 2 1.7 6 2 2.7 4 2 2.7 9	1 6.5 3 3 4.3 9 3 5.8 2 3 5.8 9	91.76 193.40 201.62 202.01	10203 215.16 224.36 224.80	3 6 7.8 5 6 0.8 5 7 0.0 5 7 0.4	2 6 5.8 3 4 5.6 3 4 5.6 3 4 5.6
04 Malang	0.1 1 7 9 0.1 0 3 0 0.1 0 0 5 0.1 0 0 1	6.7 0 1 3.0 3 2 3.7 6 3 8.5 3	3 1.51 6 2.3 1 1 1 3.9 3 1 8 4.8 4	7.4 9 1 7.0 0 3 7.0 5 7 2.8 2	41.32 95.37 208.42 409.83	7 28 3 1 5 7.6 8 3 2 2.3 5 5 9 4.6 7	9 2.6 2 2 0.9 4 5 2.3 8 5 4.4	1 9.8 6 3.2 1 2 9.9 2 5 9.7
05 Pasuruan	0.1 1 7 8 0.1 0 2 6 0.1 0 0 4 0.1 0 0 1	3.86 7.70 14.75 25.80	1 8.1 5 3 6.8 4 7 0.7 4 1 2 3.7 7	1 1.98 25.51 5 1.59 9 3.0 9	66.10 1 43.17 2 9 0.25 52 3.9 1	84.25 180.01 360.99 647.68	1 1 0.3 2 2 2.0 4 1 3.4 7 3 5.0	2 6.0 4 2.0 5 2.4 8 7.3
06 Kediri	0.1 1 7 5 0.1 0 3 7 0.1 0 0 8 0.1 0 0 2	2.2 3 4.2 2 7.5 6 1 2.3 1	1 0.4 9 2 0.1 6 3 6.2 4 5 9.0 5	2.2 4 5.3 8 1 2.0 8 2 3.2 8	1236 3016 67.93 131.01	22.85 50.32 104.17 190.06	3 6.9 7 0.0 1 2 2.6 2 0 4.2	1 4.0 1 9.7 1 8.4 1 4.1
07 Mojokerto	0.1170 0.1037 0.1008 0.1002	1.1 9 2.3 5 4.4 6 7.7 2	5.6 0 1 1.2 3 2 1.3 8 3 7.0 3	5.47 1 1.58 2 3.32 4 2.3 2	3 0.21 64.9 1 13 1.1 4 2 3 8.1 5	3581 7614 15252 27518	1 0 1.4 2 6 4.2 6 0 2.3 1,2 5 7.7	65.6 188.1 449.8 982.5
08 Madiun	$\begin{array}{c} 0.1\ 1\ 1\ 6 \\ 0.1\ 0\ 2\ 2 \\ 0.1\ 0\ 0\ 4 \\ 0.1\ 0\ 0\ 1 \end{array}$	1.07 2.15 4.11 7.08	5.07 1 0.29 1 9.7 1 3 3.9 6	4.4 6 9.4 8 1 9.1 2 3 4.7 1	24.78 53.23 107.57 195.35	2 9.85 63.52 1 27.28 22 9.31	4 9.4 1 1 9.8 2 3 5.6 4 1 6.1	1 9.5 5 6.3 1 0 8.3 1 8 6.8
09 Jember	0.1 1 2 2 0.1 0 2 6 0.1 0 0 6 0.1 0 0 1	0.7 9 1.8 3 4.1 8 9.2 6	3.7 4 8.7 5 2 0.0 4 4 4.4 2	0.64 1.9.3 5.4.6 14.3.2	3.55 1 0.8 3 3 0.7 1 8 0.5 9	729 19.58 50.75 125.01	9 1.4 1 5 8.3 2 6 8.7 4 5 0.8	84.1 1 3 8,7 2 1 7,9 3 2 5.8
10 Banyu- wangi	0.0 9 9 7 0.1 0 0 0 0.1 0 0 0 0.1 0 0 0	0.9 0 4.6 8 1 7.0 9 3 1.4 4	4.3 2 2 2.4 5 8 1.9 9 1 5 0.8 4	0.5 2 4.9 9 2 0.3 0 4 8.6 3	293 28.09 11426 273.72	725 5054 19625 42456	3 7.5 1 2 2.8 3 0 7.8 6 7 7.9	3 0.2 7 2.3 11 1.5 2 5 3.3
11 Situbo- ndo	0.1 1 8 1 0.1 0 4 7 0.1 0 1 2 0.1 0 0 3	0.0 6 0.0 9 0.1 5 0.2 6	0.28 0.4 3 0.7 2 1.2 5	0.0 2 0.0 9 0.2 3 0.4 0	0.1 1 0.5 3 1.2 9 2.2 5	0.3 9 0.9 6 2.0 1 3.50	0.3 0.7 1.3 2.3	△ 0.1 △ 0.3 △ 0.7 △ 1.2
12 Pameka - san	0.1 0 0 2 0.1 0 0 0 0.1 0 0 0 0.1 0 0 0	0.4 4 0.7 5 1.2 7 2.1 4	2.1 1 3.6 0 6.0 9 1 0.2 7	0.1 8 0.8 6 2.0 5 3.3 4	1.01 484 11.54 18.80	3.1 2 8.44 1 7.6 3 2 9.0 7	3 3 9.8 3 7 1.3 4 2 4.9 5 1 5.4	3 0 0.3 3 0 0.3 3 0 0.3 3 0 0.3

Note • Multilayered figures mean of March 1989, 1994, 1999 and 2004 respectively. 

<sup>·</sup> Demand Conversion Factor is 1.565 for I1+I2 and 1.334 for I3.

<sup>•</sup> For I4 of Pamekasan, just Madura Cement is forecasted.

Table. A-15(1) Long Term Demand Forecast of Big Customers (I4)

	0		Substation		Demand For	ecast (MW)	
Cabang	Customer		(kV) /Voltage	1989/3	1994/3	1999/3	2004/3
Surabaya Utara	Retrokimia Gresik		Segoromadu 150kV	21.0	n	11	en e
	Kunci Kedamean		n	<u>-</u> ;	6.3	tt .	11
			Segoromadu 150kV	21.0	27.3	e	11
	Semen Gresik		Segoromadu 70kV	18.0	II	Ħ	**
1	Barata		11	3.0	ff	H.	
	Carbide Factory G	resik	11	-	7.5	n	19
. !	Parama Art	a	11		· <b>-</b>	3.0	!!
			Segoromadu 70kV	21.0	28.5	31.5	T.
	PT PAL		Ujung 70kV	8.4	**	ff	11
	Jaya Pari Steel		Tandes 70kV	· <u>-</u>	- -	18.0	
	Sawahan X	· .	Sawahan 70kV	<del>-</del>	· <b>-</b>	10.5	17
	Total	,		50.4	64.2	95.7	11
!	X - SV		Gresik 150kV			22.8	97.6
		An	nual Energy	428.3GWh	573.3GWh	989.0GWh	1,612.9GWh
Ta	rget	Pe	ak Demand	51.3MW	68.7MW	118.5MW	193.3MW

Table. A-15(2) Long Term Demand Forecast of Big Customers (I4)

			Substation		Demand For	ecast (MW)	
Cabang	Customer		(kV) /Voltage	1989/3	1994/3	1999/3	2004/3
Surabaya Selatan	Ispat Indo		Waru 70kV	19.2 4.8	11	11	11
	Soda Waru Jatim Utam Steel	а	11	10.5	16.8	et .	#1 #4
	Maspion		Waru 70kV	34.5	51.3	11	11
		٠	Krian150kV	3.5	47.2	151.1	382.5
	X - SS /Include Tsarin Manunggal 30.0MW						
TIP.		A	nnual Energy	317.1GWh	821.6GWh	1,688.3GWh	3,619.4GWh
1	arget	P	eak Demand	38.0MW	98.5MW	202.4MW	433.8MW

Table. A-15(3) Long Term Demand Forecast of Big Customers (I4)

			Substation		Demand For	ecast (MW)	
Cabang	Customer	į	(kV) /Voltage	1989/3	1994/3	1999/3	2004/3
Bojonegoro	Dwima Agung Cement		Babat 150kV	18.0	11	tt.	# 1
	X - BJ /Include /Carbide Factory		Lamongan 150kV	13.9	23.4	n	11
	Lamongan 9.0			:			
٠.							
			·				
		Ann	ual Energy	265.8GWh	345.6GWh	345.6GWh	345.6GWh
T	arget	Pea	k Demand	31.9MW	41.4MW	41.4MW	41.4MW

Table. A-15(4) Long Term Demand Forecast of Big Customers (I4)

		Substation		Demand For	ecast (MW)	31.24
Cabang	Customer	(kV) /Voltage	1989/3	1994/3	1999/3	2004/3
Kediri +	Gudang Garam	Kediri 70kV	9.1	20.7	21.6	11
Malang +					e e e e e e e e e e e e e e e e e e e	
Madiun +	X - KD	Kediri 150kV		_	15.4	44.1
Pasuruan	· 	·				
			· · · · · · · · · · · · · · · · · · ·	·		
					·.	
·rp		Annial Energy	19.8+14.0 +19.5+26.0 =79.3	63.2+19.7 +56.3+42.0 =181.2	129.9+18.4 +108.3+52.4 =309.0	259.7+14.7 +186.8+87.3 =547.9
Total	arget	Peak Demand	9.5MW	21.7MW	37.0MW	65.7MW

Table. A-15(5) Long Term Demand Forecast of Big Customers (I4)

		Substatio		Demand For	ecast (MW)	
Cabang	Customer	(kV /Voltage		1994/3	1999/3	2004/3
Mojokerto	Pakerin	Mojokerto 70kV	6.0	11	11	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	Ciwikimia	tt	1.5	6.0	n	11 .
		sub total	7.5	12.0	*1	11
	X - MJ	Mojokerto 150kV	-	10.5	41.9	105.8
	ļ					
				E		
	1			1		
* .		·				
	1	Annual Energ	gy 65.6GWh	188.1GWh	449.8GWh	982.5GWh
· · · · · · · · · · · · · · · · · · ·	arget	Peak Demand	7.9MW	22.5MW	53.9MW	117.8MW

Table. A-15(6) Long Term Demand Forecast of Big Customers (I4)

0.1		Substation		Demand For	ecast (MW)	
Cabang	Customer	(kV) /Voltage	1989/3	1994/3	1999/3	2004/3
Jember +	X - JB	Jember 150kV	13.7	25.3	38.2	69.3
Banyn						
wangi +						
Situ- bordo						
	e e					
			'			
					·	
1	larget	Annual Energy	84.1+30.2 -0.1 =114.2	138.7+72.3 -0.7 =210.7	207.9+111.5 -0.7 =318.7	325.8+253.3 -1.2 =577.9
		Peak Demand	13.7MW	25.3MW	38.2MW	69.3MW

Table. A-15(7) Long Term Demand Forecast of Big Customers (14)

		Substation		Demand For	ecast (MW)	and the second
Cabang	Customer	(kV) /Voltage	1989/3	1994/3	1999/3	2004/3
Pameka- san	Madura Cement Factory	Candih (Giri Timur) 150kV	36.0	36.0	36.0	36.0
					* .	
					•	
					•	
•						
				. 1		
,	[arget -	Annual Energy	300.3GWh	300.3GWh	300.3GWh	300.3GWh
*.	iaiget	Peak Demand	36.0MW	36.0MW	36.0MW	36.0MW

RESIDENT DEPARM FOR CAST 1980/ 3 -2004/ 3 1981/ 3 1982/ 3 1989/ 3 1989/ 3 1989/ 3 2004/ 3 1881/ 3 1983/ 3 1989/ 3 1989/ 3 2004/ 3 1881/ 3 1981/ 3 1982/ 3 1989/ 3 1989/ 3 2004/ 3 1881/ 3 1981/ 3 1989/ 3 1989/ 3 2004/ 3 1981	CABANG LOFAND FORECAST 1980/ 3 - 2004/ 3 1981/ 3 1982/ 3 1984/ 5 1984/ 5 1994/ 5 1999/ 3 1999/ 3 1981/ 3 1982/ 3 1983/ 3 1984/ 5 1999/ 3 1999/ 3 1988/ 4 1988/	EGIONAL DEMAND FORECAST CABANG RESIDENTIAL SURABAYA UTARA SURABAYA UTARA WALUNO MADIUN JEMBER BANYUMANGI SITUBONDO SITUBONDO EAST JAVA COMMERCIAL COMMERCIAL	980/ 3 1980/ 3 61:844 24:641 84:641 93:384 77:947 77:947 11:845 11:845	7,1981/ 32,296 10,897 1	982/					
EGIONAL DERAND FRECAST 1980/5 - 2004/5 - 1982/5 - 1983/5 - 1984/5 - 1983/5 - 1984/5 - 1983/5 - 1984/5 - 1983/5 - 1984/5 - 1984/5 - 1983/5 - 1984/5	CABRAND PRRAND FORECAST 1980/ 3 - 2004/ 3 1987/ 3 1989/ 3 1994/ 3 1999/ 3 1989/ 3 1999/ 3 1989/ 3 1999/ 3 1989/ 3 1999/ 3 1989/ 3 1999/ 3 1989/ 3 1989/ 3 1999/ 3 1989	EGIONAL DEMAND FORECAST CABANG RESIDENTIAL SURABAYA UTARA MALANG PASURUAN MADIUN JEMBER BANYUMANGI SITUBONDO SITUBONDO EAST JAVA COMMERCIAL COMMERCIAL SURABAYA ALTARA	980/ 3 1980/ 3 480/ 3 61.884 98.4641 98.4641 98.4641 7.7003 1.845 1.845 1.845 1.845 1.845	2	982/	1	I			
ABANG  BRANCA SELATAN  BRANCA	SELECTION 13 1981/3 1982/3 1983/3 1994/3 199	ABANG ESIDENTIAL URABAYA UTARA URABAYA UTARA ULABAYA SELATA ASURUAN EDIRI OJOKERTO OJOKERTO OJOKERTO ADIUN ANTUMANGI ATURASAN AST JAVA OMMERCIATA	08 0 140 0110 0 1011 4	200001 200001 2000000 20000000000000000	982/	NNECTE	APACI	H	-	
ESTDENTIAL  PS 25.296  PS 21.552  PS 1222  PS 12	ESTOENTIAL ACTIONAL A	ESIDENTIAL URABAYA UTARA URABAYA UTARA ALANG ASURUAN EDIRI EDIRI ADIUN ANTURNANGI ITUBONDO AMEKASAN AST JAVA OMMERCIAL URABAYA UTARA	740 01-480 RV-FW-47 8 0400 RV-FW-47 8 8440 80 90 70 740 W	WWWWWWWWWWWWWWWWWWWWWW	3.65	983/	1686	176	1666	00
MARBYA MIRRA	MARNAY MITRAA 42.083 5.296 6.3.556 72.944 75.207 510.037 3  MARNAY SELATAN 64.083 5.296 5.556 72.944 75.207 510.037 3  MARNAY MITRAA 42.083 7.2962 39.782 25.155 710.028 711.009 2  MARNAY MITRAA 8.4041 75.207 20.000 40.200 71.045 32.143 10.009 711.009 2  MAYOURANG 7.700	URABAYA UTARA URABAYA SELATA ASURUAN EDIRI OJOKERTO OJOKERTO ANTUMANGI ATYUMANGI ATYUMANGI ANTENSAN AST JAVA AST JAVA	740 740 740 000 000 000 000 000	W W W O W V O & W W O & W O & W C O &	3.65	-				
MUNICAL NET SECULAR SE	ALANGE AS SELLATION OF 1979 AND 1872 AN	UNABATA SELATA ALANGA ALANGA EDIRI OJOKERTO ADIUN ANDUANGI AMERASAN AST JAVA AST JAVA OMMERCIAL	0.0 -480 RV F W L 4 4 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	000 00 00 00 00 00 00 00 00 00 00 00 00		72.94	39.90	19.02	10.03	94.01
NUMBER OF STATE OF ST	MANNENAN  CENTER  CENT	ASLAND ASLAND BOINIAN OJOKERTO ADIUN ANTUMANGI ATUBONDO AST JAVA AST JAVA OMMERCIAL URABAYA UTARA	180 07 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	20	- C	20.00	70.00	40.0	77.77	) ) ) )
Colored Colo	THE MANUAL TO THE TOTAL	EDIRIC 0JOKERTO 0JOKERTO ADIUN ADIUN ANYUMANGI ANYUMANGI ANEKASAN AST JAVA AST JAVA AST JAVA AST JAVA	00040004 1-	24.08 24.08 24.08 27.08 27.08	0 0 7 7	, c	0 4	0 . 0 0 . 0 0 . 0	, c	24.07
ANT JAVA  ANT JA	Court   Cour	ADIUN ADIUN ADIUN ANYUMANGI ITUBONDO AMILASAN AST JAVA AST JAVA AST JAVA AST JAVA	04000004 T	3.75 3.75 3.58	4	000	77	00.00	7.67	35.77
HERER HERE HERE HERE HERE HERE HERE HER	AMERICA MAIN TO TO 47 10.688 14.140 17.288 40.656 27.791 46.514 77.700 8.725 40.77 3.865 9.799 13.766 27.791 46.514 77.700 8.725 18.656 8.7.267 13.766 27.791 46.514 17.700 17.700 8.725 18.670 13.766 27.791 46.514 17.700 13.766 27.791 46.514 17.700 13.766 27.791 46.514 17.700 13.766 27.791 46.514 17.700 13.766 27.791 46.514 17.700 13.766 27.791 46.514 17.700 13.766 27.791 46.514 17.700 13.766 27.791 46.514 17.700 13.766 27.791 46.514 17.700 13.766 27.791 46.514 17.700 13.766 17.700 13.766 17.700 15.700	ADIUN EMBER ANYUMANGI ITUBONDO AMEKASAN AST JAVA OMMERCIAL URABAYA UTARA	40.7.4 40.07.4 40.04.4 7.4.004.4	0.68 3.75 3.58	8.47	1.04	2.14	65.28	11.87	62.81
HENDROOF  ANY URANGE  ANY URAN	ANTURANGE ANTURA	EMBER ANYUMANGI ITUBONDO AMEKASAN AST JAVA OMMERCIAL URABAYA UTARA	7.70 3.07 7.84 7.84 7.84 11.84	.58	4.14	7.24	0.35	4.58	87.26	01.30
ANTURANGE  ANTOR  ANTURANGE  ANTO	TUBONDO  NEKARN  AFEKARN  AFEK	ANYUMANGI ITUBONDO AMEKASAN AST JAVA OMMERCIAL URABAYA UTARA	3.07 7.6.43 7.6.43 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0	. 58	-79	3.09	62.2	8.51	5.92	05.21
TITURGNUO 1 1845 2 2087 2 200	TUBRONOO  1.845  A. 22.525  B. 207  B. 208  B.	ITUBONDO AMEKASAN AST JAVA OMMERCIAL URABAYA UTARA	7 4 . 20 7 6 . 4 . 30 1 4 . 30		. 78	5	3.76	5.20	0.28	5.97
ASTERARAN 14.204 6.697 25.066 6.670 15.164 27.457 6.5.59 18.6.	AMERARAM AME	AMEKASAN AST JAVA OMMERCIAL Urabaya Utara	76.43 18.11	.08	30	. 78	5.24	8.36	2	2.67
Name	UMBRAYA UTARA  18.118 31.780 34.223 34.491 66.155 103.563 146.599 11  LEANGE TANN  18.118 31.780 34.223 34.491 66.155 103.563 146.599 11  LEANGE TANN  18.118 31.780 34.223 34.491 66.155 103.563 146.599 11  LEANGE TANN  18.118 31.780 34.223 34.491 66.155 103.563 146.599 11  LEANGE TANN  18.118 31.780 34.223 34.491 66.155 103.563 19.571 10.599 11  LEANGE TANN  18.118 31.780 34.29	OMMERCIAL URABAYA UTARA	8	4.69	5.60	6.67	5.16	27.49	44.47	63.59
DUMERCIAL  UNABAYA UTARA  12.122 18.279 20.384 19.441 41.135 66.843 96.517 124.28 ALRG  AL	UNRENCIAL UNRENTAL UN	OMMERCIAL URABAYA UTARA UPABAYA SELATA	8.11	70.33			1		•	
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# APPENDIX - B

REPORT ON FIELD INVESTIGATION

#### APPENDIX - B

The site surveys of main transmission lines and substations to be included in the Short-term Implementation Program were carried out in Surabaya City, Madura Island, Paiton and etc.

The following is the details of field investigation:

# 1. Surabaya City and Its Surrounding Area

# 1.1. Krian Substation

The construction works are now being executed toward the completion time in 1985 as the substation for 500 kV transmission line.

At present, the construction of access road to the site from the Surabaya - Krian truck road and preparatory work of substation site are in progress.

The substation site is located on the gently-sloping hill and the excavation and compaction works up to design level have been carried out there. The transmission lines for Babatan New Substation in Surabaya City and for Gresik Power station will lead from 150 kV side of this substation.

# 1.2. Krian - Trosobo - Babatan Transmission Line (11.6 km)

As a village located at just South side of Krian S/S, the transmission line is coursed around.

The route is almost rice field and crosses 150 kV and 70 kV T/L and furthermore crosses Surabaya River, and reaches Trosobo S/S, although the span length is 400 m in crossing the Surabaya River, particular tall tower is to be erected.

Trosobo - Babatan transmission line route is also disturbed by a village and takes a roundabout course. The route also traverses rice field, sugarcane field and railway crossing. The length of Krian - Babatan line will be 11.6 km instead of 9 km previously planned because of the course avoiding the village.

# 1.3. Trosobo Substation (Future Plan)

It is assumed to construct the substation at the sugarcane plantation area where the canal is passing through at an east side and located at the north side of principal road (Waru - Krian) in future. As the ground level is low in these area, levelling works of the ground way take a lot of time. It is really rare to have an environmental problem for big villages do not exist nearby.

#### 1.4. Babatan Substation

The substation site will be determined at the location between the irrigation canals and along the road branched southward from the principal road (Waru - Krian).

The ground and the surrounding conditions are quite good comparing with Trosobo S/S site although there is now sugarcane plantation.

# 1.5. Waru - Sawahan Line (Rehabilitation - 10.6 km)

This is the rehabilitation works for 70 kV transmission line using presently 50 mm<sup>2</sup> H.D.C.C. (current capacity 260A) to ACSR 300 MCM (current capacity 440A) for the countermeasures to load increase.

The tower type is the same as the one for Waru - Bangil line, and regarding to Waru - Bangil line, the same rehabilitation

plan has been made under Surabaya City Power Distribution Project.
The strength of tower structure has already been studied.

However, as the construction of the towers is really in old time and the condition of their foundations is not clear, the strength test for tower materials, bolts and etc. will be necessary, and also the checking of the size of foundations and condition of concrete by means of test excavation will be needed.

In peak load hours of Sawahan S/S, the load on each of double circuit reaches 180A. Assuming the case that one of double circuit line is failure, it should be reinforced.

This line has to cross over a railway and pass beneath three 150 kV lines, however, these would not pose so serious problem in the execution of the work.

# 1.6. Sukolilo - Kenjeran Line (4.5 km)

Kenjeran S/S to be constructed in the Surabaya City Power Distribution Project is connected by single circuit line. The conversion to double circuit line will increase the reliability.

Substation will be constructed inside a rice field area at 450 m distance from road.

For this additional stringing work, the same towers of Sukolilo - Ujung Line are used in a section from the Sukolilo outgoing to No.14 tower.

In stringing on upper part of the towers, a careful working plan has to be set up.

# 1.7. Rungkut S/S

At present Waru - Sukolilo Line is a single circuit line, but this is scheduled to become double circuit line in the Surabaya City Power Distribution Project.

In the intermediate point of the line Rungkut S/S is established newly and double circuit line is taken in by  $\pi$  branch.

The substation is planed to be constructed at the plain grassland, but the geological condition is quite bad due to the swamp located nearby the site and the access to the transportation of equipments will not be favoured.

# 2. Madura Island

Madura is a long and narrow island extending over 163 km from east to west and 38 km from south to north, and with an area of  $5,593 \text{ km}^2$ .

It has a population of about 2.7 million.

There is one PLN branch office in Pamekasan and the branch office operates generating facilities and distribution facilities divided into four zones.

As of today, the electrification ratio is still only 3%, and there are no large enterprises nor factories. Other major power demand are the load from pumps for irrigation and town water supply, drying up facilities for tobacco and salt factries.

In recent years, the submarine cable project for interconnection between the Madura island and Java island has become formed up and, the positive introduction of a cement factory is to be set up in Madura.

Besides, 150 kV transmission line project that will cross over the island from west to east has be formulated to supply the power to sustain its regional development and up-bringing of electrification. During the site survey, the team encountered the ongoing distribution expansion work and felt the projects are in progress.

#### 2.1. Gili Timur S/S

The submarine cable from Gresik P/S is now being prepared for construction.

The project is to connect submarine cable to Gili Timur S/S which supplies the loads of both Labang (clincher plant) and Sekar Bungu (grinder plant) cement plants.

Gili Timur S/S is the origin of 150 kV transmission line running through the Madura island. The site is located at the crop field about 800 m distant from the main road (Kamal - Bangkalan).

The ground level is higher than the access road and it is considered that the drainage condition is good. The ground is covered with an organic surface soil including red clay.

# 2.2. Bangkalan P/S

There are 4 diesel power stations in the Madura island Among others, Bangkalan Power Station has been surveyed at this time.

One of five generators in the station is manufactured by AEG, West Germany in 1959 and the other four units added after 1973 are made in Holland.

The capacities of the generators varies such as 400 KVA, 420 KVA x 2 units, 670 KVA and 1,000 KVA. Distribution panel includes operation panel by each generator and also parallel operation panel, and the parallel operation of generators is being made. It is connected to the distribution facilities outside by 6 KV cable. The operation office of power station is located at the same compound as of PLN Branch Office in Madura.

# 2.3. Gili Timur - Bangkalan Line (15.5 km)

This line reaches to Bangkalan S/S running along the principal road (Kamal - Bangkalan) in north direction right after Gili Timur S/S.

The route is fairly taking a longer course because the industry sites and the quarry sites have been avoided.

# 2.4. Bangkalan S/S

This substation is planned to be established at the site facing with the principal road (Bangkalan - Sampang). The ground surface is covered by the grasses and there is no problem for site preparation and transportation of equipment and materials.

However the site is about 4 km distant from the center of Bangkalan town.

# 2.5. Bangkalan - Sampang Line (57.9 km)

Except the route section of the transmission line nearly Bangkalan S/S to keep away from the villages, transmission line is almost running along the principal road.

Therefore there is no problem for construction and maintenance.

Although the route is plain field, grassland and rice field, only 3 km of the middle portion runs through the hill of mountain base.

After passing this parts, the route passes nearby swamp place in a section of about 3 km and again passes the base of mountain, and reaches to Sampang S/S.

The demand in future is expected in nearby Sampang as there are some fish ponds and salt fields.

# 2.6. Sampang S/S

As sampang S/S site is facing on the principal road from south to north starting from Sampang and is plain fields, there are no difficulties in construction.

And it is suitable for distribution of load as it is located near by downtown of Sampang.

# 2.7. Sampang - Pamekasan Line (25.3 km)

The route is planned along the Sampang - Pamekasan bypass road located at further inside of the south coast road.

The terrain of the route is generally flat, farm land, grassland, and rice fields with sparse inhabitants. No difficulty is expected in construction and maintenance as well.

The route is almost running along the road but most of the route is taken straight.

# 2.8. Pamekasan Substation

The site is located at the side of the bypass road for Sampang and about 4 km away from Sampang town center. At present, the place is a grassland with no resident nearby, but due to the distant location from the load center, distribution plan should need careful considerations.

# 2.9. Pamekasan - PLN Cabang

Inside Pamekasan, which is the center of the island, PLN has a branch office and this office administer four zones. The survey team inspected one city water supply pumping station adjacent to PLN office. The station is to pump up water from deep well to store it in the about 20 m high tank. Their contracted kVA is 200 kVA and uses four (4) units of pump for supplying water to approx. 2,000 residents at 114 1/sec.

This would be probably one of the largest load.

# 2.10. Others

Due to the limited times, the route in the section Pamekasan - Sumenep (51.2 km) and the site for Sumenep Substation have to remain unsurveyed. It is foreseen from the data check that any particular problem will hardly occur.

As a general view, the construction of transmission facilities on the island of Madura would not present difficulties in selection of the site and the work execution as well, because the island is rather flat terrain throughout with generally solid ground conditions and favoured by fairly developed road network. However, since this is the first introduction of large transmission facilities into the island, geologic investigations are to be conducted and the results should be reflected on the determination of foundation design parameters.

As to the transmission line, the route has selected mainly along the existing roads due to putting a major consideration on the maintenance, however, more studies also be given in a direction to select economical line routes.

\* P.S.: Afterward, a re-examination took place at PLN on Pamekasan - Sumenep route, and a short-cut route came to be adopted, which results as follows;

	Route Length
Old route	51.2 KM
New route	45.6 KM _

The Route Length has become shorter by 5.6 KM.

# 3. Paiton

# 3.1. Paiton Power Station

The paiton Coal Fired Steam Power Plant Project # 1 and # 2 is scheduled for completion in 1989. For construction power supply, a transmission line of 150 kV double circuit is expected to be erected in 1986 between Probolinggo and the Site.

The switch yard site of Paiton Project is located on a hill land facing to the power station site.

The ground level is EL. 84 m.

The 150 kV outgoing facilities are planned to be constructed in the east side of 500 kV switching equipment.

# 3.2. Paiton - Kraksaan Line (19.7 km)

The outgoing line will traverse on the west hilly land until it reaches a plain.

The route up to Kraksaan takes a round about courses in the middle of plain in order to avoid villages along the trunk road.

The route passes through a flat land consisted of rice fields, sugar cane plantation, corn farm land, except the hilly portion at the outgoing.

No serious problems are foreseen in the construction, but the hauling of construction materials and time duration of the work should be planned out minutely since the route is apart from the main road.

# 3.3. Kraksaan Substation

The proposed site is located at one street behind southward of the main traffic road.

Final location of whether to be south side or north side of the street has not yet been decided.

The north area is a grassland and the other is a ricefield, both of which do not pose any problem in construction.

#### 3.4. Kraksaan - Probolinggo (31.5 km)

Like the above mentioned transmission line, the presently proposed route is taken to avoid the villages along the trunk road. Especially, the incoming portion to Probolinggo is southward aligned apart from a dense residencial area. All the way through the route would not involve any serious construction problem. Only the place which needs a careful consideration and construction program is the crossing section of two 150 kV lines nearby Probolinggo outgoing bay.

#### 3.5. Probolinggo Substation

At present, this substation receives the power supply from Bangil Substation through 70 kV line and transmit toward Jember area after the step-up to 150 kV. In the Acceleration Project, a new 150 kV line from Bangil is connected to this substation for Surabaya - Bali 150 kV interconnection.

As mentioned before, a 150 kV transmission line for construction power supply to the Paiton Project will take off from Probolinggo Substation.

With the completion of this line, this substation will have a complete 150 kV facilities and the yard could be neatly rearranged owing to removal of 30 kV bay equipment for Leces and step-up transformer.

#### 4. Bojonegoro

Due to the heavy rainfall during the rainy season, the team has met flooding over the roads at many places. Therefore, the survey of substation sites and transmission line route could not be done. As far as the relevant data reveal, it seems that both substation (Ngawl and Tuban) sites and transmission route would not pose difficulties in construction as well as selection. However, the area for Tuban substation may be suffered by rainwater during the rainy season. Then, ground conditions of the sites should be investigated sufficient enough to ensure the safety of equipment.

## Route Length

Feb. 28, JICA

	Planning length	Real length		
Sukolilo - Kenjeran	6 Km	4.5 Km		
Krian - Babatan	9 Km	11.6 Km		
Waru - Sawahan	11 Km	10.6 Km		
Probolinggo - Kraksaan	30 Km	31.5 Km		
Ngawi incomer	10 Km	2 cct x 5 km		
Kraksaan - Paiton	30 Km	19.7 Km		
Babat - Tuban	40 Km	30.9 Km		
Gili Timur - Bangkalan		15.5		
Bangkalan - Sampang	160 Km	57.9		
Sampang - Pamekasan	160 Am	149.9 Km 25.3		
Pamekasan - Sumenep		51. 2		

# APPENDIX - C

SUBREPORT ON LAMP FLICKER

## Appendix-C Subreport on Lamp Flicker

# C.1. A historical change on the problem of lamp flicker by arc furnace in Japan.

The problem of lamp flicker by arc furnace has been treated since around 1955 in Japan.

It was not until 1964 that the following concepts on flicker were established:

- . Sensitivity coefficients
- V<sub>10</sub>
- . Perception ratio, etc.

Each power corporation, however, did not come to an agreement on the actual application of them. Besides, few arc furnace users were interested in lamp flicker, and electric machine makers were not so aggressive to produce flicker reducing devices on a commercial basis.

After that, study of estimating method on flicker had been developed respectively to establish Guide-lines by each power corporation. But it was impossible to find effective countermeasures. There was nothing but one case of power supply by installing an exclusive transformer.

With the popularization of color television (no voltage stabilizer was included in early color TV), considerable complaints about flicker were occasioned one after another in around 1967. To cope with this problem, each power corporation raised the level of their own Guide-lines respectively, and explained effectiveness of some concrete countermeasures on flicker at the research meeting composed

of power corporation, arc furnace users and electric machine makers. As the result of patient negotiation with arc furnace users, saturable shunt reactor or synchronous condenser had come to be adopted for the countermeasures by each arc furnace user during 1971 to 1972.

However, considerable complaints on flicker occasioned subsequently by the following reasons:

- . Capacity increasing and productivity progress of arc furnace
- . A change of power supply system
- . Fault of estimating procedure, etc.

Consequently, the level of Guide-lines was raised again in 1972.

As thyristor Q (reactive power) compensator (Example: TQC) was realized for practical application in 1973, some countermeasures on flicker were taken whenever the capacity of arc furnace was increased by the users.

As the result of development of  $\Delta V_{10}$  calculation method using digital computer in 1976, the following studies were advanced:

- . Comparative research between digital  $\Delta v_{10}$  calculation method and analogue  $\Delta v_{10}$  measurement method adopted by each power corporation
- . Analysis method using statistical mathematics

In 1979, with the progress of the studies above, the relation between  $\Delta V_{\rm max}$  and  $\Delta V_{10}$  max concerning flicker was clarified, and each power corporation reached a consensus to adopt the predict method by  $\Delta V_{10}$  max.

Since it requires a large investment for countermeasures on flicker, the economic burden of arc furnace user is considered to be much.

However, the supply voltage to general consumer, one factor of the quality of electricity, is disturbed by flicker.

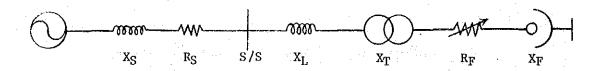
In Japan, it is regulated to maintain the quality of electricity by the Rules and Rates for Electric Service. The experience in Japan having solved the problem tells that it is very important for power corporation to cope with arc furnace users fairly and impartially by arranging and standardizing the following theoretical systems about flicker:

- . Calculation method
- . Measurement method
- . Allowable level
- . Effectiveness evaluation of reducing device

# C.2. Mutual relation between voltage fluctuation and V10

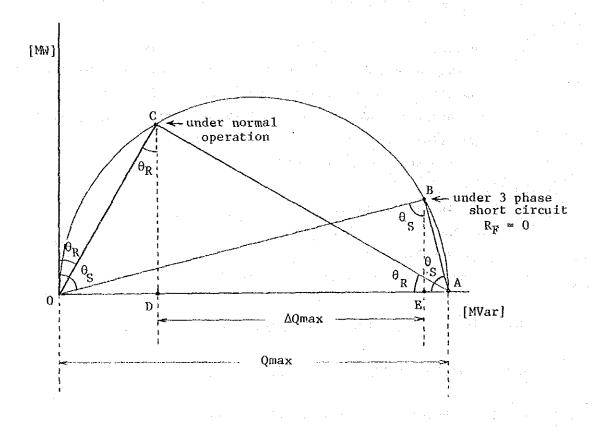
# C.2.1. Calculation of Voltage Fluctuation

#### C.2.1.1. Schematic diagram of model power system



$$X_0 \equiv X_S + X_L + X_T + X_F$$
 (%) ... 10 MVA Base

# C.2.1.2. Electric power circle diagram and reactive power fluctuation in arc furnace



$$\sin \theta_{S} \neq 1 
\cos \theta_{R} \neq 0.85$$

$$Q_{\text{max}} = \overline{OA} = \frac{100}{X_S + X_L + X_T + X_F} \times 10 = \frac{100}{X_0}$$
 (MVar)

$$\overline{OE} = \overline{OB} \sin \theta_S$$
,  $\overline{OB} = \overline{OA} \sin \theta_S$ 

$$\vec{\cdot} \cdot \vec{OE} = \vec{OA} \sin^2 \theta_S$$

$$\overline{OD} = \overline{OC} \sin \theta_R$$
,  $\overline{OC} = \overline{OA} \sin \theta_R$ 

$$\therefore \ \overline{\text{OD}} = \overline{\text{OA}} \ \sin^2 \theta_{R}$$

$$\Delta Q_{\text{max}} = \overline{OE} - \overline{OD} = \overline{OA} \sin^2 \theta - \overline{OA} \sin^2 \theta_R$$

$$= Q_{\text{max}} (\sin^2 \theta_S - \sin^2 \theta_R)$$

$$= Q_{\text{max}} (\sin^2 \theta_S - 1 + \cos^2 \theta_R)$$

$$= Q_{\text{max}} \cos^2 \theta_R$$

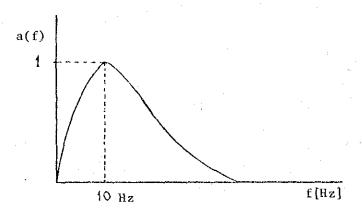
C.2.1.3. Voltage fluctuation (at S/S Bus)

$$\Delta V_{\text{max}} = Q_{\text{max}} \times \frac{X_{\text{s}}}{10} \dots 1000 \text{ Base}$$
 (V)

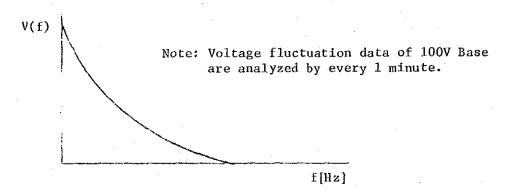
(MVar)

# C.2.2. A concept of $\Delta v_{10}$

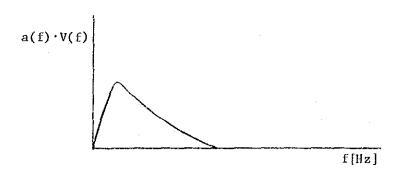
# C.2.2.1. Sensitivity coefficients ..... a(f)



# C.2.2.2. Spectra of flicker in arc furnace ... V(f)



## C.2.2.3. $a(f) \times V(f)$



C.2.2.4. A definition of  $\Delta V_{10}$ 

$$v_{10} = \sqrt{\sum_{f=1}^{\infty} [a(f) \cdot V(f)]^2}$$

Note: One  $\Delta v_{10}$  can be obtained by every 1 minute.

# C.2.2.5. A definition of $\Delta V_{10~max}$

After measuring for several hours, choose the one hour for which  $\Delta V_{10}$  is largest.

Determine mean (m) and standard deviation ( $^{\sigma}$ ) calculating 60 pieces of  $^{\Delta}V_{10}$ , and definite  $^{\Delta}V_{10}$  max by the following formula:

$$\Delta V_{10 \text{ max}} = m + 1.65\sigma$$
 ... 100V Base (V)

Note: The probability that values larger than  $\Delta V_{10~max}$  appeare is 5% when  $\Delta V_{10}$  are shown in the normal distribution.

Namely, 60 pieces x 0.05 = 3 pieces then,  $\Delta V_{10 \text{ max}}$  is the fourth value from the biggest in 60 pieces of  $\Delta V_{10}$ .

#### C.2.3. Mutual Relation

The following formula is used empirically.

$$\Delta V_{10 \text{ max}} = \frac{1}{3.6} \Delta V_{\text{max}}$$

$$= \frac{1}{3.6} \Delta Q_{\text{max}} \times \frac{X_{\text{s}}}{10}$$

$$= \frac{1}{3.6} Q_{\text{max}} \cos^2 \theta_{\text{R}} \times \frac{X_{\text{s}}}{10}$$

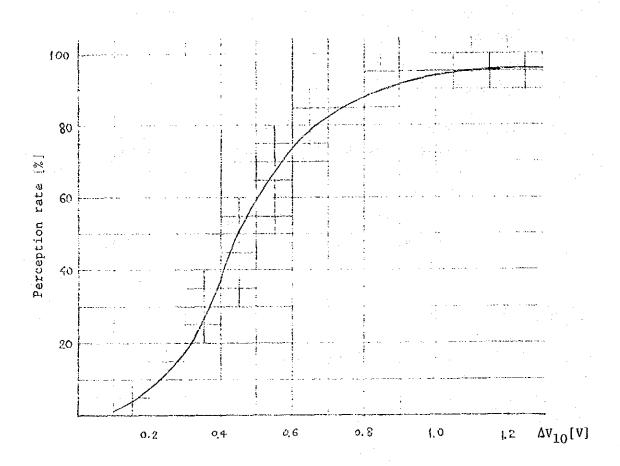
$$= \frac{1}{3.6} \cdot \frac{100 \times (0.85)^2}{X_{\text{S}}^+ X_{\text{L}}^+ X_{\text{T}}^+ X_{\text{F}}} \times X_{\text{S}}$$

$$= 20.07 \frac{X_{\text{s}}}{X_{0}} \dots 100V \text{ Base} \quad (V)$$

# C.3. Allowable Level and Countermeasures on Flicker by $\Delta V$ 10 max

## C.3.1. Allowable Level

# C.3.1.1. The relation between $\Delta\,\mathrm{V}_{10}$ and perception ratio



Perception ratio = 
$$\frac{B + C + D}{A + B + C + D}$$
 x 100 (%)

A : number of subjects who don't feel flicker at all

B : number of subjects who don't feel flicker so much

C : number of subjects who feel flicker

D : number of subjects who feel flicker nervously

#### C.3.1.2. Maximum Allowable level

Determine perception ratio 50%:  $\Delta V_{10 \text{ max}} = 0.45 \text{V}$  for maximum allowable (control) limit.

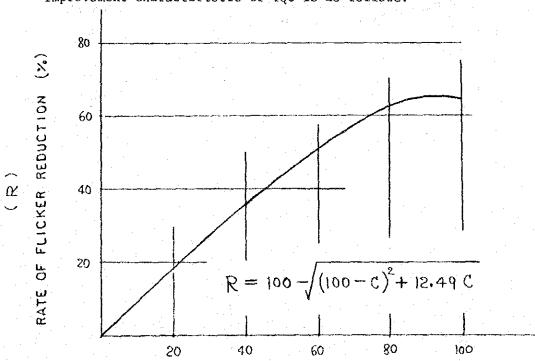
#### C.3.2. Countermeasures on Flicker

C.3.2.1. The relation between rate of flicker reduction (R) and rate of reactive power compensation (C) of TQC

$$R = \frac{\Delta V_{10 \text{ max}} \text{ without TQC } - \Delta V_{10 \text{ max}} \text{ with TQC}}{\Delta V_{10 \text{ max}} \text{ without TQC}} \times 100 \text{ (%)}$$

$$C = \frac{TQC \text{ capacity}}{Q_{\text{max}}} \times 100$$
 (%)

Improvement characteristic of TQC is as follows:



RATE OF REACTIVE POWER COMPENSATION (%)

## FLICKER REDUCTION CHARACTERISTICS

## C.3.2.2. Required capacity of TQC

Arc furnace users set up TQC or something like that to make  $\Delta\,v_{10~max}$  not exceeding 0.45V when  $\Delta v_{10~max}$  is more than 0.45 V.

(Example)

In case that present  $\Delta V_{10\text{max}} = 1.0 \text{ V}$  is expected to be reduced to maximum allowable (control) limit ( $\Delta V_{10\text{ max}} = 0.45 \text{V}$ ):

$$R = \frac{1.0 - 0.45}{1.0} \times 100 = 55 \tag{%}$$

$$C \neq 65.3$$
 (%)

Required capacity of TQC =  $0.653 Q_{max}$ 

$$= 0.653 \frac{100}{X_0} = 65.3 \cdot X^{-1}$$
 (MVar)

rc furnace	e Branch office		Head o		Remarks
users	Power sales section	Electrical section	Power sales department	System engineering dep.	
0	(Info	rmation) (Inform	ation)		(1) Scheduled date of completion, contracted pow and details of arc furnace facilities etc.
	° Reception of oral refere	nco			(2) Explaining considerable expense and a number days is also required for countermeasures o
	•	s of users' facilities (1)			flicker
	· ·	rules of power corporation (2 resentation of referred/techn			(3) Main circuit skeleton diagram, arc furnace impedance
	todaconnia rocomonia p	į			
	° Reception of reference d	ocuments/technical data			
		° Hearing required matters	for countermeasures (4)		<ul><li>(4) Kind and maker of reducing device</li><li>(5) Investigating the present condition of all a</li></ul>
() <b>-</b>			(Information)		furnace users within the same power system  Operating condition of arc furnace  Main circuit skeleton diagram
	<u> </u>	(Information)			<ul> <li>Arc furnace impedance</li> <li>(6) . Various data of ΔV<sub>10</sub>: estimated value, act</li> </ul>
	Request of t	echnical studies			measured value at present, estimated value after newly/additional installation
Data inv	vestigation (5)				. Required rate of flicker reduction . Rate of flicker reduction with TQC
:			on of technical studies asurement in advance)		. Rate of reactive power compensation and required capacity of TQC etc.
		° Technical	studies (6)		(7) Conditions of power supply system (impedance critical bus, required rate of flicker reduced)
·		Forw	arding technical reports		etc.
· · · · · · · · · · · · · · · · · · ·	Forward	ing technical reports	Investigati of study	on details	
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		Notice of	investigation results	<u> (기교 및 공격 및 교육 및 기</u> 관 (기교 ) - 기교 기교 기관 등 기교 (기교 )	

