

# COMPACTION TEST (ESSAI DE COMPACTAGE)

FOR REPORTING  
(POUR LE RAPPORT)

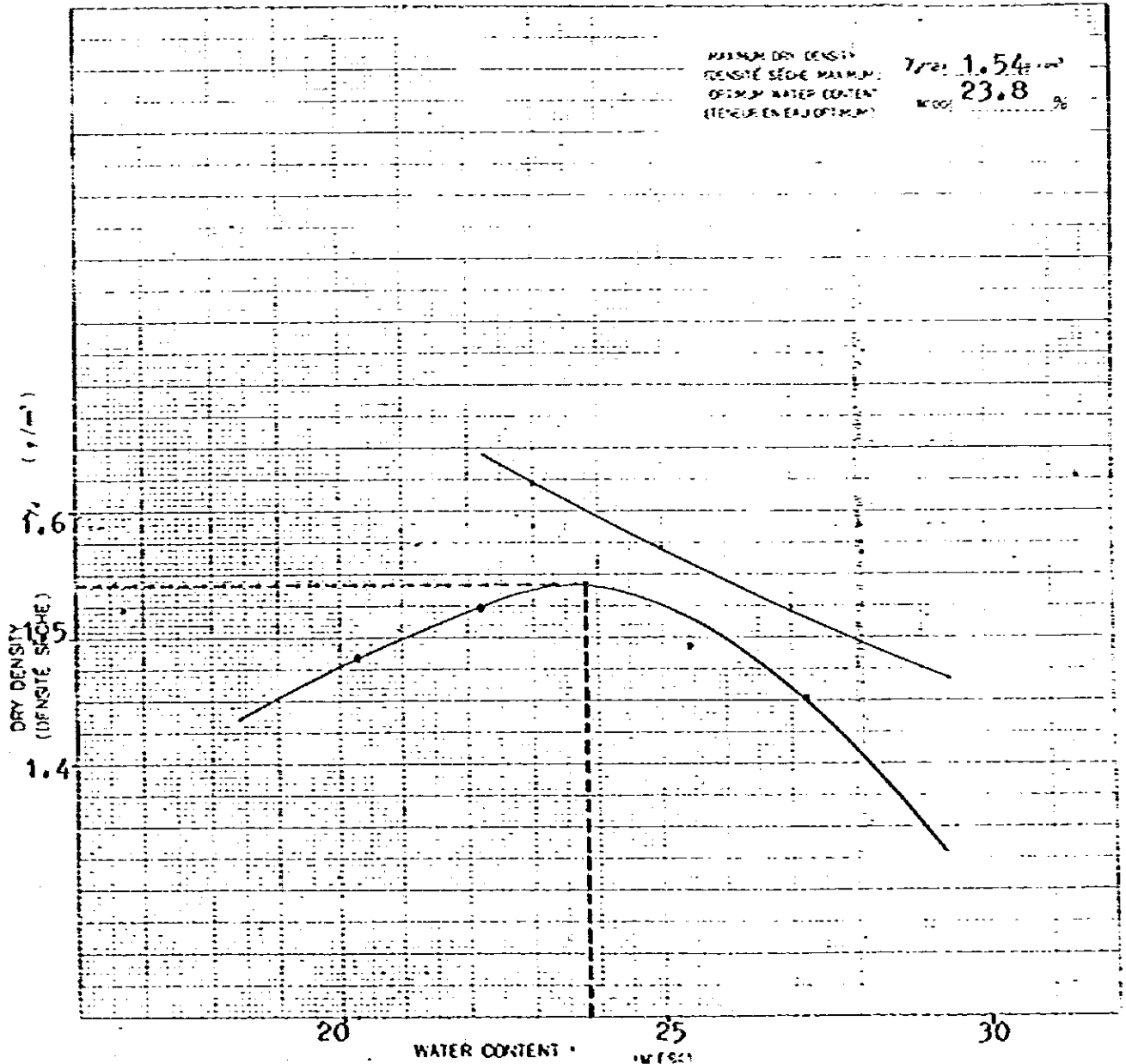
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ)	Bila Irr, ( Canal Route )	DATE (DATE)	Sept. 1981
SAMPLE NO & DEPTH (N° DE L'ENQUÊTE ET PROFONDEUR)	TP ~ 0 L ( 0.5 m ~ 1.2 m )	TESTED BY (ESSAI PAR)	Bina Mergu L.

MOLD (MOULE)	No	1	WEIGHT (POIDS)	2015	MOLD DIAMETER (DIAMÈTRE INT)	10.2	CAPACITY (CAPACITÉ)	942
RAMMER (PLOIN)	WEIGHT (POIDS)	250	HEIGHT OF DROP (HAUTEUR DE CHUTE)	30	BLOWS PER LAYER (NOMBRE DE COUPS PAR CHAQUE COUCHE)	25	NUMBER OF LAYERS (NOMBRE DE COUCHE)	3
MATERIAL USED FOR SPECIMENS (MATÉRIAU D'OSI POUR DU LES SPÉCIMENS)			REPROCESSING-DIFFERENT (RECONDITIONNÉ-AUTRE)		SOIL PREPARED FOR TEST (SOL PRÉPARÉ POUR L'ESSAI)		METHOD NO. USED (MÉTHODE N° D'OSI)	

NATURAL WATER CONTENT (TENEUR NATURELLE EN EAU) % **27.9**      WATER CONTENT AFTER AIR DRY (TENEUR EN EAU APRÈS SÈCHAGE À L' AIR LIBRE) % **-**      SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) **2.59**

MAX GRN SIZE ALLOWED (GRANULOMÈTRE MAXIMUM) **4.76**      % OF MATERIAL OVER THE MAX GRN SIZE ALLOWED (% DE MATÉRIAU DE GRANULOMÈTRE SUPÉRIEURE À CELLE ADMISE) % **-**

TEST NO (N° DE L'ESSAI)	1	2	3	4	5	6	7	8
DRY DENSITY (DENSITÉ SÈCHE) $\gamma_d$ ( $\text{g}/\text{cm}^3$ )	1.483	1.522	1.542	1.492	1.453			
MEAN WATER CONTENT (TENEUR MOYENNE EN EAU) %	20.3	22.2	23.8	25.4	27.2			



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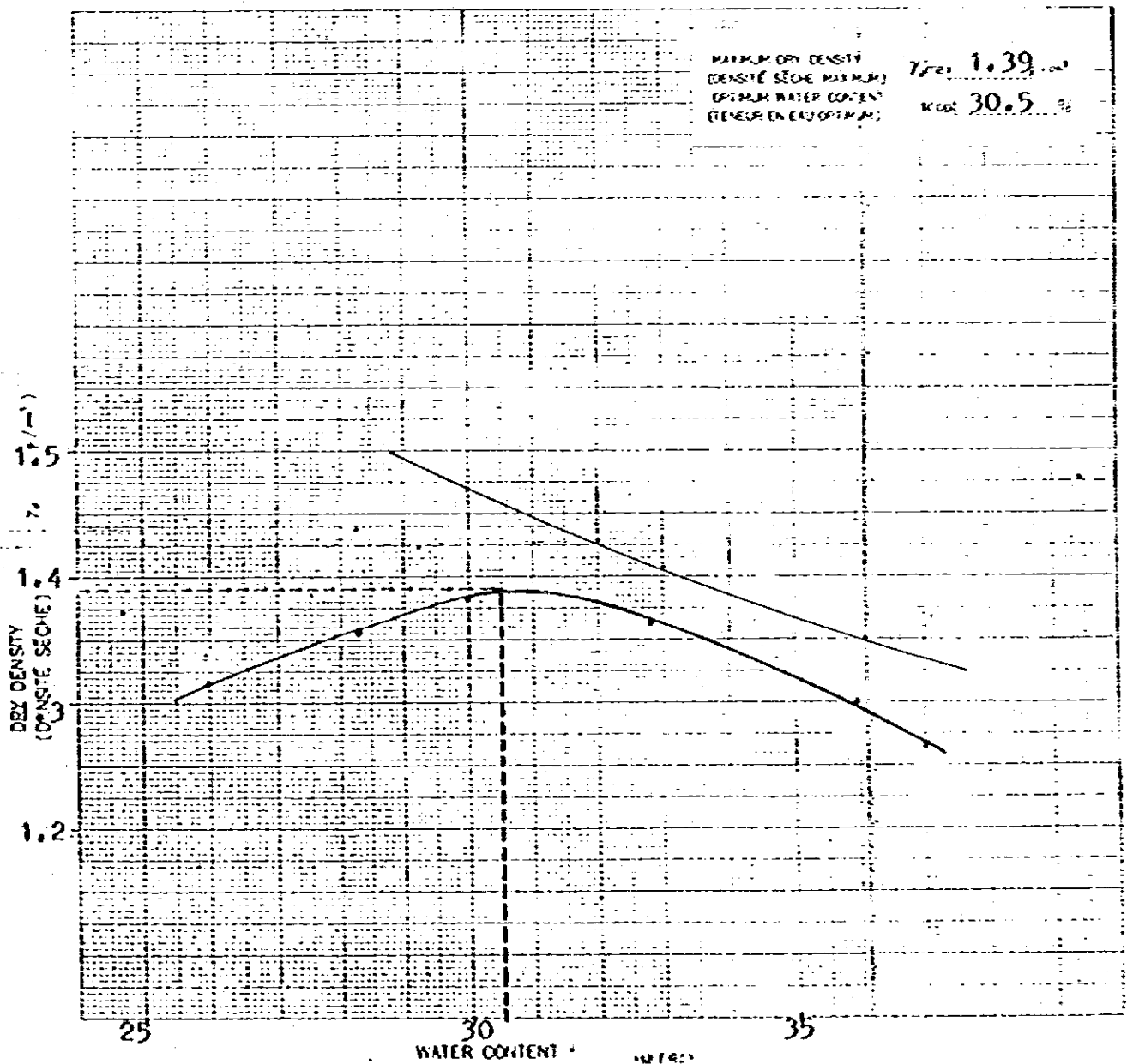
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ):	Bila Irr. ( Canal Route )	DATE (DATE):	Sept , 1981
SAMPLE NO & DEPTH (N° DE L'ÉCHANTILLON ET PROFONDEUR):	TP - 1 ( 0.5 m - 2.5 m )	TESTED BY (ESSAI PAR):	Bina Marga L.

MOULD (MOULE)	No	1	WEIGHT (POIDS)	2015	#SIDE DIAMETER (DIAMÈTRE INT.)	10.2	CAPACITY (CAPACITÉ)	942 <sup>cc</sup>
RAMMER (PLOU)	WEIGHT (POIDS)	250	HEIGHT OF DROP (HAUTEUR DE CHUTE)	30	BLOBS PER LAYER (BOBES DE COUS POUR CHAQUE COUCHE)	25	NUMBER OF LAYERS (NOMBRE DE COUCHE)	3
MATERIAL USED FOR SPECIMENS (MATÉRIAU D'USI POUR DU LES SPÉCIMENS)			REPROCESSING-DIFFERENT (RECONSTITUÉ-AUTRE)			SOIL PREPARED FOR TEST (SOL PRÉPARÉ POUR L'ESSAI)		APPROX. WET STATE (ÉTAT À L'AP. LIQ. NON SÈCHÉ)

NATURAL WATER CONTENT (TENEUR NATURELLE EN EAU)  $w$  36.7 %      WATER CONTENT AFTER AIR DRY (TENEUR EN EAU APRÈS SÈCHAGE À L' AIR LIBRE)  $w_p$         %      SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) 2.63

MAX. GRAN SIZE ALLOWED (GRAVILOMÈTRE MAXIMUM) 4.76 mm      % OF MATERIAL OVER THE MAX GRAN SIZE ALLOWED (% DE MATÉRIAU DE GRAVILOMÈTRE SUPÉRIEURE À CELLE ADISE)        %

TEST NO (N° DE L'ESSAI)	1	2	3	4	5	6	7	8
DDV DENSITY (DENSITÉ SÈCHE) $\gamma_d$ ( $\text{g}/\text{cm}^3$ )	1.315	1.355	1.384	1.365	1.305	1.267		
MEAN WATER CONTENT (TENEUR MOYENNE EN EAU) $w$ (%)	25.95	28.30	30.04	32.83	35.98	37.07		



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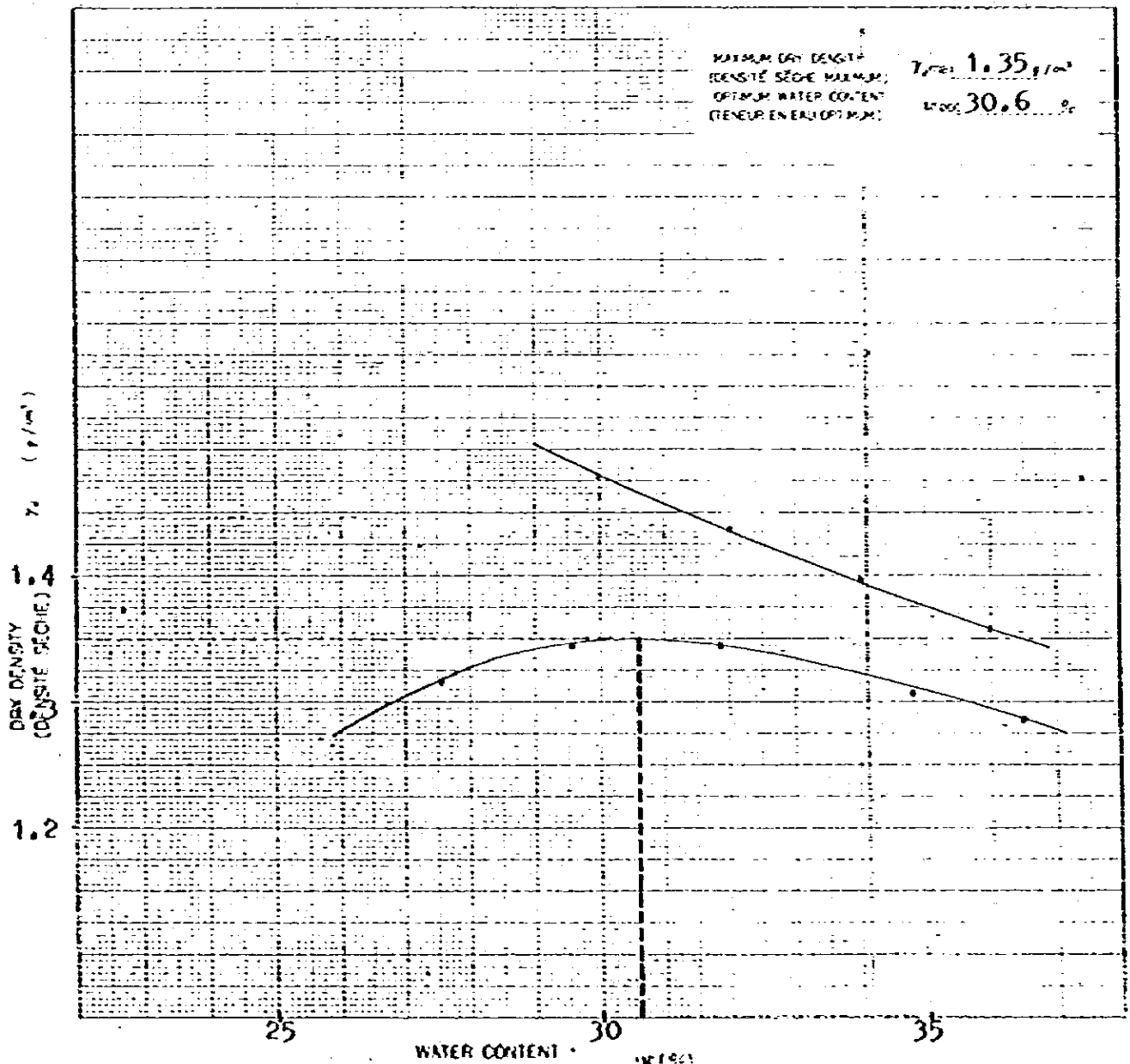
NAME OF SURVEY & LOCALITY (DENOMINATION DE L'ENQUÊTE ET LOCALITÉ):	Bila Irr. ( Canal Route )	DATE (DATE)	Sept , 1981
SAMPLE NO & DEPTH (N° DE L'ÉCHANTILLON ET PROFONDEUR):	TP - 2 ( 0.3 m - 1.4 m )	TESTED BY (ESSAI PAR):	Bina Warga L.

MOLD (MOULE)	No	1	WEIGHT (POIDS)	2015	MOLE DIAMETER (DIAMÈTRE INT.)	10.2	CAPACITY (CAPACITÉ)	942 <sup>cm<sup>3</sup></sup>
RAMMER (PLOU)	WEIGHT (POIDS)	250	HEIGHT OF DROP (HAUTEUR DE CHUTE)	30 <sup>cm</sup>	BLOWS PER LAYER (NOMBRE DE COUPS PAR COUCHE)	25	NUMBER OF LAYERS (NOMBRE DE COUCHE)	3
MATERIAL USED FOR SPECIMENS (MATÉRIAU UTILISÉ POUR DU LES SPÉCIMENS):	REPROCESSING-DIFFERENT (RECONDITIONNÉ-AUTRE)		SOIL PREPARED FOR TEST (SOL PRÉPARÉ POUR L'ESSAI)		APPROX. MOISTURE (TENEUR À L'AP. LIÈGE MAX. SÈCHE)			

NATURAL WATER CONTENT (TENEUR NATURELLE EN EAU)  $w_n$  **40.04 %**      WATER CONTENT AFTER AIR DRY (TENEUR EN EAU APRÈS SÈCHAGE À L' AIR LIÈGE) **30.6 %**      SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) **2.66**

MAX GRAN SIZE ALLOWED (GRANULOMÈTRE MAXIMUM ADMISE) **4.76 mm**      % OF MATERIAL OVER THE MAX GRAN SIZE ALLOWED (% DE MATÉRIAU DE GRANULOMÈTRE SUPÉRIEURE À CELLE ADMISE) **5%**

TEST NO (N° DE L'ESSAI)	1	2	3	4	5	6	7	8
DRY DENSITY (DENSITÉ SÈCHE) $\rho_d$ ( $\text{g/cm}^3$ )	1.316	1.345	1.345	1.306	1.286			
WATER CONTENT (TENEUR EN EAU) $w$ (%)	27.58	29.54	31.84	34.81	36.50			



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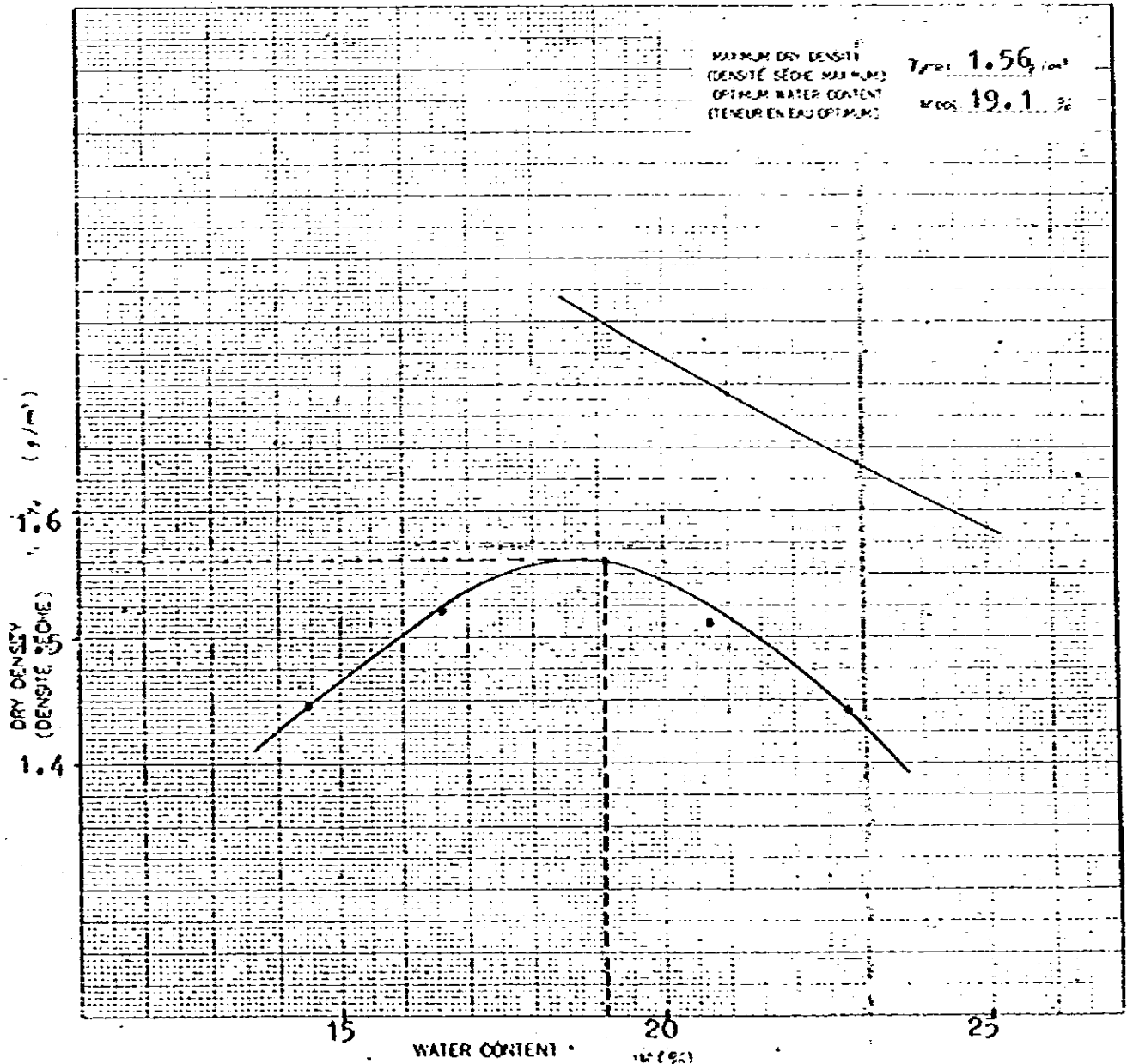
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ):	Bila Irr. ( Canal Route )	DATE (DATE)	Sept , 1981
SAMPLE NO & DEPTH (N° DE L'ÉCHANTILLON ET PROFONDEUR):	TP - 3 ( 0.8 m - 1.4 m )	TESTED BY (ESSAI PAR):	Bina Marga J.

MOLD (MOULE)	No	2	WEIGHT (POIDS)	1970	MOUSE DIAMETER (DIAMÈTRE INT)	10.2	CAPACITY (CAPACITÉ)	942
RAMMER (PLOIN)	WEIGHT (POIDS)	250	HEIGHT OF DROP (HAUTEUR DE CHUTE)	30	BLOWS PER LAYER (NOMBRE DE COUPS PAR COURSE COULÉE)	25	NUMBER OF LAYERS (NOMBRE DE COUCHE)	3
MATERIAL USED FOR SPECIMENS (MATÉRIAU D'OSI POUR OU LES SPÉCIMENS)			REPROCESSING-DIFFERENT (RECONDITIONNÉ-AUTRE)		SOIL PREPARED FOR TEST (SOL PRÉPARÉ POUR L'ESSAI)		AIR-DRIED-NOT-EGGED (SÈCHÉ À L'AIR LIBRE-NON SÈCHÉ)	

NATURAL WATER CONTENT (TENEUR NATURELLE EN EAU)  $w_n$  **35.0** %      WATER CONTENT AFTER AIR DRY (TENEUR EN EAU APRÈS SÈCHAGE À L' AIR LIBRE) \_\_\_\_\_ %      SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) **2.63**

MAX GRAN SIZE ALLOWED (GRAVLOMÈTRE MAXIMUM ADMISE) **4.76** - % OF MATERIAL OVER THE MAX GRAN SIZE ALLOWED (% DE MATÉRIAU DE GRAVLOMÈTRE SUPÉRIEURE À CELLE ADMISE) \_\_\_\_\_ %

TEST NO (N° DE L'ESSAI)	1	2	3	4	5	6	7	8
DRY DENSITY (DENSITÉ SÈCHE) $\gamma_d$ (g/cm <sup>3</sup> )	1.463	1.522	1.561	1.512	1.443			
MEAN WATER CONTENT (TENEUR MOYENNE EN EAU) $w$ (%)	14.48	16.60	19.10	20.70	22.79			



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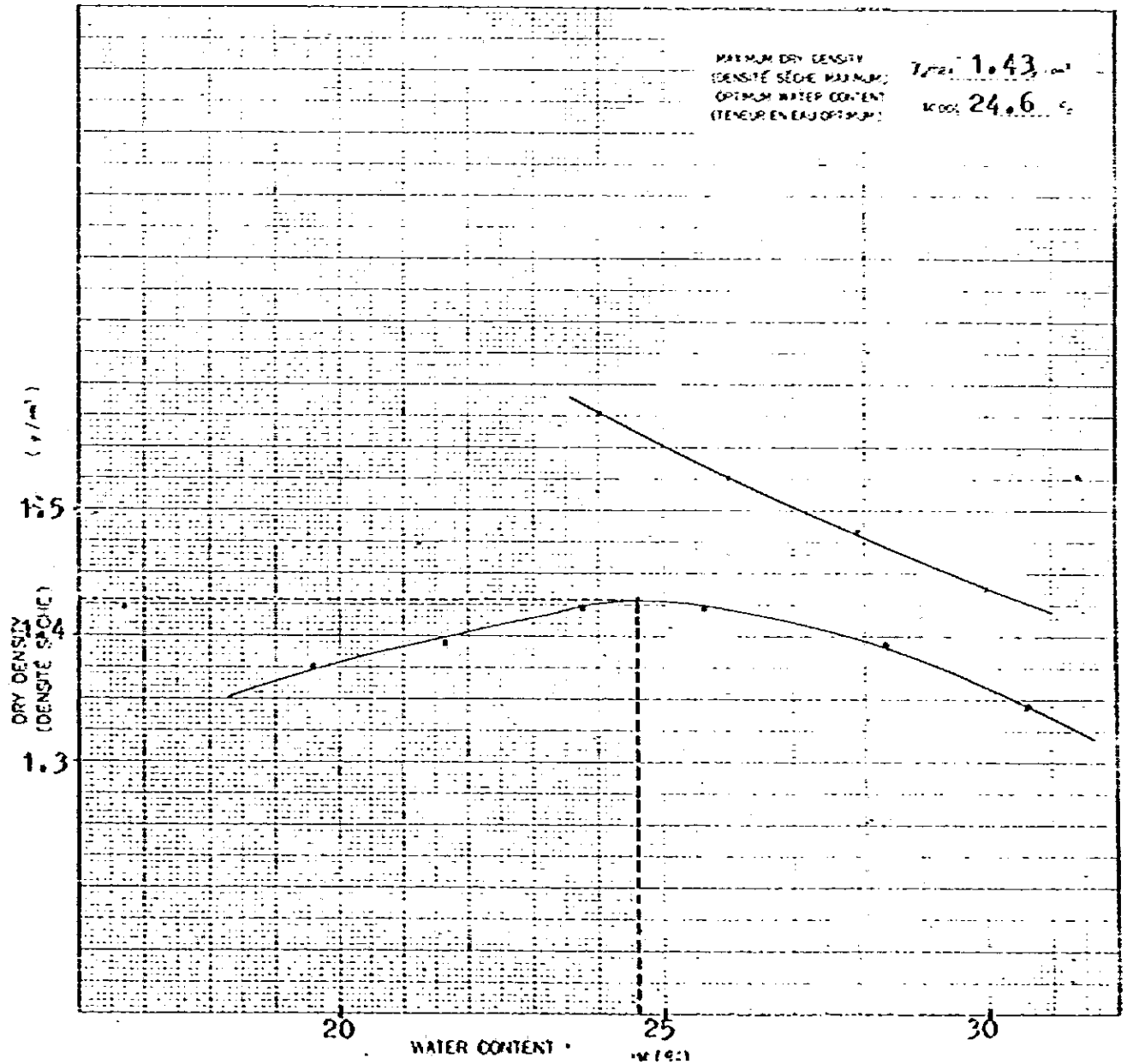
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ):	Bila Irr. ( Canal Route )	DATE (DATE):	Sept, 1981
SAMPLE NO & DEPTH (N° DE L'ÉCHANTILLON ET PROFONDEUR):	TP - 4 ( 1.0 m - 1.8 m )	TESTED BY (ESSAI PAR):	Bina Marga L.

MOLD (MOULE)	No	1	WEIGHT (POIDS)	2015	MOUSE DIAMETER (DIAMÈTRE INT.)	10.2	CAPACITY (CAPACITÉ):	942
RAMMER (PILON)	WEIGHT (POIDS)	250	HEIGHT OF DROP (HAUTEUR DE CHUTE):	30	BLOWS PER LAYER (NOMBRE DE COUPS PAR CHAQUE COUCHE)	25	NUMBER OF LAYERS (NOMBRE DE COUCHE):	3
MATERIAL USED FOR SPECIMENS (MATÉRIAU UTILISÉ POUR LES SPÉCIMENS):			REPROCESSING-DIFFERENT (RECONDITIONNÉ-AUTRE):		SOIL PREPARED FOR TEST (SOL PRÉPARÉ POUR L'ESSAI):		MOISTURE METHOD (MÉTODE T L'AR LÈGE-MO. SÈCHE)	

NATURAL WATER CONTENT (TENEUR NATURELLE EN EAU)  $w$ : **33.50** %      WATER CONTENT AFTER AIR DRY (TENEUR EN EAU APRÈS SÈCHAGE À L' AIR LÈGE) \_\_\_\_\_ %      SPECIFIC GRAVITY (POIDS SPÉCIFIQUE): **2.54**

MAX. GRAIN SIZE ALLOWED (GRANULOMÈTRE MAXIMUM ADMISE) **4.76** mm      % OF MATERIAL OVER THE MAX. GRAIN SIZE ALLOWED (POURCENT DE MATÉRIAU DE GRANULOMÈTRE SUPÉRIEURE À CELLE ADMISE) \_\_\_\_\_ %

TEST NO (N° DE L'ESSAI)	1	2	3	4	5	6	7	8
DRY DENSITY (DENSITÉ SÈCHE) $\gamma_d$ (t/m <sup>3</sup> )	1.375	1.394	1.424	1.424	1.394	1.345		
MEAN WATER CONTENT (TENEUR MOYENNE EN EAU) $w$ (%)	19.55	21.65	23.72	25.59	28.43	30.60		



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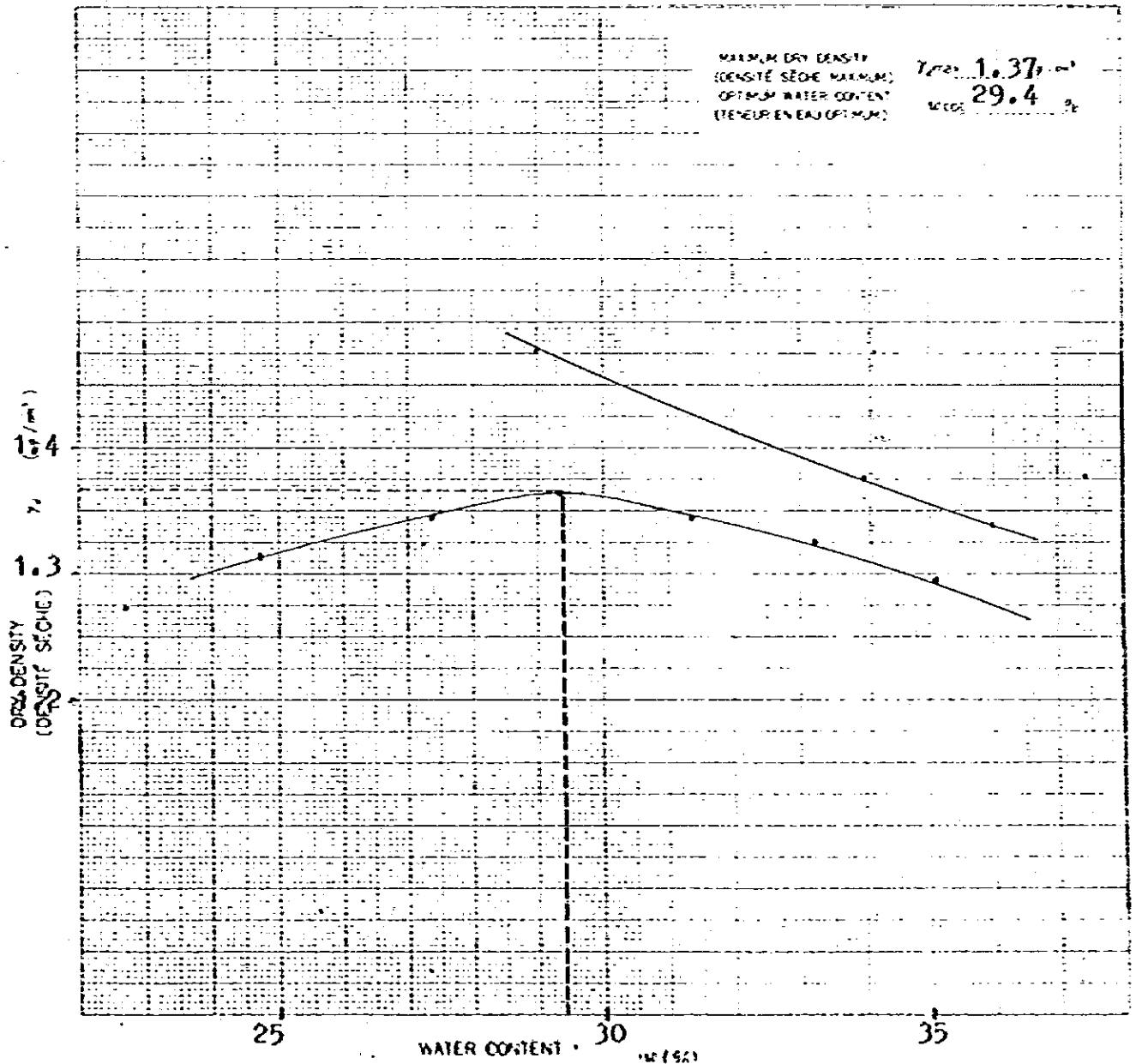
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ÉCHANTILLON ET LOCALITÉ):	Bila Irr, ( Canal Route )	DATE (DATE)	Sept, 1981
SAMPLE NO & DEPTH (N° DE L'ÉCHANTILLON ET PROFONDEUR):	TP - 5 ( 1.5 m - 2.0 m )	TESTED BY (ESSAI PAR):	Bina Marga L.

MOLD (MOULE)	NO	1	WEIGHT (POIDS)	2015	MOUSE DIAMETER (DIAMÈTRE INT.)	10.2	CAPACITY (CAPACITÉ)	942 cm <sup>3</sup>
RAMMER (PILON)	WEIGHT (POIDS)	250	HEIGHT OF DROP (HAUTEUR DE CHUTE)	30 cm	BLOWS PER LAYER (NOMBRE DE COUPS PAR CHACQUE COUCHE)	25	NUMBER OF LAYERS (NOMBRE DE COUCHE)	3
MATERIAL USED FOR SPECIMENS (MATÉRIAU UTILISÉ POUR LES SPÉCIMENS)			REPROCESSING - DIFFERENT (RECONDITIONNÉ - AUTRE)		SOIL PREPARED FOR TEST (SOL PRÉPARÉ POUR L'ESSAI)		WETTED NOT DRYED (SÉCHÉ À L'AIR LIBRE - NON SÉCHÉ)	

NATURAL WATER CONTENT (TENEUR NATURELLE EN EAU)  $w$  = **33.1** %      WATER CONTENT AFTER AIR DRY (TENEUR EN EAU APRÈS SÈCHAGE À L'AIR LIBRE)  $w_p$  = \_\_\_\_\_ %      SPECIFIC GRAVITY (POIDS SPÉCIFIQUE)  $G_s$  = **2.59**

MAX GRAM SIZE ALLOWED (GRANULOMÈTRE MAXIMUM ADMISSIBLE)  $d_{60}$  = **4.76** mm      % OF MATERIAL OVER THE MAX GRAM SIZE ALLOWED (% DE MATÉRIAU DE GRANULOMÈTRE SUPÉRIEURE À CELLE ADMISE) = \_\_\_\_\_ %

TEST NO (N° DE L'ESSAI)	1	2	3	4	5	6	7	8
DRY DENSITY (DENSITÉ SÈCHE) $\gamma_d$ (g/cm <sup>3</sup> )	1.316	1.345	1.365	1.345	1.326	1.296		
MEAN WATER CONTENT (TENEUR MOYENNE EN EAU) $w$ (%)	24.71	27.37	29.30	31.38	33.24	35.12		



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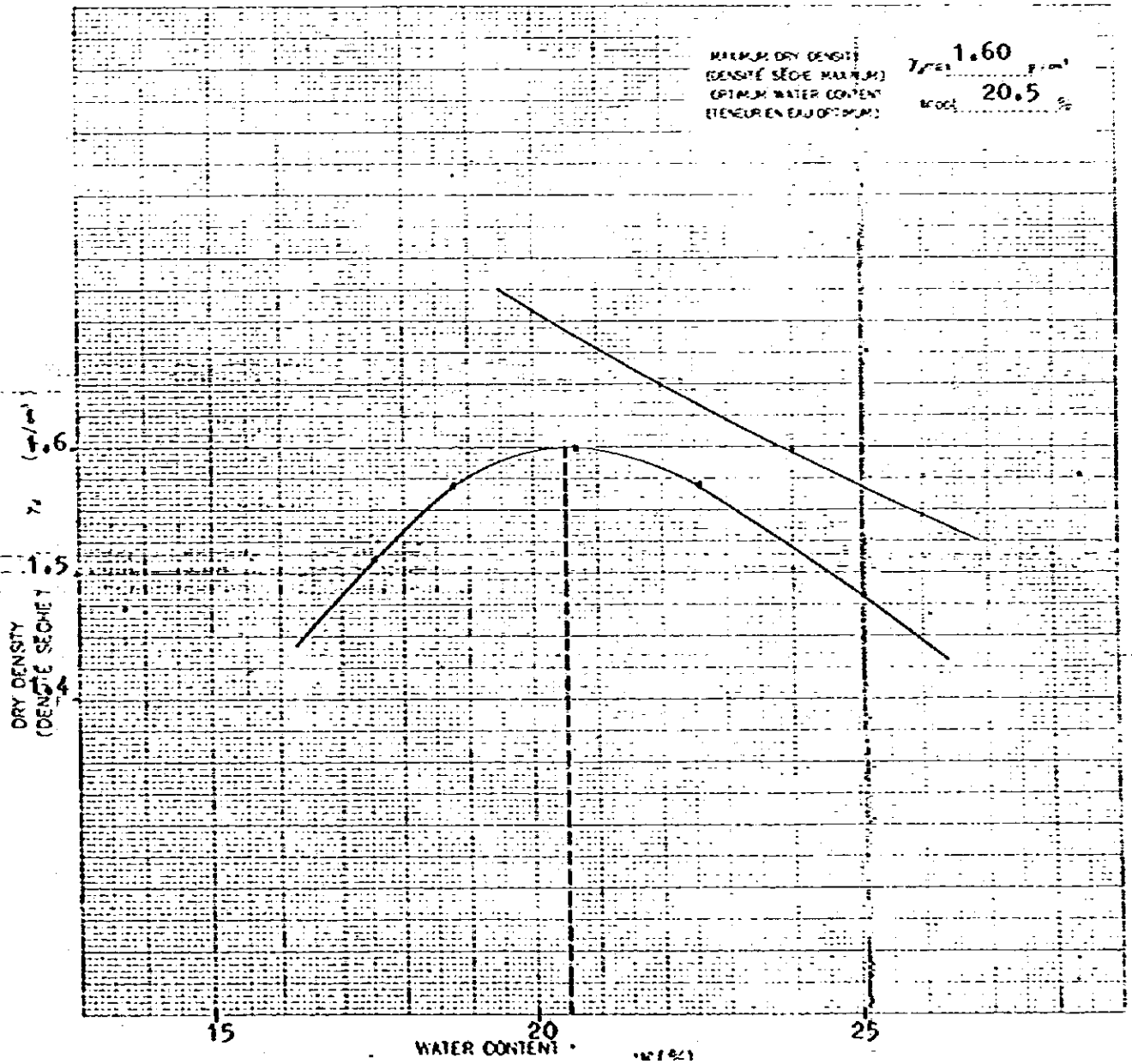
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ):	Bila Irr. ( Canal Route )	DATE (DATE)	Sept. , 1981
SAMPLE NO & DEPTH (N° DE L'ÉCHANTILLON ET PROFONDEUR):	TP - 6 ( 0.6 m - 1.4 m )	TESTED BY (ESSAI PAR):	Bina Marga L.

MOULD (MOULE)	No. 1	WEIGHT (POIDS) 2015	ROD DIAMETER (DIAMÈTRE INT.) 10.2	CAPACITY (CAPACITÉ) 942
RAMMER (PÉON)	WEIGHT (POIDS) 250	HEIGHT OF DROP (HAUTEUR DE CHUTE) 30	BLOWS PER LAYER (NOMBRE DE COUPS PAR COUCHE) 25	NUMBER OF LAYERS (NOMBRE DE COUCHE) 3
MATERIAL USED FOR SPECIMENS (MATÉRIAU CHOISI POUR LES SPÉCIMENS)		REPROCESSING-DIFFERENT (RECONDITIONNÉ-AUTRE)	SOIL PREPARED FOR TEST (SOIL PRÉPARÉ POUR L'ESSAI)	APPROVED NO. PAGE (SÉRIÉ À L'AIR LIBRE - NO. SÉRIÉ)

NATURAL WATER CONTENT (TENEUR NATURELLE EN EAU)  $w$  % 20.3 %      WATER CONTENT AFTER AIR DRY (TENEUR EN EAU APRÈS SÈCHAGE À L' AIR LIBRE) %      SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) 2.58

MAX GRAN SIZE ALLOWED (GRANULOMÈTRE MAXIMUM ADMISE) 4.75 mm      % OF MATERIAL OVER THE MAX GRAN SIZE ALLOWED (% DE MATÉRIAU DE GRANULOMÈTRE SUPÉRIEURE À CELLE ADMISE) %

TEST NO (N° DE L'ESSAI)	1	2	3	4	5	6	7	8
DRY DENSITY (DENSITÉ SÈCHE) $\gamma_d$ (g/cm <sup>3</sup> )	1.512	1.571	1.600	1.571	1.483			
MEAN WATER CONTENT (TENEUR MOYENNE EN EAU) $w$ (%)	17.55	18.75	20.65	22.56	25.10			



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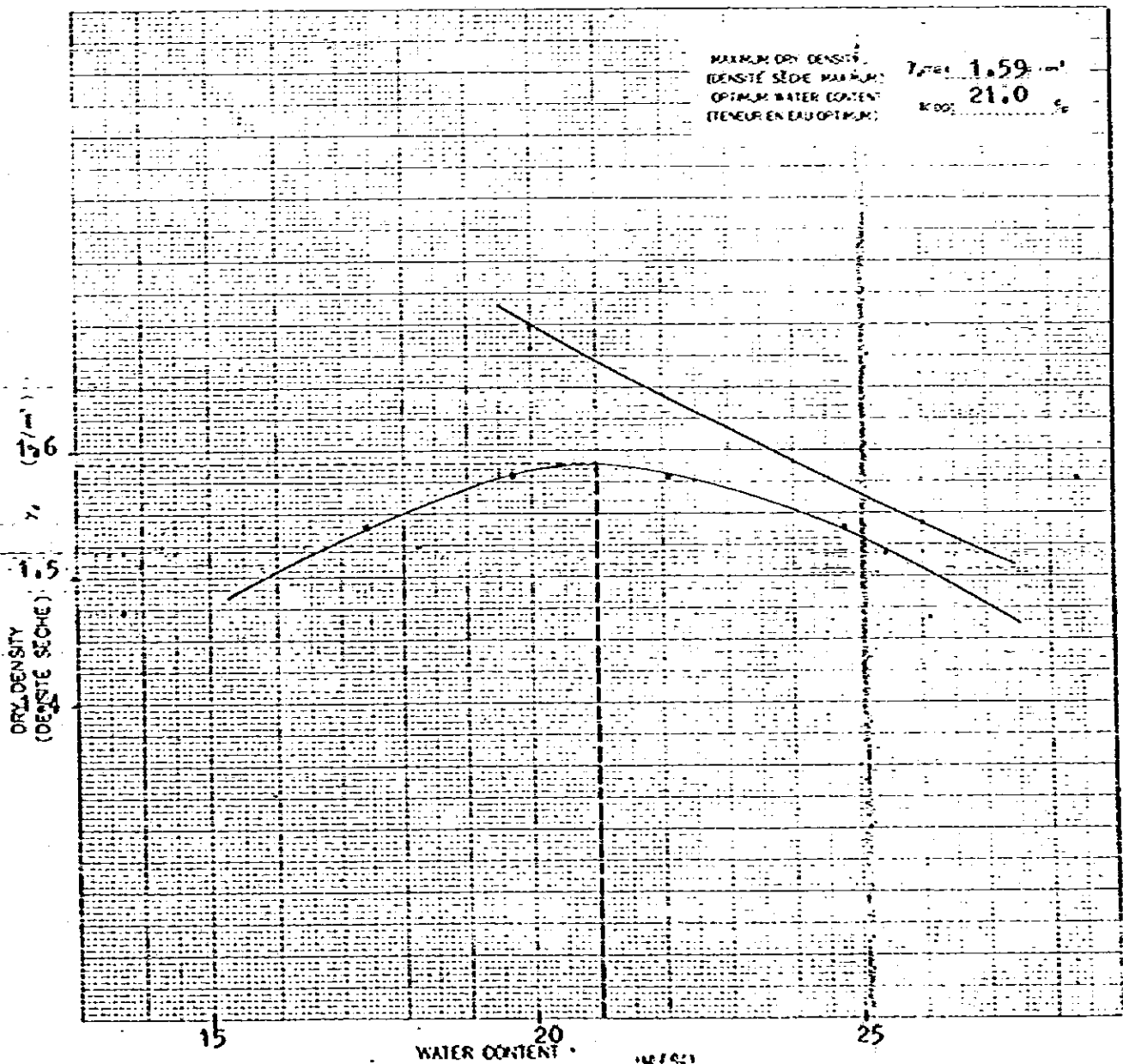
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ):	Bila Irr. (Canal Route)	DATE (DATE)	Sept. , 1981
SAMPLE NO & DEPTH (N° DE L'ÉCHANTILLON ET PROFONDEUR):	TP - 7 ( 1.6 m - 2.0 m )	TESTED BY (ESSAI PAR):	Bina Marga L.

MOULD (MOULE)	No	2	WEIGHT (POIDS)	1970	INSIDE DIAMETER (DIAMÈTRE INT.)	10.2	CAPACITY (CAPACITÉ)	942
RAMMER (PILOIN)	WEIGHT (POIDS)	250	HEIGHT OF DROP (HAUTEUR DE CHUTE)	30	BLOWS PER LAYER (NOMBRE DE COUPS PAR CHAQUE COUCHE)	25	NUMBER OF LAYERS (NOMBRE DE COUCHE)	3
MATERIAL USED FOR SPECIMENS (MATÉRIAU UTILISÉ POUR LES SPÉCIMENS)			REPROCESSING - DIFFERENT (RECONDITIONNÉ - AUTRE)		SOIL PREPARED FOR TEST (SOL PRÉPARÉ POUR L'ESSAI)		AIR DRYING - FREE (SÈCHE À L'AIR LIBRE - NON SÈCHE)	

NATURAL WATER CONTENT (TENUEUR NATURELLE EN EAU)  $w$  ..... 35.6 %      WATER CONTENT AFTER AIR DRY (TENUEUR EN EAU APRÈS SÈCHAGE À L'AIR LIBRE) .....      SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) ..... 2.58

MAX. GRAN SIZE ALLOWED (GRANULOMÈTRE MAXIMUM AUTORISÉ) ..... 4.75 ..... % OF MATERIAL OVER THE MAX GRAN SIZE ALLOWED (% DE MATÉRIAU DE GRANULOMÈTRE SUPÉRIEURE À CELLE AUTORISÉE) ..... %

TEST NO (N° DE L'ESSAI)	1	2	3	4	5	6	7	8
DRY DENSITY (DENSITÉ SÈCHE) $\gamma_d$ ( $t/m^3$ )	1.542	1.581	1.581	1.542	1.522			
MEAN WATER CONTENT (TENUEUR MOYENNE EN EAU) $w$ (%)	17.47	19.69	22.08	24.75	25.41			





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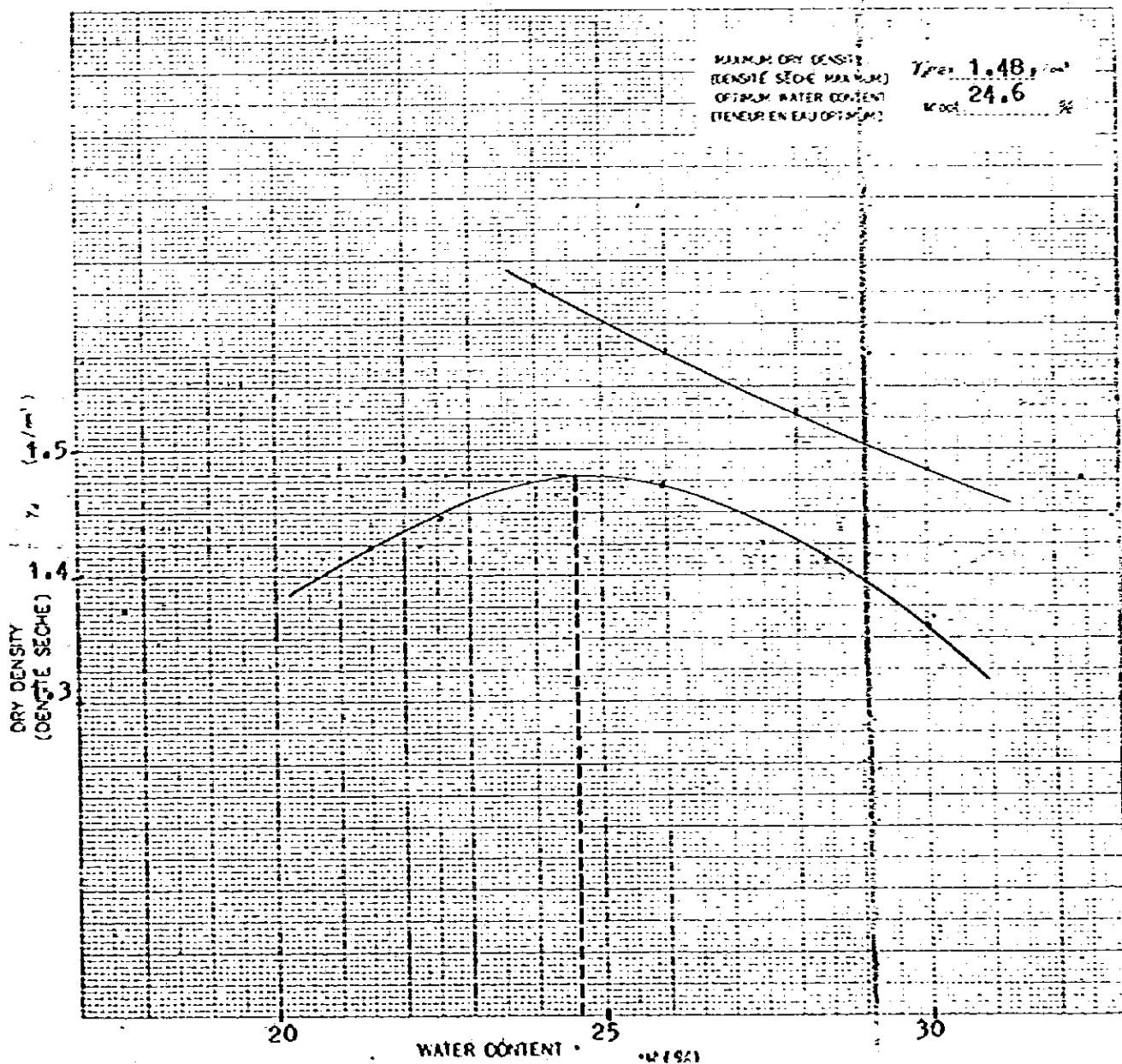
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ):	Bila Irr. ( Canal Route )	DATE (DATE)	Sept. , 1981
SAMPLE NO & DEPTH (N° DE L'ÉCHANTILLON ET PROFONDEUR):	TP - 8 ( 1.4 m - 2.0 m )	TESTED BY (ESSAI PAR)	Bina Narga J.

MOULD (MOULE)	No	2	WEIGHT (POIDS)	1970	PSIDE DIAMETER (DIAMÈTRE INT)	10.2	CAPACITY (CAPACITÉ)	942
RAMMER (PLOIN)	WEIGHT (POIDS)	250	HEIGHT OF DROP (HAUTEUR DE CHUTE)	30	BLOWS PER LAYER (NOMBRE DE COUPS PAR COUCHE)	25	NUMBER OF LAYERS (NOMBRE DE COUCHE)	3
MATERIAL USED FOR SPECIMENS (MATÉRIAU CHOISI POUR DU LES SPÉCIMENS)			REPROCESSING-DIFFERENT (RECONDITIONNÉ-AUTRE)			SOIL PREPARED FOR TEST (SOL PRÉPARÉ POUR L'ESSAI)		APPROX. NO. PAGES (SÉCÉ 7 L'AP. LÈGE. NO. SÉCÉ)

NATURAL WATER CONTENT (TENEUR NATURELLE EN EAU)  $w_n$  22.8 %      WATER CONTENT AFTER AIR-DRY (TENEUR EN EAU APRÈS SÈCHAGE À L' AIR LÈGE)      SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) 2.68

MAX GRAN SIZE ALLOWED (GRANULOMÈTRE MAXIMUM ADMISE) 4.75 mm      % OF MATERIAL OVER THE MAX GRAN SIZE ALLOWED (% DE MATÉRIAU DE GRANULOMÈTRE SUPÉRIEURE À CELLE ADMISE) %

TEST NO (N° DE L'ESSAI)	1	2	3	4	5	6	7	8
DRY DENSITY (DENSITÉ SÈCHE) $\gamma_d$ (t/m <sup>3</sup> )	1.424	1.453	1.473	1.414	1.385			
MEAN WATER CONTENT (TENEUR MOYENNE EN EAU) $w$ (%)	21.50	22.54	25.95	28.46	29.98			



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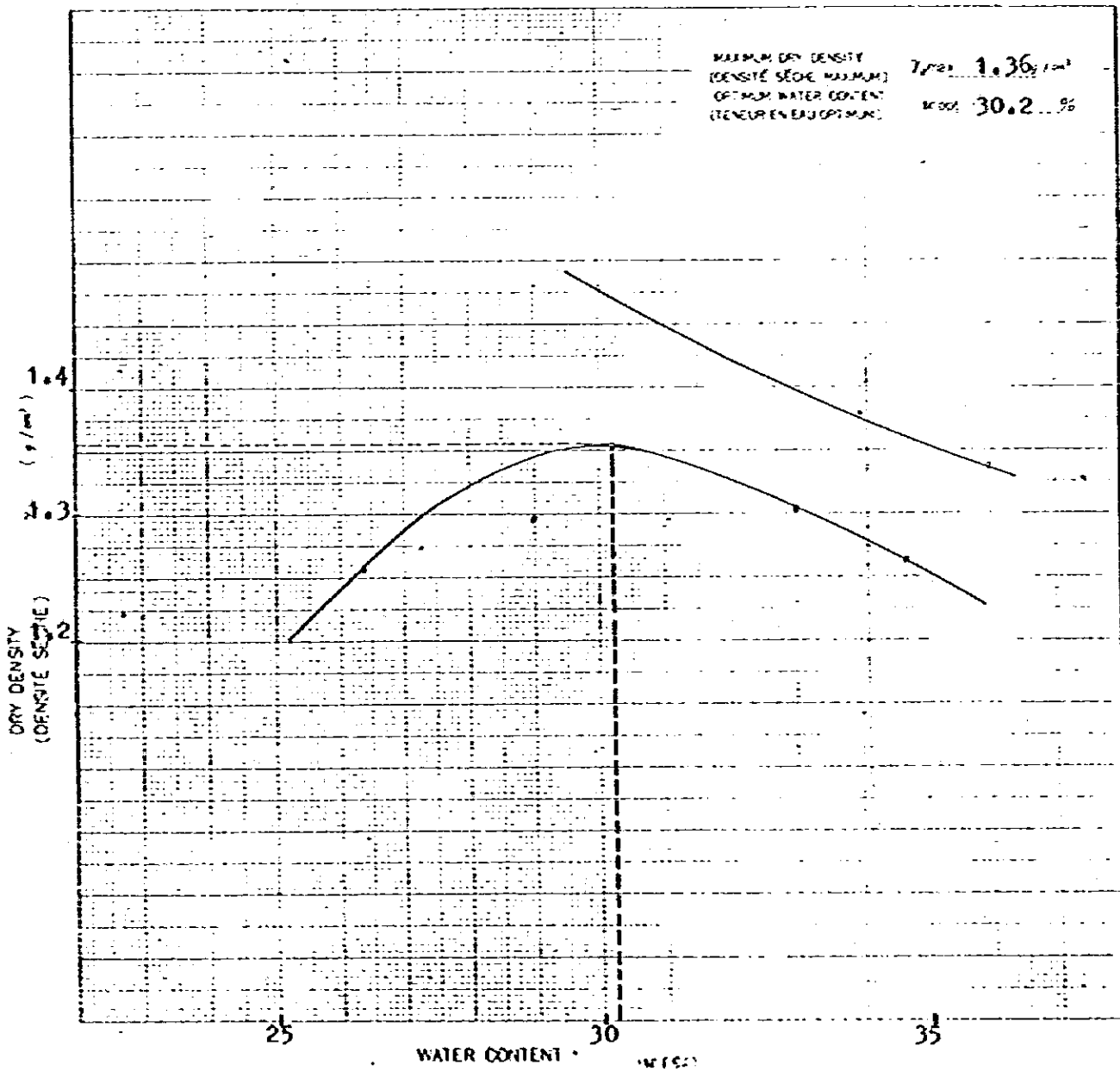
NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ)	Bila Irr. ( Flood Dike )	DATE (DATE)	Sept., 1981
SAMPLE NO & DEPTH (N° DE L'ÉCHANTILLON ET PROFONDEUR)	PW - 1 ( 0.5 m )	TESTED BY (ESSAYÉ PAR)	Bina Marga L.

MOULD (MOULE)	NO. 1	WEIGHT (POIDS)	2015	PISSE DIAMETER (DIAMÈTRE INT.)	10.2	CAPACITY (CAPACITÉ)	942	
RAMMER (PLOU)	WEIGHT (POIDS)	250	HEIGHT OF DROP (HAUTEUR DE CHUTE)	30	BLOWS PER LAYER (NOMBRE DE COUPS PAR COUCHE)	25	NUMBER OF LAYERS (NOMBRE DE COUCHE)	3
MATERIAL USED FOR SPECIMENS (MATÉRIAU UTILISÉ POUR DU LES SPÉCIMENS)	REPROCESSING-DIFFERENT (RECONDITIONNÉ-AUTRE)			SOIL PREPARED FOR TEST (SOL PRÉPARÉ POUR L'ESSAI)		ARRANGED AS PER (SÉCÉPÉ T L L'AF L'ÉPRE NON SÈCÉ)		

NATURAL WATER CONTENT (TENEUR NATURELLE EN EAU)  $w$  **43.9** % WATER CONTENT AFTER AIR DRY (TENEUR EN EAU APRÈS SÈCHAGE À L' AIR LIBRE) \_\_\_\_\_ % SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) **2.60**

MAX GRAM SIZE ALLOWED (GRAVIMÈTRE MAXIMUM) **4.76** mm % OF MATERIAL OVER THE MAX GRAM SIZE ALLOWED ( % DE MATÉRIAU DE GRAVIMÈTRE SUPÉRIEURE À CELLE ADMISE) \_\_\_\_\_ %

TEST NO (N° DE L'ESSAI)	1	2	3	4	5	6	7	8
DRY DENSITY (DENSITÉ SÈCHE) $\gamma_d$ (g/cm <sup>3</sup> )	1.257	1.296	1.355	1.305	1.266			
MEAN WATER CONTENT (TENEUR MOYENNE EN EAU) $w$ (%)	26.37	28.96	30.19	33.01	34.67			



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NAME OF SURVEY & LOCALITY (DÉNOMINATION DE L'ENQUÊTE ET LOCALITÉ)	Bila Irr. ( Flood Control )	DATE (DATE)	Sept, 1981
SAMPLE NO & DEPTH (N° DE L'ÉCHANTILLON ET PROFONDEUR)	ER - 4 ( 0.5 m - )	TESTED BY (ESSAI PAR)	Bina Karga L.

MOLD (MOULE)	No	1	WEIGHT (POIDS)	2015	MOLE DIAMETER (DIAMÈTRE INT.)	10.2	CAPACITY (CAPACITÉ)	942 cm <sup>3</sup>
RAMMER (PLOIN)	WEIGHT (POIDS)	250	HEIGHT OF DROP (HAUTEUR DE CHUTE)	30 cm	BLOKS PER LAYER (NOMBRE DE COUS PAR COUCHE)	25	NUMBER OF LAYERS (NOMBRE DE COUCHE)	3
MATERIAL USED FOR SPECIMENS (MATÉRIAU CHOSI POUR DU LES SPÉCIMENS)			REPROCESSING-DIFFERENT (RECONDITIONNÉ-AUTRE)			SOIL PREPARED FOR TEST (SOIL PRÉPARÉ POUR L'ESSAI)		APPROX. MOISTURE (SÈCHE 7 L'APRÈS NON SÈCHE)

NATURAL WATER CONTENT (TENEUR NATURELLE EN EAU)  $w$  ..... 39.1 %

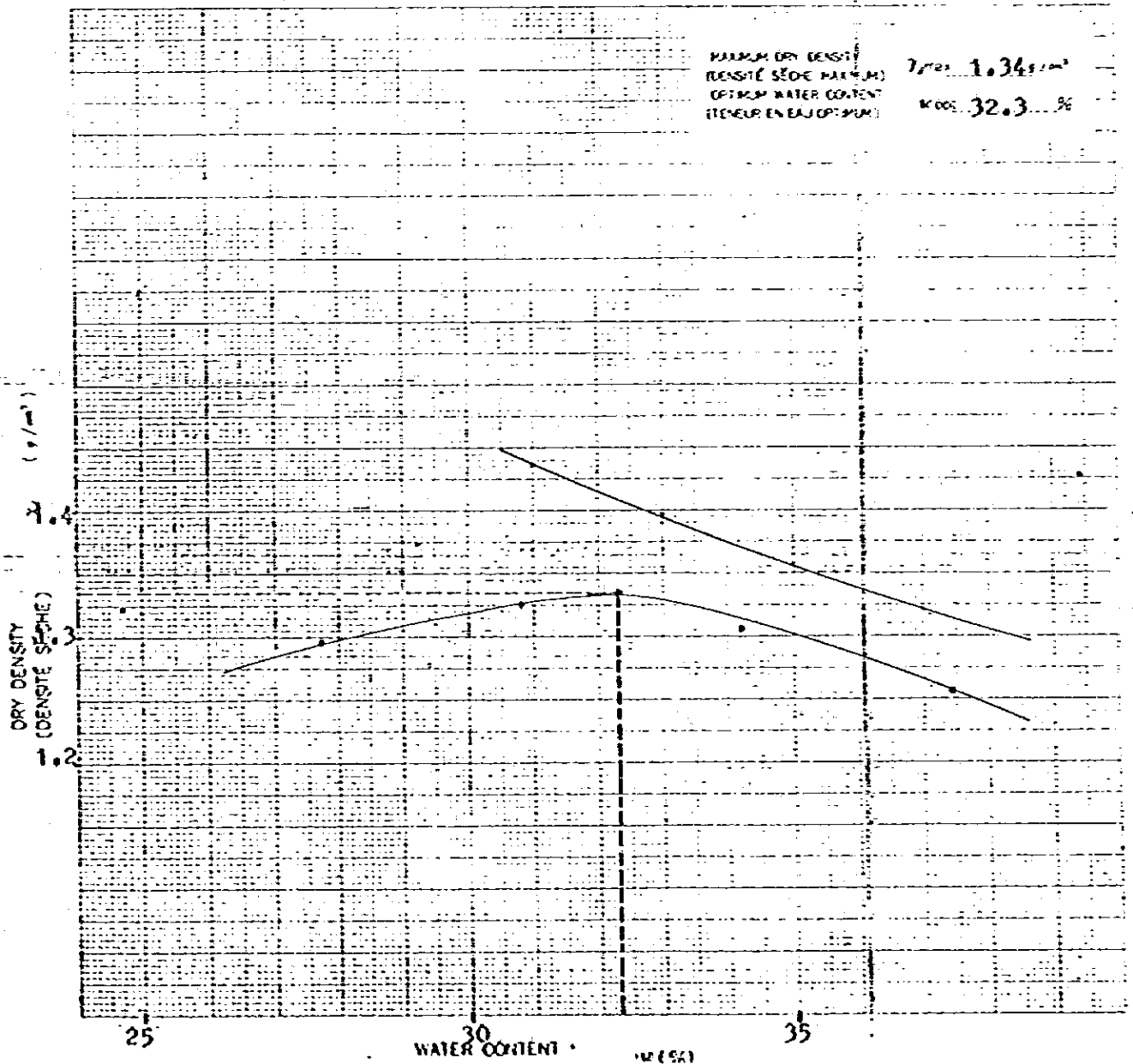
WATER CONTENT AFTER AIR DRY (TENEUR EN EAU APRÈS SÈCHE À L'AIR LIBRE) ..... %

SPECIFIC GRAVITY (POIDS SPÉCIFIQUE) ..... 2.59

MAX. GRAIN SIZE ALLOWED (GRANULOMÈTRE MAXIMUM "A") ..... 4.76 mm

% OF MATERIAL OVER THE MAX. GRAIN SIZE ALLOWED (N° DE MATÉRIAU DE GRANULOMÈTRE SUPÉRIEURE À CELLE ADMISE) ..... %

TEST NO (N° DE L'ESSAI)	1	2	3	4	5	6	7	8
DRY DENSITY (DENSITÉ SÈCHE) $\gamma_d$ (g/cm <sup>3</sup> )	1.296	1.326	1.335	1.306	1.257			
MEAN WATER CONTENT (TENEUR MOYENNE EN EAU) $w$ (%)	27.69	30.81	32.32	34.22	37.48			



# SHRINKAGE CONSTANT TEST

No. \_\_\_\_\_

LOCATION Canal Route , Date Sept. 81

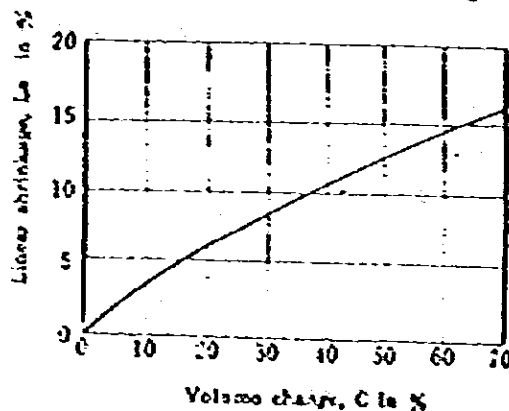
SAMPLE No. TP-2 (0.3 - 1.4M) , Test by Bina Marga Laboratory

No. _____	No. _____	No. _____
WW <u>37.72</u> DW <u>26.44</u>	WW <u>37.53</u> DW <u>26.32</u>	WW _____ DW _____
DW <u>26.44</u> TW <u>9.83</u>	DW <u>26.32</u> TW <u>9.17</u>	DW _____ TW _____
W. <u>11.28</u> W. <u>16.61</u>	W. <u>11.21</u> W. <u>17.15</u>	W. _____ W. _____
$w = 67.9 \%$	$w = 65.4 \%$	$w = \quad \quad \%$

SPECIMEN No.		1	2	3
SHRINKAGE LIMIT	Wet soil volume (Volume of mercury) $V$ cm <sup>3</sup>	18	18.2	
	Dry soil volume (Volume of mercury) $V_0$ cm <sup>3</sup>	10	10.02	
	Shrinkage volume $(V - V_0)$ cm <sup>3</sup>	8	8.18	
	$\frac{V - V_0}{V_0} \times 100\%$	48.2	47.7	
	Shrinkage limit $S = w - \left(\frac{V - V_0}{W_s} \times 100\right)\%$	19.7	17.7	
	$\frac{1}{R} - \frac{1}{G}$	0.16	0.17	
SHRINKAGE RATIO	Dry soil volume $V_0$ cm <sup>3</sup>	10.0	10.02	
	Dry Soil weight $W_s$ g	16.61	17.15	
	Shrinkage ratio $R = \frac{W_s}{V_0} \times \frac{1}{\gamma_s}$	1.66	1.71	
VOLUME CHANGE	Initial water content $w$ %	67.9	65.4	
	Shrinkage limit $s$ %	19.7	17.7	
	Volume change $C = (w_1 - s) R$	80	81.5	
	Linear Shrinkage $L_s = 10 \left(1 - \sqrt[3]{\frac{100}{C + 100}}\right)\%$	17.8	18.0	
SPECIFIC GRAVITY OF SOIL	$\frac{1}{R} - \frac{w}{100}$	0.44	0.41	
	Specific gravity of soil $G = \frac{1}{1/R - w/100}$	2.27	2.44	
	Specific gravity of soil obtained by pycnometer method	2.66	2.66	

(Remarks)  $\gamma_s$  : Unit weight of water

Curve for determining Linear shrinkage



Note : Test is made on soil sample passing 0.4mm sieve

# SHRINKAGE CONSTANT TEST

No. \_\_\_\_\_

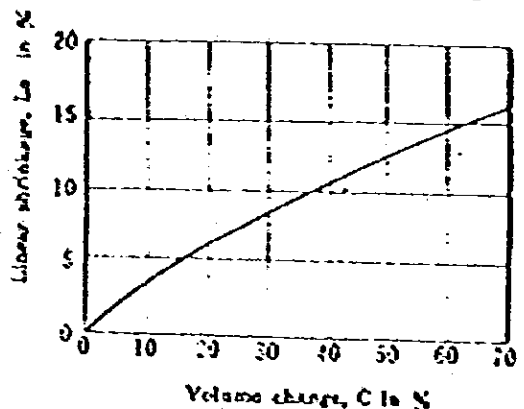
LOCATION Canal Route , Date Sept. 81  
 SAMPLE No. TP-4 (1.0 - 1.8M) , Test by Bina Marga Laboratory

No. _____	No. _____	No. _____
FW <u>36.01</u> DW <u>23.80</u>	WW _____ DW _____	WW _____ DW _____
DW <u>23.80</u> TW <u>9.82</u>	DW _____ TW _____	DW _____ TW _____
W <sub>o</sub> <u>12.21</u> W <sub>1</sub> <u>13.98</u>	W <sub>o</sub> _____ W <sub>1</sub> _____	W <sub>o</sub> _____ W <sub>1</sub> _____
$w = 87.34\%$	$w = \quad \%$	$w = \quad \%$

SPECIMEN No.	1	2	3
<b>SHRINKAGE LIMIT</b>			
Wet soil volume (Volume of mercury) $V_1$ cm <sup>3</sup>	18.00		
Dry soil volume (Volume of mercury) $V_0$ cm <sup>3</sup>	7.20		
Shrinkage volume $(V_1 - V_0)$ cm <sup>3</sup>	10.80		
$\frac{V_1 - V_0}{V_0} \times 100\%$	77.25		
Shrinkage limit $S_{ML} = \left( \frac{V_1 - V_0}{V_0} \times 100 \right) \%$	10.09		
$\frac{1}{2} - \frac{1}{G}$	0.139		
Shrinkage limit obtained from L & G $s_{ML} = \left( \frac{1}{2} - \frac{1}{G} \right) \times 100\%$	13.90		
<b>SHRINKAGE RATIO</b>			
Dry soil volume $V_0$ cm <sup>3</sup>	7.20		
Dry Soil weight $W_0$ g	13.98		
Shrinkage ratio $R = \frac{W_0}{V_0} \times \frac{1}{\gamma_w}$	1.94		
<b>VOLUME CHANGE</b>			
Initial water content $w_1$ %	87.34		
Shrinkage limit $s_{ML}$ %	10.09		
Volume change $C = (w_1 - s_{ML}) R$	148.9		
Linear Shrinkage $L = 100 \left( 1 - \sqrt[3]{\frac{100}{C + 100}} \right) \%$	26.2		
<b>SPECIFIC GRAVITY OF SOIL</b>			
$\frac{1}{K} - \frac{w_1}{100}$	0.37		
Specific gravity of soil $G = \frac{1}{1/K - w_1/100}$	2.66		
Specific gravity of soil obtained by pycnometer method	2.56		

(Remarks)  $\gamma_w$  : Unit weight of water

Curve for determining linear shrinkage



Note : Test is made on soil sample passing 0.4mm sieve

# SHRINKAGE CONSTANT TEST

No. \_\_\_\_\_

LOCATION Canal Route \_\_\_\_\_, Date Sept, 81 \_\_\_\_\_

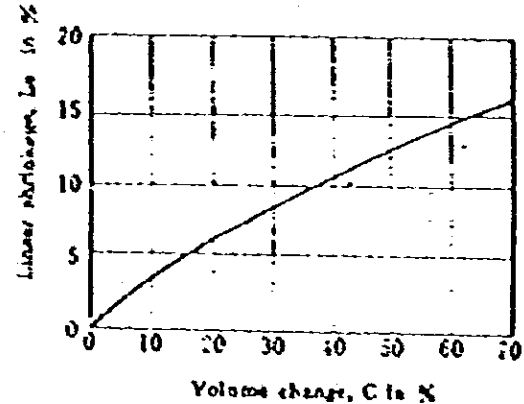
SAMPLE No. TP-7(1.6 - 2.0M) \_\_\_\_\_, Test by Bina Marga Laboratory

No. _____	No. _____	No. _____
K <sub>1</sub> W 38.65    M <sub>1</sub> W 28.20    W <sub>1</sub> W _____	D <sub>1</sub> W _____    D <sub>2</sub> W _____	W <sub>1</sub> W _____    D <sub>1</sub> W _____
M <sub>2</sub> W 28.20    T <sub>1</sub> W 9.08    D <sub>2</sub> W _____	T <sub>2</sub> W _____    T <sub>3</sub> W _____	D <sub>2</sub> W _____    T <sub>2</sub> W _____
W <sub>2</sub> 10.45    W <sub>3</sub> 19.12    W <sub>2</sub> _____	W <sub>3</sub> _____    W <sub>3</sub> _____	W <sub>2</sub> _____    W <sub>3</sub> _____
w = 54.6 %	w = _____ %	w = _____ %

SPECIMEN No.	1	2	3
<b>SHRINKAGE LIMIT</b>			
Wet soil volume (Volume of mercury) $V$ cm <sup>3</sup>	18.0		
Dry soil volume (Volume of mercury overflow) $V_0$ cm <sup>3</sup>	9.8		
Shrinkage volume $(V - V_0)$ cm <sup>3</sup>	8.2		
$\frac{V - V_0}{V_s} \times 100\%$	42.9		
Shrinkage limit $S = w \left( \frac{V - V_0}{W_s} \times 100 \right) \%$	11.7		
$\frac{1}{R} - \frac{1}{G}$	0.192		
Shrinkage limit obtained from R & G $w_s = \left( \frac{1}{R} - \frac{1}{G} \right) \times 100\%$	19.2		
<b>SHRINKAGE RATIO</b>			
Dry soil volume $V_0$ cm <sup>3</sup>	9.8		
Dry Soil weight $W_0$ g	19.12		
Shrinkage ratio $R = \frac{V_0}{V_s} - \frac{1}{w}$	1.95		
<b>VOLUME CHANGE</b>			
Initial water content $w_1$ %	54.6		
Shrinkage limit $w_s$ %	11.7		
Volume change $C = (w_1 - w_s) R$	83.6		
Linear Shrinkage $L_s = 100 \left( 1 - \sqrt[3]{\frac{100}{C + 100}} \right) \%$	18.3		
<b>SPECIFIC GRAVITY OF SOIL</b>			
$\frac{1}{R} - \frac{w_s}{100}$	0.32		
Specific gravity of soil $G_s = \frac{1}{R - \frac{w_s}{100}}$	3.09		
Specific gravity of soil obtained by pycnometer method			

(Remarks)  $w_s$  : Unit weight of water

Curve for determining linear shrinkage



Note : Test is made on soil sample passing 0.4mm sieve

SPECIFIC GRAVITY & WATER ABSORPTION OF SAND

LOCATION : Bila Irrigation Project (River Material)      DATE : September, 1981.  
 TESTED BY : Bina Karga Laboratory of P.U.

Sample no.	RM 1	RM 2	RM 4	
Test No.	1	2	3	4
(1) Wt. of Flask + Water	669.7	668.7	352.2	
(2) Wt. of Flask	169.7	168.7	102.2	
(3) Vol. of Flask	500	500	250	
=(1)-(2)				
(4) Wt. of Flask + SSD Sand	425.8	452.3	313.7	
(5) Wt. of SSD Sand	256.1	283.6	211.5	
=(4)-(2)				
(6) Wt. of Flask+Water+SSD Sand	822.3	840.2	482.4	
(7) Vol. of sand	103.5	112.1	81.3	
=(1)-(6)+(5)				
(8) Specific Gravity of SSD Sand	2.47	2.53	2.60	
=(5)/(7)				
Mean Value	2.47	2.53	2.60	
(9) Wt. of Dry Sand	250.4	277.9	208.7	
(10) Water Absorption %	2.2	2.0	1.3	
=(5)-(9)				
(9) Mean Value	2.2	2.0	1.3	

SPECIFIC GRAVITY & WATER ABSORPTION OF GRAVEL

LOCATION : BILA IRRIGATION PROJECT  
(RIVER MATERIAL)

DATE : SEPTEMBER 1981

TESTED BY : BINA MARGA LABORATORY OF P.U.

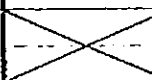
SAMPLE No. :		BRM	BRM
TEST No. :			
OVENDRY WEIGHT OF SAMPLE (A)		6114	
SATURATED SURFACE-DRY WEIGHT OF SAMPLE (B)		6202	
WEIGHT OF SAMPLE IN WATER (C)		3930	
APPARENT SPECIFIC GRAVITY = $\frac{A}{A-C}$ =		2.79	
BULK SPECIFIC GRAVITY (SATURATED SURFACE-DRY) = $\frac{B}{B-C}$ =		2.73	
BULK SPECIFIC GRAVITY (OVEN DRY) = $\frac{A}{B-C}$ =		2.69	
PERCENTAGE OF ABSORPTION (SATURATED SURFACE-DRY BASIS) = $\frac{B-A}{A} \times 100\%$ =		1.44	



LOG OF TEST PIT  
FOR BORROW AND FOUNDATION INVESTIGATIONS

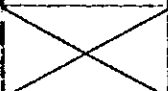
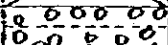
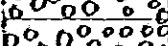
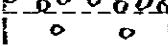
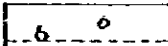
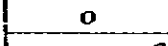
Location Bila Intake Site  
( Right Bank ) Place Paddy Field

HOLE NO. TP - 0 ( R ) EL.

DEPTH (m)	CLASSIFICATION SYMBOL		CLASSIFICATION AND DESCRIPTION OF MATERIAL
	LETTER	GRAPHIC	
0.2	CF		Lean CLAY, With some weed root ; black ; moisture .
			CLAYEY SAND, loose ; wet and moist ; terrace material ; black-dark brown ; very weak layer ; no mixture with gravel ; SAND is an infinitesimal grain .
1.0	SC		Estimation : Low bearing capacity ; foundation layer 4 or 5 m ; core material for fill-dam ; easy excavation by scoop ; terrace material . ( impossible to transport material directly )
2.0			Stopped

LOG OF TEST P11  
FOR BORROW AND FOUNDATION INVESTIGATIONS

Location Bila Intake Site Place Side of Hill  
(Left Bank)  
HOLE NO. TP - 0(L) EL. \_\_\_\_\_

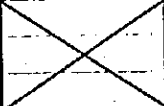
DEPTH (m.)	CLASSIFICATION SYMBOL		CLASSIFICATION AND DESCRIPTION OF MATERIAL
	LETTER	GRAPHIC	
0.25	GF		0.00-0.25m: GRAVEL-Silty CLAY; dry-moisture; with some weed roots; dark brown; approx 10-20% gravel (P+4.76) to 15-20mm mean size.
	GM-GC		
1.0	(G-M -G-C)		0.25m-0.50m: loose; approx. 60-70% gravel (P+4.76) to 200mm maximum size and to 50mm mean size; wet; light yellow brown.
			0.50m-1.20m: compact; approx. 30-50% gravel (P+4.76) to 100mm maximum size and to 15mm mean size; wet; light yellow brown; talus material.
1.4	-4.76mm C'H		-1.40m: large gravels; to 300mm maximum size; high permeability; optimum road materials; difficult excavation by scoop. Stop by large gravels.
			Estimation; 0.25m-1.40m, suitable embankment material for Canal; under 1.4m, suitable road material; Talus material, -4.76mm = C'H. (possible to transport material directly)



LOG OF TEST PIT  
FOR BORROW AND FOUNDATION INVESTIGATIONS

Location Canal route Place Boundary of paddy and hill

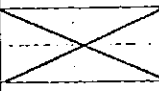

HOLE NO. TP - 2 EL.

DEPTH (m)	CLASSIFICATION SYMBOL		CLASSIFICATION AND DESCRIPTION OF MATERIAL
	LETTER	GRAPHIC	
0.3	CF		Lean CLAY, with some weed root ; black ; wet .
	CL		Silty CLAY, highly weathered siltstone ; partly sand , weathered sandstone ; moist ; light yellow brown ; no gravel .
0.9			
1.0	Sis	.....	Siltstone - Sandstone , moderately weathered ; light grey ; low cementation .
	I		- 1.10 m ground water .
	Ss	.....	Stopped by hard layer .
1.4			Estimation ; - 1.40 m high bearing capacity ; 0.9 - 1.4 m high slaking by dry shrinkage and wet expansion ; moderately embankment material after slaking with water ; difficult excavation by scoop . 0.3 - 0.9 m , Molasse soil material . ( If not dry, possible to transport directly )

LOG OF TEST PIT  
FOR BORROW AND FOUNDATION INVESTIGATIONS

Location Canal Route Place Paddy

HOLE NO. TP - 3 EL.

DEPTH (m)	CLASSIFICATION SYMBOL		CLASSIFICATION AND DESCRIPTION OF MATERIAL
	LETTER	GRAPHIC	
0.2	CF		CLAY, with some paddy's root; black wet.
			Clayey SAND, highly weathered siltstone; high clayey and silty; medium dry strength; moist; light yellow brown; no gravel.
1.0	SC		Estimation; suitable material for embankment, if sprinkle with water. Alluvial material (surface); Molasse soil material, (If not dry, possible to transport material directly)
1.6			1.6 m ground water.
1.9 - 2.0	Sis - Ss		Stopped by hard layer 1.9m - 2.0m, Siltstone-Sandstone, moderately weathered and cementation, light grey; moderate bearing capacity; difficult excavation by scoop.

LOG OF TEST PIT  
FOR BORROW AND FOUNDATION INVESTIGATIONS

Location Canal route Place Side of the hill

HOLE NO. TP - 4 EL.

DEPTH (m)	CLASSIFICATION SYMBOL		CLASSIFICATION AND DESCRIPTION OF MATERIAL
	LETTER	GRAPHIC	
0.4	CF	X	Silty CLAY, with some weed root ; black ; dry .
			CLAY, high clayey and dry strength ; high dry shrinkage ; light blue grey ; highly weathered siltstone .
1.0	CH		Estimation ; moderately suitable embankment material, but need sprinkling with water . (Molasse soil material ; impossible to transport material directly )
2.0	S-M	•••••	SAND mixture, with SILT .
2.2	(S-C)	•••••	Stopped by hard layer .
			2.0 m - 2.2 m ; mixed with gravel - maximum size 10 - 30 mm ; moderately compact with silt and silty sand ; difficult excavation by scoop ; Muddy soil material .

LOG OF TEST PIT  
FOR BORROW AND FOUNDATION INVESTIGATIONS

Location Canal Route Place ( Terrace deposit  
Kalola R. Right Bank )

HOLE NO. TP - 5 EL.

DEPTH (m)	CLASSIFICATION SYMBOL		CLASSIFICATION AND DESCRIPTION OF MATERIAL
	LETTER	GRAPHIC	
0.2	CF		CLAY, with some weed roots; black; moist.
			CLAY; high plasticity - medium plasticity; moist; black-dark brown; very weak layer; no mixture with gravel; easy excavation by scoop.
1.0	CH		Estimation; moderately suitable embankment material for core zone of fill dam; terrace material (= alluvial material) - flood plain; high bearing capacity layer is over 4 m or 5 m; impossible to transport material directly.
2.0			
3.0			Stopped

# LOG OF TEST PIT FOR BORROW AND FOUNDATION INVESTIGATIONS

Location Canal Place Boundary of Paddy and Hill.  
HOLE NO. TP - 6 EL. \_\_\_\_\_


DEPTH (m)	CLASSIFICATION SYMBOL		CLASSIFICATION AND DESCRIPTION OF MATERIAL
	LETTER	GRAPHIC	
0.4	CF	X	Lean CLAY; with some weed roots; dark brown; dry.
0.8	(G-M)	o o o o o o	0.4-0.8m: SILT MIXTURE WITH GRAVEL; clayey silt moist; space of gravels is moderately compacted by silt; light brown; approx. 30-50% gravel (P+4.76) to 15mm mean size.
1.0	SC	.....	0.8-1.0m: Clayey SAND (mixture with gravel) space of gravels compacted by silt clay; approx. 30% gravel (P+4.76) to 20-30mm maximum size; blue grey; moist.
1.5		.....	
2.0		.....	
2.4		.....	
			1.5m, ground water.
			Estimation; difficult excavation by scoop; suitable embankment material; under 2.4m highly bearing capacity; Talus material. (possible to transport material directly)
2.4			Stopped by hard layer.



LOG OF TEST PIT  
FOR BORROW AND FOUNDATION INVESTIGATIONS

Location Canal Route Place Paddy

HOLE NO. TP - 7 EL.

DEPTH (m)	CLASSIFICATION SYMBOL		CLASSIFICATION AND DESCRIPTION OF MATERIAL
	LETTER	GRAPHIC	
0.2	CE		CLAY, with some paddy's roots ; black ; wet .
			Clayey SOIL ( CLAY ) ; high or medium plasticity ; moist ; dark brown mixture with light blue and yellow brown ; without gravel .
1.0	CL		Estimation ; easy excavation by scoop ; moderately cracks at wall ; moderately suitable embankment material ; impossible to transport material directly ; Alluvial deposit .
2.0			
2.5			2.5 m , ground water
2.8			Stopped

LOG OF TEST PIT  
FOR BORROW AND FOUNDATION INVESTIGATIONS

Location Canal Route Place Boundary of Paddy and Hill


HOLE NO. TP - 8 EL.

DEPTH (m)	CLASSIFICATION SYMBOL		CLASSIFICATION AND DESCRIPTION OF MATERIAL
	LETTER	GRAPHIC	
0.3	SF	X	Silty SAND ; with some weed roots ; brown ; dry .
			CLAY ; partly with silty sand ; well compacted ; partly with clayey silt ; dry shrinkage ; light brown ; moist ; high dry strength .
1.0	CH		Estimation ; moderate bearing capacity ; difficult excavation ; suitable embankment material after sprinkling with water ; impossible to transport material directly ; Molasse soil material .
2.0			
2.1			CLAY ; high plasticity ; well compacted ; dry shrinkage ; high dry strength ; light grey ; moist .
	(CH)		Estimation ; 0.3 m - 2.1 m layer same .
2.8			Stopped by moderately hard layer .

LOG OF TEST PIT  
FOR BORROW AND FOUNDATION INVESTIGATIONS

Location Canal Place Paddy

HOLE NO. TP - 9 EL. \_\_\_\_\_

DEPTH (m)	CLASSIFICATION SYMBOL		CLASSIFICATION AND DESCRIPTION OF MATERIAL
	LETTER	GRAPHIC	
0.2	CF		CLAY; with some rice roots; dark brown; moist.
	CH		
			Estimation; hard weathered siltstone; moderately suitable embankment material; impossibility directly transportation of material; easy excavation; collapse soil material.
1.0			
1.5			Stopped by hard layer.
			1.5m, moderately cementation siltstone; dark grey; impossibility excavation by scoop; moist; highly bearing capacity.

## SWEDISH SOUNDING TEST

Location Bila Intake Site Place Paddy  
(Right Bank)

Surface Condition Dry - Moisture

-LOG OF TEST PIT-

Depth (m)	Classification		W <sub>sw</sub> (K <sub>f</sub> )	N <sub>a</sub> (times)	D (m)	L (cm)	N <sub>sw</sub> (times/m)	N	Q <sub>u</sub> (kg/cm <sup>2</sup> )	Remarks
	Letter	Graph								
0.5	CF	X	100	3.8	0.25	25	15	4	0.56	
			"	4.0	0.50	"	16	"	0.57	
			"	3.5	0.75	"	14	"	0.55	
			"	3.5	1.00	"	14	"	0.55	
			"	3.5	1.25	"	14	"	0.55	
			"	3.0	1.50	"	12	"	0.54	
1.0	SC		"	2.5	1.75	"	10	3	0.52	
			"	4.0	2.00	"	16	4	0.57	
			"	6.0	2.20	20	30	"	0.67	
1.5			"	4.0	2.50	30	13	"	0.55	
			"	3.0	2.75	25	12	"	0.54	
			"	2.5	3.00	"	10	3	0.52	
			"	4.5	3.25	"	18	4	0.58	
			"	17.0	3.50	"	68	6	0.96	Partly Sandy Soil
2.0			"	11.0	3.75	"	44	5	0.78	
			"	2.5	4.00	"	10	3	0.52	
			"	6.5	4.25	"	26	4	0.64	
2.5			"	17.0	4.38	13	131	11	1.43	gravelly soil
			Penetration is impossibility							
3.0										

Where

- W<sub>sw</sub> : Load
- N<sub>a</sub> : Number of times of half turn
- D : Penetrated depth
- L : Penetrated length
- N<sub>sw</sub> : Half turning numbers per meter ( $N_{sw} = \frac{N_a}{L} \times 100$ )
- N : N-value (gravel sand or sandy soil)  $N = 2 + 0.057 N_{sw}$   
(clay or cohesive soil)  $N = 3 + 0.05 N_{sw}$
- Q<sub>u</sub> : Unconfined compressive strength  
 $Q_u = 0.0045 W_{sw} + 0.0075 N_{sw}$

## SWEDISH SOUNDING TEST

Location Bila Intake Site Place side of the Hill  
(left bank)

Surface Condition Dry - Moisture

-LOG OF TEST PIT-

Depth (m)	Classification		W <sub>sw</sub> (K%)	N <sub>a</sub> (times)	D (m)	L (cm)	N <sub>sw</sub> (times/m)	N	Q <sub>u</sub> (kg/cm <sup>2</sup> )	Remarks	
	Letter	Graph									
0.5	GF	X	100	16	0.25	25	64	6	0.93		
	"		"	14	0.50	"	56	"	0.87		
	GM-GC	●●●●	"	5	0.75	"	20	3	0.60		
	"		"	6	1.00	"	24	4	0.63		
	"		"	8	1.25	"	32	"	0.69		
1.0	(GM-GC)	●●●●	"	5	1.50	"	20	3	0.60		
	G-C)	●●●●	"	8	1.75	"	32	4	0.69		
	"		"	78	1.95	20	390	28	3.37	Partly gravel	
	mm -476	●●●●	Penetration is impossibility.								
	CH		Another Place								
1.5			100	12	0.25	25	48	5	0.81		
			"	16	0.50	"	64	6	0.93		
			"	5	0.75	"	20	3	0.60		
	2.0			"	5	1.00	"	20	"	"	
				"	6	1.25	"	24	4	0.63	
2.5			"	8	1.50	"	32	"	0.69		
			"	8	1.75	"	32	"	"		
			"	59	2.00	"	236	18	2.22	Partly gravel	
			"	30	2.03	3	999	69	7.90		
			↓ impossibility								
3.0											

Where

W<sub>sw</sub> : Load

N<sub>a</sub> : Number of times of hell turn

D : Penetrated depth

L : Penetrated length

N<sub>sw</sub> : Half turning numbers per meter ( $N_{sw} = \frac{N_a}{L} \times 100$ )

N : N-value (gravel sand or sandy soil)  $N = 2 + 0.057 N_{sw}$

(clay or cohesive soil)  $N = 3 + 0.05 N_{sw}$

Q<sub>u</sub> : Unconfined compressive strength

$$Q_u = 0.0045 W_{sw} + 0.0075 N_{sw}$$

## SWEDISH SOUNDING TEST

Location Canal (TP-1)

Place side of the hill

Surface Condition Moisture

-LOG OF TEST PIT-

Depth (m)	Classification		W <sub>sw</sub> (k <sub>f</sub> )	N <sub>0</sub> (times)	D (m)	L (cm)	N <sub>sw</sub> (lines/m)	N	q <sub>u</sub> (t <sub>s</sub> /m <sup>2</sup> )	Remarks
	Letter	Graph								
	CF	X	100	13	0.25	25	52	5	0.84	Partly gravel and sand
			"	43	0.45	20	215	16	2.06	
0.5	CL		Penetration is impossibility							
	GF	* o o o o o o o o o o	* Another Place							
1.0		o o	100	22	0.25	25	88	8	1.11	
		o o o	"	33	0.50	"	132	11	1.44	Partly gravel
		o o	"	66	0.73	23	284	21	2.58	and sand
1.5	GM	o o o	Penetration is impossibility							
	GC	o								
	G-M	o o o								
	G-C	o o o								
2.0		o o								
	CH	-4.76 mm o o o o								
2.5		o o o o								
		o o o								
3.0		o o								
		o o								

Where

- W<sub>sw</sub> : Load
- N<sub>0</sub> : Number of times of half turn
- D : Penetrated depth
- L : Penetrated length
- N<sub>sw</sub> : Half turning numbers per meter ( $N_{sw} = \frac{N_0}{L} \times 100$ )
- N : N-Value (gravel sand or sandy soil)  $N = 2 + 0.057 N_{sw}$
- (clay or cohesive soil)  $N = 3 + 0.05 N_{sw}$
- q<sub>u</sub> : Unconfined compressive strength
- $q_u = 0.045 W_{sw} + 0.0075 N_{sw}$

## SWEDISH SOUNDING TEST

Location Canal (TP-2)

Place Boundary of Paddy end Hill

Surface Condition Moisture

-LOG OF TEST PIT-

Depth (m)	Classification		W <sub>sw</sub> (K <sub>g</sub> )	N <sub>0</sub> (times)	D (m)	L (cm)	N <sub>sw</sub> (times/m)	N	Q <sub>u</sub> (kg/cm <sup>2</sup> )	Remarks
	Letter	Graph								
0.5	CF	X	100	0	0.02	2	0	0	0.45	
			"	4	0.25	23	17	4	0.58	
			"	8	0.50	25	32	5	0.69	
			"	7	0.75	"	28	3	0.66	
			"	18	1.00	"	72	6	0.99	
			"	38	1.25	"	152	10	1.59	
			"	72	1.50	"	288	21	2.61	
1.0	S <sub>1</sub> S	.....	"	60	1.60	10	600	42	4.95	
			impossibility							
1.5	S <sub>s</sub>	.....								
2.0										
2.5										
3.0										

Where

W<sub>sw</sub> : Load

N<sub>0</sub> : Number of times of half turn

D : Penetrated depth

L : Penetrated length

N<sub>sw</sub> : Half turning numbers per meter ( $N_{sw} = \frac{N_0}{L} \times 100$ )

N : N-value (gravel sand or sandy soil)  $N = 2 + 0.057 N_{sw}$   
 (clay or cohesive soil)  $N = 3 + 0.05 N_{sw}$

Q<sub>u</sub> : Unconfined compressive strength

$$Q_u = 0.0045 W_{sw} + 0.0075 N_{sw}$$

## SWEDISH SOUNDING TEST

Location Canal (TP-3) Place Paddy

Surface Condition Moisture

—LOG OF TEST PIT—

Depth (m)	Classification		W <sub>sw</sub> (kN)	N <sub>a</sub> (times)	D (m)	L (cm)	N <sub>sw</sub> (lines/m)	N	q <sub>u</sub> (kg/cm <sup>2</sup> )	Remarks
	Letter	Graph								
0.5	CF		100	0	0.05	5	0	0	0.45	
			"	5	0.25	20	25	4	0.64	
			"	9	0.50	25	36	5	0.72	
			"	5	0.75	"	20	4	0.60	
			"	7	1.00	"	28	"	0.66	
			"	15	1.25	"	60	6	0.90	
			"	12	1.50	"	48	5	0.81	
1.0	SC		"	28	1.75	"	112	8	1.29	
			"	32	2.00	"	128	10	1.41	
			"	19	2.25	"	76	7	1.02	
			"	50	2.50	"	200	15	1.95	
1.5			"	38	2.75	"	152	12	1.59	
			"	52	3.00	"	208	16	2.01	
2.0		.....	impossibility							
			impossibility							
2.5			impossibility							
			impossibility							
3.0			impossibility							
			impossibility							

Where

W<sub>sw</sub> : Load

N<sub>a</sub> : Number of times of half turn

D : Penetrated depth

L : Penetrated length

N<sub>sw</sub> : Half turning numbers per meter ( $N_{sw} = \frac{N_a}{L} \times 100$ )

N : N-Value (gravel sand or sandy soil)  $N = 2 + 0.067 N_{sw}$   
 (clay or cohesive soil)  $N = 3 + 0.05 N_{sw}$

q<sub>u</sub> : Unconfined compressive strength

$$q_u = 0.0045 W_{sw} + 0.0075 N_{sw}$$



## SWEDISH SOUNDING TEST

Location canal (TP-4)

Place side of Hill

Surface Condition Dry

-LOG OF TEST PIT-

Depth (m)	Classification		Wsw (kg)	No (times)	D (m)	L (cm)	Nsw (times/m)	N	Qu (kg/cm <sup>2</sup> )	Remarks
	Letter	Graph								
0.5	CF	X	100	8	0.25	25	32	5	0.69	
			"	3						
			75	0	1.43	118	0	0	0.34	
			100	0	1.59	16	0	"	0.45	
			"	2.5	1.75	"	16	4	0.57	
1.0	CH		"	5	2.00	25	20	"	0.60	
			"	6	2.25	"	24	"	0.63	
			"	11	2.50	"	44	5	0.78	
			"	14.5	2.75	"	58	6	0.88	
			"	16	3.00	"	64	"	0.93	
1.5			"	24	3.25	"	96	8	1.17	
			"	24	3.50	"	"	"	1.17	
			"	31	3.75	"	124	9	1.38	
			"	21	4.00	"	84	7	1.08	
			"	50	4.14	14	355	21	3.11	
2.0	SM (SC)		"	30	4.19	5	600	33	4.95	
			impossibility							
2.5										
3.0										

Where

Wsw : Load

No : Number of times of half turn

D : Penetrated depth

L : Penetrated length

Nsw : Half turning numbers per meter ( $N_{sw} = \frac{No}{L} \times 100$ )

N : N-Value (gravel sand or sandy soil)  $N = 2 + 0.057 N_{sw}$   
 (clay or cohesive soil)  $N = 3 + 0.05 N_{sw}$

qu : Unconfined compressive strength

$$q_u = 0.0045 W_{sw} + 0.0075 N_{sw}$$

## SWEDISH SOUNDING TEST

Location Canal (TP-5) Kalola Dam site  
Place Down Stream Right Bank

### Surface Condition Moisture

-LOG OF TEST PIT-

Depth (m)	Classification		W <sub>sw</sub> (%)	N <sub>a</sub> (times)	D (m)	L (cm)	N <sub>sw</sub> (times/m)	N	Q <sub>u</sub> (kg/cm <sup>2</sup> )	Remarks	
	Letter	Graph									
0.5	CF	X	100	7	0.25	25	28	4	0.66		
			"	8.5	0.50	"	34	5	0.70		
			"	7	0.75	"	28	4	0.66		
			"	"	1.00	"	"	"	"	0.66	
			"	7.5	1.25	"	30	"	0.67		
			"	9	1.50	"	36	5	0.72		
1.0			"	7	1.75	"	28	4	0.66		
			"	5	2.00	"	20	"	0.60		
			"	6	2.25	"	24	"	0.63		
1.5	CH		"	6	2.50	"	"	"	"		
			"	7	2.75	"	28	"	0.66		
			"	6	3.00	"	24	"	0.63		
			"	6.5	3.25	"	26	"	0.64		
			"	5	3.50	"	20	"	0.60		
2.0			"	4.5	3.75	"	18	"	0.58		
			"	11	4.00	"	44	5	0.78		
			"	70	4.20	20	350	25	3.07		
2.5			↓ impossibility								
3.0											

Where

- W<sub>sw</sub> : Load
- N<sub>a</sub> : Number of times of half turn
- D : Penetrated depth
- L : Penetrated length
- N<sub>sw</sub> : Half turning numbers per meter ( $N_{sw} = \frac{N_a}{L} \times 100$ )
- N : N-Value (gravel sand or sandy soil)  $N = 2 + 0.057 N_{sw}$   
 (clay or cohesive soil)  $N = 3 + 0.05 N_{sw}$
- Q<sub>u</sub> : Unconfined compressive strength  
 $Q_u = 0.0045 W_{sw} + 0.0075 N_{sw}$

## SWEDISH SOUNDING TEST

Location Canal (TP-6)

Place boundary of Paddy and Hill

Surface Condition Dry

-LOG OF TEST PIT-

Depth (m)	Classification		Wsw (kg)	Na (times)	D (m)	L (cm)	Nsw (times/m)	N	Qu (kg/cm <sup>2</sup> )	Remarks
	Letter	Graph								
0.5	CF		100	41	0.25	25	164	11	1.68	
			"	19	0.50	"	76	7	1.02	
			"	18	0.75	"	48	5	0.81	
			"	14	1.00	"	56	6	0.87	
			"	23	1.25	"	92	8	1.14	
			"	33	1.50	"	132	10	1.44	
1.0	(GM)		"	32	1.75	"	128	9	1.41	
			"	13.5	2.00	"	54	6	0.85	
			"	50	2.20	20	250	15	2.32	
1.5	SC		↓ impossibility							
2.0										
2.5										
3.0										

Where

Wsw : Load

Na : Number of times of half turn

D : Penetrated depth

L : Penetrated length

Nsx : Half turning numbers per meter ( $Nsx = \frac{Na}{L} \times 100$ )

N : N-value (gravel sand or sandy soil)  $N = 2 + 0.057 Nsx$

(clay or cohesive soil)  $N = 3 + 0.05 Nsx$

Qu : Unconfined compressive strength

$$Qu = 0.0015 Wsw + 0.0075 Nsw$$

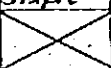



## SWEDISH SOUNDING TEST

Location Canal (TP-7)      Place Paddy

Surface Condition Dry - Moisture

-LOG OF TEST PIT-

Depth (m)	Classification		W <sub>sw</sub> (kg)	N <sub>a</sub> (times)	D (m)	L (cm)	N <sub>sw</sub> (times/m)	N	Q <sub>u</sub> (kg/cm <sup>2</sup> )	Remarks
	Letter	Graph								
0.5	CF		75	0	0.36	36	0	0	0.34	
			100	1.5	0.50	14	11	4	0.53	
			"	4	0.75	25	16	"	0.57	
			"	3.5	1.00	"	14	"	0.55	
			"	0	1.13	13	0	0	0.45	
1.0			"	2	1.25	12	16	4	0.57	
			"	3.5	1.50	25	14	"	0.55	
			"	"	1.75	"	"	"	"	
			"	"	2.00	"	"	"	"	
			"	"	2.25	"	"	"	"	
1.5	CL		"	4	2.50	"	16	"	0.57	
			"	"	2.75	"	"	"	"	
			"	"	3.00	"	"	"	"	
			"	"	3.25	"	"	"	"	
			"	5	3.50	"	20	"	0.60	
2.0			"	6	3.75	"	24	"	0.63	
			"	7	4.00	"	28	"	0.66	
			"	8	4.25	"	32	5	0.69	
			"	9.5	4.50	"	38	5	0.73	
			"	6.5	4.75	"	26	4	0.64	
2.5			"	9	5.00	"	36	5	0.72	
			"	8	5.25	"	32	"	0.69	
			"	12	5.50	"	48	"	0.81	
3.0										

Where

- W<sub>sw</sub> : Load
- N<sub>a</sub> : Number of times of half turn
- D : Penetrated depth
- L : Penetrated length
- N<sub>sw</sub> : Half turning numbers per meter ( $N_{sw} = \frac{N_a}{L} \times 100$ )
- N : N-value (gravel sand or sandy soil)  $N = 2 + 0.057 N_{sw}$   
 (clay or cohesive soil)  $N = 3 + 0.05 N_{sw}$
- Q<sub>u</sub> : Unconfined compressive strength  
 $Q_u = 0.0045 W_{sw} + 0.0075 N_{sw}$















**TOPOGRAPHY**

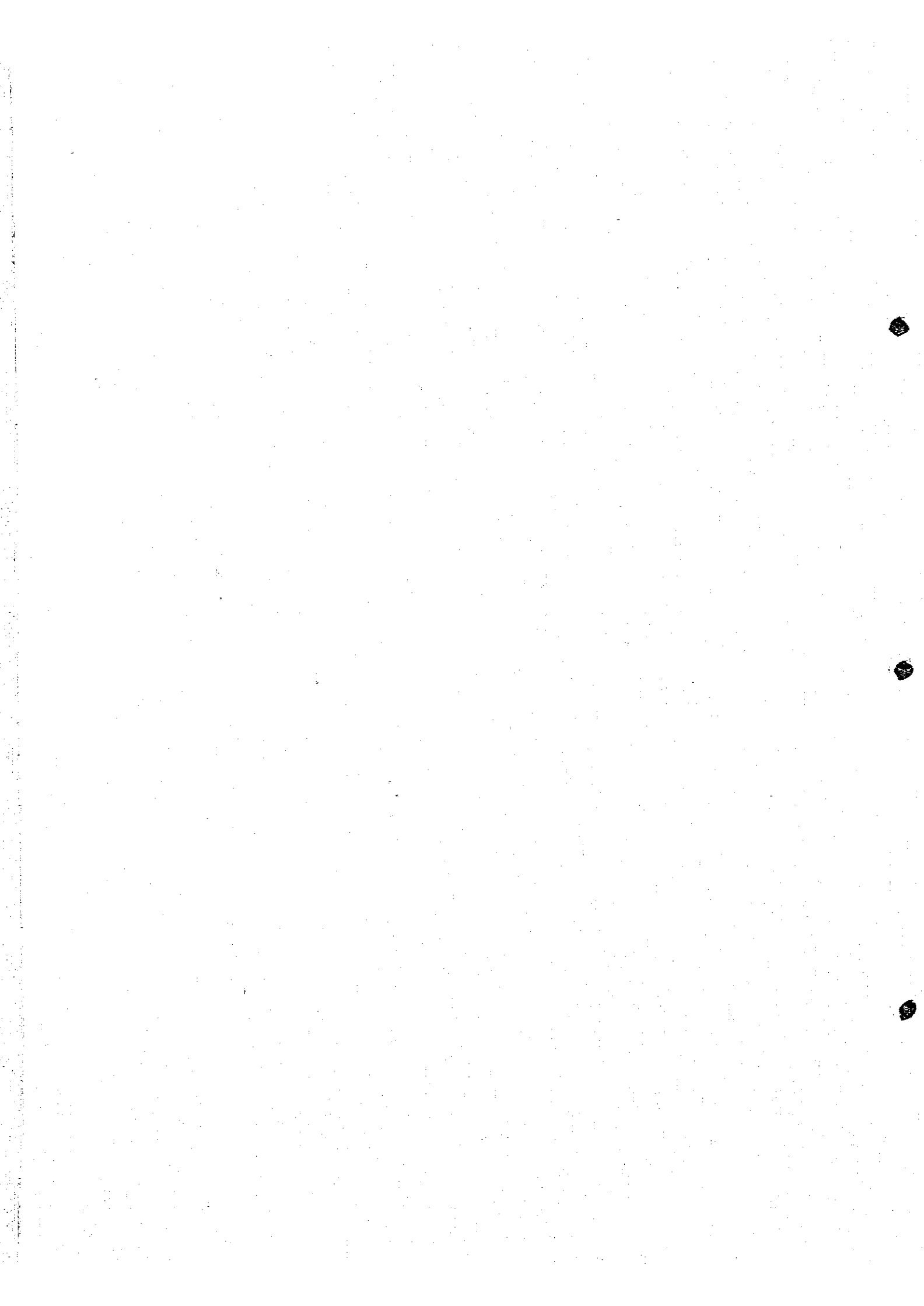


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(1) SDS (Installed by the Government of Indonesia)

No. of Bench Mark	Elevation (m)	No. of Bench Mark	Elevation (m)
A.T.G.S	0.0000	S.D.S 31	13.4356
S.D.S 1	10.5670	S.D.S 32	27.7766
S.D.S 2	3.2450	S.D.S 33	44.1856
S.D.S 3	13.0920	S.D.S 34	55.4246
S.D.S 4	45.2487	S.D.S 35	18.2575
S.D.S 5	47.1777	S.D.S 36	23.2094
S.D.S 6	90.2898	S.D.S 37	13.2814
S.D.S 7	168.3444	S.D.S 38	12.5951
S.D.S 8	371.0997	S.D.S 39	23.4880
S.D.S 9	448.5060	S.D.S 40	15.2549
S.D.S 10	355.3865	S.D.S 41	13.9869
S.D.S 11	203.0478	S.D.S 42	17.8478
S.D.S 12	113.4622	S.D.S 44	22.9218
S.D.S 13	83.5466	S.D.S 45	27.4898
S.D.S 14	100.2414	S.D.S 46	21.5427
S.D.S 15	94.4508	S.D.S 47	11.1317
S.D.S 16	94.0611	S.D.S 48	9.9165
S.D.S 17	117.8054	S.D.S 49	15.9011
S.D.S 18	100.3077	S.D.S 50	11.3865
S.D.S 19	110.1779	S.D.S 51	13.5917
S.D.S 20	169.5722	S.D.S 52	25.4389
S.D.S 21	106.9714	S.D.S 53	28.8862
S.D.S 22	49.9517	S.D.S 54	32.1824
S.D.S 24	32.2230	S.D.S 55	112.4037
S.D.S 25	100.4778	S.D.S 56	111.9408
S.D.S 26	78.3220	S.D.S 57	109.3027
S.D.S 27	123.4609	S.D.S 58	118.7548
S.D.S 28	43.3828	S.D.S 59	122.3049
S.D.S 29	30.5218	S.D.S 60	147.7449
S.D.S 30	24.1827	S.D.S 61	134.1020



No. of Bench Mark	Elevation (m)
S.D.S 62	151.9171
S.D.S 63	115.4602
S.D.S 64	97.0473
S.D.S 65	36.8354
S.D.S 66	82.6855
S.D.S 67	3.7656
S.D.S 68	2.7296
S.D.S 69	5.7167
S.D.S 70	20.0288
S.D.S 71	1.8899
S.D.S 72	4.8780
S.D.S 73	3.0401
S.D.S 74	7.5120
S.D.S 75	10.6038
S.D.S 76	23.4349
S.D.S 77	35.9890
S.D.S 78	31.5781
S.D.S 79	30.9124
S.D.S 80	26.0605
S.D.S 81	27.7715
S.D.S 82	124.1612
S.D.S 83	121.5972
S.D.S 84	201.2562
S.D.S 85	263.9072
S.D.S 86	295.4062
S.D.S 87	437.6382
S.D.S 88	224.3242
S.D.S 89	360.4512
S.D.S 90	341.0062
S.D.S 91	356.7692
S.D.S 92	77.1411
S.D.S 93	59.0939

No. of Bench Mark	Elevation (m)
S.D.S 94	17.6377
S.D.S 95	6.6689
S.D.S 96	9.9334
S.D.S 97	10.5887
S.D.S 98	4.7417
S.D.S 99	3.3087
S.D.S 100	2.8135
S.D.S 101	2.9074
S.D.S 102	10.2704
S.D.S 103	27.9966
S.D.S 104	31.6545
S.D.S 105	22.5044
S.D.S 106	20.8215
S.D.S 107	23.5084
S.D.S 108	35.3132
S.D.S 109	42.4243
S.D.S 110	72.6315
S.D.S 111	114.0239
S.D.S 112	164.3582
S.D.S 113	148.4972
S.D.S 114	131.0339
S.D.S 115	53.4962
S.D.S 116	32.8220
S.D.S 117	16.2215
S.D.S 118	1.5992
S.D.S 119	1.5152
S.D.S 120	1.3122
S.D.S 121	12.7290
S.D.S 122	21.4834
S.D.S 123	14.6122
S.D.S 124	16.8427
S.D.S 125	24.7632

No. of Bench Mark	Elevation (m)
S.D.S 126	21.5587
S.D.S 127	31.3951
S.D.S 128	32.9879
S.D.S 129	39.8012
S.D.S 130	101.7336
S.D.S 131	51.7043
S.D.S 132	19.8698
S.D.S 133	15.8798
S.D.S 134	10.9258
S.D.S 135	37.5498
S.D.S 136	45.0198
S.D.S 137	12.7878
S.D.S 138	22.8348
S.D.S 139	34.7468
S.D.S 140	11.8628
S.D.S 141	4.2788
S.D.S 142	28.6668
S.D.S 143	18.5799
S.D.S 144	8.4029

No. of Bench Mark	Elevation (m)
S.D.S 145	9.7469
S.D.S 146	12.6499
S.D.S 147	139.5329
S.D.S 148	146.0929
S.D.S 149	162.4969
S.D.S 150	264.5219
S.D.S 151	466.1229
S.D.S 201	20.7286
S.D.S 202	28.3439
S.D.S 203	59.4959
S.D.S 204	77.1339
S.D.S 205	73.3399
S.D.S 206	34.1509
S.D.S 207	34.5459
S.D.S 208	29.1879
S.D.S 210	9.3829
S.D.S 211	22.2901
S.D.S 212	26.8251
S.D.S 213	68.2551

(2) S.B.M (Installed JICA MAPPING TEAM in 1978)

No. of Bench Mark	Elevation (m)
I.S.B.M 1	23.8544
I.S.B.M 2	24.7067
I.S.B.M 3	35.8172
I.S.B.M 4	25.9589
I.S.B.M 5	21.8899
I.S.B.M 6	35.7001
I.S.B.M 7	24.0557

No. of Bench Mark	Elevation (m)
I.S.B.M 8	4.6162
I.S.B.M 9	3.5795
I.S.B.M 10	2.7679
I.S.B.M 11	4.7842
I.S.B.M 12	4.6809
I.S.B.M 13	82.1944
I.S.B.M 14	22.6260

No. of Bench Mark	Elevation (m)
I.S.B.M 15	20.2782
I.S.B.M 16	26.2635
I.S.B.M 17	26.4684
I.S.B.M 18	19.8115
I.S.B.M 19	105.8302
I.S.B.M 20	116.2114
I.S.B.M 21	78.2943
I.S.B.M 22	23.5972
I.S.B.M 23	21.5702
I.S.B.M 24	34.0039
I.S.B.M 25	40.2050
I.S.B.M 26	16.4160
I.S.B.M 27	13.0639
I.S.B.M 28	27.0359
I.S.B.M 29	22.1829
I.S.B.M 30	18.9689
I.S.B.M 31	13.1029
I.S.B.M 32	26.3931
I.S.B.M 33	28.4089
I.S.B.M 34	32.8999
I.S.B.M 35	59.4999
I.S.B.M 36	64.1119
II.S.B.M 1	34.1772
II.S.B.M 2	42.6917
II.S.B.M 3	77.8992
II.S.B.M 4	98.6375
II.S.B.M 5	118.6065
II.S.B.M 6	118.8414
II.S.B.M 7	109.2191
II.S.B.M 8	16.4218
II.S.B.M 9	108.9374
II.S.B.M 10	158.2722

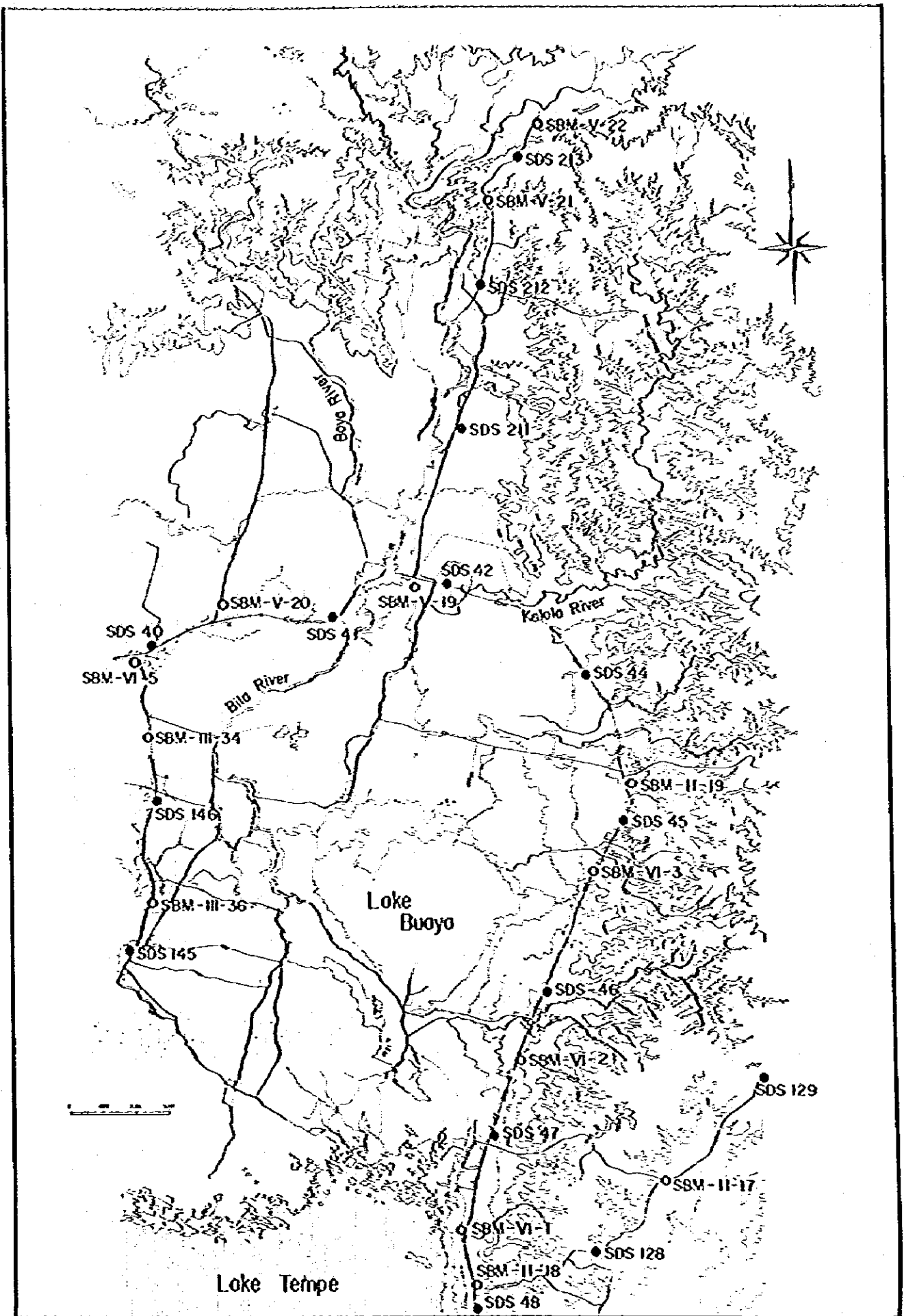
No. of Bench Mark	Elevation (m)
II.S.B.M 12	10.9630
II.S.B.M 13	12.4940
II.S.B.M 14	14.6711
II.S.B.M 15	42.6138
II.S.B.M 16	83.4885
II.S.B.M 17	38.3276
II.S.B.M 18	11.1997
II.S.B.M 19	40.2381
II.S.B.M 20	34.8628
II.S.B.M 21	18.0548
II.S.B.M 22	16.3298
III.S.B.M 1	266.1945
III.S.B.M 2	323.8043
III.S.B.M 3	416.8488
III.S.B.M 4	420.9797
III.S.B.M 5	455.2086
III.S.B.M 6	459.7916
III.S.B.M 7	389.1531
III.S.B.M 8	248.4694
III.S.B.M 9	226.7951
III.S.B.M 10	176.6381
III.S.B.M 11	82.1454
III.S.B.M 12	108.1257
III.S.B.M 13	75.0642
III.S.B.M 14	103.9502
III.S.B.M 15	73.3030
III.S.B.M 16	115.5502
III.S.B.M 17	116.5184
III.S.B.M 18	5.0026
III.S.B.M 19	141.4693
III.S.B.M 20	148.2170
III.S.B.M 21	74.8282

No. of Bench Mark	Elevation (m)
III.S.B.M 22	30.9794
III.S.B.M 23	70.8343
III.S.B.M 24	64.3002
III.S.B.M 25	26.3283
III.S.B.M 26	70.5663
III.S.B.M 27	101.0515
III.S.B.M 28	14.5061
III.S.B.M 29	20.8673
III.S.B.M 30	28.0762
III.S.B.M 31	13.5033
III.S.B.M 32	13.4982
III.S.B.M 33	12.8171
III.S.B.M 34	15.8809
III.S.B.M 35	18.4429
III.S.B.M 36	10.8229
III.S.B.M 37	35.1279
III.S.B.M 38	30.6349
III.S.B.M 39	32.9249
III.S.B.M 40	24.5459
III.S.B.M 41	29.0059
IV.S.B.M 0	163.2947
IV.S.B.M 1	203.5545
IV.S.B.M 2	217.4444
IV.S.B.M 3	244.9027
IV.S.B.M 4	221.5397
IV.S.B.M 5	172.8864
IV.S.B.M 6	167.6390
IV.S.B.M 7	163.5218
IV.S.B.M 8	75.0537
IV.S.B.M 9	64.8473
IV.S.B.M 10	35.3399
IV.S.B.M 11	13.2226

No. of Bench Mark	Elevation (m)
IV.S.B.M 12	5.2912
IV.S.B.M 13	4.8844
IV.S.B.M 14	17.9684
IV.S.B.M 15	3.6169
IV.S.B.M 16	5.3984
IV.S.B.M 17	12.1443
IV.S.B.M 18	22.9578
IV.S.B.M 19	20.1121
IV.S.B.M 20	82.8672
IV.S.B.M 21	97.0939
IV.S.B.M 22	109.2173
IV.S.B.M 23	31.0431
IV.S.B.M 24	41.7844
IV.S.B.M 25	21.6380
IV.S.B.M 26	30.7593
IV.S.B.M 27	37.6125
V.S.B.M 1	2.4680
V.S.B.M 2	19.7980
V.S.B.M 3	23.0432
V.S.B.M 4	28.3558
V.S.B.M 5	32.5817
V.S.B.M 6	31.2107
V.S.B.M 7	32.3351
V.S.B.M 8	11.0852
V.S.B.M 9	140.5799
V.S.B.M 10	138.7585
V.S.B.M 11	11.8882
V.S.B.M 12	6.0952
V.S.B.M 13	11.8516
V.S.B.M 14	10.1229
V.S.B.M 15	7.2057
V.S.B.M 16	5.1928

No. of Bench Mark	Elevation (m)
V.S.B.M 17	20.9979
V.S.B.M 18	4.7968
V.S.B.M 19	19.1271
V.S.B.M 20	17.8125
V.S.B.M 21	71.1531
V.S.B.M 22	55.6811
V.S.B.M 23	60.8234
V.S.B.M 24	58.6313
V.S.B.M 25	36.4221
VI.S.B.M 1	10.2461
VI.S.B.M 2	21.8572

No. of Bench Mark	Elevation (m)
VI.S.B.M 3	22.2964
VI.S.B.M 4	32.3654
VI.S.B.M 5	15.2511
VI.S.B.M 6	2.2422
VI.S.B.M 7	1.4312
VI.S.B.M 8	1.7552
VI.S.B.M 9	11.8653
VI.S.B.M 10	15.0742
VII.S.B.M 1	416.5862
VII.S.B.M 2	365.3082
VII.S.B.M 3	286.0812

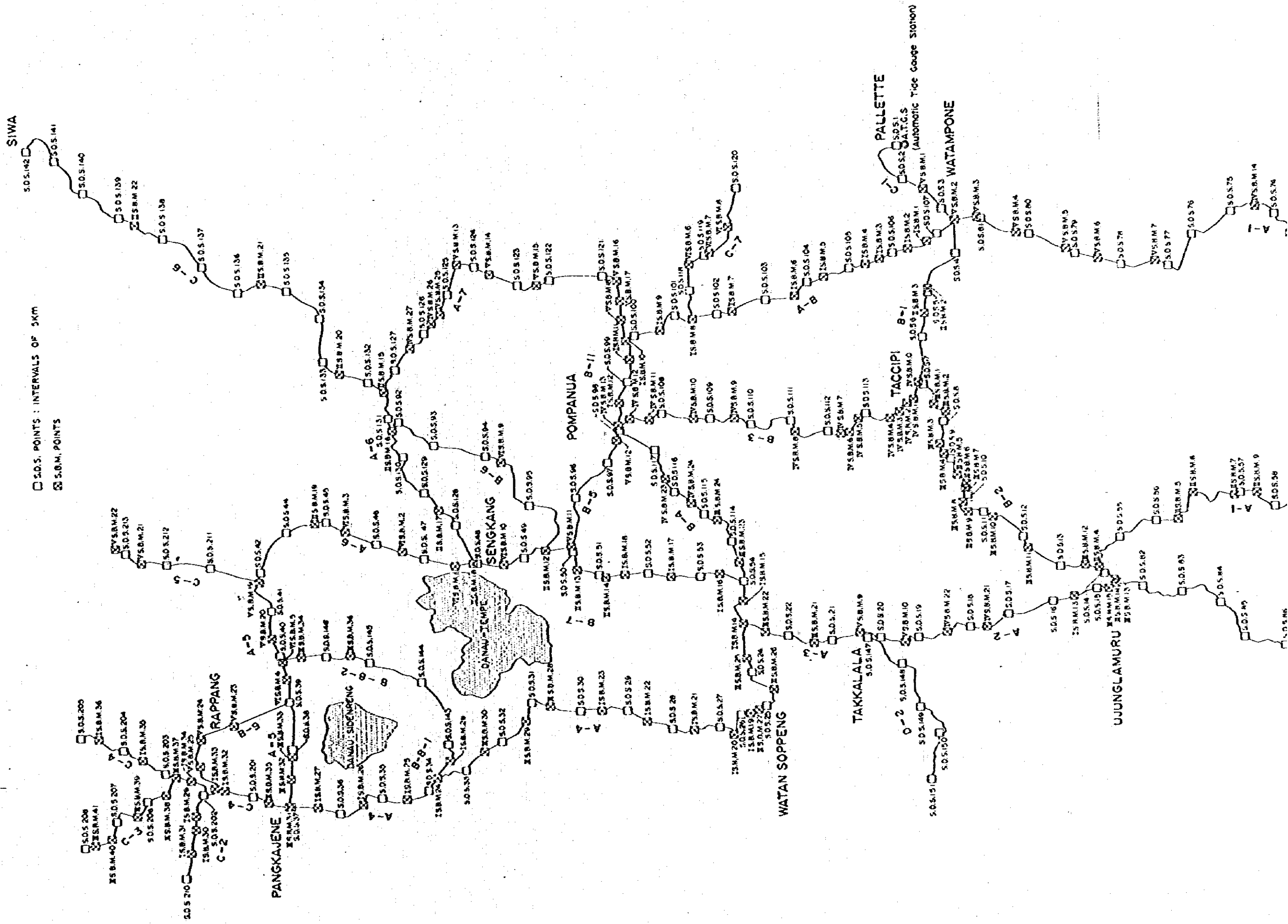
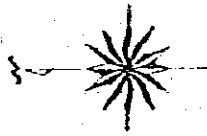


Bench Marks in the Study Area

MAPPING WORK(PART2) FOR MASTER PLAN OF THE CENTRAL SOUTH SULAWESI WATER RESOURCES DEVELOPMENT PROJECT IN INDONESIA

GUIDANCE MAP OF LEVELING

SCALE 1 : 250,000



□ S.O.S. POINTS : INTERVALS OF 5KM  
⊠ S.O.M. POINTS

