# APPENDICES

Residential	
First 100 kwh	🕈 0.575 per kwh
Next 100 kwh	.585 per kwh
Excess kwh	.590 per kwh

#### Commercial

Classification

X-1	First 150 kwh	∲0.575 per kwh
(Conn. Load: 1-5,000	Next 150 kwh	.590 per kwh
watts)	Next 300 kwh	.600 per kwh
	Excess kwh	.610 per kwh
X-2	First 600 kwh	₽0.575 per kwh
(Conn.load: over 5,000	Next 600 kwh	.590 per kwh
watts)	Next 1200 kwh	.600 per kwh
	Excess kwh	.610 per kwh

#### Industrial

678 1

Demand charge		¥10.00 per kwh
Plus Energy charge	First 200 hrs.	.550 per kwh
	Next 200 hrs.	.530 per kwh
	Excess hrs.	.510 per kwh

## Street light rates

125 w	atts Mercury	lamp	₽24.00	per	month
250 w	atts Mercury	iamp	48.00	per	month
400 w	atts Mercury	lamp	73.80	per	month

#### APPENDIX 4.2.1 DISCHARGE RATE OF THE EXISTING PUMP

The discharge rate of the pump was measured by means of potable flow meter covering fifteen existing pumping stations.

The time period for measurement was arranged in accordance with operation schedule for each pump since most pumps are being operated within the limited hours from the economical viewpoint. With regard to the situation of pump operation, measurement was conducted for a period of one hour for a majority of the pumps. However, the discharge rate at the four pumping stations (No. 2, No. 4, No. 5 and No.16) were measured through the day. Two of these pumping stations (No. 2 and No. 4) are being operated through the day. Other two pumping stations were considered for one day measurement to analyze the influence by the former two pumping stations, especially during the period when the pumps stop operating.

#### Implementation Schedule

The implementation schedule was made in consideration of the available set of potable flow meter (3 sets) and associated with other surveys. TABLE 4.2.1. 1 shows overall schedule for this survey.

M.

Date	No. of P.S.	Measurement Time		<u>R</u> .
June 18	No. 12	9:30 10:30		
· · · ·	15	9:40 10:40		
	11	11:25 12:25	· .	
	7	11:35 12:35		
	8	14:05 15:05		
	14	14:10 15:10		
		:		

TABLE 4.2.1.1 IMPLEMENTATION SCHEDULE

-2--

Date	No.of _P.S.	Measurement Time	R.M.
June 19	No. 6	8:45 9:45	
	3	8:50 9:50	
	16	10:30 11:30	No. 15 PS was repaired after measurement
	1	10:45 11:45	
	4	14:20 15:20	
	10	14:30 15:30	
	9	16:20 17:20	
June 26	4	16:00 16:00	
27	2	22:00 22:00	
July 26	5	18:00 18:00	
27	16	19:00 19:00	

Measurement Result

Measurement results for the four pumping stations are shown

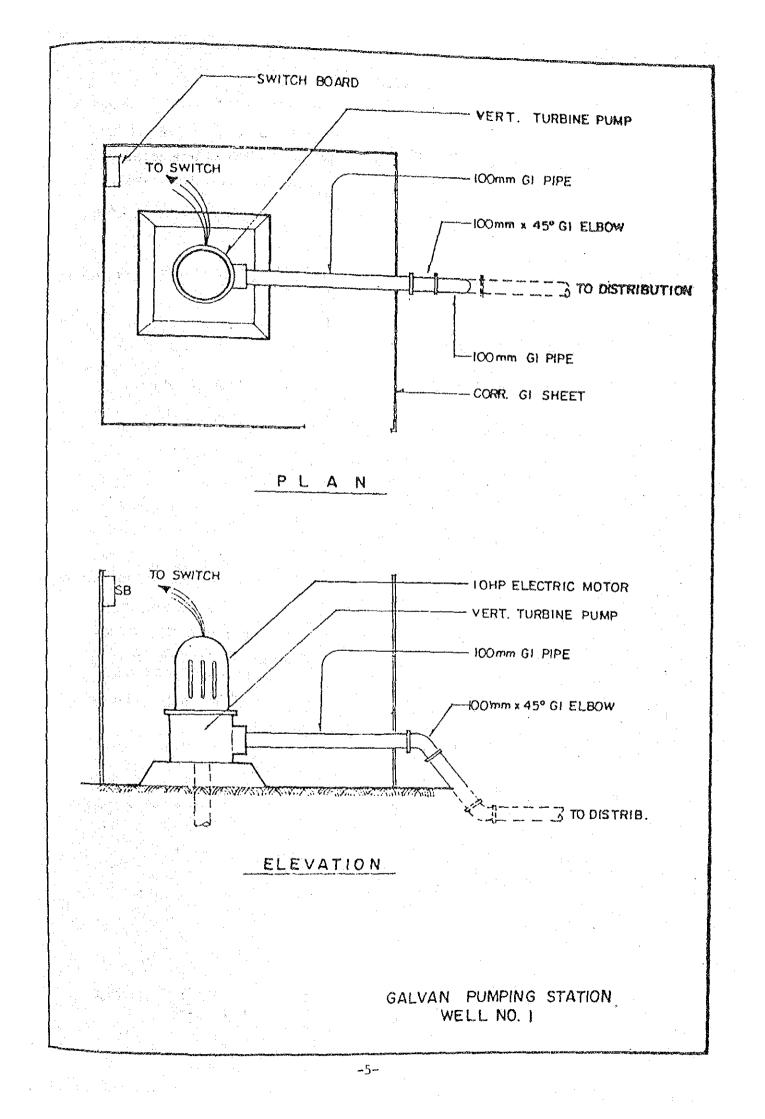
in TABLE 4.2.1.2. Regarding the results of the four pumping stations, the fluctuation of hourly discharge rates is less than 5 percent to the average figure.

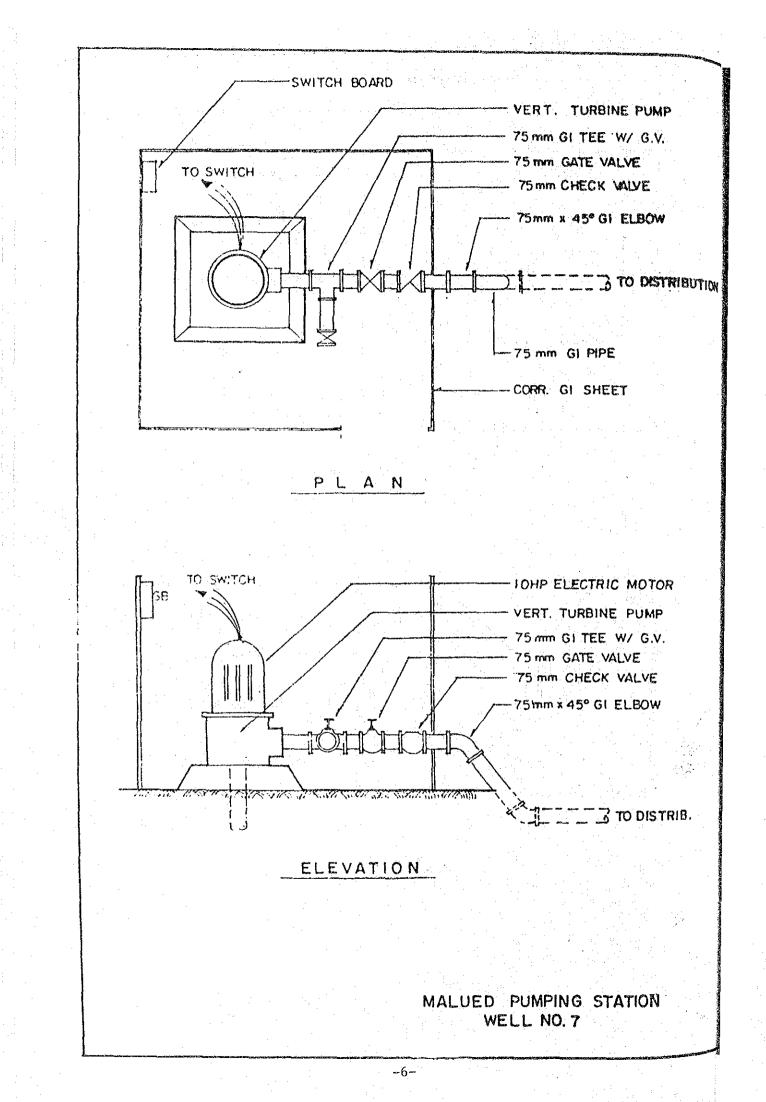
TABLE 4.2.1.2

ONE DAY MEASUREMENT RESULT AT THE FOUR PUMPING STATIONS

Pumping					
Station	n No.2 (cu.m/hr)	No. 4 (cu.m/hr)	No. 5 $(cu.m/hr)$	No. 16 (cu.m/hr)	Remarks
0 - 1	63	62	0	0	
1 - 2	62	62	0	0	
2 - 3	64	62	0	0	
3 - 4	64	63	0	0	
4 - 5	63	64	Ū	0	
5 - 6	60	64	0	0	
67	59	64	20	0	
7 - 8	61	64	20	38	
8 - 9	62	64	20	40	
9 - 10	61	64	20	41	
10 - 11	62	62	19	40	
11 - 12	62	64	20	41	
12 - 13	-	÷	20	41	
13 - 14	_		20		o. 2 & No.
14 - 15	<del>.</del>	· · · · · · · · · · · · · · · · · · ·	19	39	Brownout
15 - 16		-	19	39	
16 - 17	63	65	19	39	
17 - 18	61	65	19	39	
18 - 19	60	65	19	39	per le l'est
19 - 20	61	64	19	40	
20 - 21	61	64	19	39	
21 - 22	62	62	19	41	
22 - 23	62	61	.0	0	
23 - 24	64	62	0	0	
ourly Average	Rate				
(cu.m/hr)	62	63	19	40	
aily Dicharge					
(cu.m/hr)	1,488	1,512	456	960	
· · · · · · · · · · · · · · · · · · ·					
· · · · · · · · ·				•	
				(1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,1,	1
		÷			

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#### APPENDIX 4.2.2 PUMP EFFICIENCY TEST

The required condition in conducting pump efficiency testing are given below:

 There is an existing functioning gate valve, sounding hole and pressure gauge located properly at the pump station.

(2) There is a proper and convenient place to install the portable flow meter.

Voltage, electric current and discharge rate measurement should be made several times depending on the water pressure variation.

Selection of pump station for pump testing

During the survey, the existing facilities, of the pump stations were investigated, especially the existence of functioning gate valve, pressure gauge and sounding hole. All the pump stations had no pressure gauges and sounding holes. Out of the fifteen (15) pump stations, No. 10 located along Arellano St. has a record on pumping water level. TABLE 4.2.2.1 shows the collected information.

Pump station No. 10 was selected for this test in the light of the aforementioned requirements. However, a hole was drilled to install the pressure gauge. The reliable data about the pumping water level provided by the DAWASA engineers was also utilized.

Field measurement

Variations of water pressure and discharge rate were measured at the different opening ratio of the gate valve. TABLE 4.2.2.2 shows the test data obtained at pump station No. 10. TABLE 4.2.2.1 INFORMATION ASSOCIATED WITH THE REGUTREMENTS FOR THE TEST

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		·											 	•									
Remarks			Gate Value not	functioning Care Value act	functioning	Gate Value not	Tuncelouing		Late value no nangte					and the first state	bard value no		abandoned in 1983			Care value no handle	غميتميد	handle	
Pump* Setting	(B)	15.24	21.34	27 26	; ;	30.49	1	0	10.29	18.29	15.24	15.24	15.24		****	27.44	١	24.3		27.54	30.49		
P.M.	Ê	1	9.15	2		h8.29	ı 		۱ 	· 1	1 · :	ا ا	10.7	0 	0	1	1	1	, ,	р. С.	18-9		
Sounding	Hole	No	.=	. 4		• •	÷.	:		:	=	- <b>=</b>	: =		. '	:		No		•	=		
61 11	- ange	No	:	 :	•••••	 -	=			:	=					=	1	No			:		
Gare P	value Gauge	No	Yes	20 20 20		Yes	Yes		res 1	Yes	Yes	Yes	Yes		2	Yes	.1	Yes		Yes.	Yes		
Operation Status C	4 :00AM-	10:00PM	(IS hrs.) 24 hrs	MHC 1-M00-7	(20 hrs)	24 hrs	4:00AM-10PM	(18 hrs)	4:UUAM-IURN	4:00AM-10PM	4:00AM-10PM	(18 hrs) 4:00AM-10PM	(18 hrs) 4:00AM-10PM	(18 hrs) (18 hrs)	(18 hrs)	4:00AM-10PM	(18 hrs) 	M401-MA00: 4	(18 hrs)	4:00AM-10PM	4:00AH -	8:00PM (16 hrs)	
Year Pump		NON	=	1952	4	ADA	1960	01.0	77/0	1967	1974	1974	17 21		7367	1973	· · ·	1970	1	1677	1980		
Consc. Well		VDN	:	1952		NDA	1960	0404	0/67	1967	1974	1974	161		7167	1973	7076	1970		1977	1980		
Pump Cap.(CMD)		540	1370	1 370	2	1320	540	000,	nƙny	540	540	540	540	610	2	540	1	540		540	1320		
Type of Pump	Turbine	Pump	<b>.</b>	 2		:	5	:		=			:	=	-	1	:	=	:,		•		
Location	Galvan St. Turbine	:	In front of	City Hall	· · · · · · · · · · · · · · · · · · ·	A.B.F east	Burgos St.	, , ,	rerez sr.	Bgy Malued	Noble St.	Caranglaan	Avelland Sr		diser - 1981	Amado St.		Noble St.		88y. Malued	A.B.F West		
P.S. No.			r1	~~~~~~ (**		4	Ś		0	~	80	5	01			12		1 7	1	57	16		

\* - Data provided by the NAWASA. NDA - No data available

:	TABL	E 4.2	.2.2		
TEST	DATA ON	PUMP ST	ATION	No. 10	
	DAGUP/	N CITY,	PANGA	SINAN	

	STEP	(LPS)		PWL (m)	TDH - (m)	V AVE. (Volts)	I AVE. (Amp.)		, 2/		<u>3</u> /	Overal14/		BHP <u>6</u> /
					<u>-</u>			HP	кW	НP	KW	Eff(%)	(%)	(Hp)
÷	- 1	7.72	6.1	10.7	17.8	220	20.3	1.8	1.34	6.6	4.9	27.3	32.1	5.6
	2	7.70	6.5	10.7	18.2	225	20	1.84	1.37	6.6	4.9	27.9	32.8	5.6
ł	3	7.65	6.8	10.7	18.5	225	20	1.86	1 39	6.6	4.9	28.2	33.2	5.6
	4	7.61	7.7	10.7	19.4	225	20	1.94	145	6.6	4.9	29.4	34.6	5.6
÷	S	7.58	7.95	10.7	19.7	221	20.5	196	1 46	7.7	5.0	29.3	34.5	5.7
	6	7.51	8.4	10.7	20.1	221.7	19.5	1 98	1 48	6.4	4.8	30.9	36.4	5.4
	7	7.50	8.8	10.7	20.5	223	19.0	2.02	1.50	6.2	4.6	32.6	38.4	5.3
÷	8	7.45	9.2	10.7	20.9	222.7	18.5	2.05	1.53	6.1	4.6	33.6	39.5	5.2
	9	7.37	9.9	10.7	21.6	221	18.5	2.09	1.56	6.0	4.5	34.8	40.9	5.1
s.	10	7.32	10.2	10.7	21.9	221	18.0	2.11	1.57	5.9	4 4	35.8	42.1	5.0
:	11	6.25	13.0	10.7	24.7	220	18.0	2.03	1.51	5.8	4.3	35.0	41.2	4.9
	12	5.68	13.5	10.7	25.2	218.5	18.0	1.89	141	5.8	4.3	32.6	38.4	4.9
		L	<u> </u>			·				1				

1/	TDH	a .	Pd + Ps (PWL) + hf, WHERE hi is ASSUMED 1.0 m
2/	WHP	<b>3</b> 9	(Q x TDH) / 76.1
3/	IHP	<b>n</b> .	(VAVE x I AVE x 3 x P.F)/1000 ; ASSUMED P.F. = 0.85
<u>4</u> /	OVERALL EFF		(WHP x 100) / IHP
5/	PUMP EFF		OVERALL Eff ; ASSUMED MOTOR Eff = 0.85
<u>6</u> /	BHP	R	WHP / PUMP eff = INP × MOTOR Eff.

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APPENDIX 4.2.3 WATER PRESSURE IN THE SERVICE AREA

Variations in pressures at strategic points in the distribution system and in the pump stations were monitored on a 24-hour basis utilizing automatic pressure recorders and pressure gauges.

The following approach was employed to achieve the purpose of this pressure survey.

- A. Preparatory Work
  - Preliminary survey and discussion with the waterworks personnel to pinpoint the proposed pressure test points.
  - (2) Made some posters/placards informing the public regarding the on-going pressure survey.
  - (3) Hired some personnel/recorders for this survey.
- B. Implementation of the Survey
  - Briefing of the hired personnel/recorders regarding this pressure survey.
  - (2) Brought the personnel/recorders to their designated area.
  - (3) Field measurement itself.

The following were considered in selecting the test points:

a) All the existing pump stations should be included in this survey.b) The total number of test points should be around thirty (30).

The test point locations are shown in FIGURE 4.2.3.1. TABLE 4.2.3.1 shows the 24-hour pressure recordings.

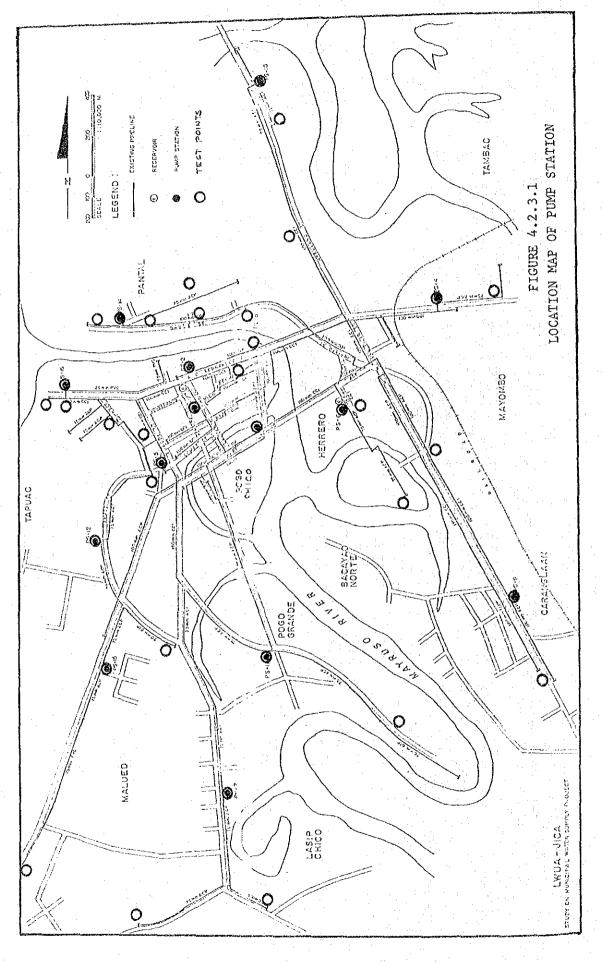
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### TABLE 4.2.3.1

· · ·			, *				
14. 14.							
				Pressure	Consumer	Dian	neter
		Location	Recorded	Range <sub>2</sub> (kg/cm <sup>2</sup> )	Туре		nnection
	No.	Pocacton	Vecordea		TADE	Within press doctrine and	
pump	1	Galvan St.	6-29-86	0.70-0.99	**		was installed
Station	2	Infront of City	6-29-86	1,22-1,33		on the	discharge pipe
11		Hall I					
u .	3	Rizal St.	6-28-86	0.25-0.49			ţi.
u	4	A.B.F. East		0.92-0.99			11
บ	5	Burgos St.	6-23-86	0.17-0.42			13
<b>D</b> 22	6	Perez St. (Mkt.)	6∽30~86	0.07-0.42	-		<b>11</b>
ji -	7.	Dag-Malved Rd.	6-27-36	0.25-0.63	<b></b>		11
9 <b>1</b>	8	Nable St.	6-28-36	0.32-0.63	-		H
<b>11</b> .	: <b>9</b>	Cuanglaan	6-29-36	0.50-0.92			11
1 <b>n</b> - 1 1 1	10	Arellano St.	6-29-86	0.63-1.0	· •		11
11 · .	11	Pogo Grande	6-27-86	0.14-0.35			- 11
<b>D</b> .	12	Amado St.	6-31-86	0.21-0.53			11
\$1	14	Nable St.	6-26-86	0.70-1.02	-		**
10 <sup>1</sup> 1	15	Dag-Binmaley Rd.	6-27-86	0.42-0.77	<b>6</b>		11
U II	16	A.B.F. East	6-28-86	1.12-1.48	. <b>vi</b> ş		3 P
Service	1	Back of Rosita	the same the				
Area	·	Mktg.	7-4-86	0.04-0.35	Public	·	<u> </u>
11	2	Fernandez St.	7-4-86	0 -0.28	Faucet		
41	3	Lasip Grande			· · ·	· ·	$\Phi_{ij} = -\frac{1}{2} e^{i \Phi_{ij}}$
· .		Elem. Sch.	7-1-86	0 -0.21	Institut	ional	¥"
11	4	Amado St.	7-2-86	0 -0.28	Public F	aucet	1.5
i) .	5	A.B.F. West Ext.	7-2-86	1.06-1.06	. 11		3/4"
U I	6	Cueenan St.	7-4-86	0.28-0.69			1 11
,n	.7	Bonifacio St.	6-27-86	0.07-0.32	11		4"
11	.8	Nable St.	6-28-86	0.07-0.63	n		3/4"
<i>u</i> 1	9	Nable St.	6-26-86	0.63-1.06	11		3/4"
<b>\$</b> 3-	10		6-27-86	0.46-0.99	<b>t</b> 1		3/4"
11	11	Avellano St.	7-03-86	0.04-0.35	н		3/4"
13	12	Avellano St.	6-26-86	0.30-1.0	17	:	λ <sup>11</sup>
at State	13	Along Nat'l. Hi-way		0.07-0.56	11		<u>j</u> n
5.9 H	14	Perez St. (Mkt.)	7-03-86	0.11-0.60	n	÷	12" 12"
	15	Pantal St.	6-26-86	0.4 -1.2	Domestic		1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1
		A.B.F. West	6-26-86	0.5 -1.2	Public F		1.5 H
н	16		6-26-86	0 -0.7	Domestic		1. 10
6 (f)	17	Caranglaan North	6-26-86	0 -0.4	Domestic		1211
<b>1</b> 1	18	Bgy, Lucao.	7-31-86	0,18-0,56	Domestic		2 ** 2 **
n, - 141	19	Lucao	6-26-86	1.5 -2.2	Commerci		3/4"
19	20	A.B.F. East		0.3 -1.0	Public F		5"
11	21	Arellano St.	6-26-86	· · · ·			12 12 17
H B	22	Lasip Grande	7-31-86	0 -0.07 1.0 -2.2	Commerica		2 .
i i i i i i i i i i i i i i i i i i i	23	A. B.F. East	6-26-86	1.0 -2.2	Jonanet 200		

24-HOUR PRESSURE RECORDING IN THE DISTRIBUTION SYSTEM

-11-



-12-

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NELL INVENTORY	Static Casing Water Dia Tovel	4.	•	150	50/200		tin.		051	100	1.2			100 0.6		5.8	;;; ;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;		125 6.1		100/63 2.4 350/200: FF:			50 8.5		0110 B 3		150 6.5		150 3.5	:.		
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	Poblacion East Calasia Buenlaç, Calasiao San Miguel, Calasiao Balani, Calasiao Balani, Calasiao San Miguel, Calasiao San Miguel, Calasiao San Miguel, Calasiao San Miguel, Calasiao Bued, Calasiao Bued, Calasiao Bued, Calasiao Calasiao Bolosan, Dagupan City Bolosan, Dagupan City Bolosan, Dagupan City Bolosan, Calasiao Cabilocan, Catatpang, D. Bonoan Gueset, Dagupa	Bonoan Gueset, Dagup Bonoan Boquig, Dagup Bonoan Boquig, Dagup Bonoan Boquig, Dagup Dagupan City Poblacion, Mangaldan Gueguelonen, Mangald Embarcadero, Mangald Angio, San Fabian Anoiang, San Fabian Anoiang, San Fabian Macayos, San Jacinto Macayos, San Jacinto Macayos, San Jacinto San Cathos City Fagal, San Carlos Ci	Bolingit, San Carl Malabago, Calasiao Malabago, Calasiao
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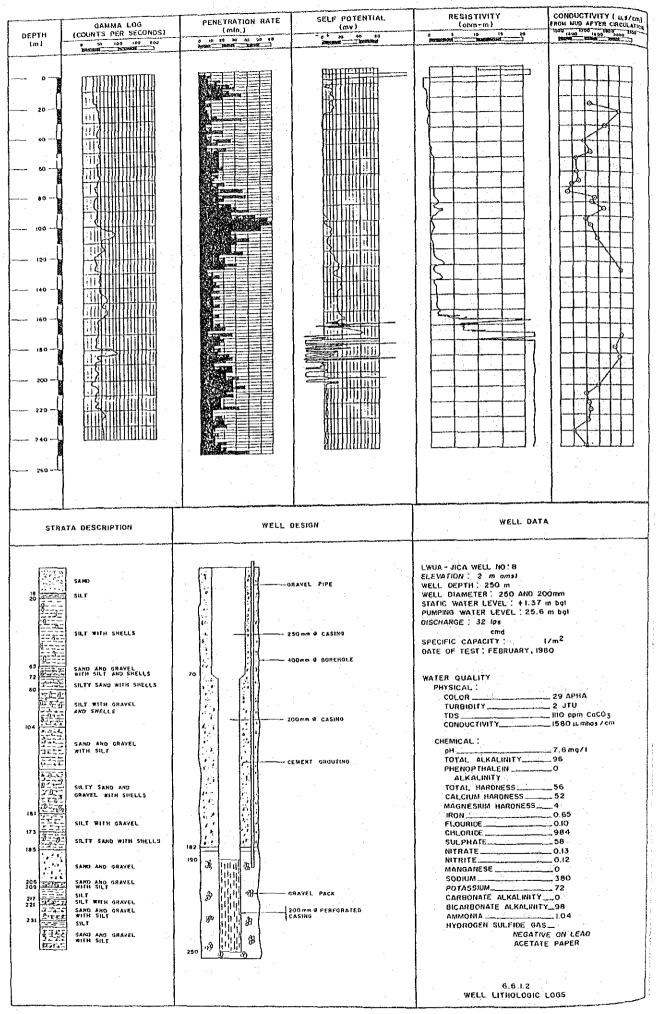
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CL-S 19003 43-60-81 8089 67-48 67-41 18974 18974 20702 20702	
-15-	

LWUA - JICA WELL NO.: 4 OWNER'S NO.: 6508 GROUND ELEVATION: BALANCOBONG, LINGAYEN GROUND ELEVATION:	176 m 176 m 59 - 350 mm	LEVEL: FF	0174 : 4	STRATA	FILE SAND			BLUE STICKY		VELLOW SAND	BLUE STICKY		BOULDER		BLUE STICKY				BLUE FINE		WELL LITHOLOGIC LOGS
LWUA - JICA WELL OWNER'S NO. 55 LOCATION: BALANG GROUND ELEVATIO	WELL DEPTH : 176 m CASING DEPTH : 176 m CASING DIAMETER : 350 mm	CASING DIAMELER, 130 mm STATIC WATER LEVEL: FF DISCHARGE :	SPECIFIC CAPACITY : TRANSMISSIVITY :	TH WELL DESIGN	<u> </u>										<b>_</b>					]	
3836	300 200	550	51	DEPTH (m)			\$0		<b>6</b>	°,		e B	ĝ		3	140		160			
LWUA - JICA WELL NO.3 OWNER'S NO. ; 44631 GROUND ELEVATION ; PUGALLON	WELL DEPTH : 52 m CASING DEPTH : 13/39 m CASING DIAMETED : 15/112 mm	CASING DIAMELER : 1307-112 MM STATIC WATER LEVEL : 2,5 m bg1 DISCHARGE : 1,6 Lps	Y : 0.74 lps/m	STRATA DESCRIPTION	BROWN CLAY	SANDY CLAY	OUICKSAND	BLUE CLAY	BLUE STICKY		COCK SAND ROCK	ZTTT SAND SAND AND GRAVEL							- 		
A WELL VO. 44 POBL/ EVATIO	TH : 5 EPTH : Meteo	MELER LER LE	SIVITY	WELL DESIGN			· .														
LWUA - JICA WELL NO.:3 OWNER'S NO. : 44691 LOCATION : POBLACION, GROUND ELEVATION :	LL DEP SING DE SING DE	TIC WA	SPECIFIC CAPACITY	L									-1	·						<u> </u>	
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1010	302	302	ີ່ຫຼີ  	OEPTH		<u>-</u>		50		A	4	50 50							<u> </u>		
	44 m 4.5/138.2 m : 350 / 200 mm		Y . 2,65 ps/m	DESCRIPTION DEP		AND GRAY SAND, PUMICE		GRAY SILT AND CLAY / SHELLS 200	SAND WITH CLAY CAT SILT AND CLAY WITH SOME TO CLAY WITH SOME	SHELLS GRAY GRAVEL		A SAND AND SILT, SAND AND SILT, SOME CLAFEYSANDY FAT, LAYERS, PUMICE SC	SAND	THE SANCEL SILT	CLAYEL CLAY	SAND, SILT, GRAVEL	AND SRLT	CAVEL WITH SOME	SANDY GRAVEL		AND SILT
WELL NO. 2 CL_14 ACABAC, BUGALLON ATION:1.4 W GMSI	44 m 4.5/138.2 m : 350 / 200 mm		Y . 2,65 ps/m	N DESCRIPTION						SHELLS GRAY GRAVEL	GRAY TO GREEN	·,	GRAY GRAVEL GRAY GRAVEL SLT, SAND	जना ए	T TIME	SAND, SILT, GRAVEL	SANOY SILT		HANDY GRAVEL		
FLL NO. 2 CL-14 KCABAC, BUGALLON KTON:1.4 m gmsi			if ic , cafacit Y ; 2,65 lps/m SMISSIVITY ;	STRATA DESCRIPTION						SHELLS	GRAY TO GREEN	·,	GRAY GRAVEL GRAY GRAVEL SLT, SAND	जना ए	T TIME		1804		220 U SRAVEL		
WELL NO. 2 CL_14 ACABAC, BUGALLON ATION:1.4 W GMSI	44 m 4.5/138.2 m : 350 / 200 mm		if ic , cafacit Y ; 2,65 lps/m SMISSIVITY ;	WELL STRATA DESIGN DESCRIPTION	BROWN TO GRAY	The start of the s		GRAY SILT AND CLAY / SHELLS	SAND WITH CLAY	SHELLS	CAN TO GREEN	Solie CLAREY/SANDY CLARES, PUMICE	مراجعت المراجع ال مراجع المراجع ال		000						
LWUA - JICA WELL NO.: 2 DWDRR'S NO.: CL - 14 OWNER'S NO.: CL - 14 CCATION : BUGALLON GROUND ELEVATION : 1,4 m gms1	WELL DEPTH : 244 m CASING DEPTH : 44,5/ 198,2 m CASING DIAMETER : 350 / 200 mm	STATIC WATER LEVEL: DISCHARGE : 56.8 1ps	SPECIFIC CATACITY 2.65 IDS/M TRANSMISSIVITY: 2.65 IDS/M	WELL STRATA DESIGN DESCRIPTION	AND BROWN TO GRAY	The start of the s		GRAY SILT AND CLAY / SHELLS	SAND WITH CLAY	SHELLS	60 C C C C C C C C C C C C C C C C C C C	Solie CLAREY/SANDY CLARES, PUMICE	مراجعت المراجع ال مراجع المراجع ال		000						
LWUA - JICA WELL NO.: 2 DWDRR'S NO.: CL - 14 OWNER'S NO.: CL - 14 CCATION : BUGALLON GROUND ELEVATION : 1,4 m gms1	WELL DEPTH : 244 m CASING DEPTH : 44,5/ 198,2 m CASING DIAMETER : 350 / 200 mm	STATIC WATER LEVEL: DISCHARGE : 56.8 1ps	SPECIFIC CATACITY 2.65 IDS/M TRANSMISSIVITY: 2.65 IDS/M	DEPTH WELL STRATA (m) DESIGN DESCRIPTION	BROWN TO GRAY	20 20 20 20 20 20 20 20 20 20 20 20 20 2		40 GRAY SILL AND CLAY / SHELLS	60 CONTRACTOR STAND WITH CLAY	STRELLS	60 C C C C C C C C C C C C C C C C C C C	BLUE SAND WITH GRAVEL 100 1 SOME CLAREY SANDY WITH GRAVEL LATERS, PUMICE	مراجعت المراجع ال مراجع المراجع ال		000						
LWUA - JICA WELL NO.: 2 DWDRR'S NO.: CL - 14 OWNER'S NO.: CL - 14 CCATION : BUGALLON GROUND ELEVATION : 1,4 m gms1	44 m 4.5/138.2 m : 350 / 200 mm	STATIC WATER LEVEL: DISCHARGE : 56.8 1ps	STEC CAPACITY : STECIFIC CAPACITY : 2.65 Ips/m VSNISSIVITY : VSNISSIVITY :	DESCRIPTION DESIGN DESCRIPTION	BROWN TO GRAY	20 20 20 20 20 20 20 20 20 20 20 20 20 2		AOH CLUE FINE SAND 40 H	60 CONTRACTOR STAND WITH CLAY	STRELLS	Carl Carl Carl Carl Carl Carl Carl Carl	BLUE SAND WITH GRAVEL 100 1 SOME CLAREY SANDY WITH GRAVEL LATERS, PUMICE	مراجعت المراجع ال مراجع المراجع ال		000						

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LL NO. 12 1832 18100, BINMALEY ATION 177 m 177 m LEVEL : LEVEL : CITY :	STRATA DESCRIPTION	C 2 3 4 5 5 6 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	SANDY CLAY	BLUE CLAY	KARD BLUE CLAY	BLUE CLAY	CLAY TURF NOCK TURF WITH CLAY TURE WITH CLAY LINESTONE LINESTONE	স্যা	.2 Igic Logs
- JICA WE R'S NO TICN: SAN. ND ELEVIN DEPTH JG DIAME G DIAME C WATER ARGE FFIC CAPA	DEPTH WELL (m) DESIGN	0 7	0 9 4	C C U c		Q N	0 0 7 9		6.6.1.2 WELL LITHOLOGIC
10 AN, BINMALEY Omm 00 mm 1.2 m bgl 0.18 lps/m	DESCRIPTION	OUICKSAND BLUE SANDY CLAY	BLUE STICKY CLAF STICKY CLAF SAND B GRAVEL FLUOW STICKY CLAY		BLUE STICKY CLAY VV BLUE TUFF BLUE SAND	ELUE SANDY	BLCC R R R R R R R R R R R R R R R R R R	SAND AND GRAVEL	
1 623 200250	DEPTH WELL (m) DESIGN	C ~	9 • •	0 C		<u>S</u>	6 0 0 0 0 0		
NO : 9 62-33 GUEL, LINGAYEN M 199 m 199 m 7 : 100 mm VEL : VEL :	STRATA DESCRIPTION	BLUE CLAY	SANDY CLAY BUUE CLAY BUUE CLAY SANDY CLAY YELLOW SANDY CLAY		BUUE CLAY BUUE CLAY SAND BUUE CLAY BUUE CLAY	SANDY CLAY SAND SAND	BLUE STONY BLUE CLAY FINE SAND FINE SAND CLAY FUE STOCK	SAND AND GRAVEL	
	DEPTH WELL (m) DESIGN	On Co N	4 n 0 0 111111	e e e e e e e e e e e e e e e e e e e	147561 F2004 0 0 C 7 C 7	0 0 0 5 7	Son Maria O O O	8	
So mm So mm	STRATA DESCRIPTION	SAND BLUE CLAY		BUUE	TUF FACEDUS CLAY	CLAY	BLUE SAND BLUE SANDY CLAY BLUE SANDY CLAY		
1 1 1 1 2 3 2 0 7 4 0 L	DEPTH WELL (m) DESIGN		Q Q Q	2 2 2	100 220 22	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 8 8		

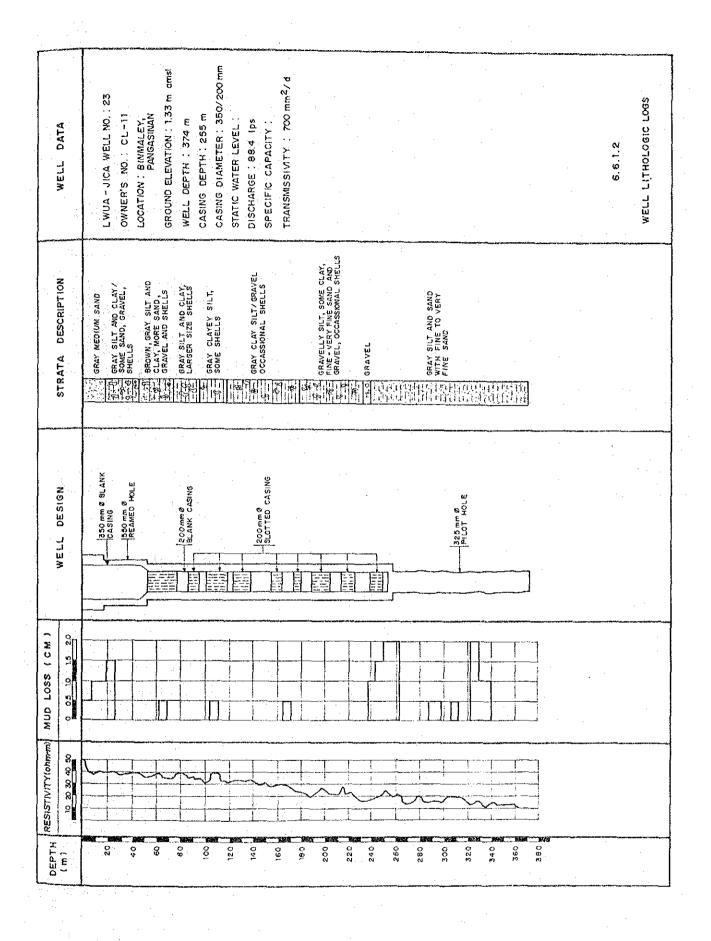
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OWNER'S NO. 7831 OWNER'S NO. 7831 LCCATION: CALOOCAN SUR, BINMALEY GROUND ELEVATION : WELL DEPTH : 258 m CASING DEPTH : CASING DIAMETER : STATIC WATER LEVEL : DISCHARGE : SPECIFIC CAPACITY : TRANSNISSIVITY :	DESCRIPTION	SAND		CLAY		CLAY	SAND CLAY SAND	CLAY	SAND	CLAY SAND	CLAY	SAND					6.6.1.2 LITHOLOGIC LOGS
CUMPA- SICA WELL NU CONTER'S NO : 7831 LOCATION : CALOOCAN RELL DEPTH : 258 m VELL DEPTH : 258 m CASING DEPTH : CASING DEPTH : CASING DIAMETER : STATIC WATER LEVEL DISCHARGE : SPECIFIC CAPACITY : TRANSMISSIVITY :	DEPTH WELL	<b>882 0</b> 8	ę	s S	 6	8	00 02 02 02	S S	ě	500 500 500 500 500 500 500 500 500 500	2 6 0 7 8 8	260					אברר רעאט 9 9
Say Seaso ON: 17 m 114 m R 100 mm EVEL: 1.2 m bgt 5 tps TTY :	STRATA DESCRIPTION	FIRE SAND	CORCASAND CANNY CLAY	BUE STORY CLAY	SAND BILLE STICKY CLAY	XELLOW	TUFFACEOUS CLAY	TUFFACEOUS CLAY		CLAY SAND	CLAT SAND AND GRAVEL						
CONTENT AND WELL NO. 10 OWNER'S NO. 12639 LOCATION: LINOC WEST, BINMALEY GROUND ELEVATION: WELL DEPTH : 117 m CASING DEPTH : 114 m CASING DEAMETER : 100 mm STATIC WATER LEVEL: 12 m bg1 DISCHARGE : 0, 95 1ps SPECIFIC CAPACITY : TRANSMISSIVITY :	DEPTH WELL		50		4 D			2000 00 80		00	120						
e voorte Bunmaley m EL: 2.1 m bgi bs 0.02 ips/m	DESCRIPTION	FINE SAND	SAND	FINE SAND	FINE SAND AND BROWN SANDY CLAY	BROWN HARD CLAY	BROWN CLAY		BLUE SANDY CLAY	A constraint of the second sec			BLUE CLAY FINE SAND	<u>er en r</u>	SANDSTONE EINE CAND	7	
CURRY'S NOT 7968 LOCATION :CULDOCAN NORTE, BINMALEY GROUND ELEVATION : WELL DEPTH : 174 m CASING DEPTH : CASING DIAMETER : STATK WATER LEVEL: 2.1m bgi DISCHARGE : 0.13 ps STATK WATER LEVEL: 2.1m bgi DISCHARGE : 0.13 ps STATK WATER LEVEL : 2.1m bgi STATK WATER MATER MATER MATER MATER MATER MATER WATER MATER M	DEPTH WELL		8		4 0		Paraset O g	ද ද ව		<u>×1100</u>	O N N N		0			0 7 7 8 7	
261. AYAN, BINMALEY a ayan, BINMALEY a ayan 0 m 100mm fel. 2.1m bgr ps . 0.23 lps/m	STRATA DESCRIPTION	SANDY CLAY				YELLOW STICKY	FINE SAND OUTCKSAND	BLUE SANDY CLAY	OUICKSAND	VELLOW CLAY	FINE SAND	BROWN CLAY BROWN CLAY					
LEVOR - JULA WELL NO. 14 OWNER'S NO: 436061 DOWNER'S NO: 436061 DOCATION: NAGUILAYAN, BINMALEY GROUND ELEVATION: WELL DEPTH : 130 m CASING DEPTH : 130 m CASING DIAMETER : 100mm STATIC WATER LEVEL : 2.1 m bg1 DISCHARGE : 0.6 lps STATIC WATER LEVEL : 2.1 m bg1 DISCHARGE : 0.6 lps STATIC WATER : 0.23 lps/m TRANSMISSIVITY:	DEPTH WELL (m) DESIGN		C C N		40		2017-30 0 0	Se .	2904	<b>0</b>	50 120 120		140				
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LWUA - JICA WELL NO: 54 OWNER'S NO: 5517 LOCATION: BONDAN BOQUIS, DAGUPAN CITY GROUND ELEVATION: WELL DEPTH: 210 m CASING DEATH: 210 m CASING DIAMETER : STATIC WATER LEVEL: DISCHARGE : SPECIFIC CAPACITY: TRANSMISSIVITY:	CEPTH WELL DESCRIPTION 20 B SIND CLAY 20 CLAY
LWUA - VICA WELL NO: 28 OWNER'S NO: 5183 LOCATION : PANTAL WEST, DAGUPAN CITY GROUND ELEVATION : WELL DEPTH : 189 m CASING DEAMETER : STATIC WATER LEVEL : DISCHARGE : STATIC WATER LEVEL : DISCHARGE : SPECIFIC CAPACITY : FRANSMISSIVITY :	CEPTH     DESTRATA     D1       Cm)     DESTRATA     D1       20     Curve     Curve     Curve       20     Curve     Curve     Curve
LWUA - JICA WELL NO: 25 OWNER'S NO: 5933 LOCATION : GROUND ELEVATION : WELL DEPTH : 143. 3m CASING DIAMETER : 100mm STATIC WATER LEVEL : DISCHARGE : DISCHARGE : SPECIFIC CAPACITY : SPECIFIC CAPACITY :	CEPTH DESTRATA Cmil H 20 20 20 20 20 20 20 20 20 20
LWUA -JICA WELL NO: 22 OWNER'S NO: 20491 LOCATION : PARAYAO, BINMALEY GROUND ELEVATION : WELL DEPTH : 90 m CASING DEPTH : 17.73 m CASING DEPTH : 17.73 m CASING DEPTH : 17.73 m CASING DEPTH : 17.73 m CASING DEPTH : 100/63 m STATIC WATER LEVEL: 1.2 m bg1 DISCHARGE : 0.63 fps SPECIFIC CAPACITY : 0.2 lps/m TRANSMISSIVITY :	CEPTH WELL DESIGN DESIGN TOWELL 20 20 20 20 20 20 20 20 20 20 20 20 20 2
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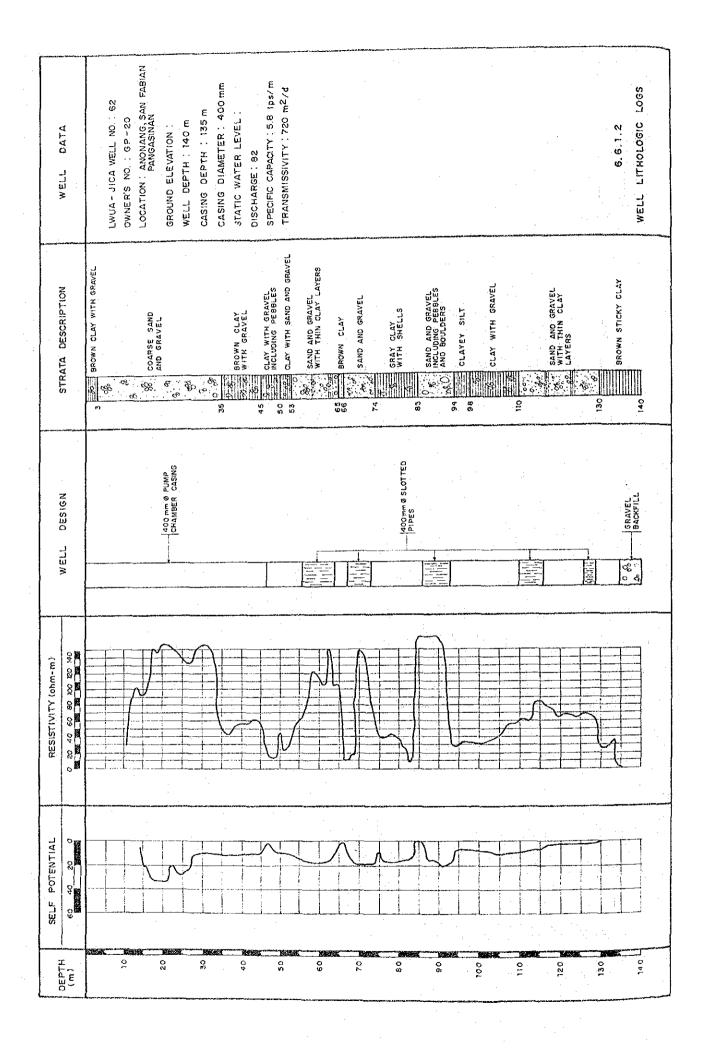


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LWUA-JICA WELL NO.: 81 OWNER'S NO.: 43~60-81 LOCATION : PASIMA, MALASIQUI GROUND ELEVATION : WELL DEPTH : 46 m CASING DEPTH : 34 m CASING DEPTH : 34 m CASING DEPTH : 34 m STATIC WATER LEVEL : 4.60 m bgl SISCHARGE : 0.63 tbs	STRATA	VELLOW CLAY	R CORAL ROCK	CLAY		QU CKSAND						LITHOLOGIC LOGS
LWUA-JICA WELL NO. : 81 OWNER'S NO.: 43~60-81 LOCATION : PASIMA, MALAS GROUND ELEVATION : WELL DEPTH : 46 m CASING DEPTH : 46 m CASING DEPTH : 34 m CASING DEATH : 46 m STATIC WATER LEVEL : 4.60 DISCHARGE : 0.63 bs	WS				1				: :	<b>1941 166</b> 84		WELL LITHO
LWUA -JICA OWNER'S 1 LOCATION GROUND EL WELL DEP CASING DE CASING DI CASING DI STATIC WA	TRAN	Ē	2	O N	Ř	\$	9 9	ç 	4	ŝ		
LWUA-JICA WELL NO. 71 OWNER'S NO.: 10795 LOCATION : MALABAGO, CALASIAO GROUND ELEVATION : WELL DEPTH : 70 m CASING DEPTH : 24/46 m CASING DEPTH : 24/46 m STATIC WATER LEVEL : DISCHARGE : 150/113 mm	STRATA	DESCRIPTION			V V V V V V STICKY CLAY STICKY CLAY				•			
LWUA -JICA WELL NO. 71 OWNER'S NO. 10795 LOCATION : MALABAGO, CALA GROUND ELEVATION : WELL DEPTH : 70 m WELL DEPTH : 24/46 m CASING DEPTH : 24/46 m CASING DEPTH : 24/46 m STATIC WATER LEVEL : 150/113 STATIC WATER LEVEL :	TRANSMISS IVITY :					i						
LWUA-JICA WELL OWNER'S NO. 11 LOCATION : MALA GROUND ELEVATIO WELL DEPTH : CASING DEPTH : CASING DEPTH : CASING DIAMETEL STATIC WATER LU	TRANSMI		50	ę	99	° C B	ŝ	C N N	5 04	o v		0
LWUA-JICA WELL NO. 70 OWNER'S NO. 5366 LOCATION : BOLINGUIT, SAN CARLOS CITY GROUND ELEVATION : WELL DEPTH : 142 m CASING DEPTH : CASING DIAMETER : STATIC WATER LEVEL : DISCHARGE :	STRATA	DESCRIFION BROWN SANDY	CLAY SAND	BLUE STICKY	BROWN STICKY CLAY CLAY YELLOW SANDY CLAY	BROWN SANDY		BLUE STICKY	BLUE SAND	· · · · · · · · · · · · · · · · · · ·		
LEWUA - JICA WELL NO. OWNER'S NO.: 5366 GROUND ELEVATION : WELL DEPTH : 42 CASING DEPTH : 42 CASING DEPTH : 42 STATIC WATER LEVEL DISCHARG E:	TRANSMISSIVITY :					· .						
LWUA - JICA WEL OWNER'S NO : LOCATION : BOI GROUND ELEVAT WELL, DEPTH : CASING DEPTH : CASING DIAMET STATIC WATER L DISCHARGE :	TRANSN DEPTH	Ē	0 7	• O \$	C 2	 6	0 0 0 7	120 120	14 04	(60		у —
NO.: 56 28 AN CITY A. CITY	STRATA	DESCRIPTION CLAY SAND		CLAY	(金子) GRAVEL (金子) GRAVEL CLAY	SANO	CLAY	SANO		SAND	SAND & GRAVEL	
LWUA-JICA WELL NO. 56 OWNERS NO. 5128 LOCATION : DAGUPAN CITY GROUND ELEVATION : WELL DEPTH : 173 m CASING DEPTH : CASING DEPTH : CASING DIAMETER : STATIC WATER LEVEL : DISCHARGE :	TRANSMISSIVITY :	DESIGN										
LWUA - JICA OWNER'S NO. LOCATION : D GROUND ELEV WELL DEPTH WELL DEPTH CASING DEPT CASING DEPT CASING DEMM STATIC WATE	TRANSN	Ê	O N	Q 4	Ç Ç	0 0	100	120	04 04	leo		0
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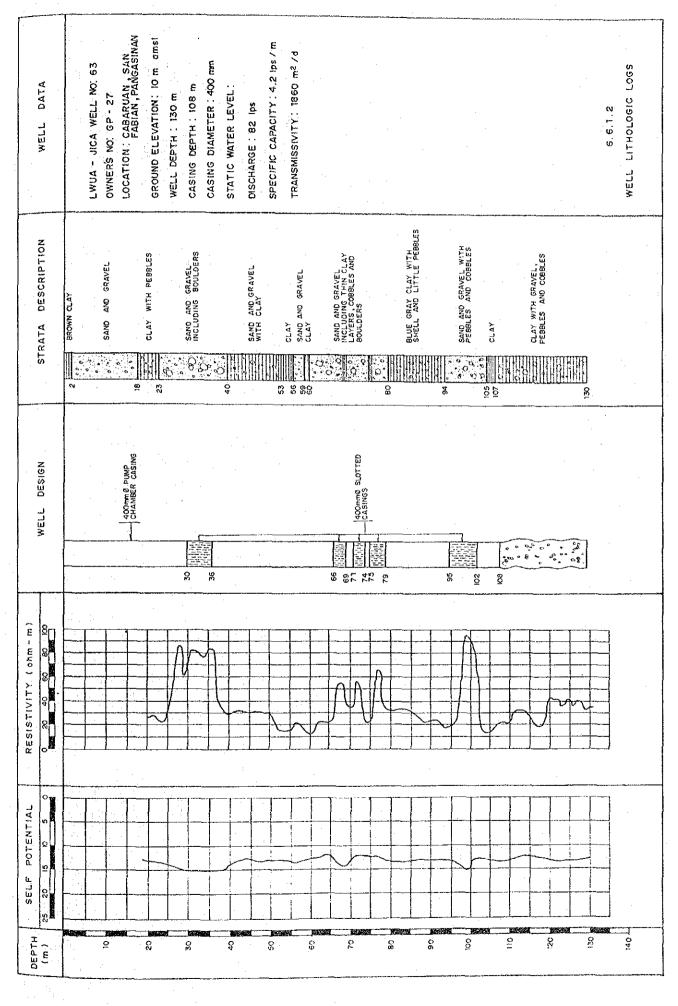
WELL DATA	LWUA-JICA WELL NO.: 61 OWNER'S NO.: 6P-26 LOCATION: ANGIO, SAN FABIAN GROUND ELEVATION: WELL DEPTH : 163 m CASING DEPTH : 153 m CASING DEATH : 159 m CASING DIAMETER: 400 mm STATIC WATER LEVEL : DISCHARGE : 82 IPS SPECIFIC CAPACITY : 480 m²/d TRANSMISSIVITY : 480 m²/d	WELL LITHOLOGIC LOGS
STRATA DESCRIPTION	13       SAND AND GRAVEL         13       SOLO SAND AND GRAVEL         17       FROWN CLAY WITH         17       SIDD AND GRAVEL         13       SIDD AND GRAVEL         33       SROWN SCLAY WITH         33       SROWN SCLAY WITH         33       SROWN SCLAY WITH         34       SAND AND GRAVEL         415       SAND AND GRAVEL         55       SAND AND GRAVEL         54       SAND AND GRAVEL         55       SAND AND GRAVEL         56       SAND AND GRAVEL         57       SAND AND GRAVEL         58       SAND AND GRAVEL         59       SAND AND GRAVEL         50       SAND AND GRAVEL         51       SAND AND GRAVEL         52       SAND AND GRAVEL         53       SAND AND GRAVEL         54       GRAY CLAY WITH FEBBLES         56       SAND AND GRAVEL         57       GRAY CLAY WITH SHELLS         58       SAND AND GRAVEL         51       GRAY CLAY         53       SAND AND GRAVEL         54       GRAY CLAY         55       GRAY SLITY CLAY         113       SAND AND GRAVE	
MELL DESIGN	46.5 46.5 55 51 11.11.11 46.5 55 51 11.11.11 46.5 55 51 11.11.11 55 51 11.11.11 52 51 11.11.11 52 51 11.11.11 52 53 11.11.11 52 53 11.11.11 52 53 11.11.11 53 53 11.11.11 53 53 11.11.11 53 53 11.11.11 53 53 11.11.11 53 53 11.11.11 53 53 11.11.11 53 53 11.11.11 53 53 11.11.11 53 53 11.11.11 53 53 11.11.11 53 54 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 11.11.11 55 55 55 55 55 55 55 55 55	
RESISTIVITY (ohm-m)		
SELF POTENTIAL		

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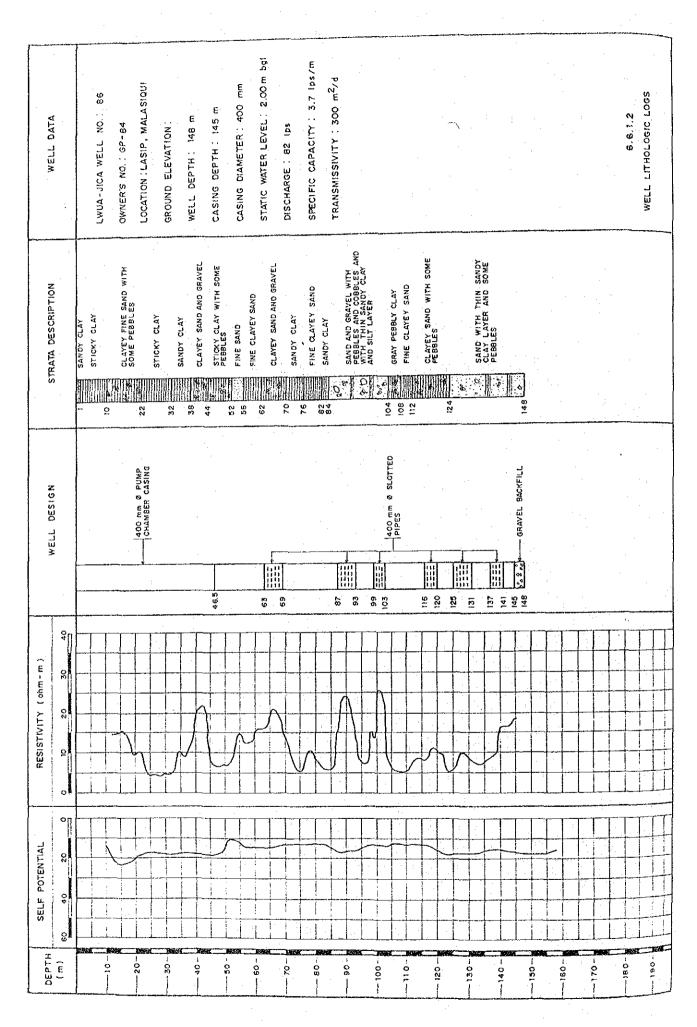


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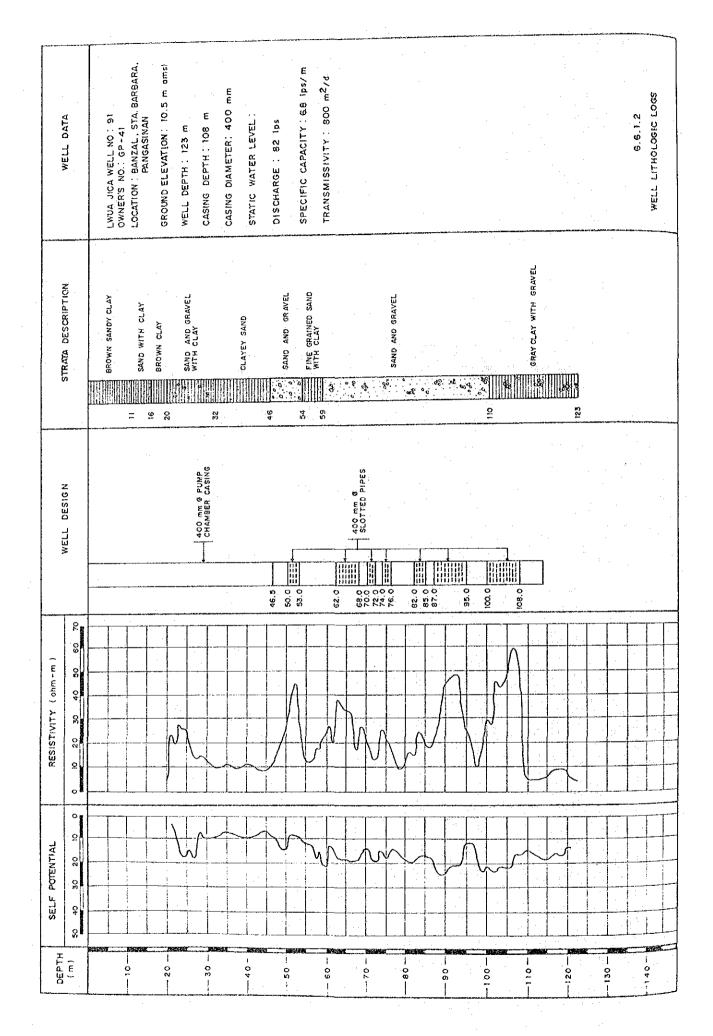
NO.: 101 7702 PAN CITY 8 m cmsi 8 m 6 C.:	STRATA DESCRIPTION DESCRIPTION CLAY SAND	CLAY	- जनगणनामस्य	CLAY AND AND GRAVE	CL.AY	CLAY CLAY SAND	ct.AY		SAND & GRAVEL		
LWUA-JICA WELL NO.: 101 OWNER'S NO.: 20702 LCCATION : DAGUPAN CIT GROUND ELEVATION : 180 WELL DEPTH : 183 m CASING DEPTH : 183 m CASING DEPTH CASING DEPTH STATIC WATER LEVEL : DISCHARGE : SPECIFIC CAPACITY : TRANSMISSIVITY :	TH WELL				o	O	6 0 F	20	C B	200	<b>1</b>
T S S S S S S S S S S S S S S S S S S S	H L L L L L L L L L L L L L L L L L L L	Ş Ş		8	0	2				Ň	
DAGUPAN CITY Macupan CITY	DESCRIPTION			CLAY			SAND	CLAY	CNAS		CLAY CLAY
WELL NO WELL NO LUCAO, 1 H: 189 TH; RER : METER : AFTER : 131 Ip AFACITY IVITY:	WELL						11][[11][[11]			<u></u>	
LWUA-JICA OWNER'S NC LOCATION : GROUND ELE WELL DEPT CASING DEP CASING DEP CASING DEP STATIC WATI DISCHARGE SPECIFIC C TRANSMISS	DEPTH ( a )	O N	4 0 4	C G	C W	0 0 0	120	64 04		OG E	0 8
LL NO. : 83 8089 8089 LACIÓN, MALASIQUÍ 0N: 62 m 62 m 62 m 62 m 51 fs 1 fs 1 fs 1 fs 1 fs 1 fs 1 fs 1 fs	STRATA DESCRIPTION E BROWN CLAY	SANDY CLAY	BLUE STICKY CLAY		YELLOW STICKY CLAY YELLOW SAND	BLUE STICKY CLAY	BLUE SANDY CLAY		· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·	
LWUA - JICA WELL NO. OWNER'S NO : 8089 OWNER'S NO : 8089 LOCATION : POBLACION GROUND ELEVATION : WELL DEPTH : 62 m VELL DEPTH : 62 m CASING DIAMETER : 25 STATIC WATER LEVEL : DISCHARGE : 1,31'105 STATIC WATER : 1,31'105 STATIC WATER : 1,31'105 TRANSMISSIVITY :	H WELL			Langer.		167.53					
L WU O WN O ROCK O REC C ASI S TAT S TAT S TAT S TAT S TAT	OEPTH (m)	<u>0</u>	0 2	Ор Г	4	D LA	8	0		8	0;
LWUA-JICA WELL NO.: 69 OWNER'S NO.: LOCATION : POBLACION, SAN CARLOS CITY GROUND ELEVATION : WELL DEPTH : 137 m WELL DEPTH : 137 m CASING DEPTH : CASING DEPTH : CASING DEPTH : CASING DEPTH : CASING DEPTH : STATIC WATER LEVEL : DISCHARGE : SPECIFIC CAPACITY : TRANSMISSIVITY :	STRATA DESCRIPTION ThLow STICKY	ANUT CLAY SANUT CLAY SANUT CRAVEL BAUE SHELLS BAUE STICKY CLAY		YELLOW CLAY	BLUE STICKY CLAY	TUFF BLUE GAY		8			-
LWUA-JICA WELL NO. : 69 OWNER'S NO.: LOCATION : POBLACION, SAN C GROUND ELEVATION : WELL DEPTH : 137 m CASING DEPTH : 137 m CASING DEPTH : 150 mm STATIC WATER LEVEL : DISCHARGE : SPECI FIC CAPACITY : TRANSMISSIVITY :	CH WELL DESIGN										
C C C C C C C C C C C C C C C C C C C	DEPTH ( # )	8 	9 9	<u> </u>	8	00	120	140		9 <u>1</u>	

WELL DATA	LWUA - JICA WELL NO: 85 OWNER'S NO: GP - 86 LOCATION: LASIP MALASIOUI, GROUND ELEVATION: WELL DEPTH: 149 m CASING DEPTH: 149 m CASING DEAMETER: 400mm STATIC WATER LEVEL: 3.3 m bgi DISCHARGE : 82 1ps DISCHARGE : 82 1ps SPECIFIC CAPACITY: 4.5 1ps/m TRANSMISSIVITY: 330 m <sup>2</sup> /d	6. 6.	WELL LITHOLOGIC LOGS
STRATA DESCRIPTION	BROWN STICKY CLAY       10       8       8       9       9       9       10       11       12       13       14       15       16       17       18       19       19       10       11       12       13       14       15       16       17       17       18       19       11       11       12       13       14       15       16       17       17       18       19       10       11       12       13       14       15       16       17       17       18       19       19       10       11       11       12       13       14       14       14       14       14       14       144       145       14		
WELL DESIGN	400mm @ PUVP. 400mm @ PUVP. 60 63 63 64 65 65 65 65 65 65 65 65 65 65 65 65 65		
RESISTIVITY (ohm-m) 0 0 20 30 40			
SELF - POT ENTIAL			



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WELL DATA	LWUA-JICA WELL NO. 58 OWNER'S NO. 69-25 LOCATION MATICMATIC.	STA BARBARA GROUND ELEVATION : WELL DEPTH : 156 m	CASING DEPTH : 154 m CASING DIAMETER : 400 mm STATIC WATER LEVEL :	DISCHARGE: 82 1ps SPECIFIC CAPACITY: 7.7 1ps/m TRANSMISSIVITY: 860 m <sup>2</sup> /d			6.6.1.2 Well Lithologic Logs
STRATA DESCRIPTION	EROWN CLAY FINE SAND B C THE SAND AND GRAVEL 12 17 17 18 19 19 19 10 10 10 10 10 10 10 10 10 10 10 10 10	26 STICKY CLAY 30 SAND 55 CLAY 56 CLAY 36 CLAY 36 CLAY 36 CLAY 37 CLAY 38 STICKY CLAY 37 STICKY CLAY	00 00 00 00 00 00	82 044 82 044 84 SAND AND GRAVEL WITH 84 63 FEBLES AND COBBLES	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	28 CAN CLAY 28 CAN CLAY 133 CAN AND GRAVEL 53 COND AND GRAVEL WITH 54 CONDERS 54 CONDERS 50 CLAY 150 CLAY 151 CLAY	
MELL DESIGN		400 mm & PUMP CHAMBER CASING			111111 - 400 mm Ø SLOTTED		
RESISTIVITY (00m-m)							
IAL 5 0							
DEPTH SELPPOTENTIAL (.m.) 25 20 15 10 5							



WELL DATA -	LWUA-JICA WELL NO: 64 OWNER'S NO: 6P - 29	LOCATION : ANONANG, SAN FABIAN, PANGASINAN GROUND ELEVATION :	WELL UETIN. 118 M CASING DEPTH : 99 M CASING DIAMETER : 400mm	STATIC WATER LEVEL : DISCHARGE : B2 105	SPECIFIC CAPACITY: 4.7 lps/m Transmissivity: 1120m²/d				6.6.1.2. Well Lithologic Logs
STRATA DESCRIPTION	1	33 - 23 - 23 - 23 - 23 - 23 - 23 - 23 -		46 39 39 39 39 39 30 39 30 30 30 30 30 30 30 30 30 30 30 30 30	් දී කත සංක සංක සංක සංක සංක සංක සංක සංක සංක සංක	70 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	(1)13 (1)13 (1)13 (1)13 (1)13 (1)13 (1)14 (1)15 (1)14 (1)15 (1)14 (1)15 (1)14 (1)15 (1)14 (1)15		
MELL DESIGN		HADIMA 0. PUMP				2.0011ED 2.0011ED 2.0011ED 2.0011ED 2.0011ED 2.0011ED		e S S S	
RESISTIVITY (ohm-m) 0 20 40 50 80 100									~
DEPTH SELF - POTENTIAL (m) 22 15 10 5 0		8			8				

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## APPENDIX 6.6.2.1 GEORESISTIVITY SURVEY

A surtace georesistivity survey was performed at the alluvial plains encompassing the municipalities of Binmaley, Calasiao, Sta. Barbara, Mangaldan and Dagupan City. The investigation was aimed to explore the stratigraphic sequence of the different lithological units in terms of resistivity and thickness; to define the extent of saline water intrusion into the shallow aquifer and to select the most favorable area for groundwater exploitation.

1) Location of Measurements

A total of 37 Vertical Electrical Soundings (VES) including some calibrations were carried out at Cullao, Malanay, Gueguesangan in Sta. Barbara; San Miguel, Ambonao, Calit and Banaoang in Calasiao; Tebeng in Dagupan City; and Amulid in Mangaldan.

2) Fieldwork

Resistivity prospecting involves the passage of an electric current into the ground through a pair of circuit electrodes (AB) and the measurement of the resulting potential drop on the earths surface between a pair of potential electrodes (MN). The arrangement of measurements was patterned after the Schlumberger configuration with a maximum current electrode separation of 1,800 m.

The impressed current (I) and the resulting potential drop (V) were recorded for consecutive MN/2 and AB/2 separation. The results

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were then recorded on the data sheet where the apparent resistivity (Pa) was calculated using the formula below:

$$PA = \frac{(AB/2)^2 - (MN/2)^2}{MN} \frac{AV}{I} \text{ or } Pa = \frac{kV}{I}$$

3) Method of Interpretation

The field data gathered were plotted on transparent double log paper with the measured apparent resistivity representing the ordinate and half the current electrode separation as abscissa.

The true layer resistivities and thicknesses were obtained by comparing the field curves with precalculated auxilliary and master curves.

4) Equipment

Georesistivity Equipment (GRM 3,000) is powered by dry cells with a maximum output of 270 volts and can read up to 3 amperes. For deeper soundings, it can be powered by a 1500 watt engine generator power supply which can provide either direct or electrorating circuit.

5) Results of Georesistivity Survey

The interpreted true resistivity values and the corresponding depths of geologic contact are presented in TABLE 6.6.2.1.1 (1) to (4) and were based from field survey graphs. TABLE 6.6.2.1 (1) DEDUCED VALUES OF CEORESISTIVITY SOUNDING MEASUREMENTS DAGUPAN CITY

Vertical         Vertical         Contrain         Resistivity         S U B - S U R F A C E LAYER           Electrical         Location         Depth from (mans 1) beth from Number:         Depth from (mass 1) beth from Sounding         3 U B - S U R F A C E LAYER           Number:         Tuilao, Sta. Barbara         6 $n$ 17.0         49.3         26.8         6         7           2         Majanay, Sta. Barbara         6 $n$ 17.0         49.3         26.8         6         7           3         San Miguel, Calasian         5 $n$ 17.0         49.3         26.8         6         7           3         San Miguel, Calasian         5 $n$ 12.0         10.0         16         2         6         7           4         Tebeng, Dagupan City         5 $n$ 9         23.2         23.2         3         10         11         10         7         21.1         10         21.1         11         11         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1         1					the second se						
Location(mams 1)Depth from cround Sur-12345Fullao, Sta. Barbara6 $h$ $17$ $11$ $20$ 99Fullao, Sta. Barbara6 $h$ $17$ $11$ $20$ 99Malanay, Sta. Barbara6 $h$ $17$ $11$ $20$ 99San Miguel, Calasian5 $h$ $17$ $11$ $20$ 99San Miguel, Calasian5 $h$ $12$ $24$ $3$ $24$ $3$ $10$ Maboneo, Calasiao5 $h$ $95$ $39$ $213$ $3$ $11$ Cuevesangen, Sta. Barbara5 $h$ $95$ $39$ $213$ $3$ $11$ Cuevesangen, Sta. Barbara5 $h$ $95$ $26$ $24$ $31$ $10$ Cuevesangen, Sta. Barbara5 $h$ $26$ $26$ $11$ $11$ $11$ Guevesangen, Sta. Barbara5 $h$ $26$ $26$ $11$ $10$ $26$ $27$ $213$ $3$ $11$ Guevesangen, Sta. Barbara5 $h$ $26$ $26$ $24$ $213$ $209$ $270$ $213$ $31$ $11$ Guevesangen, Sta. Barbara5 $h$ $26$ $24$ $213$ $10$ $27$ $213$ $213$ $213$ $213$ $213$ $213$ $213$ $213$ $213$ $213$ $213$ $212$ $212$ $212$ $212$ $212$ $212$ $212$ $212$ $212$ $212$ <			Elevation			5	ກ ຮ 1	с v	Υ Α	ĸ	
Face (m)Face (m)1711209Tullao, Sta. Barbara6 $h$ $17.0$ $47.3$ $249.3$ 8Malanay, Sta. Barbara6 $h$ $7.0$ $47.3$ $249.3$ 8Malanay, Sta. Barbara6 $h$ $5.4$ $17.0$ $49.3$ $249.3$ 8Malanay, Sta. Barbara6 $h$ $5.4$ $12.0$ $61.2$ $253.2$ $3$ Tebeng, Dagupan City5 $h$ $12.0$ $61.2$ $253.2$ $3$ Ambonao, Calasiao5 $h$ $9.5$ $39.9$ $279.9$ $3$ Ambonao, Calasiao5 $h$ $26.24.3$ $10$ $31.14$ $31.130.9$ Calit, Calasiao5 $h$ $31.14$ $20.2$ $270.9$ Banacang, Calasiao5 $h$ $31.140$ $20.2$ $271.2$ Banacang, Calasiao5 $h$ $31.146$ $20.2$ $271.2$ Ambonao, Calasiao5 $h$ $2.5$ $10.20$ $270.9$ Banacang, Calasiao5 $h$ $2.5$ $12.0$ $79.2$ Ambonao, Calasiao5 $h$ $4100$ $20.2$ $271.2$ Ambonao, Calasiao5 $h$ $2.5$ $12.0$ $79.2$ Ambonao, Calasiao5 $h$ $4100$ $270.2$ $271.2$ Ambonao, Calasiao5 $h$ $4100$ $270.2$ $271.2$ Ambonao, Calasiao5 $h$ $4100$ $270.2$ $271.2$ Ambonao, Calasiao5 $h$ $4100$ <td>1</td> <td>Location</td> <td>(nams 1)</td> <td>Depth from Cround Sur-</td> <td>г.</td> <td>5</td> <td>m</td> <td>4</td> <td>Ś</td> <td>Q</td> <td>5</td>	1	Location	(nams 1)	Depth from Cround Sur-	г.	5	m	4	Ś	Q	5
Tullao, Sta. Barbara6 $h$ 17.011209Malanay, Sta. Barbara6 $h$ 17.049.3249.3249.39Malanay, Sta. Barbara6 $h$ 5.424.8264.83San Miguel, Calasian5 $h$ 12.0102San Miguel, Calasian5 $h$ 12.0162Mabonao, Calasiao5 $h$ 9.539.9279.9Ambonao, Calasiao5 $h$ 9.543.7268.73Calit, Calasiao5 $h$ 2.629.11010Calit, Calasiao5 $h$ 2.629.11118Banacang, Calasiao5 $h$ 2.513279.913Ambonao, Calasiao5 $h$ 2.629.1120.9270.9Ambonao, Calasiao5 $h$ 2.629.1120.9271.2Ambonao, Calasiao5 $h$ 2.512.079.2271.2Ambonao, Calasiao5 $h$ 2.72.7271.2Ambonao, Calasiao5 $h$ 2.52.72.7271.2Ambonao, Calasiao5 $h$ 2.62.910202.72.7Ambonao, Calasiao5 $h$ 2.74.42.74.42.79Ambonao, Calasiao5 $h$ 2.74.42.72.72.72.7Ambonao, Calasiao5 $h$ 2.74.42.6				face (m)					:		
Tullao, Sta. Barbara6h17.049.3 $249.3$ 8Malanay, Sta. Barbara6 $h$ 5.4 $24$ $17$ 8Malanay, Sta. Barbara6 $h$ $5.4$ $24.8$ $264.8$ 8San Miguel, Calasian5 $h$ $12.0$ $61.2$ $253.2$ 3Tebeng, Dagupan City5 $h$ $9.5$ $39.9$ $279.9$ $314$ Ambonao, Calasiao5 $h$ $9.5$ $43.7$ $268.7$ $10$ Cueguesangen, Sta. Barbara5 $h$ $2.6$ $29.1$ $120.9$ $270.9$ Calit, Calasiao5 $h$ $2.6$ $29.1$ $120.9$ $270.9$ Calit, Calasiao5 $h$ $2.6$ $29.1$ $120.9$ $270.9$ Mabonao, Calasiao5 $h$ $2.6$ $29.1$ $120.9$ $270.9$ Ambonao, Calasiao5 $h$ $2.6$ $29.1$ $120.9$ $270.9$ Ambonao, Calasiao5 $h$ $2.6$ $29.1$ $120.9$ $277.2$ Ambonao, Calasiao5 $h$ $2.6$ $29.1$ $120.9$ $277.2$ Ambonao, Calasiao5 $h$ $2.5$ $28.2$ $9.5$ $273.4$ Ambonao, Calasiao5 $h$ $273.4$ $273.4$ $273.4$				Q	17.	11	20	6			
Malanay, Sta. Barbara6 $24$ $h$ $17$ $5.4$ $8$ $24.8$ $17$ $264.8$ $8$ $264.8$ San Miguel, Calasian5 $h$ $12.0$ $61.2$ $15$ $253.2$ $39.9$ $29.4$ $11$ $3$ Tebeng, Dagupan City5 $h$ $12.0$ $61.2$ $15$ $253.2$ $39.9$ $31.4$ $31.4$ $3$ Ambonao, Calasiao5 $h$ $9.5$ $7$ $43.7$ $19.5$ $268.7$ $11$ $10$ $120.9$ $270.9$ $277.9$ Calit, Calasiao5 $h$ $2.6$ $31$ $29.1$ $10.2$ $120.9$ $277.9$ $277.7$ $217.7$ Banaoang, Calasiao5 $h$ $2.5$ $10.2$ $270.9$ $271.2$ $277.2$ $1120.9$ $277.9$ $277.7$ Banaoang, Calasiao5 $h$ $2.5$ 		Tullao, Sta. Barbara	9	ų	17.0	49.3	249.3				
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San Miguel, Calasian     5     h     12.0     16     2       Tebeng, Dagupan City     5     h     12.0     61.2     253.2     3       Tebeng, Dagupan City     5     h     9.5     39.9     279.9     3       Ambonao, Calasiao     5     h     9.5     39.9     279.9     10       Cueguesangen, Starbara     5     h     2.6     29.1     120.9     270.9       Calit, Calasiao     5     h     2.6     29.1     120.9     270.9       Banaoang, Calasiao     5     h     2.6     29.1     120.9     277.2       Ambonao, Calasiao     5     h     2.6     29.1     120.9     277.2       Ambonao, Calasiao     5     h     2.5     12.0     79.2     79.2       Ambonao, Calasiao     5     h     2.7     9     11     9			ç	L L	5.4	24.8	264.8				
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Ambonao, Calasiao5h9.5 $43.7$ $268.7$ 1Gueguesangen, Sta. Barbara5h $2.6$ $29.1$ $120.9$ $270.9$ Gueguesangen, Sta. Barbara5h $2.6$ $29.1$ $120.9$ $270.9$ Galit, Calasiao5h $3.1$ $10.2$ $52.7$ $277.7$ Banaoang, Calasiao5h $3.1$ $4.6$ $79.2$ $277.7$ Ambonao, Calasiao5h $12.7$ $43.2$ $268.2$ $99$ Anulid, Mangaldan5h $11.0$ $4.8.4$ $273.4$ $10$				a	10	5	18	10		-	
Cueguesangen, Sta. Barbara     5     h     2.6     29.1     11     18       Cueguesangen, Sta. Barbara     5     h     2.6     29.1     120.9     270.9       Calit, Calasiao     5     h     3.1     10.2     52.7     277.7       Banaoang, Calasiao     5     h     3.1     10.2     52.7     277.7       Ambonao, Calasiao     5     h     12.7     46     4     11       Ambonao, Calasiao     5     h     12.7     43.2     268.2     9       Anulid, Mangaldan     5     h     11.0     48.4     273.4     10	•	Ambonao, Calasiao		11	9.5	43.7	268.7				
Gueguesangen, Sta. Barbara     5     h     2.6     29.1     120.9     270.9       Calit, Calasiao     5     h     3.1     10.2     52.7     277.7       Banaoang, Calasiao     5     h     2.5     12.0     79.2     271.2       Ambonao, Calasiao     5     h     12.7     46     4     11       Ambonao, Calasiao     5     h     12.7     43.2     217.2       Anulid, Mangaldan     5     h     11.0     48.4     273.4     10				0	2	19	11	18	11		
Calit, Calasiao     5     6     410     20     2     13       Banaoang, Calasiao     5     h     3.1     10.2     52.7     277.7       Banaoang, Calasiao     5     h     2.5     12.0     79.2     271.2       Ambonao, Calasiao     5     h     12.7     46     4     11       Anulid, Mangaldan     5     h     11-0     48.4     273.4     10			ŝ	ч	2.6	29.1	I20.9	270.9			
Calit. Calasiao     5     h     3.1     10.2     52.7     277.7       Banacang, Calasiao     5     p     31     46     4     11       Ambonao, Calasiao     5     p     12.7     45     271.2       Anulid. Mangaldan     5     h     11-0     48.4     273.4     10		í		d	410	20	2	13	18		
Banaoang, Calasiao     5     n     2.5     12.0     79.2     271.2       Ambonao, Calasiao     5     h     12.7     43.2     268.2     9       Amulid, Mangaldan     5     h     11.0     48.4     273.4     10		Calit. Calasiao	0 0 0	ų	3.1	10.2	52.7	277.7			
Banacang, Calasiac     5     h     2.5     12.0     79.2       Ambonac, Calasiac     5     h     12.7     43.2     268.2       Amulid, Mangaldan     5     h     11.0     48.4     273.4				0	31	. 97	4	11	17		
Ambonao, Calasiao     5     6     17       Ambonao, Calasiao     5     h     12.7     43.2     268.2       Anulid, Mangaldan     5     h     11.0     48.4     273.4		Banacang, Calasiao	۰ ۲	4	2.5	12.0	79.2	271.2			
Ambonao, Calasiao         5         h         12.7         43.2         268.2           Amulid, Mangaldan         5         \$         15         \$         15				a	4 1	9	17	6			
dan 5 k 11-0 48.4 273.4		Ambonao. Calasiao	יי איז	e	12.7	43.2	268.2				
dan 5 h 11.0 48.4				d	27	<i>G</i> 1	15	10			
		Anulid. Mangaldan	Ś		11.0	-	273.4				

# DEDUCED VALUES OF GEORESISTIVITY SOUNDING MEASUREMENTS

		ă	DAGUPAN CITY					-			:
VERTICAL		FLEVATION	RESISTIVITY (corm-m.)		SUB	- SURFACE	ACE	LAYE	α		
SOUTH NICH	2 4 3	1 0 III 0 III	MORE HI 100		2		4	ŝ	9	7	
			ç	80	ñ	1.2	9				
11	Caranglaan, Dagupan City	4	ч	11*0	46.2	270.6					÷
	÷		٩	Q	1	 57	6				
2	Mangin, Dagupan City	4	ų	6.2	34.1	272.1					
-		•		100	n	0.5	ور	38			•
13	Nagutlayan, Binmaley	4	c	1.6	6.4		301.9				
			٩	125	ę	0.9	۲	80			
14	Cayaman, Bitmaley	4	£	2.8	5.9	47.2	314.0				
			عر	8	10	r.	¢	65			
2	Tincao Dagunan City	4	r	2.9	9.0	57	305.4				
		-	٩	48	24	N	đ	18			
16	Malued, Dagupen City	t	£	3.1	12.7	6047	300.7				
		. :	Q	37	\$	8.0	و	23			
17	Tapuac. Degupan City	*	<u>ح</u>	2.2	8.4	37.1	303.5		   		
			<u></u>	44	21	N	Ś				
18	Pogo Lasip - Degupan City	4	c	2.8	6+2	S0.0					
			Q	9		11	~				
19	Caranglasne Dagupan City	4	L	6.8	45.6	275.6					
<del></del>			2	10	м	42	~	· · · · · · · · · · · · · · · · · · ·			
20	Bolosan, Dagupan City	- <b>t</b>		7.7	32.3	263, 3					

TABLE 6.6.2.1 (3) GEORESISTIVITY SOUNDING MEASUREMENTS DEDUCED VALUES OF

		DACUPAN CITY	A CITT							
VERTICAL ELECTRICAL	- 0 C A- T - 0 N	ELEVATION	RESISTIVITY (ohm-m)		SUB -	SURFACE	ACE	LAYE	۲	
		(momsi)	CEPTH FROM	1.	2	ک ۲	4	S.	ဖ	7
		-	٩	30	-1-6 	•				
{	amulid. Mangaldan	4	Ľ	8.2		259.6				
		• :	٩	83	· •	12	7			
	anulf de Mengaldan	4	ų	13	55.9	258.9				
			ح	6.0		ల	4			
	Mamakingkings Degunan City	-4	£	9.7	33.0	249.0		}		
			٩	0.9		2				
	Haasine Mangaldan	m	£	8.5	33.2	241.8		   		
			م	23	ø	13	8			
	Massine Mangaldan		£	5.6	34.7	236.3				
			٩	9	0.8	83	32			
	Conservition Maste Binneley	P	L.	2.6	37.7	296.27				
·			9	50	2	0.2	12	848	-	
	Carsek Mast, Decimen City	6	٢	4.2	11.3	30.1	293.8			
			٩	79	9	0.8	S			
	Calmay, Degrown City		£	3.8	8.7	50.7				
			0	ŋ	0,6		25			
	Pantal. Decupan City	5	٩	7.6	38.4	342.6		2.4		
			8	20	2	1.6	90	72		
	A Contract of Contract	- - - -	£	0	19.0	55.8	376-6			

DEDUCED VALUES OF GEORESISTIVITY SOUNDING MEASUREMENTS

		DAGUPAN CITY	CITT								
	: ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ; ;	ELEVATION	RESISTIVITY		SUB	- SUR	SURFACE	LAYE	۲ ۲	. :	-
SOUNDING C		(m.a.m.s. 1.)	MORA RANORO	-	2	3	ヤ	<b>ن</b> ې	9	7	
			٩	3:	4	13	80				
	Bomoan Longos, Decupan City	2	Ľ	6.8	52.4	285,6					
			٩	70	.\$	16	or				mandar -
*****	Talugtos Manealdan	N	۲	2.9	29_0	272.0					
			٩	760	6	1.2	σ	ន			
-	Caloocen Sur, Binnalisy	2	ч	. 8	11.4	51.9	311.9				_;
			Q	68	s	0.8	9	8	-		
	Buardlau Birmaley	7	ų	2.9	8.4		303.7				
			م	8	ø		¢	£4			_
	Sahangana Dagunan City	2	ų	9.6	11.4		340.6				
			٩	100	55		15	07			
	Bonoan Guesets Deruses City	7	Ļ	3.0	13.2	70.4	328.8				
			2	2000	150	4	18	20			
	Bonosh Cassets Dadman City	~	٢	2.2	9.9	69.4	273.4				
			و			• :					
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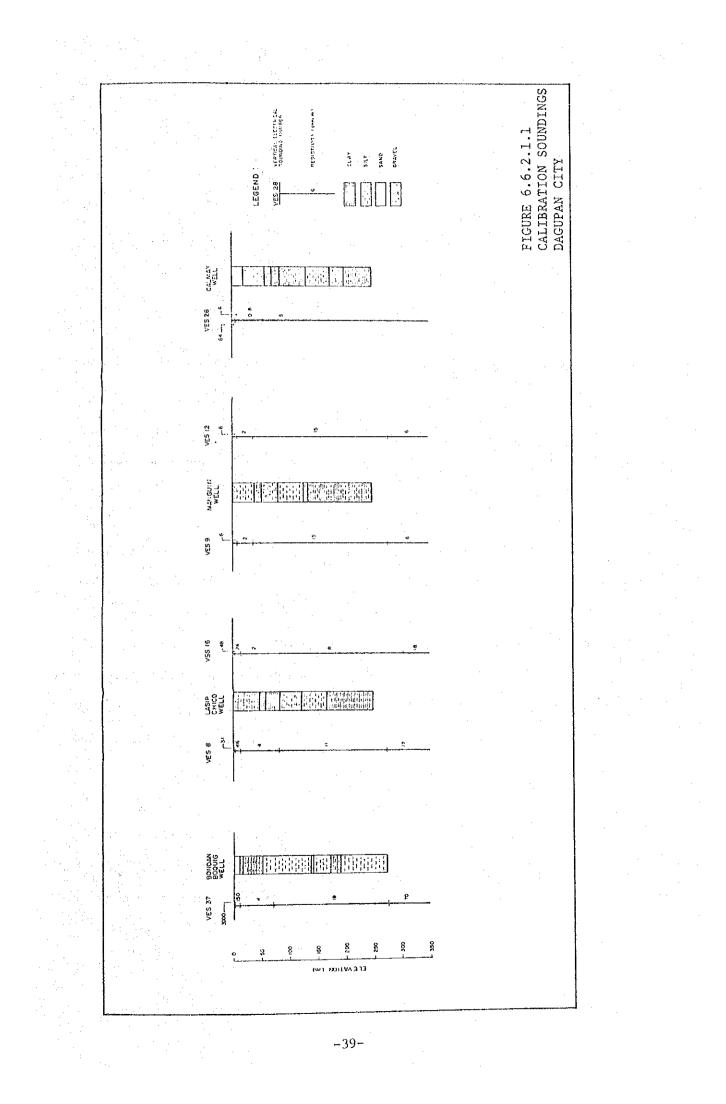
a) Calibration Soundings

For hydrogeological interpretation of electrical soundings, it is necessary to establish the pertinent resistivity of the different lithological units at depth by performing resistivity measurements at a convenient point as close as possible to a well with known lithology or to the geologic outcrops.

Six resistivity measurements were executed near deepwells drilled at Bonoan Boquig, Lasip Chico, Manguin and Calmay. The relation of resistivity to the specific lithological unit is presented in FIGURE 6.6.2.1.1 summarized below.

Range of	
Resistivity (ohm-m)	Lithological Composition
0.5 - 1.5	Clay, silt, sand and gravel intruded with
	saline water
2 - 10	Sand and gravel deposited in combination with high percentage composition of clay and silt
11 - 18	Silt, sand and gravel saturated with fresh water
23 - 72	Upper Miocene to Pliocene rock units
	(basement formation)
1000 - 3000	lsolated sand dune
· · · ·	

-38-



# b) Interpretation of Survey Results

The result of the georesistivity survey can be summarized in the following electrostratigraphic sections, isoresistivity maps and isotransverse resistance map.

Electrostratigraphic Sections

With reference to the results of the calibration soundings, the lateral and vertical relationships of the alluvial sediments maybe subdivided into five layers as shown in FIGURES 6.6.2.1.2~6.6.2.1.13

Layer 1 which exhibits low to relatively high resistivity values in the range of 0.6 to 3,000 ohm-m forms the superficial layer. The layer with resistivity responses not exceeding 10 ohm-m corresponds to clay and sand sediments saturated with fresh or brackish water. The values of 50 ohm-m or more can be correlated to comprise partly cemented sand and gravel saturated with freshwater. The coast near areas exhibiting resistivity values of 1,000 to 3,000 ohm-m corresponds to isolated sand dune.

Layer 2 comprises the fluvial sediments of clay, silt, sand and gravel intruded with saline water. The invasion occurs in the western belt of the investigation area and its approximate extent is presented

-40-

in FIGURE 6.6.3 of Main Text. This layer is believed not to exceed 70 m in depth and has resistivity value ranging from 0.5 to 1.5 ohm-m.

Layer 3 exhibits resistivity values ranging from 2 to 10 ohm-m conforming to sand and gravel deposited in combination with high percentage composition of silt and clay. This layers abuts on the basement formation at a depth of approximately 300 to 350 m below ground surface in an area northwest of Dagupan City. The extent of deposition in the southern portion tends to increase in depth as it underlies Layer 4 as shown in FIGURE 6.6.2.1.5.

Layer 4 corresponds to resistivity values in the range of 11 to 20 ohm-m. The layer is deposited as a lens-shaped formation overlying and underlying Layer 3 as shown in most electrostratigraphic sections. This layer is in near contact Layer 2 and overexploitation of groundwater upstream may lead to this association especially in zones high permeability. Most of the deepwell drilled in the study area withdraw water partly from this formation. Tapping this layer for groundwater extraction maybe possible and the aquifer may yield fair hydraulic characteristics.

-41-

Layer 5 presented resistivity values in the range of 23 to 72 ohm-m and is believed to be the basement formation. It is assumed part of the Upper Miocene rock sequence comprising mostly of fine to medium grains of clastic sediments composed of mudstone and sandstone. The lithological units are mainly exposed at the mountain plains northeast and southeast of Dagupan City.

The interfinger fronts of Layers 3, 4 and the basement formation are presented in FIGURE 6.6.3 of the Main Text.

### Isoresistivity Maps

The isoresistivity maps presented in FIGURES 6.6.2.1.14 $\sim$  6.6.2.1.16 for current electrode separations equivalent to 100,200 and 300 m, respectively, show uniform trend of resistivity increases as it enters the area immediately southeast of Dagupan City. This conforms to the sounding points located within the boundaries of 10 ohm-m or more contour line.

The resistivity measurements may indicate fair aquifer potentials with good water retention capabilities in this area. The electrostratigraphic sections revealed that this formation has resistivity values in the range of 11 - 20 m with an average thickness of 250 m.

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### Isotransverse Resistance Map

The isotransverse resistance map presented in FIGURE 6.6.2.1.17 can be regarded as a hydrogeological map because the transverse resistance is controlled by both thickness and permeability of the aquifer. The areas bounded by greater isotransverse resistance contour line should coincide to an aquifer with greater potential.

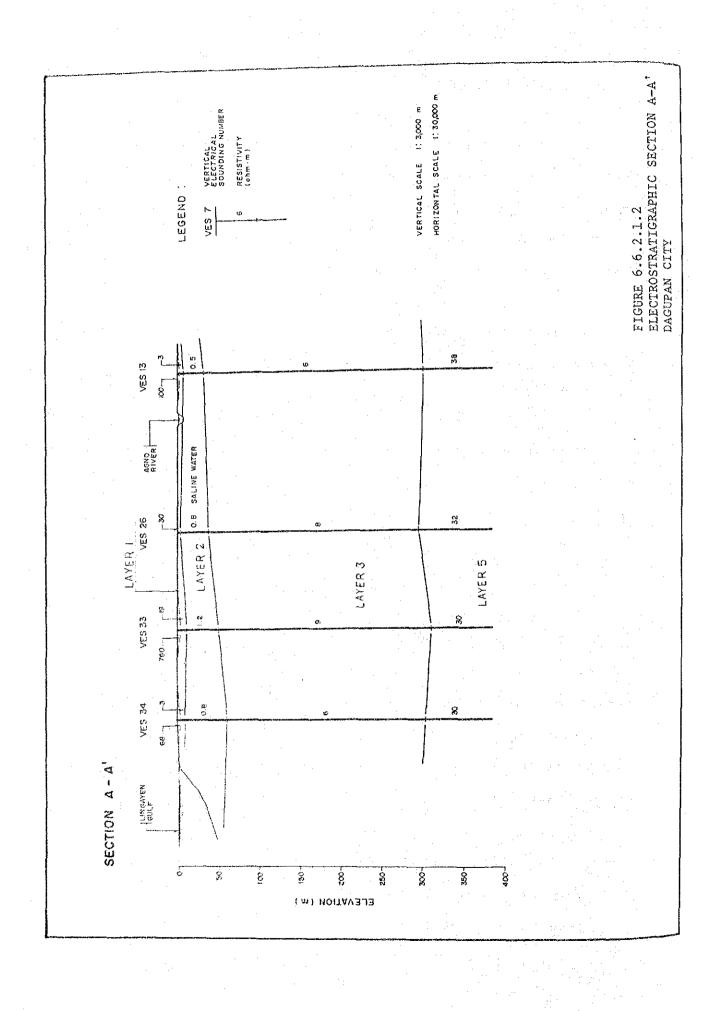
The area enclosed by 4,000 ohm-m or more contour line is presumed to comprise permeable layer capable of sustaining medium-capacity withdrawal through deepwells.

The resistivity responses were translated into its corresponding lithological units as interpreted from the calibration soundings shown in FIGURE 6.6.2.1.1.

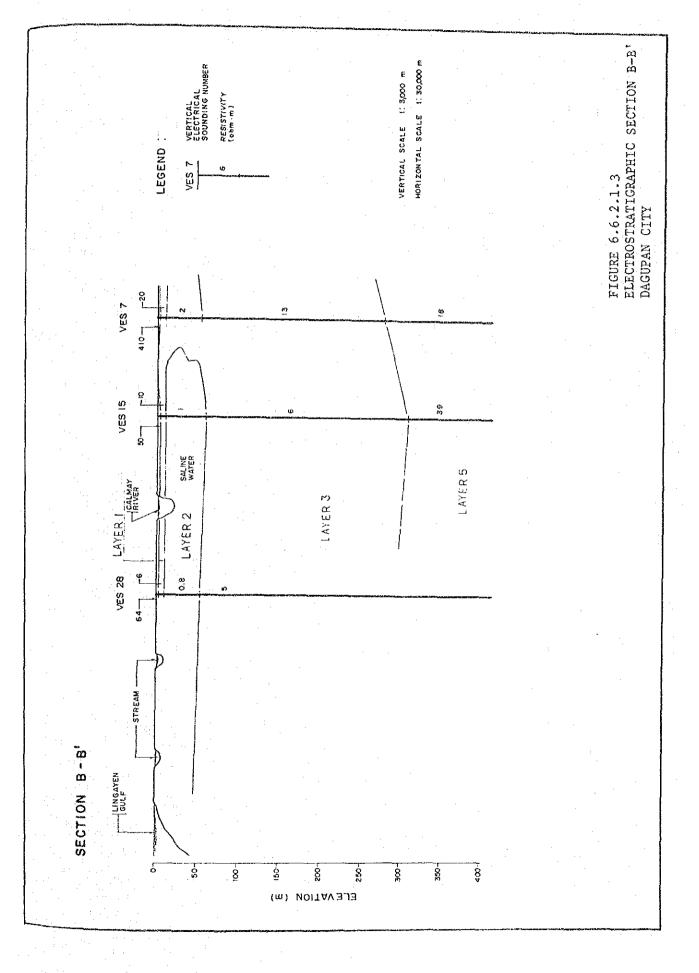
c) Findings/Recommendations

Dagupan City is situated downstream of the hydrogeological system that extends from the southern periphery of Lingayen Gulf towards the northwestern part of Tarlac Province. Uncontrolled groundwater withdrawal upstream of this system led to the intrusion of saline water into the shallow aquifer deeper inland. Hence, it is not advisable to extract water from this aquifer as rate of intrusion is not determined.

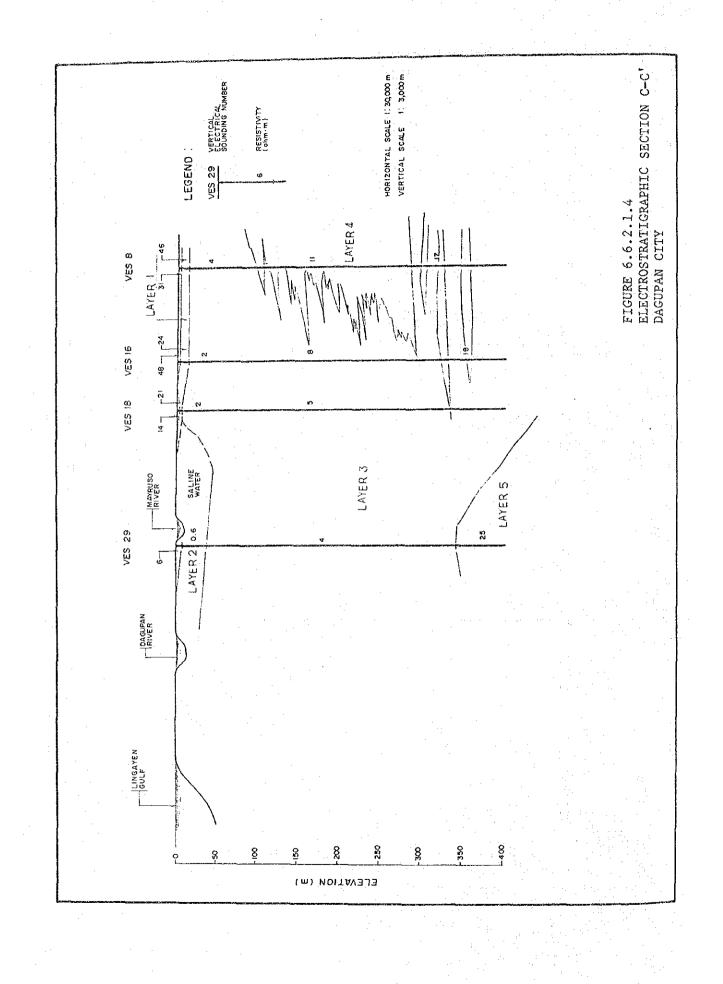
The deeper aquifer may offer fair hydraulic parameters enough to sustain medium-capacity withdrawal through deepwells. The formation has an average thickness of 250 m and has been identified in an area southeast of Dagupan City.



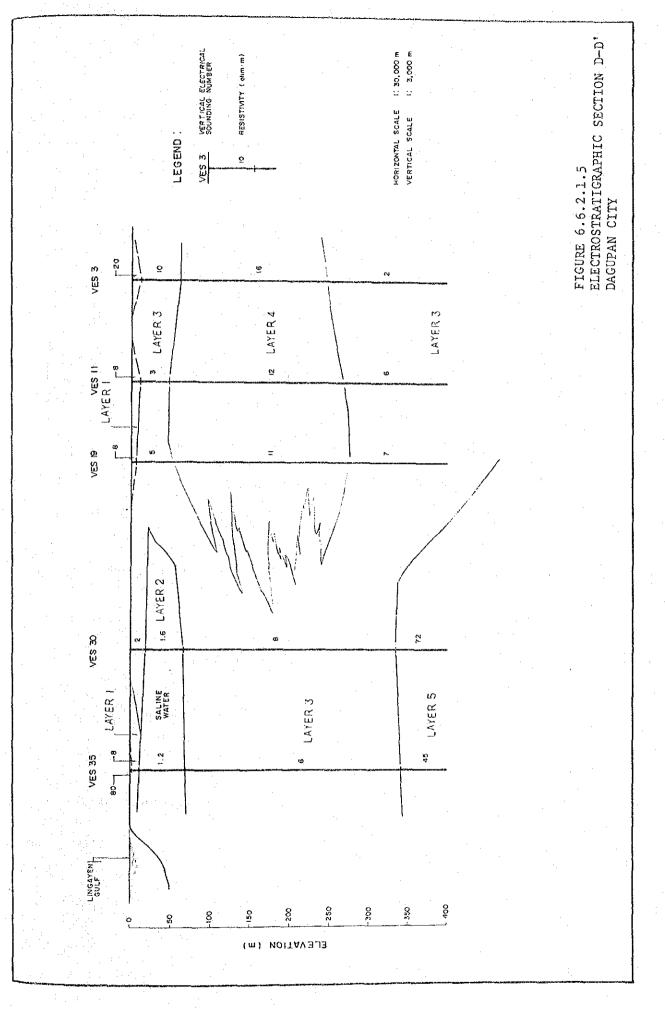
-44-



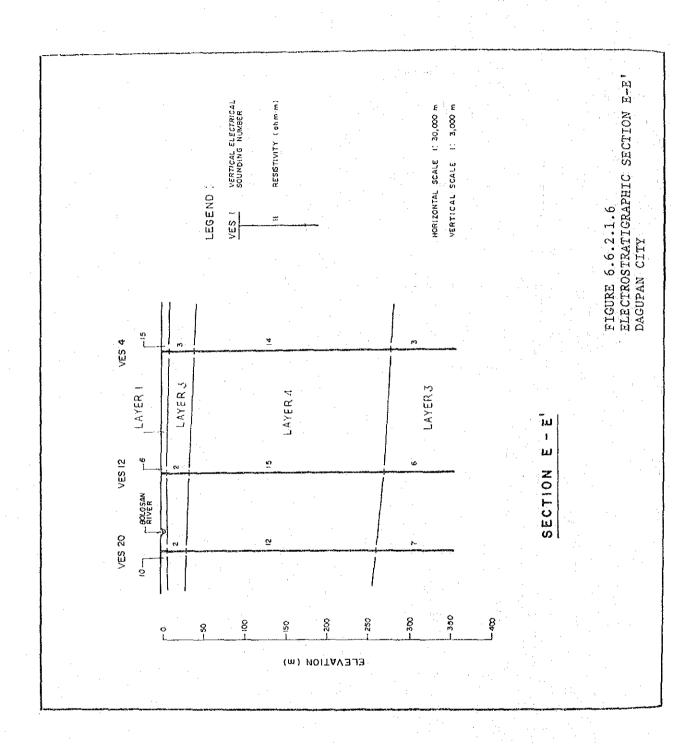
-45--



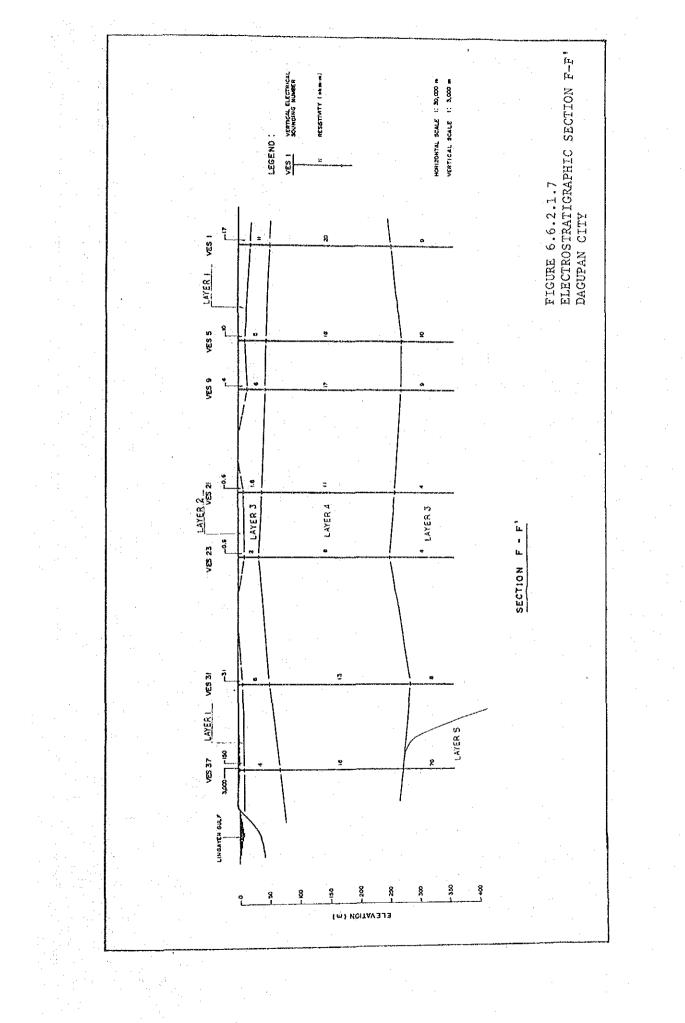
-46--



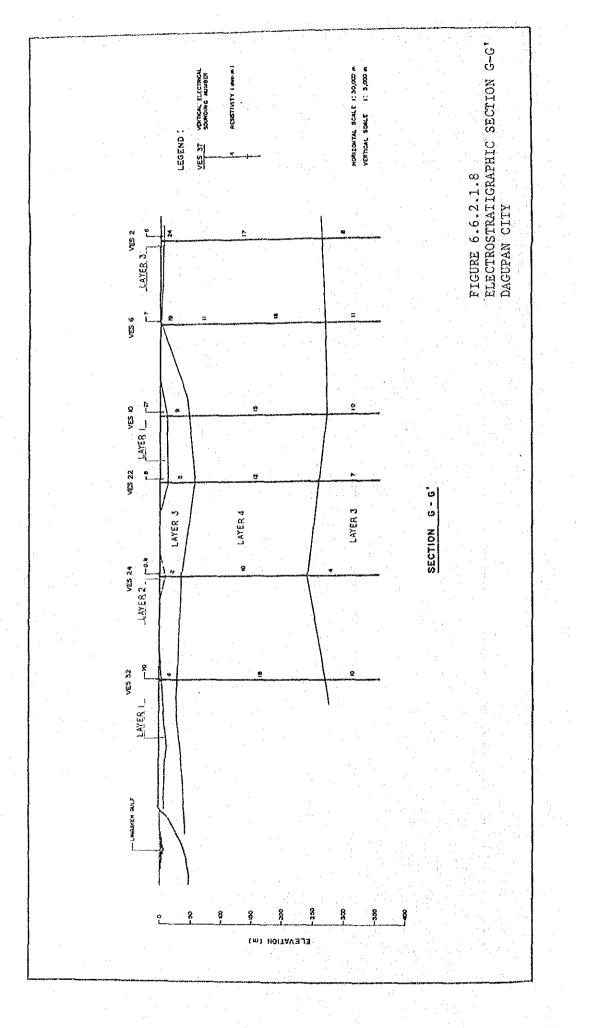
-47--



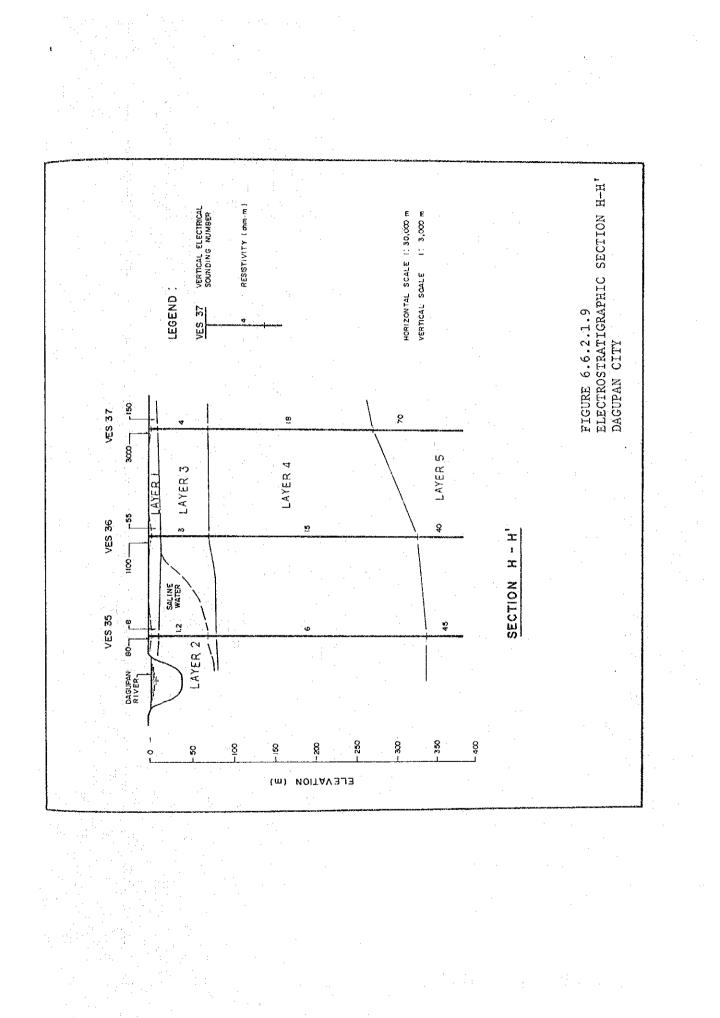
-48-



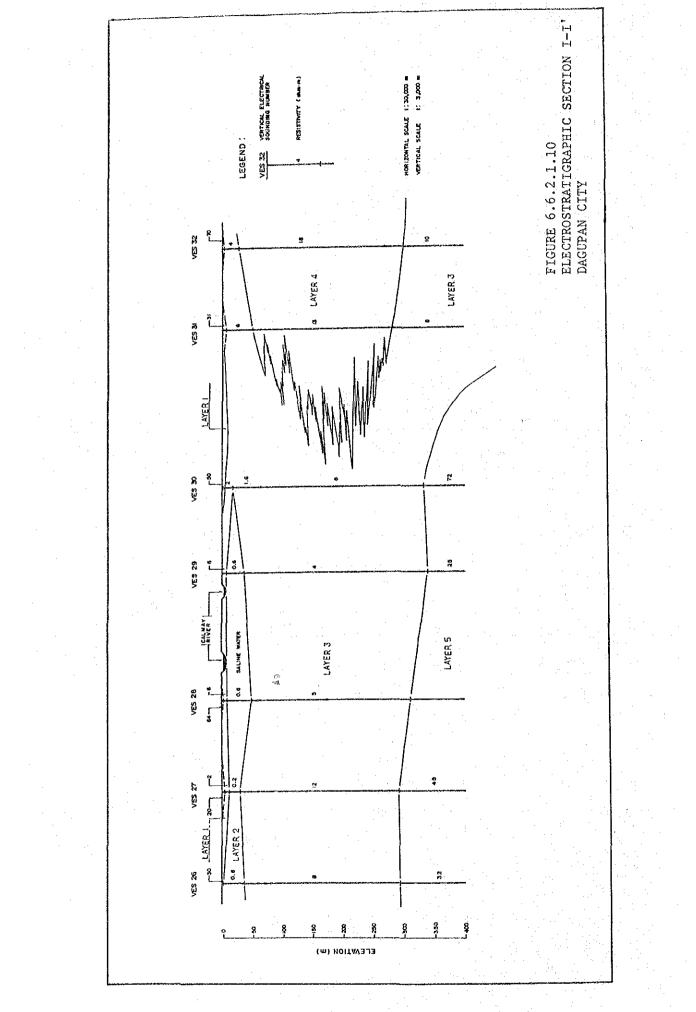
-49-



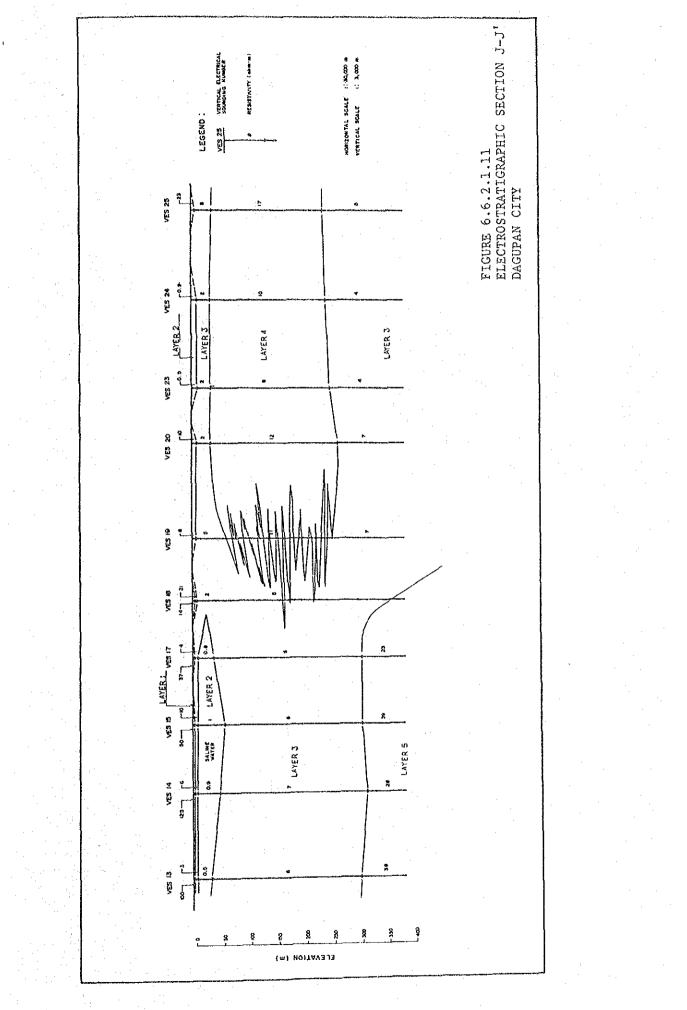
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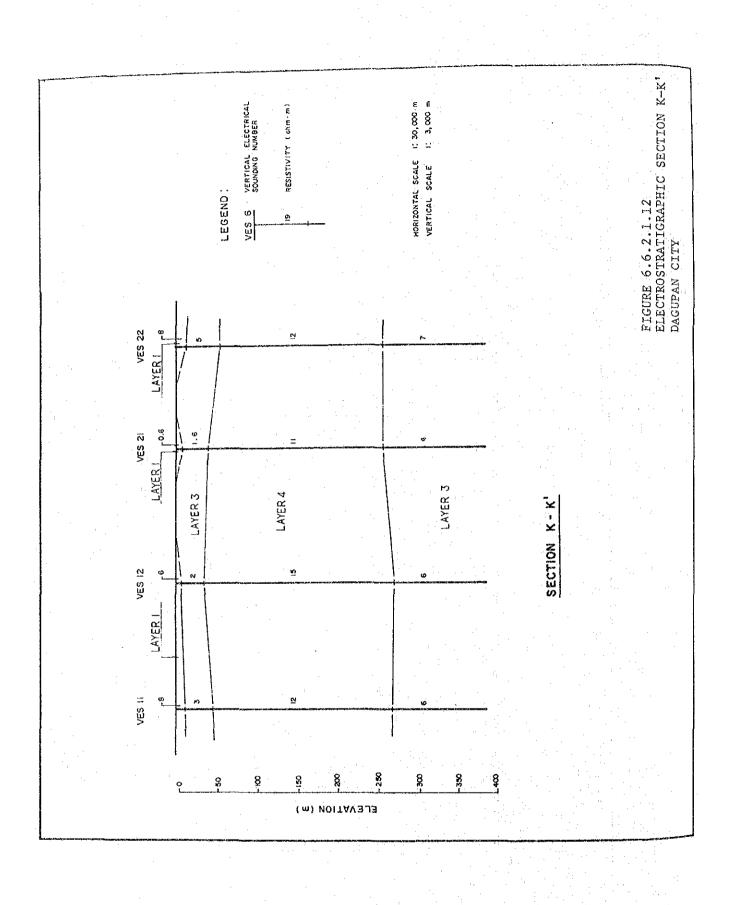
-51-

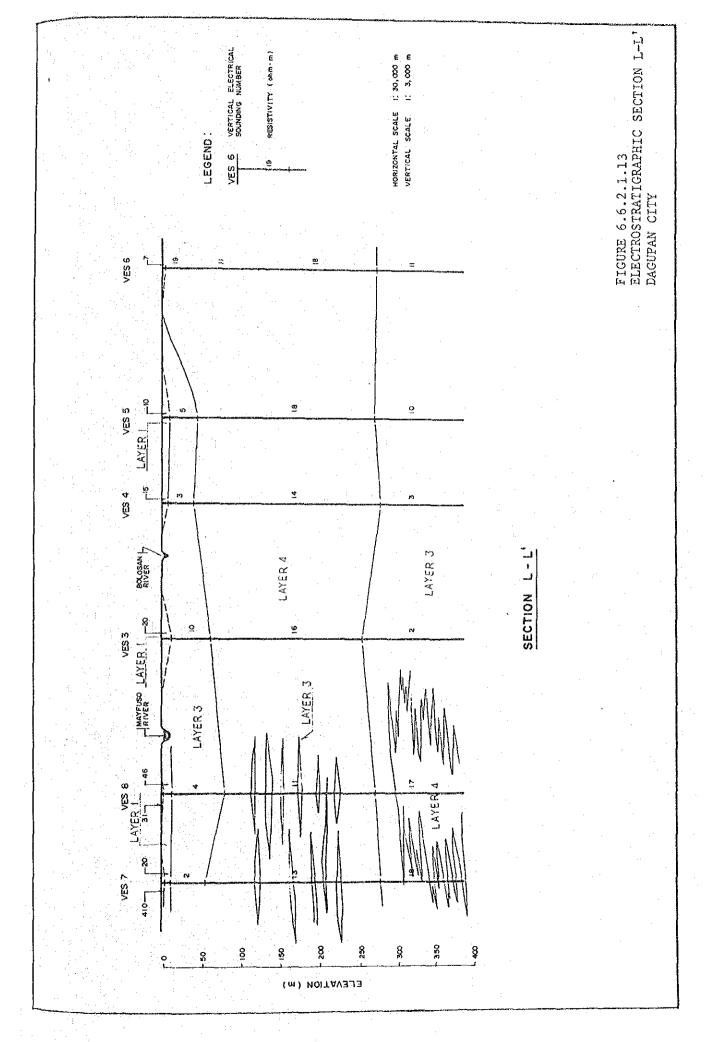


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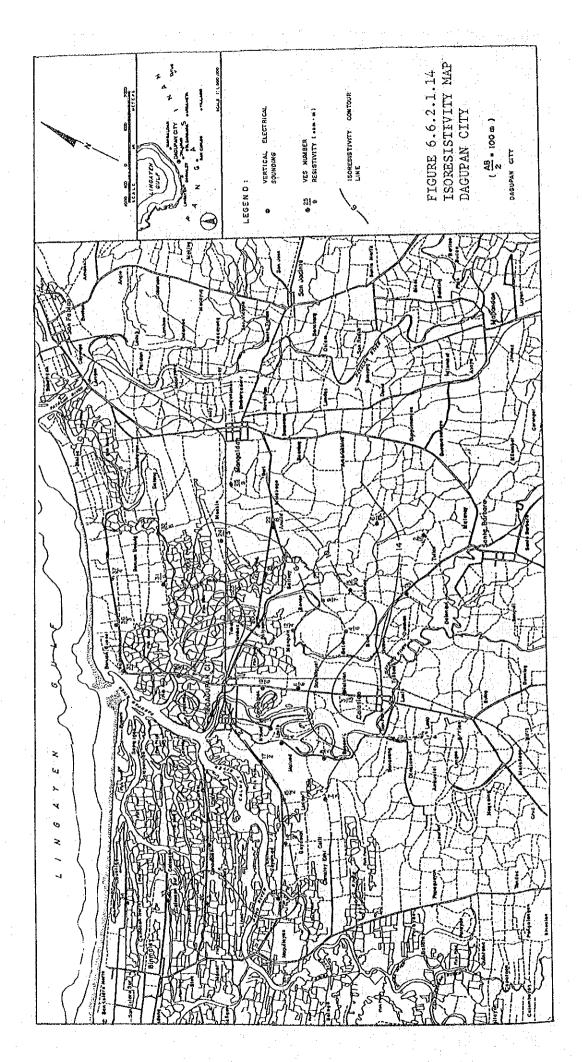


-53-

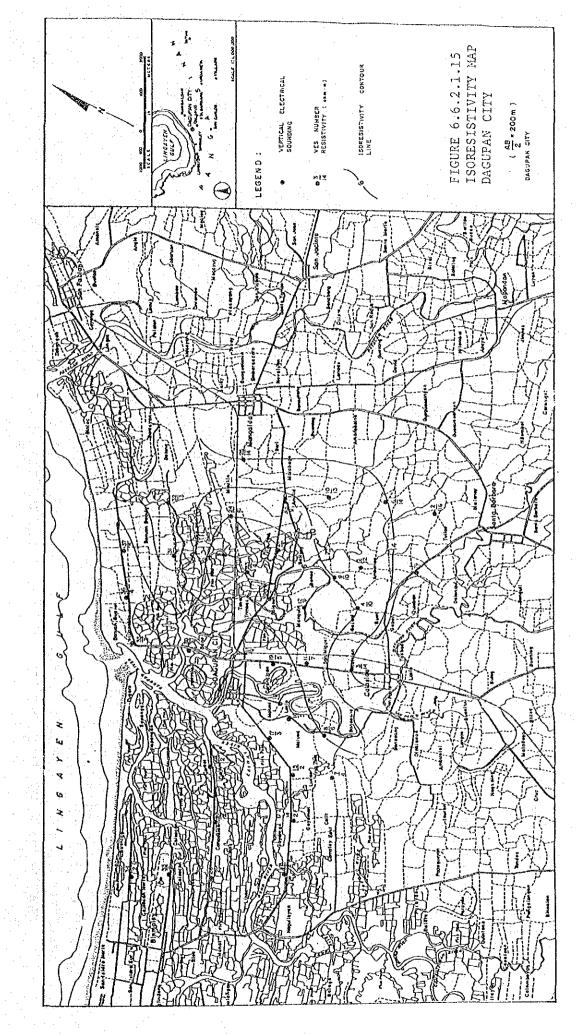




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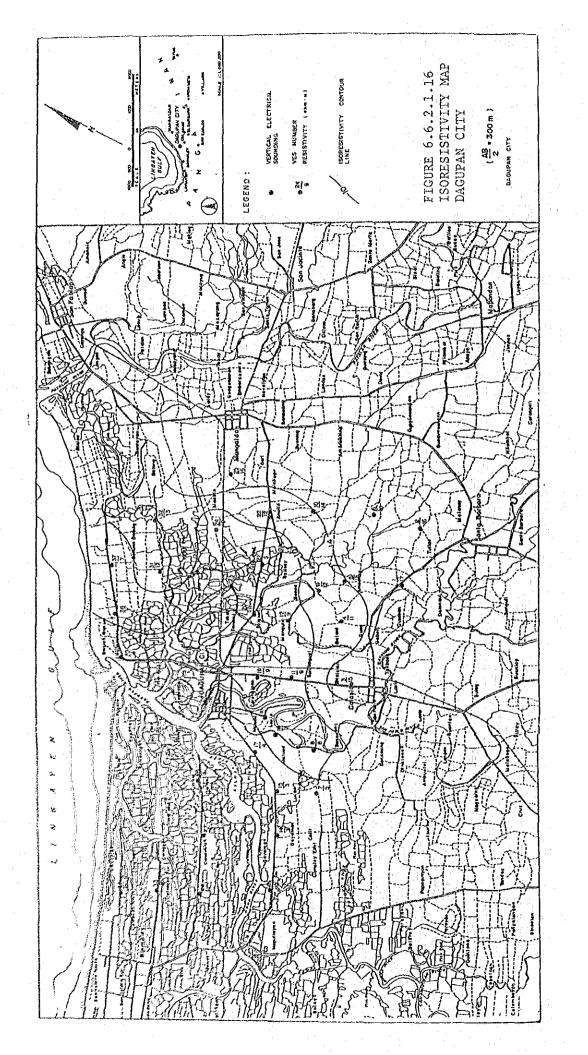


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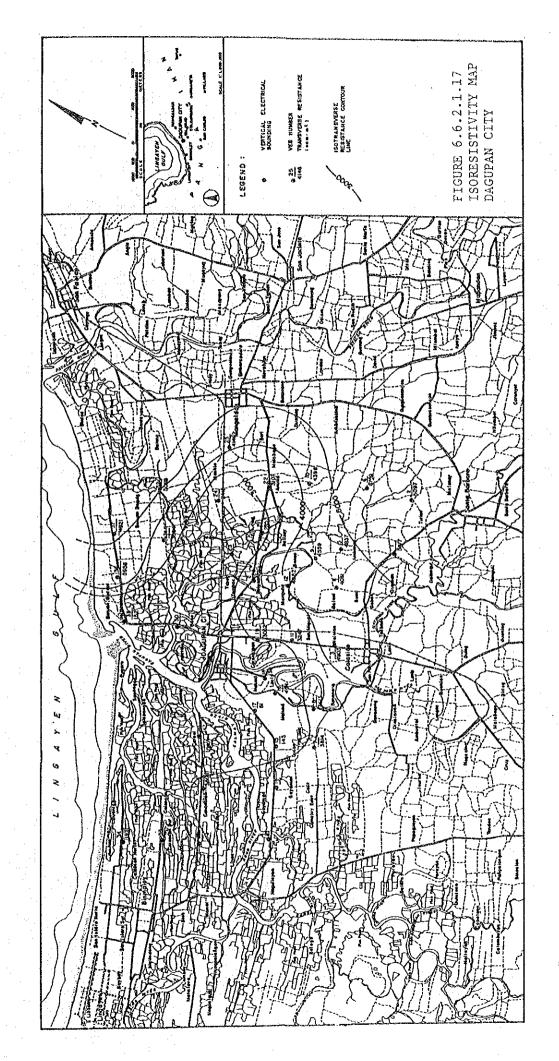


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### APPENDIX 6.7.1 WATER QUALITY EXAMINATION

(1) Objective

The objective of this survey is to evaluate the water quality of the existing sources. Furthermore, the survey is focused on the clarification of geochemical feature in relation to the hydrogeological conditions of the study area.

The examination result will be reflected in the prospective water supply plan.

(2) Implementation period

- 1) Preparatory work : July 26-27
- 2) Field examination : July 28
- 3) Sampling and laboratory analysis : July 28

(3) General Approach and Methodology

1) Sampling Points

Water samples were collected from the selected sampling points for physical, chemical and bacteriological examination.

Selection of sampling point

The sampling points were selected considering the following conditions:

- To cover all existing deep wells.

To evaluate the hydrogeological and geochemical features in the study area.

To determine the bacteriological quality of supplied water.

The selected sampling point were shown in TABLE 6.7.1.1 and FIGURE 6.7.1.1.

Item of Examination	Sample No.	Remarks
acterio- ogical xamina- ion	5       """No.         6       ""No.         7       "No.         8       ""No.         9       ""No.         10       ""No.         11       "No.         12       "No.         13       "No.         14       "No.	2, " 3, " 4, Pantal 5, Bgy IV 5, Herrera 7, Malued 3, Pantal 9, Caranglaan 10, Pantal 11, Pogo G. 12, Tapuac 14, Pantal 15, Malued 16, Pob. Oeste cte cao 7 I

TABLE 6.7.1.1 LOCATION OF SAMPLING POINT

2) Sampling and Pre-treatment

Water samples were collected and pretreated in such manner to correspond respective chemical constituents to be analyzed in the laboratory as follows:

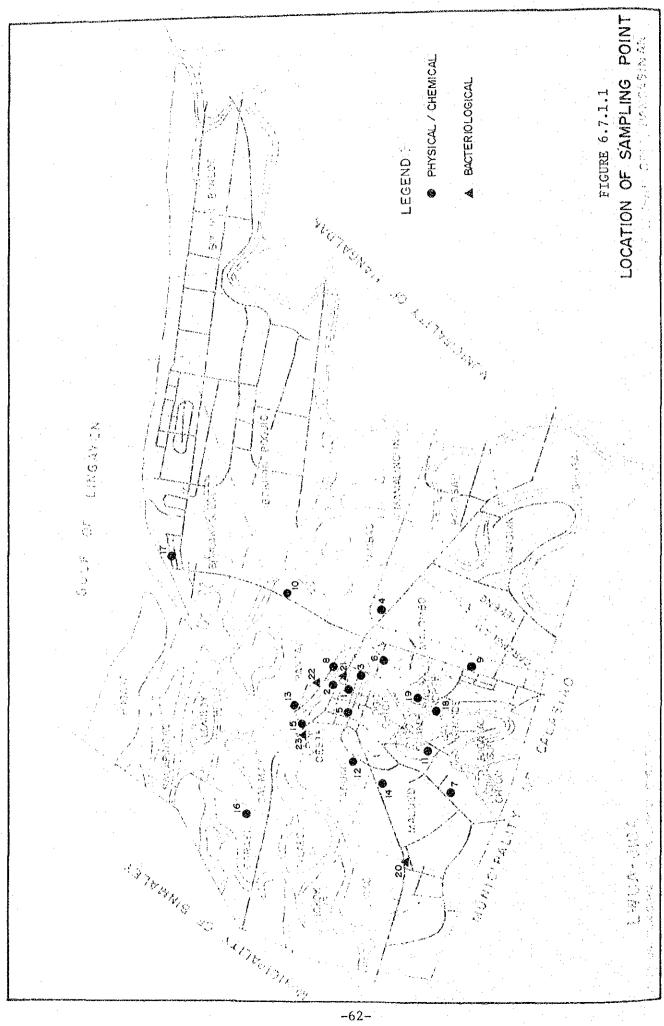
Sample Container / Pretreatment

Items to be analyzed

o 1,000 ml polyethylene bottle

Water Temperature, pH EC, TDS,  $Ca^{2+}$ ,  $Mg^{2+}$ Na<sup>+</sup>,  $\kappa^{+}$ ,  $So_4^{2+}$ ,  $Co_3^{2-}$ ,  $HCo_3^{-}$ ,  $C1^{-}$ ,  $Fe^{+}$ , Mn

(j



o 500 ml polyethylene bottle with 1 ml of conc. H2SO4 to maintain pH below 1.0

NH3-N, NO3-N, Fe<sup>+</sup>

o 100 ml predisinfected polye- Coliform Group Bacteria (MPN) thylene bottle

In addition to the chemical pretreatment, all the collected water samples in the respective polyethylene bottles were be kept in the black polyethylene bags with crushed ice to maintain water temperature below 4°C during the transportation to the laboratory.

3) Field Examination

Water temperature, pH and EC were measured in the field at the time of water sampling.

Implementation procedure

Since the collected water samples need to be delivered to the laboratory within 8 hours from the time of sampling, the water sampling was carried out in the early morning from 6:30 to 8:00 on 28 July, 1986. Thus the water samples were delivered to the Laboratory in Manila at 1:30 P.M.

(4) Result of water quality examination

The result of field and laboratory analysis is presented in TABLE 6.7.1.2.

The procedure of water quality analysis was based on the Philippine Standard Method for the Analysis of Air and Water (Volume 2).

(5) Discussion and conclusion

The following facts are obtained from the water quality analysis:

1) 7 samples out of 18 samples which were collected as drinking water sources excluding river water, are not satisfied with the National Standard for Drinking Water (NSDW).

2) Among those samples unsuitable to NSDW, three samples of P. S. No. 12, No. 16 and Deep Well (Crael) are also unsuitable for color.

3) The rest four samples of PS No. 6, No. 10, No. 14 and Shallow Well (Bacayao Norte) are unsuitable for Ca, C1 and TDS, or C1 and TDS.

4) pH range of the all samples is high. This can be recognized as the sign of sea water intrusion.

5) Turbidity of the samples is within the criteria of drinking water except for surface water sample.

6) All the samples of Fe and Mn contents are within the criteria of drinking water.

7) Sea water intrusion was expected for existing well No. 6, No. 10, No. 14 and Shallow Well of Bacayao Norte from the result of electric conductivity in the field examination. This matter was proved by the analysis of TDS, Na<sup>-</sup> and Cl<sup>-</sup>.

TABLE 6.7.1.2 WATER QUALITY ANALYSIS DAGUPAN CITY DAGUPAN CITY TDS PH EC AIK. Hard. Actd Na K Ca Mg CO3 HCO3 C1 So4 F11 Mm Co11-CO11- Temp. MALY (mg/1) (mg/1 108 (1/30) (DIU)

Sample Number and Location

	· ·	•									5									
	111 a	511.	n f 2	114	11u	110	TTT.	110	ndI.	.lla	110	112	772	- 11a	11¤	0.05	lla	110	nil	
	0.05	0.1	0.2	0.05	0.08	0.1 0	0.20	0.15	0.05	0.08	0.05	0.20	0.08	0.10	0,15	0.10	0.05	0.08	0.05	
	22.5	16.5	0	26.0	15.0	0-3 3	. 9. 0.	19.5	15.5	9	8.0	2.0	0.6	6.0	င် လ	2 0	25.5	7.0	2.0	
	27.9	18.7	18.6	18.6	23.2	928.8	27.9	18.6	32.5	390.1	27.9	13.9	598.9	27.9	62.7	34.8	13.9	32.5	301.8	
	¢.	~	<u>.</u>	۵,	•	ø	ė	۵,	ຕ່	358.7	÷	~	æ	a	ŝ	2	~	0	~	
	33.6	22.8	33.6	33.6	33,6	0	22.8	22.8	33.6	33.6	33.5	33.6		33.6	33.6	45.6	33.6	0	0	
•	۰.			·					1	14.6		÷					· •			
	- 1					÷.		1.14	1.1	26.8 ]										
	2.5	3.0	с. 8	3,2	о. С.	2.0	4.2 -	29	2.5	3.2	2.5.	1.2	5.0	2.4	2.0	3.9	3.5		4.0	
	67.5	50.0	49.0	54.5	73.5	525.0	.88.0	54.5	75.0	355.0	82.5	85.0	480.0	105.0	I12:5	138.0	41.0	18.5	300.0	
2	0	0	0	o	0	17	0	0	ò	o	ó	0	14	0	0	0	0	12	16	
2										127										•
		1		·	·					350		÷.								
	÷.	н	-	H		ř.	~		-1	5	Ä	Ř	<b>•</b> ••	2	Ä	m	Ā	-1	e.	
	367	324	348	351	328	2,710	408	373	440	1,800	427	400	2,760	251	546	364	241	067	1,590	
	8.12	7.98	8.04	7.58	7.85	7.29	7.97	7.86	7.81	7.45	8.12	8,65	7.09	8.04	.90*8	8.15	8.32	7.44	7.25	
	253	211	224	. 234	256	I. 656	280	224	288	1,152	307	288	1,792	333	371	460	179	320	986	
	0*49	0.63	.24.0	0.58	0.66	97-0	0.74	0.82	1.02	0.61	0.70	0.55	1.75	0.53	0,62	0,56	0.43	7.50	0.90	
	Pump Station #1	Pump Station #2	Pump Station #3	Pump Station #4	Pump Station #5	Pump Station 46	Pump Station \$7		Pump Station #9	Pump Station #10	Pump Station #11	Pump Station #12	5 Pump Station #14	e Pump Station #15	5 Pump Station #16	b Carael (BuP)	7 Bonuan Guesset (Spring)	3 Mayruso (River)	) Bacayao Norte (Shallow Well)	
•	ਜ :	r-i	'n	4	ŝ	4		ų.		ž	11	2	~	7	П	้		-1	ĥ	
				۰.																

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# Philippine National Standard for Drinking Water

Water Quality: Physical, Chemical and Radiological Requirements

**Bacteriological Quality Standards** 

		Requirements	the second second	
	Para	uneter	Maximum Pennissible level*	Minimum Requirements on Bacteriological Quality
-			_	
	Turbidity		5 units	
	Color		5 units (s) **	a) Chlorinated or Otherwise Disinfected Supplies
1.	Odor		Unobejctionable	
	Threshold odor number		Note more than 3	Efficient treatment culminating in chlorination or some
	Taste		Unobjectionable	other form of disinfection should yield a water free or any
	taste			coliform organism however polluted the original raw wate
	M		500 (s)	may have been. In practice it should not be possible to
	Total Solids	•	6.5 - 8.5	demonstrate the presence of coliform organisms in any
ł	pH		0.001	demonstrate the presence of conform organisms in any
	Phenolic substances			sample of 100ml. The efficacy of the purification proces
		C	3 pCi/1	and method of sampling should be looked into when
	Radioactive Subs.	Gross Alpha	•	sample of the water entering the distribution system
	а А. А. А	Gross Beta	30pCi/1	does not conform to this standard. In testing chlorinated
			0.05	uues not company to uus standard. In testing chommate
ļ	Trace Elements	Arsenic	0.05	water, presumptive positive tubes should always be sub
		Barium	1.0	jected to appropriate confirmatory tests.
1		Cadmium	0.01	
	·	Chromium	0.05	b) Non-disinfected Supplies
		Copper	1.0	() trom-disancered papping
		Cyanide	0.05	
		Fluoride	0.6	Where supplies of this sort exist, no water entering the dis
		Iron	1.0	tribution system should be considered satisfactory if i
		Lead	0.05	yields E coli in 100ml. If E. coli is absent, the presence of
ļ		Manganese	0.5 (s)	not more than 3 coliform organisms per 100ml may be
		Mercury	0.002	
	•	Selenium	0.01	tolerated in occasional samples from established non
1		-		disinfected pipes supplies, provided that they have been
		Zinc	5.0 (s)	regularly and frequently tested and that the catchment are
		- · ·		and storage conditions are found to be satisfactory. I
	Organic Cehmicals :	Synthetic	<u>.</u>	repeated samples show the presence of coliform organisms
		Detergents (MBAS)	0.5	
		Oil & Grease	Nil	steps should then be-taken to discover and, if possible, re
				move the source of pollution. If the number of coliform
	Persistent Pesticides :	Aldrin	0.001	organisms increases to more than 3 per 100ml, the supply
		DDT	0.05	should be considered unsuitable for use without disinfec
		Dieldrin	0.001	tion.
		Chlordane	0.003	tion.
		Endrin	0.0002	
1		Heptachior	0.0001	c) Individual or Small Community Supplies
		Lindane	0.004	
1		Toxaphane	0.005	Where supply of waters are individual wells, bores and
		Methoxychlor	0.1	springs everything possible should be done to preven
		2.4E	0.1	springs everynning possible shound be dolle to preven
		2,4,5T	0.01	pollution of the water. It should be possible to reduce
	bab	2,4, J I J	Nil	the coliform count of water from even a shallow well to
	PCB	<b>C</b> 1		less than 10 per 100ml. Persistent failure to achieve
	Other Chemicals :	Calcium	75	this, particularly if E. coli is repeatedly found, should
1		Chloride	200 (s)	
	· · ·	Magnesium	50 (s)	as a general rule lead to chlorination or boiling of the
1		Nitrate (NO <sub>3</sub> )	30	water for domestic consumption.
		Sulfate ·	200 (s)	
1		Hydrogen sulfide	0.05 (s)	

\* All units are in mg/2 unless, otherwise stated.

\*\* (s) - Secondary standards; compliance with the standard and analysis are not obligatory.

Excerpt from LWUA Methodology Manual

### F. COST COMPARISON

APPENDIX 7.1.1

### General

Anaylsis and evaluation of alternative are based largely on present-worth cost studies, taking into consideration the salvage values after the design period. Cost comparison is based on present worth of net disbursement during the period of 1980-2010 without any escalation factor applied to the 1980 unit prices.

If the differences between net PW cost of an alternative and that of the least-cost alternative is within the limit of cost estimating accuracy (10-15%) further cost comparison shall be made applying escalation factor to 1980 unit prices. For escalation rates, refer to Chapter VII-C: Escalation Rates. Moreover, non-economic parameters may also be influence the selection of the recommended plan.

### Construction Cost

Construction cost estimates of the proposed improvements are based on the projected July 1980 unit prices. All estimates on imported materials are based on an exchange rate of P7.40 per l US dollar. Further, it is assumed that no custom duty will be charged on items imported for the public water supply project. The cost of any facility to be replaced during the design period (1980-2010) is included under the capital cost for the particular year.

### Annual Cost

Annual costs are all costs associated with the maintenance, operation, and management of the project. These include labor, power, chemical and maintenance costs. These estimates are carried out for the period 1980-2010. The present-worth cost of annual expenditure is based on uniform and gradient series at a given interest.

Personnel and maintenance costs may abruptly increase as additional facilities are put into operation - e.g., the power cost at a pump station increases in relation to the daily pumpage of water.

### Salvage Value

The salvage values of facilities at the end of the design period 2010 are important in calculating net present worth of the total expenditures. It is assumed that the value of a facility depreciates linearly throughout its service life therefore, a facility with longer service life depreciates less than a facility with shorter service life (Refer to Table VI-1 for service life of different facilities). Moreover, a facility constructed at a later stage has higher salvage value than one constructed at an earlier stage.

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TABLE VI-1

# SERVICE LIFE CATEGORIES OF FACILITIES

Civil Works	Economic Life	Equipment	Economic Life
· · · · · · · · · · · · · · · · · · ·	30 years	Wells (pumping engine or motors)	15 years
Wells	50	Springs (vales, pipes)	50
Springs	50	Transmission (pipes, valves)	50
Iransmission Mains Storage Facilities	50	Storage (valves, pipes, level gauge, etc.)	50
Disinfection Facilities		Disinfection facilities (chlorinators, mech	
Distribution Mains	50	anical equipment and filter equipment	•
Internal Network	50	pipes, valves)	1.5
Service Connections	50	Distribution mains (pipes, valves)	50
fire Hydrants	50	Internal networks (pipes, valves)	50
perational Buildings	50	Service connections (meters, pipes)	50
peracionar bazzange		Operational buildings (workshop, etc.)	15
		Fire hydrants	30
		Vehicles	7

### Net Present Worth

The net present worth cost of an alternative scheme is the difference between the total present worth of capital cost and annual cost minus the present worth of salvage values.

For Construction Cost:  $C_{c} = C \times \frac{1}{(1+i)^{n}}$   $C_{c} = C \times \frac{1}{(1+i)^{n}} \times (1 - \frac{nx - n}{SL})$ 

For Annual Cost:

$$C_{c} = A_{c} \times \frac{1}{(1+i)^{n}}$$

where,

 $C_n$  = net present worth comparable cost

C = present worth of construction cost

 $C_s$  = present worth of salvage value (design year)

C = construction cost

SL = service life

i = discount rate

nx = number of years between design year and base year

n = number of years between year of construction and base year

A = annual cost

APPENDIX 7.2.1 ALTERNATIVE STUDY OF WATER INTAKE FACILITY 7.2.1.1. Hydraulic Simulation of Technical Alternatives

The infiltration gallery and the radial well are considered as the alternatives for water intake facility. To determine the design parameter of each facility, the following hydraulic simulation was carried out.

Radial Well

$$Q = x k x (H2 - h2)/In(R/r_{o})$$

where,

Q = planned yield; 5,400 cu.m/day

 $k = permeability coefficient; 5x10^{-4} m/sec$ 

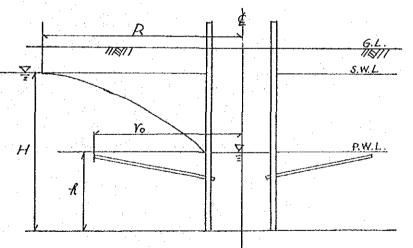
H = aquifer thickness; 15 m

h = effective aquifer thickness during pumping (m)

R = radius of influence area; 400 m

 $r_{o}$  = radius of radial collector (m)

H - h = drawdown (m)



Through the trial simulation of the above formula, the design parameter of the radial well was determined to be 9 m for the effective aquifer thickness and 15.5 m for the darius of radial collector. By these parameters, the planned yield is computed to be approximately 6,010 cu.m/day. Thus, four units of radial well can meet the required water demand.

# Infiltration Gallery

$$Q = k \times L \times (H^{2} - h_{o}^{2}) \times R^{-1} \times (t + 0.5 \times r_{o})/h_{o} \times \frac{4}{(2 \times h_{o} - t)/h_{o}}$$

where,

Q = planned yield; 5,400 2,880 cu.m/day

 $k = permeability coefficient; 5x10^{-4} m/sec$ 

L = length of gallery (m)

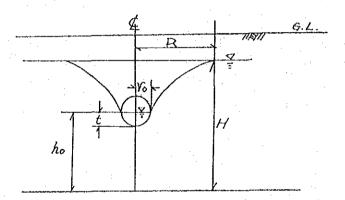
H = aquifer thickness; 15 m

 $h_o =$  height of gallery from the bottom of aquifer; 11 m

R = radius of influence area; 400 m

t = depth of water in gallery (m)

r = radius of gallery (m)



As well as the radial well, the design parameter of infiltration gallery was determined to be 1.5 m for both the depth of water in gallery and the radius of gallery, and 910 m for the gallery length. By these parameters, the planned yield is computed to be approximately 5,400 cu.m/day.

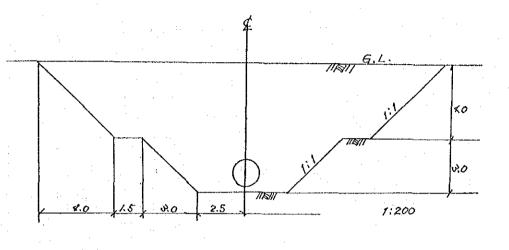
### 7.2.1.2. Cost Estimates

## Radial Well

The construction cost of the radial well is estimated to be approximately P1,240,000 per one unit, as shown in TABLE 7.2.1.1.

#### Infiltration Gallery

In order to install the infiltration gallery in the river bed, the volume of excavation and backfilling with relevant civil works is required. The following is a rough scketch of the cross-section of river bed excavation.



The given cross-section has an area of 96 sq.m. When 910 m of the required length of infiltration gallery is taken into account, the total excavation volume will be about 87,360 cu.m. At P103/cu.m of the unit cost for excavation, this work item will require at about P9.0million.

#### 7.2.1.3 Conclusion

In accordance with the above cost estimates, it is clear that the radial well is quite economical than the infiltration gallery.

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It e m         Description         Tet m         Description         Tet m         Description         Contrete Gatsson           1. Contrete Gatsson         1. Contrete Gatsson         57.0 m x 17.5 m(D)         x 1.0 m(D)					• • • •
Oncreate Gaissen         Kg         2,500         26           Steel Shoe         66,0 m(00) x 47,0 m(II) X 1.0 m(H) (t=6 mm)         Kg         2,500         26           Steel Shoe         67,0 m x 17.5 m(D)         87,0 m x 17.5 m(D)         21         23         103           Steerait         67,0 m x 17.5 m(D)         87,0 m (II) x 47.0 m(D)         x15.5 m(H)         cu.m         673         24           Steerait         67.0 m x 17.5 m(H)         67.0 m (II) x 1.5 m(H)         67         24         23         24           Obscreet         66.0 m(II) x 1.5 m(H)         67.0 m x 0.2 m(H)         10         1,110         23         24           (3.000 pst)         66.0 m x 67.0 m x 0.2 m(H)         67.0 m x 0.2 m(H)         10         1,110         24         24           (3.000 pst)         Cover with slabi g7.0 m x 0.2 m(H)         67.0 m x 9.2 m 0.3 m(A)         24         1,100         25         24           Cover with slabi g7.0 m for horizontal         12.5 m(H)         67.0 m x 9.2 m 0.3 m(A)         25         24         25         24         27           Reinforcement         20 k for every 1.0 cu.m of concrete         kg         46         1,100         25         24         27           Cover slabi 370         Cove		Unit	Q'ty	Unit Cost (Peso)	Cost (Peso)
Steel Shoe       66.0 m(CD) x 47.0 m(LD) x 1.0 m(H) (t=6 mm)       kg       2,500       26         Bispoor       07.0 m x 17.5 m(D)       47.0 m(CD) x 47.0 m(CD) x 18.5 m(H)       21       1,170       23       24         Disposit       6.0 m(CD) x 47.0 m(CD) x 18.5 m(H)       67.0 m(CD) x 17.5 m(H)       23       24         Material       67.0 m x 17.5 m(H)       67.0 m(CD) x 47.0 m(CD) x 13.5 m(H)       23       24         Material       67.0 m x 17.5 m(H)       20.0 m(CD) x 13.5 m(H)       23       24       23         (3,000 ps:)       Catsson:       66.0 m(CD) x 40.0 m(CD) x 18.5 m(H)       23       24       23       24       23         (3,000 ps:)       Cover with slab:       67.0 m x 0.3 x0.3 x0.3 x0.3 x2.3 x0.3 x0.3 x2.3 x0.3 x0.3 x0.3 x0.3 x0.3 x0.3 x0.3 x0					
Escaverion       67.0 m x 17.5 m(D)       24       24         Marenial       67.0 m x 17.5 m(D)       x 6.0 m(D) x 47.0 m(D)       x 8.5 m(H)       cu.m       673       24         Marenial       67.0 m x 17.5 m(H)       x 60.0 m(D)       x 15.5 m(H)       cu.m       673       24         Marenial       67.0 m x 17.5 m(H)       x 60.0 m(D)       x 15.5 m(H)       cu.m       673       24         Concrete       0.60.0 m(D)       x 1.0 m x 0.300.3x0.3x0.3       x 20       110       1,170       2         (3,000 pst)       cover with slub; 57.0 m x 10.0 u.m of concrete       3x0.300.3x0.3x0.3       x 20       110       1,170       2         Reinforcement       20 kg for every 1.0 u.m of concrete       3x0.300.3x0.3x0.3       x 20       110       1,170       2         Steel Mar       20 kg for every 1.0 u.m of concrete       3x0.300.3x0.3x0.3x0.3x0.3x0.3x0.3x0.3x0.	$\sim$	kg	2,500	26	65,000
<pre>67.0 m x 17.5 m(H) 67.0 m x 17.5 m(H) Caisson: 66.0 m(ID) x 1.5 m(H) for wall Caisson: 66.0 m(ID) x 1.5 m(H) for anchor 66.0 m(ID) x 1.5 m(H) for anchor Cover with siab: 67.0 m x 0.2 m(H) Cover with siab: 67.0 m x 0.2 m(H) Cover with siab: 67.0 m x 0.2 m(H) Cover visits 66.0 m x 0.2 m(H) Cover visits 67.0 m vertical Cover visits 756 110 Cover visits 75 mm x 3 m (A12 mm, 400 holes) x 2 pcs. x 48 collectors  1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2</pre>		cu.m	673	103	69,320
Caisson: 66.0 m(ID) x 1.5 m(H) for wall cu.m 231 1,170 2.1 (100 x 0.2 m(H) for wall cover with slab: 97.0 m (OD) x 1.5 m(H) for wall cover with slab: 97.0 m x 0.2 m(H) for wall cover with slab: 97.0 m x 0.2 m(H) for wall cover vith slab: 97.0 m x 0.2 m(H) for wall cover vith slab: 97.0 m x 0.2 m(H) for wall cover vish of 0 m x 07.0 m) x 1.8.5 m(H) 20 kg for every 1.0 cu.m of concrete caisson: (66.0 m x 07.0 m) x 1.8.5 m(H) cover vish i 0.3 x(0.90 x4x1.7 x4) x4 for vertical cover vish i 0.3 x(0.90 x4x1.7 x4) x4 for vertical cover vish i 0.3 x(0.90 x4x1.7 x4) x4 for vertical cover vish i 0.3 x(0.90 x4x1.7 x4) x4 for vertical cover vish i 0.3 x(0.90 x4x1.7 x4) x4 for vertical cover vish i 0.3 x(0.90 x4x1.7 x4) x4 for vertical cover vish i 0.3 x(0.90 x4x1.7 x4) x4 for vertical cover vish i 0.3 x(0.90 x4x1.7 x4) x4 for vertical cover vish i 0.3 x(0.90 x4x1.7 x4) x4 for vertical cover vish i 0.3 x(0.90 x4x1.7 x4) x4 for vertical cover vish i 0.3 x(0.90 x4x1.7 x4) x4 for vertical cover vish i 0.3 x(0.90 x4x1.7 x4) x4 for vertical cover vish i 1.3 m v 3.5 m (A12 mm, 400 holes) x 2 pcs. x 48 collectors m 144 270 cit vish i 1.60 pcs. 48 1,300 cit vish m x 3.5 m (blank) x 48 collectors m 144 270 cit vish m x 3.5 m (blank) x 48 collectors m 144 270 cit vish m x 3.5 m (blank) x 48 collectors m 144 270 cit vish m 168 1,100 cit vish m x 48 1,300 pcs. 48 1,300		田・ コン	673	24	16,150
Cover with slab: $67.0 \text{ m} \times 0.2 \text{ m}(H)$ + (0.3x0.3x4.8x4 - 0.3x0.3x2) cu.m 10 1,170 20  kg for every 1.0 cu.m of concrete 20  kg for every 1.0 cu.m of concrete $20 \text{ caisson: (66.0 \text{ m} \times 67.0 \text{ m}) s m (7.0 \text{ m}) s $	φ7.0 m(OD) x 18.5 m(H) for wal 1.5 m(H) for anchor			1,170	270,270
<pre>20 kg for every 1.0 cu.m of concrete 20 kg for every 1.0 cu.m of concrete 20 kg for every 1.0 cu.m of concrete 21 cover/slab: d7.0 m for horizontal 29 140 20 cover/slab: d7.0 m for horizontal 29 140 20 cover/slab: d7.0 m for horizontal 21 2 2 54 cf for mx 3 m (d12 mm, 400 holes) x 2 pcs. x 48 collectors 29 144 270 cf; d75 mm x 3 m (d12 mm, 400 holes) x 2 pcs. x 48 collectors 29 144 270 cf; d75 mm x 3 m (d12 mm, 400 holes) x 48 collectors 29 144 270 cf; d75 mm x 3.5 m (blank) x 48 collectors 20 144 270 cf; d75 mm x 3.5 m (blank) x 48 collectors 29 144 20 675 mm 61; d75 mm x 3.5 m (blank) x 48 collectors 20 675 mm 61; d75 mm x 48 collectors 2 676 116 2 59 of Total of Item 1 &amp; 2 59 of Total of Item 1 &amp; 2 </pre>	m x 0.2 m(H) .3x0.3x4.8x4 - 0.3x0.3x0.3x2)			1,170	11,700
Cafsson: (d6.0 m x d7.0 m) x 18.5 m(H) sq.m 756 110 Cover/slab: d7.0 m for horizontal Cover/slab: d7.0 m for horizontal 0.3x(0.90x4x1.7x4)x4 for vertical gq.m 29 140 0.3x(0.90x4x1.7x4)x4 for vertical gq.m 29 140 13 110 GI, d75 mm x 3 m (d12 mm, 400 holes) x 48 collectors m 288 270 GI, d75 mm x 3.5 m (blank) x 48 collectors m 144 270 GI, d75 mm x 3.5 m (blank) x 48 collectors m 144 270 GI, d75 mm x 3.5 m (blank) x 48 collectors m 288 270 GI, d75 mm x 3.5 m (blank) x 48 collectors m 288 270 GI, d75 mm x 3.5 m (blank) x 48 collectors m 288 270 GI, d75 mm 288 2,500 GI, d75 mm 144 270 GI, d75 mm 144 270 GI, carson Wall, t=0.5 m Radial Well, 12 m x 48 collectors m 288 1,500 Caisson Wall, t=0.5 m Radial Well, 12 m x 48 collectors m 2576 1,160 Caisson Wall, t=0.5 m Radial Well, 12 m x 48 collectors m 2576 1,160 Caisson Mall, t=0.5 m Caisson Vall, t=0.5 m Caisson Vall	u.m of concrete	Å	4.820	15	72,300
Cover/slab: \$7.0 m for horizontal       sq.m       29       140         1       0.3x(0.90x4x1.7x4)x4 for vertical       sq.m       29       140         1       0.3x(0.90x4x1.7x4)x4 for vertical       sq.m       29       140         1       61, \$75 mm x 3 m (\$12 mm, 400 holes) x 2 pcs. x 48 collectors       m       288       270         cl, \$75 mm x 3 m (\$12 mm, 300 holes) x 48 collectors       m       144       270         cl, \$75 mm x 3.5 m (\$12 mm, 300 holes) x 48 collectors       m       144       270         cl, \$75 mm x 3.5 m (\$12 mm) x 48 collectors       m       144       270         cl, \$75 mm x 3.5 m (blank) x 48 collectors       m       168       180         cl, \$75 mm x 3.5 m (blank) x 48 collectors       m       168       180         cl, \$75 mm x 3.5 m (blank) x 48 collectors       m       168       180         cl, \$75 mm x 3.5 m (blank) x 48 collectors       m       168       168         \$75 mm       875 mm       m       168       168         \$75 mm       \$76       1,160       1,160       1,160         \$76       1,200       m       576       1,160       1,160         \$75       \$76       1,160       m       1,160       1,160	.0 m) x 18.5 m(H)	EL OS		OII	83,160
1       1         61, 475 mm x 3 m (412 mm, 400 holes) x 2 pcs. x 48 collectors m       288       270         61, 475 mm x 3 m (412 mm, 300 holes) x 48 collectors m       144       270         61, 475 mm x 3.5 m (512 mm, 300 holes) x 48 collectors m       144       270         61, 475 mm x 3.5 m (512 mm, 300 holes) x 48 collectors m       144       270         61, 475 mm x 3.5 m (512 mm, 48 collectors m       144       270         61, 675 mm x 48       168       180         67, 675 mm x 1.5 m (512 m, 48       1,340         675 mm       pcs.       48       1,340         675 mm       pcs.       48       1,340         875 mm       pcs.       48       1,500         84dial Well, 12 m x 48       1,340       pcs.       48       1,500         1.6.2       1.12 m x 48       1,160       m       576       1,160         2       1.6.2       m       576       1,160       1         3       1.6.2       1.16.2 </td <td></td> <td>₽°DS SG*</td> <td></td> <td>011 071</td> <td>4,060 1,430</td>		₽°DS SG*		011 071	4,060 1,430
<pre>GI, \$75 mm x 3 m (\$12 mm, 400 holes) x 2 pcs. x 48 collectors m 288 270 GI, \$75 mm x 3 m (\$12 mm, 300 holes) x 48 collectors m 144 270 GI, \$75 mm x 3.5 m (blank) x 48 collectors m 144 270 GI, Cap, \$75 mm 168 180 pcs. 48 30 pcs. 48 1,340 pcs. 48 1,340 pcs. 48 1,340 pcs. 48 1,500 m 576 1,160 m 576 1,160 m 576 1,160 m 576 1,160 </pre>	:	•			593,390
Pipe GI, 075 mm x 3 m (012 mm, 400 holes) x 2 pcs. x 48 collectors       m       288       270         GI, 075 mm x 3. m (012 mm, 300 holes) x 48 collectors       m       144       270         GI, 075 mm x 3.5 m (012 mm, 300 holes) x 48 collectors       m       144       270         GI, 075 mm x 3.5 m (012 mm, 300 holes) x 48 collectors       m       144       270         GI, 075 mm x 3.5 m (012 mm, 300 holes) x 48 collectors       m       144       270         GI, 075 mm x 3.5 m (012 mm) x 48 collectors       m       168       180         c v5 mm x 3.5 m (012 mm) x 48 collectors       m       168       130         e 075 mm       075 mm       pcs.       48       1,340         pper 075 mm       756 mm       1,160       1,160       1,160         Item 2       Item 2       m       576 1,160       1,160       1,160         S% of Total of Item 1 & 2       5% of Total of Item 1 & 2       m       576 1,160       1,160       1,160					
CI, \$75 mm x 3 m (\$12 mm, 300 holes) x 48 collectors       m       144       270         CI, \$75 mm x 3.5 m (blank) x 48 collectors       m       168       180         CI, \$75 mm x 3.5 m (blank) x 48 collectors       m       168       180         CI, \$75 mm x 3.5 m (blank) x 48 collectors       m       168       180         cI, \$20, \$75 mm x 3.5 m (blank) x 48 collectors       m       168       180         cI, \$Cap, \$75 mm x 3.5 m (blank) x 48 collectors       pcs.       48       1,340         pper \$75 mm x 48 collectors       pcs.       48       1,500         I caisson Wall, t=0.5 m       pcs.       48       1,500         I caisson Wall, ti2 m x 48 collectors       pcs.       48       1,500         Item 2       ftem 1       576       1,160       1,160         S% of Iotal of Item 1 & 2       5% of Iotal of Item 1 & 2       1.       1.			288	270	77,760
GI, \$75 mm x 3.5 m (blank) x 48 collectors       m       168       180         GI, Cap, \$75 mm       \$75 mm       30       9cs.       48       2,690         *       \$75 mm       pcs.       48       1,340       9cs.       48       1,340         *       \$75 mm       pcs.       48       1,500       9cs.       48       1,500         *       \$76       \$1,160       m       576       1,160       1.160       1.160         Item 2       *       \$56       ftem 1 & 2       *       \$576       1,160       1.160         S% of Total of Item 1 & 2       *       \$56       ftem 1 & 2       1.160       1.1       1.160       1.1	300 holes)		144	270	38,880
CI, Cap, 075 mm       30         * 075 mm       pcs.       48       2,690         pper 075 mm       pcs.       48       1,340         l       Caisson Wall, t=0.5 m       pcs.       48       1,500         l       Caisson Wall, t=0.5 m       pcs.       48       1,500         l       Caisson Wall, t=0.5 m       pcs.       48       1,500         l       Ltem 2       m       576       1,160       1.         Item 2       *       *       556       1,160       1.         S% of Ictal of Item 1 & 2       *       *       1.       1.	x 48 coll	<b>E</b>	1.68	180	30,240
<pre>&gt;</pre>		bcs.		30	1,440
<pre>pper \$75 mm 1 Caisson Wall, t=0.5 m 1 Caisson Wall, t=0.5 m 2 Kadial Well, 12 m x 48 collectors 1 Kadial Well, 12 m x 48 collectors 1 1.500 1 2. 2 5% of Total of Item 1 &amp; 2 5% of Total of Item 1 &amp; 2 2 5%</pre>		pcs.		2,690	129,120
<pre>1 Caisson Wall, t=0.5 m Radial Well, 12 m x 48 collectors</pre>	· · ·	bcs.		I,340	64,320
<u>Item 2</u> ITEN 1 & 2 5% of Total of Item 1 & 2 <u>1</u>	t +8 collectors	hole B	•	1,160	72,000 668,160
ITEN 1 & 2 5% of Total of Item 1 & 2				÷	1,081,920
5% of Total of Item 1 & 2				· · ·	1,675,310
					83,765
				· · ·	1,759,075

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APPENDIX 7.2.2 DATA ON THE UNIT COST FOR ESTIMATION OF PROJECT COST

(1) Deep Well Construction : Peso

Depth (m)	Casing size (m/m)	Cost
200	250	940,000
200	300	1,160,000
250	150	640,000

#### BREAKDOWN OF COSTS IN %

		Local Comp	onent	]	FEC	
	Material	La	bor	Direct	Indirect	Total
		Skilled	Unskilled	DILCCC	mulleet	IUCax
Equipment	17		· · ·			
Civil Works	33	8	5	-	20 17	63
Total	50	8 8	5	•	37	100

(2) Deep Well Pump Station (Electric Motor Drive) : Thousand Peso

KW	1 <sup>1</sup>	Cost
7		450
15		560
22		640
29		720
37		790
44		840
51	÷.,	890
59		960
66		1,020
74		1,080

#### BREAKDOWN OF COSTS IN %

••••••••••••••••••••••••••••••••••••••	i	ocal Comp	onent	]	FEC	
Material	Material	La	bor	Direct	Indirect	Total
	Skilled	Unskilled		· 		
Equipment	9			42	5	56
Civil Works	21	9	. 5	-	9	44
Total	30	9	5	42	14	100

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#### (5) Pipeline Cost

Following pipe materials are presently available in the Philippines:

- GI (galvanized iron),

- PE (poly-ethylene),

- PB (poly-butylene),

- PVC (poly-vinyl-chloride),
- SP (steep pipe),
- CI (cost iron), and
- AC (asbestos cement).

Among these materials, the use of CI pipe is limited due to its high cost and AC pipe is also rare by safety reason.

Followings are comparison of unit cost at the 1985 price level.

				(Unit: ₽/	m) -
Diameter(mm)	GI	PE	PB	PVC	SP
13	20.8	13.8	9.1	-	
19	24.7	19.9	13.6	· · · - ·	
25	32.3	25.3	22.0	-	<del>-</del> . '
38	59.2	41.5	44.7		-
50	87.5	61.4	76.4	33.9	· ·
63	117.7	-0		48.0	· · · ·
75	180.3		<del></del>	81.3	
100	230.8	-		122.4	235.0
150	<b></b>	·		256.9	250.0
200		<b></b> ·		506.5	290.0
250		-	- · · ·		315.0
300	·	·. +		-	425.0
400	· _	<u> </u>		· · · ·	520.0
500	-				700.0
600					890.0

Based on the above comparison, SP is advantageous for the diameter of 200 mm and above than PVC. Thus, for the cost estimates of major transmission and distribution pipes, SP is considered for diameter of 200 mm and above, while PVC for diameter of less than 150 mm taking into account the transportation cost and easy installation.

#### (3) Booster Pump Station

$$C = (72.16 - 13.68 \log Q) \times Q^{(0.42 + 0.1 \log Q)}$$

$$(6/H - 0.25)$$
  
x H<sup>0.305(log Q - 0.7)</sup>

where,

C = cost for electric motor drive (thousand peso)

 $Q = design \ capacity \ (1/sec)$ 

H = total dynamic head (m)

#### BREAKDOWN OF COSTS IN %

	1	Local Comp	onent	l	F E C	
an an Arran an Arran Arran an Arran an Arr	Material	La	Labor Dire		Indirect	- Total
		Skilled	Unskilled	DIICOU	Indriget	·
Equipment	11			53	2	66
Civil Works	17	9	6		2	34
Total	28	9	6	53	4	100

(4) Radial Well

Inner Diameter(m)	Inner Depth (m)	Collection Pipe Length (m/hole)	Unit Cost (₽)
5	10	7.5	1,240,000
6	16	12.5	1,760,000

#### BREAKDOWN OF COSTS IN %

	l I	Local Comp	onent	]	FEC	
	Material	La	bor	- Direct	Indirect	Total
Matel 1a1	Skilled	Unskilled		· · · · · · · · · · · · · · · · · · ·		
Equipment	1		—	18	1	20
Civil Works	25	2	2	~	51	80
Total	2.6	2	2	18	52	100

Diameter (mm)	Unit Cost (P/m)
150 (PVC)	410
200(SP)	520
250(")	630
300(")	7,60
350(")	900
400(")	970
450(")	1,160
500(")	1,330
600(")	1,600
700 ( ")	1,910

Source : LWUA Design Dept.

			So	urce : LWUA	A Design Dep	τ.
						· · · · ·
		BREAKDOWN	OF COSTS	IN Z		n di si Santari Santari
	·····	Local Comp	onent	]	FEC	
	Material	La	ibor	Direct	Indirect	Total
	HILDEL LUL	Skilled	Unskille			
Equipment	23	:	_	4	27	54
Civil Works	17	7	4	÷	18	46
Total	40	7	4	4	45	100
· · · · · · · · · · · · · · · · · · ·	·······					

(6) Valve In-place Cost

Diameter (mm)	Gate Valve (₽)	Butterfly Valve (P)
50	1,700	•••
75	2,900	
100	3,900	س
150	5,300	*a
200	6,700	in an
250	11,200	ante en la companya de la companya Esta de la companya d
300	, <del></del> .	34,800
350		74,400
400		95,200
450	a da ang ang ang ang ang ang ang ang ang an	125,900
500		174,000
600		243,600
700	-	313,200

Source : LWUA Design Dept. 

## BREAKDOWN OF COSTS IN %

		Local Comp	onent	]	FEC	· · ·
Material	Labor		Direct	Indirect	Total	
		Skilled	Unskilled	DITECT	INGLIECE	IUCAL
Equipment Civil Works	9	- 3	- 6	63	5	77
Total	21	3	6	63	7	100

(7) Internal Network

(/) Internat Network			
Population Density	Total Length of	Unit Co	st (₽/ha)
	Pipeline	Diameter	Diameter
(Person/ha)	(m/ha)	(100/150)	(75/100)
50	64	18,300	14,900
60	67	19,300	15,700
75	72	20,900	16,800
100	80	23,100	18,700
150	90	25,700	21,000
200	100	28,300	
250	108	30,400	· •••
300	116	32,500	<del>-</del> .
and the second			

# BREAKDOWN OF COSTS IN %

	I	Local Component		I	F E C	_
	Material	Labor		Direct	Indirect	Total
an a	Hatel Lai	Skilled	Unskilled			
Equipment Civil Works	22 17	 7	- 4	7	27 16	56 44
Total	39	7	4	7	43	100

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## (8) In-place of Service Connections

and the second sec		TTI to be Noted and	Meters
Diameter (inch)	Without Meter ₽/unit	With Meter ₽/unit	₽/unit
1/2	450	810	400
5/8 - 3/4	520	1,280	880

SERVICE CONNECTION WITHOUT METER

#### BREAKDOWN OF COSTS IN %

			1			
		Local Comp	onent	F	ЕС	_
	Material	La	bor	- Direct	Indirect	Total
	nateriar	Skilled	Unskilled			
Equipment	9		_	60	2.5	71.5
Civil Works	17	3	6		2.5	28.5
Total	26	3	6	60	5	100

SERVICE CONNECTION WITHOUT METER BREAKDOWN OF COSTS IN %

	Local		al Component		FEC	
	Material	La	bor	Direct	Indirect	Total
	114002241	Skilled	Unskilled.			
Equipment Civil Works	4			83	2 1	89 11
Total	10	- 1	3	83	3	100

(9) Fire Hydrant In-place Cost

Type	<u>Size (mm)</u>	Unit Cost (₽)
Commercial	150	16,800
Residential	100	9,400

BREAKDOWN OF COSTS IN %

	:						
	]	Local Comp	onent	F	F E C		
	Material	La	bor	- Direct	Indirect	Total	
		Skilled	Unskilled	PIICUL			
Equipment	8			57	<b>5</b>	70	
Civil Works	10	8	10	· · · · ·	2	30	
Total	18	8	10	57	7	100	

#### (10) Elevated Tank/Ground Reservoir

Elevated Tank:  $C = 0.615 \text{ H}^{1.144} \text{v}^{0.749}$ Ground Reservoir:  $C = 20.05 \text{ v}^{0.639}$ 

where, C = cost (thousand peso)

H = overflow elevation above ground level

V = storage volume (cu.m)

BREAKDOWN OF COSTS IN %

	]	Local Component		F E C		
	Material	Material Labor		- Direct	Indirect	Total
	in corrue	Skilled	Unskilled	Direct in		iotar
			· · · · · · · · · · · · · · · · · · ·		~~~~~~	
Equipment	. 4		-	3	2	9
Civil Works	53	- 5	7	_	26	91
Tota1	57	5	7	3	28	100

(11) Gas Chlorinator In-place Cost

Туре	Water Flow Condition	Maximum Chlorine Feed (kg/day)	Unit cost $\frac{1}{(P)}$
I-A	constant	22	98,100
I-B	constant	45	119,100
II-A	Variable	22	147,700
II-B	Variable	45	169,300
			and the second

1/ Empty gas cylinders and automatic switchover include

TYPE I-A, I-B BREAKDOWN OF COSTS IN %

	Local Component			F	EC	•
	Material	La	Labor		Indirect	Total
		Skilled				
Equipment	15			41	5	61
Civil Works	25	б	3	-	5	39
Total	40	б	3	41	10	100

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#### TYPE II-A, II-B BREAKDOWN OF COSTS IN %

	]	Local Comp	onent	FEC		<b>—</b>
	Material	La	bor	Direct	Indirect	Total
	Material	Skilled	Unskilled			
Equipment	21	· · · · · · · · · · · · · · · · · · ·	- -	53	2	76 24
Civil Works Total	12	6	2	53	6	100

#### (12)

## Administration & Operation Building

Future Service Population	Administration Bldg. (Thousand Peso)	Operation Center (Thousand Peso)
30,000	1,000	810
40,000	1,110	890
50,000	1,220	990
60,000	1,320	1,090
70,000	1,410	1,180
80,000	1,500	1,280
100,000	1,610	1,380
110,000	1,820	1,590
-		

#### ADMINISTRATION BUILDING BREAKDOWN OF COSTS IN %

:						····
	]	Local Comp	onent		FEC	<b>_</b> '.
	Material	La	bor	- Direct	Indirect	Total
	Flateriar	Skilled	<b>Unskilled</b>	Direct		
Equipment	20			- ·	16	36 64
Civil Works Total	42 62	7	5		26	100

#### OPERATION CENTER BREAKDOWN OF COSTS IN %

DREARDOWN OF GOSTS IN &

	Local Component FEC							
	Material	Labor	• Direct	Indirect	Total			
	·····	Skilled Unskilled						
	<u> </u>							
Equipment	14		30	6	50			
Civil Works	26	10 5	· · · ·	9	50			
Total	40	10 5	30	15	100			

(13) Energy Cost

$$C = Np x h x Pu x (Em)^{-1}$$

$$Np = Q \times g \times H \times (Eff. \times 1,000)^{-1}$$

where,

C = cost (thousand peso) Np = pump power demand (kw) h = hours of operation P = unit power cost (P/kwH) E<sup>U</sup> = motor efficiency (0.85) Q<sup>m</sup> = water pumped (kg/sec) g = gravity constant (9.81m/sq.sec) H = manometric head (m) Eff.= pump efficiency (average = 0.70)

(14) Chemical Cost

C = (Annual Water Demand) . D .  $U_{CL} \times 10^{-3}$ where, C = annual cost for chlorine (P) D = chlorine dosage (mg/l)

 $^{U}$ CL= unit cost of chlorine gas (P/kg)

(15) Minimum Cost Diameter

Following cost function is applied to determine the most economical diameter of pipelines that are not simulated by the network analysis.

Dmin. = 187.7  $Q^{0.486} C^{-0.315} (Ec/0e)^{0.17}$ where, Dmin. = minimum cost diameter Q = water flow (1/sec) C = "C" value (Hazen William Formula) Ec = energy cost (P/kwh)

Oe = overall efficiency

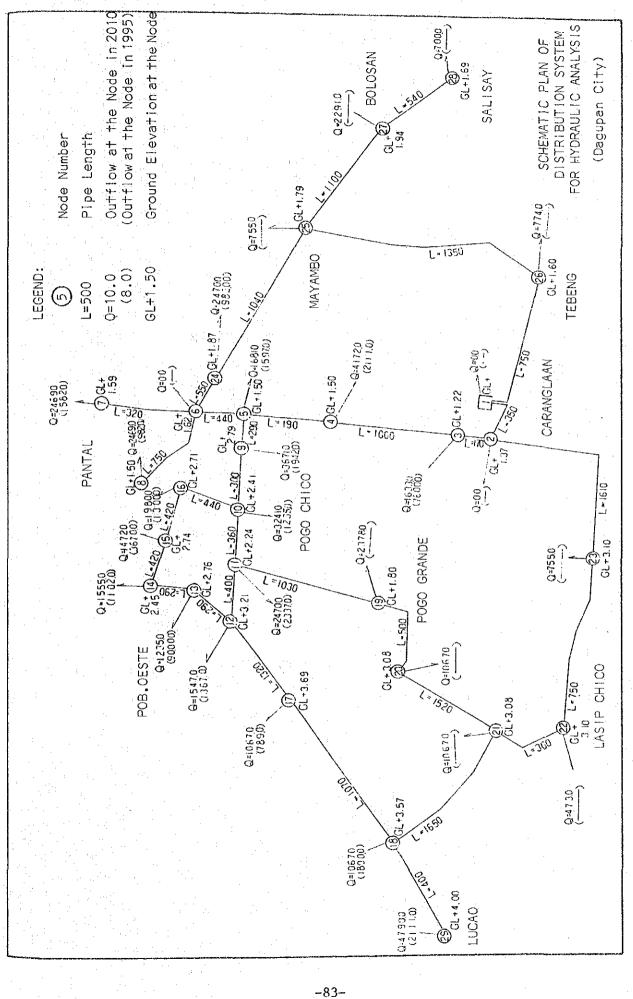
### APPENDIX 7.3.1 COMPUTER-AIDED HYDRAULIC ANALYSIS OF DISTRIBUTION SYSTEM (Dagupan City)

o List of Computed Cases

1. A.	
-A	(1995, 2010)
)-A	(Fire at LUCAO/2010)
-В	(1995, 2010)
	-A

#### o Note

This appendix shows the results of Hydraulic Analysis aided by the computer. The distribution network is shown in the figure of following page. The nodes, however, with no flow and 20.00 m in Dynamic Head was treated as a dummy node. Those nodes can be ignored and have no relation to the computation results.



ALTERNATIVE D-A (Recommended Plan, Single Pipeline Alignment) Year 1995

<< NODES >>

STATIC HEAD (m)	0.300,000,000,000,000,000,000,000,000,00
DYNAMIC HEAD (m)	
Н.G.L. ЕLEV. (m)	00000000000000000000000000000000000000
FLOW (cu.m/day)	21100000000000000000000000000000000000
GROUND ELEV (m)	8
NODE No.	-0040000000000000000000000000000000000

0.00.25

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-1005. -1372. 2300.

420 420.

300.

200000

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10-15-00-00 23333 10-15-00-1-0

40-0000000000

HEADLOSS (m) (0/00)

FLOW VEL: (cu.m/day)(m/sec)

. ≩ບ

LENGTH (m)

DIA.

NODE No.

Pipe No.

<< PIPELINE >>

-20159. 20159. 20083.

350. 1900 6

700. 600.

88888

ALTERNATIVE D-A (Recommended Plan, Single Pipeline Alignment) Year 1995

-84-

lteration Times : 11

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N. A	STATIC HEAD (m)	8338853585858583875335586793888588 83388583838585838753355222732388585
	DYNAMIC HEAD (m)	orradona and a strain
• B	H. G. L. ELEV. (m)	00004000 00004000 000040004000400040004
~	FLOW (cu.m/day)	0.00 153.00 153.00 153.00 155.00 2459.00 2
NODES >	GROUND ELEV. (m)	8
Z V V	NODE NCCE	

ALTERNATIVE D-A (Recommended Plan, Single Pipeline Alignment) Year 2010 .

tî.

Iteration limes :

ശ

~85-

ALTERNATIVE D-A (Recommended Plan, Single Pipeline Alignment) Year 2010, Fire at LUCAO

< PIPELINE >>

ALTERNATIVE D-A (Recommended Plan, Single Pipeline Alignment) Year 2010, Fire at LUCAO

<< NODES >>

STATIC HEAD (m) DYNAMIC HEAD (m) 24242424262626226224242456626272626 66446466666677667845666677466667746666 н. С. Е.Е. (в). (cu.m/day) FLOW GROUND ELEV. (m) NOD NODE 

lteration Times : 5

ALTERNATIV D-B (Parallel Pipeline Alignment of Recommended Plan) Year 1995

HEADLOSS (m) (0/00)

FLOW VEL. (cu.m/day)(m/sec)

₹o

LENGTH

DIA.

2 1 2

NODE 1 rom-

PIPE No.

Ê

350. 1700. 1900.

<< PIPELINE >>

ALTERNATIV D-B (Parallel Pipeline Alignment of Recommended Plan) Year 1995

STATIC HEAD (m) DYNAMIC HEAD H.G. E.C. E.C. (cu.m/day) FLOW  $\hat{\mathbf{x}}$ GROUND ELEV. << NODES ຂູ່ 4001-

-04000-040-000-40000

84202-5599999999782000

00400-000-002200-

280. 320.

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ω •• Iteration Times

-87-

ALTERNATIVE D-B (Parallet Pipeline Alignment of Recommended Plan) Year 2010 0.0000000044 22000000444 22000044406 HEADLOSS (m) (0/00) เต้ง 1 4.0000000004400000000000 FLOW VEL. (cu.m/day)(m/sec) - 1758. - 1758. -27005.21347. ¥ 14 Ω 20.2 (m) (m) 1000 1100 1100 1100 290 320 320 010 650 402 170. 1900. 1900. 350. 440 OIA. ខ្លួំខ្លួំខ្លួ 4505500 38 NODE No. 100000000 ~ ന ന ന លលល់លំលំលា ထတ္ထတ္လတ္ Pine.

ALTERNATIVE D-8 (Parallel Pipeline Alignment of Recommended Plan) Year 2010

<< NODES >>

STATIC HEAD (m)	83882238888888888888888888888888888888
DYNAMIC HEAD (m)	0,000,00-14
H. G. L. ELEV, (m)	99999999999999999999999999999999999999
ELOW (cu.m/day)	<b>A</b> 4132 00 00 00 00 00 00 00 00 00 00 00 00 00
GROUND ELEV.	8
NODE Non Non	-00400-000-00400-000-004000000

-88-

r--

Iteration Times :

(2) DEEP Flow (3) DEEP Flow (4) RADIA VELL RADIA VELL RADIA VELL RADIA TRANSMIS (1) Main (2) Main (2) Main (2) Main (2) Main (2) Main (2) Main 0 = 1500 0 = 3500 0 = 3500 0 = 3500 0 = 3500 0 = 200 0 = 2500 0 = 1500 0 = 100 SUB-TOTA 1) Adminini 2) Operatus SUB-TOTA	pan	UNIT COST	Phase I(	Stage 1)	Phase 10	Stace 21	Pharie	Total	housan	d Pes
(1) DEEP (2) DEEP Flow (3) DEEP Flow (4) RADIA VELL <u>SUB-TOTA</u> TRANSNIS (1) Main (2) Main (2) Main (2) Main D=3500 D=3500 D=3500 D=3500 D=3500 D=500 D=200 D=2500 D=3500 D=200 D=2500 D=5000 D=5000 D=5000 D=5000 D=5000 D=5000 D=5000 D=5000 D=5000 D=5000 D=5000 D=2500 D=2500 D=2500 D=2500 D=2500 D=5000	the second s		NUMBER	COST	NUMBER	COST	NUMBER	COST	NUMBER -	l Cost COST
(2) DEEP Flow (3) DEEP Flow (4) RADIA VELL RADIA VELL RADIA VELL RADIA TRANSMIS (1) Main (2) Main (2) Main (2) Main (2) Main (2) Main (2) Main 0 = 1500 0 = 3500 0 = 3500 0 = 3500 0 = 3500 0 = 200 0 = 2500 0 = 1500 0 = 100 SUB-TOTA 1) Adminini 2) Operatus SUB-TOTA	CEP WELL CONSTRUCTION	640000	8	5120					1	
(3) DEEP Flow (4) RADIA VELL RADIA VELL RADIA VELL RADIA VELL RADIA VELL RADIA VELL RADIA VELL RADIA VELL RADIA VELL RADIA VELL RADIA VELL RADIA VELL RADIA VELL RADIA VELL RADIA VELL RADIA D=200 D=200 D=300 D=300 D=300 D=25	EEP VELL PUMP W/HOUSE	450000	8	3600	7	4480 3150	15	9600 6750	0	· 0
Flow (4) RADIA VELL RADIA SUB-TOTA TRANSMIS (1) Main (2) Main (2) Main (2) Main (2) Main (2) Main 0 = 350 0 = 350 0 = 350 0 = 350 0 = 350 0 = 250 0 = 150 0 = 100 3) Inter Vat	low Meter D=100	25000	8	200	7	175	15	375		U 0
(4) RADIA VELL RADIA VELL RADIA TRANSMIS (1) Main (2) Main (2) Main (2) Main (2) Main (2) Main (1) Reser (3) Chlor (4) Elect (3) Chlor (4) Elect (3) Chlor (4) Elect (3) Chlor (4) Elect (3) Chlor (4) Elect (3) Chlor 0 = 350 0 = 250 0 = 350 0 = 250 0 = 350 0 = 250 0 = 250	EEP WELL PUMP REPAIR	252000	10	2520	0	· 0	10	2520	0	ŏ
VELL RADIA SUB-TOTA TRANSMIS (1)Main (2)Main (2)Main (2)Main (2)Main (2)Main (2)Main (2)Main (3)Chlor (4)Elect (3)Chlor (4)Elect (3)Chlor (4)Elect (5)0istr 1)Main 0=150 0=200 0 0=200 0 0=200 0 0=200 0 0=200 0 0=200 0 0=200 0 0=200 0 0=200 0 0=200 0 0=200 0 0=200 0 0=200 0 0=200 0 0=200 0 0=200 0 0 0	ADIAL WELL	25000 1760000	10	250 0	0	0	10	250	0	0
SUB-TOTA           TRANSMIS           (1)Main           (2)Main           (2)Main           0=150           D=200           D=200           D=200           D=300           D=350           SUB-TOTA           SIDB-TOTA           SIDB-TOTA           SIDB-TOTA           SIDB-TOTA           SIDB-TOTA           SIDB-TOTA           SUB-TOTA           SIDB-TOTA           SIDB-TOTA           SIDB-TOTA           SUB-TOTA           SOD           D=300           D=2500           D=300           D=300           D=300           D=400           D=400           D=2500           D=300	ELL PUMP	403000	0		0	0	0	0 0	4	7040 3627
TRANSNIS (1)Main (2)Main (2)Main 0=150 0=200 0=250 0=350 SUB-TOTA Slow San 01STR1BU (1)Reser (2)Pump (3)Chlor (4)Elect (3)Chlor (4)Elect (5)0istr 1)Main 0=150 0=200 0=350 0=200 0=350 0=350 0=350 0=350 0=400 0=350 0=400 0=500 0=500 0=500 0=2500 0=2500 0=2500 0=2500 0=2500 0=500 0=2500 0=2500 0=500 0=500 0=2500 0=2500 0=2500 0=500 0=2500 0=2500 0=5000 0=5000 0=5000 0=2500 0=3500 0=1/2 0=1/2 0=100 SUB-TOTA SUB-TOTA SUB-TOTA	ADIAL VELL PUMP HOUSE	634000	0	. 0	0	Ŏ	0	0	4	2536
(1)Main (2)Main (2)Main (2)Main (2)Main (2)Main (2)Main (2)Main (3)Chlor (4)Elect (3)Olstr (5)Olstr (5)Olstr (5)Olstr (5)Chlor (5)Chlor (5)Chlor (5)Chlor (7)Fire (5)Chlor (5)Chlor (7)Fire (5)Chlor (7)Chlor (7)Fire (5)Chlor (7)Ch	SMISSION FACILITIES		i	11690		7805	1	19495	1	13203
(2)Main 0=150 D=200 D=300 D=350 SUB-TOTA (3)Chlor (4)Elect (3)Chlor (4)Elect (5)Oistr 1)Main D=1500 D=200 D=200 D=200 D=200 D=200 D=200 D=400 D=400 D=400 D=400 D=400 D=400 D=250 D=200 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=200 D=500 D=500 D=200 D=500 D=500 D=500 D=500 D=500 D=200 D=500 D=200 D=500 D=200 D=500 D=200 D=500 D=200 D=500 D=200 D=500 D=200 D=500 D=500 D=200 D=500 D=200 D=500 D=200 D=250 D=100 SUB-TOTA (3)Inter Vater Vater Vater Vater Vater D=1/2 D=1/2 D=1/2 D=150 D=100 SUB-TOTA (3)Operat SUB-TOTA	ain Pipe D=600(Steel)	1600	0	0	0	0				
D=200 D=250 D=350 D=350 D=350 D=350 D=350 D=350 D=350 D=350 D=250 D=250 D=250 D=250 D=250 D=250 D=250 D=400 D=500 D=500 D=400 D=500 D=500 D=400 D=500 D=400 D=500 D=500 D=250 D=250 D=250 D=250 D=250 D=250 D=250 D=300 D=500 D=300 D=300 D=350 D=250 D=300 D=250	ain Pipe	1000	v	, v			0	0	26000	41600
D=250 D=300 D=300 D=350 SUB-TOTA SIOW San DISTRIBU (1)Reser (2)Pump (3)Chlor (4)Elect (5)Oistr 1)Main D=150 D=200 D=200 D=200 D=200 D=300 D=400 D=400 D=400 D=400 D=400 D=400 D=400 D=400 D=400 D=500 D=400 D=500 D=250 D=400 D=500 D=250 D=200 D=500 D=200 D=200 D=500 D=200 D=500 D=200 D=500 D=200 D=200 D=400 D=500 D=200 D=400 D=500 D=200 D=200 D=200 D=400 D=500 D=200 D=200 D=200 D=200 D=500 D=200 D=200 D=200 D=400 D=500 D=200 D=200 D=500 D=200 D=200 D=200 D=500 D=200 D=200 D=200 D=100 SUB-TOTA I)Admini SUB-TOTA	=150 (PVC Pipe)	410	5400		3850	1579	9250	3793		0
D=300 D=350 SUB-TOTA SUB-TOTA (1)Reser (2)Pump (3)Chlor (4)Elect (5)Distr 1)Main D=150 D=200 D=200 D=200 D=250 D=300 D=400 D=400 D=400 D=400 D=400 D=400 D=400 D=500 D=200 D=500 D=200 D=500 D=200 D=500 D=500 D=200 D=500 D=500 D=200 D=500 D=200 D=500 D=200 D=500 D=200 D=500 D=200 D=500 D=200 D=500 D=200 D=500 D=200 D=200 D=200 D=500 D=200 D=200 D=500 D=200 D=200 D=500 D=200 D=200 D=200 D=500 D=200 D=1/2 D=1/2 D=1/2 D=100 SUB-TOTA SUB-TOTA SUB-TOTA	=200 (Steel Pipe) =250 (Steel Pipe)	520 630	1500		1050	546	2550	1326		0
D=350 SUB-TOTA Slow San DISTRIBU (1) Reser (2) Pump (3) Chion (4) Elect (5) Distribut (5) Distribut D=250 D=250 D=300 D=350 D=400 D=500 D=500 D=4500 D=500 D=250 D=2	=300 (Steel Pipe)	760	1000 750	630 570	1050 550	662 418	2050 1300	1292 988	2400	0
Slow San DISTRIBU (1)Reset (2)Pump (3)Chlor (4)Elect (5)Oistr 1)Main D=150 D=200 D=250 D=250 D=300 D=400 D=350 D=400 D=400 D=400 D=400 D=400 D=500 D=400 D=500 D=400 D=500 D=250 D=250 D=250 D=250 D=200 D=250 D=200 D=250 D=200 D=500 D=250 D=200 D=250 D=200 D=250 D=200 D=250 D=200 D=250 D=200 D=500 D=250 D=200 D=250 D=200 D=500 D=250 D=200 D=250 D=200 D=250 D=200 D=250 D=250 D=200 D=250 D=200 D=500 D=250 D=250 D=250 D=200 D=500 D=250 D=250 D=250 D=250 D=250 D=250 D=200 D=500 D=250 D=250 D=200 D=500 D=200 D=500 D=200 D=500 D=500 D=200 D=500 D=200 D=500 D=200 D=500 D=500 D=200 D=500 D=200 D=500 D=500 D=500 D=200 D=500 D=500 D=200 D=500 D=500 D=200 D=500 D=200 D=500 D=500 D=200 D=500 D=200 D=500 D=500 D=200 D=500 D=200 D=500 D=200 D=500 D=200 D=500 D=200 D=200 D=200 D=200 D=500 D=200 D=500 D=500 D=200 D=500 D=1	=350 (Steel Pipe)	900	4000		700	630	4700	4230	2400	1824 0
DISTRIBU (1) Reser (2) Pump (3) Chior (4) Elect (5) Distr 1) Main D=150 D=200 D=200 D=200 D=350 D=350 D=400 D=400 D=400 D=400 D=400 D=500 D=250 D=200 D=200 D=200 D=200 D=200 D=200 D=200 D=200 D=500 D=200 D=500 D=200 D=500 D=200 D=200 D=200 D=500 D=200 D=200 D=200 D=500 D=200 D=300 D=300 D=300 D=300 D=300 D=300 D=300 D=300 D=300 D=300 D=200 D=300 D=1/2 D=1/2 D=1/2 D=1/2 D=1/2 D=1/2 D=1/2 D=1/2 D=100				7794		3835	1		1	43424
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(3) Chior (4) Elect (5) 0 istr 1) Main D=150 D=250 D=300 D=350 D=400 D=500 D=400 D=500 D=250 D=250 D=250 D=250 D=250 D=250 D=250 D=250 D=250 D=300 D=350 D=300 D=350 D=300 D=350 D=300 D=350 D=300 D=500 D=300 D=500 D=500 D=500 D=250 D=500 D=1/2 D=1/2 D=1/2 D=10 SUB-TOTA SUB-TOTA SUB-TOTA	eservoir		(2400)	2898	0	0	(2400)	2808	(4550)	4362
(3) Chlor (4) Elect (5) 01 str 1) Main D=150 D=200 D=250 D=350 D=400 D=400 D=400 D=400 D=700 R1VER D=400 D=700 R1VER D=250 D=250 D=250 D=200 D=2	ump Facility (Equip.)			1784		800		2584		3394
(4) Elect (3) Distr 1) Main D=150 D=200 D=250 D=350 D=400 D=400 D=400 D=400 D=400 D=400 D=400 D=400 D=700 RIVER D=450 D=250 D=200 D=200 D=200 D=200 D=200 D=200 D=200 D=200 D=200 D=500 D=200 D=500 D=300 D=350 D=300 D=400 D=500 D=200 D=200 D=200 D=200 D=200 D=700 D=200 D=200 D=200 D=200 D=700 D=200 D=200 D=200 D=200 D=700 D=200 D=200 D=200 D=700 D=200 D=200 D=200 D=200 D=700 D=200 D=	-do- (Civil)		ļ	1331		0		1331	1	1748
(5)0istr 1)Main D=1500 D=200 D=250 D=3500 D=400 D=400 D=400 D=400 D=400 D=400 D=500 D=200 D=250 D=250 D=250 D=250 D=250 D=250 D=250 D=250 D=250 D=250 D=300 D=450 D=500 D=500 D=500 D=500 D=500 D=250 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=1/2 D=5/4 D=1/2 D=1/2 D=150 D=100 D=1	hlorination Facility lectric Sub-station	98100	11 200KVA			0		1079	45kg/axl	
D=150 D=2500 D=2500 D=300 D=400 D=400 D=500 D=700 R1VER D=2500 D=2500 D=200 D=2500 D=2500 D=200 D=2500 D=2500 D=300 D=400 D=3500 D=400 D=500 D=400 D=500 D=400 D=500 D=400 D=400 D=400 D=400 D=400 D=400 D=300 D=400 D=400 D=250 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=250 D=2	istribution pipes		ZUUNYA	2020			200KVA	2620	400KVA	1020
D=200 D=250 D=350 D=400 D=400 D=400 D=700 R1VER D=450 D=250 D=250 D=200 D=200 D=200 D=200 D=200 D=300 D=350 D=300 D=400 D=500 D=500 D=500 D=400 D=500 D=500 D=400 D=500 D=400 D=500 D=400 D=500 D=400 D=500 D=400 D=500 D=1/2 D=500 D=1/2 D=500	ain Pipes				ļ		1			
D=250 D=300 D=3500 D=400 D=400 D=700 D=700 RIVER D=250 D=250 D=250 D=200 D=250 D=200 D=200 D=250 D=300 D=350 D=350 D=300 D=400 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=600 D=1/2	=150 (PVC Pipe)	410	0	0	0	Û	0	• 0	4160	1706
D=300 D=350 D=400 D=500 D=500 D=500 D=500 D=700 R1VER D=250 D=250 D=250 D=250 D=300 D=300 D=400 D=500 D=500 D=400 D=500 D=500 D=400 D=500 D=400 D=500 D=400 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=500 D=100 SUB-TOTA	=200 (Steel Pipe) ≈250 (Steel Pipe)	520 630	0	0	1780	926	1780	926	1030	536
D=400 D=400 D=500 D=500 D=700 R1VER D=250 D=250 D=250 D=200 D=250 D=200 D=250 D=300 D=350 D=300 D=400 D=500 D=500 D=600 D=500 D=600 D=1/2 D=1/2 D=3/4 5)Rehab Vater Vater Vater Cold L Servi Servi Servi C)Flow D=150 D=100 SUB-TOTA	=300 (Steel Pipe)	760	440	334	550 3210	347 2440	550 3650	347 2774	6150	3875 0
D=450 D=500 D=500 D=700 RIVER D=250 D=250 D=250 D=250 D=250 D=200 D=250 D=300 D=350 D=350 D=400 D=500 D=500 D=500 D=600 D=600 D=1/2 D=1/2 D=3/4 5)Rehab Vater Vate	=350 (Steel Pipe)	900	440	396	400	360	840	756	0	0
D=500 D=600 D=700 D=250 D=250 D=250 D=250 D=200 D=260 D=260 D=300 D=400 D=400 D=400 D=400 D=500 D=400 D=500 D=400 D=500 D=600 D=700 3) Inter UPT0 UPT0 4) Servi D=1/2 D=3/4 5) Rehab Vater Vater Vater Vater Servi 6) Flow D=150 D=100 SUB-TOTA	=400 (Steel Pipe)	970	300	291	0	0	300	291	0	、 0
D=600 D=700 R1VER D=450 D=250 D=250 D=250 D=300 D=300 D=300 D=400 D=4500 D=500 D=600 D=700 3) Inter UPT0 4) Servi D=1/2 D=3/4 5) Rehab Water Vater Vater Vater Servi Servi Servi Servi D=150 D=100 SUB-TOTA	≈450 (Steel Pipe) ≃500 (Steel Pipe)	1160 1330	240 290	278 386	0	0	240	278	0	. 0
D=700 R1VER D=4500 D=250 D=250 D=250 D=250 D=300 D=300 D=4500 D=4500 D=600 D=700 3) Inter UPT0 UPT0 UPT0 UPT0 UPT0 UPT0 UPT0 UPT0	=600 (Steel Pipe)	1600	1360	2176	0	0 0	290 1360	386 2176	0	. 0
D=450 D=250 D=250 D=260 D=260 D=300 D=350 D=400 D=400 D=400 D=500 D=400 D=400 D=400 D=700 D=700 3)Inter UPT0 UPT0 4)Servi D=1/2 D=3/4 5)Rehab Vater Vater Vater Old L Servi Servi 6)Flow D=600 T)Fire D=150 D=100 SUB-TOTA	=700 (Steel Pipe)	1910	- 350	669	ŏ	õ	350	669	0	0
D=250 2) Valve D=1500 D=200 D=300 D=350 D=400 D=4500 D=600 D=600 D=700 3) Inter UPT0 4) Servi D=1/2 D=3/4 5) Rehab Vater Vater Vater 01d L Servi Servi 6) Flow D=600 7) Fire D=150 D=100 SUB-TOTA	IVER CROSSING CD=1.5m	1658	120	199	D	Û	120	199	300	497
2)Valve D=150 D=200 D=250 D=300 D=400 D=500 D=500 D=600 D=700 3)Inter UPT0 UPT0 UPT0 UPT0 UPT0 4)Servi D=1/2 D=3/4 5)Rehab Water Vater Vater Vater Vater D=150 D=100 SUB-TOTA SUB-TOTA	=450 Materials =250 Materials	.626 340	120	75	0	0 0	120	75	200	0
D=150 D=2500 D=2500 D=350 D=400 D=500 D=500 D=600 D=600 D=700 3) Inter UPT0 UPT0 UPT0 UPT0 UPT0 UPT0 UPT0 UPT0		510	l	0		U	0	0	300	102
D=250 D=300 D=350 D=400 D=500 D=500 D=600 D=700 3) Inter UPT0 UPT0 4) Servi D=1/2 D=3/4 5) Rehab Vater Vater Vater 0 Id L Servi 6) Flow D=600 D=100 SUB-TOTA 1) Admini 2) Operat	=150 (Gate Valve)	5300	0	0	8	32	- 6	32	14	74
D=300 D=350 D=450 D=500 D=500 D=700 3) Inter UPT0 4) Servi D=1/2 D=3/4 5) Rehab Water 01d L Servi Servi 6) F10W D=100 CUB-TOTA 1) Admini 2) Operat SUB-TOTA	=200 (Gate Valve) =250 (Gate Valve)	6700	0	0	6 1	40	6	40	3	20
D=350 D=400 D=4500 D=500 D=700 3) Inter UPT0 UPT0 4) Servi D=1/2 D=3/4 5) Rehab Water Vater Vater Vater Vater Vater 0 Id Servi Servi 6) Flow D=100 SUB-TOTA 1) Admini 2) Operat SUB-TOTA	=300 (Butterfly Valve)	11200 34800	0	0 70	2 10	22 348	2 12	22 418	22	246 0
D=450 D=500 D=500 D=700 3)Inter UPT0 UPT0 4)Servi D=1/2 D=3/4 5)Rehab Vater Vater Vater 0Id L Servi 6)Flow D=100 SUB-TOTA 1)Admini 2)Operat SUB-TOTA	=350 (Butterfly Valve)		2	149	1	74	3	223	ŏ	ŏ
D=500 D=600 D=700 3) Inter UPT0 4) Servi D=1/2 D=3/4 5) Rehab Vater Vater Vater 0 Id L Servi 6) Flow D=600 7) Fire D=150 D=100 SUB-TOTA 1) Admini 2) Operat SUB-TOTA	=400 (Butterfly Valve)		1	95	0	0	1	95	0	0
D=600 D=700 3) Inter UPT0 UPT0 4) Servi D=1/2 D=3/4 5) Rehab Water 01d L Servi Servi 6) Flow D=600 7) Fire D=150 D=100 SUB-TOTA SUB-TOTA	=450 (Butterfly Valve) =500 (Butterfly Valve)	125900 174000	1	126	0	0		126	0	0
D=700 3) Inter UPTO 4) Servi D=1/2 D=3/4 5) Rehab Water Vater Vater Vater 01d Servi Servi 6) Flow D=600 7) Fire D=150 D=100 SUB-TOTA SUB-TOTA	=600 (Butterfly Valve)		5	174		0	15	174 1218		· 0
UPT0 UPT0 4)Servi D=1/2 D=3/4 5)Rehab Vater Vater 0Id L Servi 6)Flow D=600 7)Fire D=150 D=100 SUB-TOTA 1)Admini 2)Operat SUB-TOTA	=700 (Butterfly Valve)		1	313	i ol	Õ	Ĩ	313	0	0
UPTO 4)Servi D=1/2 D=3/4 5)Rehab Water Vater 01d L Servi Servi 6)Flow D=600 7)Fire D=100 SUB-TOTA 1)Admini 2)Operat SUB-TOTA	nternal Network	· ·						50.00		6081
4)Servi D=1/2 D=3/4 5)Rehab Vater 01d L Servi Servi 6)Flow D=600 7)Fire D=100 SUB-TOTA 1)Admini 2)Operat SUB-TOTA	PTO 1990 PTO 1995			5049		0 898		5049 898		•
D=1/2 D=3/4 5)Rehab Water Vater Servi Servi 6)Flow D=600 7)Fire D=100 SUB-TOTA 1)Admini 2)Operat SUB-TOTA	ervice Conections		<u> </u>	0	;;	030			1	*
5)Rehab Vater Vater Old L Servi 6)Flow D=600 7)Fire D=100 SUB-TOTA 1)Admini 2)Operat SUB-TOTA	=1/2	810	2279	1846	3811	3086	6090	4932	8940	7241
Water Water Old L Servi 6)Flow D=600 7)Fire D=150 D=100 SUB-TOTA SUB-TOTA SUB-TOTA		1280		22	7	3	24	31	16	20
Vater Old L Servi 6)Flow D=600 7)Fire D=100 SUB-TOTA SUB-TOTA SUB-TOTA	ehabilitation ater Meter 1/2''	400	1392	557	0	0	1392	557	1	
Servi Servi 6)Flow D=600 7)Fire D=1500 SUB-TOTA 1)Admini 2)Operat SUB-TOTA	ater Meter 3/4''	880	16	14	Ň	ŏ	16	14		
<u>Servi</u> 6)Flow <u>D=600</u> 7)Fire D=150 <u>D=100</u> SUB-TOTA 1)Admini 2)Operat SUB-TOTA	ld Laterals	· · ·		571	0	0	0	571		
6)Flow D=600 7)Fire D=150 D=100 SUB-TOTA 1)Admini 2)Operat SUB-TOTA	ervice Connect.vo/Metr		724	348	0	0	724 1401	348 1233		
D=600 7)Fire D=150 0=100 SUB-TOTA 1)Admini 2)Operat SUB-TOTA	ervice Connect.w/Meter	880	1401	1233	¥	V		1433	<u> </u>	
D=150 D=100 SUB-TOTA 1)Admini 2)Operat SUB-TOTA		215000	0	0	0	0	0	0		215
D=100 SUB-TOTA 1)Admini 2)Operat SUB-TOTA	ire Protection									1040
SUB-TOTA 1)Admini 2)Operat SUB-TOTA	=150	16800	0	- 0	0	0	0		62 281	1042 2641
1)Admini 2)Operat SUB•TOTA	-100 Total	9400	0	0 26301	0				201	34939
2)Operat SUB•TOTA	ministration Bldg				· · · · · · · · · · · · · · · · · · ·				1	1610
	eration Center		1	· · · · · · · · · · · · · · · · · · ·	ļ		1	1380	ļ0	0
Land Acq			0000	1380	ļ	0		1380 132		1610 1320
Nohio!-	Acquisition	60 300000	2200		0				22000	
Vehicle Stored M		300000	0		0	247	0			898
SUB-TOTA							+			
Replacem	ed Material & Equip.			1235		547		1782		3118
TOTAL Leakage	ed Material & Equip. TOTAL acement of Equipment					547 0 21569		1782 0 69969		14562 120400

(Unit: thousand Pesos)

	INT COCT	1988		1989		(Unit: 1990		1991	1
Daxuoan	הCOS TINU ]	1988 ND 1	COST	1985	COST		COST	NO	COST
SDERCE FACILITY	1					4	2560	2	1280
(I)DEEP VELL CONSTRUCTION	640000 450000		0	4	2560 1800	4	1800	2	900
(2)DEEP VELL PUMP V/HOUSE Flow Meter D=100	25000		- Õ	4	100	4	100	2	50
(3)DEEP VELL PUMP REPAIR	252000		Ò	10	2520		0		0
Flow Neter D=100	25000		0	10	250		0		0
(4)RADIAL VELL	1760000	1	0		Q 0		Ő		ŏ
VELL PUMP	403000 634000		0		Ŭ.	:	. 0		0
RADIAL VELL PUMP HOUSE	034000		0		7230		4460	1	2230
TRANSHISSION FACILITIES				1			<u> </u>		
(1)Main Pipe 0=600(Steel)	1600		0	1	0		0		0
(2)Hain Pipe		1		2900	0 [189	2500	1025	1050	431
D=150 (PVC Pipe)	410 520		0	1500	780	2000	0	0	Ö
D=200 (Steel Pipe) D=250 (Steel Pipe)	630		ŏ	1000	630	0	0	0	0
D=300 (Steel Pipe)	760		0	750	570	0	0	:550	418
0=350 (Steel Pige)	900		0	2500		1500		700	630
SUB-TOTAL			0	: 	5419	 	2375		1479
Slow Sand Filtration Plant									
DISTRIBUTION FACILITIES				(2400)	2898				14 14 14 14 14 14 14 14 14 14 14 14 14 1
(1)Reservoir (2)Pump Facility (Eduid.)					1784			: 1	800
-do- (Civil)				1	1331				
(3)Chlorination Facility	98100 :		   	11					
(4)Electric Sub-station				1090	2620	1990		1991	
(5)Distribution pipes		1988	1 L	1989		1220		1991	
1)Main Pipes	410		0		0		0	1.1	. 0
D=150 (PVC Pipe) D=200 (Steel Pipe)	520	1	0		ů		0	1780	926
0=250 (Steel Pipe)	630		0		0		0	550	347
D=300 (Steel Pipe)	760		0		0	440	334	3210	2440
0=350 (Steel Pipe)	900		.0		0	440 300	396 291	400	360.
0=400 (Steel Pipe)	970		0		0	240	278		ŏ
D=450 (Steel Pipe)	1160   1330			а. С	. 0	290	386		- Ő
D=500 (Steel Pipe) D=500 (Steel Pipe)	1600		ŏ	1360	2176		0		0
0=700 (Steel Pipe)	1910		0	350	669		.0		0
RIVER CROSSING CD=1.5#	-		0		0		199		0
0=450 Haterials	626 <sup>‡</sup>		0		0		75		. 0
0=250 Materials	340		0		0		0		
2) Yalves	5300		· · 0		0		· · 0	6	32
0=150 (Gate Valve) D=200 (Gate Valve)	6700		. 0	-	ŏ		0	6	40
D=250 (Gate Valve)	11200		Ō		0		0	2	22
0=300 (Butterfly Valve)		ſ	0		. 0 .	2	70	10	348
0=350 (Butterfly Valve)			0		0	2	- 149	1. I.	74
0=400 (Butterfly Valve)	95200		0		0		95		··· 0
D=150 (Butterfly Valve)			0		0		126 174		.0
0=500 (Butterfly Valve) 0=500 (Butterfly Valve)			i o	5	1218		0		0
D=700 (Butterfly Valve)		i i j	Ö	l į	313		0		0
3)Internal Network		1							
UPTO 1390		-			2525		2524	. 1	
UPTO 1995	·	i							180
4)Service Conections		ļ	Q	1139	923	1140	923	763	618
0=1/2 0=3/4	810   1280		.0	1133	10			105	1
5)Remant litation	i	;					1		
Vater Meter 1/2'	100	1392	. 557	0	0	0	Ū,		
Vater Meter 3/4**	880 (	16		0	0	0	0		
Old Laterals		ļ		·	286		285		
Service Connect.Vo/Metr		242		241	116		116 411		
Service Connect.»/Meten 6)Flov Meter	880	467	411	467	411	401	<u>*</u> 111		
0=1:00	215000		0		· 0		Ó	L j	0
7)Fire Protection	111000							[	
D=150	16800								1. C.
D=100	9400						i	ļ	
SU8-TOTAL	1		1098		18359		6844	<u> </u>	6188
1)Administration Bldg					1200				
(2)Operation Center SUB+TOTAL			. 0				0		0
Land Acquisition	50 50	2200			1380		0		
	300000	2200					0		
							149		118
Vehicle	1		20	· · ·	334				
Vehicle Stored Material & Equip. SU8-FOTAL			20 452		634	*****	149		418
Vehicle Stored Material & Equip. SU8-FOTAL Replacement of Equipment			452 0		<u>634</u> 0		149 0		418
Vehicle Stored Material & Equip. SU8-FOTAL	210	1420	452 0 1550		634 0 33022		149 0 13828		418 0 10315

bagu	1764	UNIT COST	1992 NU	COST	1992 N0	C0S7	(Unit: 1994 90	1	1995	COST
	CE FACILITY	*			·····	· · · · · · · · · · · · · · · · · · ·				) )
	EEP VELL CONSTRUCTION	640000		640	1	640	2	1280	1	640
	EEP VELL PUMP V/HOUSE		1	450	1	450	2	900	1	450
	low Meter D=100 EEP VELL PUMP REPAIR	25000	L L	25	1	25	2	50 [	l	25
	lov Meter D=100	25000		0		0		01		0
	ADIAL VELL	1760000		0		U 0		0		0
_ V	ELL PUMP	403000		0		0		0		0
	ADIAL VELL PUMP HOUSE			0		ŏ	l i	0 I		0
	TOTAL	1		1115		1115	[	2230		1115
	SMISSION FACILITIES							1		
	ain Pipe D=600(Steel) ain Pipe	1600		0		0		0 ]		0
	=150 (PVC Pipe)	110	1100	0	140	0		0		i 0
	=200 (Steel Pipe)	410 520	1100	451	400	164	900	369	400	164
	=250 (Steel Pipe)	630	0	0	0 550	0 347	450	234	600	312
	=300 (Steel Pipe)	760	ŏ	0	330	341	500	315   0	0	0
<u>[:</u> D	=350 (Steel Pipe)	900	0	0	ŏ	. 0	0	. 0	Ő	0
SUB-	TOTAL	1		451		511		918		476
	Sand Filtration Plan	t <u>i</u>		<u> </u>	;		1			1
	RIBUTION FACILITIES							l		I
	eservoir ump Facility (Eouip.)								~~~~~~~	
1471	-do- (Civil)							‡		
(3)0	hlerination facility									
	lectric Sub-station	1		**************************************			•			
	istribution pipes	1	1992		1993		1994		1995	
	ain Pipes	1								
	=150 (PVC Pipe)	410		0		0		0		0
	=200 (Steel Pipe)	520		0.		0		0		0
	=250 (Steel Pipe)	630		0		0		0 (		0
	<300 (Steel Pipe)	760		0		0		0		0
1	=330 (Steel Pipe) =400 (Steel Pipe)	900		0		0		. 0(		0
	=450 (Steel Pipe)	1160		1 <u>0</u>		0		01		0
	= SOO (Steel Pipe)	1330		Ő	. 1	0		0		: 0
	=600 (Sleel Pipe)	1600		Ő		Ő		ol		ŏ
	=700 (Steel Pipe)	1910		0		0	1	0		0
	IVER CROSSING CD=1.5m	1658		0		0		0		0
D	=450 Materials	626		0		0		0		į O
P	=250 Materials	340		0		0		0		00
	alves							ا م		
	=150 (Gate Valve)	5300		0 0		0		0		0
-	=200 (Gate Valve)	6700		a		0		0		0
1	=250 (Gate Valve) =300 (Butterfly Valve	11200 X 34800	i	0		0		0		. 0
	=350 (Butterfly Valve		1	Ő	:	ŏ		ő		, o
	=400 (Butterfly Valve		1	Ő		Ő		ō		ō
0	=450 (Butterfly Valve	125900		0		0		0		0
	=500 (Butterfly Valve			0		0		0		0
D	=600 (Butterfly Valve	) 243600		0	4	0		0		0
<u> </u>	=700 (Butterfly Valve	) <sup>'</sup> 313200		0	·····	0	1	0		. 0
	nternal Netvork	1								2
	PTO 1990			180		180		170		179
	PTO 1995			100		100				
	ervice Conections	810	762	617	762	617	762	617	762	617
	=1/2 =3/4	1280	2	3	Ĩ		2	3	1	
	enabilitation	+	<del>-</del> -	·						
	iter Heter 1/2''	100								1
	ater Meter 3/4''	880				. 1	1			: F
	ld Laterals									1
l s	ervice Connect.vo/Met	r 480			4	ĺ		[		1
S S	ervice Connect.u/Mete	n <u>880</u>			· · · · · · · · · · · · · · · · · · ·					
	lov Meter		;	0		0	•	0		, 0
	=1500	215000		V						·
	ire Protection	10000						1		
1.1.1.1.1.1	=150	16800	· ·			1		(		
	= 1 0 0 TOTAL	1 3400		800		793		799		797
	ministration Bldg	- <u> </u> ,								
	eration Center	· · ·	1	· · · · · · · · · · · · · · · · · · ·	۲ 			l		
	TOTAL	1		0		0		0		0
	Acquisition	1 60		0		0		0		0
	cle	300000		0		0		0		
	ed Material & Equip.	1		28		29 20				28 25
SUB-	TOTAL	1	<u> </u>	28						
Rent	acement of Equipment	1	<u> </u>	0		2153		3991		2115
	Bitter have a second	l ·	<u></u>	2394		2133		<u></u>		······································
TOTA	axe Detection	240								

## APPENDIX 8.2.1.B PROJECT COST WITH FOREIGN AND LOCAL CURRENCY BREAKDOWN (1986 Price Level, Dagupan City)

SUMMARY

Phase I, Stage 1

4.			housand P)
	Local	F.E.C	<u>Total</u>
Direct Construction Cost Physical Cont. (8% of D.C.C.)	21,868 1,749	26,532 2,123	48,400 3,872
Sub Total	23,617	28,655	52,272
Leakage Detection	1,020		1,020
Detailed Design (10% of S.T. in Stage 1 & Stage 2)	3,778	3,779	7,557
Construction Supervision (4% of S.T.)	1,045	1,046	2,091
Total	29,460	33,480	62,940

Phase I, Stage 2

	14 g.	(Unit: thousand ₽)			
	Local	F.E.C	<u>Total</u>		
Direct Construction Cost Physical Cont. (8% of D.C.C.)	9,604 769	11,965 957	21,569 1,726		
Sub Total	10,373	12,922	23,295		
Construction Supervision	. *		:		
(4% of S.T.)	609	223	932		
Total	10,982	13,145	24,227		

#### Phase II

	Local	(Unit: <u>F.E.C</u>	thousand ₽) <u>Total</u>
Direct Construction Cost Physical Cont. (8% of D.C.C.)	53,133 4,251	67,267 5,381	120,400 9,632
Sub Total	57,384	72,648	130,032
Detailed Design (10% of S.T.) Construction Supervision	6,501	6,502	13,003
(4% of S.T.)	5,201		5,201
Total	69,086	79,150	148,236

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The following tables show the breakdown of the project cost in each design year. The unit of all figures is thousand pesos. Project cost is further broken down into the Foreign Exchange Compornent and the Local Currency Compornent. Abbreviations in the tables are as follows:

COST Construction Cost -----Cost for Civil Work in the Foreign Exchange Compornent C.FEC ----C.DOM ----Cost for Civil Work in the Local Currency Compornent Cost for Unskilled Laborer of Civil Works in the Local C.D.UNSKL ----Currency Compornent. Cost for Equipments in the Foreign Exchange Compornent E.FEC Cost for Equipments in the Local Currency Compornent E.DOM 

COST = C.FEC + C.DOM + E.FEC + E.DOM

The exchange rates used in the cost estimates are as follows: P20 = \$1

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\$1 = ¥155

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LL- la la	1 <del></del>		······································

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			(cos	t; thousand peso)
		Stage 1	Stage 2	Phase II
Item		Cost	Cost	Cost
Operation & Maintenance	Cost			
Salary Power	1,730 p/M.M 0.50 ₽/kwH	1,080 484	1,495 746	1,806 1597
Chemical Miscellaneous Maintenance	27 ₽/kg	90 690 511	122 1,051 800	241 1,902 1,482
Total		2,855	4,214	7,028

## APPENDIX 8.2.1.C OPERATION AND MAINTENANCE COST (Dagupan City)

#### APPENDIX 9.3.1 MARKET SURVEY

The market survey was conducted by interviews to the residents in the study area using the LWUA's interview sheet as per attached in the end of this section.

The total number of respondents and its estimated coverage ratio to the total number of households in the study area are as follows:

Total Number of	Estimated Total	Coverage Ratio to
Respondents	Household	Total Household
4,050	11,616	35%

The results of the market survey are obtained as shown in TABLE 9.3.1.1.

From the market survey, the income distribution of the respondents are shown as follows:

Income Bracket $\frac{1}{2}$	Ave.Pesos	Number
₱900 and below	650	1,027
₽901 to ₽1500	1,224	1,227
₽1,501 to ₽2,500	2,121	674
₽2,501 to ₽4,500	3,501	458
₽4,501 and above	8,406	314

1/ Residential, excluding no-income and no-answer

		sta a a		
Tot	al Number of Respondents:	1050	· .	
1	. Distribution According to	) Building Ty		
		•		%
	a. Residential	· •	3727 92	
	b. Commercial	1		.64
	c. Industrial	:	54 1	.33
2.	Distribution According to S	Source of Wat	ter	
				%
	a. Connected to System	· · · · · •		.35
	b. Neighbor's Connection		567 14	
	c. Public Faucet			.22
	d. Private System		665 16	
	e. Water Vendor		26 0.	.64
	f. Others	•	15 0	. 37
3.	Average Persons Per Househo	ld		
<b>~</b> ·	The all and a second second and			
	a. Residential / Number of	Sample :	6.69 / 371	1
	b. Commercial / Number of	Sample :		57
	c. Industrial / Number of	Sample :	8.76 / 5	i4
4.	Willingness To Connect (%)			
	Residentia	l Commercia	l Industrial	Total
			1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.	
	a. Yes : 31.26	21.56	20.37	30.47
	b. No : 36.84	29.00	44.44	36.42
	c. Undecided : 0.78	0.74	0.00	0.77
	d. W/ Own Conn.: 31.12	48.70	35.19	32.35
5.	Average Monthly Water Needs			n de la companya de l La companya de la comp
•••		8		
	Type / Number of Sample	: Residentia	[] Commercial	Industrial
		: 10.23		5.50
	b. Drum / 1705	: 2.33		5.02
	c. Gallon / 194	: 62.65		10,00
	d. Others / 1122	: 55.52		118.19
6.	Ave. Monthly Electric Bills		itial Users (Pi	
	Number of Effective Respond	ents		: 3122
7.	Income Distribution			
	( Residential, Excluding No	-Income and	No-Answer )	
	: · · · ·	AVE DECO	MUMDED	
		AVE. PESO	NUMBER	
	a. P900 and Below :	650	1027	
	b. P901 to P1500 :	1224	1227	
	c. P1501 to P2500 :	2121	674	100 A
	d. P2501 to P4500 :	3501	458	the state of the second s
	e. P4501 and Above :	8406	314	
				: 1

Existing major sources of water for the respondents and willingness to connect by each source of water are :

		· · · · · · · · · · · · · · · · · · ·	· · · · · · · · · · · · · · · · · · ·
		Willingness to	Connect
Sources of Water	Distribution	Yes	No
Connected to System	32%	- %	- %
Neighbor's Connection	14	64	34
Public Faucet	36	41	58
Private System	16	37	62

Public faucet and connections to the system are the major sources of water for the respondents. The rest draw their water needs from private systems and neighbor's connections. In addition, only 1% of the respondents depends on water vendors and others for its water sources. From the above table, the majority of the respondents using neighbor's connections are willing to connect to the waterworks system, while the majority of respondents using public faucet and private system are unwilling to connect to the waterworks system.

The following results on the distribution of water sources and willingness to connect according to income bracket of the respondents are also obtained from the market survey.

					1
		Income Bracket			
Sources of Water	₽900 & below	₱901- ₱1,500	₽1,501- ₽2,500	₽2,501- ₽4,500	P4,501- & above
Connected to System	13 %	27 %	45 %	49 %	61 %
Neighbor's Connection	19	15	13	11	4
Public Faucet	53	42	27	18	10
Private System	14	15	15	21	25
Willingness to Connect					. ·
Yes	33	33	29	29	20
No	54	39	26	21	19
Undecided	1	1	1.	1	1
With Own Connection	12	27	44	49	60

TABLE 9.3.1.2 DISTRIBUTION OF WILLINGNESS TO CONNECT BY INCOME BRACKET

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As shown above, around 50% of the respondents belonging to the high income group is already connected to the existing waterworks system. However, the extention of waterworks is rather limited in the low income group, being dependent mainly on public faucet for their water sources.

As the result of market survey, the respondents' willingness to connect and the user's types are shown as follows :

	· · · · · · · · · · · · · · · · · · ·			
Answer	Residential	Commercial	Industrial	<u>Total</u>
Yes :	31.3 %	21.6 %	20.4 %	30.5 %
No :	36.8	29.0	44.4	36.4
Undecided :	0.8	0.7	0.0	0.8
With Own Conn.	: 31.1	48.7	35.2	32.3

Residential users account for 92% of the total respondents and willingness to connect on the part of the respondents is only 30% of the total, while unwillingness to connect is 36%. It is observed from the result of the market survey that one third of respondents, especially in the low income group, are not willing to connect to the waterworks system in Dagupan city.

	Respondent															that inc abs.se n are true and	· ·	lwe t
STREET	Bidg. Cond.	Code 3/														fy Llo	сц.	Interviewe
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2	P2 501	P4,500														Code	•.	
		P2,500														Condi Lian Good		
	PS01	P1,500														uilding - Very	B - Good C - Fair	D - Poor
	*	and Below		-												<u></u> .		
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APPENDIX 9.7.1 FINANCIAL INTERNAL RATE OF RETURN (FIRR)

In the calculation of Financial Internal Rate of Return (FIRR), the following two indicators are normally used to evaluate financial profitability of a project.

(1) Internal Rate of Return on Investment (IRROI)

The term IRROI indicates the internal rate of return on total capital investment, and assesses the profitability of the Project as a whole and the ability to recover funds invested in the Project.

The IRROI is calculated based on the assumption that the total capital investment is covered by its own capital. Therefore, the financial conditions such as the loan conditions on borrowed capital, changes on the ratio of equity to total capital requirement and others have no effect on the IRROI. Accordingly, the IRROI indicates the profitability of the Project itself.

(2) Internal Rate of Return on Equity (IRROE)

The term IRROE indicates the internal rate of return on equity, and assesses the profitability only with respect to equity and the ability to recover funds invested in the Project as equity. Here, the IRROE is calculated on the basis of such financial conditions proper to the Project as the loan conditions on borrowed capital and amount of capital owned.

In this study, the FIRR was calculated using the same method applied in the study report of the BACOLOD CITY WATER DISTRICT PHASE II WATER SUPPLY FEASIBILITY STUDY, DRAFT REPORT VOLUME 3 by LWUA.

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APPENDIX 9.8.1 PROPOSED WATER RATE

The proposed water rates for 1/2 inch connections of commercial users, and 3/4 inch connections of domestic and commercial users to achieve financial self-sufficiency are as follows :

(1) Water rate for 1/2 inch connections of commercial users

	Rate/				
Period	Unit	First 10cu.m	<u>11-20cu.m</u>	21-35cu.m	Above 35cu.m
1988	₽1.0	₽ 50.0	P 6.8	₽ 9.2	P13.0
1989	1.5	75.0	10.2	13.8	19.6
1990	1.5	75.0	10.2	13.8	19.6
1991	2.0	100.0	13.6	18.6	26.0
1992	2.6	130.0	17.6	24.0	33.8
1993	3.0	150.0	20.2	27.8	39.0
1994	3.2	160.0	21.6	29.6	41.6
1995	3.2	160.0	21.6	29.6	41.6
1996	3.9	195.0	26.4	36.0	50.8
1997	4.5	225.0	30.4	41.6	58.6

(2)

Water rate for 3/4 inch connection of domestic users

Period	Rate/ Unit	First 10cu.m	<u>11-20cu.m</u>	<u>21-35cu.m</u>	Above 35cu.m
1988	₽1.0	₽ 40.0	₽ 5.4	₽ 7.4	₽10.4
1989	1.5	60.0	8.2	11.0	15.7
1990	1.5	60.0	8.2	11.0	15.7
1991	2.0	80.0	10.9	14.9	20.8
1992	2.6	104.0	14.1	19.2	27.0
1993	3.0	120.0	16.2	22,2	31.2
1994	3.2	128.0	17.3	23.7	33.3
1995	3.2	128.0	17.3	23.7	33.3
1996	3,9	156.0	21.1	28.8	40,6
1997	4.5	180.0	24.3	33.3	46.9

Water rate for 3/4 inch connection of commercial users

Period	Rate/ Unit	First 10cu.m	11-20cu.m	21-35cu.m	Above 35cu.m
1988	P1.0	P1130 1000.m	P10.8	P14.8	₽20.8
1989	1.5	120.0	16.4	22.0	31.4
1990	1.5	120.0	16.4	22.0	31.4
1991	2.0	160.0	21.8	29.8	41.6
1992	2.6	208.0	28.2	38.4	54.0
1993	3.0	240.0	32.4	44.4	62.4
1994	3.2	256.0	34.6	47.4	66.6
1995	3.2	256.0	34.6	47.4	66.6
1996	3.9	312.0	42.2	57.6	81.2
1997	4.5	360.0	48.6	66.6	93.8

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# LIST OF PERSONS CONCERNED

### LIST OF PERSONS CONCERNED

### ADVISORY COMMITTEE MEMBERS

Dr. Kiyoshi Yamada

Mr. Hisashi Watanabe

Mr. Masahiro Takai

Mr. Tsutomu Sakagawa (Predecessor: Mr. Yoshiro Kaburagi) Mr. Shozo Matsuura

(Predecessor: Mr. Yoichi Seki)

- Chairman of Committee, Professor, Ritsumeikan University
- Member, for Water Supply System Planning, Nagoya City
- Member, for Water Source Planning, Kobe City
- Member, for Water Supply System Planning, Ministry of Health and Welfare

- Coordinator, Japan International Cooperation Agency (JICA)

### LWUA OFFICIALS

Mr. Porthos P. Alma Jose	- Administrator
Col. Carlos C. Leaño, Jr.	- Ex-General Manager
Mr. Salvador J. Rivera	- Sr. Deputy Administrator
Mr. Ibarra J. Olgado	<ul> <li>Deputy Administrator for Regulatory</li> </ul>
Mr. Daniel I. Castillo	- Deputy Administrator for Finance
Mr. Vitaliano J. dela Vega	- Deputy Administrator for Engineering
Mr. Alfredo B. Espino	- Manager, Planning Department
Mr. Isidoro A. Yee	- Asst. Manager, Planning Department
Mr. Roberto B. Binag	- Manager, Water Systems Development Division
Mr. Eriberto R. Calubaquib	- Manager, Water Resources Division
Mr. Antonio R. de Vera	- Project Manager IV
Mr. Armando T. Fernandes	- Manager, Construction Department
Mr. Arador R. Sambo	- Manager, Water District Formation/ Review Department
Mr. Francis C. Joven	- Manager, Formation of Water District Division

### LWUA OFFICIALS (CONT'D)

Mr. Hector A. Dayrit- Manager, Rates DivisionMr. Teofilo R. Palaganas- Area Manager, Advisory Services Div.Mr. Henry I. Pacis- Water District Development Officer

Mrs. Jean C. Leoncio

Manager, Loan Evaluation Division

### OTHER AGENCIES

NIA CONSULTANTS INC.Mr. Isidro Digal- Manager, Planning DivisionMr. Lorenzo N. Macaspac- Professional Mechanical Engineer

NWRC

Atty. Elena Luz J. Alojipan

Hearing Officer, IV

MWSS

Mr. Antonio E. Kaimo

Acting Department Manager, Planning and Design Department

### ANGELES CITY

-

Mr. Francisco G. Nepomuceno	-	City Mayor	÷
Atty, Filomeno Espiritu	-	City Treasurer	
Mr. Filomeno M. Bonifacio, Jr.	-	City Engineer	
Mr. Romeo P. Calara	, 	Sr. Mechancial Engineer	

### DAGUPAN CITY

			and the second
Mr.	Liberato L. Reyna, Sr.	-	City Mayor
Mr.	Cipriano M. Manaois		Ex-Mayor
Mr.	Juanito A. Pajaro		City Treasurer
Mr.	Silverio C. Coquia	~	Waterworks Superintendent
Mr.	Manuel B. Ravanzo		City Development Coordinator

# CABUYAO, STA. ROSA AND BINAN

Atty, Felicismo T. San Luis	بىر	Governor, Province of Laguna
Mr. Romeo G. Ballesteros		Provincial Civil Security Officer
Mr. Dante T. Reyes	64 <b>4</b>	Executive Assistant/Development Coordinator
Mr. Catalino Caparas	-	Waterworks Supervisor, Province of
		Laguna
Mr. Isidro T. Hildawa		Mayor, Municipality of Cabuyao
Mr. Cesar E. Nepomuceno	·	Mayor, Municipality of Sts. Rosa
Mr. Noe C. Zarate	-	Mayor, Municipality of Biñan
Mrs. Josefa L. Pradel		Municipal Development Coordinator, Cabuyao
Mr. Felizardo P. Manto	-	Municipal Planning and Development Coordinator, Sta. Rosa
Mr. Carito P. Torres		Municipal Census Officer, Sta. Rosa

## BAYOMBONG AND SOLANO

Mrs. Belen F. Calderon	- Governor, Province of Nueva Vizcaya
Mrs. Natalia F. Dumlao	- Ex-Governor
Mr. Clamente G. Bacani	- Provincial Secretary
Mr. Artemio P. Bahia	- Provincial Attorney
Mr. Jesus M. Calata	- Provincial Engineer
Mr. Tomas C. Garra	<ul> <li>Supervising Project Analyst</li> <li>Provincial Planning &amp; Develop't</li> <li>Office</li> </ul>
Mr. Geoffrey B. Magday	- Concurrent Provincial Waterworks Officer
Capt, Federico M. Bolusan	- Provincial Waterworks Supervisor

Mr. John Bagasao	***	Mayor, Municipality of Bayombong
Mr. Lunbert Galima		Mayor, Municipality of Solano

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# STUDY TEAM MEMBERS

Mr. Toru Hayashi	Regt.	Team Leader Legistration/Organization Nippon Jogesuido Sekkei Co., Ltd. (NJS)
Mr. Masatoshi Momose	- <b>1</b>	Water Supply System Planning, NJS
Mr. Chikara Amitani		Water Supply System Planning, NJS
Mr. Masuomi Hiroyama	***	Transmission/Distribution System Planning, NJS
Mr. Hideaki Fukui	. <del>-</del> .	Transmission/Distribution System Planning, NJS
Mr. Takafumi Kiguchi	· <u>-</u>	Facility Design, NJS
Mr. Yukio Maejima		Water Source Planning, NJS
Mr. Fumiaki Ichino	_	Water Source Planning, Richo Soil Investigation Co., Ltd.
Mr. Mitsuo Tsutsumi		Well Development, NJS
Mr. Masaaki Awamoto	-	Financial and Economic Analysis, Techno Consultants, Inc.

# MINUTES OF THE MEETINGS

# MINUTES OF THE MEETING MUNICIPAL WATER SUPPLY PROJECT STUDY

Manila, March 25, 1986

Tona Hayash'

Toru Hayashi Study Team Leader Japan International Cooperation Agency

Atty. Ibarca 01 Officer in charge LWUA

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### MINUTES OF THE MEETING

A series of meetings between JICA survey team and LWUA personnel regarding the Inception Report were held during March 18 to March 24, 1986 to confirm the objectives, scope of work and schedule for implementation of the study. Also discussed during the meetings were undertakings by both parties and approaches to the project.

The following are the items agreed upon:

J. Objective of the Study

The objective of the study is to prepare Basic Development Plan and Short Term Development Plan for the water supply projects in the following four project areas.

- 1. Angeles City, Pampanga
- 2. Dagupan City, Pangasinan
- 3. Cabuyao, Sta. Rosa and Binan, Laguna
- 4. Bayombong and Solano, Nueva Vizcaya

2. Scope of the Study

The study will be conducted in four (4) phases including works both in the Philippines and in Japan. The following are the outline of each phase:

2.1 Phase 1: Formulation of Basic Development Plan

- a) Collection and review of data and information available
- b) Implementation of field survey
- c) Outline of Basic Development Plan
- d) Preparation of framework for the Feasibility Study
- e) Preparatory work for implementation of Phase 11 study

2.2 Phase 11: Field Investigation for Preparation of the feasibility Study

- a) Field Investigation
  - o Geoelectric prospecting
  - o Test well drilling and pumping test
  - o Inventory of wells and pumping tests of selected existing wells
  - o Measurement of yield at springs

- o Testing of existing pumps
- o Measurement of unaccounted-for-water and hydraulic survey
  - o Investigation of existing water supply facilities
- b) Study of availability of materials and equipment for construction and improvement of water supply facilities and capability of local contractors
- c) Review of design criteria for design of proposed water supply facilities
- d) Study of the alternative water supply schemes
- 2.3 Phase 111: Preparation of Feasibility Study (Draft Final Report)
  - a) Preliminary design of the recommended water supply systems among alternatives
  - b) Recommendation on organization/management of the system and establishment of water districts
  - c) Implementation schedule
  - d) Cost estimation for construction, operation, and maintenance of the system
  - e) Financial study
- 2.4 Phase IV: Preparation of Final Report
- 3. Approach to the Project

3.1 Development of Master Plan

a) Study Area

Study of fundamentals for the development of Master Plan will be made covering the entire city/municipality. However, the plan for the water supply system should be limited to those areas to be covered by level II/III systems.

b) Target Year

The base year for planning is 1986 in principle and target year is 2010. In addition, the years, 1990, 1995 and 2000 shall be considered although detailed study, such as breakdown of population by sub-area shall be only made for the present, 1990 and 2010.

an

c) Plan of Water Supply System

Layout of the existing and proposed pipelines and other major facilities will be shown on the map

d) Rough Cost Estimates

Rough cost estimates will be made using cost data prepared by the LWUA for feasibility studies.

e) Water Sources

Based on the data on water resources collected during Phase f, applicable water sources will be recommended to meet the water demands and other conditions including socio-economic needs.

f) Establishment of the Water District

- Information on the willingness by the cities and municipalities as well as present problem areas in management of the existing water supply systems will be collected and evaluated to make recommendations for implementation of the water supply project.
- 3.2 Preparation of Framework for the Short Term Development Plan
  - a) Previous reports, if any, prepared by the city/municipality will be reviewed. The subject area will be recommended in consideration of existing service area, potential water resources, needs and willingness of the inhabitants, and financial viability. Marketing surveys will be conducted by the LWUA financial specialists to support the study.

b) 'Target Year -

The base year is 1986 in principle and target year is 1990 for the four project areas.

c) Water Sources

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Existing water sources including springs and deep wells will be evaluated to their maximum safe capacities. Improvement of existing source facilities and new development requirements will also be studied.

d) Preparatory work for the field survey during Phase II.

Most of the measurements in the field will be conducted during the Phase II. Since the work for test well drilling is critical, timely arrangement/procurement of equipment and material at the initial stage of the Phase II is indispensable. Detailed discussion to reach an agreement for the purpose between two parties. will be made during the last two weeks of Phase I period reflecting the result of field survey and collected information. Responsibilities by each party for implementation of the field examination will be accomplished in accordance with the minutes exchanged on October 23, 1985.

4. Schedule for Implementation of the Study

4.1 Phase 1

JICA team started field work from March 17 and is scheduled to finish its Phase I work on April 27. Discussions on the methodologies and required arrangements as well as collection and review of data will be conducted in Manila during first half of the study period. Field trip to the subject cities/municipalities will be done within two weeks during latter half of the study period. The outline of the basic development plan and framework of the short term plan will be prepared by the end of this Phase. Detailed schedule is attached herewith.

4.2 Phase II to Phase IV

Phase II field work is tentatively scheduled to start from the beginning of June 1986 and Final Report will be submitted at the end of February 1987 in Phase IV period.

5. Undertakings by JICA and LWUA

In accordance with the agreement between JICA and LWUA signed on October 23, 1985, each party will accomplish its responsibilities.

# SCHEDULE FOR IMPLEMENTATION OF THE STUDY

Date		Activities	
March 17	Mon	1st Group: Tokyo-Manila, visit to Japan Embas	BY & JICA.
18	Tue	A.M.: Courtesy call on LWUA, P.M.: Explanation of and discussions on Incep	tion Report.
19	Wed	Discussions on Inception Report, data collection arrangements.	on and required
20	Thur	Preparation of minutes and data collection.	
21	Fri	Exchange of minutes.	
22	Sat	Inner meeting of Survey Team.	
(23)	Sun	- do -	
24	Mon	Collection and review of data and information.	
25			
	Tue	2nd Group: Tokyo-Manila, review of data and in	liormation.
26	Wed	<ul> <li>Analysis of data and information collected.</li> <li>Preparatory work for the field survey</li> </ul>	
△ 27	Thur		
△28	Fri	) Analysis of data and information collected.	
$\begin{array}{c} \bigtriangleup 29\\ 30\end{array}$	Sat Sun	) B Group: Manila-Dagupan/	& C Group: Manila- Dagupan
31	Mon	A Group: Cabuyao, etc <sup>4</sup> / Dagupan City	Dagupan City
April 1	Tue	• Data collection . Data collection	
2	Wed	. Field Survey . Field Survey	
		• Discussions with • Discussions with officers officers	
3	Thur	t t	Bayombong, Solano
4	Fri	Ϋ́	
5	Sat	Preparation of Field/ Preparation of Field Report Report	C Group: Dagupan
6	Sun	e do - do	Dagupan-Manila
7	Mon		ACabuyao, etc.
8	Tue	. Data collection . Data collection	
9	Wed		Angeles City
	Thu	• Discussions with • Discussions with officers • officers	
11	Fri	¥	<b>Y</b> (92)

April	12	Sat	Preparation of Field Report	Preparation of Field Report
	13	Sun	- do -	B Group: Dagupan-Manila
	14	Mon	Review of data and in	
	15	Tue	Preparation of Basic short term plan	Development Plan and Framework of
	16	Wed	- do -	•
	17	Thur	- do -	•
	18	Fri	- do -	•
	19	Sat	- do -	
	20	Sun	Preparation of Repor	t service and the service s
	21	Mon	Preparation of Report	t state in the state of the sta
	22	Tue	- do -	
	23	Wed	- do -	
	24	Thur	Meeting with LWUA	
	25	Fri	Meeting with LWUA and	d visit to JICA and Embassy
	26	Sat	Inner meeting	
	27	Sun	Manila - Tokyo	

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MINUTES OF MEETING

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MUNICIPAL WATER SUPPLY PROJECT STUDY

Manila, June 18, 1986

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Toru Hayashi Study Team Leader Japan International Cooperation Agency

Porthos/ P. Alma Jose

Administrator Local Water Utilities Administration

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A series of meeting between the JICA study team and LWUA officials regarding the Phase II Study Program for the Municipal Water Supply Project were held from June 9 to June 18, 1986 to confirm the placement of the Progress Report, scope of work and schedule of implementation of the study. Also discussed during the meeting were undertakings by both parties and approaches to the Phase II Study.

The following are the items agreed upon:

1. Progress Report

The study team submitted ten (10) copies of the Progress Report to LWUA on June 8, 1986.

2. Contents of the Phase II Study

2.1 Plan of Water Supply System

A plan of water supply system for the years 2010 and 1995 shall be prepared showing relationship of the major facilities and shall be incorporated in the Final Reports.

### 2.2 Basic development Plan

The Basic Development Plan (2010) is recommended in the Progress Report as a result of the alternative study including potential water sources and required facilities. Supplemental description and schematic drawings will be prepared. Cost comparison between alternatives will be made based on the present cost.

2.3 Short Term Development Plan

The water supply system for the immediate improvement (1995) should be planned considering the relation to the Basic Development Plan.

2.4 Hydraulic Calculation

Hydraulic calculation on the recommended water supply system should be carried out.

2.5 Target Year

The target year for the immediate improvement is 1995. Required study for the fundamentals will be made for the year 1986 (base year), 1995 (immediate improvement) and 2010 (long term development), respectively. Implementation schedule for the year 1990 may also be included as the stage 1 of the immediate improvement program. 2.6 Design Criteria

Design criteria for feasibility study should follow the LWUA guidelines. To some extent, however, alternatives may be accepted if reasons are justifiable.

2.7 Composition of Reports

Composition of Interim Report and Draft Final Report will be finalized through the discussion between the Study Team and LWUA during the Phase II Study period.

3. Arrangement for Phase II Study

3.1 Land acquisition for Test Well Sites

LWUA shall at its own expense, be responsible for the land acquisition for test wells prior to the scheduled test well drilling.

3.2 Preparation for Drilling Equipment

In accordance with the Minutes of Meeting between JICA and LWUA dated October 23, 1985, LWUA shall at its own expense, be responsible for the provision of equipment for test well drilling.

One drilling rig shall be provided within the month of June, and another one beginning July.

Test well drilling in the three study areas shall be completed within the Phase II Study period.

3.3 Safekeeping of Materials for Test Wells

LWUA shall be responsible for safekeeping of materials for test wells which are supplied by JICA.

3.4 Field Survey

1. Schedule of the LNUA Engineers.

Required arrangements be made by the LHUA according to the following schedule:

Rodolfo Oamil :	6/16 - 7/15	(Angeles City)
Allen Lowe :		(Cabuyao, Sta.
		Rosa, Biñan)
Abelardo Buencamíno:	6/16 - 7/13	(Dagupan)
Melchor Casil :	7/13 - 8/16	(Bayombong &
		Solano)

Schedule for the two hydrogeologists will be decided after making arrangement of drilling machine.

7.6

2. Living allowance and travel cost for LWUA Engineers

LWUA is responsible for LWUA Engineer and well drillers.

In accordance with the schedule, they may work on Saturday/Sunday, if necessary.

3. Vehicle arrangement

Land Cruiser : LWUA will provide a vehicle (Land Cruiser) for the survey in Dagupan and Bayombong and Solano from June 16 (Mon) to August 15, 1986.

 Preparation of road map for Cabuyao, Sta. Rosa and Biñan.

LWUA (Allen) will prepare and confirm (in the area) the road network for the subject area planned in the progress report. Aerial photograph be utilized for this purpose. This work should be completed by the beginning of July.

#### 3.5 Market Survey

LWUA shall conduct the Market Survey for Angeles City on the third week of June.

3.6 Water Quality Analysis

Necessary arrangements for water quality analysis will be made at the LWUA laboratory or other institutions.

3.7 Electric Logging Equipment

LWUA will provide the study team with a set of electric logging equipment.

3.8 Data on Unit Cost

LWUA shall assist the study team in the collection of necessary data for unit cost.

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### 22 September 1985

### MINUTES OF AGREEMENT BETWEEN LNUA AND JICA

Discussions on the Interim Report and the requirement for completion of the Draft Final Report were made between the two parties (JICA and LWUA) from September 18 to 22, 1986. Fundamentals for planning water supply system for the four study areas and basic approach/figures which were incorporated in the Interim Report were agreed upon discussions. In addition, the following major subjects were confirmed by the two parties:

(1) Completion of Test Well Construction

The scheduled test well construction at the three sites, Degupan, Angeles, and Sta. Rosa is behind schedule due to the delay of procurement of well drilling equipment, repair of broken equipment, land acquisition for test well sites as well as unfavorable weather.

Under these circumstances, the parties agreed that LWUA will make all efforts to catch up with the delay of construction.

### (2) Draft Final Report

The major items to be included in the report are as follows:

Chapter	1	Summary and Recommendations
Chapter		General Background
Chapter	3	Description of the Study Area
Chapter	4	Existing System
Chapter	5	Population and Water Demand Projections
Chapter	6	kater Resources
Chapter	7	Analysis and Evaluation of Alternatives
Chapter	3	Recommended Plan
Chapter	9	Financial Feasibility Analysis
Chap cer-	10	Economic Feasibility Analysis
Chap ter	11	Organization and Management Study

Drawings to be prepared comprise general plan and standard drawings for major facilities.

Noted: **Sulli** ALFTEDG B, ESPINO Planning Manager

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TORU HAYASHI Team Leader - JICA

MINUTES OF MEETING MUNICIPAL WATER SUPPLY PROJECT STUDY

Manila, December 8,1986

Joru Hayashi

Toru Hayashi Study Team Leader Japan International Cooperation Agency

Porthos P. Alma Jose

Administrator Local Water Utilities Administration

### MINUTES OF THE MEETING

A series of meeting between JICA survey team and LWUA personnel regarding the Draft Final Report on Municipal Water Supply Project were held during the period December 2 to December 8, 1986 to present the report on the study and confirm its contents.

From Chapter 2 to Chapter 5, i.e., General Background, Description of the Study Area, Existing Water Supply and Sanitation Conditions, and Population and Water Demand Projections, no problem was noted since the contents of these chapters have already been discussed and concurred by both parties at the time the Progress Report and Interim Report were submitted.

The major items to be revised/~upplemented are as follows:

### Technical Aspect

- Alternative study of transmission/distribution pipeline system
  - . Staged construction of pipeline:

An economic evaluation of staging construction of transmission and distribution mains will be studied and presented in the report. Two phases of construction should at least be considered taking into consideration the following recommended construction Phases:

Phase	Ι	-	(1989-1995)
Phase	II	-	(1996-2010)

- Alternative of pipeline routes: If there are available roads, 2 alternatives will be studied for major main routes. Others will be discussed and cancelled.
- . Economic cost comparison

As per request of LWUA, economic evaluation will be made for the discount rate of 12 percent. The estimation using the rates of 10% and 15% will also be made for reference purpose.

- Hydraulic calculation for the distribution network. The computation results of alternative and recommended distribution system will be incorporated in the Appendix.
- 3. Review and revise/supplement the alternative study, Chapter 7 with reference to the presentation.
- 4. Preparation of implementation schedule using bar-chart. Based on the implementation program shown in the Draft Final Report, bar-chart showing construction period by phase will be prepared for major facilities. That for Phase II is roughly prepared.

5. Preparation of a plan of water supply facilities showing the differences of construction phases. The scale of the plan may be approximately from 1/20,000 to 1/25,000.

6. Cost estimates

Required cost for the services of leakage detection and for repair/replacement of existing pipes and accessories will be added under the following conditions:

- a) Old laterals: The subject length of the pipeline is 10-30% of the total length of existing laterals. Unit cost is that for new construction.
- b) Service Connections: Required cost is estimated based on the unit cost given below

{P850 (material) + labor cost} x No. of existing connections

c) Cost for leak detection: P240/connect x No. of existing connections

7. Study of economical sizing of pump transmission mains.

### Financial Aspect

1. Financial scheme should not include government grant since the policy of the LWUA changed two months ago. The soft loan may be utilized to supplement regular loan. LWUA can extend soft loans up to a maximum of 50% of the total project cost.

A certain percent of Water District equity to the total construction cost may be considered depending on the ability-to-pay of the W.D.

2. Per latest policy Engineering cost is computed as a fixed percentage of estimated construction cost (ECC). ECC is equal to the summation of basic construction cost, physical contingencies and price contingencies. The percentages are:

> ECC  $\leq$  P2OM = Engineering cost is 13% of ECC ECC > P2OM = Engineering cost is 10% of ECC

Construction supervision is 4% of ECC

3. Debt service table

- a) Standard procedure = Regular loan can finance disbursements for the first four (4) years and soft loan for the next 4 years. However, the combination of the two types may be adopted.
- b) Preparation of separate debt service tables for regular loan and for soft loan.

- 4. Preparation of a table for unescalated 0 & M costs
- 5. Equivalent volume of water sold
  - . Water consumption for the first 10 cu.m will be calculated using the total number of domestic connections and 10 cu.m/connection
  - Range of water consumption maybe as follows:
    - 1) First 10 cu.m, 2) 11-20 3) 21-35 4) over 35

The present percentages for the ranges from 11 cu.m to over 35 cu.m will be used for the calculation of the total equivalent volume.

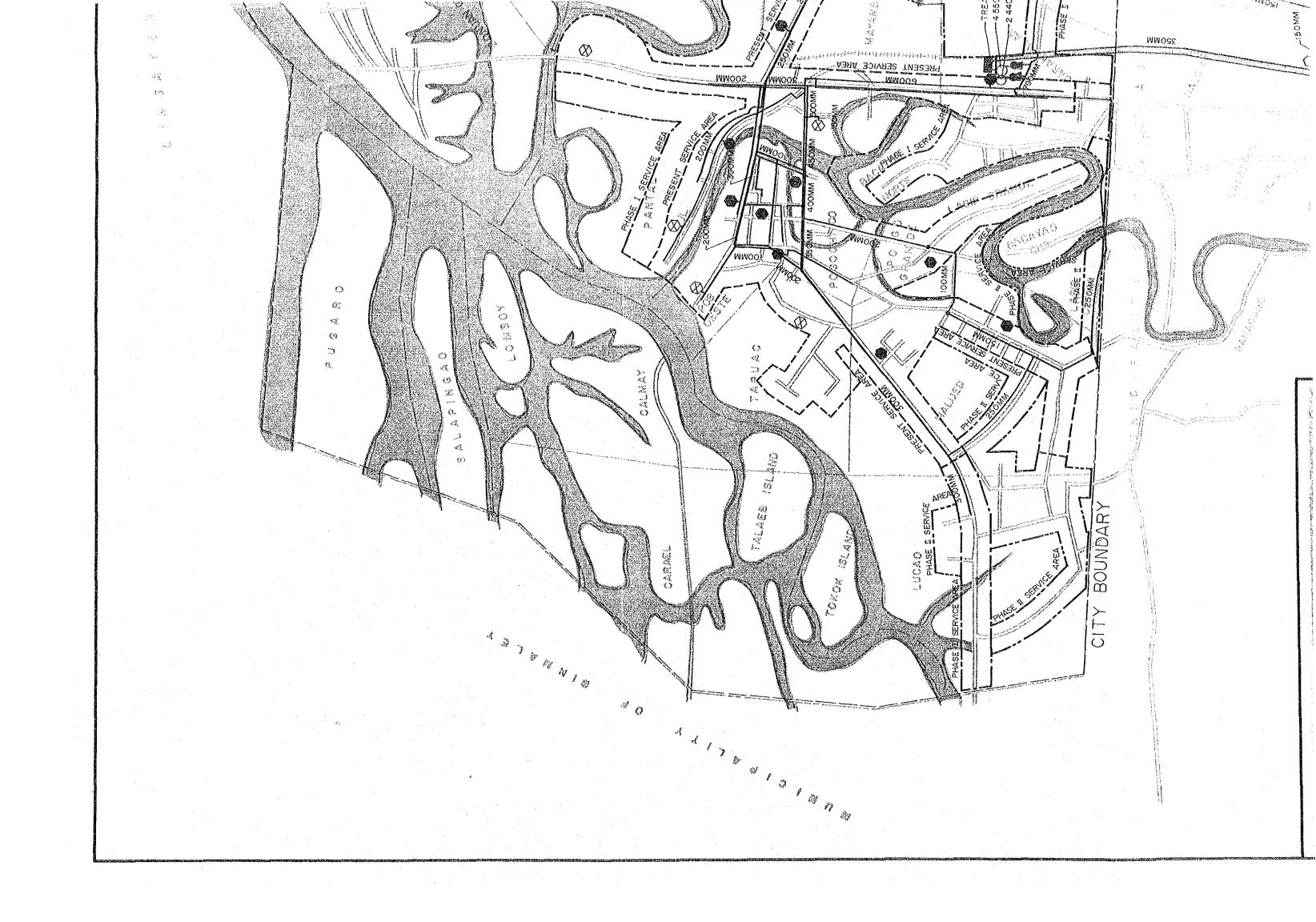
6. Financial Internal Rate of Return (FIRR) computation

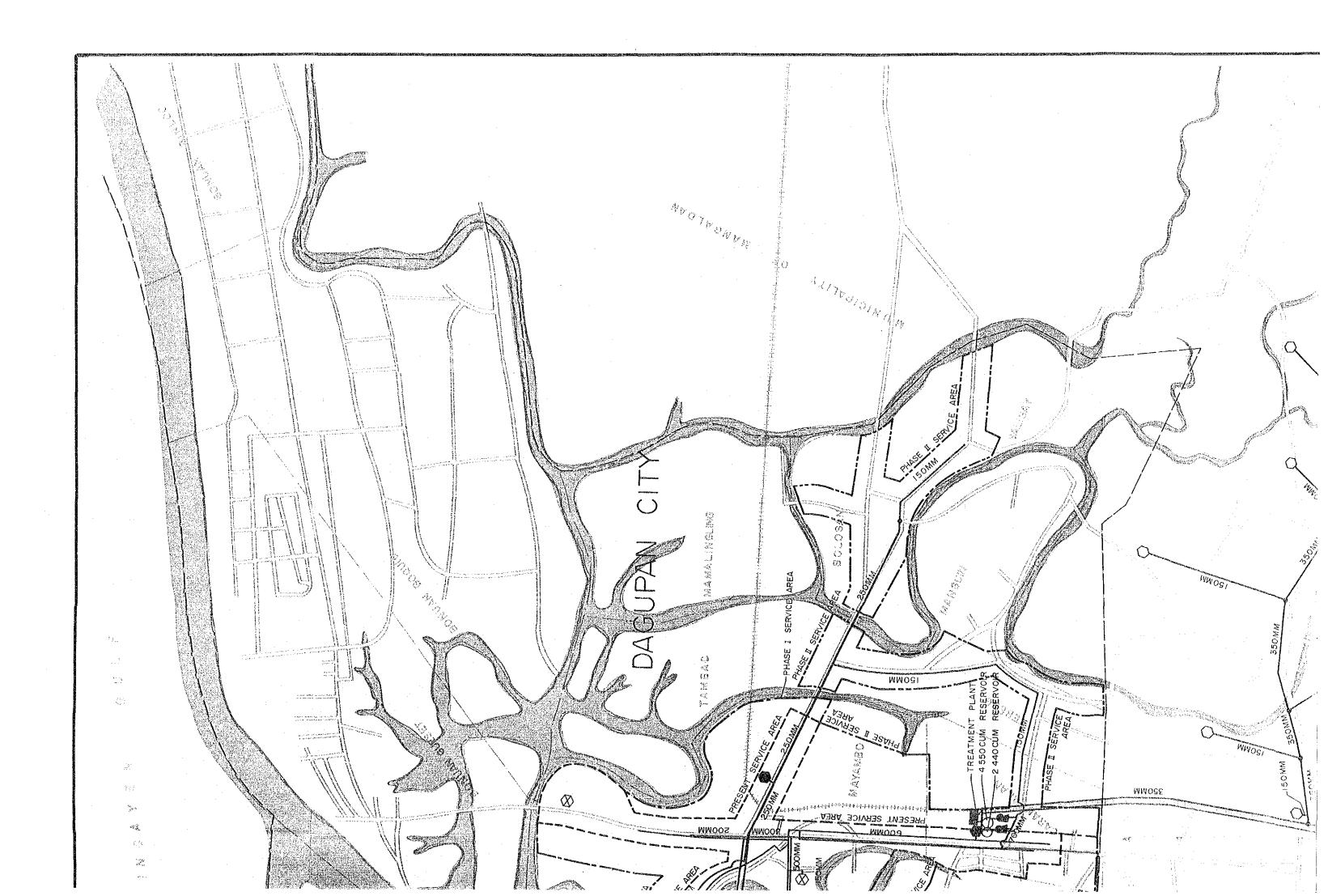
In conformance with LWUA procedure FIRR will be computed based on the total investment not just the portion funded by WD equity to measure the efficiency of the project as a whole.

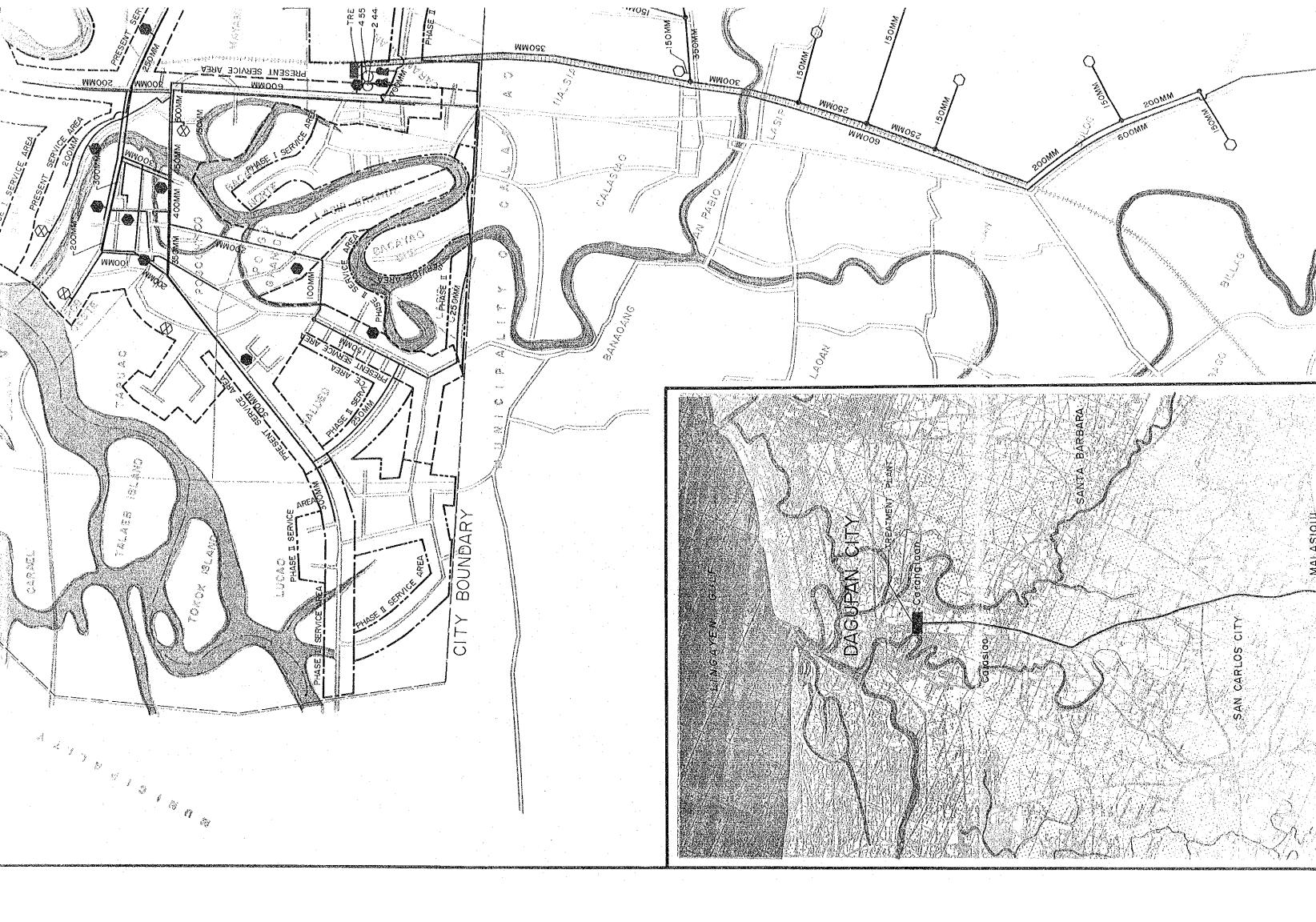
The FIRR may at least be equal to the weighted average of the interest rates of the loans (regular and soft loans). The period for this analysis can be extended (20 to 40 years).

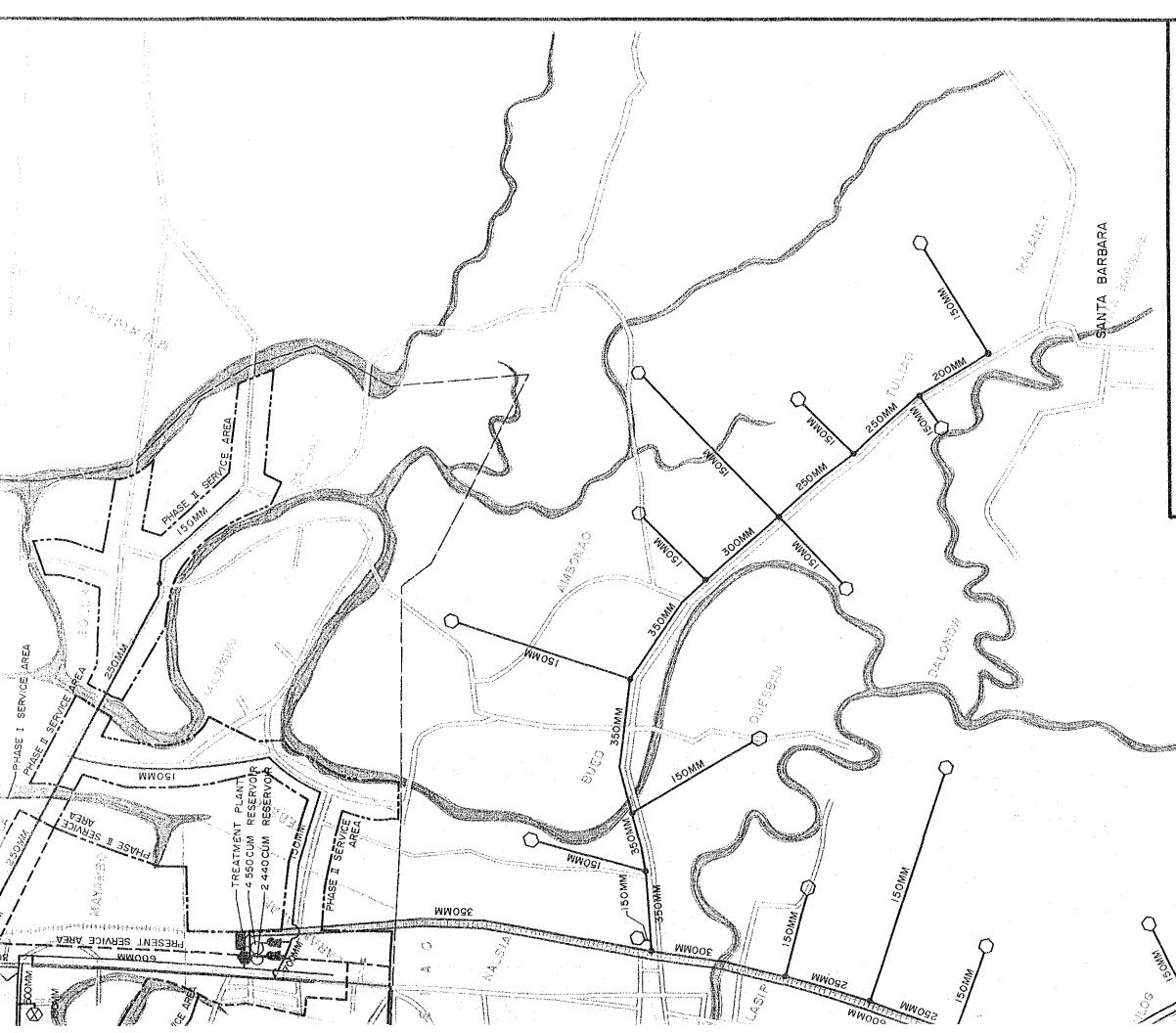
- 7. As per LWUA standards, fifteen (15%)percent inflation rate is used.
- 8. Economic Analysis

In consideration of the characteristics of the project, IERR may be lower than the desired level.

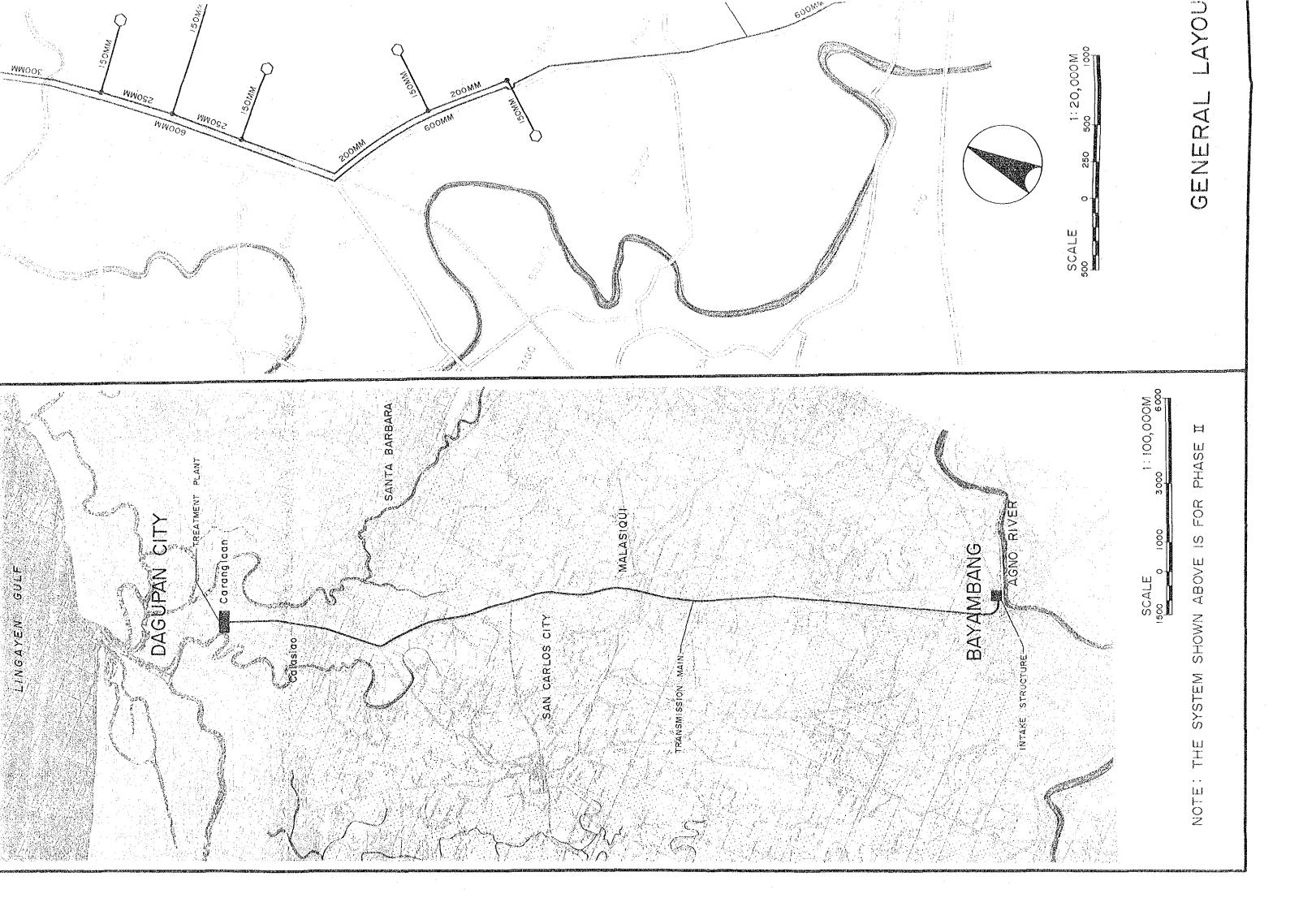


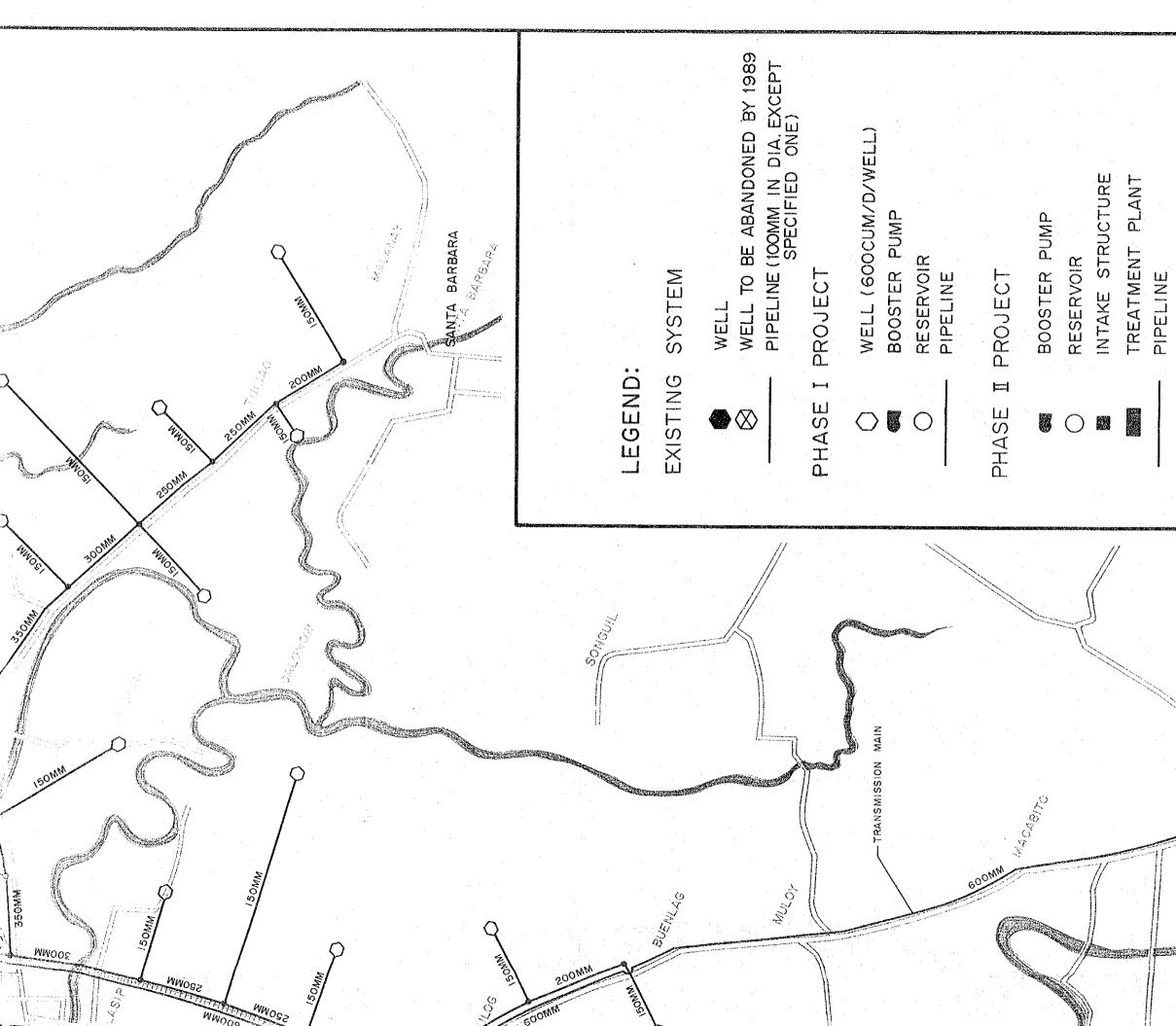






WELL TO BE ABANDONED BY 1989 PIPELINE (100MM IN DIA. EXCEPT SPECIFIED ONE) WELL (600CUM/D/WELL) BOOSTER PUMP RESERVOIR SYSTEM PROJECT WELL LEGEND: EXISTING t----1 PHASE  $\bigcirc$ MAIN SS 





WATER SUPPLY SYSTEM AREA AREA AREA AREA BOUNDARIES SERVICE SERVICE SERVICE PRESENT 日 H--4 PHASE PHASE SERVICE RECOMMENDED TY, PANGASINAN RCH 1987  $\sim$ . 00 FIGURE CITY, MARCH OF TH DAGPAN TO INTAKE STRUCTURE AT BAYAMBANG RAL LAYOUT 1: 20,000 M 

