

REPORT
FOR
THE FEASIBILITY STUDY
ON
THE CONSTRUCTION OF DRY DOCK
IN
THE SOCIALIST REPUBLIC OF THE UNION OF BURMA

SUPPLEMENTARY DATA

- 1. SURVEYING
- 2. SOIL INVESTIGATION

MARCH, 1984

JAPAN INTERNATIONAL COOPERATION AGENCY

REPORT FOR THE FEASIBILITY STUDY ON THE CONSTRUCTION OF DRY DOCK IN
THE SOCIALIST REPUBLIC OF THE UNION OF BURMA

SUPPLEMENTARY DATA

104
65.5
SDF

S D F
GR(3)
84-022

REPORT
FOR
THE FEASIBILITY STUDY
ON
THE CONSTRUCTION OF DRY DOCK
IN
THE SOCIALIST REPUBLIC OF THE UNION OF BURMA

SUPPLEMENTARY DATA

1. SURVEYING
2. SOIL INVESTIGATION

MARCH, 1984

JAPAN INTERNATIONAL COOPERATION AGENCY

JICA LIBRARY



1033994[3]

S D F
CR(3)
84-022

国際協力事業団	
受入 月日 '84. 3. 29	164
登録No. 10112	65.5
	SDF

マイクロ
ライナー

1. Objectives

2. Surveys

2-1. Survey Area	1
2-2. Items to be Surveyed	2
2-3. Datum Level	2
2-4. Survey Methods	2
(1) Control Surveying and Traversing	2
(2) Topographic Survey	3
(3) Sounding	3

3. Soil Investigation

3-1. Investigation Items and Quantities	5
3-2. Investigation Site	5
3-3. Investigation Methods	5
(1) Boring	5
(2) Standard Penetration Test	7
(3) Undisturbed Sampling	7
(4) Dutch Cone Sounding	8
(5) Laboratory Soil Test	8
3-4. Results of Soil Investigation	9
(1) Subsoil Conditions	9
(2) Results of Soil Test	13
1) Dutch Cone Sounding	13
2) Physical Tests	14
3) Unconfined Compression Test	18
4) Consolidation Test	19

Appendix

Boring Logs
Soil Test Data Sheet
Survey Map
Calculation Sheets of Traversing

1. Objectives

Upon request by the Government of the Socialist Republic of the Union of Burma, a feasibility study for the construction of a dry dock was conducted by the Japan International Cooperation Agency (JICA). In order to obtain the data required to determine primary design costs for civil works and buildings, which form the basis for calculating the construction costs of this feasibility study, surveys and soil investigation were carried out between August and December 1982.

This document comprises supplementary data based on the results of the surveys and soil investigation undertaken for the feasibility study report. The surveys and soil investigation were conducted by the Waterways Department and the Construction Corporation (CC), respectively, under the guidance and supervision of the feasibility study team.

2. Surveys

2-1. Survey Area

The surveys were carried out at the proposed project site as designated by the Burma Dockyard Corporation (BDC), including in the area set aside for future expansion.

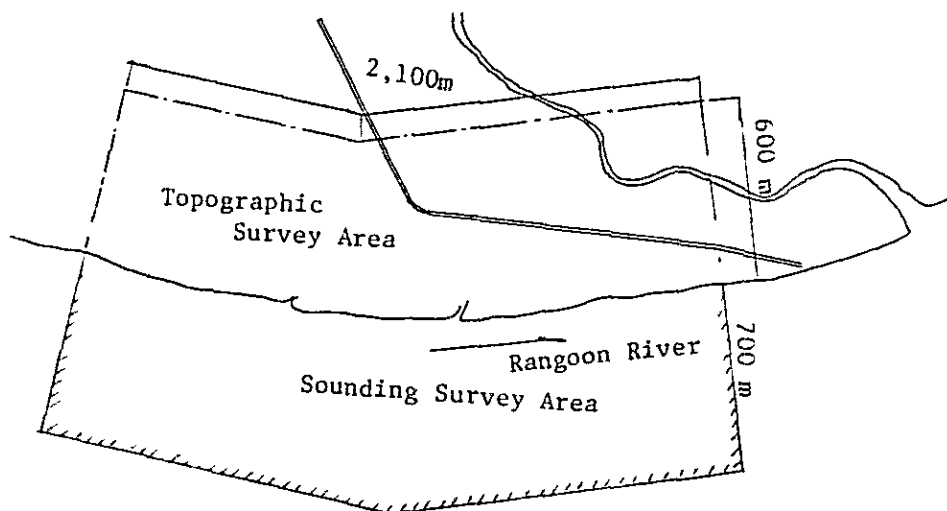


Fig. 2-1 Survey Area

2-2. Items to be Surveyed

- (1) Control Point Surveying and Traversing
- (2) Topographic Survey
- (3) Sounding

2-3. Datum Level

The Rangoon River has 4 tidal gauge points, one of which -- Chockey Point -- lies within the project site. The datum zero at Chockey Point is 0.216m lower than that for the Brooking Street Wharf Point in Rangoon Port.

This survey was performed with Chockey Point taken as datum 0.

2-4. Survey Methods

- (1) Control Surveying and Traversing

Traverse points were established at eleven locations around the periphery of the project area, and the angle and distance between points were measured. In addition, six bench marks were established on the small embankment running north-south through the site. The traverse points and bench marks are shown in Fig. 2-2.

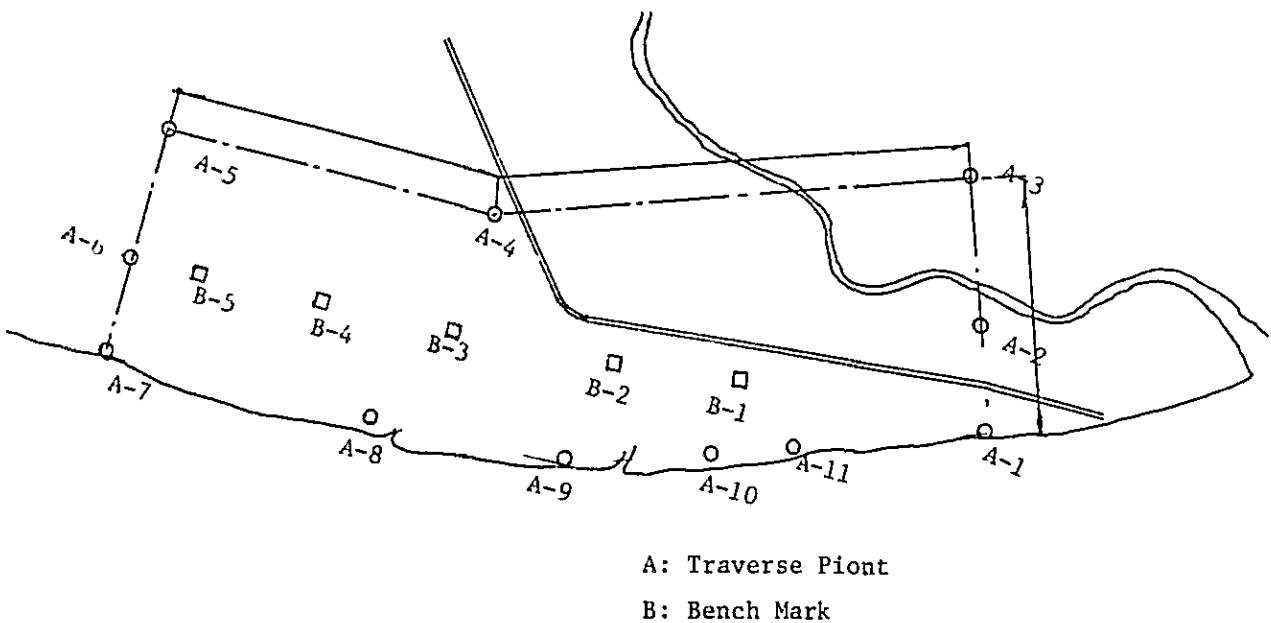


Fig. 2-2. Location of Traverse Points and Bench Marks

.

(2) Topographic Survey (Cross-Leveling)

Following the establishment of the traverse points, a topographic map was prepared based on measurements of elevations and respective distances to the base points. The following items were included in this map:

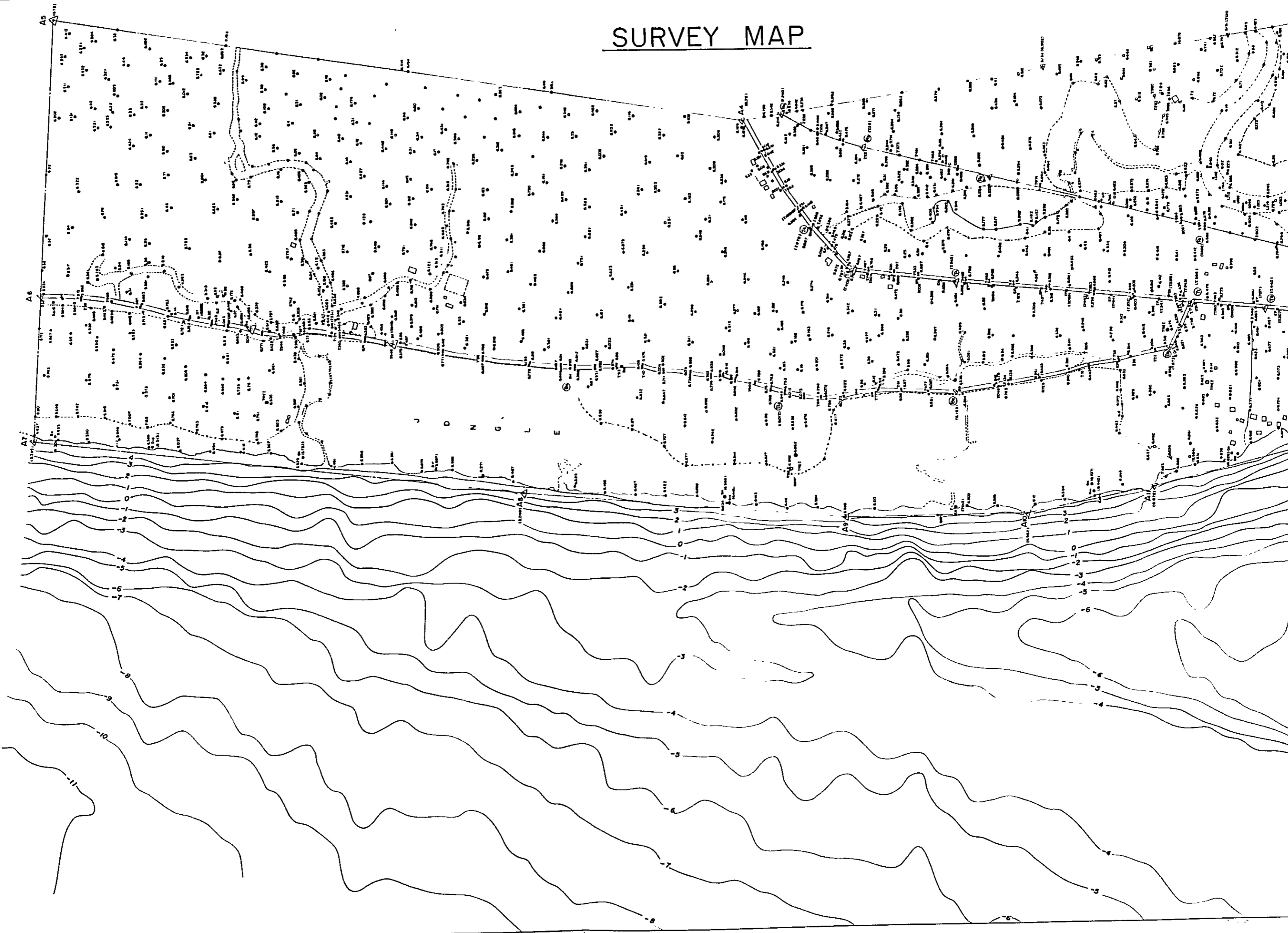
- Offshore line
- Road
- Railway
- Houses
- Embankment
- Paddy fields
- Creeks
- Concrete structures
- Bridge
- Traverse points, bench marks
- Boring and Dutch cone points

(3) Sounding

Sounding was performed using an echo sounder at 50m intervals along the coastline. The survey boat proceeded forward in accordance with guide points set up on the shore line, and measurement of distances was performed by the intersection method relying on two transit points on the shore.

A survey map based on the results of the topographic survey and sounding is given in Fig. 2-3.

SURVEY MAP



SURVEY MAP

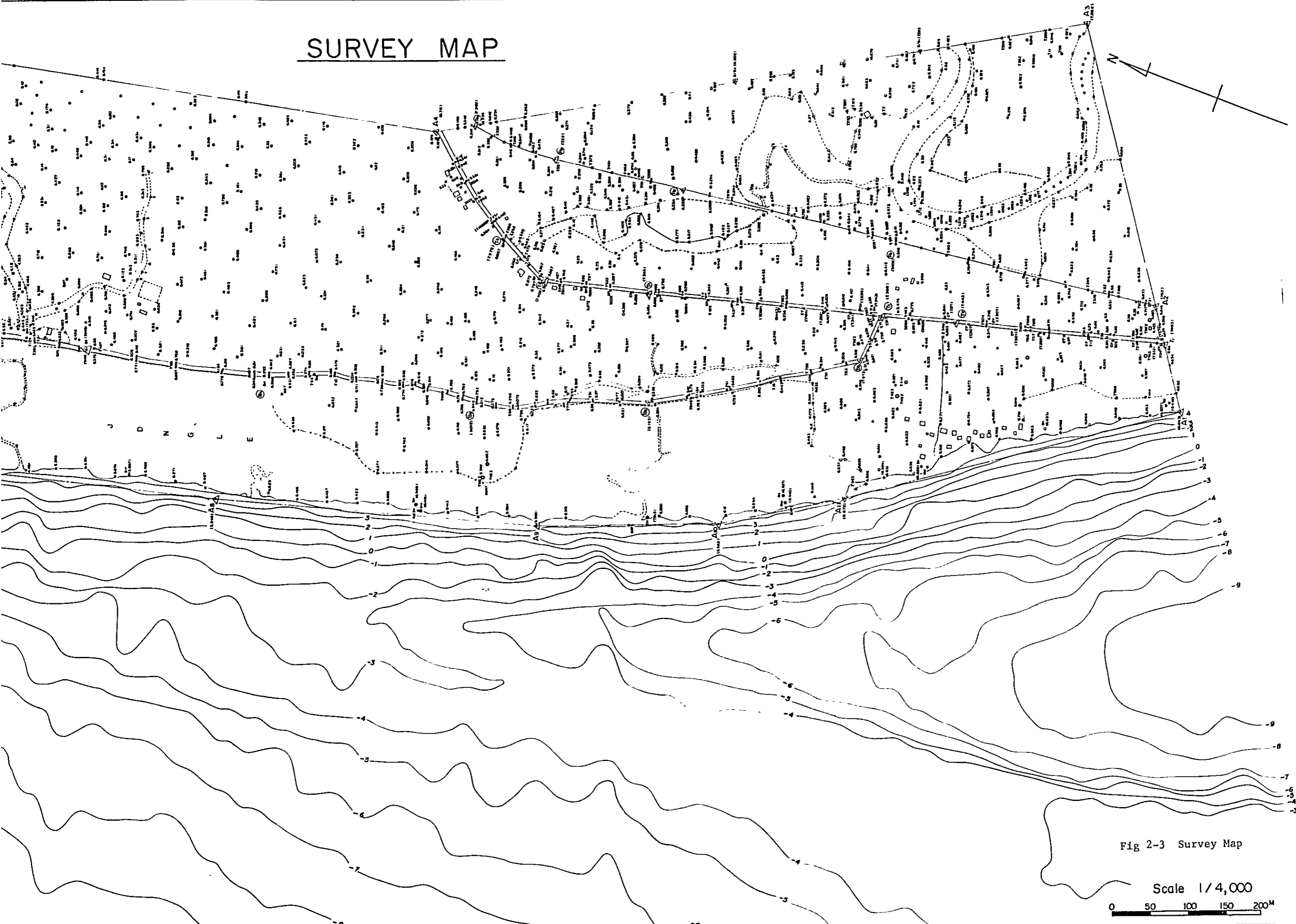
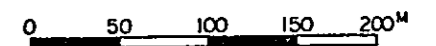


Fig 2-3 Survey Map

Scale 1/4,000



3. Soil Investigation

3-1. Investigation Items and Quantities

The investigation items and quantities are listed in Table 3-1 below.

Table 3-1. Investigation Items and Quantities

<u>Items</u>	<u>Unit</u>	<u>Quantity</u>	
Boring	m	337	10 locations
Standard penetration test	time	322	
Undisturbed sampling	time	19	
Dutch cone sounding	m	525	19 locations
Laboratory soil tests			
Natural moisture content	time	300	
LL, PL	time	50	
Grain size analysis	time	50	
Bulk density	time	13	
Unconfined compression	time	13	
Consolidation	time	10	

3-2. Investigation Site

Fig. 3-1 shows the location map for the soil investigation.

3-3. Investigation Methods

(1) Boring

Boring was conducted using 1 hand-feed boring machine and 1 hydraulic machine. The diameter of the bore holes was set at 66 to 88mm in places where standard penetration tests were performed, and 86 to 116mm in places where thin-walled sampling was performed.

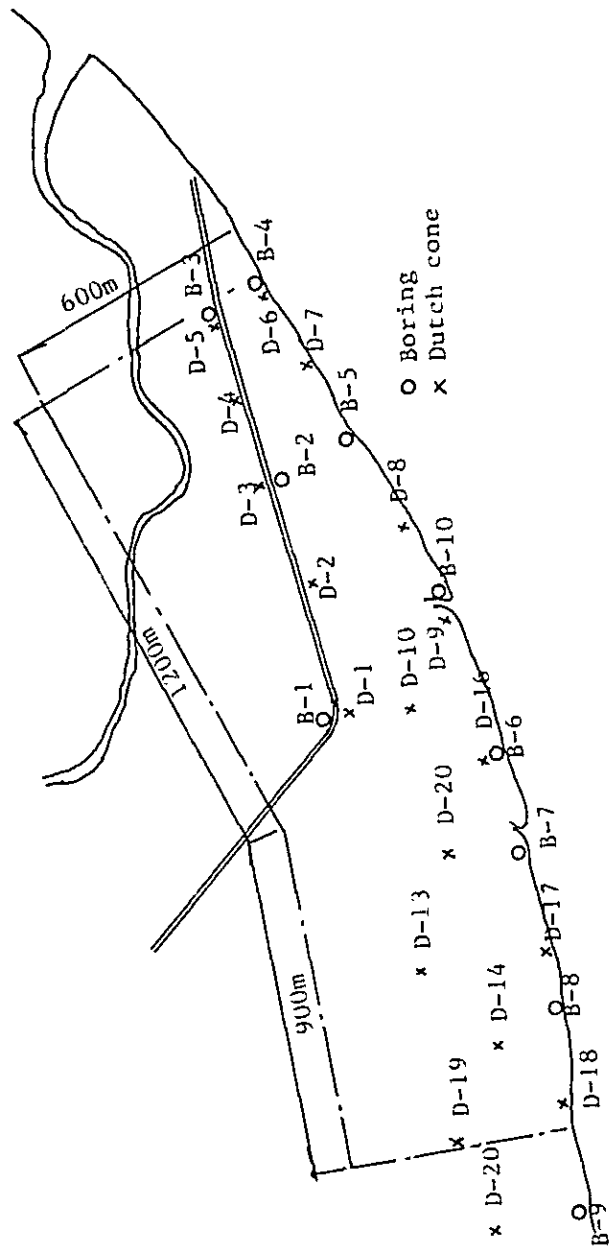


Fig 3-1 Location Map for the Soil Investigation

Bore holes No. 5 and No. 8, where thin-walled sampling was carried out, were drilled using the rotary method. All other bore holes were drilled by the percussion method.

In principle, boring was conducted to a depth exceeding 5m until the hard bearing layer was encountered. However, at bore hole No. 5 an object thought to be stone was hit at a depth of 30m, rendering drilling impossible. Boring was halted at that depth.

(2) Standard Penetration Test (SPT)

In order to extract soil samples and study relative soil strength, the Standard Penetration Test was conducted at all boring points at intervals of 1m.

The test method employed conformed to the standards given in ASTM-D-1586. The standard test method is as follows: the number of blows (N value) is measured so as to penetrate a sampler to a depth of 30cm by dropping a knocking hammer weighing 63.5kg from a height of 75cm. Measurement of the number of blows is taken at intervals of 15cm.

A portion of the samples obtained by the SPT were used for the physical tests, and the remainder were placed in sample bottles and stored at the CC Laboratory.

(3) Undisturbed Sampling

Thin-walled sampling is conducted in order to extract an undisturbed sample to serve as a specimen for mechanical test. A thin-walled sampler of fixed piston type, and a stainless sampling tube with an inside diameter of 75mm and a wall thickness of 1.5mm are used.

(4) Dutch Cone Penetration Test

The Dutch Cone Penetration test is performed as follows:

Cone shape:	Angle 60°; end area 10cm , friction sleeve attached
Measurement pitch:	10cm
Penetration speed:	1cm/sec.
Capacity of proving ring	500kg, 2t

(5) Laboratory Soil Tests

(a) Physical Tests

Physical tests are conducted on the items summarized in Table 4, in accordance with the standards specified in JIS and ASTM.

Table 4. Laboratory Soil Test

<u>Item</u>	<u>Standards for Test</u>
Specific gravity test	JIS-A-1202
Natural water content test	JIS-A-1203
Sieve analysis	JIS-A-1204
Liquid limit test	JIS-A-1205
Plastic limit test	JIS-A-1206

(b) Unconfined Compression Test

This test is performed in accordance with the method summarized below.

Testing method	Conformity with JIS-A-1216
Type of testing apparatus	Machine capable of controlling strain

Configuration and dimensions

of specimen Cylindrical shape, diameter:
5.0cm, height: 12.5cm

Rate of axial compression

loading 1%/minute

Maximum strain Breaking strain +2% or 3%

Summarized test results The coefficient of deformation
is calculated by a strain
corresponding to $E_{50} = 1/2q_u$

(c) Consolidation Test

This test is performed in accordance with the
method described as follows.

Testing method	Conformity with JIS-A-1217
Type of consolidation box	Fixed ring
Dimensions of specimen	Diameter: 6.0cm, height: 2.0cm
Loading pattern	0.1, 0.2, 0.4, 0.8, 1.6, 3.2, 6.4, 12.8 kg/cm ²
Loading time	1 hour per load

3-4. Results of Soil Investigation

(1) Subsoil Conditions

The subsoil conditions in the project area are poor owing to the presence of a soft clay deposit with a thickness of approximately 20 to 25m. In preparing a preliminary design, it will therefore be necessary to take this unfavorable foundation into consideration. It should also be noted that construction of a dockyard on such a poor foundation generally involves higher construction costs compared with dockyard construction on a favorable foundation.

A sketch of the subsoil structure in the project area is shown in Fig. 3-2.

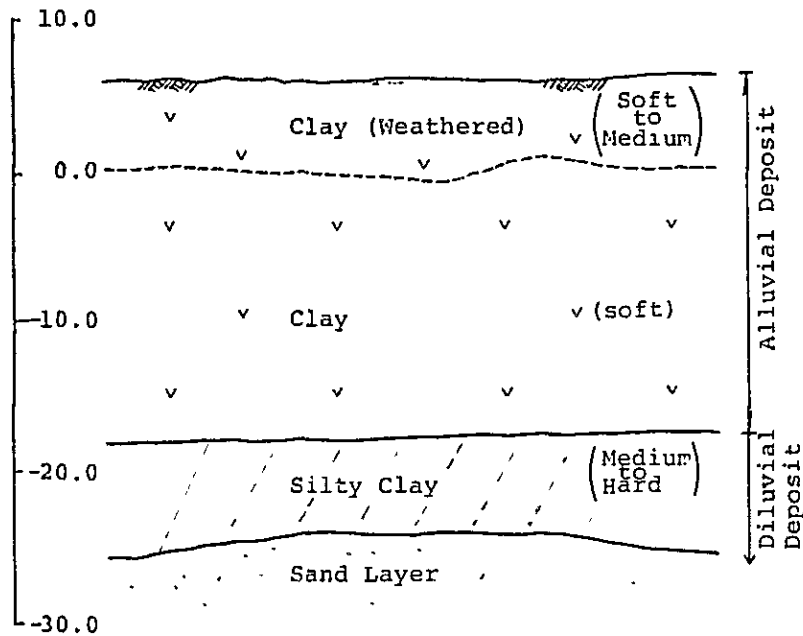


Fig. 3-2. A Sketch of Subsoil Structure

Fig. 3-3 shows a soil profile of the project area based on the results of boring and Dutch cone sounding. The subsoil of the project area comprises, from the top, a clay layer, silty clay layer and a sand layer.

(a) Clay layer

A clay layer deposit is found at a depth of 20 to 25m from the ground surface. The soil in this layer consists of clay featuring high plasticity and cohesiveness. A small amount of decayed plant material (humus) is present. A very thin layer of fine sand lies at the lower part of this layer. No shell fragments are detected. The soil layer is homogeneously composed of uniform clay, and the horizontal continuance of the soil layer is extremely good, thereby indicating that this is a marine or aqueous deposit layer from the alluvial era.

The uppermost portion of this layer is assumed to be a weathered layer to a depth of approximately 7m. While the material comprising this layer is identical to that of the lower portion, it is

relatively harder. Based on the Standard Penetration Test (SPT), the N value of the weathered layer is 2 to 5, while that of the lower part is 0 to 4, indicating that it is soft or medium soft.

(b) Silty clay layer

A relatively hard clay soil layer is found below the clay layer described above, with a thickness ranging from 5 to 10m throughout the project area. A small amount of fine sand is mixed in this layer, and this soil layer is uniform. The color of this layer is gray or milkish white. The upper portion of the subsoil is reddish brown owing to the influence of weathering, thus indicating that this layer at one time formed the ground surface. The N value of this layer ranges from 10 to 20, which is relatively hard for a clay layer. However, it does not have sufficient bearing capacity to support a pile foundation of heavier structures.

(c) Sand layer

The sand layer exists at a depth of approximately 30m from the ground surface. This layer is composed of fine to medium sand, with a small amount of silt mixed in. The soil particles are uniform. The N value of this layer exceeds 50, thus indicating that this layer possesses sufficient bearing capacity to serve as a bearing layer for a pile foundation.

Note

qc Valve and N Valve	Mark of Soil	Name of Soil	Observation
qc	[Symbol]	Top Soil	Embank material of road
		Clay	Soft to Medium Decayed plant contained Very cohesive Homogenous layer
N	[Symbol]	Silty Clay	Stiff Small quantity of fine Sand contained
		Sand	Consist of fine Sand Dense

N valve Result of Standard Penetration Test
 qc Result of Dutch Cone Sounding

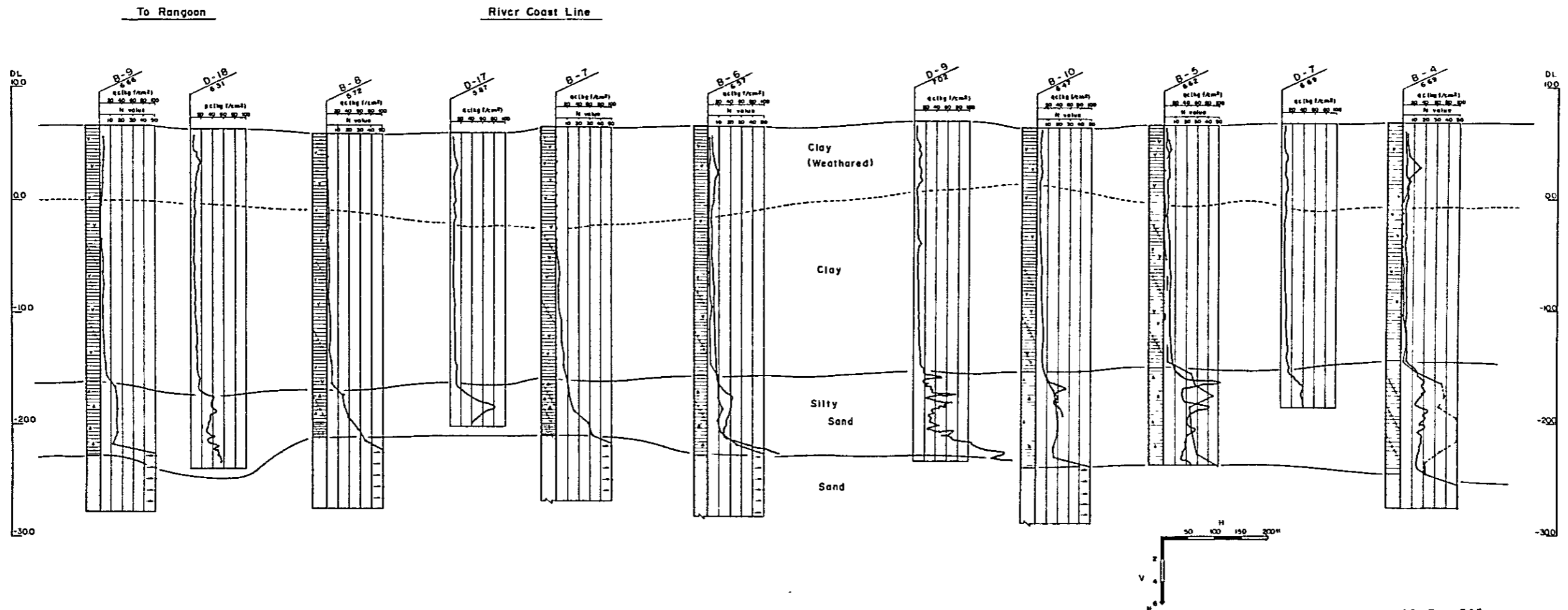
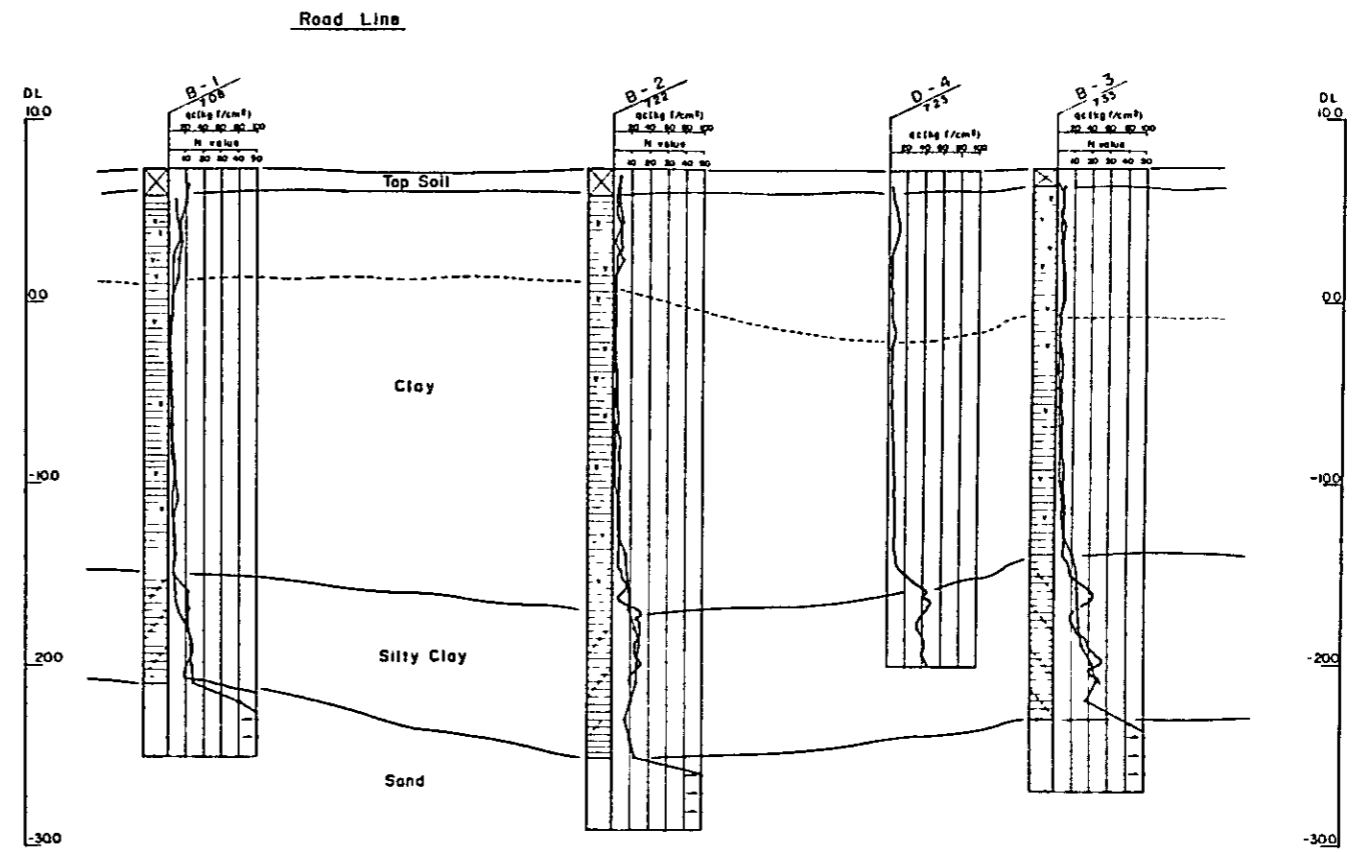


Fig 3-3 Soil Profile

(2) Results of Soil Test

(1) Dutch Cone Sounding

Fig. 3-4 shows the depth distribution of the q_c values for the clay soil layer. A wide spread exists in q_c values in the weathered layer, i.e., the upper area between 0 and approx. 7m deep. The q_c values range from 0.5 to 1.5kg/cm².

In the area below a depth of 7m, the linear q_c value increases with depth; the relationship between depth and q_c value can be expressed using the formula $q_c = 2.8 + 0.35D$.

A favorable correlation exists between the q_c value and cohesion C : $q_c = \alpha \times c$. α refers to the coefficient as determined by the shape of the cone being used. In the present test, a mantle cone was used with $\alpha =$ approx. 15. When α is 15, the cohesion depth distribution can then be expressed by the formula:

$$C = 0.19 + 0.023D \quad (C \text{ kg/cm}^2, D \text{ m}).$$

This cohesion distribution will be discussed further in the next article. The q_c value of the sand layer exceeds 200kg/cm², thereby indicating that this layer offers sufficient bearing capacity to support a pile bearing foundation.

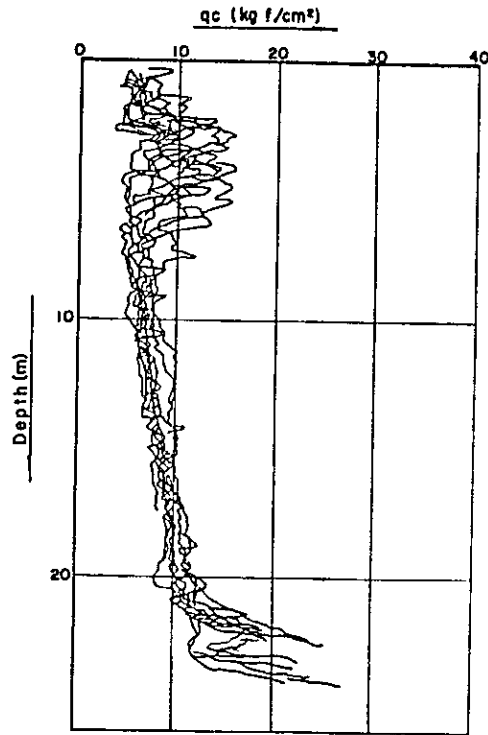


Fig. 3-4. Depth Distribution of q_c

(2) Physical Tests

(a) Natural Moisture Content

Fig. 3-5 shows the depth distribution of the natural moisture content (W_n). The weathered upper portion of the clay layer has a W_n of 30 to 50%; the lower portion, 40 to 60%. In the lower silty clay layer, the W_n ranges from 20 to 30%. As a homogeneous clay layer, the spread is considerably large. The size of this spread is believed to be due to inaccuracy in measurement

resulting from non-uniformity in oven temperature during the drying of the test materials. The W_n of the clay layer is assumed to range between 50 and 60% except for the upper weathered portion; this W_n is relatively low compared with typical clay from the alluvial era. The reason for this low W_n is the disparity in minerals comprising the clay. The clay in the testing area is assumed to be kaolinite or some similar clay mineral.

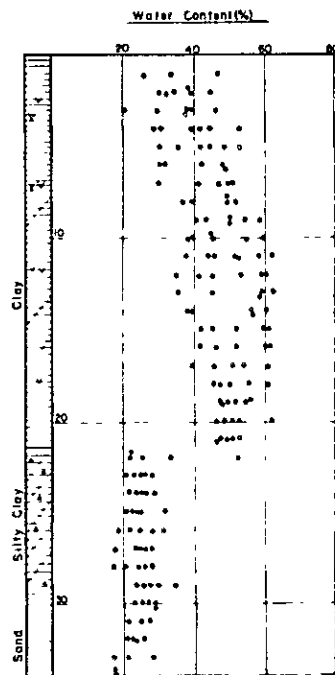


Fig. 3-5. Depth Distribution of W_n

(b) Consistency

Fig. 3-6 shows a plasticity chart based on the results of liquid limit (LL) and plastic limit (PL) tests. Because the measurement of the water content was inaccurate for the reason described above, it is possible that both WL and PL are measured too low. Based

on the test results, the portion of the plasticity chart above line A and with WL greater than 50 is categorized as CH (high-plasticity clay) according to unified classification.

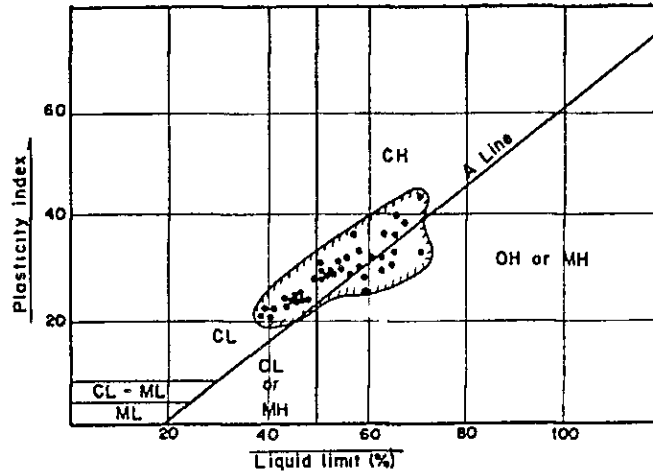


Fig. 3-6. Plasticity Chart

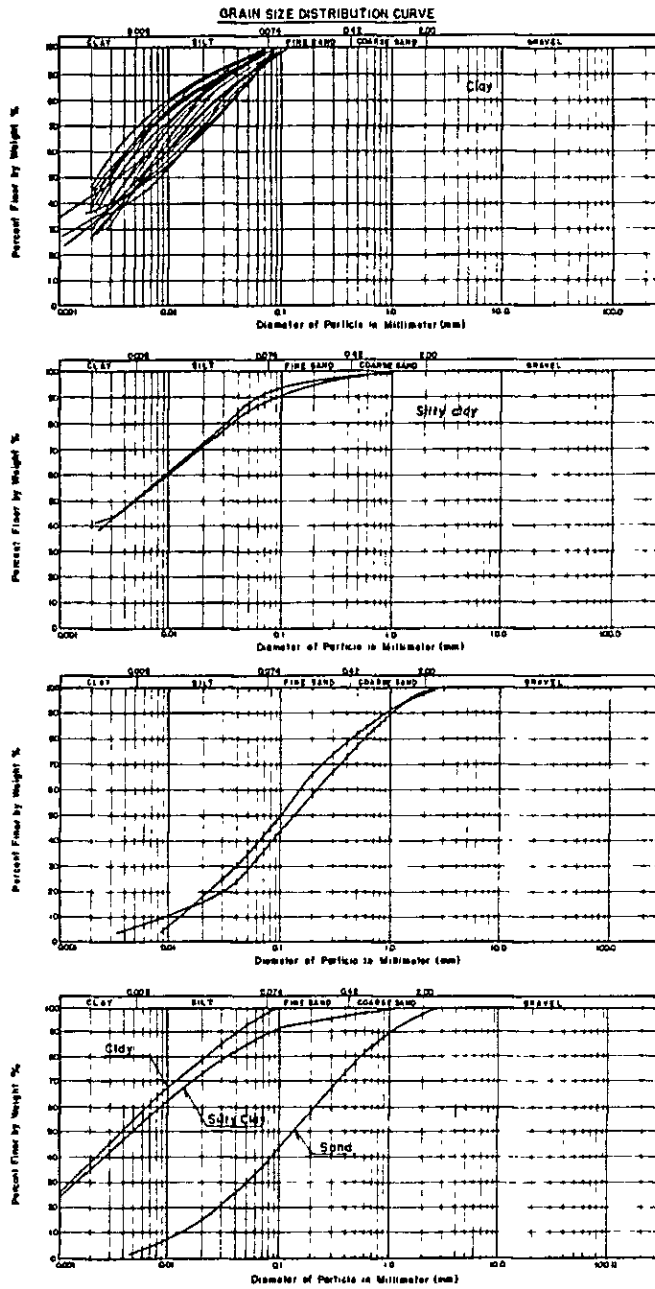
(c) Grain Size Distribution

The grain size distribution for soil in the various soil layers is shown in Fig. 3-7. The major features of the grain size in each soil layer are as follows:

Clay: Contains almost no sand with particle size exceeding 74 . Uniform clay mixed with greater than 50% of clay below 5 .

Silty clay: Contains approx. 10% fine sand and coarse sand. Shows almost identical distribution curve to that of above clay layer.

Sand: Consists of fine sand mixed with approx. 40% silt having particle size below 74 .



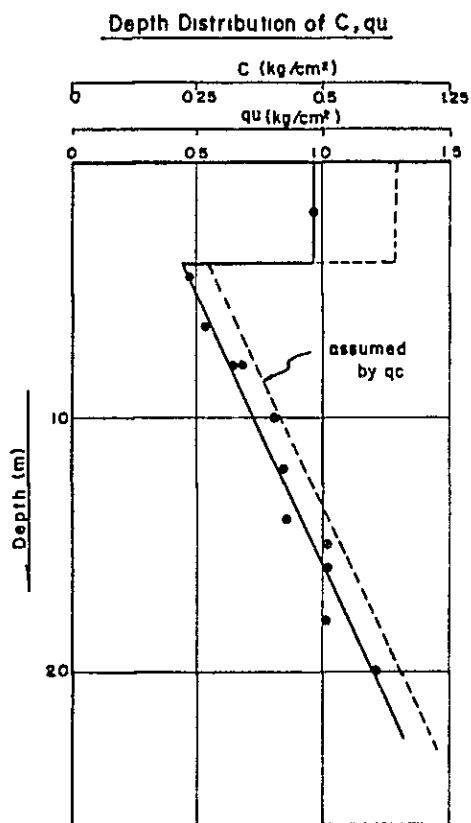
Soil Layer	Gravel %	Coarse Sand %	Fine Sand %	Silt %	Clay %	Coar'd Clay %	Dust %	OC	OC ₂	OC ₃	OC ₄	OC ₅	OC ₆	OC ₇	OC ₈	OC ₉	OC ₁₀	OC ₁₁	OC ₁₂	OC ₁₃	OC ₁₄	OC ₁₅	OC ₁₆	OC ₁₇	OC ₁₈	OC ₁₉	OC ₂₀	
Clay	0	0	2	43	55	25	0.08	0.007	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Silty Clay	0	5	5	43	47	25	1.0	0.009	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—
Sand	5	25	37	24	5	—	3.0	0.2	0.015	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—	—

Fig. 3-7. Grain Size Distribution

(3) Unconfined Compression Test

Fig. 3-8 shows the depth distribution of compression strength (q_u) based on the results of the unconfined compression test. In the figure, in addition to the q_u scale the C scale when cohesion is $C = 1/2 q_u$ is shown.

Fig. 3-8. Depth Distribution of q_u



Cohesion C increases linearly as depth increases, according to the formula $C = 0.13 + 0.024D$ (C kg/cm², D m). The distribution curve of C as assumed from the q_c value of the above Dutch cone sounding is also shown.

The distribution curve of C derived from q_u is almost identical in shape to that of C derived from q_c ; however, the value of C is approximately 0.05kg/cm^2 larger in the case of q_c . This is due to the fact that there is no disturbance involved in the case of the q_c value as the testing is performed in-site. On the other hand, with the q_u the sampling is believed to be unavoidably disturbed due to sampling and trimming of the specimen, thereby resulting in a relatively small measurement for q_u .

(4) Consolidation Tests

(a) e-log P curve

A comparative chart of the e-log P curve is shown in Fig. 3-10. The value curve in the normal consolidation area, i.e., the compression index (C_c), ranges from 0.4 to 0.6. However, as discussed below, because this soil has a large consolidation yield stress (P_y), it is necessary to take P_y into consideration when using C_c to calculate the consolidation settlement.

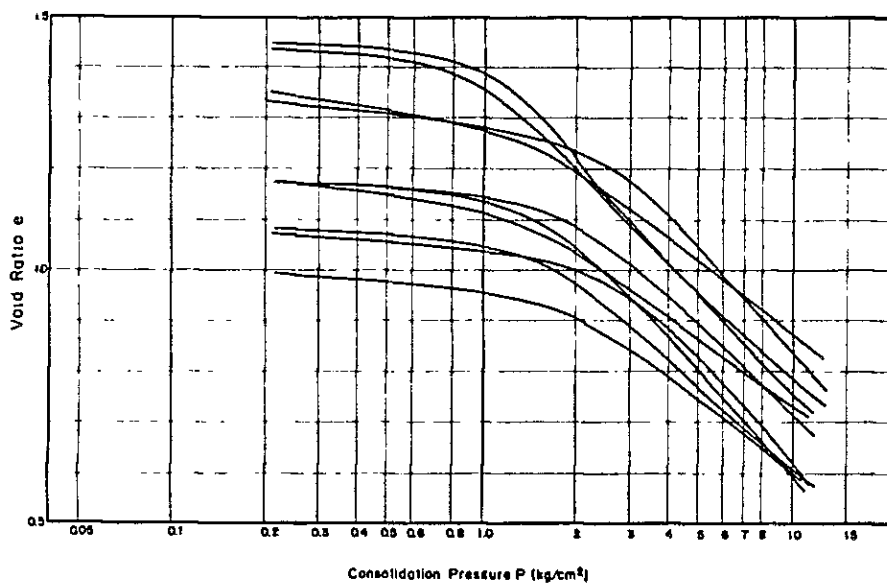


Fig. 3-10 Comparative Chart of e - log p Curve

(b) Coefficient of Consolidation (Cv)

Fig. 3-11 shows the comparative chart of Cv. The Cv for a consolidation yield stress (Py) of 1-2kg/cm² is 0.07-0.2cm²/min, which is a normal value for a high-plasticity clay.

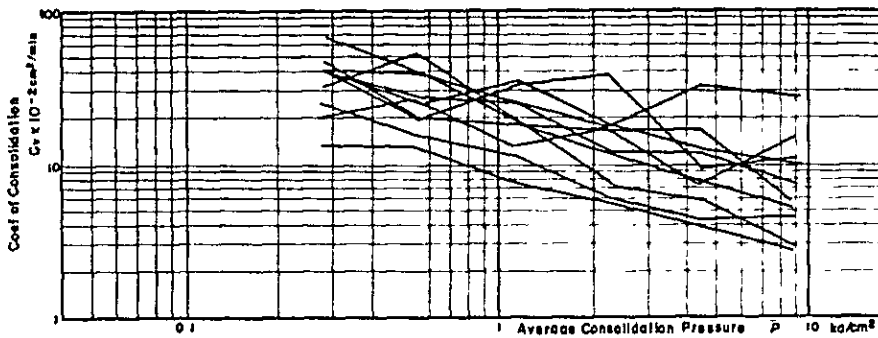


Fig. 3-11 Comparative Chart of Cv

(c) Coefficient of Volume Compressibility (Mv)

A comparative chart of Mv is shown in Fig. 3-12. The value of Mv for Py is 0.02-0.07cm², which is small for a high plasticity clay from the alluvial era. This indicates relatively small compressibility.

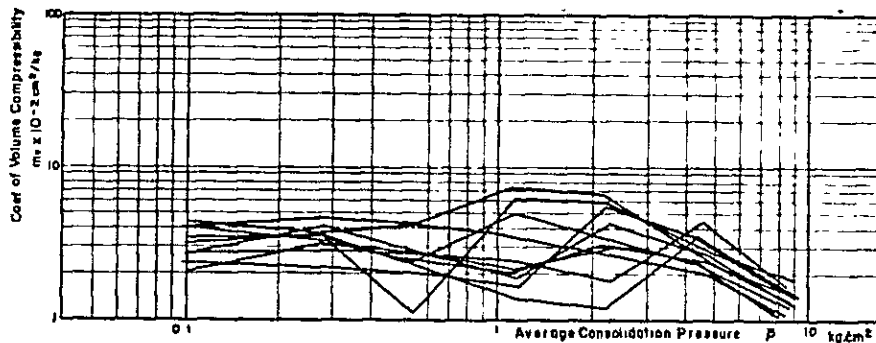


Fig. 3-12 Comparative Chart of Mv

(d) Consolidation Yield Stress (P_y)

The depth distribution of P_y is shown in Fig. 3-13. The figure shows the effective overburden load (P_o) line when the bulk density of the soil is calculated at 1.70. It is generally assumed that P_o and P_y coincide in the case of normal consolidated clay. However, the P_y and P_o coincide for clay in which a short aging period has elapsed after sediment; normally, P_y is only slightly larger than P_o . The clay in this layer shows a P_y considerably larger than its P_o , and the clay appears to be preconsolidated.

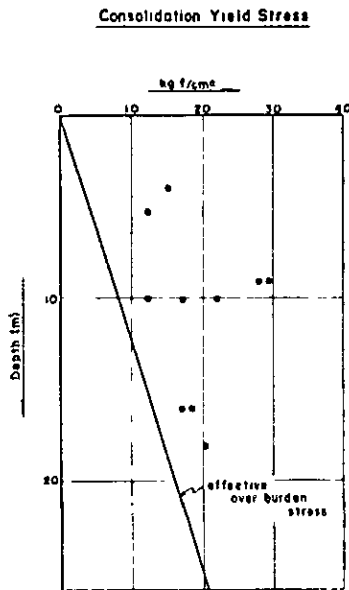


Fig. 3-13 Depth Distribution of P_y

In view of the geographical conditions of the site, however, it is improbable that a surcharge has been loaded on the site subsoil in the past. For this reason, it is theorized that the cause for the P_y greatly exceeding the P_o is either a lengthy aging period after sediment or quasi-preconsolidation effect due to secondary consolidation or chemicals in the clay minerals.

BORING LOGS

BORING LOG

BORE HOLE NO. B-1

TITLE Dry Dockyard Project

LOCATION Thilawa

BORING METHOD Percussion

OPERATED BY

DATE

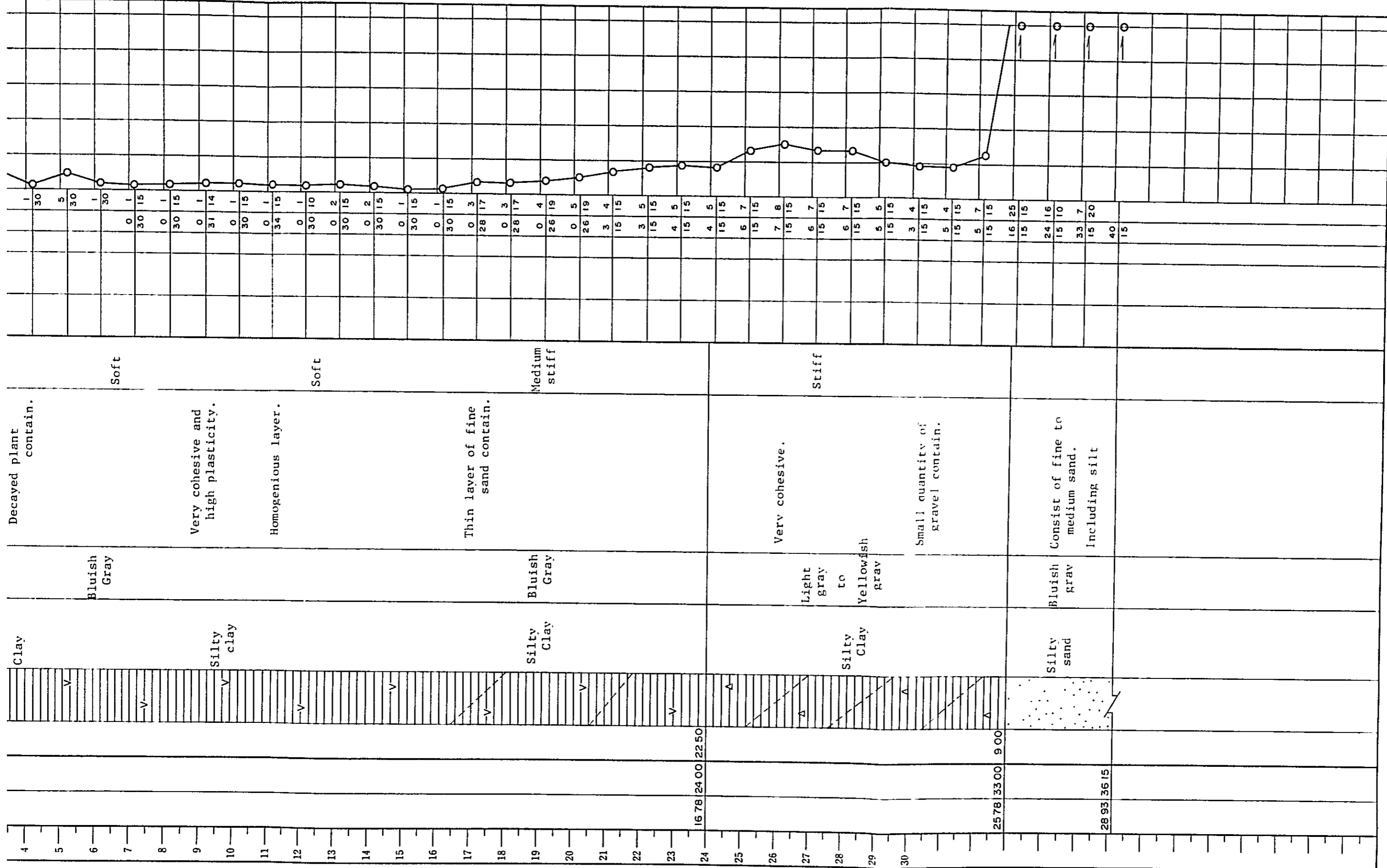
SAMPLING METHOD

CHECKED BY Suzuki

GROUND ELEVATION 7.08

SCALE (m)	ELEVATION (m)	DEPTH	THICKNESS OF LAYER (m)	SOIL TYPE		COLOR	OBSERVATION	RELATIVE DENSITY OR CONSISTENCY	STANDARD PENETRATION TEST				DEPTH (m)	NUMBER OF BLOWS	N-VALUE SHOWING NUMBER OF BLOWS PER 30cm IN GRAPH			DEPTH (m)	SAMPLING	
				GRAPHIC SYMBOL	NAME OF SOIL				NO OF BLOWS PER 10cm	NO OF BLOWS PER 20 cm	NO OF BLOWS PER 30 cm	DEPTH (m)								
1	5.58	1.50	1.50	X	Top soil	Reddish Brown	Including some gravel	Stiff												
2				V	Clay	Reddish Brown	High plasticity.	Stiff to Soft												
3				V		Very cohesive.														
4				V		High plasticity.														
5				V		Including small quantity of decayed plant.			Soft											
6				V		Very homogenous.														
7				V		Small quantity of fine sand contain.														
8				V		Clay	Bluish Gray	High plasticity.												
9				V																
10				V																
11				V																
12				V																
13				V																
14				V																
15				V																
16				V																
17				V																
18				V	Clay	Bluish Gray	High plasticity.	Stiff to Medium Stiff												
19				V																
20				V																
21				V																
22				V																
23				V																
24				V																
25				V																
26				V																
27				V		Sand	Reddish Brown	Very cohesive.	Stiff											
28				V			Small quantity of gravel contain.													
29				V			Thin layer of fine sand contain.													
30				V			Consist of fine to medium sand.													

NOTE



NOTE

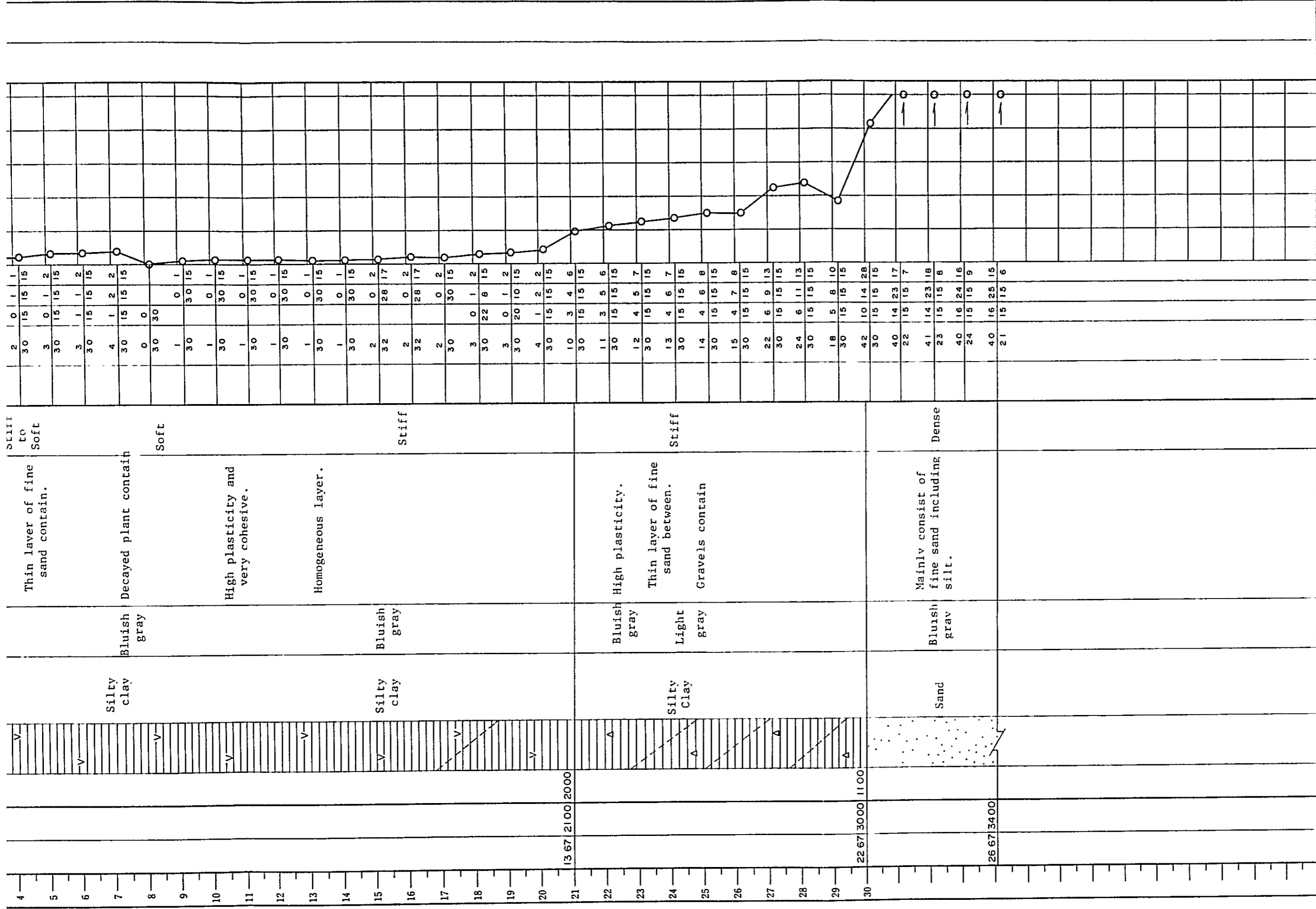
BORING LOG

TITLE Dry Dockyard Project BORE HOLE NO. B - 3
 LOCATION Thilawa BORING METHOD Percussion OPERATED BY _____
 DATE _____ SAMPLING METHOD _____ CHECKED BY Suzuki

GROUND ELEVATION 7.33

SCALE (m)	ELEVATION (m)	DEPTH	THICKNESS OF LAYER (m)	SOIL TYPE		COLOR	OBSERVATION	RELATIVE DENSITY OR CONSISTENCY	STANDARD PENETRATION TEST				DEPTH (m)	NUMBER OF BLOWS	N-VALUE SHOWING NUMBER OF BLOWS PER 30cm IN GRAPH			DEPTH (m)	SAMPLING
				GRAPHIC SYMBOL	NAME OF SOIL				NO OF BLOWS PER 10cm	NO OF BLOWS PER 20cm	NO OF BLOWS PER 30cm	DEPTH (m)			NO OF BLOWS				
1	6.33	1.00	1.00	X	Top soil	Reddish Brown	Gravels contain	Stiff	4	1	2	2							
2				V	Clay	Reddish Brown	Very cohesive.	Stiff to Soft	30	15	15	15							
3				V			Thin layer of fine sand contain.			3	0	1	2						
4				V					30	15	15	15							
5				V					2	0	1	1							
6				V					30	15	15	15							
7				V	Silty clay	Bluish gray	Decayed plant contain	Soft	2	0	1	1							
8				V						30	15	15	15						
9				V					4	1	2	2							
10				V					30	15	15	15							
11				V					0	0									
12				V					30	30									
13				V					1	0	1								
14				V					30	15	15	15							
15				V	Silty clay	Bluish gray	High plasticity and very cohesive.	Stiff	30	15	15	15							
16				V			Homogeneous layer.			0	2	28	17						
17				V					2	0	2								
18				V					32	28	17								
19				V					2	0	2								
20				V					30	15	15	15							
21				V					30	22	8	15							
22	13.67	21.00	20.00						3	0	1	2							
23				V					30	20	10	15							
24				V					4	1	2	2							
25				V					30	15	15	15							
26				V					10	3	4	6							
27				V					30	15	15	15							
28				V					30	15	15	15							
29				V					11	3	5	6							
30	22.67	30.00	11.00	V					30	15	15	15							
				V					30	15	15	15							
				V					12	4	5	7							
				V					30	15	15	15							
				V					15	4	7	8							
				V					30	15	15	15							
				V					22	6	9	13							
				V					30	15	15	15							
				V					24	6	11	13							
				V					30	15	15	15							
				V					18	5	8	10							
				V					30	15	15	15							
				V					42	10	14	28							
				V					30	15	15	15							
				V					40	14	23	17							
				V					22	15	15	7							
				V					41	14	23	18							
				V					23	15	15	8							
				V					40	16	24	16							
				V					24	15	15	9							

26.67 34.00



NOTE

BORING LOG

BORE HOLE NO. B - 4

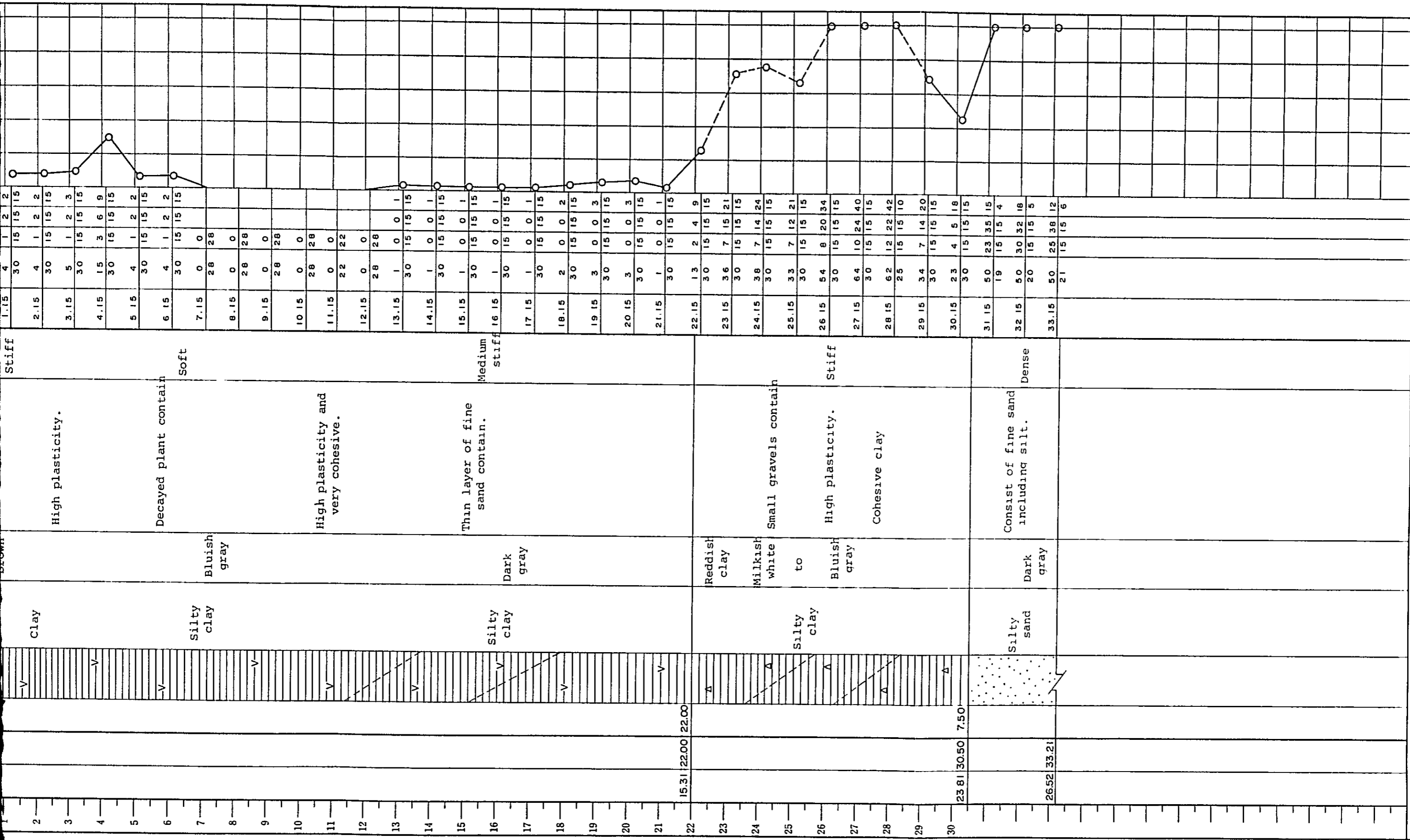
TITLE Dry Dockyard Project
 LOCATION Thilawa
 DATE

BORING METHOD Percussion
 SAMPLING METHOD

OPERATED BY
 CHECKED BY

GROUND ELEVATION 6.69

SCALE (m)	ELEVATION (m)	DEPTH	THICKNESS OF LAYER (m)	SOIL TYPE		COLOR	OBSERVATION	RELATIVE DENSITY OR CONSISTENCY	STANDARD PENETRATION TEST				DEPTH (m)	NUMBER OF BLOWS	N-VALUE SHOWING NUMBER OF BLOWS PER 30cm IN GRAPH			DEPTH (m)	SAMPLING
				GRAPHIC SYMBOL	NAME OF SOIL				NO OF BLOWS	10 cm	20 cm	30 cm			DEPTH (m)	NUMBER OF BLOWS			
1		1.15			Reddish brown	Weathered layer	Stiff		4	1	2	2							
2		2.15		V	Clay	High plasticity.			30	15	15	15							
3		3.15							4	1	2	2							
4		4.15		V					30	15	15	15							
5		5.15				Decayed plant contain	Soft		5	1	2	3							
6		6.15		V					30	15	15	15							
7		7.15			Bluish gray				4	1	2	2							
8		8.15							30	15	15	15							
9		9.15		V					0	0	0								
10		10.15				High plasticity and very cohesive.			28	28									
11		11.15		V					0	0									
12		12.15							22	22									
13		13.15							0	0									
14		14.15		V					28	28									
15		15.15			Silty clay	Thin layer of fine sand contain.	Medium stiff		1	0	0	1							
16		16.15		V					30	15	15	15							
17		17.15			Dark gray				0	0									
18		18.15		V					30	15	15	15							
19		19.15							2	0	0	2							
20		20.15							30	15	15	15							
21		21.15		V					3	0	0	3							
22		22.00	15.31						30	15	15	15							
23		23.15		V	Reddish clay				13	2	4	9							
24		24.15		V	Milky white	Small gravels contain			30	15	15	15							
25		25.15		V	to				36	7	15	21							
26		26.15		V	Bluish gray	High plasticity.	Stiff		30	15	15	15							
27		27.15		V		Cohesive clay			54	8	20	34							
28		28.15		V					30	15	15	15							
29		29.15		V					64	10	24	40							
30		30.15		V					30	15	15	15							
31		31.15							25	15	15	10							
32		32.15			Dark gray	Consist of fine sand including silt.	Dense		62	12	22	42							
33		33.15			Silty sand				25	15	15	5							
		26.52	33.21						50	25	38	12							



NOTE

BORING LOG

BORE HOLE NO. B - 5

TITLE Thilawa Dry Dock Project

LOCATION B-5 BORING METHOD Rotary OPERATED BY

OPERATED BY

DATE _____ SAMPLING METHOD Thin-wall CHECKED BY Suzuki

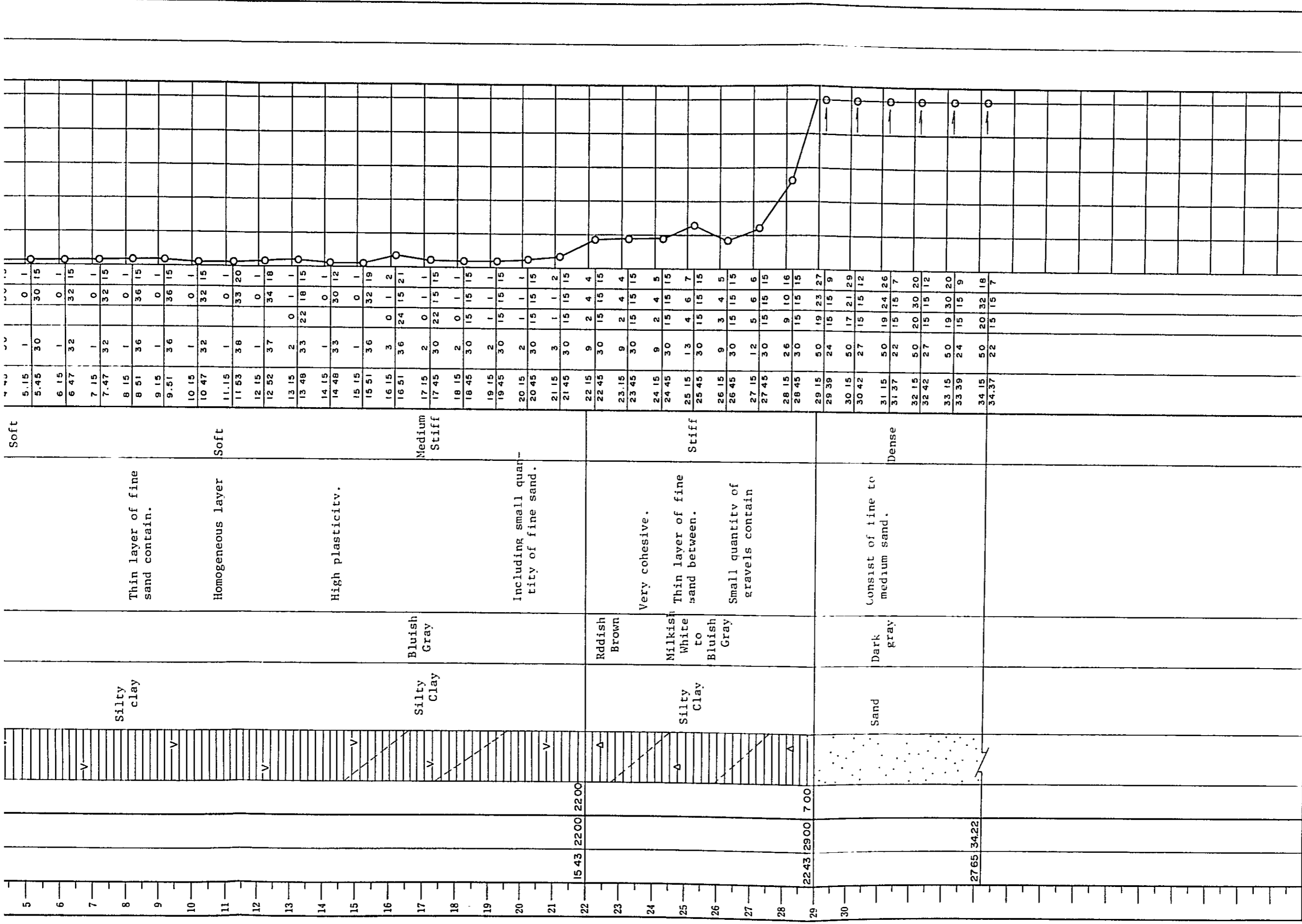
CHECKED BY Suzuki

Sampling

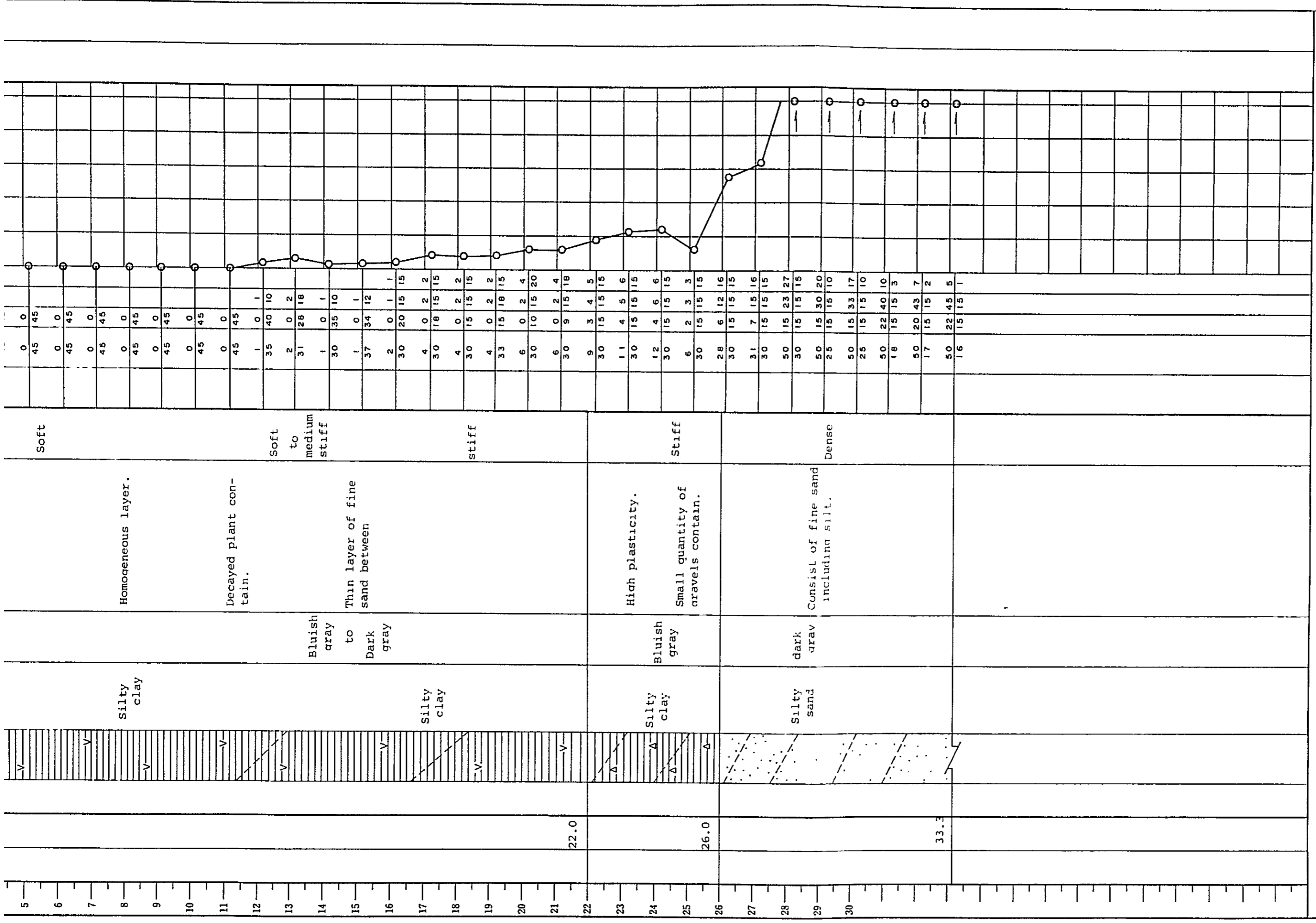
GROUND ELEVATION 6.62

SCALE (m)	ELEVATION (m)	DEPTH	THICKNESS OF LAYER (m)	SOIL TYPE		COLOR	OBSERVATION	RELATIVE DENSITY OR CONSISTENCY	DEPTH (m)	NUMBER OF BLOWS	STANDARD PENETRATION TEST			DEPTH (m)	SAMPLE NO
				GRAPHIC SYMBOL	NAME OF SOIL						NO. OF BLOWS PER 10cm	NO. OF BLOWS PER 20 cm	NO. OF BLOWS PER 30 cm		
1				V	Clay	Reddish Brown		Medium Stiff							
2				V	Clay										
3				V	Clay	Bluish Gray	High plasticity.	Soft							
4				V	Clay		Very cohesive.								
5				V	Clay										
6				V	Clay										
7				V	Clay										
8				V	Clay		Decayed plant contain.								
9				V	Clay										
10				V	Clay										
11				V	Silty Clay	Bluish Gray		Soft							
12				V	Silty Clay										
13				V	Silty Clay										
14				V	Silty Clay	Bluish Gray									
15				V	Silty Clay										
16				V	Silty Clay		Thin layer of fine sand between.	Medium stiff							
17				V	Silty Clay										
18				V	Silty Clay										
19				V	Silty Clay										
20				V	Silty Clay										
21				V	Silty Clay										
22	14.88	21.50	21.50	Δ	Silty Clay	Reddish Brown	Small quantity of gravels contain.	Stiff							
23				Δ	Silty Clay										
24				Δ	Silty Clay		High plasticity								
25				Δ	Silty Clay	Bluish Gray									
26				Δ	Silty Clay										
27				Δ	Silty Clay										
28				Δ	Silty Clay										
29				Δ	Silty Clay										
30	24.53	30.15		Δ	Silty Clay		hard ston, boring can not be								

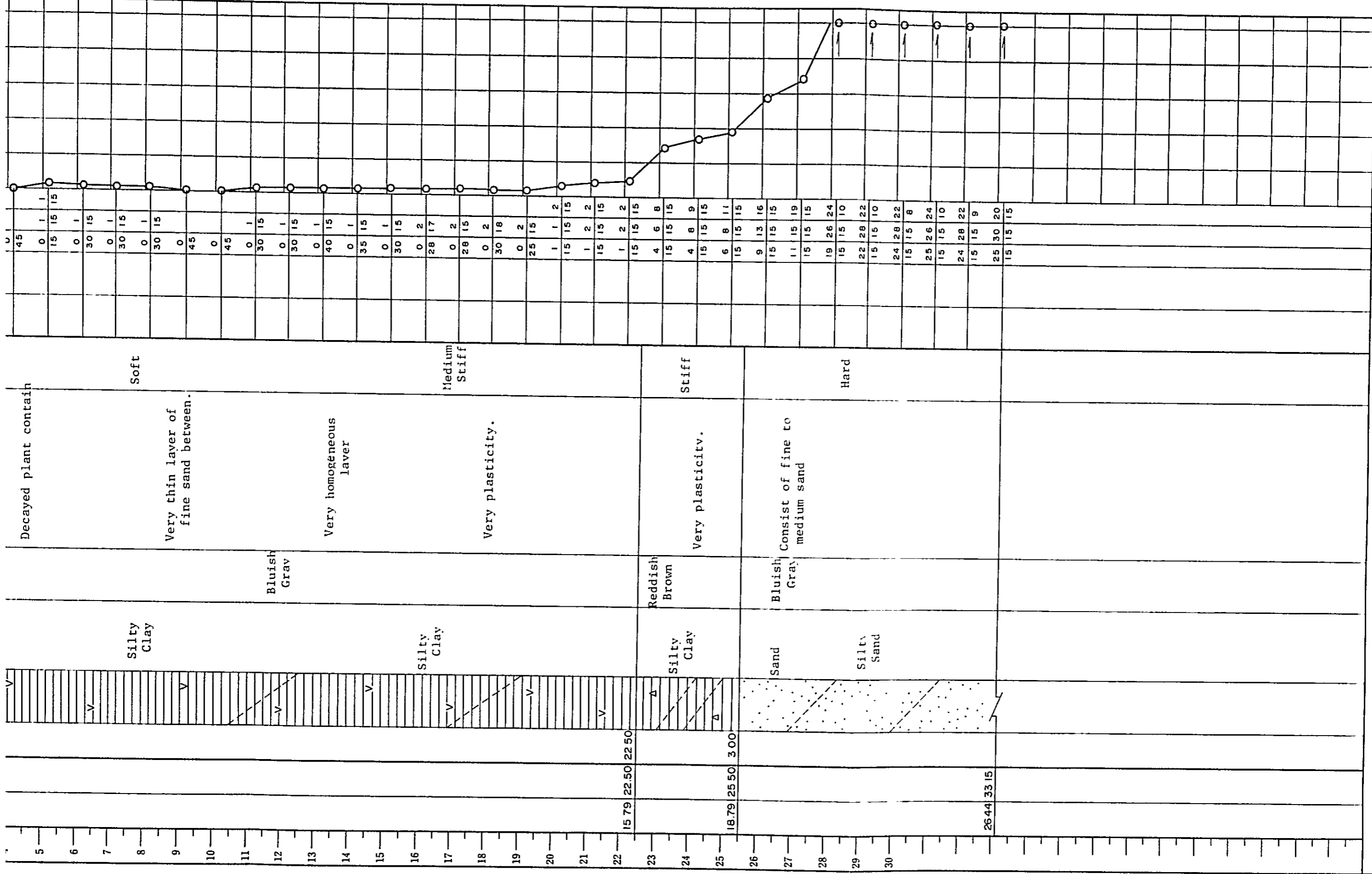
NOTE



NOTE



NOTE



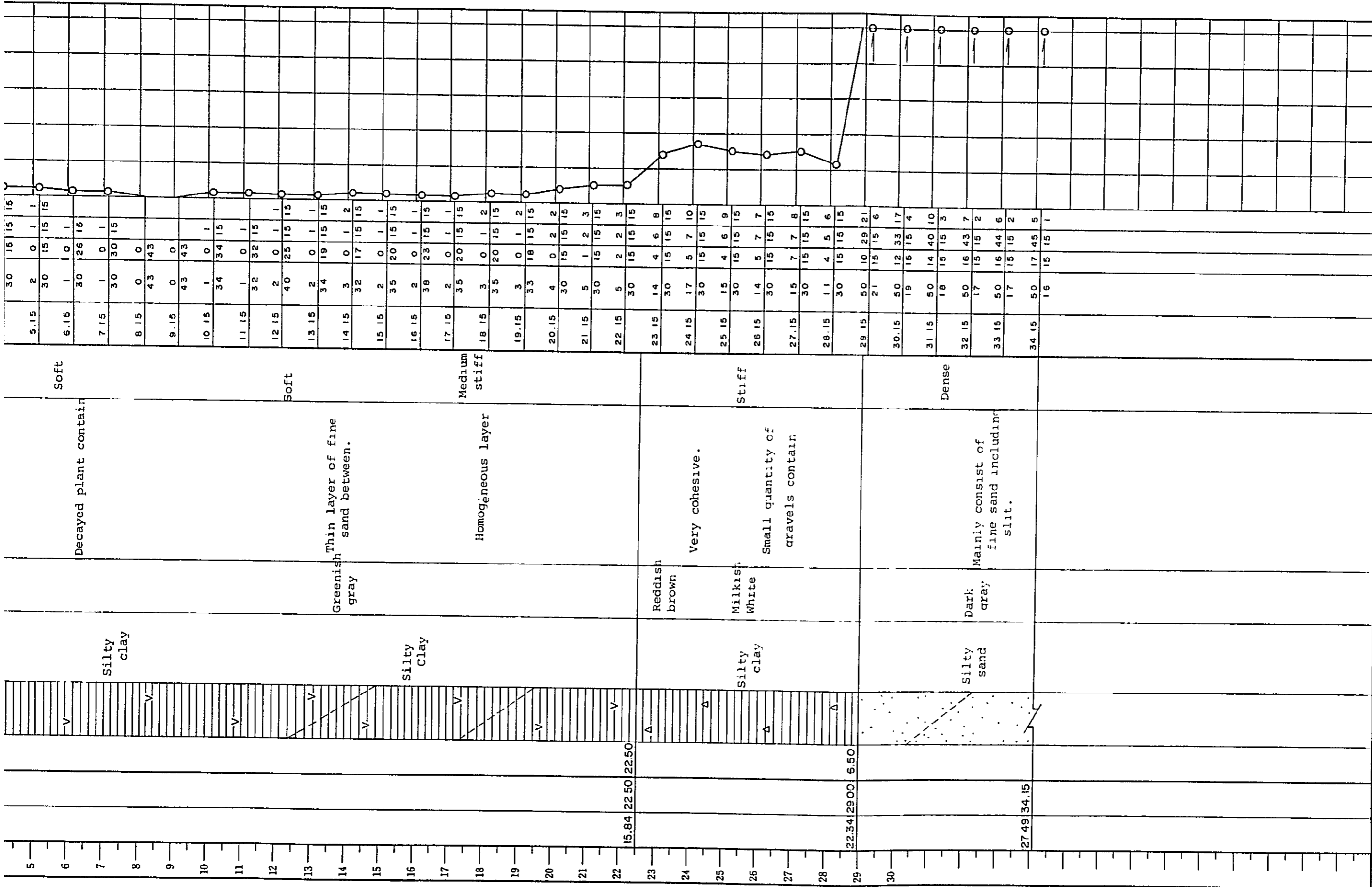
NOTE

BORING LOG

TITLE Dry Dockyard Project BORE HOLE NO. B-9
 LOCATION Thilawa BORING METHOD Percussion OPERATED BY _____
 DATE _____ SAMPLING METHOD _____ CHECKED BY _____

GROUND ELEVATION 6.66

SCALE (m)	ELEVATION (m)	DEPTH	THICKNESS OF LAYER (m)	SOIL TYPE		COLOR	OBSERVATION	RELATIVE DENSITY OR CONSISTENCY	STANDARD PENETRATION TEST				DEPTH (m)	SAMPLING
				GRAPHIC SYMBOL	NAME OF SOIL				NUMBER OF BLOWS	NO OF BLOWS PER 10 cm	N-VALUE SHOWING NUMBER OF BLOWS PER 30cm IN GRAPH			
1		1.15		Clay	Reddish brown	Medium stiff	Very cohesive and high plasticity.	Medium stiff	3	0	1	2		
2		2.15							30	15	15	15		
3		3.15		Dark gray		Soft	Decayed plant contain	Soft	3	0	1	2		
4		4.15							30	15	15	15		
5		5.15		Silty clay		Soft		Soft	2	0	1	1		
6		6.15							30	15	15	15		
7		7.15		Silty clay		Soft		Soft	1	0	1	1		
8		8.15							30	30	15	15		
9		9.15		Silty Clay		Medium stiff	Homogeneous layer	Medium stiff	0	0				
10		10.15							43	43				
11		11.15		Silty Clay		Medium stiff	Homogeneous layer	Medium stiff	0	0				
12		12.15							32	32	15	15		
13		13.15		Silty Clay		Medium stiff	Homogeneous layer	Medium stiff	2	0	1	1		
14		14.15							34	19	15	15		
15		15.15		Silty Clay		Medium stiff	Homogeneous layer	Medium stiff	3	0	1	2		
16		16.15							32	17	15	15		
17		17.15		Silty Clay		Medium stiff	Homogeneous layer	Medium stiff	2	0	1	1		
18		18.15							35	20	15	15		
19		19.15		Silty Clay		Medium stiff	Homogeneous layer	Medium stiff	2	0	1	1		
20		20.15							38	23	15	15		
21		21.15		Silty Clay		Medium stiff	Homogeneous layer	Medium stiff	3	0	1	2		
22		22.15							35	20	15	15		
23	15.84	22.50	22.50	Silty Clay		Medium stiff	Homogeneous layer	Medium stiff	3	0	1	2		
24		23.15							35	20	15	15		
25		24.15		Silty clay		Stiff	Very cohesive.	Stiff	3	0	1	2		
26		25.15							33	18	15	15		
27		26.15		Silty clay		Stiff	Very cohesive.	Stiff	4	0	2	2		
28		27.15							30	15	15	15		
29	22.34	29.00	6.50	Silty sand		Dense	Mainly consist of fine sand including	Dense	5	2	2	3		
30		30.15							30	15	15	15		
31		31.15		Silty sand		Dense	Mainly consist of fine sand including	Dense	5	7	7	8		
32		32.15							30	15	15	15		
33		33.15		Silty sand		Dense	Mainly consist of fine sand including	Dense	1	4	5	6		
									30	15	15	15		



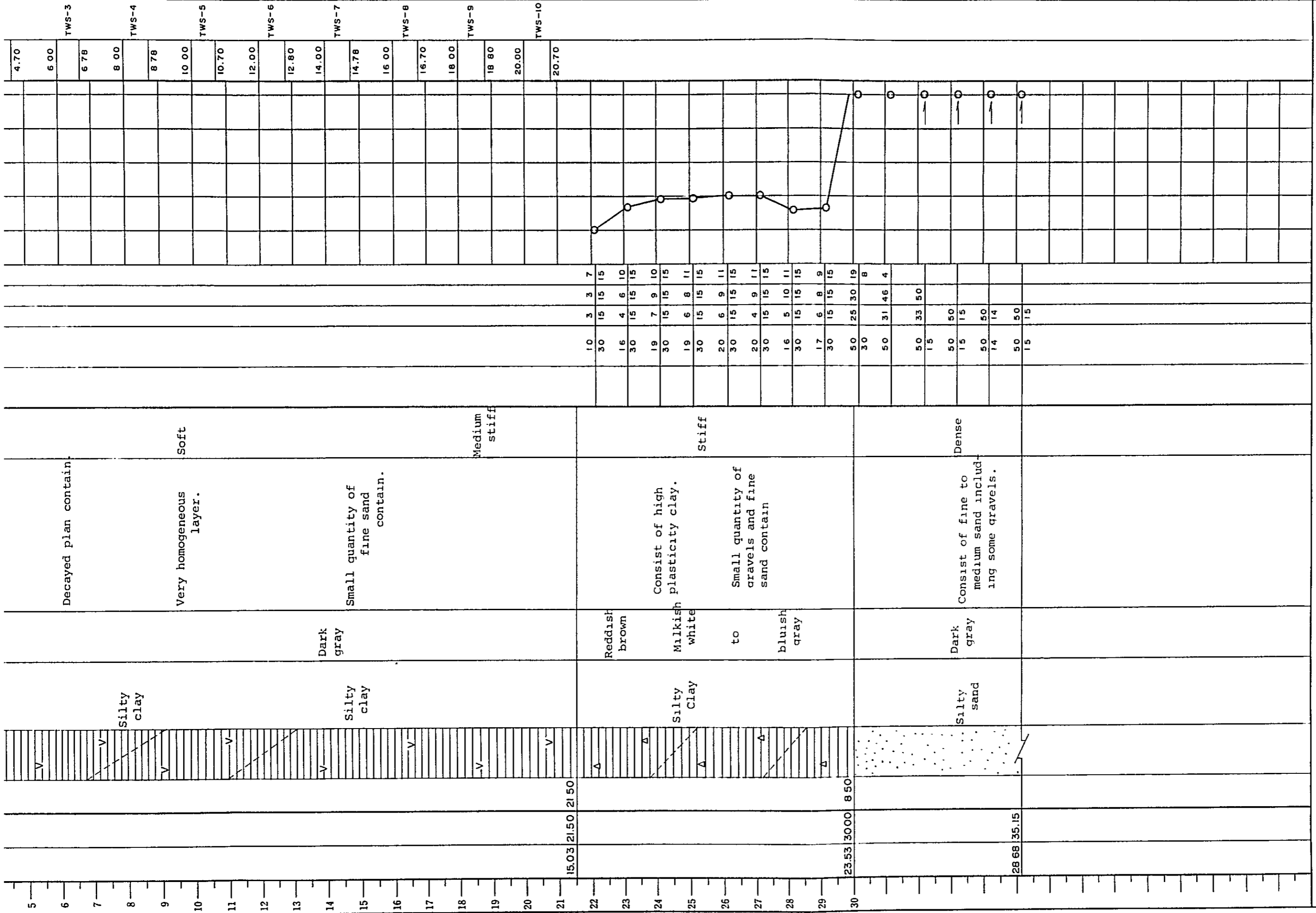
NOTE

BORING LOG

TITLE Dry Dockyard Project BORE HOLE NO. B - 10
 LOCATION Thilawa BORING METHOD Rotary OPERATED BY _____
 DATE 6 47 SAMPLING METHOD Thin-walled CHECKED BY _____

GROUND ELEVATION

SCALE (m)	ELEVATION (m)	DEPTH	THICKNESS OF LAYER (m)	SOIL TYPE		COLOR	OBSERVATION	RELATIVE DENSITY OR CONSISTENCY	STANDARD PENETRATION TEST.				DEPTH (m)	SAMPLING DEPTH (m)	SAMPLE NO
				GRAPHIC SYMBOL	NAME OF SOIL				NUMBER OF BLOWS	NO OF BLOWS FOR 10cm	NO OF BLOWS FOR 20cm	NO OF BLOWS FOR 30cm			
1															
2				V	Clay	Reddish Brown	Highly weathered	Medium stiff							
3				V		Bluish grey	Very cohesive and high plasticity	Soft							TWS-1
4				V											
5				V			Decayed plan contain.								TWS-2
6				V											
7				V	Silty clay			Soft							TWS-3
8				V											
9				V			Very homogeneous layer.								TWS-4
10				V											
11				V		Dark gray	Small quantity of fine sand contain.								TWS-5
12				V											
13				V											TWS-6
14				V											
15				V	Silty clay										TWS-7
16				V											
17				V											TWS-8
18				V											
19				V				Medium stiff							TWS-9
20				V											
21				V											TWS-10
22	15.03	21.50	21.50	Δ		Reddish brown			10	3	7				
23				Δ					30	15	15				
24				Δ					16	4	10				
25				Δ	Silty Clay	Milky white	Consist of high plasticity clay.		30	15	15				
26				Δ					19	7	10				
27				Δ					30	15	15				
28				Δ		to bluish gray	Small quantity of gravels and fine sand contain		30	15	15				
29				Δ					20	6	11				
30	23.53	30.00	8.50	Δ					30	15	15				
				Δ					17	6	9				
				Δ					30	15	15				
				Δ					50	25	30				
				Δ					30	31	46				
				Δ					50	33	50				
				Δ		Dark			15						
				Δ					50						



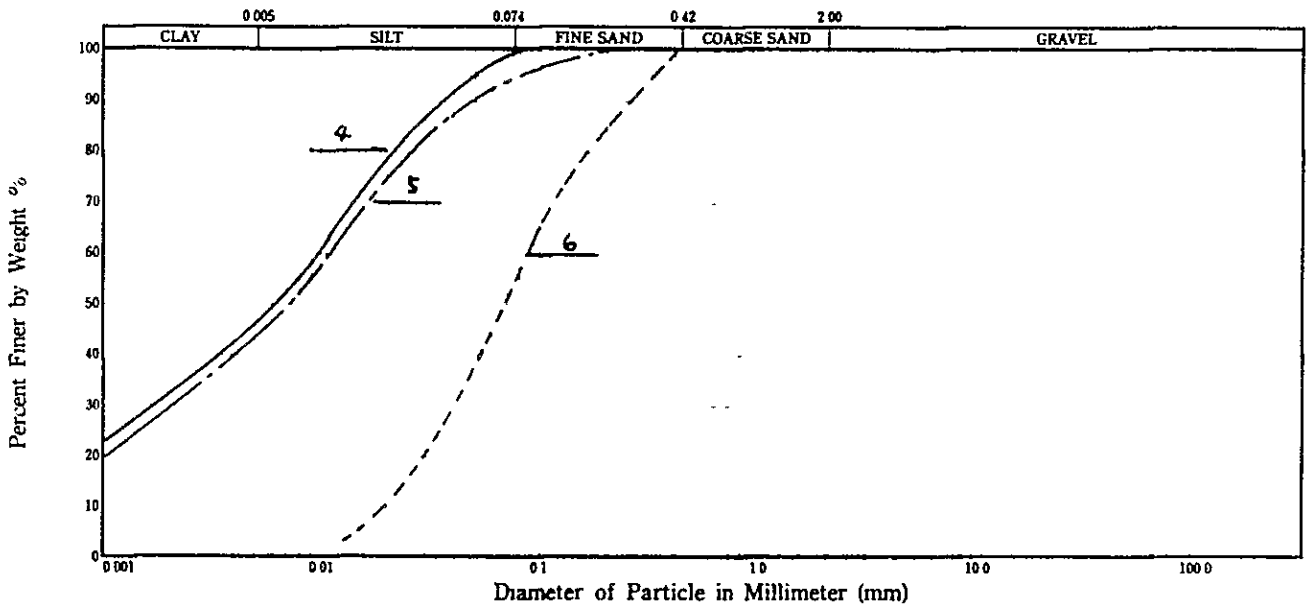
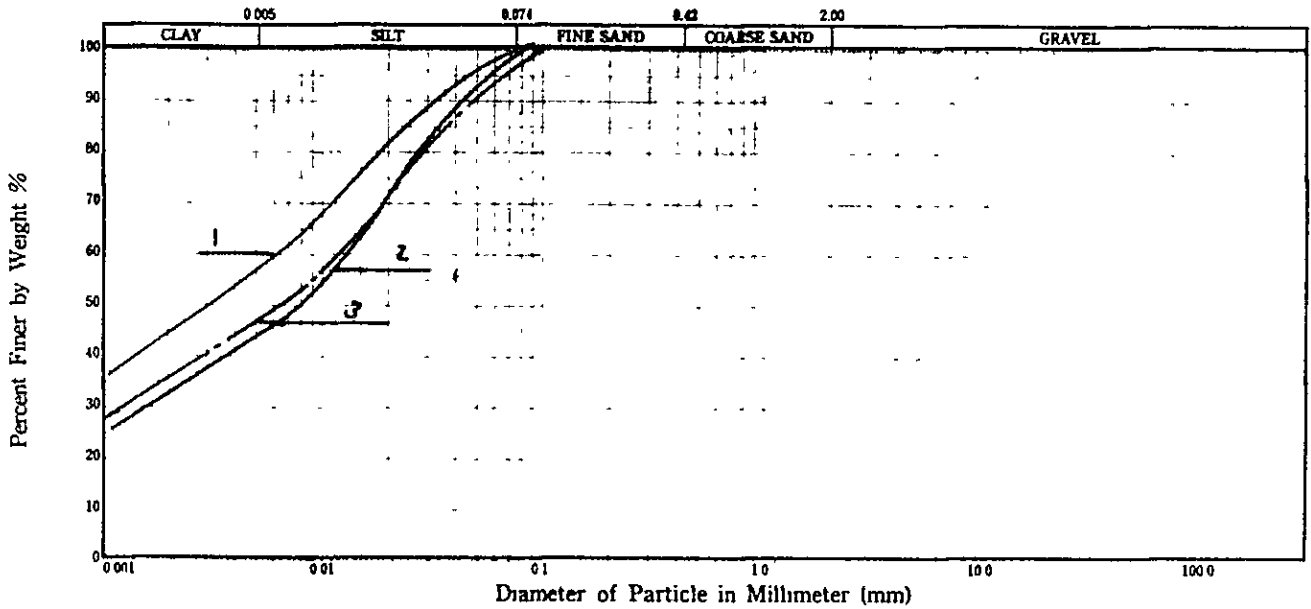
NOTE

GRAIN SIZE ANALYSIS

MECHANICAL ANALYSIS

Title, Investigation Place Thilawa Repair Dockyard Project Bore Hole No. BH-1 Date _____

GRAIN SIZE DISTRIBUTION CURVE

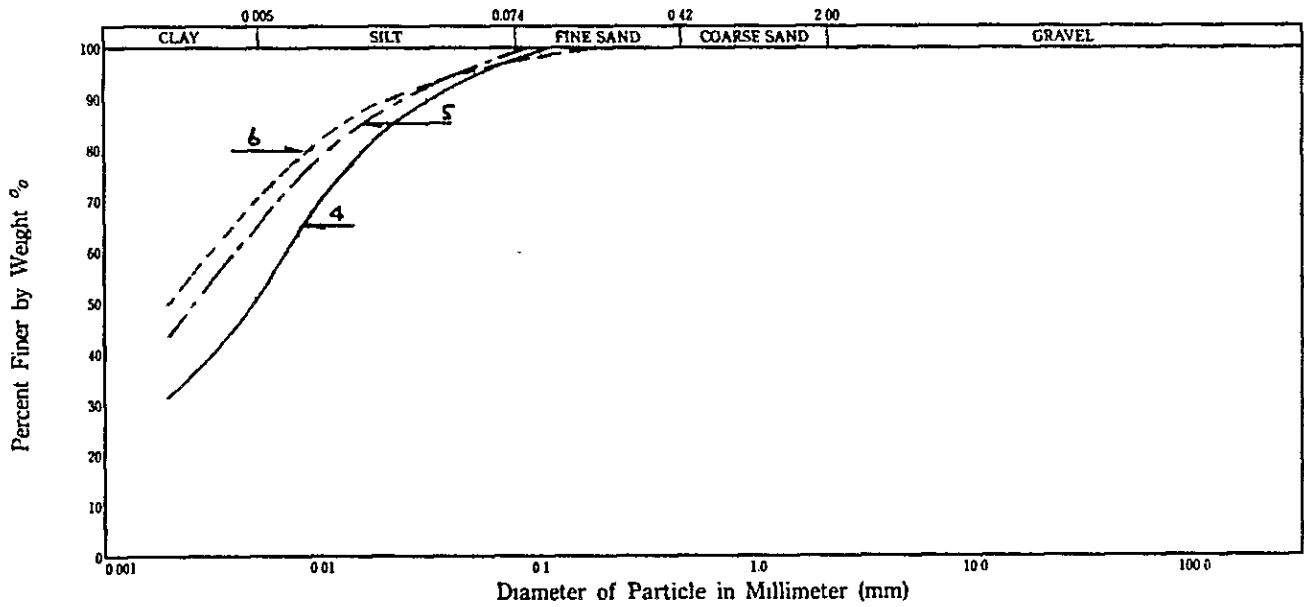
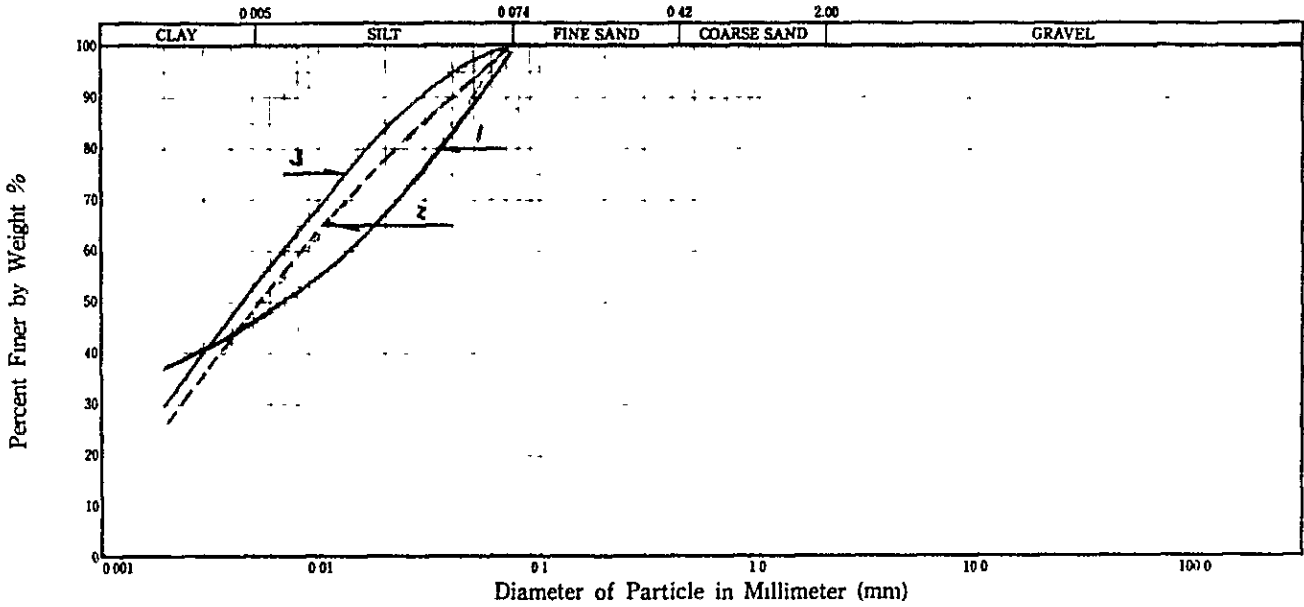


Sample No	Depth m	Gravel %	Coarse Sand %	Fine Sand %	Silt %	Clay %	(Coloid) %	D _{max} mm	D ₆₀ mm	D ₁₀ mm	Coeff of Uniformity U _c	2.00mm Under %	0.42mm Under %	0.075mm Under %	Specific Gravity G _s
1	4.0 ~ 4.5	0	0	1	42	57	20	0.074	0.006	-	-	100	100	99	
2	8.0 ~ 8.5	0	0	1	52	47	30	0.074	0.014	-	-	100	100	99	
3	11.0 ~ 11.5	0	0	3	53	44	27	0.1	0.014	-	-	100	100	97	
4	15.0 ~ 15.5	0	0	1	53	46	33	0.074	0.01	-	-	100	100	99	
5	20.0 ~ 20.5	0	0	6	49	45	29	0.3	0.01	-	-	100	100	94	
6	24.0 ~ 24.5	0	0	44	56	-	-	0.42	0.09	0.02	4.5	100	100	56	

MECHANICAL ANALYSIS

Title, Investigation Place Thilawa - Repair Dockyard Project Bore Hole No. BH-2 Date _____

GRAIN SIZE DISTRIBUTION CURVE

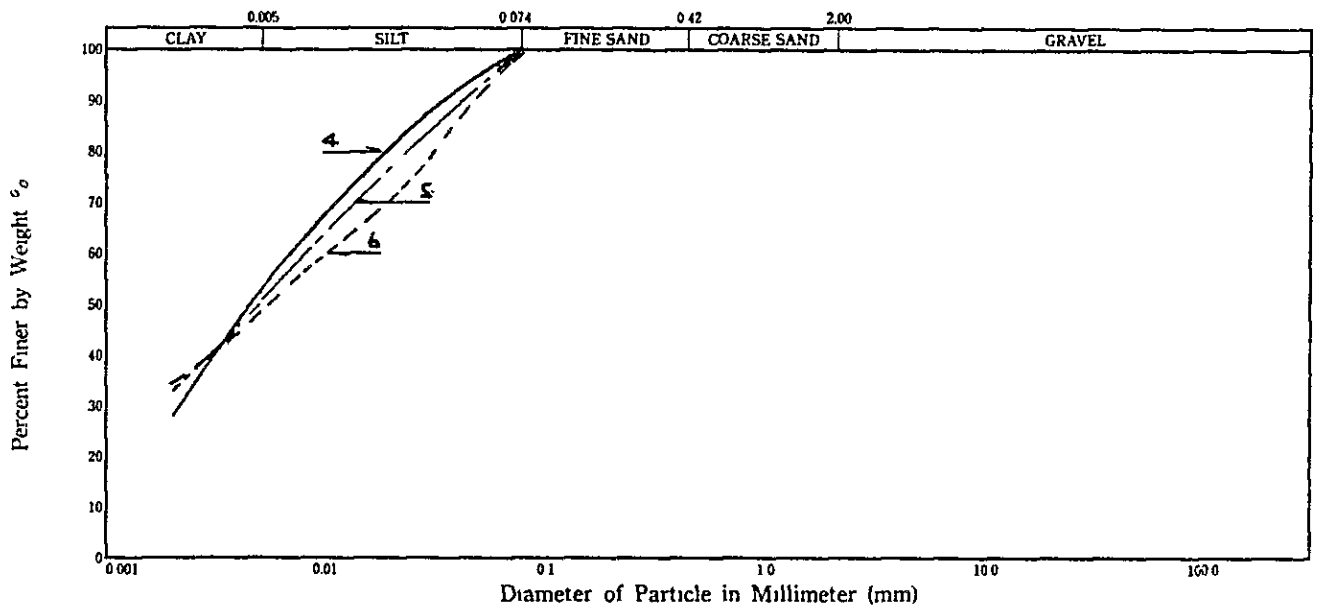
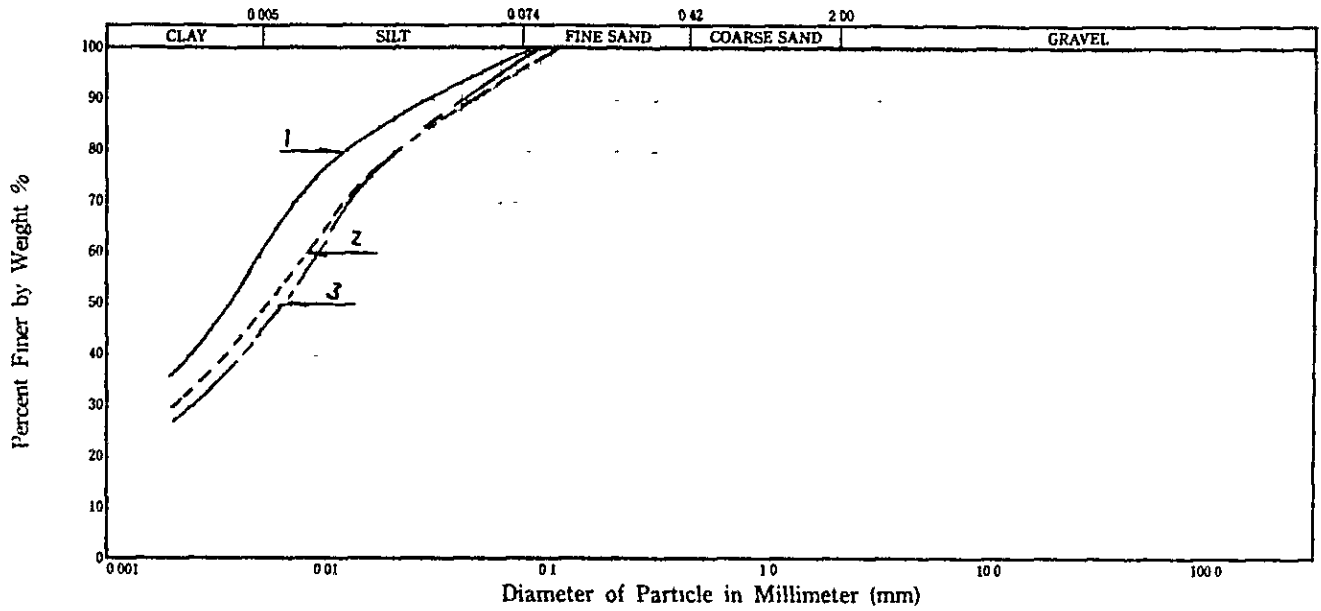


Sample No	Depth m	Gravel %	Coarse Sand %	Fine Sand %	Silt %	Clay %	(Colour) %	D _{max} mm	D _w mm	D ₁₀ mm	Coeff of Uniformity U _c	2.00mm Under %	0.42mm Under %	0.075mm Under %	Specific Gravity G _s
1	4.0 ~ 4.5	0	0	0	55	45	37	0.74	0.015	-	-	100	100	100	
2	8.0 ~ 8.5	0	0	0	35	65	30	0.74	0.008	-	-	100	100	100	
3	11.0 ~ 11.5	0	0	0	46	54	30	0.74	0.007	-	-	100	100	100	
4	15.0 ~ 15.5	0	0	4	46	50	32	0.01	0.007	-	-	100	100	96	
5	20.0 ~ 20.5	0	0	4	32	64	43	0.2	0.004	-	-	100	100	96	
6	25.0 ~ 25.5	0	0	2	28	70	50	0.074				100	100	98	

MECHANICAL ANALYSIS

Title, Investigation Place Thilawa Repair Dockyard Project Bore Hole No BH-3 Date _____

GRAIN SIZE DISTRIBUTION CURVE

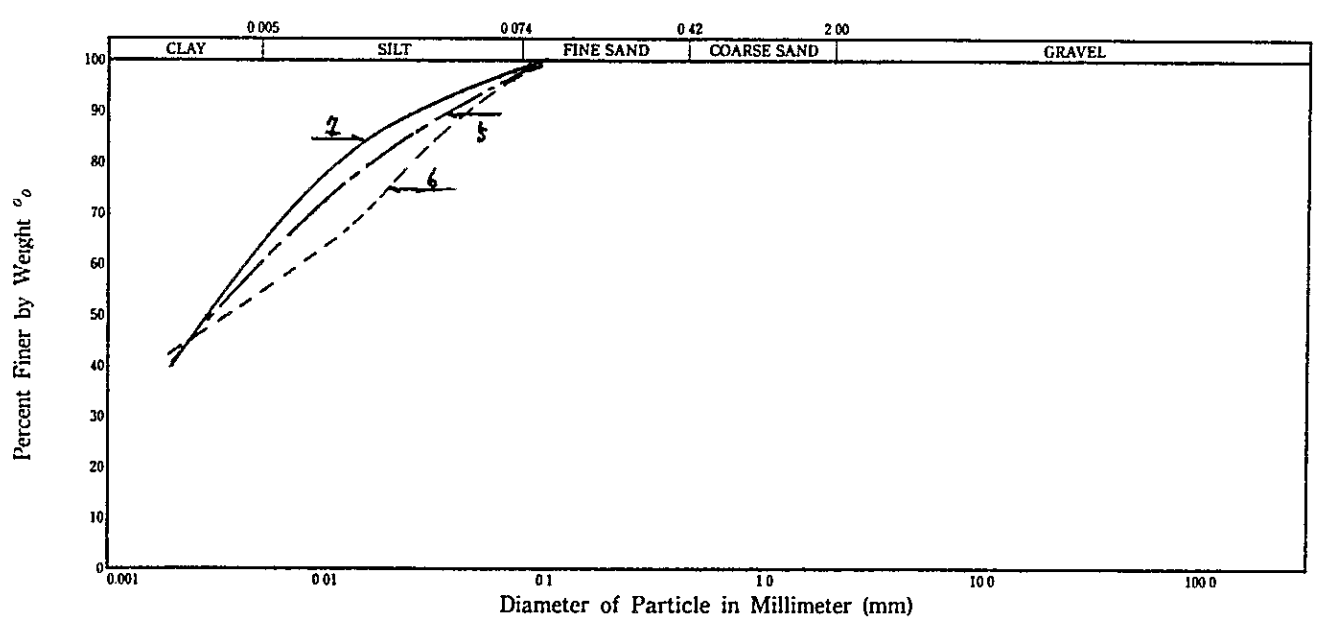
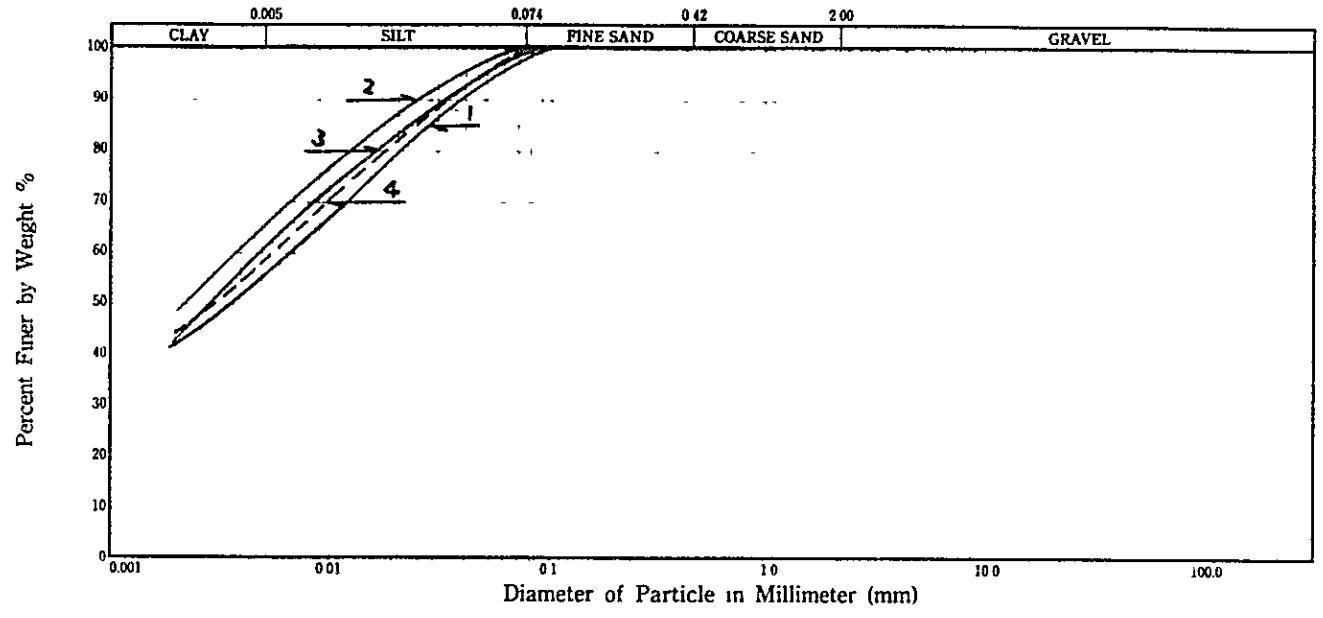


Sample No	Depth (m)	Gravel %	Coarse Sand %	Fine Sand %	Silt %	Clay %	(Coloid) %	D _{max} (mm)	D ₆₀ (mm)	D ₁₀ (mm)	Coeff of Uniformity (Uc)	200mm Under %	0.42mm Under %	0.074mm Under %	Specific Gravity (Gs)
1	4.0 ~ 4.5	0	0	2	38	60	36	0.074	0.005	-	-	100	100	98	
2	8.0 ~ 8.5	0	0	5	47	48	30	0.1	0.008	-	-	100	100	95	
3	12.0 ~ 12.5	0	0	3	54	43	27	0.1	0.009	-	-	100	100	97	
4	16.0 ~ 16.5	0	0	0	47	53	28	0.074	0.007	-	-	100	100	100	
5	21.0 ~ 21.5	0	0	0	50	50	34	0.074	0.008	-	-	100	100	100	
6	25.0 ~ 25.5	0	0	0	52	48	35	0.074	0.01	-	-	100	100	100	

MECHANICAL ANALYSIS

Title, Investigation Place Thilawa Repair Dockyard Project Bore Hole No BH-4 Date _____

GRAIN SIZE DISTRIBUTION CURVE

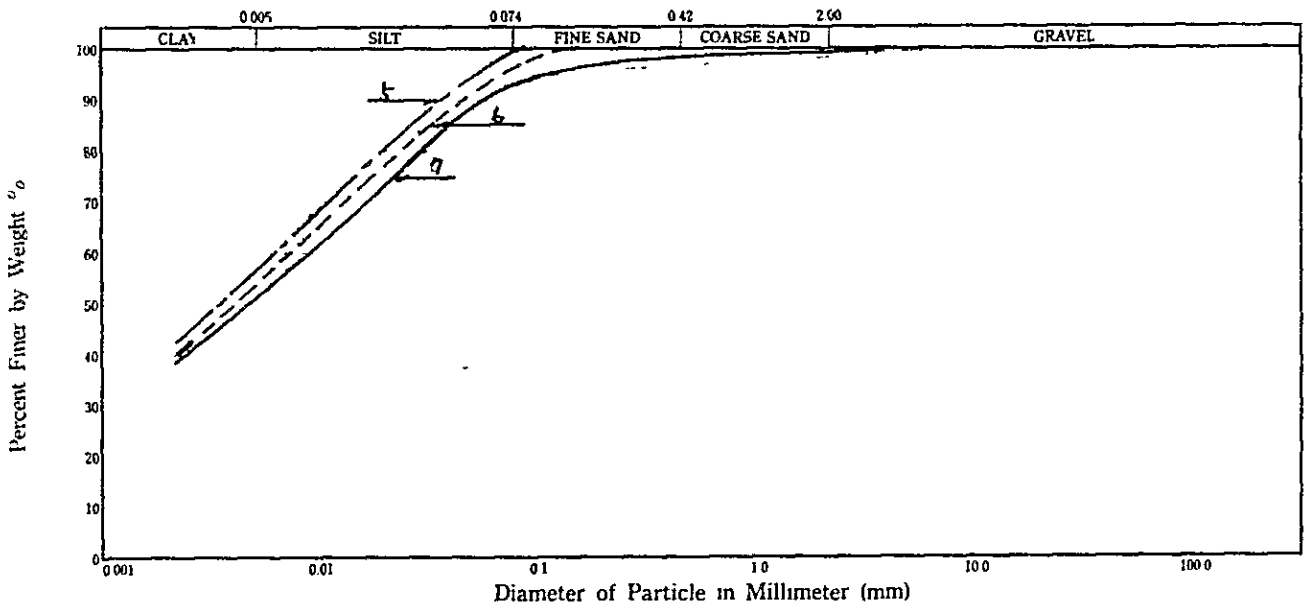
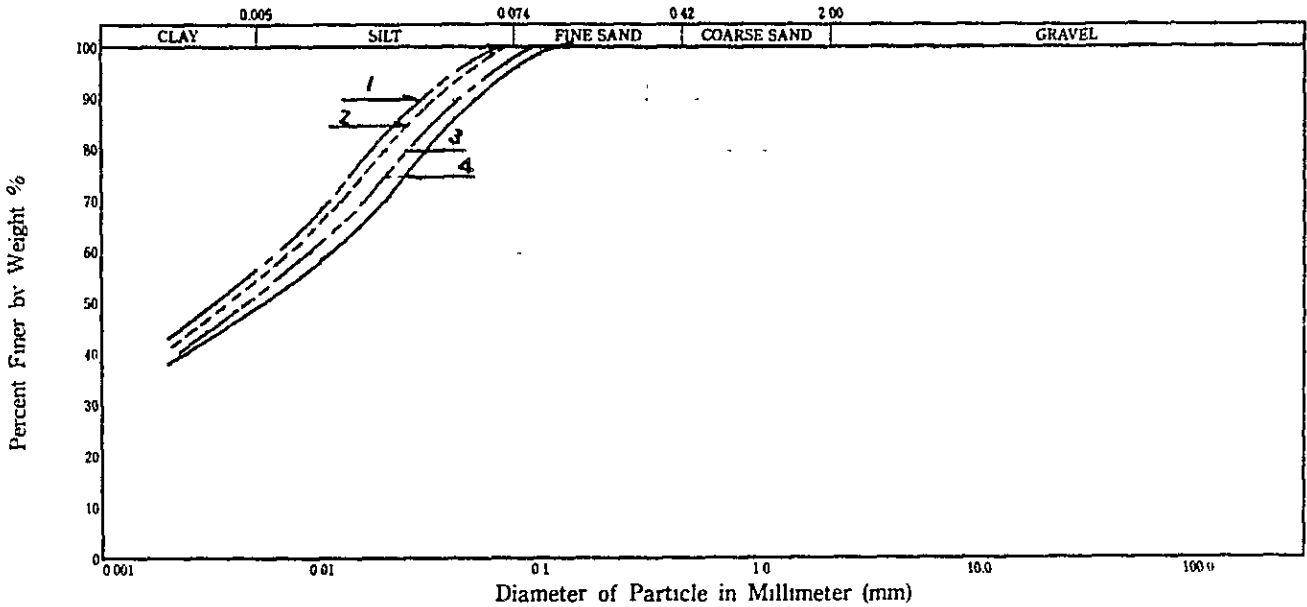


Sample No	Depth m	Gravel %	Coarse Sand %	Fine Sand %	Silt %	Clay %	(Coloid) %	D _{max} mm	D _w mm	D _u mm	Coeff of Uniformity U _c	200mm Under %	0.42mm Under %	0.074mm Under %	Specific Gravity G _s
1	3.0~3.5	0	0	3	42	55	42	0.1	0.008	-	-	100	100	97	
2	6.0~6.5	0	0	0	35	65	48	0.074	0.004	-	-	100	100	100	
3	9.0~10.5	0	0	2	38	60	42	0.1	0.005	-	-	100	100	98	
4	15.0~15.5	0	0	0	42	58	43	0.074	0.006	-	-	100	100	100	
5	18.0~18.5	0	0	2	38	60	40	0.1	0.005	-	-	100	100	98	
6	21.0~21.5	0	0	2	44	54	43	0.1	0.005	-	-	100	100	98	
7	24.0~24.5	0	0	2	34	64	40	0.1	0.004	-	-	100	100	98	

MECHANICAL ANALYSIS

Title, Investigation Place Thilawa Repair Dockyard Project Bore Hole No. BH-5 Date _____

GRAIN SIZE DISTRIBUTION CURVE

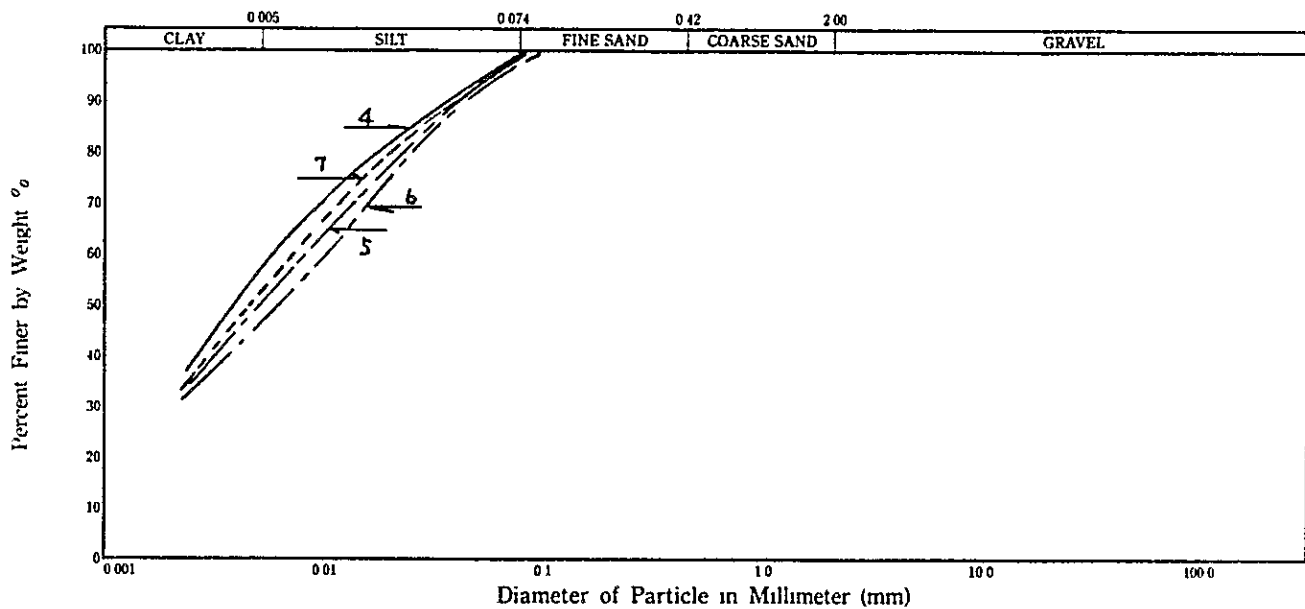
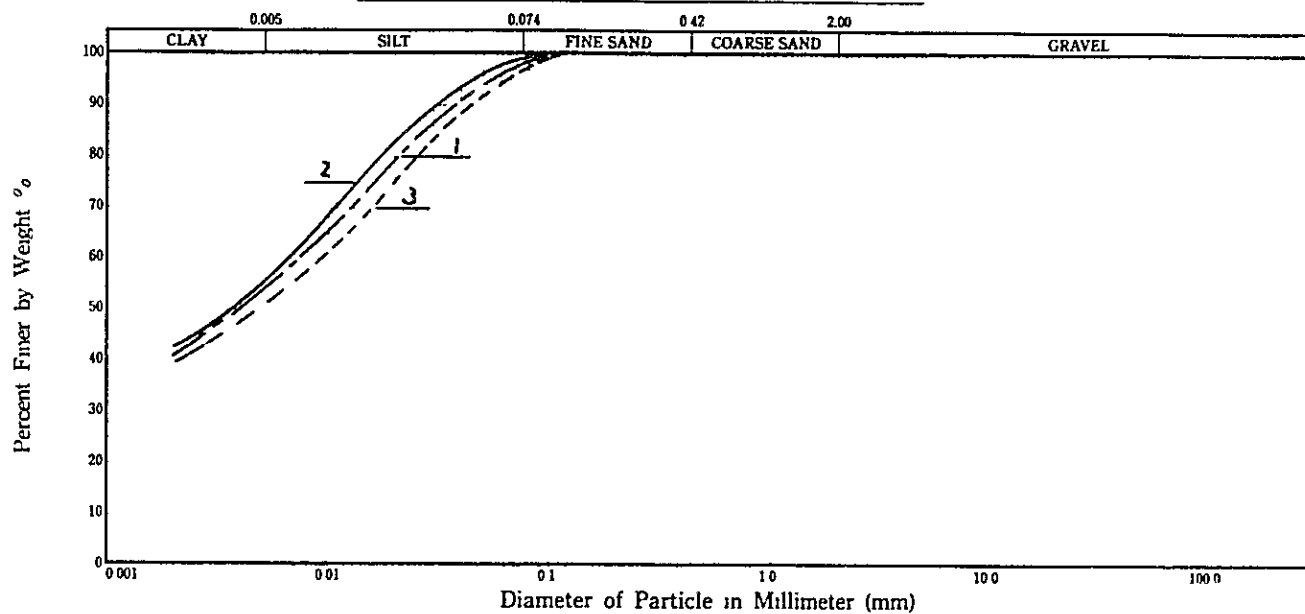


Sample No	Depth m	Gravel %	Coarse Sand %	Fine Sand %	Silt %	Clay %	(Coloid) %	D_{max} mm	D_{60} mm	D_{30} mm	Coeff. of Uniformity	200mm Under %	0.42mm Under %	0.074mm Under %	Specific Gravity G_s
1	3.0~3.3	0	0	0	43	57	44	0.074	0.006	-	-	100	100	100	
2	5.0~5.5	0	0	0	45	55	43	0.074	0.008	-	-	100	100	100	
3	8.5~9.5	0	0	3	45	52	40	0.09	0.009	-	-	100	100	97	
4	12.0~12.5	0	0	4	48	48	38	0.15	0.01	-	-	100	100	96	
5	15.0~15.7	0	0	0	44	56	42	0.074	0.006	-	-	100	100	100	
6	18.0~18.7	0	0	4	43	53	40	0.15	0.007	-	-	100	100	96	
7	21.5~22.0	0	3	4	43	50	40	2.00	0.009	-	-	100	97	93	

MECHANICAL ANALYSIS

Title, Investigation Place Thilawa Repair Dockyard Project Bore Hole No BH-6 Date _____

GRAIN SIZE DISTRIBUTION CURVE



Sample No.	Depth (m)	Gravel %	Coarse Sand %	Fine Sand %	Silt %	Clay %	(Colloid) %	D _{max} mm	D ₆₀ mm	D ₁₀ mm	Coeff of Uniformity U _c	2.00mm Under %	0.42mm Under %	0.074mm Under %	Specific Gravity G _s
1	2.0 ~ 2.5	0	0	2	45	53	41	0.09	0.008	-	-	100	100	98	
2	5.0 ~ 5.5	0	0	1	45	54	41	0.09	0.006	-	-	100	100	99	
3	8.0 ~ 8.5	0	0	3	47	50	40	0.1	0.01	-	-	100	100	97	
4	11.0 ~ 11.5	0	0	0	43	57	35	0.074	0.006	-	-	100	100	100	
5	14.0 ~ 14.5	0	0	0	48	52	30	0.074	0.009	-	-	100	100	100	
6	17.0 ~ 17.5	0	0	0	55	45	30	0.074	0.008	-	-	100	100	100	
7	20.0 ~ 20.5	0	0	3	51	46	30	0.1	0.01	-	-	100	100	97	

UNCONFINED COMPRESSION TEST

B-5

土の一軸圧縮試験

UNCONFINED COMPRESSION TEST

調査名・調査地点
Title, Investigation Place Thilawa Repair Dockyard Project

試験年月日
Date _____ 年 _____ 月 _____ 日

試料採取位置(深度)
Sampling Place, Depth 18.0 m - 18.6 m

土質名称
Soil Classification clay

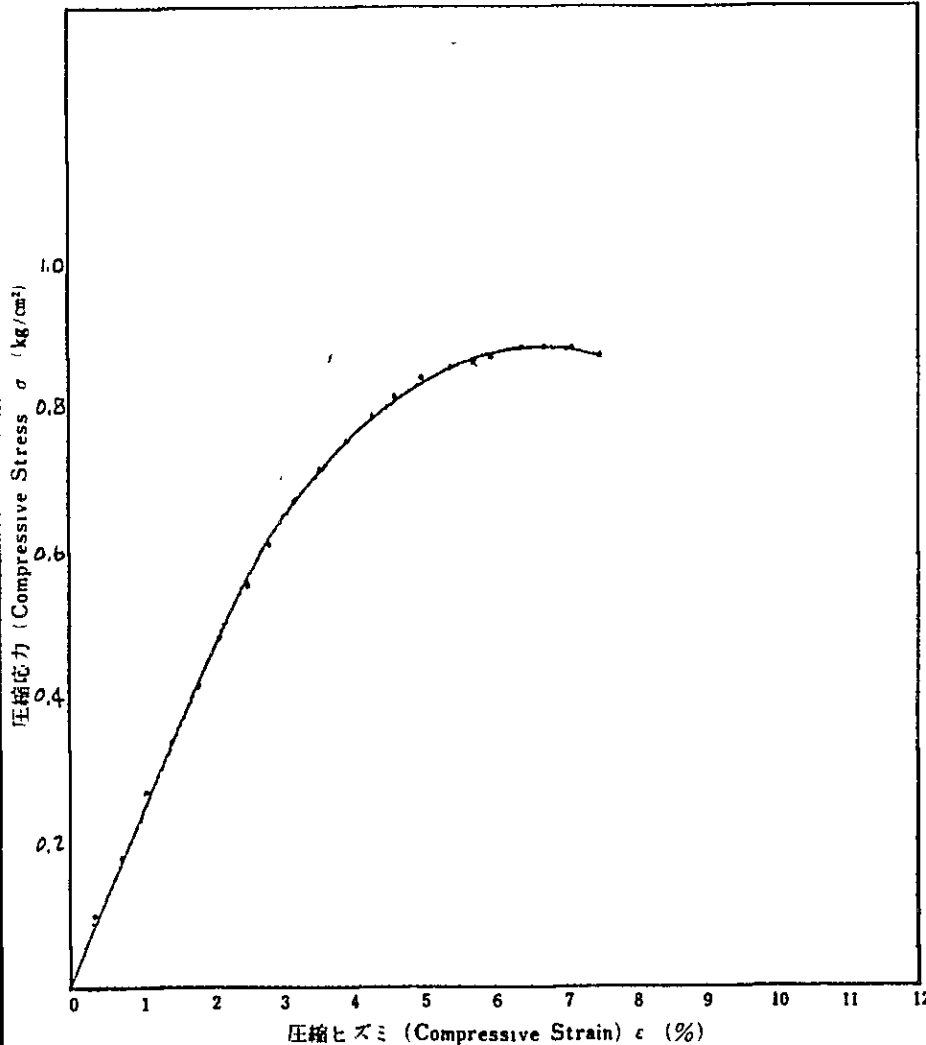
試料番号
Sample No. TWS-6

土粒子の比重
Specific Gravity _____

応力制御法
Stress Control ヒズミ制御法
Strain Control

圧縮速度
Compression Speed _____ %/min _____ mm/min

供試体番号 Specimen No.	試料の状態 Specimen Condition	供試体の寸法 Dimension of Specimen		含水比 Moisture Content w %	湿密度 Wet Density γ_{wet}	間隙率 Void Ratio e	飽和度 Degree of Saturation S _v %	軸圧縮強度 Unconfined Compressive Strength σ_u kg/cm ²	破壊時のひずみ Failure Strain e _f %	変形係数 Deformation Coefficient E ₅₀ kg/cm ²	鋭敏度 Sensitivity Ratio S _r
		高さ Height H/cm	直径 Diameter φ/cm								
1	乱さない試料 Undisturbed Sample	14.0	7.5		1.73			0.88	6.5	23	
1	乱す試料 Remolded Sample										
2	乱さない試料 Undisturbed Sample										
2	乱す試料 Remolded Sample										



試料の破壊状況
Observation at Ultimate Failure

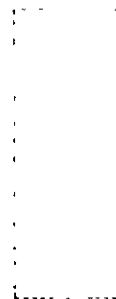
No. 1

No. 1



No. 2

No. 2



note

Decayed plants contained.

The sample was slightly disturbed.

B-5

土の一軸圧縮試験

UNCONFINED COMPRESSION TEST

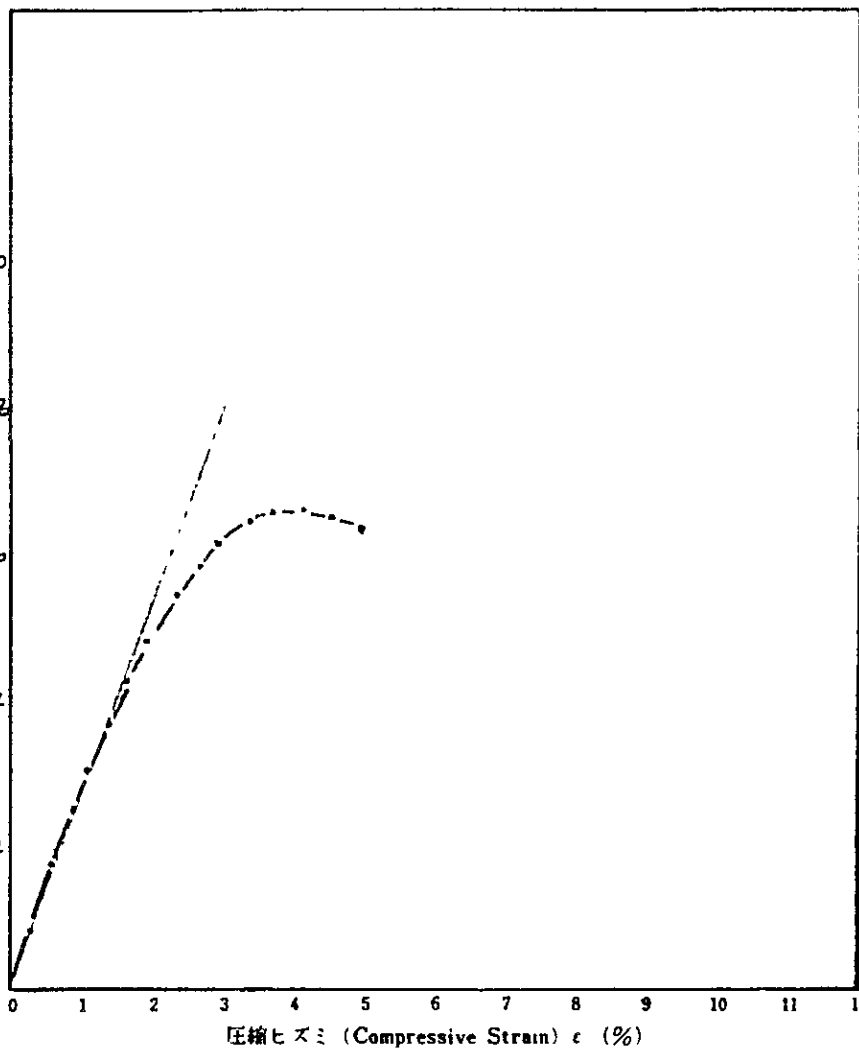
調査名・調査地点 Title, Investigation Place Thilawa Repair Dockyard Project 試験年月日 Date 年 月 日

試料採取位置(深度) Sampling Place, Depth 8.50m ~ 9.20 m 土質名称 Soil Classification clay

試料番号 Sample No. TWS - Ⅱ 土粒子の比重 Specific Gravity

応力制御法 Stress Control ひずみ制御法 Strain Control 圧縮速度 Compression Speed %/min mm/min

供試体番号 Specimen No.	試料の状態 Specimen Condition	供試体の寸法 Dimension of Specimen		含水比 Moisture Content w %	単位体積重量 Wet Density γ _w g/cm ³	間隙率 Void Ratio e	飽和度 Degree of Saturation S _v %	軸圧縮強度 Unconfined Compressive Strength σ _u kg/cm ²	破壊ひずみ Failure Strain ε %	変形係数 Deformation Coefficient E _s kg/cm ²	敏感比 Sensitivity Ratio S _i
		高さ Height H (cm)	径 Diameter φ (cm)								
1	原状土試料 Undisturbed Sample	13.0	7.5		1.72			0.66	3.7	26	
1	再製土試料 Remolded Sample										
2	原状土試料 Undisturbed Sample										
2	再製土試料 Remolded Sample										



試料の破壊状況
Observation at Ultimate Failure

No 1	No 1
No 2	No.2

75

B-5

土の一軸圧縮試験

UNCONFINED COMPRESSION TEST

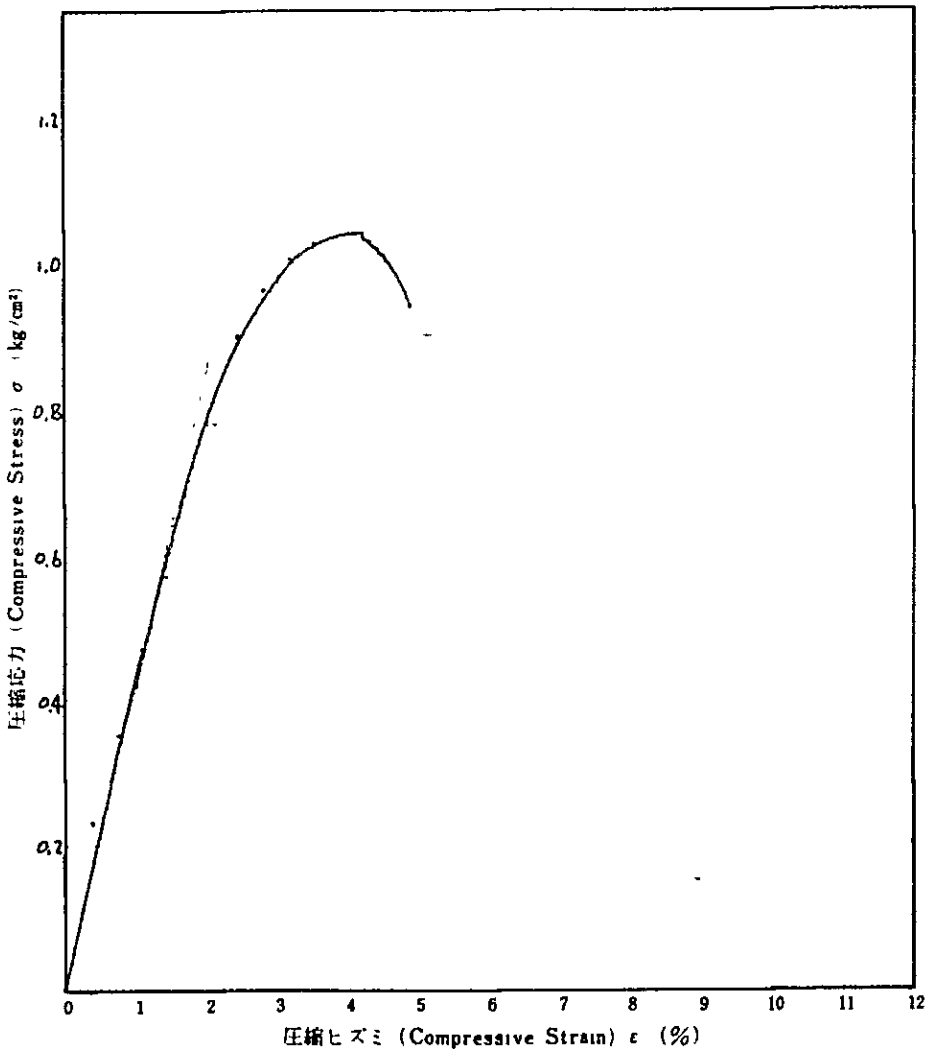
調査名・調査地点 Title, Investigation Place Thilawa Repair Dockyard Project 試験年月日 Date 年 月 日

試料採取位置(深度) Sampling Place, Depth 15.0 m - 15.5 m 土質名称 Soil Classification Clay

試料番号 Sample No TWS - V 土粒子の比重 Specific Gravity

応力制御法 Stress Control ヒズミ制御法 Strain Control 圧縮速度 ComPRESSION Speed %/min mm/min

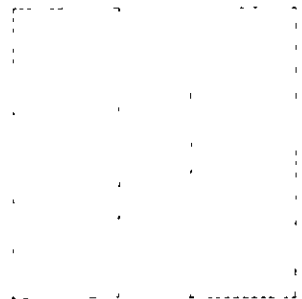
試料番号 Specimen No	試料の状態 Specimen Condition	供試体の寸法 Dimension of Specimen		含水比 Moisture Content w %	湿密度 Wet Density γ_w (kg/cm ³)	空隙率 Void Ratio e	飽和度 Degree of Saturation S _v %	軸圧縮強さ Unconfined Compressive Strength σ_u (kg/cm ²)	破壊ひずみ Failure Strain e _f %	変形係数 Deformation Coefficient E _s (kg/cm ²)	鋭敏比 Sensitivity Ratio S _r
		高さ Height H (cm)	直径 Diameter φ (cm)								
1	乱さない試料 Undisturbed Sample	14.3	7.5		1.79			1.04	4.2	44	
1	乱した試料 Remolded Sample										
2	乱さない試料 Undisturbed Sample										
2	乱した試料 Remolded Sample										



試料の破壊状況
Observation at Ultimate Failure

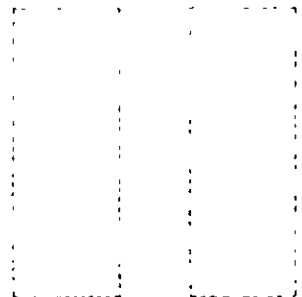
No 1

No 1



No 2

No 2



B-10

土の一軸圧縮試験

UNCONFINED COMPRESSION TEST

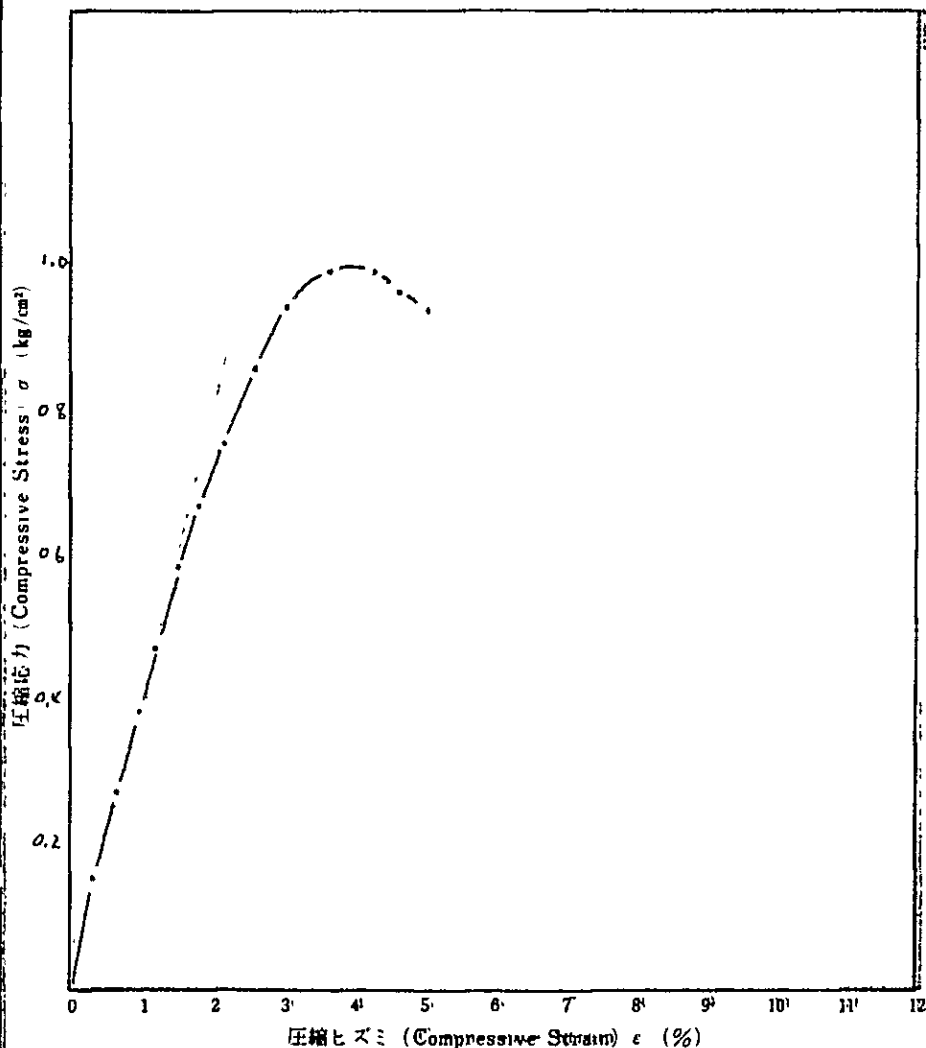
調査名・調査地点 Title, Investigation Place **Thilawa Repair Dockyard Project** 試験年月日 Date 年 月 日

試料採取位置(深度) Sampling Place, Depth **2.00 m ~ 2.50 m** 土質名称 Soil Classification

試料番号 Sample No. **TWS-1** 土粒子の比重 Specific Gravity

応力制御法 Stress Control **ヒズミ制御法 Strain Control** 圧縮速度 Compression Speed / %/min mm/min

供試体番号 Specimen No.	試料の状態 Specimen Condition	供試体寸法 Dimension of Specimen		含水比 Moisture Content w %	湿体積質量 Wet Density γ_w g/cm ³	間隙率 Void Ratio e	飽和度 Degree of Saturation S _v %	軸圧縮強度 Unconfined Compressive Strength σ_u kg/cm ²	破壊時のヒズミ Failure Strain e (%)	変形係数 Deformation Coefficient E _s kg/cm ²	縦縮率 Sensitivity Ratio S _v
		高さ Height H (cm)	直径 Diameter ϕ (cm)								
1	乱れなごみ試料 Undisturbed Sample	13.4	7.5	44.5	1.82			0.98	3.7	42	
1	再成形試料 Remolded Sample										
2	乱れなごみ試料 Undisturbed Sample										
2	再成形試料 Remolded Sample										



試料の破壊状況 Observation at Ultimate Failure

No. 1	No. 1'
No. 2	No. 2

BH-10

土の一軸圧縮試験 UNCONFINED COMPRESSION TEST

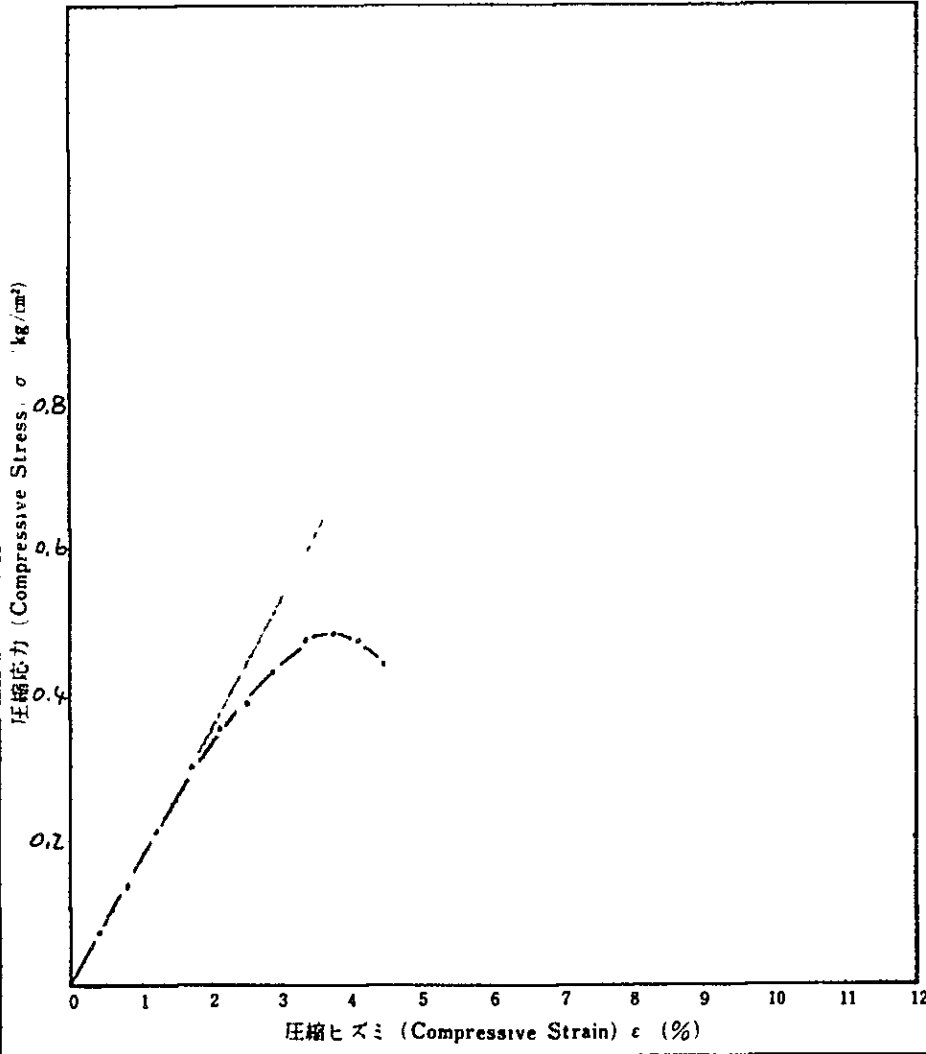
調査名・調査地点 Title, Investigation Place Thilawa Repair Dockyard Project 試験年月日 Date _____ 年 _____ 月 _____ 日

試料採取位置(深度) Sampling Place, Depth 4.00 m ~ 4.70 m 土質名称 Soil Classification Clay

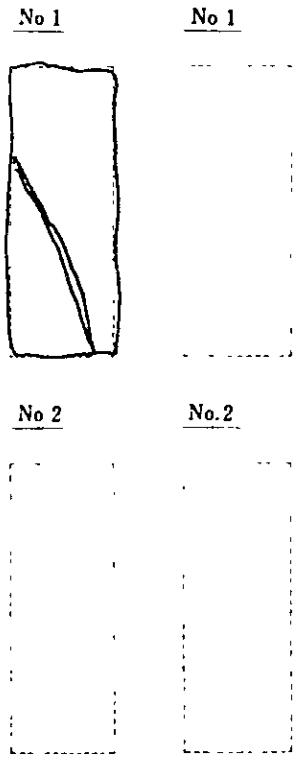
試料番号 Sample No TWS-2 土粒子の比重 Specific Gravity _____

応力制御法 Stress Control ヒズミ制御法 Strain Control 圧縮速度 Compression Speed _____ %/min _____ mm/min

試体番号 Specimen No	試料の状態 Specimen Condition	試体寸法 Dimension of Specimen		含水比 Moisture Content w %	湿体積質量 Wet Density γ_w g/cm ³	空隙率 Void Ratio e	飽和度 Degree of Saturation S _v %	軸圧縮強度 Unconfined Compressive Strength q_u kg/cm ²	破壊時歪み Failure Strain %	変形係数 Deformation Coefficient E_{50} kg/cm ²	鋭敏比 Sensitivity Ratio S _i
		高さ Height H cm	直径 Diameter ϕ cm								
1	乱さない試料 Undisturbed Sample	7.5	15.0	42.2	1.78		0.48	3.8	18		
1	乱す試料 Remolded Sample										
2	乱さない試料 Undisturbed Sample										
2	乱す試料 Remolded Sample										



試料の破壊状況
Observation at Ultimate Failure



65

BH-10

土の一軸圧縮試験

UNCONFINED COMPRESSION TEST

調査名・調査地点
Title, Investigation Place **Thilawa Repair Dockyard Project**

試験年月日
Date 年 月 日

試料採取位置(深度)
Sampling Place, Depth **6.00 m - 6.78 m**

土質名称
Soil Classification

試料番号
Sample No.

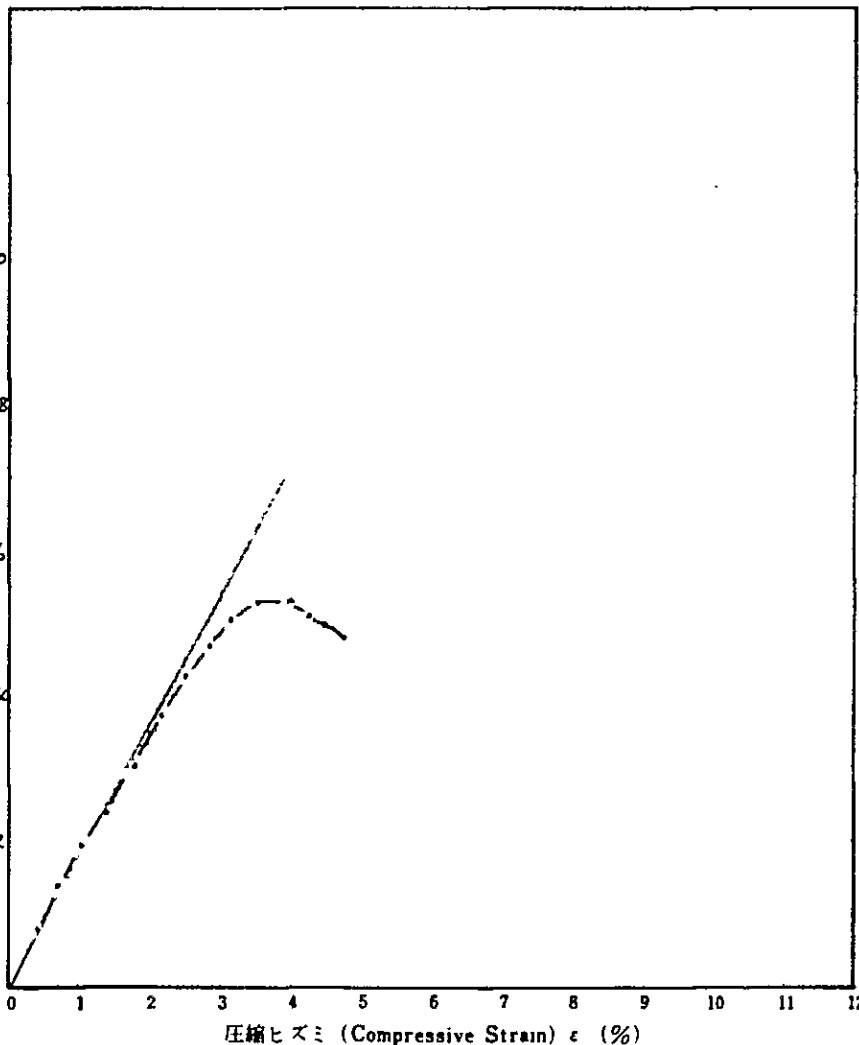
土粒子の比重
Specific Gravity

応力制御法
Stress Control

ヒズミ制御法
Strain Control

圧縮速度
Compression Speed %/min mm/min

試料番号 Specimen No.	試料の状態 Specimen Condition	試料の寸法 Dimension of Specimen		含水比 Moisture Content w %	湿り体積質量 Wet Density γ_w g/cm ³	空隙率 Void Ratio e	飽和度 Degree of Saturation S %	軸圧縮強さ Unconfined Compressive Strength σ_u kg/cm ²	破壊時のヒズミ Failure Strain ϵ_f %	変形係数 Deformation Coefficient E ₅₀ kg/cm ²	鋭敏比 Sensitivity Ratio S _r
		高さ Height H/cm	直径 Diameter ϕ /cm								
1	乱さない試料 Undisturbed Sample	15.0	7.5	46.9	1.75			0.53	3.5	18	
1	乱さない試料 Remolded Sample										
2	乱さない試料 Undisturbed Sample										
2	乱さない試料 Remolded Sample										



試料の破壊状況
Observation at Ultimate Failure

No 1	No.1
No 2	No.2

BH-10

土の一軸圧縮試験 UNCONFINED COMPRESSION TEST

調査名・調査地点
Title, Investigation Place Thilawa Repair Dockyard Project

試験年月日
Date _____ 年 _____ 月 _____ 日

試料採取位置(深度)
Sampling Place, Depth 8.00 m ~ 8.78 m

土質名称
Soil Classification clay

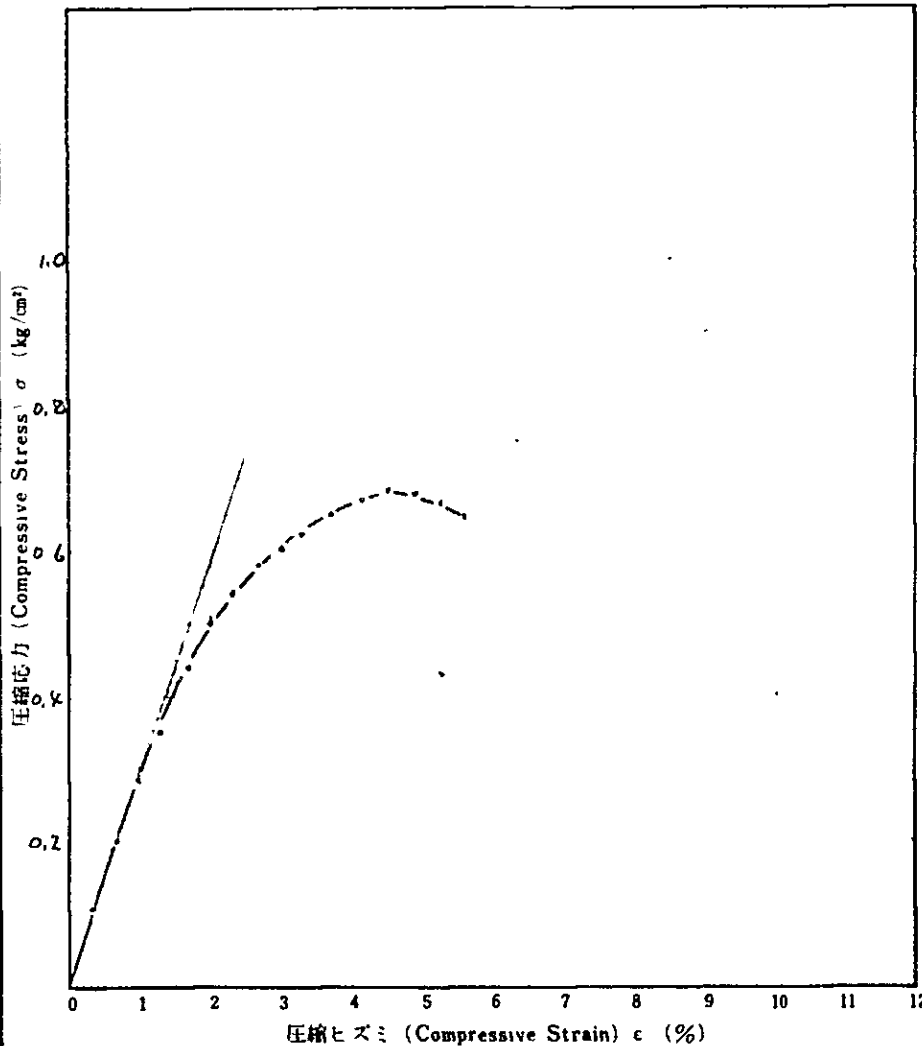
試料番号
Sample No. TWS-4

土粒子の比重
Specific Gravity _____

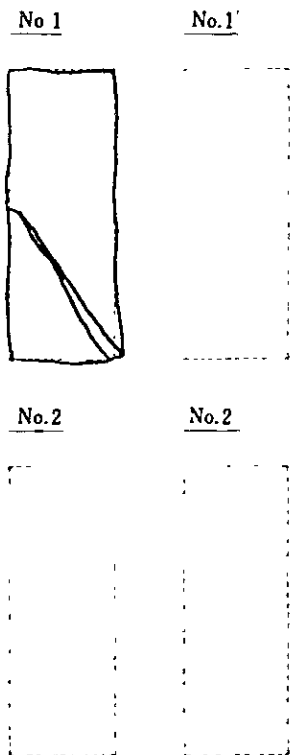
応力制御法
Stress Control ヒズミ制御法
Strain Control

圧縮速度
Compression Speed _____ %/min _____ mm/min

試料番号 Specimen No.	試料の状態 Specimen Condition	供試体寸法 Dimension of Specimen		含水比 Moisture Content %	湿体積比重 Wet Density γ_w (kg/m ³)	間隙率 Void Ratio e	飽和度 Degree of Saturation S %	軸圧縮強度 Unconfined Compressive Strength σ_u (kg/cm ²)	破壊ひずみ Failure Strain %	変形係数 Deformation Coefficient E ₅₀ (kg/cm ²)	鋭敏比 Sensitivity Ratio S _v
		高さ Height H (cm)	直径 Diameter ϕ (cm)								
1	乱さない試料 Undisturbed Sample	15.0	7.5		1.81			0.68	4.5	30	
1	練り出した試料 Remoulded Sample										
2	乱さない試料 Undisturbed Sample										
2	練り出した試料 Remoulded Sample										



試料の破壊状況
Observation at Ultimate Failure



BH-10

土の一軸圧縮試験 UNCONFINED COMPRESSION TEST

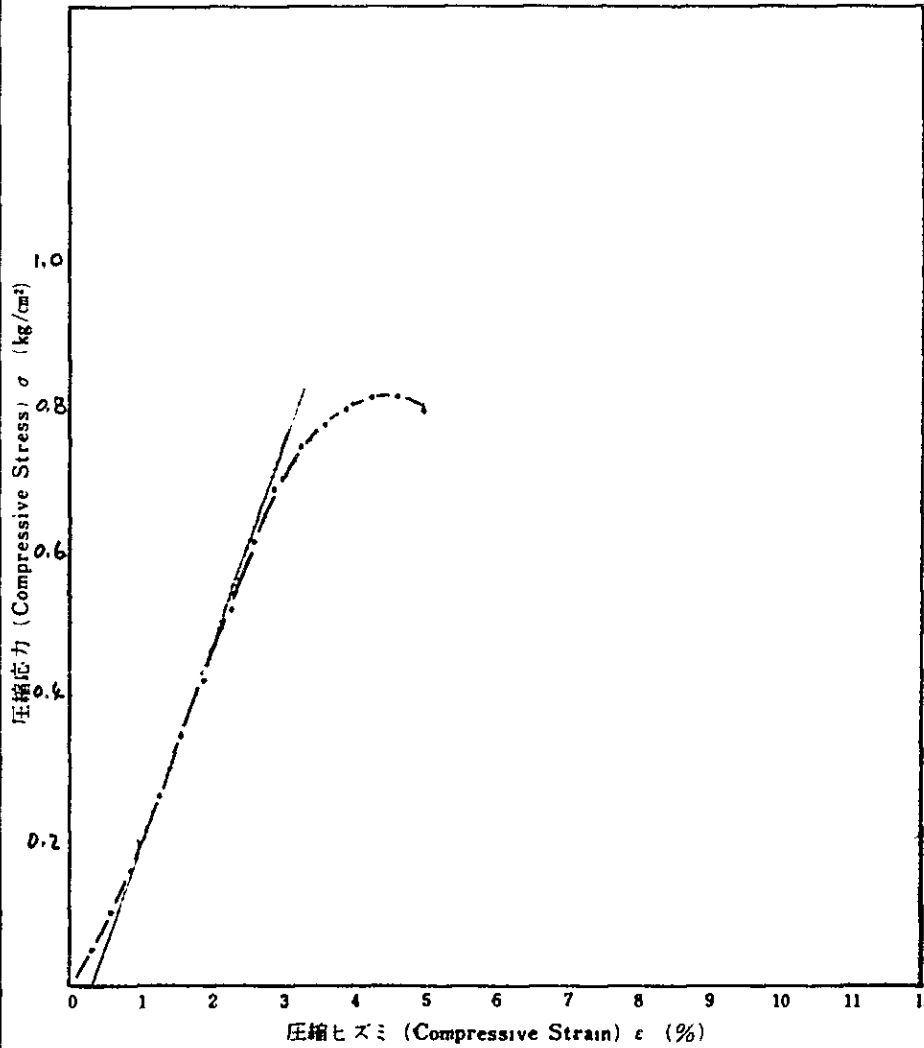
調査名・調査地点 Title, Investigation Place Thilawa Repair Dockyard Project 試験年月日 Date 年 月 日

試料採取位置(深度) Sampling Place, Depth 10.0 m ~ 10.7 m 土質名称 Soil Classification

試料番号 Sample No TWS-5 土粒子の比重 Specific Gravity

応力制御法 Stress Control ヒズミ制御法 Strain Control 圧縮速度 Compression Speed %/min mm/min

試体番号 Specimen No	試料の状態 Specimen Condition	試体の寸法 Dimension of Specimen		含水比 Moisture Content w %	湿り体積重量 Wet Density γ_{wet} g/cm^3	間隙率比 Void Ratio e	飽和度 Degree of Saturation S _w %	軸圧縮強度 Unconfined Compressive Strength q _u kg/cm^2	破壊時のひずみ Failure Strain e _f %	変形係数 Deformation Coefficient Esu kg/cm^2	敏感比 Sensitivity Ratio Sr
		高さ Height H cm	直径 Diameter ϕ cm								
1	乱れた試料 Undisturbed Sample	15.2	7.5	37.3	1.83			0.81	4.2	35	
1	整形した試料 Remolded Sample										
2	乱れた試料 Undisturbed Sample										
2	整形した試料 Remolded Sample										



試料の破壊状況
Observation at Ultimate Failure

No 1	No.1
No 2	No 2

Very fine sand contained.

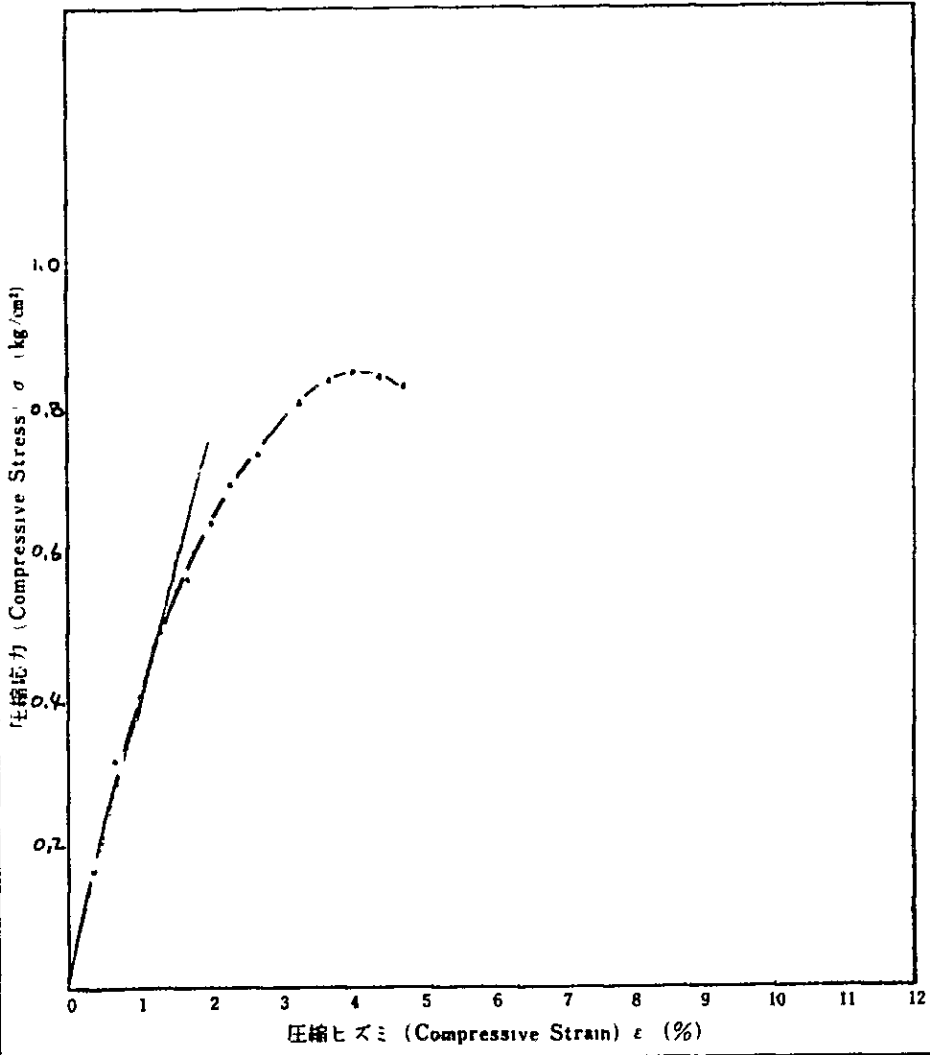
BH-10

土の一軸圧縮試験

UNCONFINED COMPRESSION TEST

調査名・調査地点 Title, Investigation Place	Thilawa Repair Dockyard Project	試験年月日 Date	年	月	日	
試料採取位置(深度) Sampling Place, Depth	12.0 m - 12.8 m	土質名称 Soil Classification				
試料番号 Sample No.	TWS-6	土粒子の比重 Specific Gravity				
応力制御法 Stress Control	ヒズミ制御法 Strain Control	圧縮速度 Compression Speed	%/min	mm/min		

供試体番号 Specimen No.	試料の状態 Specimen Condition	供試体寸法 Dimension of Specimen		含水比 Moisture Content w, %	湿り体積質量 Wet Density γ_w , g/cm ³	間キ比 Void Ratio e	飽和度 Degree of Saturation S, %	軸圧縮強度 Unconfined Compressive Strength q_u , kg/cm ²	破壊時 Failure Strain ϵ_f , %	変形係数 Deformation Coefficient E_{50} , kg/cm ²	脆性比 Sensitivity Ratio S _i
		高さ Height H, cm	直径 Diameter ϕ , cm								
1	乱雑土試料 Undisturbed Sample	15.0	7.5	45	1.73			0.85	4.0	40	
1	乱雑土試料 Remolded Sample										
2	乱雑土試料 Undisturbed Sample										
2	乱雑土試料 Remolded Sample										



試料の破壊状況
Observation at Ultimate Failure

No.1	No.1
No.2	No.2

BH-10

土の一軸圧縮試験 UNCONFINED COMPRESSION TEST

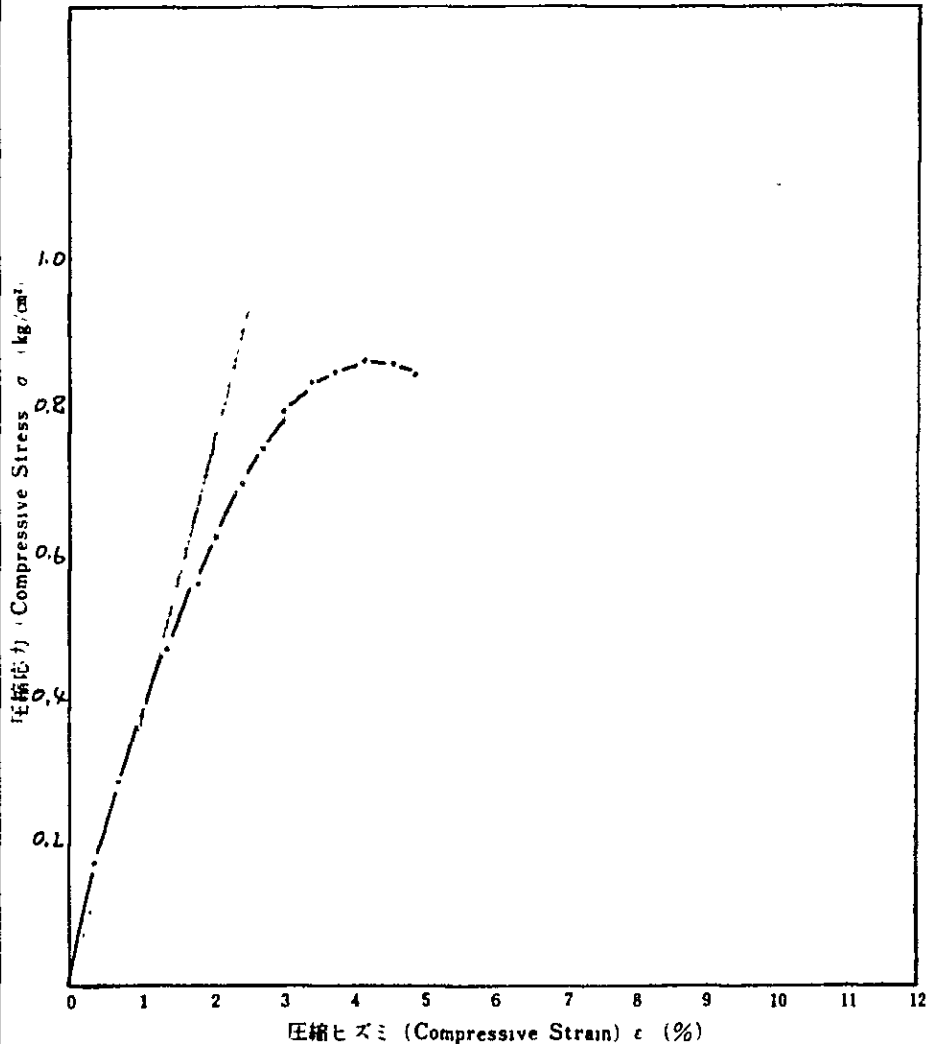
調査名・調査地点 Title, Investigation Place Thilawa Repair Dockyard Project 試験年月日 Date 年 月 日

試料採取位置(深度) Sampling Place, Depth 14.00 m - 14.78 m 土質名称 Soil Classification

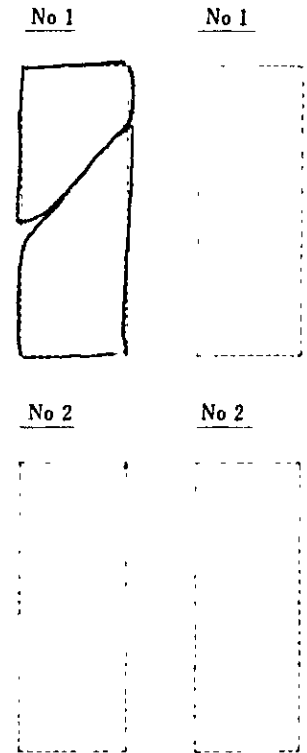
試料番号 Sample No. TWS-7 土粒子の比重 Specific Gravity

応力制御法 Stress Control 変形制御法 Strain Control 圧縮速度 Compression Speed %/min mm/min

供試体番号 Specimen No.	試料の状態 Specimen Condition	供試体の寸法 Dimension of Specimen		含水比 Moisture Content w %	単位体積重量 Wet Density γ _w g/cm ³	空隙率比 Void Ratio e	飽和度 Degree of Saturation S %	軸圧縮強度 Unconfined Compressive Strength σ _u kg/cm ²	破壊時のヒュー Failure Strain ε %	変形係数 Deformation Coefficient E _s kg/cm ²	鋭敏比 Sensitivity Ratio S _r
		高さ Height H (cm)	直径 Diameter φ (cm)								
1	乱さるゝ試料 Undisturbed Sample	14.9	7.5		1.72			0.86	4.2	37	
1	細りかゝるゝ試料 Remolded Sample										
2	乱さるゝ試料 Undisturbed Sample										
2	細りかゝるゝ試料 Remolded Sample										



試料の破壊状況
Observation at Ultimate Failure



B-10

土の一軸圧縮試験

UNCONFINED COMPRESSION TEST

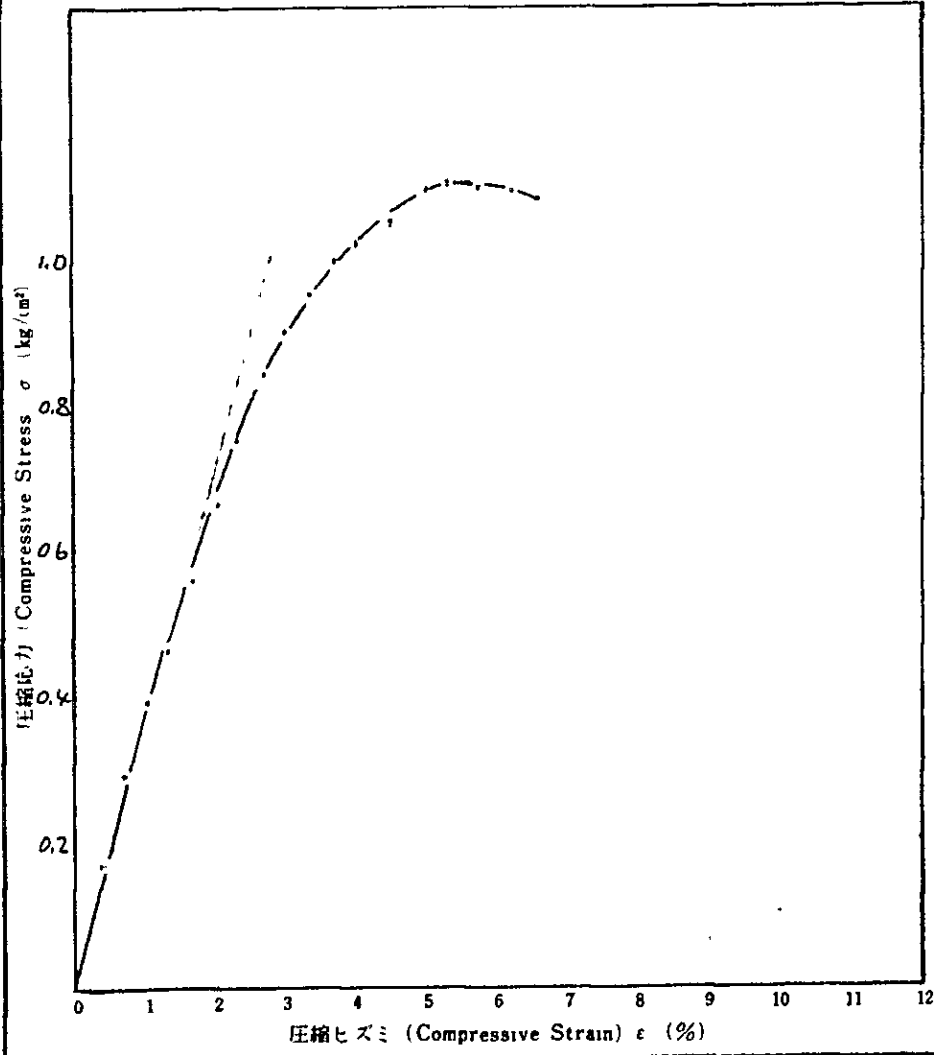
調査名・調査地点 Title, Investigation Place Thilawa Repair Dockyard Project 試験年月日 Date _____ 年 _____ 月 _____ 日

試料採取位置(深度) Sampling Place, Depth 16.0 m ~ 16.7 m 土質名称 Soil Classification Clay

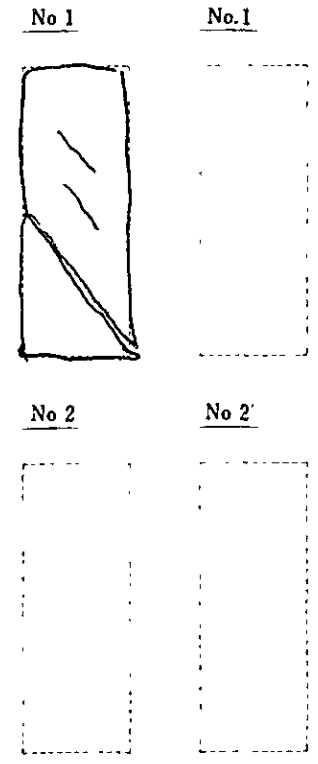
試料番号 Sample No. TWS-8 土粒子の比重 Specific Gravity _____

応力制御法 Stress Control ヒズミ制御法 Strain Control 圧縮速度 Compression Speed _____ %/min _____ mm/min

試料番号 Specimen No.	試料の状態 Specimen Condition	試料の寸法 Dimension of Specimen		含水比 Moisture Content w %	湿密度 Wet Density γ_w (kg/m ³)	空隙率 Void Ratio e	飽和度 Degree of Saturation S %	軸圧縮強度 Unconfined Compressive Strength σ_u (kg/cm ²)	破壊時ひずみ Failure Strain e (%)	変形係数 Deformation Coefficient E ₅₀ (kg/cm ²)	鋭敏比 Sensitivity Ratio S _r
		高さ Height H (cm)	直径 Diameter d (cm)								
1	乱れなす試料 Undisturbed Sample	15.0	7.5		1.74			1.10	5.5	37	
1	乱れなす試料 Remolded Sample										
2	乱れなす試料 Undisturbed Sample										
2	乱れなす試料 Remolded Sample										



試料の破壊状況
Observation at Ultimate Failure



Decayed wood contained

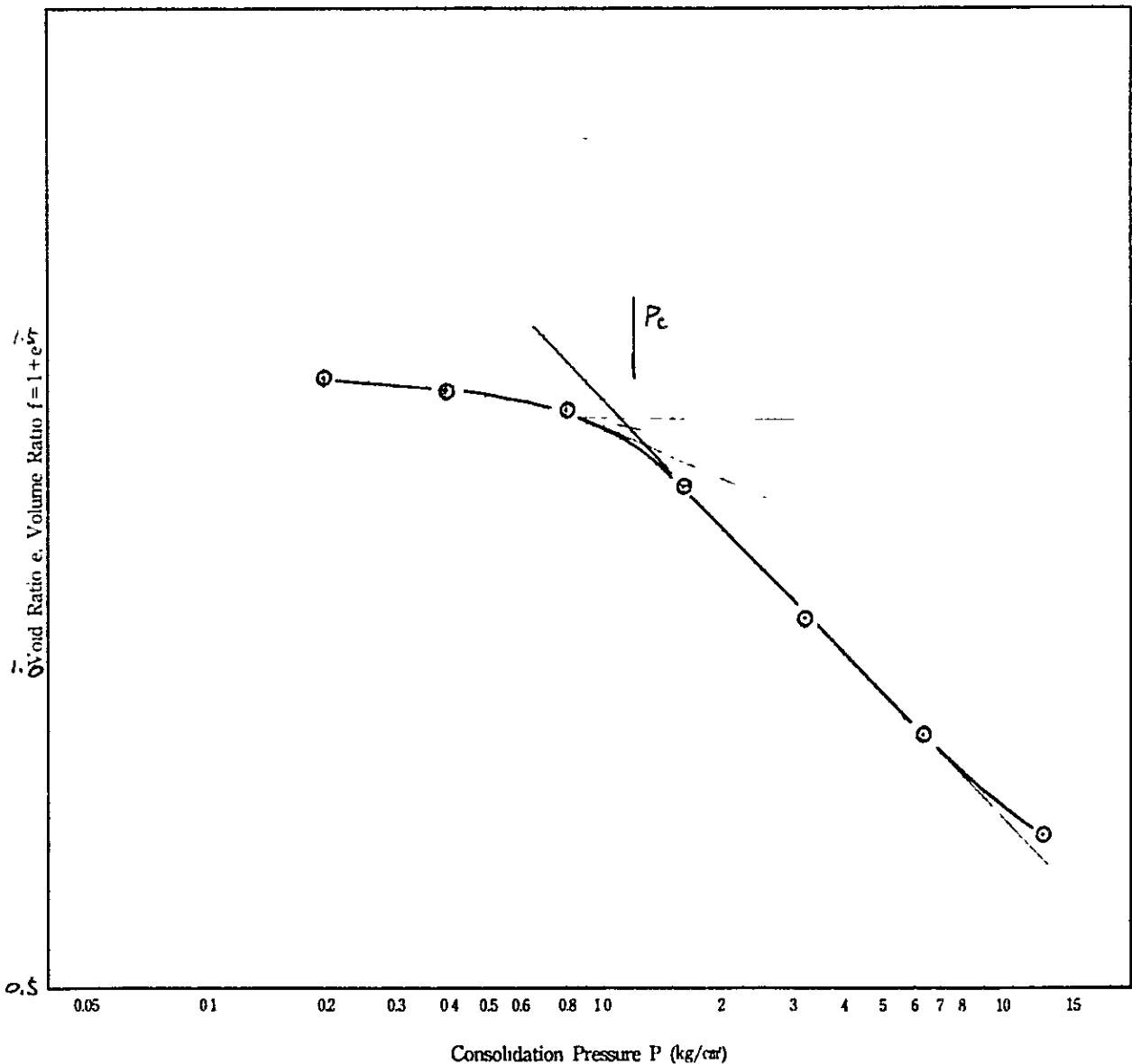
CONSOLIDATION TEST

CONSOLIDATION TEST (1)

Title, Investigation Place Thilawa Repair Dockyard Project Date _____

Sample No Sampling Elevation BH-5, D=5.0 ~ 5.7 m

Specimen Dimension	Diameter	D	6.00 cm	Moisture Content	Before Test	W _o	55.4 %	Liquid Limit	LL	%	Compression Index
	Height	2H	2.00 cm		After Test	W _f	%	Specific Gravity	G _s		
	Section Area	A	28.26 cm ²	Degree of Saturation	Before Test	S _{ro}	100 %	Initial Void Ratio	e _o	1.44	Consolidation Yield Stress
	Volume	V	56.52 cm ³		After Test	S _{rf}	%	Initial Volume Ratio	f _o	2.44	



B-5

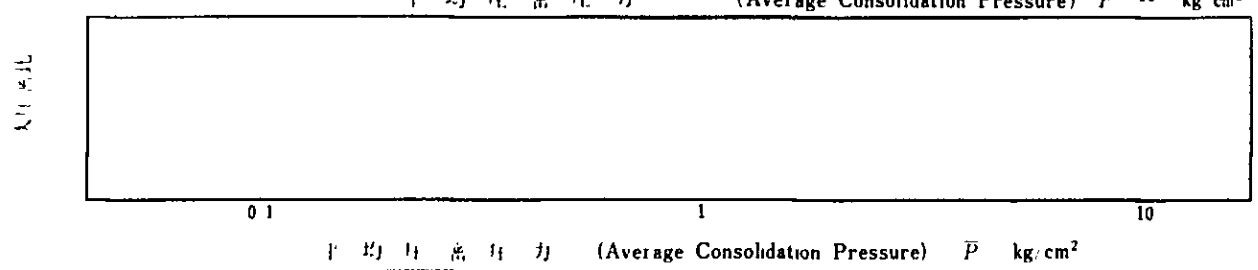
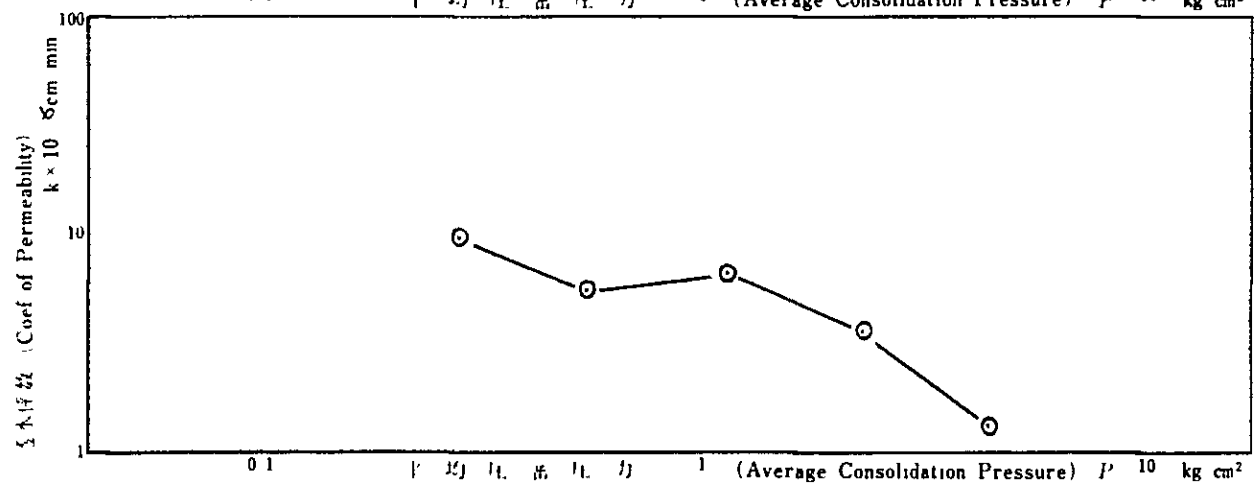
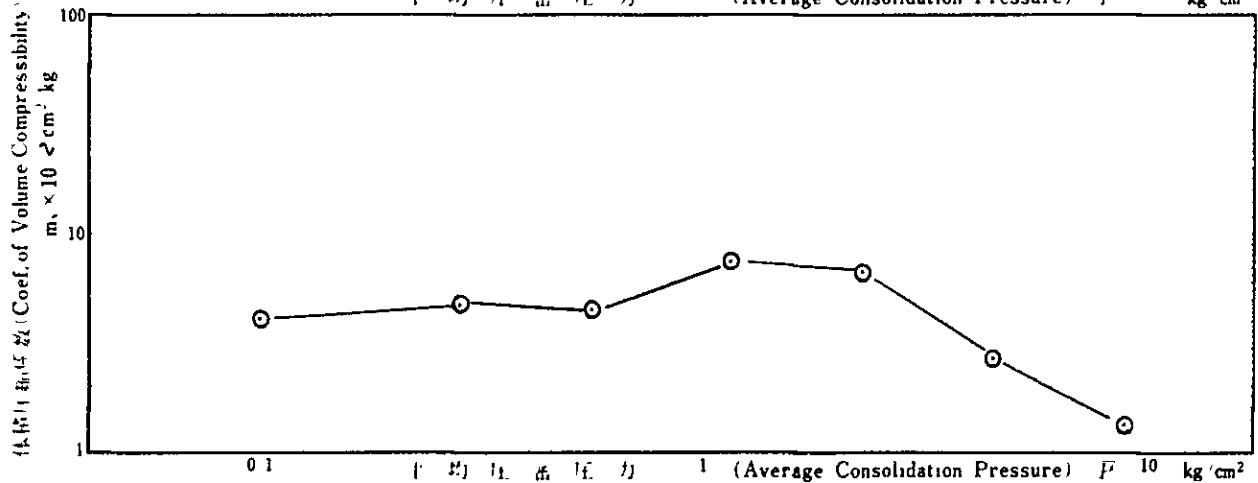
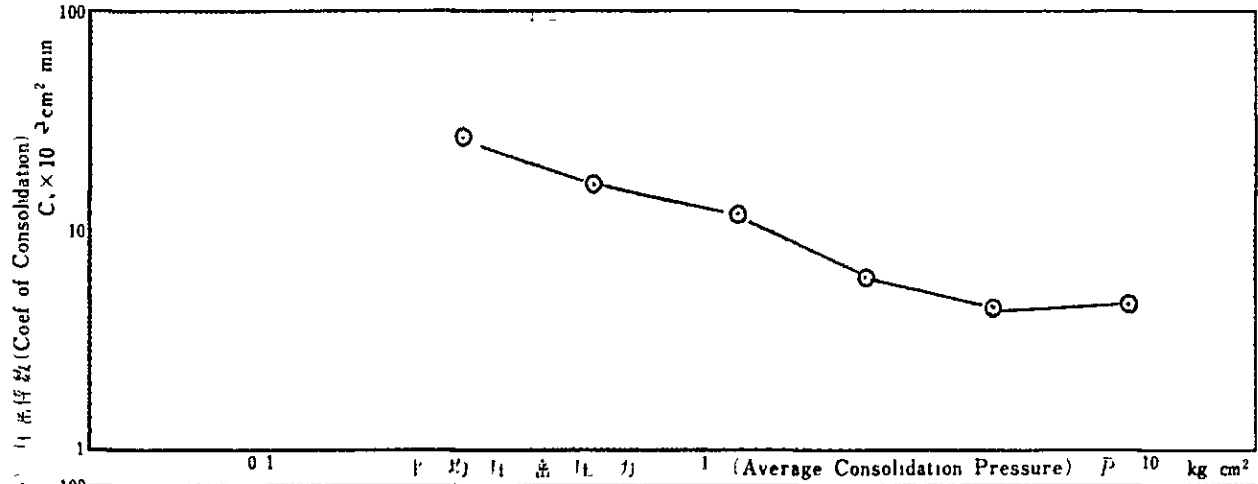
土の圧密試験 (3-3)

CONSOLIDATION TEST

調査名 調査地点
 Title Investigation Place Thilawa Repair Dockyard Project

試料番号、採取標高
 Sample No., Sampling Elevation 5.0~5.7

試験年月日
 Date 4 月 11 日 ~ 4 月 11 日

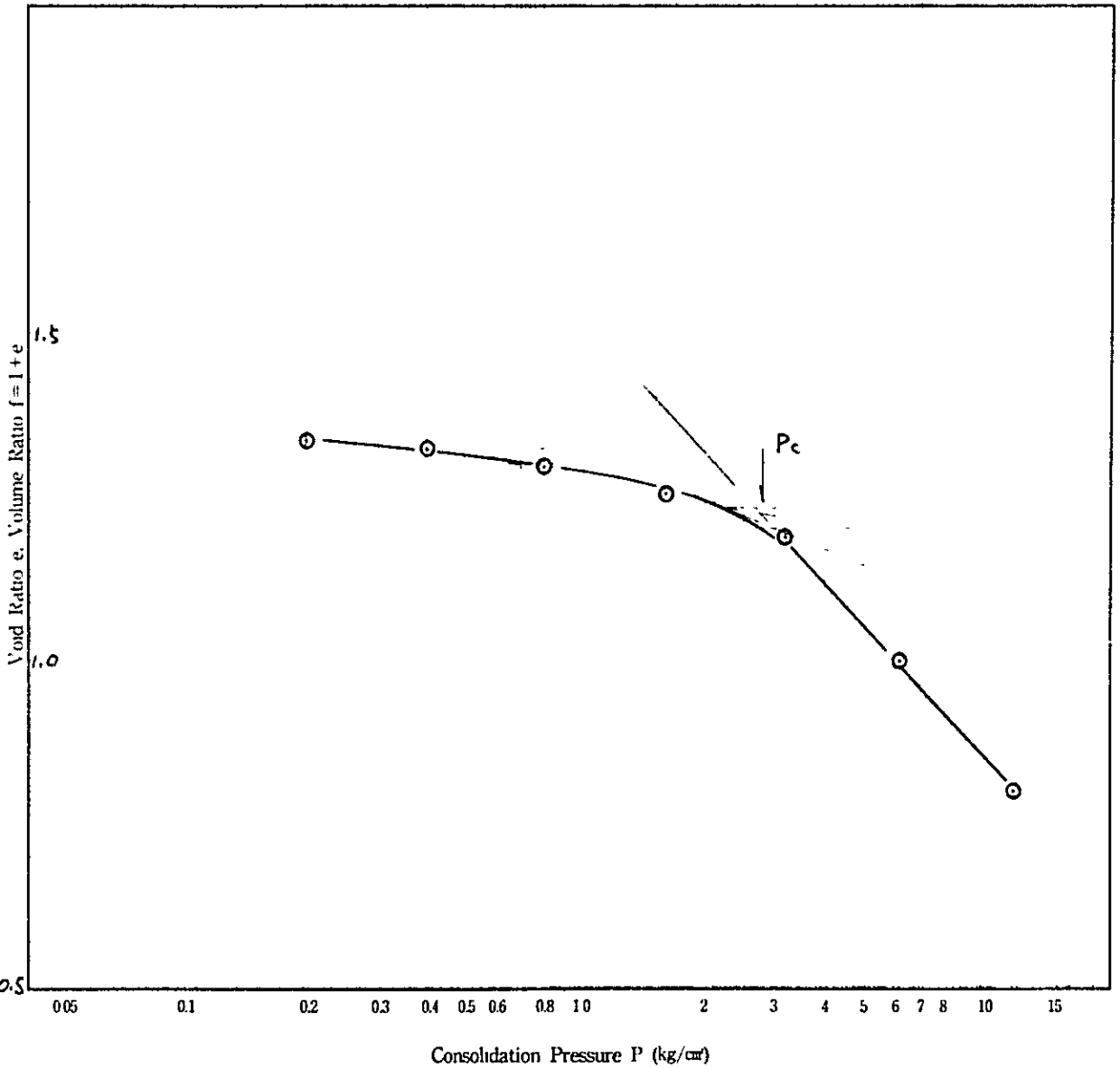


CONSOLIDATION TEST (1)

Title, Investigation Place Tillawa Repair Dockyard Project Date _____

Sample No B-5 Sampling Elevation 8.5 ~ 9.2 m

Specimen Dimension	Diameter	D.	6.00	cm	Moisture Content	Before Test	W ₀	39.1	%	Liquid Limit	LL	%	Compression Index
	Height	2H	2.00	cm		After Test	W _f	%	Specific Gravity	G _s			
	Section Area	A	28.26	cm ²	Degree of Saturation	Before Test	S ₀	%	Initial Void Ratio	e ₀	1.35	Consolidation Yield Stress	
	Volume	V	56.52	cm ³		After Test	S _f	%	Initial Volume Ratio	f ₀	2.35	P _y	



B-5

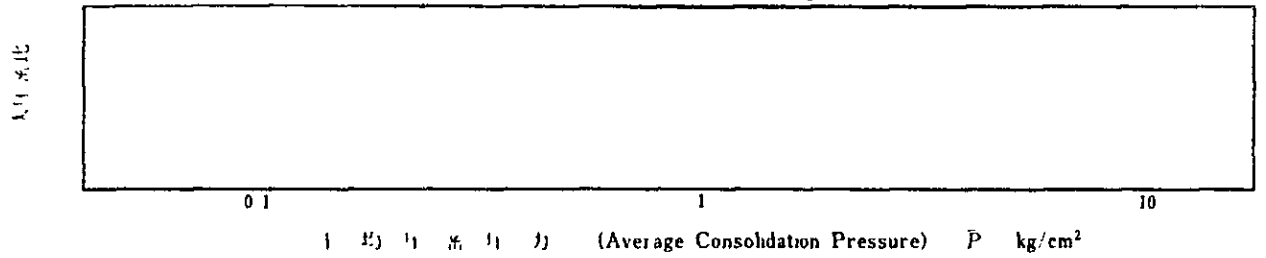
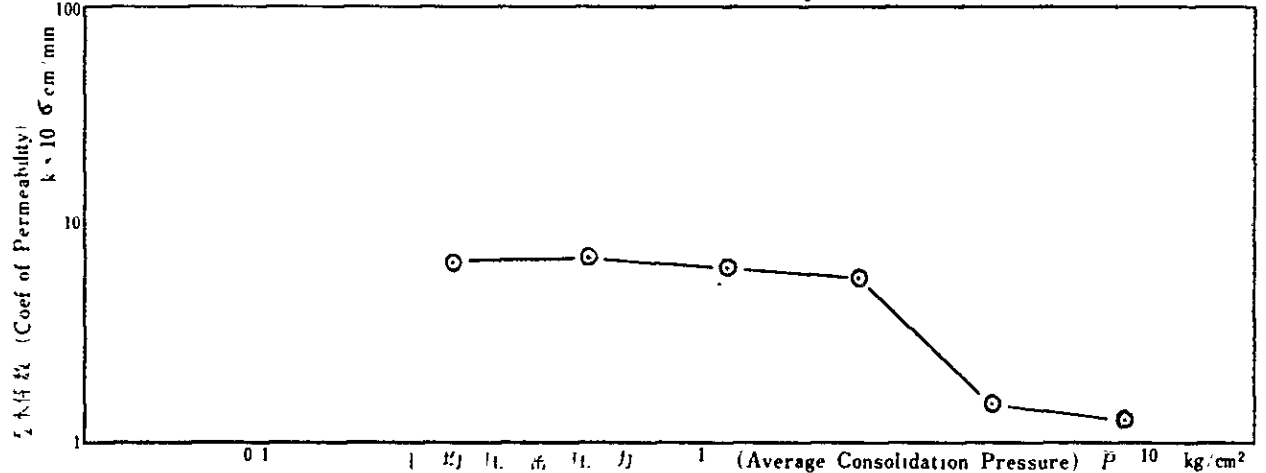
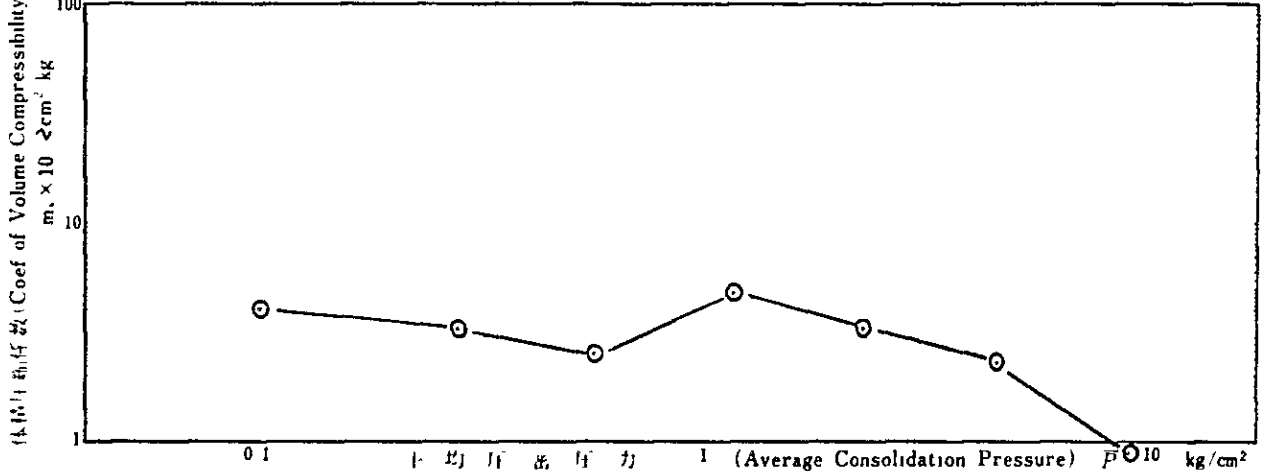
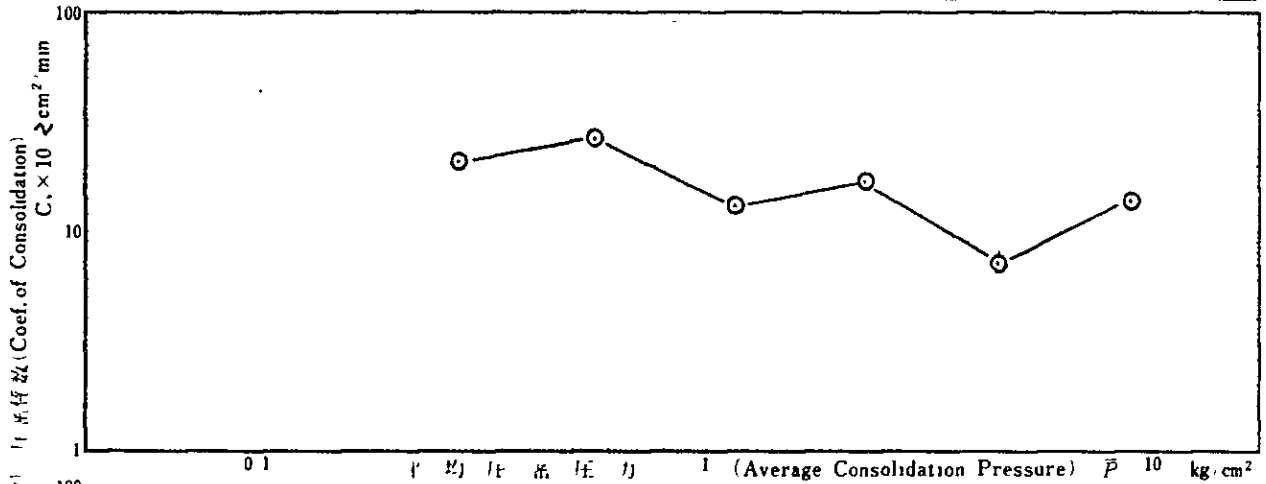
土の圧密試験 (3-3)

CONSOLIDATION TEST

調査名 調査地
 Title Investigation Place Thilawa Repair Dockyard Project

試料番号、採取標高
 Sample No., Sampling Elevation 8.5~9.2

試験年月日
 Date 年 月 日 ~ 年 月 日



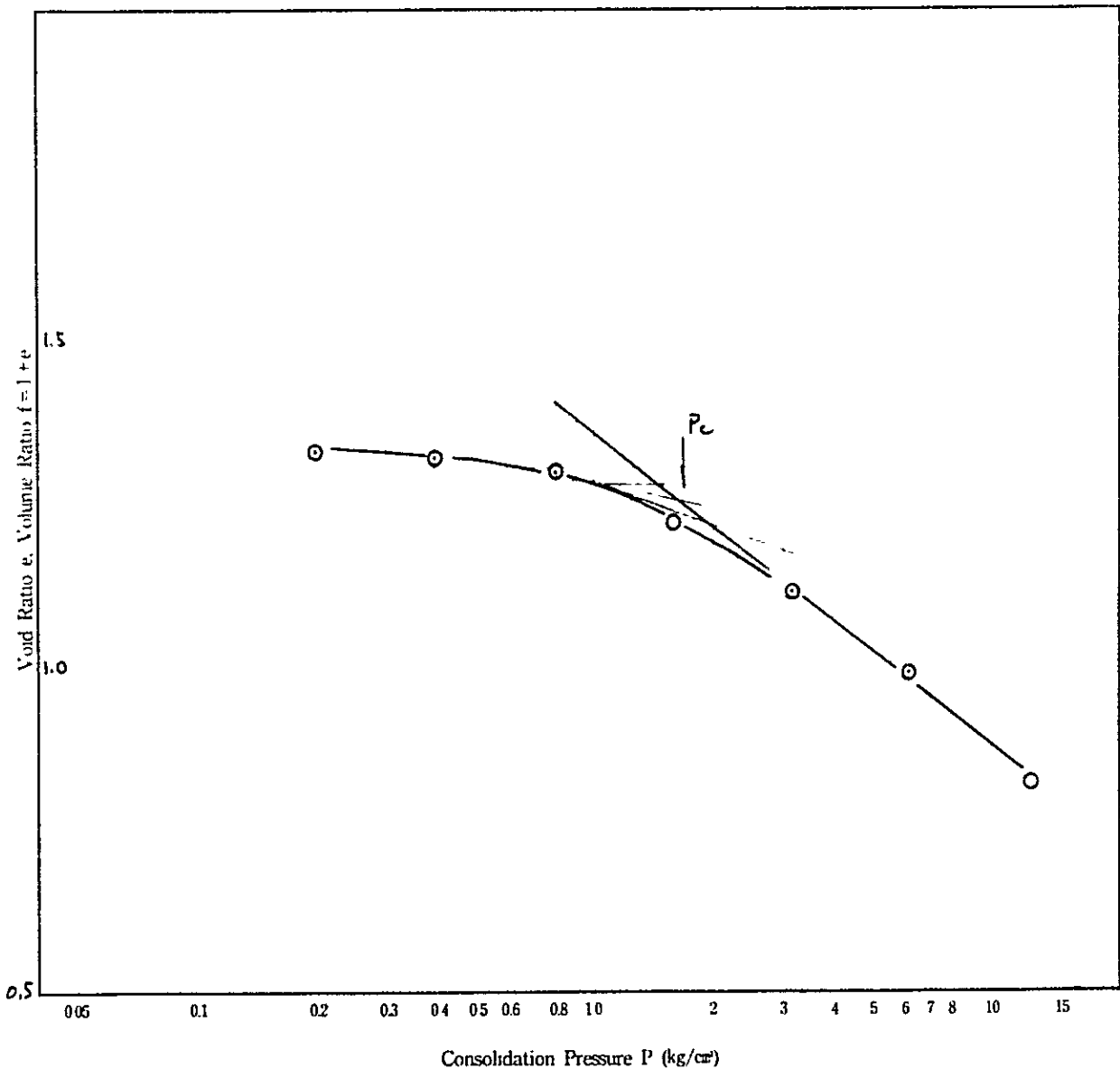
80

CONSOLIDATION TEST (1)

Title, Investigation Place Thilawa Repair Dockyard Project Date _____

Sample No BH-5 Sampling Elevation D = 12.0 ~ 12.7 m

Specimen Dimension	Diameter	D	6.0 cm	Moisture Content	Before Test	W ₀	45.7 %	Liquid Limit	LL	%	Compression Index
	Height	H	2.0 cm		After Test	W _f	%	Specific Gravity	G _s		
	Section Area	A	28.26 cm ²	Degree of Saturation	Before Test	S ₀	%	Initial Void Ratio	e ₀	1.35	Consolidation Yield Stress
	Volume	V	56.52 cm ³		After Test	S _f	%	Initial Volume Ratio	f ₀	2.35	



B-5

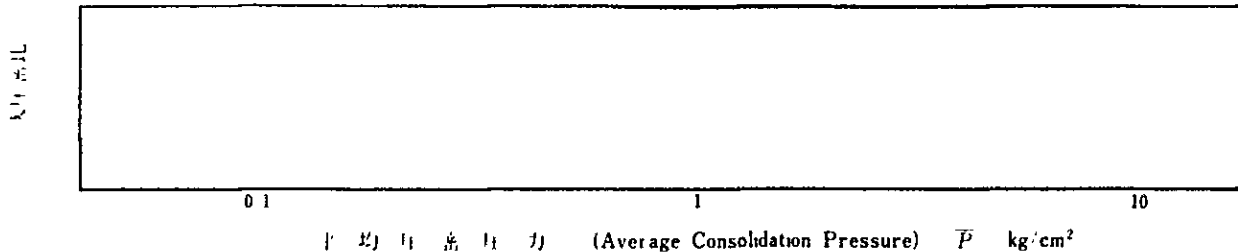
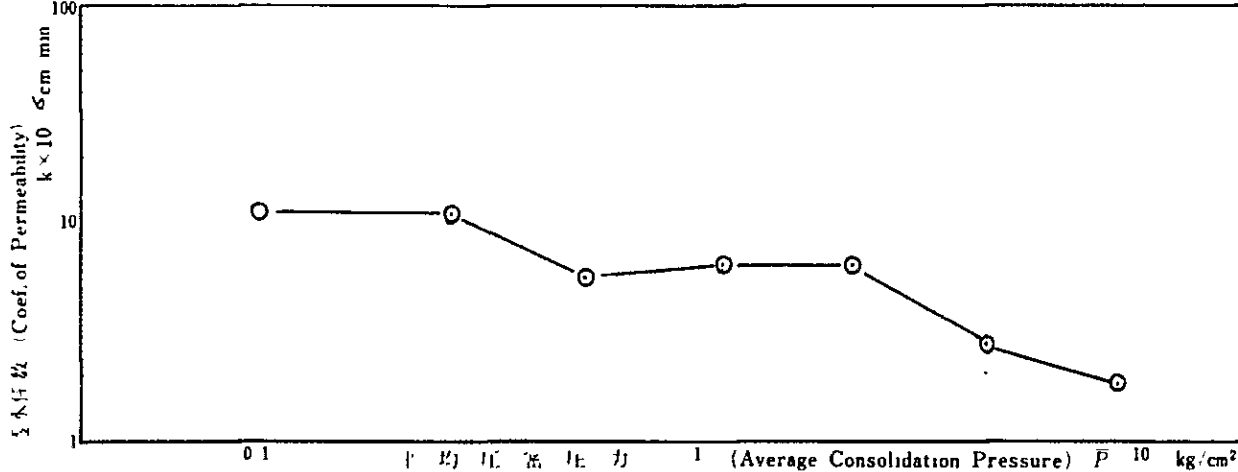
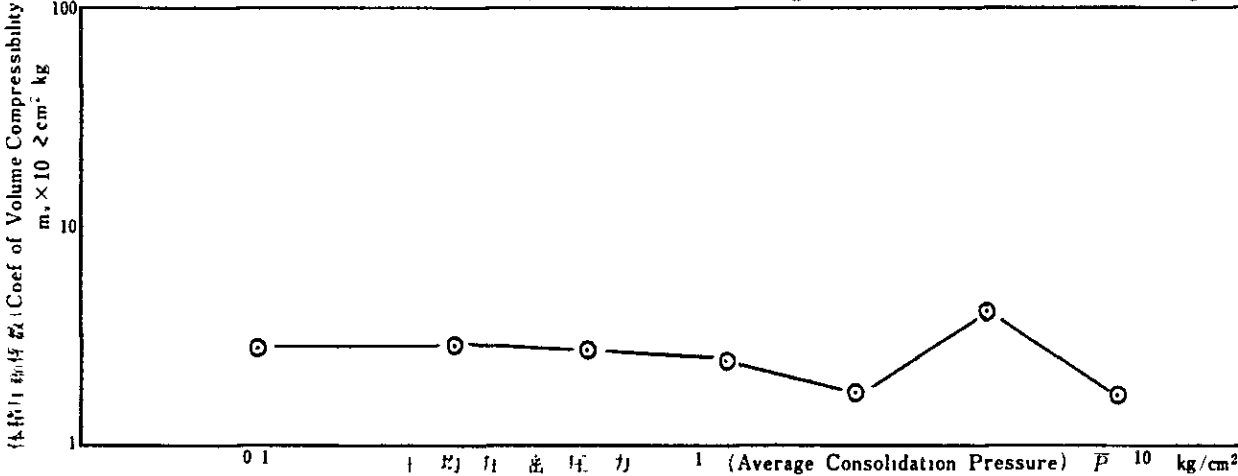
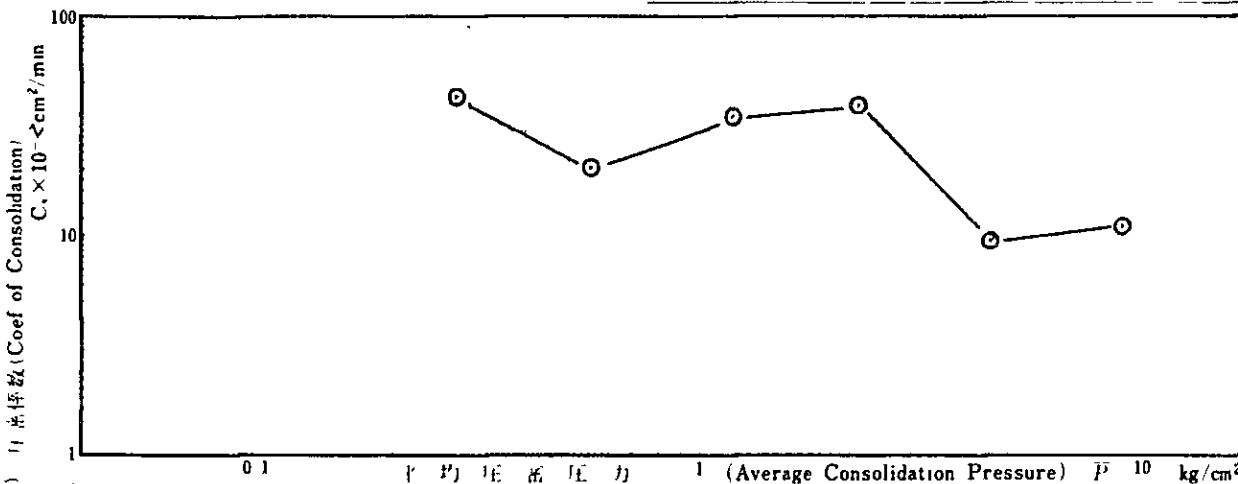
土の圧密試験 (3-3)

CONSOLIDATION TEST

調査名 調査地点
Title Investigation Place **Thilawa Repair Dockyard Project**

試料番号、採取標高
Sample No., Sampling Elevation **12.0 ~ 12.7**

試験年月日
Date 年 月 日 - 年 月 日

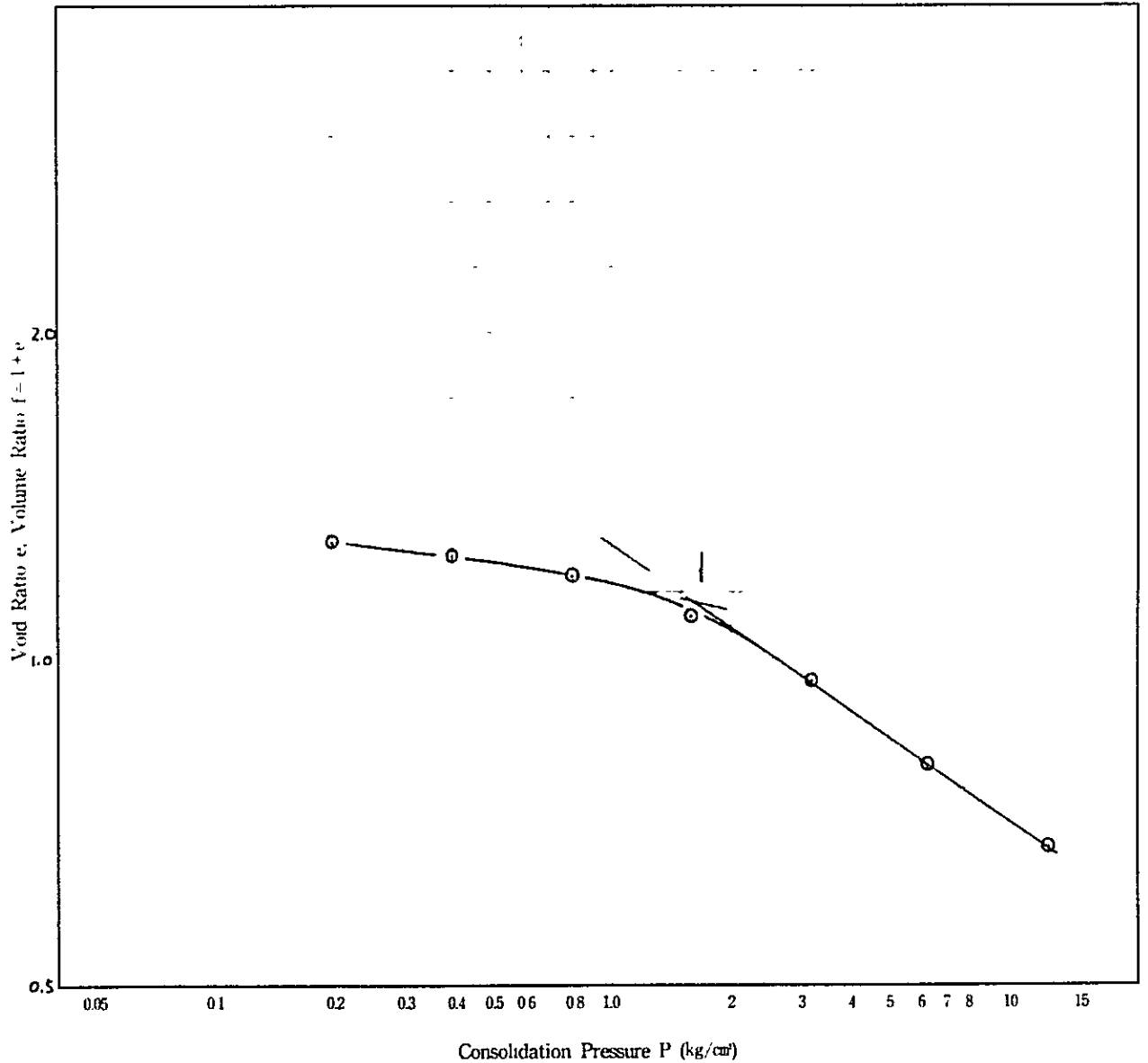


CONSOLIDATION TEST (1)

Title, Investigation Place Thilawa Repair Dockyard Project Date _____

Sample No B-5 Sampling Elevation TWS-6 18.0 ~ 18.7 m

Specimen Dimension	Diameter	D	6.0 cm	Moisture Content	Before Test	W _o	47.8 %	Liquid Limit	LL	%	Compression Index
	Height	H	2.0 cm		After Test	W _f	20.4 %	Specific Gravity	G _s	2.60	
	Section Area	A	28.26 cm ²	Degree of Saturation	Before Test	S _{ro}	100 %	Initial Void Ratio	e _o	1.19	Consolidation Yield Stress
	Volume	V	56.52 cm ³		After Test	S _{rf}	100 %	Initial Volume Ratio	f _o	2.19	



83

B-5

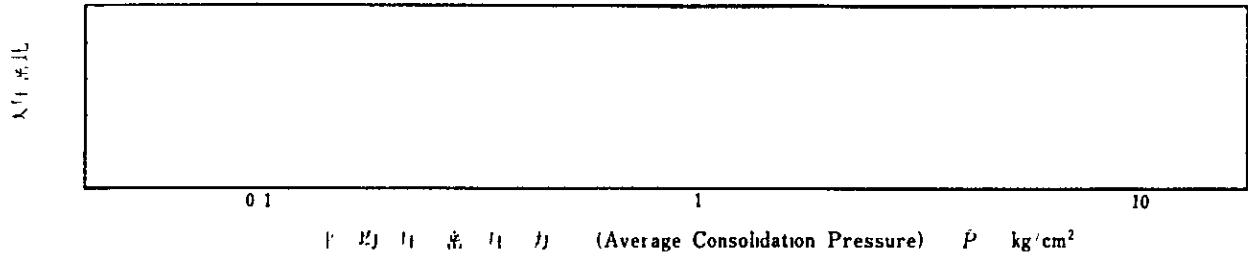
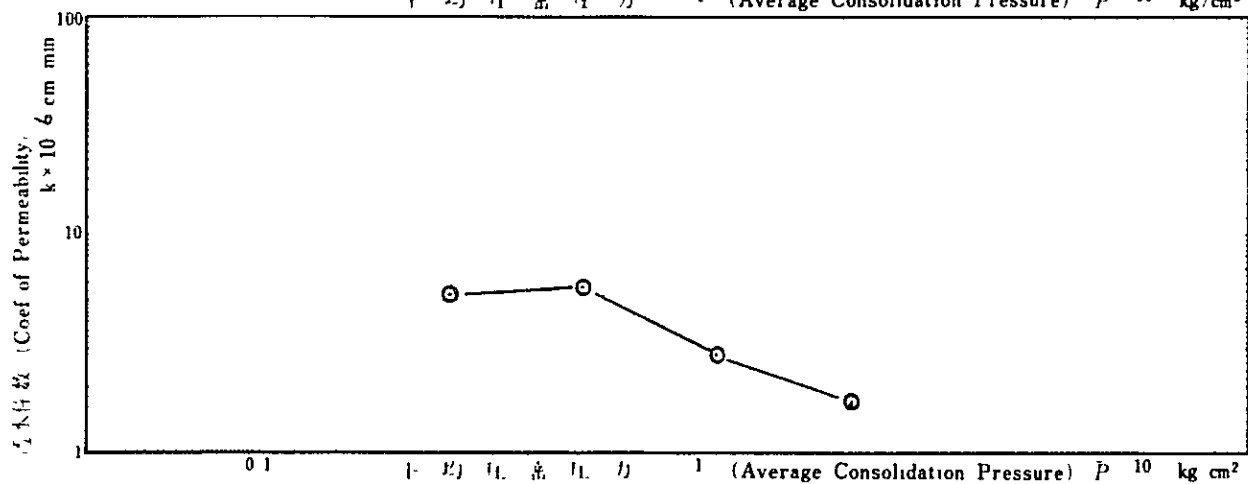
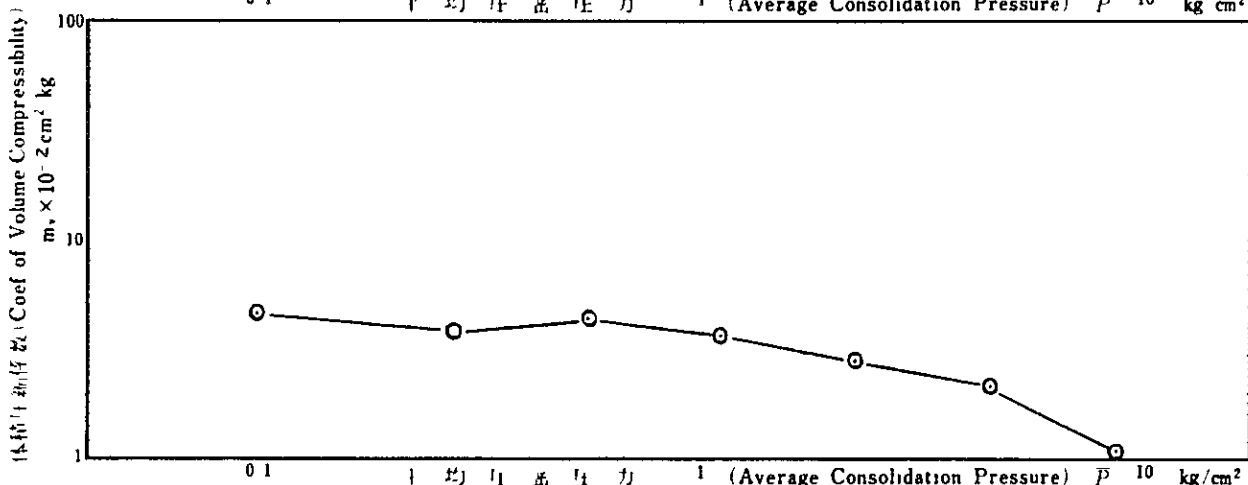
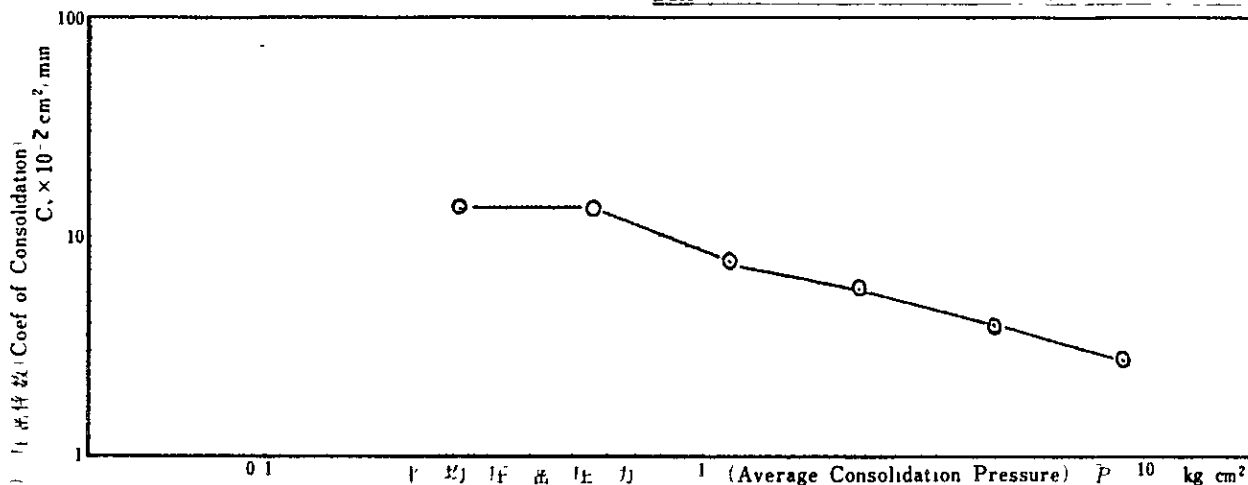
土の圧密試験 (3-3)

CONSOLIDATION TEST

調査名、調査地点
Title, Investigation Place Thilawa Repair Dockyard Project

試料番号、採取標高
Sample No., Sampling Elevation 18.0 ~ 18.7 m

試験年月日
Date _____ 年 _____ 月 _____ 日



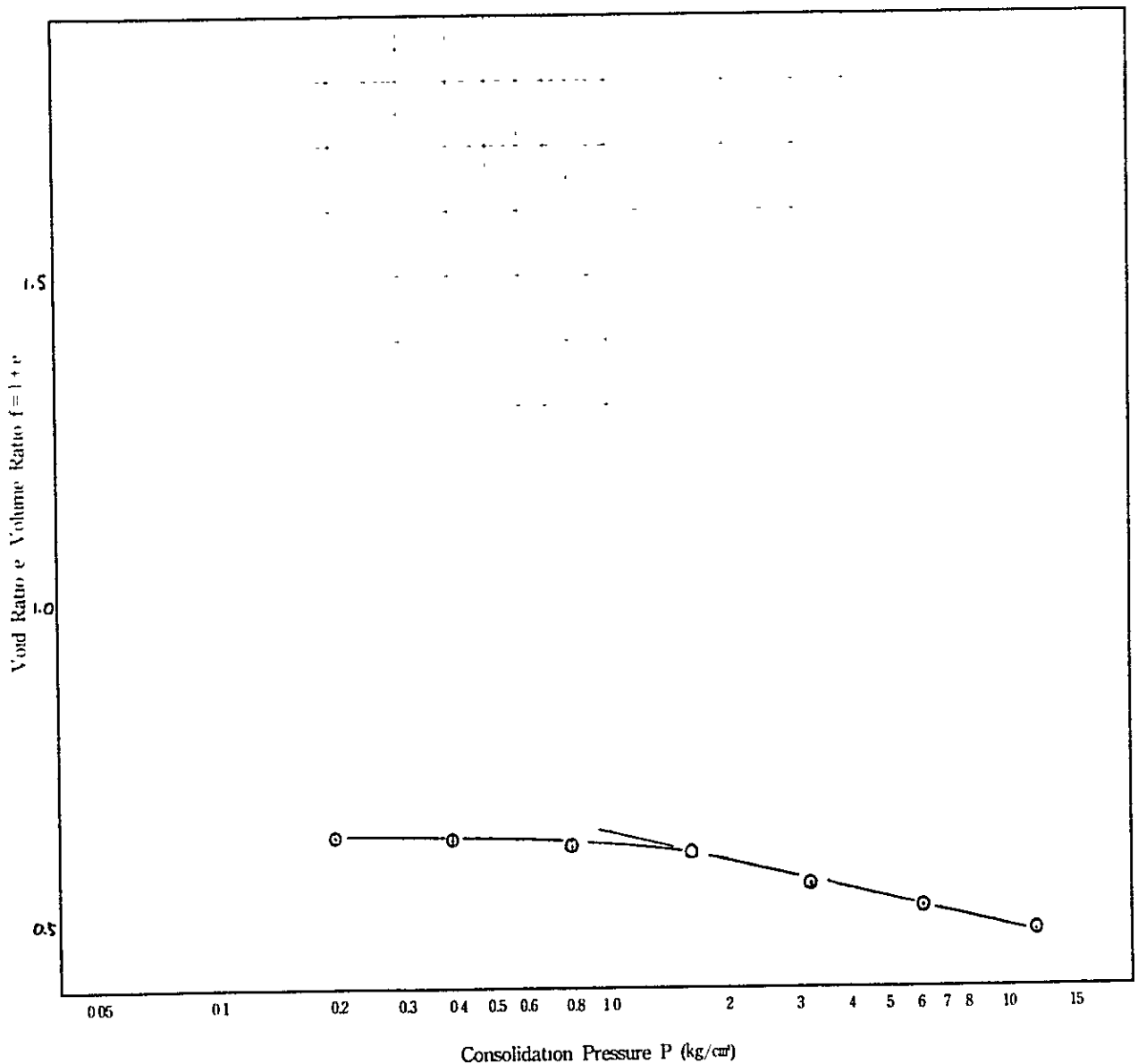
89

CONSOLIDATION TEST (1)

Title, Investigation Place Thilawa Repair Dockyard Project Date _____

Sample No. Sampling Elevation BH-5, 21.5 ~ 22.0 m

Specimen Dimension	Diameter	D	6.0 cm	Moisture Content	Before Test	W _o	23.7 %	Liquid Limit	LL	%	Compression Index
	Height	ZH	2.0 cm		After Test	W _i	18.6 %	Specific Gravity	G _s	2.60	
	Section Area	A	28.26 cm ²	Degree of Saturation	Before Test	S _{ro}	96.7 %	Initial Void Ratio	e _o	0.64	Consolidation Yield Stress
	Volume	V	56.52 cm ³		After Test	S _{rf}	100 %	Initial Volume Ratio	f _o	1.64	



8r

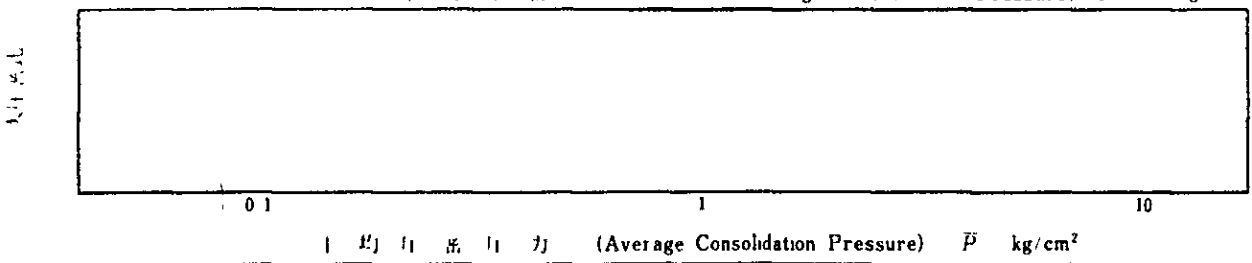
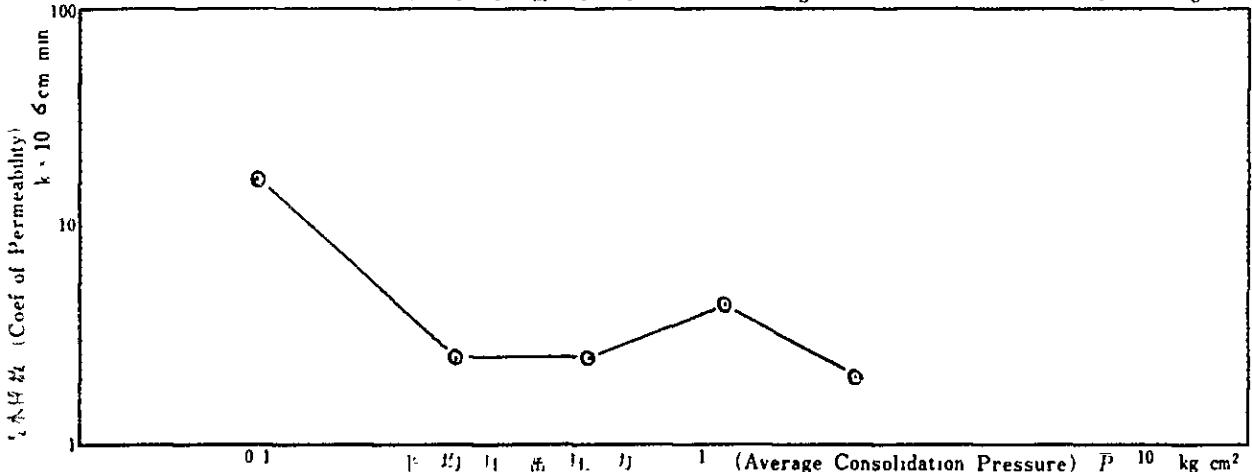
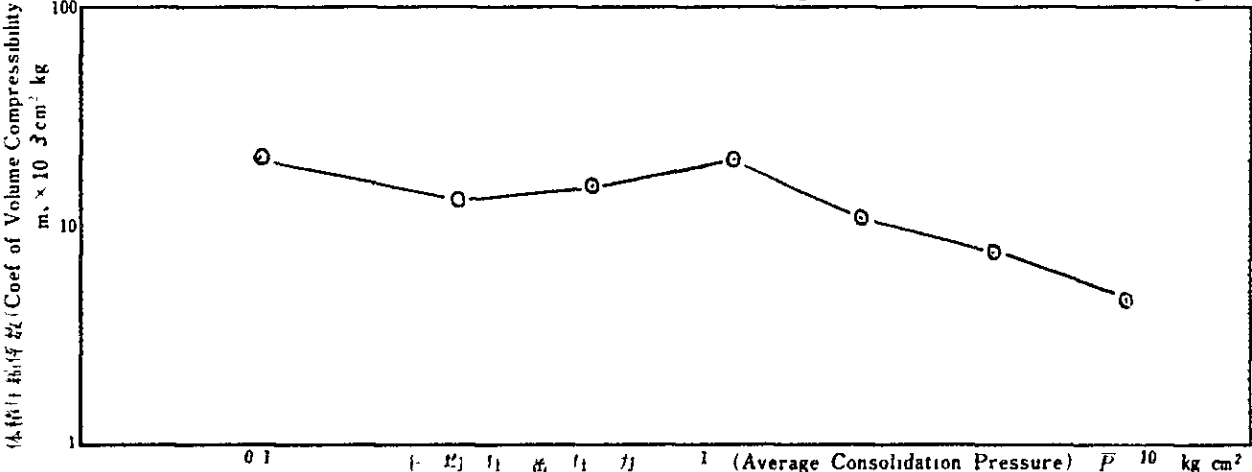
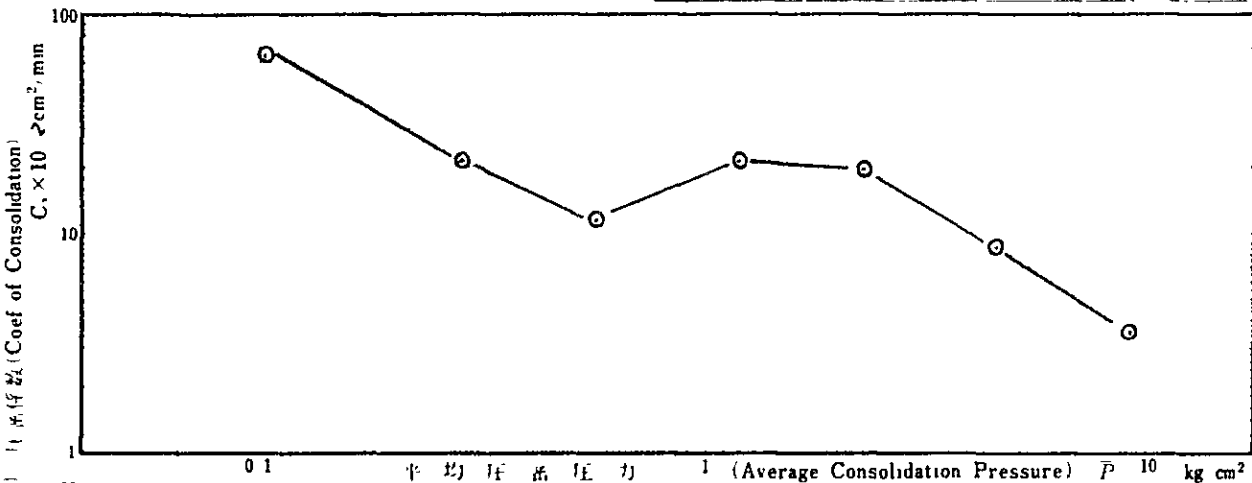
B-5

土の圧密試験 (3-3)

CONSOLIDATION TEST

調査名 調査地点
Title Investigation Place **Thilawa Repair Dockyard Project**

試料番号、採取標高
Sample No., Sampling Elevation TWS - 7 21.5 ~ 22.0 m
試験年月日
Date 4 月 11 ~ 4 月 11



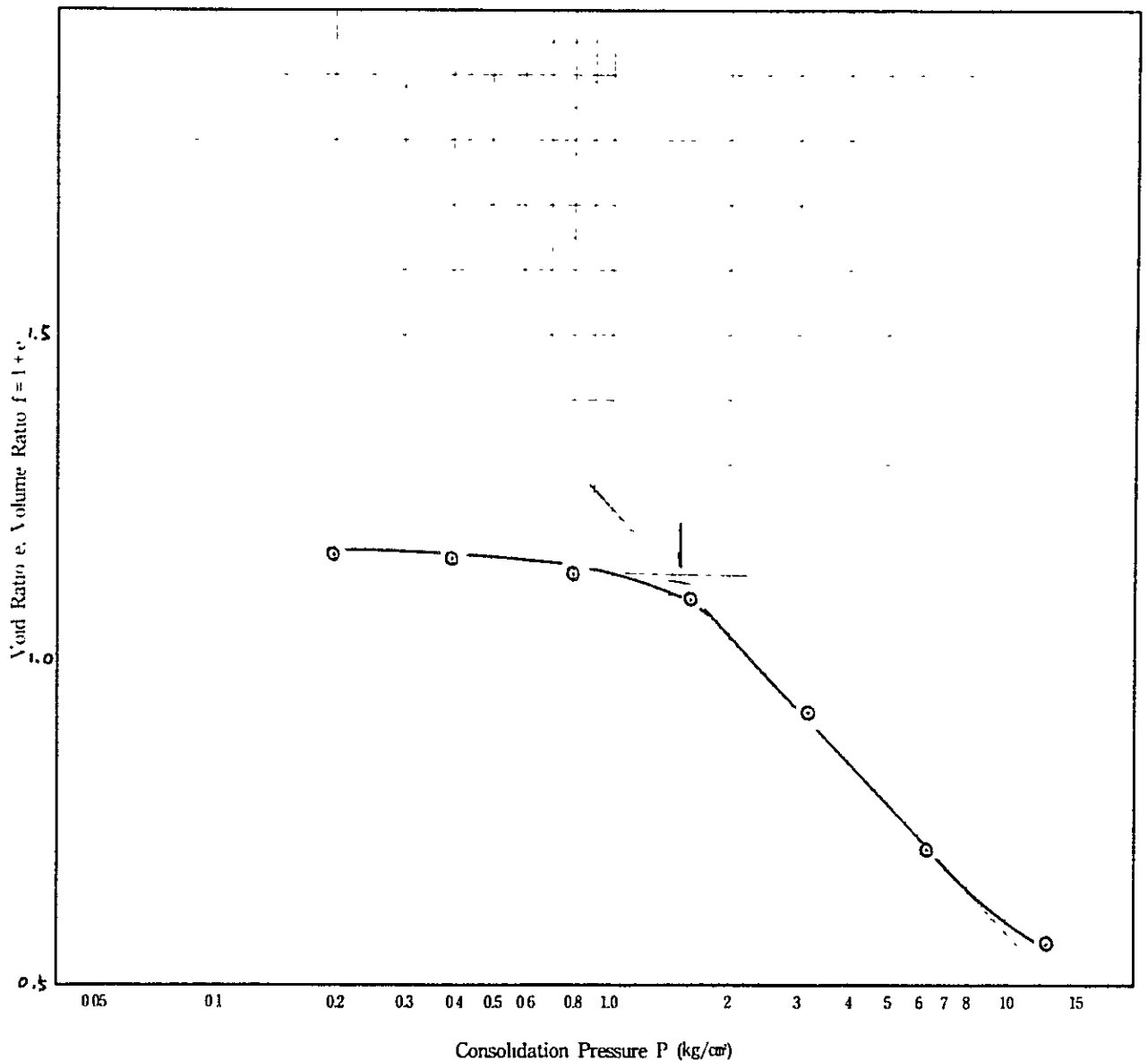
86

CONSOLIDATION TEST (1)

Title, Investigation Place Thilawa Repair Dockyard Project Date _____

Sample No B-10 Sampling Elevation TWS-2, 4.0~4.7m

Specimen Dimension	Diameter	D	6.0 cm	Moisture Content	Before Test	W ₀	47.8 %	Liquid Limit	LL	%	Compression Index
	Height	2H	2.0 cm		After Test	W _f	21.5 %	Specific Gravity	G _s	2.60	
	Section Area	A	28.26 cm ²	Degree of Saturation	Before Test	S ₀	100 %	Initial Void Ratio	e ₀	1.17	Consolidation Yield Stress
	Volume	V	56.52 cm ³		After Test	S _f	100 %	Initial Volume Ratio	f ₀	2.17	



B-10

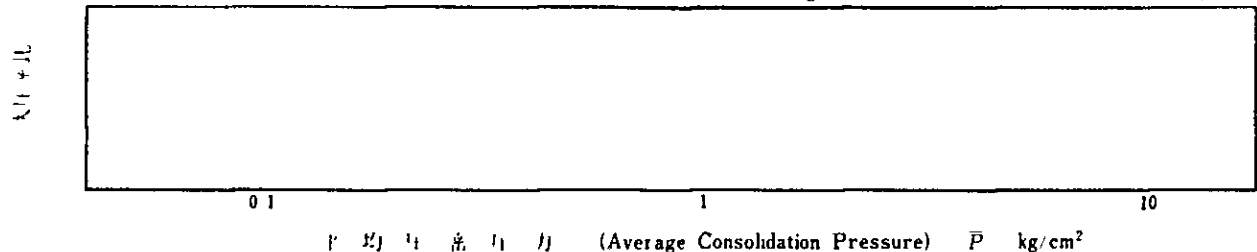
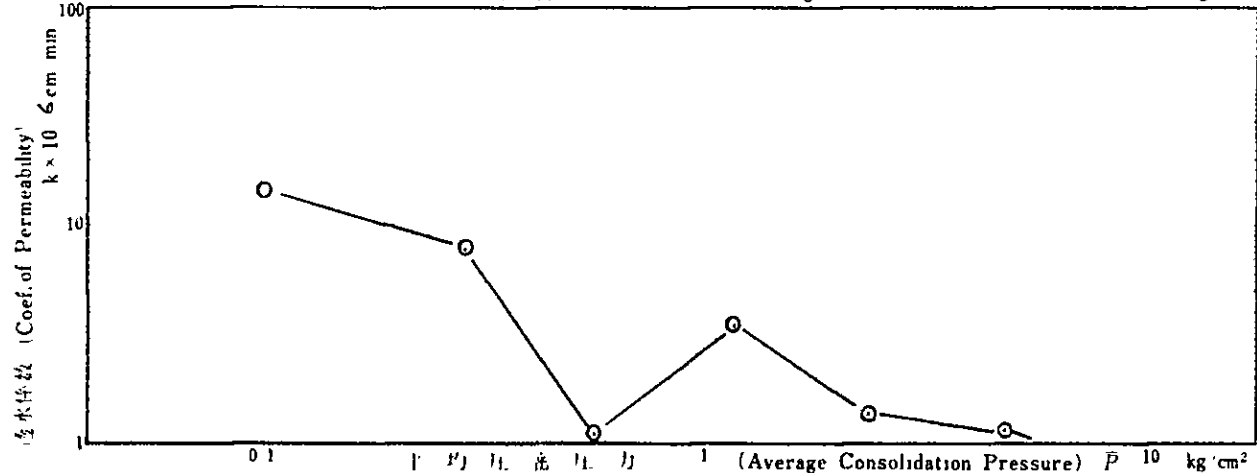
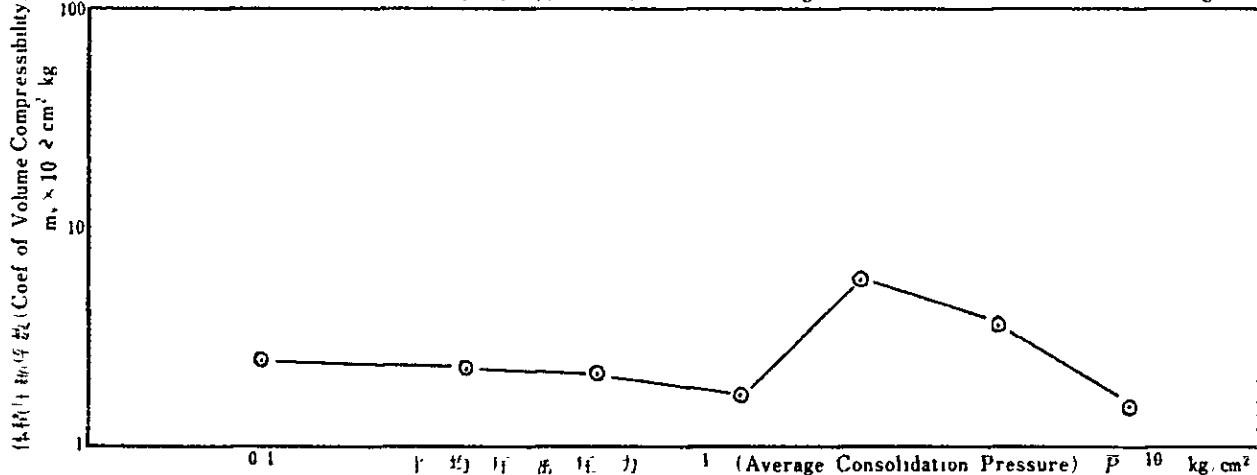
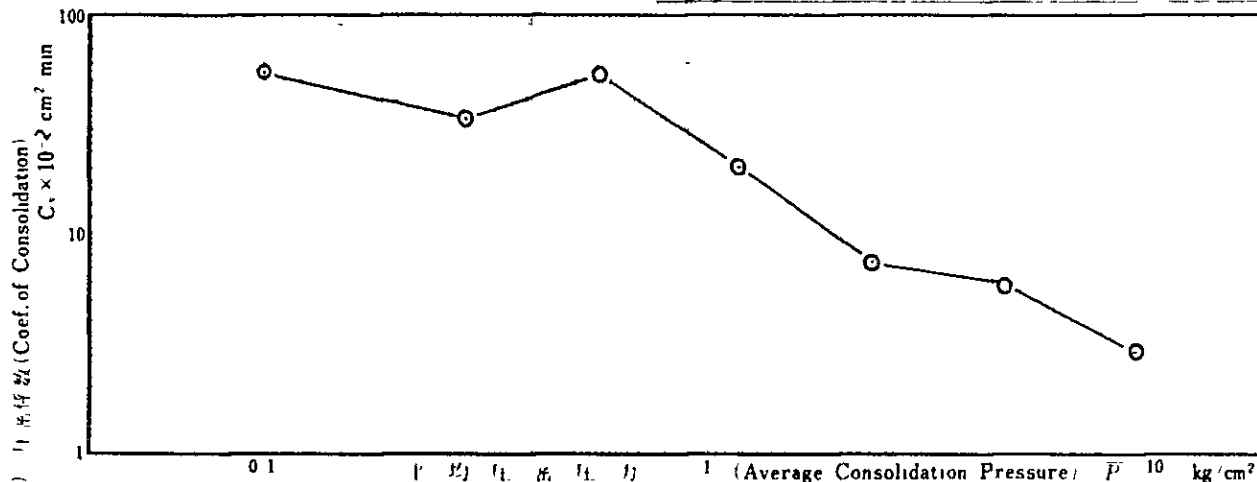
土の圧密試験 (3-3)

CONSOLIDATION TEST

調査名、調査地所
Title, Investigation Place Thilawa Repair Dockyard Project

試料番号、採取標高
Sample No., Sampling Elevation TWS-2, 4.0~4.7m

試験年月日
Date 年 月 日 ~ 年 月 日



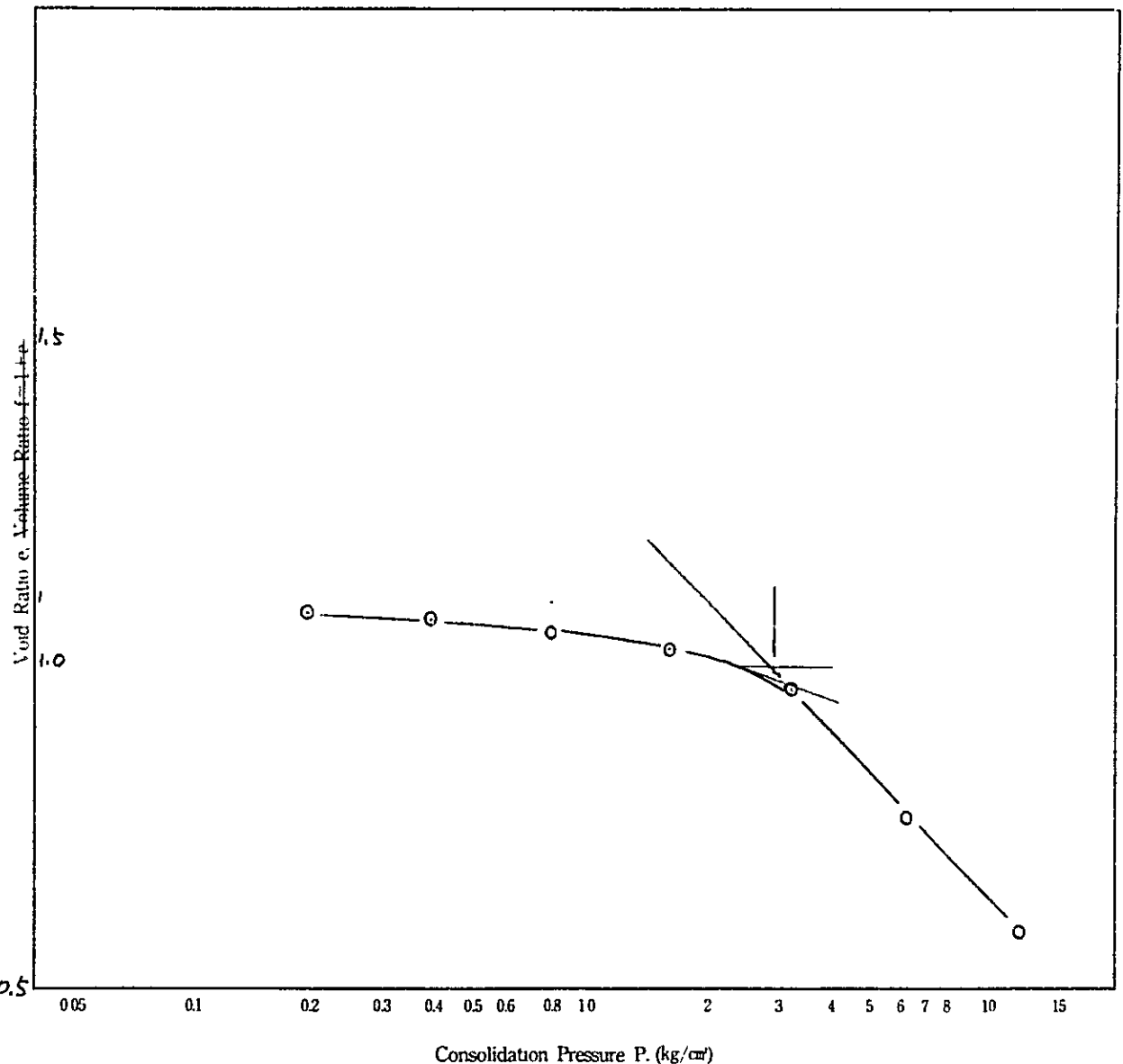
98

CONSOLIDATION TEST (1)

Title, Investigation Place Thilawa Repair Dockyard Project Date _____

Sample No. Sampling Elevation B-10 TWS-4 8.0~8.8

Specimen Dimension	Diameter	D	6.0 cm	Moisture Content	Before Test	W ₀	40.5 %	Liquid Limit	LL	%	Compression Index
	Height	H	2.0 cm		After Test	W ₁	21.3 %	Specific Gravity	G _s	2.60	
	Section Area	A	28.26 cm ²	Degree of Saturation	Before Test	S ₀	100 %	Initial Void Ratio	e ₀	0.99	Consolidation Yield Stress
	Volume	V	56.52 cm ³		After Test	S ₁	100 %	Initial Volume Ratio	f ₀	1.99	



87

B-10

土の圧密試験 (3-3)

CONSOLIDATION TEST

調査名、調査地

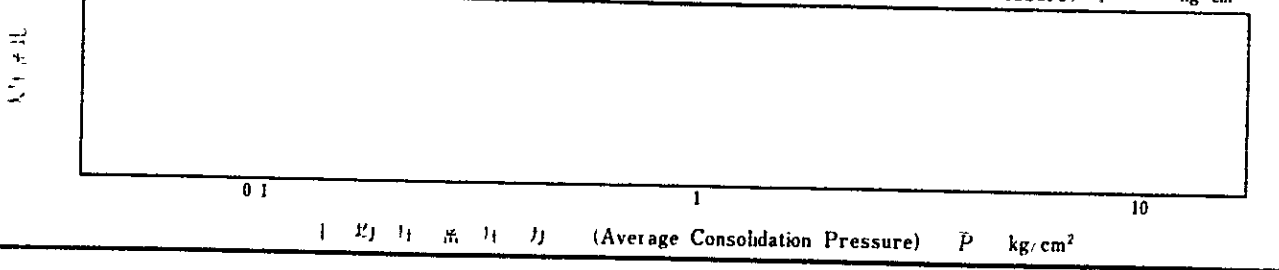
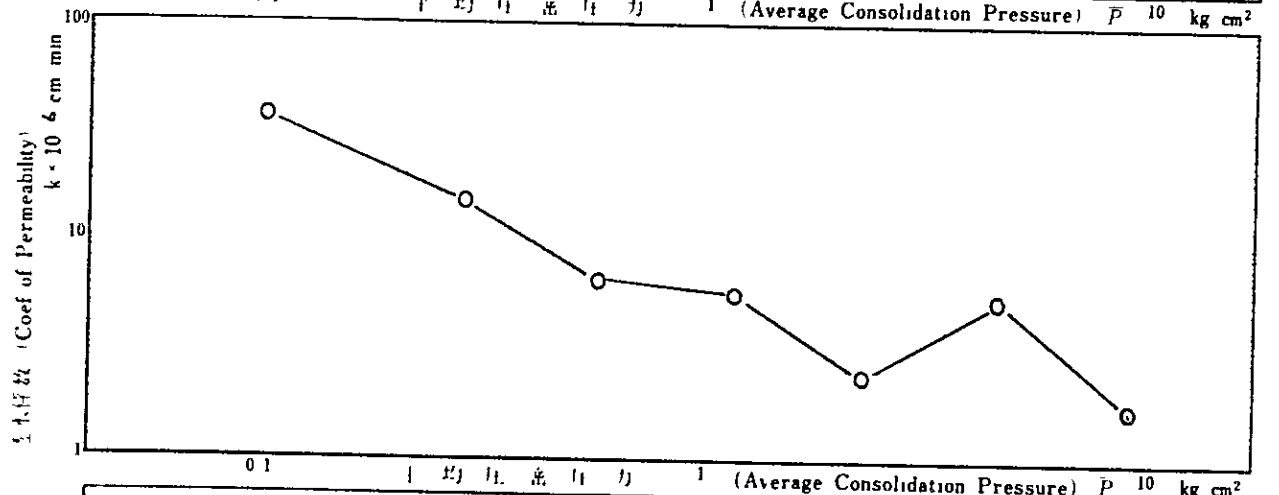
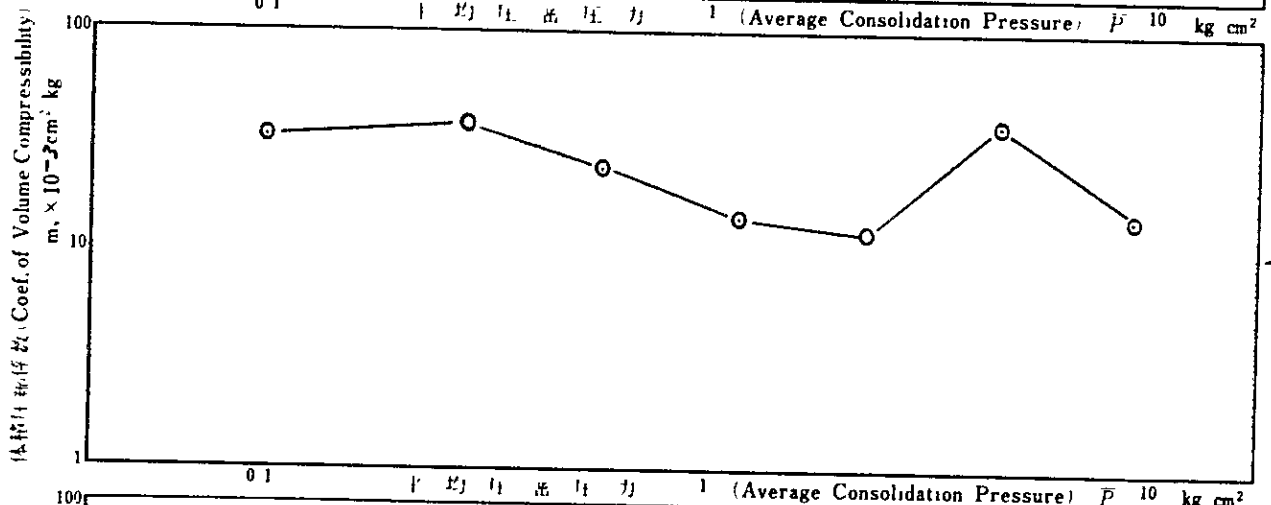
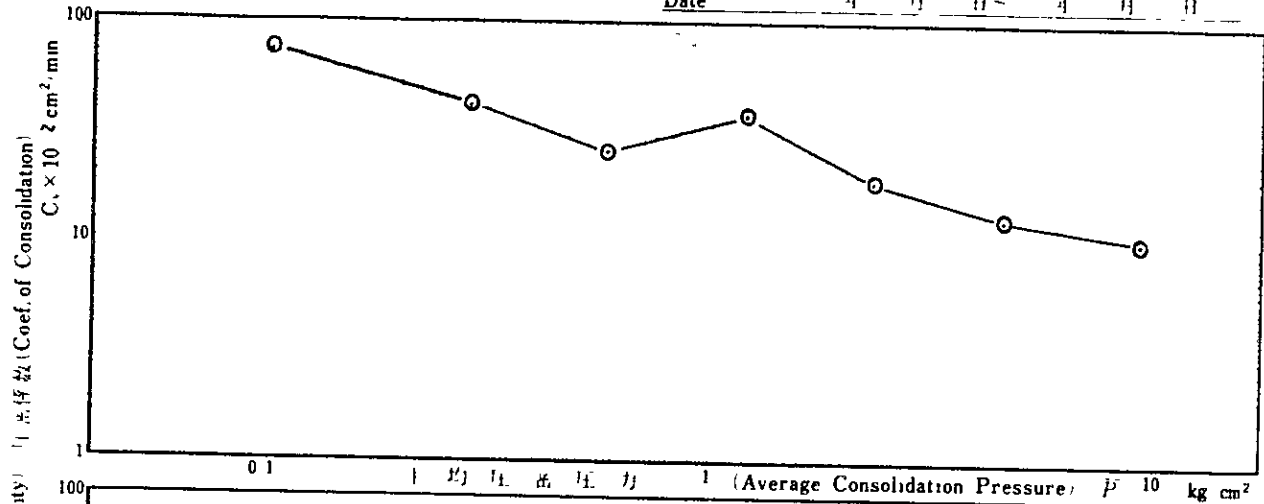
Title, Investigation Place Thilawa Repair Dockyard Project

試料番号、採取標高

Sample No., Sampling Elevation TWS-4, 8.0~8.8

試験年月日

Date 4 月 11 日 - 4 月 11 日



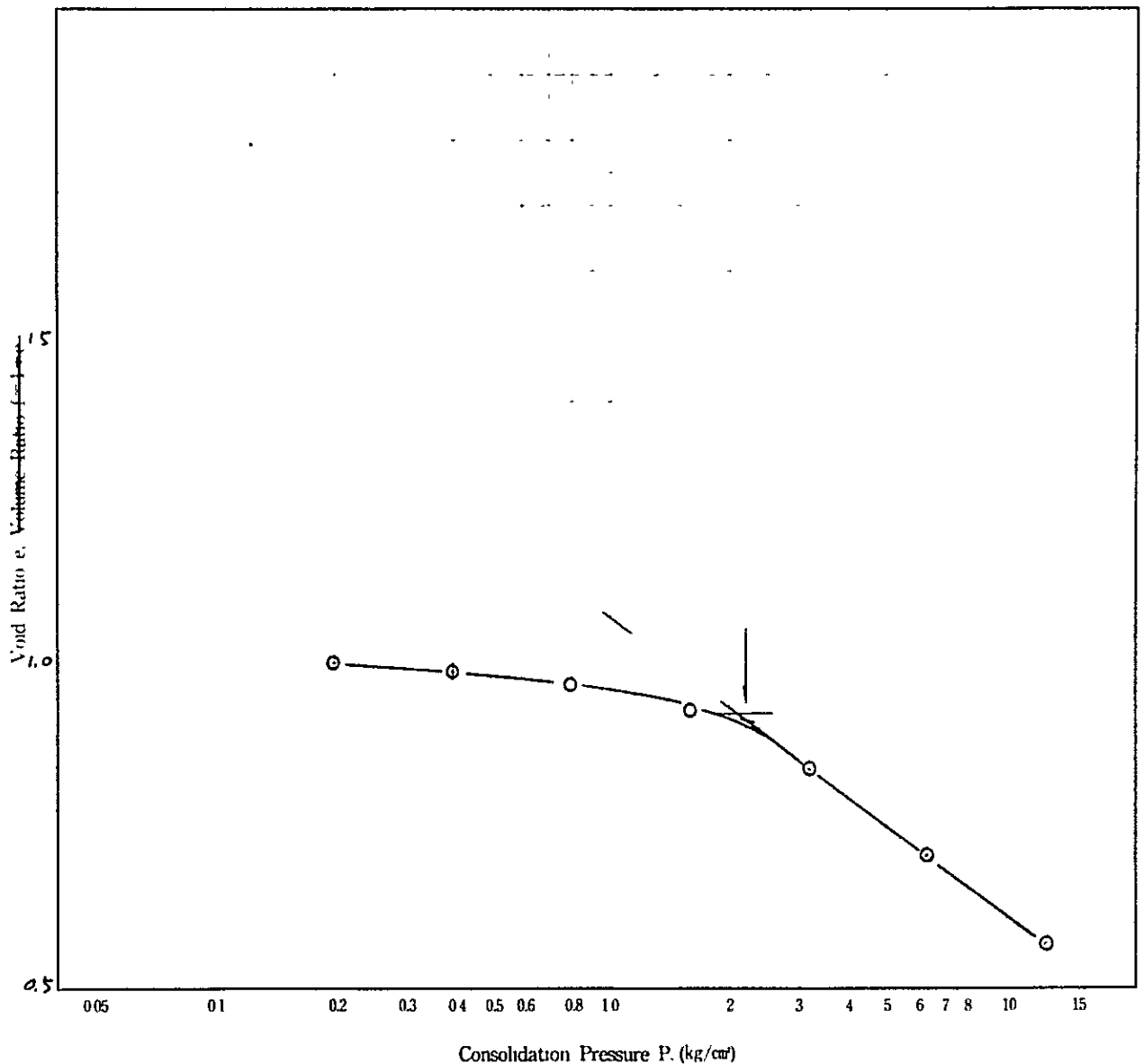
88

CONSOLIDATION TEST (1)

Title, Investigation Place Thilawa Repair Dockyard Project Date _____

Sample No. Sampling Elevation B-10, TWS-5, 10,0 ~ 10,7 m

Specimen Dimension	Diameter	D	6.0 cm	Moisture Content	Before Test	W ₀	39.5 %	Liquid Limit	LL	%	Compression Index	
	Height	H	2.0 cm		After Test	W _f	20.8 %		Specific Gravity	G _s		2.60
	Section Area	A	28.26 cm ²	Degree of Saturation	Before Test	S ₀	100 %	Initial Void Ratio		e ₀	1.01	Consolidation Yield Stress
	Volume	V	56.52 cm ³		After Test	S _f	100 %		Initial Volume Ratio	f ₀	2.01	



89

B-10

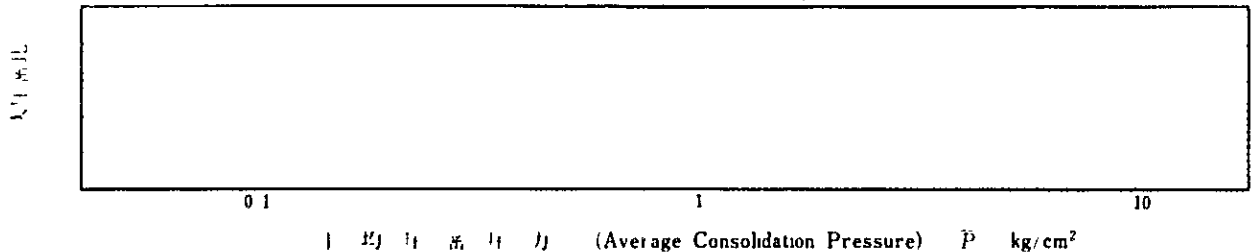
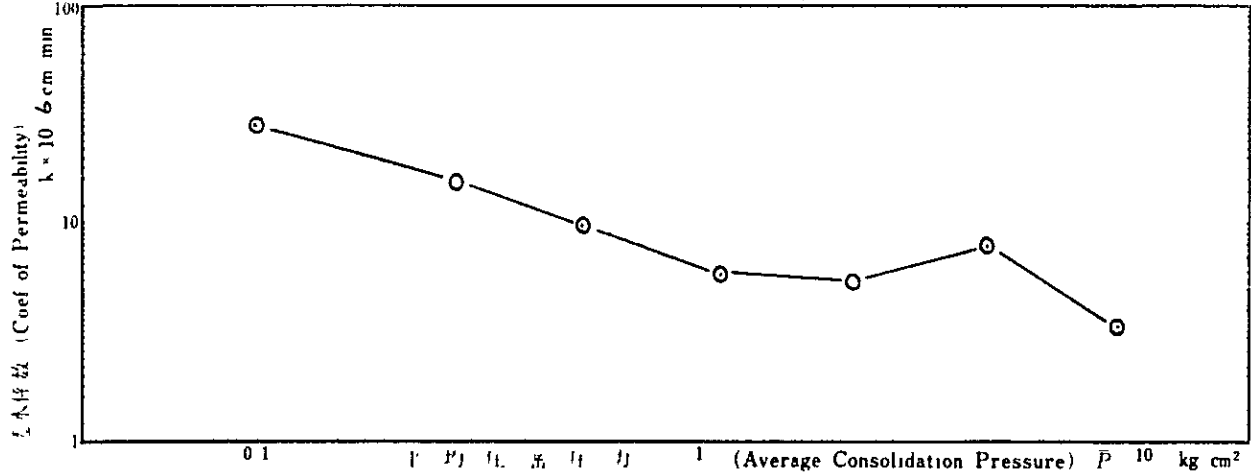
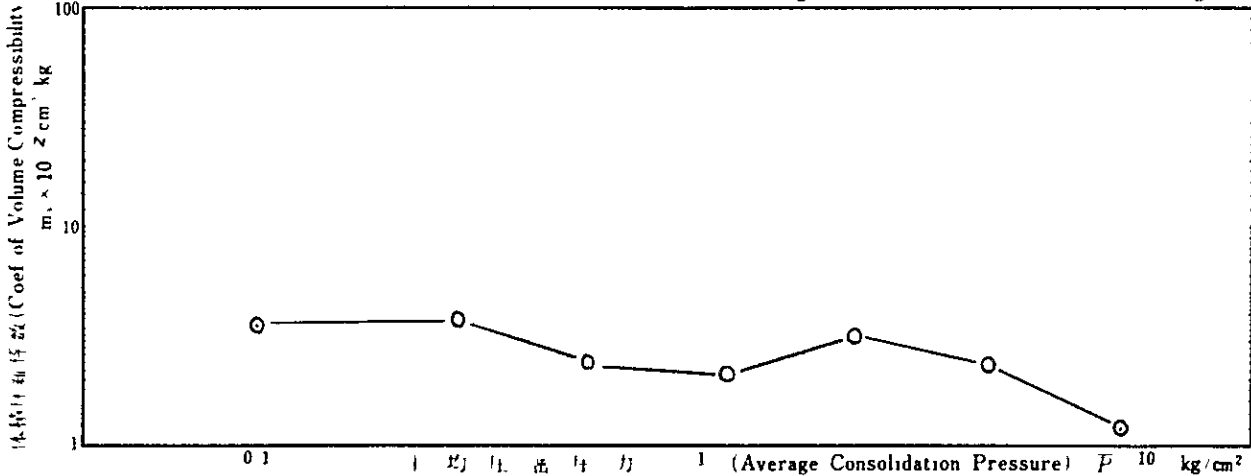
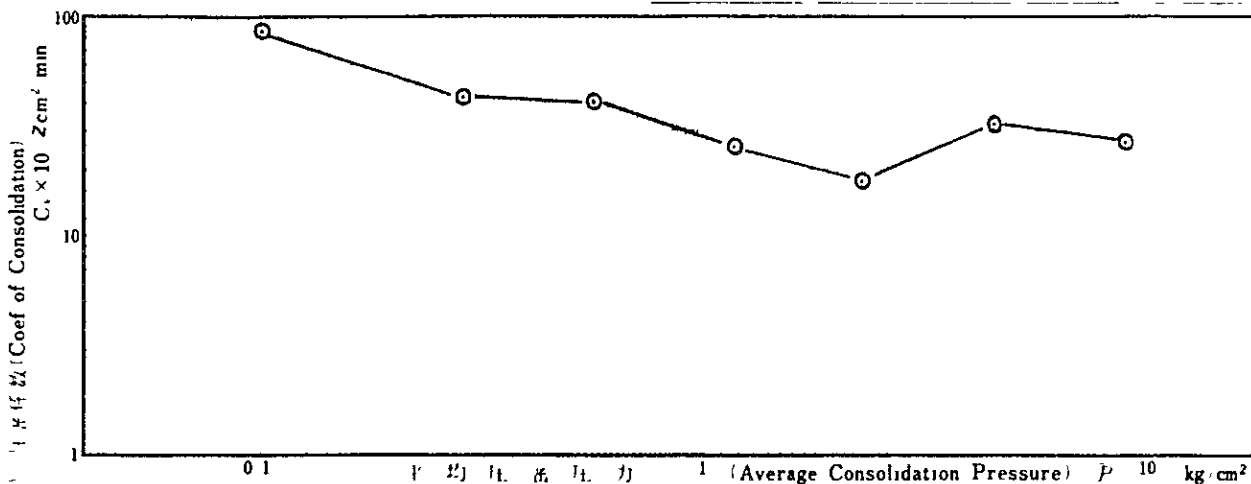
土の圧密試験 (3-3)

CONSOLIDATION TEST

調査名 調査地点
Title Investigation Place **Thilawa Repair Dockyard Project**

試料番号、採取標高 TWS-5
Sample No., Sampling Elevation **10.0 ~ 10.7**

試験年月日
Date 年 月 日 ~ 年 月 日



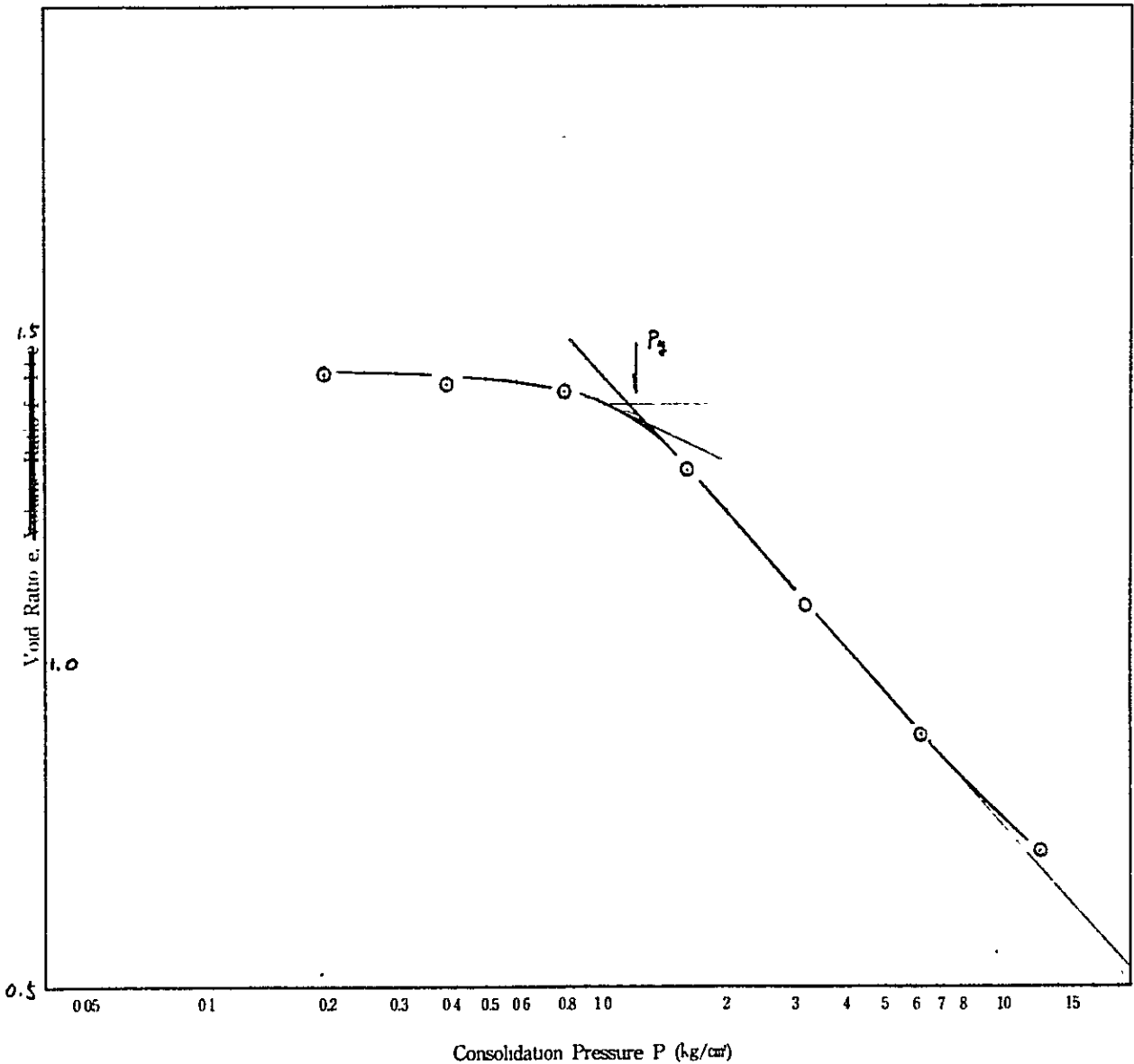
90

CONSOLIDATION TEST (1)

Title, Investigation Place Thilawa Repair Dockyard Project Date _____

Sample No B-10
 Sampling Elevation TWS-6 12.0~12.8

Specimen Dimension	Diameter	D	6.0 cm	Moisture Content	Before Test	W _o	53.7 %	Liquid Limit	LL	%	Compression Index
	Height	2H	2.0 cm		After Test	W _t	21.8 %	Specific Gravity	G _s	2.60	
	Section Area	A	28.26 cm ²	Degree of Saturation	Before Test	S _{ro}	96.3 %	Initial Void Ratio	e _o	1.45	Consolidation Yield Stress
	Volume	V	56.52 cm ³		After Test	S _{rf}	100 %	Initial Volume Ratio	f _o	2.45	



71

•

B-10

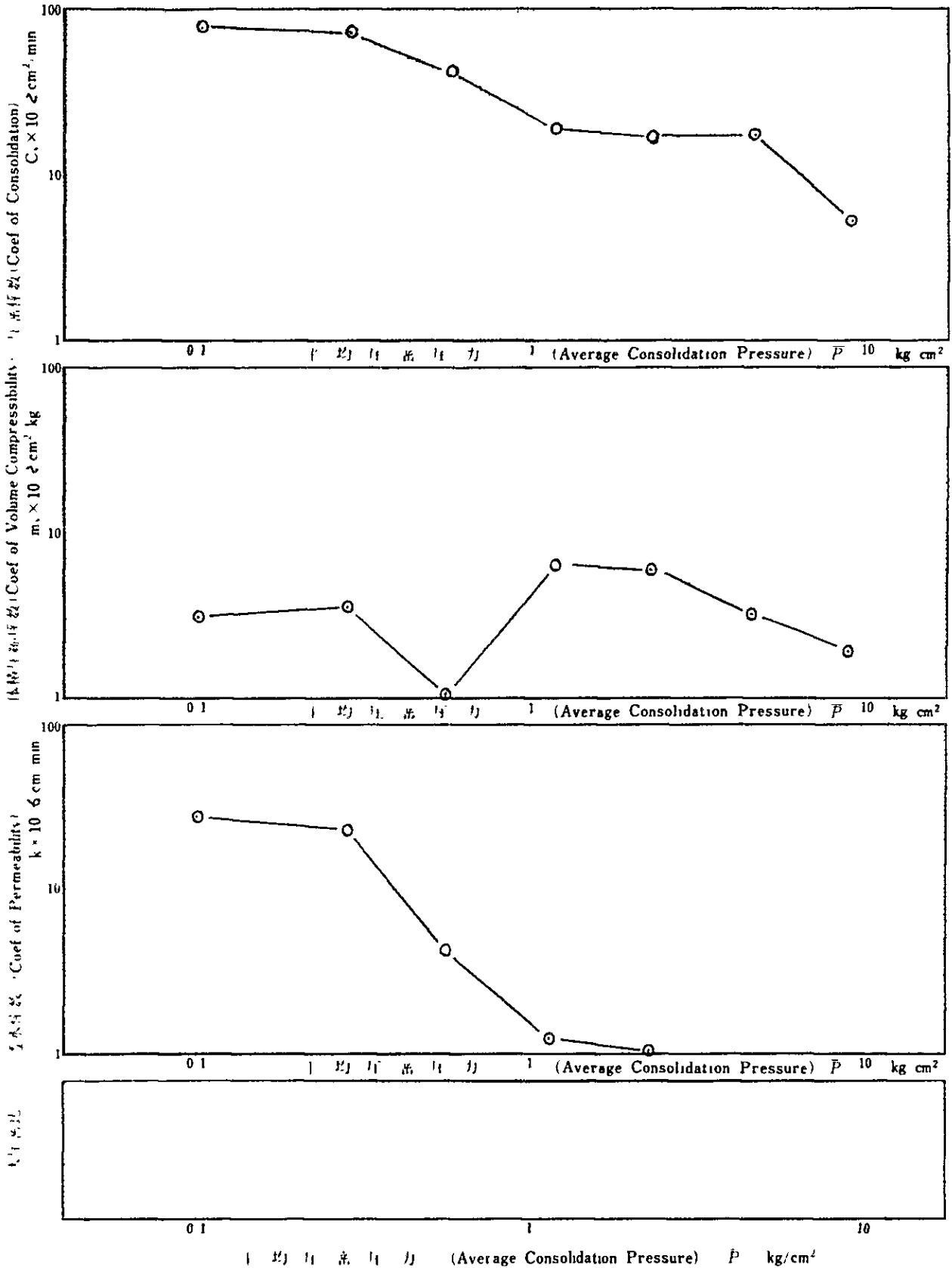
土の圧密試験 (3-3)

CONSOLIDATION TEST

調査名、調査地点
Title Investigation Place Thilawa Repair Dockyard Project

試料番号、採取標高
Sample No., Sampling Elevation TWS-10, 12.0~12.8

試験年月日
Date 4 月 日 ~ 4 月 日

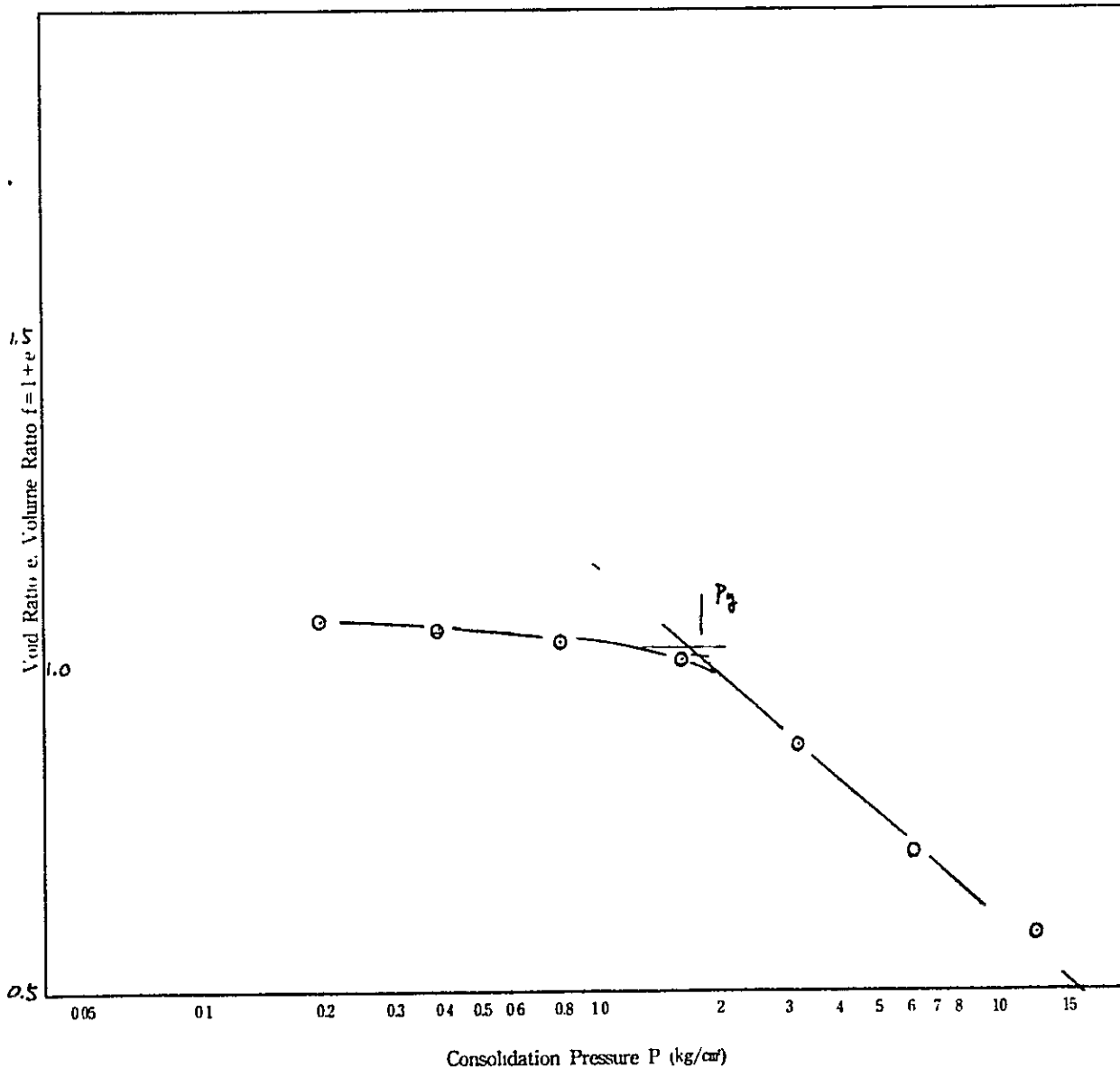


CONSOLIDATION TEST (1)

Title, Investigation Place Thilawa Repair Dockyard Project Date _____

Sample No. Sampling Elevation B-10, 16.0 ~ 16.8

Specimen Dimension	Diameter	D	6.0 cm	Moisture Content	Before Test	W _o	43.7 %	Liquid Limit	LL	%	Compression Index
	Height	H	2.0 cm		After Test	W _f	23.3 %		Specific Gravity	G _s	
	Section Area	A	28.26 cm ²	Degree of Saturation	Before Test	S _{ro}	100 %	Initial Void Ratio		e _o	1.08
	Volume	V	56.52 cm ³		After Test	S _{rf}	100 %		Initial Volume Ratio	f _o	2.08



93

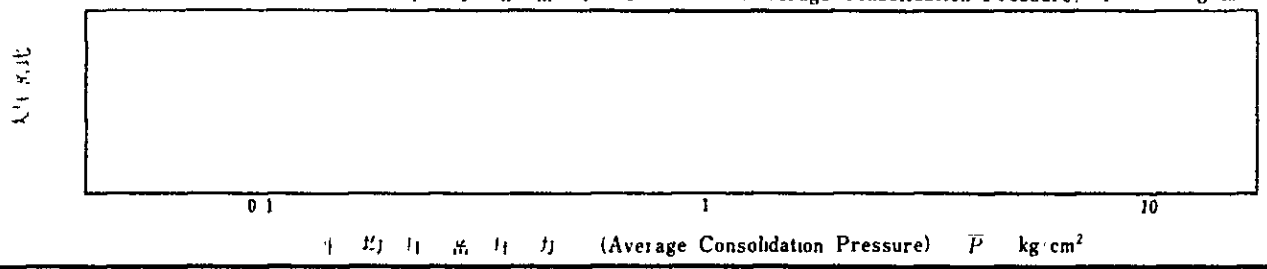
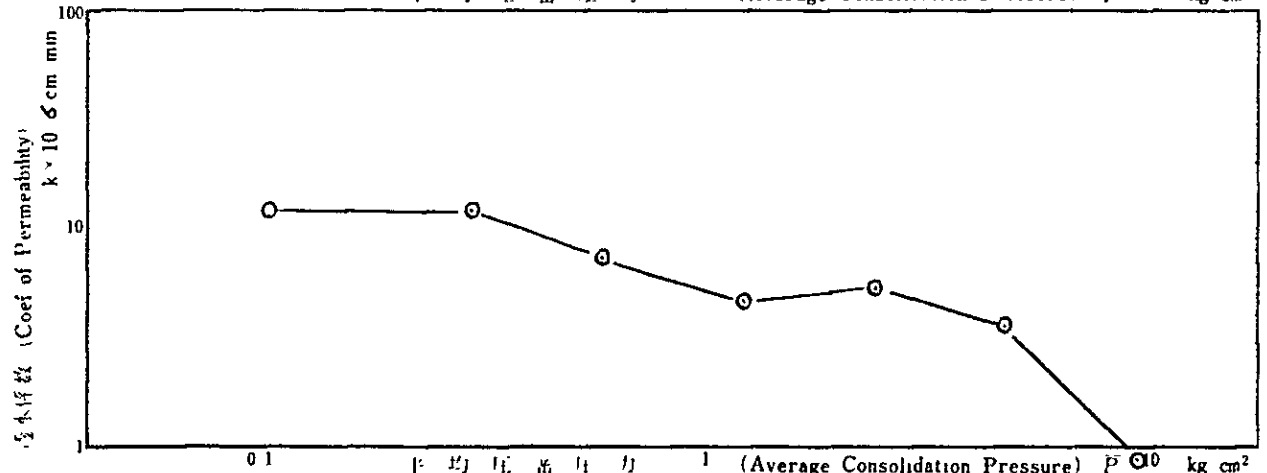
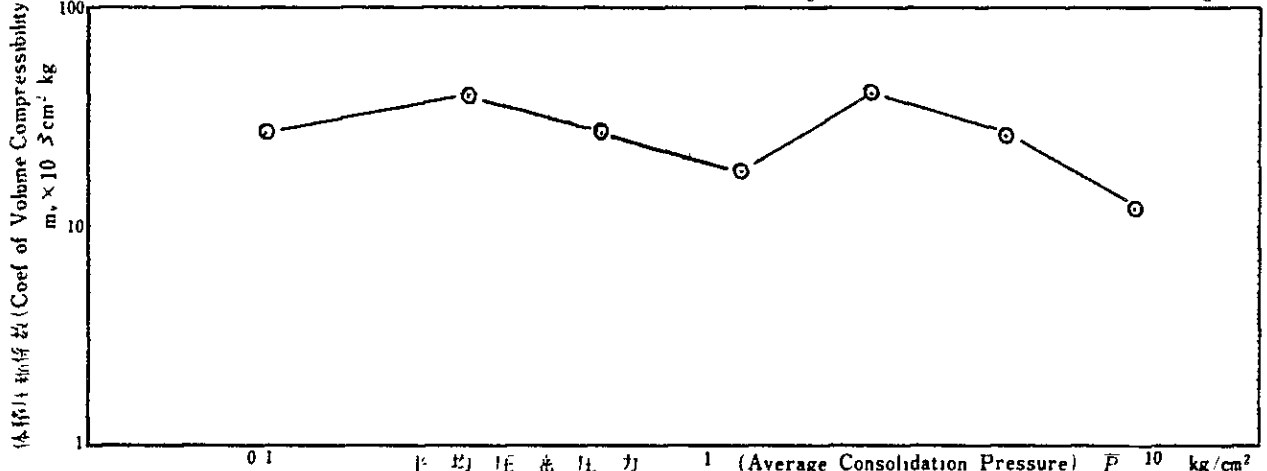
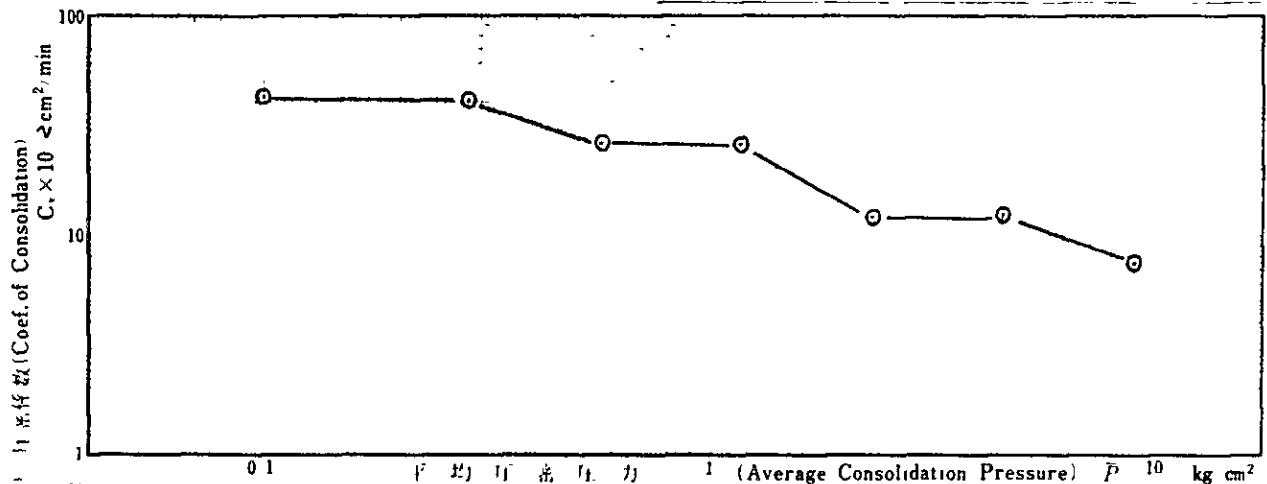
B-10

土の圧密試験 (3-3)

CONSOLIDATION TEST

調査名 調査地点
 Title Investigation Place **Thilawa Repair Dockyard Project**

試料番号、採取標高
 Sample No., Sampling Elevation **TWS-8 16.0 ~ 16.8**
 試験年月日
 Date

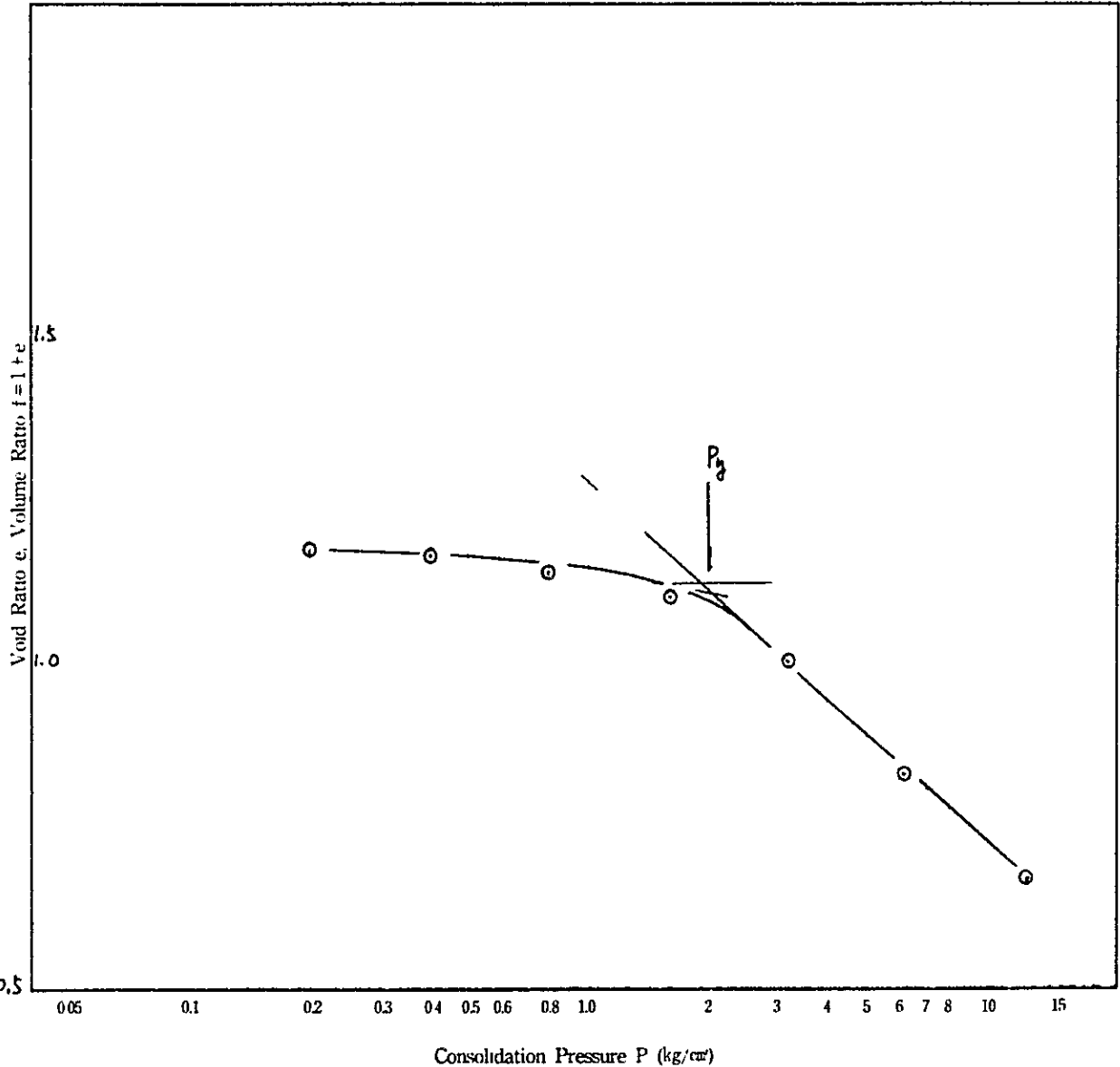


CONSOLIDATION TEST (1)

Title, Investigation Place Thilawa Repair Dockyard Project Date _____

Sample No. Sampling Elevation BH-10. 18.0 ~ 18.7 m

Specimen Dimension	Diameter	D	6.0 cm	Moisture Content	Before Test	Wo.	48.8 %	Liquid Limit	LL	%	Compression Index
	Height	H	2.0 cm		After Test	Wt	26.2 %	Specific Gravity	Gs	2.60	
	Section Area	A	28.26 cm ²	Degree of Saturation	Before Test	Sro	100 %	Initial Void Ratio	e ₀	1.18	Consolidation Yield Stress
	Volume	V	56.52 cm ³		After Test	Sri	100 %	Initial Volume Ratio	f ₀	2.18	



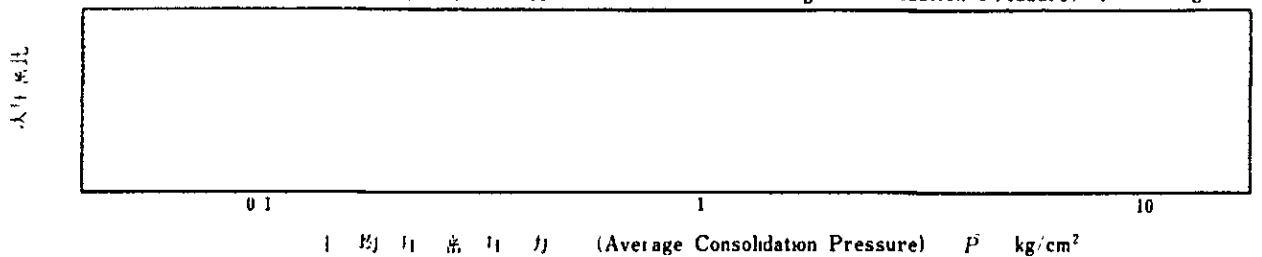
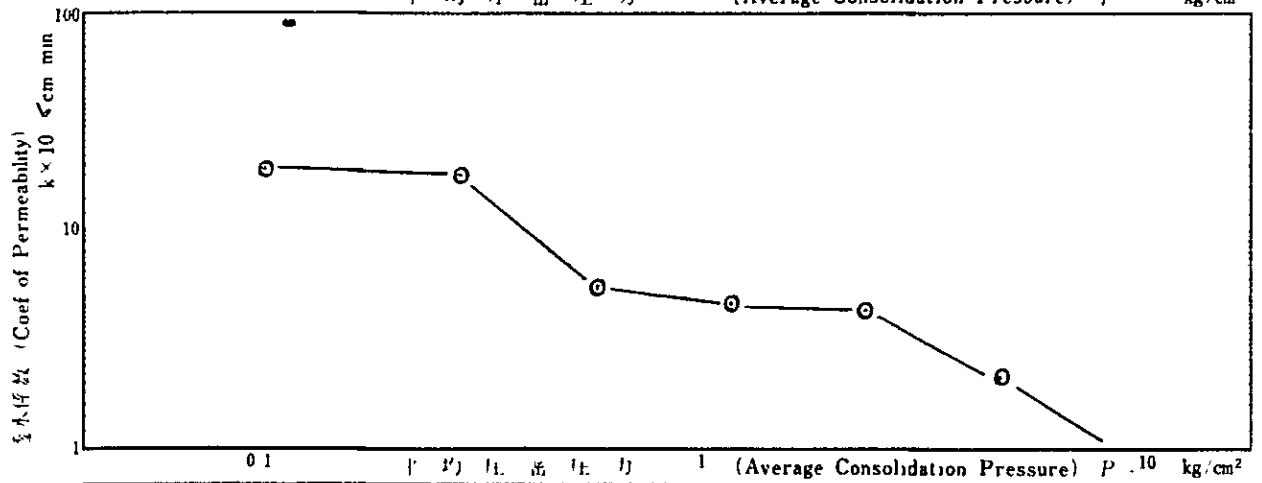
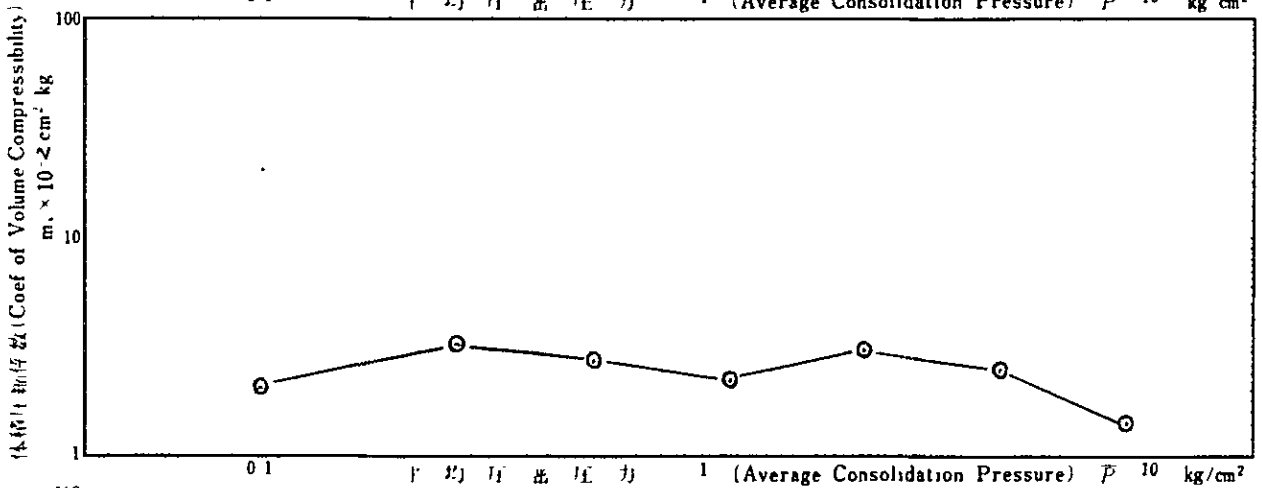
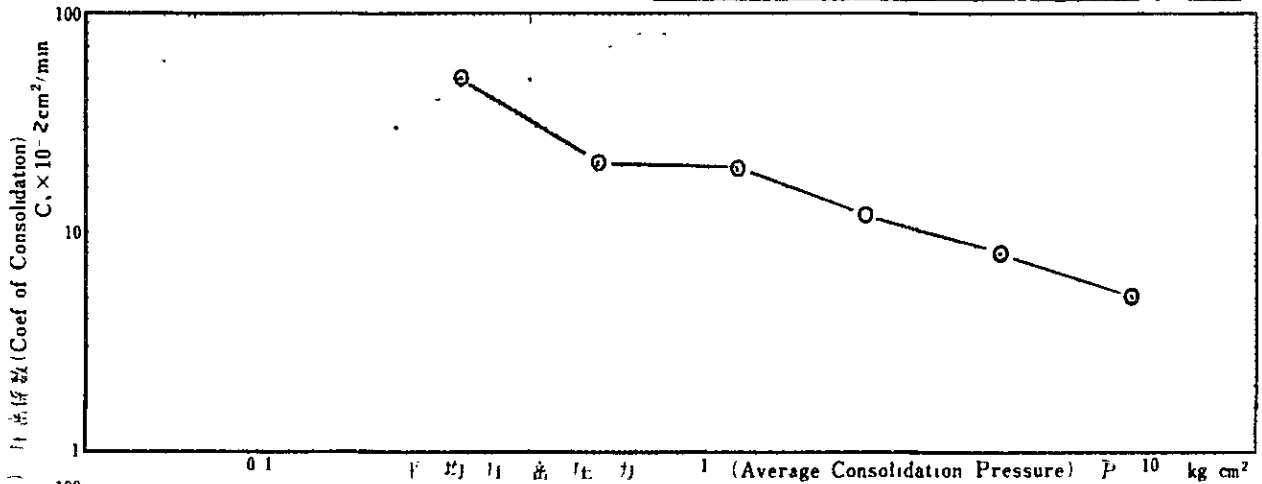
70

土の圧密試験 (3-3)

CONSOLIDATION TEST

調査名 調査地点
 Title Investigation Place Thilawa Repair Dockyard Project

試料番号、採取標高 BH-10
 Sample No., Sampling Elevation 180~187
 試験年月日 4 月 11 日 - 4 月 11 日
 Date

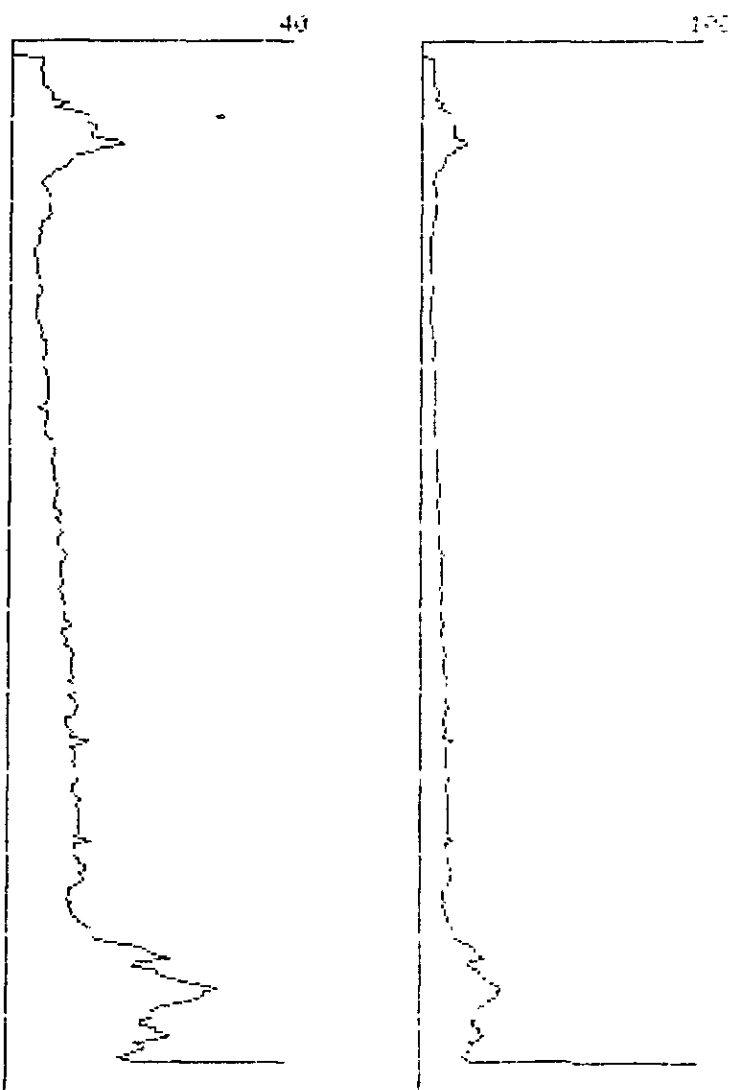


DUTCH CONE SOUNDING

21.0	26	8.4
21.1	26	8.4
21.2	25	8.2
21.3	27	8.7
21.4	26	8.4
21.5	27	8.7
21.6	28	8.9
21.7	30	9.3
21.8	32	9.7
21.9	37	10.7
22.0	40	11.5
22.1	42	11.9
22.2	61	15.9
22.3	72	18.2
22.4	76	19.0
22.5	80	19.8
22.6	90	21.9
22.7	68	17.0
22.8	66	16.9
22.9	80	19.8
23.0	81	20.2
23.1	86	21.2
23.2	97	23.5
23.3	105	25.2
23.4	120	28.3
23.5	110	26.2
23.6	110	26.2
23.7	106	25.4
23.8	95	23.1
23.9	85	21.0
24.0	77	19.5
24.1	70	18.0
24.2	70	18.0
24.3	80	20.1
24.4	80	20.1
24.5	90	22.2
24.6	80	20.1
24.7	65	17.0
24.8	73	18.6
24.9	70	18.0
25.0	60	16.1
25.1	55	15.0
25.2	65	17.1

2 + Pins

25.3	95	84.6
25.4	125	110.2
25.5	135	118.7

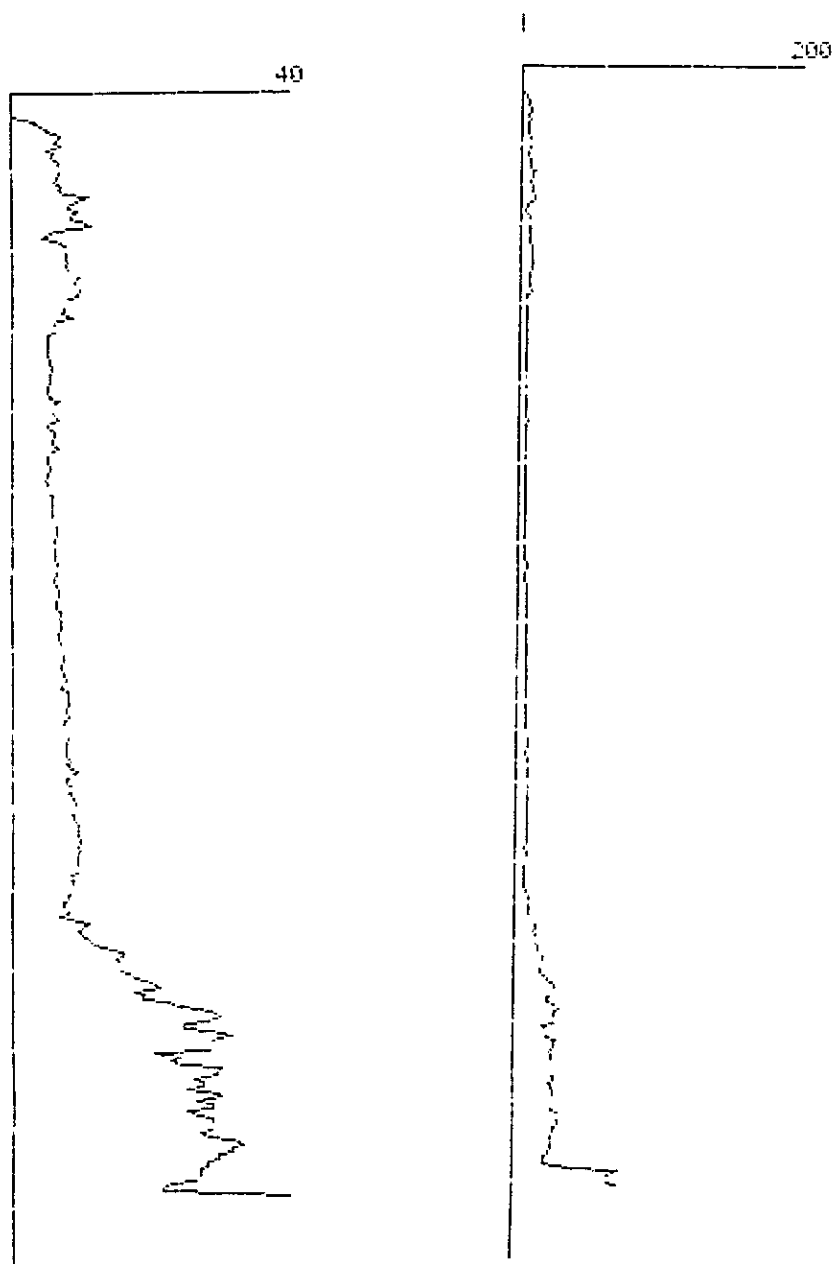


B-2

Depth Dial Qc

500k Rins

0.1	0	0.1	7.1	21	5	14.0
0.0	0	0.1	7.1	20	5	14.1
0.0	0	0.1	7.7	19	5	14.1
0.4	0	0.1	7.7	19	5	14.1
0.5	0	0.1	7.7	19	5	14.4
0.6	0	0.1	7.7	17	4	14.5
0.7	0	0.1	7.7	18	4	14.6
0.8	15		7.7	19	4	14.7
0.9	15		7.7	19	4	14.8
1.0	22		7.7	20	4	14.8
1.1	22		7.7	20	4	15.0
1.2	22		7.7	20	4	15.1
1.3	26	4.4	7.7	25	4	15.2
1.4	26	6.6	7.7	17	4	15.2
1.5	30	6.6	7.7	20	4	15.2
1.6	22	4.4	7.7	21	4	15.2
1.7	26	4.4	7.7	21	4	15.2
1.8	28	6.6	7.7	20	4	15.2
1.9	28	6.6	7.7	19	4	15.2
2.0	28	6.6	7.7	17	4	15.2
2.1	30	6.6	7.7	17	4	15.2
2.2	30	6.6	7.7	17	4	15.2
2.3	30	6.6	7.7	16	4	15.2
2.4	30	6.6	7.7	16	4	15.2
2.5	30	6.6	7.7	16	4	15.2
2.6	30	6.6	7.7	16	4	15.2
2.7	30	6.6	7.7	16	4	15.2
2.8	30	6.6	7.7	16	4	15.2
2.9	30	6.6	7.7	16	4	15.2
3.0	30	6.6	7.7	16	4	15.2
3.1	30	6.6	7.7	16	4	15.2
3.2	30	6.6	7.7	16	4	15.2
3.3	30	6.6	7.7	16	4	15.2
3.4	30	6.6	7.7	16	4	15.2
3.5	30	6.6	7.7	16	4	15.2
3.6	30	6.6	7.7	16	4	15.2
3.7	30	6.6	7.7	16	4	15.2
3.8	30	6.6	7.7	16	4	15.2
3.9	30	6.6	7.7	16	4	15.2
4.0	30	6.6	7.7	16	4	15.2
4.1	30	6.6	7.7	16	4	15.2
4.2	30	6.6	7.7	16	4	15.2
4.3	30	6.6	7.7	16	4	15.2
4.4	30	6.6	7.7	16	4	15.2
4.5	30	6.6	7.7	16	4	15.2
4.6	30	6.6	7.7	16	4	15.2
4.7	30	6.6	7.7	16	4	15.2
4.8	30	6.6	7.7	16	4	15.2
4.9	30	6.6	7.7	16	4	15.2
5.0	30	6.6	7.7	16	4	15.2
5.1	30	6.6	7.7	16	4	15.2
5.2	30	6.6	7.7	16	4	15.2
5.3	30	6.6	7.7	16	4	15.2
5.4	30	6.6	7.7	16	4	15.2
5.5	30	6.6	7.7	16	4	15.2
5.6	30	6.6	7.7	16	4	15.2
5.7	30	6.6	7.7	16	4	15.2
5.8	30	6.6	7.7	16	4	15.2
5.9	30	6.6	7.7	16	4	15.2
6.0	30	6.6	7.7	16	4	15.2
6.1	30	6.6	7.7	16	4	15.2
6.2	30	6.6	7.7	16	4	15.2
6.3	30	6.6	7.7	16	4	15.2
6.4	30	6.6	7.7	16	4	15.2
6.5	30	6.6	7.7	16	4	15.2
6.6	30	6.6	7.7	16	4	15.2
6.7	30	6.6	7.7	16	4	15.2
6.8	30	6.6	7.7	16	4	15.2
6.9	30	6.6	7.7	16	4	15.2
7.0	30	6.6	7.7	16	4	15.2
7.1	30	6.6	7.7	16	4	15.2
7.2	30	6.6	7.7	16	4	15.2
7.3	30	6.6	7.7	16	4	15.2
7.4	30	6.6	7.7	16	4	15.2
7.5	30	6.6	7.7	16	4	15.2
7.6	30	6.6	7.7	16	4	15.2
7.7	30	6.6	7.7	16	4	15.2
7.8	30	6.6	7.7	16	4	15.2
7.9	30	6.6	7.7	16	4	15.2
8.0	30	6.6	7.7	16	4	15.2
8.1	30	6.6	7.7	16	4	15.2
8.2	30	6.6	7.7	16	4	15.2
8.3	30	6.6	7.7	16	4	15.2
8.4	30	6.6	7.7	16	4	15.2
8.5	30	6.6	7.7	16	4	15.2
8.6	30	6.6	7.7	16	4	15.2
8.7	30	6.6	7.7	16	4	15.2
8.8	30	6.6	7.7	16	4	15.2
8.9	30	6.6	7.7	16	4	15.2
9.0	30	6.6	7.7	16	4	15.2
9.1	30	6.6	7.7	16	4	15.2
9.2	30	6.6	7.7	16	4	15.2
9.3	30	6.6	7.7	16	4	15.2
9.4	30	6.6	7.7	16	4	15.2
9.5	30	6.6	7.7	16	4	15.2
9.6	30	6.6	7.7	16	4	15.2
9.7	30	6.6	7.7	16	4	15.2
9.8	30	6.6	7.7	16	4	15.2
9.9	30	6.6	7.7	16	4	15.2
10.0	30	6.6	7.7	16	4	15.2



1. The first part of the document discusses the importance of maintaining accurate records of all transactions and activities. It emphasizes that proper record-keeping is essential for transparency and accountability, particularly in the context of public administration and government operations. The text highlights how detailed records can help identify inefficiencies, prevent fraud, and ensure that resources are used effectively.

2. The second part of the document focuses on the role of technology in modern record-keeping. It explores how digital systems and software solutions can streamline the process of data collection, storage, and retrieval. The author notes that while technology offers significant advantages, it also presents challenges such as data security, system integration, and the need for staff training. The text suggests that a balanced approach, combining traditional methods with modern technology, is often the most effective solution.

3. The third part of the document addresses the legal and ethical considerations surrounding record-keeping. It discusses the importance of ensuring that records are maintained in accordance with applicable laws and regulations. The text also touches upon the ethical implications of data collection and storage, particularly regarding privacy and the potential for misuse of information. The author argues that organizations must have clear policies and procedures in place to address these concerns and ensure that they are acting in a responsible and lawful manner.

4. The fourth part of the document provides practical advice for implementing a robust record-keeping system. It offers a series of steps and best practices that organizations can follow to ensure the success of their record-keeping efforts. These include conducting a thorough assessment of current practices, setting clear goals and objectives, selecting appropriate technology and software, and establishing a strong culture of record-keeping. The text also emphasizes the importance of regular audits and reviews to ensure that the system remains effective and up-to-date.

5. The final part of the document concludes by reiterating the importance of record-keeping and the potential benefits of a well-implemented system. It encourages organizations to take a proactive approach to record-keeping and to view it as a key component of their overall operational strategy. The text ends with a call to action, urging readers to take the steps necessary to improve their record-keeping practices and to ensure that their organizations are operating with the highest level of transparency and accountability.

1. The first part of the document discusses the importance of maintaining accurate records of all transactions. It emphasizes that proper record-keeping is essential for the smooth operation of any business and for the protection of its interests.

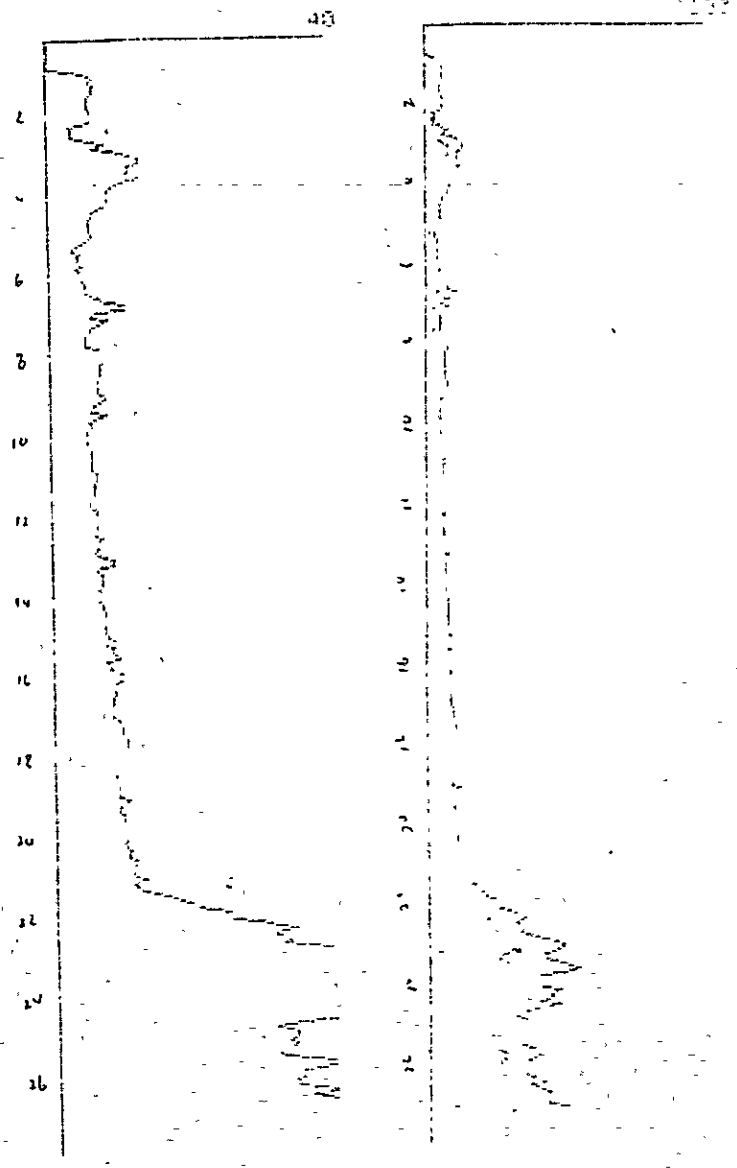
2. The second part of the document outlines the various methods and techniques used to collect and analyze data. It highlights the need for a systematic approach to data collection and the importance of ensuring the accuracy and reliability of the information gathered.

3. The third part of the document focuses on the interpretation and analysis of the collected data. It discusses the various statistical methods and techniques used to identify trends, patterns, and relationships within the data, and how these findings can be used to inform decision-making.

4. The fourth part of the document discusses the importance of communication and reporting in the data analysis process. It emphasizes the need for clear and concise communication of the findings and the importance of providing regular reports to management and other stakeholders.

5. The fifth part of the document discusses the various challenges and limitations associated with data analysis. It highlights the need for a high level of expertise and skill in data analysis and the importance of staying up-to-date with the latest developments in the field.

6. The sixth part of the document discusses the future of data analysis and the various emerging technologies and techniques that are likely to shape the field in the years ahead. It emphasizes the need for continued research and innovation in data analysis and the importance of staying at the forefront of the field.



1. The first part of the document discusses the importance of maintaining accurate records of all transactions and activities. It emphasizes that proper record-keeping is essential for transparency and accountability, particularly in financial matters. The text notes that without clear records, it becomes difficult to track expenses, revenues, and other critical data points.

2. The second section focuses on the role of technology in modern record-keeping. It highlights how digital tools and software solutions can significantly improve the efficiency and accuracy of data collection and storage. The author suggests that organizations should invest in reliable technology to ensure their records are secure, accessible, and easy to manage.

3. The third part of the document addresses the challenges associated with data management. It points out that as the volume of data grows, organizations must implement robust security measures to protect sensitive information from unauthorized access or loss. Additionally, the text discusses the importance of regular data audits to identify and correct any errors or inconsistencies in the records.

4. The final section provides practical advice for implementing a comprehensive record-keeping system. It recommends starting with a clear plan that defines the types of data to be collected, the methods of collection, and the storage solutions to be used. The author also stresses the need for ongoing training and support for staff members who will be responsible for maintaining the system.

1. The first part of the document discusses the importance of maintaining accurate records of all transactions and activities. It emphasizes that proper record-keeping is essential for transparency and accountability, particularly in the context of public administration and government operations. The text highlights that without reliable records, it becomes difficult to track the flow of funds, assess the performance of various departments, and ensure that resources are being used efficiently and effectively.

2. The second part of the document focuses on the role of technology in enhancing record-keeping and data management. It notes that modern information systems can significantly reduce the risk of errors and improve the accuracy of records. By leveraging digital tools, organizations can streamline their processes, automate data entry, and ensure that information is stored securely and is easily accessible to authorized personnel. This not only saves time and resources but also facilitates better decision-making based on up-to-date and comprehensive data.

3. The third part of the document addresses the challenges associated with maintaining large volumes of data over long periods. It acknowledges that as the amount of information grows, the complexity of managing it increases. Issues such as data redundancy, inconsistent formats, and the potential for data loss become more pronounced. To overcome these challenges, the document suggests implementing robust data governance policies, regular audits, and backup procedures. Additionally, it recommends investing in scalable and secure storage solutions to ensure that data remains intact and accessible for future reference.

4. The fourth part of the document discusses the importance of training and education in ensuring that staff members are equipped with the necessary skills to handle records and data effectively. It stresses that even the most advanced technology is only as good as the people using it. Therefore, providing ongoing training and professional development opportunities is crucial for maintaining high standards of record-keeping. This includes teaching staff about best practices, the latest software tools, and the importance of data security and privacy.

5. The fifth part of the document concludes by reiterating the overall goal of the document: to ensure that all records are maintained in a way that is accurate, secure, and accessible. It calls for a collaborative effort from all stakeholders involved in the process, from top management to front-line staff, to ensure that the organization's records are a true and reliable reflection of its activities. The document ends with a strong emphasis on the long-term benefits of a well-maintained record-keeping system, including improved operational efficiency, enhanced transparency, and better compliance with regulatory requirements.

1. The first part of the document discusses the importance of maintaining accurate records of all transactions. It emphasizes that proper record-keeping is essential for the integrity of the financial system and for the ability to detect and prevent fraud. The text also notes that records should be kept for a sufficient period to allow for a thorough audit.

2. The second part of the document outlines the specific requirements for record-keeping. It states that all transactions must be recorded in a clear and concise manner, and that the records must be accessible to all authorized personnel. The text also mentions that records should be stored in a secure and protected environment to prevent loss or damage.

3. The third part of the document discusses the role of internal controls in ensuring the accuracy of records. It explains that internal controls are designed to prevent errors and fraud, and that they should be implemented and monitored on an ongoing basis. The text also notes that internal controls should be reviewed and updated as needed to reflect changes in the organization's operations.

4. The fourth part of the document discusses the importance of training and education in ensuring the accuracy of records. It states that all personnel involved in record-keeping should receive appropriate training and education to ensure that they are able to perform their duties accurately and efficiently. The text also mentions that training should be provided on a regular basis to keep personnel up-to-date on the latest record-keeping practices.

5. The fifth part of the document discusses the importance of external audits in ensuring the accuracy of records. It explains that external audits are conducted by independent auditors to provide an objective assessment of the organization's financial records. The text also notes that external audits should be conducted on a regular basis to ensure the reliability of the financial information.

6. The sixth part of the document discusses the importance of transparency and accountability in ensuring the accuracy of records. It states that all transactions should be recorded in a transparent and accountable manner, and that the records should be available to all authorized personnel. The text also mentions that transparency and accountability are essential for building trust and confidence in the financial system.

7. The seventh part of the document discusses the importance of continuous improvement in ensuring the accuracy of records. It explains that record-keeping practices should be regularly reviewed and updated to reflect changes in the organization's operations and in the latest record-keeping practices. The text also notes that continuous improvement is essential for ensuring the accuracy and reliability of the financial records.

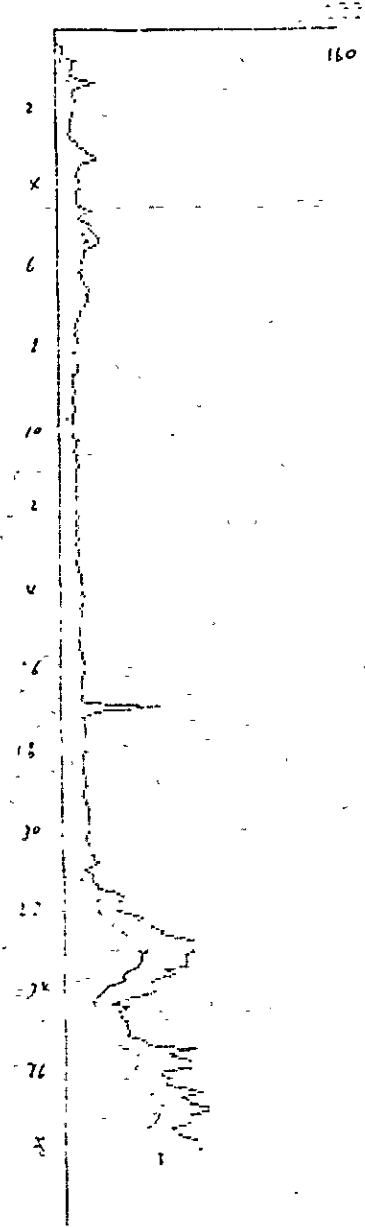
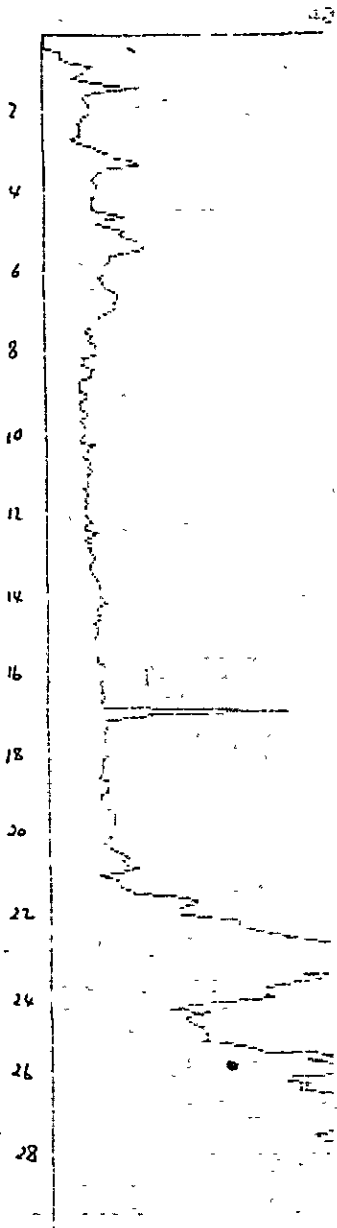
1. The first part of the document discusses the importance of maintaining accurate records of all transactions and activities. It emphasizes that proper record-keeping is essential for transparency and accountability, particularly in the context of public administration and government operations. The text highlights how detailed records can help identify inefficiencies, prevent fraud, and ensure that resources are used effectively.

2. The second part of the document focuses on the role of technology in modern record-keeping. It explores how digital systems and software solutions can streamline the process of data collection, storage, and retrieval. The author notes that while technology offers significant advantages, it also presents challenges such as data security, system integration, and the need for staff training. The text suggests that a balanced approach, combining traditional methods with modern technology, is often the most effective.

3. The third part of the document addresses the legal and regulatory requirements surrounding record-keeping. It discusses various laws and standards that govern how records must be maintained, including retention periods, access protocols, and data protection regulations. The author stresses that organizations must stay up-to-date with these requirements to avoid legal penalties and ensure compliance. It also touches upon the importance of having clear policies and procedures in place to guide record-keeping practices.

4. The fourth part of the document discusses the impact of record-keeping on decision-making and strategic planning. It argues that high-quality records provide a wealth of data that can be analyzed to identify trends, patterns, and areas for improvement. This data-driven approach allows organizations to make more informed decisions and develop strategies that are based on evidence rather than intuition. The text also mentions that good records can be invaluable during audits and investigations, providing a clear trail of events and actions.

5. The fifth and final part of the document concludes by summarizing the key points and offering recommendations for best practices. It reiterates that record-keeping is not just a bureaucratic task but a critical component of any organization's success. The author encourages organizations to invest in their record-keeping systems and processes, and to foster a culture of transparency and accountability. Finally, the text provides a list of resources and references for further reading on the topic.



Handwritten text, likely bleed-through from the reverse side of the page. The text is extremely faint and illegible due to low contrast and significant noise. It appears to be organized into several paragraphs, with some lines starting with capital letters. The overall structure suggests a formal document or letter, but the specific content cannot be discerned.

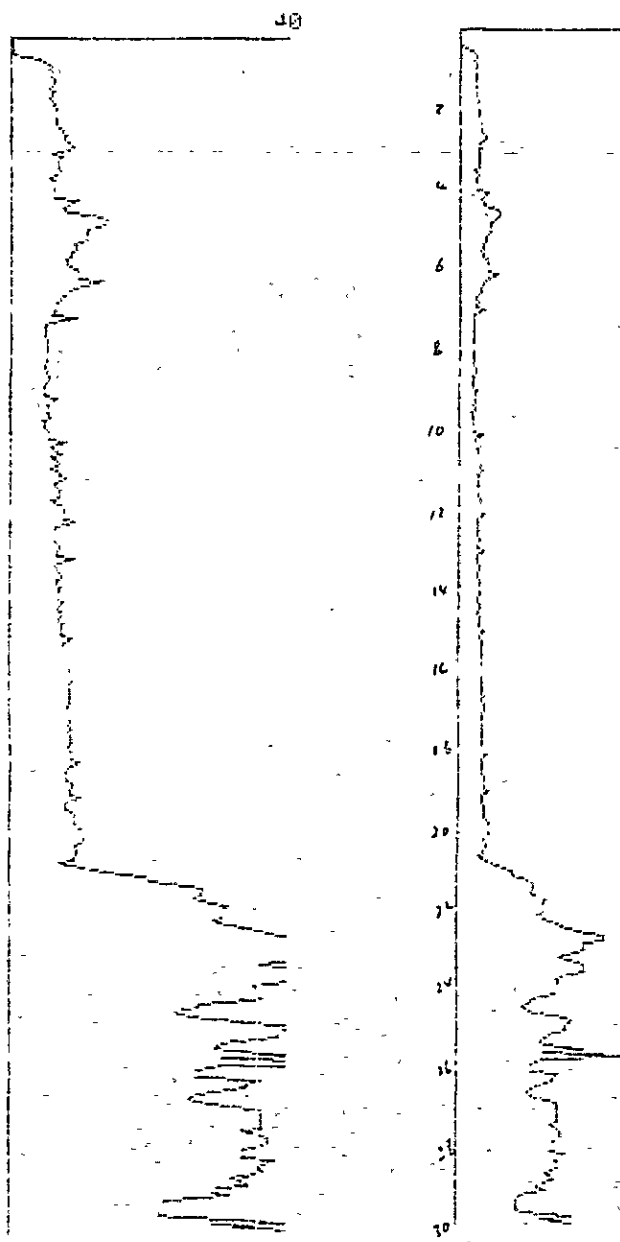
1. The first part of the document discusses the importance of maintaining accurate records of all transactions and activities. It emphasizes that proper record-keeping is essential for transparency and accountability, particularly in the context of public administration and financial management. The text highlights that without reliable records, it becomes difficult to track expenditures, assess performance, and ensure that resources are used efficiently and effectively.

2. The second part of the document focuses on the role of internal controls and audits in preventing fraud and mismanagement. It states that a robust system of internal controls is necessary to identify and mitigate risks before they become significant problems. Regular audits are also crucial for verifying the accuracy of financial statements and ensuring compliance with applicable laws and regulations. The document notes that these measures are not only protective but also contribute to the overall integrity and trustworthiness of the organization.

3. The third part of the document addresses the need for continuous improvement and innovation. It argues that organizations should not be satisfied with the status quo but should actively seek ways to enhance their operations, services, and products. This involves staying up-to-date with the latest technologies, best practices, and market trends. The text suggests that fostering a culture of innovation and learning can lead to significant competitive advantages and long-term success.

4. The fourth part of the document discusses the importance of stakeholder engagement and communication. It stresses that organizations should maintain open and transparent lines of communication with all stakeholders, including employees, customers, suppliers, and the community. Regular communication helps to build trust, address concerns, and gather valuable feedback that can inform decision-making and strategic planning. The document also notes that effective communication is key to managing change and implementing new initiatives smoothly.

5. The fifth and final part of the document concludes by summarizing the key points and reiterating the commitment to high standards of performance and integrity. It states that the organization is dedicated to providing the highest quality of service and ensuring that all activities are conducted in a fair, ethical, and transparent manner. The document ends with a call to action, encouraging all employees and stakeholders to continue working together to achieve the organization's goals and vision.



1. The first part of the document discusses the importance of maintaining accurate records of all transactions and activities. It emphasizes that proper record-keeping is essential for transparency and accountability, particularly in the context of public administration and government operations. The text highlights that without reliable records, it becomes difficult to track expenditures, assess performance, and ensure that resources are being used effectively and ethically.

2. The second part of the document addresses the challenges associated with data collection and analysis. It notes that while modern technology offers powerful tools for gathering and processing information, the quality and integrity of the data are often compromised. Issues such as incomplete reporting, inconsistent formats, and potential biases can lead to misleading conclusions. The document stresses the need for standardized protocols and rigorous quality control measures to ensure that the data being used is both accurate and trustworthy.

3. The third part of the document focuses on the role of leadership in fostering a culture of data-driven decision-making. It argues that leaders must not only understand the value of data but also create an environment where it is encouraged and supported. This involves providing training, resources, and incentives for staff to engage with data and share their findings. The text also mentions that leadership should be transparent in their own use of data, demonstrating how it informs their decisions and actions.

4. The fourth part of the document discusses the importance of communication in the data analysis process. It points out that data is only as good as its ability to be understood and acted upon. Therefore, clear and concise communication of findings is crucial. This includes using appropriate visualizations, avoiding technical jargon, and ensuring that the key messages are easily accessible to all relevant stakeholders. The document suggests that regular communication and collaboration between different departments can help to break down silos and ensure that data is being used to its full potential.

5. The fifth and final part of the document provides a summary of the key points and offers some practical recommendations. It reiterates that successful data analysis is a multi-faceted process that requires attention to detail, strong leadership, and effective communication. The document concludes by encouraging organizations to embrace a data-driven mindset and to continuously seek ways to improve their data practices. It suggests that by doing so, organizations can gain valuable insights, optimize their operations, and ultimately achieve their goals more effectively.

1. The first part of the document discusses the importance of maintaining accurate records of all transactions and activities. It emphasizes that proper record-keeping is essential for transparency and accountability, particularly in the context of public administration and government operations. The text notes that such records are often used for auditing purposes and to ensure that funds are being used as intended.

2. The second part of the document addresses the challenges associated with data collection and analysis. It highlights that while digital tools have made data gathering easier, the quality and consistency of the data can vary significantly. The document suggests that standardized protocols and regular training for staff are necessary to overcome these challenges and ensure that the data collected is reliable and useful for decision-making.

3. The third part of the document focuses on the role of technology in improving efficiency and reducing costs. It discusses various digital solutions, such as cloud storage and automated reporting systems, which can streamline processes and reduce the risk of human error. The text also mentions the importance of cybersecurity measures to protect sensitive information from unauthorized access and data breaches.

4. The fourth part of the document discusses the need for continuous improvement and innovation. It suggests that organizations should regularly evaluate their current practices and look for new ways to optimize their operations. This could involve adopting emerging technologies or reorganizing teams to better utilize resources. The document stresses that a culture of innovation and learning is essential for long-term success in a rapidly changing environment.

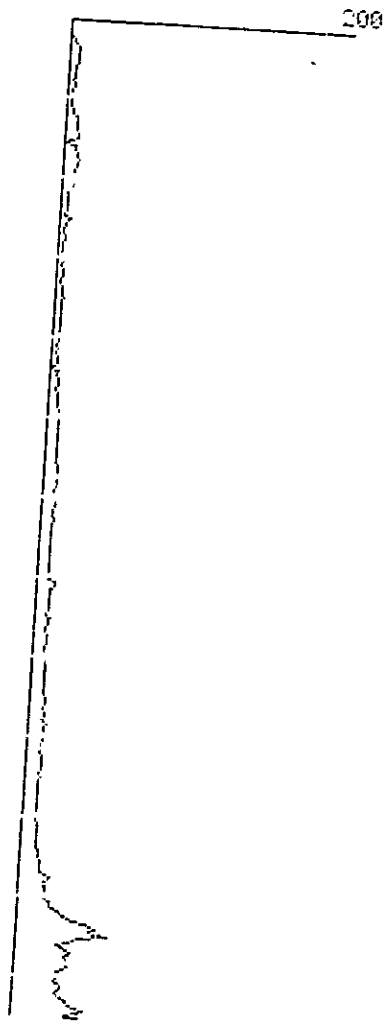
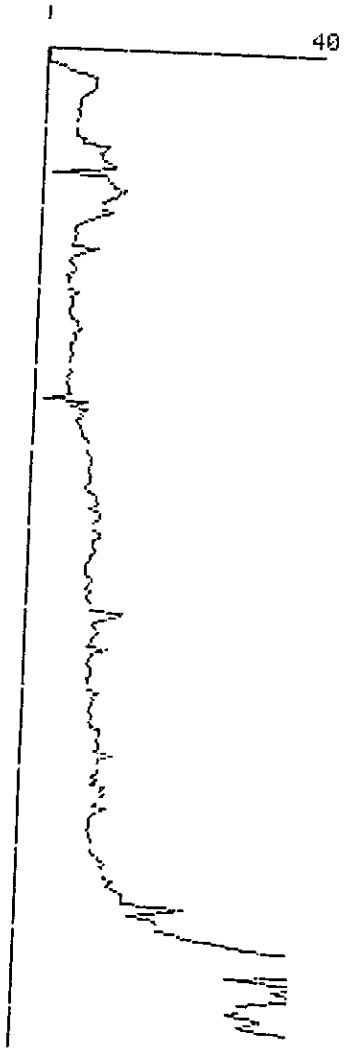
5. The fifth and final part of the document provides a summary of the key points discussed and offers some concluding thoughts. It reiterates the importance of transparency, data quality, and technological innovation in achieving organizational goals. The document concludes by encouraging all stakeholders to work together to address the challenges and opportunities outlined in the text.

Depth	Dial	Qc	500ka Rins					
0.1	1	0.3	7.0	22	5.7	14.0	33	8.9
0.2	1	0.3	7.1	25	6.3	14.1	55	13.5
0.3	1	0.3	7.2	19	5.1	14.2	50	12.5
0.4	1	0.3	7.3	20	5.3	14.3	40	10.4
0.5	12	2.6	7.4	20	5.3	14.4	35	9.5
0.6	15	3.3	7.5	18	4.8	14.5	37	9.8
0.7	24	5.1	7.6	18	4.8	14.6	40	10.4
0.8	32	6.8	7.7	18	4.8	14.7	38	10.0
0.9	33	7.0	7.8	19	5.1	14.8	35	9.9
1.0	32	6.9	7.9	17	4.6	14.9	35	9.9
1.1	32	6.9	8.0	17	4.8	15.0	32	8.8
1.2	29	6.3	8.1	19	5.2	15.1	45	11.6
1.3	24	5.3	8.2	16	4.6	15.2	35	9.5
1.4	22	4.9	8.3	17	4.9	15.3	35	9.9
1.5	22	4.9	8.4	16	4.6	15.4	32	9.1
1.6	22	4.9	8.5	17	4.8	15.5	32	9.8
1.7	20	4.4	8.6	17	4.8	15.6	35	9.5
1.8	22	4.4	8.7	19	5.2	15.7	35	9.9
1.9	21	4.6	8.8	6	1.2	15.8	34	9.9
2.0	20	4.6	8.9	30	7.5	15.9	31	8.9
2.1	19	4.4	9.0	18	5.1	16.0	32	9.0
2.2	20	4.6	9.1	30	7.6	16.1	40	10.7
2.3	25	5.6	9.2	25	6.9	16.2	35	9.9
2.4	24	5.4	9.3	27	7.0	16.3	37	10.0
2.5	42	9.1	9.4	22	6.0	16.4	35	9.9
2.6	39	8.5	9.5	24	6.4	16.5	34	9.4
2.7	36	7.9	9.6	25	6.6	16.6	34	9.4
2.8	37	8.1	9.7	26	6.8	16.7	35	9.9
2.9	40	8.7	9.8	26	6.8	16.8	36	9.9
3.0	45	9.9	9.9	29	7.4	16.9	34	9.4
3.1	45	9.9	10.0	30	7.8	17.0	35	9.9
3.2	4	1.4	10.1	30	7.8	17.1	40	10.0
3.3	40	8.9	10.2	30	8.4	17.2	40	10.0
3.4	41	9.1	10.3	34	8.6	17.3	40	10.0
3.5	44	9.7	10.4	34	8.6	17.4	39	10.0
3.6	45	9.9	10.5	32	8.2	17.5	40	10.0
3.7	53	11.6	10.6	32	8.2	17.6	40	10.0
3.8	48	10.5	10.7	37	8.4	17.7	38	10.4
3.9	45	9.9	10.8	30	8.4	17.8	50	12.0
4.0	37	8.4	10.9	30	8.4	17.9	40	10.0
4.1	45	10.0	11.0	30	7.9	18.0	40	10.0
4.2	35	8.0	11.1	30	8.9	18.1	40	10.0
4.3	26	6.5	11.2	35	9.4	18.2	35	9.9
4.4	22	5.3	11.3	37	9.4	18.3	40	10.0
4.5	20	4.9	11.4	37	9.4	18.4	35	9.9
4.6	20	4.9	11.5	38	9.6	18.5	45	12.0
4.7	21	5.1	11.6	32	8.3	18.6	40	10.0
4.8	19	4.6	11.7	38	9.6	18.7	45	12.0
4.9	19	4.6	11.8	40	10.0	18.8	40	10.0
5.0	17	4.4	11.9	40	10.0	18.9	42	11.4
5.1	35	8.1	12.0	35	9.1	19.0	37	10.5
5.2	25	6.0	12.1	40	10.1	19.1	45	12.1
5.3	19	4.8	12.2	40	10.1	19.2	38	10.7
5.4	16	4.2	12.3	35	9.1	19.3	37	10.5
5.5	18	4.6	12.4	35	9.1	19.4	35	10.0
5.6	20	5.0	12.5	35	9.1	19.5	35	10.0
5.7	21	5.2	12.6	37	9.5	19.6	35	10.0
5.8	15	3.9	12.7	33	8.7	19.7	33	9.6
5.9	18	4.6	12.8	33	8.7	19.8	35	10.0
6.0	15	4.1	12.9	32	8.5	19.9	35	10.0
6.1	23	5.8	13.0	30	8.2	20.0	35	10.2
6.2	17	4.5	13.1	30	8.2	20.1	35	10.2
6.3	18	4.7	13.2	30	8.2	20.2	40	11.2
6.4	18	4.7	13.3	33	8.8	20.3	40	11.0
6.5	18	4.7	13.4	35	9.2	20.4	45	12.3
6.6	17	4.5	13.5	33	8.8	20.5	42	11.6
6.7	17	4.5	13.6	30	8.2	20.6	45	12.4
6.8	18	4.7	13.7	34	9.0	20.7	43	11.8
6.9	22	5.5	13.8	32	8.6	20.8	45	12.4
			13.9	32	8.6	20.9	50	13.0

21.0	45	12.4
21.1	50	13.4
21.2	55	14.5
21.3	55	14.5
21.4	56	14.7
21.5	55	14.5
21.6	96	23.0
21.7	85	20.7
21.8	60	15.5
21.9	75	18.6
22.0	78	19.4
22.1	90	21.9
22.2	95	22.9
22.3	110	26.1
22.4	127	29.6
22.5	135	31.3
22.6	170	38.5
22.7	210	46.9

2 + Rins

22.8	60	54.4
22.9	55	50.1
23.0	69	62.2
23.1	45	41.7
23.2	39	36.6
23.3	38	38.9
23.4	38	35.7
23.5	42	39.1
23.6	37	34.9
23.7	38	35.7
23.8	42	39.1
23.9	38	35.7
24.0	55	50.1
24.1	38	35.7
24.2	35	33.0
24.3	35	33.0
24.4	35	33.0
24.5	35	33.0
24.6	40	37.6
24.7	41	38.4
24.8	45	41.8
24.9	55	50.1
25.0	40	37.6
25.1	50	46.2

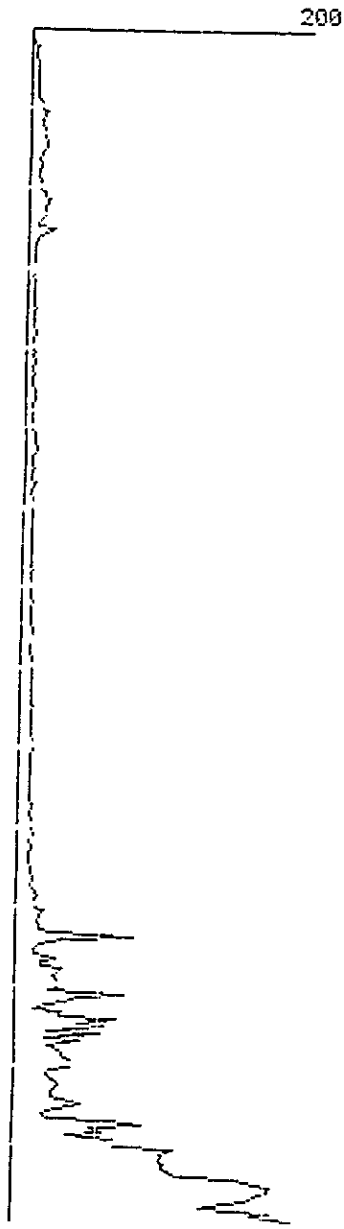
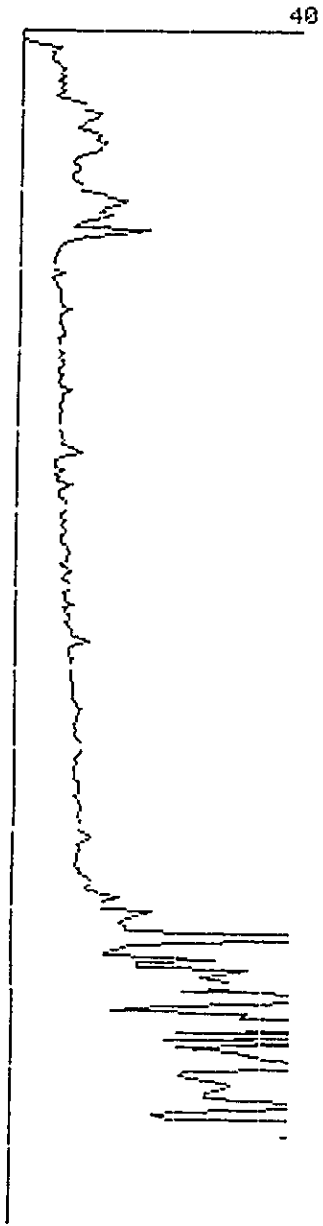


D-9

Depth	Dial	Qc						
	500kg	Rins						
0.1	0	0.1	7.0	24	6.1	14.0	26	7.5
0.2	0	0.1	7.1	30	7.3	14.1	22	6.6
0.3	0	0.1	7.2	22	5.7	14.2	23	6.9
0.4	14	3.1	7.3	22	5.7	14.3	23	6.9
0.5	25	5.3	7.4	22	5.7	14.4	29	8.1
0.6	20	4.3	7.5	22	5.7	14.5	22	6.6
0.7	21	4.5	7.6	24	6.1	14.6	24	7.1
0.8	19	4.1	7.7	25	6.3	14.7	26	7.5
0.9	22	4.7	7.8	25	6.3	14.8	26	7.5
1.0	25	5.5	7.9	21	5.5	14.9	24	7.1
1.1	27	5.9	8.0	22	5.8	15.0	26	7.6
1.2	25	5.5	8.1	25	6.4	15.1	27	7.8
1.3	27	5.9	8.2	22	5.8	15.2	27	7.8
1.4	23	5.1	8.3	24	6.2	15.3	30	8.4
1.5	27	5.9	8.4	25	6.4	15.4	39	10.3
1.6	24	5.3	8.5	22	5.8	15.5	30	8.4
1.7	27	5.9	8.6	21	5.6	15.6	26	7.6
1.8	22	4.9	8.7	24	6.2	15.7	26	7.6
1.9	27	5.9	8.8	23	6.0	15.8	26	7.6
2.0	40	8.7	8.9	22	5.8	15.9	29	8.2
2.1	50	10.8	9.0	22	6.0	16.0	26	7.8
2.2	48	10.4	9.1	30	7.6	16.1	26	7.8
2.3	42	9.1	9.2	24	6.4	16.2	26	7.8
2.4	38	8.3	9.3	24	6.4	16.3	26	7.8
2.5	35	7.7	9.4	24	6.4	16.4	28	8.3
2.6	47	10.2	9.5	22	6.0	16.5	28	8.2
2.7	50	10.8	9.6	22	6.0	16.6	28	8.2
2.8	48	10.4	9.7	23	6.2	16.7	28	8.2
2.9	53	11.4	9.8	22	6.0	16.8	28	8.2
3.0	50	11.0	9.9	22	6.0	16.9	30	8.6
3.1	50	11.0	10.0	22	6.1	17.0	30	8.7
3.2	40	8.9	10.1	23	6.3	17.1	33	9.3
3.3	35	7.8	10.2	23	6.3	17.2	32	9.1
3.4	32	7.2	10.3	24	6.5	17.3	30	8.7
3.5	35	7.8	10.4	23	6.3	17.4	30	8.7
3.6	37	8.2	10.5	30	7.8	17.5	28	8.5
3.7	34	7.6	10.6	36	9.0	17.6	25	8.4
3.8	32	7.2	10.7	27	7.1	17.7	30	8.7
3.9	32	7.2	10.8	18	5.3	17.8	29	8.5
4.0	37	8.4	10.9	18	5.3	17.9	30	8.7
4.1	50	11.1	11.0	18	5.4	18.0	33	9.5
4.2	54	11.9	11.1	24	6.6	18.1	33	9.5
4.3	65	14.2	11.2	18	5.4	18.2	30	8.9
4.4	60	13.2	11.3	21	6.0	18.3	28	8.4
4.5	52	11.5	11.4	20	5.8	18.4	29	8.7
4.6	49	10.9	11.5	30	7.9	18.5	28	8.4
4.7	57	12.5	11.6	22	6.2	18.6	28	8.4
4.8	45	10.8	11.7	21	6.0	18.7	28	8.4
4.9	37	8.4	11.8	21	6.0	18.8	28	8.4
5.0	33	7.7	11.9	24	6.6	18.9	31	9.1
5.1	80	17.5	12.0	25	7.0	19.0	31	9.2
5.2	60	13.3	12.1	21	6.2	19.1	31	9.2
5.3	39	8.9	12.2	22	6.4	19.2	30	9.0
5.4	30	7.1	12.3	24	6.8	19.3	28	8.6
5.5	25	6.0	12.4	21	6.2	19.4	31	8.2
5.6	22	5.4	12.5	23	6.6	19.5	31	9.2
5.7	22	5.4	12.6	25	7.0	19.6	32	9.4
5.8	20	5.0	12.7	22	6.4	19.7	32	9.4
5.9	19	4.8	12.8	21	6.2	19.8	31	9.4
6.0	18	4.7	12.9	22	6.4	19.9	31	9.2
6.1	25	6.2	13.0	25	7.1			
6.2	17	4.5	13.1	25	7.1			
6.3	18	4.7	13.2	27	7.5			
6.4	20	5.1	13.3	25	7.1			
6.5	21	5.3	13.4	26	7.3			
6.6	22	5.5	13.5	21	6.3			
6.7	22	5.5	13.6	25	7.1			
6.8	23	5.8	13.7	28	7.8			
6.9	23	5.8	13.8	24	6.9			
			13.9	23	6.7			

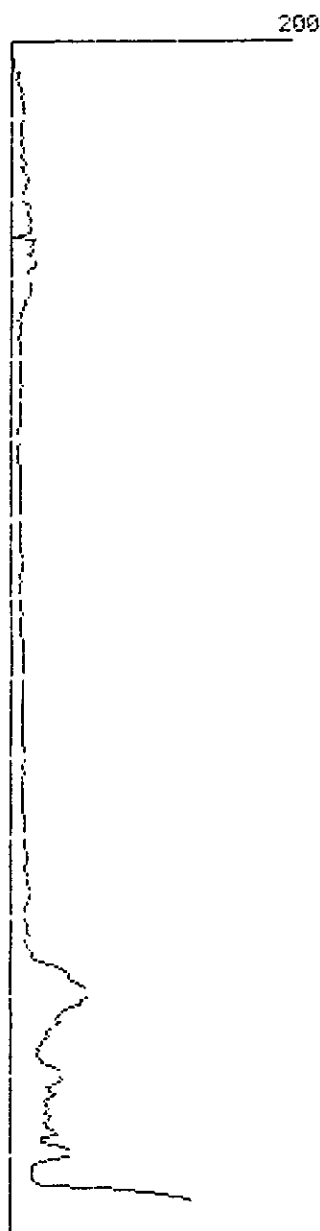
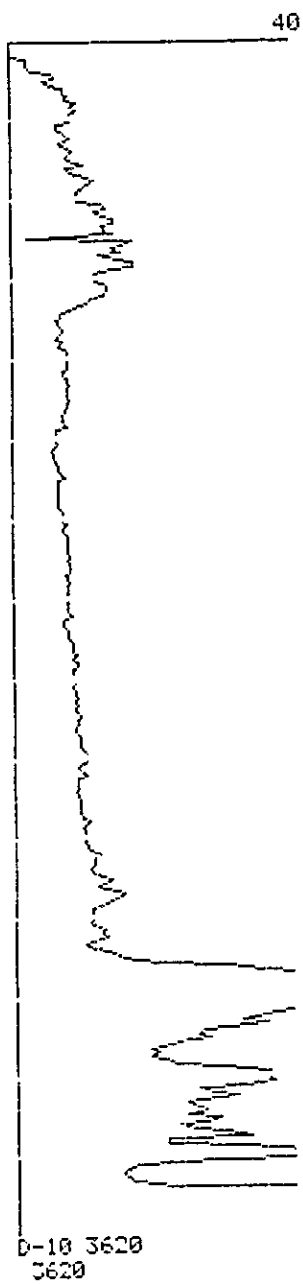
2 t Rings

20.0	31	9.3	22.8	88	78.2
20.1	33	9.8	22.9	34	32.2
20.2	40	11.2	23.0	15	16.1
20.3	35	10.2	23.1	14	15.3
20.4	30	9.1	23.2	11	12.7
20.5	31	9.3	23.3	11	12.7
20.6	31	9.3	23.4	28	27.2
20.7	30	9.1	23.5	16	17.0
20.8	30	9.1	23.6	16	17.0
20.9	30	9.1	23.7	33	31.5
21.0	28	8.9	23.8	29	28.0
21.1	30	9.3	23.9	26	25.5
21.2	31	9.5	24.0	30	29.0
21.3	35	10.3	24.1	23	23.1
21.4	38	10.9	24.2	80	71.7
21.5	40	11.4	24.3	45	41.8
21.6	35	10.3	24.4	34	32.5
21.7	38	10.9	24.5	20	20.5
21.8	45	12.4	24.6	12	13.7
21.9	55	14.5	24.7	33	31.6
22.0	45	12.5	24.8	32	30.7
22.1	75	18.8	24.9	75	67.4
22.2	65	16.7	25.0	45	42.0
22.3	60	15.7	25.1	65	59.0
22.4	55	14.6	25.2	22	22.4
22.5	60	15.7	25.3	62	56.5
22.6	60	15.7	25.4	20	20.6
22.7	110	26.1	25.5	48	44.5
			25.6	23	22.4
			25.7	27	26.6
			25.8	33	31.7
			25.9	33	31.7
			26.0	40	37.8
			26.1	23	23.3
			26.2	22	22.5
			26.3	24	24.2
			26.4	29	26.5
			26.5	30	29.5
			26.6	29	27.6
			26.7	26	25.9
			26.8	26	25.9
			26.9	33	31.9
			27.0	48	44.8
			27.1	40	38.0
			27.2	22	22.6
			27.3	18	19.2
			27.4	21	21.8
			27.5	70	63.6
			27.6	95	84.9
			27.7	55	50.8
			27.8	65	59.3
			27.9	38	36.3
			28.0	74	67.1
			28.1	120	106.4
			28.2	109	97.0
			28.3	112	99.5
			28.4	109	97.0
			28.5	113	100.4
			28.6	112	99.5
			28.7	117	103.8
			28.8	125	110.6
			28.9	170	149.0
			29.0	182	159.4
			29.1	195	170.5
			29.2	192	167.9
			29.3	185	161.9
			29.4	180	157.7
			29.5	175	153.4
			29.6	145	127.8
			29.7	140	123.6
			29.8	195	170.5
			29.9	180	157.7
			30.0	210	183.4



Depth	Dial	Gc	500Pa	Rins					
0.1	0	0.1	7.0	26	6.5	17.9	27	7.7	5
0.2	0	0.1	7.1	24	6.1	14.0	27	7.7	7
0.3	0	0.1	7.2	25	6.3	14.1	27	7.7	7
0.4	0	0.1	7.3	27	6.7	14.2	27	7.7	7
0.5	10	2.2	7.4	28	6.9	14.3	27	7.7	7
0.6	11	2.4	7.5	27	6.7	14.4	29	8.1	1
0.7	10	2.2	7.6	24	6.1	14.5	25	7.7	3
0.8	13	2.8	7.7	29	6.9	14.6	24	7.7	1
0.9	27	5.8	7.8	25	6.3	14.7	24	7.7	1
1.0	28	6.1	7.9	29	7.1	14.8	27	7.7	1
1.1	20	4.4	8.0	30	7.5	14.9	27	7.7	1
1.2	24	5.3	8.1	31	7.7	15.0	26	7.7	6
1.3	33	7.1	8.2	30	7.7	15.1	26	7.7	6
1.4	33	7.1	8.3	27	6.9	15.2	26	7.7	2
1.5	37	8.8	8.4	27	6.9	15.3	26	7.7	0
1.6	35	7.7	8.5	31	7.7	15.4	26	7.7	0
1.7	43	9.2	8.6	31	7.7	15.5	26	7.7	0
1.8	58	8.2	8.7	32	7.7	15.6	28	7.7	0
1.9	42	9.0	8.8	30	7.7	15.7	26	7.7	0
2.0	37	8.1	8.9	30	7.7	15.8	26	7.7	0
2.1	29	6.4	9.0	30	7.7	15.9	26	7.7	0
2.2	29	6.4	9.1	31	7.7	16.0	28	7.7	0
2.3	32	7.1	9.2	30	7.7	16.1	26	7.7	0
2.4	34	7.7	9.3	29	7.4	16.2	28	7.7	0
2.5	37	8.1	9.4	28	7.7	16.3	26	7.7	0
2.6	30	6.7	9.5	27	7.7	16.4	26	7.7	0
2.7	32	7.1	9.6	27	7.7	16.5	26	7.7	0
2.8	39	8.5	9.7	27	7.7	16.6	26	7.7	0
2.9	37	8.1	9.8	29	7.4	16.7	26	7.7	0
3.0	33	7.4	9.9	22	6.8	16.8	26	7.7	0
3.1	35	7.7	10.0	22	6.1	16.9	26	7.7	0
3.2	45	9.9	10.1	23	6.3	17.0	26	7.7	0
3.3	33	7.4	10.2	20	5.5	17.1	26	7.7	0
3.4	36	8.8	10.3	19	5.5	17.2	28	7.7	0
3.5	42	9.3	10.4	20	5.7	17.3	29	7.7	0
3.6	52	11.4	10.5	20	5.7	17.4	28	7.7	0
3.7	50	11.8	10.6	22	6.1	17.5	28	7.7	0
3.8	45	9.9	10.7	27	6.3	17.6	26	7.7	0
3.9	42	9.9	10.8	23	6.3	17.7	26	7.7	0
4.0	41	9.2	10.9	25	6.7	17.8	26	7.7	0
4.1	55	12.1	11.0	27	7.7	17.9	26	7.7	0
4.2	58	12.8	11.1	23	6.4	18.0	26	7.7	0
4.3	50	11.1	11.2	23	6.4	18.1	26	7.7	0
4.4	55	12.1	11.3	23	6.4	18.2	26	7.7	0
4.5	67	13.8	11.4	23	6.4	18.3	26	7.7	0
4.6	63	13.8	11.5	23	6.4	18.4	26	7.7	0
4.7	55	12.1	11.6	23	6.4	18.5	26	7.7	0
4.8	56	12.7	11.7	23	6.4	18.6	29	7.7	0
4.9	67	13.8	11.8	23	6.4	18.7	29	7.7	0
5.0	7	2.3	11.9	24	6.6	18.8	26	7.7	0
5.1	74	16.2	12.0	24	6.8	18.9	28	7.7	0
5.2	67	14.8	12.1	27	7.4	19.0	29	7.7	0
5.3	60	13.3	12.2	25	7.7	19.1	26	7.7	0
5.4	67	14.8	12.3	25	7.7	19.2	26	7.7	0
5.5	53	11.9	12.4	27	7.4	19.3	26	7.7	0
5.6	63	13.9	12.5	27	7.4	19.4	26	7.7	0
5.7	73	16.8	12.6	27	7.4	19.5	26	7.7	0
5.8	74	16.2	12.7	27	7.4	19.6	26	7.7	0
5.9	60	13.7	12.8	28	7.6	19.7	26	7.7	0
6.0	50	11.4	12.9	27	7.4	19.8	26	7.7	0
6.1	55	12.4	13.0	28	7.7	19.9	26	7.7	0
6.2	57	13.1	13.1	27	7.5	20.0	26	7.7	0
6.3	57	12.8	13.2	29	8.8	20.1	26	7.7	0
6.4	55	12.4	13.3	28	7.7	20.2	26	7.7	0
6.5	48	10.9	13.4	28	7.7	20.3	26	7.7	0
6.6	45	10.3	13.5	25	7.1	20.4	26	7.7	0
6.7	40	9.7	13.6	27	7.5	20.5	26	7.7	0
6.8	33	7.8	13.7	28	7.7	20.6	26	7.7	0
6.9	29	7.8	13.8	27	7.5	20.7	26	7.7	0
						20.8	26	7.7	0
						20.9	27	7.7	0

			2 t Pina		
21.0	42	11.8	24.0	56	51.2
21.1	48	13.0	24.1	51	47.0
21.2	43	12.0	24.2	51	47.0
21.3	39	11.1	24.3	42	39.3
21.4	51	13.6	24.4	36	34.2
21.5	55	14.5	24.5	35	33.3
21.6	50	13.4	24.6	31	29.9
21.7	48	13.0	24.7	35	33.3
21.8	41	11.6	24.8	29	28.2
21.9	36	10.5	24.9	25	24.8
22.0	36	10.7	25.0	24	24.1
22.1	35	10.5	25.1	26	25.8
22.2	38	11.1	25.2	21	21.5
22.3	43	12.1	25.3	20	20.6
22.4	41	11.7	25.4	17	18.1
22.5	45	12.5	25.5	18	18.9
22.6	36	10.7	25.6	17	18.1
22.7	31	9.6	25.7	19	19.8
22.8	37	10.9	25.8	21	21.5
22.9	46	12.7	25.9	28	27.5
23.0	51	13.9	26.0	35	33.6
23.1	53	14.3	26.1	36	34.4
23.2	75	18.9	26.2	31	30.2
23.3	118	27.9	26.3	24	24.7
23.4	142	33.1	26.4	26	25.0
23.5	165	37.6	26.5	30	29.0
23.6	172	39.1	26.6	24	24.2
23.7	175	39.7	26.7	23	23.5
23.8	195	43.9	26.8	24	24.2
23.9	220	49.1	26.9	25	25.1
			27.0	21	22.6
			27.1	27	26.9
			27.2	26	25.2
			27.3	21	21.8
			27.4	21	21.5
			27.5	28	27.7
			27.6	31	31.2
			27.7	19	20.1
			27.8	19	20.1
			27.9	31	30.3
			28.0	41	39.0
			28.1	27	27.0
			28.2	14	15.9
			28.3	13	15.1
			28.4	12	14.2
			28.5	12	14.2
			28.6	13	15.1
			28.7	14	15.9
			28.8	20	21.1
			28.9	65	59.4
			29.0	107	92.0
			29.1	115	102.2
			29.2	135	119.0
			29.3	137	121.0



D-12

Depth Dial Qc

500ks Rins

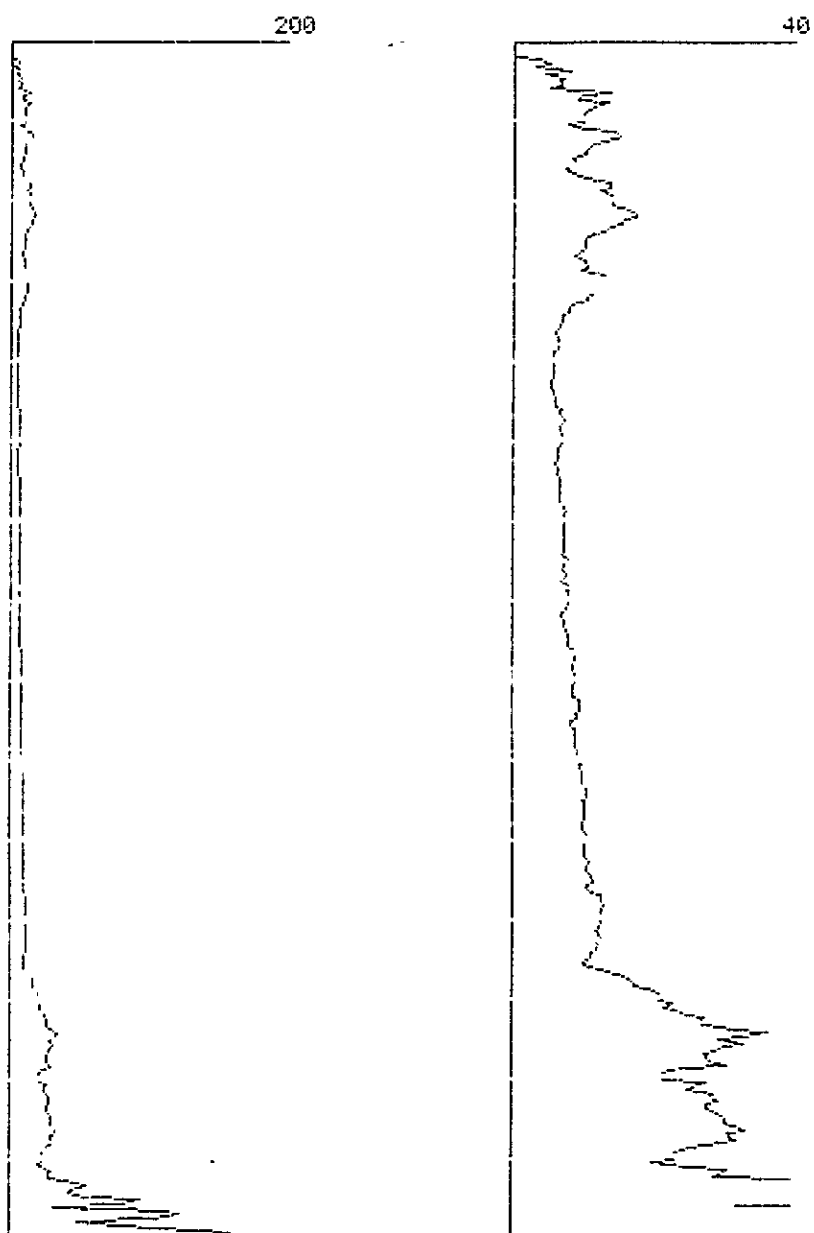
0.1	0	0.1	7.0	26	6.6	14.0	27
0.2	0	0.1	7.1	27	6.6	14.1	27
0.3	0	0.1	7.2	25	6.6	14.2	25
0.4	0	0.1	7.3	24	6.6	14.3	22
0.5	17	3.7	7.4	22	5.5	14.4	22
0.6	22	4.7	7.5	23	5.5	14.5	23
0.7	13	2.0	7.6	23	5.5	14.6	23
0.8	35	7.4	7.7	22	5.5	14.7	21
0.9	20	4.3	7.8	24	5.5	14.8	25
1.0	30	6.5	7.9	21	5.5	14.9	26
1.1	27	5.9	8.0	20	5.5	15.0	25
1.2	29	6.3	8.1	20	5.5	15.1	26
1.3	21	4.6	8.2	20	5.5	15.2	26
1.4	60	12.0	8.3	20	5.5	15.3	29
1.5	43	9.2	8.4	20	5.5	15.4	31
1.6	40	8.3	8.5	19	5.5	15.5	30
1.7	58	12.3	8.6	19	5.5	15.6	30
1.8	49	10.5	8.7	19	5.5	15.7	28
1.9	47	10.1	8.8	20	5.5	15.8	28
2.0	43	9.4	8.9	20	5.5	15.9	28
2.1	37	7.7	9.0	20	5.5	16.0	30
2.2	44	9.6	9.1	20	5.5	16.1	28
2.3	62	13.3	9.2	21	5.5	16.2	28
2.4	66	14.1	9.3	25	5.5	16.3	28
2.5	62	13.0	9.4	27	5.5	16.4	28
2.6	49	10.6	9.5	25	5.5	16.5	28
2.7	48	10.4	9.6	25	5.5	16.6	28
2.8	45	10.4	9.7	25	5.5	16.7	28
2.9	44	9.9	9.8	23	5.5	16.8	28
3.0	35	7.9	9.9	24	5.5	16.9	28
3.1	36	8.0	10.0	25	5.5	17.0	28
3.2	33	7.4	10.1	20	5.5	17.1	26
3.3	33	7.7	10.2	22	5.5	17.2	26
3.4	35	7.9	10.3	22	5.5	17.3	26
3.5	40	8.9	10.4	22	5.5	17.4	26
3.6	52	11.4	10.5	22	5.5	17.5	26
3.7	58	12.6	10.6	26	5.5	17.6	26
3.8	59	12.0	10.7	21	5.5	17.7	26
3.9	60	11.6	10.8	21	5.5	17.8	26
4.0	60	11.2	10.9	21	5.5	17.9	26
4.1	60	10.2	11.0	21	5.5	18.0	26
4.2	70	13.2	11.1	21	5.5	18.1	26
4.3	73	15.9	11.2	21	5.5	18.2	26
4.4	74	16.1	11.3	21	5.5	18.3	26
4.5	67	14.6	11.4	20	5.5	18.4	26
4.6	65	14.2	11.5	20	5.5	18.5	26
4.7	58	12.0	11.6	20	5.5	18.6	26
4.8	47	12.1	11.7	24	5.5	18.7	26
4.9	42	10.5	11.8	25	5.5	18.8	26
5.0	42	9.9	11.9	27	5.5	18.9	26
5.1	43	9.0	12.0	25	5.5	19.0	26
5.2	42	9.0	12.1	24	5.5	19.1	26
5.3	42	9.0	12.2	25	5.5	19.2	26
5.4	38	8.0	12.3	24	5.5	19.3	26
5.5	35	8.1	12.4	24	5.5	19.4	26
5.6	42	9.6	12.5	25	5.5	19.5	26
5.7	42	9.6	12.6	24	5.5	19.6	26
5.8	44	10.0	12.7	26	5.5	19.7	26
5.9	40	9.1	12.8	26	5.5	19.8	26
6.0	54	12.2	12.9	23	5.5	19.9	26
6.1	52	11.0	13.0	27	5.5	20.0	26
6.2	50	11.4	13.1	25	5.5	20.1	26
6.3	48	10.9	13.2	24	5.5	20.2	26
6.4	43	9.9	13.3	23	5.5	20.3	26
6.5	43	9.9	13.4	26	5.5	20.4	26
6.6	33	7.7	13.5	26	5.5	20.5	26
6.7	31	7.4	13.6	23	5.5	20.6	26
6.8	31	7.4	13.7	26	5.5	20.7	26
6.9	27	6.6	13.8	28	5.5	20.8	26
		16	13.9	26	5.5	20.9	26

21.0	37	10.7
21.1	40	11.4
21.2	34	10.1
21.3	34	10.1
21.4	37	10.7
21.5	42	11.8
21.6	42	11.8
21.7	42	11.8
21.8	44	12.2
21.9	43	12.0
22.0	41	11.7
22.1	41	11.7
22.2	40	11.5
22.3	38	11.1
22.4	40	11.5
22.5	41	11.7
22.6	39	11.3
22.7	40	11.5
22.8	39	11.3
22.9	36	10.7
23.0	35	10.6
23.1	32	10.0
23.2	30	9.6
23.3	33	10.6
23.4	46	12.9
23.5	52	14.1
23.6	59	15.6
23.7	60	15.8
23.8	62	16.2
23.9	70	17.9
24.0	78	19.7
24.1	86	21.0
24.2	90	20.1
24.3	87	21.5
24.4	95	23.0
24.5	106	25.5
24.6	107	24.9
24.7	105	25.0
24.8	125	29.5
24.9	145	33.6
25.0	130	30.6
25.1	114	27.0
25.2	130	30.6
25.3	117	27.9
25.4	111	26.7
25.5	105	25.4
25.6	107	25.8
25.7	108	26.1
25.8	110	26.5
25.9	90	23.3
26.0	79	20.2
26.1	106	25.8
26.2	97	23.9
26.3	84	23.3
26.4	110	28.6
26.5	109	26.4
26.6	113	27.2
26.7	106	25.8
26.8	105	25.6
26.9	110	26.6
27.0	115	27.8
27.1	117	28.2
27.2	117	28.2
27.3	123	29.4
27.4	130	30.9
27.5	118	28.4
27.6	120	28.8
27.7	124	29.7
27.8	105	25.7
27.9	95	23.6

28.0	85	21.7
28.1	70	19.5
28.2	93	23.1
28.3	118	28.5
28.4	113	27.0
28.5	109	26.1
28.6	210	47.1

2 t Pine

28.7	56	15.0
28.8	45	12.4
28.9	43	10.4
29.0	56	13.9
29.1	120	29.4
29.2	85	17.6
29.3	30	7.0
29.4	120	106.5
29.5	172	116.7
29.6	112	98.7
29.7	50	48.8
29.8	80	73.4
29.9	115	102.0
30.0	170	149.0



D-12 3825
3823

0-13

Depth Dial Qc

Depth	Dial	Qc
	500ka	Rina
0.0	0.0	0.0
0.1	0.1	0.1
0.2	0.2	0.2
0.3	0.3	0.3
0.4	0.4	0.4
0.5	0.5	0.5
0.6	0.6	0.6
0.7	0.7	0.7
0.8	0.8	0.8
0.9	0.9	0.9
1.0	1.0	1.0
1.1	1.1	1.1
1.2	1.2	1.2
1.3	1.3	1.3
1.4	1.4	1.4
1.5	1.5	1.5
1.6	1.6	1.6
1.7	1.7	1.7
1.8	1.8	1.8
1.9	1.9	1.9
2.0	2.0	2.0
2.1	2.1	2.1
2.2	2.2	2.2
2.3	2.3	2.3
2.4	2.4	2.4
2.5	2.5	2.5
2.6	2.6	2.6
2.7	2.7	2.7
2.8	2.8	2.8
2.9	2.9	2.9
3.0	3.0	3.0
3.1	3.1	3.1
3.2	3.2	3.2
3.3	3.3	3.3
3.4	3.4	3.4
3.5	3.5	3.5
3.6	3.6	3.6
3.7	3.7	3.7
3.8	3.8	3.8
3.9	3.9	3.9
4.0	4.0	4.0
4.1	4.1	4.1
4.2	4.2	4.2
4.3	4.3	4.3
4.4	4.4	4.4
4.5	4.5	4.5
4.6	4.6	4.6
4.7	4.7	4.7
4.8	4.8	4.8
4.9	4.9	4.9
5.0	5.0	5.0
5.1	5.1	5.1
5.2	5.2	5.2
5.3	5.3	5.3
5.4	5.4	5.4
5.5	5.5	5.5
5.6	5.6	5.6
5.7	5.7	5.7
5.8	5.8	5.8
5.9	5.9	5.9
6.0	6.0	6.0
6.1	6.1	6.1
6.2	6.2	6.2
6.3	6.3	6.3
6.4	6.4	6.4
6.5	6.5	6.5
6.6	6.6	6.6
6.7	6.7	6.7
6.8	6.8	6.8
6.9	6.9	6.9
7.0	7.0	7.0
7.1	7.1	7.1
7.2	7.2	7.2
7.3	7.3	7.3
7.4	7.4	7.4
7.5	7.5	7.5
7.6	7.6	7.6
7.7	7.7	7.7
7.8	7.8	7.8
7.9	7.9	7.9
8.0	8.0	8.0
8.1	8.1	8.1
8.2	8.2	8.2
8.3	8.3	8.3
8.4	8.4	8.4
8.5	8.5	8.5
8.6	8.6	8.6
8.7	8.7	8.7
8.8	8.8	8.8
8.9	8.9	8.9
9.0	9.0	9.0
9.1	9.1	9.1
9.2	9.2	9.2
9.3	9.3	9.3
9.4	9.4	9.4
9.5	9.5	9.5
9.6	9.6	9.6
9.7	9.7	9.7
9.8	9.8	9.8
9.9	9.9	9.9
10.0	10.0	10.0

21.0	45	12.4
21.1	40	11.4
21.2	42	11.8
21.3	42	11.8
21.4	43	12.0
21.5	39	11.1
21.6	40	11.4
21.7	47	12.8
21.8	53	14.1
21.9	55	14.5
22.0	60	15.7
22.1	65	16.7
22.2	69	17.5
22.3	85	20.9
22.4	89	21.7
22.5	85	20.9
22.6	109	25.8
22.7	120	28.1
22.8	125	29.0
22.9	127	29.0
23.0	135	29.0
23.1	140	30.4
23.2	135	31.4
23.3	140	32.4
23.4	137	31.4
23.5	150	34.5
23.6	150	34.5
23.7	151	34.5
23.8	175	39.7
23.9	179	40.7
24.0	195	46.1

27 5100

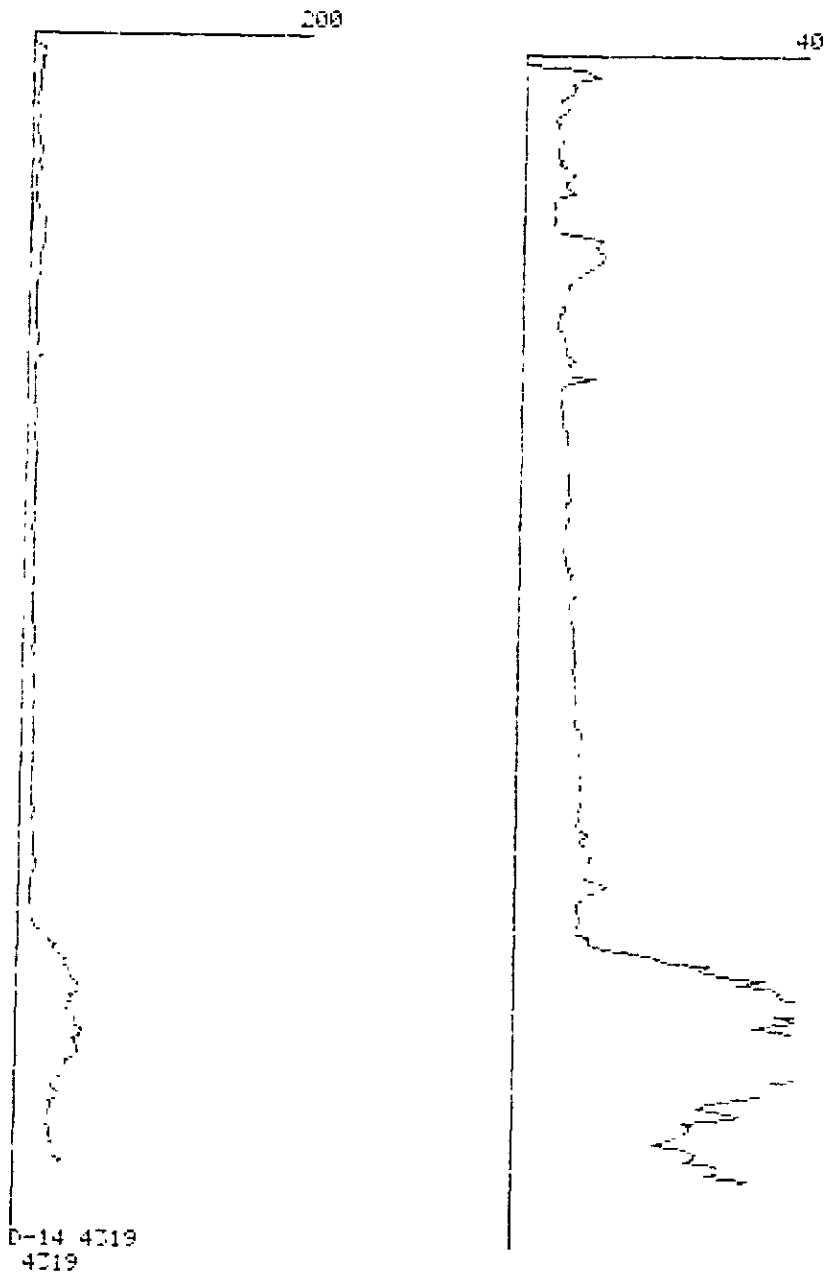
24.1	50	46.1
24.2	49	45.8
24.3	47	45.1
24.4	51	47.0
24.5	48	47.0
24.6	50	48.1
24.7	50	48.1
24.8	54	49.5
24.9	51	47.1
25.0	46	45.8
25.1	51	47.1
25.2	40	37.1
25.3	44	41.1
25.4	33	38.9
25.5	30	38.9
25.6	30	39.9
25.7	30	39.9
25.8	31	40.0
25.9	33	41.0
26.0	33	41.0
26.1	33	41.0
26.2	33	41.0
26.3	33	41.0
26.4	33	41.0
26.5	33	41.0
26.6	33	41.0
26.7	33	41.0
26.8	33	41.0
26.9	33	41.0
27.0	33	41.0
27.1	33	41.0
27.2	33	41.0
27.3	33	41.0
27.4	33	41.0
27.5	33	41.0
27.6	33	41.0
27.7	33	41.0
27.8	33	41.0
27.9	33	41.0
28.0	33	41.0



D-13 4819
4919



•



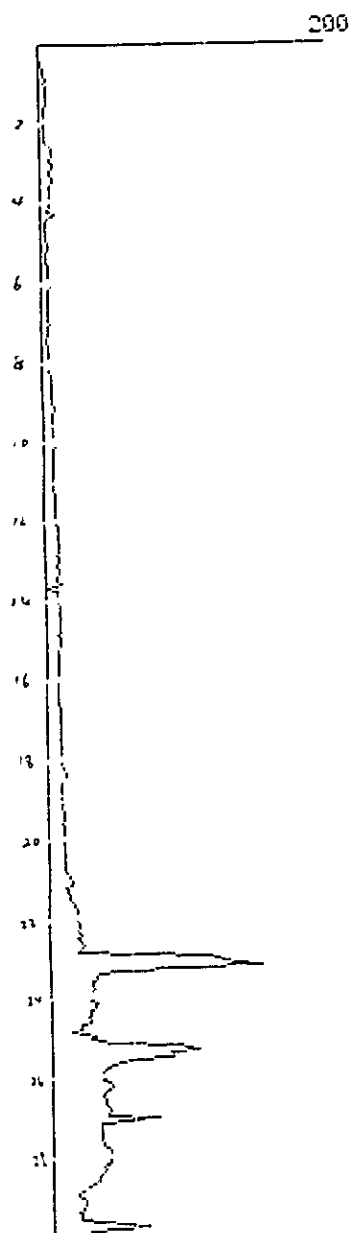
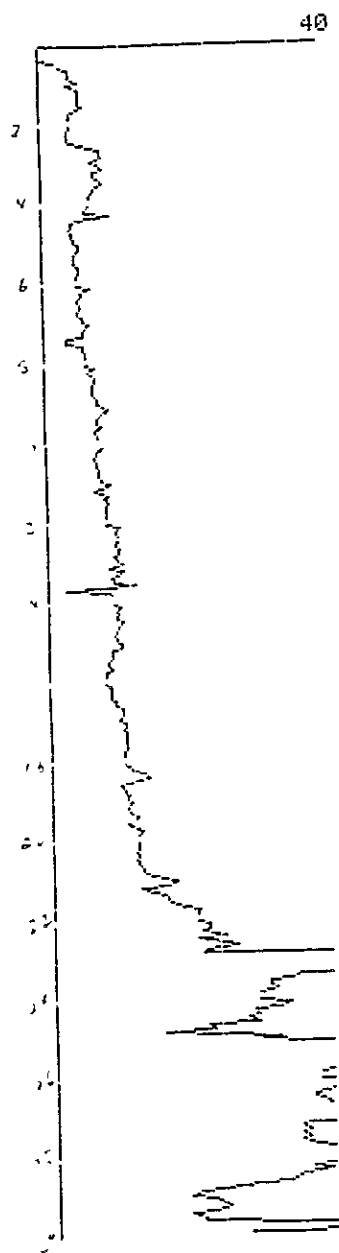
D-15

Depth	Dial	Qc	500ks	Rins						
0.1	0	0.1			7.0	20	5.3	14.0	34	9.1
0.2	0	0.1			7.1	25	6.3	14.1	38	10.0
0.3	0	0.1			7.2	22	5.7	14.2	35	9.3
0.4	0	0.1			7.3	20	5.3	14.3	37	9.8
0.5	10	2.2			7.4	20	5.3	14.4	35	9.5
0.6	14	3.1			7.5	10	3.2	14.5	40	10.4
0.7	20	4.3			7.6	10	3.2	14.6	37	9.8
0.8	20	4.3			7.7	21	5.5	14.7	37	9.8
0.9	20	4.3			7.8	21	5.5	14.8	35	9.3
1.0	25	5.5			7.9	22	5.7	14.9	34	9.1
1.1	17	3.8			8.0	22	6.0	15.0	34	9.3
1.2	25	5.5			8.1	27	6.9	15.1	37	9.9
1.3	24	5.3			8.2	23	6.0	15.2	37	9.9
1.4	25	5.5			8.3	26	6.7	15.3	31	8.7
1.5	25	5.5			8.4	27	6.9	15.4	31	8.7
1.6	25	5.5			8.5	27	6.8	15.5	31	8.7
1.7	27	5.9			8.6	26	6.7	15.6	28	8.0
1.8	20	4.4			8.7	26	6.7	15.7	28	8.0
1.9	18	4.0			8.8	26	6.7	15.8	31	8.7
2.0	18	4.2			8.9	27	6.9	15.9	27	7.8
2.1	18	4.2			9.0	28	7.2	16.0	27	8.0
2.2	17	4.0			9.1	28	7.2	16.1	30	8.6
2.3	17	4.0			9.2	35	8.7	16.2	29	8.4
2.4	16	3.7			9.3	32	8.0	16.3	29	8.4
2.5	20	4.6			9.4	30	7.6	16.4	30	8.6
2.6	30	6.7			9.5	28	7.2	16.5	33	9.2
2.7	37	8.1			9.6	28	7.2	16.6	32	9.2
2.8	37	8.1			9.7	31	7.3	16.7	37	10.2
2.9	39	8.5			9.8	27	7.0	16.8	37	10.0
3.0	31	7.0			9.9	27	7.0	16.9	37	10.0
3.1	55	7.8			10.0	26	7.3	17.0	35	9.3
3.2	39	8.5			10.1	30	7.8	17.1	37	10.2
3.3	32	7.2			10.2	26	6.9	17.2	37	10.2
3.4	32	7.2			10.3	26	6.9	17.3	36	10.0
3.5	35	7.8			10.4	25	6.7	17.4	38	10.4
3.6	38	8.5			10.5	26	6.9	17.5	38	10.4
3.7	33	7.4			10.6	26	6.9	17.6	37	10.2
3.8	32	7.2			10.7	28	7.3	17.7	37	10.2
3.9	30	6.8			10.8	27	7.1	17.8	38	10.4
4.0	28	6.5			10.9	28	7.3	17.9	36	10.0
4.1	27	6.3			11.0	28	7.5	18.0	36	10.1
4.2	25	5.9			11.1	34	8.7	18.1	38	10.5
4.3	42	9.4			11.2	28	7.5	18.2	40	10.9
4.4	19	4.6			11.3	24	6.8	18.3	48	12.6
4.5	17	4.2			11.4	32	8.0	18.4	50	13.0
4.6	16	4.0			11.5	30	7.9	18.5	43	11.6
4.7	15	3.8			11.6	32	8.3	18.6	52	9.7
4.8	16	4.0			11.7	31	8.1	18.7	34	9.1
4.9	17	4.2			11.8	31	8.1	18.8	35	9.9
5.0	17	4.4			11.9	31	8.1	18.9	39	10.7
5.1	21	5.2			12.0	31	8.2	19.0	37	10.5
5.2	20	5.0			12.1	40	10.1	19.1	39	10.9
5.3	19	4.8			12.2	37	9.5	19.2	37	10.5
5.4	17	4.4			12.3	37	9.5	19.3	37	10.5
5.5	17	4.4			12.4	39	9.9	19.4	39	10.9
5.6	17	4.4			12.5	37	9.5	19.5	42	11.5
5.7	20	5.0			12.6	37	9.5	19.6	39	10.9
5.8	20	5.0			12.7	40	10.1	19.7	36	10.2
5.9	20	5.0			12.8	38	9.7	19.8	40	11.1
6.0	18	4.7			12.9	35	9.1	19.9	45	12.1
6.1	27	6.6			13.0	38	9.8	20.0	41	11.4
6.2	20	5.1			13.1	40	10.3	20.1	42	11.6
6.3	21	5.3			13.2	32	8.6	20.2	41	11.4
6.4	19	4.9			13.3	40	10.3	20.3	40	11.2
6.5	18	4.7			13.4	38	9.8	20.4	42	11.6
6.6	20	5.1			13.5	33	8.8	20.5	40	11.2
6.7	20	5.1			13.6	34	9.0	20.6	41	11.4
6.8	19	4.9			13.7	47	11.7	20.7	43	11.8
6.9	21	5.3			13.8	4	2.8	20.8	44	12.0
					13.9	31	8.4	20.9	46	12.5

2 t Pina

21.0	56	14.7
21.1	65	16.6
21.2	60	15.5
21.3	42	11.8
21.4	50	13.4
21.5	57	14.9
21.6	59	15.3
21.7	60	15.5
21.8	69	17.4
21.9	80	19.7
22.0	77	19.2
22.1	85	20.9
22.2	85	20.9
22.3	80	19.8
22.4	95	22.9
22.5	77	19.2
22.6	95	22.9
22.7	103	24.6
22.8	81	20.0
22.9	80	19.8

23.0	120	105.7
23.1	125	109.9
23.2	140	122.7
23.3	150	138.1
23.4	50	46.0
23.5	35	33.2
23.6	33	31.5
23.7	30	28.9
23.8	30	28.9
23.9	31	29.0
24.0	28	27.7
24.1	33	31.6
24.2	31	29.9
24.3	27	26.5
24.4	28	27.3
24.5	26	25.6
24.6	28	27.7
24.7	20	20.5
24.8	21	21.4
24.9	13	14.5
25.0	31	30.0
25.1	28	27.5
25.2	43	40.3
25.3	96	85.5
25.4	111	98.7
25.5	88	79.7
25.6	90	80.4
25.7	58	53.1
25.8	45	42.0
25.9	40	37.7
26.0	37	35.7
26.1	41	38.7
26.2	43	40.4
26.3	39	37.0
26.4	36	34.4
26.5	36	34.4
26.6	38	36.1
26.7	38	36.1
26.8	41	38.7
26.9	42	39.6
27.0	40	38.0
27.1	80	72.1
27.2	35	33.7
27.3	34	32.9
27.4	35	33.7
27.5	34	32.9
27.6	35	33.7
27.7	34	32.9
27.8	36	34.6
27.9	39	37.1
28.0	42	39.8
28.1	42	39.8
28.2	35	33.9
28.3	38	36.4
28.4	34	33.0
28.5	33	32.2
28.6	32	31.3
28.7	27	27.0
28.8	21	21.9
28.9	18	19.4
29.0	16	17.8
29.1	20	21.2
29.2	21	22.1
29.3	22	22.9
29.4	20	21.2
29.5	16	17.8
29.6	18	19.5
29.7	18	19.5
29.8	52	48.3
29.9	70	63.9
30.0	25	25.6



D-16

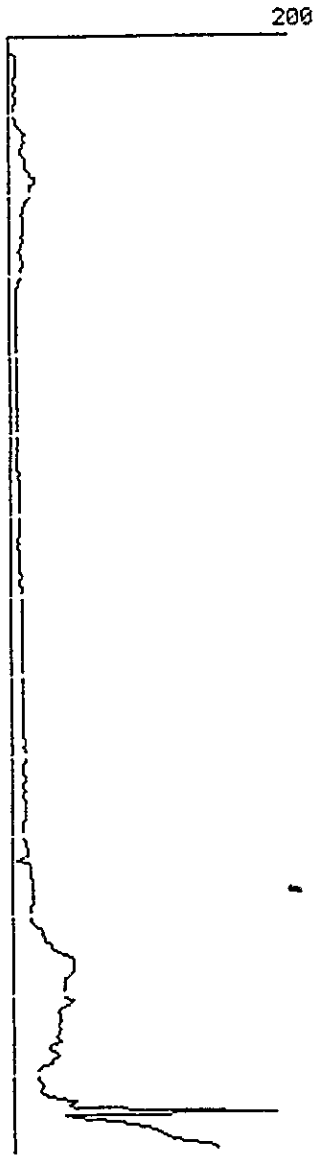
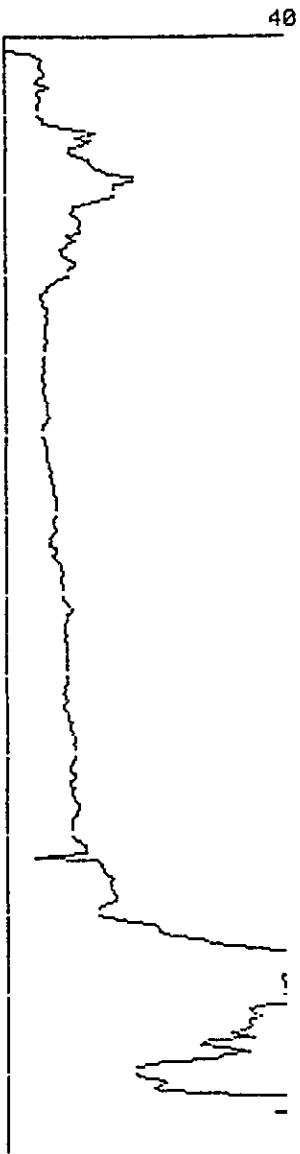
Depth Dial Rc

500kg Rins								
			7.0	22	5.7	14.0	28	7.9
0.1	0	0.1	7.1	21	5.5	14.1	28	7.9
0.2	0	0.1	7.2	22	5.7	14.2	30	8.3
0.3	0	0.1	7.3	22	5.7	14.3	32	8.7
0.4	0	0.1	7.4	20	5.3	14.4	33	8.9
0.5	15	3.3	7.5	20	5.3	14.5	31	8.5
0.6	22	4.7	7.6	20	5.3	14.6	31	8.5
0.7	24	5.1	7.7	20	5.3	14.7	30	8.3
0.8	23	4.9	7.8	22	5.7	14.8	29	8.1
0.9	23	4.9	7.9	21	5.5	14.9	29	8.1
1.0	25	5.5	8.0	20	5.4	15.0	28	8.0
1.1	24	5.3	8.1	18	5.0	15.1	30	8.4
1.2	20	4.4	8.2	20	5.4	15.2	29	8.2
1.3	18	4.0	8.3	18	5.0	15.3	30	8.4
1.4	27	5.9	8.4	20	5.4	15.4	30	8.4
1.5	22	4.9	8.5	18	5.0	15.5	30	8.4
1.6	20	4.4	8.6	18	5.0	15.6	30	8.4
1.7	21	4.6	8.7	18	5.0	15.7	30	8.4
1.8	22	4.9	8.8	20	5.4	15.8	30	8.4
1.9	20	4.4	8.9	18	5.0	15.9	30	8.4
2.0	19	4.4	9.0	18	5.1	16.0	30	8.6
2.1	22	5.0	9.1	19	5.3	16.1	30	8.6
2.2	22	5.0	9.2	19	5.3	16.2	29	8.4
2.3	30	6.7	9.3	20	5.5	16.3	28	8.2
2.4	48	10.4	9.4	20	5.5	16.4	28	8.2
2.5	56	12.1	9.5	20	5.5	16.5	27	8.0
2.6	45	9.8	9.6	20	5.5	16.6	28	8.2
2.7	53	11.4	9.7	22	6.0	16.7	30	8.6
2.8	49	10.6	9.8	20	5.5	16.8	26	7.8
2.9	40	8.7	9.9	18	5.1	16.9	26	7.8
3.0	40	8.9	10.0	17	5.1	17.0	28	8.3
3.1	43	9.5	10.1	18	5.3	17.1	29	8.5
3.2	52	11.4	10.2	19	5.5	17.2	28	8.3
3.3	51	11.2	10.3	20	5.7	17.3	32	9.1
3.4	55	12.0	10.4	20	5.7	17.4	30	8.7
3.5	57	12.4	10.5	20	5.7	17.5	30	8.7
3.6	64	13.9	10.6	20	5.7	17.6	31	8.9
3.7	80	17.2	10.7	20	5.7	17.7	33	9.3
3.8	79	17.0	10.8	21	5.9	17.8	33	9.3
3.9	68	14.7	10.9	22	6.1	17.9	32	9.1
4.0	67	14.6	11.0	23	6.4	18.0	32	9.3
4.1	61	13.4	11.1	21	6.0	18.1	32	9.3
4.2	50	11.1	11.2	23	6.4	18.2	31	9.1
4.3	42	9.4	11.3	23	6.4	18.3	30	8.9
4.4	42	9.4	11.4	24	6.6	18.4	30	8.9
4.5	41	9.2	11.5	24	6.6	18.5	32	9.3
4.6	45	10.0	11.6	24	6.6	18.6	32	9.3
4.7	46	10.3	11.7	25	6.9	18.7	30	8.9
4.8	46	10.3	11.8	26	7.1	18.8	30	8.9
4.9	45	10.0	11.9	25	6.9	18.9	32	9.3
5.0	45	10.2	12.0	24	6.8	19.0	31	9.2
5.1	37	8.5	12.1	23	6.6	19.1	31	9.2
5.2	43	9.8	12.2	23	6.6	19.2	32	9.4
5.3	38	8.7	12.3	23	6.6	19.3	33	9.6
5.4	36	8.3	12.4	25	7.0	19.4	35	10.0
5.5	32	7.5	12.5	23	6.6	19.5	35	10.0
5.6	34	7.9	12.6	20	6.0	19.6	34	9.8
5.7	37	8.5	12.7	21	6.2	19.7	32	9.4
5.8	42	9.6	12.8	20	6.0	19.8	30	9.0
5.9	42	9.6	12.9	25	7.0	19.9	31	9.2
6.0	37	8.7	13.0	24	6.9	20.0	30	9.1
6.1	30	7.2	13.1	21	6.3	20.1	31	9.3
6.2	27	6.6	13.2	24	6.9	20.2	35	10.2
6.3	23	5.8	13.3	25	7.1	20.3	38	10.6
6.4	22	5.5	13.4	27	7.5	20.4	39	11.0
6.5	19	4.9	13.5	27	7.5	20.5	39	11.0
6.6	19	4.9	13.6	28	7.8	20.6	4	3.7
6.7	20	5.1	13.7	27	7.5	20.7	45	12.3
6.8	20	5.1	13.8	27	7.5	20.8	47	12.7
6.9	22	5.5	13.9	28	7.8	20.9	48	12.9

21.0	48	13.0
21.1	50	13.4
21.2	54	14.3
21.3	53	14.1
21.4	53	14.1
21.5	52	13.9
21.6	54	14.3
21.7	55	14.5
21.8	55	14.5
21.9	50	13.4
22.0	45	12.5
22.1	50	13.6
22.2	66	16.9
22.3	80	19.8
22.4	83	20.4
22.5	83	20.4
22.6	92	22.3
22.7	110	26.1
22.8	115	27.1
22.9	130	30.2
23.0	160	36.6
23.1	180	40.8
23.2	190	42.8
23.3	190	42.8
23.4	186	42.0
23.5	190	42.8
23.6	175	39.7
23.7	160	36.6
23.8	160	36.6
23.9	161	36.8
24.0	160	36.7
24.1	190	43.0
24.2	170	38.8
24.3	150	34.6
24.4	138	32.2
24.5	140	32.6
24.6	146	33.8
24.7	140	32.6
24.8	138	32.2
24.9	140	32.6
25.0	135	31.7
25.1	125	29.6
25.2	140	32.7
25.3	111	26.7
25.4	106	25.6
25.5	121	28.8
25.6	137	32.1
25.7	121	28.8
25.8	115	27.5
25.9	85	21.3
26.0	65	17.2
26.1	67	17.7
26.2	84	21.2
26.3	85	21.4
26.4	78	19.9
26.5	84	21.2
26.6	135	31.8
26.7	195	44.3
26.8	170	39.1
26.9	195	44.3

2 t Rings

27.0	200	174.5
27.1	37	35.4
27.2	60	55.0
27.3	80	72.1
27.4	100	89.2
27.5	109	96.8
27.6	115	102.0
27.7	117	103.7
27.8	130	114.8
27.9	150	131.8
28.0	155	136.2



D-17

Depth Dial Qc

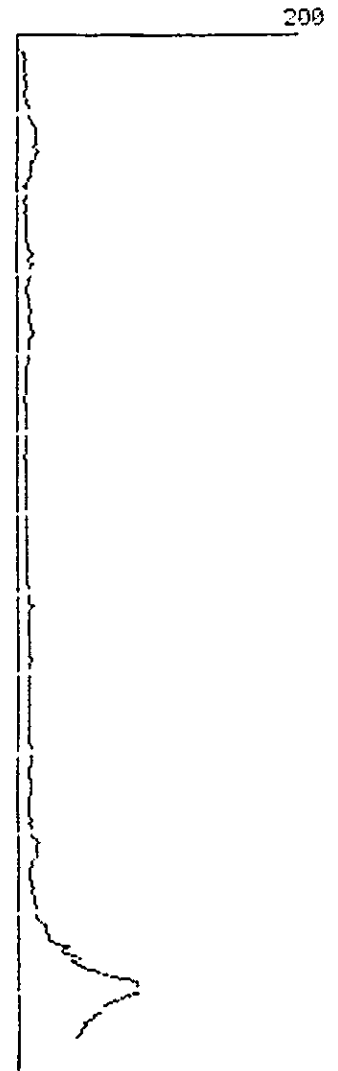
500kg Rings

0.1	0	0.1	7.0	41	9.6	14.0	30	8.3
0.2	0	0.1	7.1	38	9.0	14.1	31	8.5
0.3	0	0.1	7.2	37	8.8	14.2	33	8.9
0.4	0	0.1	7.3	39	9.2	14.3	45	11.4
0.5	26	5.5	7.4	43	10.0	14.4	30	8.3
0.6	25	5.3	7.5	44	10.3	14.5	31	8.5
0.7	30	6.4	7.6	52	11.9	14.6	32	8.7
0.8	27	5.8	7.7	45	10.5	14.7	31	8.5
0.9	27	5.8	7.8	37	8.8	14.8	29	8.1
1.0	27	5.9	7.9	32	7.8	14.9	29	8.1
1.1	30	6.5	8.0	32	7.9	15.0	28	8.0
1.2	26	5.7	8.1	34	8.3	15.1	29	8.2
1.3	30	6.5	8.2	33	8.1	15.2	29	8.2
1.4	29	6.3	8.3	30	7.5	15.3	29	8.2
1.5	29	6.3	8.4	26	6.7	15.4	29	8.2
1.6	28	6.1	8.5	29	7.3	15.5	30	8.4
1.7	27	5.9	8.6	25	6.4	15.6	31	8.7
1.8	29	6.3	8.7	25	6.4	15.7	33	9.1
1.9	33	7.1	8.8	27	6.9	15.8	33	9.5
2.0	37	8.1	8.9	24	6.2	15.9	32	8.9
2.1	40	8.7	9.0	23	6.2	16.0	30	8.6
2.2	45	9.8	9.1	24	6.4	16.1	30	8.6
2.3	53	11.4	9.2	22	6.0	16.2	31	8.8
2.4	60	12.9	9.3	22	6.0	16.3	33	9.2
2.5	63	13.5	9.4	25	6.6	16.4	33	9.2
2.6	60	12.9	9.5	25	6.6	16.5	33	9.2
2.7	60	12.9	9.6	26	6.8	16.6	33	9.2
2.8	63	13.5	9.7	26	6.8	16.7	31	8.8
2.9	57	12.3	9.8	25	6.6	16.8	32	9.0
3.0	65	14.1	9.9	24	6.4	16.9	33	9.2
3.1	58	12.6	10.0	25	6.7	17.0	32	9.1
3.2	57	12.4	10.1	24	6.5	17.1	29	8.5
3.3	48	10.5	10.2	23	6.3	17.2	30	8.7
3.4	45	9.9	10.3	23	6.3	17.3	32	9.1
3.5	46	10.1	10.4	23	6.3	17.4	29	8.5
3.6	46	10.1	10.5	24	6.5	17.5	30	8.7
3.7	45	9.9	10.6	22	6.1	17.6	30	8.7
3.8	37	8.2	10.7	23	6.3	17.7	28	8.3
3.9	32	7.2	10.8	24	6.5	17.8	30	8.7
4.0	30	6.9	10.9	23	6.3	17.9	31	8.9
4.1	30	6.9	11.0	23	6.4	18.0	32	9.1
4.2	25	5.9	11.1	22	6.2	18.1	32	9.1
4.3	28	6.5	11.2	23	6.4	18.2	33	9.5
4.4	28	6.5	11.3	24	6.6	18.3	32	9.3
4.5	26	6.1	11.4	25	6.9	18.4	31	9.1
4.6	27	6.3	11.5	27	7.3	18.5	31	9.1
4.7	31	7.1	11.6	25	6.9	18.6	31	9.1
4.8	30	6.9	11.7	25	6.9	18.7	33	9.5
4.9	28	6.5	11.8	26	7.1	18.8	33	9.5
5.0	29	6.9	11.9	27	7.3	18.9	33	9.5
5.1	32	7.5	12.0	26	7.2	19.0	34	9.8
5.2	32	7.5	12.1	25	7.0	19.1	32	9.4
5.3	33	7.7	12.2	25	7.0	19.2	31	9.2
5.4	39	8.9	12.3	25	7.0	19.3	29	8.8
5.5	40	9.1	12.4	25	7.0	19.4	30	9.0
5.6	50	11.2	12.5	26	7.2	19.5	29	8.8
5.7	42	9.6	12.6	25	7.0	19.6	29	8.8
5.8	40	9.1	12.7	25	7.0	19.7	29	8.8
5.9	48	10.8	12.8	25	7.0	19.8	33	9.6
6.0	47	10.7	12.9	25	7.0	19.9	29	8.8
6.1	34	8.0	13.0	25	7.1	20.0	31	9.3
6.2	34	8.0	13.1	25	7.1	20.1	40	11.2
6.3	30	7.2	13.2	25	7.1	20.2	60	15.4
6.4	30	7.2	13.3	26	7.3	20.3	47	12.7
6.5	32	7.6	13.4	25	7.1	20.4	46	12.5
6.6	37	8.7	13.5	27	7.5	20.5	46	12.5
6.7	35	8.2	13.6	27	7.5	20.6	47	12.7
6.8	37	8.7	13.7	27	7.5	20.7	43	11.8
6.9	39	9.1	13.8	25	7.1	20.8	37	10.6
			13.9	26	7.3	20.9	31	9.3

21.0	28	8.9
21.1	28	8.9
21.2	28	8.9
21.3	33	9.9
21.4	33	9.9
21.5	40	11.4
21.6	30	9.3
21.7	38	10.9
21.8	39	11.1
21.9	41	11.6
22.0	45	12.5
22.1	49	13.4
22.2	60	15.7
22.3	75	18.8
22.4	75	18.8
22.5	78	19.4
22.6	86	21.1
22.7	85	20.9
22.8	109	25.8
22.9	150	34.4
23.0	127	29.7
23.1	145	33.5
23.2	185	41.8
23.3	155	35.6
23.4	185	41.8
23.5	195	43.9
23.6	250	55.3

2 t Rins

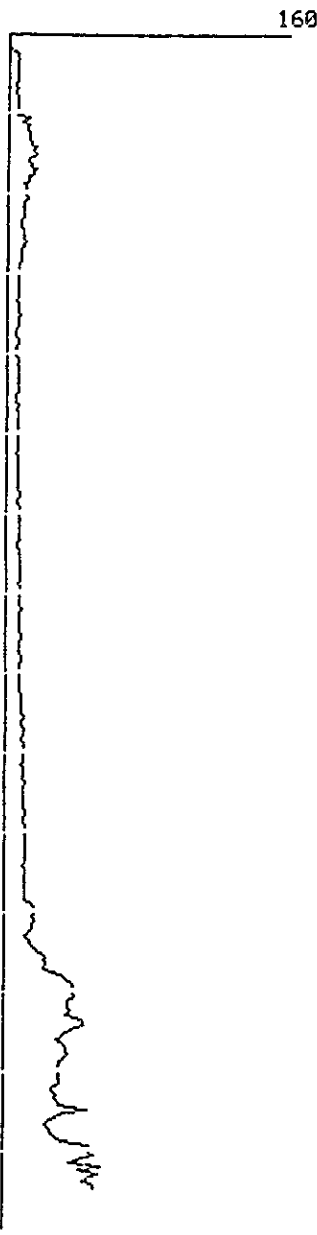
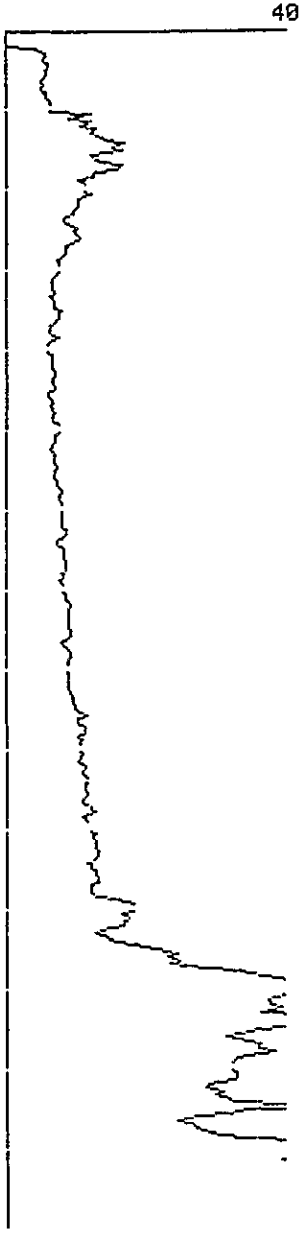
23.7	62	56.2
23.8	78	69.8
23.9	87	77.5
24.0	87	77.7
24.1	78	70.0
24.2	70	63.2
24.3	65	58.9
24.4	60	54.6
24.5	62	56.3
24.6	55	50.4
24.7	55	50.4
24.8	48	44.4
24.9	50	46.1
25.0	45	42.0
25.1	45	42.0
25.2	42	39.4



D-18

Depth	Dial	Qc	500kg Rins						
0.1	0	0.1	7.0	26	6.5	14.0	28	7.9	
0.2	0	0.1	7.1	31	7.6	14.1	29	8.1	
0.3	0	0.1	7.2	30	7.3	14.2	29	8.1	
0.4	0	0.1	7.3	29	7.1	14.3	30	8.3	
0.5	18	3.9	7.4	27	6.7	14.4	32	8.7	
0.6	25	5.3	7.5	24	6.1	14.5	30	8.3	
0.7	25	5.3	7.6	24	6.1	14.6	30	8.3	
0.8	24	5.1	7.7	23	5.9	14.7	30	8.3	
0.9	26	5.5	7.8	29	7.1	14.8	30	8.3	
1.0	26	5.7	7.9	25	6.3	14.9	30	8.3	
1.1	25	5.5	8.0	22	5.8	15.0	30	8.4	
1.2	25	5.5	8.1	24	6.2	15.1	32	8.9	
1.3	23	5.1	8.2	24	6.2	15.2	31	8.7	
1.4	22	4.9	8.3	25	6.4	15.3	30	8.4	
1.5	23	5.1	8.4	25	6.4	15.4	26	7.6	
1.6	21	4.6	8.5	24	6.2	15.5	27	7.8	
1.7	24	5.3	8.6	26	6.7	15.6	30	8.4	
1.8	25	5.5	8.7	26	6.7	15.7	32	8.9	
1.9	26	5.7	8.8	25	6.4	15.8	31	8.7	
2.0	27	6.0	8.9	25	6.4	15.9	30	8.4	
2.1	52	11.2	9.0	25	6.6	16.0	30	8.6	
2.2	39	8.5	9.1	22	6.0	16.1	30	8.6	
2.3	52	11.2	9.2	21	5.7	16.2	29	8.4	
2.4	46	10.0	9.3	22	6.0	16.3	29	8.4	
2.5	55	11.9	9.4	23	6.2	16.4	30	8.6	
2.6	52	11.2	9.5	22	6.0	16.5	30	8.6	
2.7	57	12.3	9.6	24	6.4	16.6	31	8.8	
2.8	61	13.1	9.7	25	6.6	16.7	32	9.0	
2.9	73	15.6	9.8	24	6.4	16.8	33	9.2	
3.0	65	14.1	9.9	24	6.4	16.9	33	9.2	
3.1	70	15.1	10.0	27	7.1	17.0	33	9.3	
3.2	51	11.2	10.1	25	6.7	17.1	35	9.8	
3.3	53	11.6	10.2	24	6.5	17.2	40	10.8	
3.4	57	12.4	10.3	24	6.5	17.3	35	9.8	
3.5	70	15.1	10.4	23	6.3	17.4	35	9.8	
3.6	67	14.5	10.5	22	6.1	17.5	37	10.2	
3.7	54	11.8	10.6	25	6.7	17.6	39	10.6	
3.8	53	11.6	10.7	25	6.7	17.7	39	10.6	
3.9	44	9.7	10.8	25	6.7	17.8	35	9.8	
4.0	47	10.5	10.9	24	6.5	17.9	37	10.2	
4.1	50	11.1	11.0	25	6.9	18.0	36	10.1	
4.2	44	9.8	11.1	24	6.6	18.1	37	10.3	
4.3	44	9.8	11.2	24	6.6	18.2	35	9.9	
4.4	43	9.6	11.3	24	6.6	18.3	34	9.7	
4.5	42	9.4	11.4	26	7.1	18.4	38	10.5	
4.6	41	9.2	11.5	26	7.1	18.5	38	10.5	
4.7	36	8.2	11.6	29	7.7	18.6	37	10.3	
4.8	34	7.8	11.7	28	7.5	18.7	39	10.7	
4.9	37	8.4	11.8	27	7.3	18.8	41	11.2	
5.0	43	9.8	11.9	27	7.3	18.9	38	10.5	
5.1	40	9.1	12.0	27	7.4	19.0	38	10.7	
5.2	42	9.6	12.1	27	7.4	19.1	38	10.7	
5.3	44	10.0	12.2	27	7.4	19.2	39	10.9	
5.4	40	9.1	12.3	27	7.4	19.3	38	10.7	
5.5	35	8.1	12.4	27	7.4	19.4	37	10.5	
5.6	35	8.1	12.5	30	8.0	19.5	39	10.9	
5.7	35	8.1	12.6	30	8.0	19.6	40	11.1	
5.8	32	7.5	12.7	29	7.8	19.7	43	11.7	
5.9	30	7.1	12.8	25	7.0	19.8	37	10.5	
6.0	30	7.2	12.9	25	7.0	19.9	38	10.7	
6.1	29	7.0	13.0	28	7.8	20.0	40	11.2	
6.2	25	6.2	13.1	28	7.8	20.1	43	11.8	
6.3	25	6.2	13.2	28	7.8	20.2	42	11.6	
6.4	25	6.2	13.3	28	7.8	20.3	43	11.8	
6.5	25	6.2	13.4	30	8.2	20.4	43	11.8	
6.6	27	6.6	13.5	30	8.2	20.5	43	11.8	
6.7	24	6.0	13.6	30	8.2	20.6	44	12.0	
6.8	27	6.6	13.7	27	7.5	20.7	44	12.0	
6.9	27	6.6	13.8	28	7.8	20.8	42	11.6	
			13.9	26	7.3	20.9	39	11.0	

			2 t Ring		
21.0	40	11.4	27.1	33	32.0
21.1	43	12.0	27.2	30	29.5
21.2	43	12.0	27.3	25	25.2
21.3	44	12.2	27.4	22	22.6
21.4	44	12.2	27.5	24	24.3
21.5	40	11.4	27.6	25	25.2
21.6	39	11.1	27.7	26	26.0
21.7	39	11.1	27.8	29	28.6
21.8	43	12.0	27.9	33	32.0
21.9	55	14.5	28.0	50	46.7
22.0	65	16.7	28.1	53	49.2
22.1	58	15.2	28.2	41	39.0
22.2	62	16.1	28.3	38	36.4
22.3	59	15.4	28.4	56	51.8
22.4	60	15.7	28.5	43	40.7
22.5	51	13.8	28.6	55	50.9
22.6	41	11.7	28.7	50	46.7
22.7	48	13.2	28.8	47	44.1
22.8	51	13.8	28.9	51	47.5
22.9	56	14.8	29.0	52	48.5
23.0	72	18.3			
23.1	81	20.2			
23.2	93	22.7			
23.3	87	21.4			
23.4	95	23.1			
23.5	88	21.6			
23.6	110	26.2			
23.7	133	31.0			
23.8	147	33.9			
23.9	158	36.2			
24.0	166	38.0			
24.1	168	38.4			
24.2	155	35.7			
24.3	150	34.6			
24.4	152	35.1			
24.5	158	36.3			
24.6	145	33.6			
24.7	173	39.4			
24.8	191	43.2			
24.9	192	43.4			
25.0	157	36.2			
25.1	145	33.7			
25.2	131	30.8			
25.3	123	29.2			
25.4	137	32.1			
25.5	145	33.7			
25.6	143	33.3			
25.7	153	35.4			
25.8	137	32.1			
25.9	130	30.6			
26.0	126	29.9			
26.1	130	30.8			
26.2	130	30.8			
26.3	127	30.1			
26.4	110	26.6			
26.5	109	26.4			
26.6	120	28.7			
26.7	115	27.6			
26.8	125	29.7			
26.9	127	30.1			
27.0	200	45.5			



21.0	21.0	21.0	21.0
21.1	21.1	21.1	21.1
21.2	21.2	21.2	21.2
21.3	21.3	21.3	21.3
21.4	21.4	21.4	21.4
21.5	21.5	21.5	21.5
21.6	21.6	21.6	21.6
21.7	21.7	21.7	21.7
21.8	21.8	21.8	21.8
21.9	21.9	21.9	21.9
22.0	22.0	22.0	22.0
22.1	22.1	22.1	22.1
22.2	22.2	22.2	22.2
22.3	22.3	22.3	22.3
22.4	22.4	22.4	22.4
22.5	22.5	22.5	22.5
22.6	22.6	22.6	22.6
22.7	22.7	22.7	22.7
22.8	22.8	22.8	22.8
22.9	22.9	22.9	22.9
23.0	23.0	23.0	23.0
23.1	23.1	23.1	23.1
23.2	23.2	23.2	23.2
23.3	23.3	23.3	23.3
23.4	23.4	23.4	23.4
23.5	23.5	23.5	23.5
23.6	23.6	23.6	23.6
23.7	23.7	23.7	23.7
23.8	23.8	23.8	23.8
23.9	23.9	23.9	23.9
24.0	24.0	24.0	24.0
24.1	24.1	24.1	24.1
24.2	24.2	24.2	24.2
24.3	24.3	24.3	24.3
24.4	24.4	24.4	24.4
24.5	24.5	24.5	24.5
24.6	24.6	24.6	24.6
24.7	24.7	24.7	24.7
24.8	24.8	24.8	24.8
24.9	24.9	24.9	24.9
25.0	25.0	25.0	25.0

