

#### 4.2 Comparative Study on Alternative Flood Control Plan

Supplement data in this section are as follows;

- Breakdown of work quantity and construction cost for alternatives ( Table 4.2.1 )
- Design discharge distributions for alternatives (Fig. 4.2.1)
- Design profiles of the Widas river for alternatives (Fig. 4.2.2)

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (1/26)

WORK ITEM	QUANTITY		COST		QUANTITY		COST		QUANTITY		COST		QUANTITY		COST			
	QTY	UNIT	QTY	UNIT	QTY	UNIT	QTY	UNIT	QTY	UNIT	QTY	UNIT	QTY	UNIT	QTY	UNIT		
DEPOSITS (1000 CB)	1522	CB	8347	720	2570				2553	6519	701	2524						
EXCAVATION (1000 CB)	2262	CB	5320	720	1584	890	2047	265	567	2383	5991	720	1584	1144	2629	230	524	
EMBANKMENT (1000 CB)	737	CB	2799	316	770	441	770	416	915	933	2799	316	770	523	1144	374	867	
SEWAGEMENT																		
RETAINMENT (SH)	48116	SH	1845	12043	358	21665	542	30913	773	48116	1845	12243	567	30045	751	20753	674	
RETAINMENT (SR)	68145	SR	1045	7682	161	21665	433	30912	618	68145	1045	7682	161	30045	401	20752	537	
BRIDGE																		
ROAD I		(MS)	1		1		1			1		1		1				
		(SH)			765	1017	1260	1674				765	1017	126	1674			
II		(MS)	1		2		3			1		2		2		3		
		(SH)			1190	1428	586	705	882	1058		1190	1428	588	705	882	1058	
III		(MS)	9		2		8			9		2		9		8		
		(SH)			2350	2350	600	1044	1183	1183		2350	2380	600	1274	1274	798	798
RAILWAY		(MS)	1		1		1			1		1		1				
		(M)	85		1316	84	1050			85		1316	84	1050				
DRAINAGE CONDUIT																		
I		(MS)	4		180	2	90	6	270	4	180	2	90	6	270	3	135	
II		(MS)	4		240	4	240	3	180	1	60	4	240	3	180	1	60	
III		(MS)	4		380	1	95			4	380	1	95			1	95	
DIVERSION WEIR (MS)																		
		(M)			15		450	15	450		15		450	15	450		450	
IRRIGATION HEAD WORKS (MS)					1		2		3		1		2		2		2	
		(M)			33		3300	23	2300	21	2100		33		3300	30	3000	
SIDE OVERFLOW DIKE																		
		(M)	3		2600	1820				3		2600	1820					
DROP STRUCTURE																		
		(M)			2346	12103	11808	8125				2346	12106	13851	6710			
ADUUCT																		
		(MS)																
		(M)																
SYPHONE																		
		(MS)			1		70	105	70	105		1		70	105	70	105	
GRAVEL RETAILING																		
		(M)																
RELOCATION OF ROAD																		
		(M)																
SUB-TOTAL			2346		12103	11808	8125			2347	12106	13851	6710					
LAND ACQUISITION																		
RESIDENTIAL (1000 SH)																		
OTHERS (1000 SH)																		
BUILDING COMPENSATION																		
I		(MS)	5127	5127	800	954	589	689		5153	5153	800	1029	1029	612	612		
II		(MS)	245	343	55	77	375	553	400	245	343	55	77	445	623	400	560	
III		(MS)																
SUB-TOTAL			5472		877	1307	1249			5496	877	1307	1249					
TOTAL			29416		12780	13315	9374			29433	12783	13303	7882				65791	



(MILLION, RP)

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (3/26)

WORK ITEM RIVER	KIDAS			KEDUNGSOKO			U.L.O			KUNCIK			DIVERSION CHANNEL			TOTAL		
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
DREDGING (1000 CB)	2122	6356	621	2174														
EXCAVATION (1000 CB)	2121	4666	620	1364	784	1803	265	583										
EMBANKMENT (1000 CB)	925	2775	316	790	362	796	416	915										
REVEINEMENT																		
METASCHORY ( SN)	46116	1845	7683	231	19330	483	30913	773										
DYMASCHORY ( N)	46115	1015	7682	161	19330	387	30912	618										
BRIDGE																		
ROAD I ( NOS)			1		1													
(SN)			745	1017	1260	1676												
II ( NOS)	1				2		3											
(SN)	1190	1428	588	706	882	1058												
III ( NOS)	9		2		6		8											
(SN)	2350	2350	600	600	1064	1183												
RAILWAY ( NOS)			1		1													
(N)			85	1318	84	1059												
DRAINAGE CULVERT																		
I ( NOS)	4	180	2	90	6	270	4	180										
II ( NOS)	4	260	4	260	3	195	1	65										
III ( NOS)	5	475	1	95			1	95										
DIVERSION WEIR ( NOS)																		
(N)			15	450	15	450	15	450										
IRRIGATION HEAD WORKS ( NOS)			1		2		3											
(N)			33	3300	23	2300	21	2100										
SIDE OVERFLOW DIKE ( NOS)	3	2013																
(N)			2875															
DROP STRUCTURE ( NOS)																		
(N)																		
ADUCT ( NOS)																		
(N)																		
SYPHONE ( NOS)																		
(N)			1		70	105	70	105										
BRANEL METALLINE ( N)																		
RELOCATION OF ROAD ( N)																		
SUB-TOTAL	23373	11400	11285	8125														
LAND ACQUISITION																		
RESIDENTIAL (1000 SH)	5127	5127	800	800	816	816	689	689										
OTHERS (1000 SH)																		
BUILDING COMPENSATION																		
I ( NOS)																		
II ( NOS)	245	343	55	77	365	511	400	560										
III ( NOS)																		
SUB-TOTAL	5470	5470	877	877	1327	1249												
TOTAL	28843	12277	12612	9374														
			28547	12277	17612	9374												

(MILLION. RP)

(MILLION. RP)

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST ( 4/26 )

	W.D.A.S.				KEDUNGSOKO				U.L.O.				KUNCIK				DIVERSION CHANNEL				TOTAL				
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	
WORK UPON RIVER																									
BREDDING (1000 CH)	1814	5442	6121	2174																					
EXCAVATION (1000 CH)	1813	3789	420	1364	784	1903	245	583																	
EMBANKMENT (1000 CH)	925	2775	316	790	362	776	416	915																	
REVEGETMENT																									
METAMASONRY (SM)	46116	1845	7683	231	19330	483	30913	773																	
DRY MASONRY (SM)	46115	1015	7682	161	19330	387	30912	618																	
BRIDGE																									
ROAD I			1		1																				
(SM)			765	1017	260	1676																			
ROAD II			1		2																				
(MS)			1190	1428	588	706	982	1059																	
III			9		6			8																	
(MS)			2350	2350	600	1064	1084	1183																	
RAILWAY																									
(MS)			1		1																				
(H)			85	1318	84	1050																			
DRAINAGE CULVERT																									
I			4	180	2	90	6	270	4	180															
(MS)			4	260	4	260	3	195	1	65															
II			6	570	1	95			1	95															
III																									
(MS)																									
DIVERSION WEIR (MS)																									
(H)																									
(H)																									
IRRIGATION HEAD WORKS (MS)																									
(H)																									
(H)																									
SIDE OVERFLOW DIKE (MS)																									
(H)			33	3300	23	2300	21	2100																	
DAOP STRUCTURE (MS)																									
(H)			3	2337																					
ARQUEDUCT (MS)																									
(H)																									
(H)																									
SYMPHONIC (MS)																									
(H)			1		70	105	70	105																	
GRAVEL METALLING (H)																									
(H)																									
RELOCATION OF ROAD (H)																									
(H)																									
SUB-TOTAL	2291	11400	11400	8125	2291	11400	11400	8125	2291	11400	11400	8125	2291	11400	11400	8125	2291	11400	11400	8125	2291	11400	11400	8125	
LAND ACQUISITION																									
RESIDENTIAL (1000 SR)	5127	5127	800	816	816	689	689																		
OTHERS (1000 SR)																									
BUILDING COMPENSATION																									
I	245	343	55	77	365	511	400	560																	
II																									
III																									
(MS)			5470	877	1327	1249																			
SUB-TOTAL	27561	12277	12277	12612	9374	61824																			
TOTAL	29852	12707	12707	9386	21795	15603	7882	65791																	

(MILLION, RP)

(MILLION, RP)

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (5/26)

WORK ITEM RIVER	KIDAS				KEDURUSOKO				U.L.O				KUNCIK				DIVERSION CHANNEL				TOTAL			
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
DREDGING (1000 CM)	2127	6411	618	2163																				
EXCAVATION (1000 CM)	2137	4701	617	1367																				
EMBANKMENT (1000 CM)	925	2775	316	790																				
REVEGETATION																								
RETAINMENT (SM)	46116	1845	7683	230	27710	683	26953	674																
DRY MASONRY (SM)	46115	1015	7682	161	27710	551	26952	539																
BRIDGE																								
ROAD I			1		1																			
(SM)			765	1017	126	1676																		
(MS)					2																			
ROAD II			1																					
(MS)			1190	1428																				
(SM)			9		9																			
(MS)			2380	2380	600	600	1274	798	798															
RAILWAY			1		1																			
(MS)			85	1318	84	1050																		
DRAINAGE CULVERT																								
I			4	180	2	80	270	3	135															
(MS)			4	260	4	260	3	195	1	65														
II			4	475	1	95																		
III																								
DIVERSION WEIR (MS)																								
(MS)					15	450	15	450	15	450														
DIVERSION HEAD WORKS (MS)			1		1																			
(MS)			33	3300	30	3000	14	1400																
SIDE OVERFLOW DIVE			3	2013																				
(MS)			2875																					
DROP STRUCTURE																								
(MS)																								
AQUEDUCT																								
(MS)																								
SYPHONE																								
(MS)																								
GRAVEL RETAINING																								
(MS)																								
RELOCATION OF ROAD																								
(MS)																								
SUB-TOTAL			23483		11381		13068		6710															
LAND ACQUISITION																								
RESIDENTIAL (1000 SM)			5153	5153	800	800	878	878	612	612														
OTHERS (1000 SM)																								
BUILDING COMPENSATION																								
I																								
II			245	343	55	77	415	581	400	560														
III																								
SUB-TOTAL			5496		877		1459		1172															
TOTAL			28979		12259		14927		7882															
TOTAL			63347																					







Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (8/26)

WORK ITEM RIVER	SCHEME II (CASE 2)			SCHEME III (CASE 1)			TOTAL		
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	
DREDGING (1000 CB)	1842	5526	618	2163	2031	6093	495	1470	
EXCAVATION (1000 CB)	1842	4052	617	1257	2031	5166	487	1076	
EMBANKMENT (1000 CB)	925	2775	316	790	733	2775	308	770	
RETAINMENT									
MASONRY (SQ)	46116	1845	7683	230	15105	378	26353	674	
CONCRETE (SQ)	46115	1015	7682	161	15105	305	26952	535	
BRIDGE									
ROAD I (NO)	1	765	1017	1	315	419	1	1260	
II (NO)	1	1190	1428	3	882	1058	2	569	
III (NO)	9	2681	600	620	798	798	6	1064	
RAILWAY (NO)	1	85	1318	1	35	438	1	84	
DRAINAGE CULTURE									
I (NO)	4	180	2	70	3	135	6	270	
II (NO)	4	260	4	260	1	65	3	195	
III (NO)	6	570	1	95	1	95	3	285	
DIVERSION WEIR (NO)									
I (NO)	1	15	450	15	450	15	450	15	
II (NO)	33	3300	14	1400	14	1400	25	3300	
III (NO)	3	2237	1	1	2	2	2	2	
IRRIGATION HEAD WORKS (NO)									
I (NO)	1740	1218	1000	700	1	1	1	1	
II (NO)	2	2	2	2	33	3300	2	2	
III (NO)	2	2	2	2	2	2	2	2	
SIDE OVERFLOW PIPE (NO)									
I (NO)	1	1	1	1	1	1	1	1	
II (NO)	1	1	1	1	1	1	1	1	
III (NO)	1	1	1	1	1	1	1	1	
DROP STRUCTURE (NO)									
I (NO)	1	1	1	1	1	1	1	1	
II (NO)	1	1	1	1	1	1	1	1	
III (NO)	1	1	1	1	1	1	1	1	
HAZARDOUS (NO)									
I (NO)	1	1	1	1	1	1	1	1	
II (NO)	1	1	1	1	1	1	1	1	
III (NO)	1	1	1	1	1	1	1	1	
SPRINGS (NO)									
I (NO)	1	1	1	1	1	1	1	1	
II (NO)	1	1	1	1	1	1	1	1	
III (NO)	1	1	1	1	1	1	1	1	
GRAVEL METALLING (NO)									
I (NO)	1	1	1	1	1	1	1	1	
II (NO)	1	1	1	1	1	1	1	1	
III (NO)	1	1	1	1	1	1	1	1	
REDUCTION OF ROAD (NO)									
I (NO)	1	1	1	1	1	1	1	1	
II (NO)	1	1	1	1	1	1	1	1	
III (NO)	1	1	1	1	1	1	1	1	
SUB-TOTAL	23925	11381	4246	6710	4059	21939	8461	11800	
LAND ACQUISITION									
RESIDENTIAL (1000 SF)									
OTHERS (1000 SF)	5344	5344	600	240	612	612	166	166	
BUILDING COMPENSATION									
I (NO)	270	378	55	77	70	126	400	560	
II (NO)	1	1	1	1	1	1	1	1	
III (NO)	1	1	1	1	1	1	1	1	
SUB-TOTAL	5722	877	366	1172	214	5470	856	1507	
TOTAL	28791	12258	4612	7882	4772	27409	9317	13315	
TOTAL									

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (9/26)

SCHEME III (CASE I)  
 LIMITED CARRYING CAPACITY AT K. SOLO BRIDGES, Q = 145 CM/SEC  
 CAPACITY OF K. SOLO RETARDING BASIN  
 V = 6.7 X MILLION CM  
 CAPACITY OF OLD RETARDING BASIN  
 V = 4.0 X MILLION CM

SCHEME III (CASE I)  
 LIMITED CARRYING CAPACITY AT K. SOLO BRIDGES, Q = 145 CM/SEC  
 CAPACITY OF K. SOLO RETARDING BASIN  
 V = 6.7 X MILLION CM  
 CAPACITY OF OLD RETARDING BASIN  
 V = 2.0 X MILLION CM

WORK ITEM RIVER	MILLION, RF)											
	WIDAS		KEMUNGSOK		U.L.D		KUNCIK		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
DRESSING (1000 CM)	1868	5664	435	1533								
EXCAVATION (1000 CM)	1868	4110	434	955	784	1083	245	583				
EMBANKMENT (1000 CM)	925	2775	308	770	362	796	416	915				
REVEINEMENT												
BETRAKUNY (SN)	46116	1845	4560	137	19330	483	30913	773				
OPRAKUNY (SN)	46115	1315	4559	96	19330	387	30912	618				
BRIDGE												
ROAD I					1							
SH					280	1676						
II					2							
SH					1190	1428						
III					5							
SH					2350	2350						
RAILWAY												
(NS)					84	1050						
DRAINAGE CULVERT												
I					4	180						
II					4	240						
III					4	380						
DIVERSION WEIR (NS)					4	380						
(N)					1							
IRRIGATION HEAD WORKS (NS)					15	450						
(N)					2							
SIDE OUTFLOW DIKE (NS)					35	3380						
(N)					3							
DROP STRUCTURE (NS)					2015	1411						
(N)												
ARBUENCT (NS)												
(N)												
SYPHONE (NS)												
(N)												
GRAVEL METALLING (NS)												
(N)												
RELOCATION OF ROAD (N)												
SUB-TOTAL	21358	8236	8236	11285	8125	20958	8236	11285	8125			
LAND ACQUISITION												
RESIDENTIAL (1000 SH)												
GRASS (1000 SH)	5127	5127	766	816	816	689	689	689	689	689	689	689
BUILDING COMPENSATION												
I												
II												
III												
SUB-TOTAL	5470	5470	836	1327	1249	1327	836	1327	1327	1327	1327	1327
TOTAL	26828	9072	9072	12612	9374	26428	9072	12612	9374			57566

(SCHEME III, CASE I)

LIMITED CARRYING CAPACITY AT K. SONG BRIDGES, Q = 145 CM/SEC  
 CAPACITY OF K. SONG RETARDING BASIN, V = 6.7 X MILLION CM  
 CAPACITY OF OLD RETARDING BASIN, V = 9.0 X MILLION CM

(MILLION, RP)

WORK ITEM RIVER	WIDMS		KEDUNSSOKO		ULG		KUNDIR		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
DREDGING (1000 CM)	1514	4592	455	1523								
EXCAVATION (1000 CM)	1514	3331	424	955	784	1083	252	563				
EMBANKMENT (1000 CM)	925	2775	308	770	362	776	416	915				
RETAINMENT												
METHADORY (SH)	46116	1845	4560	137	17330	483	32113	773				
DRYMASSORY (SH)	46115	1015	4259	76	57230	387	30712	618				
BRIDGE												
Road I (MS)					1							
(SH)					260	1676						
II (MS)	1				2		3					
(SH)	1190	1428			588	706	882	1058				
III (MS)	9		1		6		8					
(SH)	2350	2350	300	300	1064	1064	1183	1183				
RAILWAY (MS)					1							
(SH)					84	1050						
DRAINAGE CULVERT												
I (MS)	4	180			6	270	4	180				
II (MS)	4	260			3	195	1	65				
III (MS)	5	475			5	475	1	95				
DIVERSION WEIR (MS)					1		1					
(SH)					15	450	15	450				
IRRIGATION HEAD WORKS (MS)					2		3					
(SH)					33	3300	23	2300				
SIDE OVERTLOW DIVE (MS)	3		2				21	2100				
(SH)	2345	1642	1000	700								
DROP STRUCTURE (MS)												
(SH)												
ABUDDUCT (MS)												
(SH)												
SPYDOME (MS)					1		1					
(SH)					70	105	70	105				
GRAVEL METALLING (SH)												
RELOCATION OF ROAD (SH)												
SUB-TOTAL	17853		8756		11785		8125					

LAND ACQUISITION	WIDMS		KEDUNSSOKO		ULG		KUNDIR		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
RESIDENTIAL (1000 SH)	5127	5127	766	766	816	816	689	689				
OTHERS (1000 SH)												
BUILDING COMPENSATION												
I (MS)												
II (MS)	245	343	50	70	365	511	400	560				
III (MS)												
SUB-TOTAL	5470		836		1327		1249					
TOTAL	23313		9592		12612		9374					

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (10/26)

(MILLION, RP)

(SCHEME III, CASE I)

LIMITED CARRYING CAPACITY AT K. SONG BRIDGES, Q = 195 CM/SEC  
 CAPACITY OF K. SONG RETARDING BASIN, V = 4.2 X MILLION CM  
 CAPACITY OF OLD RETARDING BASIN, V = 9.0 X MILLION CM

WORK ITEM RIVER	WIDMS		KEDUNSSOKO		ULG		KUNDIR		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
DREDGING (1000 CM)	2119	6357	521	1824								
EXCAVATION (1000 CM)	2118	4660	521	1146	870	2047	265	583				
EMBANKMENT (1000 CM)	923	2799	308	770	441	970	416	915				
RETAINMENT												
METHADORY (SH)	46116	1845	4553	218	21665	542	30913	773				
DRYMASSORY (SH)	46115	1015	4252	152	21665	433	30912	618				
BRIDGE												
Road I (MS)					1							
(SH)					465	162	1260	1676				
II (MS)	1				2		3					
(SH)	1190	1428			588	706	882	1058				
III (MS)	9		1		6		8					
(SH)	2350	2350	300	300	1064	1064	1183	1183				
RAILWAY (MS)					1							
(SH)					45	207	84	1050				
DRAINAGE CULVERT												
I (MS)	4	180			6	270	4	180				
II (MS)	4	260			3	195	1	65				
III (MS)	5	475			5	475	1	95				
DIVERSION WEIR (MS)					1		1					
(SH)					15	450	15	450				
IRRIGATION HEAD WORKS (MS)					2		3					
(SH)					33	3300	23	2300				
SIDE OVERTLOW DIVE (MS)	3		2				21	2100				
(SH)	2345	1642	1000	700								
DROP STRUCTURE (MS)												
(SH)												
ABUDDUCT (MS)												
(SH)												
SPYDOME (MS)					1		1					
(SH)					70	105	70	105				
GRAVEL METALLING (SH)												
RELOCATION OF ROAD (SH)												
SUB-TOTAL	22593		9079		11808		8125					

LAND ACQUISITION	WIDMS		KEDUNSSOKO		ULG		KUNDIR		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
RESIDENTIAL (1000 SH)	5127	5127	766	766	766	766	954	954	689	689		
OTHERS (1000 SH)												
BUILDING COMPENSATION												
I (MS)												
II (MS)	245	343	50	70	375	523	400	560				
III (MS)												
SUB-TOTAL	5470		836		1307		1249					
TOTAL	29063		9915		13715		9374					

LIMITED CARRYING CAPACITY AT K.SONG BRIDGES, Q = 195 CM/SEC  
 CAPACITY OF X.SONG RETARDING BASIN, V = 4.2 X MILLION CM  
 CAPACITY OF OLD RETARDING BASIN, V = 4.0 X MILLION CM

LIMITED CARRYING CAPACITY AT K.SONG BRIDGES, Q = 195 CM/SEC  
 CAPACITY OF X.SONG RETARDING BASIN, V = 4.2 X MILLION CM  
 CAPACITY OF OLD RETARDING BASIN, V = 4.0 X MILLION CM

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (11/26)

WORK ITEM/RIVER	(MILLION, RP)				(MILLION, RP)			
	WIDAS	KEDUNGSOKO	ULO	KURCIR	WIDAS	KEDUNGSOKO	ULO	KURCIR
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
	TOTAL				TOTAL			
DREDGING (1000 CM)	1945	5025	452	1582	1816	5440	452	1582
EXCAVATION (1000 CM)	1944	4277	451	972	1816	3975	451	1972
EMBANKMENT (1000 CM)	925	2775	208	770	925	2775	208	770
REVEINEMENT								
RETAINMASONRY (SM)	46116	1845	4560	137	46116	1845	4560	137
DRYMASONRY (SM)	46115	1015	4559	96	46115	1015	4559	96
BRIDGE								
ROAD I			1	162			1	162
II			405	162			405	162
III			2	1676			2	1676
RAILWAY								
RAILWAY (NS)	1190	1428	588	706	1190	1428	588	706
RAILWAY (M)	9		8		9		8	
RAILWAY (H)	2350	2350	300	1064	2350	2350	300	1064
RAILWAY (NS)	1		1		1		1	
RAILWAY (M)	45		84	1050	45		84	1050
RAILWAY (H)								
DRAINAGE CULVERT								
I	4	180	6	270	4	180	6	270
II	4	260	2	130	4	260	2	130
III	4	380	4	380	4	380	4	380
DRAINAGE WEIR (NS)								
DRAINAGE WEIR (M)								
DRAINAGE WEIR (H)								
IRIGATION HEAD WORKS (NS)								
IRIGATION HEAD WORKS (M)								
IRIGATION HEAD WORKS (H)								
SIDE OVERFLOW DIKE (NS)								
SIDE OVERFLOW DIKE (M)								
SIDE OVERFLOW DIKE (H)								
DROP STRUCTURE								
AGUEDIUCT								
AGUEDIUCT (NS)								
AGUEDIUCT (M)								
AGUEDIUCT (H)								
SPHONGE								
SPHONGE (NS)								
SPHONGE (M)								
SPHONGE (H)								
GRAVEL METALLING								
RELOCATION OF ROAD								
RELOCATION OF ROAD (NS)								
RELOCATION OF ROAD (M)								
RELOCATION OF ROAD (H)								
SUB-TOTAL	21950	8546	11285	8125	21556	8546	11285	8125
LAND ACQUISITION								
RESIDENTIAL (1000 SR)								
OTHERS (1000 SR)								
BUILDING COMPENSATION								
I	5127	5127	766	816	5127	5127	766	816
II	245	343	50	70	245	343	50	70
III								
SUB-TOTAL	5570	856	1327	1249	5470	856	1327	1249
TOTAL	27422	9382	12612	9374	27026	9382	12612	9374

LIMITED CARRYING CAPACITY AT K. SOND BRIDGES, Q = 300 CM/SEC  
 CAPACITY OF K. SOND RETARDING BASIN, V = 1.9 X MILLION CM  
 CAPACITY OF ULO RETARDING BASIN, V = 0.0 X MILLION CM

LIMITED CARRYING CAPACITY AT K. SOND BRIDGES, Q = 195 CM/SEC  
 CAPACITY OF K. SOND RETARDING BASIN, V = 4.2 X MILLION CM  
 CAPACITY OF ULO RETARDING BASIN, V = 6.0 X MILLION CM

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (12/26)

WORK ITEM/RIVER	(MILLION, RP)											
	WIDAS		KEDUNESOD		ULO		KUNCIK		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
PREBIDING (1000 CM)	1603	4607	452	1582	1	1676	1	1676				
ELEVATION (1000 CM)	1603	3527	451	1992	784	1083	265	583				
EMBANKMENT (1000 CM)	925	2773	308	770	362	796	416	915				
REVEINMENT												
RETARDATORY (SM)	46116	1845	4560	137	19730	682	22713	773				
RETARDATORY (SM)	46115	1015	4559	96	13330	357	30912	619				
BRIDGE												
ROAD I (M)	1	403	1	162	1	1676	1	1676				
ROAD II (M)	1	1	2	260	2	1576	3	1576				
ROAD III (M)	9	1428	1	1190	588	706	632	1058				
RAILWAY (M)	2350	2350	300	300	1064	1064	1183	1183				
DISCHARGE CONVEY (M)												
I (M)	4	180	6	270	4	180	4	180				
II (M)	4	260	2	120	3	175	1	65				
III (M)	5	475	4	380	1	95	1	95				
DIVERSION WEIR (M)												
I (M)	1	1	1	1	1	1	1	1				
IRRIGATION HEAD WORKS (M)												
I (M)	33	3300	2	2	15	450	15	450				
II (M)	2	2	2	2	2	2	2	2				
III (M)	2420	1694	700	490	23	2300	21	2100				
SIDE OVERFLOW DIKE (M)												
I (M)	3	3	33	3300	23	2300	21	2100				
II (M)	2420	1694	700	490								
DIAPHRAGM (M)												
I (M)												
II (M)												
III (M)												
SYPHONE (M)												
I (M)												
II (M)												
III (M)												
GRAVEL RETAILLINGS (M)												
RELOCATION OF ROAD (M)												
SUB-TOTAL	20432	8544	8544	11295				8125				
LAND ACQUISITION												
RESIDENTIAL (1000 SM)												
OTHERS (1000 SM)	5127	5127	766	766	816	816	689	689				
BUILDING COMPENSATION												
I (M)												
II (M)	245	343	50	70	365	511	400	360				
III (M)												
SUB-TOTAL	5470	636		1327		1249		1249				
TOTAL	25700	9362		12610		9374		9374				63170



LIMITED CARRYING CAPACITY AT X-SHED BRIDGES , Q = 300 CM/SEC  
 CAPACITY OF X-SHED RETARDING BASIN  
 CAPACITY OF ULD RETARDING BASIN

(MILLION. RP)

WORK ITEM/RIVER	MIDAS		KEDINGSOKO		ULD		KUNCIER		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
BREEDING (1000 CH)	1743	5229	520	1820								
EXCAVATION (1000 CH)	1742	3632	519	1152	784	1683	265	593				
EMBANKMENT (1000 CH)	925	2775	308	770	362	796	416	915				
REVEINEMENT	46116	1845	4560	137	19330	483	30913	773				
METHASORRY (SH)	46115	1015	4559	96	19330	387	30912	618				
BRIDGE												
ROAD I (MS)			1		1							
(SM)			630	838	1260	1676						
II (MS)			1		2							
(SM)			1190	1428	598	706	882	1058				
III (MS)			9		6							
(SM)			2350	2350	300	1064	1064	1183				
RAILWAY (MS)			1		1							
(SM)			70	1085	84	1050						
DRAINAGE CULVERT												
I (MS)			4	185	6	270	4	180				
II (MS)			4	280	2	130	3	195				
III (MS)			5	475	3	285	1	95				
DIVERSION WEIR (MS)					1		1					
(SM)					15	450	15	450				
IRRIGATION HEAD WORKS (MS)			1		2		3					
(SM)			35	3300	23	2300	21	2100				
SIDE OVERTLOW DIKE (MS)			3		1							
(SM)			2845	1972	500	550						
PROP STRUCTURE												
ABUTMENT (MS)												
(SM)												
SYMPHON (MS)												
(SM)												
GRAVEL RETAILLING (MS)												
RELOCATION OF ROAD (MS)												
SUB-TOTAL			21281	10253	10253	11285	8125	8125				

LAND ACQUISITION	MIDAS		KEDINGSOKO		ULD		KUNCIER		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
RESIDENTIAL (1000 SH)												
OTHERS (1000 SH)	5127	5127	766	766	816	816	689	689				
BUILDING COMPENSATION												
I (MS)												
II (MS)			245	343	50	70	365	511	400	560		
III (MS)												
SUB-TOTAL			5470	5470	826	826	1327	1249	1249	1249		
TOTAL			26851	11089	12612	9374	5926	5926				

LIMITED CARRYING CAPACITY AT X-SHED BRIDGES , Q = 145 CM/SEC  
 CAPACITY OF X-SHED RETARDING BASIN  
 CAPACITY OF ULD RETARDING BASIN

(MILLION. RP)

WORK ITEM/RIVER	MIDAS		KEDINGSOKO		ULD		KUNCIER		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
BREEDING (1000 CH)	2077	6231	514	1777								
EXCAVATION (1000 CH)	2076	4657	514	1151	1142	2677	238	574				
EMBANKMENT (1000 CH)	933	2799	308	770	520	1144	394	867				
REVEINEMENT	46116	1845	7453	210	30045	751	26753	674				
METHASORRY (SH)	46115	1015	7252	152	30045	601	26952	529				
BRIDGE												
ROAD I (MS)					1							
(SM)					1260	1676						
II (MS)					2							
(SM)			1190	1428	508	705	892	1058				
III (MS)			9		7							
(SM)			2380	2380	300	1074	1074	798				
RAILWAY (MS)												
(SM)					84	1050						
DRAINAGE CULVERT												
I (MS)			4	180	6	270	3	135				
II (MS)			4	280	2	130	3	195				
III (MS)			5	475	3	285	1	95				
DIVERSION WEIR (MS)					1		1					
(SM)					15	450	15	450				
IRRIGATION HEAD WORKS (MS)			1		2		2					
(SM)			35	3300	23	2300	30	3000				
SIDE OVERTLOW DIKE (MS)			3		1							
(SM)			2845	1972	500	550						
PROP STRUCTURE												
ABUTMENT (MS)												
(SM)												
SYMPHON (MS)												
(SM)												
GRAVEL RETAILLING (MS)												
RELOCATION OF ROAD (MS)												
SUB-TOTAL			22404	8975	12851	12851	6710	6710				

LAND ACQUISITION	MIDAS		KEDINGSOKO		ULD		KUNCIER		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
RESIDENTIAL (1000 SH)												
OTHERS (1000 SH)	5153	5153	718	718	1027	1027	612	612				
BUILDING COMPENSATION												
I (MS)												
II (MS)			245	343	45	63	465	633	400	560		
III (MS)												
SUB-TOTAL			5476	5476	781	781	1652	1652	1172	1172		
TOTAL			27900	9756	15503	15503	7822	7822				

LIMITED CARRYING CAPACITY AT K.SOKO BRIDGES, Q = 145 CM/SEC  
 CAPACITY OF K.SOKO RETARDING BASIN  
 P, V = 4.8 X MILLION CM  
 CAPACITY OF OLD RETARDING BASIN  
 V = 4.0 X MILLION CM

LIMITED CARRYING CAPACITY AT K.SOKO BRIDGES, Q = 145 CM/SEC  
 CAPACITY OF K.SOKO RETARDING BASIN  
 P, V = 4.8 X MILLION CM  
 CAPACITY OF OLD RETARDING BASIN  
 V = 2.0 X MILLION CM

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (15/26)

WORK ITEM/TYPE	WIDNS (MILLION, RP)				KUNCIK DIVERSION CHANNEL (MILLION, RP)				KUNCIK EVERESICH CHANNEL (MILLION, RP)				TOTAL					
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST		
RECORDING (1000 CM)	1923	5772	441	1544														
EXCAVATION (1000 CM)	1923	4231	440	988	959	2206	988	2206	238	524								
EMBANKMENT (1000 CM)	925	2775	308	770	404	887	354	867	384	867								
REVEGETATION																		
RETARDATORY (SH)	46116	1845	4560	137	27710	693	26753	674										
RETARDATORY (SH)	46116	1015	4559	96	27710	564	26752	539										
BRIDGE																		
ROAD I					1													
(SH)					1260	1676												
(NS)					2													
II					1190	1428												
(SH)					508	706	882	1058										
(NS)					9													
III					2380	2380												
(SH)					300	300	1274	1274	798	798								
(NS)					1													
RAILWAY					84	1050												
(NS)																		
DRAINAGE CULVERT																		
I					4	180												
(NS)					6	270	3	135										
II					4	260	2	120	3	195	1	65						
(NS)					3	380	5	475	1	95	1	95						
III																		
(NS)					15	450	15	450										
DIVERSION WEIR (NS)					1													
(NS)					2													
IRRIGATION HEAD WORKS (NS)					1													
(NS)					33	3300	30	3000	14	1400								
SIDE OVERFLOW DIKE (NS)					3													
(NS)					2275	1592	1000	700										
DROP STRUCTURE (NS)																		
(NS)																		
ARIEDUCT (NS)																		
(NS)																		
SYPHONE (NS)					1													
(NS)					70	105	70	105										
GRAVEL RETAILLING (NS)																		
RELOCATION OF ROAD (NS)																		
SUB-TOTAL		21859		8420		13068		6710				21851		8420		13068		6710
LAND ACQUISITION																		
RESIDENTIAL (1000 SH)																		
OTHERS (1000 SH)					5155	5155	718	718	878	878	612	612						
BUILDING COMPENSATION																		
I (NS)					245	343	45	63	415	581	400	560						
II (NS)																		
III (NS)																		
SUB-TOTAL					5476	5476	781	1459	1172	1459	1172							
TOTAL					27355	27355	7201	14827	7882	14827	7882							
					58765	58765	9201	14827	7882	14827	7882							
					58765	58765	9201	14827	7882	14827	7882							



LIMITED CARRYING CAPACITY AT K.SIKO BRIDGES , Q = 195 CM/SEC  
 CAPACITY OF K.SIKO RETAINING BASIN , V = 3.2 X MILLION CM  
 CAPACITY OF ULO RETAINING BASIN , V = 0.0 X MILLION CM

LIMITED CARRYING CAPACITY AT K.SIKO BRIDGES , Q = 145 CM/SEC  
 CAPACITY OF K.SIKO RETAINING BASIN , V = 4.8 X MILLION CM  
 CAPACITY OF ULO RETAINING BASIN , V = 8.0 X MILLION CM

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (16/26)

WORK ITEM/RAJDER	(MILLION, RP)										(MILLION, RP)													
	HIGHS		KEDURUSOPO		ULU		PUNCIK		DIVERSION CHANNEL		TOTAL		HIGHS		KEDURUSOPO		ULU		PUNCIK		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
DEBRISING (1000 CM)	1854	4072	441	1544																				
EXCAVATION (1000 CM)	1833	3371	440	763	959	2206	230	324																
EMBANKMENT (1000 CM)	725	2775	308	776	404	889	374	867																
REVEGET																								
RETAINING WALL (CM)	48116	1845	4560	137	2710	637	2053	674																
DRYHATCHWAY (SM)	48115	1015	4557	76	2710	554	2652	537																
BRIDGE																								
ROAD I (M)																								
II (M)																								
III (M)																								
RAILWAY (M)																								
DRAINAGE CULVERT																								
I (M)	4	180			6	370	3	135																
II (M)	4	240	2	130	3	195	1	65																
III (M)	5	475	5	475			1	95																
DIVERSION WEIR (M)																								
I (M)					15	450	15	450																
II (M)					2		2																	
III (M)					33	3300	30	2000	14	1400														
IRRIGATION HEAD WORKS (M)																								
I (M)	3		2																					
II (M)	2665	1866	1000	700																				
DRIP STRUCTURE (M)																								
APENDUCT (M)																								
SYPHONE (M)																								
GRAVEL METALLING (M)																								
RELOCATION OF ROAD (M)																								
SUB-TOTAL		20657		8120		13068		6710																
LAND ACQUISITION																								
RESIDENTIAL (1000 SM)																								
OTHERS (1000 SM)	5153	5153	718	718	878	878	612	612																
BUILDING COMPENSATION																								
I (M)																								
II (M)	245	343	45	62	415	581	400	560																
III (M)																								
SUB-TOTAL		5476		781		1459		1172																
TOTAL		26183		9201		14527		7882																

LIMITED CARRYING CAPACITY AT K. SOND BRIDGES, Q = 195 CM/SEC  
 CAPACITY OF K. SOND RETAINING BASIN, V = 3.2 X MILLION CM  
 CAPACITY OF OLD RETAINING BASIN, V = 4.0 X MILLION CM

LIMITED CARRYING CAPACITY AT K. SOND BRIDGES, Q = 195 CM/SEC  
 CAPACITY OF K. SOND RETAINING BASIN, V = 3.2 X MILLION CM  
 CAPACITY OF OLD RETAINING BASIN, V = 4.0 X MILLION CM

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (17/26)

WORK ITEM/TYPE	(MILLION. RP)						(MILLION. RP)					
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
	KEDURONG		KUNCI		KEDURONG		KUNCI		KEDURONG		KUNCI	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
PRELIMS (1000 CM)	1886	5657	465	1626								
EXCAVATION (1000 CM)	1885	4198	464	1021	959	2266	230	524	959	2266	230	524
EMBANKMENT (1000 CM)	925	2775	208	770	404	889	394	867	404	889	394	867
RETAINMENT												
RETAINMENT (CM)	46116	1845	4560	137	27710	673	26723	674	46116	1845	4560	137
RETAINMENT (SR)	46115	1015	4559	96	27710	554	26952	539	46115	1015	4559	96
BRIDGE												
ROAD I	1		1		1				1		1	
ROAD II	405	162	1260	1676	2				405	162	1260	1676
ROAD III	1190	1428			588	706	882	1058	1190	1428		
RAILWAY	9		9		9				9		9	
RAILWAY (MS)	2380	2380	300	1274	1274	798	798		2380	2380	300	1274
RAILWAY (N)	1		1		1				1		1	
RAILWAY (N)	45	207	84	1050					45	207	84	1050
DRAINAGE CULVERT												
DRAINAGE I	4	180	6	270	3	135			4	180	6	270
DRAINAGE II	4	280	2	150	3	195			4	280	2	150
DRAINAGE III	4	380	4	380					4	380	4	380
DRAINAGE (MS)	1		1		1				1		1	
DRAINAGE (N)	15	450	15	450	15	450			15	450	15	450
IRRIGATION HEAD WORKS (MS)	1		1		2				1		2	
IRRIGATION HEAD WORKS (N)	33	3300	30	3000	14	1400			33	3300	30	3000
SIDE OVERFLOW RIPE (N)	2515	1761	700	490					2515	1761	700	490
DROP STRUCTURE (MS)												
DROP STRUCTURE (N)	1		1		1				1		1	
AQUEDUCT (MS)												
AQUEDUCT (N)	70	105	70	105	70	105			70	105	70	105
SPYHOLE (MS)												
SPYHOLE (N)												
GRAVEL METALLING (N)												
RELOCATION OF ROAD (N)												
SUB-TOTAL	22417	8621	13063	6710	8621	13068	6710		22416	8621	13068	6710
LAND ACQUISITION												
RESIDENTIAL (1000 SR)	5153	5153	718	878	878	612	612		5153	5153	718	878
OTHERS (1000 SR)												
BUILDING COMPENSATION												
I (MS)												
II (MS)	245	343	45	63	415	581	490	560	245	343	45	63
III (MS)												
SUB-TOTAL	5498	5498	781	1489	1172	1172			5496	5496	781	1489
TOTAL	27913	9492	14527	7882	9492	14527	7882		27612	9492	14527	7882
TOTAL												

LIMITED CARRYING CAPACITY AT K.SORO BRIDGES, Q = 175 CM/SEC  
 CAPACITY OF K.SORO RETARDING BASIN  
 CAPACITY OF WLD RETARDING BASIN

(MILLION. RP)

WORK ITEM/RIVER	KIDGS		KEDUSSORO		KUNCIK		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
DREDGING (1000 CM)	3716	5148	485	1828						
EXCAVATION (1000 CM)	1715	2775	454	1021	589	2265	228	524		
EMBANKMENT (1000 CM)	925	2775	308	770	404	889	394	887		
RETAINMENT										
METASOROY (SM)	46116	1845	4560	137	27710	693	26783	674		
ORIMASOROY (SM)	46115	1015	4559	96	27710	564	26952	539		
BRIDGE										
ROAD I (NOS)			1		1					
GN (NOS)			405	162	1260	1676				
II (NOS)			1		2		3			
III (NOS)			1190	1428	588	784	882	1038		
RAILWAY (NOS)			2380	2380	300	1274	778	778		
DRAINAGE CULVERT (N)			45	207	84	1080				
I (NOS)			4	180	6	270	3	135		
II (NOS)			4	260	3	195	1	65		
III (NOS)			3	475	4	386	1	75		
DIVERSION WEIR (NOS)					1		1			
(N)					15	450	15	450		
IRRIGATION HEAD WORKS (NOS)			1		2		2			
(N)			33	3300	30	3000	14	1400		
SIDE OVERTLOW DIVE (NOS)			3		1					
(N)			2885	2020	700	490				
DAMP STRUCTURE (NOS)										
(N)										
AVENUECT (NOS)										
(N)										
SYPHONE (NOS)										
(N)										
GRANEL METALLING (N)										
RELOCATION OF ROAD (N)										
SUB-TOTAL	21295		6261		12068		6710		23415	

LAND ACQUISITION	KIDGS		KEDUSSORO		KUNCIK		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
RESIDENTIAL (1000 SQ)										
OTHERS (1000 SQ)	5153	5153	718	718	878	878	612	612		
BUILDING COMPENSATION										
I (NOS)										
II (NOS)	245	345	65	65	415	581	400	560		
III (NOS)										
SUB-TOTAL	5496		781		1493		1172		5496	
TOTAL	26795		7042		14527		7882		38606	

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (18/26)

LIMITED CARRYING CAPACITY AT K.SORO BRIDGES, Q = 300 CM/SEC  
 CAPACITY OF K.SORO RETARDING BASIN  
 CAPACITY OF WLD RETARDING BASIN

(MILLION. RP)

WORK ITEM/RIVER	KIDGS		KEDUSSORO		KUNCIK		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
DREDGING (1000 CM)	2201	6603	647	2477						
EXCAVATION (1000 CM)	2261	6842	548	1426	1143	5879	236	524		
EMBANKMENT (1000 CM)	933	2779	308	770	520	1414	394	887		
RETAINMENT										
METASOROY (SM)	46116	1845	4555	138	26945	751	26783	674		
ORIMASOROY (SM)	46115	1015	4552	152	26945	661	26952	539		
BRIDGE										
ROAD I (NOS)			1		1					
GN (NOS)			450	828	125	1676				
II (NOS)			1		2		3			
III (NOS)			1190	1428	588	765	882	1038		
RAILWAY (NOS)			2380	2380	300	1274	778	778		
DRAINAGE CULVERT (N)			45	207	84	1080				
I (NOS)			4	180	6	270	3	135		
II (NOS)			4	260	2	150	3	195		
III (NOS)			3	475	5	385	1	75		
DIVERSION WEIR (NOS)					1		1			
(N)					15	450	15	450		
IRRIGATION HEAD WORKS (NOS)			1		2		2			
(N)			33	3300	30	3000	14	1400		
SIDE OVERTLOW DIVE (NOS)			3		1					
(N)			2540	1778	500	350				
DAMP STRUCTURE (NOS)										
(N)										
AVENUECT (NOS)										
(N)										
SYPHONE (NOS)										
(N)										
GRANEL METALLING (N)										
RELOCATION OF ROAD (N)										
SUB-TOTAL	23415		6261		12068		6710		23415	

LAND ACQUISITION	KIDGS		KEDUSSORO		KUNCIK		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
RESIDENTIAL (1000 SQ)										
OTHERS (1000 SQ)	5153	5153	718	718	1027	1027	612	612		
BUILDING COMPENSATION										
I (NOS)										
II (NOS)	245	345	45	65	445	623	460	560		
III (NOS)										
SUB-TOTAL	5496		781		1652		1172		5496	
TOTAL	28911		7042		15553		7882		38606	



LIMITED CARRYING CAPACITY AT K. SOND BRIDGES, Q = 300 CM/SEC  
 CAPACITY OF K. SOND RETARDING BASIN, V = 1.5 X MILLION CM  
 CAPACITY OF U.L.O RETARDING BASIN, V = 6.0 X MILLION CM

LIMITED CARRYING CAPACITY AT K. SOND BRIDGES, Q = 145 CM/SEC  
 CAPACITY OF K. SOND RETARDING BASIN, V = 4.3 X MILLION CM  
 CAPACITY OF U.L.O RETARDING BASIN, V = 0.0 X MILLION CM

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (20/26)

WORK ITEM/TYPE	MILLION. RP)				MILLION. RP)			
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
BREASTING (1000 CH)	1840	5529	530	1855	2194	5522	442	1547
EXCAVATION (1000 CH)	1840	4048	530	1160	757	2205	270	524
EMBANKMENT (1000 CH)	925	2775	308	770	404	829	294	867
REVEINMENT								
METHURINARY (SM)	43116	1845	4530	137	27710	573	26953	674
DRY MASSURRY (SM)	43115	1015	4557	56	27710	554	26952	533
BRIDGE								
ROAD I			1				1	
			630	833	1250	1676		
II			1				3	
			1190	1428	588	706	882	1058
III			9		9		5	
			2360	2380	300	1274	798	798
RAILWAY			1		1			
			70	1085	84	1050		
BRAIRNAGE CULVERT								
I			4	130	6	270	3	135
II			4	240	3	195	1	65
III			5	475	5	285	1	95
DIVERSION WEIR (MOS)								
			15	450	15	450	15	450
IRRIGATION HEAD WORKS (MOS)			1		1		1	
			33	3200	30	3000	14	1400
SIDE OVERFLOW DIKE (M)			3		3			
			3185	2230	500	350		
DROP STRUCTURE								
			2120	1484	1000	700		
ABSEDUCT								
			4	180	2	120	3	135
			4	240	2	120	1	65
			3	285	5	475	1	95
SPHPHONE								
			15	450	15	450	15	450
			33	3200	14	1400	14	1400
GRAVEL METALLING								
			2120	1484	1000	700		
RELOCATION OF ROAD (M)								
			23983	6564	4330	6710	4957	
SUB-TOTAL			5344	5344	716	716	183	183
LAND ACQUISITION								
RESIDENTIAL (1000 SM)			270	378	45	63	90	126
OTHERS (1000 SM)								
BUILDING COMPENSATION								
I								
II								
III								
SUB-TOTAL			5722	781	309	1172	214	
TOTAL			29105	7345	4635	7982	4273	55244



LIMITED CARRYING CAPACITY AT X-SHOE BRIDGES , Q = 145 CM/SEC  
 CAPACITY OF X-SHOE RETARDING BASIN , V = 4.8 X MILLION CM  
 CAPACITY OF ULD RETARDING BASIN , V = 6.0 X MILLION CM

WORK ITEM/RYER	(MILLION, RP)											
	MIDAS		REDUNDSOVD		ULD		KUNCIK		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST

DRAINING (1000 CM)	1586	4759	441	1544								
EXCAVATION (1000 CM)	1568	3497	440	948	326	750	238	574	590	1500		
EMBANKMENT (1000 CM)	925	3775	308	770	131	255	374	867	40	120		
REVEGETATION												
WETLANDRY (SR)	46116	1845	4560	137	15183	378	26953	674	12330	370		
DRYLANDRY (SR)	46115	1015	4559	96	15105	303	26952	539	12330	260		
ROAD I (INDS)									1		1	
ROAD II (INDS)	1								315	417		
III (INDS)	1190	1428										
RAILWAY (INDS)	9		1		5			882	1058			
SEWERAGE (INDS)	2681	2681	300	300	620	620	799	798	650	650		
BRIDGE (INDS)									1			
RESERVOIR (INDS)									35	438		
ROAD I (INDS)	4	180			2	90	3	135	2	90		
ROAD II (INDS)	4	260			2	130			1	65		
ROAD III (INDS)	5	475			5	475			1	95		
DIVERSION WEIR (INDS)					1							
IRRIGATION HEAD WORKS (INDS)					15	450	15	450				
SIDE OVERFLOW DIKE (INDS)	3		33	3300	14	1400	14	1400				
DROP STRUCTURE (INDS)	2725	1409	1000	700								
ADJUNCT (INDS)									1			
SYPHON (INDS)									40	120		
GRAVEL RETAILING (INDS)									1			
RELOCATION OF ROAD (INDS)									60	47		
SUB-TOTAL	20814		8433		4246		6710		4057			

LIMITED CARRYING CAPACITY AT X-SHOE BRIDGES , Q = 195 CM/SEC  
 CAPACITY OF X-SHOE RETARDING BASIN , V = 3.2 X MILLION CM  
 CAPACITY OF ULD RETARDING BASIN , V = 6.0 X MILLION CM

WORK ITEM/RYER	(MILLION, RP)											
	MIDAS		REDUNDSOVD		ULD		KUNCIK		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST

DRAINING (1000 CM)	1586	4759	441	1670								
EXCAVATION (1000 CM)	1568	4857	440	1047	311	715	238	504	504	1500		
EMBANKMENT (1000 CM)	925	3775	308	770	170	374	394	657	40	120		
REVEGETATION												
WETLANDRY (SR)	46116	1845	4560	218	15105	378	26952	674	12330	370		
DRYLANDRY (SR)	46115	1015	4559	152	15105	303	26952	539	12330	260		
ROAD I (INDS)											1	
ROAD II (INDS)	1			495	142						315	419
ROAD III (INDS)	1190	1428						3				
RAILWAY (INDS)	9							5				
SEWERAGE (INDS)	2681	2681	300	300	620	620	798	798	630	630		
BRIDGE (INDS)									1			
RESERVOIR (INDS)									45	267		
ROAD I (INDS)	4	180			2	90	3	135	2	90		
ROAD II (INDS)	4	260			2	130			1	65		
ROAD III (INDS)	5	475			5	475			1	95		
DIVERSION WEIR (INDS)					1							
IRRIGATION HEAD WORKS (INDS)					15	450	15	450				
SIDE OVERFLOW DIKE (INDS)	3		33	3300	14	1400	14	1400				
DROP STRUCTURE (INDS)	2725	1409	1000	700								
ADJUNCT (INDS)											1	
SYPHON (INDS)									40	120		
GRAVEL RETAILING (INDS)									1			
RELOCATION OF ROAD (INDS)									60	47		
SUB-TOTAL	20814		8433		4320		6710		4057			

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (22/26)

WORK ITEM/RYER	(MILLION, RP)											
	MIDAS		REDUNDSOVD		ULD		KUNCIK		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST

DRAINING (1000 CM)	1586	4759	441	1670								
EXCAVATION (1000 CM)	1568	4857	440	1047	311	715	238	504	504	1500		
EMBANKMENT (1000 CM)	925	3775	308	770	170	374	394	657	40	120		
REVEGETATION												
WETLANDRY (SR)	46116	1845	4560	218	15105	378	26952	674	12330	370		
DRYLANDRY (SR)	46115	1015	4559	152	15105	303	26952	539	12330	260		
ROAD I (INDS)											1	
ROAD II (INDS)	1			495	142						315	419
ROAD III (INDS)	1190	1428						3				
RAILWAY (INDS)	9							5				
SEWERAGE (INDS)	2681	2681	300	300	620	620	798	798	630	630		
BRIDGE (INDS)									1			
RESERVOIR (INDS)									45	267		
ROAD I (INDS)	4	180			2	90	3	135	2	90		
ROAD II (INDS)	4	260			2	130			1	65		
ROAD III (INDS)	5	475			5	475			1	95		
DIVERSION WEIR (INDS)					1							
IRRIGATION HEAD WORKS (INDS)					15	450	15	450				
SIDE OVERFLOW DIKE (INDS)	3		33	3300	14	1400	14	1400				
DROP STRUCTURE (INDS)	2725	1409	1000	700								
ADJUNCT (INDS)											1	
SYPHON (INDS)									40	120		
GRAVEL RETAILING (INDS)									1			
RELOCATION OF ROAD (INDS)									60	47		
SUB-TOTAL	20814		8433		4320		6710		4057			

LIMITED CARRYING CAPACITY AT K.SORO BRIDGES, Q = 195 CM/SEC  
 CAPACITY OF K.SORO RETARDING BASIN, V = 3.2 X MILLION CM  
 CAPACITY OF OLD RETARDING BASIN, V = 2.0 X MILLION CM

WORK ITEM/RISE	(MILLION, RP)										
	KIDAS		KEPUNESOKO		ULO		KUNCIR		DIVERSION CHANNEL		TOTAL
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	
CARPENING (1000 CM)	2009	6027	405	1628							
EXCAVATION (1000 CM)	2007	4420	464	1021	326	750	238	524	524	300	1500
EMPAWMENT (1000 CM)	925	2775	308	770	116	255	394	867	867	40	120
REVEINENT											
RETASURRY (SM)	46116	1845	4560	137	15105	378	26953	674	12330	674	12330
DRY-PASURRY (SM)	46115	1015	4559	96	15105	303	24952	539	12330	539	12330
BRIDGE											
ROAD I (NOS)			1							1	
(SM)			405	162						315	419
II (NOS)	1						3				
(SM)	1190	1428					882	1058			
III (NOS)	9		1		5		5		4		
(SM)	2681	2681	300	300	620	620	778	778	630	630	
RAILWAY (NOS)	1		1						1		
(M)	45	207	45	207					35	438	
DRAINAGE CULVERT											
I (NOS)	4	180			2	90	3	135	2	90	
(SM)	4	250	2	130			1	65	1	65	
II (NOS)	4	380	4	380			1	95			
(SM)					15	450	15	450			
III (NOS)			1		1		2				
(SM)			33	3300	14	1400	14	1400			
DIVERSION WEIR (NOS)			1				1				
(M)	2595	1317	700	490							
IRIGATION HEAD WORKS (NOS)			1							1	
(M)										40	120
DROP STRUCTURE (NOS)										1	
(M)										60	47
ARQUEDUCT (NOS)											
(M)											
SYPHONE (NOS)											
(M)											
GRABEL RETALLING (NOS)											
(M)											
RELOCATION OF ROAD (NOS)											
(M)											
SUB-TOTAL		22828		8621		4246		6710		4093	
LAID ACQUISITION											
RESIDENTIAL (1000 SM)											
OTHERS (1000 SM)	5344	5344	718	718	240	240	612	612	186	186	
BUILDING COMPENSATION											
I (NOS)											
(SM)	270	378	45	63	90	125	400	560	28	28	
III (NOS)											
(SM)											
SUB-TOTAL		5722		781		366		1172		214	
TOTAL		28550		9402		4612		7882		4273	
		54227		1402		4612		7882		4273	

LIMITED CARRYING CAPACITY AT K.SORO BRIDGES, Q = 195 CM/SEC  
 CAPACITY OF K.SORO RETARDING BASIN, V = 3.2 X MILLION CM  
 CAPACITY OF OLD RETARDING BASIN, V = 4.0 X MILLION CM

WORK ITEM/RISE	(MILLION, RP)										
	KIDAS		KEPUNESOKO		ULO		KUNCIR		DIVERSION CHANNEL		TOTAL
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	
CARPENING (1000 CM)	1862	5586	445	1628							
EXCAVATION (1000 CM)	1862	4996	464	1021	326	750	238	524	524	300	1500
EMPAWMENT (1000 CM)	925	2775	308	770	116	255	394	867	867	40	120
REVEINENT											
RETASURRY (SM)	46116	1845	4560	137	15105	378	26953	674	12330	674	12330
DRY-PASURRY (SM)	46115	1015	4559	96	15105	303	24952	539	12330	539	12330
BRIDGE											
ROAD I (NOS)			1							1	
(SM)			405	162						315	419
II (NOS)	1						3				
(SM)	1190	1428					882	1058			
III (NOS)	9		1		5		5		4		
(SM)	2681	2681	300	300	620	620	778	778	630	630	
RAILWAY (NOS)	1		1						1		
(M)	45	207	45	207					35	438	
DRAINAGE CULVERT											
I (NOS)	4	180			2	90	3	135	2	90	
(SM)	4	250	2	130			1	65	1	65	
II (NOS)	4	380	4	380			1	95			
(SM)					15	450	15	450			
III (NOS)			1		1		2				
(SM)			33	3300	14	1400	14	1400			
DIVERSION WEIR (NOS)			1				1				
(M)	2595	1317	700	490							
IRIGATION HEAD WORKS (NOS)											
(M)											
DROP STRUCTURE (NOS)											
(M)											
ARQUEDUCT (NOS)											
(M)											
SYPHONE (NOS)											
(M)											
GRABEL RETALLING (NOS)											
(M)											
RELOCATION OF ROAD (NOS)											
(M)											
SUB-TOTAL		22336		8621		4246		6710		4093	
LAID ACQUISITION											
RESIDENTIAL (1000 SM)											
OTHERS (1000 SM)	5344	5344	718	718	240	240	612	612	186	186	
BUILDING COMPENSATION											
I (NOS)											
(SM)	270	378	45	63	90	125	400	560	28	28	
III (NOS)											
(SM)											
SUB-TOTAL		5722		781		366		1172		214	
TOTAL		28550		9402		4612		7882		4273	
		54227		1402		4612		7882		4273	



LIMITED CARRYING CAPACITY AT K.SORO BRIDGES, Q = 390 CM/SEC  
CAPACITY OF K.SORO RETARDING BASIN, V = 1.6 X MILLION CM  
CAPACITY OF OLD RETARDING BASIN, V = 0.9 X MILLION CM

LIMITED CARRYING CAPACITY AT K.SORO BRIDGES, Q = 195 CM/SEC  
CAPACITY OF K.SORO RETARDING BASIN, V = 3.2 X MILLION CM  
CAPACITY OF OLD RETARDING BASIN, V = 6.0 X MILLION CM

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (24/26)

WORK ITEM/RIVER	MILLION, Rp					MILLION, Rp						
	WIDAS	KEDUNGSOLO	OLD	KUNCIK	DIVERSION CHANNEL	TOTAL	WIDAS	KEDUNGSOLO	OLD	KUNCIK	DIVERSION CHANNEL	TOTAL
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
DREDGING (1000 CM)	1680	5040	465	1428	324	750	228	524	500	1500	524	500
EXCAVATION (1000 CM)	1679	3374	464	1021	116	255	384	867	40	120	867	40
EMBANKMENT (1000 CM)	925	2775	308	770	770	2310	2092	6946	578	2022	2281	5718
RETENTION							933	2799	308	770	170	374
METASANDARY (SM)	46116	1845	4550	137	15105	378	26953	674	12330	370	46116	1845
DRYMASORARY (SM)	46115	1015	4559	96	15105	303	26952	539	12330	260	46115	1015
BRIDGE												
ROAD I (MS)			1	405					1	650		
(SM)												
II (MS)			1	1970					1	1478		
(SM)												
III (MS)			9	2681					9	1478		
(SM)												
RAILWAY (MS)			1	2681					1	2681		
(SM)												
RAILWAY (M)			45	207					45	207		
IRRIGATION CULTURE												
I (MS)			4	190					4	190		
(MS)												
II (MS)			4	260					4	260		
(MS)												
III (MS)			5	475					5	475		
(MS)												
DIVERSION WEIR (MS)			1	285					1	285		
(M)												
IRRIGATION HEAD WORKS (MS)			1	450					1	450		
(M)												
SIDE OVERFLOW DIKE (MS)			3	3300					3	3300		
(M)												
DROP STRUCTURE (MS)			2925	2048					2925	2048		
(M)												
ADUUCT (MS)			1	40					1	40		
(M)												
SYPHONE (MS)			1	60					1	60		
(M)												
GRAVEL METALLING (M)			70	105					70	105		
RELOCATION OF ROAD (M)												
SUB-TOTAL	21441	8821	4246	6710	4029	24177	10723	4330	6710	4029	24177	10723
LAND ACQUISITION												
RESIDENTIAL (1000 \$)	5344	318	718	240	612	186	5344	318	718	240	612	186
OTHERS (1000 \$)												
BUILDING COMPENSATION												
I (MS)	270	378	45	63	90	126	270	378	45	63	90	126
(MS)												
II (MS)												
(MS)												
III (MS)												
(MS)												
SUB-TOTAL	5722	781	366	1172	214	5722	781	366	1172	214	5722	781
TOTAL	27163	9402	4612	7882	4273	29877	11854	4629	7882	4273	29877	11854

LIMITED CARRYING CAPACITY AT K. SOLO BRIDGES, Q = 300 CM/SEC  
 CAPACITY OF K. SOLO RETARDING BASIN  
 CAPACITY OF WLD RETARDING BASIN

LIMITED CARRYING CAPACITY AT K. SOLO BRIDGES, Q = 300 CM/SEC  
 CAPACITY OF K. SOLO RETARDING BASIN  
 CAPACITY OF WLD RETARDING BASIN

Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (25/26)

WORK ITEM/RIVER	MILLION, RP											
	WIDAS		KEDUNGSOKO		WLD		KUNCIAR		DIVERSION CHANNEL		TOTAL	
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST
SEDIMENT (1000 CM)	2124	5772	530	1855								
EXCAVATION (1000 CM)	2124	4273	530	1166	324	715	238	524	503	1500		
EMBANKMENT (1000 CM)	925	2775	308	770	115	255	394	867	40	120		
RETAINMENT												
METASANDRY (SN)	46116	1845	4560	137	15105	378	26953	674	12330	370		
GRAVEL SANDRY (SN)	46115	1015	4559	96	15105	303	26952	539	12330	266		
ROAD I			1						1			
ROAD II			630	838					630	838		
ROAD III			1				3		315	419		
ROAD IV			1190	1428			882	1058				
ROAD V			9				5		4			
RAILWAY (NS)	2681	1681	300	300	620	620	798	798	630	630		
RAILWAY (N)									1			
RAILWAY (N)									35	438		
BRIDGE												
BRIDGE I			4	180	2	90	3	135	2	90		
BRIDGE II			4	260	2	130	1	65	1	65		
BRIDGE III			4	380	3	285	1	95	1	95		
DIVERSION WEIR (NS)												
DIVERSION WEIR (N)									15	450		
DIVERSION WEIR (N)									1			
IRRIGATION HEAD WORKS (NS)									33	3300		
IRRIGATION HEAD WORKS (N)									1			
IRRIGATION HEAD WORKS (N)									14	1400		
SIDE OVERFLOW DIKE (NS)			3	2011	1				1			
SIDE OVERFLOW DIKE (N)			2872	500	330				40	120		
DEEP STRUCTURE (NS)									1			
DEEP STRUCTURE (N)									1			
AGENCY (NS)									60	47		
AGENCY (N)												
SPHONGE (NS)												
SPHONGE (N)									70	105		
GRAVEL METALLING (N)												
RELOCATION OF ROAD (N)												
SUB-TOTAL	23522	10312	4246	6710	4059				23130	10312	4246	6710
LAND ACQUISITION												
RESIDENTIAL (1000 SQ)												
OTHERS (1000 SQ)	5344	5344	718	718	240	240	612	612	186	186		
BUILDING COMPRESSION												
I (NS)												
II (NS)	270	378	45	63	90	126	400	560	20	28		
III (NS)												
SUB-TOTAL	5722	5722	781	781	356	356	1172	1172	214	214		
TOTAL	29344	11093	4412	7002	4733	37004			20832	11093	4412	7002

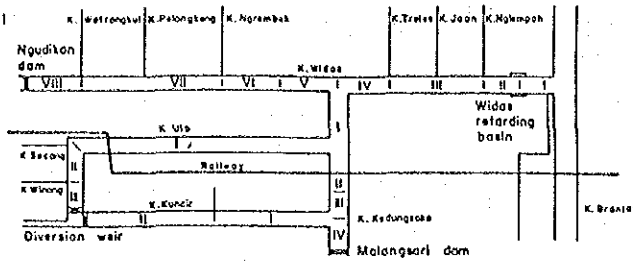
Table 4.2.1. BREAKDOWN OF CONSTRUCTION COST (26/26)

(SCHEME III, CASE 3)

LIMITED CARRYING CAPACITY AT K. SOND BRIDGES, Q. = 300 CM/SEC  
 CAPACITY OF K. SOND RETARDING BASIN, V = 1.6 X MILLION CM  
 CAPACITY OF ULO RETARDING BASIN, V = 6.0 X MILLION CM

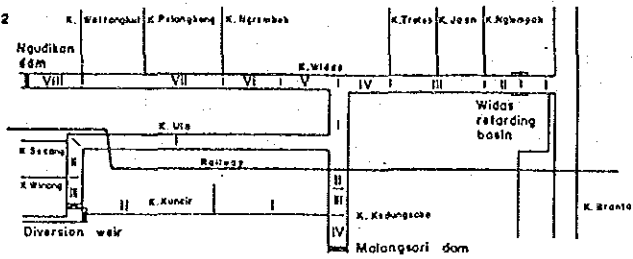
WORK ITEM/RIVER	RIDGES		REDUNSDAD		ULO		KUNDIR		DIVERSION CHANNEL		TOTAL
	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	QUANTITY	COST	
DRAINAGE (1000 CM)	1882	5406	520	1855							
EXCAVATION (1000 CM)	1882	3964	520	1168	326	750	238	524	500	1500	
EMBANKMENT (1000 CM)	925	2775	308	770	116	285	394	867	40	120	
REVEINMENT											
METASANDRY (SM)	46116	1845	4560	137	15105	378	26953	674	12330	370	
DRYMASANDRY (SM)	46115	1015	4559	96	15105	303	26952	539	12330	260	
BRIDGE											
ROAD I (MS)			1						1		
ROAD II (SM)			630	838					315	419	
ROAD III (MS)	1						3				
RAILWAY											
RAILWAY (MS)	1190	1428					882	1058			
RAILWAY (SM)	9		1		5		5		4		
RAILWAY (SP)	2681	2681	300	300	620	620	798	798	630	630	
RAILWAY (MS)			1						1		
RAILWAY (M)			70	1085					35	438	
DRAINAGE CULVERT											
I (MS)	4	180			2	90	3	135	2	90	
II (MS)	4	260	2	130			1	65	1	65	
III (MS)	5	475	3	285			1	95			
DIVERSION WEIR (MS)					1		1				
DIVERSION WEIR (M)					15	450	15	450			
IRRIGATION HEAD WORKS (MS)			1		1		2				
IRRIGATION HEAD WORKS (M)			33	3300	14	1400	14	1400			
STOE OVERFLOW DIVE (MS)	3		1								
STOE OVERFLOW DIVE (M)			3205	2244	500	350					
DROP STRUCTURE (MS)											
DROP STRUCTURE (M)									1		
ARQUEDUCT (MS)									40	120	
ARQUEDUCT (M)									1		
SYRPHQUE (MS)									60	47	
SYRPHQUE (M)							70	105			
GRAVEL METALLING (M)											
RELOCATION OF ROAD (M)											
SUB-TOTAL	22273		10312		4246		6710		4059		
LAND ACQUISITION											
RESIDENTIAL (1000 SM)											
OTHERS (1000 SM)	5344	5344	718	718	240	240	612	612	186	186	
BUILDING COMPENSATION											
I (MS)											
II (MS)	270	378	45	63	90	126	400	560	20	28	
III (MS)											
SUB-TOTAL	5722		781		366		1172		214		
TOTAL	27795		11093		5412		7882		4272		55855

Scheme I Case 1



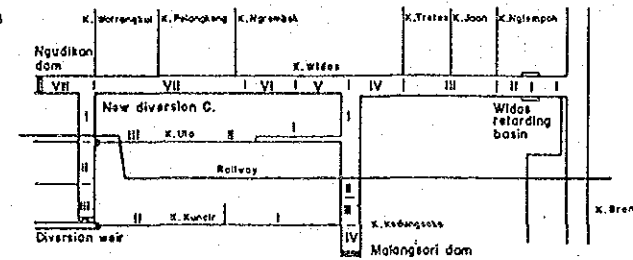
RETARDING CAPACITY (x 10 <sup>6</sup> m <sup>3</sup> )			DESIGN DISCHARGE (m <sup>3</sup> /sec)																				
ULO	WIDAS	KED.SOKO	WIDAS RIVER					KED.SOKO RIVER				ULO RIVER			KUNCIR RIVER		NEW DIVERSION CHANNEL						
R.B	R.B	R.B	I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	III	I	II	I	II	III	
9.2			270	449	406	573	544	544	559	433	448	463	470	460	219	156	94	101	94				

Scheme I Case 2



RETARDING CAPACITY (x 10 <sup>6</sup> m <sup>3</sup> )			DESIGN DISCHARGE (m <sup>3</sup> /sec)																				
ULO	WIDAS	KED.SOKO	WIDAS RIVER					KED.SOKO RIVER				ULO RIVER			KUNCIR RIVER		NEW DIVERSION CHANNEL						
R.B	R.B	R.B	I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	III	I	II	I	II	I	II
9.3			270	450	409	576	544	544	559	433	446	455	465	460	223	216	188	94	0				

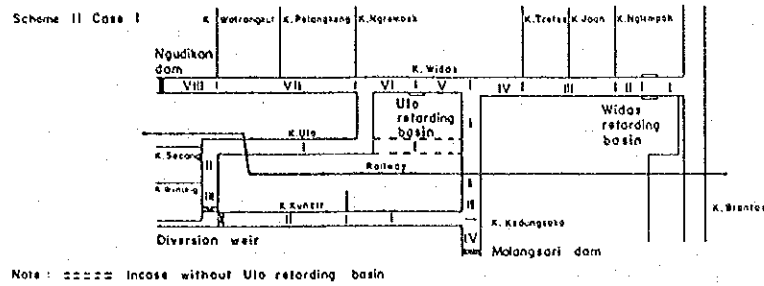
Scheme I Case 3



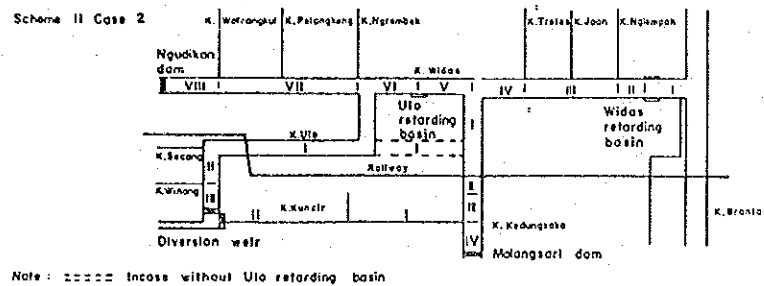
Note: ===== Increase without ulo retarding basin

RETARDING CAPACITY (x 10 <sup>6</sup> m <sup>3</sup> )			DESIGN DISCHARGE (m <sup>3</sup> /sec)																				
ULO	WIDAS	KED.SOKO	WIDAS RIVER					KED.SOKO RIVER				ULO RIVER			KUNCIR RIVER		NEW DIVERSION CHANNEL						
R.B	R.B	R.B	I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	III	I	II	I	II	I	II
9.4			270	457	457	622	586	586	586	433	325	455	465	460	33	33	0	94	0	223	216	188	

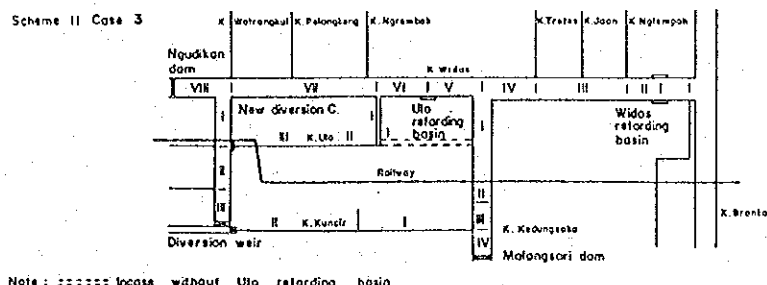
Fig. 4.2.1 DESIGN DISCHARGE DISTRIBUTIONS FOR SCHEME I (1/5)



RETARDING CAPACITY ( $\times 10^6 \text{ m}^3$ )			DESIGN DISCHARGE ( $\text{m}^3/\text{sec}$ )																			
ULO	WIDAS	KED.SOKO	WIDAS RIVER						KED.SOKO RIVER						ULO RIVER		KUNCIR RIVER		NEW DIVERSION CHANNEL			
A.B	A.B	A.B	I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	III	I	II	I	II	III
0.0	9.2		270	549	606	573	544	544	559	433	448	463	470	660	219	156	94	101	94			
2.0	9.2		270	532	627	593	450	614	559	433	322	463	"	"	"	"	"	"	"	"	"	"
4.0	9.2		"	451	604	569	360	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"
6.0	8.4		"	437	562	511	285	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"

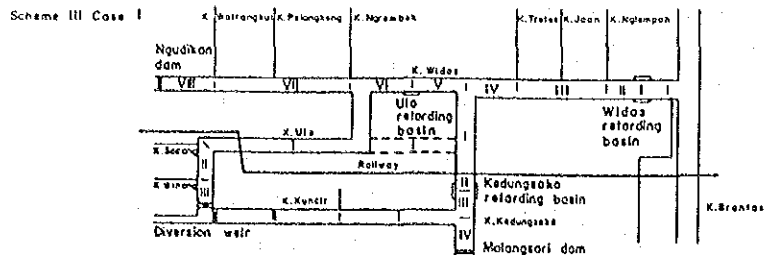


RETARDING CAPACITY ( $\times 10^6 \text{ m}^3$ )			DESIGN DISCHARGE ( $\text{m}^3/\text{sec}$ )																			
ULO	WIDAS	KED.SOKO	WIDAS RIVER						KED.SOKO RIVER						ULO RIVER		KUNCIR RIVER		NEW DIVERSION CHANNEL			
A.B	A.B	A.B	I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	III	I	II	I	II	III
0.0	9.3		270	430	609	576	544	544	559	433	446	455	465	460	223	216	188	94	0			
2.0	9.3		"	453	630	596	460	621	"	"	318	"	"	"	"	"	"	"	"	"	"	"
4.0	9.3		"	453	613	576	375	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"
6.0	8.7		"	444	560	528	310	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"



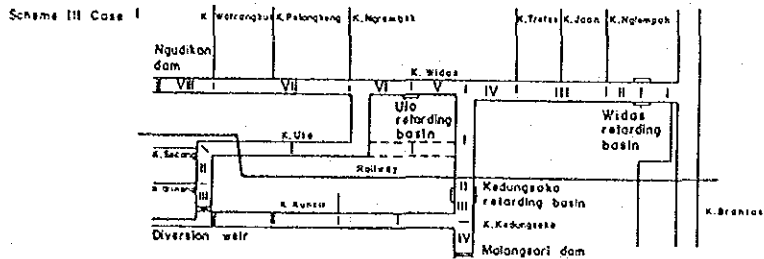
RETARDING CAPACITY ( $\times 10^6 \text{ m}^3$ )			DESIGN DISCHARGE ( $\text{m}^3/\text{sec}$ )																			
ULO	WIDAS	KED.SOKO	WIDAS RIVER						KED.SOKO RIVER						ULO RIVER		KUNCIR RIVER		NEW DIVERSION CHANNEL			
A.B	A.B	A.B	I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	III	I	II	I	II	III
0.0	9.4		270	457	657	622	584	544	586	433	325	455	465	460	33	33	0	94	0	223	216	188
2.0	9.4		"	458	656	622	453	591	"	"	318	"	"	"	"	"	"	"	"	"	"	"
4.0	9.3		"	456	615	583	370	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"
6.0	8.6		"	446	561	530	370	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"

Fig. 4.2.1 DESIGN DISCHARGE DISTRIBUTIONS FOR SCHEME II ( 2 / 5 )



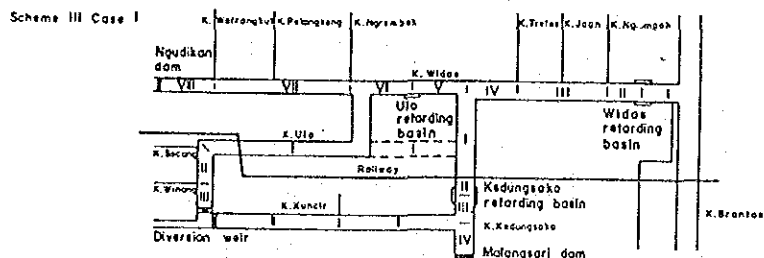
Note: ■■■■ Incase without Ulo retarding basin

RETARDING CAPACITY ( $\times 10^6 \text{ m}^3$ )			DESIGN DISCHARGE ( $\text{m}^3/\text{sec}$ )																		
ULO R.B.	WIDAS R.B.	KED.SOKO R.B.	WIDAS RIVER								KED.SOKO RIVER				ULO RIVER			KUNCIR RIVER		NEW DIVERSION CHANNEL	
			I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	III	I	II	III	
0.0	6.4	6.7	270	410	533	496	564	544	559	433	233	145	470	460	219	156	94	101	94		
										(606)											
2.0	6.4	"	"	409	569	510	450	614	"	"	138	"	"	"	"	"	"	"	"	"	"
4.0	6.4	"	"	406	513	480	350	"	"	"	"	"	"	"	"	"	"	"	"	"	"
6.0	5.7	"	"	389	443	413	285	"	"	"	"	"	"	"	"	"	"	"	"	"	"



Note: ■■■■ Incase without Ulo retarding basin

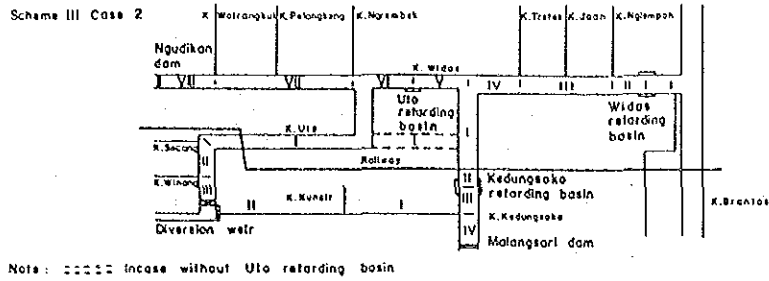
RETARDING CAPACITY ( $\times 10^6 \text{ m}^3$ )			DESIGN DISCHARGE ( $\text{m}^3/\text{sec}$ )																		
ULO R.B.	WIDAS R.B.	KED.SOKO R.B.	WIDAS RIVER								KED.SOKO RIVER				ULO RIVER			KUNCIR RIVER		NEW DIVERSION CHANNEL	
			I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	III	I	II	III	
0.0	7.4	4.2	270	421	555	514	564	544	559	433	261	195	470	460	219	156	94	101	94		
										(606)											
2.0	7.4	"	"	423	572	535	450	614	"	"	167	"	"	"	"	"	"	"	"	"	"
4.0	7.3	"	"	420	519	503	350	"	"	"	"	"	"	"	"	"	"	"	"	"	"
6.0	6.3	"	"	403	484	444	285	"	"	"	"	"	"	"	"	"	"	"	"	"	"



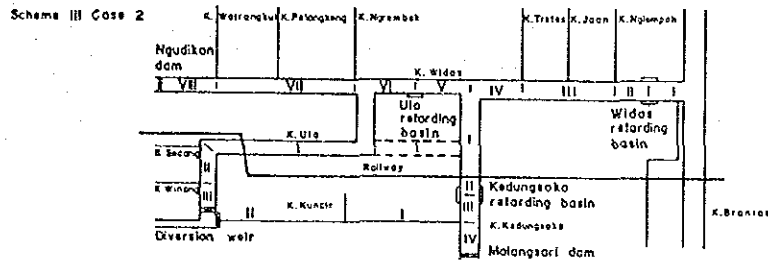
Note: ■■■■ Incase without Ulo retarding basin

RETARDING CAPACITY ( $\times 10^6 \text{ m}^3$ )			DESIGN DISCHARGE ( $\text{m}^3/\text{sec}$ )																		
ULO R.B.	WIDAS R.B.	KED.SOKO R.B.	WIDAS RIVER								KED.SOKO RIVER				ULO RIVER			KUNCIR RIVER		NEW DIVERSION CHANNEL	
			I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	III	I	II	III	
0.0	8.8	1.9	270	440	589	554	564	544	559	433	398	300	470	460	249	156	94	101	94		
										(606)											
2.0	8.9	"	"	443	609	574	430	614	"	"	234	"	"	"	"	"	"	"	"	"	"
4.0	7.4	"	"	426	563	529	360	"	"	"	"	"	"	"	"	"	"	"	"	"	"
6.0	7.4	"	"	425	509	459	285	"	"	"	"	"	"	"	"	"	"	"	"	"	"

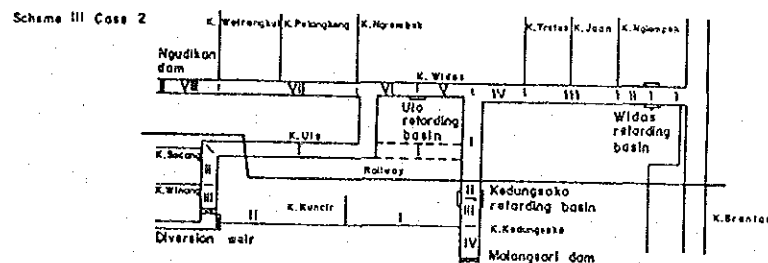
Fig. 4.2.1 DESIGN DISCHARGE DISTRIBUTIONS FOR SCHEME III (3/5)



RETARDING CAPACITY ( x 10 <sup>6</sup> m <sup>3</sup> )			DESIGN DISCHARGE ( m <sup>3</sup> /sec )																				
ULO	VIDAS	KED.SOKO	VIDAS RIVER					KED.SOKO RIVER				ULO RIVER			KUNCIR RIVER		NEW DIVERSION CHANNEL						
R.B	R.B	R.B	I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	III	I	II	I	II	III	
0.0	7.2	4.8	270	419	543	506	544	564	559	433	256	145	465	460	223	216	188	94	0				
2.0	7.2	"	"	423	563	521	480	621	"	"	143	"	"	"	"	"	"	"	"	"	"	"	"
4.0	7.2	"	"	423	538	501	375	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"
6.0	6.7	"	"	412	473	441	310	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"



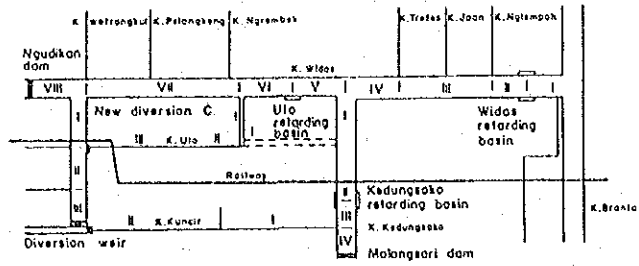
RETARDING CAPACITY ( x 10 <sup>6</sup> m <sup>3</sup> )			DESIGN DISCHARGE ( m <sup>3</sup> /sec )																				
ULO	VIDAS	KED.SOKO	VIDAS RIVER					KED.SOKO RIVER				ULO RIVER			KUNCIR RIVER		NEW DIVERSION CHANNEL						
R.B	R.B	R.B	I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	III	I	II	I	II	III	
0.0	8.0	3.2	270	431	565	529	544	544	559	433	293	195	465	460	223	216	188	94	0				
2.0	8.0	"	"	435	586	546	460	621	"	"	179	"	"	"	"	"	"	"	"	"	"	"	"
4.0	8.0	"	"	435	561	525	375	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"
6.0	7.4	"	"	424	504	472	310	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"



RETARDING CAPACITY ( x 10 <sup>6</sup> m <sup>3</sup> )			DESIGN DISCHARGE ( m <sup>3</sup> /sec )																				
ULO	VIDAS	KED.SOKO	VIDAS RIVER					KED.SOKO RIVER				ULO RIVER			KUNCIR RIVER		NEW DIVERSION CHANNEL						
R.B	R.B	R.B	I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	III	I	II	I	II	III	
0.0	9.0	1.6	270	446	598	563	544	544	559	433	390	300	465	460	223	216	188	94	0				
2.0	9.0	"	"	450	619	583	480	621	"	"	239	"	"	"	"	"	"	"	"	"	"	"	"
4.0	9.0	"	"	450	599	561	375	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"
6.0	8.6	"	"	440	546	514	310	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"	"

Fig. 4.2.1 DESIGN DISCHARGE DISTRIBUTIONS FOR SCHEME III ( 4 / 5 )

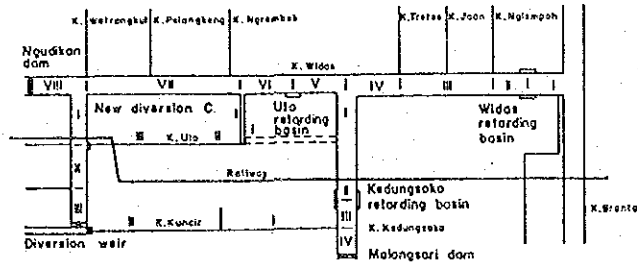
Scheme III Case 3



Note: ::::: Incase without Ulo retarding basin

ULO R.B	RETARDING CAPACITY ( $\times 10^6 \text{ m}^3$ )		DESIGN DISCHARGE ( $\text{m}^3/\text{sec}$ )																			
	VIDAS R.B	KED.SOKO R.B	VIDAS RIVER						KED.SOKO RIVER						ULO RIVER		KUNCIR RIVER		NEW DIVERSION CHANNEL			
			I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	I	II	I	II		
0.0	7.5	4.8	270	430	575	546	584	584	586	433	150	145	465	460	33	33	0	94	0	223	216	188
2.0	7.5	"	"	430	575	545	455	491	"	"	143	"	"	"	"	"	"	"	"	"	"	"
4.0	7.4	"	"	428	533	500	370	"	"	"	"	"	"	"	"	"	"	"	"	"	"	
6.0	6.7	"	"	414	474	463	310	"	"	"	"	"	"	"	"	"	"	"	"	"	"	

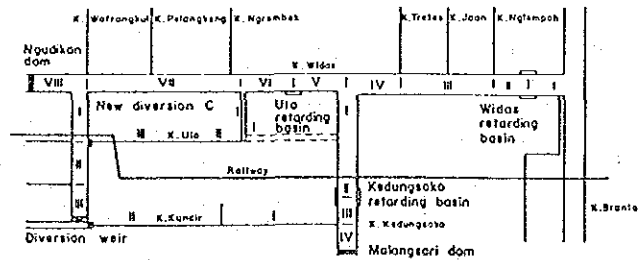
Scheme III Case 3



Note: ::::: Incase without Ulo retarding basin

ULO R.B	RETARDING CAPACITY ( $\times 10^6 \text{ m}^3$ )		DESIGN DISCHARGE ( $\text{m}^3/\text{sec}$ )																			
	VIDAS R.B	KED.SOKO R.B	VIDAS RIVER						KED.SOKO RIVER						ULO RIVER		KUNCIR RIVER		NEW DIVERSION CHANNEL			
			I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	I	II	I	II		
0.0	8.2	3.2	270	442	604	569	584	584	586	433	183	193	465	460	33	33	0	94	0	223	216	188
2.0	8.2	"	"	442	603	568	455	591	"	"	179	"	"	"	"	"	"	"	"	"	"	"
4.0	8.1	"	"	440	562	527	370	"	"	"	"	"	"	"	"	"	"	"	"	"	"	
6.0	7.4	"	"	426	506	474	310	"	"	"	"	"	"	"	"	"	"	"	"	"	"	

Scheme III Case 3

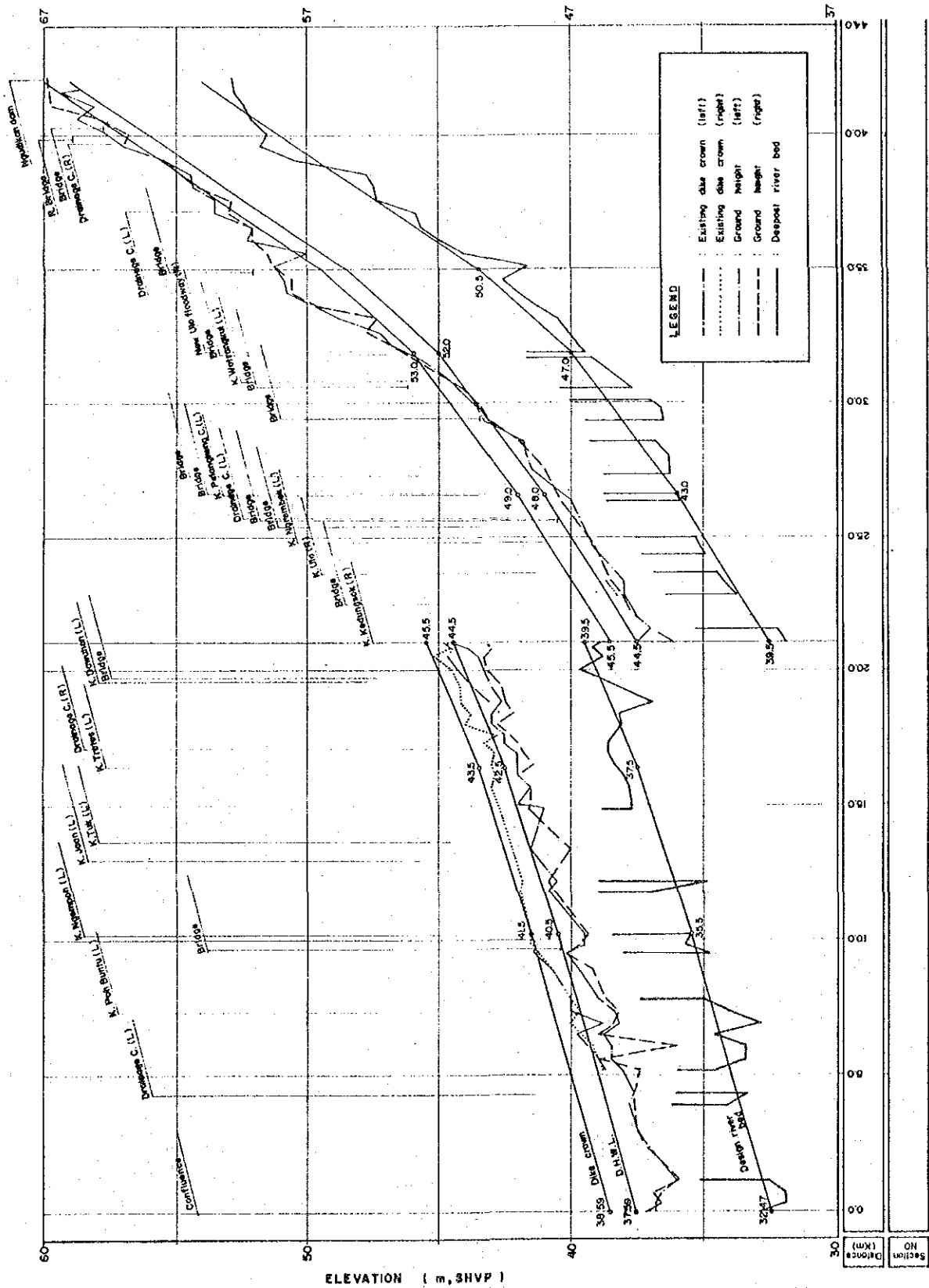


Note: ::::: Incase without Ulo retarding basin

ULO R.B	RETARDING CAPACITY ( $\times 10^6 \text{ m}^3$ )		DESIGN DISCHARGE ( $\text{m}^3/\text{sec}$ )																			
	VIDAS R.B	KED.SOKO R.B	VIDAS RIVER						KED.SOKO RIVER						ULO RIVER		KUNCIR RIVER		NEW DIVERSION CHANNEL			
			I	II	III	IV	V	VI	VII	VIII	I	II	III	IV	I	II	I	II	I	II		
0.0	9.2	1.6	270	455	643	607	584	584	586	433	245	300	465	460	33	33	0	94	0	223	216	188
2.0	9.2	"	"	455	642	607	455	591	"	"	239	"	"	"	"	"	"	"	"	"	"	"
4.0	9.1	"	"	454	601	568	370	"	"	"	"	"	"	"	"	"	"	"	"	"	"	
6.0	8.4	"	"	442	517	516	310	"	"	"	"	"	"	"	"	"	"	"	"	"	"	

Fig. 4.2.1 DESIGN DISCHARGE DISTRIBUTIONS FOR SCHEME III (5/5)





**Fig. 4.2.2 DESIGN PROFILE OF THE WIDAS RIVER ( I / 3 )**

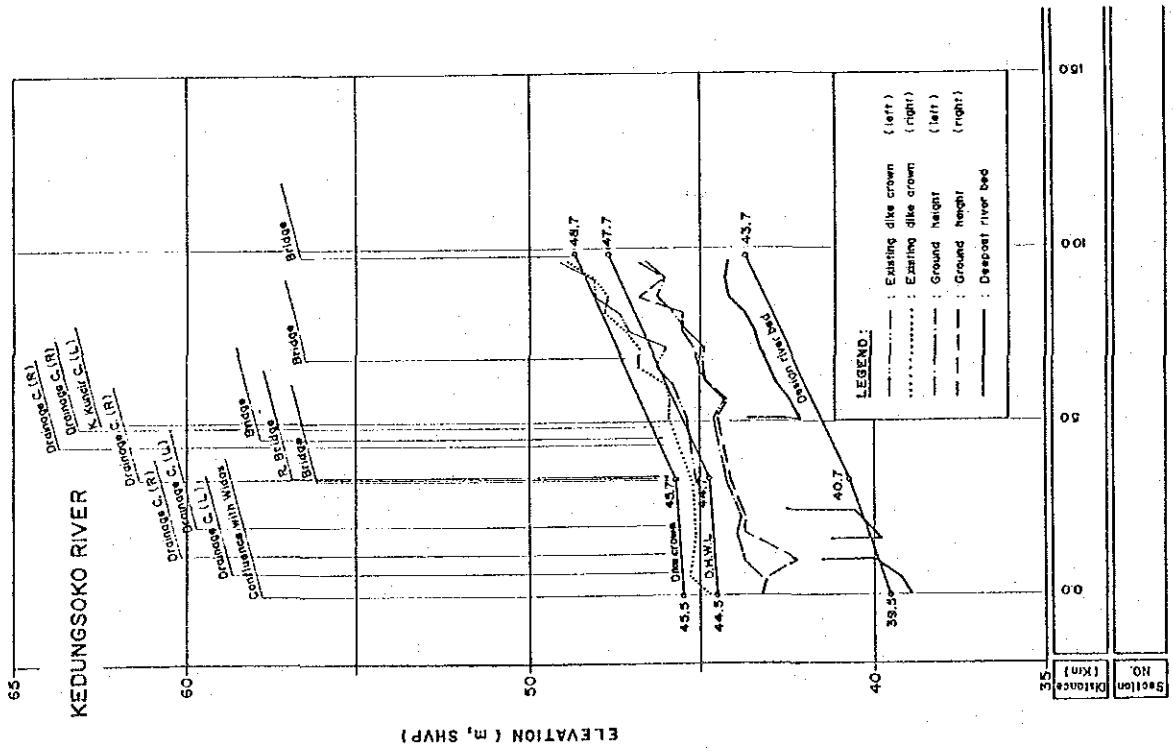
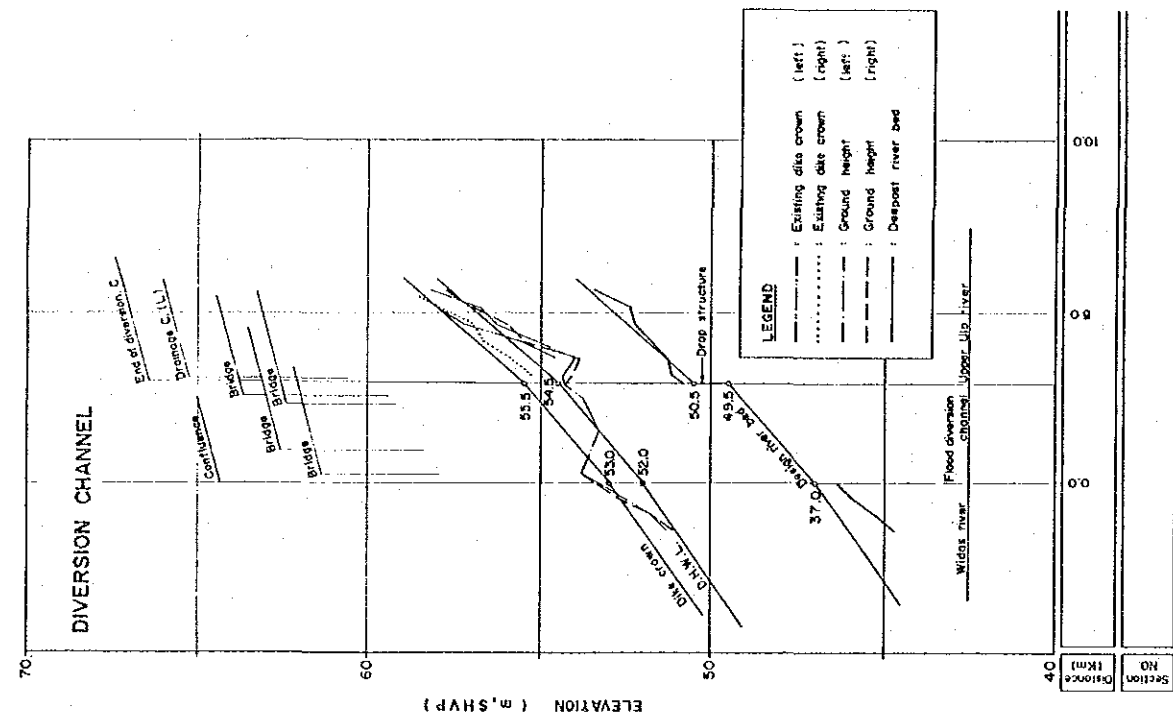


Fig. 4.2.2 DESIGN PROFILE OF THE KEDUNGSOKO AND NEW DIVERSION CHANNEL ( 2 / 3 )

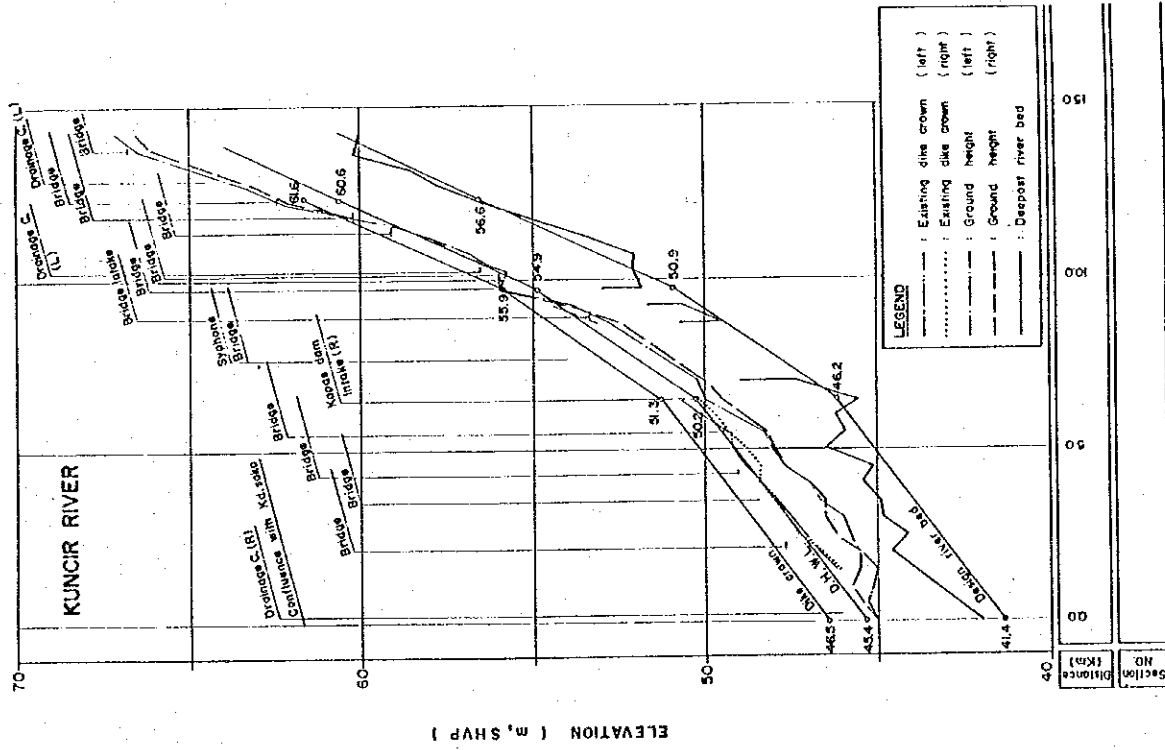
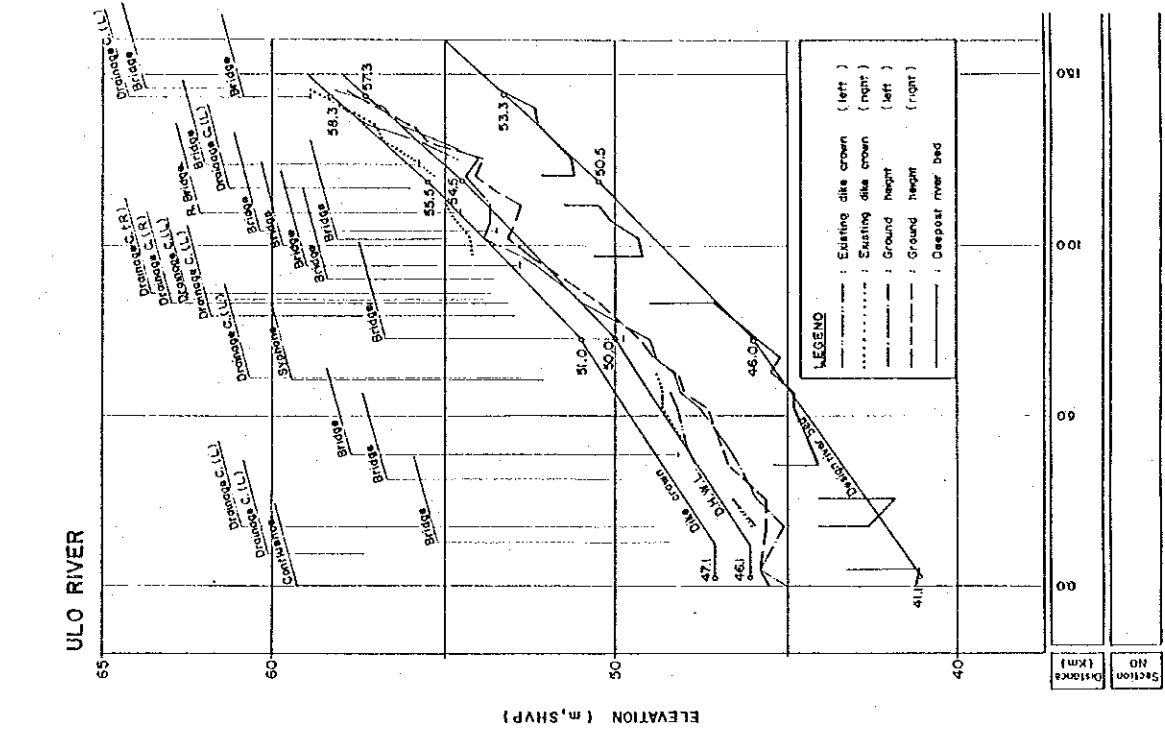


Fig. 4.2.2 DESIGN PROFILE OF THE KUNCIR AND ULO RIVERS (3/3)

### 4.3 Hydraulic study on retarding basin

#### 4.3.1 Side overflow dike

##### (1) General

Side overflow dike is to be constructed on the alignment of river dike as a lower part of river dike to reduce flood peaks immediately downstream in the river. The degree of flood peak reduction is determined by the location, the length, and the crest elevation of the side overflow dike. These dimensions are studied here on the Widas, the Ulo and the Kedungsoko retarding basins to satisfy the design flood discharge distribution in the Widas river basin river system for the 25-yr probable flood.

##### (2) Fundamental equations

Fundamental equations used for flood routing at a retarding basin with side overflow dike are as follows;

In a river :

##### (a) Continuity equation

$$\frac{dQ}{dx} = -q$$

##### (b) Equation of motion of non-uniform flow

$$\frac{dH}{dx} = \frac{i - \frac{Q^2}{C^2 R A^2} + \frac{\alpha \cdot Q^2 \cdot \frac{\partial A}{\partial x}}{g \cdot A^3} + \frac{\alpha \cdot q \cdot Q}{g \cdot A^2}}{1 - \frac{\alpha \cdot Q^2}{g A^3} \frac{\partial A}{\partial H}}$$

In a retarding basin :

##### (a) Continuity equation

$$\frac{dV}{dt} = q$$

At a side overflow dike :

##### (a) Discharge equation

$$q = K \cdot \sqrt{2g} \cdot h^{3/2} \quad (\text{perfect overflow})$$
$$= K' \cdot h_2 \cdot \sqrt{2g} (h_1 - h_2) \quad (\text{submerged overflow})$$

Here, Q : discharge in a river (m<sup>3</sup>/s)  
x : distance along the river (m)  
q : overflow discharge (m<sup>3</sup>/s)  
H : water depth (m)  
i : slope of the river bed  
C : Chezy's coefficient  
R : hydraulic mean radius (m)

- A : cross sectional area ( $m^2$ )
- $\alpha$  : coefficient of velocity distribution
- g : gravity acceleration ( $m/sec^2$ )
- V : storage volume in the retarding basin ( $m^3$ )
- t : time
- K : coefficient of perfect overflow
- K' : coefficient of submerged overflow
- h : water depth over the crest of side overflow dike
- $h_1, h_2$  : water depths over the crest of side overflow dike  
in the river and the retarding basin

### (3) Routing method

Flood routing is conducted to get the flood discharge hydrograph in the river immediately downstream of the side overflow dike and the variation of water level in the retarding basin due to the overflow discharge over the side overflow dike, to a given probable flood discharge hydrograph in the river immediately upstream of the side overflow dike.

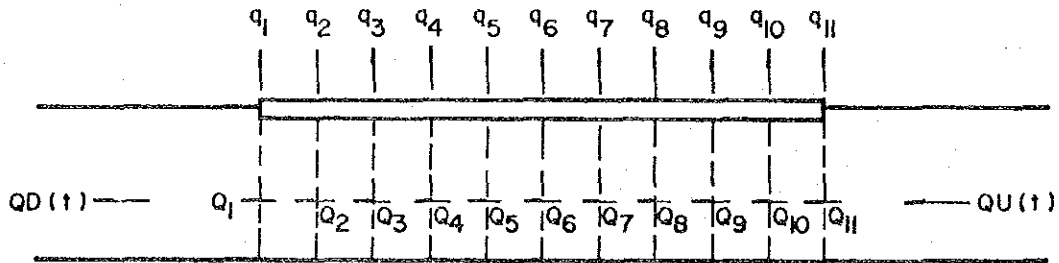
The procedure to calculate the streamflow downstream QD (t) from the streamflow upstream QU (t) of the side overflow dike at a time point t is as follows.

- (a) The reach of the side overflow dike is divided into ten reaches along the river course, and accordingly eleven cross sections are considered in the reach of the side overflow dike. Number is given to the cross sections from 1 to 11, from the downstream to the upstream.
- (b) The value of  $Q_1$  as the discharge at the cross section 1 most downstream is assumed.
- (c) The water depth  $H_1$  at the cross section 1 is calculated with  $Q_1$  through the stage discharge relation at the cross section 1.
- (d) Overflow discharge  $q_1$  at the cross section 1 is calculated with  $H_1$  and the water level in the retarding basin  $H_B$  through the overflow discharge equation.
- (e) The water depth  $H_2$  at the cross section 2 is calculated with  $Q_1, q_1$  and  $H_1$  through the equation of motion of non-uniform flow.
- (f) Overflow discharge  $q_2$  at the cross section 2 is calculated with  $H_2$  and  $H_B$  through the overflow discharge equation.
- (g) The discharge  $Q_2$  at the cross section 2 is calculated with  $Q_1, q_1$  and  $q_2$  through the equation :  $Q_2 = Q_1 + (q_1 + q_2)/2 \times \Delta x$ , where  $\Delta x$  is the distance between the cross section 1 and 2.
- (h) The water depth  $H_3$  at the cross section 3 is calculated with  $Q_2, q_2$  and  $H_2$  through the equation of motion of non-uniform flow.

- (i) The above same procedure is repeated up to the cross section 11, the cross section most upstream.
- (j) The calculated discharge  $Q_{11}$  at the cross section most upstream with the above procedure is checked if  $Q_{11}$  is equal to the given hydrograph discharge  $QU(t)$ .
- (k) When the discharge  $Q_{11}$  is not equal to  $QU(t)$ , a new value  $Q_1$  is assumed again and the procedure from (c) to (j) is conducted again.
- (l) When the calculated discharge  $Q_{11}$  is equal to  $QU(t)$ , then  $Q_1$  is the discharge downstream of the side overflow dike,  $QD(t)$ .

After getting the value  $QD(t)$ , the streamflow downstream of the side overflow dike, the water level in the retarding basin is calculated through the following procedure.

- (a) The additional volume of overflow discharge over the side overflow dike is calculated.
- (b) The accumulated volume of stored flood water in the retarding basin is calculated.
- (c) The water level in the retarding basin is calculated through the relation between the elevation and the volume capacity of the retarding basin.



(4) Widas retarding basin

The needed function of the Widas retarding basin is determined through the study on the optimum flood control plan of the Widas river systems. The Widas retarding basin should reduce the flood peak of about  $410 \text{ m}^3/\text{s}$  of the Widas river for 25-year probable flood to less than  $240 \text{ m}^3/\text{s}$ . This comes from the limit of  $270 \text{ m}^3/\text{s}$  allowed to inflow to K. Brantas. The remaining  $30 \text{ m}^3/\text{s}$  is the outflow from Al canal.

At the same time, the maximum storage volume of the Widas retarding basin is determined around  $13.6 \times 10^6 \text{ m}^3$  for 25-year probable flood through the study on the optimum flood control plan.

The dimensions of side overflow dike of the Widas retarding basin are determined on the basis of the above criteria as follows.

- (a) Storage capacity and area

Storage capacity and area curves used for the flood routing of the Widas retarding basin are shown in Table 4.3.1 and Fig. 4.3.1.

The curves are obtained from the topographic map of the scale 1/10,000.

In measuring the area, the design plan of the retarding basin shown in Fig. 4.4.4 is considered.

(b) Stage discharge relation

Stage discharge relation at the downstream end of the side overflow dike is calculated by the uniform flow formula.

The longitudinal profile and the river cross section used for the calculation is shown in Figs. 4.3.2 and 4.3.3.

The calculated stage discharge relation is shown in Table 4.3.2 and Fig. 4.3.4.

(c) River cross section

River cross section in the reach of the side overflow dike is assumed to be the same as that in the reach downstream of the side overflow dike except the side overflow dike.

(d) Location

The location of the side overflow dike of the Widas retarding basin is determined in view of the necessary storage capacity of the retarding basin and the design alignment of the river dike. When the location of the side overflow dike is too downstream near to the confluence with K. Brantas, the design high water level in the retarding basin inevitably becomes lower and the storage capacity of the retarding basin could not be enough for the necessary flood peak reduction of the Widas river.

The location is determined at the same time selecting the reach where the alignment of the river dike is straight.

Thus the downstream end of the side overflow dike is determined to be 4,900 m from the confluence with K. Brantas.

(e) Slope of river bed

The slope of river bed in the reach of the side overflow dike is planned to be the same with that in the downstream reach. The slope of design river bed downstream of the side overflow dike is 1/3,400.

(f) Dead volume of retarding basin

The dead volume of the Widas retarding basin is assumed to be the storage volume of the retarding basin when the water level in the retarding basin is as high as the design high water level of K. Brantas 37.59 m, from the conservative viewpoint.

(g) Length and crest elevation

The longer the side overflow dike is, the less the discharge in the river downstream of the side overflow dike becomes, and the more the storage volume in the retarding basin becomes. And this relation is the function of the crest elevation of the side overflow dike. With certain length of the side overflow dike, the higher the crest is, the more the discharge downstream in the river becomes and the less the storage volume of the retarding basin becomes.

These relations are shown in Fig. 4.3.5.

In consideration of these relations shown in Fig. 4.3.5 and that the maximum overflow depth over the crest of side overflow dike should be at least around 0.5 m from the practical view point, and the criteria for the Widas retarding basin aforementioned, the length and the crest elevation of the side overflow dike is determined as follows:

$$\begin{aligned}L &= 400 \text{ m} \\W &= 4.4 \text{ m}\end{aligned}$$

where  $L$  is the length and  $W$  is the relative height of the crest to the design river bed.

(h) Cross-section and longitudinal profile

The design river cross-section and the longitudinal profile in the reach of the side overflow dike is shown in Figs. 4.3.2 and 4.3.3.

(i) Flood routing

Flood routing is conducted with the dimensions of the side overflow dike decided in the above and the other features of the design of the river and the retarding basin on the following conditions.

(1) River condition

River cross section for 25-year probable flood and that for 10-year probable flood.

(ii) Flood hydrograph

Flood hydrograph with the return periods of 25-year, 10-year, 5-year, 2-year and 1.05-year.

The results are given in Table 4.3.4 and Figs. 4.3.7 - 4.3.9 the summary is given in Tables 4.3.5 - 4.3.6.

The results for 25-year river cross-section and for 25-yr flood is as follows.

- (i) Flood peak 410.3 m<sup>3</sup>/s
- (ii) Reduced flood peak 210.9 m<sup>3</sup>/s
- (iii) Peak cut volume 9.88 x 10<sup>6</sup> m<sup>3</sup>
- (iv) Maximum water level in the retarding basin 38.6 m SHVP
- (v) Maximum inundation area in the retarding basin 13.2 km<sup>2</sup>



(j) Supplement

Stage discharge relation

Stage discharge relation at the downstream end of the side overflow dike used for determining the dimensions of side overflow dike is calculated by the uniform flow formula. Actual stage discharge relation varies according to the water level in K. Brantas at the confluence with the Widas river. Some stage discharge relations are made depending on the water levels in K. Brantas by using non-uniform formula. The results are shown in Fig. 4.3.10, showing that the stage discharge relation made by the uniform formula has a substantial basis for designing the side overflow dike.

Flood hydrograph

Flood hydrograph used for designing the side overflow dike is only of one type, the type that the flood peak is almost in the midst of a flood, center concentrated type so to speak. Flood routing is also conducted assuming other two types of flood hydrographs. The one is of a flat type and the other is of a type that the flood peak occurs in the end of a flood. They are named type 1 for the former and type 2 for the latter and the results of flood routing are shown in Fig. 4.3.11.

The comparison is given below briefly.

	Original type	Type 1	Type 2
Peak discharge	410m <sup>3</sup> /s -- 211m <sup>3</sup> /s	325m <sup>3</sup> /s -- 201m <sup>3</sup> /s	499m <sup>3</sup> /s -- 221m <sup>3</sup> /s
Max. water level	38.57 m SHVP	38.60 m SHVP	38.62 m SHVP

Left and right retarding basins

In the calculation of overflow discharge, the following are assumed.

- (i) The overflow discharge is twice of the discharge calculated in the equation previously given because the side overflow dike is planned on the both sides of the river.
- (ii) Although the storage capacity of the Widas retarding basin is different on the left side and the right side, the water levels on the both sides will be raised on the same rate.

Actually, because of the difference of the storage capacity of the retarding basin on the left side and the right side, the water levels are different on the left and the right sides. Accordingly in the hydraulic condition of submerged overflow, the total overflow discharge can not be the twice of the overflow discharge calculated with the said equation on the above assumption.

For the confirmation of the adequacy of the result obtained on the

said assumption the flood routing for 25-yr probable flood and 25-yr cross section is conducted with the final dimensions of the side overflow dike for left and right sides and the comparison is given below.

Assumption : same water level

- (i) Q peak : 210.9 m<sup>3</sup>/s
- (ii) V max. : 13.57 x 10<sup>6</sup> m<sup>3</sup>
- (iii) H max. : 38.57 m SHVP

Different water level

- (i) Q peak : 215.9 m<sup>3</sup>/s
- (ii) V max. : 13.37 x 10<sup>6</sup> m<sup>3</sup>
- (iii) H<sub>L</sub>, max. : 38.69 m SHVP
- H<sub>R</sub>, max. : 38.56 m SHVP

where; Q peak : peak discharge downstream in river  
V max. : maximum storage volume  
H max. : maximum water level in retarding basin  
V max. : maximum total storage volume in retarding basin  
H<sub>L</sub> max. : maximum water level in the left retarding basin  
H<sub>R</sub> max. : maximum water level in the right retarding basin

#### (5) Ulo retarding basin

The needed function of the Ulo retarding basin is determined through the study on the optimum flood control plan of the Widas river systems as well as that of the Widas retarding basin as follows.

- (i) The flood peak of about 591 m<sup>3</sup>/s of the Widas river for 25-year probable flood should be reduced to less than 370 m<sup>3</sup>/s.
- (ii) The maximum storage volume of the Ulo retarding basin should be around 4.8 x 10<sup>6</sup> m<sup>3</sup> for 25-year probable flood.

The dimensions of side overflow dike along the Widas river of the Ulo retarding basin are determined on the basis of the above criteria as follows.

##### (a) Storage capacity and area

Storage capacity and area curves used for the flood routing of the Ulo retarding basin are shown in Table 4.3.1 and Fig.4.3.1.

The curves are obtained from the topographic map of the scale 1/10,000.

In measuring the area, the design plan of the retarding basin shown in Fig. 4.4.4 is considered.

(b) Stage discharge relation

Stage discharge relation at the downstream end of the side overflow dike is calculated by the uniform flow formula. The longitudinal profile and the river cross section used for the calculation is shown in Figs. 4.3.2 and 4.3.3.

The calculated stage discharge relation is shown in Table 4.3.2 and Fig. 4.3.4.

(c) Cross section

River cross section in the reach of the side overflow dike is assumed to be the same as that in the reach downstream of the side overflow dike except the side overflow dike.

(d) Location

The location of the side overflow dike of the Ulo retarding basin is determined in consideration that the site should be as downstream as possible so long as the storage capacity is enough for the flood peak reduction and that the crest elevation of the side overflow dike should be heigher than the design high water level in the Widas river at the confluence with the Kedungsoko river.

The downstream end of the side overflow dike is thus determined to be 700 m from the confluence with the Kedungsoko river.

(e) Slope of river bed

The slope of river bed in the reach of the side overflow dike is planned to be the same with that in the downstream reach. The slope of design river bed downstream of the side overflow dike is 1/1,590.

(f) Dead volume of retarding basin

The dead volume of the Ulo retarding basin is assumed to be zero because the river course of the Ulo river is planned to be changed to join the Widas river before coming into the Ulo retarding basin. Accordingly the drainage area of the Ulo retarding basin is so small as same as about 5 km<sup>2</sup>.

(g) Length and crest elevation

The relations between the length of the side overflow dike, the crest elevation of the side overflow dike, the discharge in the river downstream of the side overflow dike, and the storage volume in the retarding basin are as mentioned in the part of the Widas retarding basin. And such relations are shown in Fig. 4.3.5.

In consideration of these relations shown in Fig. 4.3.5 and that the maximum overflow depth over the crest of side over-

flow dike should be at least around 0.5 m from the practical view point, and the criteria for the Ulo retarding basin, the length and the crest elevation of the side overflow dike is determined as follows;

$$\begin{aligned}L &= 550 \text{ m} \\W &= 4.5 \text{ m}\end{aligned}$$

where L is the length and W is the relative height of the crest to the design river bed.

(h) Cross section and longitudinal profile

The design river cross section and the longitudinal profile in the reach of the side overflow dike is shown in Figs. 4.3.6 and 4.3.2.

(i) Flood routing

Flood routing is conducted with the dimensions of the side overflow dike decided in the above and the other features of the design of the river and the retarding basin on the following conditions.

(i) River condition

River cross section for 25-year probable flood and that for 10-year probable flood.

(ii) Flood hydrograph

Flood hydrograph with the return periods of 25-year, 10-year, 5-year, 2-year and 1.05-year.

The results are given in Table 4.3.4 and Figs. 4.3.7 - 4.3.9 and the summary is given in Tables 4.3.5 - 4.3.6.

The results for 25-year river cross section and for 25-year flood is as follows;

- (i) Flood peak 590.7 m<sup>3</sup>/s
- (ii) Reduced flood peak 364.0 m<sup>3</sup>/s
- (iii) Peak cut volume 4.78 x 10<sup>6</sup> m<sup>3</sup>
- (iv) Maximum water level in the retarding basin 44.4 m SHVP
- (v) Maximum inundation area in the retarding basin 6.3 km<sup>2</sup>

(j) Supplement

Stage discharge relation

In consideration of the same matters described in the section of the Widas retarding basin, the stage discharge relation made by the uniform flow formula and some stage discharge relations made by non-uniform flow formula depending on some water levels in the Widas river at the confluence with the Kedungsoko river are compared in Fig. 4.3.10. This also shows that the stage

discharge relation made by the uniform flow formula has a substantial basis for designing the side overflow dike.

#### Flood hydrograph

As discussed in the section of the Widas retarding basin, flood routing is conducted for other types of flood hydrograph and the result is shown in Fig. 4.3.11. The brief comparison is given below.

	Original type	Type 1	Type 2
Peak discharge	591m <sup>3</sup> /s -- 364m <sup>3</sup> /s	426 m <sup>3</sup> /s -- 330 m <sup>3</sup> /s	665 m <sup>3</sup> /s -- 378 m <sup>3</sup> /s
Max. water level	44.36 m SHVP	44.30 m SHVP	44.43 m SHVP

#### (6) Kedungsoko retarding basin

The needed function of the Kedungsoko retarding basin is determined through the study on the optimum flood control plan of the Widas river systems as well as that of the other retarding basins as follows.

- (i) The flood peak of about 455 m<sup>3</sup>/s of the Kedungsoko river for 25-year probable flood should be reduced to less than 200 m<sup>3</sup>/s.
- (ii) The maximum storage volume of the Kedungsoko retarding basin should be around 4.8 x 10<sup>6</sup> m<sup>3</sup> for 25-year probable flood.

The dimensions of side overflow dike along the Kedungsoko river of the Kedungsoko retarding basin are determined on the basis of the above criteria as follows.

##### (a) Storage capacity and area

Storage capacity and area curves used for the flood routing of the Kedungsoko retarding basin are shown in Table 4.3.1 and Fig. 4.3.1.

The curves are obtained from the topographic map of the scale of 1/10,000. In measuring the area, the design plan of the retarding basin shown in Fig. 4.4.4 is considered.

##### (b) Stage discharge relation

Stage discharge relation at the downstream end of the side overflow dike is calculated by the uniform flow formula. The longitudinal profile and the river cross section used for the calculation is shown in Figs. 4.3.2 and 4.3.3.

The calculated stage discharge relation is shown in Table 4.3.2 and Fig. 4.3.4.

(c) Cross section

River cross section in the reach of the side overflow dike is assumed to be the same as that in the reach downstream of the side overflow dike except the side overflow dike.

(d) Location

The location of the side overflow dike of the Kedungsoko retarding basin is determined in consideration of the topographic conditions. The Kedungsoko retarding basin should reduce the flood peaks of the Kedungsoko river and the Kuncir river.

Thus the location of the side overflow dike should be downstream of the confluence of the Kuncir river with the Kedungsoko river. And at the same time the side overflow dike can not be so near to the railway bridge. The distance between the two is only about 1.3 km.

The location is determined at around the middle of this reach. The downstream end of the side overflow dike is thus determined to be 500 m from the railway bridge.

(e) Slope of river bed

The slope of river bed in the reach of the side overflow dike is planned to be the same with that in the downstream reach. The slope of design river bed downstream of the side overflow dike is 1/1,950.

(f) Dead volume of retarding basin

The dead volume of the Kedungsoko retarding basin is assumed to be  $1.0 \times 10^6 \text{ m}^3$  on the basis of the run-off analysis result because the Kedungsoko retarding basin has its own drainage area of about 34 km<sup>2</sup>.

(g) Length and crest elevation

The relations between the length of the side overflow dike, the crest elevation of the side overflow dike, the discharge in the river downstream of the side overflow dike, and the storage volume in the retarding basin, are as mentioned in the preceding part of the other retarding basins. And such relations are shown in Fig. 4.3.5.

In consideration of these relations shown in Fig. 4.3.5 and that the maximum overflow depth over the crest of side overflow dike should be at least around 0.5 m from the practical view point, and the criteria for the Kedungsoko retarding basin aforementioned, the length and the crest elevation of the side overflow dike is determined as follows;

$$\begin{aligned} L &= 360 \text{ m} \\ W &= 3.5 \text{ m} \end{aligned}$$

where L is the length and W is the relative height of the crest to the design river bed.

(h) Cross section and longitudinal profile

The design river cross section and the longitudinal profile in the reach of the side overflow dike is shown in Figs. 4.3.6 and 4.3.2.

(i) Flood routing

Flood routing is conducted with the dimensions of the side overflow dike decided in the above and the other features of the design of the river and the retarding basin on the following conditions.

(i) River condition

River cross section for 25-year probable flood and that for 10-year probable flood.

(ii) Flood hydrograph

Flood hydrographs with the return periods of 25-year, 10-year, 5-year, 2-year and 1.05-year.

The results are given in Table 4.3.4 and Figs. 4.3.7 - 4.3.9 and the summary is given in Tables 4.3.5 - 4.3.6.

The result for 25-year river cross section and for 25-year probable flood is as follows;

- (i) Flood peak 455.3 m<sup>3</sup>/s
- (ii) Reduced flood peak 196.6 m<sup>3</sup>/s
- (iii) Peak cut volume 4.12 x 10<sup>6</sup> m<sup>3</sup>
- (iv) Maximum water level in the retarding basin 44.6 m SHVP
- (v) Maximum inundation area in the retarding basin 6.5 km<sup>2</sup>

(j) Supplement

Stage discharge relation

As well as the other retarding basins, the stage discharge relation made by the uniform flow formula and some stage discharge relations made by non-uniform flow formula depending on some water levels in the Widas river at the confluence with the Kedungsoko river are compared in Fig. 4.3.10. This also shows that the stage discharge relation made by the uniform formula has a substantial basis for designing the side overflow dike.

Flood hydrograph

As well as the other retarding basins, flood routing is conducted for other types of flood hydrograph, and the result is shown in Fig. 4.3.11. The brief comparison is given below.

	Original type	Type 1	Type 2
Peak discharge	455 m <sup>3</sup> /s -- 197 m <sup>3</sup> /s	322 m <sup>3</sup> /s -- 179 m <sup>3</sup> /s	491 m <sup>3</sup> /s -- 201 m <sup>3</sup> /s
Max. water level	44.59 m SHVP	44.66 m SHVP	44.66 m SHVP

#### Left and right retarding basins

The side overflow dike of the Kedungsoko retarding basin is planned on the both sides of the Kedungsoko river similar to the Widas retarding basin. Accordingly the same problem on the overflow discharge over the side overflow dike and the water level in the retarding basin on the left side and on the right side exists. But in the case of the Kedungsoko retarding basin, because of the locational constraint the side overflow dike is planned in the reach where the alignment of the river dike is convex to the right. It can be said that the overflow discharge to the right side retarding basin would be more than that to the left side because of the design alignment of the river dike convex to the right.

And the storage capacity of the right side retarding basin is about 4 times of that of the left side retarding basin. The effect of the bend of river dike alignment is not included in the equation of overflow discharge. This should be later confirmed by model test on the stage of detailed design.

#### (7) Summary

The fundamental dimensions of the three retarding basins are given below for summary, and partly shown in Fig. 4.3.12.

##### (a) Widas retarding basin

###### (i) Length of side overflow dike

$L = 400$  m on both sides of the Widas river

###### (ii) Relative height of the crest of side overflow dike to the design river bed

$W = 4.4$  m

(iii) Design flood peak cut : 455.3 m<sup>3</sup>/s ----- 210.9 m<sup>3</sup>/s

(iv) Design dead volume : 3.7 x 10<sup>6</sup> m<sup>3</sup>

(v) Design maximum storage volume 13.6 x 10<sup>6</sup> m<sup>3</sup>

(vi) Design peak cut volume : 9.9 x 10<sup>6</sup> m<sup>3</sup>

(vii) Design maximum inundation area : 13.2 km<sup>2</sup>

(viii) Design maximum inundation depth : 2.4 m

(ix) Design high water level : 38.6 m SHVP



(b) Ulo retarding basin

- (i) Length of side overflow dike

$L = 550$  m on the right side of the Widas river

- (ii) Relative height of the crest of side overflow dike to the design river bed

$W = 4.5$  m

- (iii) Design flood peak cut :  $590.7 \text{ m}^3/\text{s}$  -----  $364.0 \text{ m}^3/\text{s}$

- (iv) Design dead volume :  $0.0 \times 10^6 \text{ m}^3$

- (v) Design maximum storage volume :  $4.8 \times 10^6 \text{ m}^3$

- (vi) Design peak cut volume :  $4.8 \times 10^6 \text{ m}^3$

- (vii) Design maximum inundation area :  $6.3 \text{ km}^2$

- (viii) Design high water level :  $44.4 \text{ m.SHVP}$

(c) Kedungsoko retarding basin

- (i) Length of side overflow dike

$L = 360$  m on the both sides of the Kedungsoko river

- (ii) Relative height of the crest of side overflow dike to the design river bed

$W = 3.5$  m

- (iii) Design flood peak cut :  $455.3 \text{ m}^3/\text{s}$  -----  $196.6 \text{ m}^3/\text{s}$

- (iv) Design dead volume :  $1.0 \times 10^6 \text{ m}^3$

- (v) Design maximum storage volume :  $5.1 \times 10^6 \text{ m}^3$

- (vi) Design peak cut volume :  $4.1 \times 10^6 \text{ m}^3$

- (vii) Design maximum inundation area :  $6.5 \text{ km}^2$

- (viii) Design high water level :  $44.6 \text{ m.SHVP}$

#### 4.3.2 Drainage sluice

##### (1) General

Flood water stored in a retarding basin should be drained as soon as practicable after a flood. Because the storage capacity of the retarding basin should be reserved for a next coming flood during a rainy season.

The rate of draw down of the retarding basin depends on the dimensions of drainage sluice to be constructed to the retarding basin.

The dimensions of drainage sluices of the Widas, the Ulo and the Kedungsoko retarding basins are studied here.

##### (2) Fundamental equations

Fundamental equations for emptying a retarding basin with a drainage sluice used here are as follows;

###### (a) Continuity equation

$$\frac{dV}{dt} = - Q$$

###### (b) Discharge equation

$$Q = C1 \cdot B \cdot W \cdot \sqrt{2g \cdot \Delta H}$$

(pipe flow, submerged)

$$Q = C2 \cdot B \cdot h2 \cdot \sqrt{2g \cdot \Delta H}$$

(open channel, submerged)

$$Q = C3 \cdot B \cdot h1 \cdot \sqrt{2g \cdot h1}$$

(open channel, perfect flow)

$$Q = C1 \cdot B \cdot W \cdot \sqrt{2g \cdot h1}$$

(pipe flow, perfect flow)

Here; V : storage volume in the retarding basin (m<sup>3</sup>)  
t : time  
Q : discharge through drainage sluice (m<sup>3</sup>/s)  
C1, C2, C3 : constants  
B : width of sluice (m)  
W : height of sluice (m)  
g : gravity acceleration (m/s<sup>2</sup>)  
 $\Delta H$  : H1 - H2 (m)  
H1 : water level in the retarding basin  
H2 : water level in the river  
h1 : water depth in the retarding basin

### (3) Drainage calculation

Drainage calculation is carried out to get the draw down conditions of the retarding basin and the discharge hydrograph through the drainage sluice. On the condition that the drainage sluice would be opened after a flood, it is assumed that there is no inflow to the retarding basin in the drainage calculation.

The procedure to calculate the draw down of the retarding basin and the discharge hydrograph through the drainage sluice is as follows.

- (a) At a time point  $t$ , the water level in the retarding basin  $HB(t)$  is assumed.
- (b) Then the outflow discharge through drainage sluice  $QO(t)$  is calculated with the discharge equation by using  $HB(t)$  and the water level in the river  $HR(t)$ .
- (c) The average outflow discharge is calculated with  $QO(t)$  and the outflow discharge at a preceding time point  $QO(t-1)$ .
- (d) The storage volume in the retarding basin at a time point  $t$  is calculated with the equation ;

$$V(t) = V(t-1) - ( QO(t) + QO(t-1) ) / 2.0 \times \Delta t$$

where  $\Delta t$  is the time interval.

- (e) The water level in the retarding basin  $HB'(t)$  is calculated with  $V(t)$  through the volume curve of the retarding basin.
- (f) When  $HB'(t)$  is not equal to  $HB(t)$ , then the new value  $HB(t)$  is assumed, and the procedure from (b) to (e) is again conducted.
- (g) When these two values are the same, then the water level in the retarding basin at time point  $t$  is obtained as  $HB(t)$ .
- (h) In the above calculation, the influence of the outflow discharge in the river is taken into account.

### (4) Widas retarding basin

The dimensions of the drainage sluice of the Widas retarding basin are determined here so as to drain the storage volume of about  $13.6 \times 10^6 \text{ m}^3$  in about 2-3 days. The storage volume of  $13.6 \times 10^6 \text{ m}^3$  is the design storage volume for 25-year probable flood. In determining the dimensions of the drainage sluice, it is taken into account that the flow velocity in the drainage sluice does not exceed 3.5 m/sec as a standard.

The dimensions are determined as follows;

- (a) Storage capacity and area

Storage capacity and area curves used here are the same ones

used in the study of overflow dike and are shown in Fig.4.3.1.

(b) Discharge hydrograph in river

In the case of the Widas retarding basin, actually there are two retarding basins on the left side and on the right side of the Widas river. But in the drainage calculation, it is assumed that the retarding basin is just one and the stored flood water in the retarding basin is released to K. Brantas.

The design flood discharge hydrograph in K. Brantas is shown in Table 4.3.8.

(c) Stage discharge relation

Stage discharge relation in K. Brantas is the one in K. Brantas of the Brantas River Middle Reach Improvement Project, and is shown in Table 4.3.7.

(d) Dimensions of sluice

The dimensions of the sluice discussed here are the bed elevation, width and the height of the opening of the sluice.

By assuming some values on these dimensions, drainage calculations are carried out. And the relations between these values and the necessary time to empty the retarding basin and the maximum flow velocity through the sluice are obtained and shown in Fig.4.3.13.

In consideration of the relations shown in Fig.4.3.13 and the criteria for determining the dimensions of sluice aforementioned, the dimensions of the drainage sluice are determined and the drawdown of the water level in the retarding basin and the out-flow discharge hydrograph are shown in Fig. 4.3.14.

The dimensions of the sluices are determined as follows;

The left side

bed elevation	35.0 m SHVP
height	4.0 m
width	3.0 m x 2 gates

The right side

bed elevation	35.0 m SHVP
height	4.0 m
width	4.0 m x 2 gates

Necessary time to empty the retarding basin is 1.8 days.

In determining the dimensions of the sluices on the left side and the right side, the following are considered.

- (1) The necessary width is divided into two approximately

proportional to the storage volume of the retarding basins on the left and right sides.

- (ii) In consideration of an emergency case, each sluice should have two gates.
- (iii) When the width of a gate is too narrow, obstacles would be stopped at the gate and the smooth flow through the sluice would be disturbed.

The locations of the sluices are shown in Fig. 4.4.4.

(5) Ulo retarding basin

The design storage volume of the Ulo retarding basin is  $4.8 \times 10^6 \text{ m}^3$ . The same criteria as those of the Widas retarding basin to determine the dimensions of the sluice are used here for the Ulo retarding basin.

(a) Storage capacity and area

Storage capacity and area curves used here are the same ones used in the study of side overflow dike and are shown in Fig.4.3.1.

(b) Discharge hydrograph in river

The flood water stored in the Ulo retarding basin is to be released to the Kedungsoko river at the confluence of the existing Ulo river and the Kedungsoko river. But the confluence is not so far from the confluence of the Kedungsoko river with the Widas river.

And the distance is about 1.3 km and the design river bed slope is  $1/2,800$ . Accordingly, taking into account the influence of the backwater from the Widas river, the 25-yr probable flood hydrograph in the Widas river is used here. The hydrograph is shown in Table 4.3.8.

(c) Stage discharge relation

In consideration of the above mentioned matter, the stage discharge relation is calculated in Table 4.3.7.

(d) Dimensions of sluice

The dimensions of the sluice of the Ulo retarding basin are determined with the same procedure as that of the Widas retarding basin.

The relations between the bed elevation, width, height of the opening of the sluice, and, necessary time to empty the retarding basin and maximum flow velocity through the sluice are shown in Fig 4.3.13.

With the same consideration as in the case of the Widas retarding basin, the dimensions of the sluice of the Ulo retarding basin

are determined and the drawdown hydrograph of the basin and the outflow discharge hydrograph are shown in Fig. 4.3.14.

The dimensions are as follows;

bed elevation	42.0 m SHVP
height	3.0 m
width	4.0 m x 2 gates

Necessary time to empty the retarding basin is 2.2 days.

The location of the sluice is shown in Fig. 4.4.4.

(6) Kedungsoko retarding basin

The design storage volume of the Kedungsoko retarding basin is  $5.1 \times 10^6 \text{ m}^3$ .

The same criteria as the other retarding basins to determine the dimensions of the sluice are used here for the Kedungsoko retarding basin.

(a) Storage capacity and area

Storage capacity and area curves used here are the same ones used in the study of side overflow dike and are shown in Fig. 4.3.1.

(b) Discharge hydrograph in river

The flood water stored in the Kedungsoko retarding basin is to be released to Kedungsoko river after a flood.

Accordingly the discharge hydrograph in the Kedungsoko river for 25-yr probable flood is used and shown in Table. 4.3.8.

(c) Stage discharge relation

Stage discharge relation in the Kedungsoko river at the planned location is calculated in uniform flow and shown in Table 4.3.7.

(d) Dimensions of sluice

The dimensions of the sluice of the Kedungsoko retarding basin are determined with the same procedure as that of the other retarding basins. The relations between the bed elevation, width, height of the opening of the sluice, and, necessary time to empty the retarding basin and maximum flow velocity through the sluice are shown in Fig. 4.3.13.

With the same consideration as in the other retarding basins, the dimensions of the sluices of the Kedungsoko retarding basin are determined and the drawdown hydrograph and the outflow discharge hydrograph are shown in Fig. 4.3.14.

The dimensions of the sluices are as follow.

The left side :  
bed elevation 41.0 m SHVP

height 2.0 m  
width 2.0 m x 2 gates

The right side :

bed elevation 41.0 m SHVP  
height 2.5 m  
width 2.5 m x 2 gates

Necessary time to empty the retarding basin is 1.8 days.

In determining the dimensions of the sluices on the left side and the right side, the same consideration is given as in the case of the Widas retarding basin.

The locations of the sluices are shown in Fig. 4.4.4.

### 4.3.3 Drainage canal

#### (1) General

Flood water stored in a retarding basin should be drained as soon as practicable after a flood. In this case, it is needed to provide a drainage canal so as to lead the flood water smoothly to the drainage sluice.

The drainage canal also functions as a canal to drain the runoff in the retarding basin even when there occurs no overflow over the side overflow dike.

#### (2) Widas retarding basin

In the case of the Widas retarding basin the drainage condition is not in a condition that the flood water stored in the retarding basin can smoothly reach the location of planned drainage sluices.

Accordingly new drainage canals are planned as shown in Fig.4.3.15.

##### (a) Canal width

The design width of the canal is principally based on the width of the drainage sluice.

##### (b) Slope of canal bed

The design slope of the canal bed is principally based on the design bed slope of the Widas river.

#### (3) Ulo retarding basin

The downstream reach of the existing Ulo river is planned to change the river course to join the Widas river in the upstream of the Ulo retarding basin in order to minimize the dead volume of the retarding basin. Accordingly the existing Ulo river in the Ulo retarding basin can be used as the drainage canal. The other existing drainage canals, presently joining the Kedungsoko river separately are to be connected to the existing Ulo river in front of the planned drainage sluice of the Ulo retarding basin as shown in Fig. 4.4.4.

A new canal to connect the drainage sluice to the location of side overflow is also planned as shown in Fig. 4.4.4 in consideration of the existing drainage canals.

#### (4) Kedungsoko retarding basin

Kedungsoko retarding basin has two retarding basins on the left and the right sides of the Kedungsoko river.

As for the left side, the existing Kuncir river is planned to join the Kedungsoko river rather upstream of the existing confluence. Accordingly the existing Kuncir river near the drainage sluice can be used as a drainage canal. Therefore no new drainage canal is planned on the left side.



As for the right side, there exist irrigation and drainage canals in the Kedungsoko retarding basin presently joining the Kedungsoko river. Accordingly no new drainage canal is planned on the side except the connecting canal of these canals to lead them to the drainage sluice as shown in Fig. 4.4.4.

#### 4.3.4 Sediment volume

##### (1) General

Sediment volume in the retarding basins is studied here. Though the sediment discharge formula for the Widas river is not available, a sediment discharge formula is studied for K. Brantas because the sediment measurement has been carried out in K. Brantas. It is said that the sediment load in the Widas river is less than that in K. Brantas because of the vegetation condition in the basin. For the study of sediment volume of the retarding basins in the Widas river basin, the sediment discharge formula in K. Brantas is employed here.

##### (2) Sediment discharge formula

Sediment volume in retarding basin is mainly expected from the suspended load and wash load contained in flood water overflowing the side overflow dike of a retarding basin.

It is assumed here that the bed load will not overflow the side overflow dike.

According to the hydrological analysis result, the sediment discharge formula for suspended load and wash load is

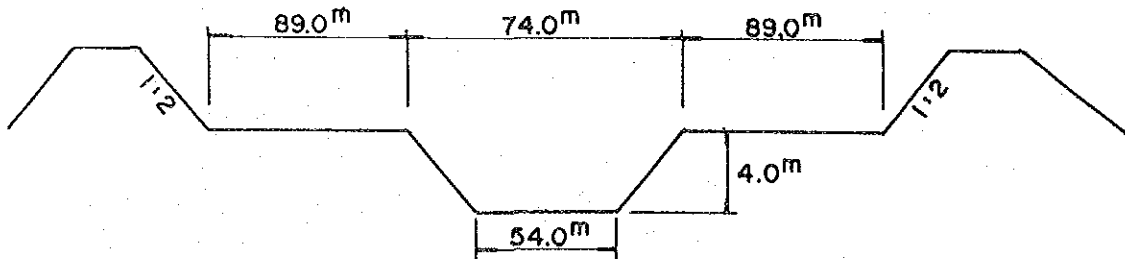
$$q_{sw} = 4.901 \times 10^{-3} \times (h \times U_*^2)^{0.733}$$

where ;  $q_{sw}$  : suspended load + wash load (m<sup>3</sup>/s/m)  
 $h$  : water depth (m)  
 $U_*$  : friction velocity (m/s)

##### (3) Widas retarding basin

###### (a) Cross section of the Widas river

Design cross-section of the Widas river in the upstream reach of the side overflow dike of the Widas retarding basin is as follows.



###### (b) River bed slope

Design river bed slope is planned to be 1/3,400.

###### (c) Manning's coefficient of roughness

Design coefficient of roughness is 0.03 for low water channel

and 0.05 for high water channel.

(d) Hydraulic characteristics

Assuming the uniform flow in the channel, the hydraulic characteristics are as follows.

(i) Low-water channel

h (m)	P (m)	A (m <sup>2</sup> )	R (m)	Q (m <sup>3</sup> /s)
4.0	75.54	256.0	3.389	330.2
4.5	75.54	293.0	3.389	413.5
5.0	75.54	330.0	4.369	504.1

(ii) High-water channel

h (m)	P (m)	A (m <sup>2</sup> )	R (m)	Q (m <sup>3</sup> /s)
4.0	0	0	0	0
4.5	180.7	89.6	0.496	19.3
5.0	183.4	180.5	0.984	61.3

In the above,

- h : water depth (m),
- P : wetted perimeter (m),
- A : cross sectional area (m<sup>2</sup>),
- R : hydraulic mean radius (m),
- Q : discharge (m<sup>3</sup>/s)

Although the flood discharge in this reach of the Widas river varies during a flood, the design peak discharge is 410.3 m<sup>3</sup>/s. The water depth corresponding to this discharge in the above table is 4.405 m.

Hydraulic characteristics to this water depth for low-water channel and high water channel are as follows.

(i) Low-water channel

h (m)	R (m)	Q (m <sup>2</sup> )	B <sub>*</sub> (m)	U <sub>*</sub> <sup>2</sup> (m <sup>3</sup> /s)	h.U <sub>*</sub> <sup>2</sup> (m <sup>3</sup> /s <sup>2</sup> )
4.405	3.786	397.1	54	0.01091	0.04807

(ii) High water channel

h (m)	R (m)	Q (m <sup>2</sup> )	B <sub>*</sub> (m)	U <sub>*</sub> <sup>2</sup> (m <sup>3</sup> /s)	(h-4).U <sub>*</sub> <sup>2</sup> (m <sup>3</sup> /s <sup>2</sup> )
4.405	0.402	13.6	178	0.001159	0.0004693

(e) Sedimentation in the Widas retarding basin

(i) Sediment discharge

(i) Sediment discharge

Substituting the hydraulic values obtained in the above to the sediment discharge formula previously mentioned, the sediment discharge to the design flood peak  $410.3 \text{ m}^3/\text{s}$  is obtained as follows.

$$Q_{sw1} = q_{sw1} \times B_* = 0.02861 \quad : \text{ low water channel}$$

$$Q_{sw2} = q_{sw2} \times B_* = 0.003169 \quad : \text{ high water channel}$$

Accordingly the total sediment discharge  $Q_{sw}$  is as follows.

$$Q_{sw} = Q_{sw1} + Q_{sw2} = 0.0318 \text{ m}^3/\text{s}$$

Therefore ;

$$Q_{sw}/Q = 0.0318/410.3 = 7.7452 \times 10^{-5}$$

(ii) Sediment volume

Assuming that the retarding basin is filled with the flood water when the flood discharge is  $410.3 \text{ m}^3/\text{s}$ , the sediment volume and the mean depth of the sediment of the Widas retarding basin are,

$$V_{sw} = 7.745 \times 10^{-5} \times 13.6 \times 10^6 \text{ m}^3 = 1053.3 \text{ m}^3$$

$$h_{sw} = 1053.3 \text{ m}^3 / 13.2 \text{ km}^2 = 0.08 \text{ mm}$$

Where ;

$V_{sw}$  : volume of sediment ( $\text{m}^3$ )

$h_{sw}$  : mean depth of sediment (mm)

Even when the retarding basin is fully filled with the 25-yr probable flood every year, the sediment depth is only 0.08 mm per year.

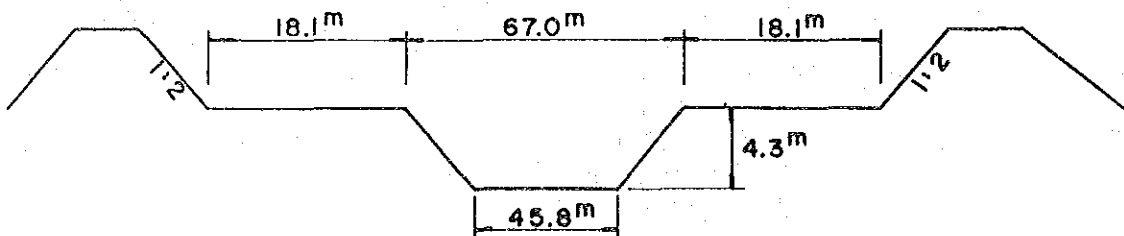
Accordingly it is concluded that there is no need to take into account the design dead volume due to sediment, though the very local sedimentation in the retarding basin should be taken care of.

(4) Ulo retarding basin

With the same procedure as that of the Widas river, the sediment volume in the Ulo retarding basin is calculated as follows.

(a) Cross-section

Design cross-section of the Widas river in the upstream reach of the side overflow dike of the Ulo retarding basin is as follows.



(b) River bed slope

Design river bed slope is planned to be 1/1,590.

(c) Manning's coefficient of roughness

Design coefficient of roughness is 0.03 for low water channel and 0.05 for high water channel.

(d) Hydraulic characteristics

For the design flood peak discharge  $590.7 \text{ m}^3/\text{s}$ , the hydraulic characteristics are as follows.

(i) Low-water channel

h	R	Q	$B_*$	$U_*^2$	$h \cdot U_*^2$
(m)	(m)	( $\text{m}^3/\text{s}$ )	(m)	( $\text{m}/\text{s}$ )	( $\text{m}^3/\text{s}^2$ )
4.813	4.015	584.8	45.8	0.02475	0.1191

(ii) High-water channel

h	R	Q	$B_*$	$U_*^2$	$(h-4.3) \cdot U_*^2$
4.813	0.494	6.0	36.2	0.003045	0.001562

(e) Sedimentation in the Ulo retarding basin

(i) Sediment discharge

Substituting the hydraulic values in the sediment discharge formula, the sediment discharge to the design flood peak  $590.7 \text{ m}^3/\text{s}$  is obtained as follows.

$$Q_{sw1} = q_{sw1} \times B_* = 0.0472 \quad : \text{ low-water channel}$$

$$Q_{sw2} = q_{sw2} \times B_* = 0.001556 \quad : \text{ high-water channel}$$

The total sediment discharge is then,

$$Q_{sw} = Q_{sw1} + Q_{sw2} = 0.04876 \text{ m}^3/\text{s}$$

Therefore,

$$Q_{sw}/Q = 0.04876/590.7 = 8.2539 \times 10^{-5}$$

(ii) Sediment volume

On the same assumption as that of the Widas retarding basin, the sediment volume and the mean depth of the sediment in the Ulo retarding basin per year are,

$$V_{sw} = 8.2539 \times 10^{-5} \times 4.8 \times 10 = 396.2 \text{ m}^3$$

$$h_{sw} = 396.2 \text{ m}^3 / 6.3 \text{ km}^2 = 0.06 \text{ mm}$$

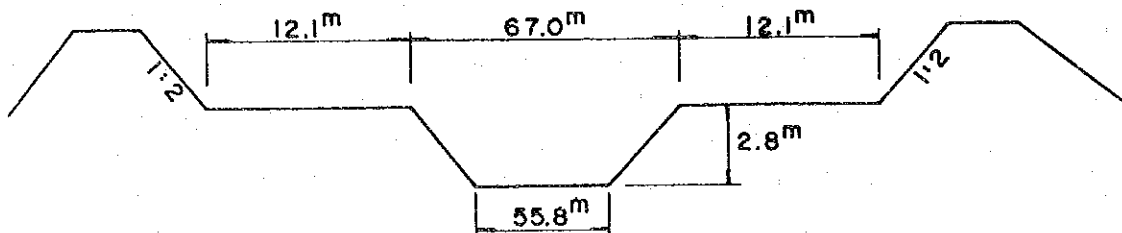
Accordingly it is concluded that there is no need to take into account the design dead volume due to sediment.

(5) Kedungsoko retarding basin

With the same procedure, the sediment volume in the Kedungsoko retarding basin is calculated as follows.

(a) Cross-section

Design cross-section of the Kedungsoko river in the upstream reach of the side overflow dike of the Kedungsoko retarding basin is as follows.



(b) River bed slope

Design river bed slope is planned to be 1/1,950.

(c) Manning's coefficient of roughness

Design coefficient of roughness is 0.03 for low-water channel and 0.05 for high water channel.

(d) Hydraulic characteristics

For the design flood peak discharge  $455.3 \text{ m}^3/\text{s}$ , the hydraulic characteristics are as follows.

(i) Low-water channel

h	R	Q	$B_*$	$U_*^2$	$h \cdot U_*^2$
(m)	(m)	( $\text{m}^3/\text{s}$ )	(m)	( $\text{m}^2/\text{s}^2$ )	( $\text{m}^3/\text{s}^2$ )
3.94	3.634	443.0	55.8	0.01826	0.07194

(ii) High-water channel

h	R	Q	$B_*$	$U_*^2$	$h \cdot U_*^2$
(m)	(m)	( $\text{m}^3/\text{s}$ )	(m)	( $\text{m}^2/\text{s}^2$ )	( $\text{m}^3/\text{s}^2$ )
3.94	1.030	13.947	24.2	0.00518	0.00591

(e) Sedimentation in the Kedungsoko retarding basin

(i) Sediment discharge

Substituting the hydraulic values in the sediment discharge formula, the sediment discharge to the design flood peak  $455.3 \text{ m}^3/\text{s}$

is obtained as follows.

$$Q_{sw1} = q_{sw1} \times B_* = 0.03973 \quad : \text{ low-water channel}$$

$$Q_{sw2} = q_{sw2} \times B_* = 0.00276 \quad : \text{ high-water channel}$$

Accordingly the total sediment discharge  $Q_{sw}$  is,

$$Q_{sw} = Q_{sw1} + Q_{sw2} = 0.04249 \text{ m}^3/\text{s}$$

Therefore ,

$$Q_{sw}/Q = 0.04249/455.3 = 9.3323 \times 10^{-5}$$

(ii) Sediment volume

On the same assumption as that of the Widas retarding basin, the sediment volume and the mean depth of the sediment in the Kedung-soko retarding basin per year are,

$$V_{sw} = 9.3323 \times 10^{-5} \times 5.1 \times 10^6 \text{ m}^3 = 475.9 \text{ m}^3$$

$$h_{sw} = 475.9 \text{ m}^3 / 6.5 \text{ km}^2 = 0.07 \text{ mm}$$

Accordingly it is concluded that there is no need to take into account the design dead volume due to sediment.

Table 4.3.1 STORAGE CAPACITY AND AREA OF WIDAS RETARDING BASIN (1/3)

1. Right side

H (m)	A (km <sup>2</sup> )	$\bar{V}$ (x10 <sup>6</sup> m <sup>3</sup> )
36.2	0.0	0.0
37.0	1.222	0.489
38.0	7.051	4.625
39.0	10.394	13.348

2. Left side

H (m)	A (km <sup>2</sup> )	$\bar{V}$ (x10 <sup>6</sup> m <sup>3</sup> )
36.4	0.0	0.0
37.0	0.992	0.298
38.0	3.268	2.428
39.0	4.751	6.437

3. Total

H (m)	A (km <sup>2</sup> )	$\bar{V}$ (x10 <sup>6</sup> m <sup>3</sup> )
36.2	0.0	0.0
37.0	2.214	0.786
38.0	10.319	7.053
39.0	15.145	19.785

Table 4.3.1 STORAGE CAPACITY AND AREA OF KEDUNGSOKO RETARDING BASIN (3/3)

1. Right side

H (m)	A (km <sup>2</sup> )	$\bar{V}$ (x10 <sup>6</sup> m <sup>3</sup> )
43.50	2.858	0.0
44.00	2.858	1.429
45.00	7.591	6.653

2. Left side

H (m)	A (km <sup>2</sup> )	$\bar{V}$ (x10 <sup>6</sup> m <sup>3</sup> )
43.2	0.0	0.0
44.0	0.399	0.160
45.0	2.754	1.736

3. Total

H (m)	A (km <sup>2</sup> )	$\bar{V}$ (x10 <sup>6</sup> m <sup>3</sup> )
43.2	0.0	0.0
44.0	3.257	1.589
45.0	10.345	8.389

Table 4.3.1 STORAGE CAPACITY AND AREA OF ULO RETARDING BASIN (2/3)

H (m)	A (km <sup>2</sup> )	$\bar{V}$ (x10 <sup>6</sup> m <sup>3</sup> )
43.0	0.0	0.0
44.0	5.589	2.794
45.0	7.505	9.341
46.0	9.553	17.870
		4.102



Table 4.3.2 STAGE DISCHARGE RELATION OF WIDAS RIVER  
AT WIDAS RETARDING BASIN (1/3)

Cross-section for 25-year probable flood

h (m)	3.9	4.0	4.4	4.8	5.2	5.6	6.0
Q (m <sup>3</sup> /s)	133.4	141.1	171.3	220.3	269.2	323.5	383.0

Table 4.3.2 STAGE DISCHARGE RELATION OF WIDAS RIVER  
AT DOWNSTREAM OF ULO RETARDING BASIN (2/3)

Cross-section for 25-year probable flood

h (m)	4.3	4.4	4.8	5.2	5.6	6.0
Q (m <sup>3</sup> /s)	265.9	278.2	341.8	416.4	500.6	593.7

Cross-section for 10-year probable flood

h (m)	4.3	4.4	4.8	5.2	5.6	6.0
Q (m <sup>3</sup> /s)	218.4	230.2	286.8	354.4	431.7	517.8

Table 4.3.2 STAGE DISCHARGE RELATION OF KEDUNGSOKO RIVER  
OF KEDUNGSOKO RETARDING BASIN (3/3)

Cross-section for 25-year probable flood

h (m)	3.1	3.4	3.8	4.2	4.6	5.0
Q (m <sup>3</sup> /s)	112.8	139.0	182.1	232.8	290.3	354.2

Cross-section for 10-year probable flood

h (m)	3.1	3.4	3.8	4.2	4.6	5.0
Q (m <sup>3</sup> /s)	98.3	122.3	162.4	210.1	264.6	325.5

Legend :

- h = elevation from the design low-water channel bed
- Q = discharge

Table 4.3.3 PROBABLE FLOOD AT WIDAS RETARDING BASIN (1/3)

Return Period Time	River Condition							
	For 10-year flood				For 25-year flood			
	1.05	2	5	10	2	5	10	25
1	60.1	79.4	97.0	106.5	79.4	97.1	106.5	119.6
2	75.4	99.5	122.6	135.2	99.5	122.8	135.5	151.4
3	102.7	135.6	163.4	177.6	135.7	164.0	178.4	195.9
4	137.6	181.7	212.6	227.9	182.0	213.8	230.4	249.6
5	175.2	231.4	260.4	266.0	232.0	261.0	267.9	275.7
6	199.8	263.8	277.5	285.5	264.2	278.7	289.3	300.9
7	209.7	276.9	295.8	305.6	277.6	297.8	311.6	325.8
8	219.5	289.8	313.2	324.3	291.0	316.0	332.2	348.1
9	228.4	301.6	328.9	340.9	303.3	332.4	350.3	367.7
10	235.9	311.5	341.9	354.8	313.6	346.2	365.5	384.3
11	241.4	318.8	351.5	365.5	321.2	356.5	377.3	397.3
12	244.5	322.8	357.2	372.3	325.6	362.8	385.2	406.3
13	245.0	323.5	358.5	374.7	326.5	364.7	388.5	410.3
14	242.9	320.7	356.2	372.6	323.9	362.5	386.9	410.1
15	238.0	314.3	349.9	366.5	317.9	356.2	380.7	405.0
16	229.3	302.8	339.9	356.8	306.7	346.5	370.6	395.0
17	216.7	286.1	324.6	342.4	290.0	331.6	356.3	381.3
18	201.8	266.4	304.0	322.5	270.2	310.9	336.3	362.5
19	167.3	220.9	281.1	299.1	231.5	287.5	312.0	338.1
20	129.1	170.4	258.2	274.9	176.8	264.0	286.5	311.1
21	103.8	137.0	191.5	238.5	140.8	207.2	262.0	284.4
22	86.7	114.5	148.8	177.8	116.8	158.0	200.2	259.5
23	75.5	99.7	121.7	140.0	100.9	127.2	153.1	192.4
24	68.6	90.6	104.5	116.5	91.3	107.7	124.3	148.7
25	63.8	84.3	94.9	102.3	84.8	96.6	106.9	122.8
26	61.3	80.9	89.9	95.8	81.2	90.9	98.2	108.7
27	61.0	80.6	89.0	94.3	80.8	89.7	95.9	103.6

Table 4.3.3 PROBABLE FLOOD AT ULO RETARDING BASIN (2/3)

Time (hr)	Return Period ( yr )				Unit : m <sup>3</sup> /s
	1.05	2	5	10	25
1	25.4	40.0	47.1	52.1	56.3
2	32.0	50.5	63.0	73.2	81.3
3	63.1	99.6	133.9	161.2	186.5
4	121.8	192.1	254.6	304.7	352.8
5	179.2	282.7	366.5	434.8	494.9
6	215.8	340.5	436.8	515.1	570.0
7	234.7	370.3	468.6	547.4	590.7
8	238.1	375.6	467.6	539.8	584.1
9	225.6	355.9	435.8	497.1	554.0
10	200.0	315.6	380.7	430.5	498.1
11	168.1	265.2	315.6	354.2	424.8
12	136.2	214.9	251.9	281.3	348.3
13	108.8	171.7	197.2	218.8	278.7
14	87.0	137.3	154.4	169.8	219.6
15	70.7	111.5	122.7	134.1	173.1
16	59.3	93.5	101.2	109.1	138.6
17	50.8	80.2	86.1	92.2	113.6

Table 4.3.3 PROBABLE FLOOD AT KEDUNGSOKO RETARDING BASIN (3/3)

Time (hr)	Return Period ( yr )				Unit : m <sup>3</sup> /s
	1.05	2	5	10	25
1	14.0	18.2	21.9	24.1	27.3
2	28.4	37.0	47.1	54.5	64.0
3	63.3	82.5	107.9	128.0	152.5
4	114.2	148.9	195.0	230.6	274.3
5	166.3	216.9	280.2	326.9	384.5
6	206.4	269.2	341.3	392.4	455.3
7	217.0	283.0	351.0	398.3	455.2
8	189.4	247.1	298.7	333.8	374.8
9	146.2	190.7	224.1	246.9	272.1
10	111.1	144.9	166.7	181.6	197.2
11	88.1	114.9	130.4	140.7	151.2
12	73.2	95.5	107.3	115.1	123.0
13	62.4	81.4	90.8	97.0	103.6
14	53.4	69.8	77.5	82.6	88.0
15	46.4	60.5	66.8	71.1	75.5

Table 4.3.4 FLOOD ROUTING IN THE WIDAS RETARDING BASIN (1/7)

(Q-1.05yr & River 10-yr)

Q <sub>u/s</sub> (m <sup>3</sup> /s)	H <sub>u/s</sub> (m)	Q <sub>d/s</sub> (m <sup>3</sup> /s)	H <sub>d/s</sub> (m)	q <sub>w</sub> (m <sup>3</sup> /s)	H <sub>b</sub> (m)	V <sub>b</sub> (x10 <sup>6</sup> m <sup>3</sup> )
60.1	26.837	60.1	26.873	0	27.59	3.69
75.4	27.119	75.4	27.069	0	27.59	3.69
102.7	27.521	102.7	27.419	0	27.59	3.69
132.6	27.924	132.6	27.856	0	27.59	3.69
175.1	28.403	175.1	28.287	0	27.59	3.69
199.8	28.480	183.1	28.265	16.7	27.59	3.69
209.7	28.498	184.9	28.282	24.8	27.60	3.75
219.4	28.509	186.3	28.297	32.9	27.61	3.84
228.4	28.521	188.0	28.410	40.4	27.63	3.96
235.9	28.531	189.1	28.421	46.8	27.64	4.11
241.4	28.538	189.9	28.428	51.5	27.66	4.27
244.5	28.541	190.4	28.433	54.1	27.69	4.48
245.0	28.542	190.5	28.433	52.9	27.71	4.45
242.0	28.539	190.1	28.430	52.7	27.74	4.45
238.0	28.533	189.4	28.424	48.6	27.74	5.04
229.2	28.522	188.1	28.411	41.1	27.78	5.21
218.6	28.508	186.1	28.393	30.5	27.80	5.26
201.8	28.483	183.3	28.368	18.3	27.81	5.47
167.2	28.328	167.2	28.200	0	27.82	5.34
129.1	27.873	129.1	27.257	0	27.82	5.34
103.1	27.536	103.1	27.433	0	27.82	5.34
86.7	27.304	86.7	27.214	0	27.82	5.34
75.5	27.151	75.5	27.070	0	27.82	5.34

Legend :

- Q<sub>u/s</sub> : discharge upstream of side overflow dike
- H<sub>u/s</sub> : water level upstream of side overflow dike
- Q<sub>d/s</sub> : discharge downstream of side overflow dike
- H<sub>d/s</sub> : water level downstream of side overflow dike
- q<sub>w</sub> : overflow discharge
- H<sub>b</sub> : water level in retarding basin
- V<sub>b</sub> : storage volume in retarding basin

(Q-2yr & River 10-yr)

Q <sub>u/s</sub> (m <sup>3</sup> /s)	H <sub>u/s</sub> (m)	Q <sub>d/s</sub> (m <sup>3</sup> /s)	H <sub>d/s</sub> (m)	q <sub>w</sub> (m <sup>3</sup> /s)	H <sub>b</sub> (m)	V <sub>b</sub> (x10 <sup>6</sup> m <sup>3</sup> )
79.4	27.204	79.4	27.120	0	27.59	3.69
99.5	27.478	99.5	27.378	0	27.59	3.69
135.6	27.958	135.6	27.840	0	27.59	3.69
181.6	28.444	178.9	28.326	2.7	27.59	3.69
231.3	28.925	188.4	28.414	42.9	27.59	3.70
263.7	28.563	193.1	28.458	70.6	27.61	3.85
276.9	28.577	194.9	28.475	82.0	27.64	4.11
289.8	28.590	196.6	28.490	93.2	27.68	4.41
301.6	28.602	198.1	28.504	103.5	27.72	4.74
311.5	28.611	199.3	28.516	112.2	27.77	5.11
318.7	28.618	200.2	28.524	118.5	27.82	5.52
322.8	28.621	200.7	28.529	122.1	27.87	5.94
323.5	28.622	200.8	28.530	122.7	27.92	6.38
320.7	28.619	200.5	28.526	120.2	27.98	6.83
314.3	28.614	199.7	28.519	114.6	28.02	7.26
302.8	28.603	198.2	28.506	104.6	28.06	7.67
286.0	28.585	196.1	28.486	89.9	28.09	8.05
266.4	28.566	193.5	28.461	72.9	28.13	8.37
220.8	28.511	186.8	28.399	34.0	28.15	8.63
170.3	28.352	170.3	28.234	0	28.16	8.76
137.0	27.974	137.0	27.858	0	28.16	8.76
114.5	27.679	114.5	27.570	0	28.16	8.76
99.7	27.481	99.7	27.380	0	28.16	8.76

Legend :

- Q<sub>u/s</sub> : discharge upstream of side overflow dike
- H<sub>u/s</sub> : water level upstream of side overflow dike
- Q<sub>d/s</sub> : discharge downstream of side overflow dike
- H<sub>d/s</sub> : water level downstream of side overflow dike
- q<sub>w</sub> : overflow discharge
- H<sub>b</sub> : water level in retarding basin
- V<sub>b</sub> : storage volume in retarding basin

(Q-5yr & River 10-yr)

Q <sub>u/s</sub> (m <sup>3</sup> /s)	H <sub>u/s</sub> (m)	Q <sub>d/s</sub> (m <sup>3</sup> /s)	H <sub>d/s</sub> (m)	q <sub>w</sub> (m <sup>3</sup> /s)	H <sub>b</sub> (m)	V <sub>b</sub> (x10 <sup>6</sup> m <sup>3</sup> )
97.0	27.444	97.0	27.316	0	27.59	3.69
122.6	27.787	122.6	27.674	0	27.59	3.69
163.3	28.276	163.3	28.157	0	27.59	3.69
212.6	28.800	185.4	28.286	27.2	27.59	3.69
260.3	28.539	192.6	28.455	47.7	27.60	3.79
272.5	28.578	195.0	28.473	82.5	27.64	4.03
295.8	28.598	197.3	28.497	98.5	27.67	4.33
313.2	28.613	199.5	28.518	113.7	27.72	4.69
328.9	28.627	201.5	28.536	127.4	27.77	5.09
341.9	28.638	203.0	28.550	138.9	27.82	5.55
351.5	28.647	204.2	28.561	147.3	27.88	6.05
357.1	28.651	204.8	28.567	152.3	27.95	6.58
358.4	28.652	205.0	28.568	153.4	28.01	7.13
354.1	28.650	204.7	28.559	151.4	28.06	7.68
349.9	28.645	204.0	28.559	145.9	28.11	8.23
339.9	28.637	202.6	28.548	137.1	28.16	8.75
324.8	28.623	200.9	28.531	123.7	28.21	9.25
303.9	28.608	198.4	28.507	105.5	28.25	9.69
281.1	28.581	195.4	28.480	85.7	28.29	10.07
258.1	28.557	192.3	28.451	65.8	28.31	10.38
191.3	28.465	181.4	28.369	10.1	28.34	10.62
148.8	28.127	149.9	28.008	-1.1	28.34	10.64
121.7	27.789	122.8	27.676	-1.1	28.34	10.65
104.5	27.559	105.6	27.455	-1.1	28.34	10.65
94.9	27.429	95.9	27.322	-1.0	28.34	10.64
89.9	27.361	90.9	27.267	-1.0	28.34	10.64

Legend :

- Q<sub>u/s</sub> : discharge upstream of side overflow dike
- H<sub>u/s</sub> : water level upstream of side overflow dike
- Q<sub>d/s</sub> : discharge downstream of side overflow dike
- H<sub>d/s</sub> : water level downstream of side overflow dike
- q<sub>w</sub> : overflow discharge
- H<sub>b</sub> : water level in retarding basin
- V<sub>b</sub> : storage volume in retarding basin

(Q-10yr & River 10-yr)

Q <sub>u/s</sub> (m <sup>3</sup> /s)	H <sub>u/s</sub> (m)	Q <sub>d/s</sub> (m <sup>3</sup> /s)	H <sub>d/s</sub> (m)	q <sub>w</sub> (m <sup>3</sup> /s)	H <sub>b</sub> (m)	V <sub>b</sub> (x10 <sup>6</sup> m <sup>3</sup> )
106.5	27.572	106.5	27.467	0	27.59	3.69
135.2	27.953	135.2	27.835	0	27.59	3.69
177.5	28.430	177.4	28.312	0	27.59	3.69
227.9	28.971	187.9	28.409	40.0	27.59	3.69
265.0	28.565	193.4	28.461	72.6	27.61	3.84
285.4	28.586	196.0	28.485	89.4	27.64	4.10
303.4	28.605	198.6	28.509	107.0	27.68	4.42
324.3	28.623	200.9	28.530	123.4	27.73	4.81
340.9	28.637	202.9	28.549	138.0	27.78	5.25
354.7	28.649	204.5	28.564	150.2	27.85	5.75
363.4	28.658	205.8	28.576	159.6	27.98	6.44
372.3	28.664	206.6	28.583	165.7	27.98	6.86
374.7	28.666	206.9	28.584	167.8	28.04	7.46
372.6	28.664	206.6	28.584	166.0	28.10	8.06
368.4	28.659	205.9	28.577	160.5	28.15	8.66
358.7	28.651	204.8	28.567	151.9	28.21	9.24
342.4	28.639	203.1	28.551	139.3	28.26	9.78
322.5	28.621	200.7	28.528	121.8	28.31	10.29
299.1	28.599	197.8	28.501	101.3	28.35	10.72
274.9	28.575	194.6	28.472	80.3	28.38	11.09
238.5	28.535	189.6	28.426	48.9	28.41	11.38
177.8	28.476	181.4	28.368	-5.6	28.42	11.53
139.9	28.250	161.3	28.134	-21.4	28.42	11.53
116.5	28.951	135.2	27.835	-18.7	28.41	11.44
102.3	27.734	118.8	27.625	-16.3	28.41	11.39
95.8	27.623	110.5	27.519	-14.7	28.40	11.33
94.3	27.580	107.4	27.479	-13.1	28.40	11.24
98.4	27.618	110.0	27.512	-11.6	28.39	11.23
102.4	27.767	119.8	27.637	-10.4	28.39	11.19

Legend :

- Q<sub>u/s</sub> : discharge upstream of side overflow dike
- H<sub>u/s</sub> : water level upstream of side overflow dike
- Q<sub>d/s</sub> : discharge downstream of side overflow dike
- H<sub>d/s</sub> : water level downstream of side overflow dike
- q<sub>w</sub> : overflow discharge
- H<sub>b</sub> : water level in retarding basin
- V<sub>b</sub> : storage volume in retarding basin

Table 4.3.4 FLOOD ROUTING IN THE WIDAS RETARDING BASIN (2/7)

(Q-2yr & River 25-yr)							(Q-5yr & River 25-yr)						
$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_v$ ( $m^3/s$ )	Hb (m)	Vb ( $\times 10^6 m^3$ )	$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_v$ ( $m^3/s$ )	Hb (m)	Vb ( $\times 10^6 m^3$ )
29.4	37.204	29.4	37.120	0	37.59	3.69	97.1	37.446	97.1	37.347	0	37.59	3.69
95.3	37.478	95.5	37.378	0	37.59	3.69	122.8	37.790	122.8	37.676	0	37.59	3.69
135.7	37.940	35.7	37.862	0	37.59	3.69	163.9	38.282	163.9	38.163	0	37.59	3.69
181.9	38.445	179.0	38.727	2.9	37.59	3.69	213.8	38.302	165.6	38.388	28.7	37.59	3.69
232.0	38.526	188.5	38.415	43.5	37.59	3.70	260.9	38.560	192.7	38.454	68.2	37.61	3.78
264.1	38.563	193.2	38.459	70.9	37.61	3.86	278.7	38.579	195.1	38.477	83.6	37.64	4.06
277.6	38.578	195.0	38.475	82.6	37.64	4.11	297.8	38.598	197.6	38.500	100.7	37.67	4.34
291.0	38.591	196.7	38.492	94.3	37.68	4.41	315.9	38.615	199.9	38.521	116.0	37.72	4.70
303.7	38.603	198.3	38.506	104.3	37.72	4.75	332.4	38.630	201.9	38.540	130.5	37.77	5.12
313.6	38.613	199.6	38.518	114.0	37.76	5.13	348.2	38.642	203.5	38.555	142.7	37.83	5.59
321.2	38.620	200.5	38.527	120.7	37.82	5.54	364.6	38.651	204.7	38.566	151.2	37.89	6.10
325.6	38.626	201.1	38.532	124.5	37.87	5.97	362.7	38.656	205.5	38.573	157.2	37.96	6.65
326.5	38.625	201.2	38.625	125.3	37.93	6.42	364.6	38.658	205.7	38.575	158.9	38.02	7.21
323.9	38.622	200.8	38.530	123.1	37.98	6.87	362.4	38.658	205.4	38.573	157.0	38.07	7.79
317.8	38.617	200.1	38.523	117.7	38.03	7.32	356.1	38.650	204.7	38.568	151.4	38.13	8.35
308.7	38.606	198.7	38.510	108.0	38.07	7.74	346.5	38.642	203.6	38.555	142.9	38.18	8.90
290.0	38.590	196.6	38.490	93.4	38.11	8.13	331.6	38.629	201.8	38.539	129.8	38.22	9.41
270.2	38.570	194.0	38.466	76.2	38.14	8.47	310.9	38.610	199.2	38.515	111.7	38.27	9.88
231.4	38.525	188.4	38.415	43.0	38.16	8.74	287.4	38.586	198.3	38.487	91.1	38.31	10.28
176.7	38.422	176.7	38.304	0	38.18	8.89	263.9	38.563	193.1	38.458	70.8	38.34	10.61
140.8	38.005	140.8	37.907	0	38.18	8.89	207.1	38.492	184.4	38.378	22.7	38.36	10.86
116.8	37.710	116.8	37.599	0	38.18	8.89	137.9	38.267	162.7	38.149	-4.8	38.37	10.95
100.9	37.497	100.9	37.396	0	38.18	8.89	127.2	37.905	131.7	37.700	-4.5	38.37	10.93
91.3	37.387	91.3	37.273	0	38.18	8.89	107.7	37.647	111.9	37.536	-4.7	38.36	10.91
84.8	37.278	84.8	37.189	0	38.18	8.89	76.6	37.490	100.5	37.391	-3.9	38.35	10.90
81.2	37.229	81.2	37.143	0	38.18	8.89	70.8	37.410	94.6	37.315	-3.7	38.36	10.88
80.8	37.224	80.8	37.138	0	38.18	8.89	69.7	37.391	93.2	37.297	-3.5	38.36	10.87

Legend :

- $Q_{u/s}$  : discharge upstream of side overflow dike
- $H_{u/s}$  : water level upstream of side overflow dike
- $Q_{d/s}$  : discharge downstream of side overflow dike
- $H_{d/s}$  : water level downstream of side overflow dike
- $q_v$  : overflow discharge
- Hb : water level in retarding basin
- Vb : storage volume in retarding basin

Legend :

- $Q_{u/s}$  : discharge upstream of side overflow dike
- $H_{u/s}$  : water level upstream of side overflow dike
- $Q_{d/s}$  : discharge downstream of side overflow dike
- $H_{d/s}$  : water level downstream of side overflow dike
- $q_v$  : overflow discharge
- Hb : water level in retarding basin
- Vb : storage volume in retarding basin

(Q-10yr & River 25-yr)						
$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_v$ ( $m^3/s$ )	Hb (m)	Vb ( $\times 10^6 m^3$ )
106.5	37.572	106.5	37.467	0	37.59	3.69
135.5	37.957	135.5	37.839	0	37.59	3.69
178.3	38.453	177.8	38.316	0.5	37.59	3.69
230.3	38.524	188.3	38.413	42.0	37.59	3.69
267.9	38.567	193.7	38.463	74.2	37.61	3.83
289.3	38.590	196.5	38.490	92.8	37.64	4.11
311.6	38.611	199.3	38.516	112.3	37.69	4.45
332.2	38.630	201.9	38.539	130.3	37.74	4.85
350.3	38.646	204.0	38.560	146.3	37.79	5.32
365.6	38.658	205.8	38.576	159.6	37.86	5.85
377.3	38.668	207.2	38.589	170.1	37.93	6.42
385.2	38.674	208.1	38.579	177.1	38.00	7.03
388.3	38.677	208.4	38.601	180.1	38.06	7.67
388.9	38.676	208.3	38.599	178.6	38.12	8.32
380.7	38.671	207.6	38.592	173.1	38.18	8.98
370.6	38.663	206.4	38.582	164.2	38.24	9.59
358.2	38.651	204.7	38.568	151.5	38.30	10.18
336.3	38.633	202.3	38.544	134.0	38.35	10.72
312.0	38.611	199.4	38.516	112.4	38.39	11.20
284.5	38.587	196.1	38.486	90.4	38.42	11.61
262.0	38.564	193.5	38.457	68.5	38.45	11.94
200.3	38.523	189.7	38.426	10.8	38.47	12.18
153.0	38.496	185.7	38.389	-32.7	38.47	12.22
124.3	38.362	171.3	38.245	-47.0	38.46	12.10
106.9	38.076	145.4	37.959	-38.5	38.45	11.93
98.2	37.888	130.2	37.772	-32.0	38.44	11.79
95.9	37.790	123.0	37.678	-27.1	38.43	11.68

Legend :

- $Q_{u/s}$  : discharge upstream of side overflow dike
- $H_{u/s}$  : water level upstream of side overflow dike
- $Q_{d/s}$  : discharge downstream of side overflow dike
- $H_{d/s}$  : water level downstream of side overflow dike
- $q_v$  : overflow discharge
- Hb : water level in retarding basin
- Vb : storage volume in retarding basin

Table 4.3.4 FLOOD ROUTING IN THE WIDAS RETARDING BASIN (3/7)

( Q-25yr & River 25-yr )

$Q_u/s$ ( $m^3/s$ )	$H_u/s$ (m)	$Q_d/s$ ( $m^3/s$ )	$H_d/s$ (m)	qw ( $m^3/s$ )	W (m)	Vb ( $\times 10^6 m^3$ )
151.4	38.144	351.4	38.025	0	37.59	3.69
195.8	38.473	182.3	38.358	13.5	37.59	3.69
249.6	38.547	191.1	38.440	58.5	37.60	3.74
275.7	38.576	195.7	38.473	81.0	37.62	3.95
300.9	38.601	198.0	38.501	102.9	37.64	4.24
325.8	38.624	201.1	38.532	124.7	37.71	4.61
348.1	38.644	203.8	38.557	144.3	37.76	5.08
367.7	38.660	206.0	38.578	161.7	37.83	5.58
384.3	38.674	208.0	38.594	176.3	37.90	6.16
397.3	38.684	209.4	38.610	187.9	37.98	6.60
406.3	38.691	210.5	38.619	193.8	38.04	7.47
410.3	38.694	210.9	38.624	199.1	38.11	8.18
410.1	38.694	210.9	38.623	199.2	38.14	8.60
405.0	38.690	210.3	38.618	194.7	38.24	9.61
395.0	38.682	209.7	38.608	185.8	38.31	10.32
381.2	38.671	207.6	38.593	173.7	38.37	10.98
362.5	38.656	205.4	38.573	157.1	38.42	11.61
338.1	38.635	202.6	38.546	135.5	38.47	12.18
311.1	38.616	200.6	38.527	110.5	38.50	12.66
284.4	38.610	200.4	38.528	83.8	38.55	13.06
259.5	38.611	201.1	38.532	58.4	38.56	13.36
192.4	38.601	199.3	38.517	-7.1	38.57	13.57
148.6	38.589	197.2	38.497	-48.6	38.57	13.55
122.8	38.571	194.5	38.471	-71.7	38.55	13.37
102.7	38.547	191.1	38.439	-82.4	38.54	13.11
103.5	38.519	187.2	38.403	-83.7	38.52	12.82
107.0	38.430	177.5	38.313	-70.5	38.49	12.52
117.9	38.387	173.6	38.270	-55.7	38.47	12.26
133.2	38.435	176.2	38.319	-45.0	38.46	12.06
148.3	38.464	181.6	38.351	-33.3	38.45	11.90
161.3	38.471	182.7	38.361	-21.6	38.44	11.78
171.0	38.477	183.5	38.368	-12.5	38.43	11.70
176.6	38.480	184.0	38.373	-7.4	38.43	11.66
177.2	38.480	183.9	38.372	-6.7	38.43	11.63
172.4	38.473	183.0	38.364	-10.6	38.42	11.61
163.0	38.457	180.9	38.345	-17.9	38.42	11.57
153.0	38.382	173.4	38.268	-20.4	38.42	11.51
144.5	38.262	167.4	38.146	-17.9	38.41	11.43
135.7	38.142	151.5	38.026	-15.8	38.41	11.37
125.8	38.011	140.0	37.896	-14.2	38.40	11.31
115.4	37.858	128.1	37.745	-12.5	38.40	11.26
105.9	37.710	117.0	37.602	-11.1	38.39	11.21
97.4	37.581	107.4	37.479	-10.0	38.39	11.17
89.8	37.465	98.8	37.369	-9.0	38.38	11.14
83.0	37.361	91.2	37.271	-8.2	38.38	11.11
77.3	37.274	84.8	37.189	-7.5	38.38	11.08
73.1	37.208	80.0	37.127	-6.9	38.38	11.05
71.4	37.178	77.7	37.098	-6.3	38.37	11.03
73.8	37.204	79.4	37.123	-5.8	38.37	11.00
81.3	37.302	86.7	37.214	-5.6	38.37	10.98
93.5	37.443	98.4	37.368	-5.1	38.37	10.96
108.5	37.660	113.2	37.558	-4.7	38.37	10.94
122.8	37.847	127.2	37.733	-4.4	38.37	10.93
132.6	37.972	136.6	37.855	-4.2	38.36	10.91

- Legend :
- $Q_u/s$  : Discharge upstream of side overflow dike
  - $H_u/s$  : water level upstream of side overflow dike
  - $Q_d/s$  : discharge downstream of side overflow dike
  - $H_d/s$  : water level downstream of side overflow dike
  - qw : overflow discharge
  - W : water level in retarding basin
  - Vb : storage volume in retarding basin

Table 4.3.4 FLOOD ROUTING IN THE ULO RETARDING BASIN (4/7)

( Q-2yr & River 10-yr )							( Q-5yr & River 10-yr )						
$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_v$ ( $m^3/s$ )	$H_B$ (m)	$V_B$ ( $\times 10^6 m^3$ )	$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_v$ ( $m^3/s$ )	$H_B$ (m)	$V_B$ ( $\times 10^6 m^3$ )
192.1	44.352	192.1	44.078	0	43.00	0	133.9	43.807	133.9	43.559	0	43.00	0
242.4	44.882	257.0	44.530	25.6	43.00	0	254.5	44.872	248.4	44.474	6.1	43.00	0
340.4	44.978	220.7	44.621	69.7	43.04	0.09	346.5	45.016	270.2	44.653	90.3	43.01	0.02
370.3	45.022	277.0	44.662	93.3	43.16	0.34	436.7	45.111	289.6	44.765	147.1	43.16	0.35
395.4	45.029	274.0	44.669	97.6	43.31	0.68	488.6	45.151	295.3	44.782	173.3	43.40	0.88
355.8	45.001	274.0	44.642	81.8	43.48	1.03	487.8	45.150	295.1	44.781	172.5	43.45	1.50
315.5	44.939	265.2	44.584	50.3	43.61	1.33	435.8	45.110	289.4	44.744	146.4	43.82	2.12
265.2	44.847	251.9	44.497	13.3	43.68	1.51	380.7	45.036	279.0	44.675	101.7	43.96	2.65
214.9	44.555	214.9	44.212	0	43.67	1.55	315.5	44.639	265.2	44.584	50.3	44.04	3.01
171.7	44.165	171.7	43.863	0	43.67	1.55	251.9	44.815	247.4	44.467	4.5	44.07	3.20
137.3	43.840	137.3	43.586	0	43.67	1.55	197.2	44.997	197.2	44.069	0	44.07	3.21
111.5	43.588	111.5	43.378	0	43.67	1.55	154.4	44.601	154.4	43.724	0	44.07	3.21
93.5	43.407	93.5	43.231	0	43.67	1.55	122.7	43.698	122.7	43.468	0	44.07	3.21
80.2	43.271	80.2	43.125	0	43.67	1.55	101.2	43.485	101.2	43.293	0	44.07	3.21
							84.1	43.332	84.1	43.173	0	44.07	3.21

( Q-10yr & River 10-yr )							( Q-25yr & River 10-yr )						
$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_v$ ( $m^3/s$ )	$H_B$ (m)	$V_B$ ( $\times 10^6 m^3$ )	$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_v$ ( $m^3/s$ )	$H_B$ (m)	$V_B$ ( $\times 10^6 m^3$ )
161.2	44.067	161.2	43.779	0	43.00	0	186.5	44.300	186.5	43.983	0	43.00	0
304.6	44.921	262.6	44.567	42.0	43.00	0	352.8	44.997	273.4	44.638	79.4	43.00	0
434.8	45.109	289.3	44.743	145.5	43.07	0.15	494.9	45.183	299.8	44.812	195.1	43.13	0.29
515.1	45.207	303.2	44.834	211.9	43.31	0.68	570.0	45.271	312.0	44.892	258.0	43.45	0.29
547.4	45.245	308.4	44.869	239.0	43.44	1.44	590.7	45.295	315.3	44.914	278.4	43.76	1.92
539.8	45.236	307.2	44.860	232.6	43.67	2.30	584.1	45.287	314.2	44.907	269.9	44.01	2.91
497.1	45.186	300.1	44.814	197.0	44.06	3.14	556.0	45.253	309.5	44.876	244.5	44.20	3.68
430.4	45.103	288.3	44.737	141.9	44.19	3.84	494.1	45.187	300.3	44.815	197.8	44.26	4.74
354.2	45.099	273.7	44.640	80.3	44.28	4.36	424.8	45.096	287.4	44.731	137.4	44.47	5.42
281.2	44.879	256.6	44.528	24.6	44.34	4.85	348.3	44.990	272.4	44.637	75.9	44.34	5.99
218.8	44.589	218.8	44.243	0	44.33	4.73	278.8	44.881	258.6	44.542	20.2	44.38	6.24
169.8	44.147	169.8	43.848	0	44.33	4.73	219.5	44.683	232.3	44.352	-12.8	44.39	6.31
134.1	43.809	134.1	43.560	0	44.33	4.73	173.1	44.289	184.6	43.968	-11.5	44.38	6.22
109.1	43.564	109.1	43.359	0	44.33	4.73	136.6	43.937	149.1	43.681	-10.5	44.37	6.22
92.2	43.394	92.2	43.222	0	44.33	4.73	113.6	43.687	123.2	43.432	-9.6	44.37	6.19

( Q-2yr & River 25-yr )							( Q-5yr & River 25-yr )						
$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_v$ ( $m^3/s$ )	$H_B$ (m)	$V_B$ ( $\times 10^6 m^3$ )	$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_v$ ( $m^3/s$ )	$H_B$ (m)	$V_B$ ( $\times 10^6 m^3$ )
192.1	43.951	192.1	43.640	0	43.00	0	133.9	43.416	133.9	43.167	0	43.00	0
242.4	44.716	282.4	44.369	0	43.00	0	234.6	44.491	254.6	44.148	0	43.00	0
340.4	44.891	309.3	44.346	30.9	43.00	0	366.4	44.932	316.4	44.587	50.0	43.00	0
370.3	44.938	317.3	44.393	53.0	43.03	0.11	436.8	45.029	332.7	44.685	104.1	43.08	0.18
375.6	45.946	318.7	44.601	56.9	43.14	0.30	468.6	45.068	339.4	44.725	129.2	43.26	0.55
355.8	44.916	313.4	44.571	42.2	43.23	0.51	467.4	45.067	339.2	44.724	128.4	43.47	1.02
315.6	44.845	302.3	44.499	13.3	43.30	0.64	435.4	45.021	332.3	44.684	103.3	43.65	1.48
265.2	44.580	245.2	44.234	0	43.33	0.71	360.7	45.953	319.9	44.608	60.8	43.75	1.85
214.9	44.151	214.9	43.875	0	43.33	0.71	315.6	44.845	302.2	44.499	13.3	43.81	2.07
171.7	43.768	171.7	43.474	0	43.33	0.71	251.9	44.468	251.9	43.126	0	43.82	2.12
137.3	43.449	137.3	43.184	0	43.33	0.71	197.2	44.996	197.2	43.681	0	43.82	2.12
111.5	43.200	111.5	42.985	0	43.33	0.71	154.4	43.609	154.4	43.333	0	43.82	2.12
93.5	43.021	93.5	42.838	0	43.33	0.71	122.7	43.309	122.7	43.076	0	43.82	2.12
80.2	42.883	80.2	42.720	0	43.33	0.71	101.2	43.098	101.2	42.901	0	43.82	2.12
							84.1	42.946	84.1	42.778	0	43.82	2.12

Legend :

- $Q_{u/s}$  : discharge upstream of side overflow dike
- $H_{u/s}$  : water level upstream of side overflow dike
- $Q_{d/s}$  : discharge downstream of side overflow dike
- $H_{d/s}$  : water level downstream of side overflow dike
- $q_v$  : overflow discharge
- $H_B$  : water level in retarding basin
- $V_B$  : storage volume in retarding basin

Legend :

- $Q_{u/s}$  : discharge upstream of side overflow dike
- $H_{u/s}$  : water level upstream of side overflow dike
- $Q_{d/s}$  : discharge downstream of side overflow dike
- $H_{d/s}$  : water level downstream of side overflow dike
- $q_v$  : overflow discharge
- $H_B$  : water level in retarding basin
- $V_B$  : storage volume in retarding basin

Table 4.3.4 FLOOD ROUTING IN THE ULO RETARDING BASIN (5/7)

(Q-10yr & River 25-yr)							(Q-25yr & River 25-yr)						
$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_w$ ( $m^3/s$ )	Hb (m)	Vb ( $\times 10^6 m^3$ )	$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_w$ ( $m^3/s$ )	Hb (m)	Vb ( $\times 10^6 m^3$ )
161.2	43.672	161.1	43.289	0	43.00	0	166.5	43.901	166.5	43.394	0	43.00	0
304.6	44.821	298.5	44.474	6.1	43.00	0	332.7	44.911	312.8	44.366	39.9	43.00	0
434.8	45.026	332.2	44.683	102.6	43.01	0.02	491.9	45.099	346.8	44.757	150.1	43.07	0.14
515.1	45.122	349.0	44.780	166.1	43.18	0.39	570.0	45.182	360.0	44.841	210.0	43.32	0.68
547.4	45.158	355.5	44.816	191.9	43.46	0.98	590.7	45.204	364.0	44.863	226.7	43.64	1.44
539.8	45.150	354.0	44.808	185.8	43.70	1.68	584.1	45.197	362.7	44.856	221.4	43.85	2.26
497.1	45.101	345.3	44.759	142.8	43.88	2.35	553.9	45.165	356.8	44.823	197.1	44.05	3.05
430.5	45.020	331.3	44.677	99.2	44.02	2.89	498.1	45.102	345.5	44.760	152.6	44.18	3.76
334.1	44.977	313.2	44.588	40.9	44.08	3.23	424.9	45.073	330.1	44.689	94.7	44.27	4.31
231.2	44.706	281.2	44.360	0	44.11	3.40	348.2	44.904	311.6	44.559	36.6	44.36	4.65
218.8	44.185	218.8	43.857	0	44.11	3.40	278.4	44.689	278.6	44.341	0	44.36	4.78
169.4	43.751	169.8	43.459	0	44.11	3.40	219.6	44.192	219.6	43.864	0	44.36	4.78
134.1	43.418	134.1	43.168	0	44.11	3.40	173.1	43.781	173.1	43.486	0	44.36	4.78
109.1	43.176	109.1	42.965	0	44.11	3.40	138.6	43.461	138.6	43.205	0	44.36	4.78
92.2	43.008	92.2	42.828	0	44.11	3.40	112.6	43.220	112.6	43.002	0	44.36	4.78

Table 4.3.4 FLOOD ROUTING IN THE KEDUNGSOKO RETARDING BASIN (6/7)

(Q-1.05yr & River 10-yr)							(Q-2yr & River 10-yr)						
$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_w$ ( $m^3/s$ )	Hb (m)	Vb ( $\times 10^6 m^3$ )	$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_w$ ( $m^3/s$ )	Hb (m)	Vb ( $\times 10^6 m^3$ )
114.8	44.433	114.2	44.268	0	43.85	0.99	148.8	44.699	136.3	44.513	12.5	43.85	0.99
184.3	44.732	139.5	44.547	24.8	43.83	0.99	215.9	44.809	147.3	44.623	69.4	43.84	1.05
206.4	44.794	145.8	44.609	40.6	43.87	1.10	269.7	44.875	154.5	44.691	114.7	43.92	1.30
217.0	44.809	147.4	44.623	49.6	43.93	1.31	283.0	44.892	156.2	44.707	126.8	44.02	1.71
189.4	44.770	143.2	44.584	46.2	43.98	1.37	247.0	44.848	151.5	44.663	95.3	44.11	2.16
146.2	44.693	135.8	44.508	10.4	44.03	1.73	190.7	44.771	143.4	44.586	47.3	44.18	2.51
111.1	44.618	111.1	44.232	0	44.03	1.77	144.9	44.690	135.5	44.505	9.4	44.21	2.68
88.1	44.101	88.1	43.926	0	44.03	1.77	114.9	44.463	114.9	44.278	0	44.22	2.71
75.2	43.878	75.2	43.720	0	44.07	1.77	83.3	44.210	83.3	44.027	0	44.22	2.71
67.4	43.712	67.4	43.572	0	44.03	1.77	81.4	44.001	81.4	43.833	0	44.22	2.71
53.5	43.572	53.5	43.449	0	44.03	1.77	69.8	43.826	69.8	43.674	0	44.22	2.71
46.4	43.459	46.4	43.352	0	44.03	1.77	60.5	43.682	60.5	43.546	0	44.22	2.71

(Q-5yr & River 10-yr)							(Q-10yr & River 10-yr)						
$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_w$ ( $m^3/s$ )	Hb (m)	Vb ( $\times 10^6 m^3$ )	$Q_{u/s}$ ( $m^3/s$ )	$H_{u/s}$ (m)	$Q_{d/s}$ ( $m^3/s$ )	$H_{d/s}$ (m)	$q_w$ ( $m^3/s$ )	Hb (m)	Vb ( $\times 10^6 m^3$ )
195.0	44.778	144.1	44.592	50.9	43.83	0.99	127.9	44.610	127.9	44.425	0	43.85	0.99
280.2	44.889	155.9	44.704	124.3	43.90	1.18	230.5	44.827	149.3	44.643	81.2	43.89	0.99
343.3	44.958	163.4	44.775	177.9	44.01	1.63	326.9	44.942	161.6	44.759	165.3	43.92	1.39
351.0	44.968	164.4	44.786	186.4	44.13	2.27	392.5	45.012	169.7	44.830	222.6	44.06	1.89
298.6	44.910	158.2	44.726	140.4	44.26	2.94	299.2	45.018	170.5	44.836	227.7	44.21	2.60
224.1	44.819	148.4	44.633	75.7	44.34	3.43	233.8	44.950	162.5	44.767	171.5	44.33	3.51
166.7	44.733	139.5	44.547	27.2	44.39	3.72	244.8	44.848	151.5	44.663	95.3	44.45	4.13
130.3	44.634	130.3	44.450	0	44.40	3.82	181.6	44.757	141.9	44.572	39.7	44.50	4.47
107.3	44.372	107.3	44.187	0	44.40	3.82	140.6	44.683	135.1	44.501	5.5	44.52	4.61
80.8	44.141	80.8	43.963	0	44.40	3.82	115.1	44.494	112.8	44.312	- 2.7	44.52	4.63
77.5	43.943	77.5	43.780	0	44.40	3.82	97.0	44.264	99.6	44.083	- 2.6	44.52	4.62
66.8	43.760	66.8	43.632	0	44.40	3.82	82.6	44.052	85.0	43.883	- 2.4	44.52	4.61
							71.1	43.837	73.4	43.723	- 2.3	44.51	4.60

Legend :

- $Q_{u/s}$  : discharge upstream of side overflow dike
- $H_{u/s}$  : water level upstream of side overflow dike
- $Q_{d/s}$  : discharge downstream of side overflow dike
- $H_{d/s}$  : water level downstream of side overflow dike
- $q_w$  : overflow discharge
- Hb : water level in retarding basin
- Vb : storage volume in retarding basin

Legend :

- $Q_{u/s}$  : discharge upstream of side overflow dike
- $H_{u/s}$  : water level upstream of side overflow dike
- $Q_{d/s}$  : discharge downstream of side overflow dike
- $H_{d/s}$  : water level downstream of side overflow dike
- $q_w$  : overflow discharge
- Hb : water level in retarding basin
- Vb : storage volume in retarding basin



Table 4.3.4 FLOOD ROUTING IN THE KEDUNGSOKO RETARDING BASIN (7/7)

( Q-25yr & River 10-yr )

Q <sub>u/s</sub> (m <sup>3</sup> /s)	H <sub>u/s</sub> (m)	Q <sub>d/s</sub> (m <sup>3</sup> /s)	H <sub>d/s</sub> (m)	q <sub>w</sub> (m <sup>3</sup> /s)	H <sub>b</sub> (m)	V <sub>b</sub> (x10 <sup>6</sup> m <sup>3</sup> )
152.4	44.704	132.0	44.521	15.4	43.83	0.99
274.3	44.892	155.1	44.697	119.2	43.86	1.06
384.4	45.004	168.8	44.822	215.6	43.97	1.48
455.3	45.077	177.2	44.895	278.1	44.13	2.26
455.2	45.074	177.2	44.895	278.0	44.31	3.26
374.8	44.994	167.4	44.811	207.2	44.47	4.26
372.0	44.879	154.8	44.694	117.2	44.57	5.01
197.1	44.749	148.9	44.619	50.2	44.63	5.43
151.2	44.740	144.2	44.593	7.0	44.65	5.41
123.0	44.713	141.4	44.569	-18.6	44.66	5.44
103.5	44.687	138.4	44.535	-34.9	44.65	5.57
87.9	44.554	125.0	44.395	-37.1	44.63	5.44
75.3	44.307	103.9	44.143	-29.4	44.61	5.31
63.7	44.084	88.4	43.929	-22.7	44.60	5.21
57.9	43.903	74.3	43.763	-18.4	44.59	5.13
51.5	43.760	66.8	43.632	-13.3	44.58	5.06
44.1	43.641	59.1	43.524	-13.0	44.57	5.01
41.5	43.541	52.7	43.438	-11.2	44.57	4.98
37.6	43.457	47.3	43.364	- 9.7	44.56	4.92
34.3	43.387	42.9	43.303	- 8.6	44.55	4.89
31.6	43.329	39.5	43.253	- 7.7	44.55	4.83
29.4	43.281	36.3	43.212	- 6.9	44.55	4.83
27.4	43.239	33.6	43.175	- 6.2	44.54	4.80
24.7	43.252	34.3	43.184	- 5.4	44.54	4.78
39.2	43.418	44.4	43.374	- 5.2	44.54	4.77

( Q-2yr & River 25-yr )

Q <sub>u/s</sub> (m <sup>3</sup> /s)	H <sub>u/s</sub> (m)	Q <sub>d/s</sub> (m <sup>3</sup> /s)	H <sub>d/s</sub> (m)	q <sub>w</sub> (m <sup>3</sup> /s)	H <sub>b</sub> (m)	V <sub>b</sub> (x10 <sup>6</sup> m <sup>3</sup> )
148.8	44.646	148.8	44.461	0	43.85	0
216.9	44.779	163.2	44.599	53.7	43.85	0
269.2	44.845	171.3	44.670	97.9	43.96	1.19
283.0	44.861	173.3	44.687	109.7	43.99	1.55
217.1	44.818	168.0	44.641	79.1	44.07	1.94
190.7	44.740	158.7	44.558	32.0	44.13	2.23
164.8	44.607	144.8	44.422	0	44.15	2.34
114.9	44.278	114.9	44.093	0	44.15	2.34
95.3	44.023	95.3	43.852	0	44.15	2.34
81.4	43.832	81.4	43.676	0	44.15	2.34
69.8	43.672	69.8	43.532	0	44.15	2.34
60.5	43.540	60.5	43.416	0	44.15	2.34

( Q-10yr & River 25-yr )

Q <sub>u/s</sub> (m <sup>3</sup> /s)	H <sub>u/s</sub> (m)	Q <sub>d/s</sub> (m <sup>3</sup> /s)	H <sub>d/s</sub> (m)	q <sub>w</sub> (m <sup>3</sup> /s)	H <sub>b</sub> (m)	V <sub>b</sub> (x10 <sup>6</sup> m <sup>3</sup> )
124.0	44.631	124.0	44.245	0	43.85	0.99
230.4	44.797	163.4	44.618	65.2	43.85	0.99
324.9	44.904	179.5	44.741	147.6	43.91	1.23
392.4	44.975	188.2	44.816	204.2	44.03	1.77
398.2	44.981	189.0	44.822	209.2	44.18	2.50
373.8	44.916	180.2	44.749	153.6	44.31	3.25
314.9	44.818	168.0	44.640	78.9	44.40	3.81
181.6	44.725	157.1	44.542	24.5	44.44	4.09
140.6	44.566	140.6	44.381	0	44.45	4.18
115.1	44.280	115.1	44.095	0	44.45	4.18
97.0	44.043	97.0	43.870	0	44.45	4.18
82.8	43.849	82.8	43.691	0	44.45	4.18
71.1	43.690	71.1	43.548	0	44.45	4.18

Legend :

- Q<sub>u/s</sub> : discharge upstream of side overflow dike
- H<sub>u/s</sub> : water level upstream of side overflow dike
- Q<sub>d/s</sub> : discharge downstream of side overflow dike
- H<sub>d/s</sub> : water level downstream of side overflow dike
- q<sub>w</sub> : overflow discharge
- H<sub>b</sub> : water level in retarding basin
- V<sub>b</sub> : storage volume in retarding basin

( Q-1.03yr & River 25-yr )

Q <sub>u/s</sub> (m <sup>3</sup> /s)	H <sub>u/s</sub> (m)	Q <sub>d/s</sub> (m <sup>3</sup> /s)	H <sub>d/s</sub> (m)	q <sub>w</sub> (m <sup>3</sup> /s)	H <sub>b</sub> (m)	V <sub>b</sub> (x10 <sup>6</sup> m <sup>3</sup> )
114.2	44.349	114.2	44.044	0	43.85	0
166.3	44.697	134.1	44.513	32.2	43.85	0.99
206.4	44.764	161.5	44.583	44.9	43.86	1.04
217.0	44.779	163.3	44.599	53.7	43.90	1.21
169.4	44.738	158.5	44.556	30.9	43.95	1.40
144.1	44.620	146.1	44.435	0	43.98	1.51
111.1	44.229	111.1	44.045	0	43.98	1.51
89.1	43.923	88.1	43.760	0	43.98	1.51
73.2	43.567	73.2	43.440	0	43.98	1.51
62.4	43.567	62.4	43.440	0	43.98	1.51
55.5	43.440	55.5	43.329	0	43.98	1.51
46.4	43.337	46.4	43.241	0	43.98	1.51

( Q-3yr & River 25-yr )

Q <sub>u/s</sub> (m <sup>3</sup> /s)	H <sub>u/s</sub> (m)	Q <sub>d/s</sub> (m <sup>3</sup> /s)	H <sub>d/s</sub> (m)	q <sub>w</sub> (m <sup>3</sup> /s)	H <sub>b</sub> (m)	V <sub>b</sub> (x10 <sup>6</sup> m <sup>3</sup> )
194.9	44.747	159.5	44.565	35.4	43.45	0.89
280.2	44.857	172.9	44.684	107.3	43.45	1.13
341.3	44.923	181.2	44.738	180.1	43.98	1.51
351.0	44.933	182.5	44.749	168.5	44.10	2.09
298.7	44.878	175.5	44.707	123.2	44.22	2.70
224.1	44.749	164.4	44.609	59.7	44.29	3.14
184.7	44.698	154.2	44.514	12.5	44.33	3.36
130.4	44.637	130.4	44.271	0	44.33	3.40
107.3	44.179	107.3	43.998	0	44.33	3.40
90.8	43.960	90.8	43.793	0	44.33	3.40
77.5	43.779	77.5	43.628	0	44.33	3.40
66.8	43.630	66.8	43.495	0	44.33	3.40

( Q-25yr & River 25-yr )

Q <sub>u/s</sub> (m <sup>3</sup> /s)	H <sub>u/s</sub> (m)	Q <sub>d/s</sub> (m <sup>3</sup> /s)	H <sub>d/s</sub> (m)	q <sub>w</sub> (m <sup>3</sup> /s)	H <sub>b</sub> (m)	V <sub>b</sub> (x10 <sup>6</sup> m <sup>3</sup> )
152.4	44.664	150.6	44.479	1.8	43.85	0.99
274.3	44.851	172.0	44.676	102.3	43.85	1.01
384.5	44.967	187.2	44.807	197.3	43.94	1.37
455.3	45.035	196.4	44.884	258.7	44.10	2.09
455.2	45.035	196.5	44.884	258.7	44.17	3.02
374.8	44.957	185.8	44.796	189.0	44.42	3.95
272.1	44.848	171.7	44.674	100.4	44.52	4.43
197.3	44.732	160.3	44.574	36.7	44.57	4.99
131.1	44.691	155.2	44.524	- 4.1	44.59	5.12
123.0	44.551	140.4	44.379	-17.4	44.59	5.11
102.6	44.306	118.1	44.133	-14.5	44.58	5.04
88.0	44.077	100.4	43.913	-12.4	44.57	4.99
75.5	43.886	84.2	43.734	-10.7	44.56	4.95
65.7	43.733	73.1	43.598	- 9.4	44.56	4.91
57.9	43.609	64.2	43.488	- 8.3	44.55	4.87
51.5	43.507	58.9	43.397	- 7.4	44.55	4.84
46.1	43.419	52.8	43.320	- 6.7	44.55	4.82
41.5	43.343	47.3	43.259	- 6.0	44.54	4.79
37.6	43.279	43.1	43.200	- 5.5	44.54	4.77
34.3	43.224	39.3	43.153	- 5.0	44.54	4.75
31.6	43.179	36.2	43.115	- 4.6	44.53	4.73
29.4	43.141	33.7	43.083	- 4.3	44.53	4.72
27.4	43.107	31.4	43.054	- 4.0	44.53	4.70
24.7	43.123	32.4	43.067	- 3.7	44.53	4.69
39.2	43.275	42.4	43.194	- 3.4	44.52	4.67
64.1	43.631	67.3	43.501	- 3.2	44.53	4.64
92.5	44.019	95.5	43.852	- 3.0	44.52	4.65

Legend :

- Q<sub>u/s</sub> : discharge upstream of side overflow dike
- H<sub>u/s</sub> : water level upstream of side overflow dike
- Q<sub>d/s</sub> : discharge downstream of side overflow dike
- H<sub>d/s</sub> : water level downstream of side overflow dike
- q<sub>w</sub> : overflow discharge
- H<sub>b</sub> : water level in retarding basin
- V<sub>b</sub> : storage volume in retarding basin

Table 4.3.5 FLOOD PEAK REDUCTION AND ITS VOLUME

Widas Retarding Basin

River Cross-section	Return Period of Flood (Year)	Peak Discharge		Volume (x10 <sup>6</sup> m <sup>3</sup> )
		Before reduction (m <sup>3</sup> /s)	After reduction (m <sup>3</sup> /s)	
10-yr plan	10	375	207	7.86
	5	358	205	6.97
	2	324	201	5.07
	1.05	245	191	1.85
25-yr plan	25	410	211	9.88
	10	389	208	8.53
	5	365	206	7.26
	2	327	201	5.20

Ulo Retarding Basin

River Cross-section	Return Period of Flood (Year)	Peak Discharge		Volume (x10 <sup>6</sup> m <sup>3</sup> )
		Before reduction (m <sup>3</sup> /s)	After reduction (m <sup>3</sup> /s)	
10-yr plan	10	547	308	4.73
	5	469	295	3.21
	2	376	278	1.55
25-yr plan	25	591	364	4.78
	10	547	356	3.39
	5	469	339	2.12
	2	376	319	0.71

Kedungsoko Retarding basin

River Cross-section	Return Period of Flood (Year)	Peak Discharge		Volume (X10 <sup>6</sup> m <sup>3</sup> )
		Before reduction (m <sup>3</sup> /s)	After reduction (m <sup>3</sup> /s)	
10-yr plan	10	398	171	3.63
	5	351	165	2.82
	2	283	156	1.71
	1.05	217	147	0.77
25-yr plan	25	455	197	4.12
	10	398	189	3.18
	5	351	183	2.40
	2	283	173	1.34
	1.05	217	163	0.51

Table 4.3.6 MAXIMUM WATER LEVEL, INUNDATION AREA AND STORAGE VOLUME IN RETARDING BASIN (Cross-section for 10-year probable flood) (1/2)

Return Period (Year)	Retarding Basin								
	Widas			U l o			Kedungsoko		
	Hb (m)	Vb ( $\times 10^6 m^3$ )	A ( $km^2$ )	Hb (m)	Vb ( $\times 10^6 m^3$ )	A ( $km^2$ )	Hb (m)	Vb ( $\times 10^6 m^3$ )	A ( $km^2$ )
1.05	37.82	5.54	9.15	-	-	-	44.03	1.77	3.35
2	38.46	8.76	11.15	43.67	1.55	4.20	44.22	2.71	4.25
5	38.34	10.66	12.08	44.07	3.21	5.75	44.40	3.82	5.30
10	38.42	11.55	12.45	44.35	4.73	6.25	44.52	4.63	6.05

Legend :

Hb : maximum water level in retarding basin  
Vb : maximum storage volume in retarding basin  
A : maximum inundation area

Table 4.3.6 MAXIMUM WATER LEVEL, INUNDATION AREA AND STORAGE VOLUME IN RETARDING BASIN (Cross-section for 25-year probable flood) (2/2)

Return Period (Year)	Retarding Basin								
	Widas			U l o			Kedungsoko		
	Hb (m)	Vb ( $\times 10^6 m^3$ )	A ( $km^2$ )	Hb (m)	Vb ( $\times 10^6 m^3$ )	A ( $km^2$ )	Hb (m)	Vb ( $\times 10^6 m^3$ )	A ( $km^2$ )
1.05	-	-	-	-	-	-	43.98	1.51	3.20
2	38.18	8.89	11.25	43.33	0.71	2.20	44.15	2.34	3.90
5	38.37	10.95	12.25	43.82	2.12	4.90	44.33	3.40	4.85
10	38.47	12.22	12.70	44.11	3.40	5.80	44.45	4.18	5.60
25	38.57	13.57	13.20	44.36	4.78	6.30	44.59	5.12	6.50

Legend :

Hb : maximum water level in retarding basin  
Vb : maximum storage volume in retarding basin  
A : maximum inundation area

Table 4.3.7 STAGE DISCHARGE RELATION IN K. BRANTAS USED FOR STUDY ON DRAINAGE SLUICE OF WIDAS RETARDING BASIN (1/3)

Elevation (m)	Q (m <sup>3</sup> /s)
34.00	100.00
34.55	200.00
35.26	400.00
35.83	600.00
36.30	800.00
36.72	1000.00
37.10	1200.00
37.45	1400.00
37.59	1500.00
37.60	1600.00

Table 4.3.7 STAGE DISCHARGE RELATION IN THE KEDUNGSOKO RIVER USED FOR STUDY ON DRAINAGE SLUICE OF ULO RETARDING BASIN (2/3)

Elevation (m)	Q (m <sup>3</sup> /s)
39.50	0
40.50	31.71
41.50	101.85
42.50	202.92
43.50	332.66
43.70	361.96
44.00	419.38
44.50	536.36
45.00	674.69
45.50	831.97

Table 4.3.7 STAGE DISCHARGE RELATION IN THE KEDUNGSOKO RIVER USED FOR STUDY ON DRAINAGE SLUICE OF KEDUNGSOKO RETARDING BASIN (3/3)

Elevation (m)	Q (m <sup>3</sup> /s)
40.75	0
41.75	15.92
42.75	52.18
43.75	106.35
43.85	112.75
43.95	120.79
44.15	139.04
44.35	159.57
44.55	182.12
44.75	206.56
44.95	232.78
45.15	260.70
45.35	290.28
45.55	321.45
45.75	354.20

Table 4.3.8 DESIGN FLOOD DISCHARGE HYDROGRAPH IN K. BRANTAS USED FOR STUDY ON DRAINAGE SLUICE OF WIDAS RETARDING BASIN (1/3)

No.	Q (m <sup>3</sup> /s)	No.	Q (m <sup>3</sup> /s)	No.	Q (m <sup>3</sup> /s)
1	1198.1	25	895.2	49	895.2
2	1180.8	26	895.2	50	895.2
3	1163.1	27	895.2	51	895.2
4	1145.0	28	895.2	52	895.2
5	1126.6	29	895.2	53	895.2
6	1107.9	30	895.2	54	895.2
7	1089.1	31	895.2	55	895.2
8	1070.2	32	895.2	56	895.2
9	1051.2	33	895.2	57	895.2
10	1032.1	34	895.2	58	895.2
11	1013.1	35	895.2	59	895.2
12	994.3	36	895.2	60	895.2
13	959.0	37	895.2	61	895.2
14	895.2	38	895.2	62	895.2
15	895.2	39	895.2	63	895.2
16	895.2	40	895.2	64	895.2
17	895.2	41	895.2	65	895.2
18	895.2	42	895.2	66	895.2
19	895.2	43	895.2	67	895.2
20	895.2	44	895.2	68	895.2
21	895.2	45	895.2	69	895.2
22	895.2	46	895.2	70	895.2
23	895.2	47	895.2	71	895.2
24	895.2	48	895.2	72	895.2

Table 4.3.8 25-YEAR PROBABLE FLOOD HYDROGRAPH IN THE  
WIDAS RIVER AT THE CONFLUENCE WITH THE  
KEDUNGSOKO RIVER (2/3)

No.	Q (m <sup>3</sup> /s)	No.	Q (m <sup>3</sup> /s)	No.	Q (m <sup>3</sup> /s)
1	263.0	20	203.0	39	100.7
2	224.9	21	202.2	40	133.9
3	193.0	22	180.6	41	155.5
4	163.9	23	172.5	42	161.8
5	138.3	24	150.3	43	160.3
6	115.3	25	129.0	44	157.3
7	87.2	26	112.5	45	152.1
8	86.2	27	99.9	46	144.0
9	78.7	28	89.5	47	132.0
10	73.1	29	80.6	48	121.0
11	68.8	30	73.0	49	107.0
12	65.8	31	66.5	50	92.0
13	66.1	32	61.2	51	80.0
14	73.1	33	56.4	52	70.0
15	87.9	34	52.2	53	61.0
16	109.9	35	49.0	54	54.0
17	136.4	36	48.3	55	52.0
18	165.1	37	53.6	56	51.0
19	189.9	38	70.6		

Table 4.3.8 25-YEAR PROBABLE FLOOD HYDROGRAPH IN THE KEDUNGSOKO RIVER (3/3)

No.	Q (m <sup>3</sup> /s)	No.	Q (m <sup>3</sup> /s)
1	151.2	24	147.4
2	123.0	25	135.0
3	103.6	26	117.4
4	88.0	27	101.0
5	75.5	28	88.5
6	65.7	29	78.4
7	57.9	30	69.5
8	51.5	31	61.6
9	46.1	32	54.7
10	41.5	33	48.8
11	36.6	34	43.8
12	34.3	35	39.6
13	31.6	36	36.1
14	29.4	37	36.9
15	27.4	38	50.3
16	28.7	39	70.7
17	39.2	40	79.1
18	64.1	41	72.9
19	92.5	42	65.1
20	114.1	43	60.8
21	134.0	44	58.1
22	149.0	45	55.2
23	152.8	46	51.3

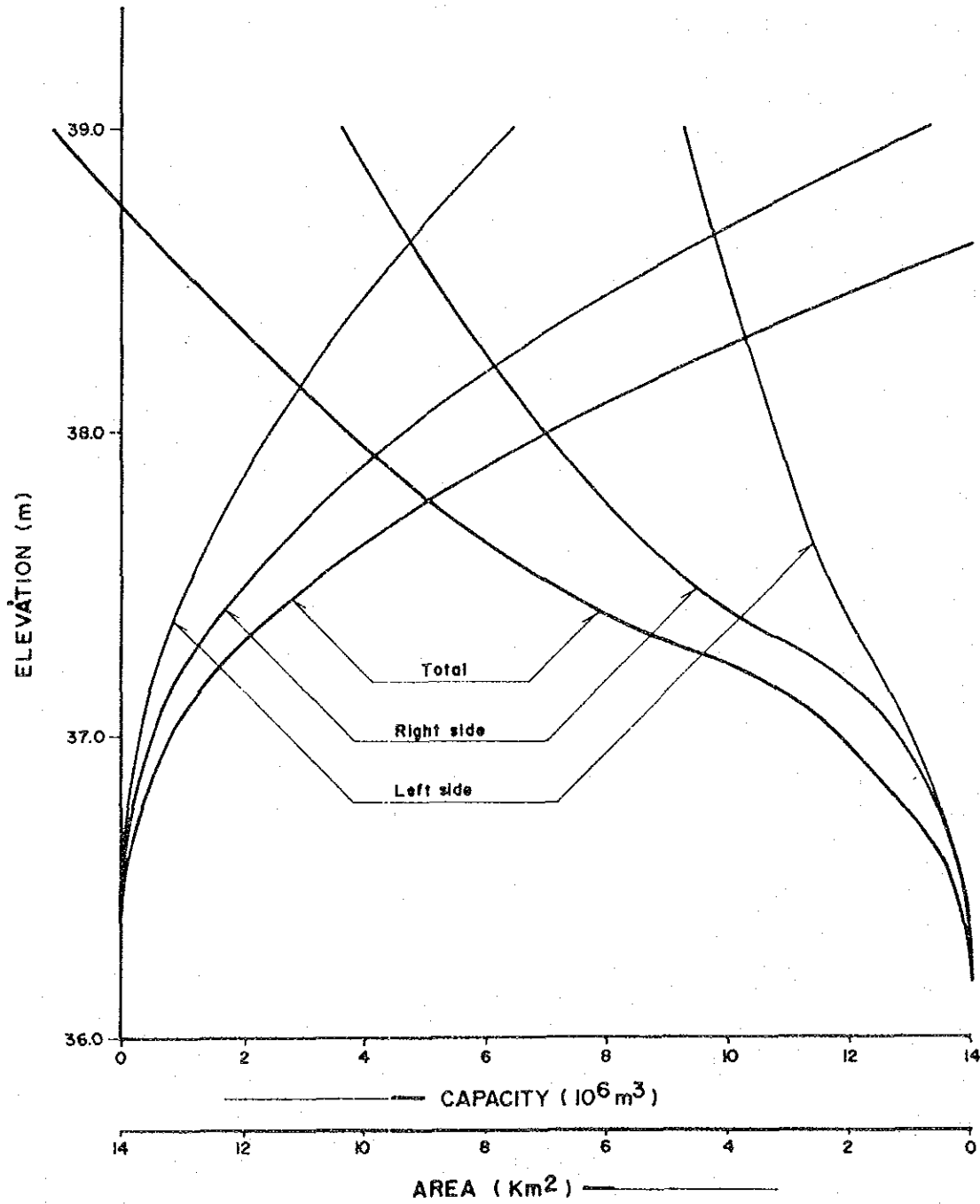


Fig. 4.3.1 STORAGE CAPACITY AND AREA OF WIDAS RETARDING BASIN (1/3)



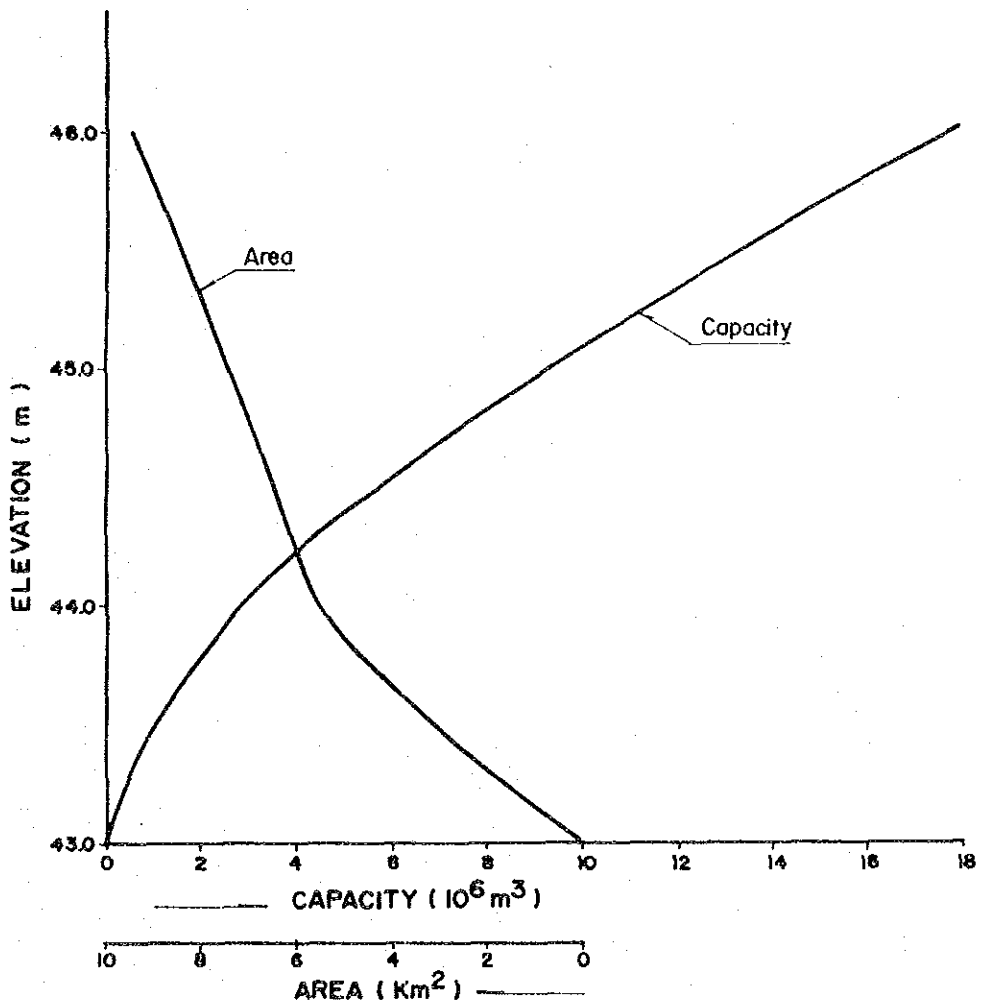
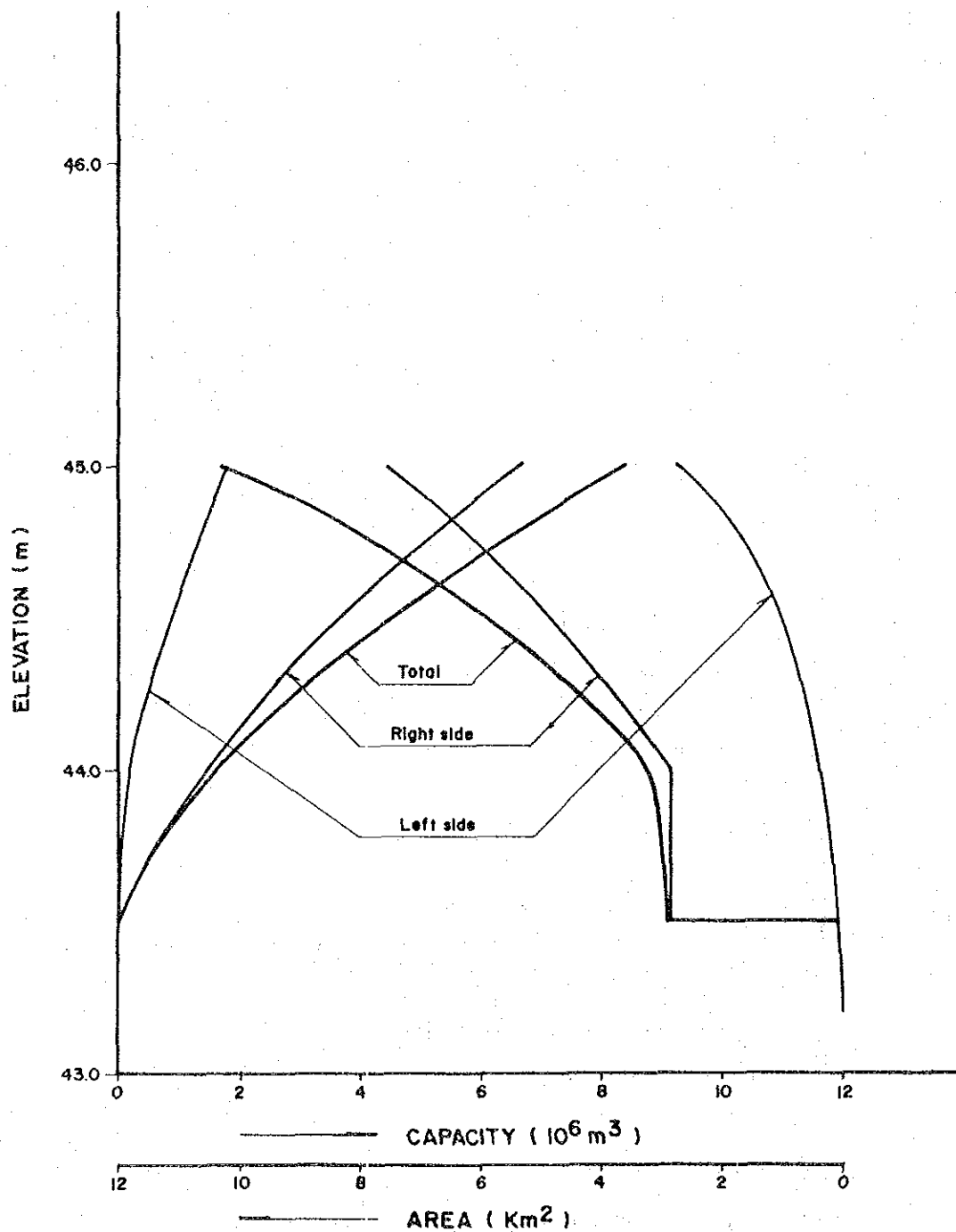


Fig. 4.3.1 STORAGE CAPACITY AND AREA OF ULO RETARDING BASIN (2/3)



**Fig. 4.3.1 STORAGE CAPACITY AND AREA OF KEDUNGSOKO RETARDING BASIN ( 3/3 )**

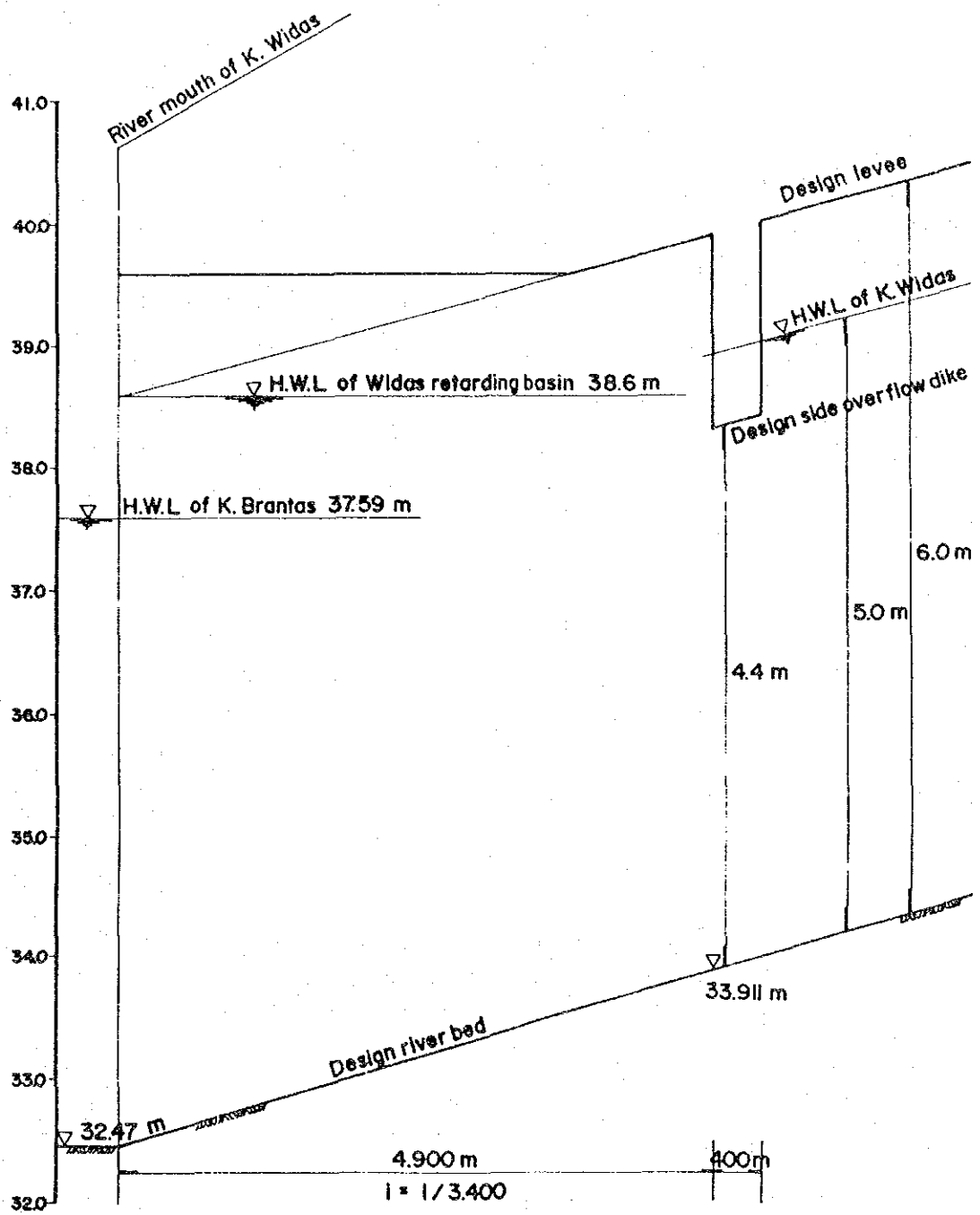


Fig. 4.3.2 LONGITUDINAL PROFILE OF WIDAS RIVER AT WIDAS RETARDING BASIN (1/3)

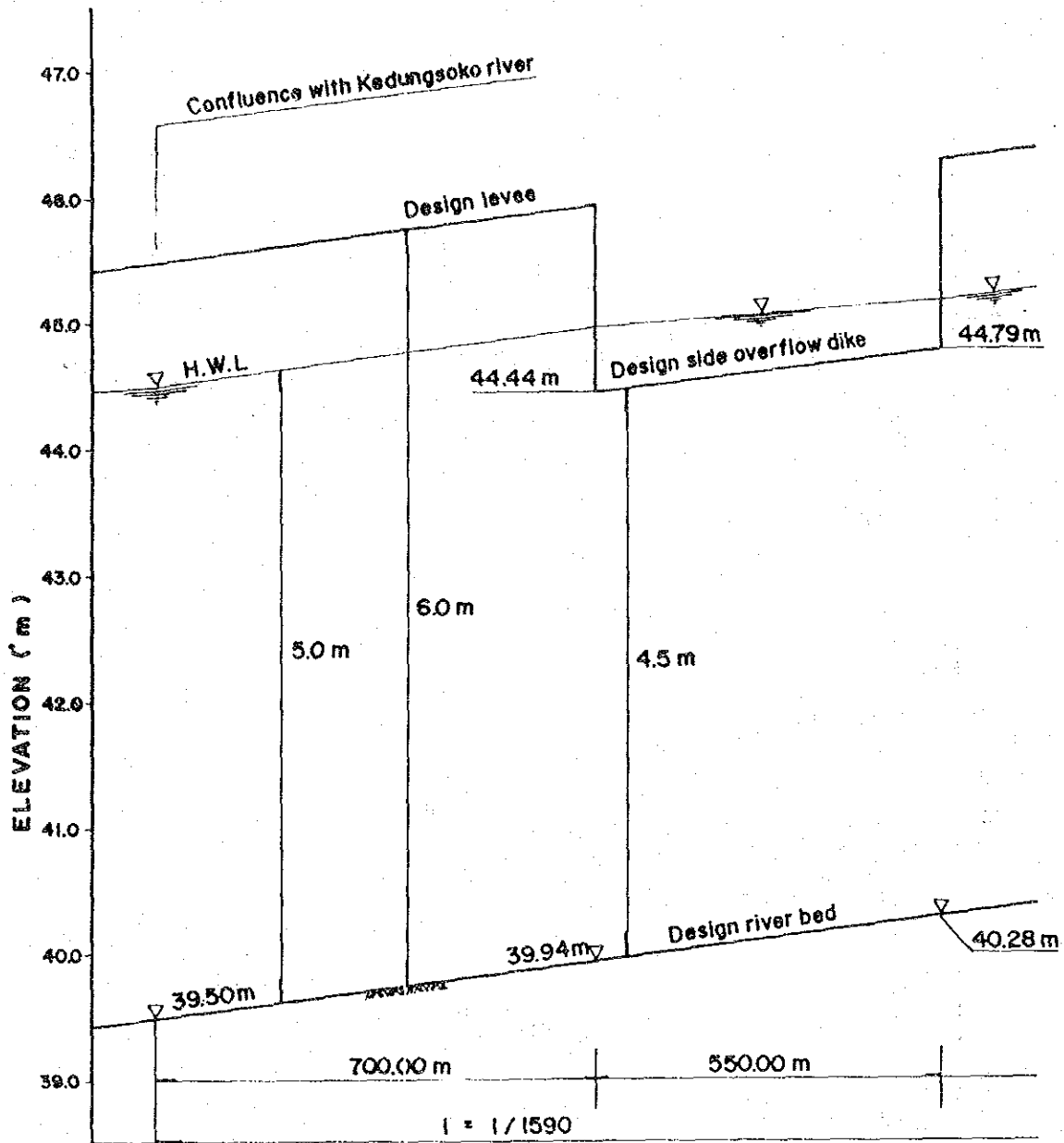
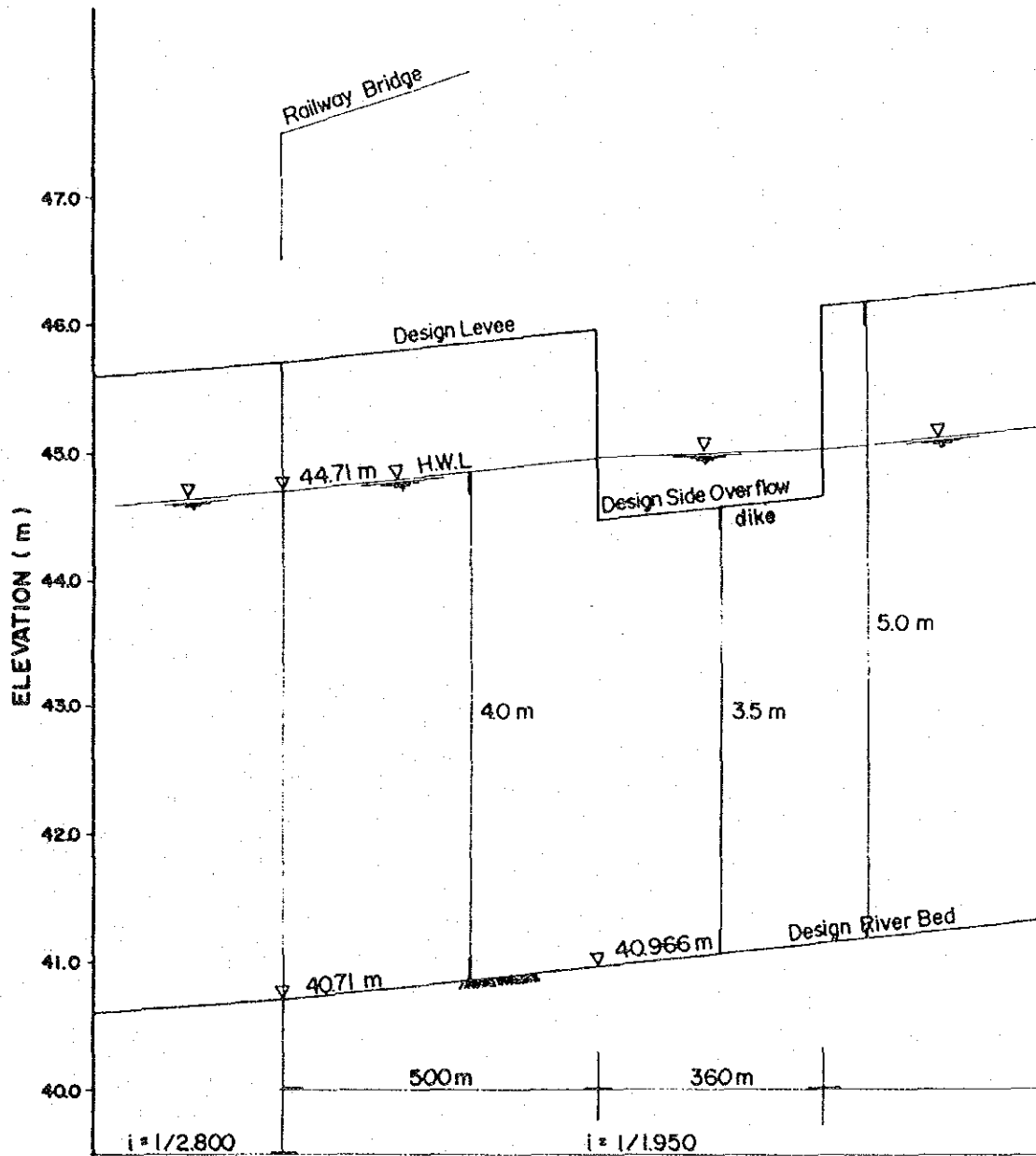
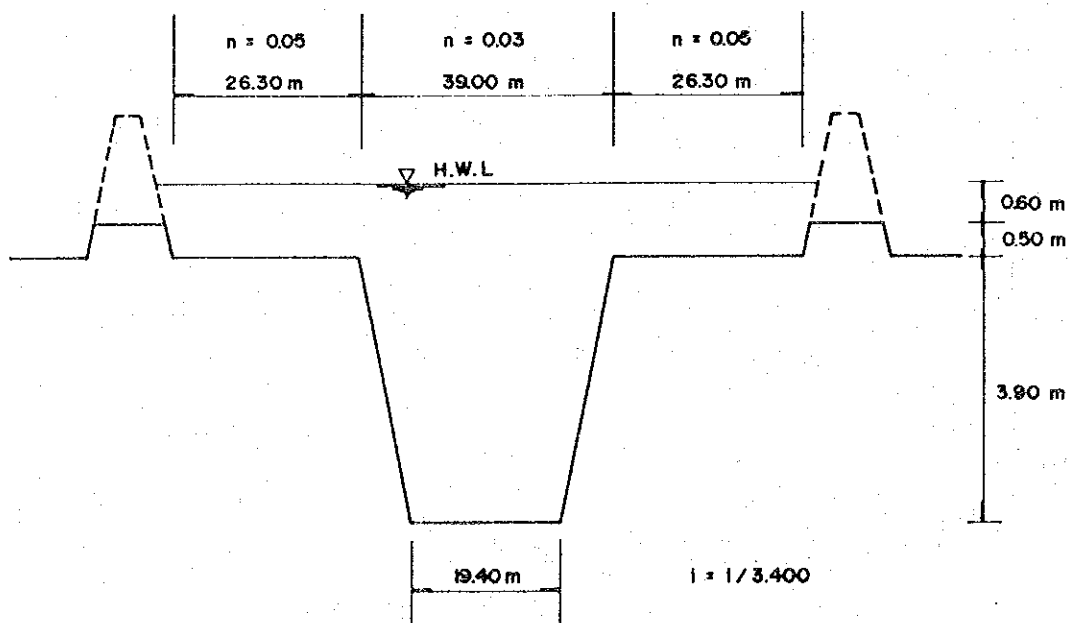
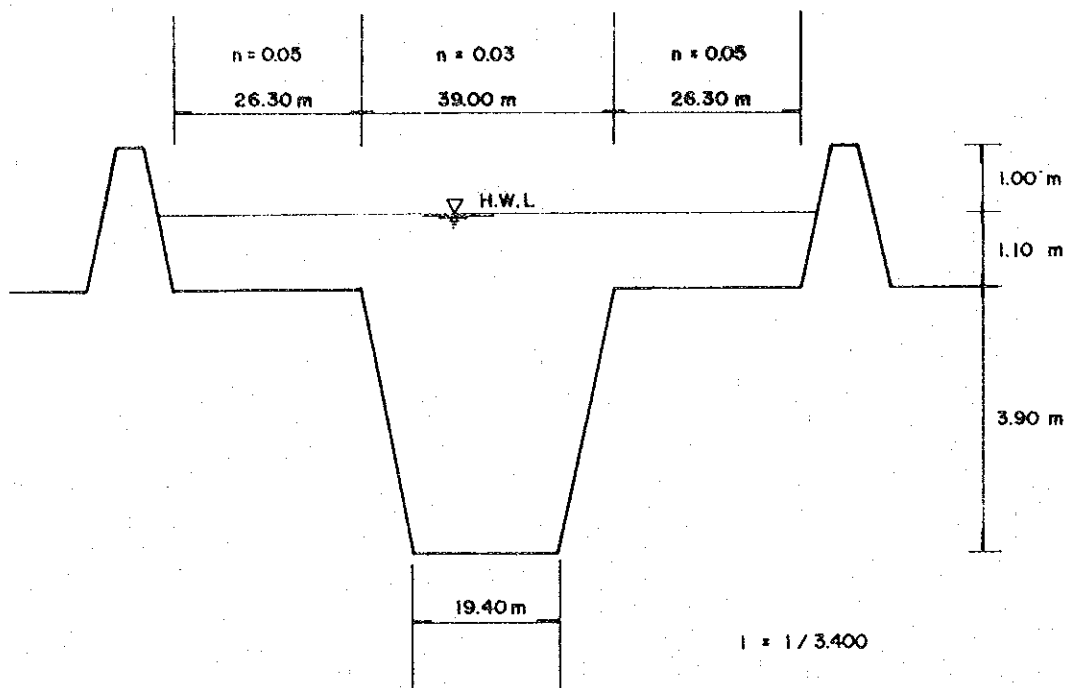


Fig. 4.3.2 LONGITUDINAL PROFILE OF WIDAS RIVER AT ULO RETARDING BASIN (2/3)



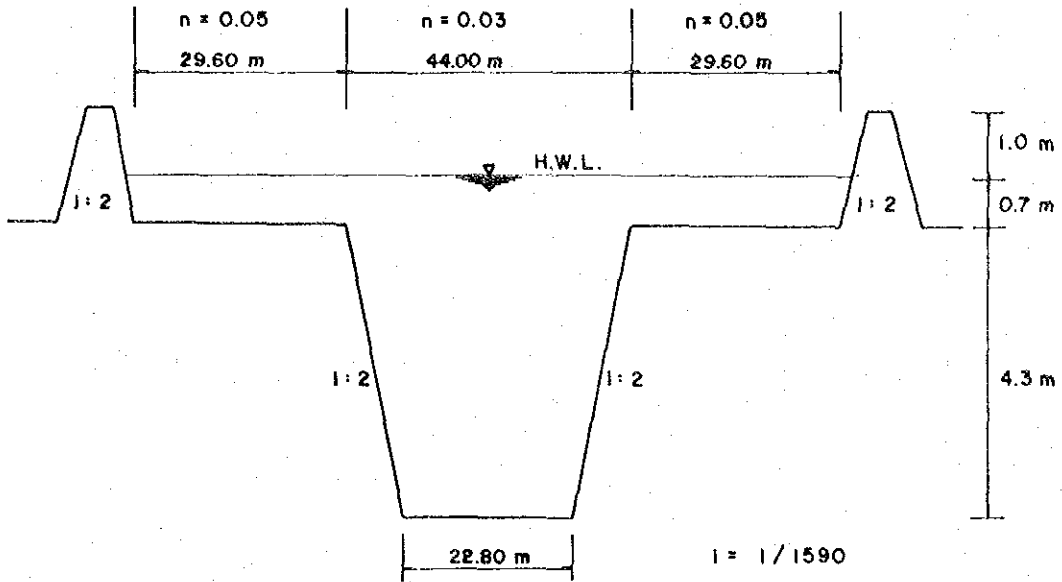
**Fig. 4.3.2 LONGITUDINAL PROFILE OF KEDUNGSOKO RIVER AT KEDUNGSOKO RETARDING BASIN ( 3/3 )**



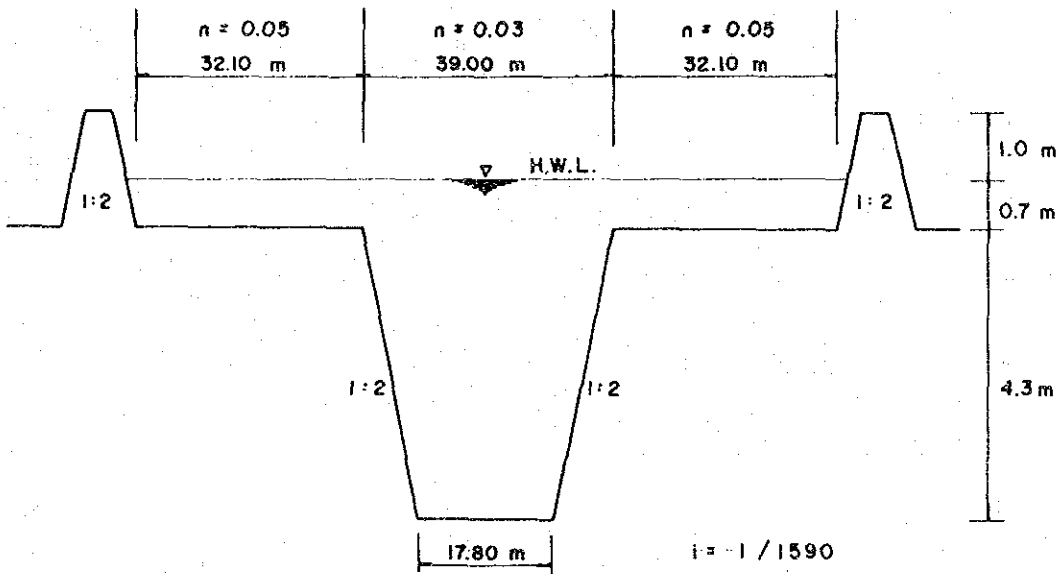
$n$  : Manning's coefficient of roughness  
 $i$  : Slope of design river bed

**Fig. 4.3.3 DESIGN CROSS - SECTION OF WIDAS RIVER IN THE REACH OF WIDAS RETARDING BASIN (1/3)**

1. Cross-section for 25-yr probable flood



2. Cross-section for 10-yr probable flood

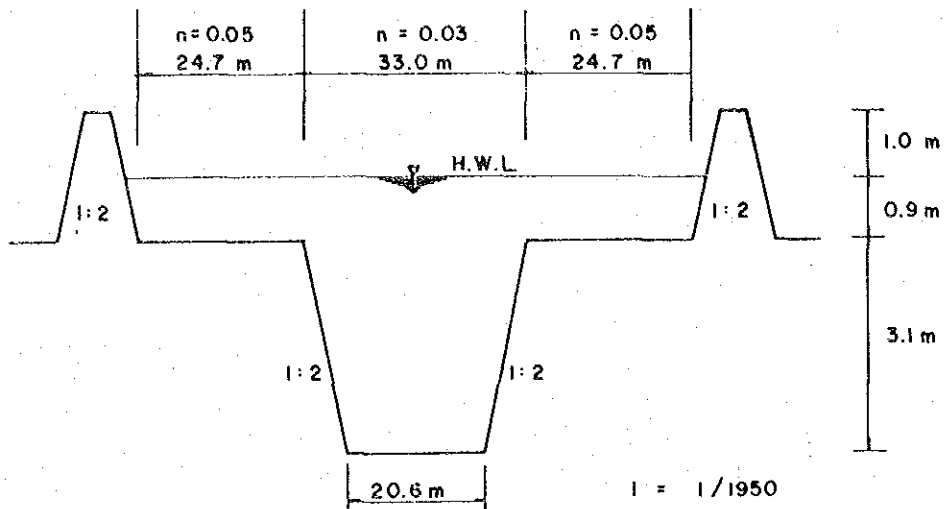


$n$  : Manning coefficient of roughness

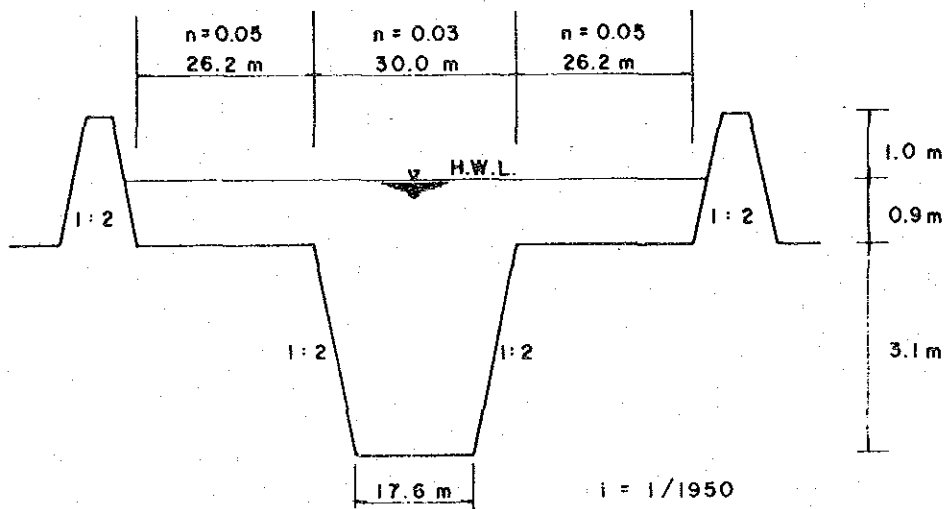
$i$  : Slope of design river bed

Fig. 4.3.3 DESIGN CROSS-SECTION OF WIDAS RIVER  
DOWNSTREAM OF ULO RETARDING BASIN (2/3)

1. Cross-section for 25-yr probable flood



2. Cross-section for 10-yr probable flood



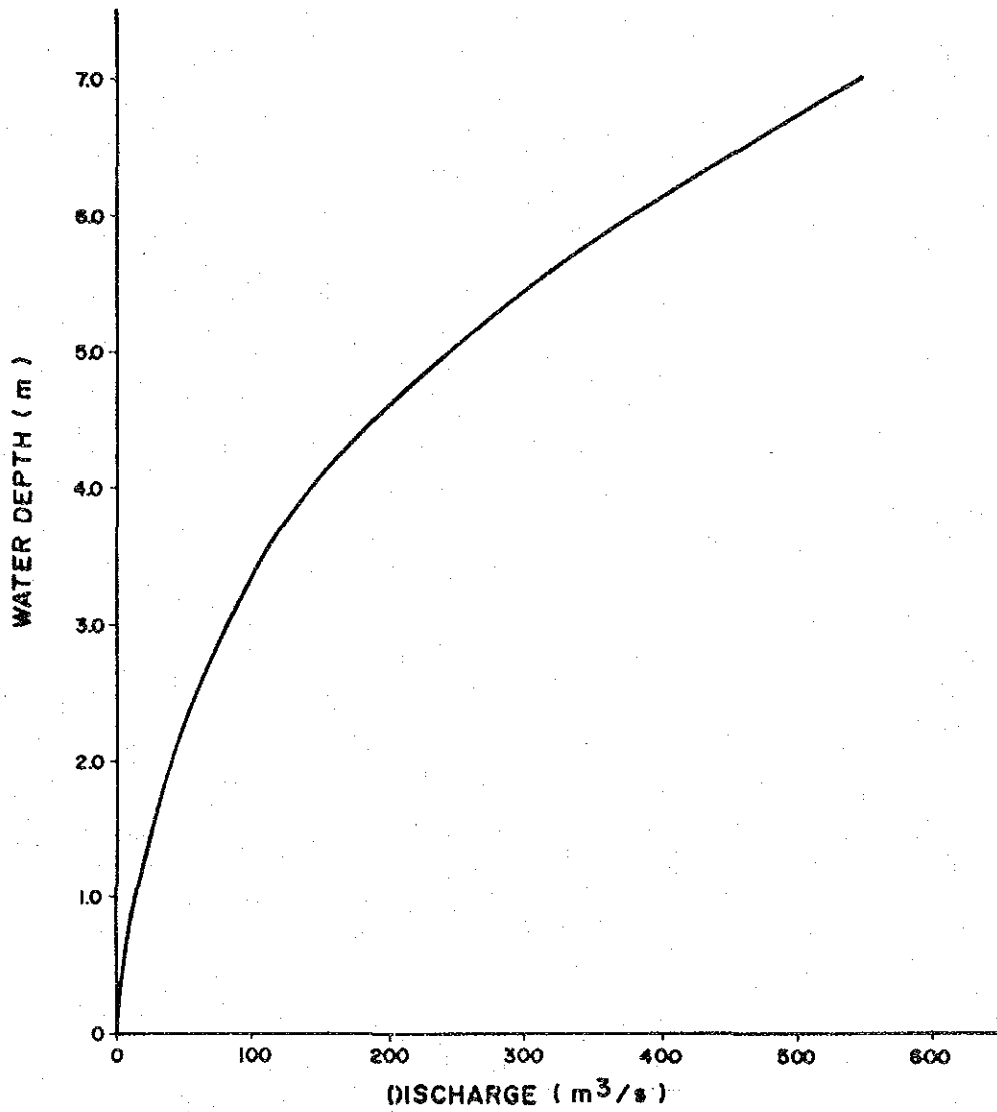
$n$  : Manning's coefficient of roughness

$i$  : Slope of design river bed

Fig. 4.3.3

DESIGN CROSS-SECTION OF KEDUNGSOKO RIVER  
DOWNSTREAM OF KEDUNGSOKO RETARDING BASIN (3/3)





**Fig. 4.3.4 STAGE DISCHARGE RELATION OF WIDAS RIVER DOWNSTREAM OF WIDAS RETARDING BASIN (1/3)**

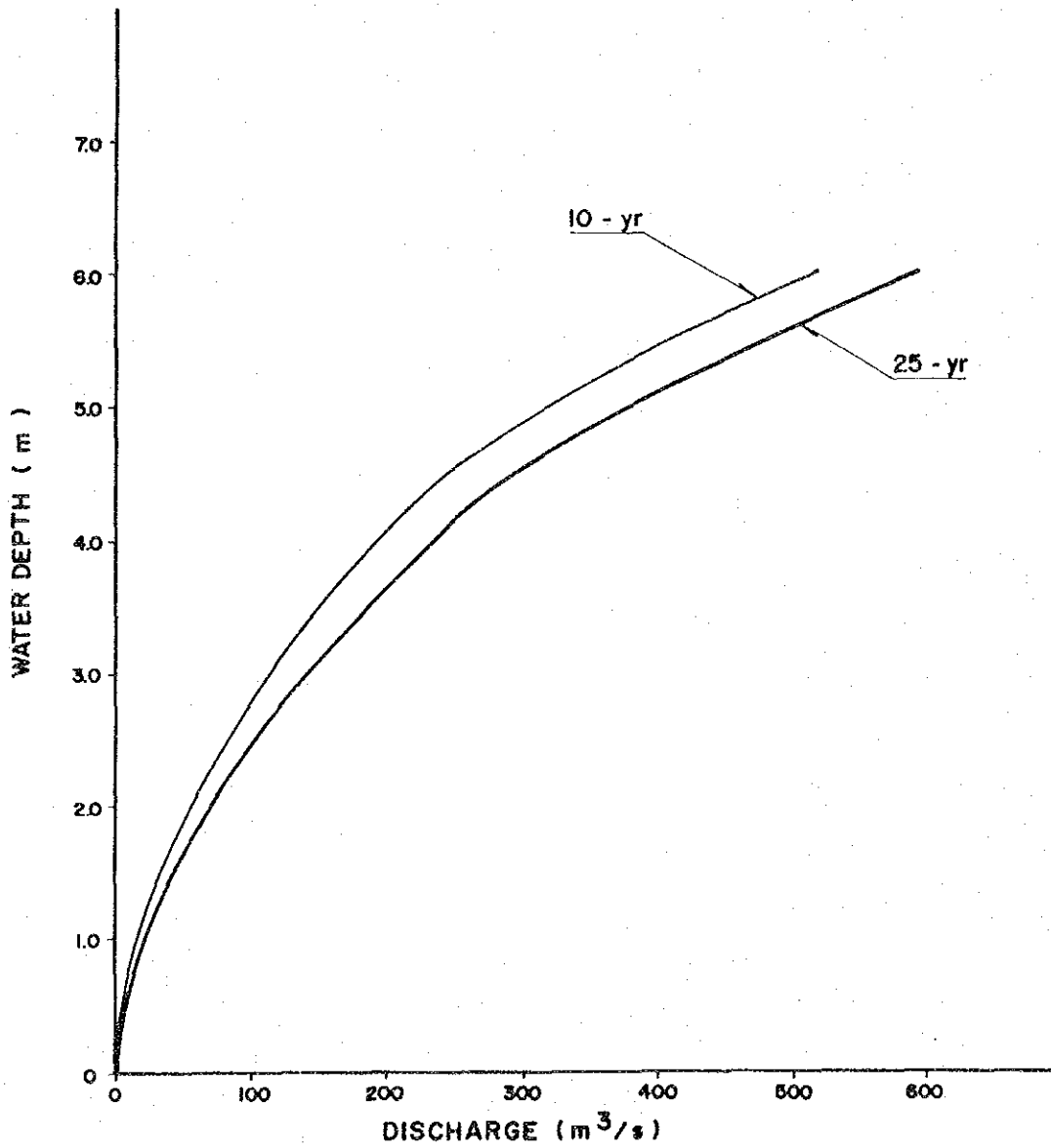
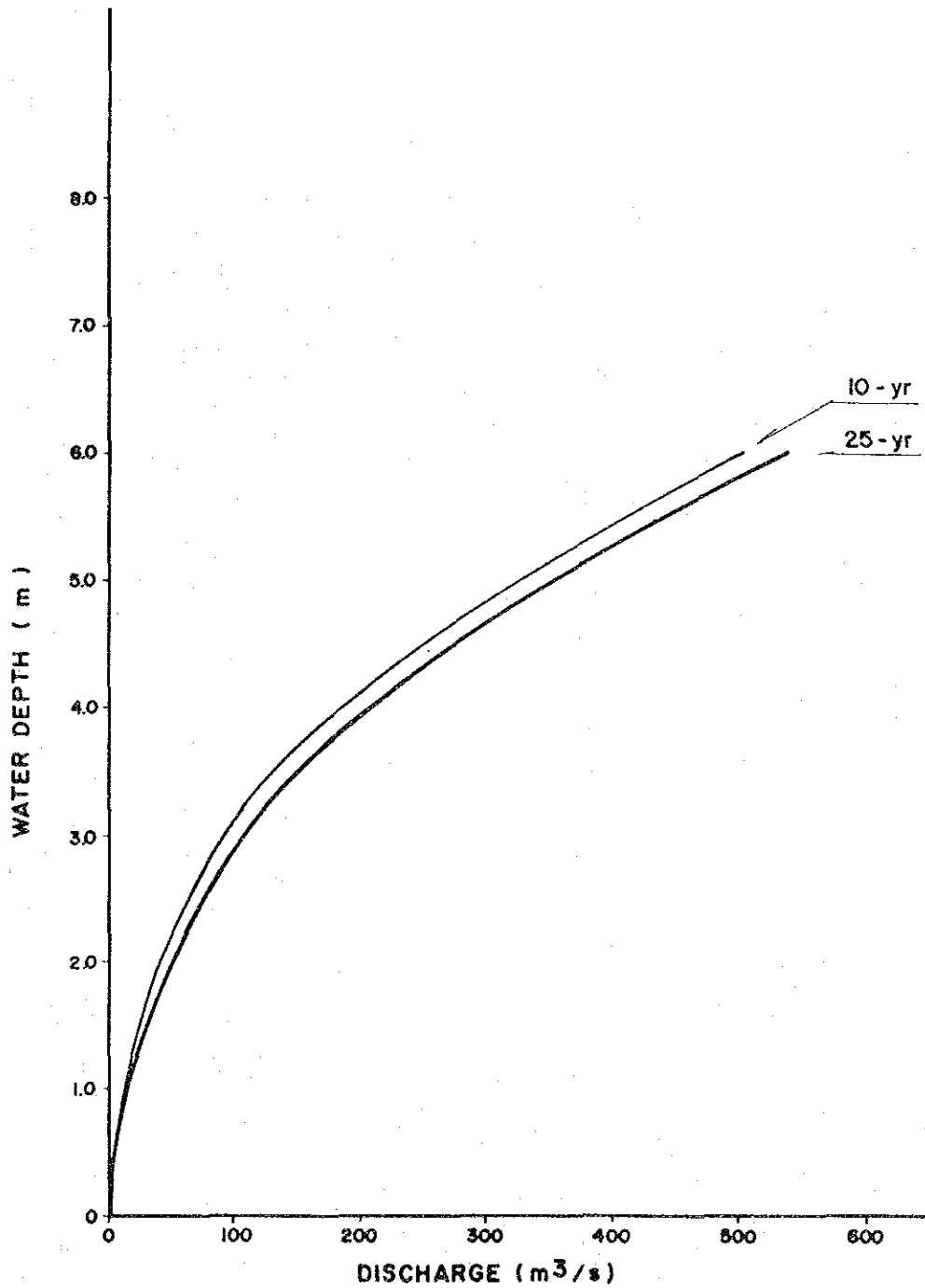


Fig. 4.3.4 STAGE DISCHARGE RELATION OF WIDAS RIVER  
DOWNSTREAM ULO RETARDING BASIN (2/3)



**Fig. 4.3.4 STAGE DISCHARGE RELATION OF KEDUNGSOKO RIVER DOWNSTREAM OF KEDUNGSOKO RETARDING BASIN (3/3)**

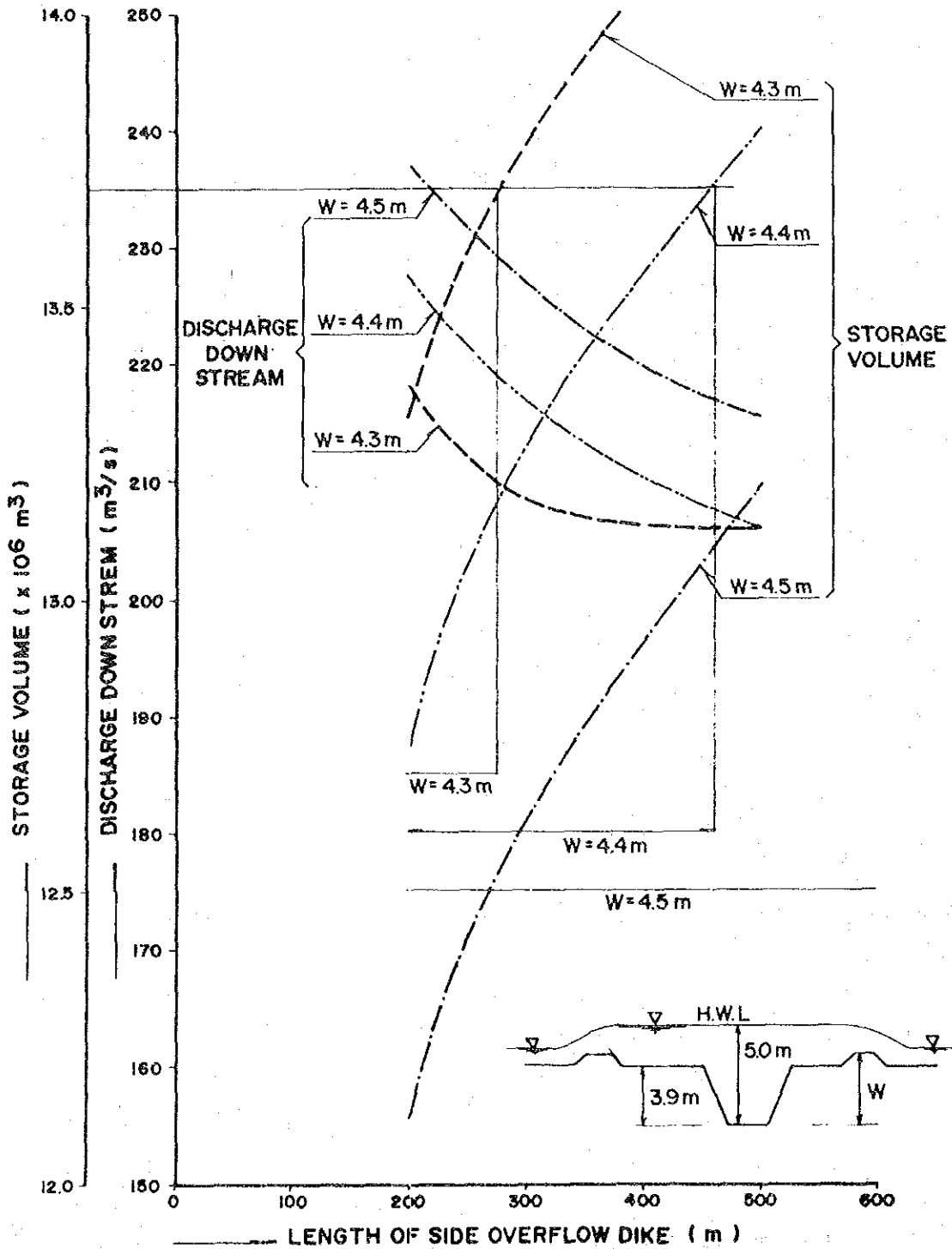


Fig. 4.3.5 FUNCTION OF SIDE OVERFLOW DIKE OF WIDAS RETARDING BASIN ( 1/3 )

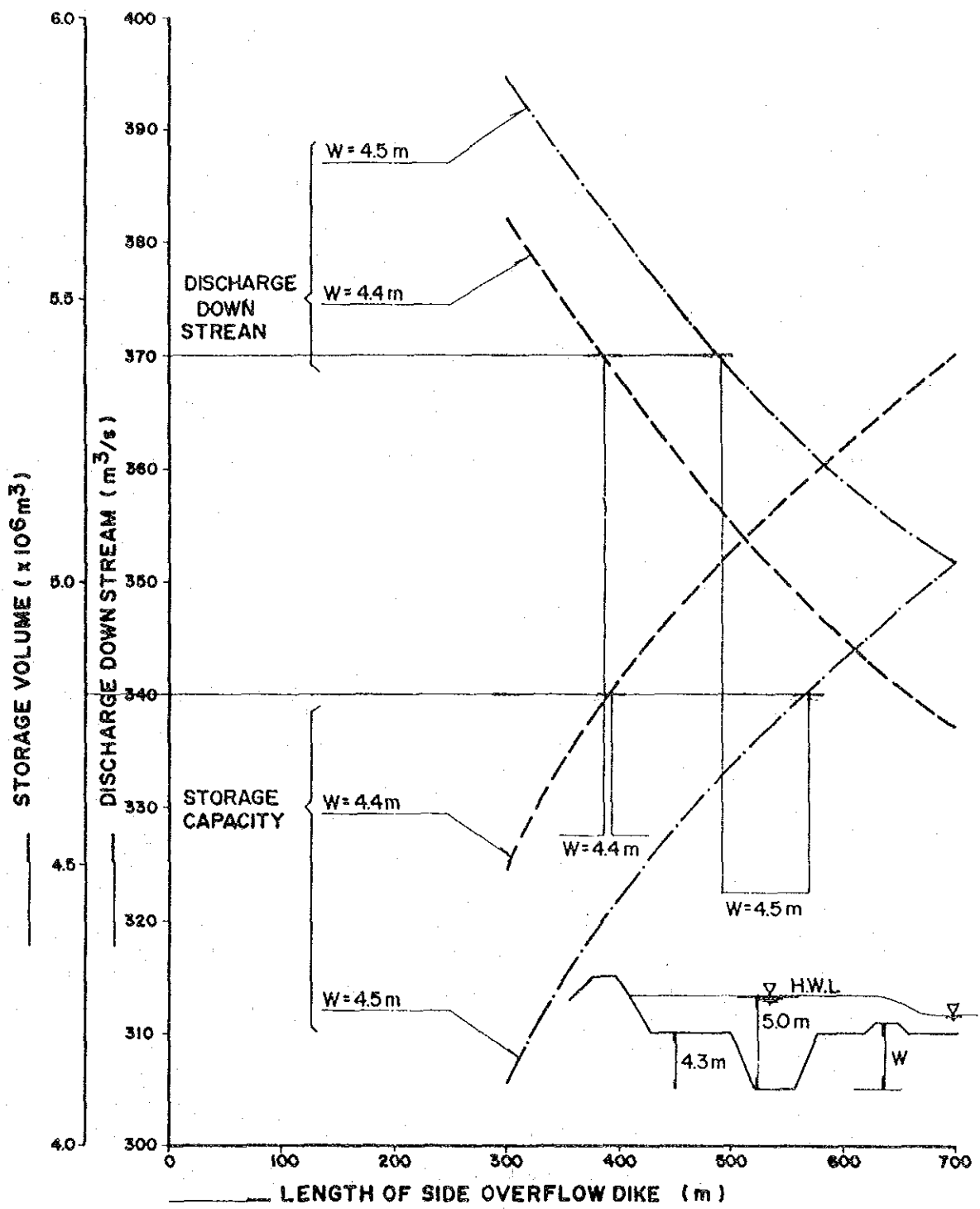


Fig. 4.3.5 FUNCTION OF SIDE OVERFLOW DIKE OF ULO RETARDING BASIN (2/3)

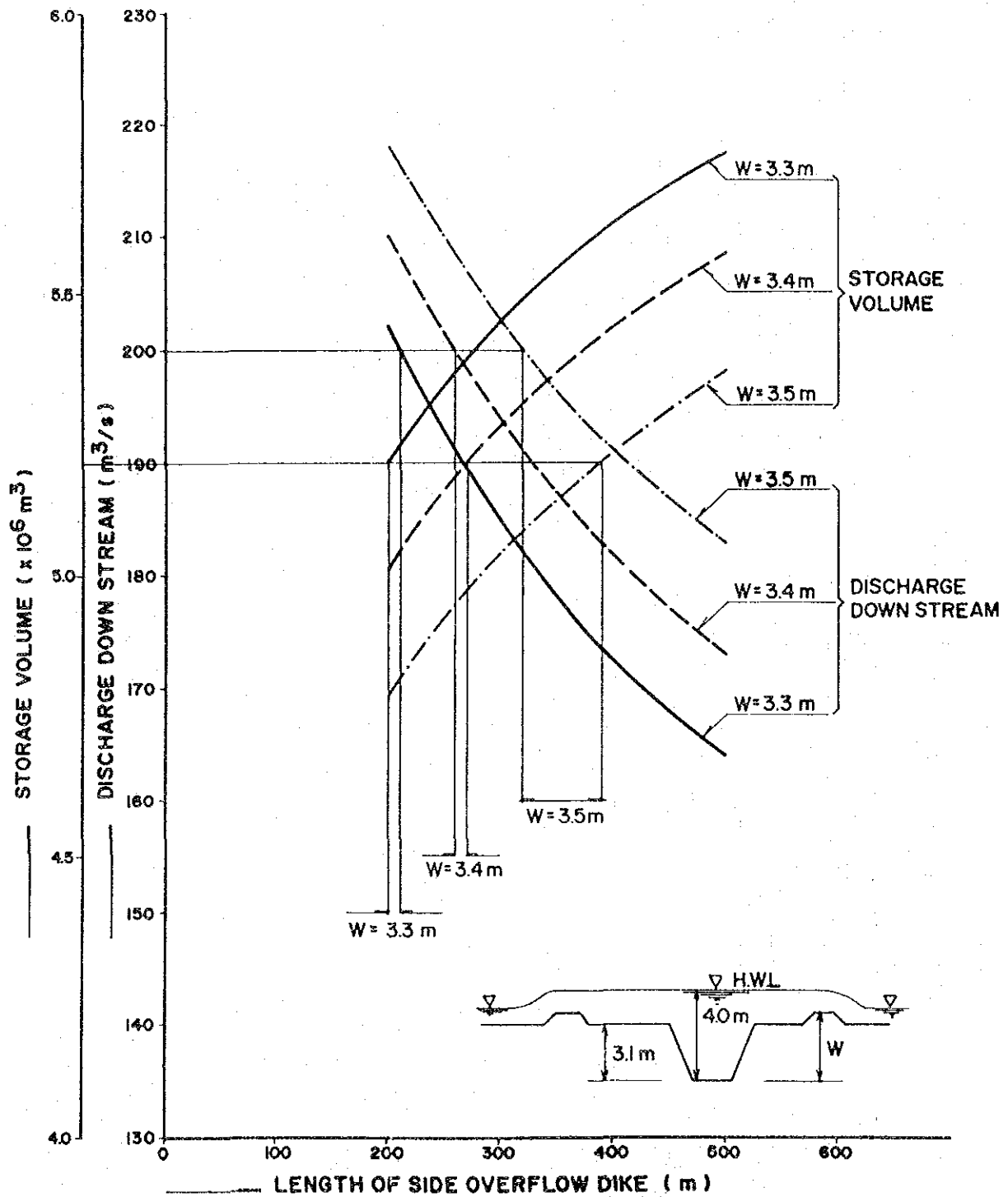
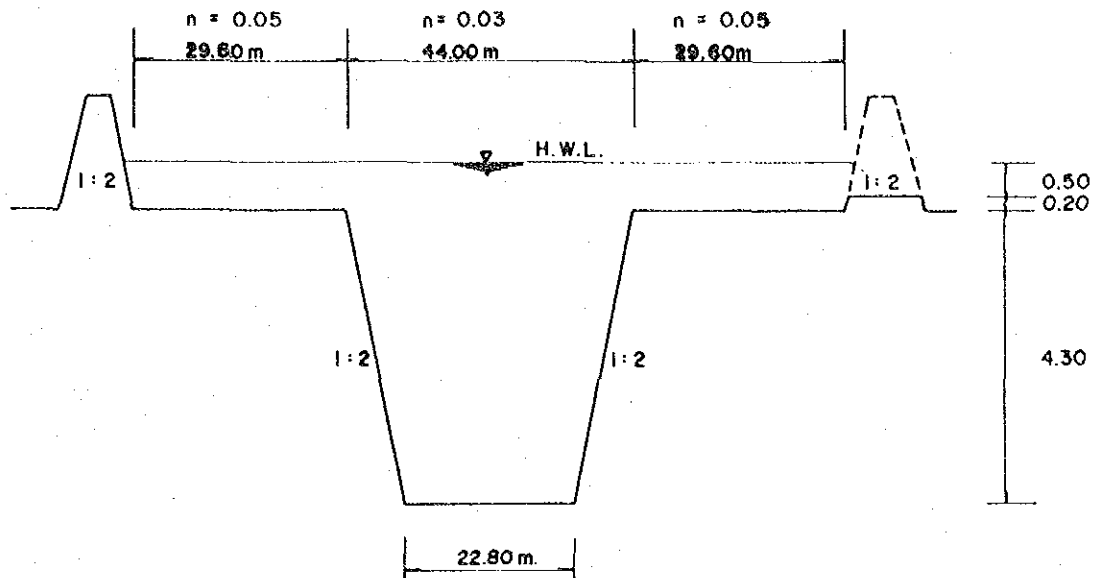


Fig. 4.3.5 FUNCTION OF SIDE OVERFLOW DIKE OF KEDUNGSOKO RETARDING BASIN ( 3/3 )

1. Cross-section for 25-yr probable flood



2. Cross-section for 10-yr probable flood

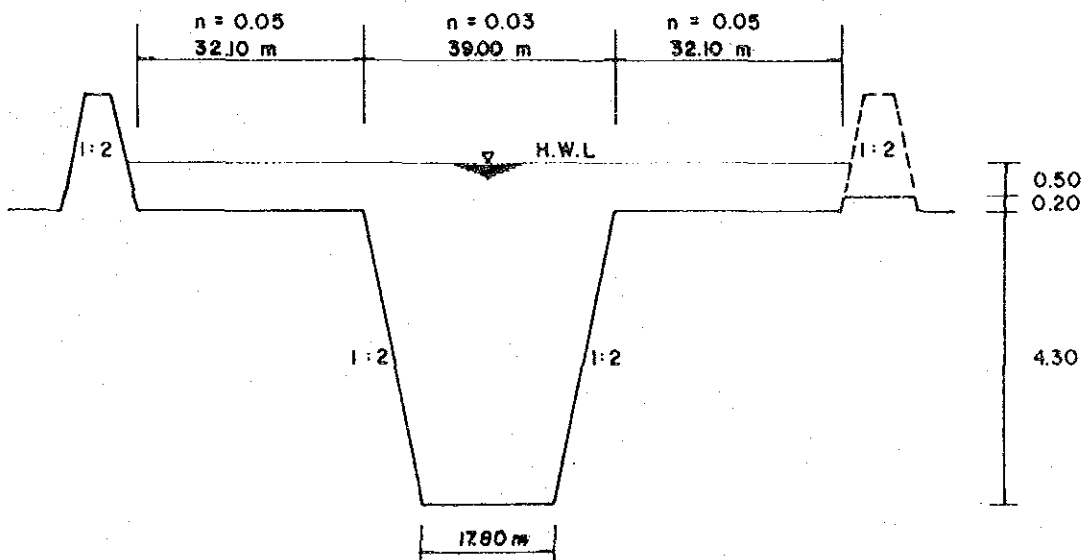
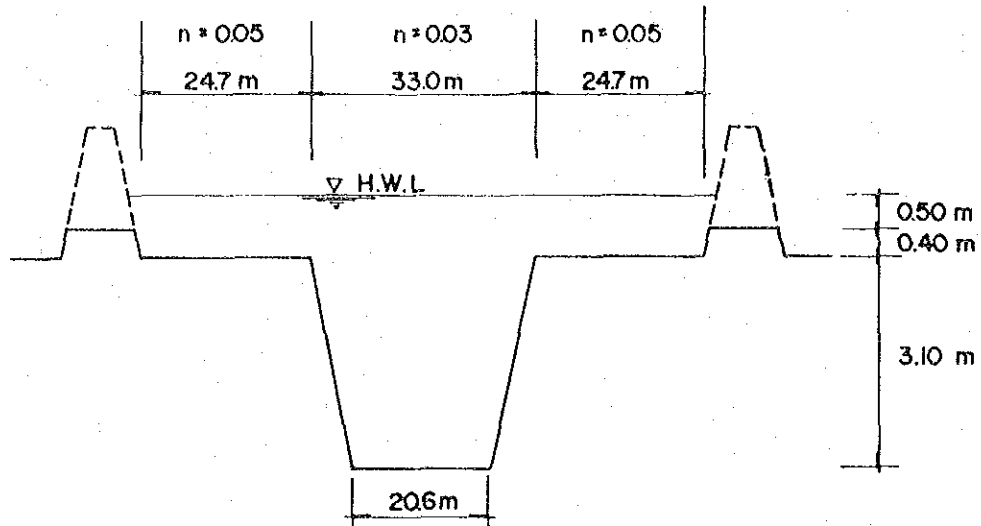
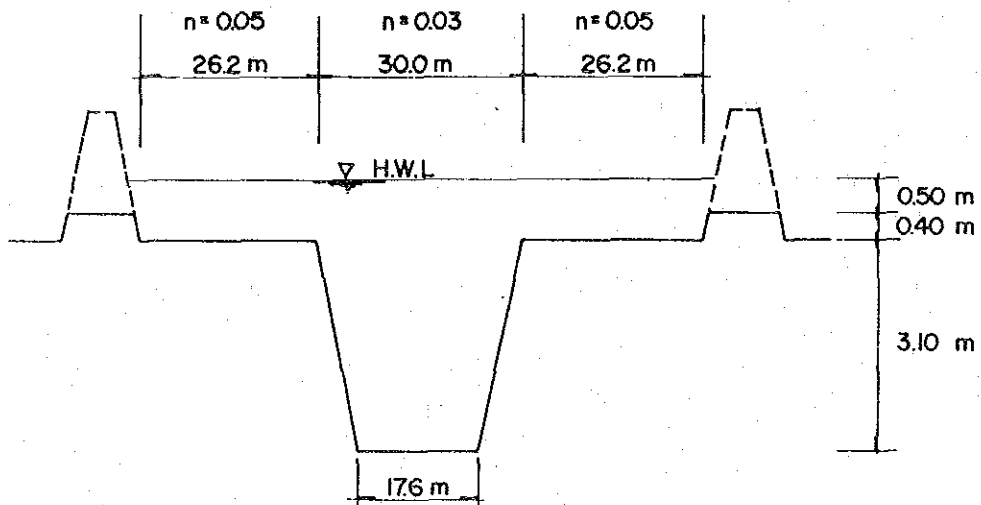


Fig. 4.3.6 DESIGN CROSS-SECTION OF WIDAS RIVER AT SIDE OVERFLOW DIKE OF ULO RETARDING BASIN (1/2)

**1. CROSS SECTION FOR 25 - yr PROBABLE FLOOD**



**2. CROSS SECTION FOR 10 - yr PROBABLE FLOOD**



**Fig. 4.3.6 DESIGN CROSS SECTION OF KEDUNGSOKO RIVER AT SIDE OVERFLOW DIKE OF KEDUNGSOKO RETARDING BASIN ( 2/2 )**



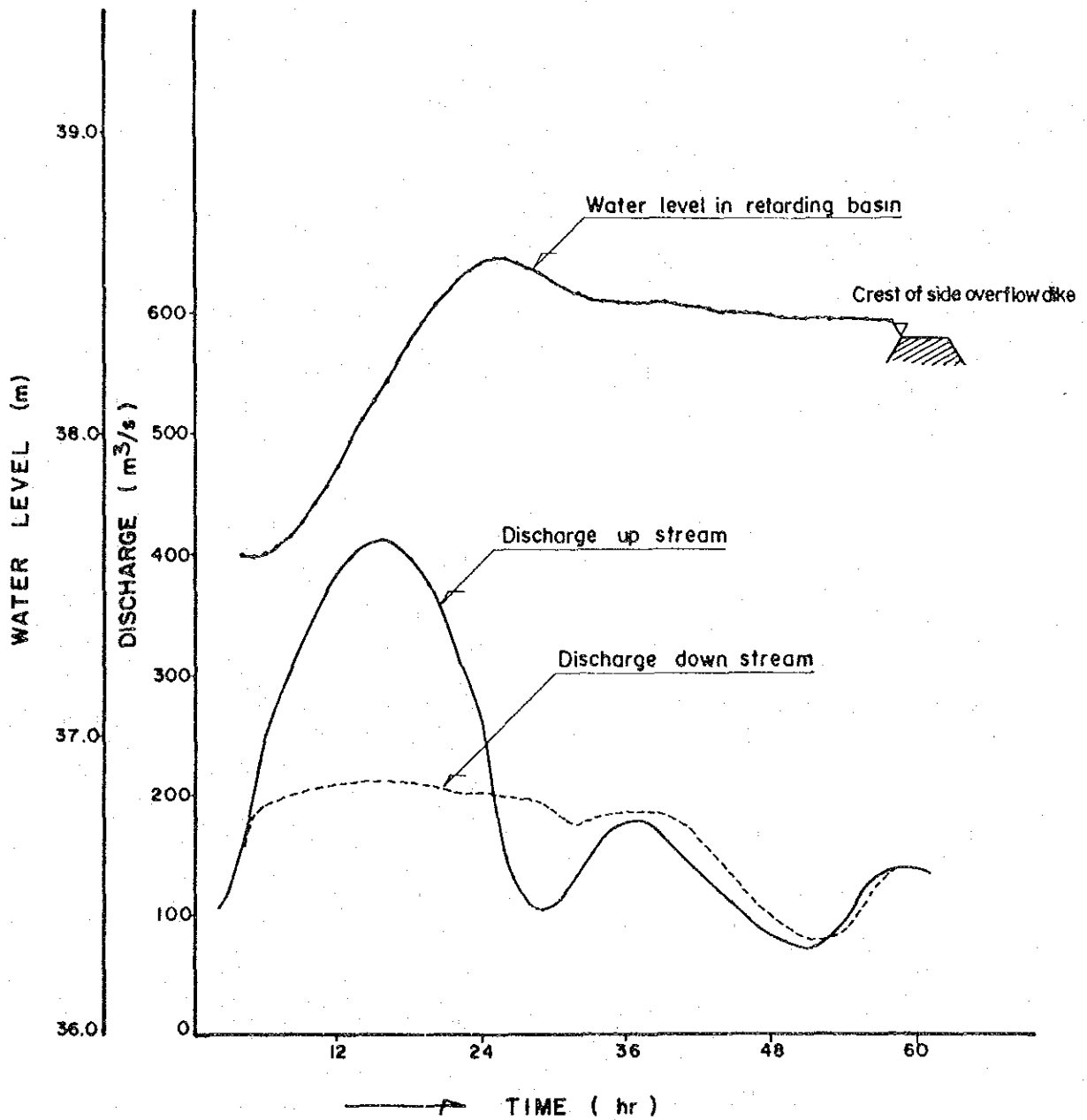


Fig. 4.3.7 FLOOD ROUTING IN THE WIDAS RETARDING BASIN (1/3)

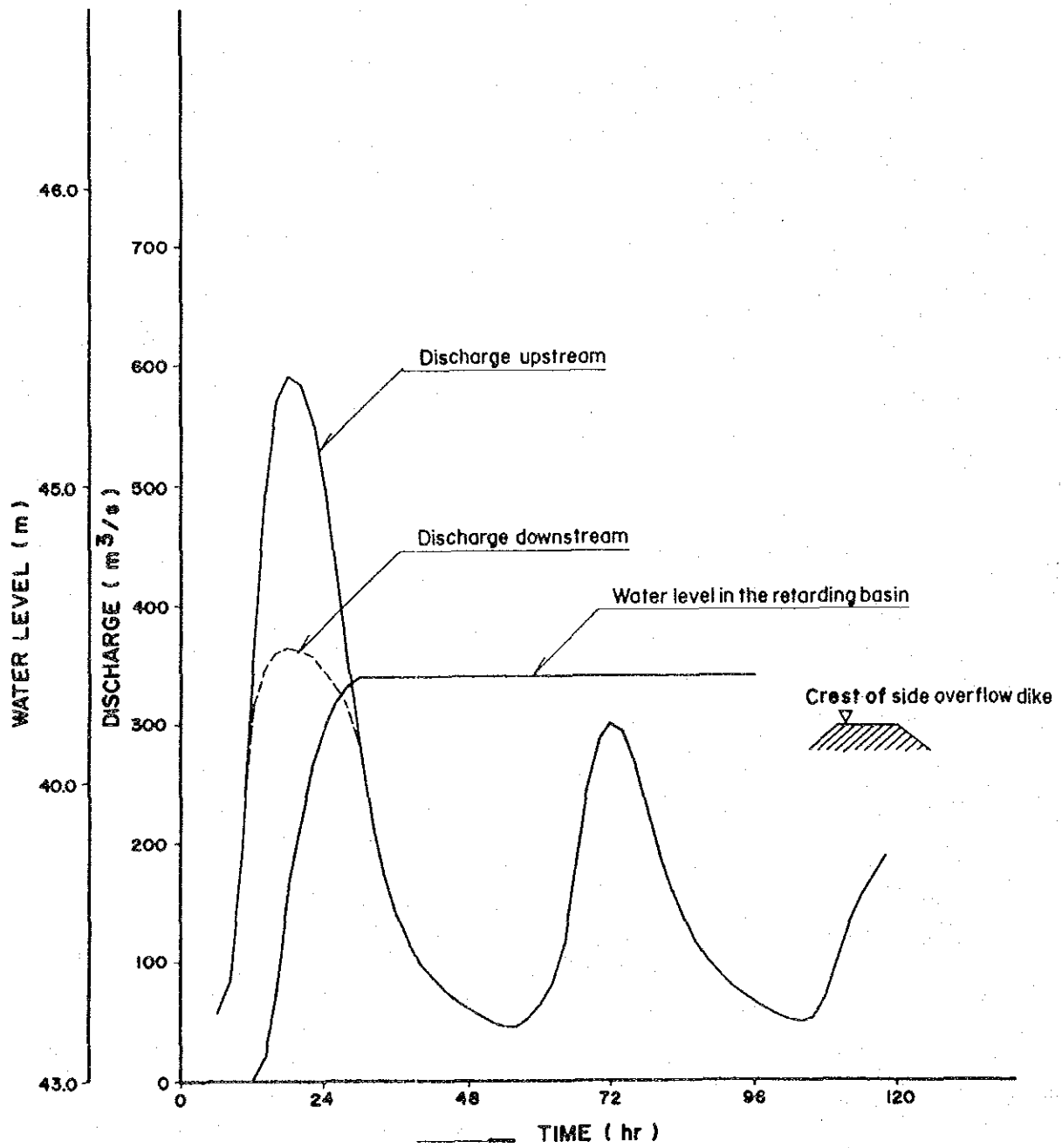


Fig. 4.3.7 FLOOD ROUTING IN THE ULO RETARDING BASIN (2/3)

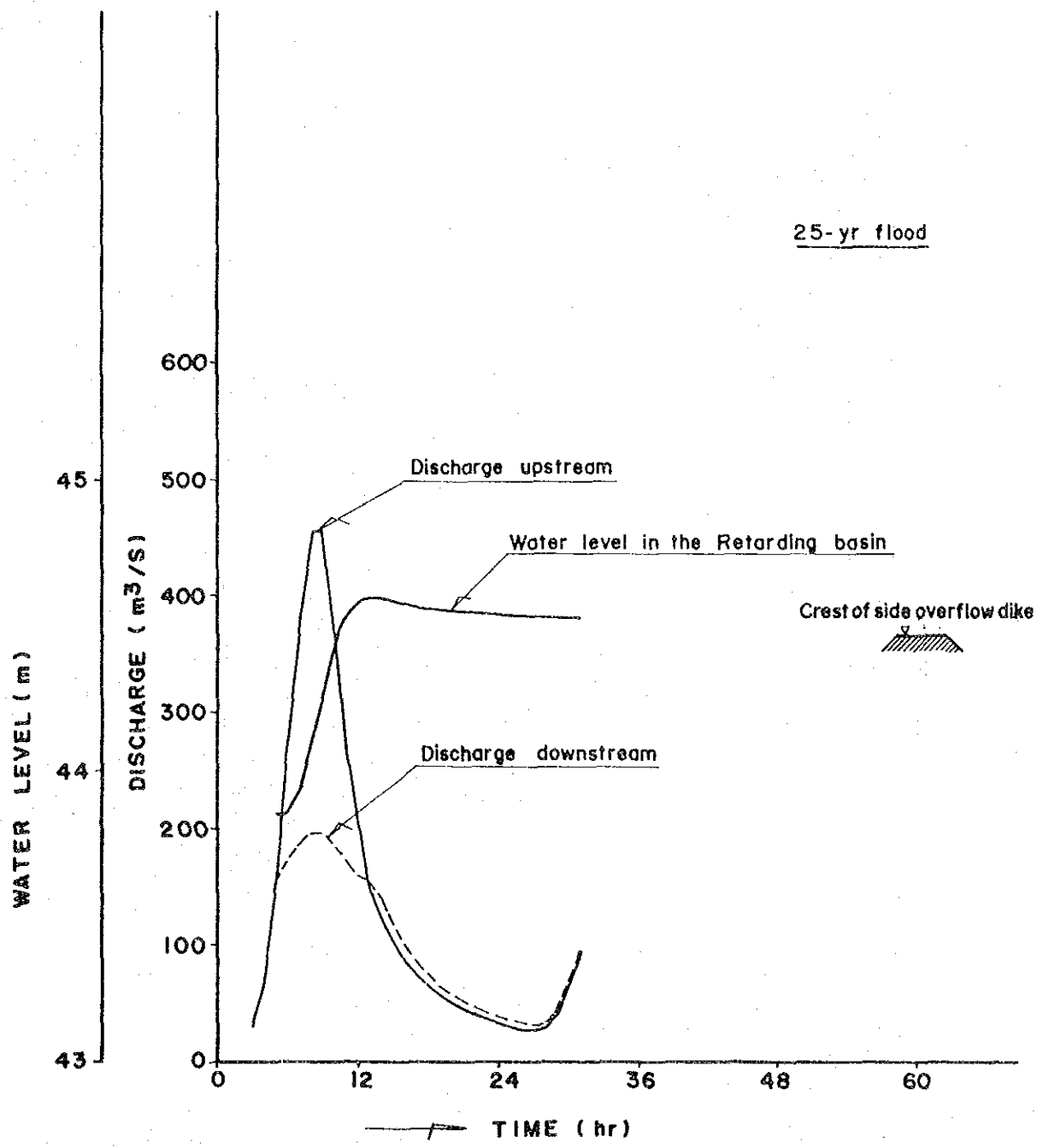


Fig. 4.3.7 FLOOD ROUTING IN THE KEDUNGSOKO RETARDING BASIN ( 3/3 )

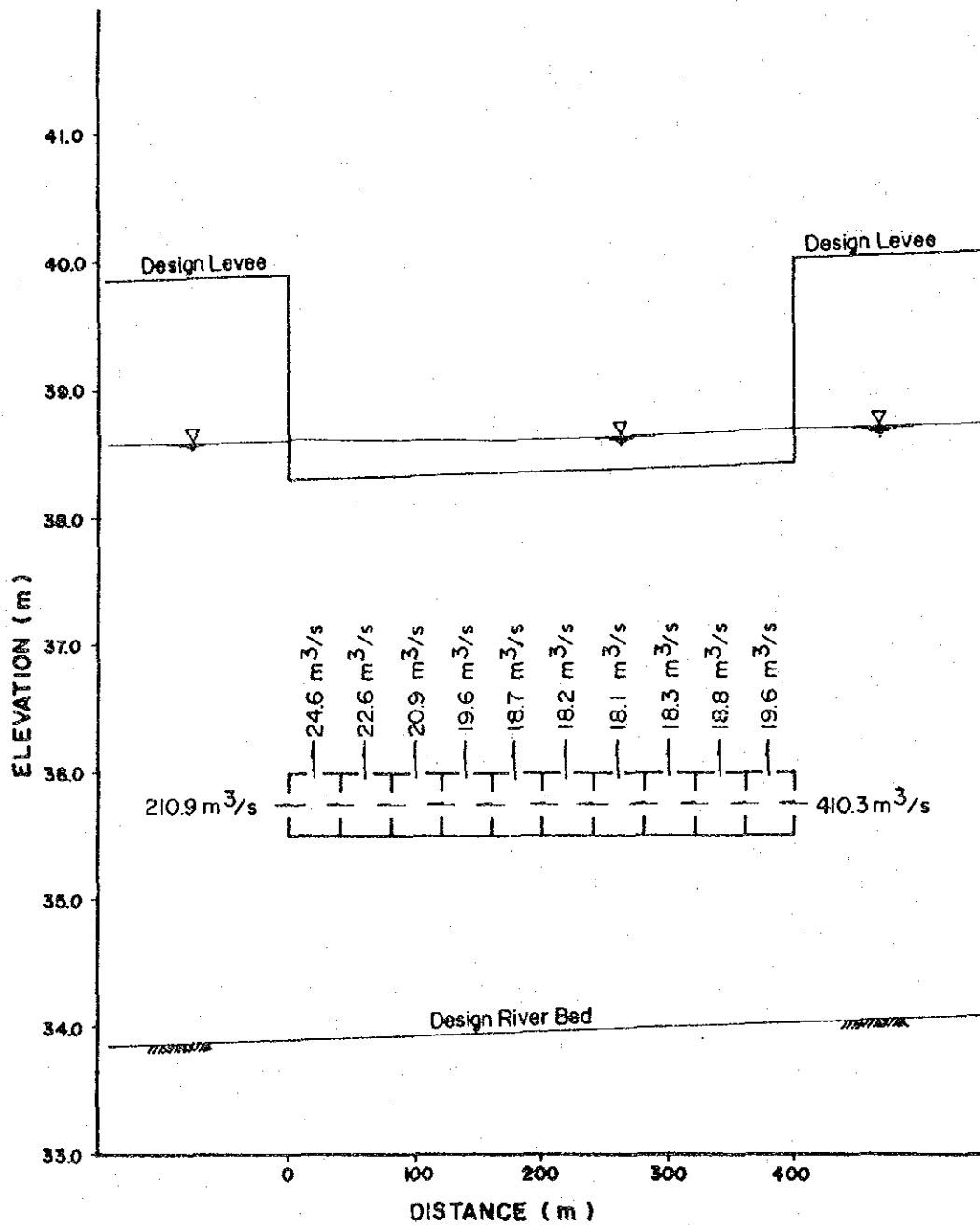
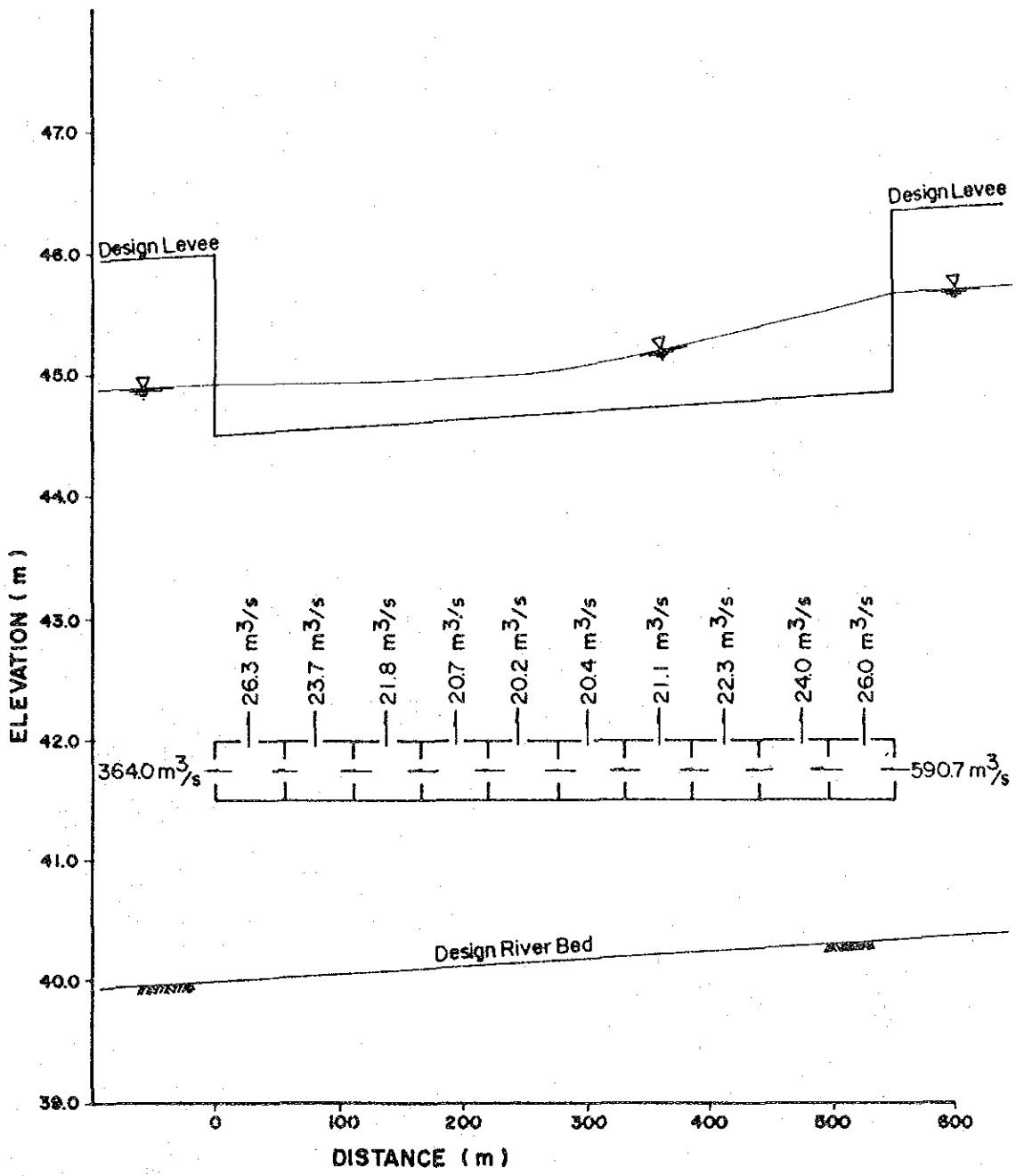


Fig. 4.3.8 WATER LEVEL AND DISCHARGE AT SIDE OVERFLOW DIKE OF WIDAS RETARDING BASIN (1/3)



**Fig. 4.3.8 WATER LEVEL AND DISCHARGE AT SIDE OVERFLOW DIKE OF ULO RETARDING BASIN ( 2/3 )**

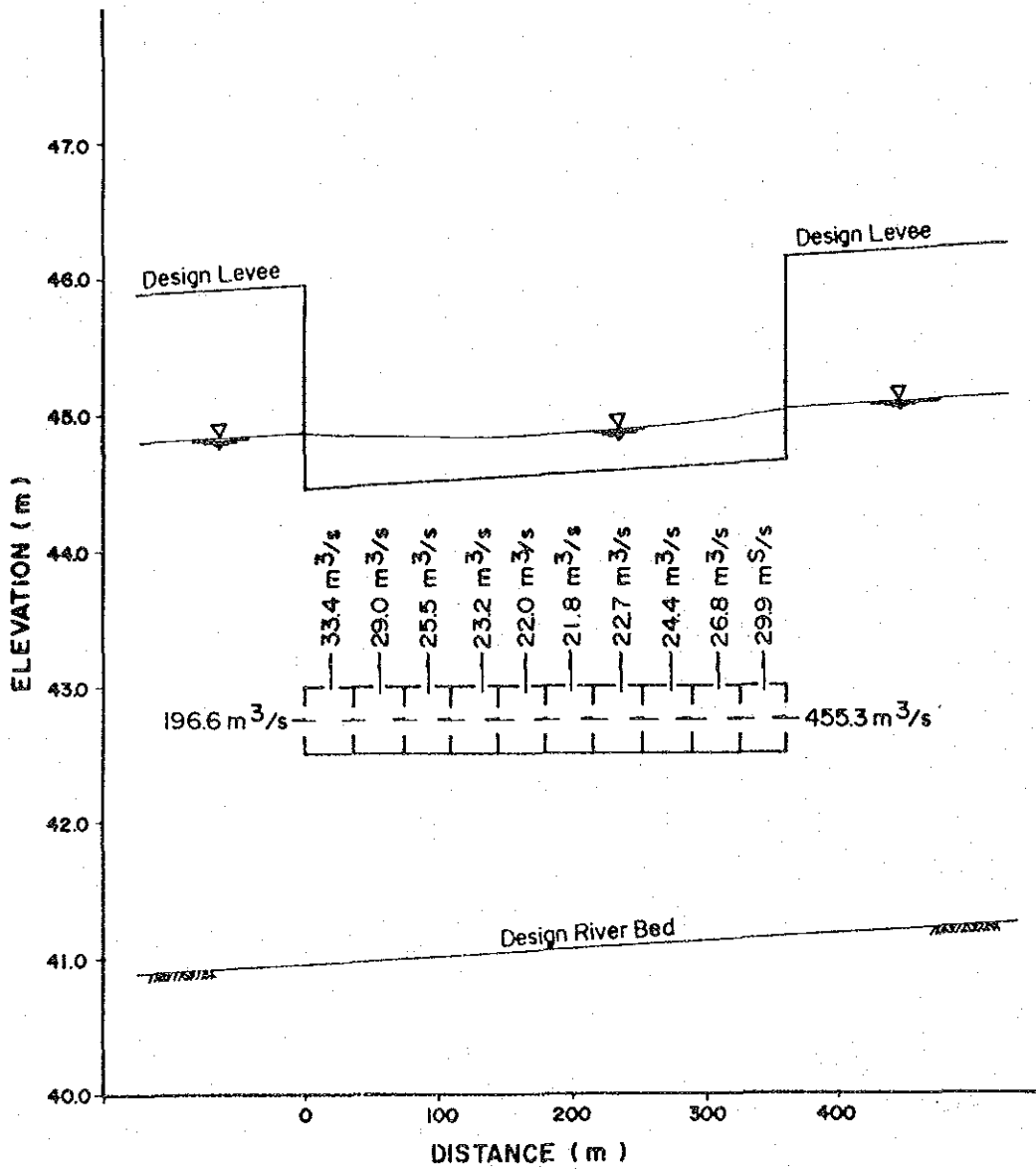
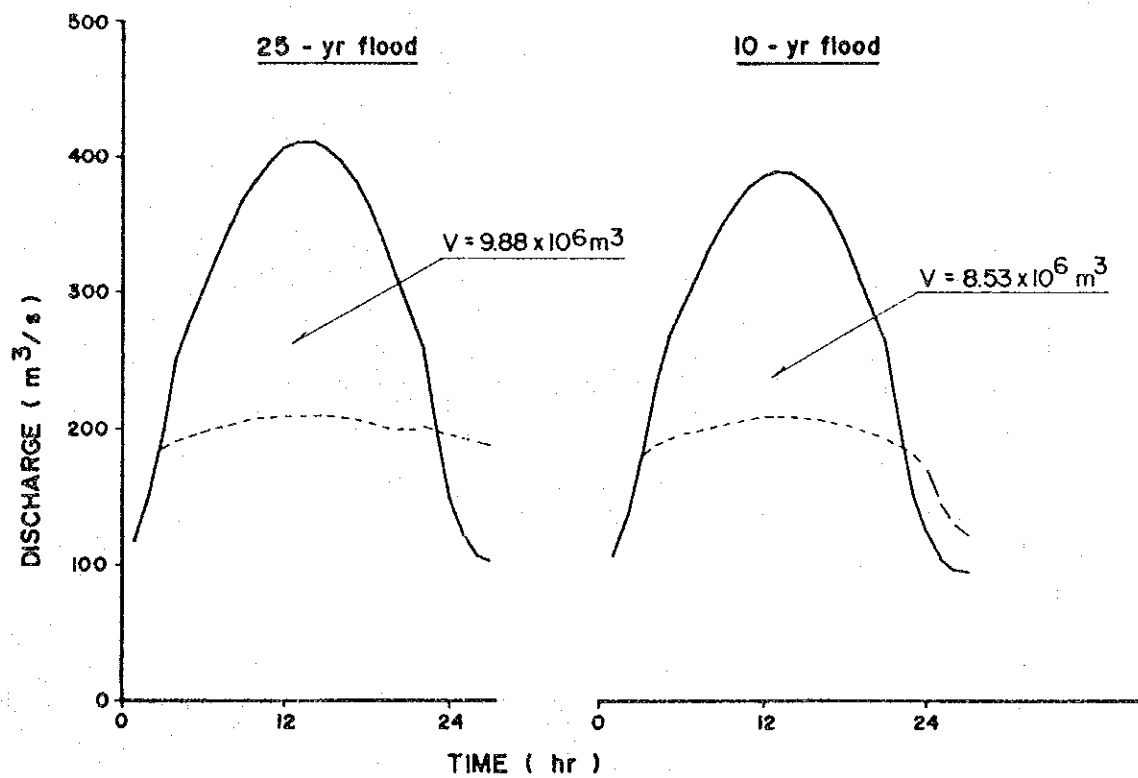
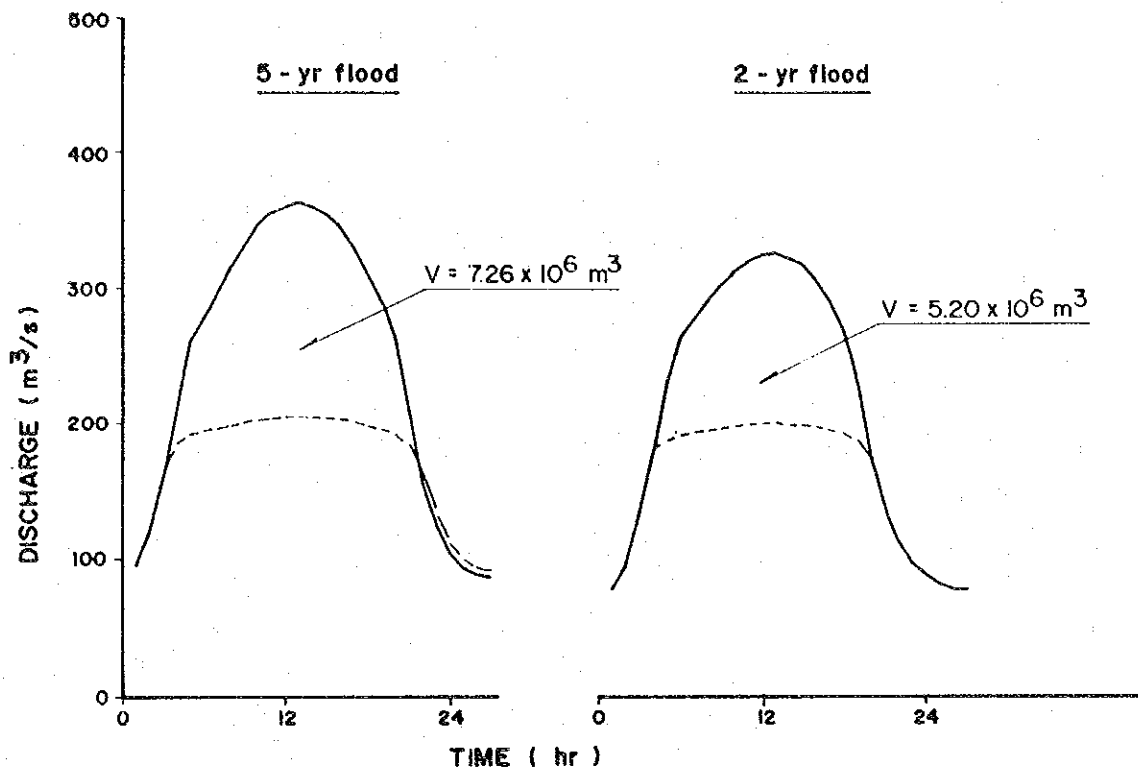
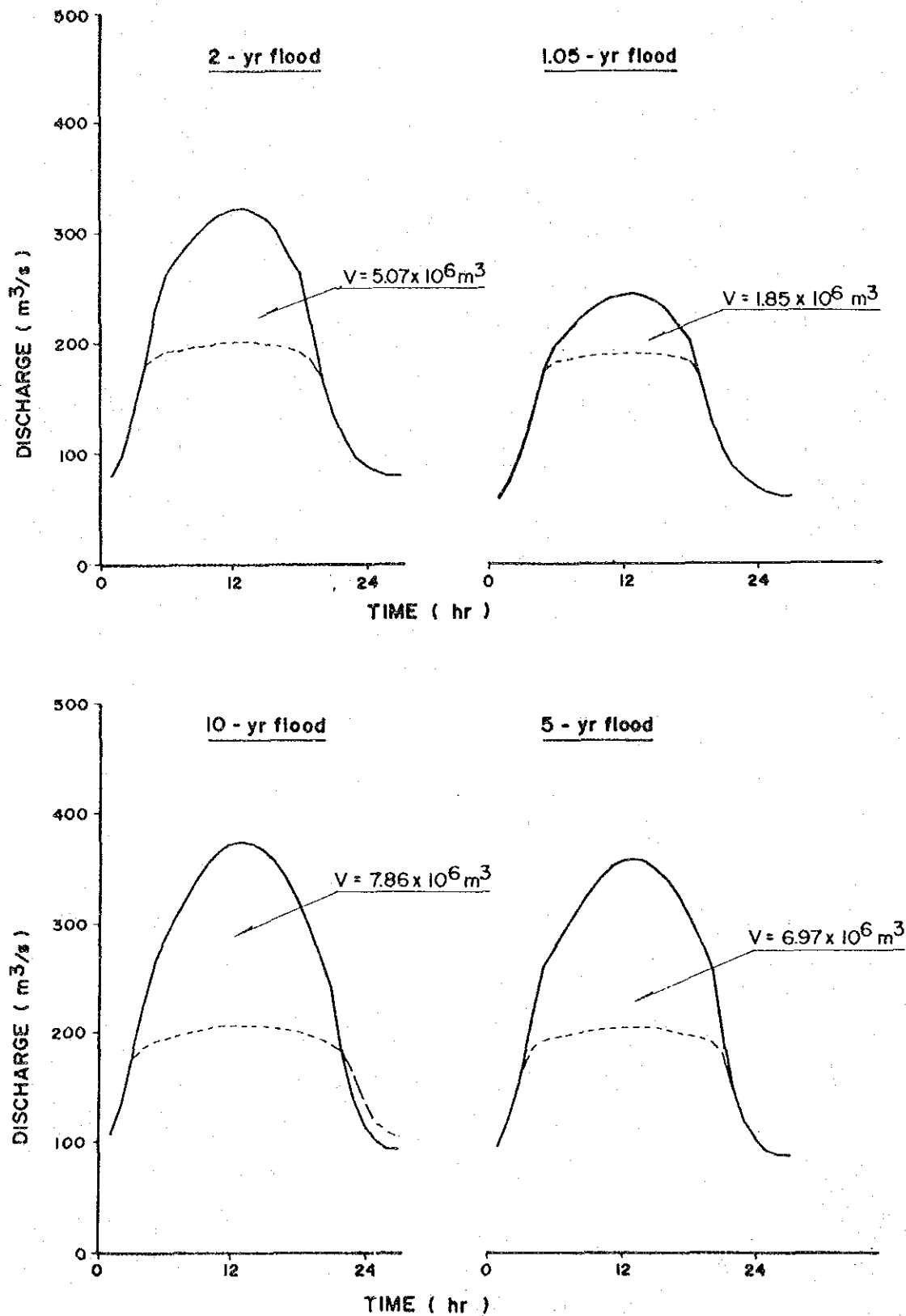


Fig. 4.3.8 WATER LEVEL AND DISCHARGE AT SIDE OVERFLOW DIKE OF KEDUNGSOKO RETARDING BASIN (3/3)

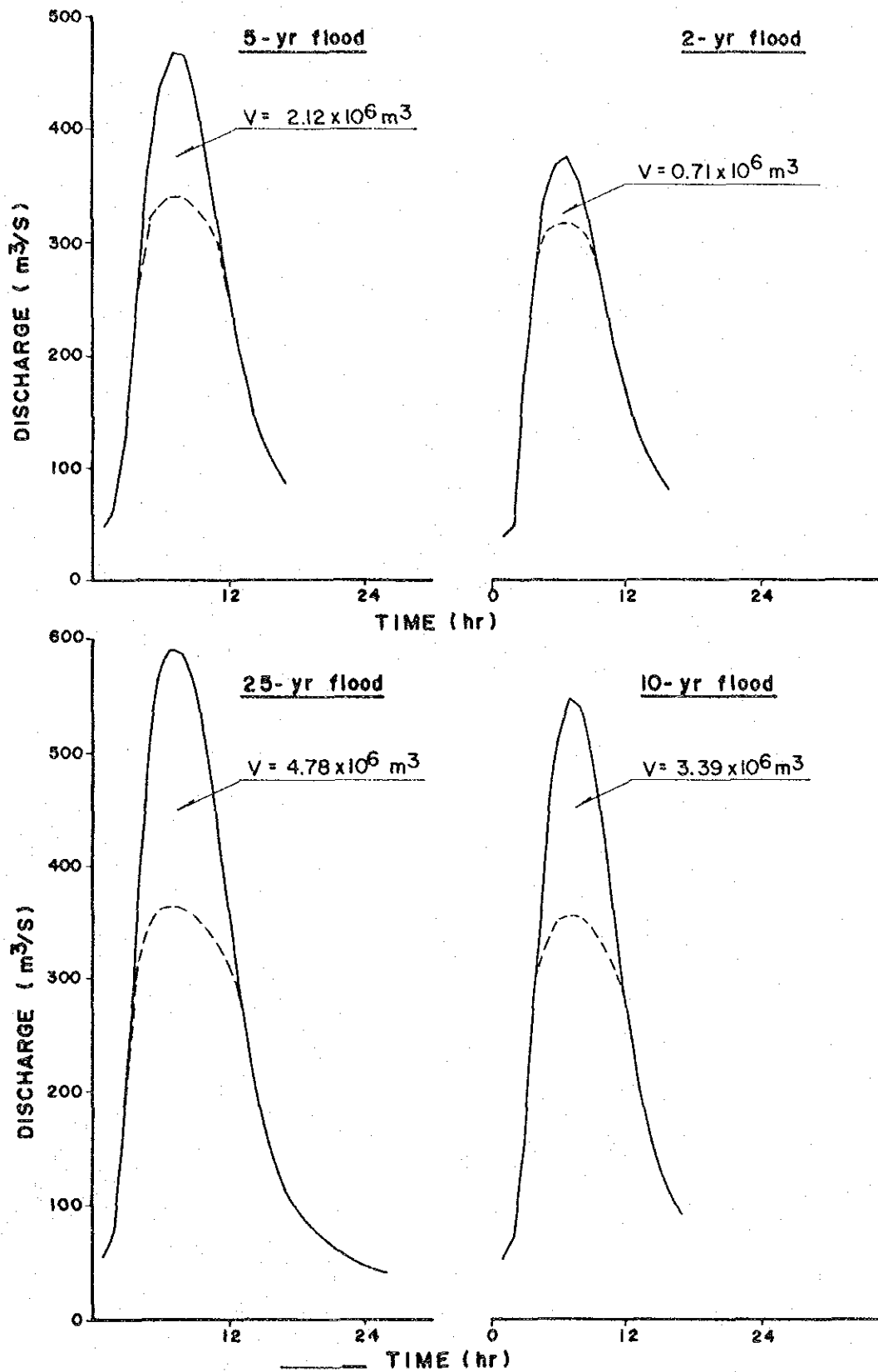


**Fig. 4.3.9 REGULATING EFFECT OF WIDAS RETARDING BASIN  
( River cross - section for 25 - yr probable flood ) (1/6)**



**Fig. 4.3.9 REGULATING EFFECT OF WIDAS RETARDING BASIN  
( River cross - section for 10 - yr probable flood ) ( 2 / 6 )**





**Fig. 4.3.9 REGULATING EFFECT OF ULO RETARDING BASIN**  
 (River cross-section for 25-yr probable flood) (3/6)

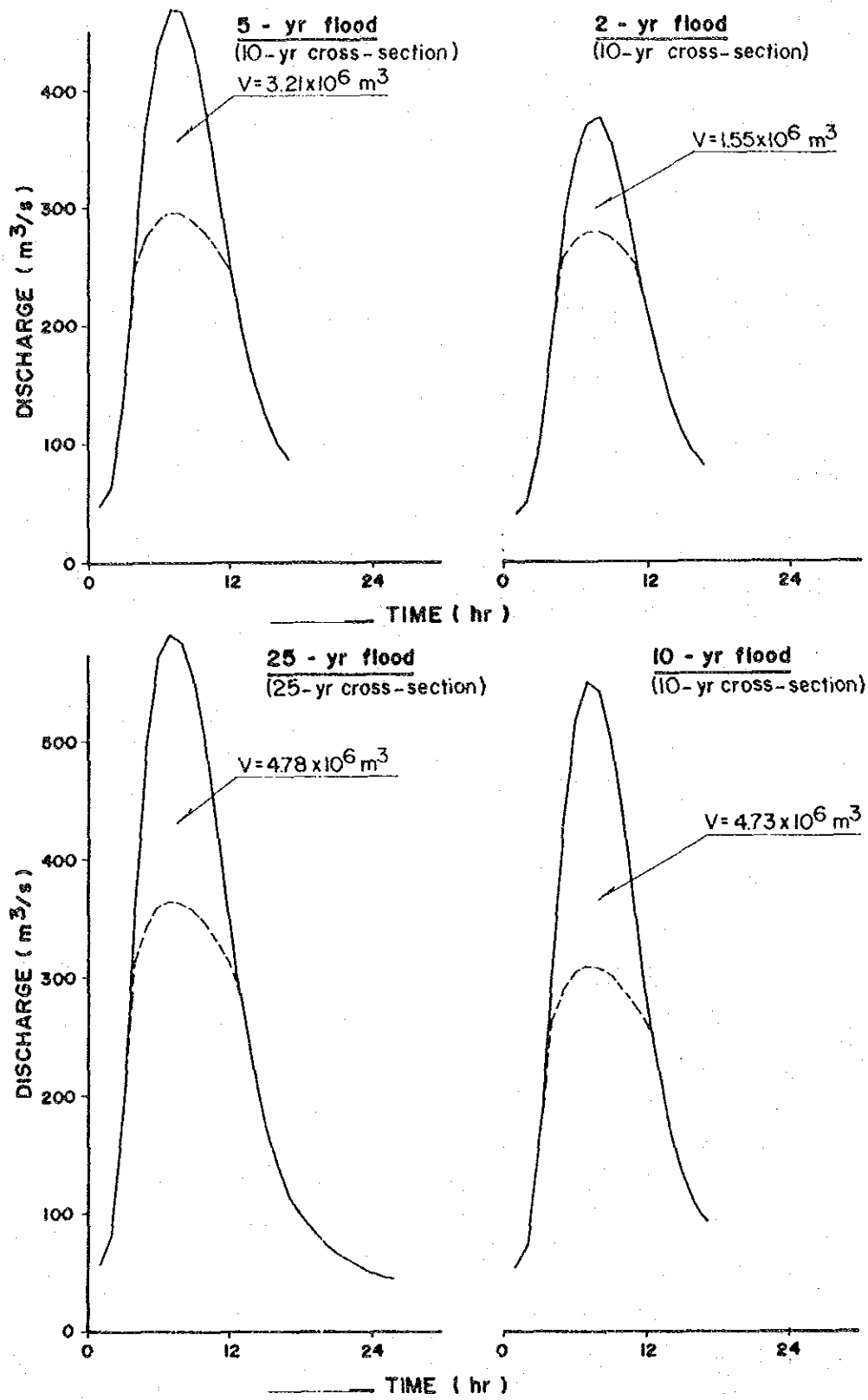


Fig. 4.3.9 REGULATING EFFECT OF ULO RETARDING BASIN  
( River cross - section for 10 - yr probable flood ) ( 4 / 6 )

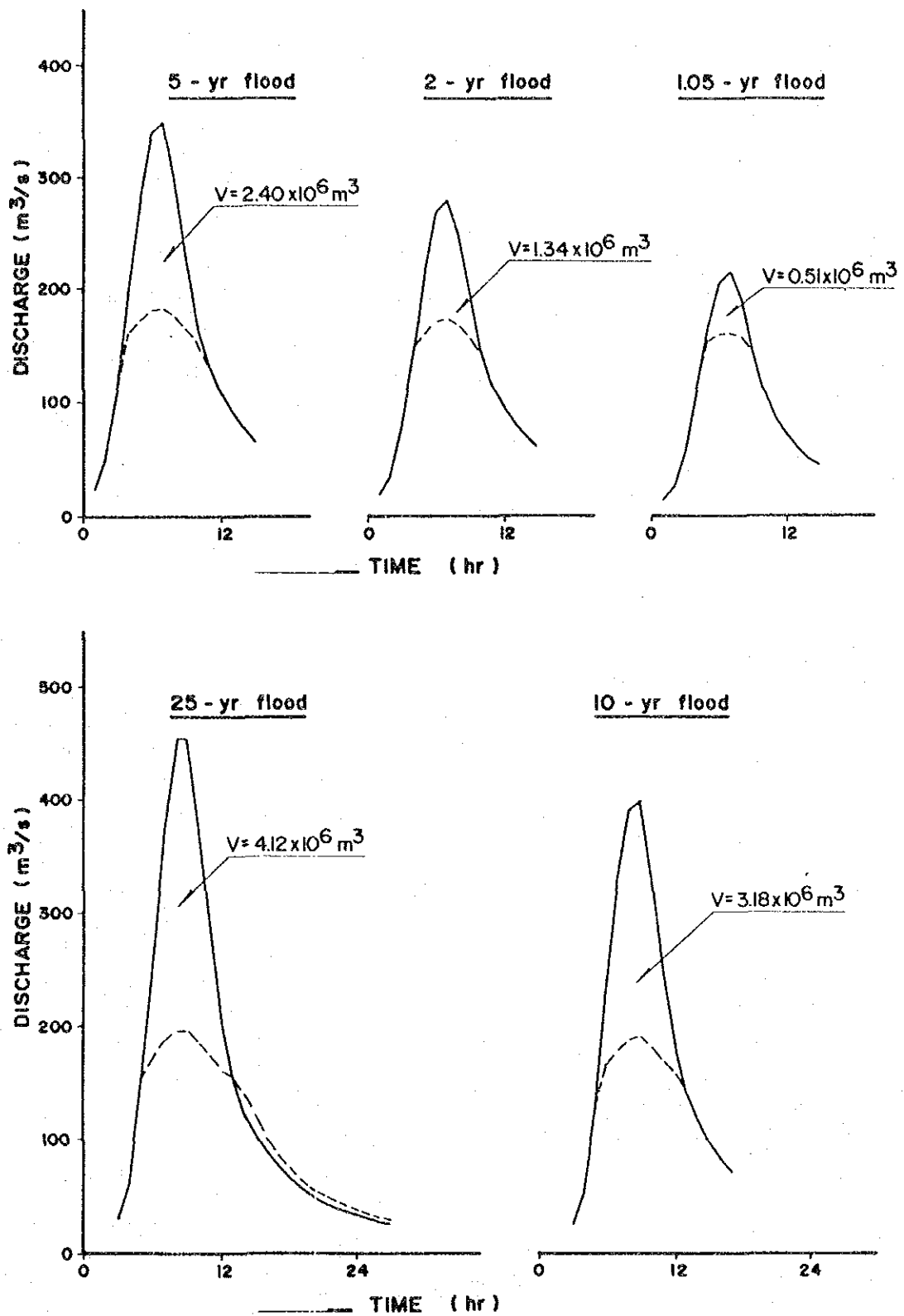


Fig. 4.3.9 REGULATING EFFECT OF KEDUNGSOKO RETARDING BASIN  
(River cross - section for 25 - yr probable flood) (5/6)

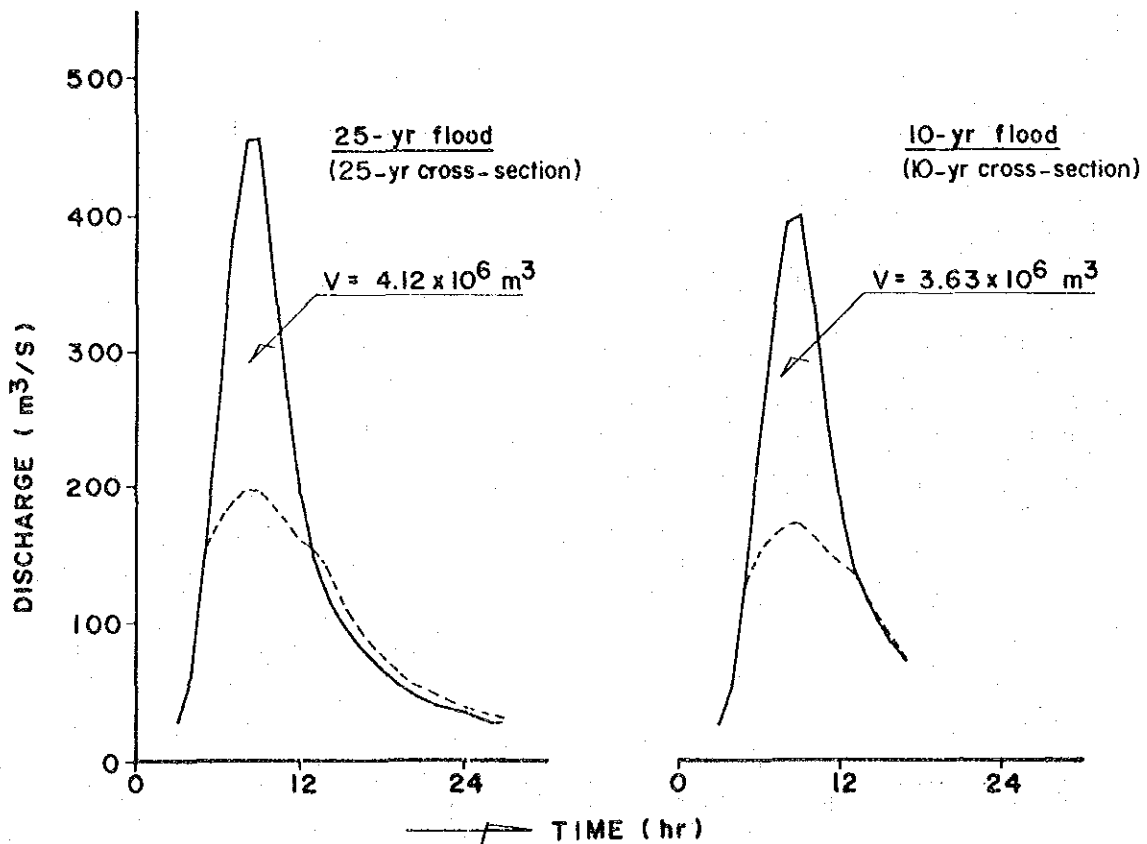
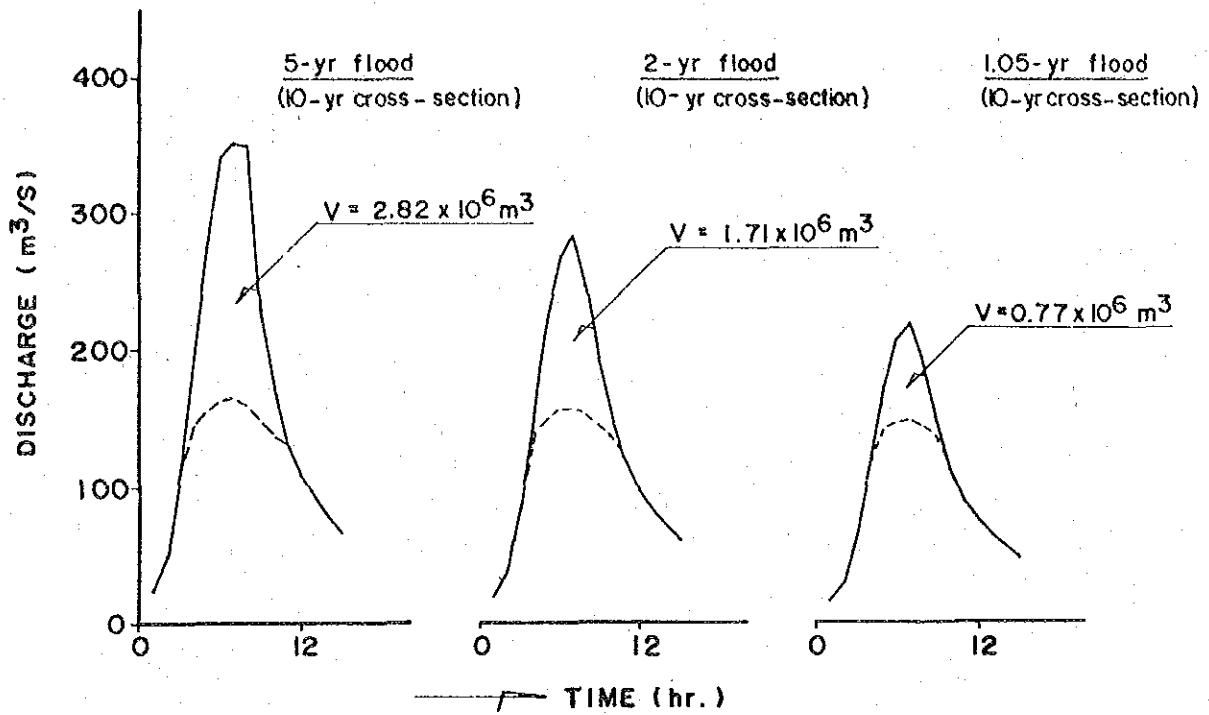
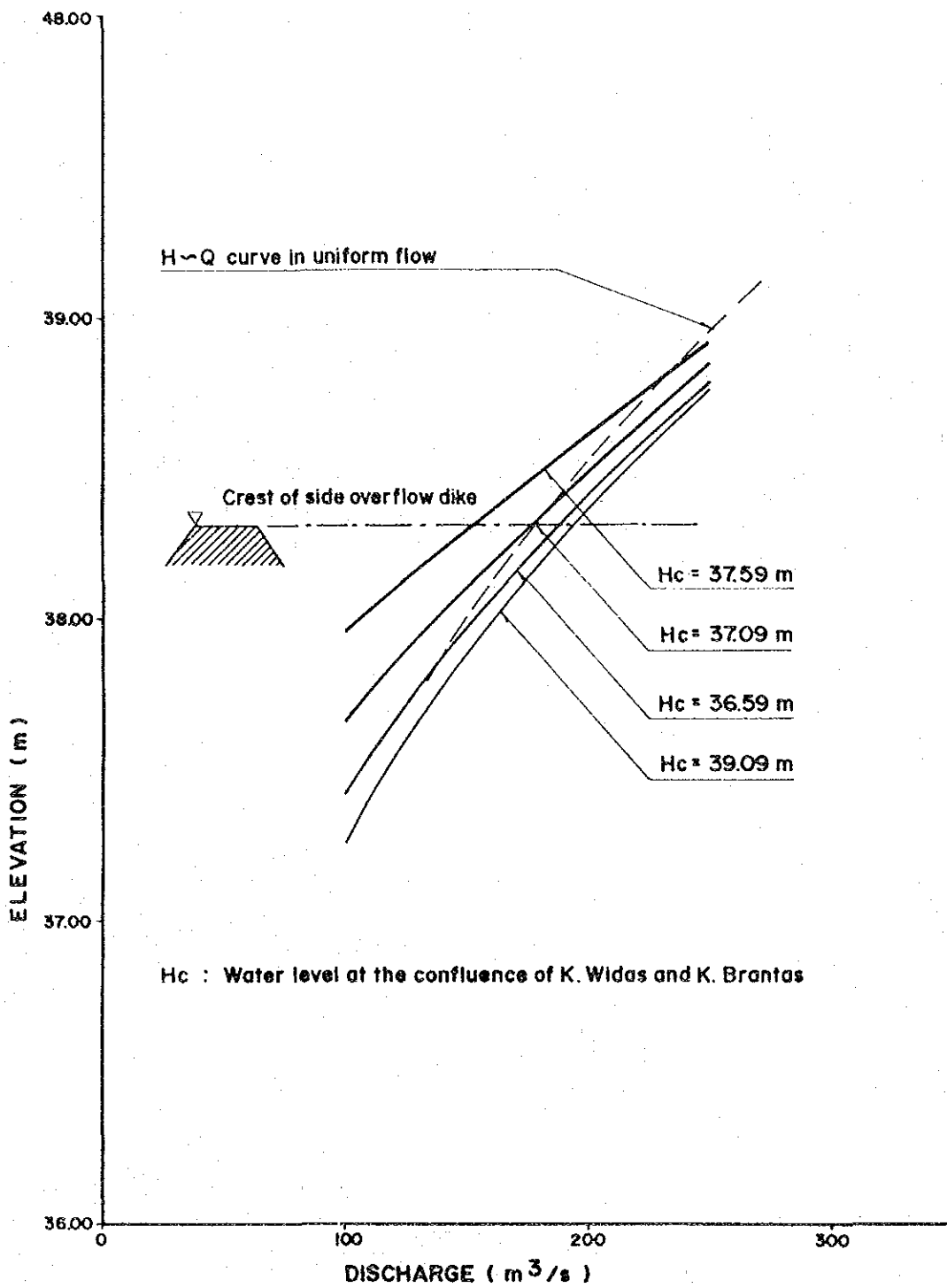
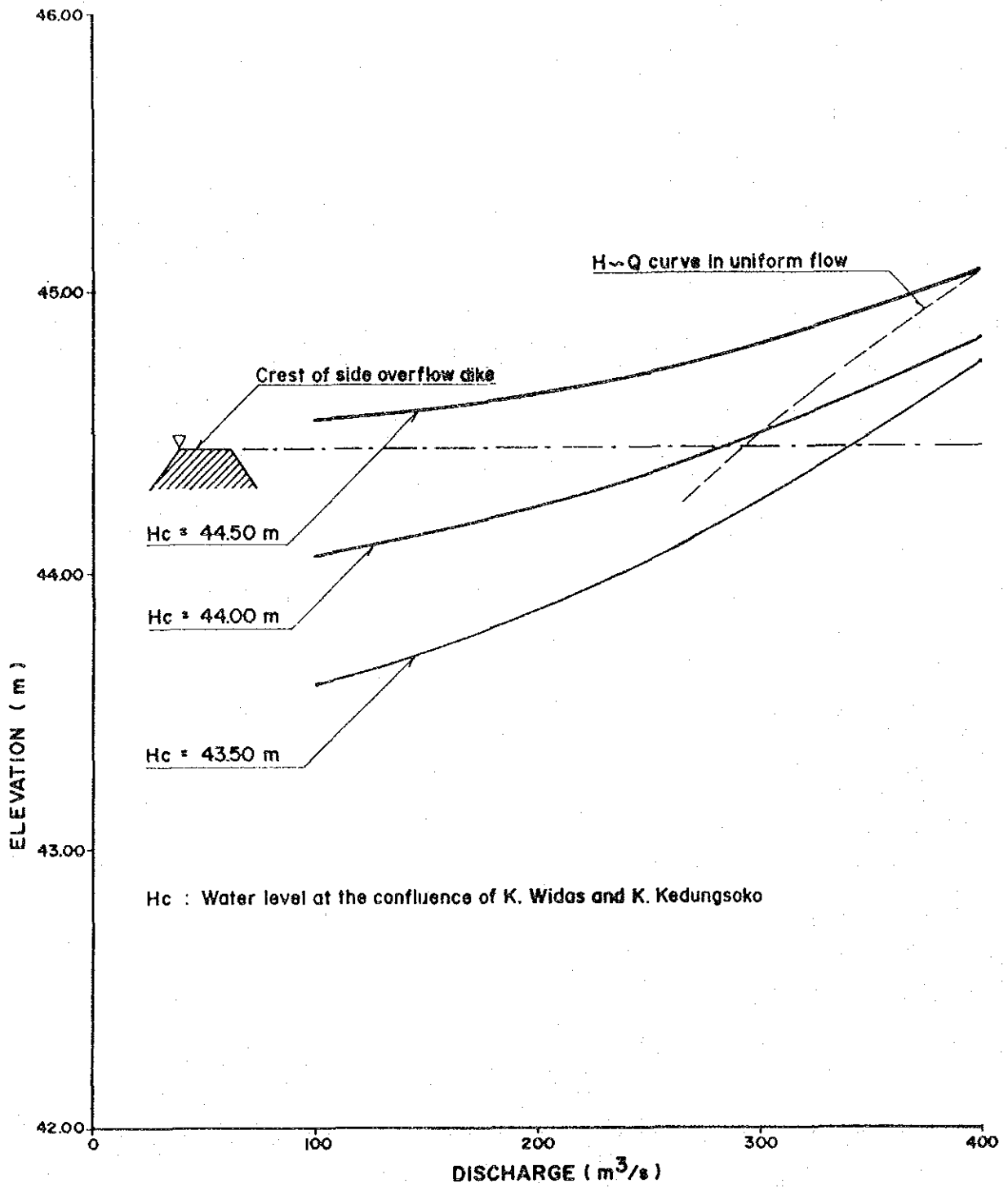


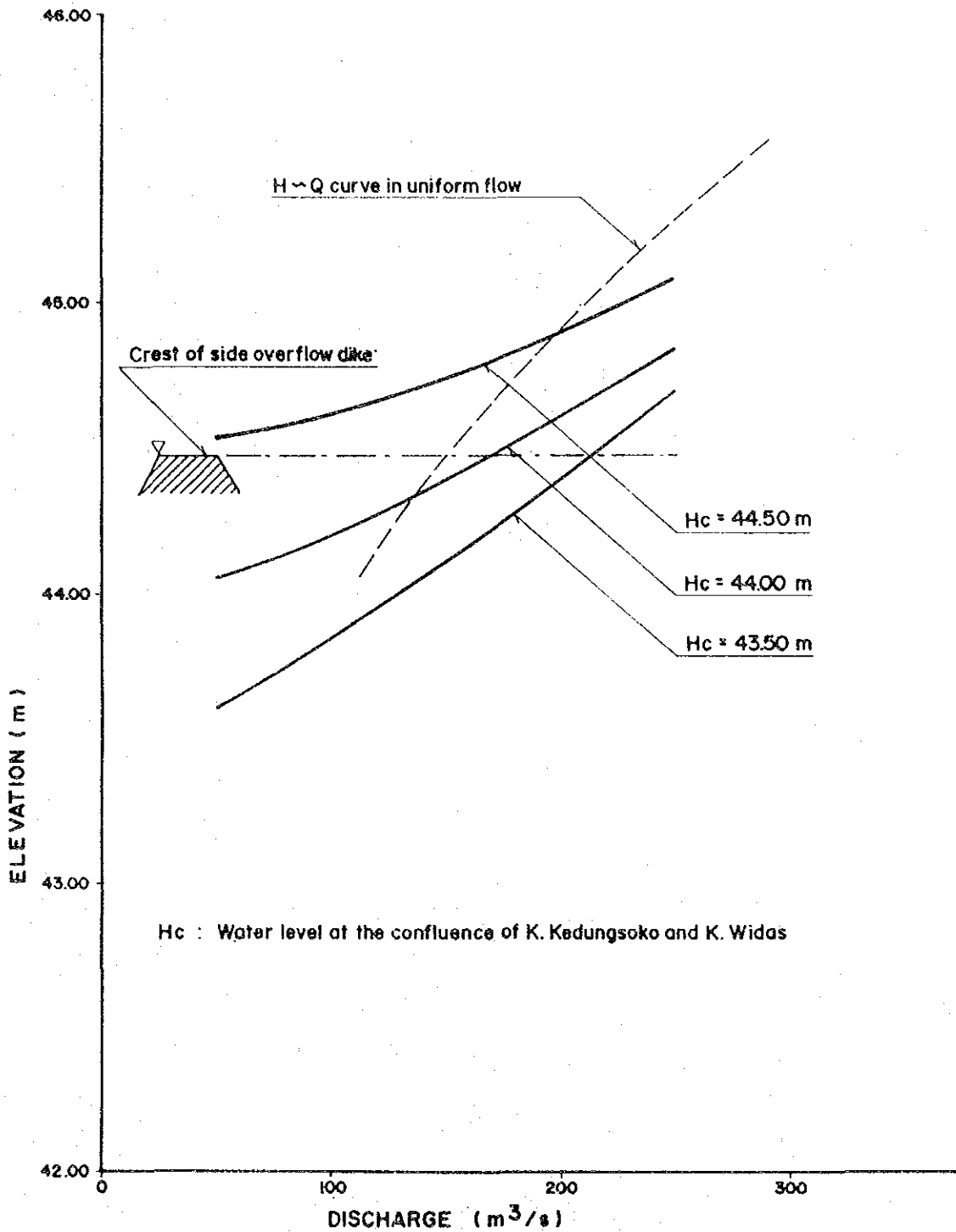
Fig. 4.3.9 REGULATING EFFECT OF KEDUNGSOKO RETARDING BASIN (River cross-section for 10-yr probable flood) (6/6)



**Fig. 4.3.10 STAGE DISCHARGE RELATION OF K. WIDAS AT DOWNSTREAM END OF SIDE OVERFLOW DIKE OF WIDAS RETARDING BASIN (1/3)**



**Fig. 4.3.10 STAGE DISCHARGE RELATION OF K. WIDAS AT DOWNSTREAM END OF SIDE OVERFLOW DIKE OF ULO RETARDING BASIN (2/3)**



**Fig. 4. 3. 10 STAGE DISCHARGE RELATION OF K. KEDUNGSOKO AT DOWNSTREAM END OF SIDE OVERFLOW DIKE OF KEDUNGSOKO RETARDING BASIN ( 3 / 3 )**

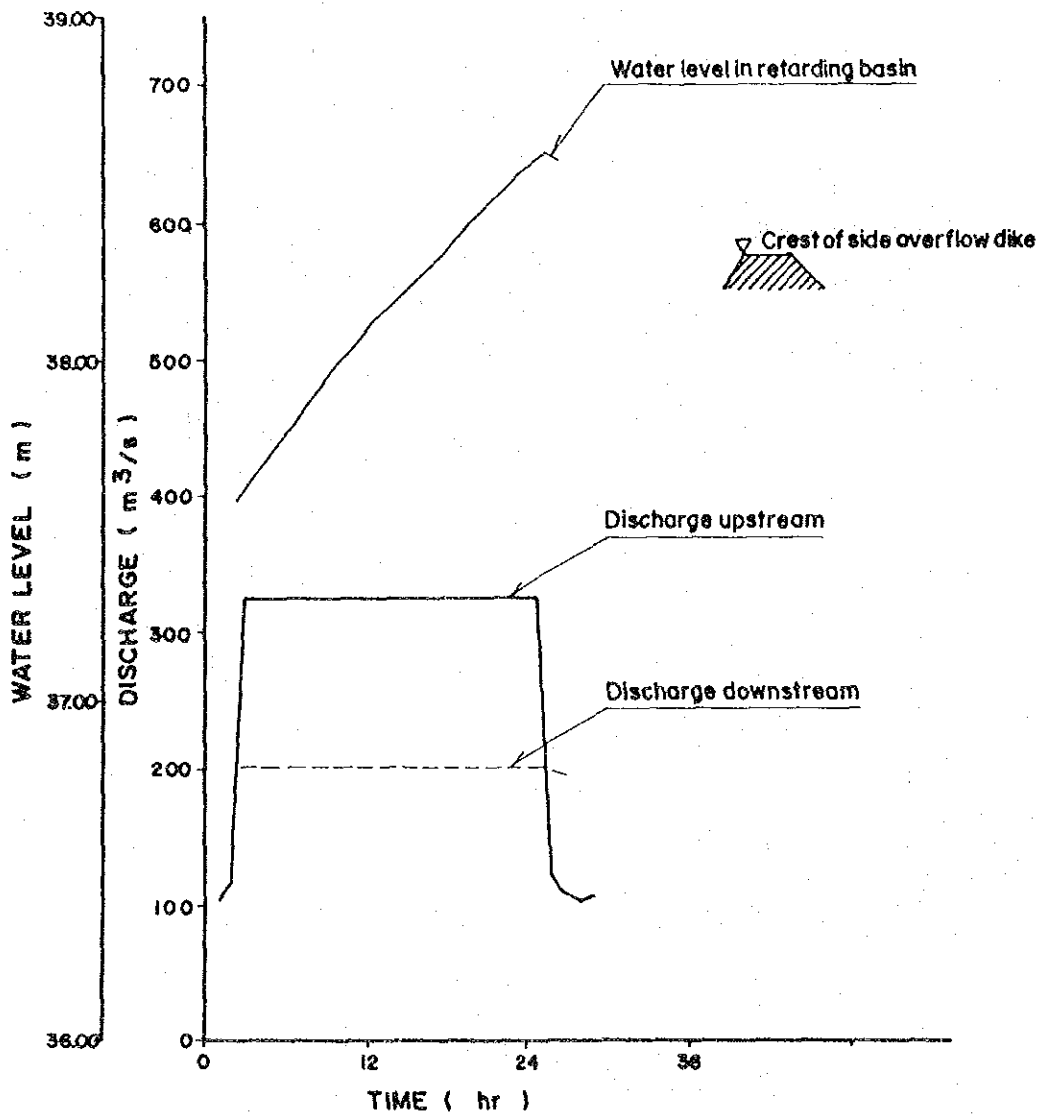
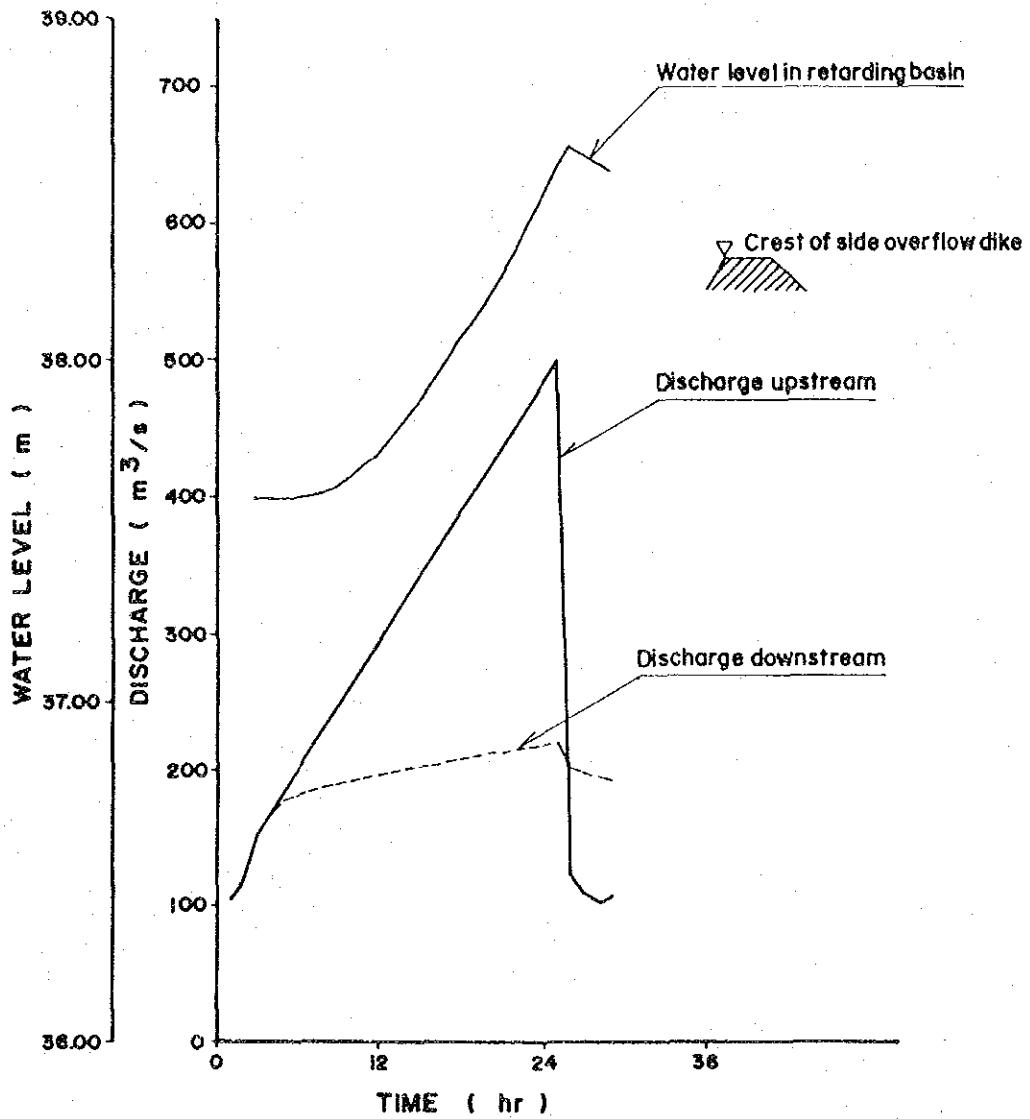


Fig. 4.3.11 FLOOD ROUTING IN THE WIDAS RETARDING BASIN  
( Flood hydrograph : type I ) ( 1/6 )





**Fig. 4.3. II FLOOD ROUTING IN THE WIDAS RETARDING BASIN  
( Flood hydrograph : type 2 ) ( 2/6 )**

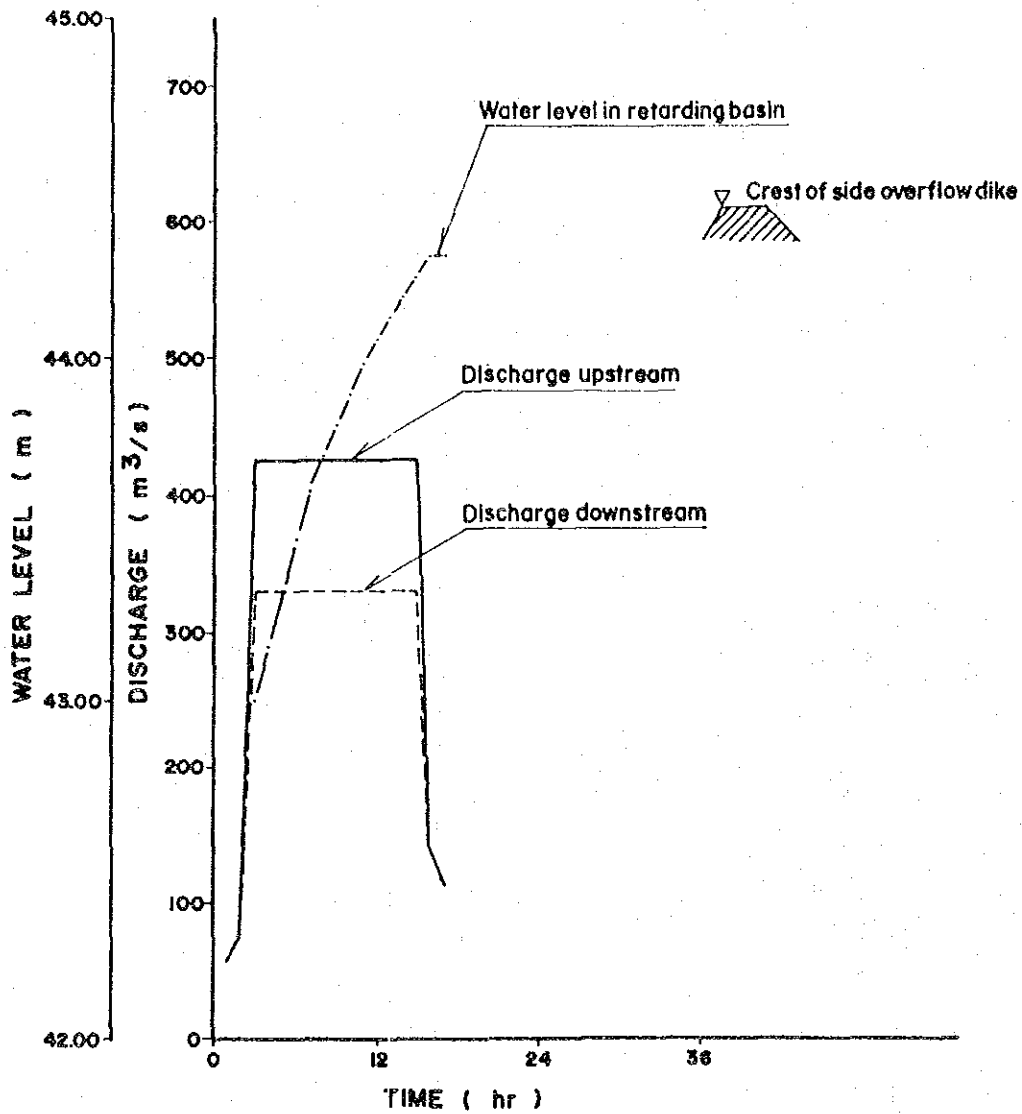
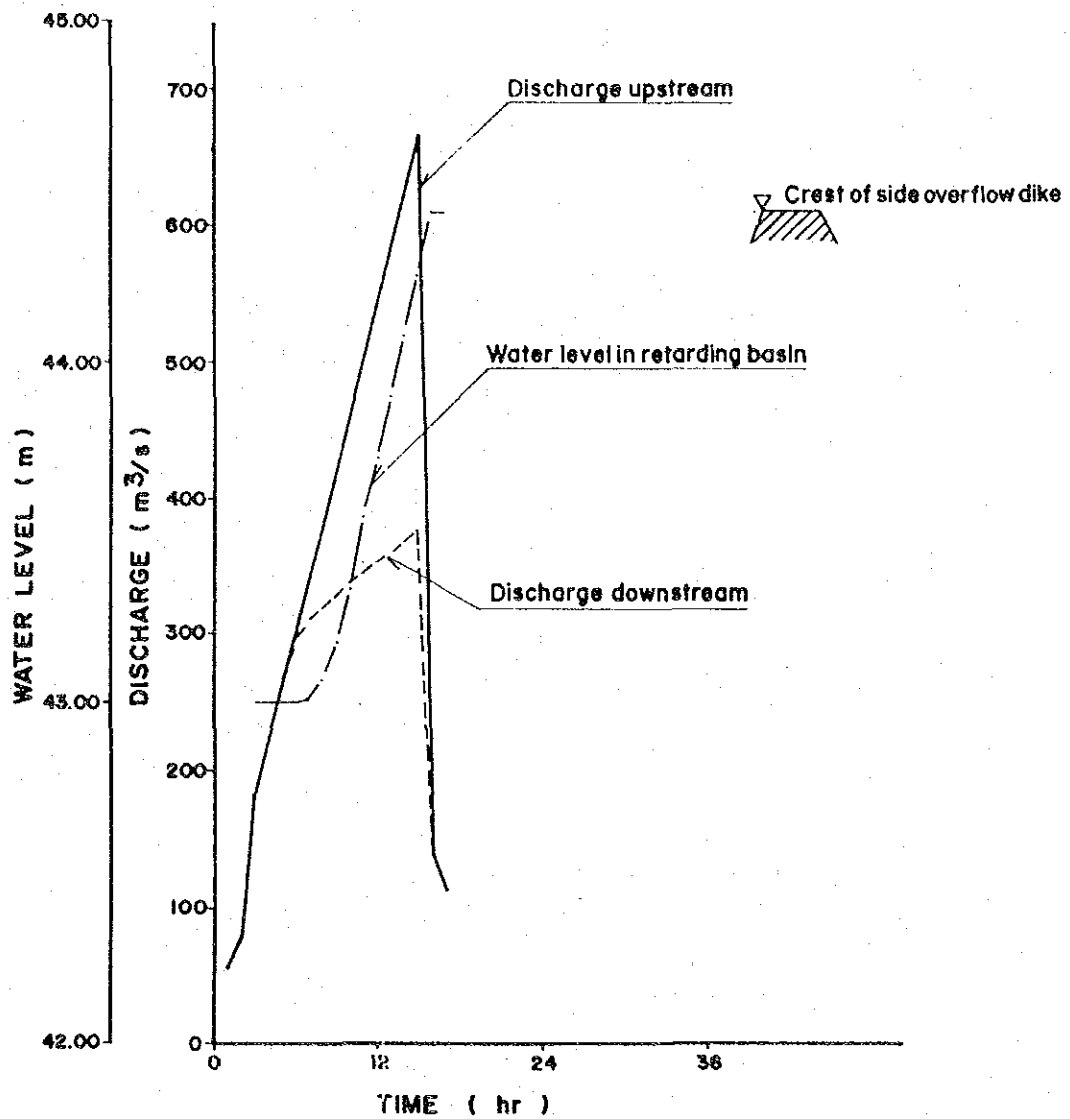


Fig. 4.3.II FLOOD ROUTING IN THE ULO RETARDING BASIN  
( Flood hydrograph : type I ) ( 3/6 )



**Fig. 4.3.II FLOOD ROUTING IN THE ULO RETARDING BASIN  
( Flood hydrograph : type 2 ) ( 4/6 )**

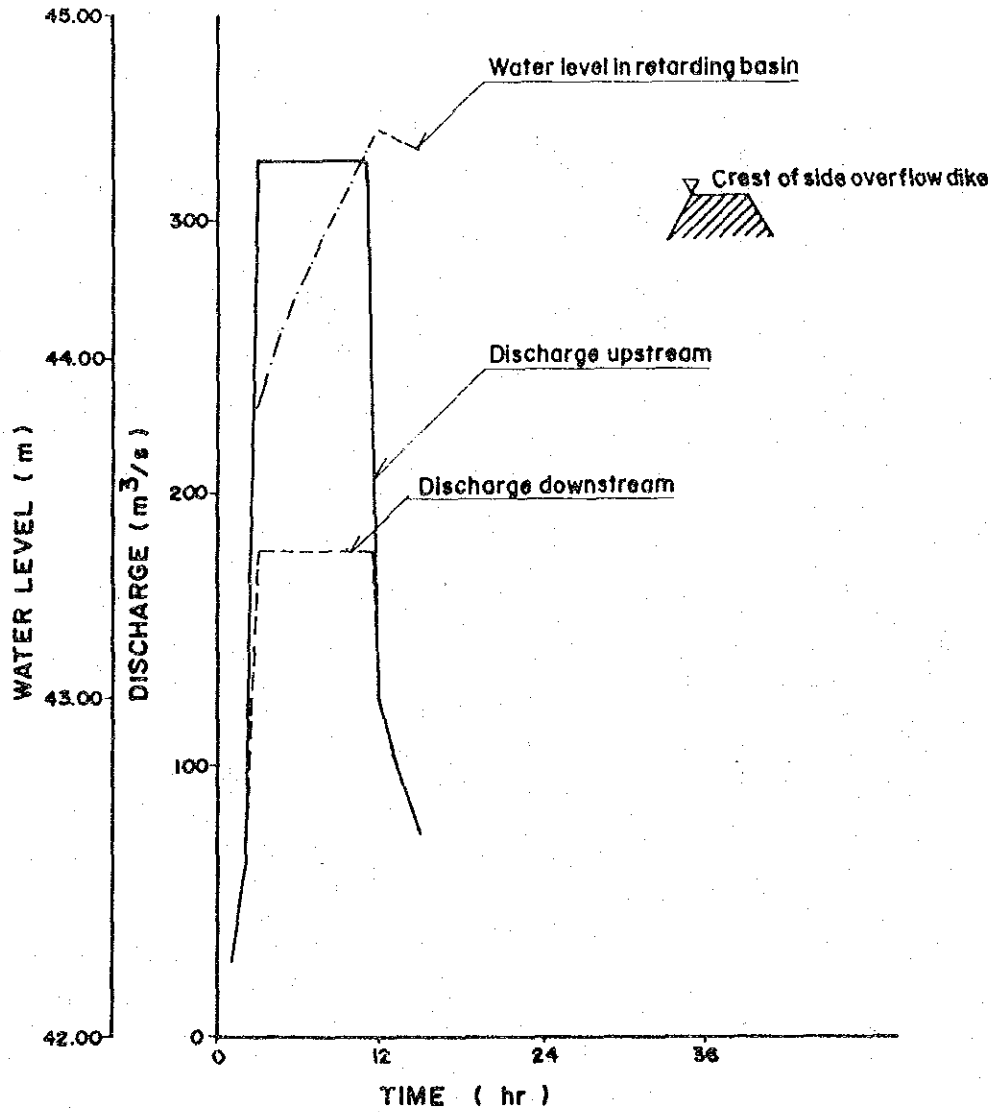
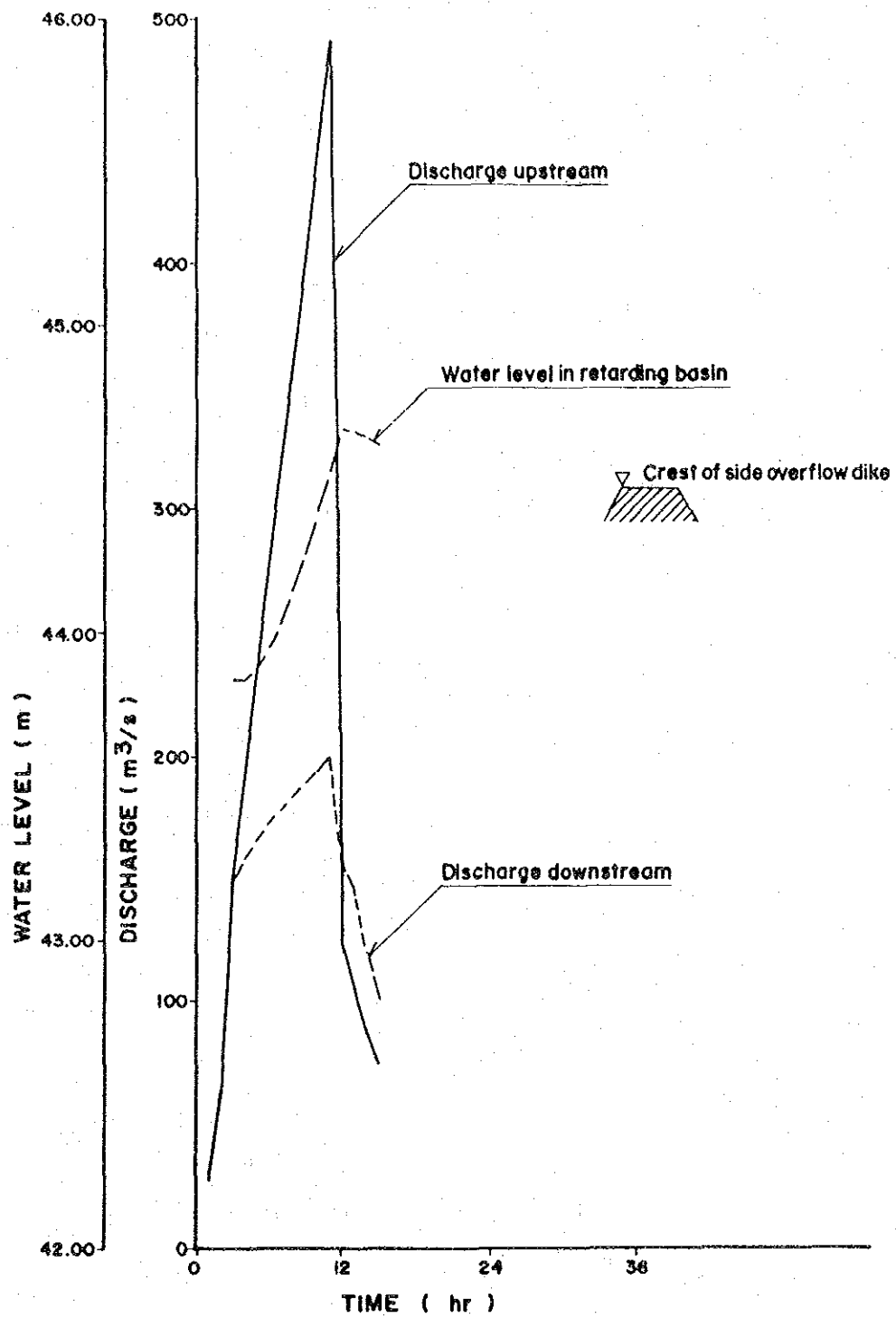


Fig. 4.3.II FLOOD ROUTING IN THE KEDUNGSOKO RETARDING BASIN ( Flood hydrograph : type I ) ( 5/6 )



**Fig. 4.3.II FLOOD ROUTING IN THE KEDUNGSOKO RETARDING BASIN ( Flood hydrograph : type 2 ) ( 6/6 )**

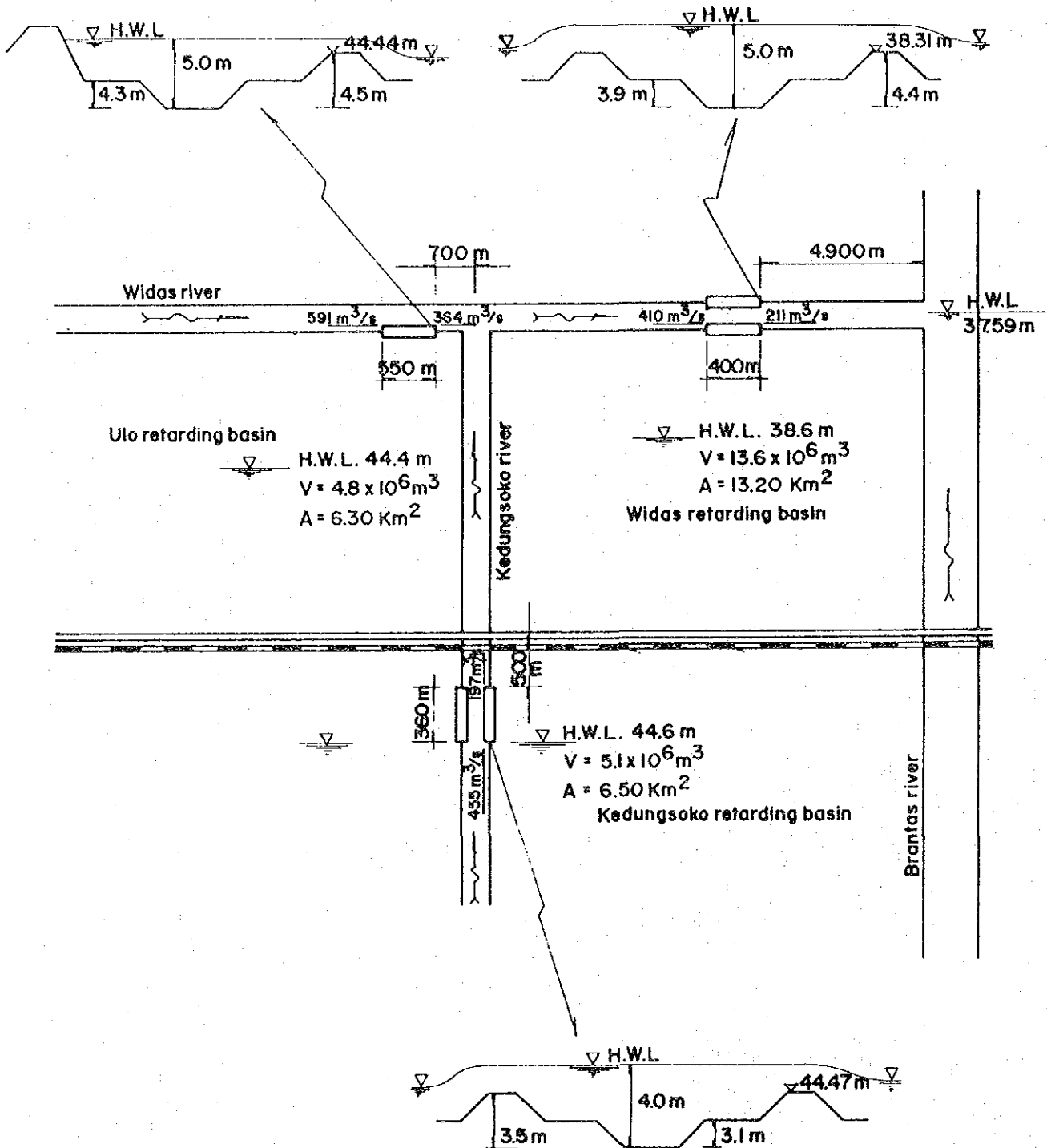
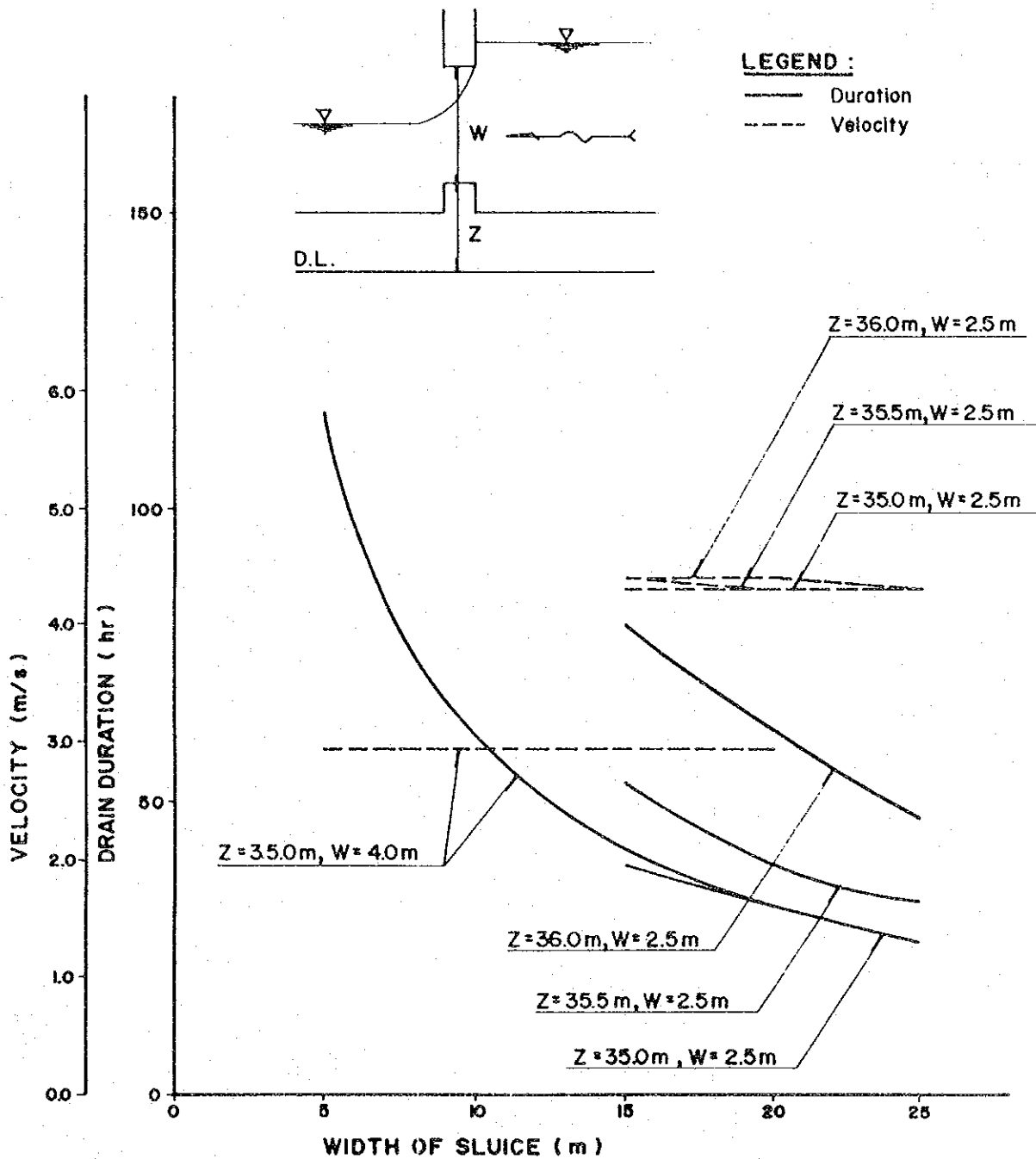


Fig. 4. 3.12 LOCATION DIAGRAM OF RETARDING BASINS



**Fig. 4.3.13 DRAIN DURATION AND MAXIMUM DRAIN VELOCITY OF WIDAS RETARDING BASIN (1/3)**

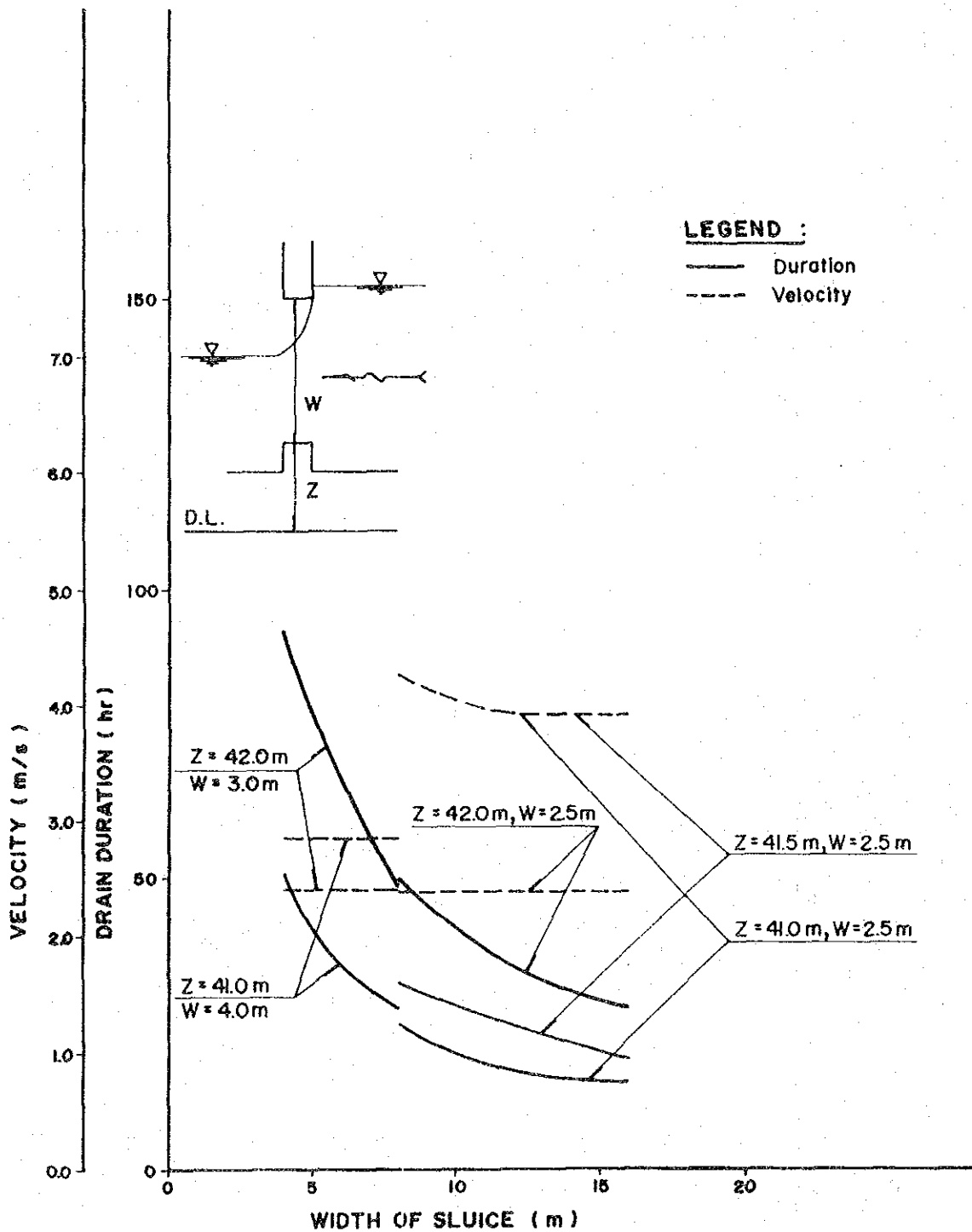
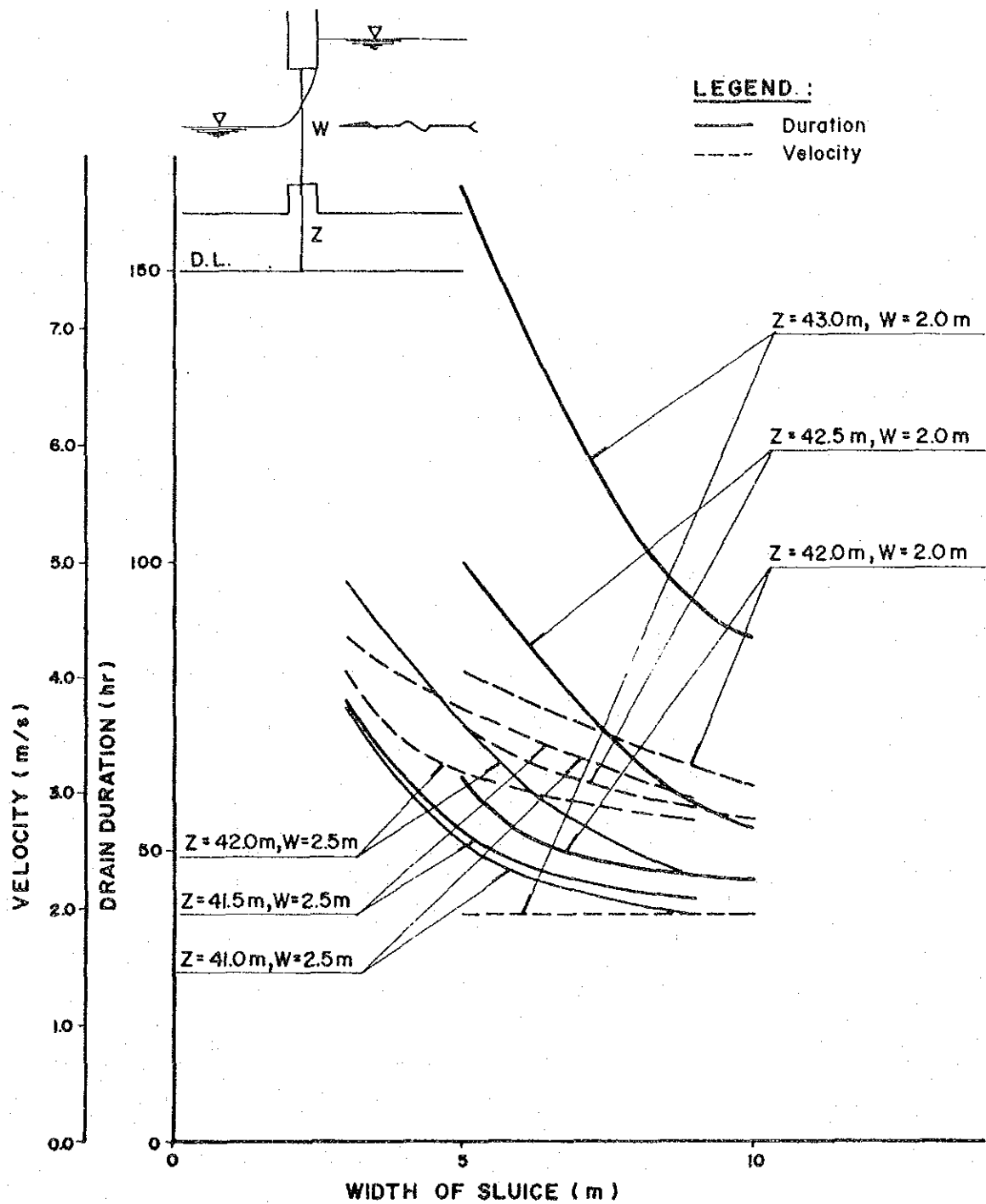


Fig. 4.3.13 DRAIN DURATION AND MAXIMUM DRAIN VELOCITY OF ULO RETARDING BASIN ( 2 / 3 )





**Fig. 4.3.13 DRAIN DURATION AND MAXIMUM DRAIN VELOCITY OF KEDUNGSOKO RETARDING BASIN ( 3/3 )**

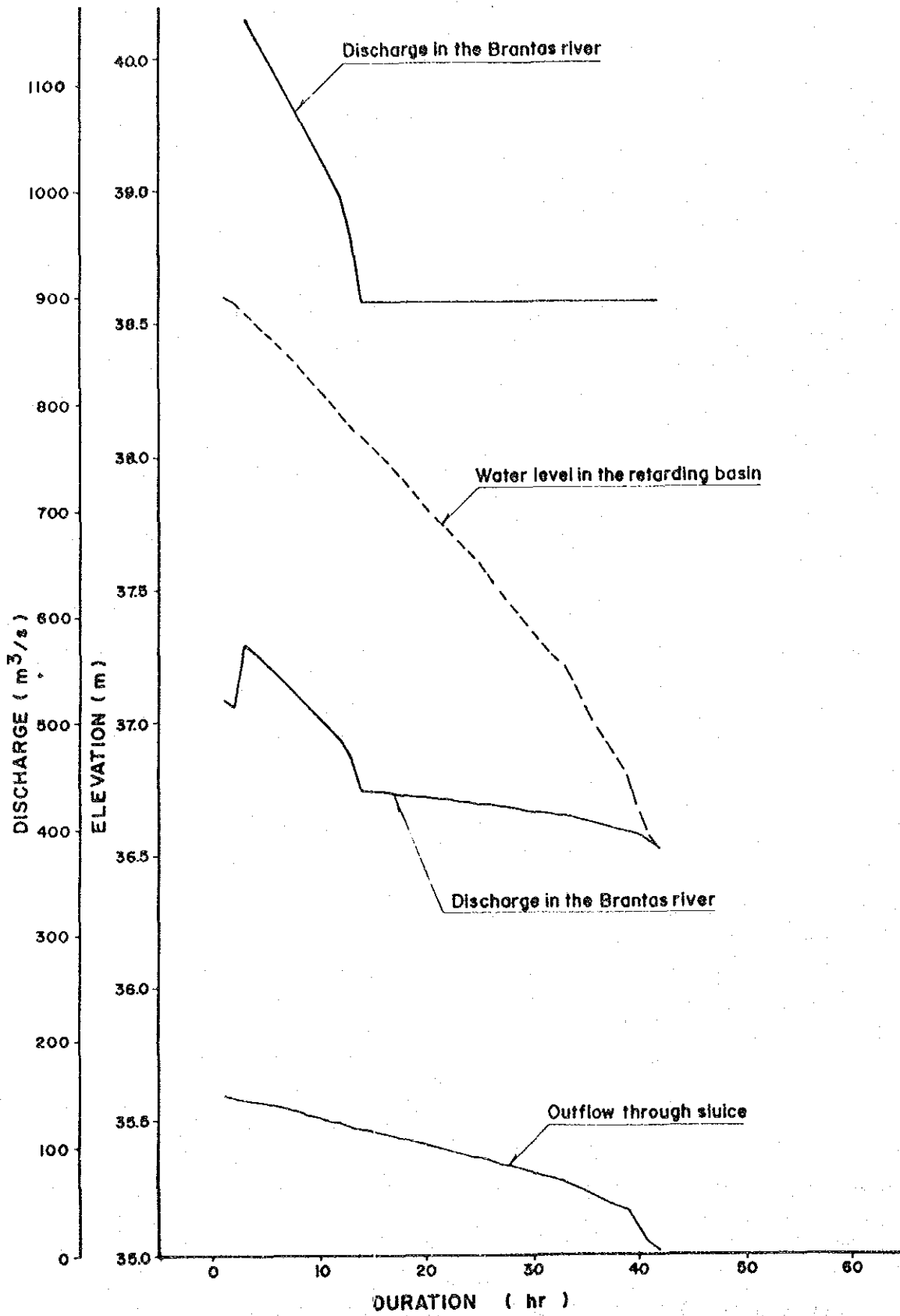
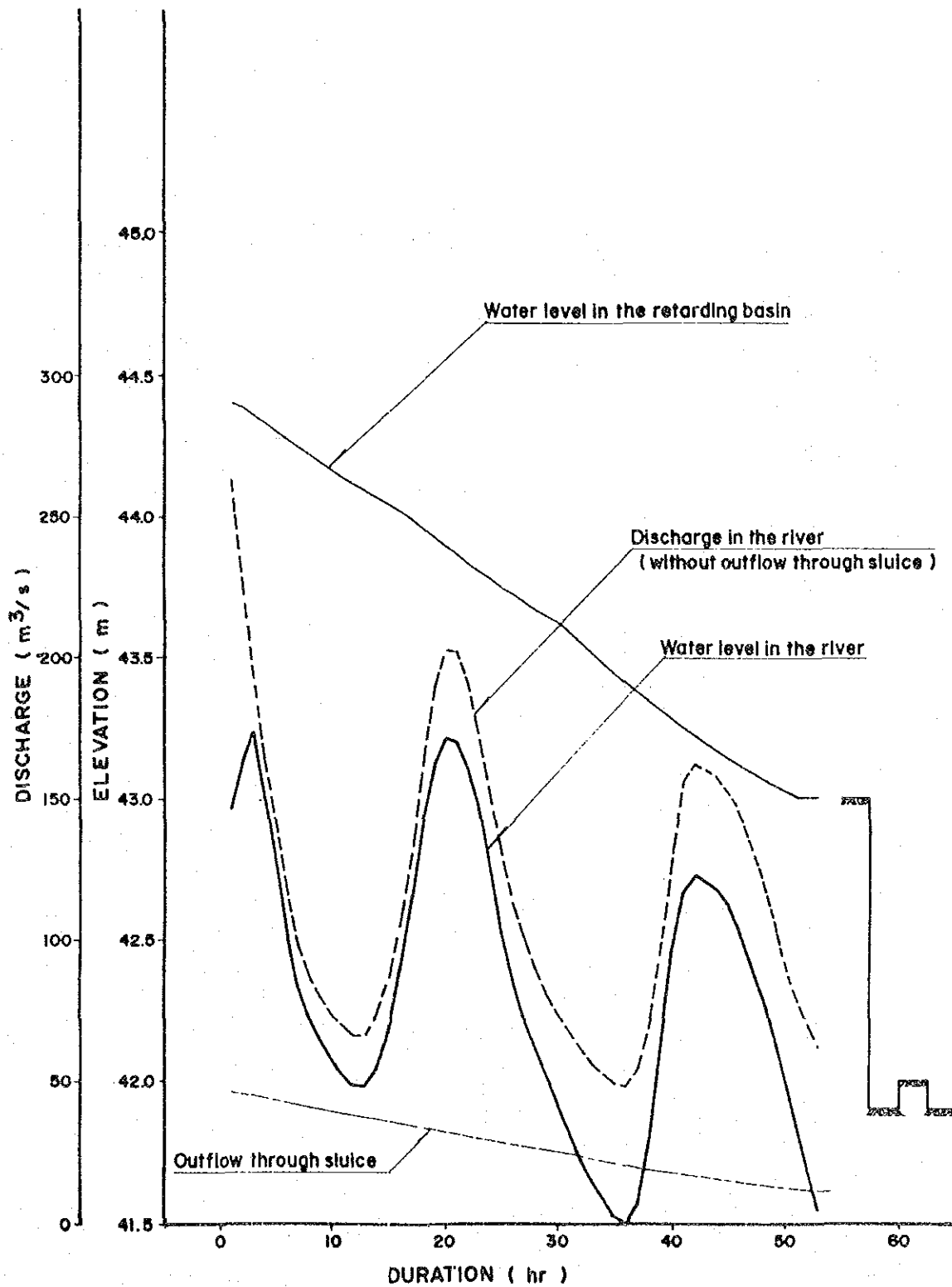


Fig. 4.3.14 FLOOD WATER DRAINAGE THROUGH SLUICE OF WIDAS RETARDING BASIN (1/3)



**Fig. 4.3.14 FLOOD WATER DRAINAGE THROUGH SLUICE OF ULO RETARDING BASIN ( 2 / 3 )**

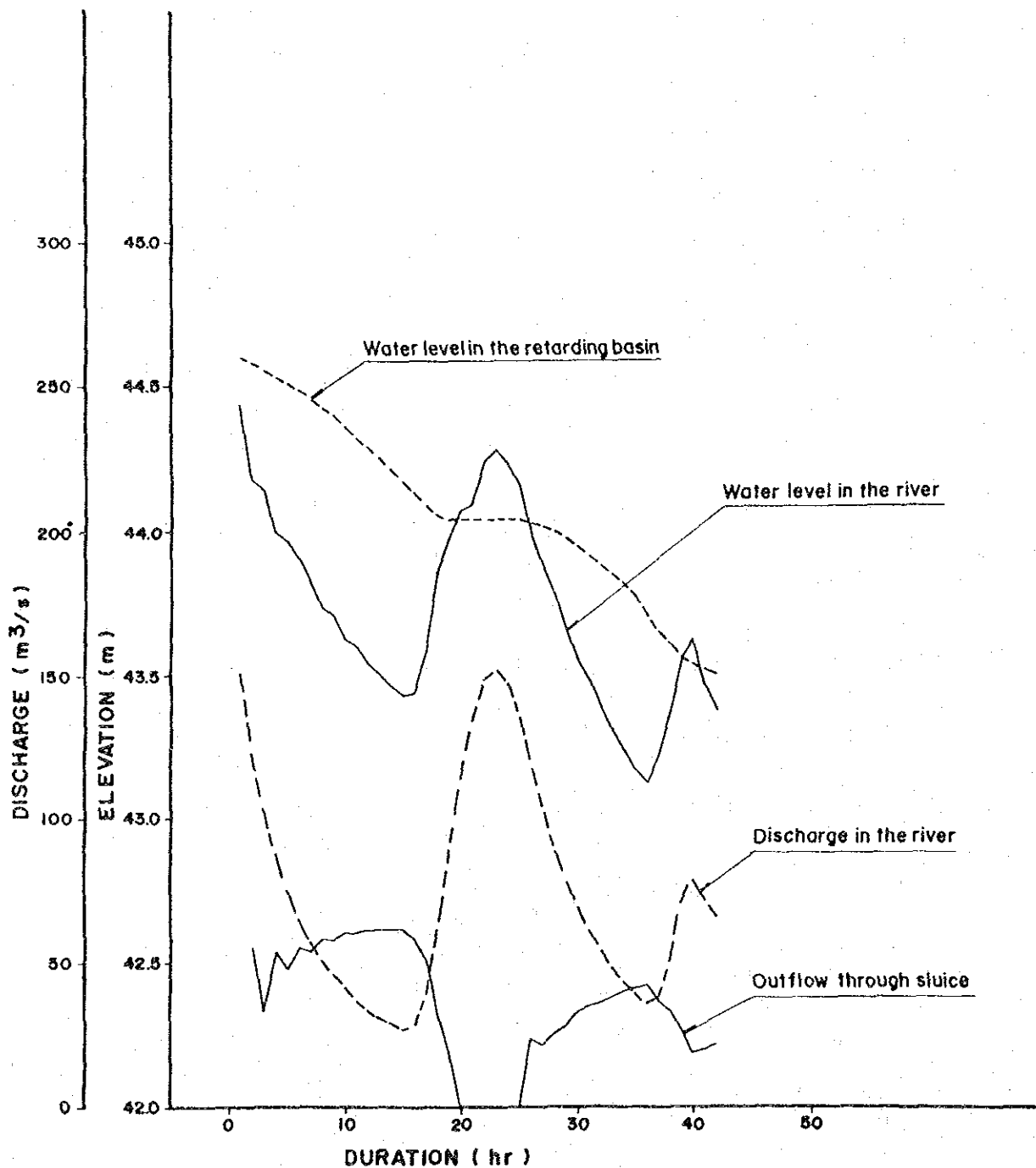
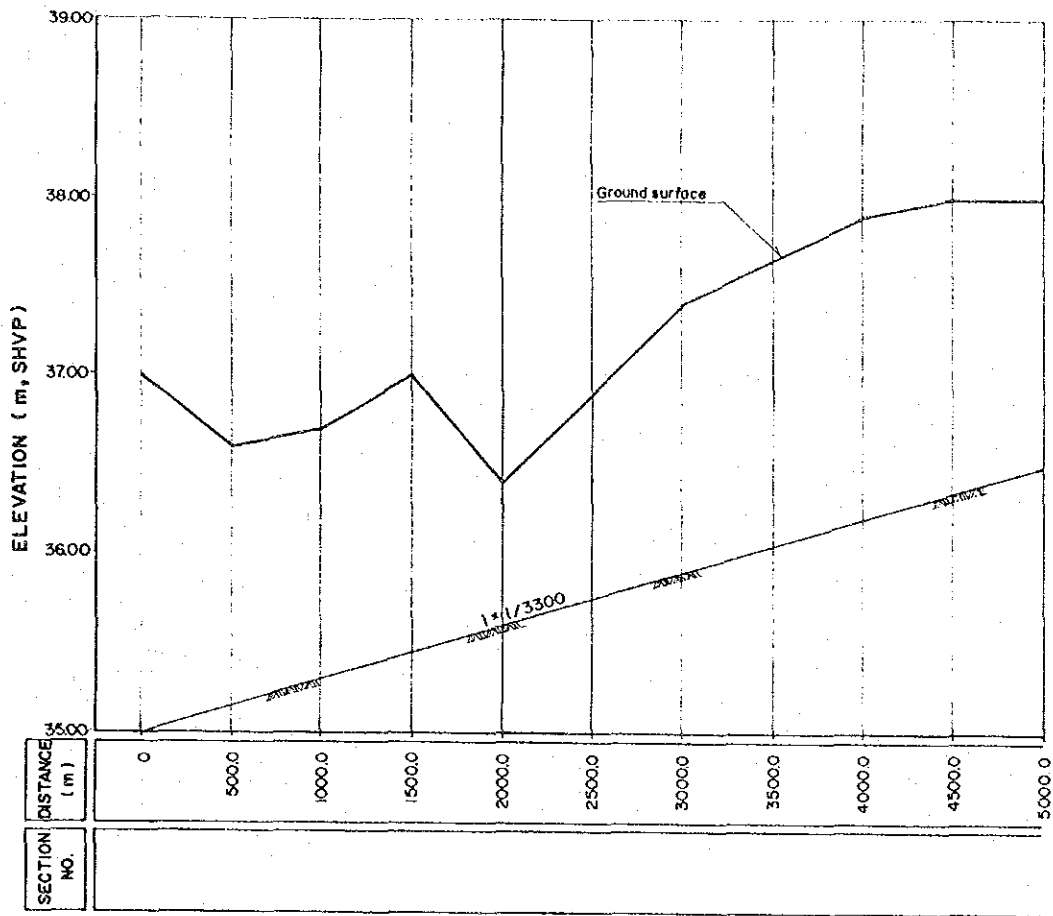


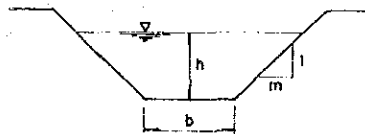
Fig. 4.3.14 FLOOD WATER DRAINAGE THROUGH SLUICE OF KEDUNGSOKO RETARDING BASIN ( 3/3 )



**(A)**  $Q = 10 \text{ m}^3/\text{s}$   
 $b = 6.00 \text{ m}$   
 $h = 1.67 \text{ m}$   
 $m = 2.00 \text{ m}$   
 $n = 0.03$   
 $i = 1/3300$   
 $v = 0.64 \text{ m/s}$

**(B)**  $Q = 6 \text{ m}^3/\text{s}$   
 $b = 4.00 \text{ m}$   
 $h = 1.50 \text{ m}$   
 $m = 2.00 \text{ m}$   
 $n = 0.03$   
 $i = 1/3300$   
 $v = 0.57 \text{ m/s}$

**(C)**  $Q = 3 \text{ m}^3/\text{s}$   
 $b = 2.00 \text{ m}$   
 $h = 1.32 \text{ m}$   
 $m = 2.00 \text{ m}$   
 $n = 0.03$   
 $i = 1/3300$   
 $v = 0.49 \text{ m/s}$



**Fig. 4. 3. 15 LONGITUDINAL PROFILE AND STANDARD CROSS - SECTION OF DRAINAGE CANAL OF LEFT WIDAS RETARDING BASIN (1/3)**

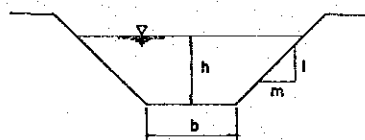
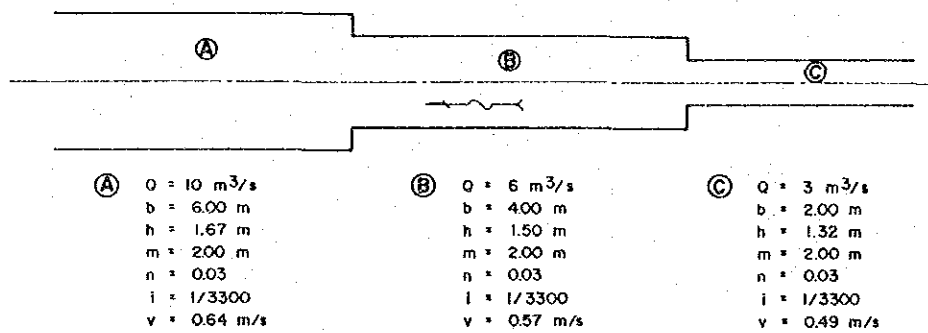
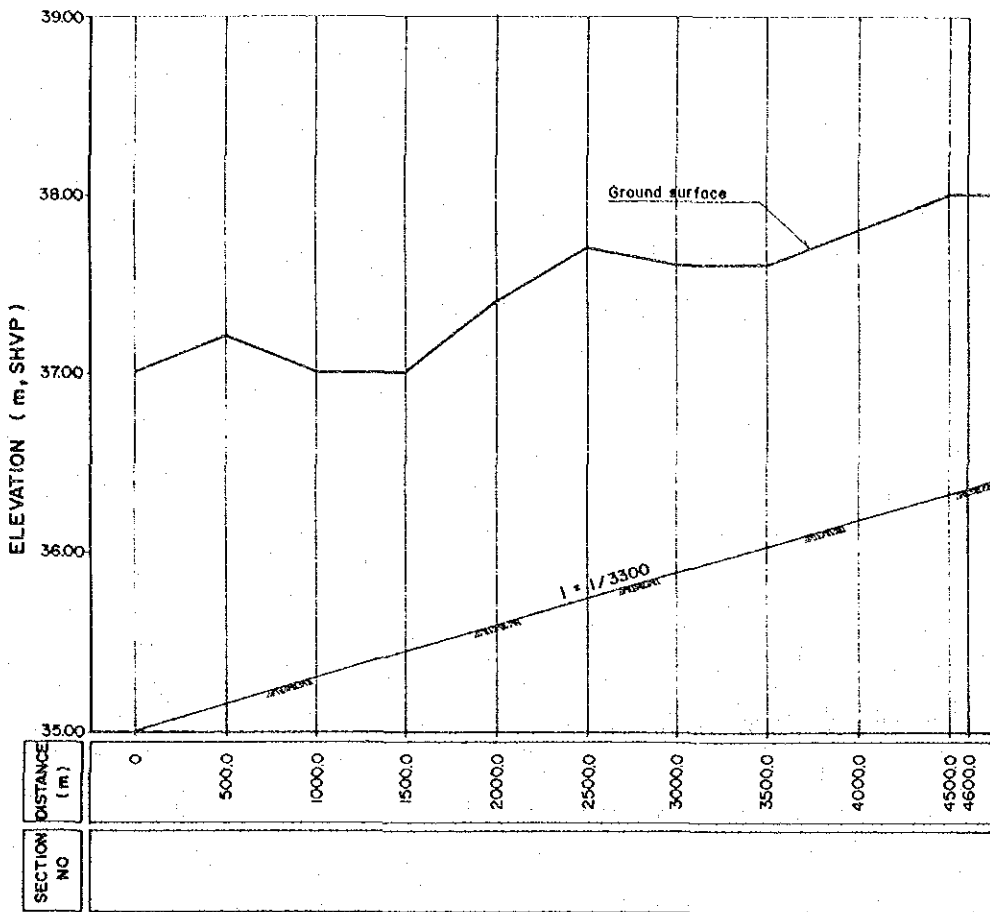
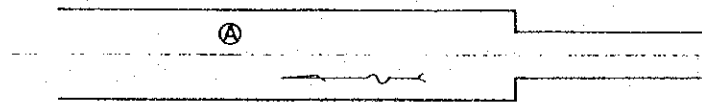
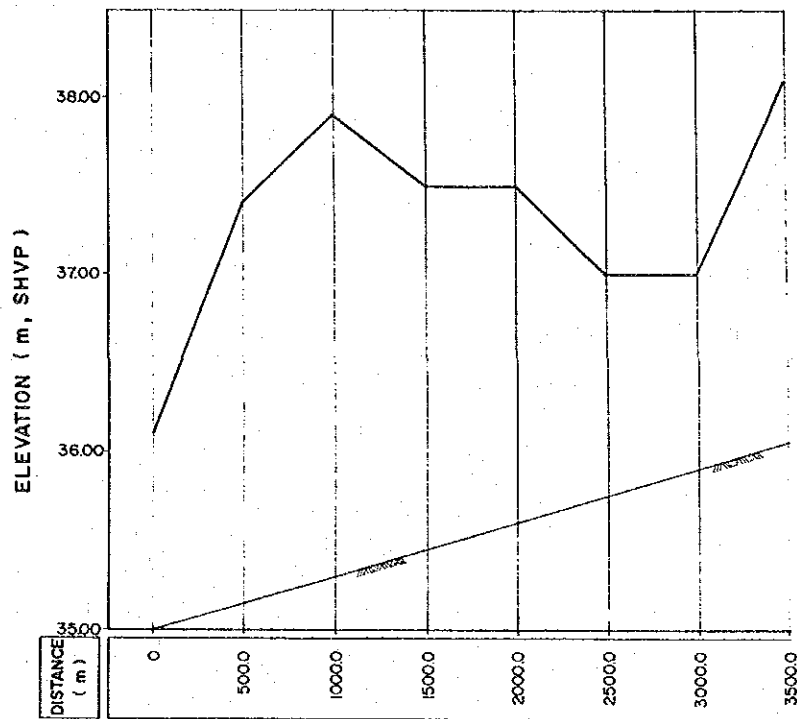


Fig. 4.3.15 LONGITUDINAL PROFILE AND STANDARD CROSS - SECTION OF DRAINAGE CANAL FROM SIDE OVERFLOW DIKE TO DRAINAGE SLUICE OF RIGHT WIDAS RETARDING BASIN ( 2/3 )



(A)  $Q = 6 \text{ m}^3/\text{s}$   
 $b = 4.00 \text{ m}$   
 $h = 1.50 \text{ m}$   
 $m = 2.00 \text{ m}$   
 $n = 0.03$   
 $i = 1/3300$   
 $v = 0.57 \text{ m/s}$

(B)  $Q = 3 \text{ m}^3/\text{s}$   
 $b = 2.00 \text{ m}$   
 $h = 1.32 \text{ m}$   
 $m = 2.00 \text{ m}$   
 $n = 0.03$   
 $i = 1/3300$   
 $v = 0.49 \text{ m/s}$

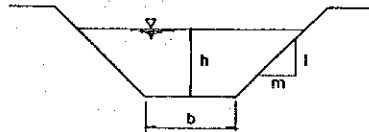


Fig. 4.3.15 LONGITUDINAL PROFILE AND STANDARD CROSS - SECTION OF DRAINAGE CANAL IN UPSTREAM REACH OF RIGHT WIDAS RETARDING BASIN ( 3/3 )

#### 4.4 Proposed River Channel Improvement

##### 1. River width

In general, river width is determined based on not only scale of design discharge but also river channel profile, topography, geology, land use in the riparian area and so on.

In this plan, river width is determined considering the following aspects of design standard and present condition.

##### Design standard of rivers in Japan

Design standard in Japan is as follows;

Design discharge ( m <sup>3</sup> /s )	River width ( m )
300	40 - 60
500	60 - 80
1000	90 - 100

On the other hand, actual river width which currently designed and/or under construction and/or constructed is given on Fig. 4.4.1 showing relationship among river width, design discharge and basin area.

##### Present river width

Out of the objective rivers, the upper reach of Kedungsoko river has been improved essentially involving construction of flood dikes on the both banks. In this plan, these existing dikes are fully utilized by strengthening and heightening. For the others, the river width including high-water channel has been not yet fixed and varies depending on the scale of flood discharges.

In some rivers especially Widas river, excessive meandering, are remarkable in locations and such excessive ones are smoothed by cut-off channel considering stability of river channel. In determination of river width, it is considered to cover such large meandering of river course, that is, river width is determined considering the extent of the large meandering of the existing river course.

Under the above considerations, river width of the respective rivers is determined as shown below.



River	By basin area		By design discharge		Present average river width (m)	Proposed river width (m)
	Area (km <sup>2</sup> )	River width (m)	Design discharge (m <sup>3</sup> /s)	River width (m)		
Lower Widas	1350-1200	350-310	570-530	90-80	300-400	300-100
Upper Widas	690- 230	250-150	640-440	100-70	100- 50	110- 50
Diversions + Upper Ulo	230- 220	150-140	230-190	50	Upper Ulo 40	50
Kedungsoko	500	210	470-200	75-50	100	100- 90
Kuncir	60	70	95	50	30	40

## 2. Longitudinal profile

Design profile is determined considering profile of the existing river channel. The river bed elevation is set at the average upper line of the deepest river bed in the existing channel.

Design high-water level is determined based on the following criteria. For rivers which diking system have been employed or are to be employed, the high-water level is set not so as to heighten the existing flood water level or max. flood level in the past, in principle. For rivers which are improved by excavation of low-water channel without diking system, it is set below average existing ground height as low as possible.

The design elevations of dike crown, high-water level and river bed are shown in Table 4.4.1.

## 3. River cross-section and its cross-sectional area

Double section consisting of high-water channel and low-water channel is adopted to river channel section considering large fluctuation of river discharge and stability in principle. However, also single section with berm is adopted to the lower Ulo which is newly connected to the middle Widas river.

The required cross-sectional area is estimated by uniform flow method. The adopted Manning's coefficient roughness "n" is as follows;

- n = 0.03 for low-water channel
- n = 0.05 for high-water channel

The major proposed dimensions of typical cross-section for comprehensive plan and first stage plan are given in Table 4.4.2. Those typical cross-sections are shown on Figs. 4.4.2 and 4.4.3 respectively.

Based on the above design profile and typical cross-section, the river cross-sections at the respective surveyed cross-sections are proposed as explained later (Fig. 4.4.5). For reference, carrying capacity of the proposed river channel of the comprehensive plan is checked by non-uniform flow calculation and the results are shown in Table 4.4.3. According to

the Table 4.4.3, it shows that the proposed river channel can be flown design discharge below the design HWL for almost whole stretches.

#### 4. Bank protection works

The bank protection works consisting of wetmasonry and gabion are provided at flow attacking places and/or along densely populated areas. The right bank of the new diversion channel and Upper Ulo river is protected by wetmasonry type revetment for almost whole stretches to prevent Nganjuk urban area from breach of flood dike due to flow attacking.

Length and area of bank protection works are shown in Table 4.4.4 and locations of major bank protection works are shown on Fig. 4.4.4. Approximate 40% of total bank protection works for comprehensive plan is constructed by first stage plan considering existing condition.

#### 5. Layout of proposed dike alignment and related river structures

Feasibility designs for comprehensive plan and first stage plan are made based on the typical cross-section and longitudinal profile. The proposed dike alignment, controllable retarding basin, related structures and river cross-sections are given on Figs. 4.4.4 and 4.4.5.

The controllable retarding basins and related river structures are described in the sections of 4.3 and 4.5 in this ANNEX-4, respectively.

#### 6. Design discharge and river width of secondary tributaries

The secondary tributary is improved mainly by construction of back-water levee including minor excavation. The objective tributaries are 12 rivers in total. Such tributaries are improved for 5-yr flood for comprehensive plan and first stage plan.

The design discharges of the above tributaries are estimated based on the specific discharges which were calculated by hydrological study and those are summarized below.

	Net Area (km <sup>2</sup> )	Specific discharge (m <sup>3</sup> /s/km <sup>2</sup> )	Design discharge (m <sup>3</sup> /s)
Lower Widas			
Pohbuntu	61	1.38	85
Nglempoh	13	1.87	25
Jaan	11	1.87	25
Tributary	10	1.44	15
Tretes	31	1.44	45
Upper Widas			
Ngrembek	46	1.27	60
Tributary	6	1.27	10
Pelangkengi	72	2.49	180
Wotrangkul	44	1.63	75
Upper Ulo			
Secong	63	1.51	100
Winong	11	2.18	25
Kuncir			
Gonggang - Malang	37	0.54	20

For the above design discharges, the following proposed river width and length are provisionally adopted to tributary improvement for cost estimate considering existing river width and its carrying capacity. The "n" values of 0.035 for low-water channel and 0.05 for high-water channel are adopted.

River	Existing Condition		Design Condition			
	Average River width ( m )	Average Carrying Capacity (m <sup>3</sup> /s)	Design HWL of Conf. (m.SHVP)	Design Dike Crown of Conf. (m.SHVP)	Design River Width ( m )	Length to be Improved ( km )
<b>Lower Widas</b>						
Pohbuntu	20	-	39.13	40.13	30	0.9
Nglempoh	10	15	40.50	41.50	20	1.6
Jaan	20	35	41.39	42.39	30	1.3
Tributary	10	-	41.55	42.55	20	1.2
Tretes	25	15	42.50	43.50	35	1.5
<b>Upper Widas</b>						
Ngrembek	35	180	46.86	47.86	45	1.5
Tributary	25	40	47.24	48.24	35	1.5
Pelangkengi	50	180	47.80	48.80	60	2.9
Wotrangkul	45	120	50.93	51.93	55	2.5
<b>Upper Ulo</b>						
Secong	30	40	54.50	55.50	40	1.5
Winong	20	90	57.30	58.30	30	0.5
<b>Kuncir</b>						
Gonggang-Malang	10	10	45.83	46.63	20	0.8

All canal a main drainageway in Warujayeng irrigation area is to be improved for 5-yr flood of 70 m<sup>3</sup>/s by Waru-Turi Project.

#### 7. Merit and demerit of construction of surrounding dike of retarding basin

Surrounding dike of a retarding basin essentially aims protect the inland from flood water retarded in the retarding basin. But even without the surrounding dike, the inundation condition of the retarding basin would be improved with the construction of river dike and side overflow dike than in the present condition, depending on the hydrological and topographical features.

Here are the brief discussions on whether to construct surrounding dikes or not.

##### (1) Cost

In the case of construction of surrounding dike, the following costs are needed.

- (a) Land acquisition cost
- (b) Construction cost of dike
- (c) Construction cost of sluices or culverts
- (d) Operation and Maintenance cost