(8) Dissolved Matters Case 2, Case 3 (1/3)

Y	M	Cu	Zn	As	Cu	Zn	As
21	7	0.0076	0.0198	0.0036	0.0076	0.0198	0.0036
21	8	0.0074	0.0154	0.0031	0.0074	0.0154	0.0031
21	9	0.0056	0.0146	0.0030	0.0056	0.0146	0.0030
21	10	0.0047	0.0139	0.0030	0.0047	0.0139	0.0030
21	11	0.0035	0.0151	0.0031	0.0035	0.0151	0.0031
21	12	0.0028	0.0173	0.0033	0.0028	0.0173	0.0033
22	1	0.0018	0.0200	0.0032	0.0023	0.0199	0.0034
22	2	0.0018	0.0190	0.0032	0.0022	0.0227	0.0037
22	3	0.0021	0.0178	0.0031	0.0026	0.0253	0.0040
22	4	0.0025	0.0160	0.0030	0.0032	0.0287	0.0045
22	5	0.0025	0.0131	0.0028	0.0046	0.0305	0.0045
22	6	0.0025	0.0104	0.0027	0.0056	0.0271	0.0042
22	7	0.0025	0.0082	0.0025	0.0072	0.0194	0.0036
22	8	0.0024	0.0078	0.0025	0.0072	0.0152	0.0031
22	9	0.0021	0.0078	0.0024	0.0055	0.0144	0.0030
22	10	0.0019	0.0073	0.0024	0.0045	0.0137	0.0030
22	11	0.0018	0.0072	0.0024	0.0033	0.0148	0.0031
22	12	0.0018	0.0071	0.0025	0.0025	0.0170	0.0032
23	1	0.0018	0.0071	0.0025	0.0023	0.0196	0.0034
23	2	0.0018	0.0071	0.0025	0.0022	0.0225	0.0036
23	3	0.0021	0.0072	0.0025	0.0026	0.0252	0.0040
23	4	0.0025	0.0072	0.0025	0.0033	0.0286	0.0045
23	5	0.0025	0.0071	0.0025	0.0046	0.0304	0.0045
23	6	0.0025	0.0068	0.0025	0.0056	0.0271	0.0042
23	7	0.0025	0.0066	0.0024	0.0072	0.0193	0.0036
23	8	0.0024	0.0072	0.0024	0.0072	0.0151	0.0031
23	9	0.0021	0.0074	0.0024	0.0055	0.0144	0.0030
23	10	0.0019	0.0070	0.0024	0.0045	0.0137	0.0030
23	11	0.0018	0.0069	0.0024	0.0033	0.0148	0.0031
23	12	0.0018	0.0069	0.0024	0.0025	0.0170	0.0032
24	1	0.0018	0.0069	0.0024	0.0023	0.0196	0.0034
24	2	0.0018	0.0070	0.0025	0.0022	0.0225	0.0036
24	3	0.0021	0.0071	0.0025	0.0026	0.0252	0.0040
24	4	0.0025	0.0071	0.0025	0.0033	0.0286	0.0045
24	5	0.0025	0.0070	0.0025	0.0047	0.0304	0.0045
24	6	0.0025	0.0068	0.0025	0.0056	0.0270	0.0042
24	7	0.0025	0.0066	0.0024	0.0073	0.0193	0.0036
24	8	0.0024	0.0072	0.0024	0.0072	0.0151	0.0031
24	9	0.0021	0.0074	0.0024	0.0055	0.0143	0.0030
24	10	0.0019	0.0071	0.0024	0.0045	0.0137	0.0030
24	11	0.0018	0.0070	0.0024	0.0033	0.0148	0.0031
24	12	0.0018	0.0069	0.0024	0.0025	0.0170	0.0032
25	1	0.0018	0.0070	0.0024	0.0023	0.0196	0.0034
25	2	0.0018	0.0070	0.0025	0.0022	0.0225	0.0036
25	3	0.0021	0.0071	0.0025	0.0026	0.0252	0.0040
25	4	0.0025	0.0071	0.0025	0.0033	0.0286	0.0045
25	5	0.0025	0.0070	0.0025	0.0047	0.0304	0.0045
25	6	0.0025	0.0068	0.0025	0.0056	0.0270	0.0042

(8) Dissolved Matters Case 2, Case 3 (2/3)

Y	M	Cu	Zn	As	Cu	Zn	As
25	7	0.0025	0.0066	0.0024	0.0073	0.0193	0.0036
25	8	0.0024	0.0072	0.0024	0.0072	0.0150	0.0031
25	9	0.0021	0.0075	0.0024	0.0055	0.0143	0.0030
25	10	0.0020	0.0071	0.0024	0.0045	0.0136	0.0030
25	11	0.0019	0.0070	0.0024	0.0033	0.0148	0.0031
25	12	0.0018	0.0070	0.0024	0.0025	0.0170	0.0032
26	1	0.0018	0.0070	0.0024	0.0023	0.0196	0.0034
26	2	0.0019	0.0070	0.0025	0.0022	0.0225	0.0036
26	3	0.0021	0.0071	0.0025	0.0026	0.0251	0.0040
26	4	0.0025	0.0072	0.0025	0.0033	0.0286	0.0045
26	5	0.0026	0.0070	0.0025	0.0047	0.0304	0.0045
26	6	0.0025	0.0068	0.0025	0.0056	0.0270	0.0042
26	7	0.0025	0.0066	0.0024	0.0073	0.0192	0.0036
26	8	0.0024	0.0072	0.0024	0.0072	0.0150	0.0031
26	9	0.0021	0.0075	0.0024	0.0055	0.0143	0.0030
26	10	0.0020	0.0071	0.0024	0.0045	0.0142	0.0030
26	11	0.0019	0.0070	0.0024	0.0033	0.0147	0.0031
26	12	0.0018	0.0070	0.0024	0.0025	0.0169	0.0032
27	1	0.0018	0.0070	0.0024	0.0024	0.0196	0.0034
27	2	0.0019	0.0070	0.0025	0.0023	0.0225	0.0036
27	3	0.0021	0.0071	0.0025	0.0026	0.0251	0.0040
27	4	0.0026	0.0072	0.0025	0.0033	0.0286	0.0045
27	5	0.0026	0.0070	0.0025	0.0047	0.0304	0.0045
27	6	0.0025	0.0068	0.0025	0.0057	0.0269	0.0042
27	7	0.0025	0.0066	0.0024	0.0073	0.0192	0.0036
27	8	0.0024	0.0073	0.0034	0.0072	0.0150	0.0031
27	9	0.0021	0.0075	0.0024	0.0055	0.0142	0.0030
27	10	0.0020	0.0071	0.0024	0.0045	0.0136	0.0030
27	11	0.0019	0.0070	0.0024	0.0033	0.0147	0.0031
27	12	0.0018	0.0070	0.0024	0.0025	0.0169	0.0032
28	1	0.0018	0.0070	0.0024	0.0024	0.0196	0.0034
28	2	0.0019	0.0070	0.0025	0.0023	0.0225	0.0037
28	3	0.0022	0.0071	0.0025	0.0026	0.0251	0.0040
28	4	0.0026	0.0072	0.0025	0.0033	0.0286	0.0045
28	5	0.0026	0.0070	0.0025	0.0047	0.0304	0.0045
28	6	0.0026	0.0068	0.0025	0.0057	0.0269	0.0042
28	7	0.0026	0.0066	0.0024	0.0073	0.0191	0.0036
28	8	0.0024	0.0073	0.0024	0.0072	0.0149	0.0031
28	9	0.0021	0.0076	0.0024	0.0055	0.0142	0.0030
28	10	0.0020	0.0072	0.0024	0.0045	0.0135	0.0030
28	11	0.0019	0.0070	0.0024	0.0033	0.0147	0.0031
28	12	0.0018	0.0070	0.0024	0.0025	0.0169	0.0032
29	1	0.0018	0.0070	0.0024	0.0024	0.0195	0.0034
29	2	0.0019	0.0071	0.0025	0.0023	0.0225	0.0037
29	3	0.0022	0.0071	0.0025	0.0026	0.0251	0.0040
29	4	0.0026	0.0072	0.0025	0.0033	0.0286	0.0045
29	5	0.0026	0.0070	0.0025	0.0047	0.0304	0.0045
29	6	0.0026	0.0068	0.0025	0.0057	0.0269	0.0042

(8) Dissolved Matters Case 2, Case 3 (3/3)

Y	M	Cu	Zn	As	Cu	Zn	As
29	7	0.0026	0.0066	0.0024	0.0073	0.0191	0.0035
29	8	0.0024	0.0073	0.0024	0.0072	0.0149	0.0031
29	9	0.0021	0.0076	0.0024	0.0055	0.0141	0.0030
29	10	0.0020	0.0072	0.0024	0.0045	0.0135	0.0030
29	11	0.0019	0.0070	0.0024	0.0033	0.0147	0.0031
29	12	0.0018	0.0070	0.0024	0.0025	0.0169	0.0032
30	1	0.0018	0.0070	0.0024	0.0024	0.0195	0.0034
30	2	0.0019	0.0071	0.0025	0.0023	0.0225	0.0037
30	3	0.0022	0.0071	0.0025	0.0026	0.0251	0.0040
30	4	0.0026	0.0072	0.0025	0.0033	0.0286	0.0045
30	5	0.0026	0.0070	0.0025	0.0047	0.0304	0.0045
30	6	0.0026	0.0068	0.0025	0.0057	0.0269	0.0042
30	7	0.0026	0.0066	0.0024	0.0074	0.0190	0.0035
30	8	0.0024	0.0074	0.0024	0.0072	0.0148	0.0031
30	9	0.0021	0.0076	0.0024	0.0055	0.0141	0.0030
30	10	0.0020	0.0072	0.0024	0.0045	0.0135	0.0030
30	11	0.0019	0.0070	0.0024	0.0033	0.0146	0.0031
30	12	0.0018	0.0070	0.0024	0.0025	0.0169	0.0032
31	1	0.0018	0.0070	0.0024	0.0024	0.0195	0.0034
31	2	0.0019	0.0071	0.0025	0.0023	0.0225	0.0037
31	3	0.0022	0.0071	0.0025	0.0026	0.0251	0.0040
31	4	0.0026	0.0072	0.0025	0.0033	0.0286	0.0045
31	5	0.0026	0.0070	0.0025	0.0048	0.0304	0.0045
31	6	0.0026	0.0068	0.0025	0.0057	0.0268	0.0042
31	7	0.0026	0.0066	0.0024	0.0074	0.0190	0.0035
31	8	0.0025	0.0074	0.0024	0.0072	0.0148	0.0031
31	9	0.0021	0.0077	0.0024	0.0055	0.0141	0.0030
31	10	0.0020	0.0072	0.0024	0.0045	0.0134	0.0030
31	11	0.0019	0.0071	0.0024	0.0033	0.0146	0.0031
31	12	0.0018	0.0070	0.0024	0.0025	0.0169	0.0032

(9) Suspended Solids Run-1 (Soluble) (1/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
1	9	1099	4.7	303	88	391	7.6	1.6	0.0	3.5	0.5	0.0	123	53	0
1	10	1647	3.9	397	122	519	7.2	1.4	0.0	3.3	0.4	0.0	120	52	0
1	11	3056	2.9	662	226	888	6.5	1.0	0.0	3.0	0.2	0.0	114	49	0
1	12	3743	2.6	787	0	787	6.3	1.1	0.0	2.9	0.2	0.0	155	65	0
2	1	2254	3.3	551	0	551	6.8	2.1	0.0	3.1	0.4	0.0	172	68	0
2	2	1422	3.8	475	0	475	7.1	3.1	0.0	3.3	0.5	0.0	189	70	0
2	3	1028	3.8	558	0	558	7.1	3.3	0.0	3.3	0.6	0.0	193	73	0
2	4	2117	2.0	2245	0	2245	5.8	0.8	0.0	2.7	0.2	0.0	151	65	0
2	5	1038	2.8	1222	0	1222	6.4	1.8	0.0	3.0	0.4	0.0	168	68	0
2	6	719	3.4	899	292	1192	6.8	2.2	0.0	3.1	0.4	0.0	132	52	0
2	7	880	3.1	994	331	1326	6.6	1.3	0.0	3.1	0.3	0.0	118	50	0
2	8	1908	2.8	965	334	1300	6.4	0.7	0.0	3.0	0.2	0.0	109	48	0
2	9	1053	4.9	274	78	352	7.8	2.7	0.0	3.6	0.5	0.0	138	54	0
2	10	1641	4.0	397	122	519	7.2	1.8	0.0	3.3	0.4	0.0	126	52	0
2	11	3044	2.9	663	226	889	6.5	1.2	0.0	3.0	0.2	0.0	117	49	0
2	12	3729	2.6	787	0	787	6.3	1.3	0.0	2.9	0.2	0.0	158	65	0
3	1	2244	3.3	552	0	552	6.8	2.3	0.0	3.1	0.4	0.0	176	68	0
3	2	1414	3.9	476	0	476	7.1	3.4	0.0	3.3	0.5	0.0	193	70	0
3	3	1025	3.8	562	0	562	7.1	3.5	0.0	3.3	0.6	0.0	196	73	0
3	4	2096	2.0	2249	0	2249	5.8	0.9	0.0	2.7	0.2	0.0	152	65	0
3	5	1028	2.8	1224	0	1224	6.4	1.8	0.0	3.0	0.4	0.0	169	68	0
3	6	712	3.4	901	292	1193	6.8	2.3	0.0	3.2	0.4	0.0	133	52	0
3	7	873	3.1	996	332	1328	6.6	1.3	0.0	3.1	0.3	0.0	118	50	0
3	8	1877	2.8	956	330	1286	6.4	0.7	0.0	3.0	0.2	0.0	109	48	0
3	9	1049	4.9	274	78	352	7.8	2.7	0.0	3.6	0.5	0.0	138	54	0
3	10	1635	4.0	398	122	519	7.2	1.8	0.0	3.3	0.4	0.0	126	52	0
3	11	3033	2.9	663	226	889	6.5	1.2	0.0	3.0	0.2	0.0	117	49	0
3	12	3715	2.6	788	0	788	6.3	1.3	0.0	2.9	0.2	0.0	158	65	0
4	1	2235	3.3	552	0	552	6.8	2.3	0.0	3.1	0.4	0.0	176	68	0
4	2	1406	3.9	476	0	476	7.2	3.4	0.0	3.3	0.5	0.0	194	70	0
4	3	1023	3.8	566	0	566	7.1	3.5	0.0	3.3	0.6	0.0	196	73	0
4	4	2076	2.0	2254	0	2254	5.8	0.9	0.0	2.7	0.2	0.0	152	65	0
4	5	1017	2.8	1226	0	1226	6.4	1.8	0.0	3.0	0.4	0.0	169	68	0
4	6	705	3.4	902	292	1195	6.8	2.3	0.0	3.2	0.5	0.0	133	52	0
4	7	865	3.1	998	332	1330	6.7	1.3	0.0	3.1	0.3	0.0	118	50	0
4	8	1846	2.8	947	326	1273	6.4	0.7	0.0	3.0	0.2	0.0	109	48	0
4	9	1045	5.0	274	78	352	7.8	2.7	0.0	3.6	0.5	0.0	138	54	0
4	10	1629	4.0	398	122	520	7.2	1.8	0.0	3.3	0.4	0.0	126	52	0
4	11	3021	2.9	664	226	890	6.5	1.2	0.0	3.0	0.2	0.0	117	49	0
4	12	3701	2.6	788	0	788	6.3	1.3	0.0	2.9	0.2	0.0	158	65	0
5	1	2225	3.3	552	0	552	6.8	2.3	0.0	3.1	0.4	0.0	176	68	0
5	2	1397	3.9	476	0	476	7.2	3.4	0.0	3.3	0.5	0.0	194	70	0
5	3	1021	3.8	570	0	570	7.1	3.5	0.0	3.3	0.6	0.0	195	73	0
5	4	2055	2.0	2258	0	2258	5.8	0.9	0.0	2.7	0.2	0.0	152	65	0
5	5	1007	2.8	1228	0	1228	6.4	1.8	0.0	3.0	0.4	0.0	169	68	0
5	6	698	3.4	904	292	1196	6.8	2.3	0.0	3.2	0.5	0.0	133	53	0

(9) Suspended Solids Run-1 (Soluble) (2/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
5	7	857	3.2	1000	332	1332	6.7	1.3	0.0	3.1	0.3	0.0	118	50	0
5	8	1817	2.8	939	322	1261	6.4	0.7	0.0	3.0	0.2	0.0	109	48	0
5	9	1041	5.0	274	78	352	7.8	2.7	0.0	3.6	0.5	0.0	138	54	0
5	10	1623	4.0	398	122	520	7.2	1.8	0.0	3.3	0.4	0.0	126	52	0
5	11	3010	2.9	664	226	890	6.5	1.2	0.0	3.0	0.2	0.0	117	49	0
5	12	3687	2.6	788	0	788	6.3	1.3	0.0	2.9	0.2	0.0	158	65	0
6	1	2216	3.3	553	0	553	6.8	2.3	0.0	3.1	0.4	0.0	176	68	0
6	2	1389	3.9	476	0	476	7.2	3.4	0.0	3.3	0.5	0.0	194	70	0
6	3	1018	3.8	574	0	574	7.1	3.5	0.0	3.3	0.6	0.0	195	73	0
6	4	2035	2.0	2263	0	2263	5.9	0.9	0.0	2.7	0.2	0.0	152	65	0
6	5	997	2.9	1230	0	1230	6.4	1.8	0.0	3.0	0.4	0.0	169	68	0
6	6	691	3.4	906	292	1198	6.8	2.3	0.0	3.2	0.5	0.0	133	53	0
6	7	850	3.2	1002	332	1334	6.7	1.3	0.0	3.1	0.3	0.0	118	50	0
6	8	1788	2.9	930	318	1248	6.5	0.7	0.0	3.0	0.2	0.0	109	48	0
6	9	1037	5.0	274	78	353	7.8	2.7	0.0	3.6	0.5	0.0	138	54	0
6	10	1617	4.0	398	122	520	7.2	1.8	0.0	3.3	0.4	0.0	126	52	0
6	11	2998	2.9	664	226	890	6.5	1.2	0.0	3.0	0.2	0.0	117	49	0
6	12	3673	2.6	789	0	789	6.3	1.3	0.0	2.9	0.2	0.0	158	65	0
7	1	2207	3.3	553	0	553	6.8	2.3	0.0	3.1	0.4	0.0	176	68	0
7	2	1381	3.9	477	0	477	7.2	3.4	0.0	3.3	0.5	0.0	194	70	0
7	3	1016	3.8	578	0	578	7.1	3.4	0.0	3.3	0.6	0.0	195	73	0
7	4	2014	2.0	2266	0	2266	5.9	0.9	0.0	2.7	0.2	0.0	152	65	0
7	5	987	2.9	1232	0	1232	6.5	1.8	0.0	3.0	0.4	0.0	169	68	0
7	6	684	3.4	907	292	1200	6.9	2.3	0.0	3.2	0.5	0.0	133	53	0
7	7	842	3.2	1004	332	1336	6.7	1.3	0.0	3.1	0.3	0.0	118	50	0
7	8	1760	2.9	922	315	1236	6.5	0.7	0.0	3.0	0.2	0.0	109	48	0
7	9	1033	5.0	275	78	353	7.8	2.7	0.0	3.6	0.5	0.0	137	54	0
7	10	1610	4.0	399	122	520	7.2	1.8	0.0	3.3	0.4	0.0	126	52	0
7	11	2987	2.9	665	226	891	6.5	1.2	0.0	3.0	0.2	0.0	116	49	0
7	12	3659	2.6	789	0	789	6.3	1.3	0.0	2.9	0.2	0.0	158	65	0
8	1	2197	3.3	553	0	553	6.8	2.3	0.0	3.1	0.4	0.0	176	68	0
8	2	1373	3.9	477	0	477	7.2	3.4	0.0	3.3	0.5	0.0	194	70	0
8	3	1014	3.8	582	0	582	7.1	3.4	0.0	3.3	0.7	0.0	195	73	0
8	4	1994	2.0	2269	0	2269	5.9	0.9	0.0	2.7	0.2	0.0	152	66	0
8	5	977	2.9	1234	0	1234	6.5	1.8	0.0	3.0	0.4	0.0	169	68	0
8	6	677	3.5	909	292	1201	6.9	2.3	0.0	3.2	0.5	0.0	133	53	0
8	7	835	3.2	1006	332	1338	6.7	1.3	0.0	3.1	0.3	0.0	118	50	0
8	8	1732	2.9	914	311	1225	6.5	0.7	0.0	3.0	0.2	0.0	109	48	0
8	9	1029	5.0	275	78	353	7.8	2.7	0.0	3.6	0.5	0.0	137	54	0
8	10	1604	4.0	399	122	521	7.3	1.8	0.0	3.4	0.4	0.0	126	52	0
8	11	2975	2.9	665	226	891	6.5	1.2	0.0	3.0	0.2	0.0	116	49	0
8	12	3644	2.7	790	0	790	6.3	1.3	0.0	2.9	0.2	0.0	158	65	0
9	1	2188	3.4	554	0	554	6.8	2.3	0.0	3.1	0.4	0.0	176	68	0
9	2	1365	3.9	477	0	477	7.2	3.4	0.0	3.3	0.5	0.0	194	70	0
9	3	1011	3.8	586	0	586	7.1	3.4	0.0	3.3	0.7	0.0	194	73	0
9	4	1973	2.0	2272	0	2272	5.9	0.9	0.0	2.7	0.2	0.0	152	66	0
9	5	967	2.9	1236	0	1236	6.5	1.8	0.0	3.0	0.4	0.0	169	69	0
9	6	670	3.5	911	292	1203	6.9	2.3	0.0	3.2	0.5	0.0	133	53	0

(9) Suspended Solids Run-1 (Soluble) (3/8)

					SS			Cu			Zn				
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
9	7	827	3.2	1008	332	1340	6.7	1.3	0.0	3.1	0.3	0.0	118	50	0
9	8	1705	2.9	906	307	1213	6.5	0.8	0.0	3.0	0.2	0.0	109	48	0
9	9	1025	5.0	275	78	353	7.8	2.6	0.0	3.6	0.5	0.0	137	54	0
9	10	1598	4.0	399	122	521	7.3	1.8	0.0	3.4	0.4	0.0	126	52	0
9	11	2964	2.9	666	226	892	6.5	1.2	0.0	3.0	0.2	0.0	116	49	0
9	12	3630	2.7	790	0	790	6.3	1.3	0.0	2.9	0.2	0.0	158	65	0
10	1	2179	3.4	554	0	554	6.8	2.3	0.0	3.1	0.4	0.0	176	68	0
10	2	1357	3.9	477	0	477	7.2	3.4	0.0	3.3	0.5	0.0	194	70	0
10	3	1009	3.8	590	0	590	7.1	3.4	0.0	3.3	0.7	0.0	194	73	0
10	4	1953	2.0	2275	0	2275	5.9	0.9	0.0	2.7	0.2	0.0	152	66	0
10	5	957	2.9	1238	0	1238	6.5	1.9	0.0	3.0	0.4	0.0	169	69	0
10	6	663	3.5	912	292	1205	6.9	2.3	0.0	3.2	0.5	0.0	133	53	0
10	7	819	3.2	1010	332	1342	6.7	1.3	0.0	3.1	0.3	0.0	118	50	0
10	8	1679	3.0	898	304	1202	6.5	0.8	0.0	3.0	0.2	0.0	110	48	0
10	9	1021	5.0	275	78	353	7.8	2.6	0.0	3.6	0.5	0.0	137	54	0
10	10	1592	4.0	399	122	521	7.3	1.8	0.0	3.4	0.4	0.0	126	52	0
10	11	2952	2.9	666	226	892	6.5	1.2	0.0	3.0	0.2	0.0	116	49	0
10	12	3616	2.7	791	0	791	6.3	1.3	0.0	2.9	0.2	0.0	158	65	0
11	1	2169	3.4	554	0	554	6.8	2.3	0.0	3.1	0.4	0.0	176	68	0
11	2	1349	3.9	478	0	478	7.2	3.4	0.0	3.3	0.5	0.0	194	70	0
11	3	1006	3.8	595	0	595	7.1	3.4	0.0	3.3	0.7	0.0	194	73	0
11	4	1932	2.0	2278	0	2278	5.9	0.9	0.0	2.7	0.2	0.0	152	66	0
11	5	947	2.9	1240	0	1240	6.5	1.9	0.0	3.0	0.4	0.0	169	69	0
11	6	656	3.5	914	292	1206	6.9	2.3	0.0	3.2	0.5	0.0	133	53	0
11	7	812	3.2	1012	333	1344	6.7	1.3	0.0	3.1	0.3	0.0	117	50	0
11	8	1653	3.0	890	300	1191	6.6	0.8	0.0	3.0	0.2	0.0	110	48	0
11	9	1017	5.0	275	78	353	7.8	2.6	0.0	3.6	0.5	0.0	137	54	0
11	10	1586	4.0	400	122	521	7.3	1.8	0.0	3.4	0.4	0.0	126	52	0
11	11	2941	3.0	666	226	892	6.5	1.2	0.0	3.0	0.2	0.0	116	49	0
11	12	3602	2.7	791	0	791	6.3	1.3	0.0	2.9	0.2	0.0	158	65	0
12	1	2160	3.4	555	0	555	6.8	2.3	0.0	3.2	0.4	0.0	176	68	0
12	2	1340	3.9	478	0	478	7.2	3.4	0.0	3.3	0.5	0.0	194	70	0
12	3	1004	3.8	599	0	599	7.1	3.4	0.0	3.3	0.7	0.0	194	73	0
12	4	1912	2.1	2281	0	2281	5.9	0.9	0.0	2.7	0.2	0.0	152	66	0
12	5	937	2.9	1242	0	1242	6.5	1.9	0.0	3.0	0.4	0.0	169	69	0
12	6	649	3.5	916	292	1208	6.9	2.3	0.0	3.2	0.5	0.0	133	53	0
12	7	804	3.3	1014	333	1346	6.7	1.3	0.0	3.1	0.3	0.0	117	50	0
12	8	1628	3.0	883	297	1180	6.6	0.8	0.0	3.0	0.2	0.0	110	48	0
12	9	1013	5.0	276	78	354	7.8	2.6	0.0	3.6	0.5	0.0	137	54	0
12	10	1579	4.0	400	122	522	7.3	1.8	0.0	3.4	0.4	0.0	126	52	0
12	11	2930	3.0	667	226	893	6.5	1.2	0.0	3.0	0.2	0.0	116	49	0
12	12	3588	2.7	792	0	792	6.3	1.3	0.0	2.9	0.2	0.0	158	65	0
13	1	2150	3.4	555	0	555	6.8	2.3	0.0	3.2	0.4	0.0	176	68	0
13	2	1332	4.0	478	0	478	7.2	3.4	0.0	3.3	0.5	0.0	194	71	0
13	3	1001	3.8	604	0	604	7.1	3.4	0.0	3.3	0.7	0.0	193	73	0
13	4	1892	2.1	2284	0	2284	5.9	0.9	0.0	2.7	0.2	0.0	152	66	0
13	5	927	3.0	1244	0	1244	6.5	1.9	0.0	3.0	0.4	0.0	169	69	0
13	6	642	3.6	917	292	1210	6.9	2.3	0.0	3.2	0.5	0.0	133	53	0

(9) Suspended Solids Run-1 (Soluble) (4/8)

					SS			Cu			Zn				
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
13	7	797	3.3	1016	333	1349	6.7	1.3	0.0	3.1	0.3	0.0	117	50	0
13	8	1604	3.0	876	294	1170	6.6	0.8	0.0	3.0	0.2	0.0	110	49	0
13	9	1009	5.0	276	78	354	7.8	2.6	0.0	3.6	0.5	0.0	136	54	0
13	10	1573	4.0	400	122	522	7.3	1.8	0.0	3.4	0.4	0.0	126	52	0
13	11	2918	3.0	667	226	893	6.5	1.2	0.0	3.0	0.2	0.0	116	49	0
13	12	3574	2.7	792	0	792	6.3	1.3	0.0	2.9	0.2	0.0	158	65	0
14	1	2141	3.4	555	0	555	6.8	2.3	0.0	3.2	0.4	0.0	176	68	0
14	2	1324	4.0	479	0	479	7.2	3.5	0.0	3.3	0.5	0.0	194	71	0
14	3	998	3.8	608	0	608	7.1	3.3	0.0	3.3	0.7	0.0	193	73	0
14	4	1871	2.1	2287	0	2287	5.9	0.9	0.0	2.7	0.2	0.0	152	66	0
14	5	917	3.0	1246	0	1246	6.5	1.9	0.0	3.0	0.4	0.0	169	69	0
14	6	635	3.6	919	292	1212	7.0	2.3	0.0	3.2	0.5	0.0	133	53	0
14	7	789	3.3	1018	333	1351	6.8	1.2	0.0	3.1	0.3	0.0	117	50	0
14	8	1580	3.1	869	291	1159	6.6	0.8	0.0	3.1	0.2	0.0	110	49	0
14	9	1005	5.1	276	78	354	7.8	2.6	0.0	3.6	0.5	0.0	136	54	0
14	10	1567	4.0	400	122	522	7.3	1.8	0.0	3.4	0.4	0.0	125	52	0
14	11	2907	3.0	668	226	894	6.5	1.2	0.0	3.0	0.2	0.0	116	49	0
14	12	3560	2.7	793	0	793	6.3	1.3	0.0	2.9	0.2	0.0	158	66	0
15	1	2132	3.4	556	0	556	6.8	2.3	0.0	3.2	0.4	0.0	176	68	0
15	2	1316	4.0	479	0	479	7.2	3.5	0.0	3.3	0.5	0.0	194	71	0
15	3	996	3.8	613	0	613	7.1	3.3	0.0	3.3	0.7	0.0	193	73	0
15	4	1851	2.1	2291	0	2291	5.9	0.9	0.0	2.7	0.2	0.0	153	66	0
15	5	907	3.0	1249	0	1249	6.5	1.9	0.0	3.0	0.4	0.0	169	69	0
15	6	628	3.6	921	292	1214	7.0	2.3	0.0	3.2	0.5	0.0	133	53	0
15	7	781	3.3	1020	333	1353	6.8	1.2	0.0	3.1	0.3	0.0	117	51	0
15	8	1556	3.1	862	288	1149	6.6	0.8	0.0	3.1	0.2	0.0	110	49	0
15	9	1001	5.1	276	78	354	7.8	2.6	0.0	3.6	0.5	0.0	136	54	0
15	10	1561	4.1	401	122	522	7.3	1.8	0.0	3.4	0.4	0.0	125	52	0
15	11	2895	3.0	668	226	894	6.5	1.2	0.0	3.0	0.2	0.0	116	49	0
15	12	3546	2.7	793	0	793	6.3	1.3	0.0	2.9	0.2	0.0	158	66	0
16	1	2122	3.4	556	0	556	6.8	2.3	0.0	3.2	0.4	0.0	177	68	0
16	2	1308	4.0	479	0	479	7.2	3.5	0.0	3.3	0.5	0.0	195	71	0
16	3	993	3.8	617	0	617	7.1	3.3	0.0	3.3	0.7	0.0	193	73	0
16	4	1830	2.1	2294	0	2294	5.9	0.9	0.0	2.7	0.2	0.0	153	66	0
16	5	896	3.0	1251	0	1251	6.6	1.9	0.0	3.0	0.4	0.0	169	69	0
16	6	621	3.6	923	292	1215	7.0	2.3	0.0	3.2	0.5	0.0	133	53	0
16	7	774	3.3	1022	333	1355	6.8	1.2	0.0	3.1	0.3	0.0	117	51	0
16	8	1533	3.1	855	285	1139	6.6	0.8	0.0	3.1	0.2	0.0	110	49	0
16	9	998	5.1	276	78	355	7.8	2.5	0.0	3.6	0.5	0.0	136	54	0
16	10	1555	4.1	401	122	523	7.3	1.8	0.0	3.4	0.4	0.0	125	52	0
16	11	2884	3.0	669	226	895	6.5	1.2	0.0	3.0	0.2	0.0	116	49	0
16	12	3532	2.7	794	0	794	6.3	1.3	0.0	2.9	0.2	0.0	158	66	0
17	1	2113	3.4	557	0	557	6.8	2.3	0.0	3.2	0.4	0.0	177	68	0
17	2	1300	4.0	479	0	479	7.3	3.5	0.0	3.4	0.6	0.0	195	71	0
17	3	990	3.8	622	0	622	7.1	3.3	0.0	3.3	0.7	0.0	192	73	0
17	4	1810	2.1	2297	0	2297	5.9	0.9	0.0	2.7	0.2	0.0	153	66	0
17	5	886	3.0	1253	0	1253	6.6	1.9	0.0	3.0	0.4	0.0	169	69	0
17	6	614	3.6	925	292	1217	7.0	2.3	0.0	3.2	0.5	0.0	133	53	0

(9) Suspended Solids Run-1 (Soluble) (5/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
17	7	766	3.3	1024	333	1358	6.8	1.2	0.0	3.1	0.3	0.0	117	51	0
17	8	1510	3.2	848	282	1130	6.7	0.8	0.0	3.1	0.2	0.0	110	49	0
17	9	994	5.1	277	78	355	7.8	2.5	0.0	3.6	0.5	0.0	136	55	0
17	10	1549	4.1	401	122	523	7.3	1.8	0.0	3.4	0.4	0.0	125	52	0
17	11	2872	3.0	669	226	895	6.5	1.2	0.0	3.0	0.3	0.0	116	49	0
17	12	3518	2.7	794	0	794	6.3	1.3	0.0	2.9	0.2	0.0	158	66	0
18	1	2104	3.4	557	0	557	6.8	2.3	0.0	3.2	0.4	0.0	177	68	0
18	2	1291	4.0	480	0	480	7.3	3.5	0.0	3.4	0.6	0.0	195	71	0
18	3	988	3.8	627	0	627	7.1	3.3	0.0	3.3	0.7	0.0	192	73	0
18	4	1789	2.1	2301	0	2301	5.9	0.9	0.0	2.7	0.2	0.0	153	66	0
18	5	876	3.0	1255	0	1255	6.6	1.9	0.0	3.0	0.4	0.0	169	69	0
18	6	607	3.7	927	292	1219	7.0	2.3	0.0	3.2	0.5	0.0	133	53	0
18	7	758	3.4	1027	333	1360	6.8	1.2	0.0	3.1	0.3	0.0	117	51	0
18	8	1488	3.2	842	279	1120	6.7	0.8	0.0	3.1	0.2	0.0	110	49	0
18	9	990	5.1	277	78	355	7.8	2.5	0.0	3.6	0.5	0.0	135	55	0
18	10	1542	4.1	401	122	523	7.3	1.7	0.0	3.4	0.4	0.0	125	52	0
18	11	2861	3.0	669	226	895	6.5	1.2	0.0	3.0	0.3	0.0	116	49	0
18	12	3503	2.7	794	0	794	6.3	1.3	0.0	2.9	0.2	0.0	158	66	0
19	1	2094	3.4	557	0	557	6.8	2.3	0.0	3.2	0.4	0.0	177	68	0
19	2	1283	4.0	480	0	480	7.3	3.5	0.0	3.4	0.6	0.0	195	71	0
19	3	985	3.8	632	0	632	7.1	3.3	0.0	3.3	0.7	0.0	192	73	0
19	4	1769	2.1	2304	0	2304	6.0	1.0	0.0	2.7	0.2	0.0	153	66	0
19	5	866	3.1	1258	0	1258	6.6	1.9	0.0	3.0	0.4	0.0	169	69	0
19	6	600	3.7	929	293	1221	7.0	2.3	0.0	3.2	0.5	0.0	133	54	0
19	7	751	3.4	1029	334	1362	6.8	1.2	0.0	3.2	0.3	0.0	117	51	0
19	8	1467	3.2	835	276	1111	6.7	0.8	0.0	3.1	0.2	0.0	110	49	0
19	9	986	5.1	277	78	355	7.8	2.5	0.0	3.6	0.5	0.0	135	55	0
19	10	1536	4.1	402	122	523	7.3	1.7	0.0	3.4	0.4	0.0	125	52	0
19	11	2849	3.0	670	226	896	6.6	1.2	0.0	3.0	0.3	0.0	116	49	0
19	12	3489	2.7	795	0	795	6.4	1.3	0.0	2.9	0.2	0.0	157	66	0
20	1	2085	3.4	558	0	558	6.9	2.4	0.0	3.2	0.4	0.0	177	68	0
20	2	1275	4.0	480	0	480	7.3	3.5	0.0	3.4	0.6	0.0	195	71	0
20	3	982	3.8	637	0	637	7.1	3.3	0.0	3.3	0.7	0.0	192	73	0
20	4	1748	2.2	2308	0	2308	6.0	1.0	0.0	2.8	0.2	0.0	153	66	0
20	5	856	3.1	1260	0	1260	6.6	1.9	0.0	3.1	0.4	0.0	170	69	0
20	6	593	3.7	931	293	1223	7.0	2.3	0.0	3.3	0.5	0.0	133	54	0
20	7	743	3.4	1031	334	1365	6.8	1.2	0.0	3.2	0.3	0.0	117	51	0
20	8	1445	3.2	829	273	1102	6.7	0.8	0.0	3.1	0.2	0.0	110	49	0
20	9	982	5.1	277	78	355	7.9	2.5	0.0	3.6	0.5	0.0	135	55	0
20	10	1530	4.1	402	122	524	7.3	1.7	0.0	3.4	0.4	0.0	125	52	0
20	11	2838	3.0	670	226	896	6.6	1.2	0.0	3.0	0.3	0.0	116	49	0
20	12	3475	2.7	795	0	795	6.4	1.3	0.0	2.9	0.2	0.0	157	66	0
21	1	2076	3.4	558	0	558	6.9	2.4	0.0	3.2	0.4	0.0	177	68	0
21	2	1267	4.1	480	0	480	7.3	3.5	0.0	3.4	0.6	0.0	195	71	0
21	3	979	3.8	642	0	642	7.1	3.3	0.0	3.3	0.7	0.0	191	73	0
21	4	1728	2.2	2311	0	2311	6.0	1.0	0.0	2.8	0.2	0.0	153	66	0
21	5	846	3.1	1262	0	1262	6.6	1.9	0.0	3.1	0.4	0.0	170	69	0
21	6	586	3.7	933	460	1393	7.1	2.3	0.0	3.3	0.5	0.0	117	47	0

(9) Suspended Solids Run-1 (Soluble) (6/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
21	7	735	3.4	1033	525	1559	6.8	1.2	0.0	3.2	0.3	0.0	102	45	0
21	8	1424	3.3	823	425	1248	6.7	0.8	0.0	3.1	0.2	0.0	97	43	0
21	9	977	5.1	278	123	400	7.9	2.5	0.0	3.6	0.6	0.0	120	49	0
21	10	1523	4.1	402	192	594	7.3	1.7	0.0	3.4	0.4	0.0	110	46	0
21	11	2825	3.0	671	355	1026	6.6	1.2	0.0	3.0	0.3	0.0	102	43	0
21	12	3459	2.7	796	0	796	6.4	1.3	0.0	2.9	0.2	0.0	157	66	0
22	1	2065	3.4	558	0	558	6.9	2.4	0.0	3.2	0.4	0.0	177	68	0
22	2	1258	4.1	480	0	480	7.3	3.5	0.0	3.4	0.6	0.0	195	71	0
22	3	976	3.8	648	0	648	7.1	3.2	0.0	3.3	0.7	0.0	191	73	0
22	4	1705	2.2	2316	0	2316	6.0	1.0	0.0	2.8	0.3	0.0	153	66	0
22	5	835	3.1	1265	0	1265	6.6	1.9	0.0	3.1	0.4	0.0	170	70	0
22	6	578	3.7	935	460	1395	7.1	2.3	0.0	3.3	0.5	0.0	117	47	0
22	7	727	3.4	1036	525	1562	6.9	1.2	0.0	3.2	0.3	0.0	102	45	0
22	8	1401	3.3	816	420	1236	6.8	0.8	0.0	3.1	0.2	0.0	97	43	0
22	9	973	5.1	278	123	401	7.9	2.4	0.0	3.6	0.6	0.0	119	49	0
22	10	1516	4.1	402	192	594	7.3	1.7	0.0	3.4	0.4	0.0	110	46	0
22	11	2812	3.0	671	355	1027	6.6	1.2	0.0	3.0	0.3	0.0	101	43	0
22	12	3443	2.7	797	0	797	6.4	1.3	0.0	2.9	0.2	0.0	157	66	0
23	1	2054	3.5	559	0	559	6.9	2.4	0.0	3.2	0.4	0.0	177	68	0
23	2	1248	4.1	481	0	481	7.3	3.5	0.0	3.4	0.6	0.0	195	71	0
23	3	972	3.8	654	0	654	7.1	3.2	0.0	3.3	0.7	0.0	191	74	0
23	4	1681	2.2	2320	0	2320	6.0	1.0	0.0	2.8	0.3	0.0	153	66	0
23	5	823	3.1	1268	0	1268	6.6	1.9	0.0	3.1	0.4	0.0	170	70	0
23	6	571	3.8	938	460	1398	7.1	2.3	0.0	3.3	0.5	0.0	117	47	0
23	7	718	3.5	1039	526	1565	6.9	1.2	0.0	3.2	0.3	0.0	102	45	0
23	8	1378	3.3	809	415	1225	6.8	0.8	0.0	3.1	0.2	0.0	97	43	0
23	9	968	5.1	278	123	401	7.9	2.4	0.0	3.6	0.6	0.0	119	49	0
23	10	1509	4.1	403	192	594	7.3	1.7	0.0	3.4	0.4	0.0	110	46	0
23	11	2799	3.0	672	355	1027	6.6	1.2	0.0	3.0	0.3	0.0	101	43	0
23	12	3427	2.7	797	0	797	6.4	1.3	0.0	2.9	0.2	0.0	157	66	0
24	1	2043	3.5	559	0	559	6.9	2.4	0.0	3.2	0.4	0.0	177	69	0
24	2	1239	4.1	481	0	481	7.3	3.6	0.0	3.4	0.6	0.0	195	71	0
24	3	969	3.8	660	0	660	7.1	3.2	0.0	3.3	0.7	0.0	191	74	0
24	4	1658	2.2	2324	0	2324	6.0	1.0	0.0	2.8	0.3	0.0	153	66	0
24	5	812	3.2	1271	0	1271	6.7	1.9	0.0	3.1	0.5	0.0	170	70	0
24	6	563	3.8	940	460	1400	7.1	2.3	0.0	3.3	0.5	0.0	117	48	0
24	7	709	3.5	1042	526	1568	6.9	1.2	0.0	3.2	0.3	0.0	102	45	0
24	8	1356	3.3	803	411	1213	6.8	0.8	0.0	3.1	0.2	0.0	97	43	0
24	9	964	5.2	278	123	401	7.9	2.4	0.0	3.6	0.6	0.0	119	49	0
24	10	1502	4.1	403	192	594	7.3	1.7	0.0	3.4	0.4	0.0	110	46	0
24	11	2786	3.0	672	355	1028	6.6	1.2	0.0	3.0	0.3	0.0	101	43	0
24	12	3411	2.7	798	0	798	6.4	1.3	0.0	2.9	0.2	0.0	157	66	0
25	1	2033	3.5	560	0	560	6.9	2.4	0.0	3.2	0.4	0.0	177	69	0
25	2	1230	4.1	481	0	481	7.3	3.6	0.0	3.4	0.6	0.0	196	71	0
25	3	965	3.8	667	0	667	7.1	3.2	0.0	3.3	0.7	0.0	190	74	0
25	4	1635	2.2	2329	0	2329	6.0	1.0	0.0	2.8	0.3	0.0	153	67	0
25	5	800	3.2	1274	0	1274	6.7	2.0	0.0	3.1	0.5	0.0	170	70	0
25	6	555	3.8	943	460	1403	7.1	2.3	0.0	3.3	0.5	0.0	117	48	0

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(9) Suspended Solids Run-1 (Soluble) (7/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
25	7	700	3.5	1044	526	1571	6.9	1.2	0.0	3.2	0.3	0.0	102	45	0
25	8	1334	3.4	796	406	1202	6.8	0.8	0.0	3.2	0.2	0.0	97	43	0
25	9	959	5.2	279	123	401	7.9	2.4	0.0	3.6	0.6	0.0	119	49	0
25	10	1495	4.1	403	192	595	7.3	1.7	0.0	3.4	0.4	0.0	110	46	0
25	11	2773	3.0	673	355	1028	6.6	1.2	0.0	3.0	0.3	0.0	101	43	0
25	12	3395	2.7	798	0	798	6.4	1.3	0.0	2.9	0.2	0.0	157	66	0
26	1	2022	3.5	560	0	560	6.9	2.4	0.0	3.2	0.4	0.0	177	69	0
26	2	1221	4.1	481	0	481	7.3	3.6	0.0	3.4	0.6	0.0	196	72	0
26	3	962	3.8	673	0	673	7.1	3.2	0.0	3.3	0.7	0.0	190	74	0
26	4	1611	2.2	2333	0	2333	6.0	1.0	0.0	2.8	0.3	0.0	153	67	0
26	5	789	3.2	1277	0	1277	6.7	2.0	0.0	3.1	0.5	0.0	170	70	0
26	6	547	3.8	945	460	1406	7.1	2.3	0.0	3.3	0.6	0.0	117	48	0
26	7	692	3.5	1047	526	1574	6.9	1.2	0.0	3.2	0.3	0.0	102	45	0
26	8	1313	3.4	790	402	1192	6.8	0.8	0.0	3.2	0.2	0.0	97	43	0
26	9	955	5.2	279	123	402	7.9	2.4	0.0	3.7	0.6	0.0	119	49	0
26	10	1488	4.2	404	192	595	7.3	1.7	0.0	3.4	0.4	0.0	110	46	0
26	11	2759	3.0	673	355	1029	6.6	1.2	0.0	3.0	0.3	0.0	101	43	0
26	12	3379	2.8	799	0	799	6.4	1.3	0.0	3.0	0.2	0.0	157	66	0
27	1	2011	3.5	561	0	561	6.9	2.4	0.0	3.2	0.4	0.0	177	69	0
27	2	1211	4.1	481	0	481	7.3	3.6	0.0	3.4	0.6	0.0	196	72	0
27	3	958	3.8	680	0	680	7.1	3.2	0.0	3.3	0.7	0.0	190	74	0
27	4	1588	2.3	2338	0	2338	6.0	1.0	0.0	2.8	0.3	0.0	153	67	0
27	5	777	3.2	1280	0	1280	6.7	2.0	0.0	3.1	0.5	0.0	170	70	0
27	6	539	3.9	948	460	1408	7.2	2.3	0.0	3.3	0.6	0.0	117	48	0
27	7	683	3.6	1050	527	1577	6.9	1.2	0.0	3.2	0.3	0.0	102	45	0
27	8	1292	3.4	784	397	1181	6.9	0.8	0.0	3.2	0.2	0.0	97	43	0
27	9	950	5.2	279	123	402	7.9	2.4	0.0	3.7	0.6	0.0	118	49	0
27	10	1481	4.2	404	192	595	7.3	1.7	0.0	3.4	0.4	0.0	110	47	0
27	11	2746	3.1	674	355	1029	6.6	1.2	0.0	3.0	0.3	0.0	101	43	0
27	12	3362	2.8	799	0	799	6.4	1.3	0.0	3.0	0.2	0.0	157	66	0
28	1	2001	3.5	561	0	561	6.9	2.4	0.0	3.2	0.4	0.0	177	69	0
28	2	1202	4.2	482	0	482	7.3	3.6	0.0	3.4	0.6	0.0	196	72	0
28	3	955	3.8	687	0	687	7.1	3.1	0.0	3.3	0.7	0.0	189	74	0
28	4	1565	2.3	2343	0	2343	6.0	1.0	0.0	2.8	0.3	0.0	154	67	0
28	5	766	3.3	1283	0	1283	6.7	2.0	0.0	3.1	0.5	0.0	170	70	0
28	6	531	3.9	951	460	1411	7.2	2.3	0.0	3.3	0.6	0.0	117	48	0
28	7	674	3.6	1053	527	1580	7.0	1.1	0.0	3.2	0.4	0.0	102	45	0
28	8	1272	3.5	778	393	1171	6.9	0.8	0.0	3.2	0.3	0.0	97	44	0
28	9	946	5.2	279	123	402	7.9	2.3	0.0	3.7	0.6	0.0	118	49	0
28	10	1474	4.2	404	192	596	7.3	1.7	0.0	3.4	0.4	0.0	109	47	0
28	11	2733	3.1	674	355	1030	6.6	1.2	0.0	3.1	0.3	0.0	101	43	0
28	12	3346	2.8	800	0	800	6.4	1.3	0.0	3.0	0.2	0.0	157	66	0
29	1	1990	3.5	561	0	561	6.9	2.4	0.0	3.2	0.4	0.0	177	69	0
29	2	1193	4.2	482	0	482	7.3	3.6	0.0	3.4	0.6	0.0	196	72	0
29	3	951	3.8	694	0	694	7.1	3.1	0.0	3.3	0.7	0.0	189	74	0
29	4	1541	2.3	2348	0	2348	6.1	1.0	0.0	2.8	0.3	0.0	154	67	0
29	5	754	3.3	1287	0	1287	6.7	2.0	0.0	3.1	0.5	0.0	170	70	0
29	6	523	3.9	953	460	1414	7.2	2.3	0.0	3.3	0.6	0.0	117	48	0

(9) Suspended Solids Run-1 (Soluble) (8/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
29	7	665	3.6	1056	527	1584	7.0	1.1	0.0	3.2	0.4	0.0	102	45	0
29	8	1252	3.5	772	389	1161	6.9	0.8	0.0	3.2	0.3	0.0	98	44	0
29	9	941	5.2	280	123	402	7.9	2.3	0.0	3.7	0.6	0.0	118	49	0
29	10	1467	4.2	404	192	596	7.3	1.7	0.0	3.4	0.4	0.0	109	47	0
29	11	2720	3.1	675	355	1030	6.6	1.2	0.0	3.1	0.3	0.0	101	43	0
29	12	3330	2.8	801	0	801	6.4	1.3	0.0	3.0	0.2	0.0	157	66	0
30	1	1979	3.5	562	0	562	6.9	2.4	0.0	3.2	0.4	0.0	177	69	0
30	2	1183	4.2	482	0	482	7.3	3.6	0.0	3.4	0.6	0.0	196	72	0
30	3	947	3.8	701	0	701	7.1	3.1	0.0	3.3	0.7	0.0	189	74	0
30	4	1518	2.3	2353	0	2353	6.1	1.0	0.0	2.8	0.3	0.0	154	67	0
30	5	743	3.3	1290	0	1290	6.8	2.0	0.0	3.1	0.5	0.0	170	70	0
30	6	515	4.0	956	460	1417	7.2	2.3	0.0	3.3	0.6	0.0	117	48	0
30	7	657	3.6	1059	527	1587	7.0	1.1	0.0	3.2	0.4	0.0	102	45	0
30	8	1232	3.5	766	385	1151	6.9	0.8	0.0	3.2	0.3	0.0	98	44	0
30	9	937	5.2	280	123	403	7.9	2.3	0.0	3.7	0.6	0.0	118	49	0
30	10	1460	4.2	405	192	596	7.4	1.6	0.0	3.4	0.4	0.0	109	47	0
30	11	2707	3.1	675	355	1031	6.6	1.2	0.0	3.1	0.3	0.0	101	43	0
30	12	3314	2.8	801	0	801	6.4	1.3	0.0	3.0	0.3	0.0	157	66	0
31	1	1968	3.5	562	0	562	6.9	2.4	0.0	3.2	0.4	0.0	177	69	0
31	2	1174	4.2	482	0	482	7.4	3.6	0.0	3.4	0.6	0.0	196	72	0
31	3	943	3.9	708	0	708	7.1	3.1	0.0	3.3	0.7	0.0	189	74	0
31	4	1495	2.3	2358	0	2358	6.1	1.0	0.0	2.8	0.3	0.0	154	67	0
31	5	731	3.3	1293	0	1293	6.8	2.0	0.0	3.1	0.5	0.0	170	70	0
31	6	507	4.0	959	460	1419	7.2	2.3	0.0	3.4	0.6	0.0	117	48	0
31	7	648	3.6	1063	528	1590	7.0	1.1	0.0	3.2	0.4	0.0	102	45	0
31	8	1213	3.6	761	381	1142	6.9	0.8	0.0	3.2	0.3	0.0	98	44	0
31	9	932	5.2	280	123	403	7.9	2.3	0.0	3.7	0.6	0.0	118	49	0
31	10	1453	4.2	405	192	597	7.4	1.6	0.0	3.4	0.4	0.0	109	47	0
31	11	2694	3.1	676	355	1031	6.6	1.2	0.0	3.1	0.3	0.0	101	43	0
31	12	3298	2.8	802	0	802	6.4	1.3	0.0	3.0	0.3	0.0	157	66	0

(10) Suspended Solids Run-1 (Total) (1/8)

				SS			Cu			Zn					
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
1	9	1099	4.7	303	88	391	32.3	1.6	1.1	10.6	0.5	1.9	467	173	10
1	10	1647	3.9	397	122	519	30.5	1.4	1.1	10.0	0.4	1.9	461	171	10
1	11	3056	2.9	662	226	888	27.4	1.0	1.1	9.0	0.2	1.9	447	169	10
1	12	3743	2.6	787	0	787	26.6	1.1	0.0	8.7	0.2	0.0	579	187	11
2	1	2254	3.3	551	0	551	28.6	2.1	0.0	9.4	0.4	0.0	597	190	11
2	2	1422	3.8	475	0	475	30.2	3.1	0.0	9.9	0.5	0.0	614	192	11
2	3	1028	3.8	558	0	558	30.1	3.3	0.0	9.9	0.6	0.0	617	195	11
2	4	2117	2.0	2245	0	2245	24.5	0.8	0.0	8.0	0.2	0.0	576	186	11
2	5	1038	2.8	1222	0	1222	27.1	1.8	0.0	8.9	0.4	0.0	592	191	11
2	6	719	3.4	899	292	1192	28.8	2.2	1.1	9.5	0.4	1.9	469	172	10
2	7	880	3.1	994	331	1326	28.1	1.3	1.1	9.3	0.3	1.9	453	170	10
2	8	1908	2.8	965	334	1300	27.0	0.7	1.1	8.9	0.2	1.9	441	167	10
2	9	1053	4.9	274	78	352	32.8	2.7	1.1	10.8	0.5	1.9	483	174	10
2	10	1641	4.0	397	122	519	30.5	1.8	1.1	10.0	0.4	1.9	467	171	10
2	11	3044	2.9	663	226	889	27.4	1.2	1.1	9.1	0.2	1.9	450	169	10
2	12	3729	2.6	787	0	787	26.6	1.3	0.0	8.8	0.2	0.0	582	187	11
3	1	2244	3.3	552	0	552	28.6	2.3	0.0	9.4	0.4	0.0	601	190	11
3	2	1414	3.9	476	0	476	30.2	3.4	0.0	9.9	0.5	0.0	618	192	11
3	3	1025	3.8	562	0	562	30.1	3.5	0.0	9.9	0.6	0.0	620	195	11
3	4	2096	2.0	2249	0	2249	24.6	0.9	0.0	8.0	0.2	0.0	577	186	11
3	5	1028	2.8	1224	0	1224	27.1	1.8	0.0	8.9	0.4	0.0	593	191	11
3	6	712	3.4	901	292	1193	28.8	2.3	1.1	9.5	0.4	1.9	470	172	10
3	7	873	3.1	996	332	1328	28.1	1.3	1.1	9.3	0.3	1.9	453	170	10
3	8	1877	2.8	956	330	1286	27.1	0.7	1.1	8.9	0.2	1.9	442	167	10
3	9	1049	4.9	274	78	352	32.8	2.7	1.1	10.8	0.5	1.9	484	174	10
3	10	1635	4.0	398	122	519	30.5	1.8	1.1	10.0	0.4	1.9	467	171	10
3	11	3033	2.9	663	226	889	27.4	1.2	1.1	9.1	0.2	1.9	450	169	10
3	12	3715	2.6	788	0	788	26.6	1.3	0.0	8.8	0.2	0.0	582	187	11
4	1	2235	3.3	552	0	552	28.7	2.3	0.0	9.4	0.4	0.0	601	190	11
4	2	1406	3.9	476	0	476	30.3	3.4	0.0	10.0	0.5	0.0	618	192	11
4	3	1023	3.8	566	0	566	30.1	3.5	0.0	9.9	0.6	0.0	620	195	11
4	4	2076	2.0	2254	0	2254	24.6	0.9	0.0	8.0	0.2	0.0	577	186	11
4	5	1017	2.8	1226	0	1226	27.2	1.8	0.0	9.0	0.4	0.0	593	191	11
4	6	705	3.4	902	292	1195	28.9	2.3	1.1	9.5	0.5	1.9	470	172	10
4	7	865	3.1	998	332	1330	28.1	1.3	1.1	9.3	0.3	1.9	453	170	10
4	8	1846	2.8	947	326	1273	27.2	0.7	1.1	9.0	0.2	1.9	442	167	10
4	9	1045	5.0	274	78	352	32.8	2.7	1.1	10.8	0.5	1.9	483	174	10
4	10	1629	4.0	398	122	520	30.6	1.8	1.1	10.1	0.4	1.9	467	172	10
4	11	3021	2.9	664	226	890	27.5	1.2	1.1	9.1	0.2	1.9	451	169	10
4	12	3701	2.6	788	0	788	26.6	1.3	0.0	8.8	0.2	0.0	582	187	11
5	1	2225	3.3	552	0	552	28.7	2.3	0.0	9.5	0.4	0.0	601	190	11
5	2	1397	3.9	476	0	476	30.3	3.4	0.0	10.0	0.5	0.0	618	192	11
5	3	1021	3.8	570	0	570	30.1	3.5	0.0	9.9	0.6	0.0	620	195	11
5	4	2055	2.0	2258	0	2258	24.7	0.9	0.0	8.1	0.2	0.0	577	186	11
5	5	1007	2.8	1228	0	1228	27.2	1.8	0.0	9.0	0.4	0.0	593	191	11
5	6	693	3.4	904	292	1196	28.9	2.3	1.1	9.5	0.5	1.9	470	172	10

(10) Suspended Solids Run-1 (Total) (2/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
5	7	857	3.2	1000	332	1332	28.2	1.3	1.1	9.3	0.3	1.9	453	170	10
5	8	1817	2.8	939	322	1261	27.3	0.7	1.1	9.0	0.2	1.9	442	168	10
5	9	1041	5.0	274	78	352	32.9	2.7	1.1	10.8	0.5	1.9	483	174	10
5	10	1623	4.0	398	122	520	30.6	1.8	1.1	10.1	0.4	1.9	467	172	10
5	11	3010	2.9	664	226	890	27.5	1.2	1.1	9.1	0.2	1.9	451	169	10
5	12	3687	2.6	788	0	788	26.6	1.3	0.0	8.8	0.2	0.0	582	188	11
6	1	2216	3.3	553	0	553	28.7	2.3	0.0	0.0	9.5	0.4	601	190	11
6	2	1389	3.9	476	0	476	30.3	3.4	0.0	10.0	0.5	0.0	618	192	11
6	3	1018	3.8	574	0	574	30.1	3.5	0.0	9.9	0.6	0.0	620	195	11
6	4	2035	2.0	2263	0	2263	24.7	0.9	0.0	8.1	0.2	0.0	577	186	11
6	5	997	2.9	1230	0	1230	27.3	1.8	0.0	9.0	0.4	0.0	593	191	11
6	6	691	3.4	906	292	1198	29.0	2.3	1.1	9.5	0.5	1.9	470	172	10
6	7	850	3.2	1002	332	1334	28.2	1.3	1.1	9.3	0.3	1.9	454	170	10
6	8	1788	2.9	930	318	1248	27.3	0.7	1.1	9.0	0.2	1.9	443	168	10
6	9	1037	5.0	274	78	353	32.9	2.7	1.1	10.8	0.5	1.9	483	174	10
6	10	1617	4.0	398	122	520	30.6	1.8	1.1	10.1	0.4	1.9	467	172	10
6	11	2998	2.9	664	226	890	27.5	1.2	1.1	9.1	0.2	1.9	451	169	10
6	12	3673	2.6	789	0	789	26.7	1.3	0.0	8.8	0.2	0.0	582	188	11
7	1	2207	3.3	553	0	553	28.7	2.3	0.0	9.5	0.4	0.0	601	190	11
7	2	1381	3.9	477	0	477	30.3	3.4	0.0	10.0	0.5	0.0	618	192	11
7	3	1016	3.8	578	0	578	30.1	3.4	0.0	9.9	0.6	0.0	620	195	11
7	4	2014	2.0	2266	0	2266	24.8	0.9	0.0	8.1	0.2	0.0	577	186	11
7	5	987	2.9	1232	0	1232	27.3	1.8	0.0	9.0	0.4	0.0	593	191	11
7	6	684	3.4	907	292	1200	29.0	2.3	1.1	9.6	0.5	1.9	470	172	10
7	7	842	3.2	1004	332	1336	28.3	1.3	1.1	9.3	0.3	1.9	454	170	10
7	8	1760	2.9	922	315	1236	27.4	0.7	1.1	9.0	0.2	1.9	443	168	10
7	9	1033	5.0	275	78	353	32.9	2.7	1.1	10.8	0.5	1.9	483	174	10
7	10	1610	4.0	399	122	520	30.6	1.8	1.1	10.1	0.4	1.9	467	172	10
7	11	2987	2.9	665	226	891	27.5	1.2	1.1	9.1	0.2	1.9	451	169	10
7	12	3659	2.6	789	0	789	26.7	1.3	0.0	8.8	0.2	0.0	582	188	11
8	1	2197	3.3	553	0	553	28.7	2.3	0.0	9.5	0.4	0.0	601	190	11
8	2	1373	3.9	477	0	477	30.4	3.4	0.0	10.0	0.5	0.0	619	192	11
8	3	1014	3.8	582	0	582	30.1	3.4	0.0	9.9	0.7	0.0	619	195	11
8	4	1994	2.0	2269	0	2269	24.8	0.9	0.0	8.1	0.2	0.0	577	187	11
8	5	977	2.9	1234	0	1234	27.4	1.8	0.0	9.0	0.4	0.0	593	191	11
8	6	677	3.5	909	292	1201	29.1	2.3	1.1	9.6	0.5	1.9	470	172	10
8	7	835	3.2	1006	332	1338	28.3	1.3	1.1	9.3	0.3	1.9	454	170	10
8	8	1732	2.9	914	311	1225	27.5	0.7	1.1	9.1	0.2	1.9	443	163	10
8	9	1029	5.0	275	78	353	32.9	2.7	1.1	10.8	0.5	1.9	483	174	10
8	10	1604	4.0	399	122	521	30.7	1.8	1.1	10.1	0.4	1.9	467	172	10
8	11	2975	2.9	665	226	891	27.5	1.2	1.1	9.1	0.2	1.9	451	169	10
8	12	3644	2.7	790	0	790	26.7	1.3	0.0	8.8	0.2	0.0	582	188	11
9	1	2188	3.4	554	0	554	28.8	2.3	0.0	9.5	0.4	0.0	601	190	11
9	2	1365	3.9	477	0	477	30.4	3.4	0.0	10.0	0.5	0.0	619	192	11
9	3	1011	3.8	586	0	586	30.1	3.4	0.0	9.9	0.7	0.0	619	195	11
9	4	1973	2.0	2272	0	2272	24.8	0.9	0.0	8.1	0.2	0.0	577	187	11
9	5	967	2.9	1236	0	1236	27.4	1.8	0.0	9.0	0.4	0.0	593	191	11
9	6	670	3.5	911	292	1203	29.1	2.3	1.1	9.6	0.5	1.9	471	172	10

(10) Suspended Solids Run-1 (Total) (3/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
9	7	827	3.2	1008	332	1340	28.4	1.3	1.1	9.4	0.3	1.9	454	170	10
9	8	1705	2.9	906	307	1213	27.6	0.8	1.1	9.1	0.2	1.9	444	168	10
9	9	1025	5.0	275	78	353	32.9	2.6	1.1	10.8	0.5	1.9	483	174	10
9	10	1598	4.0	399	122	521	30.7	1.8	1.1	10.1	0.4	1.9	467	172	10
9	11	2964	2.9	666	226	892	27.5	1.2	1.1	9.1	0.2	1.9	451	169	10
9	12	3630	2.7	790	0	790	26.7	1.3	0.0	8.8	0.2	0.0	582	188	11
10	1	2179	3.4	554	0	554	28.8	2.3	0.0	9.5	0.4	0.0	601	190	11
10	2	1357	3.9	477	0	477	30.4	3.4	0.0	10.0	0.5	0.0	619	192	11
10	3	1009	3.8	590	0	590	30.1	3.4	0.0	9.9	0.7	0.0	619	195	11
10	4	1953	2.0	2275	0	2275	24.9	0.9	0.0	8.1	0.2	0.0	577	187	11
10	5	957	2.9	1238	0	1238	27.5	1.9	0.0	9.1	0.4	0.0	593	191	11
10	6	663	3.5	912	292	1205	29.2	2.3	1.1	9.6	0.5	1.9	471	173	10
10	7	819	3.2	1010	332	1342	28.4	1.3	1.1	9.4	0.3	1.9	454	170	10
10	8	1679	3.0	898	304	1202	27.6	0.8	1.1	9.1	0.2	1.9	444	168	10
10	9	1021	5.0	275	78	353	33.0	2.6	1.1	10.9	0.5	1.9	483	174	10
10	10	1592	4.0	399	122	521	30.7	1.8	1.1	10.1	0.4	1.9	467	172	10
10	11	2952	2.9	666	226	892	27.6	1.2	1.1	9.1	0.2	1.9	451	169	10
10	12	3616	2.7	791	0	791	26.7	1.3	0.0	8.8	0.2	0.0	582	188	11
11	1	2169	3.4	554	0	554	28.8	2.3	0.0	9.5	0.4	0.0	601	191	11
11	2	1349	3.9	478	0	478	30.5	3.4	0.0	10.0	0.5	0.0	619	193	11
11	3	1006	3.8	595	0	595	30.1	3.4	0.0	9.9	0.7	0.0	619	195	11
11	4	1932	2.0	2278	0	2278	24.9	0.9	0.0	8.1	0.2	0.0	577	187	11
11	5	947	2.9	1240	0	1240	27.5	1.9	0.0	9.1	0.4	0.0	594	191	11
11	6	656	3.5	914	292	1206	29.2	2.3	1.1	9.6	0.5	1.9	471	173	10
11	7	812	3.2	1012	333	1344	28.4	1.3	1.1	9.4	0.3	1.9	454	170	10
11	8	1653	3.0	890	300	1191	27.7	0.8	1.1	9.2	0.2	1.9	444	168	10
11	9	1017	5.0	275	78	353	33.0	2.6	1.1	10.9	0.5	1.9	482	174	10
11	10	1586	4.0	400	122	521	30.7	1.8	1.1	10.1	0.4	1.9	467	172	10
11	11	2941	3.0	666	226	892	27.6	1.2	1.1	9.1	0.2	1.9	451	169	10
11	12	3602	2.7	791	0	791	26.7	1.3	0.0	8.8	0.2	0.0	582	188	11
12	1	2160	3.4	555	0	555	28.8	2.3	0.0	9.5	0.4	0.0	601	191	11
12	2	1340	3.9	478	0	478	30.5	3.4	0.0	10.0	0.5	0.0	619	193	11
12	3	1004	3.8	599	0	599	30.2	3.4	0.0	9.9	0.7	0.0	618	195	11
12	4	1912	2.1	2281	0	2281	24.9	0.9	0.0	8.1	0.2	0.0	577	187	11
12	5	937	2.9	1242	0	1242	27.5	1.9	0.0	9.1	0.4	0.0	594	191	11
12	6	649	3.5	916	292	1208	29.3	2.3	1.1	9.7	0.5	1.9	471	173	10
12	7	804	3.3	1014	333	1346	28.5	1.3	1.1	9.4	0.3	1.9	454	170	10
12	8	1628	3.0	883	297	1180	27.8	0.8	1.1	9.2	0.2	1.9	444	168	10
12	9	1013	5.0	276	78	354	33.0	2.6	1.1	10.9	0.5	1.9	482	174	10
12	10	1579	4.0	400	122	522	30.7	1.8	1.1	10.1	0.4	1.9	467	172	10
12	11	2930	3.0	667	226	893	27.6	1.2	1.1	9.1	0.2	1.9	451	169	10
12	12	3588	2.7	792	0	792	26.7	1.3	0.0	8.8	0.2	0.0	582	188	11
13	1	2150	3.4	555	0	555	28.8	2.3	0.0	9.5	0.4	0.0	601	191	11
13	2	1332	4.0	478	0	478	30.5	3.4	0.0	10.0	0.5	0.0	619	193	11
13	3	1001	3.8	604	0	604	30.2	3.4	0.0	9.9	0.7	0.0	618	195	11
13	4	1892	2.1	2284	0	2284	25.0	0.9	0.0	8.2	0.2	0.0	577	187	11
13	5	927	3.0	1244	0	1244	27.6	1.9	0.0	9.1	0.4	0.0	594	192	11
13	6	642	3.6	917	292	1210	29.3	2.3	1.1	9.7	0.5	1.9	471	173	10

(10) Suspended Solids Run-1 (Total) (4/8)

					SS			Cu			Zn				
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
13	7	797	3.3	1016	333	1349	28.5	1.3	1.1	9.4	0.3	1.9	454	170	10
13	8	1604	3.0	876	294	1170	27.9	0.8	1.1	9.2	0.2	1.9	445	168	10
13	9	1009	5.0	276	78	354	33.0	2.6	1.1	10.9	0.5	1.9	482	174	10
13	10	1573	4.0	400	122	522	30.7	1.8	1.1	10.1	0.4	1.9	467	172	10
13	11	2918	3.0	667	226	893	27.6	1.2	1.1	9.1	0.2	1.9	451	169	10
13	12	3574	2.7	792	0	792	26.8	1.3	0.0	8.8	0.2	0.0	582	188	11
14	1	2141	3.4	555	0	555	28.9	2.3	0.0	9.5	0.4	0.0	601	191	11
14	2	1324	4.0	479	0	479	30.6	3.5	0.0	10.1	0.5	0.0	619	193	11
14	3	998	3.8	608	0	608	30.2	3.3	0.0	9.9	0.7	0.0	618	195	11
14	4	1871	2.1	2287	0	2287	25.0	0.9	0.0	8.2	0.2	0.0	577	187	11
14	5	917	3.0	1246	0	1246	27.6	1.9	0.0	9.1	0.4	0.0	594	192	11
14	6	635	3.6	919	292	1212	29.4	2.3	1.1	9.7	0.5	1.9	471	173	10
14	7	789	3.3	1018	333	1351	28.6	1.2	1.1	9.4	0.3	1.9	454	170	10
14	8	1580	3.1	869	291	1159	27.9	0.8	1.1	9.2	0.2	1.9	445	168	10
14	9	1005	5.1	276	78	354	33.1	2.6	1.1	10.9	0.5	1.9	482	174	10
14	10	1567	4.0	400	122	522	30.8	1.8	1.1	10.1	0.4	1.9	467	172	10
14	11	2907	3.0	668	226	894	27.6	1.2	1.1	9.1	0.2	1.9	451	169	10
14	12	3560	2.7	793	0	793	26.8	1.3	0.0	8.8	0.2	0.0	582	188	11
15	1	2132	3.4	556	0	556	28.9	2.3	0.0	9.5	0.4	0.0	601	191	11
15	2	1316	4.0	479	0	479	30.6	3.5	0.0	10.1	0.5	0.0	619	193	11
15	3	996	3.8	613	0	613	30.2	3.3	0.0	9.9	0.7	0.0	618	195	11
15	4	1851	2.1	2291	0	2291	25.0	0.9	0.0	8.2	0.2	0.0	577	187	11
15	5	907	3.0	1249	0	1249	27.7	1.9	0.0	9.1	0.4	0.0	594	192	11
15	6	628	3.6	921	292	1214	29.5	2.3	1.1	9.7	0.5	1.9	472	173	10
15	7	781	3.3	1020	333	1353	28.6	1.2	1.1	9.4	0.3	1.9	454	170	10
15	8	1556	3.1	862	288	1149	28.0	0.8	1.1	9.2	0.2	1.9	445	168	10
15	9	1001	5.1	276	78	354	33.1	2.6	1.1	10.9	0.5	1.9	482	174	10
15	10	1561	4.1	401	122	522	30.8	1.8	1.1	10.1	0.4	1.9	467	172	10
15	11	2895	3.0	668	226	894	27.7	1.2	1.1	9.1	0.2	1.9	451	169	10
15	12	3546	2.7	793	0	793	26.8	1.3	0.0	8.8	0.2	0.0	582	188	11
16	1	2122	3.4	556	0	556	28.9	2.3	0.0	9.5	0.4	0.0	601	191	11
16	2	1308	4.0	479	0	479	30.6	3.5	0.0	10.1	0.5	0.0	619	193	11
16	3	993	3.8	617	0	617	30.2	3.3	0.0	9.9	0.7	0.0	617	195	11
16	4	1830	2.1	2294	0	2294	25.1	0.9	0.0	8.2	0.2	0.0	578	187	11
16	5	896	3.0	1251	0	1251	27.7	1.9	0.0	9.2	0.4	0.0	594	192	11
16	6	621	3.6	923	292	1215	29.5	2.3	1.1	9.7	0.5	1.9	472	173	10
16	7	774	3.3	1022	333	1355	28.7	1.2	1.1	9.5	0.3	1.9	454	170	10
16	8	1533	3.1	855	285	1139	28.1	0.8	1.1	9.3	0.2	1.9	446	169	10
16	9	998	5.1	276	78	355	33.1	2.5	1.1	10.9	0.5	1.9	482	174	10
16	10	1555	4.1	401	122	523	30.8	1.8	1.1	10.1	0.4	1.9	467	172	10
16	11	2884	3.0	669	226	895	27.7	1.2	1.1	9.1	0.2	1.9	451	169	10
16	12	3532	2.7	794	0	794	26.8	1.3	0.0	8.8	0.2	0.0	582	188	11
17	1	2113	3.4	557	0	557	28.9	2.3	0.0	9.5	0.4	0.0	601	191	11
17	2	1300	4.0	479	0	479	30.7	3.5	0.0	10.1	0.6	0.0	619	193	11
17	3	990	3.8	622	0	622	30.2	3.3	0.0	9.9	0.7	0.0	617	195	11
17	4	1810	2.1	2297	0	2297	25.1	0.9	0.0	8.2	0.2	0.0	578	187	11
17	5	888	3.0	1253	0	1253	27.8	1.9	0.0	9.2	0.4	0.0	594	192	11
17	6	614	3.6	925	292	1217	29.6	2.3	1.1	9.7	0.5	1.9	472	173	10

(10) Suspended Solids Run-1 (Total) (5/8)

					SS			Cu			Zn				
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
17	7	766	3.3	1024	333	1358	28.7	1.2	1.1	9.5	0.3	1.9	454	170	10
17	8	1510	3.2	848	282	1130	28.2	0.8	1.1	9.3	0.2	1.9	446	169	10
17	9	994	5.1	277	78	355	33.1	2.5	1.1	10.9	0.5	1.9	482	174	10
17	10	1549	4.1	401	122	523	30.8	1.8	1.1	10.1	0.4	1.9	467	172	10
17	11	2872	3.0	669	226	895	27.7	1.2	1.1	9.1	0.3	1.9	451	169	10
17	12	3518	2.7	794	0	794	26.8	1.3	0.0	8.8	0.2	0.0	582	188	11
18	1	2104	3.4	557	0	557	28.9	2.3	0.0	9.5	0.4	0.0	601	191	11
18	2	1291	4.0	480	0	480	30.7	3.5	0.0	10.1	0.6	0.0	619	193	11
18	3	988	3.8	627	0	627	30.2	3.3	0.0	9.9	0.7	0.0	617	195	11
18	4	1789	2.1	2301	0	2301	25.1	0.9	0.0	8.2	0.2	0.0	578	187	11
18	5	876	3.0	1255	0	1255	27.8	1.9	0.0	9.2	0.4	0.0	594	192	11
18	6	607	3.7	927	292	1219	29.6	2.3	1.1	9.8	0.5	1.9	472	173	10
18	7	758	3.4	1027	333	1360	28.8	1.2	1.1	9.5	0.3	1.9	454	170	10
18	8	1488	3.2	842	279	1120	28.2	0.8	1.1	9.3	0.2	1.9	446	169	10
18	9	990	5.1	277	78	355	33.2	2.5	1.1	10.9	0.5	1.9	481	174	10
18	10	1542	4.1	401	122	523	30.8	1.7	1.1	10.1	0.4	1.9	467	172	10
18	11	2861	3.0	669	226	895	27.7	1.2	1.1	9.2	0.3	1.9	451	169	10
18	12	3503	2.7	794	0	794	26.8	1.3	0.0	8.8	0.2	0.0	582	188	11
19	1	2094	3.4	557	0	557	29.0	2.3	0.0	9.6	0.4	0.0	601	191	11
19	2	1283	4.0	480	0	480	30.7	3.5	0.0	10.1	0.6	0.0	620	193	11
19	3	985	3.8	632	0	632	30.2	3.3	0.0	9.9	0.7	0.0	617	196	11
19	4	1769	2.1	2304	0	2304	25.2	1.0	0.0	8.2	0.2	0.0	578	187	11
19	5	866	3.1	1258	0	1258	27.9	1.9	0.0	9.2	0.4	0.0	594	192	11
19	6	600	3.7	929	293	1221	29.7	2.3	1.1	9.8	0.5	1.9	472	173	10
19	7	751	3.4	1029	334	1362	28.8	1.2	1.1	9.5	0.3	1.9	454	170	10
19	8	1467	3.2	835	276	1111	28.3	0.8	1.1	9.3	0.2	1.9	446	169	10
19	9	986	5.1	277	78	355	33.2	2.5	1.1	10.9	0.5	1.9	481	174	10
19	10	1536	4.1	402	122	523	30.9	1.7	1.1	10.1	0.4	1.9	467	172	10
19	11	2849	3.0	670	226	896	27.7	1.2	1.1	9.2	0.3	1.9	451	169	10
19	12	3489	2.7	795	0	795	26.9	1.3	0.0	8.8	0.2	0.0	582	188	11
20	1	2085	3.4	558	0	558	29.0	2.4	0.0	9.6	0.4	0.0	601	191	11
20	2	1275	4.0	480	0	480	30.8	3.5	0.0	10.1	0.6	0.0	620	193	11
20	3	982	3.8	637	0	637	30.2	3.3	0.0	9.9	0.7	0.0	616	196	11
20	4	1748	2.2	2308	0	2308	25.2	1.0	0.0	8.2	0.2	0.0	578	187	11
20	5	856	3.1	1260	0	1260	27.9	1.9	0.0	9.2	0.4	0.0	594	192	11
20	6	593	3.7	931	293	1223	29.8	2.3	1.1	9.8	0.5	1.9	472	173	10
20	7	743	3.4	1031	334	1365	28.9	1.2	1.1	9.5	0.3	1.9	454	170	10
20	8	1445	3.2	829	273	1102	28.4	0.8	1.1	9.4	0.2	1.9	447	169	10
20	9	982	5.1	277	78	355	33.2	2.5	1.1	10.9	0.5	1.9	481	174	10
20	10	1530	4.1	402	122	524	30.9	1.7	1.1	10.2	0.4	1.9	467	172	10
20	11	2838	3.0	670	226	896	27.7	1.2	1.1	9.2	0.3	1.9	451	169	10
20	12	3475	2.7	795	0	795	26.9	1.3	0.0	8.9	0.2	0.0	582	188	11
21	1	2076	3.4	558	0	558	29.0	2.4	0.0	9.6	0.4	0.0	601	191	11
21	2	1267	4.1	480	0	480	30.8	3.5	0.0	10.1	0.6	0.0	620	193	11
21	3	979	3.8	642	0	642	30.2	3.3	0.0	9.9	0.7	0.0	616	196	11
21	4	1728	2.2	2311	0	2311	25.2	1.0	0.0	8.3	0.2	0.0	578	188	11
21	5	846	3.1	1262	0	1262	28.0	1.9	0.0	9.2	0.4	0.0	594	192	11
21	6	586	3.7	933	460	1393	29.8	2.3	1.8	9.8	0.5	2.9	424	166	9

(10) Suspended Solids Run-1 (Total) (6/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
21	7	735	3.4	1033	525	1559	28.9	1.2	1.8	9.5	0.3	2.9	407	163	9
21	8	1424	3.3	823	425	1248	28.5	0.8	1.8	9.4	0.2	2.9	400	162	9
21	9	977	5.1	278	123	400	33.2	2.5	1.8	10.9	0.6	2.9	435	167	9
21	10	1523	4.1	402	192	594	30.9	1.7	1.8	10.2	0.4	2.9	420	165	9
21	11	2825	3.0	671	355	1026	27.8	1.2	1.8	9.2	0.3	2.9	403	162	9
21	12	3459	2.7	796	0	796	26.9	1.3	0.0	8.9	0.2	0.0	582	188	11
22	1	2065	3.4	558	0	558	29.0	2.4	0.0	9.6	0.4	0.0	601	191	11
22	2	1258	4.1	480	0	480	30.8	3.5	0.0	10.1	0.6	0.0	620	193	11
22	3	976	3.8	648	0	648	30.2	3.2	0.0	9.9	0.7	0.0	616	196	11
22	4	1705	2.2	2316	0	2316	25.3	1.0	0.0	8.3	0.3	0.0	578	188	11
22	5	835	3.1	1265	0	1265	28.1	1.9	0.0	9.3	0.4	0.0	594	192	11
22	6	578	3.7	935	460	1395	29.9	2.3	1.8	9.8	0.5	2.9	424	166	9
22	7	727	3.4	1036	525	1562	29.0	1.2	1.8	9.6	0.3	2.9	407	163	9
22	8	1401	3.3	816	420	1236	28.6	0.8	1.8	9.4	0.2	2.9	400	162	9
22	9	973	5.1	278	123	401	33.3	2.4	1.8	11.0	0.6	2.9	435	167	9
22	10	1516	4.1	402	192	594	30.9	1.7	1.8	10.2	0.4	2.9	420	165	9
22	11	2812	3.0	671	355	1027	27.8	1.2	1.8	9.2	0.3	2.9	403	162	9
22	12	3443	2.7	797	0	797	26.9	1.3	0.0	8.9	0.2	0.0	582	188	11
23	1	2054	3.5	559	0	559	29.1	2.4	0.0	9.6	0.4	0.0	601	191	11
23	2	1248	4.1	481	0	481	30.8	3.5	0.0	10.1	0.6	0.0	620	193	11
23	3	972	3.8	654	0	654	30.2	3.2	0.0	9.9	0.7	0.0	615	196	11
23	4	1681	2.2	2320	0	2320	25.3	1.0	0.0	8.3	0.3	0.0	578	188	11
23	5	823	3.1	1268	0	1268	28.1	1.9	0.0	9.3	0.4	0.0	594	192	11
23	6	571	3.8	938	460	1398	30.0	2.3	1.8	9.9	0.5	2.9	424	166	9
23	7	718	3.5	1039	526	1565	29.1	1.2	1.8	9.6	0.3	2.9	407	163	9
23	8	1378	3.3	809	415	1225	28.7	0.8	1.8	9.5	0.2	2.9	401	162	9
23	9	968	5.1	278	123	401	33.3	2.4	1.8	11.0	0.6	2.9	435	167	9
23	10	1509	4.1	403	192	594	30.9	1.7	1.8	10.2	0.4	2.9	420	165	9
23	11	2799	3.0	672	355	1027	27.8	1.2	1.8	9.2	0.3	2.9	403	162	9
23	12	3427	2.7	797	0	797	26.9	1.3	0.0	8.9	0.2	0.0	582	188	11
24	1	2043	3.5	559	0	559	29.1	2.4	0.0	9.6	0.4	0.0	601	191	11
24	2	1239	4.1	481	0	481	30.9	3.6	0.0	10.2	0.6	0.0	620	193	11
24	3	969	3.8	660	0	660	30.2	3.2	0.0	9.9	0.7	0.0	615	196	11
24	4	1658	2.2	2324	0	2324	25.4	1.0	0.0	8.3	0.3	0.0	578	188	11
24	5	812	3.2	1271	0	1271	28.2	1.9	0.0	9.3	0.5	0.0	594	192	11
24	6	563	3.8	940	460	1400	30.1	2.3	1.8	9.9	0.5	2.9	424	166	9
24	7	709	3.5	1042	526	1568	29.1	1.2	1.8	9.6	0.3	2.9	407	163	9
24	8	1356	3.3	803	411	1213	28.7	0.8	1.8	9.5	0.2	2.9	401	162	9
24	9	964	5.2	278	123	401	33.3	2.4	1.8	11.0	0.6	2.9	434	167	9
24	10	1502	4.1	403	192	594	31.0	1.7	1.8	10.2	0.4	2.9	420	165	9
24	11	2786	3.0	672	355	1028	27.8	1.2	1.8	9.2	0.3	2.9	403	162	9
24	12	3411	2.7	798	0	798	27.0	1.3	0.0	8.9	0.2	0.0	582	188	11
25	1	2033	3.5	560	0	560	29.1	2.4	0.0	9.6	0.4	0.0	601	191	11
25	2	1230	4.1	481	0	481	30.9	3.6	0.0	10.2	0.6	0.0	620	194	11
25	3	965	3.8	667	0	667	30.2	3.2	0.0	9.9	0.7	0.0	615	196	11
25	4	1635	2.2	2329	0	2329	25.4	1.0	0.0	8.3	0.3	0.0	578	188	11
25	5	800	3.2	1274	0	1274	28.3	2.0	0.0	9.3	0.5	0.0	594	192	11
25	6	555	3.8	943	460	1403	30.1	2.3	1.8	9.9	0.5	2.9	425	166	9

(10) Suspended Solids Run-1 (Total) (7/8)

					SS			Cu			Zn				
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
25	7	700	3.5	1044	526	1571	29.2	1.2	1.8	9.6	0.3	2.9	407	163	9
25	8	1334	3.4	796	406	1202	28.8	0.8	1.8	9.5	0.2	2.9	401	162	9
25	9	959	5.2	279	123	401	33.4	2.4	1.8	11.0	0.6	2.9	434	168	9
25	10	1495	4.1	403	192	595	31.0	1.7	1.8	10.2	0.4	2.9	420	165	9
25	11	2773	3.0	673	355	1028	27.8	1.2	1.8	9.2	0.3	2.9	403	162	9
25	12	3395	2.7	798	0	798	27.0	1.3	0.0	8.9	0.2	0.0	582	188	11
26	1	2022	3.5	560	0	560	29.1	2.4	0.0	9.6	0.4	0.0	601	191	11
26	2	1221	4.1	481	0	481	30.9	3.6	0.0	10.2	0.6	0.0	620	194	11
26	3	962	3.8	673	0	673	30.2	3.2	0.0	9.9	0.7	0.0	615	196	11
26	4	1611	2.2	2333	0	2333	25.5	1.0	0.0	8.3	0.3	0.0	578	188	11
26	5	789	3.2	1277	0	1277	28.3	2.0	0.0	9.3	0.5	0.0	594	193	11
26	6	547	3.8	945	460	1406	30.2	2.3	1.8	9.9	0.6	2.9	425	166	9
26	7	692	3.5	1047	526	1574	29.3	1.2	1.8	9.6	0.3	2.9	407	163	9
26	8	1313	3.4	790	402	1192	28.9	0.8	1.8	9.5	0.2	2.9	402	162	9
26	9	955	5.2	279	123	402	33.4	2.4	1.8	11.0	0.6	2.9	434	168	9
26	10	1488	4.2	404	192	595	31.0	1.7	1.8	10.2	0.4	2.9	420	165	9
26	11	2759	3.0	673	355	1029	27.9	1.2	1.8	9.2	0.3	2.9	403	162	9
26	12	3379	2.8	799	0	799	27.0	1.3	0.0	8.9	0.2	0.0	582	188	11
27	1	2011	3.5	561	0	561	29.2	2.4	0.0	9.6	0.4	0.0	601	191	11
27	2	1211	4.1	481	0	481	31.0	3.6	0.0	10.2	0.6	0.0	620	194	11
27	3	958	3.8	680	0	680	30.2	3.2	0.0	9.9	0.7	0.0	614	196	11
27	4	1588	2.3	2338	0	2338	25.5	1.0	0.0	8.4	0.3	0.0	578	188	11
27	5	777	3.2	1280	0	1280	28.4	2.0	0.0	9.4	0.5	0.0	594	193	11
27	6	539	3.9	948	460	1408	30.3	2.3	1.8	10.0	0.6	2.9	425	166	9
27	7	683	3.6	1050	527	1577	29.3	1.2	1.8	9.7	0.3	2.9	408	163	9
27	8	1292	3.4	784	397	1181	29.0	0.8	1.8	9.6	0.2	2.9	402	162	9
27	9	950	5.2	279	123	402	33.4	2.4	1.8	11.0	0.6	2.9	434	168	9
27	10	1481	4.2	404	192	595	31.0	1.7	1.8	10.2	0.4	2.9	419	165	9
27	11	2746	3.1	674	355	1029	27.9	1.2	1.8	9.2	0.3	2.9	403	162	9
27	12	3362	2.8	799	0	799	27.0	1.3	0.0	8.9	0.2	0.0	582	188	11
28	1	2001	3.5	561	0	561	29.2	2.4	0.0	9.6	0.4	0.0	601	191	11
28	2	1202	4.2	482	0	482	31.0	3.6	0.0	10.2	0.6	0.0	621	194	11
28	3	955	3.8	687	0	687	30.2	3.1	0.0	9.9	0.7	0.0	614	196	11
28	4	1565	2.3	2343	0	2343	25.6	1.0	0.0	8.4	0.3	0.0	578	188	11
28	5	766	3.3	1283	0	1283	28.5	2.0	0.0	9.4	0.5	0.0	595	193	11
28	6	531	3.9	951	460	1411	30.4	2.3	1.8	10.0	0.6	2.9	425	167	9
28	7	674	3.6	1053	527	1580	29.4	1.1	1.8	9.7	0.4	2.9	408	164	9
28	8	1272	3.5	778	393	1171	29.1	0.8	1.8	9.6	0.3	2.9	402	162	9
28	9	946	5.2	279	123	402	33.5	2.3	1.8	11.0	0.6	2.9	434	168	9
28	10	1474	4.2	404	192	596	31.1	1.7	1.8	10.2	0.4	2.9	419	165	9
28	11	2733	3.1	674	355	1030	27.9	1.2	1.8	9.2	0.3	2.9	403	162	9
28	12	3346	2.8	800	0	800	27.0	1.3	0.0	8.9	0.2	0.0	582	188	11
29	1	1990	3.5	561	0	561	29.2	2.4	0.0	9.6	0.4	0.0	601	191	11
29	2	1193	4.2	482	0	482	31.0	3.6	0.0	10.2	0.6	0.0	621	194	11
29	3	951	3.8	694	0	694	30.2	3.1	0.0	9.9	0.7	0.0	614	196	11
29	4	1541	2.3	2348	0	2348	25.6	1.0	0.0	8.4	0.3	0.0	578	188	11
29	5	754	3.3	1287	0.	1287	28.5	2.0	0.0	9.4	0.5	0.0	595	193	11
29	6	523	3.9	953	460	1414	30.5	2.3	1.8	10.0	0.6	2.9	426	167	9

(10) Suspended Solids Run-1 (Total) (8/8)

					SS			Cu			Zn				
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
29	7	665	3.6	1056	527	1584	29.5	1.1	1.8	9.7	0.4	2.9	408	164	9
29	8	1252	3.5	772	389	1161	29.2	0.8	1.8	9.6	0.3	2.9	403	162	9
29	9	941	5.2	280	123	402	33.5	2.3	1.8	11.0	0.6	2.9	434	168	9
29	10	1467	4.2	404	192	596	31.1	1.7	1.8	10.2	0.4	2.9	419	165	9
29	11	2720	3.1	675	355	1030	27.9	1.2	1.8	9.2	0.3	2.9	403	162	9
29	12	3330	2.8	801	0	801	27.1	1.3	0.0	8.9	0.2	0.0	582	188	11
30	1	1979	3.5	562	0	562	29.3	2.4	0.0	9.6	0.4	0.0	601	191	11
30	2	1183	4.2	482	0	482	31.1	3.6	0.0	10.2	0.6	0.0	621	194	11
30	3	947	3.8	701	0	701	30.2	3.1	0.0	9.9	0.7	0.0	613	196	11
30	4	1518	2.3	2353	0	2353	25.7	1.0	0.0	8.4	0.3	0.0	579	189	11
30	5	743	3.3	1290	0	1290	28.6	2.0	0.0	9.4	0.5	0.0	595	193	11
30	6	515	4.0	956	460	1417	30.6	2.3	1.8	10.1	0.6	2.9	426	167	9
30	7	657	3.6	1059	527	1587	29.6	1.1	1.8	9.7	0.4	2.9	408	164	9
30	8	1232	3.5	766	385	1151	29.3	0.8	1.8	9.7	0.3	2.9	403	162	9
30	9	937	5.2	280	123	403	33.5	2.3	1.8	11.0	0.6	2.9	434	168	9
30	10	1460	4.2	405	192	596	31.1	1.6	1.8	10.2	0.4	2.9	419	165	9
30	11	2707	3.1	675	355	1031	28.0	1.2	1.8	9.2	0.3	2.9	403	162	9
30	12	3314	2.8	801	0	801	27.1	1.3	0.0	8.9	0.3	0.0	582	188	11
31	1	1968	3.5	562	0	562	29.3	2.4	0.0	9.6	0.4	0.0	601	191	11
31	2	1174	4.2	482	0	482	31.1	3.6	0.0	10.2	0.6	0.0	621	194	11
31	3	943	3.9	708	0	708	30.2	3.1	0.0	9.9	0.7	0.0	613	196	11
31	4	1495	2.3	2358	0	2358	25.7	1.0	0.0	8.4	0.3	0.0	579	189	11
31	5	731	3.3	1293	0	1293	28.7	2.0	0.0	9.5	0.5	0.0	595	193	11
31	6	507	4.0	959	460	1419	30.7	2.3	1.8	10.1	0.6	2.9	426	167	9
31	7	648	3.6	1063	528	1590	29.6	1.1	1.8	9.8	0.4	2.9	408	164	9
31	8	1213	3.6	761	381	1142	29.4	0.8	1.8	9.7	0.3	2.9	403	162	9
31	9	932	5.2	280	123	403	33.6	2.3	1.8	11.0	0.6	2.9	433	168	9
31	10	1453	4.2	405	192	597	31.1	1.6	1.8	10.2	0.4	2.9	419	165	9
31	11	2694	3.1	676	355	1031	28.0	1.2	1.8	9.2	0.3	2.9	403	162	9
31	12	3298	2.8	802	0	802	27.1	1.3	0.0	8.9	0.3	0.0	582	188	11

(11) Suspended Solids Run-3 (Soluble) (1/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
1	9	4012	2.1	1508	567	2075	5.9	0.3	0.0	2.7	0.1	0.0	101	46	0
1	10	1385	4.3	343	102	445	7.4	2.0	0.0	3.4	0.4	0.0	129	53	0
1	11	3632	2.7	766	268	1035	6.3	1.0	0.0	2.9	0.2	0.0	113	48	0
1	12	3765	2.6	791	0	791	6.3	1.2	0.0	2.9	0.2	0.0	156	65	0
2	1	2410	3.2	561	0	561	6.7	2.1	0.0	3.1	0.3	0.0	172	67	0
2	2	1702	3.7	492	0	492	7.0	3.0	0.0	3.2	0.4	0.0	187	69	0
2	3	1088	4.0	477	0	477	7.3	3.9	0.0	3.4	0.7	0.0	202	73	0
2	4	1570	2.5	1394	0	1394	6.2	1.4	0.0	2.9	0.3	0.0	162	67	0
2	5	959	2.9	1142	0	1142	6.5	1.8	0.0	3.0	0.4	0.0	168	68	0
2	6	842	3.1	1026	342	1368	6.6	2.0	0.0	3.1	0.4	0.0	129	52	0
2	7	857	3.1	1043	349	1392	6.6	0.9	0.0	3.1	0.2	0.0	112	49	0
2	8	582	5.7	260	70	331	8.2	2.5	0.0	3.8	0.6	0.0	135	55	0
2	9	1873	3.7	442	139	581	7.0	1.5	0.0	3.3	0.3	0.0	122	51	0
2	10	786	5.7	216	58	275	8.2	2.5	0.0	3.8	0.6	0.0	135	56	0
2	11	3637	2.7	770	270	1040	6.3	0.9	0.0	2.9	0.2	0.0	111	48	0
2	12	3608	2.7	781	0	781	6.3	1.1	0.0	2.9	0.2	0.0	155	65	0
3	1	2069	3.4	542	0	542	6.8	2.3	0.0	3.2	0.4	0.0	175	68	0
3	2	1179	4.1	456	0	456	7.3	3.6	0.0	3.4	0.6	0.0	196	71	0
3	3	1424	2.9	988	0	988	6.5	2.0	0.0	3.0	0.4	0.0	172	69	0
3	4	3437	1.5	3376	0	3376	5.3	0.6	0.0	2.5	0.1	0.0	147	64	0
3	5	758	3.3	948	0	948	6.7	2.4	0.0	3.1	0.4	0.0	179	70	0
3	6	718	3.4	907	295	1201	6.8	2.2	0.0	3.1	0.4	0.0	131	52	0
3	7	950	3.1	988	330	1319	6.6	1.4	0.0	3.1	0.3	0.0	119	50	0
3	8	624	4.7	410	119	529	7.6	1.7	0.0	3.5	0.4	0.0	124	52	0
3	9	1070	4.9	278	80	358	7.7	2.2	0.0	3.6	0.5	0.0	132	54	0
3	10	3238	2.8	700	241	942	6.4	1.1	0.0	3.0	0.2	0.0	114	49	0
3	11	3619	2.7	770	270	1040	6.3	1.1	0.0	2.9	0.2	0.0	115	48	0
3	12	3557	2.7	782	0	782	6.3	1.4	0.0	2.9	0.2	0.0	160	65	0
4	1	2067	3.4	542	0	542	6.8	2.6	0.0	3.2	0.4	0.0	182	68	0
4	2	1167	4.1	457	0	457	7.3	4.0	0.0	3.4	0.6	0.0	203	71	0
4	3	1348	3.0	947	0	947	6.5	2.2	0.0	3.0	0.4	0.0	176	70	0
4	4	2241	1.9	2400	0	2400	5.7	0.9	0.0	2.7	0.2	0.0	153	65	0
4	5	1109	2.7	1318	0	1318	6.3	1.9	0.0	2.9	0.3	0.0	170	68	0
4	6	726	3.3	925	301	1226	6.8	2.5	0.0	3.1	0.5	0.0	136	52	0
4	7	825	3.1	1030	343	1373	6.6	2.1	0.0	3.1	0.4	0.0	130	52	0
4	8	840	3.1	1047	349	1397	6.6	0.9	0.0	3.1	0.2	0.0	112	49	0
4	9	3399	2.4	1139	413	1552	6.1	0.7	0.0	2.8	0.1	0.0	108	47	0
4	10	1682	3.9	417	129	546	7.2	2.2	0.0	3.3	0.4	0.0	132	52	0
4	11	3613	2.7	772	270	1042	6.3	1.3	0.0	2.9	0.2	0.0	117	48	0
4	12	3605	2.7	783	0	783	6.3	1.5	0.0	2.9	0.2	0.0	164	65	0
5	1	2076	3.4	544	0	544	6.8	2.8	0.0	3.2	0.4	0.0	185	68	0
5	2	1201	4.0	460	0	460	7.3	4.2	0.0	3.4	0.6	0.0	208	71	0
5	3	1281	3.1	879	0	879	6.6	2.5	0.0	3.1	0.5	0.0	181	70	0
5	4	3130	1.6	3188	0	3188	5.4	0.7	0.0	2.5	0.1	0.0	149	64	0
5	5	2733	1.7	2857	0	2857	5.5	1.0	0.0	2.6	0.2	0.0	154	65	0
5	6	777	3.2	989	326	1314	6.7	1.6	0.0	3.1	0.3	0.0	123	50	0

(11) Suspended Solids Run-3 (Soluble) (2/8)

Y	M	TR	DO	SS			Cu			Zn			Cu	Zn	As
				MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT			
5	7	1725	3.1	794	266	1061	6.6	1.2	0.0	3.1	0.2	0.0	116	49	0
5	8	628	6.4	182	47	229	8.5	4.3	0.0	4.0	0.7	0.0	157	57	0
5	9	1220	4.6	313	91	404	7.6	2.0	0.0	3.5	0.5	0.0	129	53	0
5	10	1858	3.7	445	139	584	7.1	1.5	0.0	3.3	0.4	0.0	122	51	0
5	11	1951	3.6	463	146	609	7.0	1.6	0.0	3.2	0.3	0.0	122	51	0
5	12	3718	2.6	794	0	794	6.3	1.1	0.0	2.9	0.2	0.0	154	65	0
6	1	2407	3.2	560	0	560	6.7	2.0	0.0	3.1	0.3	0.0	171	67	0
6	2	1574	3.8	487	0	487	7.1	3.0	0.0	3.3	0.5	0.0	187	69	0
6	3	992	4.1	493	0	493	7.3	3.8	0.0	3.4	0.7	0.0	201	74	0
6	4	2191	1.9	2406	0	2406	5.8	0.8	0.0	2.7	0.2	0.0	150	65	0
6	5	2052	2.0	2285	0	2285	5.8	1.0	0.0	2.7	0.2	0.0	155	66	0
6	6	1682	2.2	1924	711	2636	6.0	1.4	0.0	2.8	0.2	0.0	118	48	0
6	7	1082	2.7	1320	458	1779	6.4	2.1	0.0	2.9	0.4	0.0	130	50	0
6	8	798	3.2	1024	339	1363	6.7	1.4	0.0	3.1	0.3	0.0	119	50	0
6	9	2696	2.5	1123	401	1525	6.2	0.8	0.0	2.9	0.1	0.0	110	47	0
6	10	1997	3.5	492	157	649	6.9	2.1	0.0	3.2	0.3	0.0	130	51	0
6	11	1576	4.0	390	119	509	7.3	2.5	0.0	3.4	0.4	0.0	136	52	0
6	12	3484	2.7	754	0	754	6.4	1.3	0.0	2.9	0.2	0.0	159	65	0
7	1	2449	3.2	561	0	561	6.7	2.4	0.0	3.1	0.3	0.0	178	67	0
7	2	1569	3.8	487	0	487	7.1	3.4	0.0	3.3	0.5	0.0	195	69	0
7	3	1027	4.0	513	0	513	7.3	4.1	0.0	3.4	0.7	0.0	206	73	0
7	4	3691	1.5	3737	0	3737	5.2	0.5	0.0	2.4	0.1	0.0	145	64	0
7	5	2573	1.8	2775	0	2775	5.6	0.9	0.0	2.6	0.2	0.0	153	65	0
7	6	1869	2.1	2133	799	2932	5.9	1.4	0.0	2.7	0.2	0.0	118	48	0
7	7	848	3.1	1088	363	1451	6.6	2.7	0.0	3.1	0.4	0.0	139	52	0
7	8	730	3.3	961	313	1274	6.8	2.2	0.0	3.1	0.4	0.0	132	52	0
7	9	1230	3.0	994	336	1329	6.5	1.5	0.0	3.0	0.3	0.0	121	50	0
7	10	1376	3.4	696	226	922	6.8	2.2	0.0	3.1	0.4	0.0	131	51	0
7	11	1346	3.5	658	212	870	6.9	2.7	0.0	3.2	0.5	0.0	138	53	0
7	12	1125	3.4	739	0	739	6.8	3.0	0.0	3.2	0.6	0.0	189	71	0
8	1	1831	2.1	2110	0	2110	5.9	1.1	0.0	2.7	0.2	0.0	156	66	0
8	2	2874	1.7	3071	0	3071	5.5	0.8	0.0	2.5	0.1	0.0	152	64	0
8	3	3333	1.6	3475	0	3475	5.3	0.8	0.0	2.5	0.1	0.0	152	64	0
8	4	2225	1.9	2497	0	2497	5.7	1.4	0.0	2.7	0.2	0.0	163	65	0
8	5	1472	2.3	1754	0	1754	6.1	2.0	0.0	2.8	0.3	0.0	176	67	0
8	6	1649	2.2	1938	715	2652	6.0	1.9	0.0	2.8	0.2	0.0	126	48	0
8	7	957	2.9	1220	415	1635	6.5	2.9	0.0	3.0	0.4	0.0	141	51	0
8	8	718	3.4	961	312	1273	6.8	2.6	0.0	3.1	0.4	0.0	137	52	0
8	9	1258	2.9	1043	354	1397	6.5	1.2	0.0	3.0	0.2	0.0	116	49	0
8	10	2212	3.0	749	252	1001	6.6	1.8	0.0	3.0	0.3	0.0	126	50	0
8	11	2352	3.0	735	248	982	6.6	1.9	0.0	3.0	0.3	0.0	126	50	0
8	12	2480	2.9	751	0	751	6.5	2.0	0.0	3.0	0.3	0.0	171	67	0
9	1	1500	3.7	521	0	521	7.1	3.4	0.0	3.3	0.5	0.0	195	70	0
9	2	842	4.4	453	0	453	7.4	4.8	0.0	3.4	0.7	0.0	215	74	0
9	3	1463	2.4	1763	0	1763	6.1	1.2	0.0	2.8	0.3	0.0	157	67	0
9	4	1190	2.6	1479	0	1479	6.3	1.6	0.0	2.9	0.3	0.0	164	67	0
9	5	1314	2.5	1612	0	1612	6.2	1.5	0.0	2.9	0.3	0.0	164	67	0
9	6	785	3.2	1044	344	1388	6.7	2.4	0.0	3.1	0.4	0.0	134	52	0

(11) Suspended Solids Run-3 (Soluble) (3/8)

					SS			Cu			Zn				
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
9	7	701	3.4	952	308	1260	6.8	2.1	0.0	3.2	0.4	0.0	130	52	0
9	8	1045	3.1	1012	339	1351	6.6	1.4	0.0	3.1	0.3	0.0	119	50	0
9	9	2201	2.6	1116	394	1510	6.3	0.7	0.0	2.9	0.2	0.0	108	47	0
9	10	1998	3.5	497	159	656	6.9	1.9	0.0	3.2	0.3	0.0	127	51	0
9	11	3026	2.9	676	230	906	6.5	1.5	0.0	3.0	0.2	0.0	120	49	0
9	12	3675	2.6	797	0	797	6.3	1.3	0.0	2.9	0.2	0.0	160	65	0
10	1	2444	3.2	567	0	567	6.7	2.3	0.0	3.1	0.3	0.0	177	67	0
10	2	1723	3.7	499	0	499	7.0	3.2	0.0	3.2	0.4	0.0	191	69	0
10	3	1163	4.0	494	0	494	7.2	3.9	0.0	3.4	0.6	0.0	202	72	0
10	4	1187	3.1	923	0	923	6.6	2.3	0.0	3.1	0.5	0.0	177	70	0
10	5	1403	2.5	1582	0	1582	6.2	1.4	0.0	2.9	0.3	0.0	162	67	0
10	6	896	3.0	1179	397	1576	6.6	2.0	0.0	3.0	0.4	0.0	128	51	0
10	7	690	3.4	950	307	1256	6.9	2.1	0.0	3.2	0.4	0.0	130	52	0
10	8	914	3.2	960	316	1276	6.7	1.9	0.0	3.1	0.4	0.0	127	52	0
10	9	1009	3.2	948	314	1262	6.7	1.8	0.0	3.1	0.4	0.0	126	51	0
10	10	808	3.7	691	216	907	7.1	2.9	0.0	3.3	0.6	0.0	141	55	0
10	11	1644	2.2	1991	734	2725	6.0	1.1	0.0	2.8	0.2	0.0	113	48	0
10	12	1801	2.1	2161	0	2161	5.9	1.2	0.0	2.7	0.2	0.0	157	66	0
11	1	1262	2.5	1592	0	1592	6.2	1.7	0.0	2.9	0.3	0.0	168	67	0
11	2	1861	2.1	2228	0	2228	5.9	1.3	0.0	2.7	0.2	0.0	161	66	0
11	3	2536	1.8	2881	0	2881	5.6	1.1	0.0	2.6	0.2	0.0	157	65	0
11	4	1942	2.0	2317	0	2317	5.9	1.5	0.0	2.7	0.2	0.0	166	66	0
11	5	1299	2.5	1637	0	1637	6.2	2.2	0.0	2.9	0.3	0.0	178	67	0
11	6	661	3.5	929	298	1227	6.9	3.1	0.0	3.2	0.4	0.0	144	52	0
11	7	979	3.2	992	329	1320	6.7	2.1	0.0	3.1	0.4	0.0	129	51	0
11	8	300	6.5	263	68	331	8.6	2.9	0.0	4.0	0.6	0.0	140	56	0
11	9	1960	3.6	474	150	624	7.0	1.6	0.0	3.2	0.3	0.0	122	51	0
11	10	2754	3.1	629	211	840	6.6	1.3	0.0	3.0	0.3	0.0	118	49	0
11	11	3474	2.7	765	266	1031	6.4	1.4	0.0	2.9	0.2	0.0	119	49	0
11	12	3005	2.8	762	0	762	6.4	1.8	0.0	3.0	0.3	0.0	168	66	0
12	1	1498	3.7	519	0	519	7.1	3.3	0.0	3.3	0.5	0.0	193	70	0
12	2	865	4.2	505	0	505	7.4	4.2	0.0	3.4	0.7	0.0	206	73	0
12	3	1642	2.2	2018	0	2018	6.0	1.0	0.0	2.8	0.3	0.0	155	66	0
12	4	1715	2.2	2103	0	2103	6.0	1.2	0.0	2.8	0.2	0.0	158	66	0
12	5	1284	2.5	1640	0	1640	6.2	1.7	0.0	2.9	0.3	0.0	167	67	0
12	6	790	3.2	1090	360	1450	6.7	2.4	0.0	3.1	0.4	0.0	135	52	0
12	7	756	3.3	1052	345	1397	6.7	1.1	0.0	3.1	0.3	0.0	116	50	0
12	8	3032	2.4	1157	416	1573	6.2	0.8	0.0	2.8	0.2	0.0	110	47	0
12	9	1608	3.9	454	140	594	7.2	2.1	0.0	3.3	0.4	0.0	130	51	0
12	10	2081	3.5	500	160	660	6.9	2.0	0.0	3.2	0.3	0.0	128	51	0
12	11	3494	2.7	771	269	1040	6.4	1.4	0.0	2.9	0.2	0.0	119	48	0
12	12	3332	2.7	783	0	783	6.4	1.6	0.0	2.9	0.2	0.0	165	66	0
13	1	1970	3.5	546	0	546	6.9	2.9	0.0	3.2	0.4	0.0	187	69	0
13	2	1134	4.1	462	0	462	7.3	4.3	0.0	3.4	0.6	0.0	209	72	0
13	3	967	3.5	749	0	749	6.9	2.9	0.0	3.2	0.6	0.0	186	72	0
13	4	1184	2.6	1543	0	1543	6.3	1.4	0.0	2.9	0.3	0.0	161	68	0
13	5	850	3.1	1170	0	1170	6.6	1.9	0.0	3.1	0.4	0.0	170	69	0
13	6	1016	2.8	1361	468	1829	6.4	1.7	0.0	3.0	0.4	0.0	124	51	0

(11) Suspended Solids Run-3 (Soluble) (4/8)

				SS			Cu			Zn					
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
13	7	759	3.3	1067	350	1417	6.7	0.9	0.0	3.1	0.2	0.0	113	49	0
13	8	2182	3.0	807	273	1081	6.5	1.0	0.0	3.0	0.2	0.0	113	49	0
13	9	897	5.3	250	69	319	8.0	3.0	0.0	3.7	0.6	0.0	142	55	0
13	10	2103	3.5	506	162	668	6.9	1.5	0.0	3.2	0.3	0.0	122	51	0
13	11	3478	2.7	771	268	1040	6.4	1.2	0.0	2.9	0.2	0.0	116	49	0
13	12	3310	2.7	785	0	785	6.4	1.4	0.0	2.9	0.2	0.0	160	66	0
14	1	2033	3.4	556	0	556	6.9	2.4	0.0	3.2	0.4	0.0	177	68	0
14	2	1397	3.9	488	0	488	7.2	3.2	0.0	3.3	0.5	0.0	190	70	0
14	3	898	4.3	475	0	475	7.4	3.9	0.0	3.4	0.7	0.0	201	74	0
14	4	1154	2.8	1289	0	1289	6.4	1.5	0.0	3.0	0.4	0.0	163	69	0
14	5	1659	2.2	2089	0	2089	6.0	1.1	0.0	2.8	0.3	0.0	156	66	0
14	6	706	3.4	1014	328	1342	6.8	1.2	0.0	3.2	0.3	0.0	117	50	0
14	7	2601	2.5	1127	400	1527	6.2	0.9	0.0	2.9	0.2	0.0	112	48	0
14	8	2902	2.7	873	303	1176	6.4	1.1	0.0	2.9	0.2	0.0	114	48	0
14	9	626	6.4	188	48	236	8.6	4.1	0.0	4.0	0.7	0.0	154	57	0
14	10	2389	3.3	565	185	750	6.7	1.3	0.0	3.1	0.3	0.0	118	50	0
14	11	3449	2.7	769	267	1037	6.4	1.2	0.0	2.9	0.2	0.0	117	49	0
14	12	3114	2.8	771	0	771	6.4	1.6	0.0	3.0	0.3	0.0	164	66	0
15	1	1599	3.7	525	0	525	7.0	3.2	0.0	3.3	0.5	0.0	190	70	0
15	2	894	4.2	505	0	505	7.4	4.2	0.0	3.4	0.7	0.0	206	74	0
15	3	3813	1.5	4208	0	4208	5.2	0.5	0.0	2.4	0.1	0.0	144	64	0
15	4	1526	2.3	1963	0	1963	6.1	1.4	0.0	2.8	0.3	0.0	162	67	0
15	5	2156	1.9	2644	0	2644	5.8	1.1	0.0	2.7	0.2	0.0	158	66	0
15	6	1707	2.2	2168	803	2971	6.0	1.5	0.0	2.8	0.2	0.0	121	48	0
15	7	646	3.5	954	304	1258	6.9	3.2	0.0	3.2	0.5	0.0	146	53	0
15	8	138	7.7	269	65	334	9.1	2.6	0.0	4.2	0.6	0.0	136	56	0
15	9	850	5.5	241	66	307	8.1	2.1	0.0	3.7	0.6	0.0	131	55	0
15	10	770	5.8	223	60	283	8.2	1.9	0.0	3.8	0.6	0.0	128	56	0
15	11	2203	3.4	530	171	702	6.8	1.0	0.0	3.2	0.3	0.0	114	50	0
15	12	3588	2.7	799	0	799	6.3	0.9	0.0	2.9	0.2	0.0	150	65	0
16	1	2302	3.3	558	0	558	6.8	2.0	0.0	3.1	0.4	0.0	170	68	0
16	2	1324	4.0	476	0	476	7.2	3.2	0.0	3.3	0.6	0.0	190	71	0
16	3	1102	3.5	724	0	724	6.9	2.7	0.0	3.2	0.6	0.0	183	72	0
16	4	3584	1.5	4050	0	4050	5.3	0.5	0.0	2.4	0.1	0.0	144	64	0
16	5	6097	1.2	6384	0	6384	4.9	0.4	0.0	2.2	0.1	0.0	142	63	0
16	6	1072	2.7	1472	511	1983	6.4	2.2	0.0	2.9	0.4	0.0	131	51	0
16	7	744	3.3	1085	355	1440	6.8	1.1	0.0	3.1	0.2	0.0	116	49	0
16	8	2063	3.1	727	242	968	6.6	1.4	0.0	3.1	0.2	0.0	119	49	0
16	9	1672	3.9	424	130	555	7.2	2.5	0.0	3.3	0.4	0.0	135	52	0
16	10	1869	3.7	465	146	611	7.0	2.1	0.0	3.3	0.4	0.0	130	51	0
16	11	3411	2.7	768	266	1034	6.4	1.5	0.0	2.9	0.2	0.0	121	49	0
16	12	2978	2.8	766	0	766	6.4	1.9	0.0	3.0	0.3	0.0	170	67	0
17	1	1465	3.8	515	0	515	7.1	3.9	0.0	3.3	0.6	0.0	204	71	0
17	2	1086	3.6	711	0	711	7.0	3.5	0.0	3.2	0.6	0.0	197	72	0
17	3	4684	1.3	5131	0	5131	5.0	0.5	0.0	2.3	0.1	0.0	144	63	0
17	4	4386	1.4	4868	0	4868	5.1	0.6	0.0	2.4	0.1	0.0	147	64	0
17	5	759	3.3	1113	0	1113	6.7	1.1	0.0	3.1	0.2	0.0	152	65	0
17	6	1503	3.9	480	148	628	7.2	2.2	0.0	3.3	0.3	0.0	132	51	0

(11) Suspended Solids Run-3 (Soluble) (5/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
17	7	1378	4.3	362	108	470	7.4	2.7	0.0	3.4	0.4	0.0	138	53	0
17	8	1207	4.6	324	95	419	7.6	2.5	0.0	3.5	0.5	0.0	136	54	0
17	9	880	5.4	250	69	319	8.0	2.6	0.0	3.7	0.6	0.0	136	55	0
17	10	3567	2.7	800	280	1080	6.3	1.0	0.0	2.9	0.2	0.0	112	48	0
17	11	3418	2.7	776	269	1045	6.4	1.2	0.0	2.9	0.2	0.0	116	49	0
17	12	3397	2.7	796	0	796	6.4	1.3	0.0	2.9	0.2	0.0	158	65	0
18	1	2200	3.4	559	0	559	6.8	2.5	0.0	3.1	0.4	0.0	179	68	0
18	2	1345	4.0	480	0	480	7.2	3.7	0.0	3.3	0.6	0.0	199	71	0
18	3	1103	3.6	687	0	687	7.0	3.3	0.0	3.2	0.6	0.6	193	73	0
18	4	2411	1.8	2981	0	2981	5.7	0.8	0.0	2.6	0.2	0.0	150	65	0
18	5	1923	2.1	2484	0	2484	5.9	1.2	0.0	2.7	0.2	0.0	157	66	0
18	6	2269	1.9	2852	1104	3956	5.7	1.1	0.0	2.6	0.2	0.0	114	47	0
18	7	665	3.5	1010	324	1334	6.9	2.1	0.0	3.2	0.4	0.0	130	51	0
18	8	202	8.1	190	45	235	9.3	3.6	0.0	4.3	0.8	0.0	148	58	0
18	9	295	9.3	103	23	126	9.8	3.2	0.0	4.5	1.0	0.0	142	60	0
18	10	780	5.7	228	61	290	8.2	1.1	0.0	3.8	0.6	0.0	117	56	0
18	11	3433	2.7	778	270	1049	6.4	0.6	0.0	2.9	0.2	0.0	107	48	0
18	12	3434	2.7	787	0	787	6.4	1.0	0.0	2.9	0.2	0.0	152	66	0
19	1	1894	3.5	546	0	546	6.9	2.1	0.0	3.2	0.4	0.0	171	69	0
19	2	1023	4.3	457	0	457	7.4	3.4	0.0	3.4	0.7	0.0	193	73	0
19	3	1073	3.2	981	0	981	6.7	1.9	0.0	3.1	0.5	0.0	169	71	0
19	4	3632	1.5	4239	0	4239	5.3	0.5	0.0	2.4	0.1	0.0	144	64	0
19	5	805	3.2	1195	0	1195	6.7	2.1	0.0	3.1	0.4	0.0	173	70	0
19	6	596	3.7	932	293	1226	7.0	2.3	0.0	3.3	0.5	0.0	133	54	0
19	7	843	3.2	1110	366	1476	6.7	0.7	0.0	3.1	0.2	0.0	109	49	0
19	8	922	4.9	333	95	428	7.7	2.0	0.0	3.6	0.5	0.0	129	54	0
19	9	609	6.5	187	48	235	8.6	2.8	0.0	4.0	0.7	0.0	138	57	0
19	10	1137	4.8	311	90	401	7.7	1.5	0.0	3.5	0.5	0.0	121	54	0
19	11	3416	2.7	778	270	1048	6.4	0.9	0.0	2.9	0.2	0.0	111	49	0
19	12	3377	2.7	784	0	784	6.4	1.2	0.0	2.9	0.3	0.0	157	66	0
20	1	1864	3.5	560	0	560	6.9	1.9	0.0	3.2	0.4	0.0	168	68	0
20	2	1469	3.8	505	0	505	7.1	2.4	0.0	3.3	0.4	0.0	175	69	0
20	3	1256	3.9	521	0	521	7.2	2.6	0.0	3.3	0.5	0.0	179	71	0
20	4	1966	2.8	1025	0	1025	6.4	1.4	0.0	3.0	0.3	0.0	160	67	0
20	5	1905	2.8	1051	0	1051	6.4	1.5	0.0	3.0	0.3	0.0	162	67	0
20	6	1921	2.8	1053	363	1416	6.4	1.3	0.0	3.0	0.3	0.0	118	49	0
20	7	1651	3.3	734	240	974	6.8	1.1	0.0	3.1	0.2	0.0	116	49	0
20	8	785	5.7	231	62	293	8.2	3.2	0.0	3.8	0.6	0.0	144	56	0
20	9	884	5.4	254	70	324	8.0	2.2	0.0	3.7	0.6	0.0	132	55	0
20	10	820	5.6	240	65	305	8.1	1.9	0.0	3.8	0.6	0.0	128	56	0
20	11	3031	2.9	707	241	948	6.5	0.9	0.0	3.0	0.2	0.0	111	49	0
20	12	3453	2.7	789	0	789	6.4	1.2	0.0	2.9	0.2	0.0	155	66	0
21	1	1915	3.5	553	0	553	6.9	2.2	0.0	3.2	0.4	0.0	173	69	0
21	2	1176	4.1	476	0	476	7.3	3.2	0.0	3.4	0.6	0.0	189	71	0
21	3	929	3.9	640	0	640	7.2	3.0	0.0	3.3	0.7	0.0	186	73	0
21	4	1192	2.6	1693	0	1693	6.3	1.2	0.0	2.9	0.3	0.0	157	68	0
21	5	618	3.6	981	0	981	7.0	1.7	0.0	3.2	0.5	0.0	164	69	0
21	6	981	3.3	997	515	1512	6.7	1.3	0.0	3.1	0.3	0.0	104	45	0

(11) Suspended Solids Run-3 (Soluble) (6/8)

					SS			Cu			Zn				
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
21	7	1857	2.8	1107	602	1710	6.4	0.9	0.0	3.0	0.2	0.0	97	42	0
21	8	3553	2.4	1177	668	1845	6.1	0.8	0.0	2.8	0.2	0.0	95	41	0
21	9	2222	3.3	628	324	953	6.7	1.6	0.0	3.1	0.3	0.0	107	44	0
21	10	1942	3.6	490	244	734	7.0	2.1	0.0	3.2	0.4	0.0	114	45	0
21	11	604	6.5	188	76	263	8.6	3.8	0.0	4.0	0.7	0.0	135	51	0
21	12	2701	3.1	645	0	645	6.6	1.1	0.0	3.1	0.3	0.0	154	66	0
22	1	2318	3.3	568	0	568	6.8	1.8	0.0	3.1	0.4	0.0	167	68	0
22	2	1509	3.9	496	0	496	7.2	2.8	0.0	3.3	0.5	0.0	183	70	0
22	3	940	4.2	504	0	504	7.4	3.8	0.0	3.4	0.8	0.0	199	75	0
22	4	2511	1.8	3234	0	3234	5.6	0.6	0.0	2.6	0.2	0.0	147	65	0
22	5	2901	1.7	3646	0	3646	5.5	0.7	0.0	2.5	0.2	0.0	149	65	0
22	6	1346	2.5	1911	1078	2989	6.2	1.6	0.0	2.9	0.3	0.0	107	43	0
22	7	627	3.6	1008	503	1511	7.0	2.1	0.0	3.2	0.4	0.0	114	46	0
22	8	1449	2.9	1087	581	1668	6.5	1.2	0.0	3.0	0.3	0.0	101	43	0
22	9	1978	3.1	793	416	1209	6.6	1.2	0.0	3.1	0.2	0.0	101	43	0
22	10	1277	4.5	347	161	508	7.5	2.7	0.0	3.5	0.5	0.0	122	47	0
22	11	3348	2.8	776	422	1198	6.4	1.3	0.0	3.0	0.2	0.0	102	42	0
22	12	3471	2.7	800	0	800	6.4	1.4	0.0	2.9	0.2	0.0	161	66	0
23	1	2213	3.4	569	0	569	6.8	2.4	0.0	3.1	0.4	0.0	178	68	0
23	2	1530	3.9	498	0	498	7.1	3.4	0.0	3.3	0.5	0.0	195	70	0
23	3	909	4.4	477	0	477	7.4	4.6	0.0	3.4	0.8	0.0	212	75	0
23	4	1826	2.1	2518	0	2518	5.9	0.9	0.0	2.7	0.2	0.0	152	66	0
23	5	755	3.3	1188	0	1188	6.7	2.0	0.0	3.1	0.5	0.0	171	70	0
23	6	663	3.5	1068	538	1606	6.9	2.2	0.0	3.2	0.5	0.0	115	47	0
23	7	680	3.5	1093	554	1647	6.9	0.8	0.0	3.2	0.3	0.0	97	44	0
23	8	519	6.1	255	105	360	8.4	2.3	0.0	3.9	0.6	0.0	119	50	0
23	9	1726	3.9	449	218	667	7.2	1.4	0.0	3.3	0.4	0.0	106	46	0
23	10	724	6.0	220	92	312	8.4	2.3	0.0	3.9	0.7	0.0	118	50	0
23	11	3350	2.8	780	425	1205	6.4	0.9	0.0	3.0	0.2	0.0	97	42	0
23	12	3314	2.8	791	0	791	6.4	1.2	0.0	3.0	0.3	0.0	156	66	0
24	1	1876	3.6	550	0	550	6.9	2.4	0.0	3.2	0.4	0.0	176	69	0
24	2	1013	4.3	459	0	459	7.4	3.9	0.0	3.4	0.7	0.0	200	73	0
24	3	1445	2.7	1360	0	1360	6.4	1.6	0.0	2.9	0.4	0.0	165	69	0
24	4	2700	1.7	3527	0	3527	5.5	0.7	0.0	2.6	0.2	0.0	149	65	0
24	5	594	3.7	989	0	989	7.0	2.6	0.0	3.3	0.6	0.0	181	71	0
24	6	563	3.8	948	464	1412	7.1	2.2	0.0	3.3	0.5	0.0	116	47	0
24	7	783	3.4	1031	524	1555	6.8	1.3	0.0	3.2	0.4	0.0	104	45	0
24	8	518	5.3	392	172	563	7.9	1.5	0.0	3.7	0.5	0.0	109	48	0
24	9	985	5.1	283	125	408	7.8	2.0	0.0	3.6	0.6	0.0	114	49	0
24	10	2981	2.9	710	379	1089	6.5	1.0	0.0	3.0	0.3	0.0	99	43	0
24	11	3331	2.8	780	424	1204	6.4	1.1	0.0	3.0	0.2	0.0	100	42	0
24	12	3262	2.8	792	0	792	6.4	1.4	0.0	3.0	0.3	0.0	160	66	0
25	1	1872	3.6	550	0	550	6.9	2.7	0.0	3.2	0.5	0.0	183	69	0
25	2	999	4.4	459	0	459	7.4	4.3	0.0	3.4	0.7	0.0	207	74	0
25	3	1340	2.8	1285	0	1285	6.4	1.8	0.0	3.0	0.4	0.0	169	70	0
25	4	1751	2.2	2496	0	2496	6.0	1.1	0.0	2.8	0.2	0.0	155	66	0
25	5	865	3.1	1371	0	1371	6.6	2.1	0.0	3.0	0.4	0.0	172	69	0
25	6	567	3.8	967	474	1441	7.1	2.6	0.0	3.3	0.6	0.0	121	48	0

(11) Suspended Solids Run-3 (Soluble) (7/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
25	7	643	3.5	1075	539	1614	6.9	2.2	0.0	3.2	0.5	0.0	115	47	0
25	8	659	3.5	1100	554	1654	6.9	0.8	0.0	3.2	0.3	0.0	97	44	0
25	9	2811	2.6	1038	573	1610	6.3	0.7	0.0	2.9	0.2	0.0	94	42	0
25	10	1501	4.1	404	192	595	7.3	2.2	0.0	3.4	0.4	0.0	115	46	0
25	11	3322	2.8	782	425	1206	6.4	1.2	0.0	3.0	0.2	0.0	102	42	0
25	12	3308	2.8	793	0	793	6.4	1.5	0.0	3.0	0.3	0.0	163	66	0
26	1	1880	3.6	552	0	552	6.9	2.8	0.0	3.2	0.4	0.0	185	69	0
26	2	1031	4.3	463	0	463	7.4	4.4	0.0	3.4	0.7	0.0	210	73	0
26	3	1249	3.0	1160	0	1160	6.5	2.1	0.0	3.0	0.5	0.0	173	71	0
26	4	2434	1.8	3340	0	3340	5.6	0.8	0.0	2.6	0.2	0.0	150	65	0
26	5	2121	2.0	2996	0	2996	5.8	1.1	0.0	2.7	0.2	0.0	157	66	0
26	6	608	3.7	1040	516	1556	7.0	1.6	0.0	3.2	0.3	0.0	107	45	0
26	7	1322	3.6	696	349	1045	6.9	1.3	0.0	3.2	0.3	0.0	104	44	0
26	8	577	6.7	185	74	259	8.7	3.8	0.0	4.0	0.8	0.0	135	52	0
26	9	1121	4.8	317	144	461	7.7	1.8	0.0	3.5	0.5	0.0	111	48	0
26	10	1707	3.9	452	219	671	7.2	1.4	0.0	3.3	0.4	0.0	106	46	0
26	11	1792	3.8	470	230	700	7.1	1.5	0.0	3.3	0.4	0.0	107	45	0
26	12	3414	2.7	804	0	804	6.4	1.1	0.0	2.9	0.2	0.0	153	66	0
27	1	2205	3.4	568	0	568	6.8	2.1	0.0	3.2	0.4	0.0	171	68	0
27	2	1399	4.0	494	0	494	7.2	3.2	0.0	3.3	0.5	0.0	189	71	0
27	3	936	4.1	562	0	562	7.3	3.7	0.0	3.4	0.8	0.0	197	75	0
27	4	1685	2.2	2479	0	2479	6.0	0.9	0.0	2.8	0.3	0.0	152	67	0
27	5	1586	2.3	2363	0	2363	6.0	1.2	0.0	2.8	0.3	0.0	157	67	0
27	6	1300	2.5	1994	1119	3113	6.2	1.6	0.0	2.9	0.3	0.0	105	43	0
27	7	835	3.1	1376	721	2097	6.6	2.3	0.0	3.1	0.5	0.0	115	46	0
27	8	621	3.6	1078	537	1615	7.0	1.2	0.0	3.2	0.3	0.0	103	44	0
27	9	2486	2.6	1142	631	1773	6.3	0.7	0.0	2.9	0.2	0.0	94	41	0
27	10	1711	3.9	454	221	675	7.2	2.2	0.0	3.3	0.4	0.0	116	46	0
27	11	1447	4.2	395	187	582	7.4	2.3	0.0	3.4	0.4	0.0	118	47	0
27	12	3197	2.8	764	0	764	6.4	1.3	0.0	3.0	0.2	0.0	158	66	0
28	1	2245	3.4	569	0	569	6.8	2.3	0.0	3.2	0.4	0.0	176	68	0
28	2	1393	4.0	494	0	494	7.2	3.5	0.0	3.3	0.6	0.0	195	71	0
28	3	972	4.1	588	0	588	7.3	3.8	0.0	3.4	0.8	0.0	201	75	0
28	4	2804	1.7	3854	0	3854	5.5	0.6	0.0	2.5	0.2	0.0	147	65	0
28	5	1979	2.0	2912	0	2912	5.9	1.1	0.0	2.7	0.2	0.0	156	66	0
28	6	1437	2.4	2208	1258	3466	6.1	1.6	0.0	2.8	0.3	0.0	106	43	0
28	7	652	3.5	1137	572	1709	6.9	2.9	0.0	3.2	0.5	0.0	124	47	0
28	8	562	3.8	1010	495	1505	7.1	2.1	0.0	3.3	0.5	0.0	114	47	0
28	9	1063	3.3	1034	534	1568	6.7	1.4	0.0	3.1	0.3	0.0	104	44	0
28	10	1282	3.6	721	361	1083	6.9	2.0	0.0	3.2	0.4	0.0	113	46	0
28	11	1272	3.6	683	339	1022	7.0	2.5	0.0	3.2	0.5	0.0	120	47	0
28	12	985	3.7	730	0	730	7.1	3.2	0.0	3.3	0.7	0.0	191	74	0
29	1	1401	2.4	2185	0	2185	6.1	1.1	0.0	2.8	0.3	0.0	156	67	0
29	2	2197	1.9	3226	0	3226	5.8	0.9	0.0	2.7	0.2	0.0	153	65	0
29	3	2548	1.8	3643	0	3643	5.6	1.0	0.0	2.6	0.2	0.0	154	65	0
29	4	1700	2.2	2599	0	2599	6.0	1.5	0.0	2.8	0.3	0.0	166	67	0
29	5	1124	2.7	1824	0	1824	6.3	2.2	0.0	2.9	0.4	0.0	178	68	0
29	6	1259	2.5	2011	1124	3135	6.2	2.0	0.0	2.9	0.3	0.0	112	43	0

(11) Suspended Solids Run-3 (Soluble) (8/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
29	7	730	3.3	1275	653	1928	6.8	2.9	0.0	3.1	0.5	0.0	124	47	0
29	8	550	3.8	1012	493	1505	7.1	2.4	0.0	3.3	0.5	0.0	118	47	0
29	9	1081	3.2	1086	564	1650	6.7	1.0	0.0	3.1	0.2	0.0	99	43	0
29	10	2115	3.1	771	403	1174	6.6	1.6	0.0	3.1	0.3	0.0	107	44	0
29	11	2274	3.1	755	396	1152	6.6	1.7	0.0	3.1	0.3	0.0	108	44	0
29	12	2416	3.0	773	0	773	6.6	1.8	0.0	3.0	0.3	0.0	167	67	0
30	1	1472	3.8	539	0	539	7.1	3.2	0.0	3.3	0.5	0.0	191	71	0
30	2	767	4.7	443	0	443	7.6	4.9	0.0	3.5	0.9	0.0	216	76	0
30	3	1105	2.7	1804	0	1804	6.4	1.2	0.0	2.9	0.4	0.0	157	69	0
30	4	904	3.0	1544	0	1544	6.5	1.6	0.0	3.0	0.4	0.0	164	69	0
30	5	998	2.8	1680	0	1680	6.4	1.6	0.0	3.0	0.4	0.0	165	69	0
30	6	596	3.7	1095	542	1637	7.0	2.4	0.0	3.3	0.6	0.0	118	48	0
30	7	534	3.9	1003	486	1489	7.2	1.9	0.0	3.3	0.5	0.0	112	47	0
30	8	871	3.4	1058	538	1596	6.8	1.2	0.0	3.2	0.4	0.0	102	45	0
30	9	1957	2.8	1120	607	1727	6.4	0.6	0.0	3.0	0.2	0.0	93	42	0
30	10	1710	3.9	460	223	683	7.2	1.9	0.0	3.3	0.4	0.0	112	46	0
30	11	2770	3.0	686	362	1048	6.6	1.4	0.0	3.0	0.3	0.0	104	43	0
30	12	3364	2.8	808	0	808	6.4	1.3	0.0	3.0	0.2	0.0	158	66	0
31	1	2235	3.4	575	0	575	6.8	2.3	0.0	3.2	0.4	0.0	175	68	0
31	2	1541	3.9	507	0	507	7.2	3.2	0.0	3.3	0.5	0.0	191	70	0
31	3	972	4.3	496	0	496	7.4	4.1	0.0	3.4	0.8	0.0	204	75	0
31	4	1004	3.2	1157	0	1157	6.7	2.0	0.0	3.1	0.5	0.0	171	71	0
31	5	1160	2.6	1938	0	1938	6.3	1.3	0.0	2.9	0.4	0.0	159	68	0
31	6	676	3.5	1235	625	1860	6.9	2.1	0.0	3.2	0.5	0.0	114	47	0
31	7	522	3.9	1001	483	1485	7.2	2.0	0.0	3.3	0.6	0.0	114	48	0
31	8	745	3.6	1003	500	1504	7.0	1.8	0.0	3.2	0.5	0.0	111	47	0
31	9	849	3.5	990	498	1488	6.9	1.7	0.0	3.2	0.5	0.0	109	46	0
31	10	689	4.1	707	336	1044	7.3	2.9	0.0	3.4	0.7	0.0	124	50	0
31	11	1236	2.6	2072	1154	3226	6.2	1.1	0.0	2.9	0.3	0.0	100	44	0
31	12	1352	2.4	2247	0	2247	6.2	1.3	0.0	2.8	0.3	0.0	158	68	0

(12) Suspended Solids Run-3 (Total) (1/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
1	9	4012	2.1	1508	567	2075	24.9	0.3	1.1	8.1	0.1	1.9	429	164	9
1	10	1385	4.3	343	102	445	31.4	2.0	1.1	10.3	0.4	1.9	471	172	10
1	11	3632	2.7	766	268	1035	26.7	1.0	1.1	8.8	0.2	1.9	445	167	10
1	12	3765	2.6	791	0	791	26.6	1.2	0.0	8.7	0.2	0.0	581	187	11
2	1	2410	3.2	561	0	561	28.4	2.1	0.0	9.4	0.3	0.0	596	190	11
2	2	1702	3.7	492	0	492	29.7	3.0	0.0	9.8	0.4	0.0	612	191	11
2	3	1088	4.0	477	0	477	30.7	3.9	0.0	10.1	0.7	0.0	627	195	11
2	4	1570	2.5	1394	0	1394	26.1	1.4	0.0	8.6	0.3	0.0	587	189	11
2	5	959	2.9	1142	0	1142	27.4	1.8	0.0	9.1	0.4	0.0	593	191	11
2	6	842	3.1	1026	342	1368	28.0	2.0	1.1	9.3	0.4	1.9	464	171	10
2	7	857	3.1	1043	349	1392	27.9	0.9	1.1	9.2	0.2	1.9	447	169	10
2	8	582	5.7	260	70	331	34.7	2.5	1.1	11.4	0.6	1.9	484	175	10
2	9	1873	3.7	442	139	581	29.8	1.5	1.1	9.8	0.3	1.9	461	171	10
2	10	786	5.7	216	58	275	34.7	2.5	1.1	11.4	0.6	1.9	484	176	10
2	11	3637	2.7	770	270	1040	26.7	0.9	1.1	8.8	0.2	1.9	443	167	10
2	12	3608	2.7	781	0	781	26.7	1.1	0.0	8.8	0.2	0.0	580	188	11
3	1	2069	3.4	542	0	542	28.9	2.3	0.0	9.5	0.4	0.0	599	191	11
3	2	1179	4.1	456	0	456	30.8	3.6	0.0	10.1	0.6	0.0	621	193	11
3	3	1424	2.9	988	0	988	27.4	2.0	0.0	9.0	0.4	0.0	596	192	11
3	4	3437	1.5	3376	0	3376	22.4	0.6	0.0	7.4	0.1	0.0	571	187	11
3	5	758	3.3	948	0	948	28.5	2.4	0.0	9.4	0.4	0.0	603	192	11
3	6	718	3.4	907	295	1201	28.8	2.2	1.1	9.5	0.4	1.9	468	172	10
3	7	950	3.1	988	330	1319	28.0	1.4	1.1	9.2	0.3	1.9	455	170	10
3	8	624	4.7	410	119	529	32.3	1.7	1.1	10.6	0.4	1.9	468	172	10
3	9	1070	4.9	278	80	358	32.7	2.2	1.1	10.8	0.5	1.9	477	174	10
3	10	3238	2.8	700	241	942	27.2	1.1	1.1	9.0	0.2	1.9	447	168	10
3	11	3619	2.7	770	270	1040	26.7	1.1	1.1	8.8	0.2	1.9	447	168	10
3	12	3557	2.7	782	0	782	26.7	1.4	0.0	8.8	0.2	0.0	585	188	11
4	1	2067	3.4	542	0	542	28.9	2.6	0.0	9.5	0.4	0.0	606	191	11
4	2	1167	4.1	457	0	457	30.8	4.0	0.0	10.1	0.6	0.0	628	194	11
4	3	1348	3.0	947	0	947	27.6	2.2	0.0	9.1	0.4	0.0	601	192	11
4	4	2241	1.9	2400	0	2400	24.3	0.9	0.0	7.9	0.2	0.0	578	186	11
4	5	1109	2.7	1318	0	1318	26.8	1.9	0.0	8.8	0.3	0.0	595	190	11
4	6	726	3.3	925	301	1226	28.7	2.5	1.1	9.5	0.5	1.9	473	172	10
4	7	825	3.1	1030	343	1373	28.1	2.1	1.1	9.3	0.4	1.9	466	172	10
4	8	840	3.1	1047	349	1397	28.0	0.9	1.1	9.3	0.2	1.9	448	169	10
4	9	3399	2.4	1139	413	1552	25.8	0.7	1.1	8.5	0.1	1.9	438	166	9
4	10	1682	3.9	417	129	546	30.3	2.2	1.1	10.0	0.4	1.9	472	171	10
4	11	3613	2.7	772	270	1042	26.7	1.3	1.1	8.8	0.2	1.9	450	168	10
4	12	3605	2.7	783	0	783	26.7	1.5	0.0	8.8	0.2	0.0	588	188	11
5	1	2076	3.4	544	0	544	28.9	2.8	0.0	9.5	0.4	0.0	610	191	11
5	2	1201	4.0	460	0	460	30.8	4.2	0.0	10.1	0.6	0.0	632	193	11
5	3	1281	3.1	879	0	879	28.0	2.5	0.0	9.2	0.5	0.0	606	193	11
5	4	3130	1.6	3188	0	3188	22.8	0.7	0.0	7.5	0.1	0.0	573	187	11
5	5	2733	1.7	2857	0	2857	23.4	1.0	0.0	7.7	0.2	0.0	579	187	11
5	6	777	3.2	989	326	1314	28.4	1.6	1.1	9.4	0.3	1.9	459	170	10

(12) Suspended Solids Run-3 (Total) (2/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
5	7	1725	3.1	794	266	1061	27.9	1.2	1.1	9.2	0.2	1.9	451	169	10
5	8	628	6.4	182	47	229	36.2	4.3	1.1	11.9	0.7	1.9	508	177	10
5	9	1220	4.6	313	91	404	32.0	2.0	1.1	10.5	0.5	1.9	472	173	10
5	10	1858	3.7	445	139	584	29.8	1.5	1.1	9.8	0.4	1.9	461	171	10
5	11	1951	3.6	463	146	609	29.6	1.6	1.1	9.7	0.3	1.9	461	171	10
5	12	3718	2.6	794	0	794	26.6	1.1	0.0	8.8	0.2	0.0	578	187	11
6	1	2407	3.2	560	0	560	28.5	2.0	0.0	9.4	0.3	0.0	595	190	11
6	2	1574	3.8	487	0	487	29.9	3.0	0.0	9.9	0.5	0.0	612	192	11
6	3	992	4.1	493	0	493	30.8	3.8	0.0	10.1	0.7	0.0	625	196	11
6	4	2191	1.9	2406	0	2406	24.4	0.8	0.0	8.0	0.2	0.0	575	186	11
6	5	2052	2.0	2285	0	2285	24.7	1.0	0.0	8.1	0.2	0.0	580	187	11
6	6	1682	2.2	1924	711	2636	25.3	1.4	1.1	8.3	0.2	1.9	447	167	9
6	7	1082	2.7	1320	458	1779	26.9	2.1	1.1	8.9	0.4	1.9	462	170	10
6	8	798	3.2	1024	339	1363	28.3	1.4	1.1	9.3	0.3	1.9	455	169	10
6	9	2696	2.5	1123	401	1525	26.2	0.8	1.1	8.6	0.1	1.9	441	166	9
6	10	1997	3.5	492	157	649	29.3	2.1	1.1	9.7	0.3	1.9	469	170	10
6	11	1576	4.0	390	119	509	30.7	2.5	1.1	10.1	0.4	1.9	477	172	10
6	12	3484	2.7	754	0	754	26.9	1.3	0.0	8.8	0.2	0.0	584	188	11
7	1	2449	3.2	561	0	561	28.4	2.4	0.0	9.4	0.3	0.0	602	190	11
7	2	1569	3.8	487	0	487	30.0	3.4	0.0	9.9	0.5	0.0	619	192	11
7	3	1027	4.0	513	0	513	30.7	4.1	0.0	10.1	0.7	0.0	631	196	11
7	4	3691	1.5	3737	0	3737	22.2	0.5	0.0	7.3	0.1	0.0	569	187	11
7	5	2573	1.8	2775	0	2775	23.6	0.9	0.0	7.8	0.2	0.0	578	187	11
7	6	1869	2.1	2133	799	2932	25.0	1.4	1.1	8.2	0.2	1.9	446	166	9
7	7	848	3.1	1088	363	1451	28.0	2.7	1.1	9.2	0.4	1.9	474	172	10
7	8	730	3.3	961	313	1274	28.7	2.2	1.1	9.5	0.4	1.9	468	171	10
7	9	1230	3.0	994	336	1329	27.7	1.5	1.1	9.1	0.3	1.9	456	169	10
7	10	1376	3.4	696	226	922	28.8	2.2	1.1	9.5	0.4	1.9	468	171	10
7	11	1346	3.5	658	212	870	29.1	2.7	1.1	9.6	0.5	1.9	476	172	10
7	12	1125	3.4	739	0	739	28.9	3.0	0.0	9.5	0.6	0.0	614	194	11
8	1	1831	2.1	2110	0	2110	25.1	1.1	0.0	8.2	0.2	0.0	581	187	11
8	2	2874	1.7	3071	0	3071	23.2	0.8	0.0	7.6	0.1	0.0	576	186	11
8	3	3333	1.6	3475	0	3475	22.6	0.8	0.0	7.4	0.1	0.0	577	187	11
8	4	2225	1.9	2497	0	2497	24.3	1.4	0.0	7.9	0.2	0.0	588	186	11
8	5	1472	2.3	1754	0	1754	25.8	2.0	0.0	8.5	0.3	0.0	601	188	11
8	6	1649	2.2	1938	715	2652	25.4	1.9	1.1	8.3	0.2	1.9	455	167	9
8	7	957	2.9	1220	415	1635	27.5	2.9	1.1	9.1	0.4	1.9	475	171	10
8	8	718	3.4	961	312	1273	28.8	2.6	1.1	9.5	0.4	1.9	474	171	10
8	9	1258	2.9	1043	354	1397	27.5	1.2	1.1	9.1	0.2	1.9	450	168	10
8	10	2212	3.0	749	252	1001	27.8	1.8	1.1	9.2	0.3	1.9	460	170	10
8	11	2352	3.0	735	248	982	27.7	1.9	1.1	9.2	0.3	1.9	461	169	10
8	12	2480	2.9	751	0	751	27.6	2.0	0.0	9.1	0.3	0.0	595	189	11
9	1	1500	3.7	521	0	521	29.8	3.4	0.0	9.8	0.5	0.0	620	192	11
9	2	842	4.4	453	0	453	31.5	4.8	0.0	10.4	0.7	0.0	640	196	11
9	3	1463	2.4	1763	0	1763	25.8	1.2	0.0	8.5	0.3	0.0	582	188	11
9	4	1190	2.6	1479	0	1479	26.6	1.6	0.0	8.7	0.3	0.0	589	190	11
9	5	1314	2.5	1612	0	1612	26.2	1.5	0.0	8.6	0.3	0.0	589	189	11
9	6	785	3.2	1044	344	1388	28.3	2.4	1.1	9.4	0.4	1.9	470	172	10

(12) Suspended Solids Run-3 (Total) (3/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
9	7	701	3.4	952	308	1260	28.9	2.1	1.1	9.5	0.4	1.9	467	172	10
9	8	1045	3.1	1012	339	1351	27.9	1.4	1.1	9.2	0.3	1.9	454	170	10
9	9	2201	2.6	1116	394	1510	26.5	0.7	1.1	8.7	0.2	1.9	439	167	10
9	10	1998	3.5	497	159	656	29.3	1.9	1.1	9.7	0.3	1.9	465	170	10
9	11	3026	2.9	676	230	906	27.5	1.5	1.1	9.1	0.2	1.9	454	169	10
9	12	3675	2.6	797	0	797	26.7	1.3	0.0	8.8	0.2	0.0	584	187	11
10	1	2444	3.2	567	0	567	28.4	2.3	0.0	9.4	0.3	0.0	601	190	11
10	2	1723	3.7	499	0	499	29.7	3.2	0.0	9.8	0.4	0.0	616	191	11
10	3	1163	4.0	494	0	494	30.7	3.9	0.0	10.1	0.6	0.0	626	194	11
10	4	1187	3.1	923	0	923	28.1	2.3	0.0	9.3	0.5	0.0	601	193	11
10	5	1403	2.5	1582	0	1582	26.2	1.4	0.0	8.6	0.3	0.0	587	189	11
10	6	896	3.0	1179	397	1576	27.7	2.0	1.1	9.2	0.4	1.9	463	171	10
10	7	690	3.4	950	307	1256	29.0	2.1	1.1	9.6	0.4	1.9	467	172	10
10	8	914	3.2	960	316	1276	28.4	1.9	1.1	9.4	0.4	1.9	464	172	10
10	9	1009	3.2	948	314	1262	28.3	1.8	1.1	9.3	0.4	1.9	461	171	10
10	10	808	3.7	691	216	907	29.9	2.9	1.1	9.8	0.6	1.9	481	174	10
10	11	1644	2.2	1991	734	2725	25.4	1.1	1.1	8.3	0.2	1.9	442	167	9
10	12	1801	2.1	2161	0	2161	25.1	1.2	0.0	8.2	0.2	0.0	582	187	11
11	1	1262	2.5	1592	0	1592	26.3	1.7	0.0	8.7	0.3	0.0	592	189	11
11	2	1861	2.1	2228	0	2228	25.0	1.3	0.0	8.2	0.2	0.0	586	187	11
11	3	2536	1.8	2881	0	2881	23.7	1.1	0.0	7.8	0.2	0.0	582	187	11
11	4	1942	2.0	2317	0	2317	24.9	1.5	0.0	8.1	0.2	0.0	591	187	11
11	5	1299	2.5	1637	0	1637	26.2	2.2	0.0	8.6	0.3	0.0	603	189	11
11	6	661	3.5	929	298	1227	29.2	3.1	1.1	9.6	0.4	1.9	482	172	10
11	7	979	3.2	992	329	1320	28.2	2.1	1.1	9.3	0.4	1.9	465	171	10
11	8	300	6.5	263	68	331	36.4	2.9	1.1	12.0	0.6	1.9	491	176	10
11	9	1960	3.6	474	150	624	29.5	1.6	1.1	9.7	0.3	1.9	461	171	10
11	10	2754	3.1	629	211	840	27.9	1.3	1.1	9.2	0.3	1.9	453	169	10
11	11	3474	2.7	765	266	1031	26.9	1.4	1.1	8.9	0.2	1.9	451	168	10
11	12	3005	2.8	762	0	762	27.2	1.8	0.0	9.0	0.3	0.0	592	189	11
12	1	1498	3.7	519	0	519	29.9	3.3	0.0	9.8	0.5	0.0	618	193	11
12	2	865	4.2	505	0	505	31.1	4.2	0.0	10.2	0.7	0.0	630	196	11
12	3	1642	2.2	2018	0	2018	25.4	1.0	0.0	8.3	0.3	0.0	579	188	11
12	4	1715	2.2	2103	0	2103	25.3	1.2	0.0	8.3	0.2	0.0	582	187	11
12	5	1284	2.5	1640	0	1640	26.3	1.7	0.0	8.6	0.3	0.0	591	189	11
12	6	790	3.2	1090	360	1450	28.3	2.4	1.1	9.3	0.4	1.9	471	172	10
12	7	756	3.3	1052	345	1397	28.5	1.1	1.1	9.4	0.3	1.9	452	169	10
12	8	3032	2.4	1157	416	1573	26.0	0.8	1.1	8.6	0.2	1.9	440	166	9
12	9	1608	3.9	454	140	594	30.2	2.1	1.1	10.0	0.4	1.9	471	171	10
12	10	2081	3.5	500	160	660	29.2	2.0	1.1	9.6	0.3	1.9	466	170	10
12	11	3494	2.7	771	269	1040	26.9	1.4	1.1	8.8	0.2	1.9	452	168	10
12	12	3332	2.7	783	0	783	26.9	1.6	0.0	8.9	0.2	0.0	589	188	11
13	1	1970	3.5	546	0	546	29.1	2.9	0.0	9.6	0.4	0.0	612	191	11
13	2	1134	4.1	462	0	462	31.0	4.3	0.0	10.2	0.6	0.0	634	194	11
13	3	967	3.5	749	0	749	29.3	2.9	0.0	9.7	0.6	0.0	610	194	11
13	4	1184	2.6	1543	0	1543	26.6	1.4	0.0	8.7	0.3	0.0	586	190	11
13	5	850	3.1	1170	0	1170	28.0	1.9	0.0	9.2	0.4	0.0	594	192	11
13	6	1016	2.8	1361	468	1829	27.2	1.7	1.1	9.0	0.4	1.9	457	170	10

(12) Suspended Solids Run-3 (Total) (4/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
13	7	759	3.3	1067	350	1417	28.5	0.9	1.1	9.4	0.2	1.9	449	169	10
13	8	2182	3.0	807	273	1081	27.6	1.0	1.1	9.1	0.2	1.9	447	168	10
13	9	897	5.3	250	69	319	33.8	3.0	1.1	11.1	0.6	1.9	489	175	10
13	10	2103	3.5	506	162	668	29.2	1.5	1.1	9.6	0.3	1.9	460	170	10
13	11	3478	2.7	771	268	1040	26.9	1.2	1.1	8.9	0.2	1.9	449	168	10
13	12	3310	2.7	785	0	785	26.9	1.4	0.0	8.9	0.2	0.0	585	188	11
14	1	2033	3.4	556	0	556	29.0	2.4	0.0	9.6	0.4	0.0	601	190	11
14	2	1397	3.9	488	0	488	30.4	3.2	0.0	10.0	0.5	0.0	615	192	11
14	3	898	4.3	475	0	475	31.3	3.9	0.0	10.3	0.7	0.0	625	196	11
14	4	1154	2.8	1289	0	1289	27.2	1.5	0.0	9.0	0.4	0.0	587	191	11
14	5	1659	2.2	2089	0	2089	25.4	1.1	0.0	8.3	0.3	0.0	580	188	11
14	6	706	3.4	1014	328	1342	28.9	1.2	1.1	9.5	0.3	1.9	454	170	10
14	7	2601	2.5	1127	400	1527	26.4	0.9	1.1	8.7	0.2	1.9	443	167	9
14	8	2902	2.7	873	303	1176	26.9	1.1	1.1	8.9	0.2	1.9	447	168	10
14	9	626	6.4	188	48	236	36.2	4.1	1.1	11.9	0.7	1.9	505	177	10
14	10	2389	3.3	565	185	750	28.5	1.3	1.1	9.4	0.3	1.9	455	170	10
14	11	3449	2.7	769	267	1037	26.9	1.2	1.1	8.9	0.2	1.9	449	168	10
14	12	3114	2.8	771	0	771	27.1	1.6	0.0	8.9	0.3	0.0	589	189	11
15	1	1599	3.7	525	0	525	29.8	3.2	0.0	9.8	0.5	0.0	615	193	11
15	2	894	4.2	505	0	505	31.1	4.2	0.0	10.2	0.7	0.0	631	196	11
15	3	3813	1.5	4208	0	4208	22.1	0.5	0.0	7.3	0.1	0.0	568	187	11
15	4	1526	2.3	1963	0	1963	25.6	1.4	0.0	8.4	0.3	0.0	586	188	11
15	5	2156	1.9	2644	0	2644	24.4	1.1	0.0	8.0	0.2	0.0	583	187	11
15	6	1707	2.2	2168	803	2971	25.3	1.5	1.1	8.3	0.2	1.9	449	167	9
15	7	646	3.5	954	304	1258	29.3	3.2	1.1	9.7	0.5	1.9	484	173	10
15	8	138	7.7	269	65	334	38.6	2.6	1.1	12.8	0.6	1.9	491	177	10
15	9	850	5.5	241	66	307	34.2	2.1	1.1	11.3	0.6	1.9	479	175	10
15	10	770	5.8	223	60	283	34.9	1.9	1.1	11.5	0.6	1.9	477	176	10
15	11	2203	3.4	530	171	702	28.9	1.0	1.1	9.5	0.3	1.9	452	170	10
15	12	3588	2.7	799	0	799	26.7	0.9	0.0	8.8	0.2	0.0	575	188	11
16	1	2302	3.3	558	0	558	28.7	2.0	0.0	9.5	0.4	0.0	594	191	11
16	2	1324	4.0	476	0	476	30.6	3.2	0.0	10.1	0.6	0.0	615	193	11
16	3	1102	3.5	724	0	724	29.3	2.7	0.0	9.7	0.6	0.0	608	195	11
16	4	3584	1.5	4050	0	4050	22.3	0.5	0.0	7.4	0.1	0.0	569	187	11
16	5	6097	1.2	6384	0	6384	20.6	0.4	0.0	6.9	0.1	0.0	566	187	11
16	6	1072	2.7	1472	511	1983	27.0	2.2	1.1	8.9	0.4	1.9	464	170	10
16	7	744	3.3	1085	355	1440	28.6	1.1	1.1	9.4	0.2	1.9	452	169	10
16	8	2063	3.1	727	242	968	28.1	1.4	1.1	9.3	0.2	1.9	454	169	10
16	9	1672	3.9	424	130	555	30.4	2.5	1.1	10.0	0.4	1.9	476	171	10
16	10	1869	3.7	465	146	611	29.8	2.1	1.1	9.8	0.4	1.9	470	171	10
16	11	3411	2.7	768	266	1034	27.0	1.5	1.1	8.9	0.2	1.9	454	168	10
16	12	2978	2.8	766	0	766	27.2	1.9	0.0	9.0	0.3	0.0	595	189	11
17	1	1465	3.8	515	0	515	30.1	3.9	0.0	9.9	0.6	0.0	628	194	11
17	2	1086	3.6	711	0	711	29.4	3.5	0.0	9.7	0.6	0.0	622	194	11
17	3	4684	1.3	5131	0	5131	21.4	0.5	0.0	7.1	0.1	0.0	568	187	11
17	4	4386	1.4	4868	0	4868	21.6	0.6	0.0	7.2	0.1	0.0	572	187	11
17	5	759	3.3	1113	0	1113	28.5	1.1	0.0	9.4	0.2	0.0	577	187	11
17	6	1503	3.9	480	148	628	30.3	2.2	1.1	10.0	0.3	1.9	472	171	10

(12) Suspended Solids Run-3 (Total) (5/8)

					SS			Cu			Zn				
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
17	7	1378	4.3	362	108	470	31.4	2.7	1.1	10.3	0.4	1.9	481	173	10
17	8	1207	4.6	324	95	419	32.0	2.5	1.1	10.5	0.5	1.9	480	173	10
17	9	880	5.4	250	69	319	33.9	2.6	1.1	11.2	0.6	1.9	484	175	10
17	10	3567	2.7	800	280	1080	26.8	1.0	1.1	8.8	0.2	1.9	445	168	10
17	11	3418	2.7	776	269	1045	26.9	1.2	1.1	8.9	0.2	1.9	449	168	10
17	12	3397	2.7	796	0	796	26.9	1.3	0.0	8.9	0.2	0.0	583	188	11
18	1	2200	3.4	559	0	559	28.8	2.5	0.0	9.5	0.4	0.0	603	191	11
18	2	1345	4.0	480	0	480	30.6	3.7	0.0	10.1	0.6	0.0	624	193	11
18	3	1103	3.6	687	0	687	29.6	3.3	0.0	9.7	0.6	0.0	618	195	11
18	4	2411	1.8	2981	0	2981	23.9	0.8	0.0	7.8	0.2	0.0	575	187	11
18	5	1923	2.1	2484	0	2484	24.9	1.2	0.0	8.1	0.2	0.0	582	187	11
18	6	2269	1.9	2852	1104	3956	24.2	1.1	1.1	7.9	0.2	1.9	439	166	9
18	7	665	3.5	1010	324	1334	29.2	2.1	1.1	9.6	0.4	1.9	468	171	10
18	8	202	8.1	190	45	235	39.5	3.6	1.1	13.1	0.8	1.9	504	178	10
18	9	295	9.3	103	23	126	41.5	3.2	1.1	13.8	1.0	1.9	500	182	10
18	10	780	5.7	228	61	290	34.8	1.1	1.1	11.5	0.6	1.9	466	176	10
18	11	3433	2.7	778	270	1049	26.9	0.6	1.1	8.9	0.2	1.9	440	168	10
18	12	3434	2.7	787	0	787	26.9	1.0	0.0	8.9	0.2	0.0	576	188	11
19	1	1894	3.5	546	0	546	29.3	2.1	0.0	9.6	0.4	0.0	596	192	11
19	2	1023	4.3	457	0	457	31.3	3.4	0.0	10.3	0.7	0.0	617	195	11
19	3	1073	3.2	981	0	981	28.3	1.9	0.0	9.3	0.5	0.0	593	193	11
19	4	3632	1.5	4239	0	4239	22.2	0.5	0.0	7.4	0.1	0.0	568	187	11
19	5	805	3.2	1195	0	1195	28.2	2.1	0.0	9.3	0.4	0.0	597	192	11
19	6	596	3.7	932	293	1226	29.7	2.3	1.1	9.8	0.5	1.9	473	173	10
19	7	843	3.2	1110	366	1476	28.4	0.7	1.1	9.4	0.2	1.9	445	169	10
19	8	922	4.9	333	95	428	32.7	2.0	1.1	10.8	0.5	1.9	474	174	10
19	9	609	6.5	187	48	235	36.3	2.8	1.1	12.0	0.7	1.9	490	177	10
19	10	1137	4.8	311	90	401	32.4	1.5	1.1	10.7	0.5	1.9	466	174	10
19	11	3416	2.7	778	270	1048	26.9	0.9	1.1	8.9	0.2	1.9	443	168	10
19	12	3377	2.7	784	0	784	27.0	1.2	0.0	8.9	0.3	0.0	581	188	11
20	1	1864	3.5	560	0	560	29.3	1.9	0.0	9.6	0.4	0.0	592	190	11
20	2	1469	3.8	505	0	505	30.2	2.4	0.0	9.9	0.4	0.0	600	191	11
20	3	1256	3.9	521	0	521	30.5	2.6	0.0	10.0	0.5	0.0	604	193	11
20	4	1966	2.8	1025	0	1025	27.2	1.4	0.0	9.0	0.3	0.0	585	190	11
20	5	1905	2.8	1051	0	1051	27.1	1.5	0.0	8.9	0.3	0.0	587	190	11
20	6	1921	2.8	1053	363	1416	27.1	1.3	1.1	8.9	0.3	1.9	451	169	10
20	7	1651	3.3	734	240	974	28.6	1.1	1.1	9.4	0.2	1.9	452	169	10
20	8	785	5.7	231	62	293	34.7	3.2	1.1	11.4	0.6	1.9	493	176	10
20	9	884	5.4	254	70	324	33.9	2.2	1.1	11.2	0.6	1.9	479	175	10
20	10	820	5.6	240	65	305	34.4	1.9	1.1	11.3	0.6	1.9	476	176	10
20	11	3031	2.9	707	241	948	27.5	0.9	1.1	9.1	0.2	1.9	445	169	10
20	12	3453	2.7	789	0	789	26.9	1.2	0.0	8.9	0.2	0.0	580	188	11
21	1	1915	3.5	553	0	553	29.2	2.2	0.0	9.6	0.4	0.0	597	191	11
21	2	1176	4.1	476	0	476	31.0	3.2	0.0	10.2	0.6	0.0	614	193	11
21	3	929	3.9	640	0	640	30.3	3.0	0.0	10.0	0.7	0.0	611	196	11
21	4	1192	2.6	1693	0	1693	26.6	1.2	0.0	8.7	0.3	0.0	581	190	11
21	5	618	3.6	981	0	981	29.5	1.7	0.0	9.7	0.5	0.0	589	192	11
21	6	981	3.3	997	515	1512	28.5	1.3	1.8	9.4	0.3	2.9	407	163	9

(12) Suspended Solids Run-3 (Total) (6/8)

				SS			Cu			Zn					
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
21	7	1857	2.8	1107	602	1710	27.0	0.9	1.8	8.9	0.2	2.9	396	161	9
21	8	3553	2.4	1177	668	1845	25.9	0.8	1.8	8.5	0.2	2.9	391	159	9
21	9	2222	3.3	628	324	953	28.5	1.6	1.8	9.4	0.3	2.9	410	162	9
21	10	1942	3.6	490	244	734	29.6	2.1	1.8	9.7	0.4	2.9	420	164	9
21	11	604	6.5	188	76	263	36.4	3.8	1.8	12.0	0.7	2.9	457	171	9
21	12	2701	3.1	645	0	645	28.0	1.1	0.0	9.2	0.3	0.0	579	189	11
22	1	2318	3.3	568	0	568	28.7	1.8	0.0	9.5	0.4	0.0	592	190	11
22	2	1509	3.9	496	0	496	30.3	2.8	0.0	10.0	0.5	0.0	608	192	11
22	3	940	4.2	504	0	504	31.2	3.8	0.0	10.3	0.8	0.0	623	197	11
22	4	2511	1.8	3234	0	3234	23.7	0.6	0.0	7.8	0.2	0.0	571	187	11
22	5	2901	1.7	3646	0	3646	23.1	0.7	0.0	7.6	0.2	0.0	574	187	11
22	6	1346	2.5	1911	1078	2989	26.1	1.6	1.8	8.6	0.3	2.9	403	161	9
22	7	627	3.6	1008	503	1511	29.5	2.1	1.8	9.7	0.4	2.9	419	164	9
22	8	1449	2.9	1087	581	1668	27.5	1.2	1.8	9.1	0.3	2.9	402	162	9
22	9	1978	3.1	793	416	1209	28.0	1.2	1.8	9.3	0.2	2.9	403	162	9
22	10	1277	4.5	347	161	508	31.8	2.7	1.8	10.5	0.5	2.9	434	166	9
22	11	3348	2.8	776	422	1198	27.0	1.3	1.8	8.9	0.2	2.9	401	161	9
22	12	3471	2.7	800	0	800	26.9	1.4	0.0	8.9	0.2	0.0	585	188	11
23	1	2213	3.4	569	0	569	28.8	2.4	0.0	9.5	0.4	0.0	602	190	11
23	2	1530	3.9	498	0	498	30.2	3.4	0.0	9.9	0.5	0.0	619	192	11
23	3	909	4.4	477	0	477	31.5	4.6	0.0	10.4	0.8	0.0	637	197	11
23	4	1826	2.1	2518	0	2518	25.1	0.9	0.0	8.2	0.2	0.0	577	187	11
23	5	755	3.3	1188	0	1188	28.5	2.0	0.0	9.4	0.5	0.0	596	193	11
23	6	663	3.5	1068	538	1606	29.2	2.2	1.8	9.6	0.5	2.9	420	165	9
23	7	680	3.5	1093	554	1647	29.1	0.8	1.8	9.6	0.3	2.9	402	162	9
23	8	519	6.1	255	105	360	35.7	2.3	1.8	11.8	0.6	2.9	439	169	9
23	9	1726	3.9	449	218	667	30.2	1.4	1.8	9.9	0.4	2.9	414	164	9
23	10	724	6.0	220	92	312	35.3	2.3	1.8	11.6	0.7	2.9	438	169	9
23	11	3350	2.8	780	425	1205	27.0	0.9	1.8	8.9	0.2	2.9	395	161	9
23	12	3314	2.8	791	0	791	27.0	1.2	0.0	8.9	0.3	0.0	580	188	11
24	1	1876	3.6	550	0	550	29.4	2.4	0.0	9.7	0.4	0.0	601	192	11
24	2	1013	4.3	459	0	459	31.4	3.9	0.0	10.3	0.7	0.0	625	196	11
24	3	1445	2.7	1360	0	1360	26.9	1.6	0.0	8.9	0.4	0.0	590	192	11
24	4	2700	1.7	3527	0	3527	23.4	0.7	0.0	7.7	0.2	0.0	573	187	11
24	5	594	3.7	989	0	989	29.8	2.6	0.0	9.8	0.6	0.0	605	193	11
24	6	563	3.8	948	464	1412	30.1	2.2	1.8	9.9	0.5	2.9	423	166	9
24	7	783	3.4	1031	524	1555	29.0	1.3	1.8	9.5	0.4	2.9	408	164	9
24	8	518	5.3	392	172	563	33.6	1.5	1.8	11.1	0.5	2.9	425	166	9
24	9	985	5.1	283	125	408	33.2	2.0	1.8	10.9	0.6	2.9	429	167	9
24	10	2981	2.9	710	379	1089	27.5	1.0	1.8	9.1	0.3	2.9	399	162	9
24	11	3331	2.8	780	424	1204	27.1	1.1	1.8	8.9	0.2	2.9	399	161	9
24	12	3262	2.8	792	0	792	27.1	1.4	0.0	8.9	0.3	0.0	585	188	11
25	1	1872	3.6	550	0	550	29.4	2.7	0.0	9.7	0.5	0.0	608	192	11
25	2	999	4.4	459	0	459	31.5	4.3	0.0	10.4	0.7	0.0	632	196	11
25	3	1340	2.8	1285	0	1285	27.2	1.8	0.0	9.0	0.4	0.0	593	192	11
25	4	1751	2.2	2496	0	2496	25.2	1.1	0.0	8.2	0.2	0.0	580	188	11
25	5	865	3.1	1371	0	1371	27.9	2.1	0.0	9.2	0.4	0.0	597	192	11
25	6	567	3.8	967	474	1441	30.0	2.6	1.8	9.9	0.6	2.9	428	166	9

(12) Suspended Solids Run-3 (Total) (7/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
25	7	643	3.5	1075	539	1614	29.3	2.2	1.8	9.7	0.5	2.9	420	166	9
25	8	659	3.5	1100	554	1654	29.2	0.8	1.8	9.6	0.3	2.9	402	162	9
25	9	2811	2.6	1038	573	1610	26.7	0.7	1.8	8.8	0.2	2.9	392	160	9
25	10	1501	4.1	404	192	595	31.0	2.2	1.8	10.2	0.4	2.9	425	165	9
25	11	3322	2.8	782	425	1206	27.1	1.2	1.8	8.9	0.2	2.9	401	161	9
25	12	3308	2.8	793	0	793	27.0	1.5	0.0	8.9	0.3	0.0	587	188	11
26	1	1880	3.6	552	0	552	29.4	2.8	0.0	9.7	0.4	0.0	610	192	11
26	2	1031	4.3	463	0	463	31.4	4.4	0.0	10.3	0.7	0.0	635	196	11
26	3	1249	3.0	1160	0	1160	27.7	2.1	0.0	9.2	0.5	0.0	598	193	11
26	4	2434	1.8	3340	0	3340	23.9	0.8	0.0	7.8	0.2	0.0	575	187	11
26	5	2121	2.0	2996	0	2996	24.5	1.1	0.0	8.0	0.2	0.0	582	187	11
26	6	608	3.7	1040	516	1556	29.6	1.6	1.8	9.8	0.3	2.9	414	163	9
26	7	1322	3.6	696	349	1045	29.4	1.3	1.8	9.7	0.3	2.9	409	163	9
26	8	577	6.7	185	74	259	36.7	3.8	1.8	12.1	0.8	2.9	457	171	9
26	9	1121	4.8	317	144	461	32.4	1.8	1.8	10.7	0.5	2.9	425	167	9
26	10	1707	3.9	452	219	671	30.3	1.4	1.8	10.0	0.4	2.9	414	164	9
26	11	1792	3.8	470	230	700	30.0	1.5	1.8	9.9	0.4	2.9	414	164	9
26	12	3414	2.7	804	0	804	26.9	1.1	0.0	8.9	0.2	0.0	578	188	11
27	1	2205	3.4	568	0	568	28.9	2.1	0.0	9.5	0.4	0.0	596	191	11
27	2	1399	4.0	494	0	494	30.6	3.2	0.0	10.1	0.5	0.0	614	193	11
27	3	936	4.1	562	0	562	31.0	3.7	0.0	10.2	0.8	0.0	622	197	11
27	4	1685	2.2	2479	0	2479	25.3	0.9	0.0	8.3	0.3	0.0	577	188	11
27	5	1586	2.3	2363	0	2363	25.5	1.2	0.0	8.4	0.3	0.0	582	188	11
27	6	1300	2.5	1994	1119	3113	26.2	1.6	1.8	8.6	0.3	2.9	402	161	9
27	7	835	3.1	1376	721	2097	28.1	2.3	1.8	9.3	0.5	2.9	417	164	9
27	8	621	3.6	1078	537	1615	29.5	1.2	1.8	9.7	0.3	2.9	409	163	9
27	9	2486	2.6	1142	631	1773	26.6	0.7	1.8	8.8	0.2	2.9	392	160	9
27	10	1711	3.9	454	221	675	30.3	2.2	1.8	10.0	0.4	2.9	424	164	9
27	11	1447	4.2	395	187	582	31.1	2.3	1.8	10.2	0.4	2.9	428	165	9
27	12	3197	2.8	764	0	764	27.2	1.3	0.0	9.0	0.2	0.0	582	188	11
28	1	2245	3.4	569	0	569	28.8	2.3	0.0	9.5	0.4	0.0	601	191	11
28	2	1393	4.0	494	0	494	30.6	3.5	0.0	10.1	0.6	0.0	620	193	11
28	3	972	4.1	588	0	588	30.8	3.8	0.0	10.1	0.8	0.0	626	197	11
28	4	2804	1.7	3854	0	3854	23.3	0.6	0.0	7.6	0.2	0.0	571	187	11
28	5	1979	2.0	2912	0	2912	24.8	1.1	0.0	8.1	0.2	0.0	581	187	11
28	6	1437	2.4	2208	1258	3466	25.9	1.6	1.8	8.5	0.3	2.9	401	161	9
28	7	652	3.5	1137	572	1709	29.3	2.9	1.8	9.6	0.5	2.9	429	166	9
28	8	562	3.8	1010	495	1505	30.1	2.1	1.8	9.9	0.5	2.9	422	165	9
28	9	1063	3.3	1034	534	1568	28.5	1.4	1.8	9.4	0.3	2.9	407	163	9
28	10	1282	3.6	721	361	1083	29.4	2.0	1.8	9.7	0.4	2.9	418	164	9
28	11	1272	3.6	683	339	1022	29.6	2.5	1.8	9.8	0.5	2.9	426	166	9
28	12	985	3.7	730	0	730	29.9	3.2	0.0	9.8	0.7	0.0	615	196	11
29	1	1401	2.4	2185	0	2185	26.0	1.1	0.0	8.5	0.3	0.0	581	189	11
29	2	2197	1.9	3226	0	3226	24.3	0.9	0.0	8.0	0.2	0.0	578	187	11
29	3	2548	1.8	3643	0	3643	23.7	1.0	0.0	7.8	0.2	0.0	579	187	11
29	4	1700	2.2	2599	0	2599	25.3	1.5	0.0	8.3	0.3	0.0	591	188	11
29	5	1124	2.7	1824	0	1824	26.8	2.2	0.0	8.8	0.4	0.0	603	191	11
29	6	1259	2.5	2011	1124	3135	26.3	2.0	1.8	8.7	0.3	2.9	408	162	9

(12) Suspended Solids Run-3 (Total) (8/8)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
29	7	730	3.3	1275	653	1928	28.7	2.9	1.8	9.5	0.5	2.9	428	165	9
29	8	550	3.8	1012	493	1505	30.2	2.4	1.8	9.9	0.5	2.9	425	165	9
29	9	1081	3.2	1086	564	1650	28.3	1.0	1.8	9.3	0.2	2.9	402	162	9
29	10	2115	3.1	771	403	1174	28.1	1.6	1.8	9.3	0.3	2.9	409	163	9
29	11	2274	3.1	755	396	1152	28.0	1.7	1.8	9.3	0.3	2.9	410	162	9
29	12	2416	3.0	773	0	773	27.8	1.8	0.0	9.2	0.3	0.0	592	190	11
30	1	1472	3.8	539	0	539	30.2	3.2	0.0	9.9	0.5	0.0	615	193	11
30	2	767	4.7	443	0	443	32.3	4.9	0.0	10.6	0.9	0.0	641	198	11
30	3	1105	2.7	1804	0	1804	26.9	1.2	0.0	8.9	0.4	0.0	582	191	11
30	4	904	3.0	1544	0	1544	27.7	1.6	0.0	9.2	0.4	0.0	589	192	11
30	5	998	2.8	1680	0	1680	27.3	1.6	0.0	9.0	0.4	0.0	589	192	11
30	6	596	3.7	1095	542	1637	29.7	2.4	1.8	9.8	0.6	2.9	424	166	9
30	7	534	3.9	1003	486	1489	30.4	1.9	1.8	10.0	0.5	2.9	421	166	9
30	8	871	3.4	1058	538	1596	28.9	1.2	1.8	9.5	0.4	2.9	407	163	9
30	9	1957	2.8	1120	607	1727	27.2	0.6	1.8	9.0	0.2	2.9	392	160	9
30	10	1710	3.9	460	223	683	30.3	1.9	1.8	10.0	0.4	2.9	420	164	9
30	11	2770	3.0	686	362	1048	27.8	1.4	1.8	9.2	0.3	2.9	405	162	9
30	12	3364	2.8	808	0	808	27.0	1.3	0.0	8.9	0.2	0.0	583	188	11
31	1	2235	3.4	575	0	575	28.9	2.3	0.0	9.5	0.4	0.0	600	190	11
31	2	1541	3.9	507	0	507	30.3	3.2	0.0	10.0	0.5	0.0	615	192	11
31	3	972	4.3	496	0	496	31.4	4.1	0.0	10.3	0.8	0.0	629	197	11
31	4	1004	3.2	1157	0	1157	28.3	2.0	0.0	9.3	0.5	0.0	595	194	11
31	5	1160	2.6	1938	0	1938	26.7	1.3	0.0	8.8	0.4	0.0	584	191	11
31	6	676	3.5	1235	625	1860	29.1	2.1	1.8	9.6	0.5	2.9	419	166	9
31	7	522	3.9	1001	483	1485	30.5	2.0	1.8	10.0	0.6	2.9	422	166	9
31	8	745	3.6	1003	500	1504	29.5	1.8	1.8	9.7	0.5	2.9	417	166	9
31	9	849	3.5	990	498	1488	29.2	1.7	1.8	9.6	0.5	2.9	414	165	9
31	10	689	4.1	707	336	1044	30.9	2.9	1.8	10.2	0.7	2.9	434	169	9
31	11	1236	2.6	2072	1154	3226	26.4	1.1	1.8	8.7	0.3	2.9	397	162	9
31	12	1352	2.4	2247	0	2247	26.1	1.3	0.0	8.6	0.3	0.0	583	190	11

(13) Suspended Solids Case 2 (Soluble) (1/3)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
20	7	743	3.4	1031	334	1365	6.8	1.2	0.0	3.2	0.3	0.0	117	51	0
20	8	1445	3.2	829	273	1102	6.7	0.8	0.0	3.1	0.2	0.0	110	49	0
20	9	982	5.1	277	78	355	7.9	2.5	0.0	3.6	0.5	0.0	135	55	0
20	10	1530	4.1	402	122	524	7.3	1.7	0.0	3.4	0.4	0.0	125	52	0
20	11	2838	3.0	670	226	896	6.6	1.2	0.0	3.0	0.3	0.0	116	49	0
20	12	3475	2.7	795	0	795	6.4	1.3	0.0	2.9	0.2	0.0	157	66	0
21	1	2076	3.4	558	0	558	6.9	2.4	0.0	3.2	0.4	0.0	177	68	0
21	2	1267	4.1	480	0	480	7.3	3.5	0.0	3.4	0.6	0.0	195	71	0
21	3	979	3.8	642	0	642	7.1	3.3	0.0	3.3	0.7	0.0	191	73	0
21	4	1728	2.2	2311	0	2311	6.0	1.0	0.0	2.8	0.2	0.0	153	66	0
21	5	846	3.1	1262	0	1262	6.6	1.9	0.0	3.1	0.4	0.0	170	69	0
21	6	586	3.7	933	460	1393	7.1	2.3	0.0	3.3	0.5	0.0	117	47	0
21	7	735	3.4	1033	525	1559	6.8	1.2	0.0	3.2	0.3	0.0	102	45	0
21	8	1424	3.3	823	425	1248	6.7	0.8	0.0	3.1	0.2	0.0	97	43	0
21	9	977	5.1	278	123	400	7.9	2.5	0.0	3.6	0.6	0.0	120	49	0
21	10	1523	4.1	402	192	594	7.3	1.7	0.0	3.4	0.4	0.0	110	46	0
21	11	2825	3.0	671	355	1026	6.6	1.2	0.0	3.0	0.3	0.0	102	43	0
21	12	3459	2.7	796	0	796	6.4	1.3	0.0	2.9	0.2	0.0	157	66	0
22	1	2065	3.4	506	0	506	6.9	1.9	0.0	3.0	0.0	0.0	185	63	0
22	2	1258	4.1	436	0	436	7.3	2.2	0.0	3.2	0.0	0.0	189	63	0
22	3	976	3.8	588	0	588	7.1	1.4	0.0	3.1	0.0	0.0	174	63	0
22	4	1705	2.2	2103	0	2103	6.0	0.3	0.0	2.6	0.0	0.0	152	63	0
22	5	835	3.1	1146	0	1146	6.6	0.4	0.0	2.9	0.0	0.0	155	63	0
22	6	579	3.7	848	460	1308	7.1	0.4	0.0	3.1	0.0	0.0	99	41	0
22	7	727	3.4	939	525	1465	6.9	0.2	0.0	3.0	0.0	0.0	95	40	0
22	8	1401	3.3	740	420	1160	6.8	0.1	0.0	2.9	0.0	0.0	94	40	0
22	9	973	5.1	252	123	375	7.9	0.4	0.0	3.4	0.0	0.0	102	42	0
22	10	1517	4.1	365	192	556	7.3	0.2	0.0	3.2	0.0	0.0	98	41	0
22	11	2812	3.0	608	355	964	6.6	0.1	0.0	2.9	0.0	0.0	93	40	0
22	12	3444	2.7	722	0	722	6.4	0.1	0.0	2.8	0.0	0.0	148	63	0
23	1	2055	3.5	507	0	507	6.9	0.2	0.0	3.0	0.0	0.0	149	63	0
23	2	1249	4.1	436	0	436	7.3	0.3	0.0	3.2	0.0	0.0	151	63	0
23	3	973	3.8	593	0	593	7.1	0.2	0.0	3.1	0.0	0.0	149	63	0
23	4	1683	2.2	2106	0	2106	6.0	0.1	0.0	2.6	0.0	0.0	146	63	0
23	5	824	3.1	1149	0	1149	6.6	0.1	0.0	2.9	0.0	0.0	147	63	0
23	6	571	3.8	850	460	1310	7.1	0.1	0.0	3.1	0.0	0.0	96	41	0
23	7	719	3.5	942	526	1467	6.9	0.1	0.0	3.0	0.0	0.0	94	40	0
23	8	1380	3.3	734	416	1149	6.8	0.1	0.0	2.9	0.0	0.0	93	40	0
23	9	969	5.1	252	123	375	7.9	0.3	0.0	3.4	0.0	0.0	101	42	0
23	10	1510	4.1	365	192	557	7.3	0.2	0.0	3.2	0.0	0.0	98	41	0
23	11	2800	3.0	609	355	964	6.6	0.1	0.0	2.9	0.0	0.0	93	40	0
23	12	3428	2.7	723	0	723	6.4	0.1	0.0	2.8	0.0	0.0	147	63	0
24	1	2044	3.5	507	0	507	6.9	0.2	0.0	3.0	0.0	0.0	149	63	0
24	2	1240	4.1	436	0	436	7.3	0.3	0.0	3.2	0.0	0.0	150	63	0
24	3	969	3.8	598	0	598	7.1	0.2	0.0	3.1	0.0	0.0	149	63	0
24	4	1660	2.2	2110	0	2110	6.0	0.0	0.0	2.6	0.0	0.0	146	63	0
24	5	813	3.2	1151	0	1151	6.7	0.1	0.0	2.9	0.0	0.0	147	63	0
24	6	564	3.8	852	460	1312	7.1	0.1	0.0	3.1	0.0	0.0	96	41	0

(13) Suspended Solids Case 2 (Soluble) (2/3)

				SS			Cu			Zn					
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
24	7	710	3.5	944	526	1470	6.9	0.1	0.0	3.0	0.0	0.0	94	40	0
24	8	1359	3.3	728	411	1139	6.8	0.1	0.0	3.0	0.0	0.0	94	40	0
24	9	964	5.2	252	123	375	7.9	0.3	0.0	3.4	0.0	0.0	101	42	0
24	10	1503	4.1	365	192	557	7.3	0.2	0.0	3.2	0.0	0.0	98	41	0
24	11	2787	3.0	609	355	964	6.6	0.1	0.0	2.9	0.0	0.0	93	40	0
24	12	3413	2.7	723	0	723	6.4	0.1	0.0	2.8	0.0	0.0	147	63	0
25	1	2034	3.5	507	0	507	6.9	0.2	0.0	3.0	0.0	0.0	149	63	0
25	2	1231	4.1	436	0	436	7.3	0.3	0.0	3.2	0.0	0.0	150	63	0
25	3	966	3.8	604	0	604	7.1	0.2	0.0	3.1	0.0	0.0	149	63	0
25	4	1638	2.2	2114	0	2114	6.0	0.0	0.0	2.6	0.0	0.0	146	63	0
25	5	802	3.2	1154	0	1154	6.7	0.1	0.0	2.9	0.0	0.0	147	63	0
25	6	556	3.8	854	460	1315	7.1	0.1	0.0	3.1	0.0	0.0	96	41	0
25	7	702	3.5	946	526	1473	6.9	0.1	0.0	3.0	0.0	0.0	94	40	0
25	8	1338	3.4	723	407	1129	6.8	0.1	0.0	3.0	0.0	0.0	94	40	0
25	9	960	5.2	252	123	375	7.9	0.3	0.0	3.4	0.0	0.0	101	42	0
25	10	1496	4.1	366	192	557	7.3	0.2	0.0	3.2	0.0	0.0	98	41	0
25	11	2775	3.0	610	355	965	6.6	0.1	0.0	2.9	0.0	0.0	93	40	0
25	12	3398	2.7	724	0	724	6.4	0.1	0.0	2.8	0.0	0.0	147	63	0
26	1	2024	3.5	508	0	508	6.9	0.2	0.0	3.0	0.0	0.0	149	63	0
26	2	1222	4.1	436	0	436	7.3	0.3	0.0	3.2	0.0	0.0	150	63	0
26	3	963	3.8	609	0	609	7.1	0.2	0.0	3.1	0.0	0.0	149	63	0
26	4	1616	2.2	2118	0	2118	6.0	0.0	0.0	2.6	0.0	0.0	146	63	0
26	5	791	3.2	1157	0	1157	6.7	0.1	0.0	2.9	0.0	0.0	147	63	0
26	6	548	3.8	857	460	1317	7.1	0.1	0.0	3.1	0.0	0.0	96	41	0
26	7	694	3.5	949	526	1475	6.9	0.1	0.0	3.0	0.0	0.0	94	41	0
26	8	1317	3.4	717	403	1120	6.8	0.1	0.0	3.0	0.0	0.0	94	40	0
26	9	956	5.2	253	123	376	7.9	0.3	0.0	3.4	0.0	0.0	101	42	0
26	10	1490	4.2	366	192	557	7.3	0.2	0.0	3.2	0.0	0.0	98	41	0
26	11	2762	3.0	610	355	965	6.6	0.1	0.0	2.9	0.0	0.0	93	40	0
26	12	3382	2.8	724	0	724	6.4	0.1	0.0	2.8	0.0	0.0	147	63	0
27	1	2014	3.5	508	0	508	6.9	0.2	0.0	3.0	0.0	0.0	149	63	0
27	2	1214	4.1	436	0	436	7.3	0.3	0.0	3.2	0.0	0.0	150	63	0
27	3	959	3.8	615	0	615	7.1	0.2	0.0	3.1	0.0	0.0	149	63	0
27	4	1594	2.3	2122	0	2122	6.0	0.0	0.0	2.6	0.0	0.0	146	63	0
27	5	780	3.2	1159	0	1159	6.7	0.1	0.0	2.9	0.0	0.0	147	63	0
27	6	541	3.9	859	460	1319	7.2	0.1	0.0	3.1	0.0	0.0	96	41	0
27	7	685	3.5	951	527	1478	6.9	0.1	0.0	3.0	0.0	0.0	94	41	0
27	8	1297	3.4	712	398	1110	6.9	0.1	0.0	3.0	0.0	0.0	94	40	0
27	9	952	5.2	253	123	376	7.9	0.3	0.0	3.4	0.0	0.0	101	42	0
27	10	1483	4.2	366	192	558	7.3	0.2	0.0	3.2	0.0	0.0	98	41	0
27	11	2750	3.1	610	355	966	6.6	0.1	0.0	2.9	0.0	0.0	93	40	0
27	12	3367	2.8	725	0	725	6.4	0.1	0.0	2.8	0.0	0.0	147	63	0
28	1	2004	3.5	508	0	508	6.9	0.2	0.0	3.0	0.0	0.0	149	63	0
28	2	1205	4.1	437	0	437	7.3	0.3	0.0	3.2	0.0	0.0	150	63	0
28	3	956	3.8	621	0	621	7.1	0.2	0.0	3.1	0.0	0.0	149	63	0
28	4	1572	2.3	2126	0	2126	6.0	0.0	0.0	2.6	0.0	0.0	146	63	0
28	5	769	3.2	1162	0	1162	6.7	0.1	0.0	2.9	0.0	0.0	147	63	0
28	6	533	3.9	861	460	1322	7.2	0.1	0.0	3.1	0.0	0.0	96	41	0

(13) Suspended Solids Case 2 (Soluble) (3/3)

					SS			Cu			Zn				
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
28	7	677	3.6	954	527	1481	6.9	0.1	0.0	3.0	0.0	0.0	94	41	0
28	8	1278	3.5	707	394	1101	6.9	0.1	0.0	3.0	0.0	0.0	94	40	0
28	9	947	5.2	253	123	376	7.9	0.3	0.0	3.4	0.0	0.0	101	42	0
28	10	1476	4.2	366	192	558	7.3	0.2	0.0	3.2	0.0	0.0	98	41	0
28	11	2738	3.1	611	355	966	6.6	0.1	0.0	2.9	0.0	0.0	93	40	0
28	12	3352	2.8	725	0	725	6.4	0.1	0.0	2.8	0.0	0.0	147	63	0
29	1	1993	3.5	509	0	509	6.9	0.2	0.0	3.0	0.0	0.0	149	63	0
29	2	1196	4.2	437	0	437	7.3	0.3	0.0	3.2	0.0	0.0	150	63	0
29	3	952	3.8	627	0	627	7.1	0.2	0.0	3.1	0.0	0.0	149	63	0
29	4	1549	2.3	2130	0	2130	6.1	0.0	0.0	2.6	0.0	0.0	146	63	0
29	5	758	3.3	1165	0	1165	6.7	0.1	0.0	2.9	0.0	0.0	147	63	0
29	6	526	3.9	864	460	1324	7.2	0.1	0.0	3.1	0.0	0.0	96	41	0
29	7	669	3.6	957	527	1484	7.0	0.1	0.0	3.0	0.0	0.0	94	41	0
29	8	1259	3.5	702	390	1092	6.9	0.1	0.0	3.0	0.0	0.0	94	40	0
29	9	943	5.2	253	123	376	7.9	0.3	0.0	3.4	0.0	0.0	101	42	0
29	10	1469	4.2	367	192	558	7.3	0.2	0.0	3.2	0.0	0.0	98	41	0
29	11	2725	3.1	611	355	967	6.6	0.1	0.0	2.9	0.0	0.0	93	40	0
29	12	3336	2.8	726	0	726	6.4	0.1	0.0	2.8	0.0	0.0	147	63	0
30	1	1983	3.5	509	0	509	6.9	0.2	0.0	3.0	0.0	0.0	149	63	0
30	2	1187	4.2	437	0	437	7.3	0.3	0.0	3.2	0.0	0.0	150	63	0
30	3	948	3.8	633	0	633	7.1	0.2	0.0	3.1	0.0	0.0	149	63	0
30	4	1527	2.3	2134	0	2134	6.1	0.0	0.0	2.6	0.0	0.0	146	63	0
30	5	747	3.3	1168	0	1168	6.8	0.1	0.0	2.9	0.0	0.0	147	63	0
30	6	518	4.0	866	460	1326	7.2	0.1	0.0	3.1	0.0	0.0	96	41	0
30	7	660	3.6	959	527	1487	7.0	0.1	0.0	3.0	0.0	0.0	94	41	0
30	8	1240	3.5	697	386	1083	6.9	0.1	0.0	3.0	0.0	0.0	94	41	0
30	9	939	5.2	254	123	376	7.9	0.3	0.0	3.4	0.0	0.0	101	42	0
30	10	1463	4.2	367	192	558	7.4	0.2	0.0	3.2	0.0	0.0	98	41	0
30	11	2713	3.1	612	355	967	6.6	0.1	0.0	2.9	0.0	0.0	93	40	0
30	12	3321	2.8	726	0	726	6.4	0.1	0.0	2.8	0.0	0.0	147	63	0
31	1	1973	3.5	510	0	510	6.9	0.2	0.0	3.0	0.0	0.0	149	63	0
31	2	1178	4.2	437	0	437	7.4	0.3	0.0	3.2	0.0	0.0	150	63	0
31	3	945	3.8	639	0	639	7.1	0.2	0.0	3.1	0.0	0.0	149	63	0
31	4	1505	2.3	2138	0	2138	6.1	0.0	0.0	2.6	0.0	0.0	146	63	0
31	5	736	3.3	1171	0	1171	6.8	0.1	0.0	2.9	0.0	0.0	147	63	0
31	6	511	4.0	869	460	1329	7.2	0.1	0.0	3.1	0.0	0.0	96	41	0
31	7	652	3.6	962	528	1490	7.0	0.1	0.0	3.0	0.0	0.0	95	41	0
31	8	1222	3.6	692	383	1074	6.9	0.1	0.0	3.0	0.0	0.0	94	41	0
31	9	934	5.2	254	123	377	7.9	0.3	0.0	3.4	0.0	0.0	101	42	0
31	10	1456	4.2	367	192	559	7.4	0.2	0.0	3.2	0.0	0.0	98	41	0
31	11	2700	3.1	612	355	968	6.6	0.1	0.0	2.9	0.0	0.0	93	40	0
31	12	3306	2.8	727	0	727	6.4	0.1	0.0	2.8	0.0	0.0	147	63	0

(14) Suspended Solids Case 2 (Total) (1/3)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
20	7	743	3.4	1031	334	1365	28.9	1.2	1.1	9.5	0.3	1.9	454	170	10
20	8	1445	3.2	829	273	1102	28.4	0.8	1.1	9.4	0.2	1.9	447	169	10
20	9	982	5.1	277	78	355	33.2	2.5	1.1	10.9	0.5	1.9	481	174	10
20	10	1530	4.1	402	122	524	30.9	1.7	1.1	10.2	0.4	1.9	467	172	10
20	11	2838	3.0	670	226	896	27.7	1.2	1.1	9.2	0.3	1.9	451	169	10
20	12	3475	2.7	795	0	795	26.9	1.3	0.0	8.9	0.2	0.0	582	188	11
21	1	2076	3.4	558	0	558	29.0	2.4	0.0	9.6	0.4	0.0	601	191	11
21	2	1267	4.1	480	0	480	30.8	3.5	0.0	10.1	0.6	0.0	620	193	11
21	3	979	3.8	642	0	642	30.2	3.3	0.0	9.9	0.7	0.0	616	196	11
21	4	1728	2.2	2311	0	2311	25.2	1.0	0.0	8.3	0.2	0.0	578	188	11
21	5	846	3.1	1262	0	1262	28.0	1.9	0.0	9.2	0.4	0.0	594	192	11
21	6	586	3.7	933	460	1393	29.8	2.3	1.8	9.8	0.5	2.9	424	166	9
21	7	735	3.4	1033	525	1559	28.9	1.2	1.8	9.5	0.3	2.9	407	163	9
21	8	1424	3.3	823	425	1248	28.5	0.8	1.8	9.4	0.2	2.9	400	162	9
21	9	977	5.1	278	123	400	33.2	2.5	1.8	10.9	0.6	2.9	435	167	9
21	10	1523	4.1	402	192	594	30.9	1.7	1.8	10.2	0.4	2.9	420	165	9
21	11	2825	3.0	671	355	1026	27.8	1.2	1.8	9.2	0.3	2.9	403	162	9
21	12	3459	2.7	796	0	796	26.9	1.3	0.0	8.9	0.2	0.0	582	188	11
22	1	2065	3.4	506	0	506	27.9	1.9	0.0	5.7	0.0	0.0	630	120	1
22	2	1258	4.1	436	0	436	29.6	2.2	0.0	6.0	0.0	0.0	634	120	1
22	3	976	3.8	588	0	588	29.0	1.4	0.0	5.9	0.0	0.0	619	120	1
22	4	1705	2.2	2103	0	2103	24.3	0.3	0.0	4.9	0.0	0.0	597	120	1
22	5	835	3.1	1146	0	1146	27.0	0.4	0.0	5.5	0.0	0.0	600	120	1
22	6	579	3.7	848	460	1308	28.8	0.4	1.8	5.9	0.0	2.9	412	117	2
22	7	727	3.4	939	525	1465	27.9	0.2	1.8	5.7	0.0	2.9	405	117	2
22	8	1401	3.3	740	420	1160	27.5	0.1	1.8	5.6	0.0	2.9	403	117	2
22	9	973	5.1	252	123	375	32.0	0.4	1.8	6.5	0.0	2.9	424	117	2
22	10	1517	4.1	365	192	556	29.7	0.2	1.8	6.1	0.0	2.9	413	117	2
22	11	2812	3.0	608	355	964	26.7	0.1	1.8	5.4	0.0	2.9	399	117	2
22	12	3444	2.7	722	0	722	25.9	0.1	0.0	5.3	0.0	0.0	593	120	1
23	1	2055	3.5	507	0	507	28.0	0.2	0.0	5.7	0.0	0.0	594	120	1
23	2	1249	4.1	436	0	436	29.7	0.3	0.0	6.0	0.0	0.0	596	120	1
23	3	973	3.8	593	0	593	29.0	0.2	0.0	5.9	0.0	0.0	594	120	1
23	4	1683	2.2	2106	0	2106	24.4	0.1	0.0	5.0	0.0	0.0	591	120	1
23	5	824	3.1	1149	0	1149	27.0	0.1	0.0	5.5	0.0	0.0	592	120	1
23	6	571	3.8	850	460	1310	28.8	0.1	1.8	5.9	0.0	2.9	408	117	2
23	7	719	3.5	942	526	1467	28.0	0.1	1.8	5.7	0.0	2.9	404	117	2
23	8	1380	3.3	734	416	1149	27.6	0.1	1.8	5.6	0.0	2.9	402	117	2
23	9	969	5.1	252	123	375	32.0	0.3	1.8	6.5	0.0	2.9	422	117	2
23	10	1510	4.1	365	192	557	29.8	0.2	1.8	6.1	0.0	2.9	413	117	2
23	11	2800	3.0	609	355	964	26.7	0.1	1.8	5.4	0.0	2.9	399	117	2
23	12	3428	2.7	723	0	723	25.9	0.1	0.0	5.3	0.0	0.0	592	120	1
24	1	2044	3.5	507	0	507	28.0	0.2	0.0	5.7	0.0	0.0	594	120	1
24	2	1240	4.1	436	0	436	29.7	0.3	0.0	6.0	0.0	0.0	595	120	1
24	3	969	3.8	598	0	598	29.0	0.2	0.0	5.9	0.0	0.0	594	120	1
24	4	1660	2.2	2110	0	2110	24.4	0.0	0.0	5.0	0.0	0.0	591	120	1
24	5	813	3.2	1151	0	1151	27.1	0.1	0.0	5.5	0.0	0.0	592	120	1
24	6	564	3.8	852	460	1312	28.9	0.1	1.8	5.9	0.0	2.9	409	117	2

(14) Suspended Solids Case 2 (Total) (2/3)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
24	7	710	3.5	944	526	1470	28.0	0.1	1.8	5.7	0.0	2.9	404	117	2
24	8	1359	3.3	728	411	1139	27.6	0.1	1.8	5.6	0.0	2.9	402	117	2
24	9	964	5.2	252	123	375	32.1	0.3	1.8	6.5	0.0	2.9	422	117	2
24	10	1503	4.1	365	192	557	29.8	0.2	1.8	6.1	0.0	2.9	413	117	2
24	11	2787	3.0	609	355	964	26.8	0.1	1.8	5.4	0.0	2.9	399	117	2
24	12	3413	2.7	723	0	723	25.9	0.1	0.0	5.3	0.0	0.0	592	120	1
25	1	2034	3.5	507	0	507	28.0	0.2	0.0	5.7	0.0	0.0	594	120	1
25	2	1231	4.1	436	0	436	29.7	0.3	0.0	6.0	0.0	0.0	595	120	1
25	3	966	3.8	604	0	604	29.0	0.2	0.0	5.9	0.0	0.0	594	120	1
25	4	1638	2.2	2114	0	2114	24.5	0.0	0.0	5.0	0.0	0.0	591	120	1
25	5	802	3.2	1154	0	1154	27.2	0.1	0.0	5.5	0.0	0.0	592	120	1
25	6	556	3.8	854	460	1315	29.0	0.1	1.8	5.9	0.0	2.9	409	117	2
25	7	702	3.5	946	526	1473	28.1	0.1	1.8	5.7	0.0	2.9	404	117	2
25	8	1338	3.4	723	407	1129	27.7	0.1	1.8	5.6	0.0	2.9	403	117	2
25	9	960	5.2	252	123	375	32.1	0.3	1.8	6.5	0.0	2.9	422	117	2
25	10	1496	4.1	366	192	557	29.8	0.2	1.8	6.1	0.0	2.9	413	117	2
25	11	2775	3.0	610	355	965	26.8	0.1	1.8	5.4	0.0	2.9	399	117	2
25	12	3398	2.7	724	0	724	25.9	0.1	0.0	5.3	0.0	0.0	592	120	1
26	1	2024	3.5	508	0	508	28.0	0.2	0.0	5.7	0.0	0.0	594	120	1
26	2	1222	4.1	436	0	436	29.8	0.3	0.0	6.1	0.0	0.0	595	120	1
26	3	963	3.8	609	0	609	29.1	0.2	0.0	5.9	0.0	0.0	594	120	1
26	4	1616	2.2	2118	0	2118	24.5	0.0	0.0	5.0	0.0	0.0	591	120	1
26	5	791	3.2	1157	0	1157	27.2	0.1	0.0	5.5	0.0	0.0	592	120	1
26	6	548	3.8	857	460	1317	29.1	0.1	1.8	5.9	0.0	2.9	409	117	2
26	7	694	3.5	949	526	1475	28.1	0.1	1.8	5.7	0.0	2.9	405	117	2
26	8	1317	3.4	717	403	1120	27.8	0.1	1.8	5.7	0.0	2.9	403	117	2
26	9	956	5.2	253	123	376	32.1	0.3	1.8	6.5	0.0	2.9	423	117	2
26	10	1490	4.2	366	192	557	29.8	0.2	1.8	6.1	0.0	2.9	413	117	2
26	11	2762	3.0	610	355	965	26.8	0.1	1.8	5.4	0.0	2.9	399	117	2
26	12	3382	2.8	724	0	724	26.0	0.1	0.0	5.3	0.0	0.0	592	120	1
27	1	2014	3.5	508	0	508	28.1	0.2	0.0	5.7	0.0	0.0	594	120	1
27	2	1214	4.1	436	0	436	29.8	0.3	0.0	6.1	0.0	0.0	595	120	1
27	3	959	3.8	615	0	615	29.1	0.2	0.0	5.9	0.0	0.0	594	120	1
27	4	1594	2.3	2122	0	2122	24.5	0.0	0.0	5.0	0.0	0.0	591	120	1
27	5	780	3.2	1159	0	1159	27.3	0.1	0.0	5.6	0.0	0.0	592	120	1
27	6	541	3.9	859	460	1319	29.1	0.1	1.8	5.9	0.0	2.9	409	117	2
27	7	685	3.5	951	527	1478	28.2	0.1	1.8	5.7	0.0	2.9	405	117	2
27	8	1297	3.4	712	398	1110	27.9	0.1	1.8	5.7	0.0	2.9	404	117	2
27	9	952	5.2	253	123	376	32.1	0.3	1.8	6.5	0.0	2.9	423	117	2
27	10	1483	4.2	366	192	558	29.8	0.2	1.8	6.1	0.0	2.9	413	117	2
27	11	2750	3.1	610	355	966	26.8	0.1	1.8	5.5	0.0	2.9	400	117	2
27	12	3367	2.8	725	0	725	26.0	0.1	0.0	5.3	0.0	0.0	592	120	1
28	1	2004	3.5	508	0	508	28.1	0.2	0.0	5.7	0.0	0.0	594	120	1
28	2	1205	4.1	437	0	437	29.8	0.3	0.0	6.1	0.0	0.0	595	120	1
28	3	956	3.8	621	0	621	29.1	0.2	0.0	5.9	0.0	0.0	594	120	1
28	4	1572	2.3	2126	0	2126	24.6	0.0	0.0	5.0	0.0	0.0	591	120	1
28	5	769	3.2	1162	0	1162	27.4	0.1	0.0	5.6	0.0	0.0	592	120	1
28	6	533	3.9	861	460	1322	29.2	0.1	1.8	5.9	0.0	2.9	410	117	2

(14) Suspended Solids Case 2 (Total) (3/3)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
28	7	677	3.6	954	527	1481	28.3	0.1	1.8	5.7	0.0	2.9	405	117	2
28	8	1278	3.5	707	394	1101	28.0	0.1	1.8	5.7	0.0	2.9	404	117	2
28	9	947	5.2	253	123	376	32.2	0.3	1.8	6.5	0.0	2.9	423	117	2
28	10	1476	4.2	336	192	558	29.9	0.2	1.8	6.1	0.0	2.9	413	117	2
28	11	2738	3.1	611	355	966	26.8	0.1	1.8	5.5	0.0	2.9	400	117	2
28	12	3352	2.8	725	0	725	26.0	0.1	0.0	5.3	0.0	0.0	592	120	1
29	1	1993	3.5	509	0	509	28.1	0.2	0.0	5.7	0.0	0.0	594	120	1
29	2	1196	4.2	437	0	437	29.9	0.3	0.0	6.1	0.0	0.0	595	120	1
29	3	952	3.8	627	0	627	29.1	0.2	0.0	5.9	0.0	0.0	594	120	1
29	4	1549	2.3	2130	0	2130	24.6	0.0	0.0	5.0	0.0	0.0	591	120	1
29	5	758	3.3	1165	0	1165	27.4	0.1	0.0	5.6	0.0	0.0	592	120	1
29	6	526	3.9	864	460	1324	29.3	0.1	1.8	6.0	0.0	2.9	410	117	2
29	7	669	3.6	957	527	1484	28.3	0.1	1.8	5.8	0.0	2.9	405	117	2
29	8	1259	3.5	702	390	1092	28.1	0.1	1.8	5.7	0.0	2.9	404	117	2
29	9	943	5.2	253	123	376	32.2	0.3	1.8	6.6	0.0	2.9	423	117	2
29	10	1469	4.2	367	192	558	29.9	0.2	1.8	6.1	0.0	2.9	413	117	2
29	11	2725	3.1	611	355	967	26.9	0.1	1.8	5.5	0.0	2.9	400	117	2
29	12	3336	2.8	726	0	726	26.0	0.1	0.0	5.3	0.0	0.0	592	120	1
30	1	1983	3.5	509	0	509	28.1	0.2	0.0	5.7	0.0	0.0	594	120	1
30	2	1187	4.2	437	0	437	29.9	0.3	0.0	6.1	0.0	0.0	595	120	1
30	3	948	3.8	633	0	633	29.1	0.2	0.0	5.9	0.0	0.0	594	120	1
30	4	1527	2.3	2134	0	2134	24.7	0.0	0.0	5.0	0.0	0.0	591	120	1
30	5	747	3.3	1168	0	1168	27.5	0.1	0.0	5.6	0.0	0.0	592	120	1
30	6	518	4.0	866	460	1326	29.4	0.1	1.8	6.0	0.0	2.9	410	117	2
30	7	660	3.6	959	527	1487	28.4	0.1	1.8	5.8	0.0	2.9	406	117	2
30	8	1240	3.5	697	386	1083	28.1	0.1	1.8	5.7	0.0	2.9	405	117	2
30	9	939	5.2	254	123	376	32.2	0.3	1.8	6.6	0.0	2.9	423	117	2
30	10	1463	4.2	367	192	558	29.9	0.2	1.8	6.1	0.0	2.9	413	117	2
30	11	2713	3.1	612	355	967	26.9	0.1	1.8	5.5	0.0	2.9	400	117	2
30	12	3321	2.8	726	0	726	26.0	0.1	0.0	5.3	0.0	0.0	592	120	1
31	1	1973	3.5	510	0	510	28.2	0.2	0.0	5.7	0.0	0.0	594	120	1
31	2	1178	4.2	437	0	437	29.9	0.3	0.0	6.1	0.0	0.0	595	120	1
31	3	945	3.8	639	0	639	29.1	0.2	0.0	5.9	0.0	0.0	594	120	1
31	4	1505	2.3	2138	0	2138	24.7	0.0	0.0	5.0	0.0	0.0	591	120	1
31	5	736	3.3	1171	0	1171	27.6	0.1	0.0	5.6	0.0	0.0	592	120	1
31	6	511	4.0	869	460	1329	29.5	0.1	1.8	6.0	0.0	2.9	411	117	2
31	7	652	3.6	962	528	1490	28.5	0.1	1.8	5.8	0.0	2.9	406	117	2
31	8	1222	3.6	692	383	1074	28.2	0.1	1.8	5.7	0.0	2.9	405	117	2
31	9	934	5.2	254	123	377	32.3	0.3	1.8	6.6	0.0	2.9	423	117	2
31	10	1456	4.2	367	192	559	29.9	0.2	1.8	6.1	0.0	2.9	413	117	2
31	11	2700	3.1	612	355	968	26.9	0.1	1.8	5.5	0.0	2.9	400	117	2
31	12	3306	2.8	727	0	727	26.1	0.1	0.0	5.3	0.0	0.0	592	120	1

(15) Suspended Solids Case-3 (Soluble) (1/3)

Y	M	TR	DO	SS			Cu			Zn			Cu	Zn	As
				MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT			
20	7	743	3.4	1031	334	1365	6.8	1.2	0.0	3.2	0.3	0.0	117	51	0
20	8	1445	3.2	829	273	1102	6.7	0.8	0.0	3.1	0.2	0.0	110	49	0
20	9	982	5.1	277	78	355	7.9	2.5	0.0	3.6	0.5	0.0	135	55	0
20	10	1530	4.1	402	122	524	7.3	1.7	0.0	3.4	0.4	0.0	125	52	0
20	11	2838	3.0	670	226	896	6.6	1.2	0.0	3.0	0.3	0.0	116	49	0
20	12	3475	2.7	795	0	795	6.4	1.3	0.0	2.9	0.2	0.0	157	66	0
21	1	2076	3.4	558	0	558	6.9	2.4	0.0	3.2	0.4	0.0	177	68	0
21	2	1267	4.1	480	0	480	7.3	3.5	0.0	3.4	0.6	0.0	195	71	0
21	3	979	3.8	642	0	642	7.1	3.3	0.0	3.3	0.7	0.0	191	73	0
21	4	1728	2.2	2311	0	2311	6.0	1.0	0.0	2.8	0.2	0.0	153	66	0
21	5	846	3.1	1262	0	1262	6.6	1.9	0.0	3.1	0.4	0.0	170	69	0
21	6	586	3.7	933	460	1393	7.1	2.3	0.0	3.3	0.5	0.0	117	47	0
21	7	735	3.4	1033	525	1559	6.8	1.2	0.0	3.2	0.3	0.0	102	45	0
21	8	1424	3.3	823	425	1248	6.7	0.8	0.0	3.1	0.2	0.0	97	43	0
21	9	977	5.1	278	123	400	7.9	2.5	0.0	3.6	0.6	0.0	120	49	0
21	10	1523	4.1	402	192	594	7.3	1.7	0.0	3.4	0.4	0.0	110	46	0
21	11	2825	3.0	671	355	1026	6.6	1.2	0.0	3.0	0.3	0.0	102	43	0
21	12	3459	2.7	796	0	796	6.4	1.3	0.0	2.9	0.2	0.0	157	66	0
22	1	2065	3.4	52	0	52	0.0	2.4	0.0	0.2	0.4	0.0	483	121	0
22	2	1258	4.1	45	0	45	0.0	3.5	0.0	0.2	0.6	0.0	678	151	0
22	3	976	3.8	60	0	60	0.0	3.2	0.0	0.2	0.7	0.0	631	175	0
22	4	1708	2.2	213	0	213	0.0	0.9	0.0	0.2	0.2	0.0	227	99	0
22	5	837	3.1	119	0	119	0.0	1.9	0.0	0.2	0.4	0.0	396	132	0
22	6	581	3.7	87	460	547	0.0	2.2	0.0	0.2	0.5	0.0	71	23	0
22	7	730	3.4	97	525	622	0.0	1.2	0.0	0.2	0.3	0.0	37	17	0
22	8	1407	3.3	77	421	498	0.0	0.8	0.0	0.2	0.2	0.0	24	13	0
22	9	975	5.1	26	123	149	0.0	2.3	0.0	0.2	0.6	0.0	73	24	0
22	10	1519	4.1	37	192	229	0.0	1.7	0.0	0.2	0.4	0.0	52	20	0
22	11	2818	3.0	63	355	418	0.0	1.1	0.0	0.2	0.3	0.0	37	14	0
22	12	3452	2.7	74	0	74	0.0	1.2	0.0	0.2	0.2	0.0	269	92	0
23	1	2061	3.5	52	0	52	0.0	2.3	0.0	0.2	0.4	0.0	465	121	0
23	2	1255	4.1	45	0	45	0.0	3.4	0.0	0.2	0.6	0.0	660	151	0
23	3	974	3.8	61	0	61	0.0	3.1	0.0	0.2	0.7	0.0	618	175	0
23	4	1699	2.2	213	0	213	0.0	0.9	0.0	0.2	0.3	0.0	225	99	0
23	5	832	3.1	119	0	119	0.0	1.9	0.0	0.2	0.4	0.0	393	132	0
23	6	578	3.7	87	460	547	0.0	2.2	0.0	0.2	0.5	0.0	71	23	0
23	7	726	3.4	97	525	622	0.0	1.1	0.0	0.2	0.3	0.0	37	17	0
23	8	1398	3.3	76	419	495	0.0	0.8	0.0	0.2	0.2	0.0	24	13	0
23	9	973	5.1	26	123	149	0.0	2.3	0.0	0.2	0.6	0.0	73	24	0
23	10	1516	4.1	37	192	229	0.0	1.6	0.0	0.2	0.4	0.0	52	20	0
23	11	2813	3.0	63	355	418	0.0	1.1	0.0	0.2	0.3	0.0	37	14	0
23	12	3446	2.7	74	0	74	0.0	1.2	0.0	0.2	0.2	0.0	268	92	0
24	1	2056	3.5	52	0	52	0.0	2.3	0.0	0.2	0.4	0.0	465	121	0
24	2	1251	4.1	45	0	45	0.0	3.4	0.0	0.2	0.6	0.0	660	151	0
24	3	973	3.8	61	0	61	0.0	3.1	0.0	0.2	0.7	0.0	616	176	0
24	4	1690	2.2	213	0	213	0.0	0.9	0.0	0.2	0.3	0.0	225	100	0
24	5	828	3.1	119	0	119	0.0	1.9	0.0	0.2	0.4	0.0	393	133	0
24	6	575	3.8	87	460	548	0.0	2.2	0.0	0.2	0.5	0.0	71	23	0

(15) Suspended Solids Case-3 (Soluble) (2/3)

				SS			Cu			Zn					
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
24	7	723	3.4	97	526	623	0.0	1.1	0.0	0.2	0.3	0.0	37	17	0
24	8	1389	3.3	76	417	493	0.0	0.8	0.0	0.2	0.2	0.0	24	13	0
24	9	971	5.1	26	123	149	0.0	2.3	0.0	0.2	0.6	0.0	73	24	0
24	10	1514	4.1	37	192	229	0.0	1.6	0.0	0.2	0.4	0.0	52	20	0
24	11	2808	3.0	63	355	418	0.0	1.1	0.0	0.2	0.3	0.0	37	14	0
24	12	3439	2.7	74	0	74	0.0	1.2	0.0	0.2	0.2	0.0	268	92	0
25	1	2052	3.5	52	0	52	0.0	2.3	0.0	0.2	0.4	0.0	465	121	0
25	2	1247	4.1	45	0	45	0.0	3.4	0.0	0.2	0.6	0.0	660	152	0
25	3	972	3.8	61	0	61	0.0	3.1	0.0	0.2	0.7	0.0	615	176	0
25	4	1681	2.2	213	0	213	0.0	0.9	0.0	0.2	0.3	0.0	225	100	0
25	5	824	3.1	119	0	119	0.0	1.9	0.0	0.2	0.4	0.0	394	133	0
25	6	572	3.8	87	460	548	0.0	2.2	0.0	0.2	0.5	0.0	71	23	0
25	7	720	3.5	97	526	623	0.0	1.1	0.0	0.2	0.3	0.0	36	17	0
25	8	1380	3.3	76	415	491	0.0	0.8	0.0	0.2	0.2	0.0	24	14	0
25	9	969	5.1	26	123	149	0.0	2.3	0.0	0.2	0.6	0.0	72	24	0
25	10	1511	4.1	37	192	229	0.0	1.6	0.0	0.2	0.4	0.0	52	20	0
25	11	2803	3.0	63	355	418	0.0	1.1	0.0	0.2	0.3	0.0	37	14	0
25	12	3433	2.7	74	0	74	0.0	1.2	0.0	0.2	0.2	0.0	268	92	0
26	1	2048	3.5	52	0	52	0.0	2.3	0.0	0.2	0.4	0.0	465	122	0
26	2	1244	4.1	45	0	45	0.0	3.4	0.0	0.2	0.6	0.0	661	152	0
26	3	970	3.8	61	0	61	0.0	3.1	0.0	0.2	0.7	0.0	614	176	0
26	4	1672	2.2	214	0	214	0.0	0.9	0.0	0.2	0.3	0.0	226	100	0
26	5	819	3.1	119	0	119	0.0	1.9	0.0	0.2	0.4	0.0	394	133	0
26	6	568	3.8	87	460	548	0.0	2.2	0.0	0.2	0.5	0.0	71	23	0
26	7	716	3.5	97	526	623	0.0	1.1	0.0	0.2	0.3	0.0	36	17	0
26	8	1371	3.3	76	414	489	0.0	0.8	0.0	0.2	0.2	0.0	24	14	0
26	9	968	5.1	26	123	149	0.0	2.3	0.0	0.2	0.6	0.0	72	24	0
26	10	1508	4.1	37	192	229	0.0	1.6	0.0	0.2	0.4	0.0	52	20	0
26	11	2798	3.0	63	355	419	0.0	1.1	0.0	0.2	0.3	0.0	37	14	0
26	12	3427	2.7	74	0	74	0.0	1.2	0.0	0.2	0.2	0.0	268	92	0
27	1	2044	3.5	52	0	52	0.0	2.3	0.0	0.2	0.4	0.0	465	122	0
27	2	1240	4.1	45	0	45	0.0	3.4	0.0	0.2	0.6	0.0	661	153	0
27	3	969	3.8	61	0	61	0.0	3.1	0.0	0.2	0.7	0.0	612	176	0
27	4	1663	2.2	214	0	214	0.0	0.9	0.0	0.2	0.3	0.0	226	100	0
27	5	815	3.2	119	0	119	0.0	1.9	0.0	0.2	0.4	0.0	394	134	0
27	6	565	3.8	88	460	548	0.0	2.2	0.0	0.2	0.5	0.0	71	23	0
27	7	713	3.5	97	526	623	0.0	1.1	0.0	0.2	0.3	0.0	36	17	0
27	8	1363	3.3	75	412	487	0.0	0.8	0.0	0.2	0.2	0.0	24	14	0
27	9	966	5.2	26	123	149	0.0	2.3	0.0	0.2	0.6	0.0	72	24	0
27	10	1505	4.1	37	192	229	0.0	1.6	0.0	0.2	0.4	0.0	52	20	0
27	11	2793	3.0	63	355	419	0.0	1.1	0.0	0.2	0.3	0.0	37	14	0
27	12	3420	2.7	74	0	74	0.0	1.2	0.0	0.2	0.2	0.0	268	92	0
28	1	2040	3.5	52	0	52	0.0	2.3	0.0	0.2	0.4	0.0	465	122	0
28	2	1236	4.1	45	0	45	0.0	3.4	0.0	0.2	0.6	0.0	662	153	0
28	3	968	3.8	62	0	62	0.0	3.1	0.0	0.2	0.7	0.0	611	177	0
28	4	1654	2.2	214	0	214	0.0	0.9	0.0	0.2	0.3	0.0	226	101	0
28	5	810	3.2	119	0	119	0.0	1.9	0.0	0.2	0.5	0.0	394	134	0
28	6	562	3.8	88	460	548	0.0	2.2	0.0	0.2	0.5	0.0	71	24	0

(15) Suspended Solids Case-3 (Soluble) (3/3)

					SS			Cu			Zn				
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
28	7	710	3.5	97	526	623	0.0	1.1	0.0	0.2	0.3	0.0	36	17	0
28	8	1354	3.4	75	410	485	0.0	0.8	0.0	0.2	0.2	0.0	24	14	0
28	9	964	5.2	26	123	149	0.0	2.3	0.0	0.2	0.6	0.0	72	24	0
28	10	1503	4.1	38	192	229	0.0	1.6	0.0	0.2	0.4	0.0	52	20	0
28	11	2787	3.0	63	355	419	0.0	1.1	0.0	0.2	0.3	0.0	37	14	0
28	12	3414	2.7	74	0	74	0.0	1.2	0.0	0.2	0.2	0.0	267	92	0
29	1	2035	3.5	52	0	52	0.0	2.3	0.0	0.2	0.4	0.0	465	122	0
29	2	1233	4.1	45	0	45	0.0	3.4	0.0	0.2	0.6	0.0	662	153	0
29	3	967	3.8	62	0	62	0.0	3.1	0.0	0.2	0.7	0.0	610	177	0
29	4	1645	2.2	214	0	214	0.0	1.0	0.0	0.2	0.3	0.0	227	101	0
29	5	806	3.2	119	0	119	0.0	1.9	0.0	0.2	0.5	0.0	395	135	0
29	6	559	3.8	88	460	548	0.0	2.2	0.0	0.2	0.5	0.0	71	24	0
29	7	706	3.5	97	526	624	0.0	1.1	0.0	0.2	0.3	0.0	36	17	0
29	8	1346	3.4	75	408	483	0.0	0.8	0.0	0.2	0.2	0.0	24	14	0
29	9	962	5.2	26	123	149	0.0	2.3	0.0	0.2	0.6	0.0	71	24	0
29	10	1500	4.1	38	192	229	0.0	1.6	0.0	0.2	0.4	0.0	51	20	0
29	11	2782	3.0	63	355	419	0.0	1.1	0.0	0.2	0.3	0.0	37	14	0
29	12	3408	2.7	74	0	74	0.0	1.2	0.0	0.2	0.2	0.0	267	93	0
30	1	2031	3.5	52	0	52	0.0	2.3	0.0	0.2	0.4	0.0	465	122	0
30	2	1229	4.1	45	0	45	0.0	3.4	0.0	0.2	0.6	0.0	662	154	0
30	3	965	3.8	62	0	62	0.0	3.1	0.0	0.2	0.7	0.0	608	177	0
30	4	1636	2.2	214	0	214	0.0	1.0	0.0	0.2	0.3	0.0	227	101	0
30	5	802	3.2	119	0	119	0.0	1.9	0.0	0.2	0.5	0.0	395	135	0
30	6	556	3.8	88	460	548	0.0	2.2	0.0	0.2	0.5	0.0	71	24	0
30	7	703	3.5	98	526	624	0.0	1.1	0.0	0.2	0.3	0.0	36	17	0
30	8	1337	3.4	75	406	481	0.0	0.8	0.0	0.2	0.2	0.0	24	14	0
30	9	960	5.2	26	123	149	0.0	2.3	0.0	0.2	0.6	0.0	71	24	0
30	10	1497	4.1	38	192	229	0.0	1.6	0.0	0.2	0.4	0.0	51	20	0
30	11	2777	3.0	63	355	419	0.0	1.1	0.0	0.2	0.3	0.0	37	14	0
30	12	3401	2.7	75	0	75	0.0	1.2	0.0	0.2	0.2	0.0	267	93	0
31	1	2027	3.5	52	0	52	0.0	2.3	0.0	0.2	0.4	0.0	465	123	0
31	2	1225	4.1	45	0	45	0.0	3.4	0.0	0.2	0.6	0.0	663	154	0
31	3	964	3.8	62	0	62	0.0	3.1	0.0	0.2	0.7	0.0	607	177	0
31	4	1627	2.2	215	0	215	0.0	1.0	0.0	0.2	0.3	0.0	227	102	0
31	5	797	3.2	120	0	120	0.0	1.9	0.0	0.2	0.5	0.0	395	135	0
31	6	553	3.8	88	460	548	0.0	2.2	0.0	0.2	0.5	0.0	71	24	0
31	7	700	3.5	98	526	624	0.0	1.1	0.0	0.2	0.3	0.0	36	17	0
31	8	1329	3.4	74	404	479	0.0	0.8	0.0	0.2	0.2	0.0	24	14	0
31	9	959	5.2	26	123	149	0.0	2.3	0.0	0.2	0.6	0.0	71	24	0
31	10	1494	4.1	38	192	229	0.0	1.6	0.0	0.2	0.4	0.0	51	20	0
31	11	2772	3.0	63	355	419	0.0	1.1	0.0	0.2	0.3	0.0	37	14	0
31	12	3395	2.7	75	0	75	0.0	1.2	0.0	0.2	0.2	0.0	267	93	0

(16) Suspended Solids Case 3 (Total) (1/3)

				SS			Cu			Zn					
Y	M	TR	DO	MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
20	7	743	3.4	1031	334	1365	28.9	1.2	1.1	9.5	0.3	1.9	454	170	10
20	8	1445	3.2	829	273	1102	28.4	0.8	1.1	9.4	0.2	1.9	447	169	10
20	9	982	5.1	277	78	355	33.2	2.5	1.1	10.9	0.5	1.9	481	174	10
20	10	1530	4.1	402	122	524	30.9	1.7	1.1	10.2	0.4	1.9	467	172	10
20	11	2838	3.0	670	226	896	27.7	1.2	1.1	9.2	0.3	1.9	451	169	10
20	12	3475	2.7	795	0	795	26.9	1.3	0.0	8.9	0.2	0.0	582	188	11
21	1	2076	3.4	558	0	558	29.0	2.4	0.0	9.6	0.4	0.0	601	191	11
21	2	1267	4.1	480	0	480	30.8	3.5	0.0	10.1	0.6	0.0	620	193	11
21	3	979	3.8	642	0	642	30.2	3.3	0.0	9.9	0.7	0.0	616	196	11
21	4	1728	2.2	2311	0	2311	25.2	1.0	0.0	8.3	0.2	0.0	578	188	11
21	5	846	3.1	1262	0	1262	28.0	1.9	0.0	9.2	0.4	0.0	594	192	11
21	6	586	3.7	933	460	1393	29.8	2.3	1.8	9.8	0.5	2.9	424	166	9
21	7	735	3.4	1033	525	1559	28.9	1.2	1.8	9.5	0.3	2.9	407	163	9
21	8	1424	3.3	823	425	1248	28.5	0.8	1.8	9.4	0.2	2.9	400	162	9
21	9	977	5.1	278	123	400	33.2	2.5	1.8	10.9	0.6	2.9	435	167	9
21	10	1523	4.1	402	192	594	30.9	1.7	1.8	10.2	0.4	2.9	420	165	9
21	11	2825	3.0	671	355	1026	27.8	1.2	1.8	9.2	0.3	2.9	403	162	9
21	12	3459	2.7	796	0	796	26.9	1.3	0.0	8.9	0.2	0.0	582	188	11
22	1	2065	3.4	52	0	52	1.1	2.4	0.0	3.9	0.4	0.0	709	878	110
22	2	1258	4.1	45	0	45	1.2	3.5	0.0	4.1	0.6	0.0	904	908	110
22	3	976	3.8	60	0	60	1.1	3.2	0.0	4.0	0.7	0.0	857	932	110
22	4	1708	2.2	213	0	213	0.9	0.9	0.0	3.3	0.2	0.0	454	856	110
22	5	837	3.1	119	0	119	1.1	1.9	0.0	3.8	0.4	0.0	623	889	109
22	6	581	3.7	87	460	547	1.1	2.2	1.8	4.0	0.5	2.9	165	237	22
22	7	730	3.4	97	525	622	1.1	1.2	1.8	3.9	0.3	2.9	130	228	21
22	8	1407	3.3	77	421	498	1.1	0.8	1.8	3.8	0.2	2.9	117	224	21
22	9	975	5.1	26	123	149	1.3	2.3	1.8	4.4	0.6	2.9	169	248	23
22	10	1519	4.1	37	192	229	1.2	1.7	1.8	4.1	0.4	2.9	146	236	22
22	11	2818	3.0	63	355	418	1.1	1.1	1.8	3.7	0.3	2.9	129	223	21
22	12	3452	2.7	74	0	74	1.0	1.2	0.0	3.6	0.2	0.0	495	849	109
23	1	2061	3.5	52	0	52	1.1	2.3	0.0	3.9	0.4	0.0	692	878	110
23	2	1255	4.1	45	0	45	1.2	3.4	0.0	4.1	0.6	0.0	886	908	110
23	3	974	3.8	61	0	61	1.1	3.1	0.0	4.0	0.7	0.0	844	932	110
23	4	1699	2.2	213	0	213	0.9	0.9	0.0	3.3	0.3	0.0	451	856	110
23	5	832	3.1	119	0	119	1.1	1.9	0.0	3.8	0.4	0.0	619	890	109
23	6	578	3.7	87	460	547	1.1	2.2	1.8	4.0	0.5	2.9	164	237	22
23	7	726	3.4	97	525	622	1.1	1.1	1.8	3.9	0.3	2.9	129	228	21
23	8	1398	3.3	76	419	495	1.1	0.8	1.8	3.8	0.2	2.9	117	224	21
23	9	973	5.1	26	123	149	1.3	2.3	1.8	4.4	0.6	2.9	168	248	23
23	10	1516	4.1	37	192	229	1.2	1.6	1.8	4.1	0.4	2.9	146	236	22
23	11	2813	3.0	63	355	418	1.1	1.1	1.8	3.7	0.3	2.9	129	223	21
23	12	3446	2.7	74	0	74	1.0	1.2	0.0	3.6	0.2	0.0	495	849	109
24	1	2056	3.5	52	0	52	1.1	2.3	0.0	3.9	0.4	0.0	691	878	110
24	2	1251	4.1	45	0	45	1.2	3.4	0.0	4.1	0.6	0.0	886	908	110
24	3	973	3.8	61	0	61	1.1	3.1	0.0	4.0	0.7	0.0	842	933	110
24	4	1690	2.2	213	0	213	0.9	0.9	0.0	3.3	0.3	0.0	451	856	110
24	5	828	3.1	119	0	119	1.1	1.9	0.0	3.8	0.4	0.0	620	890	109
24	6	575	3.8	87	460	548	1.1	2.2	1.8	4.0	0.5	2.9	164	237	22

(16) Suspended Solids Case 3 (Total) (2/3)

Y	M	TR	DO	SS			Cu			Zn					
				MINE	NT	TOTAL	MINE	OH	NT	MINE	OH	NT	Cu	Zn	As
24	7	723	3.4	97	526	623	1.1	1.1	1.8	3.9	0.3	2.9	129	229	21
24	8	1389	3.3	76	417	493	1.1	0.8	1.8	3.8	0.2	2.9	117	224	21
24	9	971	5.1	26	123	149	1.3	2.3	1.8	4.4	0.6	2.9	168	248	23
24	10	1514	4.1	37	192	229	1.2	1.6	1.8	4.1	0.4	2.9	148	236	22
24	11	2808	3.0	63	355	418	1.1	1.1	1.8	3.7	0.3	2.9	129	223	21
24	12	3439	2.7	74	0	74	1.0	1.2	0.0	3.6	0.2	0.0	494	849	109
25	1	2052	3.5	52	0	52	1.1	2.3	0.0	3.9	0.4	0.0	691	879	110
25	2	1247	4.1	45	0	45	1.2	3.4	0.0	4.1	0.6	0.0	886	909	110
25	3	972	3.8	61	0	61	1.1	3.1	0.0	4.0	0.7	0.0	841	933	110
25	4	1681	2.2	213	0	213	0.9	0.9	0.0	3.3	0.3	0.0	452	857	110
25	5	824	3.1	119	0	119	1.1	1.9	0.0	3.8	0.4	0.0	620	891	109
25	6	572	3.8	87	460	548	1.1	2.2	1.8	4.0	0.5	2.9	164	237	22
25	7	720	3.5	97	526	623	1.1	1.1	1.8	3.9	0.3	2.9	129	229	21
25	8	1380	3.3	76	415	491	1.1	0.8	1.8	3.8	0.2	2.9	117	224	21
25	9	969	5.1	26	123	149	1.3	2.3	1.8	4.5	0.6	2.9	168	248	23
25	10	1511	4.1	37	192	229	1.2	1.6	1.8	4.1	0.4	2.9	146	237	22
25	11	2803	3.0	63	355	418	1.1	1.1	1.8	3.7	0.3	2.9	129	223	21
25	12	3433	2.7	74	0	74	1.0	1.2	0.0	3.6	0.2	0.0	494	849	109
26	1	2048	3.5	52	0	52	1.1	2.3	0.0	3.9	0.4	0.0	691	879	110
26	2	1244	4.1	45	0	45	1.2	3.4	0.0	4.1	0.6	0.0	887	909	110
26	3	970	3.8	61	0	61	1.1	3.1	0.0	4.0	0.7	0.0	840	933	110
26	4	1672	2.2	214	0	214	0.9	0.9	0.0	3.3	0.3	0.0	452	857	110
26	5	819	3.1	119	0	119	1.1	1.9	0.0	3.8	0.4	0.0	620	891	109
26	6	568	3.8	87	460	548	1.1	2.2	1.8	4.0	0.5	2.9	164	238	22
26	7	716	3.5	97	526	623	1.1	1.1	1.8	3.9	0.3	2.9	129	229	21
26	8	1371	3.3	76	414	489	1.1	0.8	1.8	3.8	0.2	2.9	117	224	21
26	9	968	5.1	26	123	149	1.3	2.3	1.8	4.5	0.6	2.9	168	248	23
26	10	1508	4.1	37	192	229	1.2	1.6	1.8	4.1	0.4	2.9	146	237	22
26	11	2798	3.0	63	355	419	1.1	1.1	1.8	3.7	0.3	2.9	129	223	21
26	12	3427	2.7	74	0	74	1.0	1.2	0.0	3.6	0.2	0.0	494	850	109
27	1	2044	3.5	52	0	52	1.1	2.3	0.0	3.9	0.4	0.0	691	879	110
27	2	1240	4.1	45	0	45	1.2	3.4	0.0	4.1	0.6	0.0	887	909	110
27	3	969	3.8	61	0	61	1.1	3.1	0.0	4.0	0.7	0.0	838	933	110
27	4	1663	2.2	214	0	214	0.9	0.9	0.0	3.3	0.3	0.0	452	857	110
27	5	815	3.2	119	0	119	1.1	1.9	0.0	3.8	0.4	0.0	620	891	109
27	6	565	3.8	88	460	548	1.1	2.2	1.8	4.0	0.5	2.9	164	238	22
27	7	713	3.5	97	526	623	1.1	1.1	1.8	3.9	0.3	2.9	129	229	21
27	8	1363	3.3	75	412	487	1.1	0.8	1.8	3.9	0.2	2.9	117	224	21
27	9	966	5.2	26	123	149	1.3	2.3	1.8	4.5	0.6	2.9	167	248	23
27	10	1505	4.1	37	192	229	1.2	1.6	1.8	4.1	0.4	2.9	146	237	22
27	11	2793	3.0	63	355	419	1.1	1.1	1.8	3.7	0.3	2.9	129	223	21
27	12	3420	2.7	74	0	74	1.0	1.2	0.0	3.6	0.2	0.0	494	850	109
28	1	2040	3.5	52	0	52	1.1	2.3	0.0	3.9	0.4	0.0	691	879	110
28	2	1236	4.1	45	0	45	1.2	3.4	0.0	4.1	0.6	0.0	888	910	110
28	3	968	3.8	62	0	62	1.1	3.1	0.0	4.0	0.7	0.0	837	933	110
28	4	1654	2.2	214	0	214	0.9	0.9	0.0	3.3	0.3	0.0	453	858	110
28	5	810	3.2	119	0	119	1.1	1.9	0.0	3.8	0.5	0.0	621	892	109
28	6	562	3.8	88	460	548	1.1	2.2	1.8	4.0	0.5	2.9	164	238	22

(16) Suspended Solids Case 3 (3/3)

Y	M	TR	DO	SS MINE	SS NT	SS TOTAL	Cu MINE	Cu OH	Cu NT	Zn MINE	Zn OH	Zn NT	Cu	Zn	As
28	7	710	3.5	97	526	623	1.1	1.1	1.8	3.9	0.3	2.9	129	229	21
28	8	1354	3.4	75	410	485	1.1	0.8	1.8	3.9	0.2	2.9	117	225	21
28	9	964	5.2	26	123	149	1.3	2.3	1.8	4.5	0.6	2.9	167	248	23
28	10	1503	4.1	38	192	229	1.2	1.6	1.8	4.1	0.4	2.9	145	237	22
28	11	2787	3.0	63	355	419	1.1	1.1	1.8	3.7	0.3	2.9	129	223	21
28	12	3414	2.7	74	0	74	1.0	1.2	0.0	3.6	0.2	0.0	494	850	109
29	1	2035	3.5	52	0	52	1.1	2.3	0.0	3.9	0.4	0.0	692	879	110
29	2	1233	4.1	45	0	45	1.2	3.4	0.0	4.1	0.6	0.0	888	910	110
29	3	967	3.8	62	0	62	1.1	3.1	0.0	4.0	0.7	0.0	836	934	110
29	4	1645	2.2	214	0	214	1.0	1.0	0.0	3.3	0.3	0.0	453	858	110
29	5	806	3.2	119	0	119	1.1	1.9	0.0	3.8	0.5	0.0	621	892	109
29	6	559	3.8	88	460	548	1.1	2.2	1.8	4.0	0.5	2.9	164	238	22
29	7	706	3.5	97	526	624	1.1	1.1	1.8	3.9	0.3	2.9	129	229	21
29	8	1346	3.4	75	408	483	1.1	0.8	1.8	3.9	0.2	2.9	117	225	21
29	9	962	5.2	26	123	149	1.3	2.3	1.8	4.5	0.6	2.9	167	248	23
29	10	1500	4.1	38	192	229	1.2	1.6	1.8	4.1	0.4	2.9	145	237	22
29	11	2782	3.0	63	355	419	1.1	1.1	1.8	3.7	0.3	2.9	128	223	21
29	12	3408	2.7	74	0	74	1.0	1.2	0.0	3.6	0.2	0.0	494	850	109
30	1	2031	3.5	52	0	52	1.1	2.3	0.0	3.9	0.4	0.0	692	880	110
30	2	1229	4.1	45	0	45	1.2	3.4	0.0	4.1	0.6	0.0	889	911	110
30	3	965	3.8	62	0	62	1.1	3.1	0.0	4.0	0.7	0.0	835	934	110
30	4	1636	2.2	214	0	214	1.0	1.0	0.0	3.3	0.3	0.0	453	858	110
30	5	802	3.2	119	0	119	1.1	1.9	0.0	3.8	0.5	0.0	621	892	109
30	6	556	3.8	88	460	548	1.1	2.2	1.8	4.0	0.5	2.9	164	238	22
30	7	703	3.5	98	526	624	1.1	1.1	1.8	3.9	0.3	2.9	129	229	21
30	8	1337	3.4	75	406	481	1.1	0.8	1.8	3.9	0.2	2.9	117	225	21
30	9	960	5.2	26	123	149	1.3	2.3	1.8	4.5	0.6	2.9	167	248	23
30	10	1497	4.1	38	192	229	1.2	1.6	1.8	4.1	0.4	2.9	145	237	22
30	11	2777	3.0	63	355	419	1.1	1.1	1.8	3.7	0.3	2.9	128	223	21
30	12	3401	2.7	75	0	75	1.0	1.2	0.0	3.6	0.2	0.0	494	850	109
31	1	2027	3.5	52	0	52	1.1	2.3	0.0	3.9	0.4	0.0	692	880	110
31	2	1225	4.1	45	0	45	1.2	3.4	0.0	4.1	0.6	0.0	889	911	110
31	3	964	3.8	62	0	62	1.1	3.1	0.0	4.0	0.7	0.0	833	934	110
31	4	1627	2.2	215	0	215	1.0	1.0	0.0	3.3	0.3	0.0	454	859	110
31	5	797	3.2	120	0	120	1.1	1.9	0.0	3.8	0.5	0.0	622	893	109
31	6	553	3.8	88	460	548	1.1	2.2	1.8	4.0	0.5	2.9	164	238	22
31	7	700	3.5	98	526	624	1.1	1.1	1.8	3.9	0.3	2.9	129	229	21
31	8	1329	3.4	74	404	479	1.1	0.8	1.8	3.9	0.2	2.9	117	225	21
31	9	959	5.2	26	123	149	1.3	2.3	1.8	4.5	0.6	2.9	167	248	23
31	10	1494	4.1	38	192	229	1.2	1.6	1.8	4.1	0.4	2.9	145	237	22
31	11	2772	3.0	63	355	419	1.1	1.1	1.8	3.7	0.3	2.9	128	223	21
31	12	3395	2.7	75	0	75	1.0	1.2	0.0	3.6	0.2	0.0	493	850	109

APPENDIX "F"

DATA OF THE ASSESSMENT OF IRRIGATION WATER QUALITY

CONTENTS FOR APPENDIX "F"

DATA OF THE ASSESSMENT OF IRRIGATION WATER QUALITY

LIST OF TABLES FOR APPENDIX "F"

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APPENDIX "F" DATA OF THE ASSESSMENT OF IRRIGATION WATER QUALITY

1. Introduction

(1) Objective of the Study

The future quality of water to be released from the proposed San Roque dam is projected under the condition that all of mine tailings are directly discharged to tributaries of the Agno River without any treatment and impounded in the reservoir of the proposed San Roque dam as planned in the ELC's feasibility study. The main objective of the Study in the irrigation sector is to evaluate the projected water quality from the viewpoint of agricultural use. For this purpose, field observation works are conducted to examine the influences of physical, chemical and mineral properties of mine tailings on (1) irrigation water, (2) paddy soils and (3) rice plant growth and its yield. In addition, collection of relevant informations and data are conducted in the Government agencies concerned. In due consideration the results of aforesaid observation and analysis, the assessment of irrigation water quality is undertaken.

(2) Outline of the Study

For one year up to November 1984, the field observation works in respect to irrigation water, soil and crop were continuously undertaken in the two existing irrigation systems managed by the National Irrigation Administration (herein referred to as NIA). The one is the Agno River Irrigation System (herein referred to as ARIS) diverting polluted river water for irrigation purposes and the other is the Ambayoan-Diapolo Rivers Irrigation System (herein referred to as ADRIS) taking clear river water. In addition, relevant informations and data were collected from NIA's Headquarters, Region I Office and ARIS and ADRIS Project Offices during the field work period.

With regard to irrigation water quality, monitoring works were carried out to observe quality and quantity of canal water and to take water samples for laboratory tests at 10 monitoring points in the ARIS area and two monitoring points in the ADRIS area. As regards soils, master pit survey was performed in the proposed San Roque irrigation development area for observing soil profile and taking soil samples to determine natural background of heavy metals quantitatively and to clarify vertical change in heavy metal contents in soils. Random sampling of soils was done in the ARIS area to check accumulation of heavy metals and to clarify horizontal change in heavy metal contents in surface soils of paddy fields. With regard to crop, growing condition of the dry and wet seasons rice plants was observed at five monitoring paddy fields in the ARIS area and one in the ADRIS area. At harvesting time, sampling works were conducted for yield survey and yield component analysis as well as for laboratory tests.

All the samples of irrigation water, soils and rice plants taken through the field observation period were analyzed in Japan to determine copper, lead, zinc, cadmium and arsenic among heavy metals quantitatively. Soil samples collected at the 10 master pits were also tested in the NIA Engineering Laboratory in terms of chemical and physical characteristics. Uptaking of nutrient elements by rice plants was tested in Japan.

(3) Scope of the Study

No alternative case in assessing the reservoir water quality is considered in the Study. Accordingly, the evaluation of projected quality of released water from the proposed San Roque dam is made from the viewpoint of agricultural use for only one case in which all of the mine tailings discharged to the Agno River system are impounded into the reservoir of the proposed San Roque dam. The following three cases are excluded from the scope of the Study:

(a) The existing treatment system of mine tailings will be on the present level and the proposed San Roque dam will be constructed. In other words, the water quality of inflow into the reservoir of porposed San Roque dam is same as the current water quality of the Agno River.

(b) The present water quality of the Agno River will be maintained in the future and the proposed San Roque dam is not constructed.

(c) All of the mine tailings will be discharged to the Agno River system and the proposed San Roque dam will not be constructed. In other words, the water quality of the Agno River at the existing ARIS intake dam site becomes the worst.

2. Present Situation of Study Area

(1) Topography and Soils

The future irrigation development area to be benefited under the proposed San Roque Multipurpose Project is located in the Province of Pangasinan. It occupies the northwestern part of the Central Luzon plain which is the most famous rice bowl in the Philippines. The gross study area is around 119,000 ha, almost of which comprise a flat alluvial plain facing the Gulf of Lingayen in the northwesternmost. The Agno River flows through the center of this plain from the south to the west and then to the north. In the east side of the plain, the Dagupan River system flows to the Gulf of Lingayen, functioning as a natural drainage network in the proposed San Roque irrigation development area.

Typical soils are derived from alluviums and extend over 105,000 ha or 88% of the gross study area. Furthermore, the recent alluvial soils are observed on a fan developing on the outskirts of plain where the Agno River flows out from the mountainous area. The alluvial soils are silt loam to silty clay in texture, deep in effective solum and good in permeability. The soils on the fan have a wide variation of texture from sandy loam to clay, deep solum and a wider range of permeability.

(2) Present Land Use and Irrigation

In the study area, there exists cultivated land of approximately 89,000 ha in total. Out of this, paddy fields share about 84,000 ha among which 63,000 ha are single cropping area of rice followed by diversified crop cultivation or fallow during the dry season.

There are three large-scale NIA irrigation systems, namely ARIS, ADRIS and the Lower Agno River Irrigation System (herein referred to as LARIS). Each commanded area is 20,200 ha in gross for ARIS, 6,600 ha for ADRIS and 10,200 ha for LARIS. In addition, 36 communal irrigation schemes provide a total paddy field of 7,800 ha with irrigation water by utilizing springs or small rivers. Paddy fields of another 2,000 ha secure irrigation water source by pumping up groundwater. Accordingly, 46,800 ha or nearly 55% of the total paddy fields in the study area are equipped with irrigation facilities. The location of NIA irrigation systems and communal irrigation schemes in the study area is as illustrated in Figure F-1.

(3) Agricultural Production

The present cropping pattern prevailing in the area with year-round irrigation water source facilities is double cropping of rice, while it comprises a combination of rice as the wet season crop and industrial crops like tobacco and cotton or cash crops such as corn, mongo, peanut and vegetables as the dry season crop as well as single cropping rice only for the wet season. In the rainfed paddy fields, similar cropping patterns are popular. The total cropped area for the wet season in the proposed San Roque irrigation development area comprises 79,200 ha for rice, 4,090 ha for corn and 5,320 ha for sugarcane. For the dry season, on the other hand, fallow area occupies 52,000 ha and crops are grown in the remaining 31,400 ha including 10,100 ha for rice, 5,300 ha for industrial crops and 16,000 ha for cash crops. The present cropping area in the proposed San Roque irrigation development area is as shown in Table F-1. Cropping intensity varies widely depending on availability of irrigation water resources. It is 135% on an average in the proposed San Roque irrigation development area. In detail, the crop intensity is 158% for ARIS, 163% for ADRIS, 137% for LARIS and 110% for the rainfed cultivation area.

The average crop yield at present is 3.0 ton/ha for paddy both for the dry and wet season croppings, 2.3 ton/ha for paddy under the rainfed condition, 1.2 ton/ha for corn, 0.4 ton/ha for mongo, 0.8 ton/ha for peanut, 1.7 ton/ha for tobacco, 1.5 ton/ha for cotton and 5.6 ton/ha for sugarcane.

The annual crop production in the proposed San Roque irrigation development area averages about 237,000 tons for paddy, 8,000 tons for corn, 4,000 tons for mongo, 1,000 tons for peanut, 7,500 tons for tobacco and 30,000 tons for sugarcane.

(4) Socio-Economic Situation

A total of 34 municipalities is totally or partially included into the proposed San Roque irrigation development area. According to the 1980 census, the total population of 34 municipalities was about 1,203,000 persons. Of these, around 771,000 persons lived in the future benefited area of proposed San Roque irrigation development. The population density was 650 persons/km^2.

The population belonging to productive age shared about 57% of the total population. The labour force working population was about 190,000 persons with a share of 30% for the total population and 43% for the population belonging to productive age. The persons engaged in gainful activities covered 95% of labour force working population, and about half of them or 90,000 persons made their living by farming. The remaining population belonging to productive age comprised half for children and pupil and another half for housewives. Therefore, socio-economic activities in the proposed San Roque irrigation development area depend closely on the vicissitude of agricultural production.

(5) Environment

Since 1952, about 10 study reports have been prepared describing the effect of mining activities accompanied with disposal of huge mine tailings in the catchment area of the Agno River, including JICA Report in 1978 and ELC Feasibility Report for San Roque Multipurpose Project in 1979. In these reports, it is pointed out that the annual sediment load of the Agno River is estimated to be around 5,500,000 tons out of which 3,000,000 tons are derived from mine tailings. Also, mine tailings share 96% of sediment load for the dry season and 45% for the wet season. The Man and the Biosphere published the report on the "Integrated Ecological Programme on the Control of Sedimentation of Rivers and Canals in Existing Irrigation Systems" in 1980 as the final output of interagency research on ecological studies led by NIA. This report shows the contents of heavy metals in sediments on canal bed of ARIS, namely copper of 146 to 997 mg/kg, lead of 9.7 to 46.9 mg/kg, zinc of 13.4 to 32.4 mg/kg and cadmium of 0.61 to 1.24 mg/kg. Furthermore, the reduction rate of paddy yield is estimated to be 20 to 50% due to inflow and settling of large quantities of sediments in paddy fields resulting in aggravation of environment for normal growth of rice plant, especially physical properties of soils in plant root zone.

3. Existing Irrigation Systems and Outline of Future Development Plan

(1) Existing Irrigation Facilities

1) Agno River Irrigation System

Since 1957, ARIS has been operated in the right bank area of the Agno River. The downstream service area was expanded to some extent by constructing the Sinocalan intake. Presently, the total net irrigation area covers 20,200 ha. The irrigation water is diverted from the Agno River through the ARIS intake dam with design capacity of 38.0 m^3/sec. It is distributed to paddy fields through the main canal of 46 km, laterals of 207 km and watercourses and farm ditches of 411 km in total. The overall canal density is about 33 m/ha on an average. Small rivers function as natural drainage channels for ARIS. All the canals are formed of earth lining except for the first 1-km section of main canal and sections with canal structures both of which are of concrete lining.

The existing two reservoirs such as Ambuklao and Binga, located in the upper reaches of the Agno River, are operated for hydroelectric power generation. The water level at the ARIS intake dam site shows, therefore, daily fluctuation caused by the actual operation of power stations. The ARIS intake dam is located at 2.5 km downstream from the proposed San Roque dam site and on the right bank where the Agno River flows into the Pangasinan plain from the mountainous areas. As no sand settling basin is installed in the ARIS intake dam, a large quantity of sand and silt is transported into the main canal when irrigation water is diverted. These sand and silt are derived from mine tailings for the dry season and a mixture of mine tailings and soils eroded from the catchment area for the wet season. A coarse portion of mine tailings is used as embankment materials of storage dams to impound mine tailings so that it is eroded by rainfall and discharged to tributaries of the Agno River. As shown in Table F-2, the NIA ARIS Project Office is always suffering from siltation of the main canal and laterals in its service area and entails an annual expenditure to large extent for desiltation. Furthermore, annual volume of siltation in the ARIS area exceeds over the physical and financial capabilities of the NIA ARIS Project Office for desiltation resulting in reduction of the design capacity of the main canal and laterals as well as expansion of sub-laterals and farm ditches buried under sand and silt. According to the report of NIA ARIS Project Office, the actual irrigation service area in 1983 was 10,300 ha for the wet season cropping and 2,000 ha for the dry season cropping as shown in Table F-3.

Currently, the NIA ARIS Project Office has executed a countermeasure to convert irrigation water source from the Agno River to small rivers and ponds for supplemental provision of clear irrigation water for the wet season cropping. This countermeasure consisting of seven schemes targets to cover 7,100 ha in total.

2) Lower Agno River Irrigation System

The left bank area of the Agno River has been benefited by LARIS since 1976. The irrigation service area is 10,200 ha and the irrigation water is diverted from the Agno River through an intake dam with the design capacity of 20.0 m^3/sec, located at the point of 20 km downstream from the ARIS intake dam. The canal system consists of the main canal of 31 km, laterals with the total length of 161 km and watercourses and farm ditches of 550 km in total. The overall canal density is 73 m/ha on an average. Except for sections of canal structures installed, all the canals are composed of earth lining. There is no drainage canal system. Small rivers of 59 km in total length are utilized as natural drains.

The Agno River is very wide and its river channel undergoes many changes at the LARIS intake dam site. The water level also fluctuates by the effect of reservoir operation of the Ambuklao and Binga dams. Therefore, stable intake of water for LARIS is hardly secured every year. The actual result of irrigation water supply in 1983 was reported to be 7,400 ha for the wet season cropping and 2,900 ha for the dry season cropping.

3) Ambayoan-Diapolo Rivers Irrigation System

There are two intake dams in the ADRIS area each of which diverts clear river water for irrigation purposes. The irrigation service area totals 10,500 ha out of which 8,100 ha depend its irrigation water source on the Ambayoan River and the remaining 2,400 ha take irrigation water from the Diapolo River. The former has been operated since 1975 and the latter from 1970. The total length of canal is 41 km for the main, 135 km for laterals and 385 km for watercourses and farm ditches. The overall canal density is 53 m/ha on an average.

Due to seasonal fluctuation of run-off from the small catchment areas of the Ambayoan and Diapolo Rivers, the actual irrigation area in the recent years averages 5,200 ha for the wet season cropping and 1,200 ha for the dry season cropping.

(2) Future Irrigation Development Plan

In 1979, the feasibility study on the San Roque Multipurpose Project was completed by the Electroconsult (herein referred to as ELC) and EDCOP. For the purpose of detailed irrigation study, ELC carried out the feasibility study on irrigation component of the Lower Agno River (San Roque) Multipurpose Project and submitted the report to NIA in 1981. In this report, three configuration plans were compared for selecting an irrigation development plan with the highest priority. As a result, the integrated plan for the intake of irrigation water was proposed, comprising a combination of reshaping and upgrading works of the existing ARIS intake dam to supply irrigation water to 70,800 ha including the existing ARIS, LARIS and ADRIS areas as well as the new ARIS Extention area.

1) Proposed cropping patterns

The future cropping patterns proposed in the ELC Feasibility Report consist of the following seven types; (a) double cropping of rice, (b) rice followed by cotton to be grown as the dry season crop, (c) rice followed by tobacco, (d) rice followed by one of cash crops like mongo, corn and peanuts, (e) rice followed by two crops of vegetables (f) triple cropping of vegetables and (g) perennial cropping of sugarcane. Based on the results of land capability classification study, the different cropping pattern was proposed by ELC for the respective components of San Roque irrigation development area as shown in Table V-4.

The target yields of respective crops for one cropping were anticipated to be 4.5 ton/ha for rice, 2.3 ton/ha for cotton, 2.0 ton/ha for tobacco, 1.0 ton/ha for mongo, 80 ton/ha for sugarcane and 10 ton/ha for vegetables. Proper water management and farming practices were pointed out to be required for realizing each target yield.

2) Irrigation water demand

In the ELC Feasibility Report, irrigation water requirement was calculated based on the following consideration. The basin rainfall in the proposed San Roque irrigation development area was estimated for 21 years from 1950 to 1970 on the basis of point rainfalls in Baguio and Dagupan. The potential evapotranpiration was obtained from the monthly observation records of pan evaporation for 18 years available in the proposed San Roque irrigation development area. The crop coefficient was estimated taking into account experimental records. The daily deep percolation rate was determined to be 2.3 mm based on the results of field tests. From these, crop irrigation requirement at farm level was calculated. Then, taking into account the actual results in NIA's existing irrigation service areas of the central Luzon, the irrigation efficiency was determined to be 55% for rice cropping and 50% for upland crop cultivation. Based on this, crop irrigation requirement at diversion works and diversion water requirement for each system were calculated.

Through the comparison of three configulation plans from the viewpoint of maximization of irrigation area, the integrated plan of intake dam was selected. The proposed irrigation service area was also determined to be 26,850 ha for ARIS and 23,700 ha for ARIS Extension in the right bank area of Agno River and 7,600 ha for ADRIS and 12,650 ha for LARIS in the left bank area.

3) Proposed irrigation development plan

Irrigation water required for covering 70,800 ha will be diverted from the Agno River through the integrated San Roque intake dam for which the existing ARIS intake dam will be reshaped. The water will be conveyed to the reregulating pond. The design capacity is 290 m^3/sec for the intake dam and 4,600,000 m^3 for the reregulating pond. The two separate outlets will supply water from the reregulating pond to the right and left bank irrigation sectors. The outlet to ARIS and ARIS Extension has a discharge capacity of 85.2 m^3/sec. The total length of the right bank main canal is 131 km. The existing ARIS main canal will be expanded. The total canal length is 541 km for laterals and 3,339 km for watercourses and farm ditches. The overall canal density will become 79 m/ha. All the canals except for the first 1-km section of main canal and related structures are formed of earth lining. The drainage canals of 505 km will be newly constructed.

The outlet to ADRIS and LARIS has a discharge capacity of 34.4 m^3/sec. The left bank main canal will across the Agno River by siphon. The total length of left bank main canal is 52 km with laterals of 235 km and watercourses and farm ditches of 1,346 km in total. The overall canal density will become 80 m/ha. All of the canals are formed of earth lining except for the section of related structures. The drainage canal to be newly constructed is 125 km in the total length.

4. Performance of Survey

(1) Methodology of Survey

1) Irrigation water quality survey

For the establishment of monitoring point, the field reconnaissance was made in November and December 1983 followed by the discussion with NIA. As a result, a total of 10 monitoring points was selected as describing in the Inception Report. These consisted of four monitoring points for year-round observation and another four monitoring points for wet season observation in the ARIS area. In addition, two monitoring points were established in the ADRIS area for comparison purposes of irrigation water quality.

The irrigation water supply for the 1983/84 dry season cropping to the ARIS area was commenced in December 1983. In 1983, however, the water shed of the Agno River had a little rainfall and the release from the existing Ambuklao and Binga dams was reduced. As a result, the discharge at the ARIS intake dam site was remarkably declined when the dry season irrigation water supply was commenced. Under such a water shortage condition, the NIA ARIS Project Office revised its irrigation water distribution plan for the dry season cropping and reduced its irrigation service area from 5,600 ha to 2,500 ha. In line with the final irrigation water distribution plan of NIA ARIS Project Office, two monitoring points were relocated to the revised irrigation service area.

Usually, NIA has performed desilting works of the upper reaches of main canal for two or three weeks in November to secure minimum canal capacity required for irrigation water supply planned every dry season. According to NIA, it was observed that the quantity of sand and silt including mine tailings was considerable large during the 1983/1984 dry season. Desiltation of the first 1-km distance of main canal was continuously carried out through the dry season. Additional water sampling works were undertaken once every three weeks on an average to grasp the correlation between the increase in siltation during 1983/84 dry season and the effect of river bed dredging work done at a point 500 m upstream from the ARIS intake dam to construct a bridge crossing over the Agno River.

The supplemental irrigation water supply to the 1984 wet season cropping area in the ARIS area was commenced in June 1984. As the irrigation service area was limited to 8,400 ha among the total area of 20,200 ha even though the present capacity of canal was fully utilized, minor relocation of monitoring points was made through the discussion with NIA before starting the field observation works for the wet season. For covering the whole irrigation service area, additional two monitoring points were established in the ARIS area. Thus, the field observation works of irrigation water quality for the wet season were made at 10 monitoring points in the ARIS area and two monitoring points in the ADRIS area. The location of monitoring points is as illustrated in Figure F-2. The details of observation works at the respective monitoring points are as summarized in Table F-5.

The monitoring works of irrigation water quality were principally made once a week. The monitoring items were water temperature, pH, electric conductivity, dissolved oxygen and turbidity. Water sampling was conducted once every two weeks at the respective monitoring points.

Discharge measurement work was principally performed twice to three times a week at the starting point of main canal of ARIS and once a week at the diversion point of laterals on which the monitoring point was established, while it was done once a day at the intake dam site of ADRIS. At each monitoring point, 24-hour continuous observation work was carried out one to two times during the 1984 wet season.

2) Soil survey

The random soil sampling was done at 204 sites in paddy fields of 19,500 ha in the ARIS area during the fallow period of 1983/84 dry season to clarify the accumulation of heavy metals in surface soils at the inlet part of paddy fields in the ARIS area. Additional 43 surface soil samples were taken from paddy fields in the ARIS and communal irrigation scheme areas after harvesting the dry season crop.

The selection of sampling points was made by referring to aerophotographs with a scale of 1/10,000 and topographic maps having a scale of 1/4,000. After confirmation of land use condition at each selected point, the random soil sampling was conducted.

To determine quantitatively natural background of heavy metal contents in soils of the proposed San Roque irrigation development area, the master pit survey was carried out in March and April 1984 at four sites in the ARIS area, three sites in the proposed extension area of ARIS, one site in the ADRIS area and two sites in the LARIS area in collaboration with the staff of the Project Development Department of NIA Headquarters. At the respective pit sites, profile observation up to 150 cm in depth and soil sampling works were performed.

To grasp horizontal distribution of heavy metals in surface and subsurface paddy soils in the ARIS area, surface soils up to 15 cm in depth and subsurface soils up to 30 cm were collected at inlet, middle and outlet parts of the six monitoring paddy fields for observing crop growth.

Sediments on canal bed were taken at 10 monitoring points of irrigation water quality in the ARIS area to determine heavy metals quantitatively.

All the soil samples collected were air-dired, ground in a mortar and passed through a 2-mm sieve for preparing samples of laboratory test in Japan. The sediment samples on canal bed were separated into four fractions, i.e. above 2 mm, 2 to 0.2 mm, 0.2 to 0.02 mm and below 0.02 mm. Heavy metal contents of each fraction were examined.

3) Crop survey

The monitoring paddy field was selected at two sites in the ARIS area and one site in the ADRIS area to seize difference in growing condition, yield with its component and uptake of heavy metals and nutrient elements. For the crop survey in the wet season, another three sites were supplemented in the ARIS area. At each monitoring paddy field, growing condition of rice plant was observed and yield survey was performed. In addition, samples were collected for yield component analysis and laboratory tests.

At the respective monitoring paddy fields, four plots were selected for observation purpose. These plots are irrigated under plot-to-plot condition. The first plot is located adjacent to the inlet from watercourse or settling basin. The last plot connects to the drainage channel through the outlet. Three hills of rice plant were selected in the inlet portion of each plot and were observed once a week in terms of plant height and number of tillers. In parallel with the monitoring works on crop growth, interview survey was done to collect information on farming practices of farmers who managed the monitoring paddy fields. At harvesting time, all the hills grown in an area of 1 m^2 were cut at inlet, center and outlet portions of each plot under a series of plot-to-plot irrigation in the respective monitoring paddy fields and in some of paddy fields at which the random soil sampling was made. After counting number of tillers of all hills, six hills with an average number of tillers in each cutting spot were chosen for estimating yield and analyzing yield components.

After harvesting, these observed hills were separated into root, stem, leaf and grain for heavy metal and nutrient analysis.

To clarify the distribution of paddy yield in the ARIS area, yield survey and yield component analysis were undertaken at eight places for the dry season crop and 18 places for the wet season crop. At each place, the cutting survey with the same methodology above-mentioned was conducted.

4) Laboratory tests

Laboratory tests carried out in the Engineering Research Laboratory of Nippon Koei Co., Ltd. in Tokyo comprised heavy metal analysis of irrigation water, paddy soils and rice plant, suspended solid content of irrigation water, and nutrient uptake of rice plant. The chemical and physical analyses of soil samples taken through the master pit survey were performed by the NIA Engineering Laboratory in the Philippines.

The heavy metal analysis was made in conforming with the official quideline adopted in 1979 by the Ministry of Agriculture, Forestry and Fisheries, Japan. The items of laboratory test on irrigation water sample consisted of suspended solid and dissolved copper, zinc, lead, cadmium and arsenic.

The items of soil analysis comprised the soluble type of heavy metals and the extractable type of heavy metals. The former is defined as an element to be easily absorbed by crops. For quantitative analysis of soluble heavy metals, extraction was prepared by using 0.1-normal solution of hydrochloric acid for copper, zinc and cadmium, 1-normal solution of hydrochloric acid for arsenic and 1-normal solution of ammonium acetate for lead. The latter is also defined as an element to be possibly translocated from soils to crops. The extractable heavy metals were examined by preparing decomposition by a solution of perchloric, sulfuric and nitric acids. The atomic absorption spectrophotometer was employed in determing the both types of heavy metals quantitatively. As for sediments on the canal bed, the soluble type of heavy metals was examined by each particle size. The rice plants were tested to determine heavy metals like copper, lead, zinc, cadmium and arsenic and nutrient elements such as nitrogen, phosphorus and potassium.

(2) Number of Samples

The number of samples collected through the monitoring period is 143 for the dry season irrigation water and 160 for the wet season irrigation water, totalling 303 in water samples. The soil samples total 447 comprising 247 taken at the random soil sampling, 48 collected at the master pit survey and 152 taken from surface and subsurface layers in the monitoring paddy fields. The sediment samples are 10 in total and separated into 30 based on the particle size distribution for the laboratory test. Rice plants collected are 18 samples for the dry season and 23 samples for the wet season, totalling 41 samples. As these are separated into five portions, the total number of test pieces becomes 205.

The actual performance of laboratory tests is as tabulated in Table F-6.

5. Results of Irrigation Water Quality Survey

(1) Discharge

Throughout 1983, the water shed of the Agno River had a little rainfall and the total rainfall during six months of the wet season was 603 mm in the ARIS area as shown in Table F-7. This rainfall is only one third of the average rainfall of 1,870 mm for the same months between 1978 and 1982. As a result, the discharge at the ARIS intake dam site was remarkably declined from the beginning of 1983 and it was very difficult to divert irrigation water from the Agno River. The actual intake discharge at the ARIS intake dam averaged 1.53 m^3/sec for the period from November 1983 to April 1984, being equivalent to one fourth of the average intake discharge of 6.54 m^3/sec for the same period of the last five years.

From the middle of April 1984, the ARIS area had periodically plentiful rainfall up to July though the total precipitation was below the average of the same period for the last five years from 1978 to 1982. The supplemental irrigation water supply program to the wet season cropping in the ARIS area and the actual water distribution was smoothly done to meet the paddling water requirement throughout the planned area. After August, monthly rainfall was over 500 mm for three months due to the effect of typhoon and the total rainfall during this period was 1,840 mm. The intake discharge varied between 1.29 and 8.73 m^3/sec and averaged 4.73 m^3/sec throughout the wet season in 1984. This corresponds to about 55% of the average intake discharge of 8.54 m^3/sec during the period from 1978 to 1982.

The NIA ARIS Project Office has been continuously undertaking discharge measurement at the station of 320 m downstream from the starting point of main canal. Table F-8 shows the discharge measurement records at this station for the monitoring period under the Study. The measured discharge is equivalent to the intake dam. The maximum intake discharge was 9.07 m^3/sec on March 19 for the dry season and 29.53 m^3/sec on August 2 for the wet season.

As the water level of the Agno River fluctuated in response to the change in outflow from the Binga dam based on the reservoir operation for power generation, discharge measurement works every three hours were carried out at the respective monitoring points for one day every month from July to September. The measurement records as shown in Table F-8 indicate that the maximum discharge is ordinarily 1.6 times as much as the minimum one.

The discharge measurement works at the respective monitoring points were conducted by the NIA ARIS and ADRIS Project Offices. All the discharge measurement records are as shown in Tables F-9 thru F-15. In performing discharge measurement at each monitoring point, no irrigation water is supplied to laterals, on which the monitoring point is established, in accordance with the irrigation water distribution program of NIA. In such case, no discharge measurement record is obtained.

(2) Field Observation Records on Irrigation Water Quality

Tables F-16 thru F-27 show the observation records on water temperature, turbidity, pH, electric conductivity and dissolved oxygen at the respective monitoring points. According to the observation records at the Monitoring Point No. 1 established on the main canal at the diversion point of Lateral A, water temperature and dissolved oxygen fluctuated in response to the observation time, while other three items severally indicated the change in observed records. The range of observation records was 23.2 to 29.5°C for water temperature, 7.8 to 8.8 for pH, 260 to 1,000 μS/cm for electric conductivity and 3.6 to 9.5 mg/ℓ for dissolved oxygen. The turbidity usually exceeded over 500 ppm, but it declined to around 100 ppm when the intake water became clear. This tendency of change in water quality was similar to the observation records obtained at the Fixed Point E which was established on the main stream of the Agno River at a point of 500 m upstream from the existing ARIS intake dam.

Through a comparison between observation records at the Monitoring Point