

**THE REPUBLIC OF THE PHILIPPINES**

**THE FEASIBILITY STUDY**

**ON**

**THE DEVELOPMENT PROJECT**

**ON**

**THE METEOROLOGICAL TELECOMMUNICATION SYSTEM**

**FINAL REPORT**

**(APPENDIX)**

**JANUARY 1985**

**JAPAN INTERNATIONAL COOPERATION AGENCY**



No.

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ON

THE DEVELOPMENT PROJECT

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THE METEOROLOGICAL TELECOMMUNICATION SYSTEM

FINAL REPORT

(APPENDIX)

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JANUARY 1985

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## Appendix A



## Appendix A. Study Results and Analytic Evaluation

Appendix A (\*1) Calculation method of receiving input power, corrective value based on the test and atmospheric refractivity

Atmospheric refractivity on the ground surface:

$$N(s) = \left( \frac{77.6}{273 + T} \right) \times \left( P + \frac{4810 \times e_s \times Rh}{273 + T} \right)$$

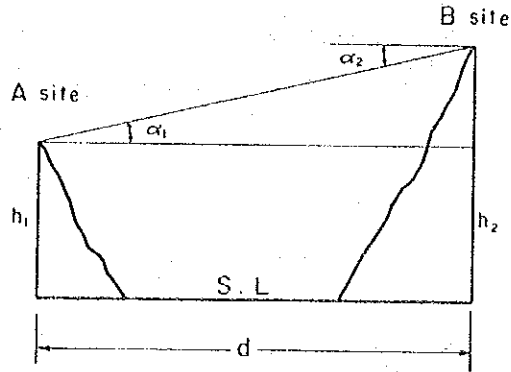
T : Temperature (°C), P: Atmospheric pressure (mb)

Rh: Relative humidity

$e_s$ : Saturation vapor pressure (mb)

Receiving power for the OH communication generally varies every moment by fading. Therefore, if the standard receiving power is assumed to be the receiving power at a time rate of 50%, then the receiving power levels obtained at certain intervals within a certain time period must be accumulated to determine the accumulative percentage of the receiving power with respect to time rate. This time we used a personal computer for this analysis and processing. Of these accumulative percentage values, the receiving power levels at a time rate of 50% are picked up for further calculation of the accumulative percentage in order to obtain the standard receiving power (level at a time rate of 50%) for the radio link subjected to the propagation test. The difference between this value and the estimated standard value on the site for propagation tests is "the corrective value based on the propagation test."

Appendix A (\*2) Calculation method of the height of an obstruction on the propagation route



$$\tan \alpha_1 = - \left( \frac{h_1 - h_2}{d} + \frac{d}{2Ka} \right)$$

$$\tan \alpha_2 = - \left( \frac{h_2 - h_1}{d} + \frac{d}{2Ka} \right)$$

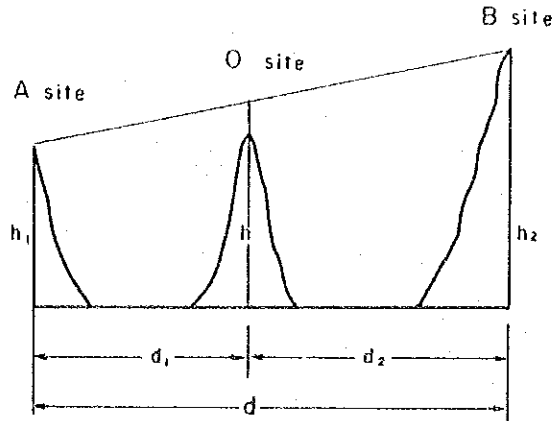
$\alpha_1, \alpha_2 > 0$ : angle of elevation

$\alpha_1, \alpha_2 < 0$ : angle of depression

- d: Distance between A and B sites
- $h_1$ : Height above sea level of A site
- $h_2$ : Height above sea level of B site
- $\alpha_1$ : Vertical angle of B site viewed from A site
- $\alpha_2$ : Vertical angle of A site viewed from B site
- a : Radius of earth (6370 km)
- K : Refractive index of light (1.15)

In practice, the height above the sea level of one of the two sites is measured with a pocket altimeter.  $\alpha$  is measured with a transit compass while d is actually measured or determined with a map.

Appendix A (\*3) Method of calculating the minimum required antenna height



- $h_1$  : Height above sea level of A site  
 $h_2$  : Height above sea level of B site  
 $h$  : Height above sea level of O site  
 $d$  : Distance between A and O sites  
 $d_1$  : Distance between O and B sites  
 $d_2$  : Distance between A and B sites  
 $a$  : Radius of earth (6370 km)  
 $K$  : Refractive index of radiowave (4/3)

$$h_1 = \frac{hd - h_2d_1}{d_2} + \frac{d_1d}{2Ka}$$

The following must also be taken into consideration:

- . The first Fresnel's zone is ensured against obstructions except for 800 MHz-band routes.
- . The correction of 7 meters is added to the determined height of an obstruction above the sea level to allow for the height of trees and measurement errors.
- . The possible future raising or lowering of the height due to the leveling of ground of each site is not taken into consideration.

Appendix A (\*4) Terrain profile, system data sheet, receiving power and fading rise/depth and receiving power with respect to time rate

(\*4) 1

Terrain profile: Fig. A.1, (1/19) - (19/19)

The heights above sea level of the points of test and survey, the antenna heights, and the heights above sea level of obstructions determined through measurement and site survey are overwritten on the terrain profile made during map survey.

(\*4) 2

System data sheet for propagation test: Table A.1, (1/11) - (11/11)

For each radio link subjected to the 800 MHz-band propagation test, the estimated values on site for the propagation test are written into the system data sheet on map for the propagation test.

"The estimated values on map for the propagation test" are the standard receiving power levels calculated before the test is actually made on the site. These values are referred to check whether the specifications for devices and materials used for the test are valid or invalid and whether the test is possible or impossible. "The estimated values on site for the propagation test" are the standard receiving power levels calculated according to the specifications used for the actual test. Based upon these calculated standard receiving power values, "the corrective values based on the propagation test" are calculated.

(\*4) 3

Receiving power and fading rise/depth: Fig. A.3, (1/32) - (32/32)

Based upon the accumulative percentage values of the receiving power with respect to time rate that are output from the personal computer for each measurement time interval, the receiving power at time rates of 1%, 5%, 50%, 95%, 99%, and 99.95% is graphed while the differences between the receiving power at time rates of 1%, 5%, 95%, and 99.95% and the receiving power at a time rate of



50% are expressed as the "fading rise and depth" which are also graphed.

The above data allow us to determine the quantitative and qualitative receiving power variations with time.

(\*4) 4

Receiving power with respect to time rate: Fig. A.4,  
(1/22) - (22/22)

Of the accumulative percentage values of receiving power with respect to time rate that are output from the personal computer for each measurement time interval, representative data are plotted on a normalized probability chart.

Appendix A (\*5) Results of measurement on  
obstructions on selected routes

(\*5) 1

The results of measurement of obstructions between BALOD and CAPACUAN are shown in Fig. A.1 (5/19). The measurement results are as follows.

° Obstruction measurements on the BALOD side (including tree heights)

h : Height above sea level of BALOD (from measurement with a pocket altimeter) + Transit compass height =  
53m + 1.5m

$\alpha_1$ : +1°32'20" (by transit compass)

d : 1.26km (measured with a map)

$$h_2 : d \cdot \tan \alpha_1 + h_1 + \frac{d^2}{2Ka} = 1,260\text{m} \times \tan (1^\circ 32' 20'') + \\ (53\text{m} + 1.5\text{M} + \frac{(1260)^2}{2 \times 1.15 \times 6370000}) \\ = 88.5\text{m}$$

° Obstruction measurements on the CAPACUAN side (including tree heights)

$h_2$ : Height above sea level of CAPACUAN (by pocket altimeter) + Transit compass height = 310m + 1.5m

$\alpha_2$ : -40'30" (by transit compass)

$d$  : 8.2km (by a map)

$$h_1 = d \cdot \tan \alpha_2 + h_2 + \frac{d^2}{2Ka} = 219.5m$$

(\*5) 2

An unobstructed view from CAPACUAN to TINAMBACAN was confirmed as had been expected from the map survey. The terrain profile is shown in Fig. A.1 (6/19).

(\*5) 3

A site survey was performed at the 490m highland site of the BALOD-490m highland-TINAMBACAN route. However, the view from this site to the other site could not be checked, and no measurement data could be obtained.

(\*5) 4

The data regarding the 800 MHz-band propagation test with the BALOD-CAPACUAN route is as follows.

° System data sheet for the 800 MHz-band propagation test ..... Table A.1, (5/11)

° Height and Rotation antenna pattern ..... Fig. A.6, A.7

(\*5) 5

For the approach links, MALABOG-LEGASPI, BALOD-CATARMAN, DANAQO-MACTAN Radar, and MALASAG-CAGAYAN DE ORO, the test was performed on the two links: MALABOG-LEGASPI and DANAQO-MACTAN RADAR. The results are shown in Fig. A.1, (9/19 - 11/19).

A site survey on the BALOD-CATARMAN and MALASAG-CAGAYAN DE ORO links revealed little problem, and measurement was not made on these links.

Appendix A (\*6) Evaluation of the minimum required antenna height

(\*6) 1

BALOD-CAPACUAN-TINAMBACAN

$h_1$ : Minimum required antenna height at the BALOD station

$h$ : Height above sea level of propagation route at obstruction point (Height above sea level of obstruction + Measurement errors and tree height (7m) + Depth of first Fresnel's zone at obstruction point)

$d$ : Distance between BALOD and CAPACUAN

$h_2$ : Antenna height above sea level at CAPACUAN

$d_1$ : Distance between BALOD and obstruction

$d_2$ : Distance between CAPACUAN and obstruction

$\beta$ : Altitude at BALOD

° Minimum required antenna height at the BALOD station, if a back-to-back coupling antenna system is used at CAPACUAN:

$$h_1 = \frac{hd - h_2 d_1}{d_2} + \frac{d_1 d}{2Ka} - \beta = \frac{(88.5^m + 7.4 + 7^m) \times 25700^m - 1260^m \times (310^m + 15^m)}{24440m} + \frac{1260m \times 25700m}{2 \times 4/3 \times 6370000m} - 53m = 40.4m$$

\* Between BALOD and CAPACUAN, the minimum required antenna height at the BALOD station with respect to the obstruction 17.5km distant from BALOD is 39.8m. Therefore, the minimum required antenna height at the BALOD station is 40.4m. In this case, an antenna height of 15m is assumed at CAPACUAN.

\* Since a line of sight is ensured between CAPACUAN and TINAMBACAN, the antenna height is 15m at CAPACUAN while 10m at TINAMBACAN.

- ° BALOD station minimum required antenna height, if a reflector plate (tower height of reflector 5m) is installed at CAPACUAN:

$$\begin{aligned}
 h_1 &= \frac{(219.5\text{m} + 15.8\text{m} + 7\text{m}) \times 25700\text{m} - 17500\text{m} \times (310\text{m} + 15\text{m})}{8200\text{m}} \\
 &+ \frac{17500\text{m} \times 25700\text{m}}{2 \times 4/3 + 6370000\text{m}} - 53\text{m} \\
 &= 60.6\text{m}
 \end{aligned}$$

- \* Between BALOD and CAPACUAN, the minimum required antenna height at the BALOD station with respect to the obstruction 1.26km distant from BALOD is 40.9m.

(\*6) 2

BALOD-490m highland-TINAMBACAN

$h_1$ : Minimum required antenna height at the BALOD station or TINAMBACAN station

$h$ : Height above sea level of propagation route at the obstruction point

$d$ : Distance between BALOD and the 490m highland site or between TINAMBACAN and the 490m highland site

$h_2$ : Antenna height above sea level at the 490m highland site

$d_1$ : Distance between BALOD and the obstruction or between TINAMBACAN and the obstruction

$d_2$ : Distance between the 490m highland site and the obstruction

$\beta$ : Altitude at TINAMBACAN

BALOD station minimum required antenna height if a back-to-back coupling antenna system is used at 490m highland site:

$$\begin{aligned}
 h_1 &= \frac{(80\text{m} + 20\text{m} + 8\text{m}) \times 24500\text{m} - (490\text{m} + 15\text{m}) \times 1500\text{m}}{23000\text{m}} \\
 &+ \frac{1500\text{m} \times 24500\text{m}}{2 \times 4/3 \times 6370000\text{m}} - 53\text{m} \\
 &= 31.3\text{m}
 \end{aligned}$$

TINAMBACAN station minimum required antenna height if a back-to-back coupling antenna system is used at the 490m highland site:

$$\begin{aligned}
 h_1 &= \frac{(300\text{m}+20\text{m}+15.4\text{m}) \times 21000\text{m} - (496\text{m}+15\text{m}) \times 10500\text{m}}{10500\text{m}} \\
 &+ \frac{10500\text{m} \times 21000\text{m}}{2 \times 4/3 \times 6370000\text{m}} - 145\text{m} \\
 &= 33.8\text{m}
 \end{aligned}$$

\* The antenna height at the 490m highland site is 15m.

◦ Minimum required antenna height at the BALOD station if a reflector plate is installed in the 490m highland site:

$$\begin{aligned}
 h_1 &= \frac{(432\text{m} + 70\text{m} + 9.1\text{m}) \times 24500\text{m} - (490\text{m}+5\text{m}) \times 22500\text{m}}{2000\text{m}} \\
 &+ \frac{22500\text{m} \times 24500\text{m}}{2 \times 4/3 \times 6370000\text{m}} - 53\text{m} \\
 &= 59.2\text{m}
 \end{aligned}$$

\* The minimum required antenna height with respect to the other obstruction between BALOD and the 490m highland site is 31.9m.

◦ Minimum required antenna height at the TINAMBACAN station if a reflector plate is installed in the 490m highland site:

$$\begin{aligned}
 h_1 &= \frac{(300\text{m}+20\text{m}+15.4\text{m}) \times 21000\text{m} - (490\text{m}+5\text{m}) \times 10500\text{m}}{10500\text{m}} \\
 &+ \frac{10500\text{m} \times 21000\text{m}}{2 \times 4/3 \times 6370000\text{m}} - 145\text{m} \\
 &= 43.8\text{m}
 \end{aligned}$$

Profile

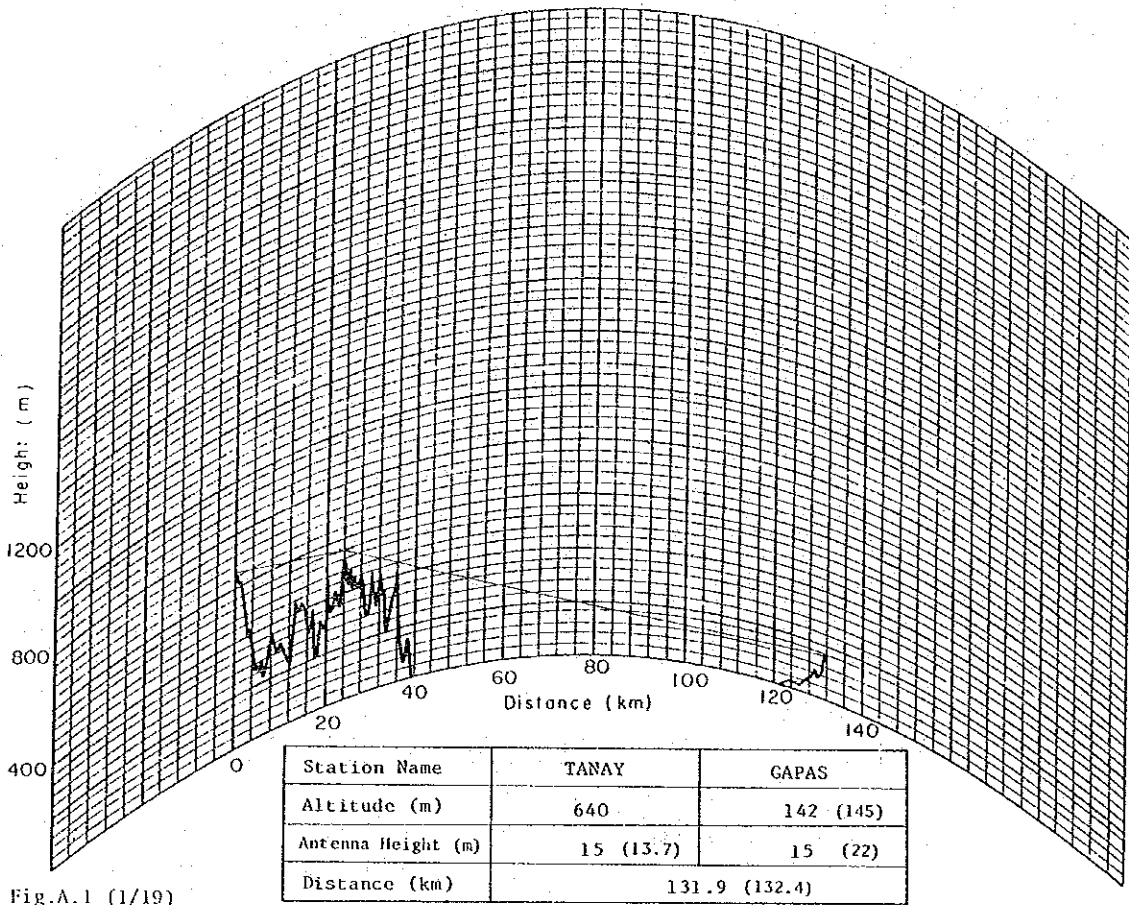


Fig.A.1 (1/19)

Profile

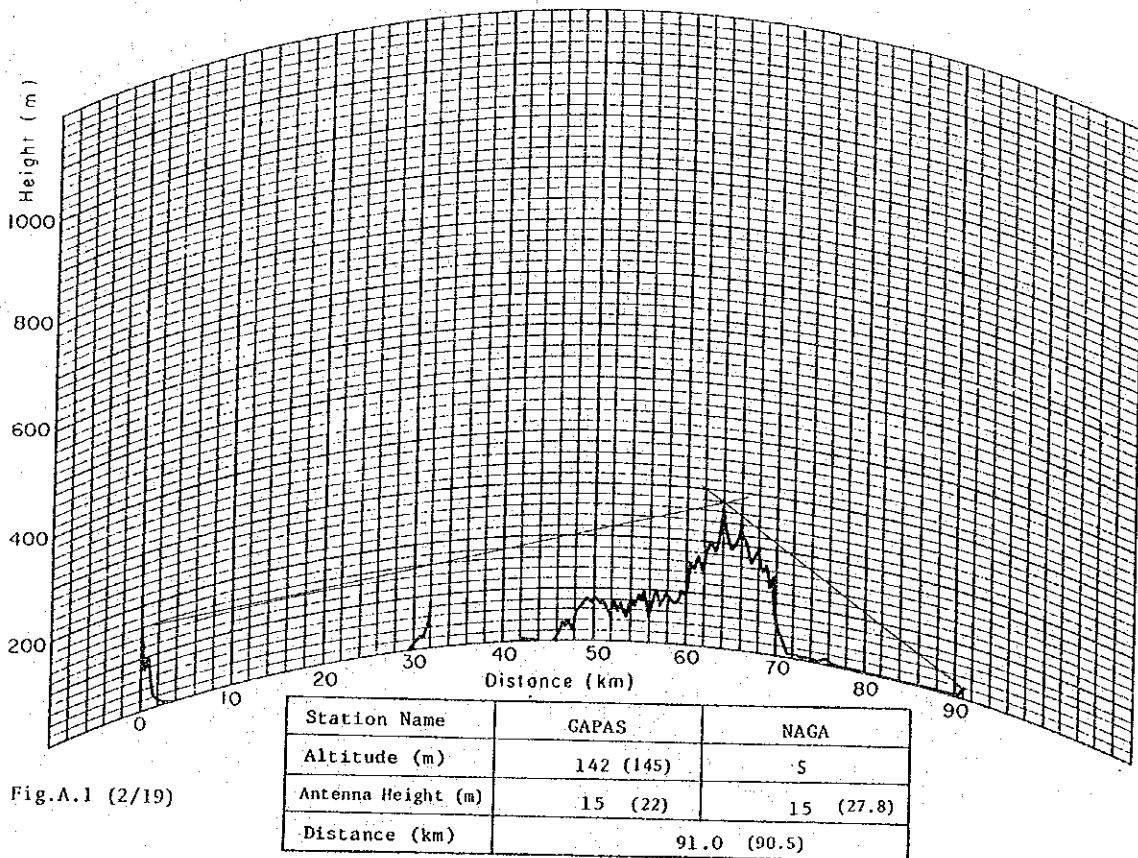


Fig.A.1 (2/19)

Profile

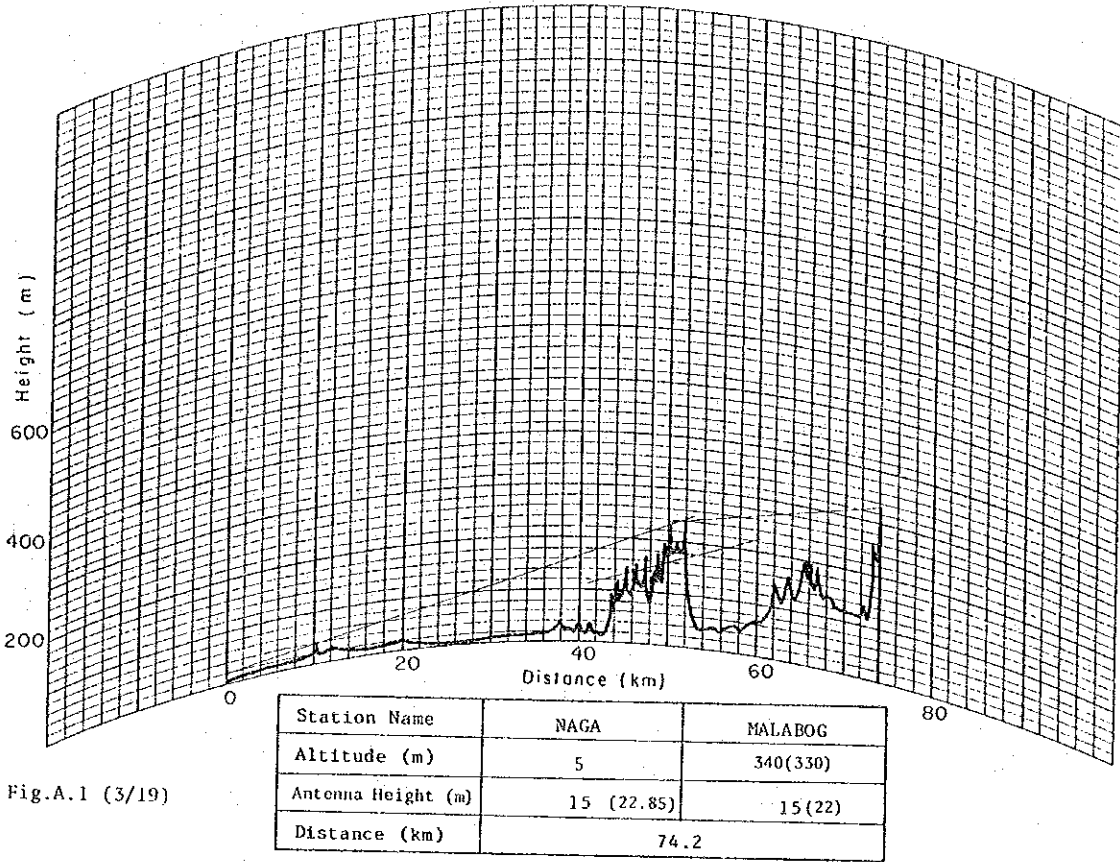


Fig.A.1 (3/19)

Profile

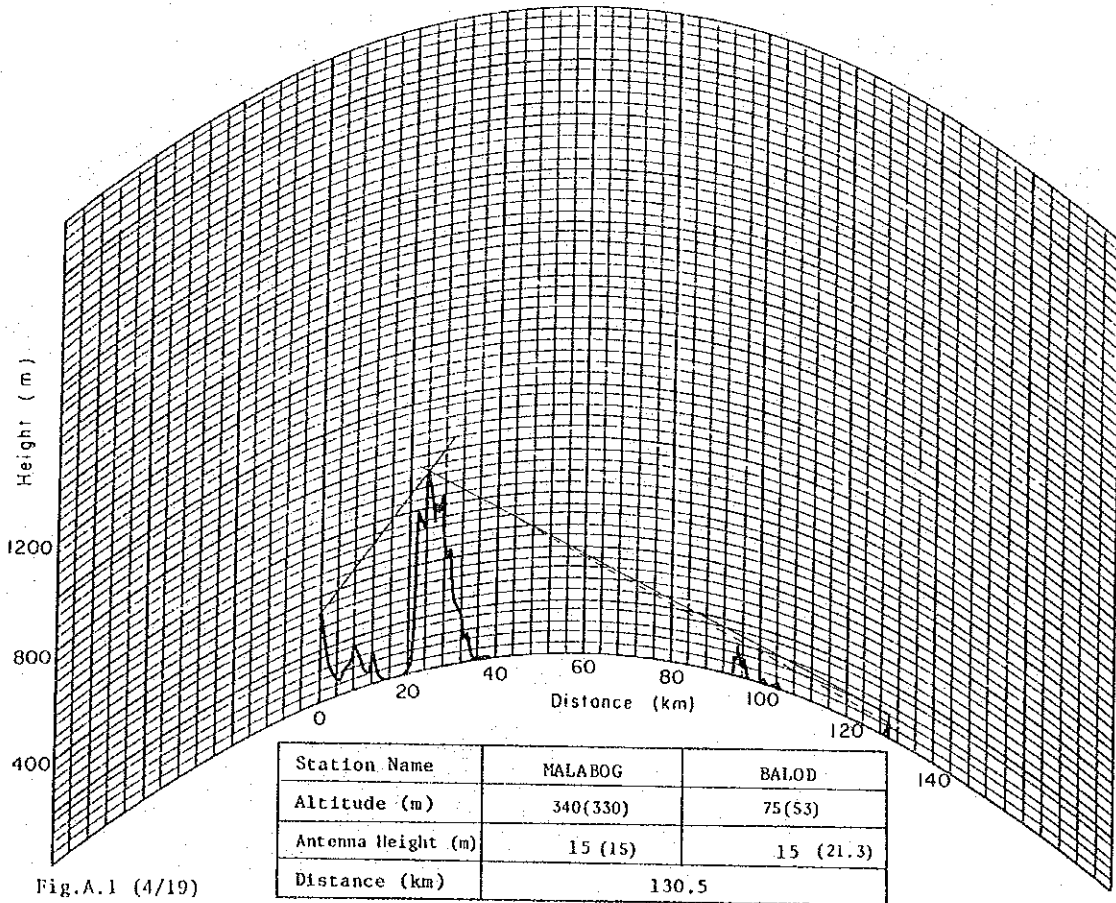


Fig.A.1 (4/19)

Profile

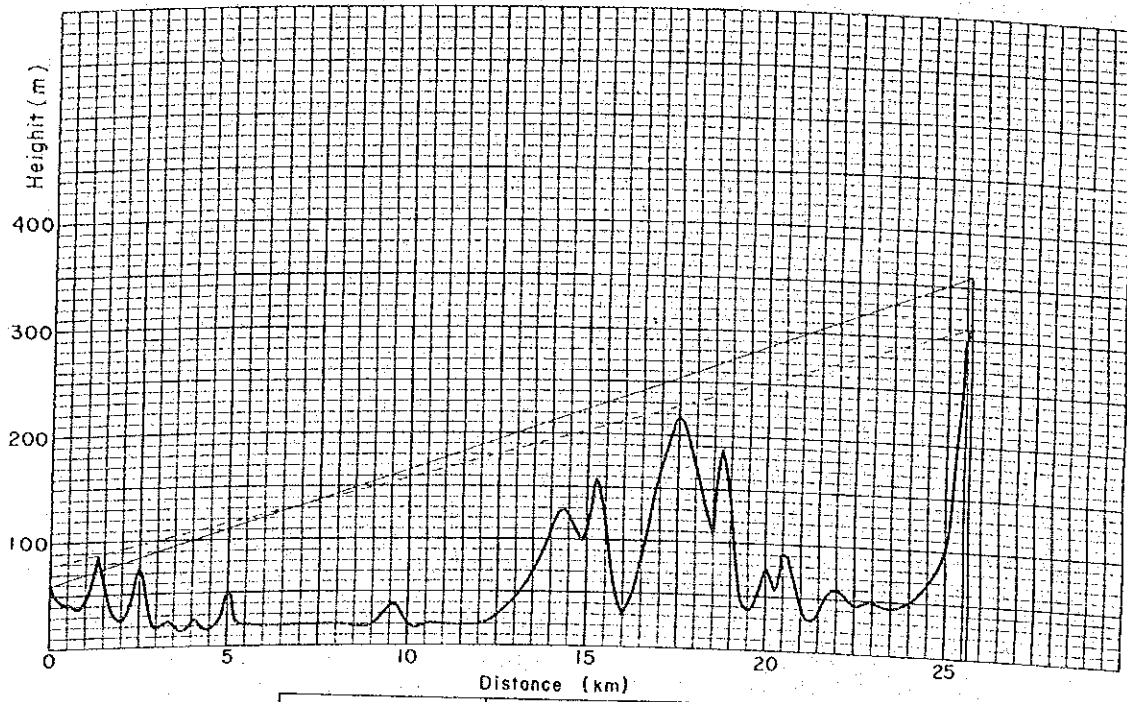


Fig. A.1 (5/19)

Station Name	BALOD	CAPACUAN
Altitude (m)	60(53)	360(310)
Antenna Height (m)		
Distance (km)	25.7	

Profile

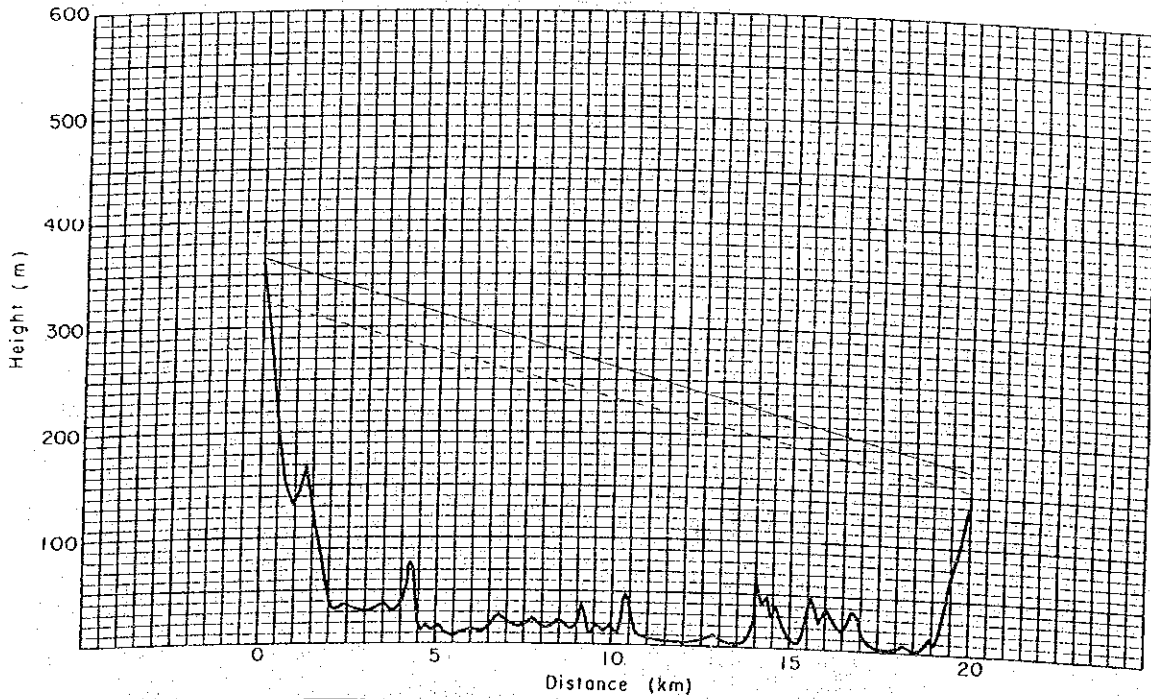


Fig. A.1 (6/19)

Station Name	CAPACUAN	TINAMBACAN
Altitude (m)	360(310)	140(145)
Antenna Height (m)	7 (15)	35 (10)
Distance (km)	20.0	



Profile

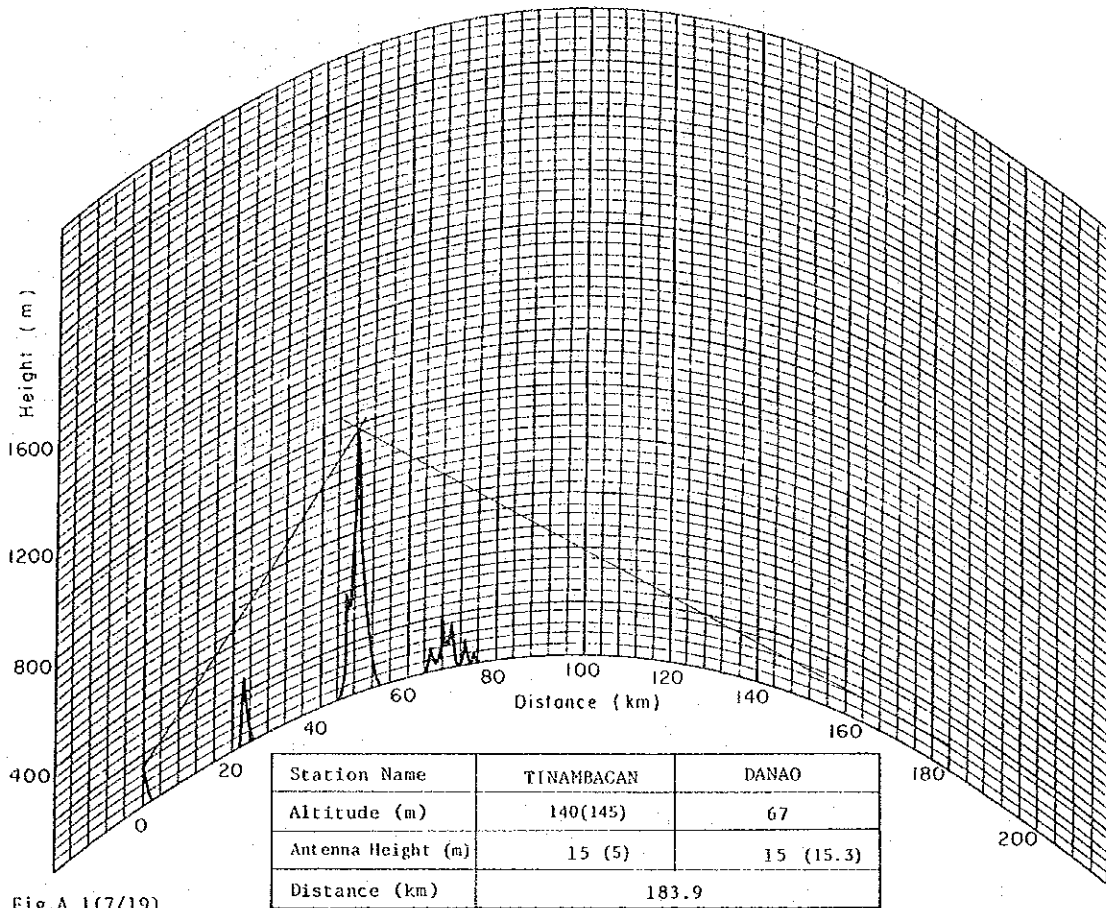


Fig.A.1(7/19)

Profile

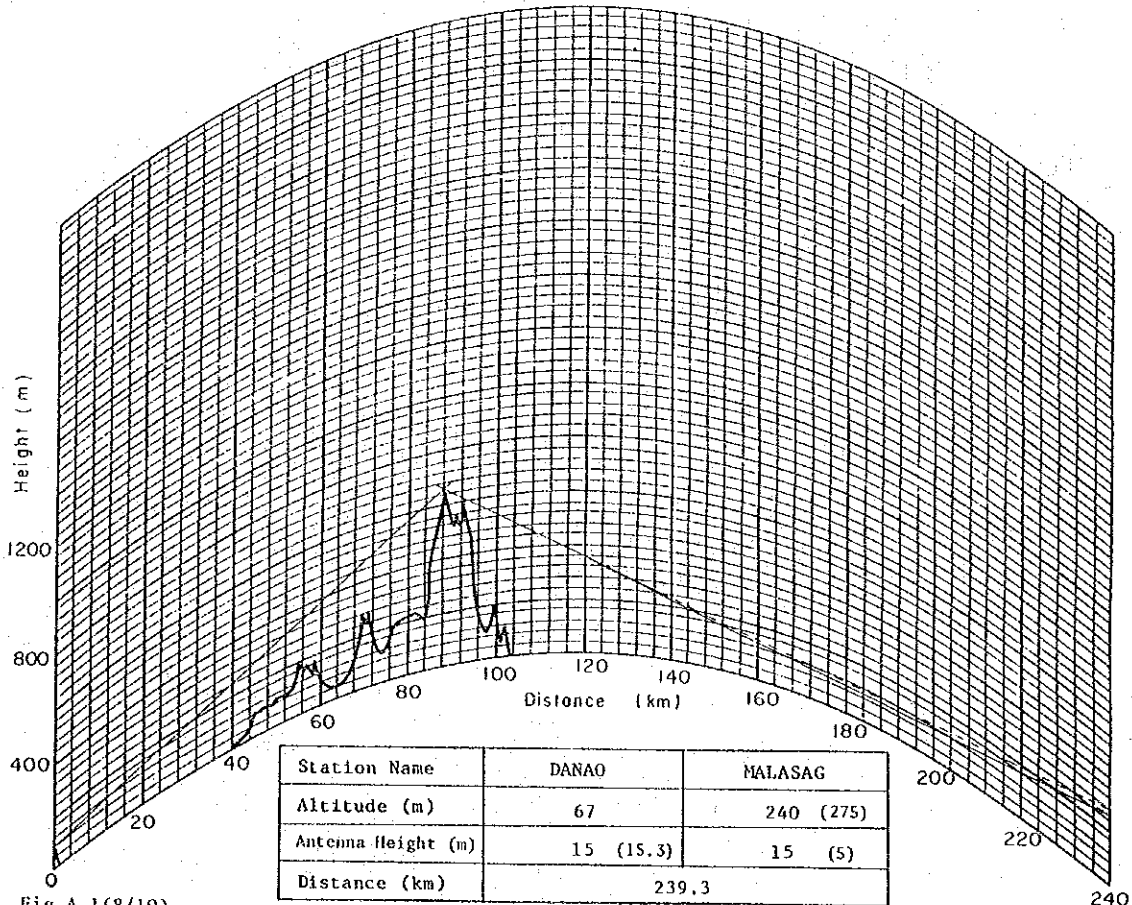


Fig.A.1(8/19)

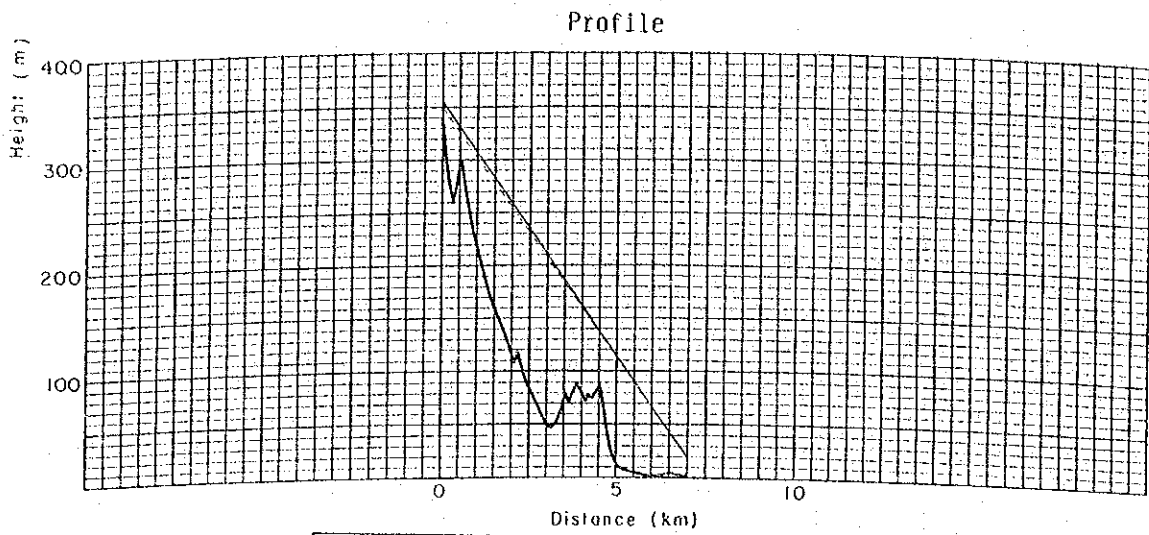


Fig. A.1(9/19)

Station Name	MALABOG-1	LEGASPI
Altitude (m)	340(330)	5
Antenna Height (m)	15 (20)	15 (20)
Distance (km)	7.0	

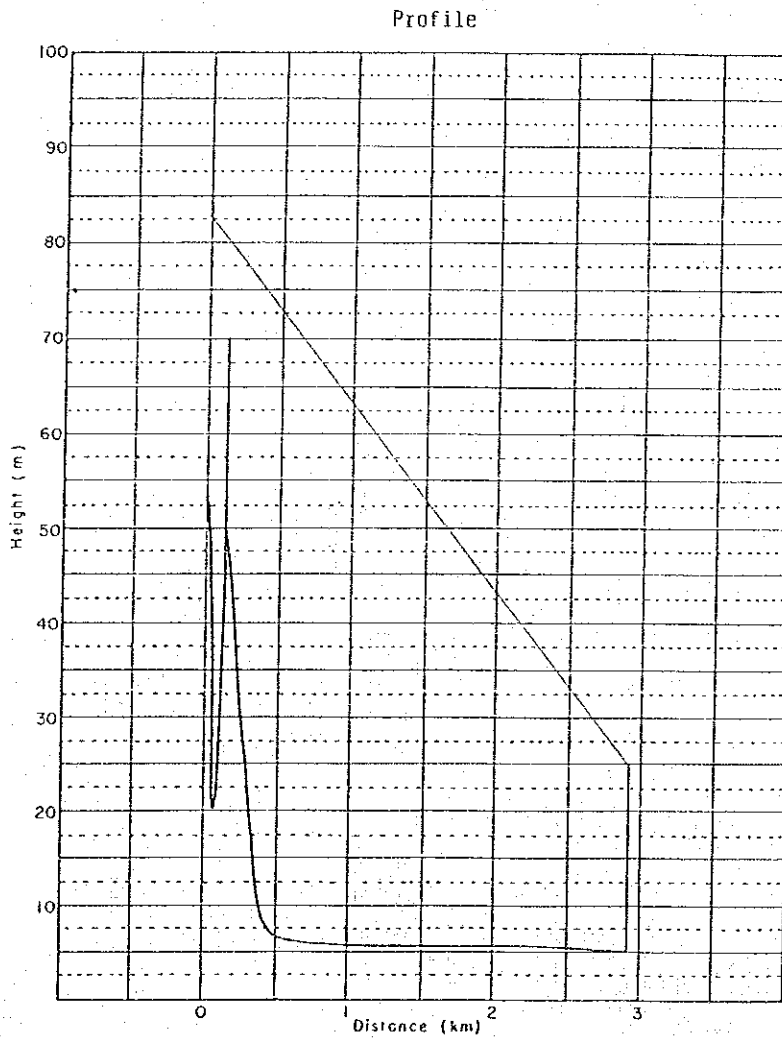


Fig. A.1(10/19)

Station Name	BALOD	CATARMAN
Altitude (m)	53	5
Antenna Height (m)	30	20
Distance (km)	2.9	

Profile

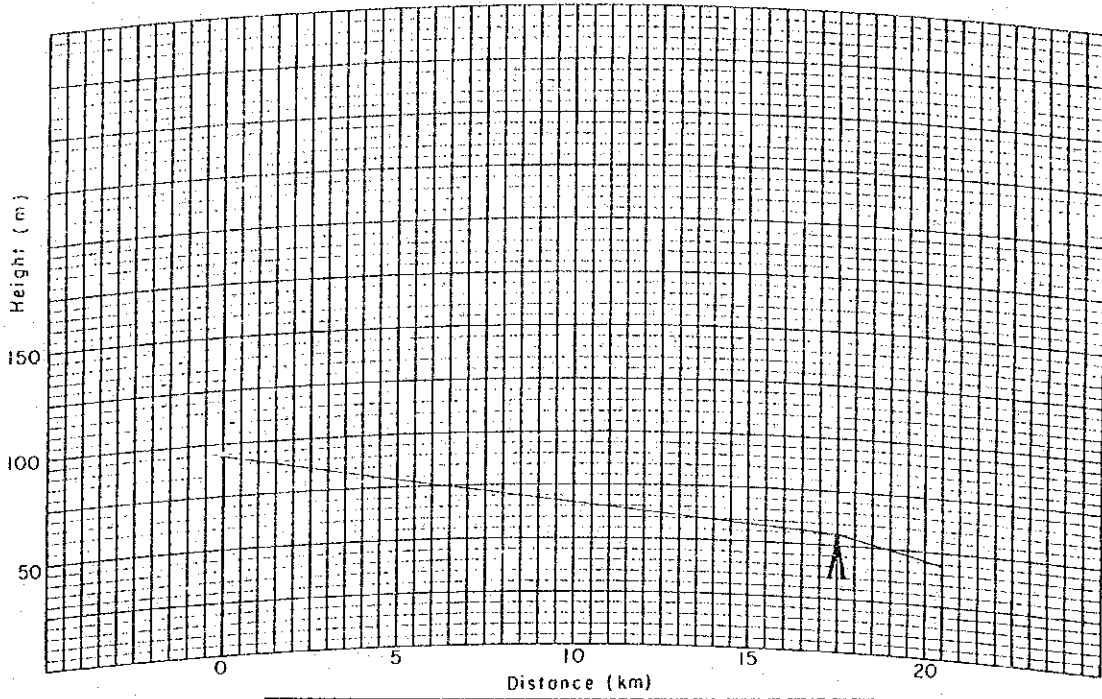


Fig.A.1(11/19)

Station Name	DANAO	MACTAN RADAR
Altitude (m)	67	24.8
Antenna Height (m)	20	20
Distance (km)	20.5	

Profile

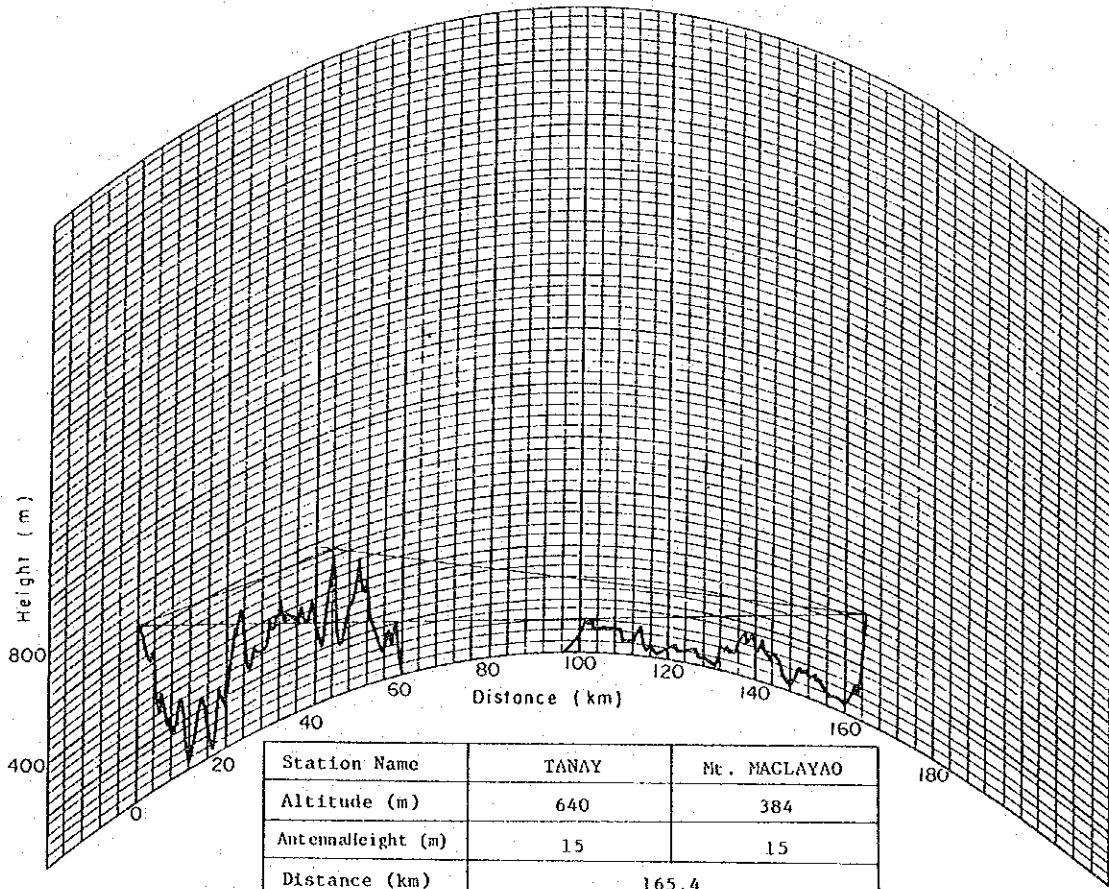


Fig. A.1( 12/19)

Station Name	TANAY	Mt. MACLAYAO
Altitude (m)	640	384
Antenna Height (m)	15	15
Distance (km)	165.4	

Profile

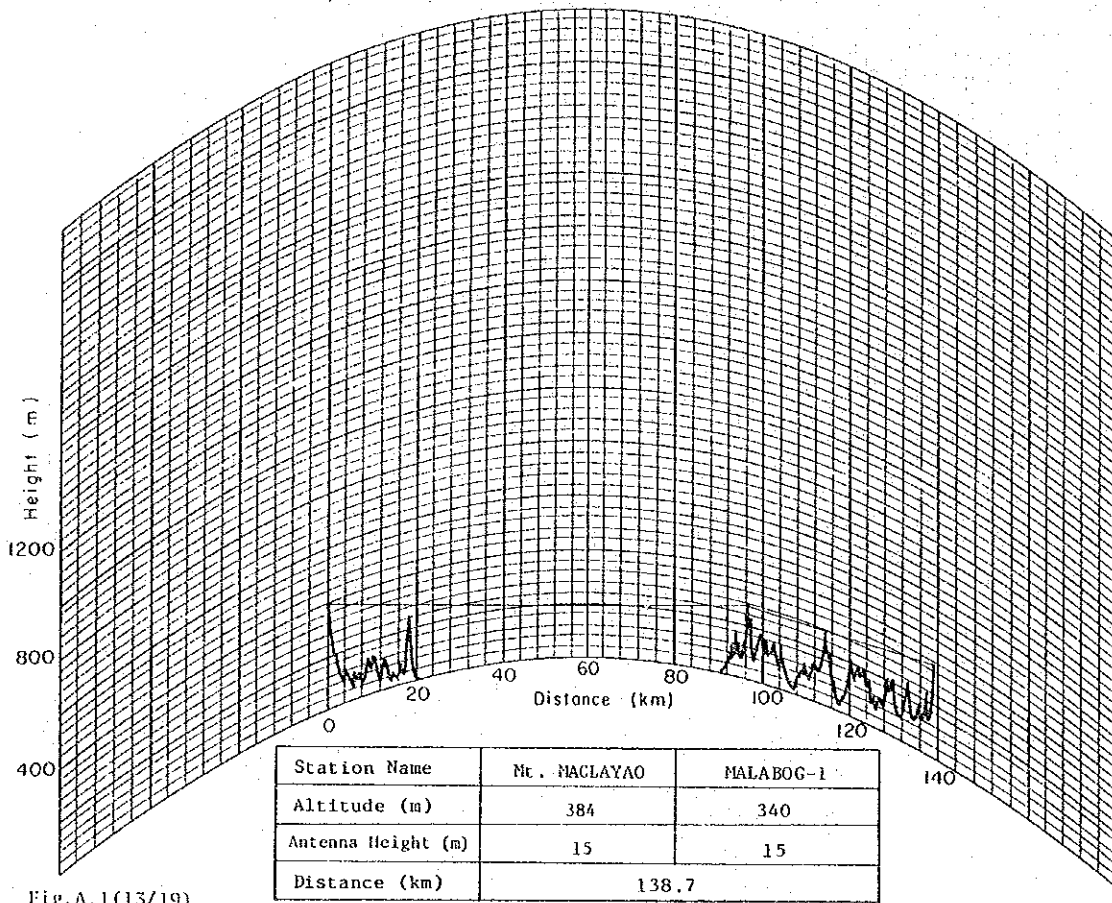


Fig. A.1(13/19)

Profile

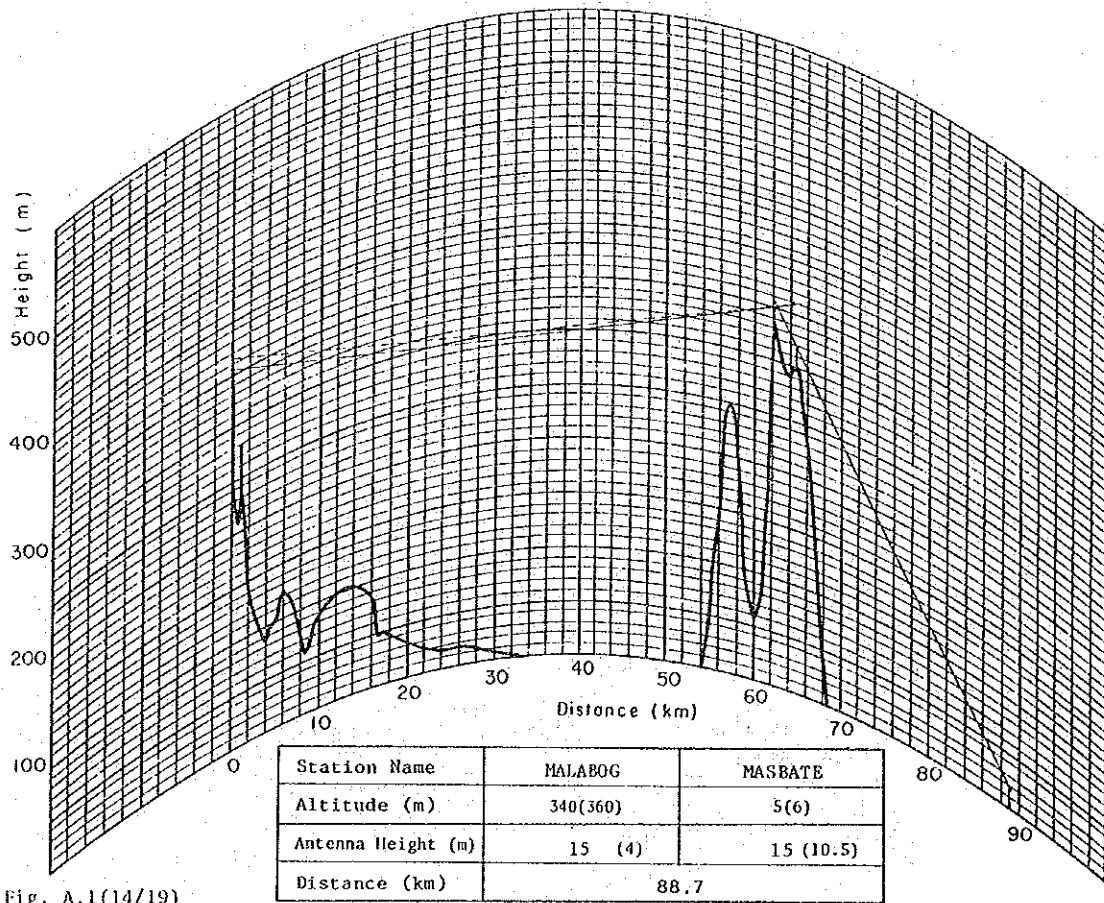


Fig. A.1(14/19)

Profile

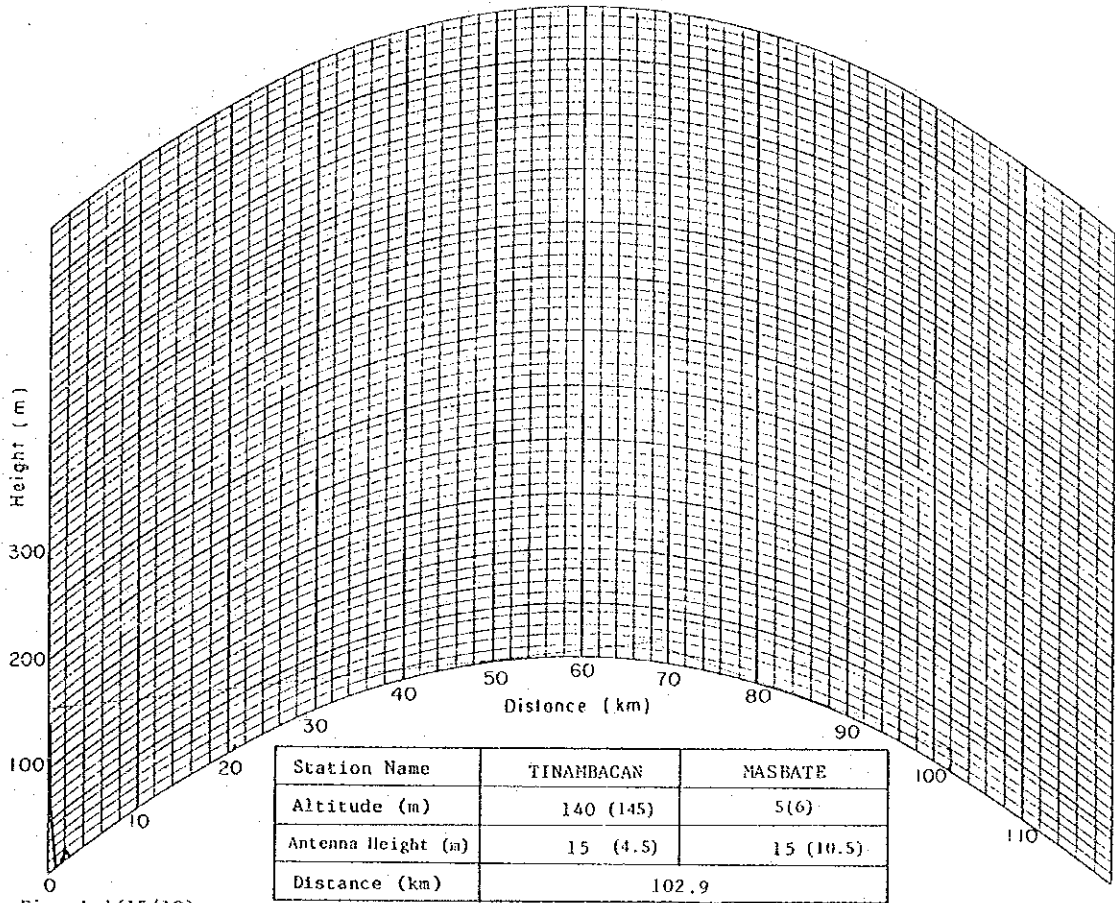


Fig. A.1(15/19)

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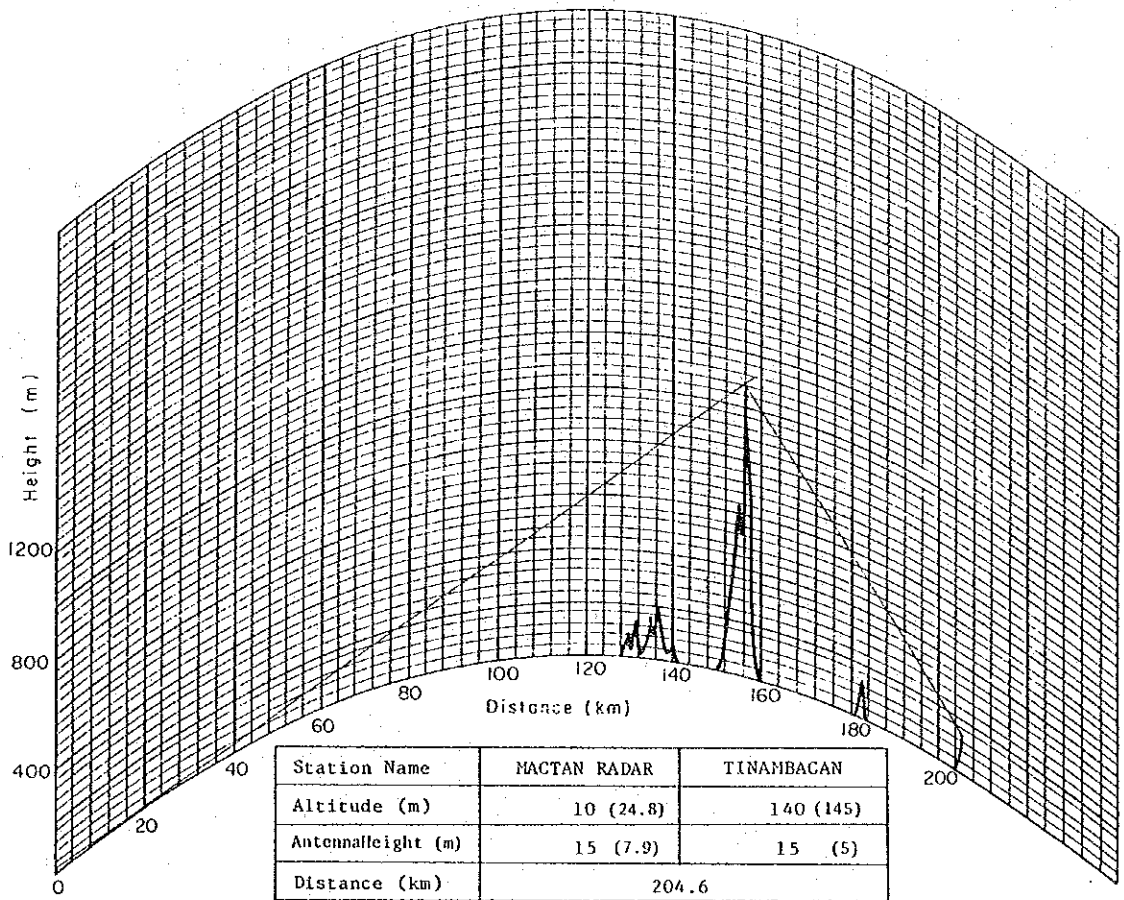


Fig.A.1(16/19)

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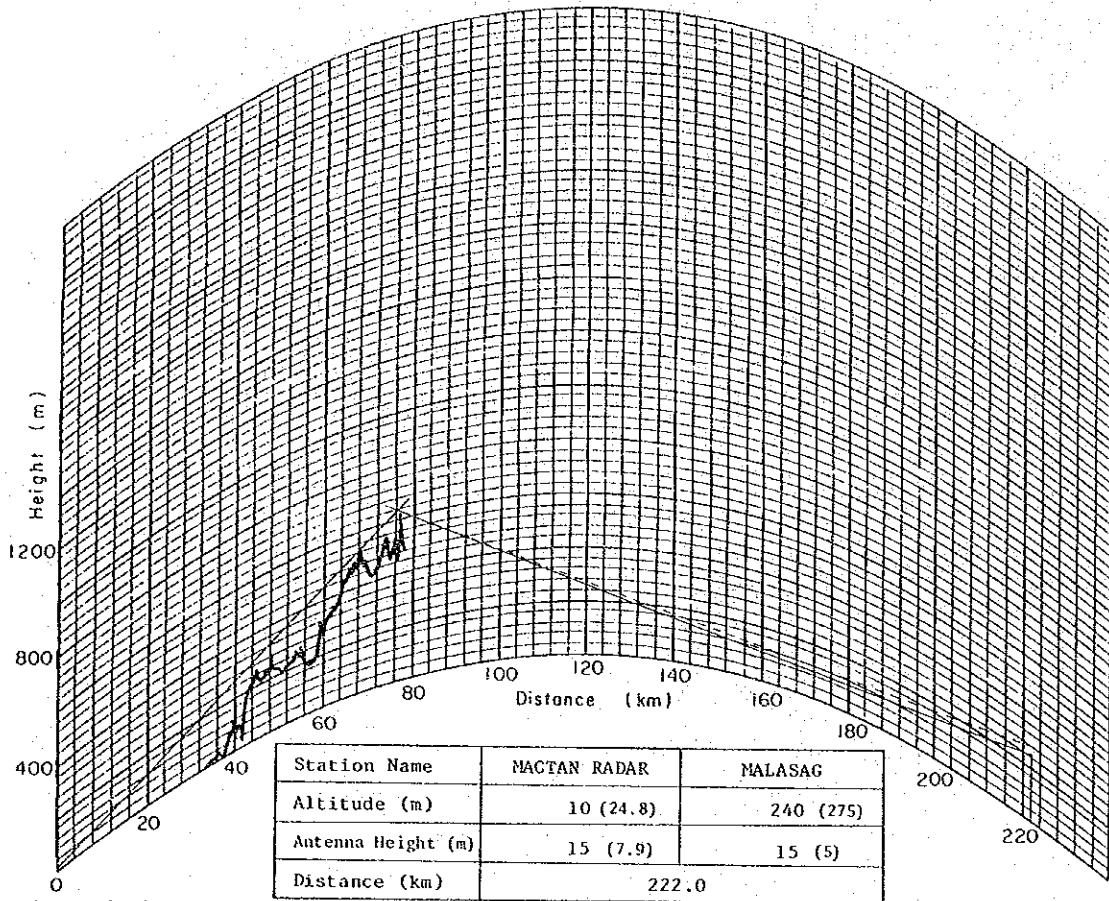


Fig.A.1(17/19)

### Profile

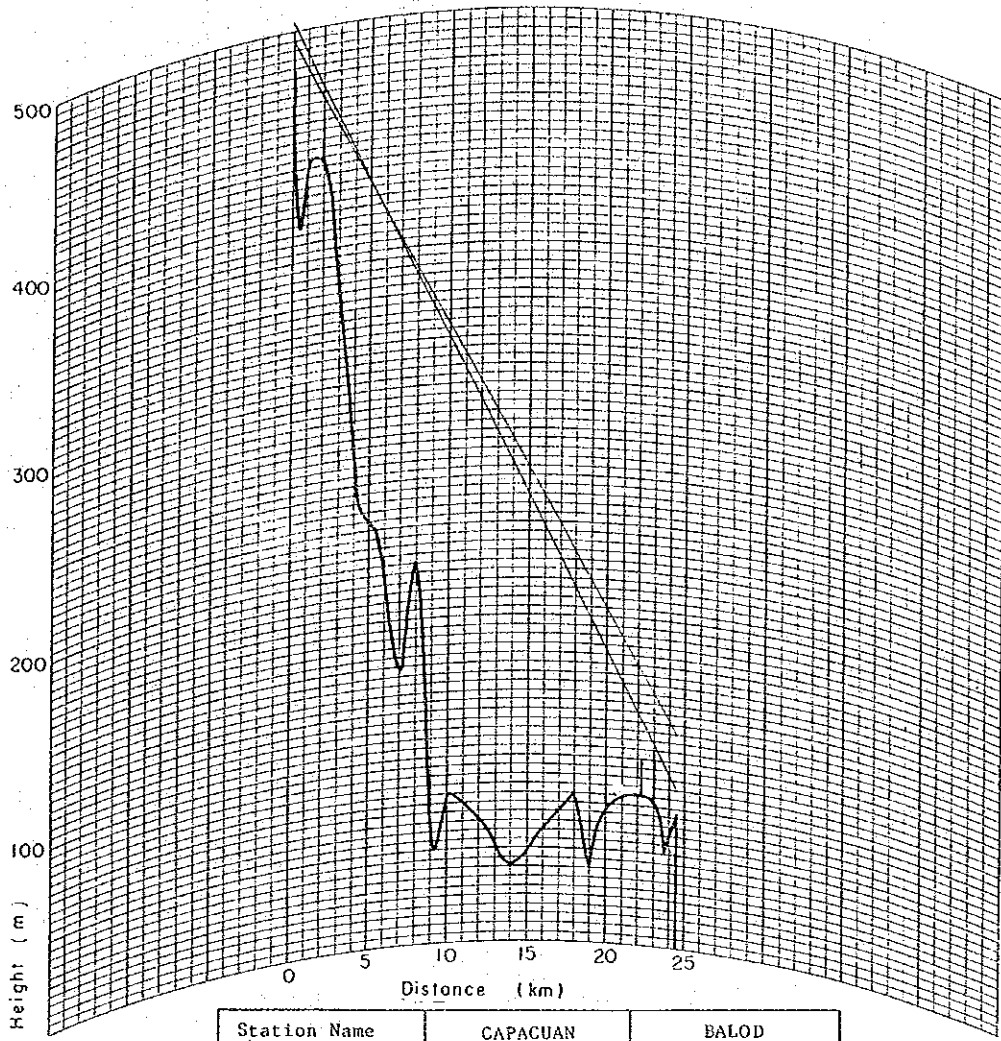


Fig. A.1(18/19)

Station Name	CAPACUAN	BALOD
Altitude (m)	490	55
Antenna Height (m)	-	15
Distance (km)	24.5	

### Profile

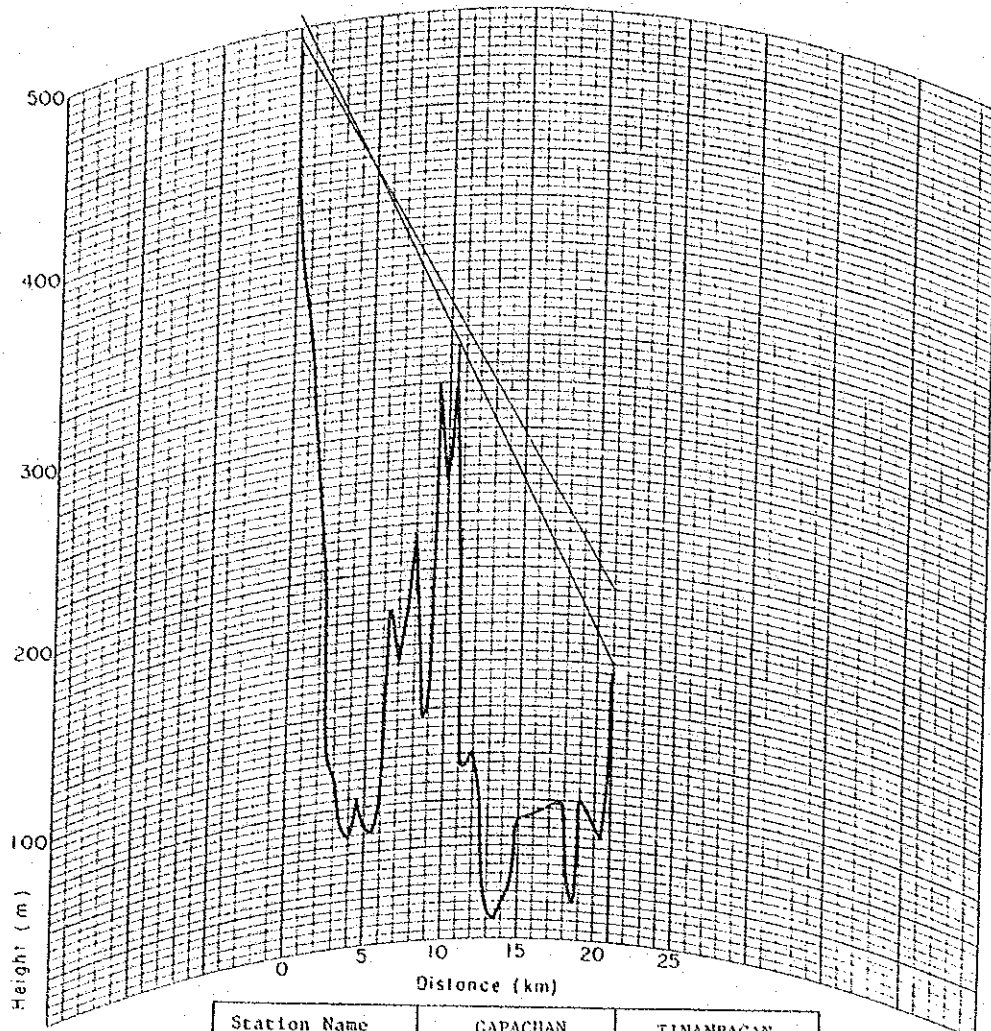


Fig.A.1 (19/19)

Station Name	CAPACUAN	TINANBAGAN
Altitude (m)	490	145
Antenna Height (m)		
Distance (km)	21.0	



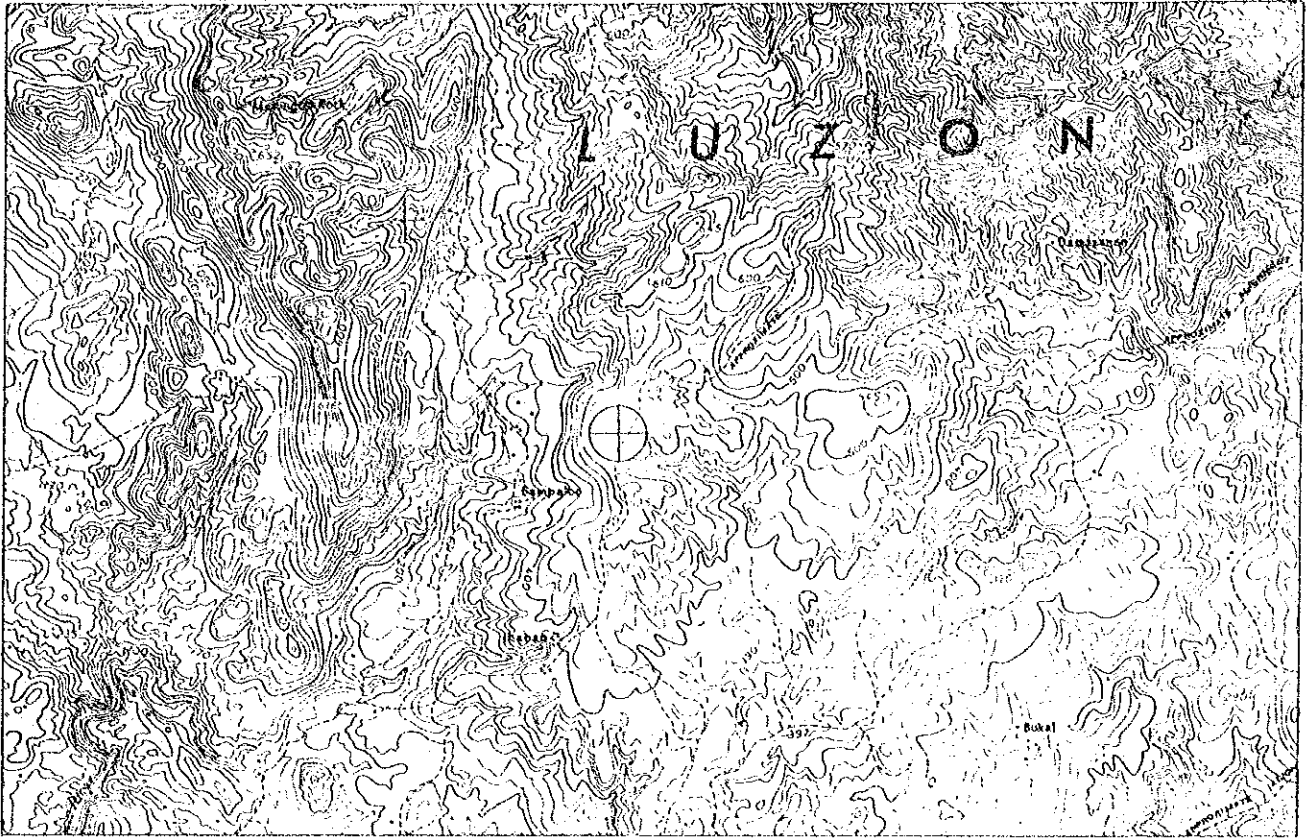


Fig. A.2(1/12)

TANAY

1/250,000

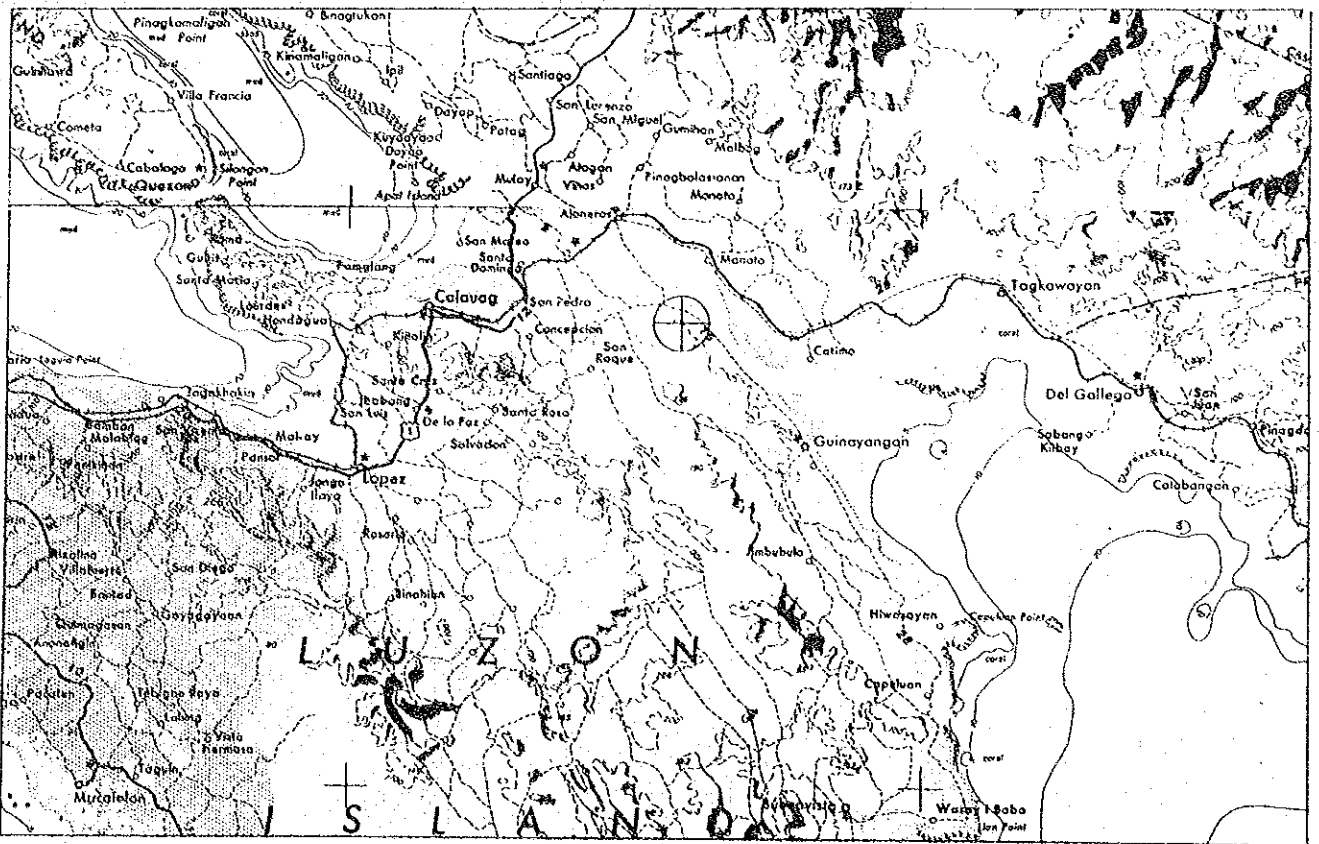


Fig. A.2(2/12)

GAPAS

1/250,000

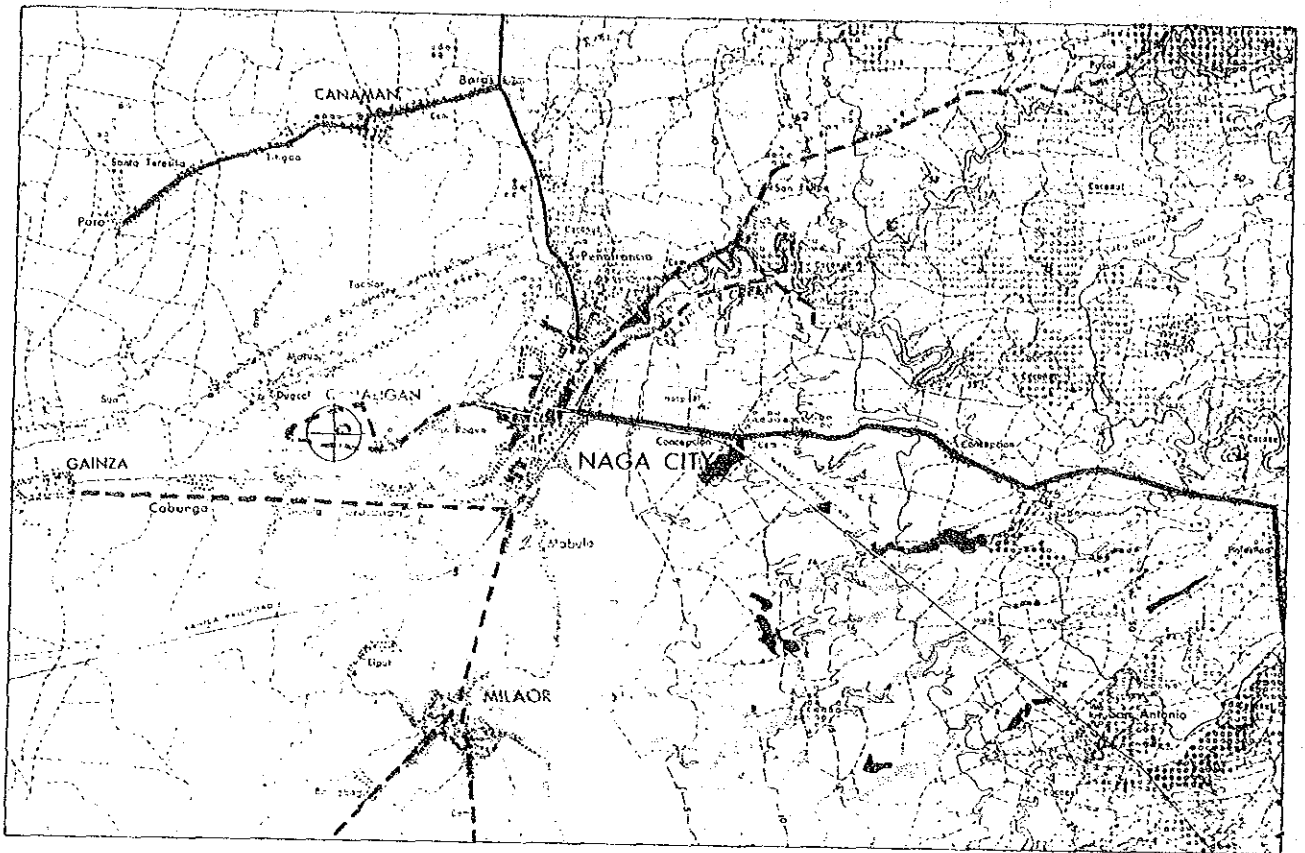


Fig. A.2(3/12)

1/50,000

NAGA

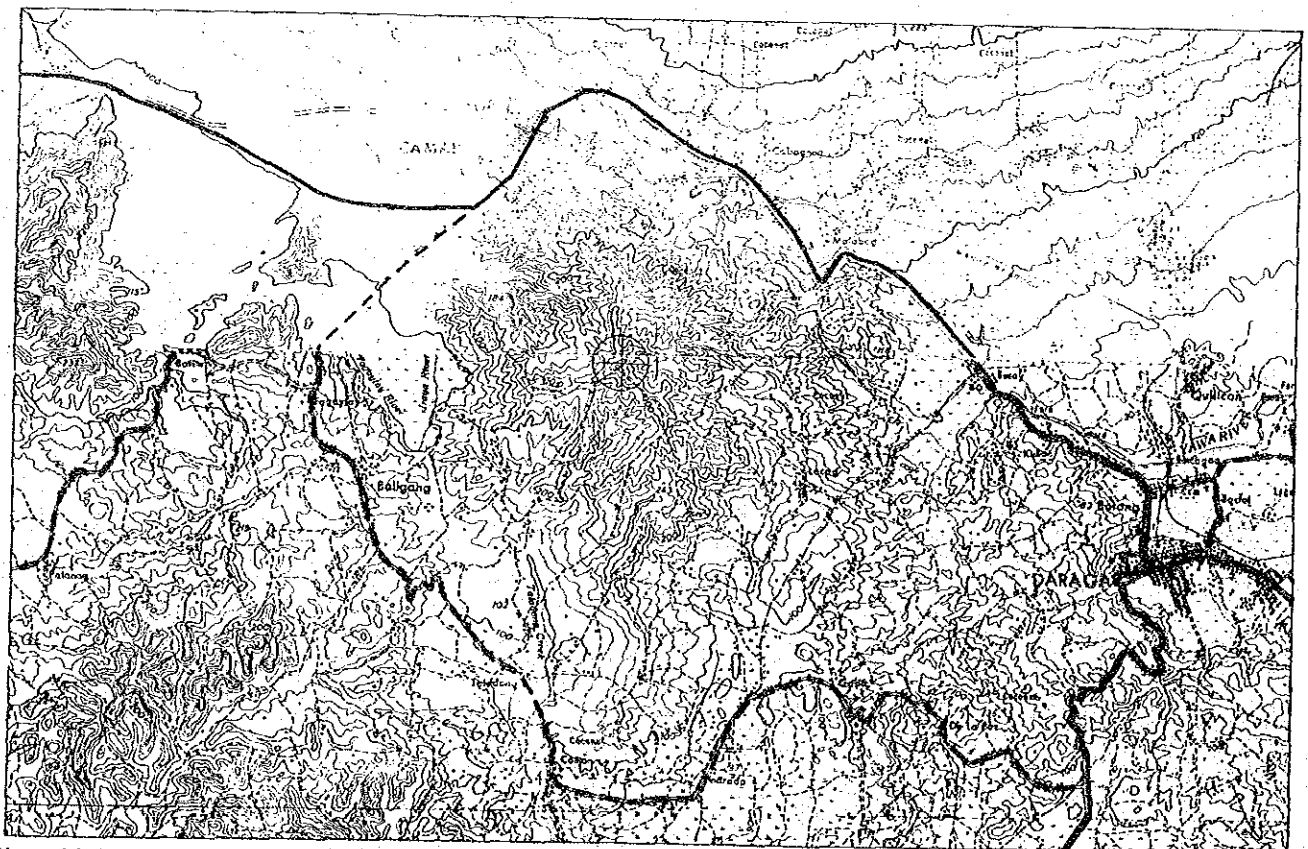


Fig. A.2(4/12)

1/50,000

MALABOG

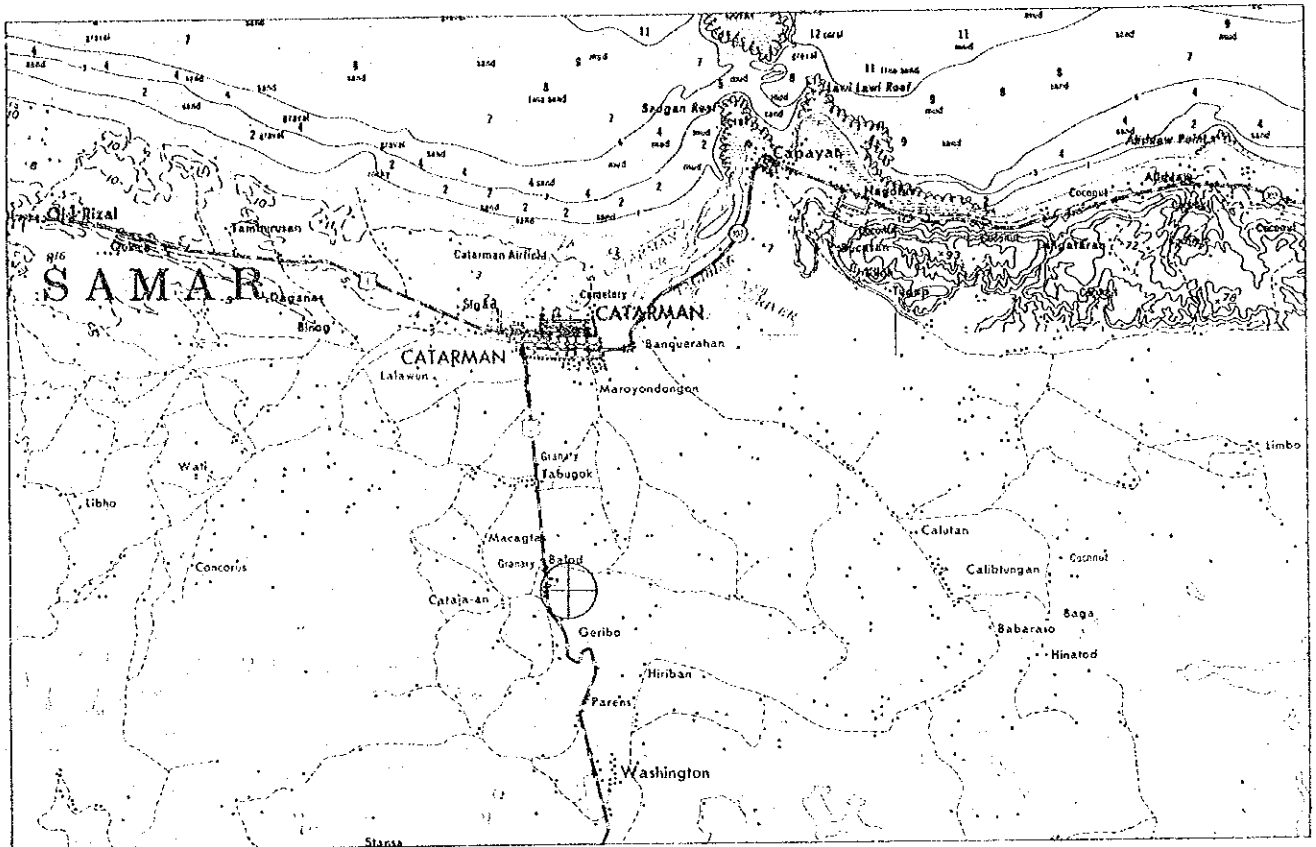


Fig. A.2(5/12)

1/50,000

BALOD

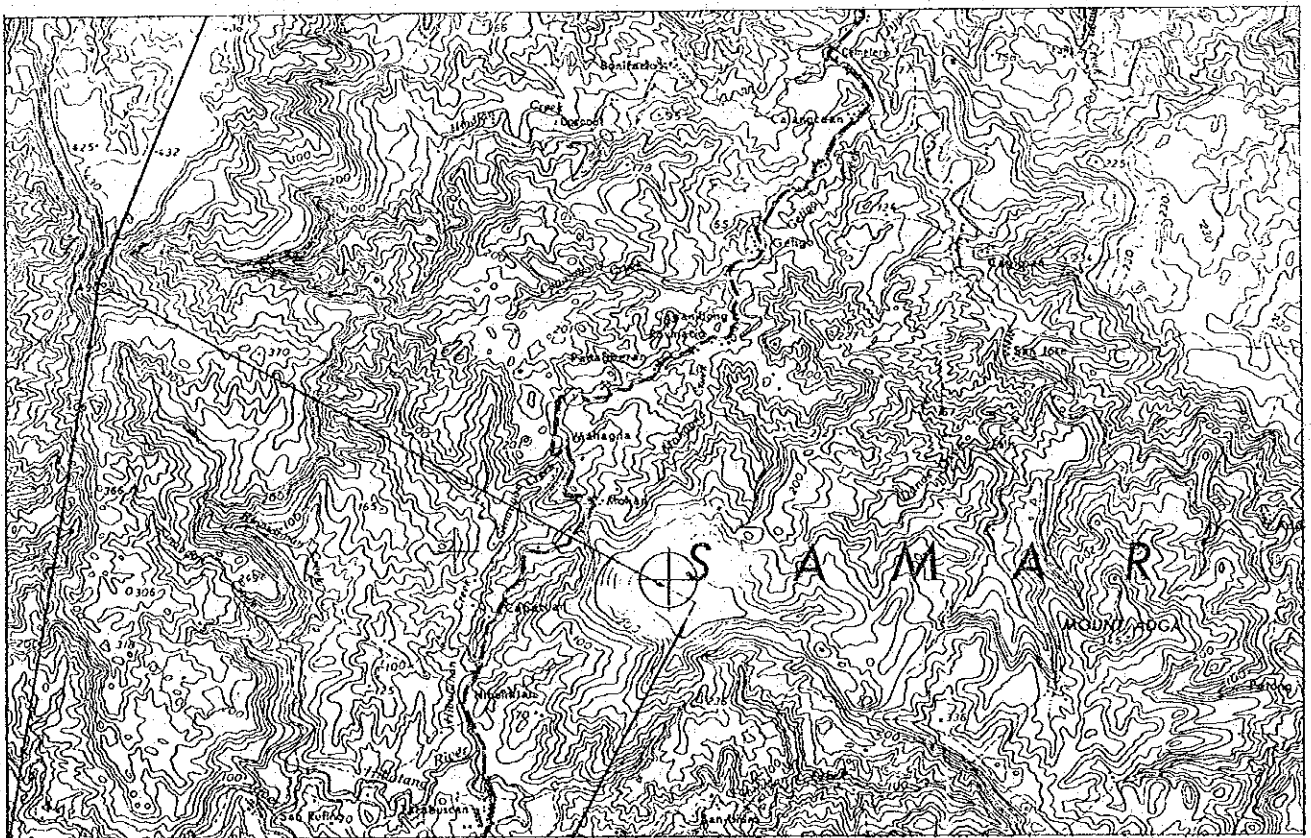


Fig. A.2(6/12)

1/50,000

CAPAGUAN

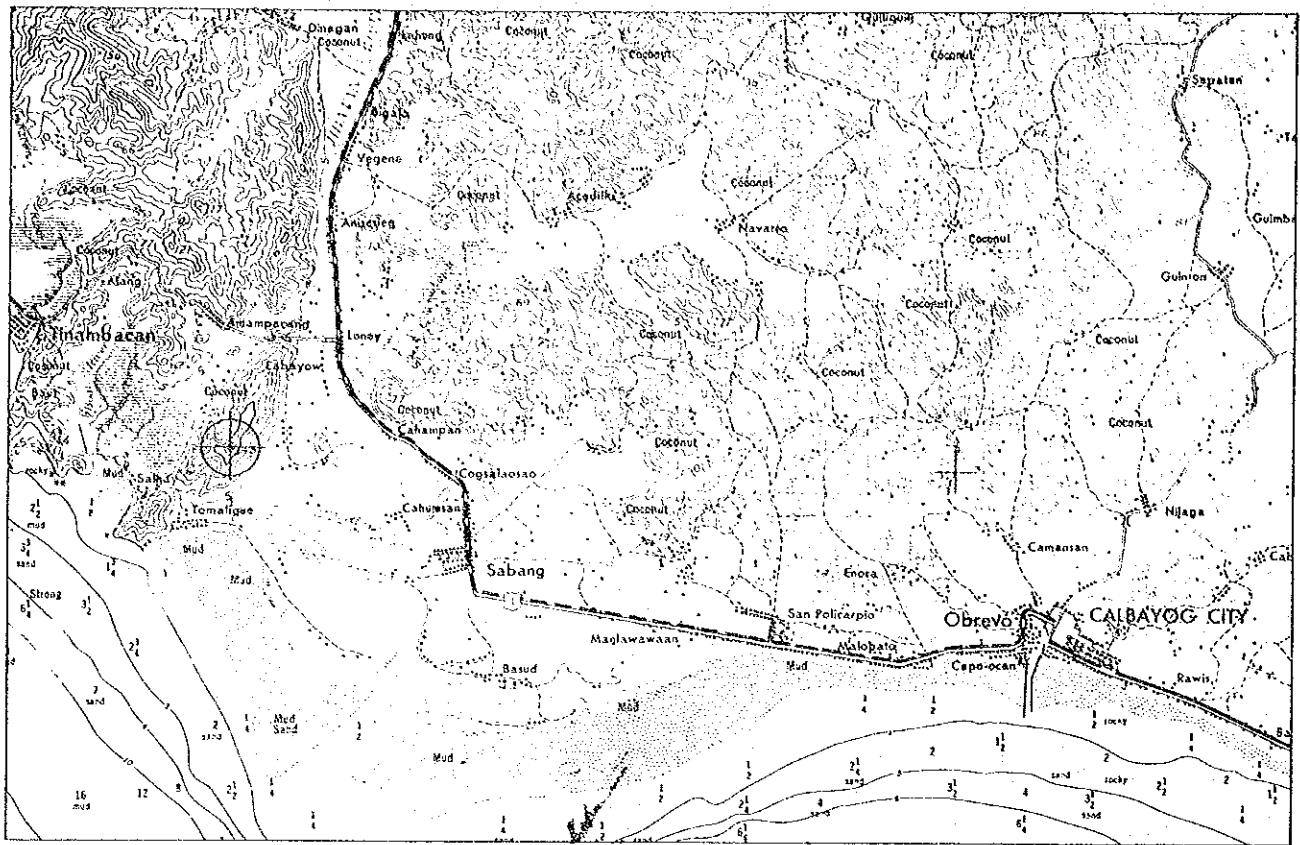


Fig.A.2 (7/12)

1/50,000

TINAMBACAN

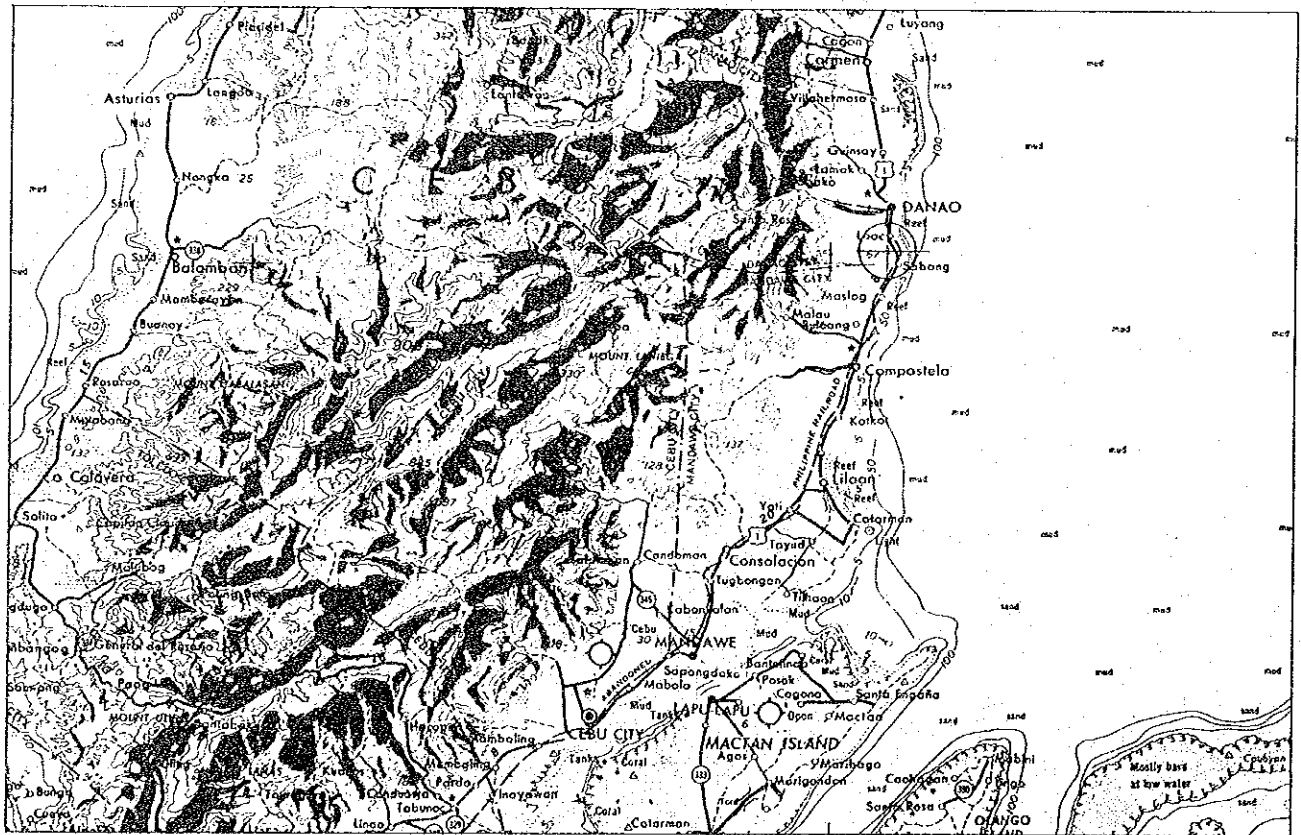


Fig.A.2(8/12)

1/250,000

DANAÓ

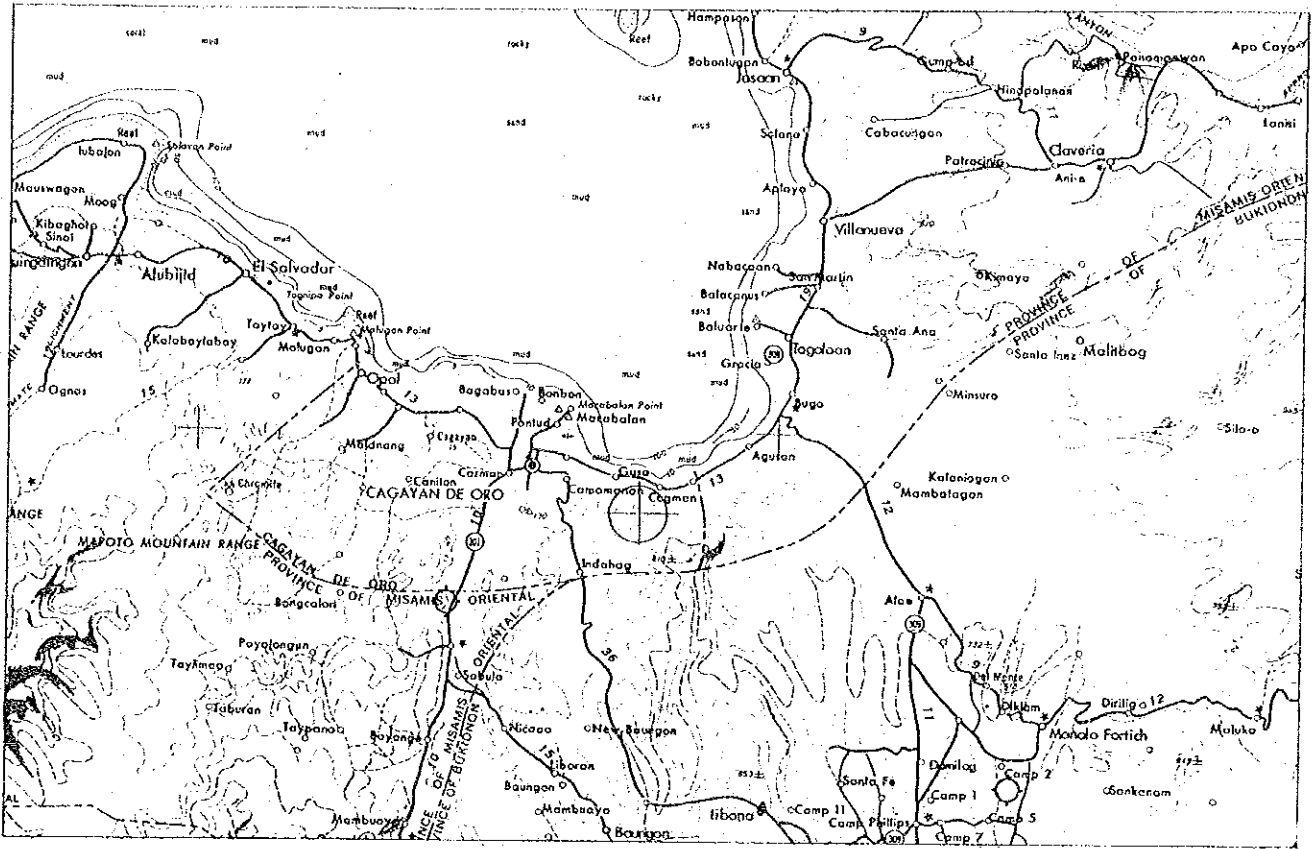


Fig. A.2 (9/12)

CAGAYAN DE ORO

1/250,000

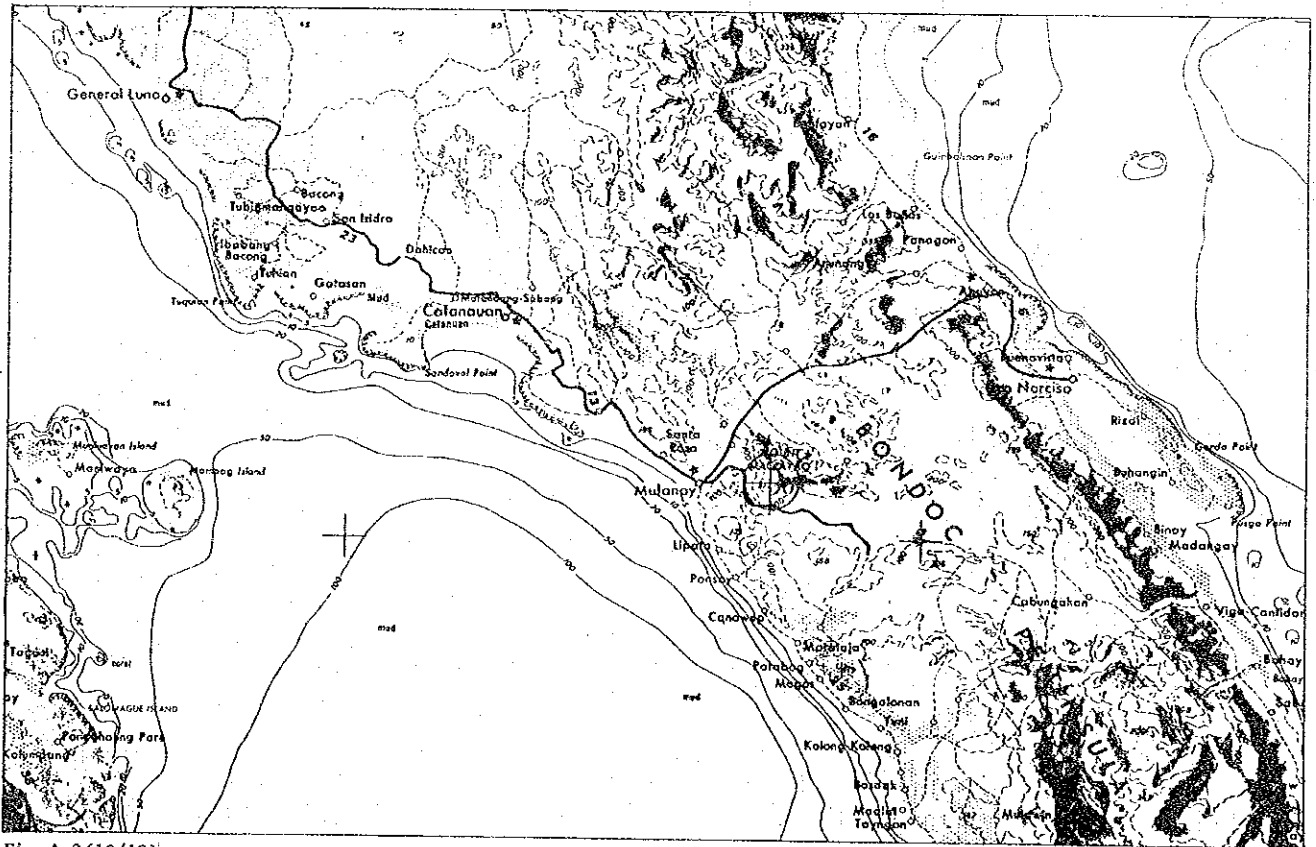


Fig. A.2 (10/12)

MACLAYAO

1/250,000

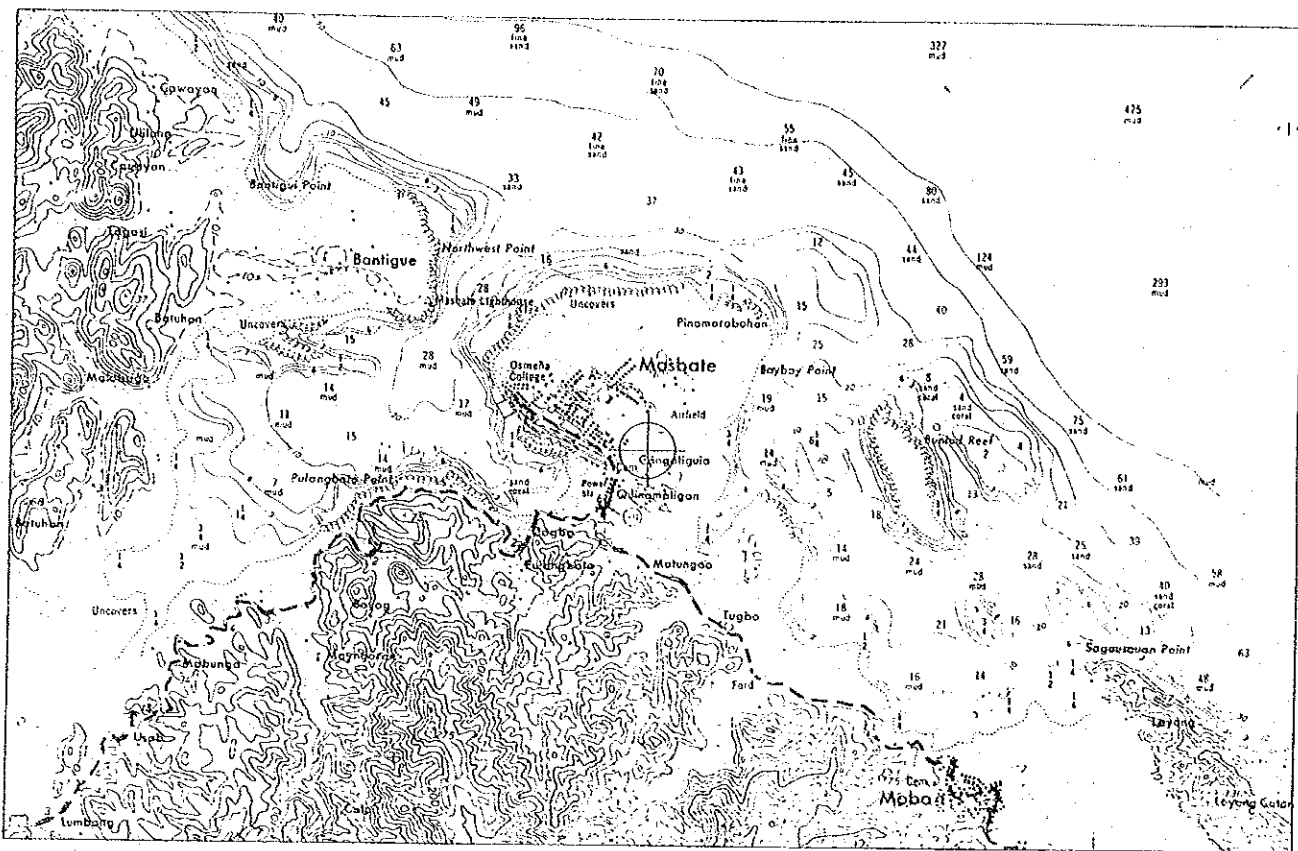


Fig. A.2 (11/12)

MASBATE

1/50,000

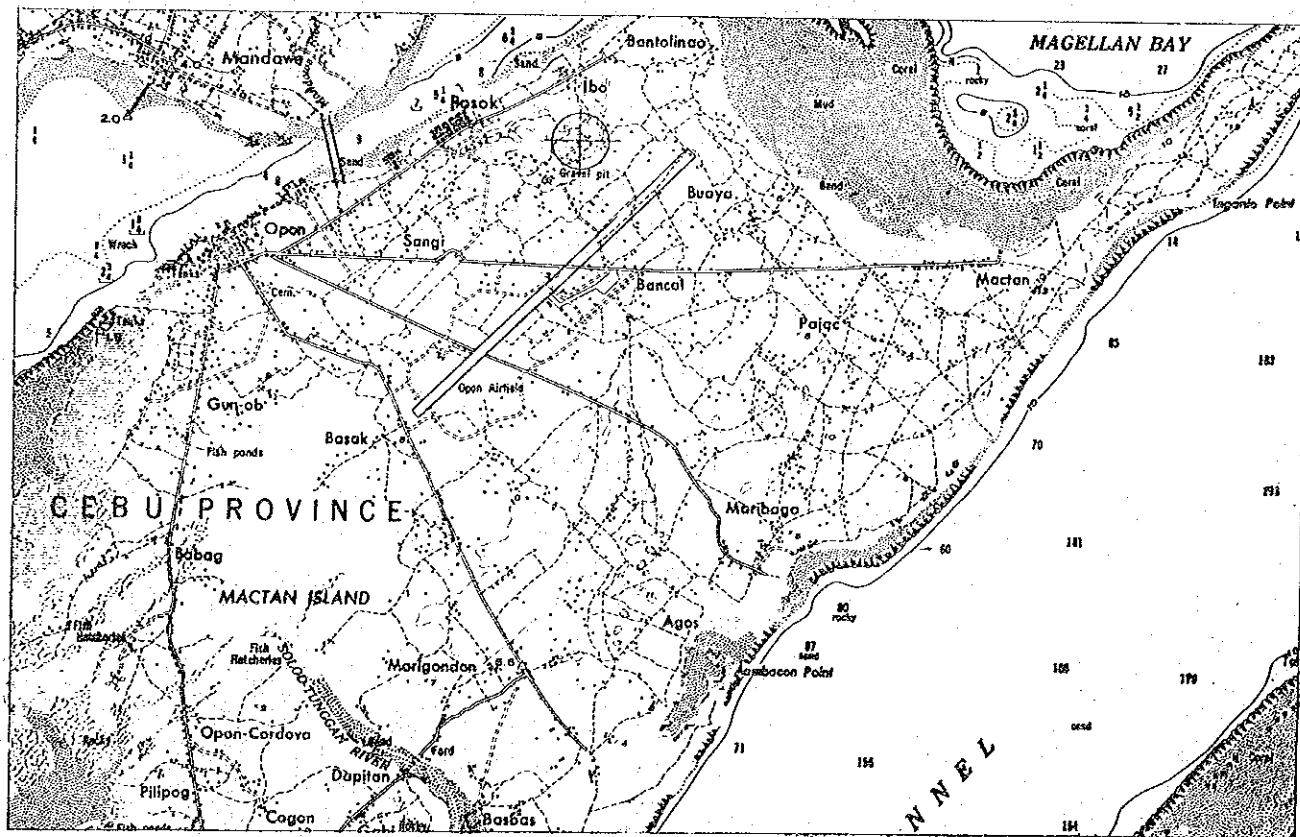


Fig. A.2 (12/12)

CEBU



Receiving Power

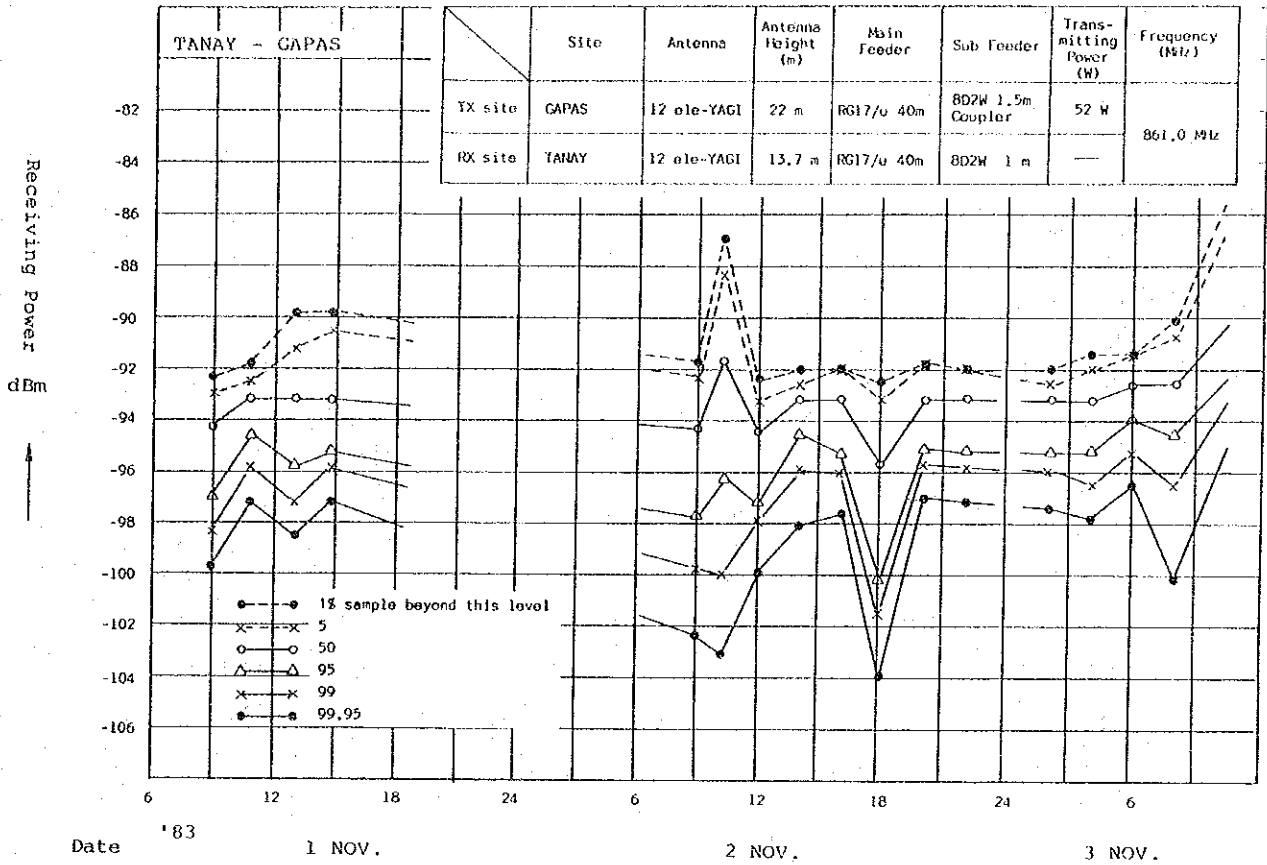


Fig.A.3(1/32)

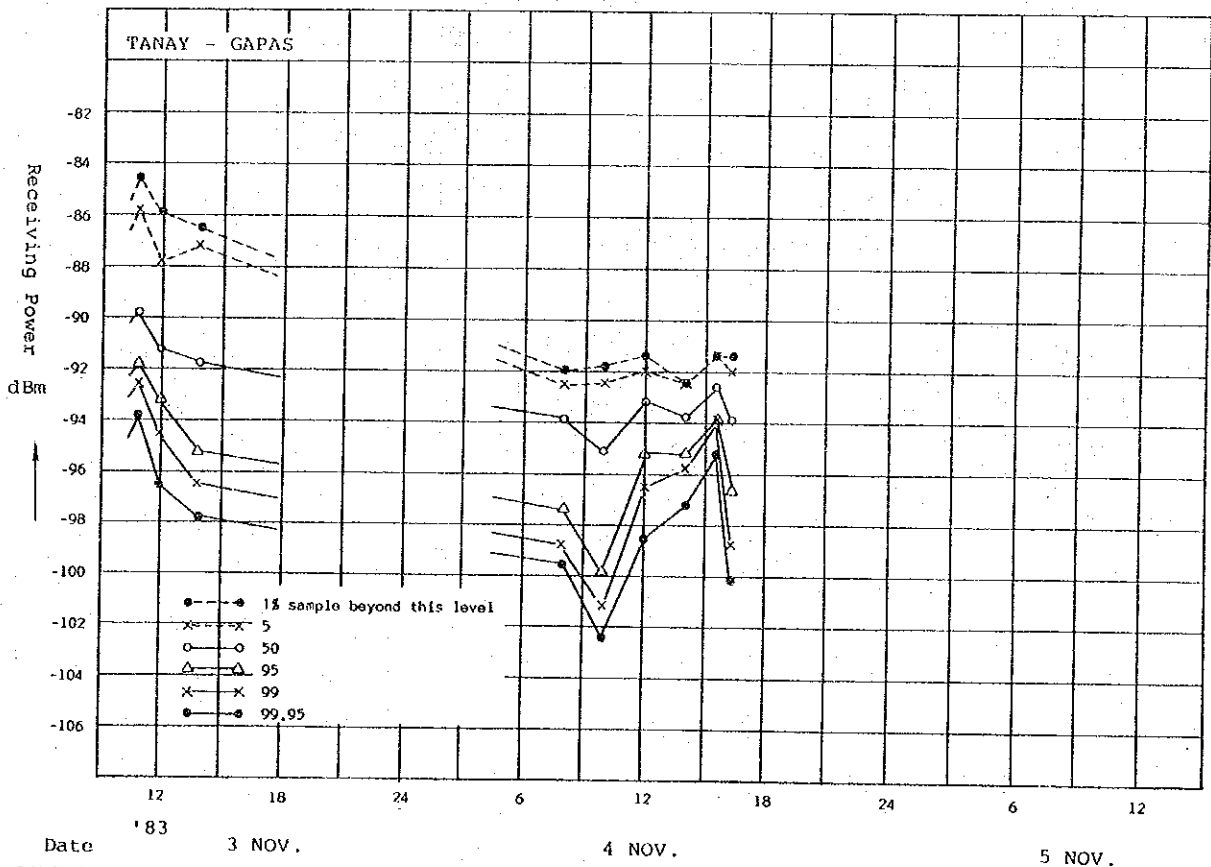


Fig.A.3(2/32)

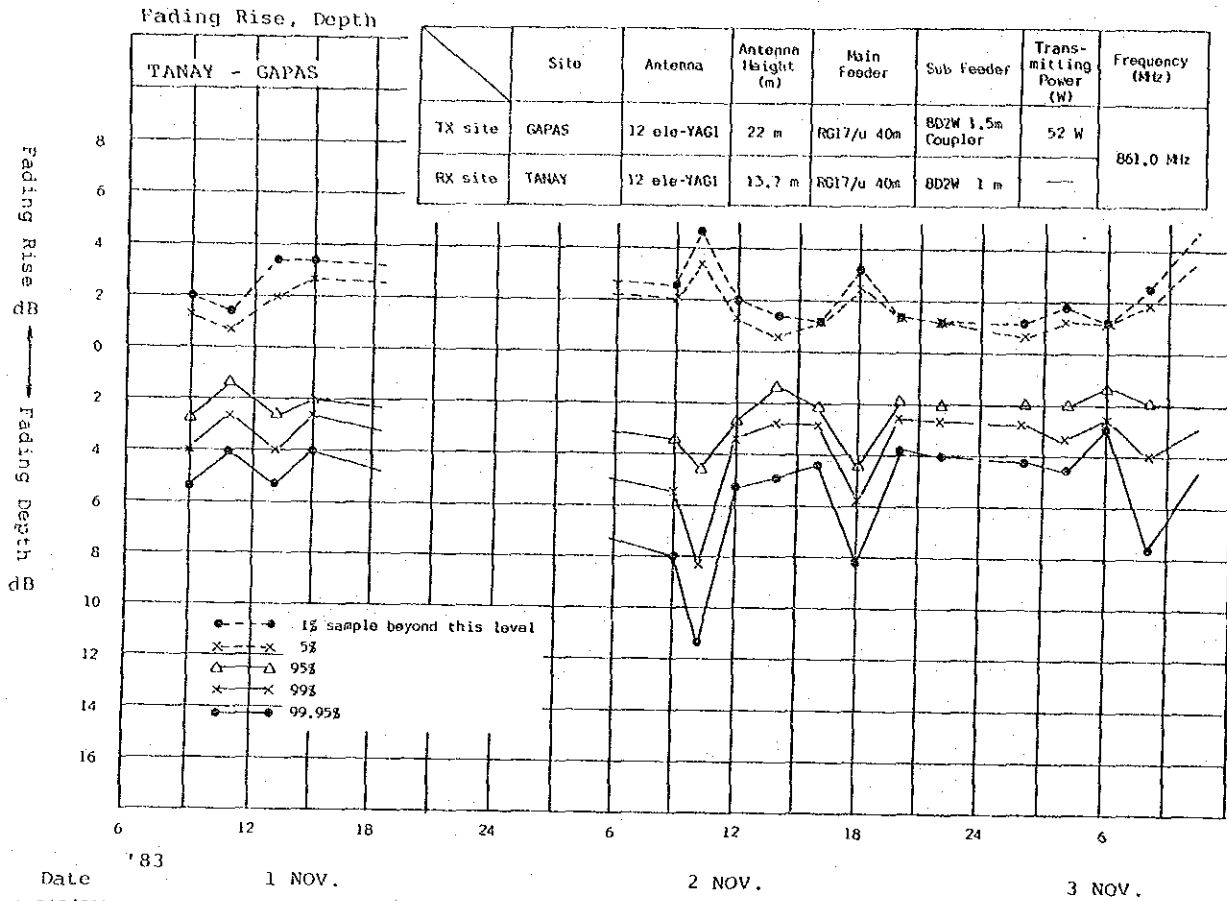


Fig. A.5(5/32)

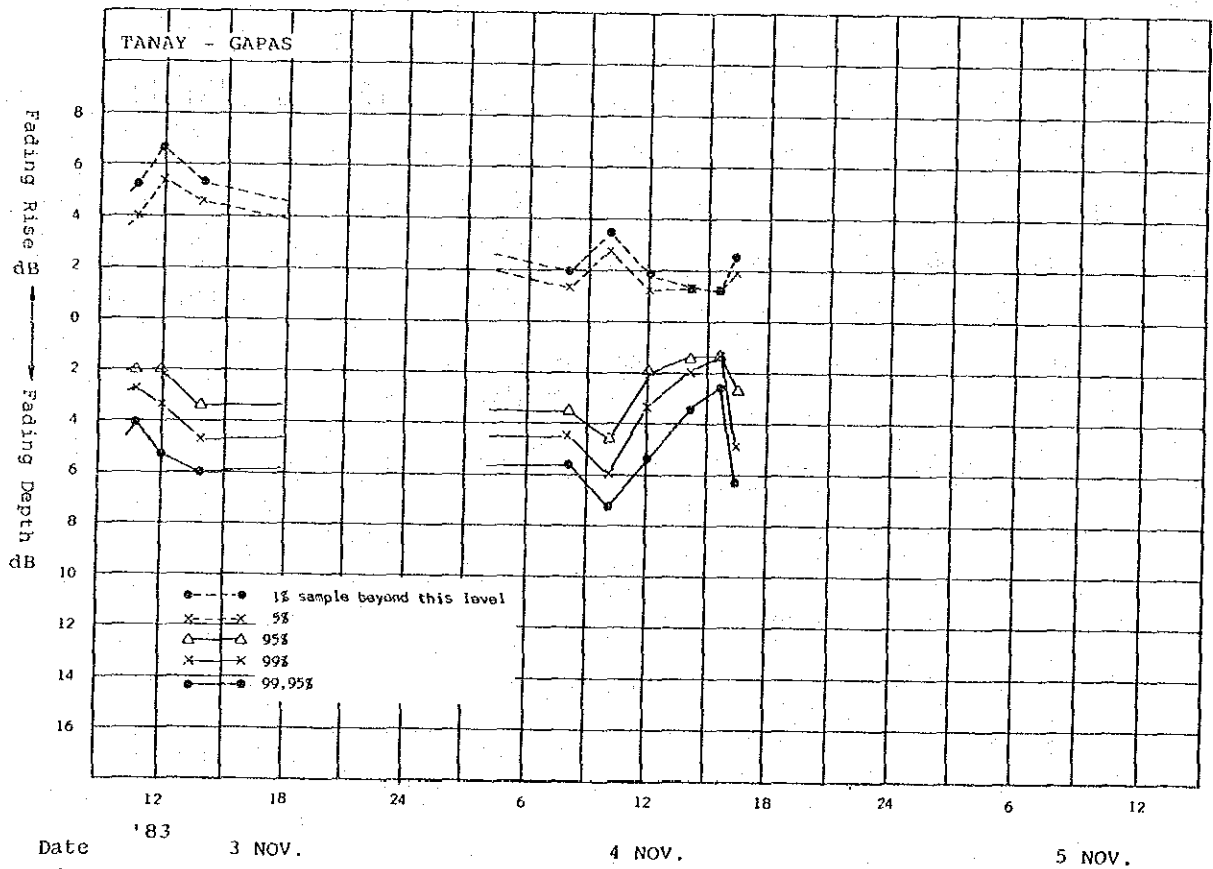


Fig. A.3(4/32)



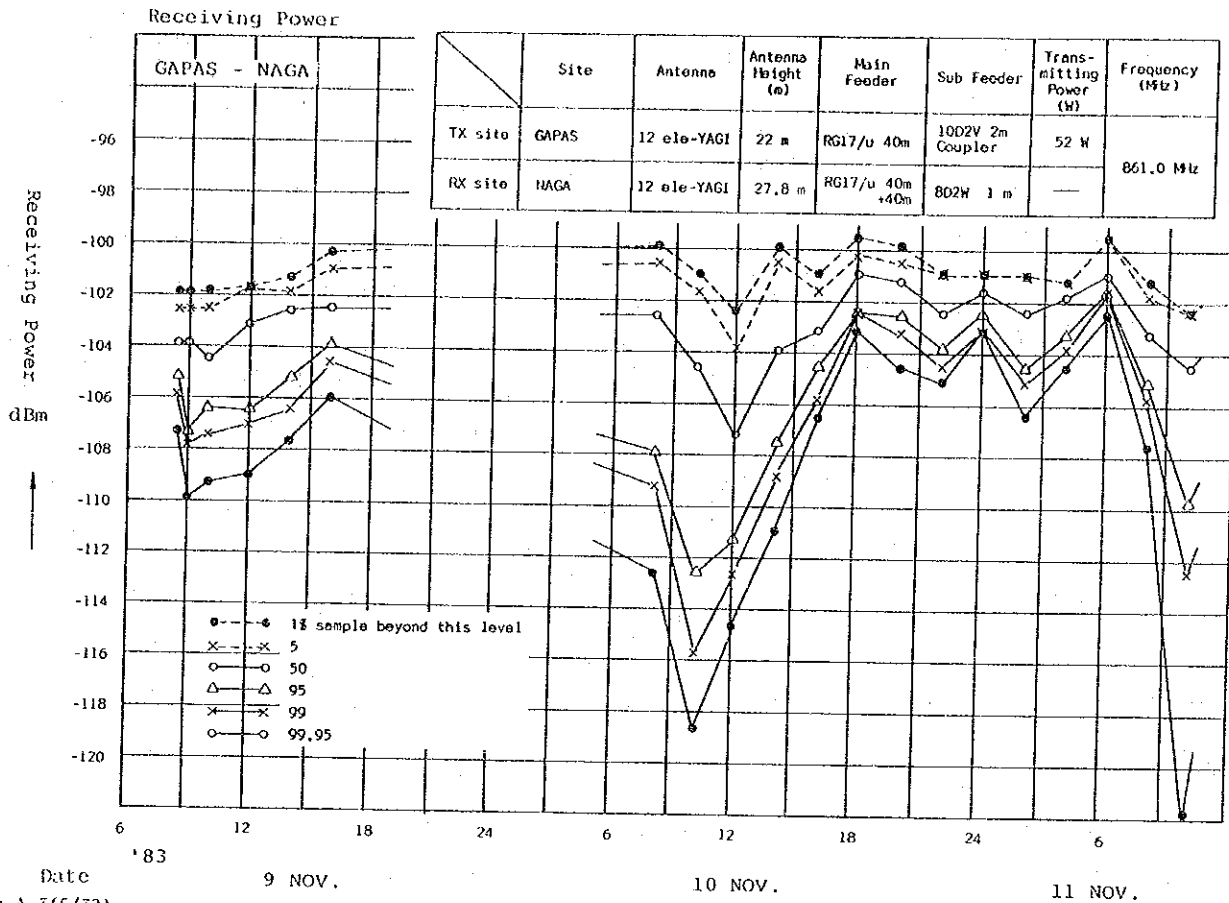


Fig.A.3(5/32)

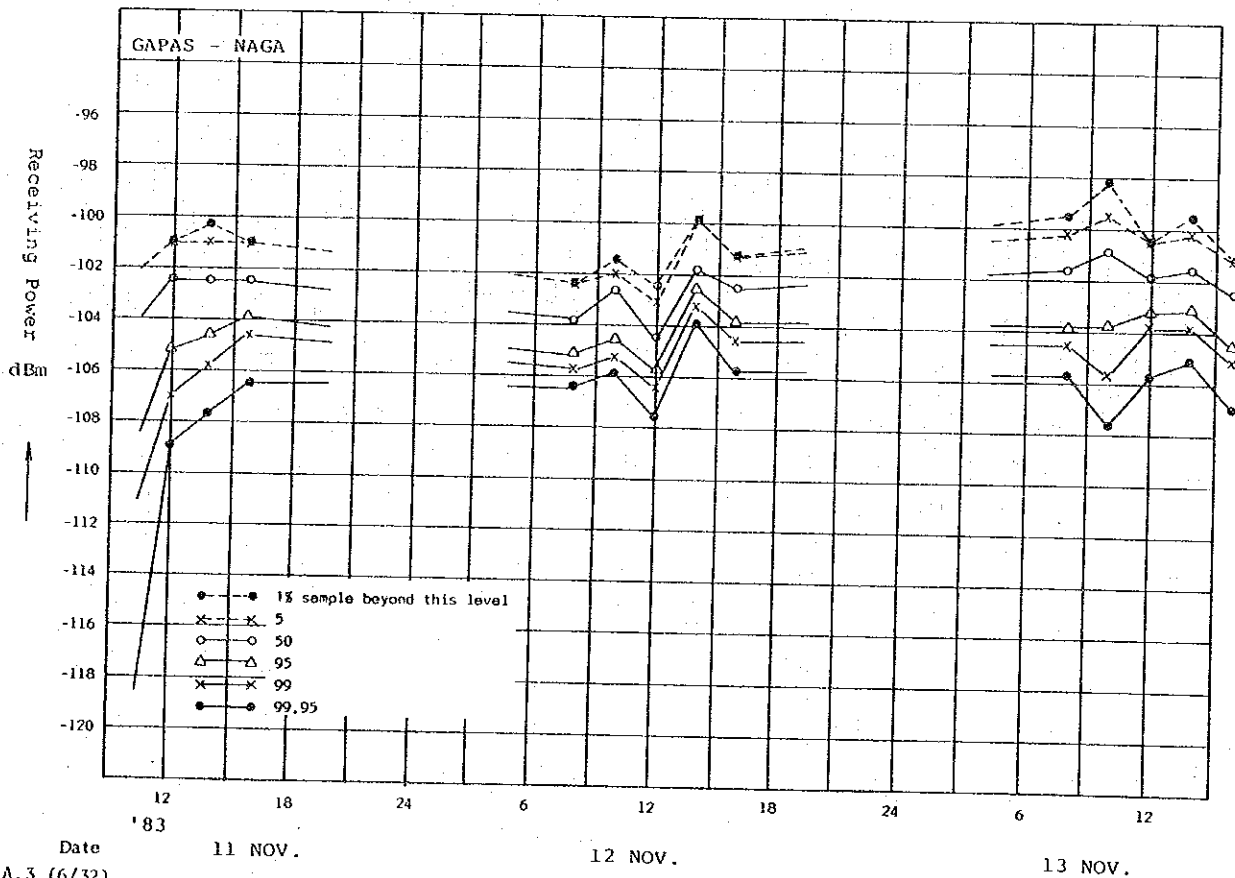


Fig.A.3 (6/32)

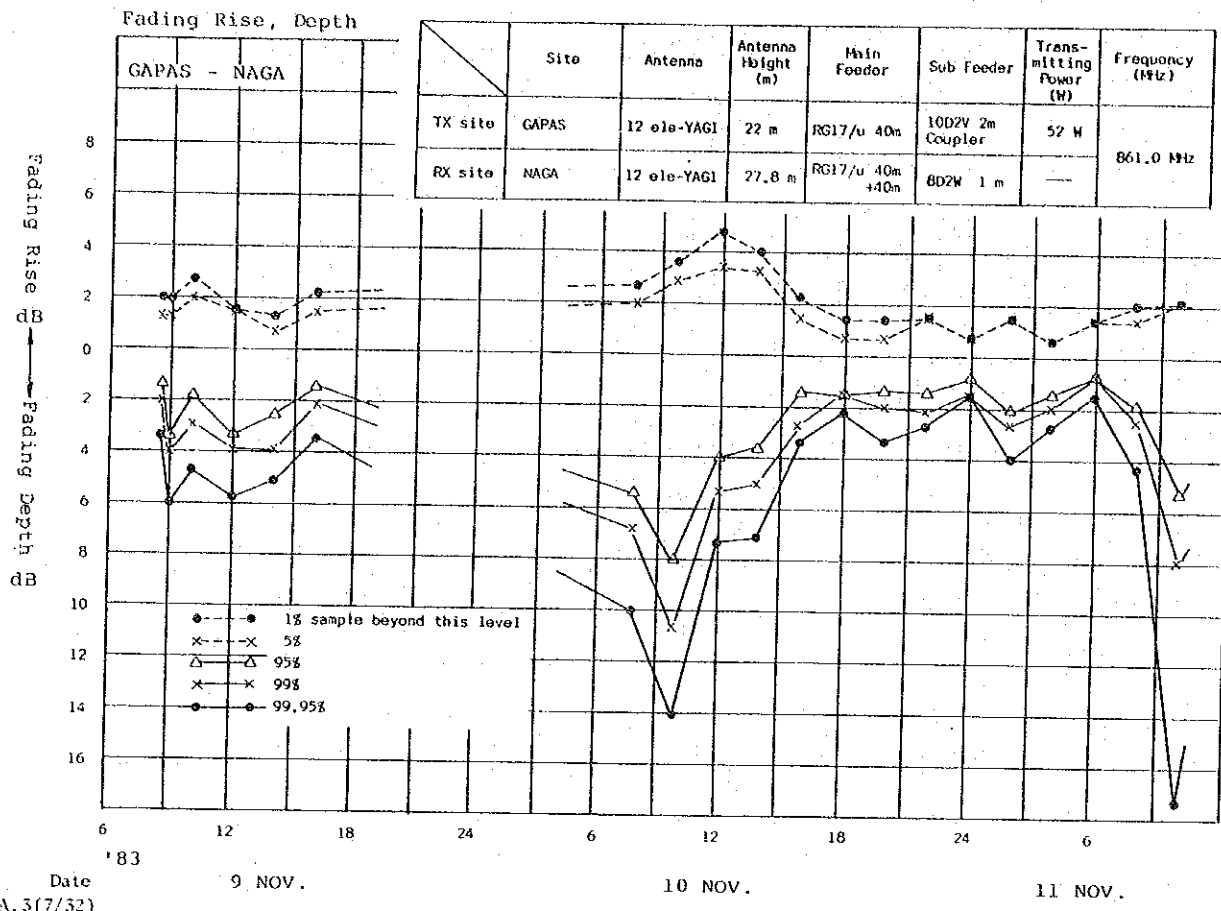


Fig.A.3(7/32)

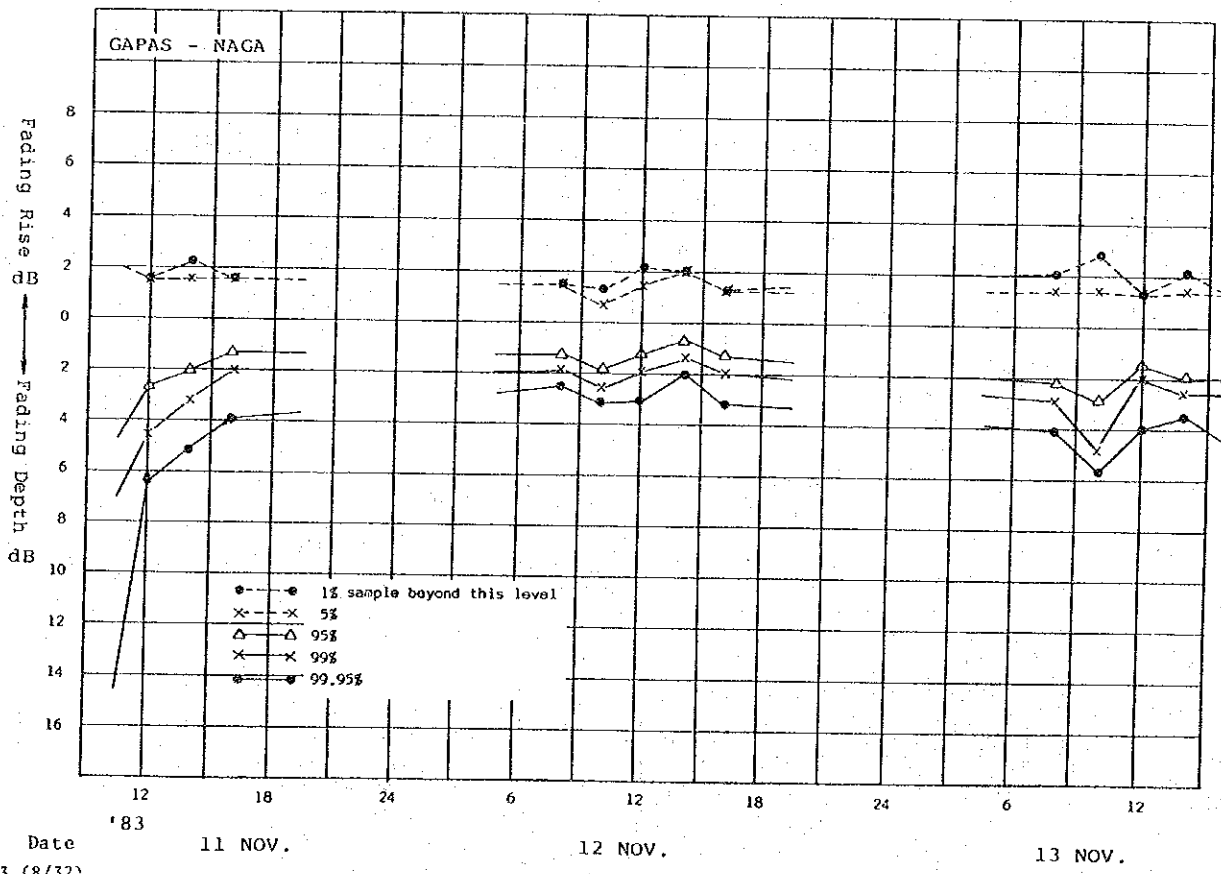


Fig.A.3 (8/32)

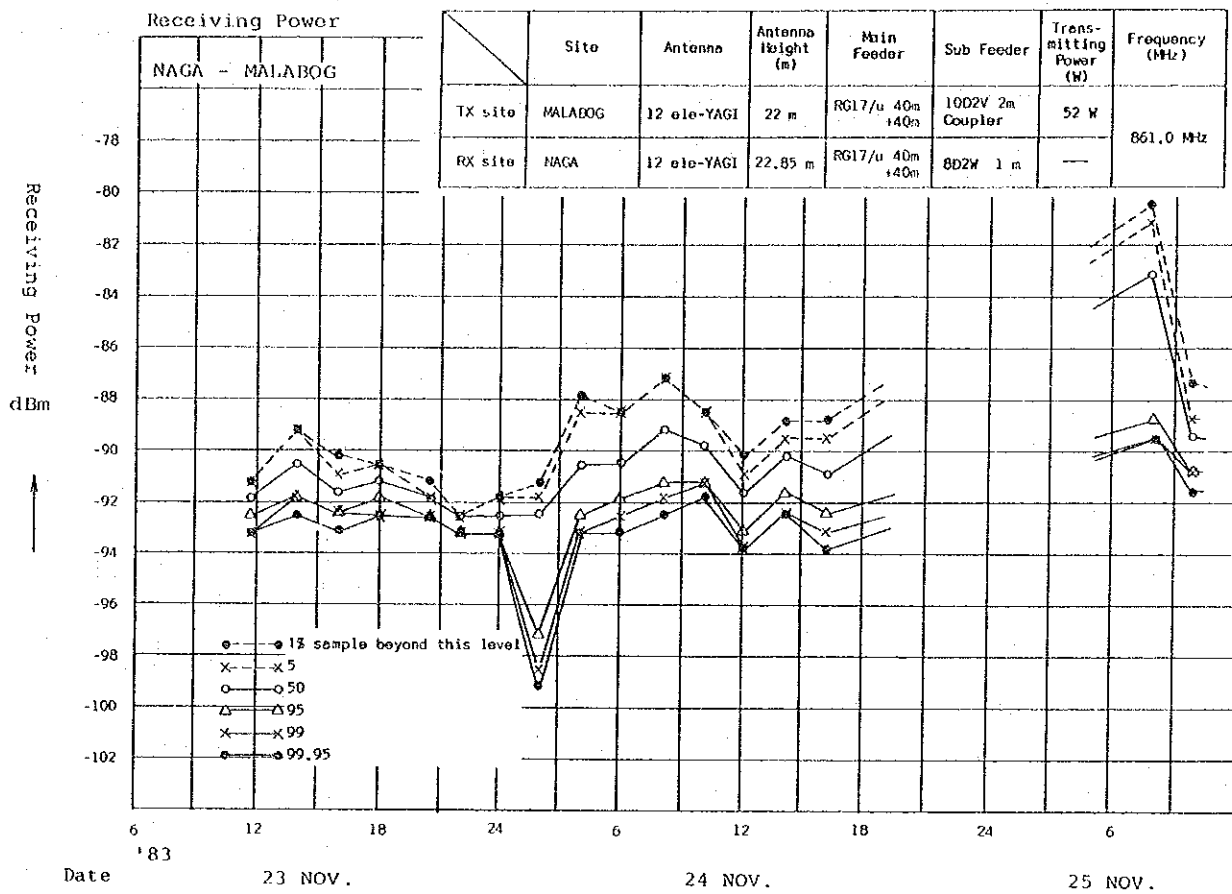


Fig.A.3 (9/32)

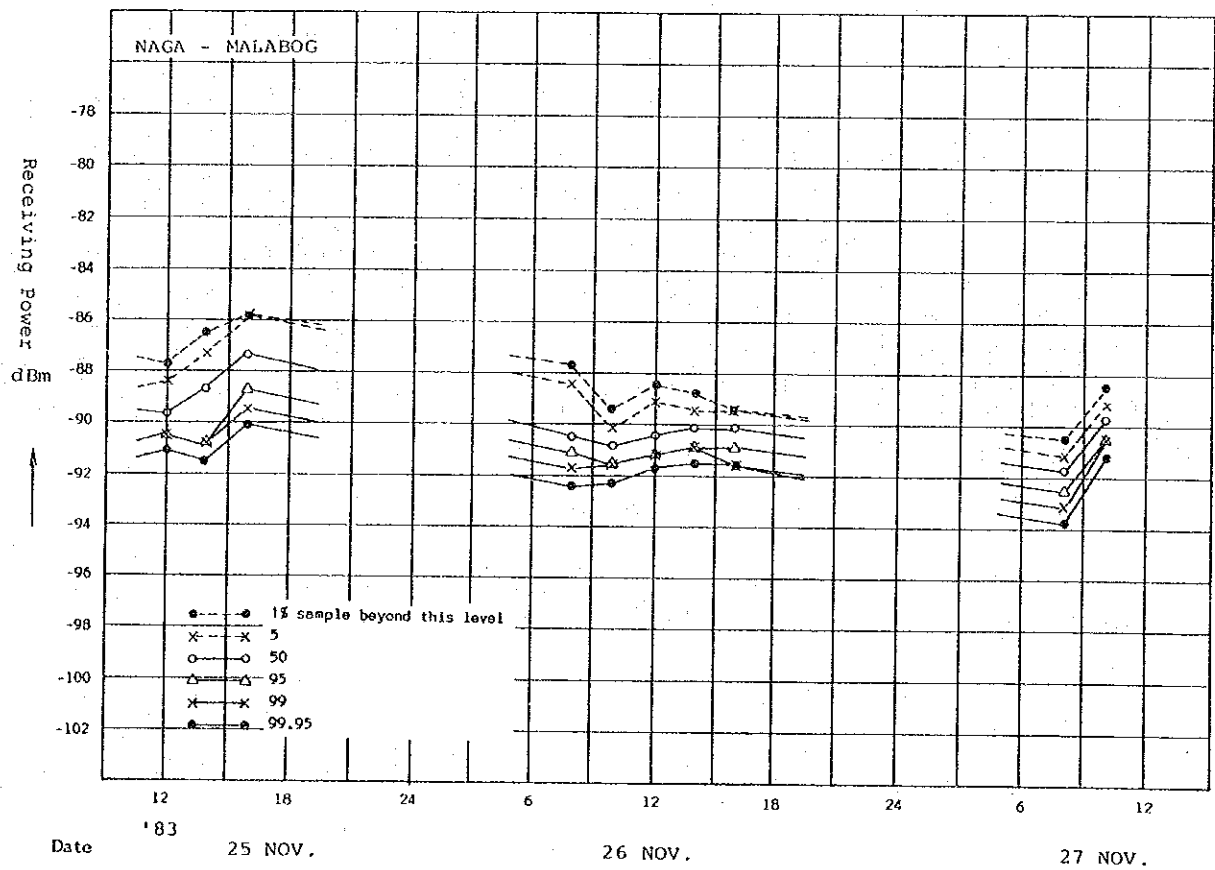


Fig.A.3 (10/32)

Fading Rise, Depth

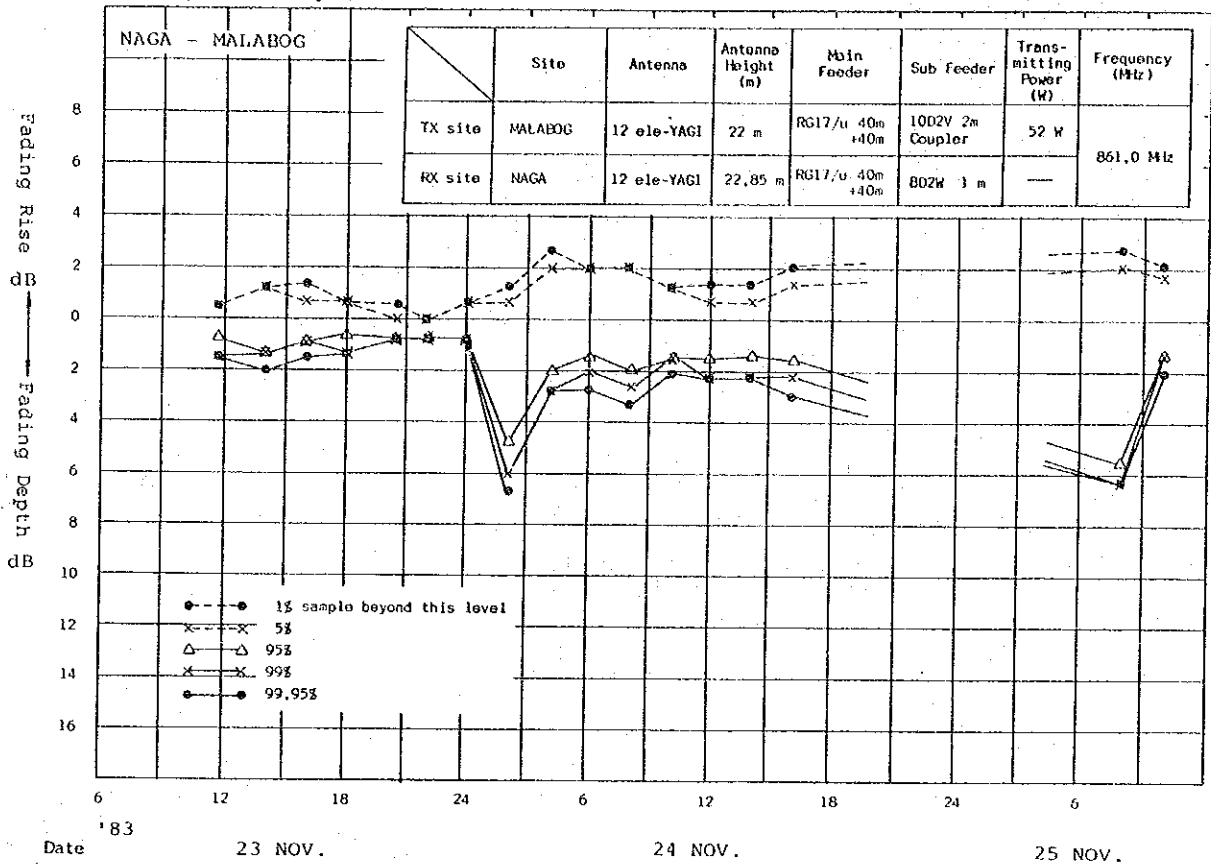


Fig.A.3 (11/32)

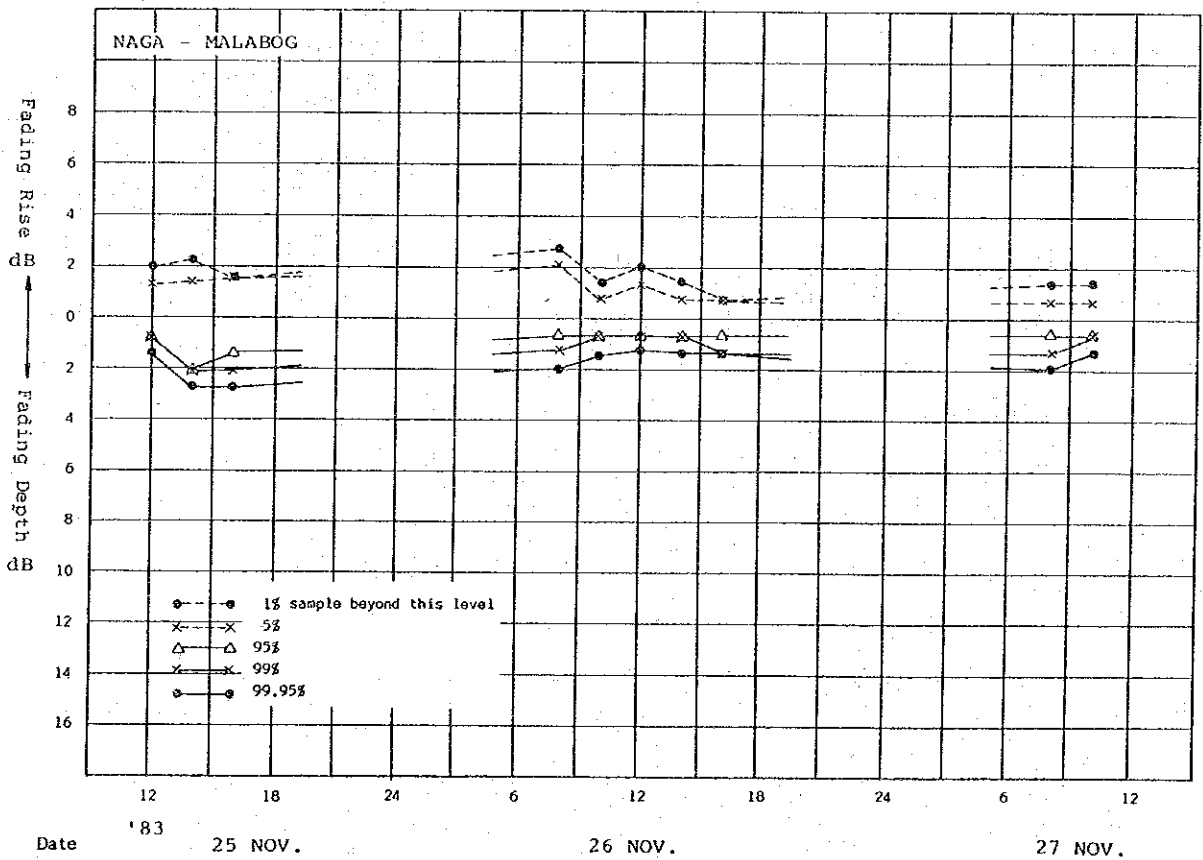
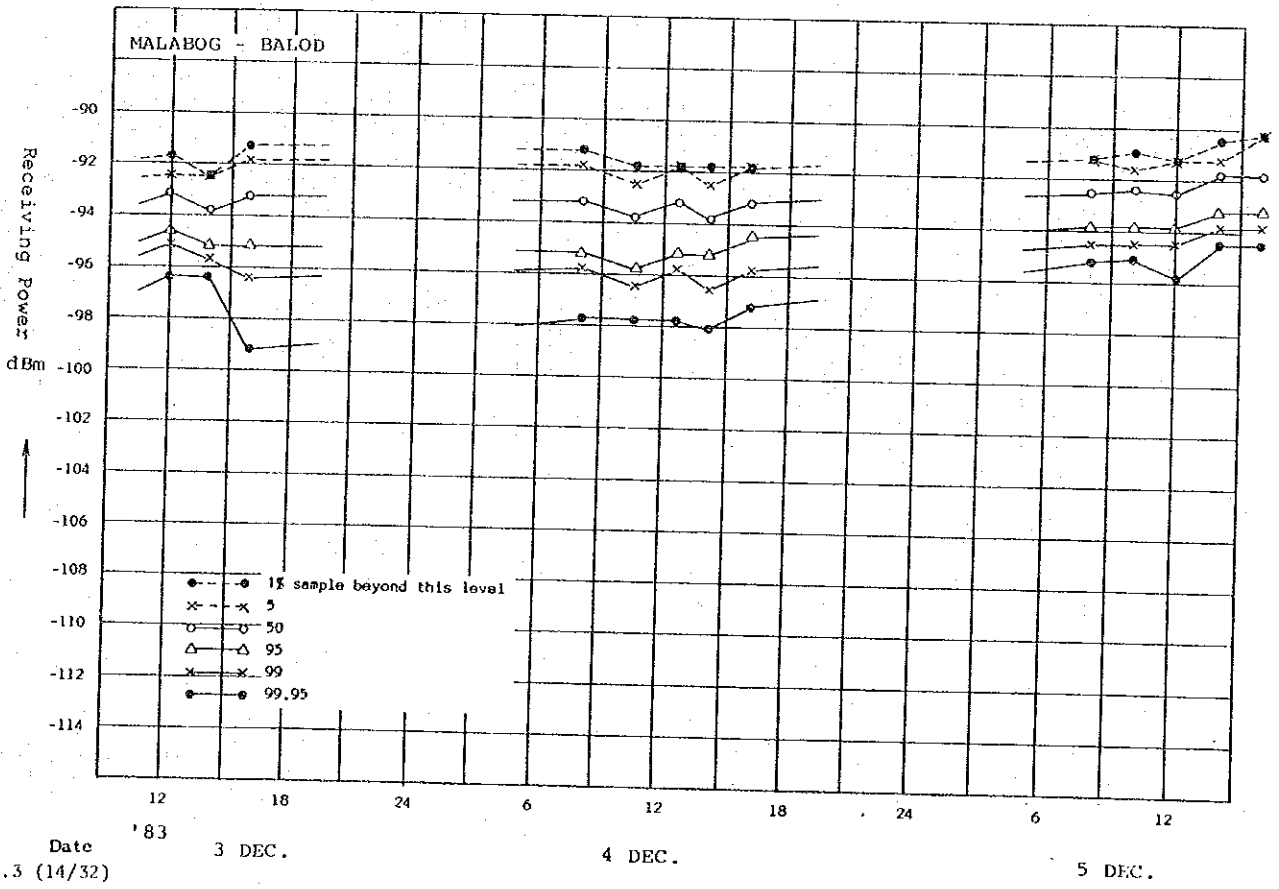
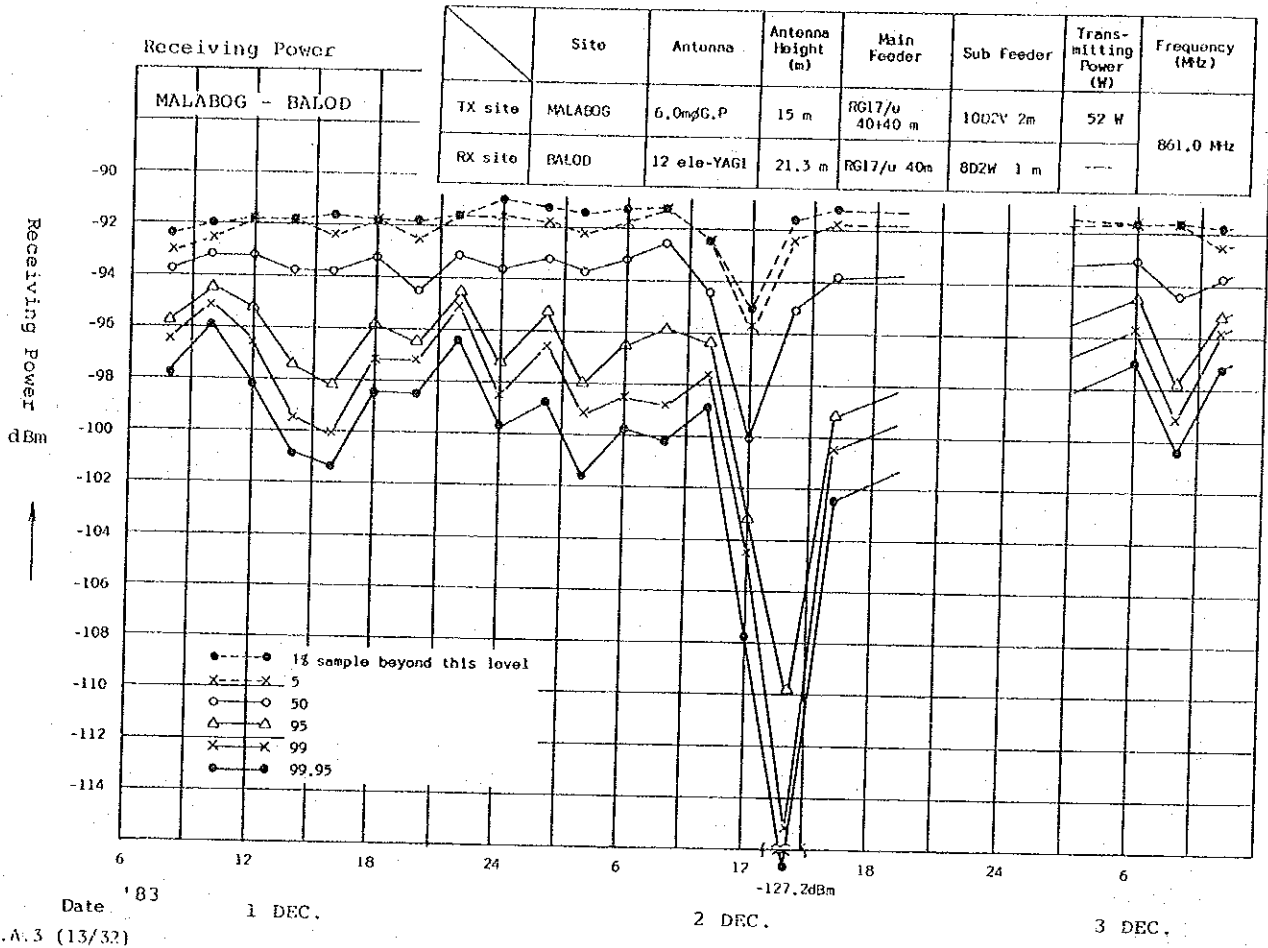


Fig.A.3 (12/32)



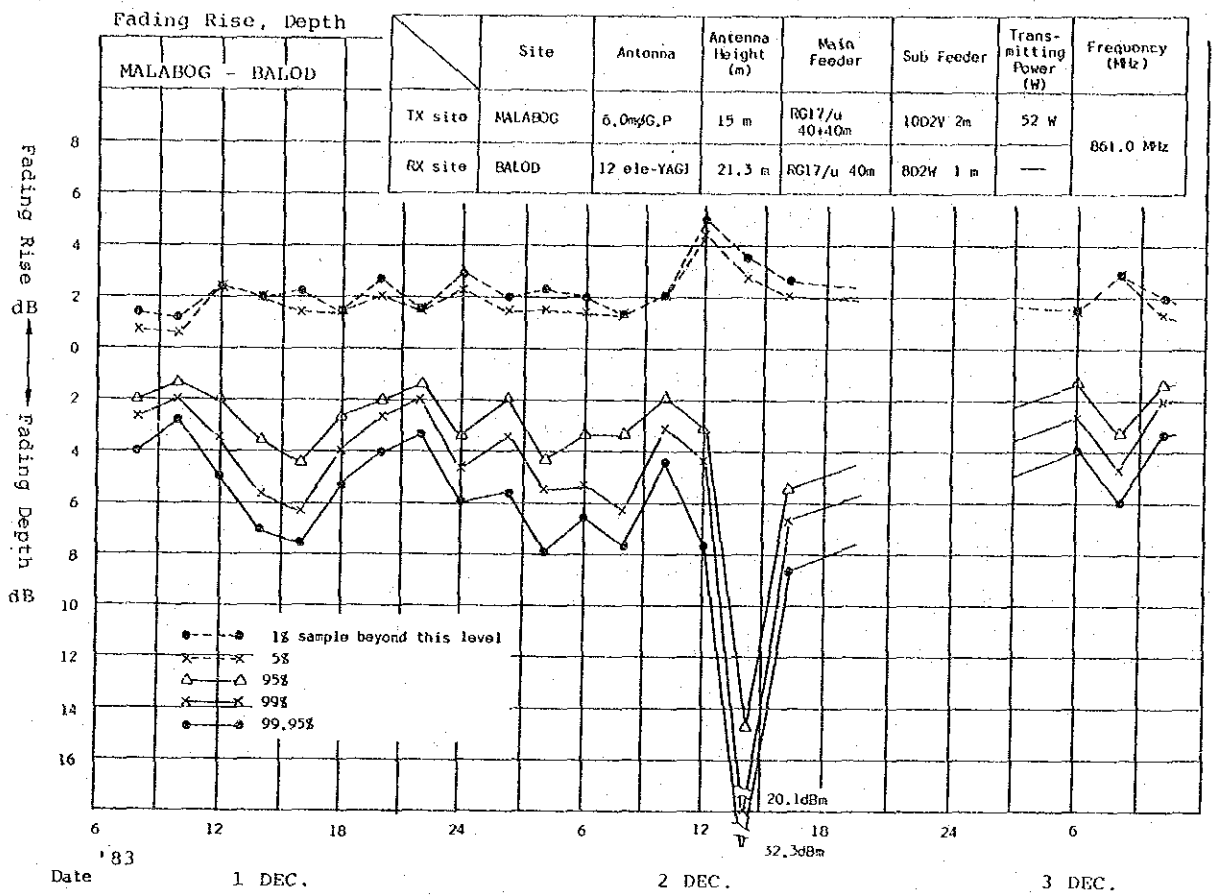


Fig.A.3 (15/32)

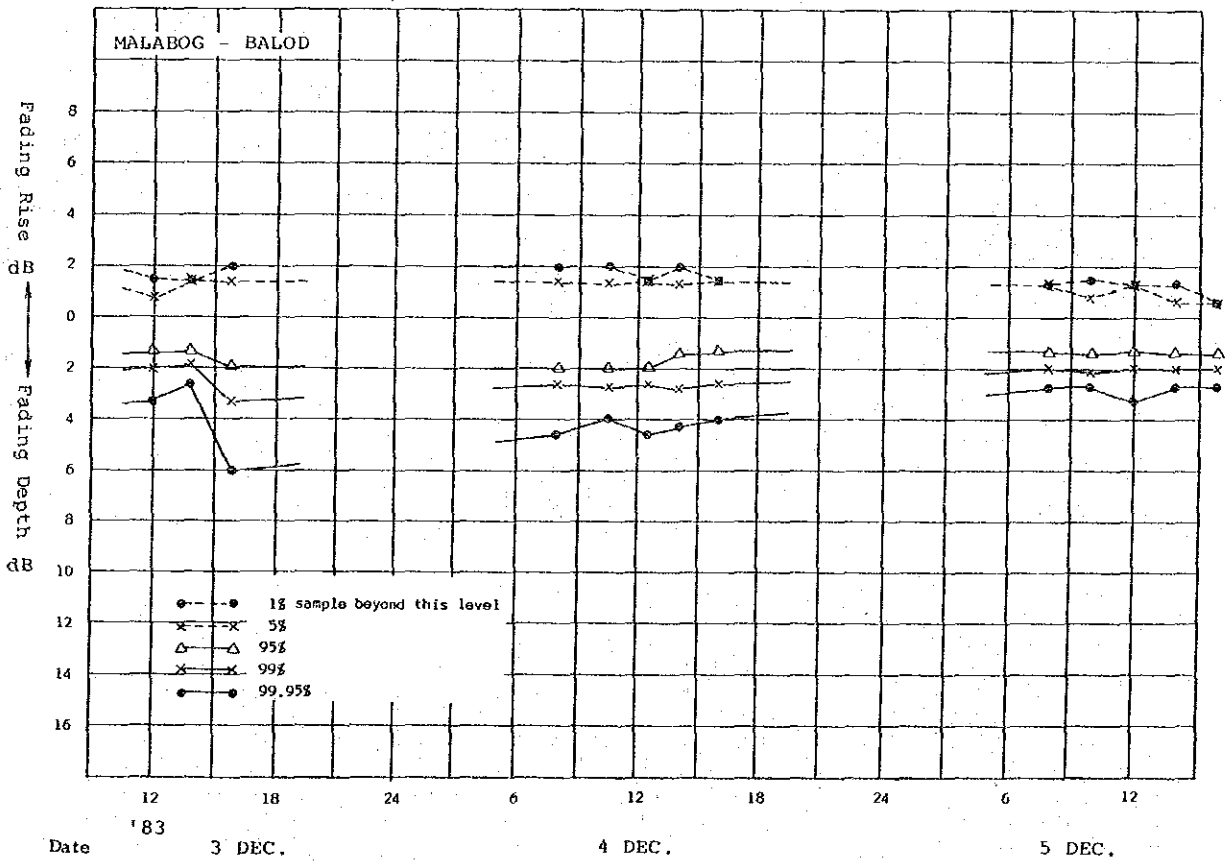


Fig.A.3 (16/32)

Receiving Power

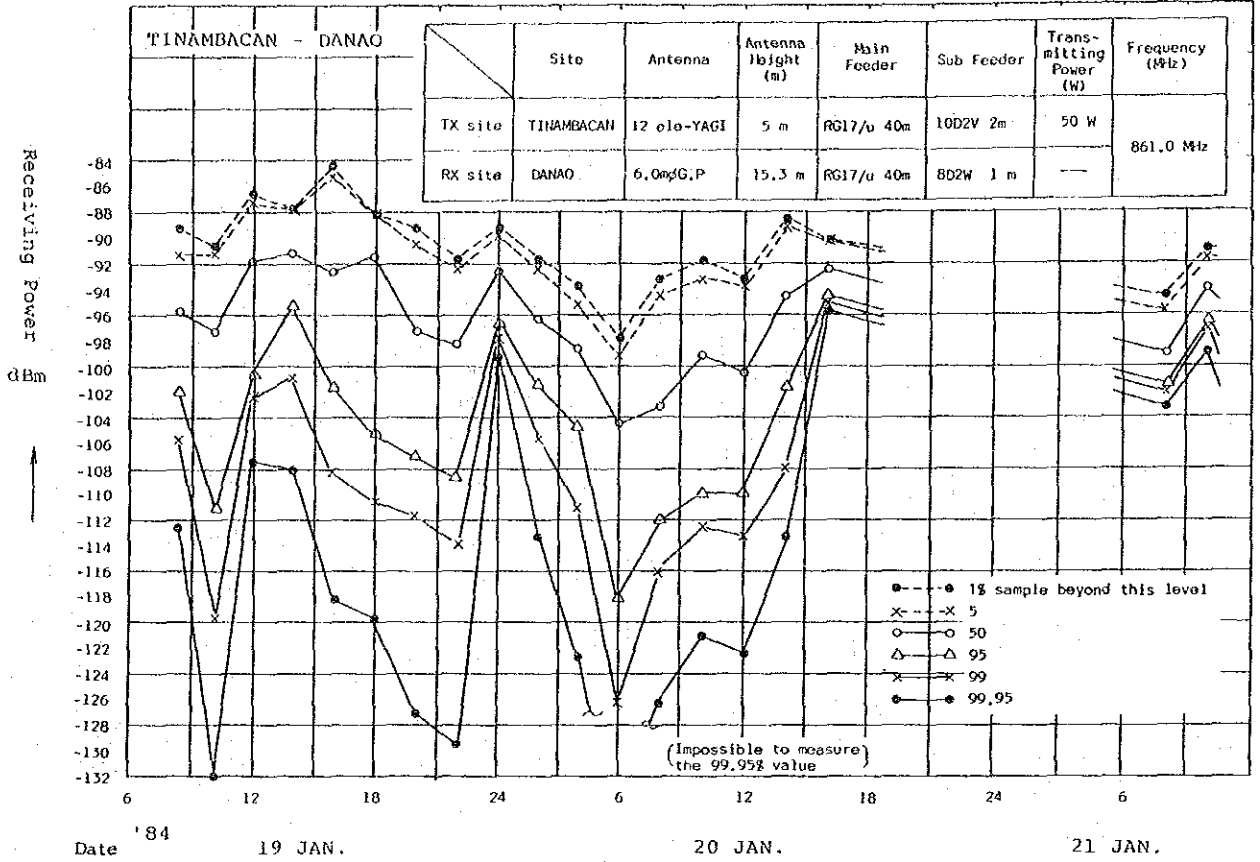


Fig.A.3 (17/32)

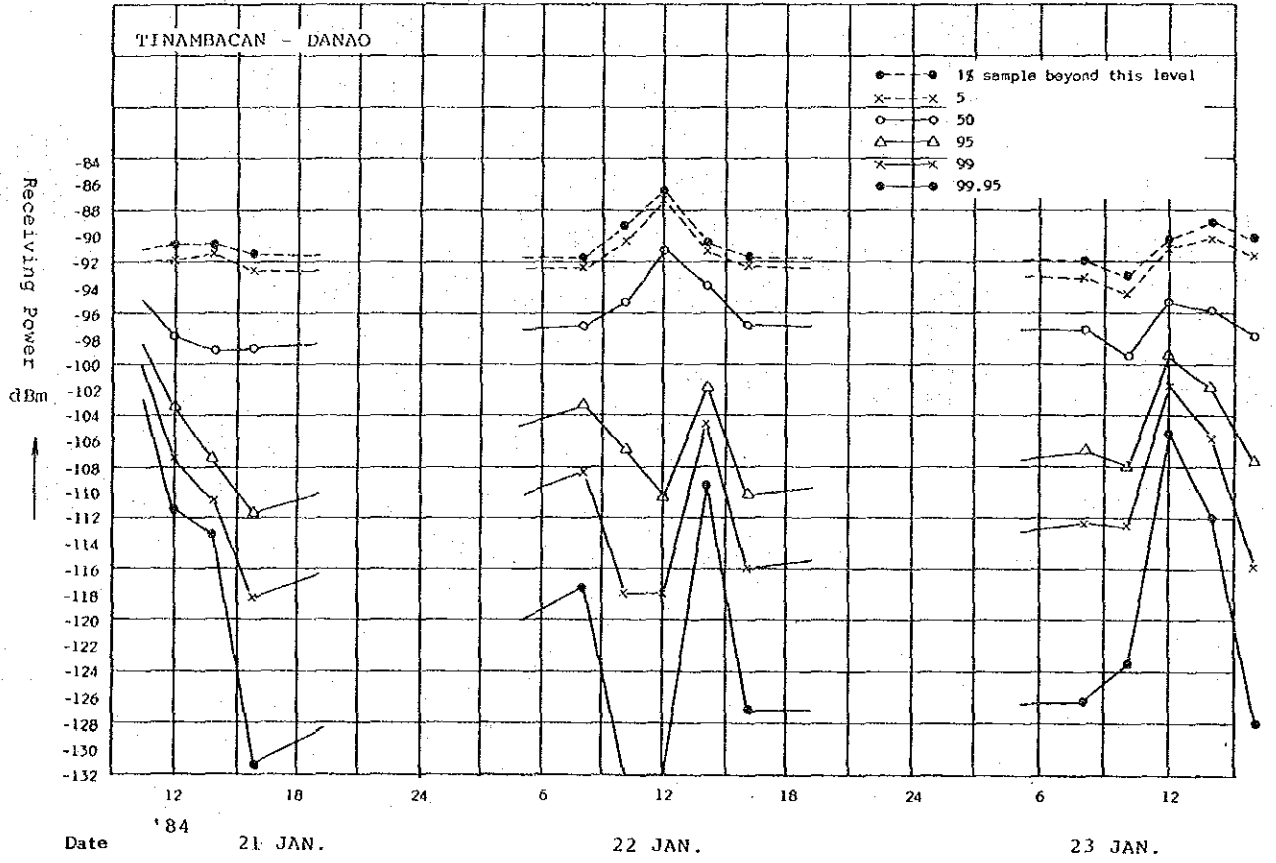


Fig.A.3 (18/32)

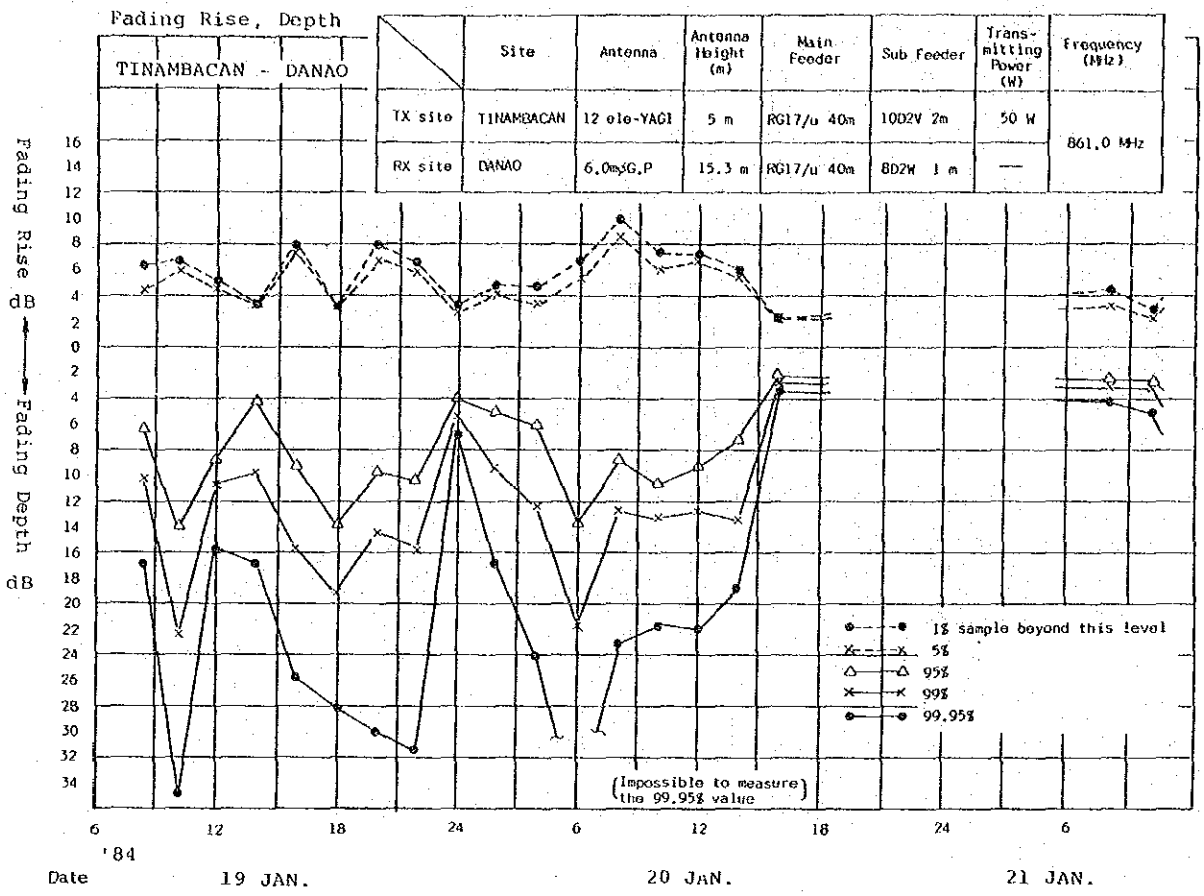


Fig.A.3 (19/32)

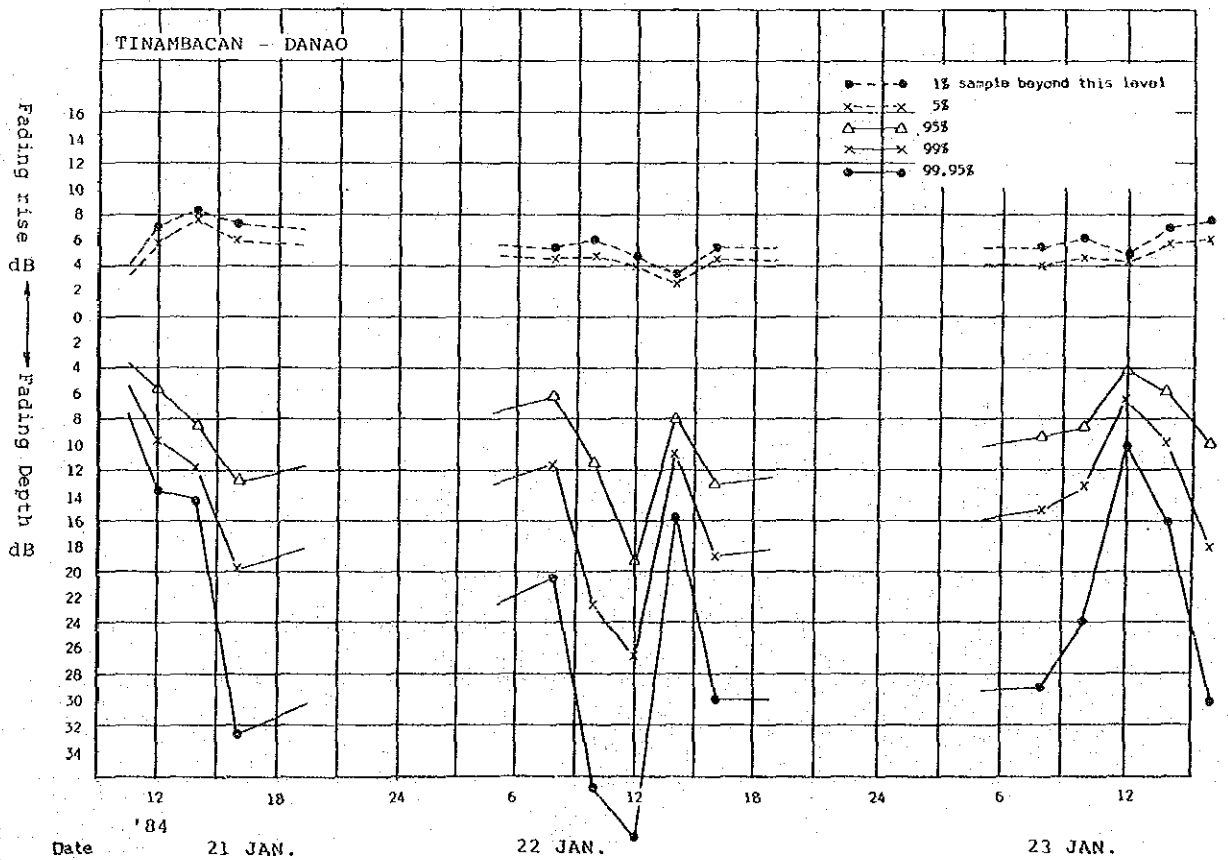


Fig.A.3 (20/32)



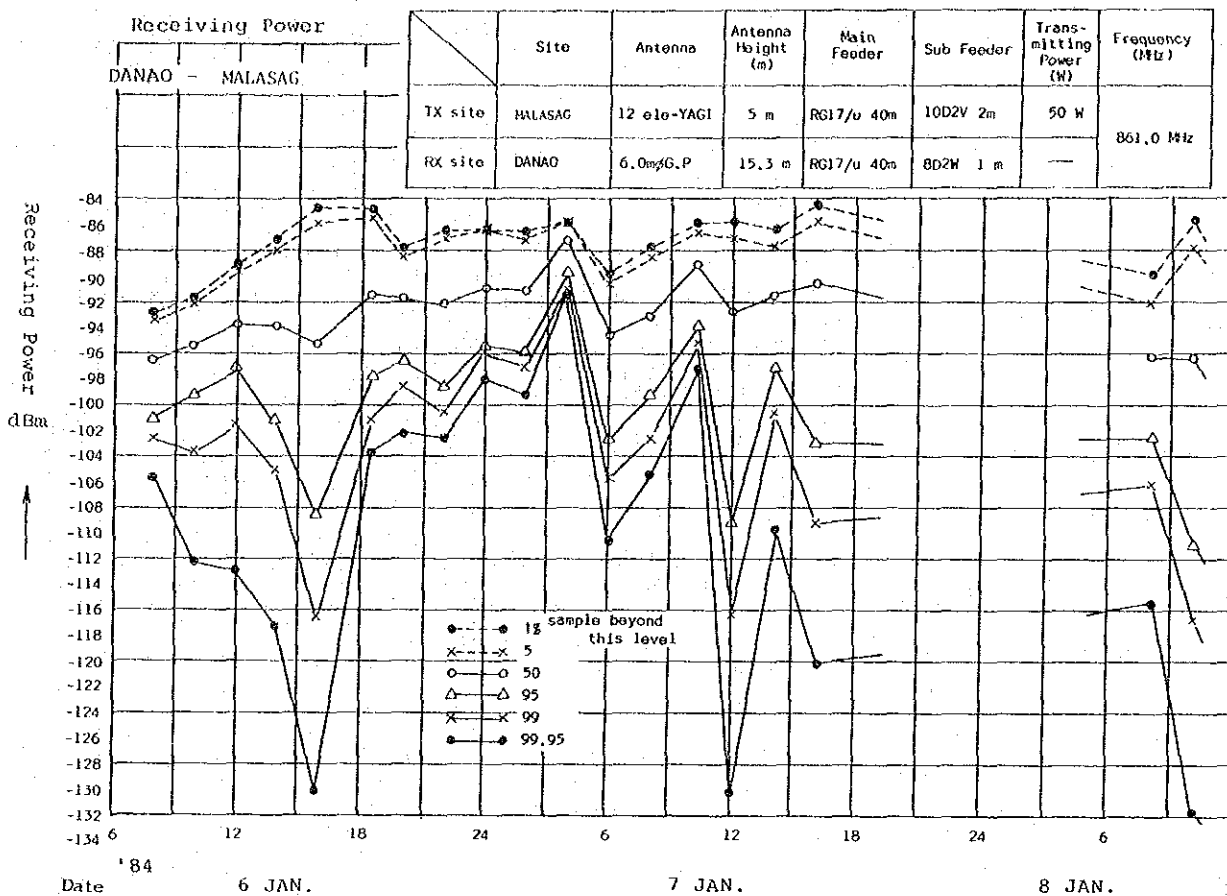


Fig.A.3 (21/32)

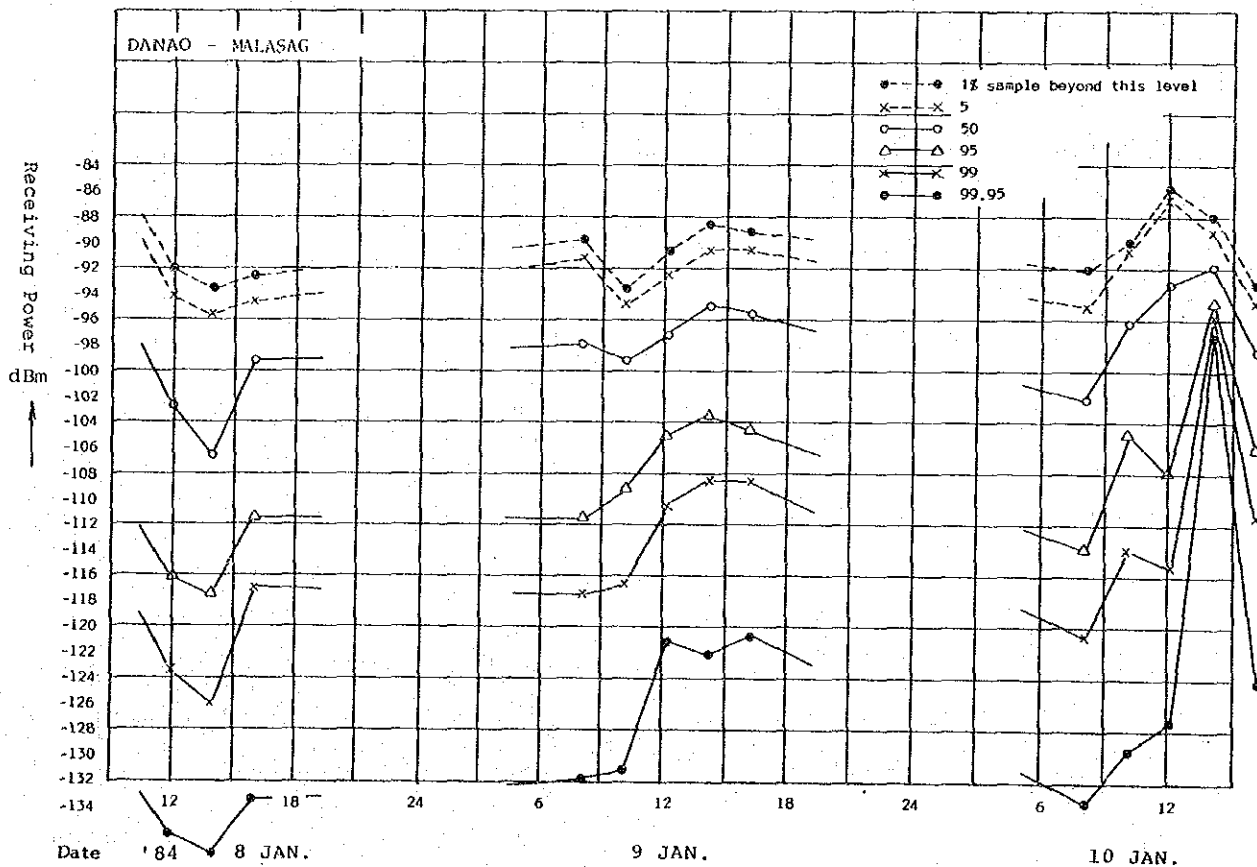


Fig.A.3 (22/32)

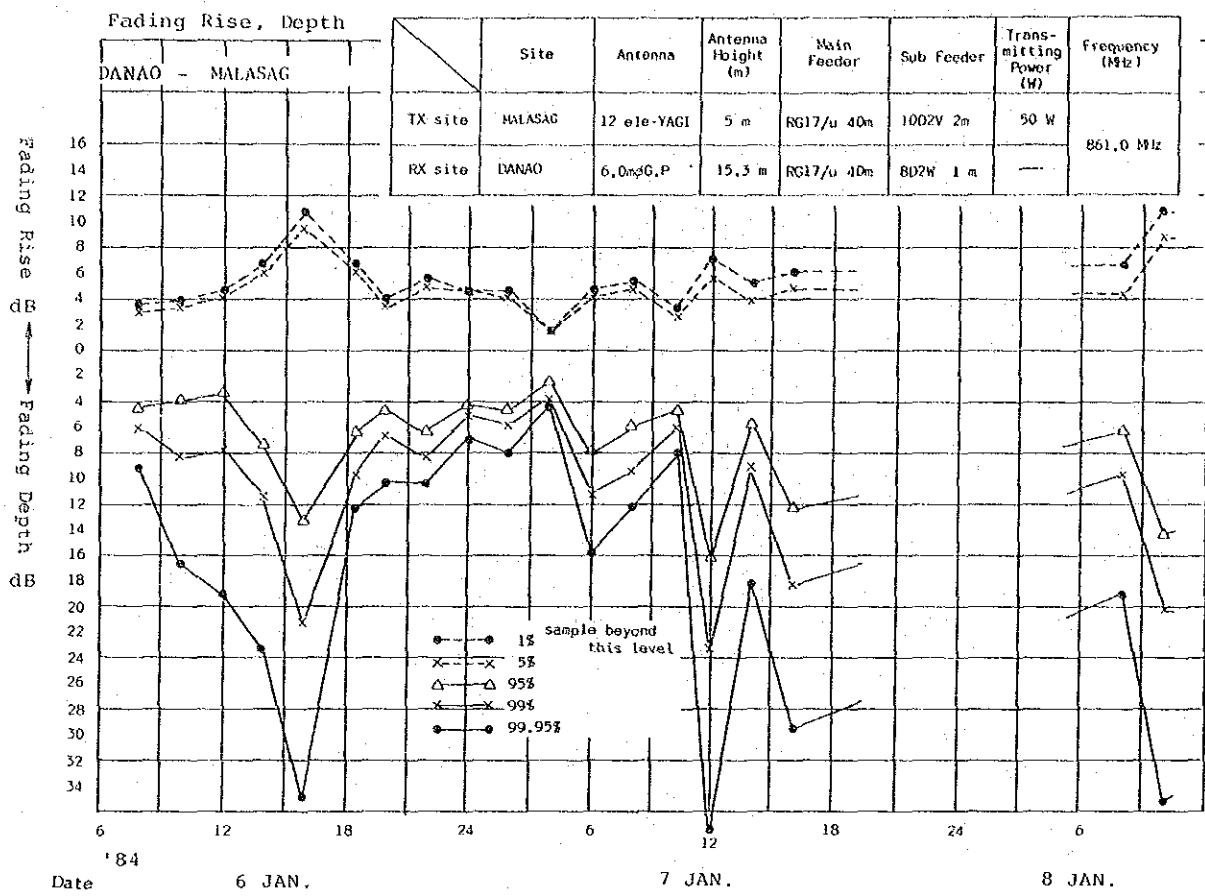


Fig.A.3( 23/32)

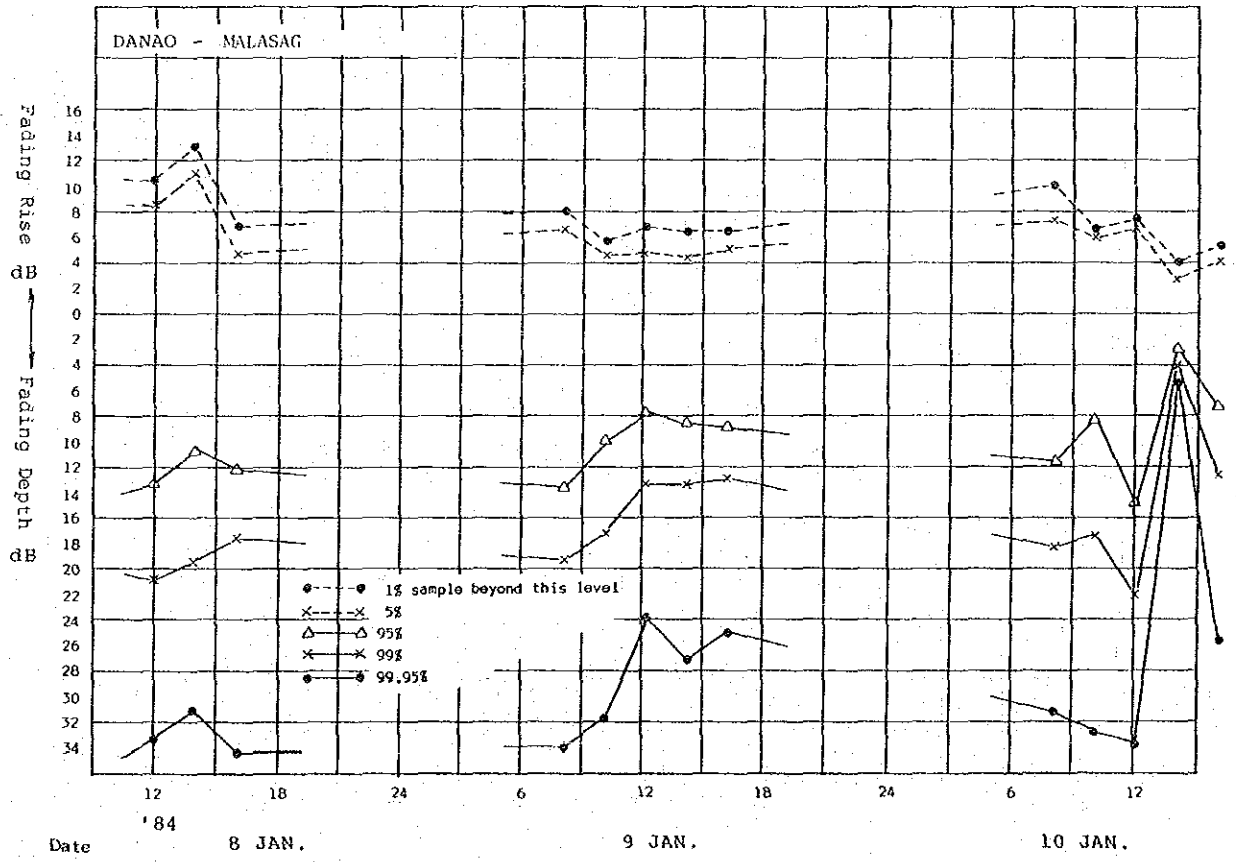


Fig.A.3 (24/32)

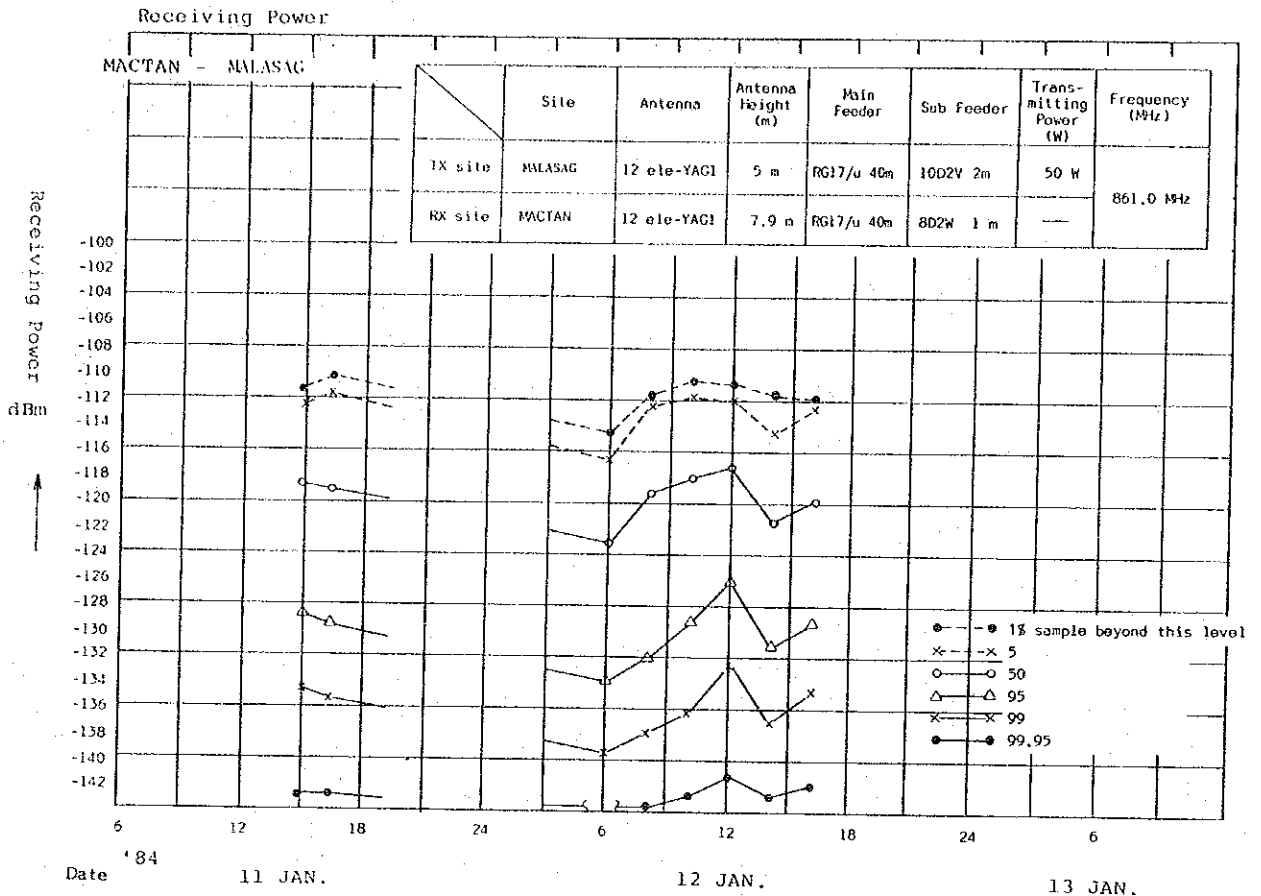


Fig.A.3 (25/52)

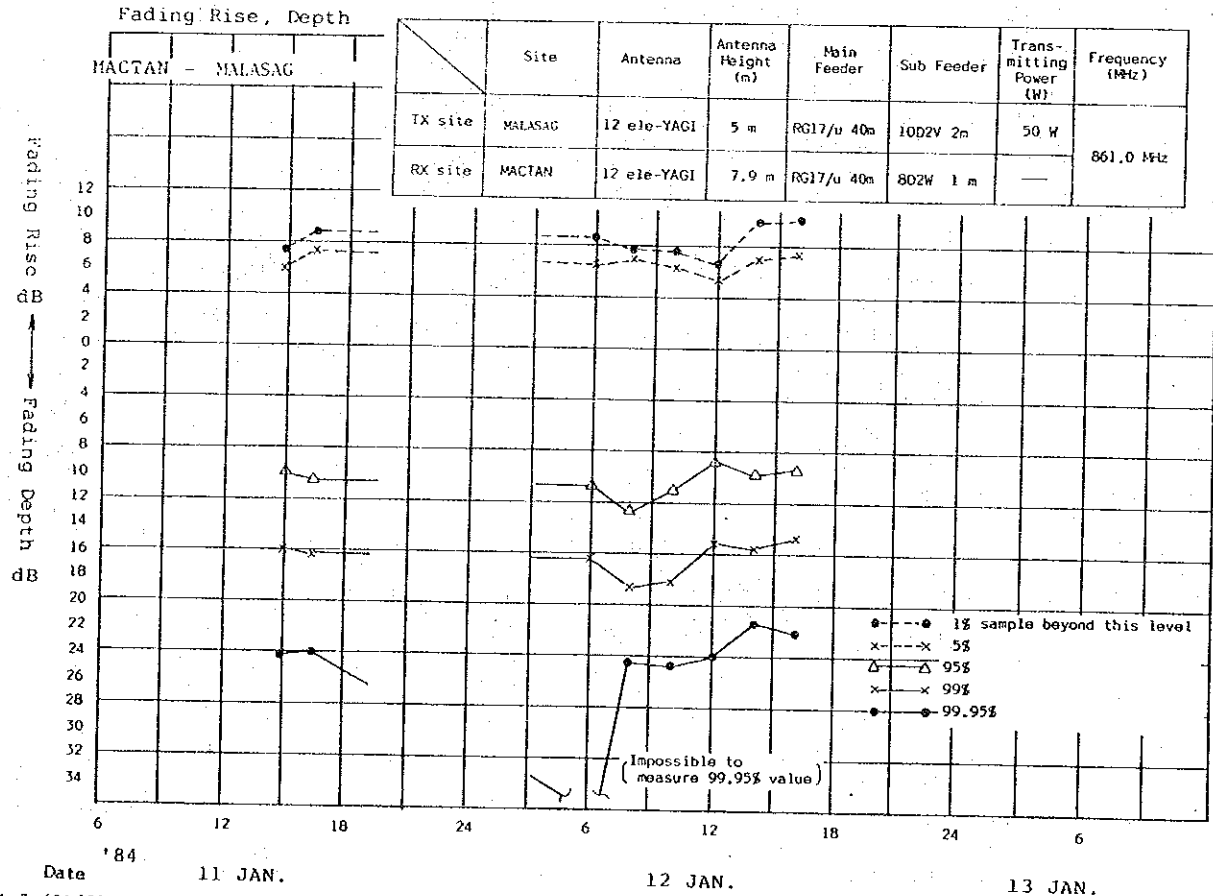


Fig.A.3 (26/32)

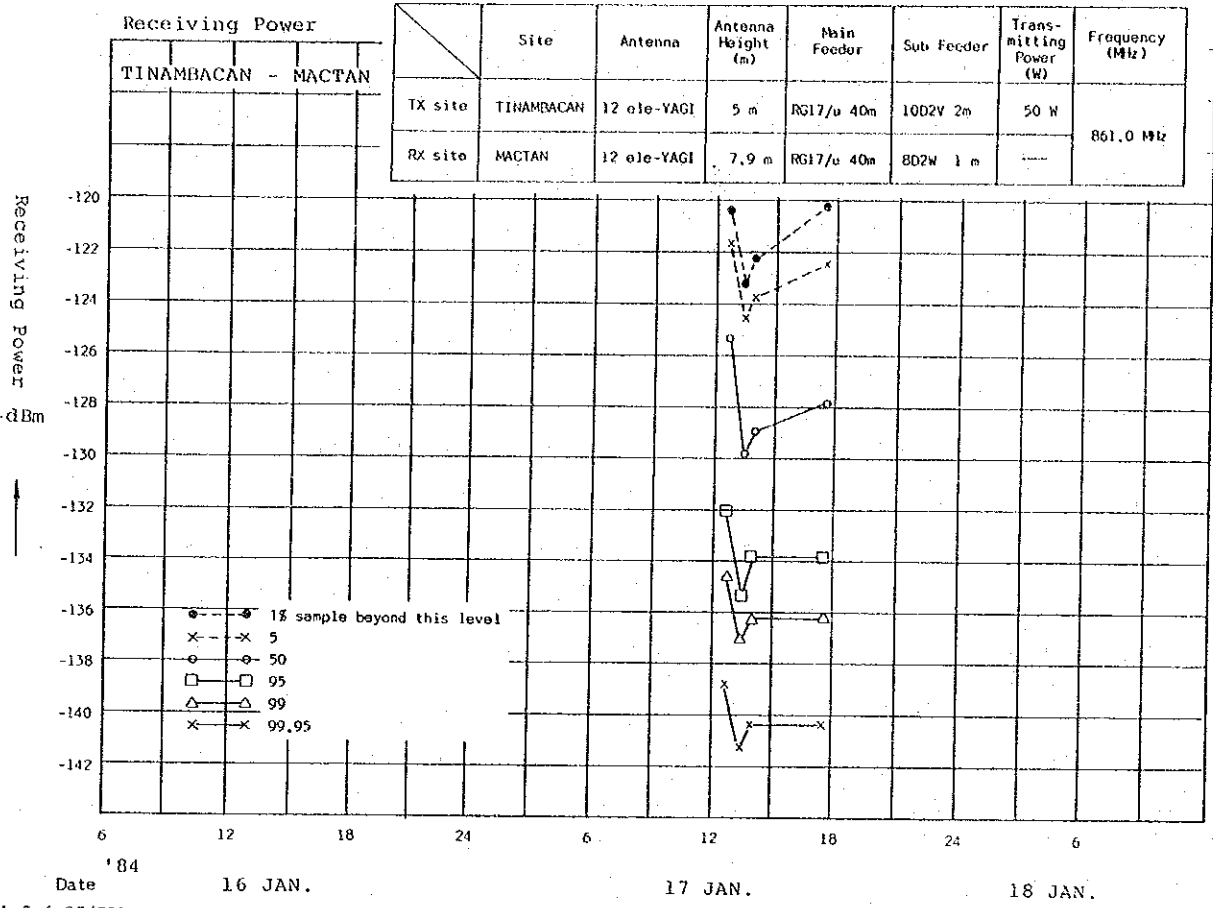


Fig.A.3 ( 27/32)

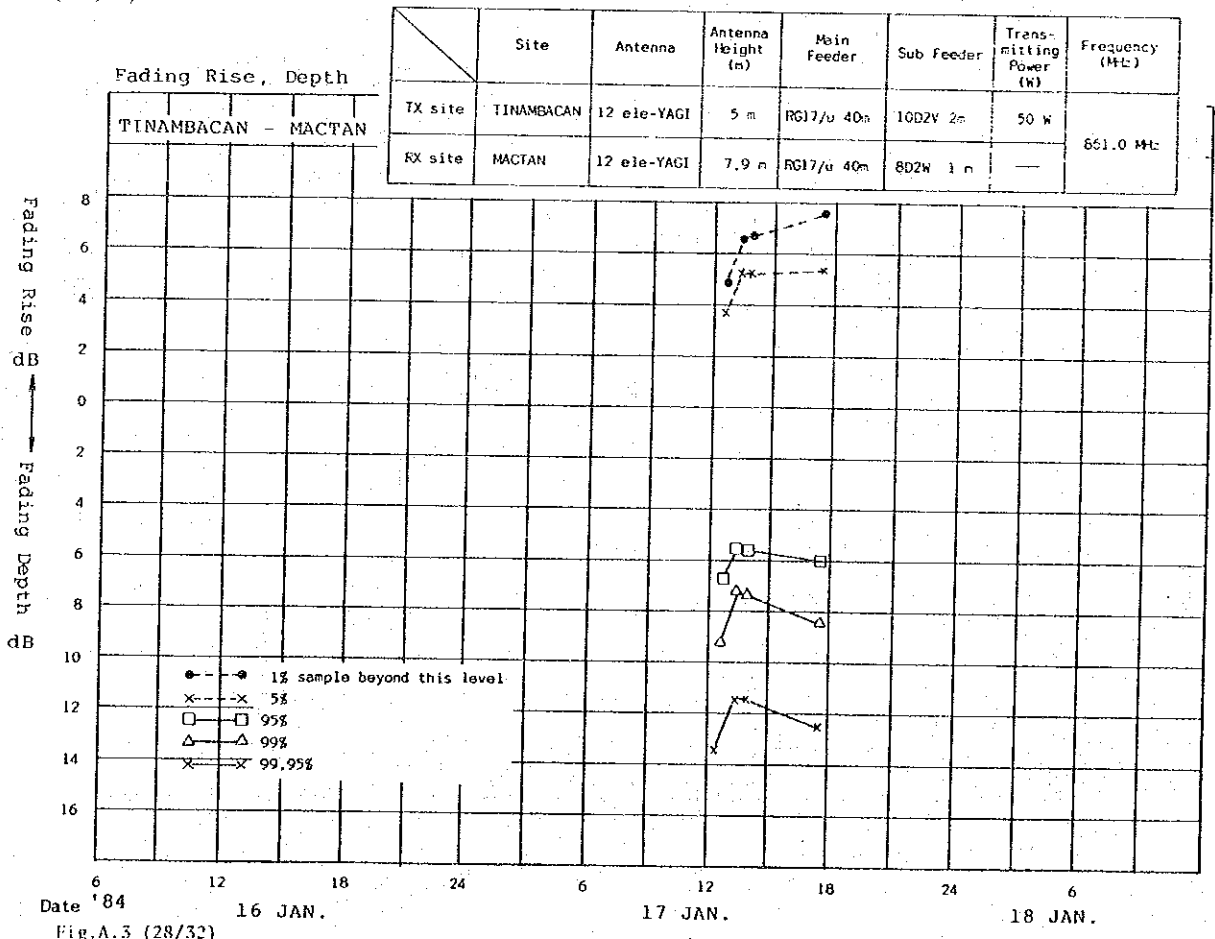


Fig.A.3 (28/32)

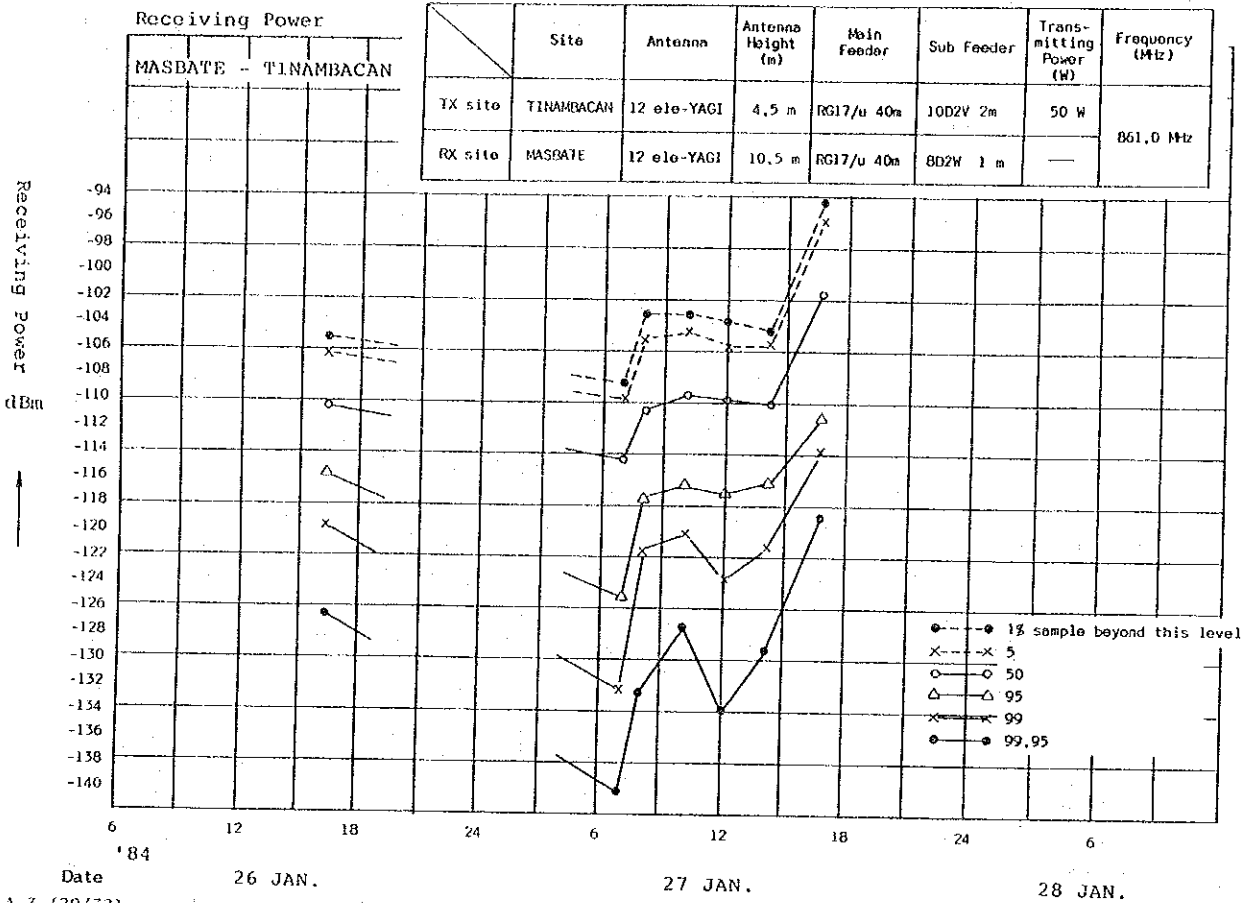


Fig.A.3 (29/32)

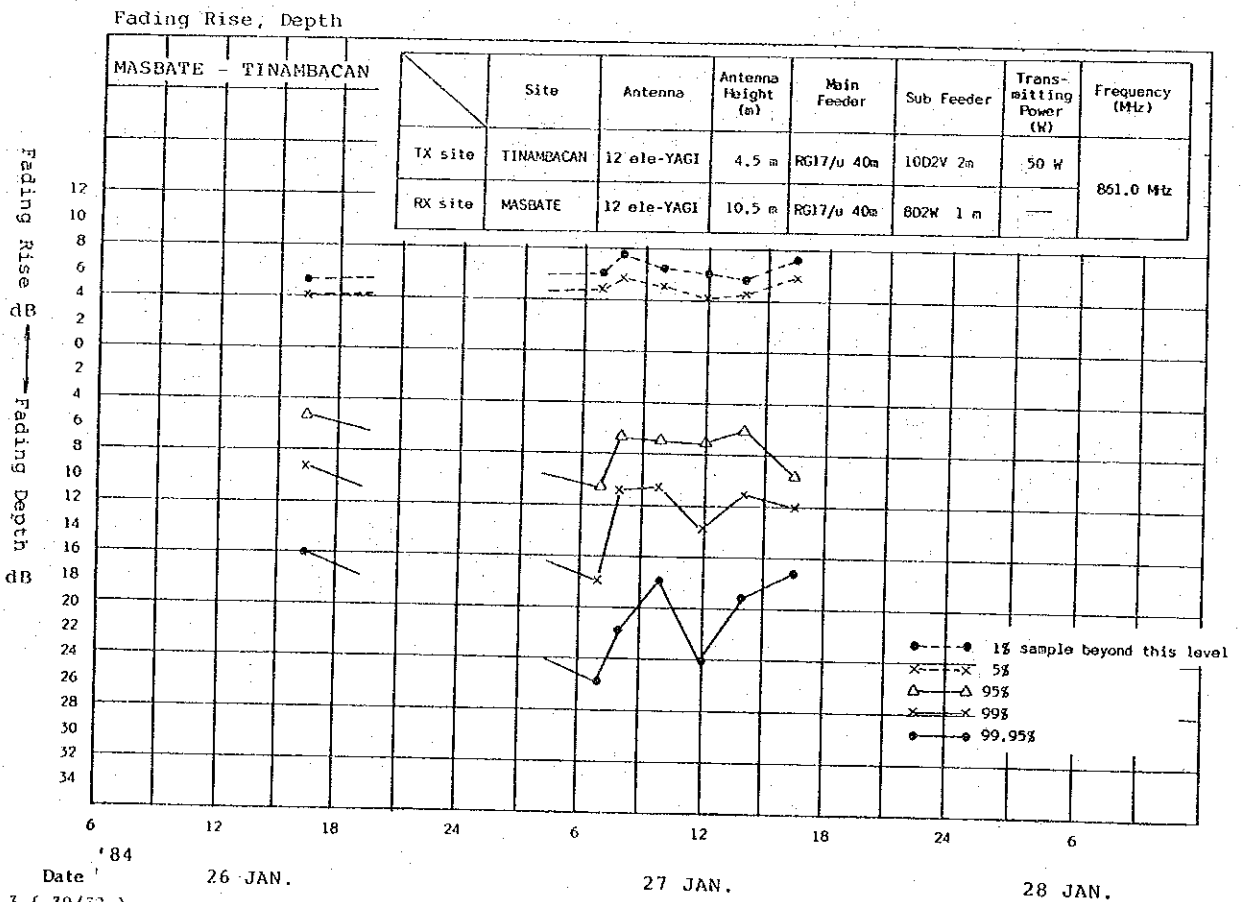


Fig.A.3 (30/32)

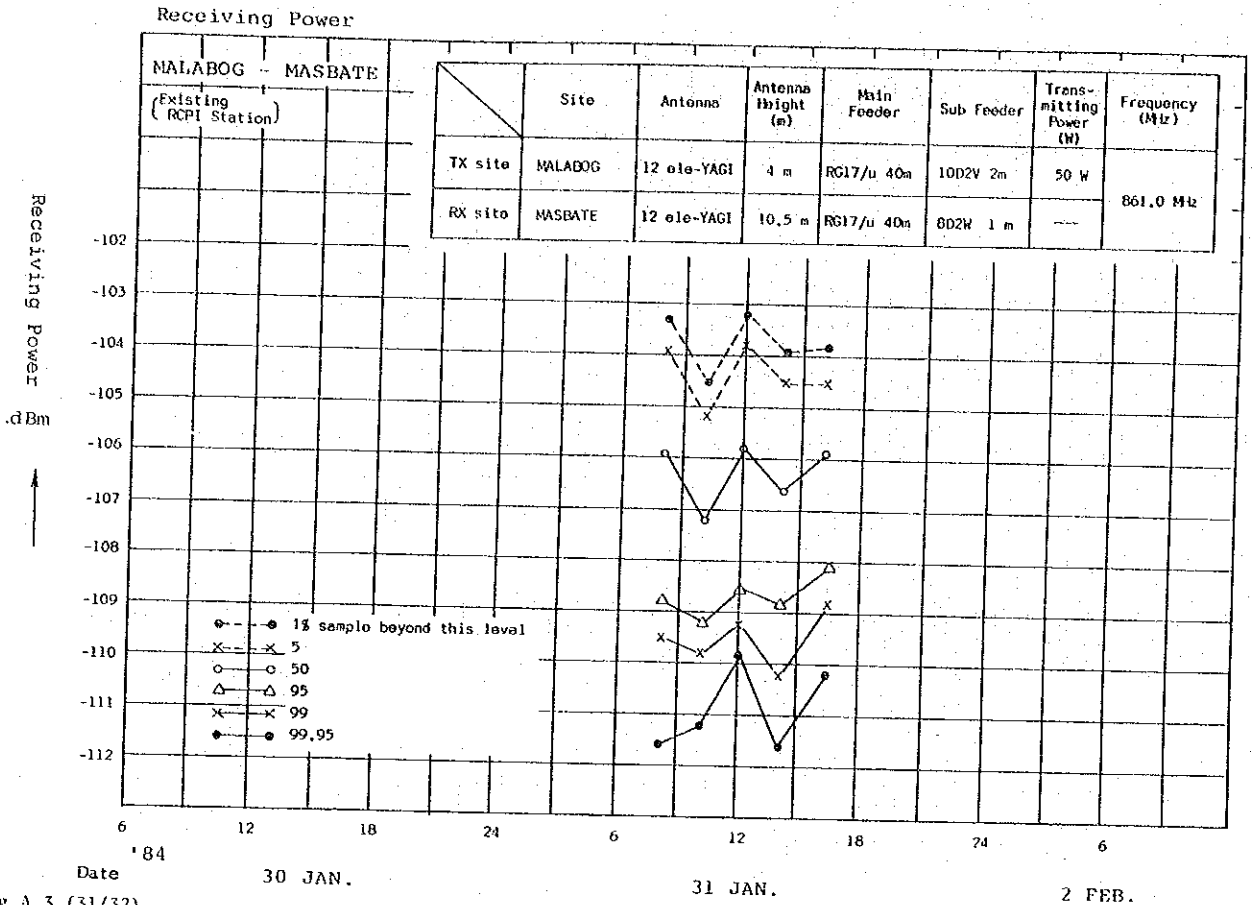


Fig.A.3 (31/32)

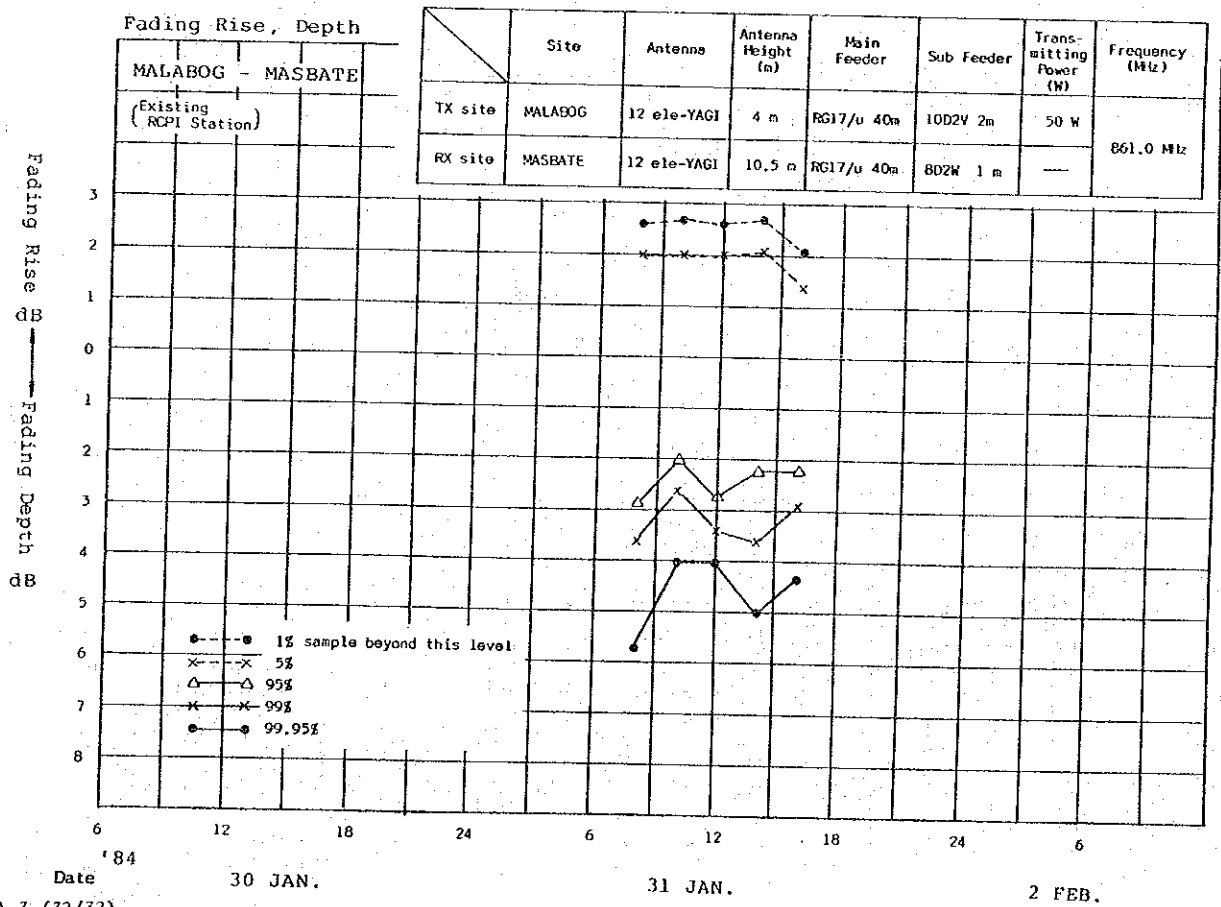


Fig.A.3 (32/32)