



ユアム川

水力発電開発計画

調査報告書

(II)

(Appendix 1, 2, 3, 4, 5)

1984年3月

国際協力事業団

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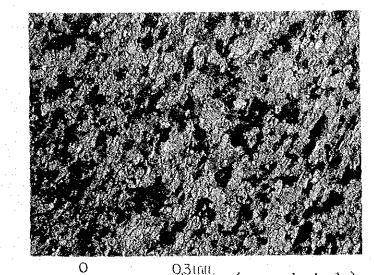
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	国際協力事業団	
	受入 '84. 6. 13 122 月日 '84. 6. 13 122	
	登録No. 10375 MPN	
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A1 GEOLOGY

Micrograph and Petrographic Description of Rock (Plate 1 of 5)



600 m upstream of A dam axis, right bank of Yuam River.

Rock name:

Locality: 5

Limestone (massive)

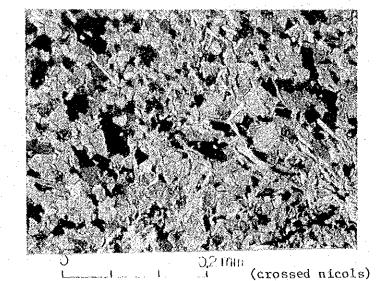
Petrographic description: Chief consisting minerals are calcite >> muscovite, quartz and chlorite. Dolomite and potassium feldspar are trace in amount.

Locality: 9

200 m upstream of A dam axis, right bank of Yuam River. (EL. 150 m)

Rock name:

Limestone (laminated)



Petrographic description:

Chief consisting minerals are calcite > white mica, quartz. Banding texture consisting of calcite-rich and mica-rich layers is observed.

Micrograph and Petrographic Description of Rock (Plate 2 of 5)

Locality: 13

l km downstream of A dam axis, left bank of Yuam River.

Rock name:

Sandy limestone

Petrographic description:

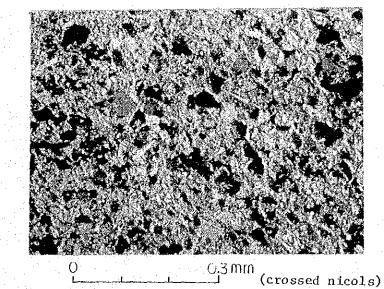
muscovite.

Locality: 16

Tributary of Huai Uya Kra (EL. 460 m)

Rock name:

Siliceous limestone (or calcareous sandstone)



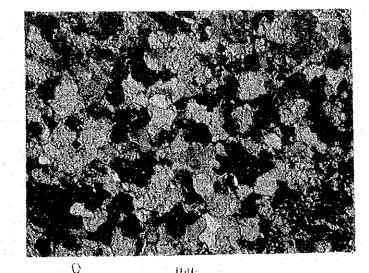
21015

(crossed nicols)

Petrographic description:

Chief consisting minerals are calcite, quartz and white mica. Clay minerals are trace in amount, less than 0.1%.

Micrograph and Petrographic Description of Rock (Plate 3 of 5)



Petrographic description: Chief consisting minerals are dolomite, calcite, quartz. Accessory minerals are muscouvite and pyrite.

Locality: 20

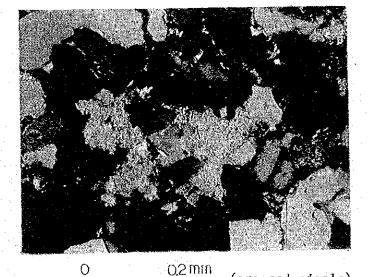
Locality: 18 Huai Uya Kra

Rock name:

Calcareous sandstone

Huai Mae Lamu

Rock name: Sandstone



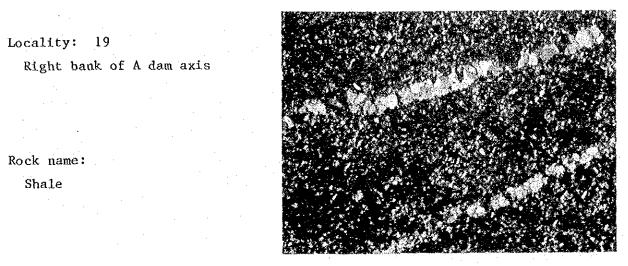
(crossed nicols)

Petrographic description:

Chief consisting minerals are quartz, dolomite and plagioclase. A trace amount of montmorillonite is found.

Ι.

Micrograph and Petrographic Description of Rock (Plate 4 of 5)

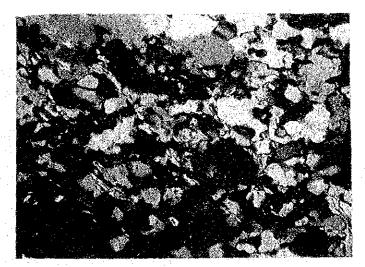


Petrographic description: Chief consisting minerals are quartz, white mica, graphite and plagioclase. Quartz veins are common.

Locality:

Huai la cho Kra (about 5 km upstream of Damsite A)

Rock name: Quartzose sandstone



Petrographic description: Chief consisting minerals are quartz, potassium feldspar and muscovite. A trace amount of tourmaline, zircon and apatite is found.

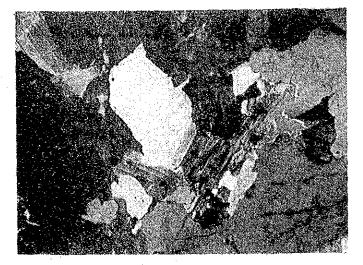
Micrograph and Petrographic Description of Rock

(Plate 5 of 5)

Locality:

Rock name: Granite

Damsite C (about 12 km upstream of Damsite A)



CEMIE

(crossed nicols)

Petrographic description:

Chief consisting minerals are quartz, potassium feldspar, plagioclase, biotite and muscovite. Mica is partly replaced by chlorite and montmorillonite.

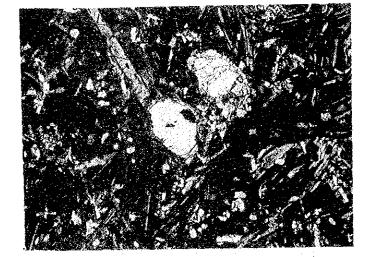
1.

Locality:

Ngao river (about 3 km upstream of junction of Yuan river and Ngao river)

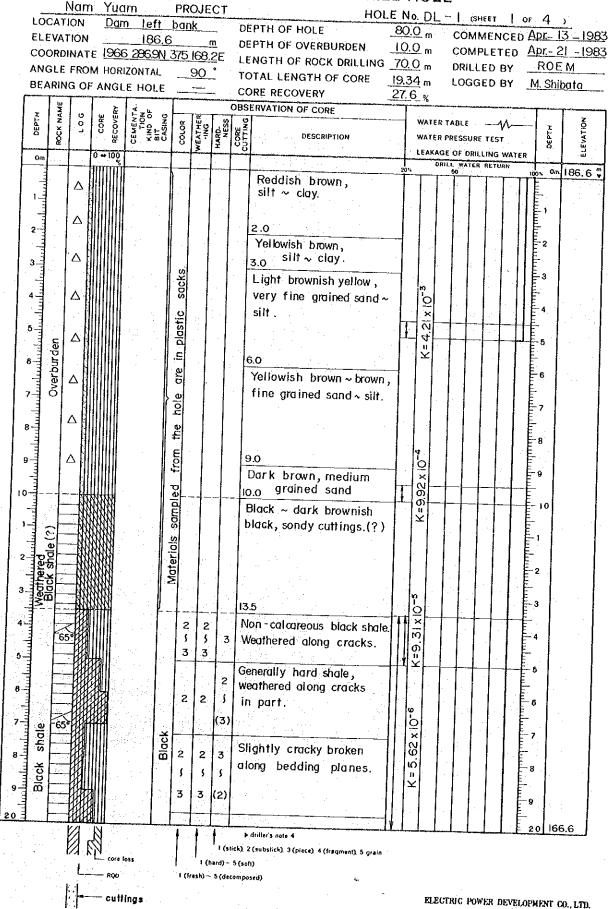
Rock name:

Basalt



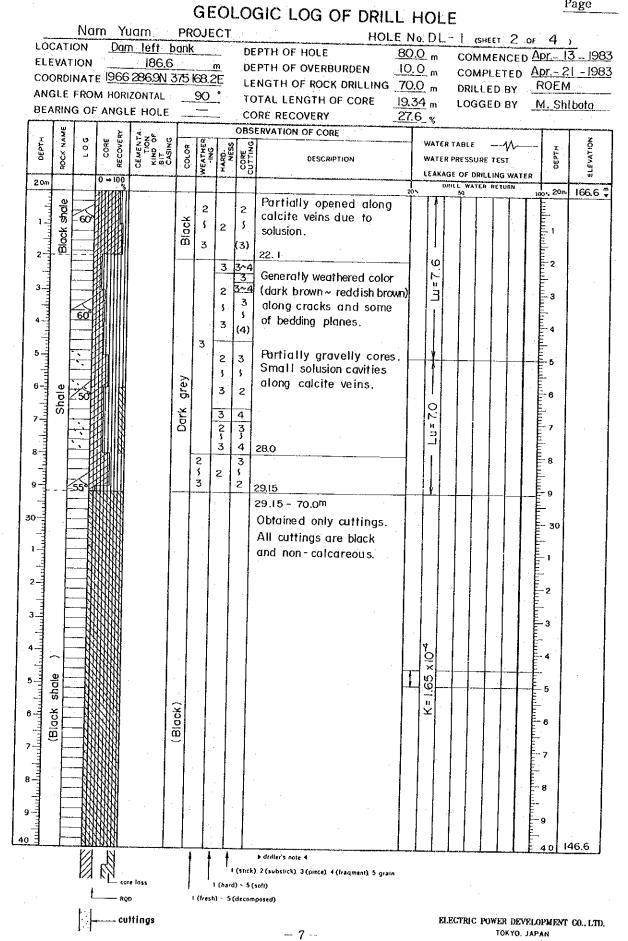
Petrographic description: Phenocrysts are of olivine, plagioclase and clinopyroxne. Microphenocrysts are of plagioclase, clinopyroxne and magnetite.



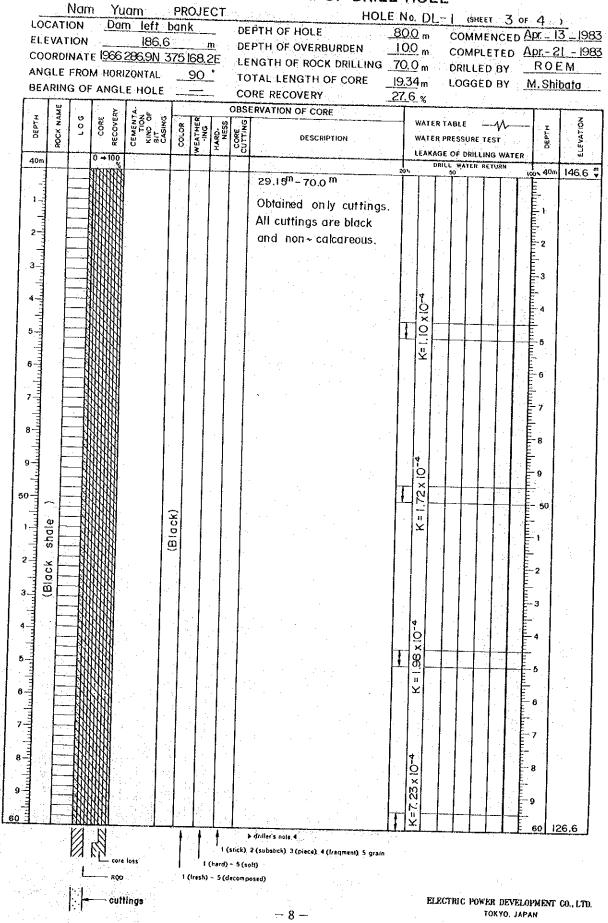


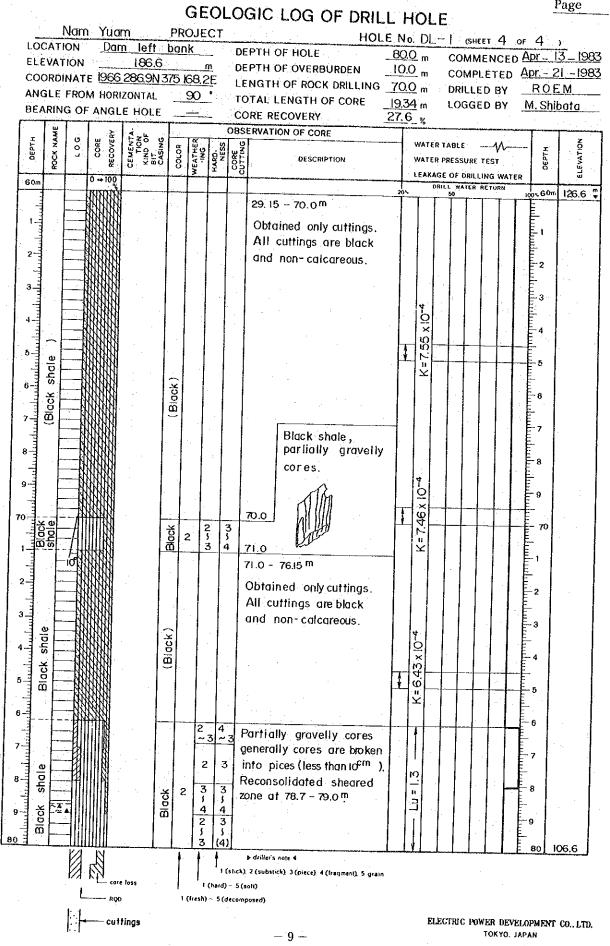
- 6 -

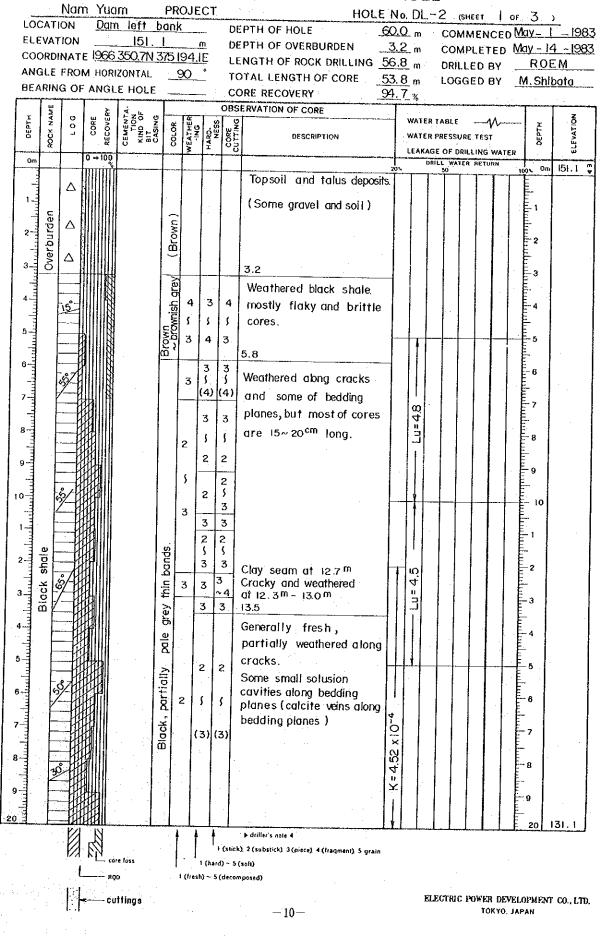
TOKYO, JAPAN

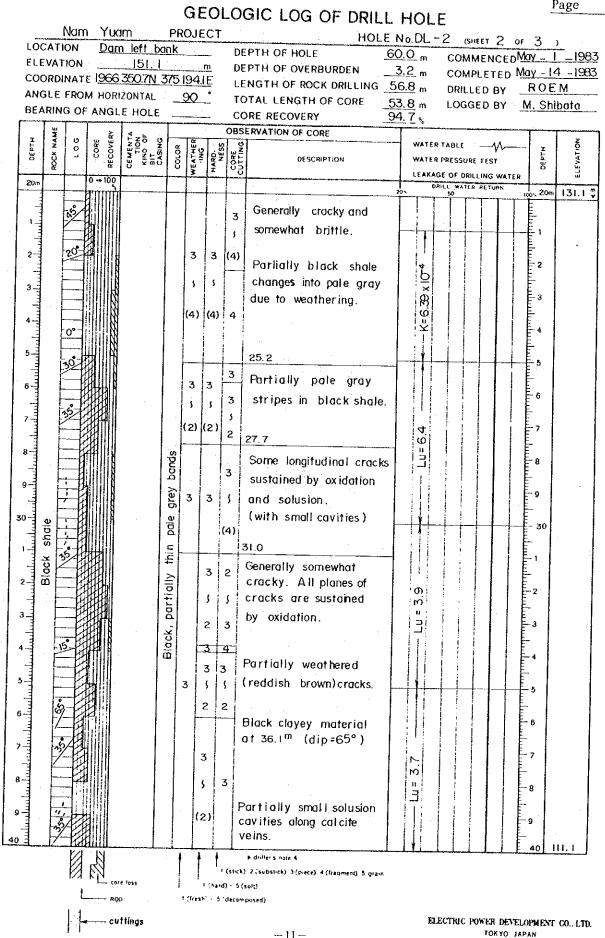


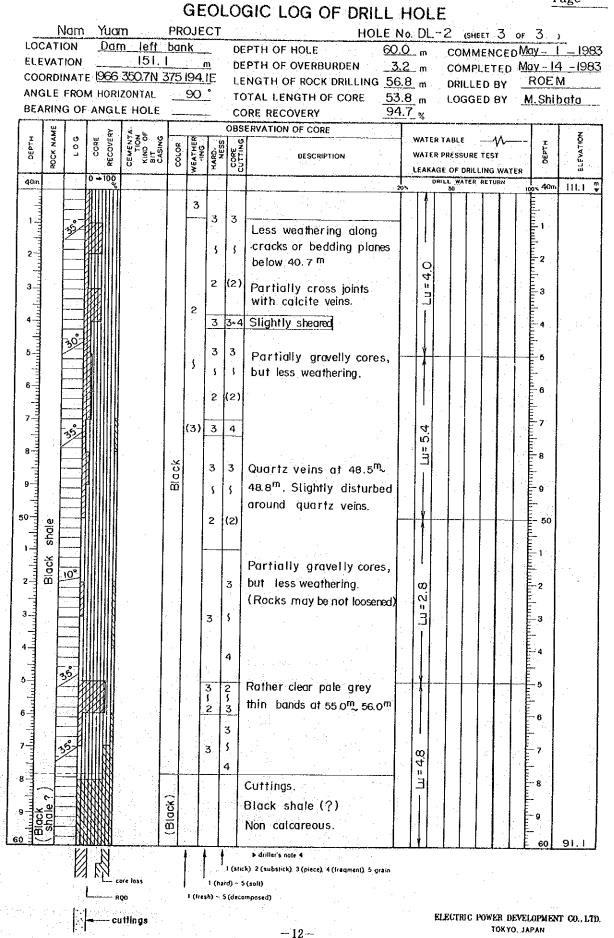
GEOLOGIC LOG OF DRILL HOLE

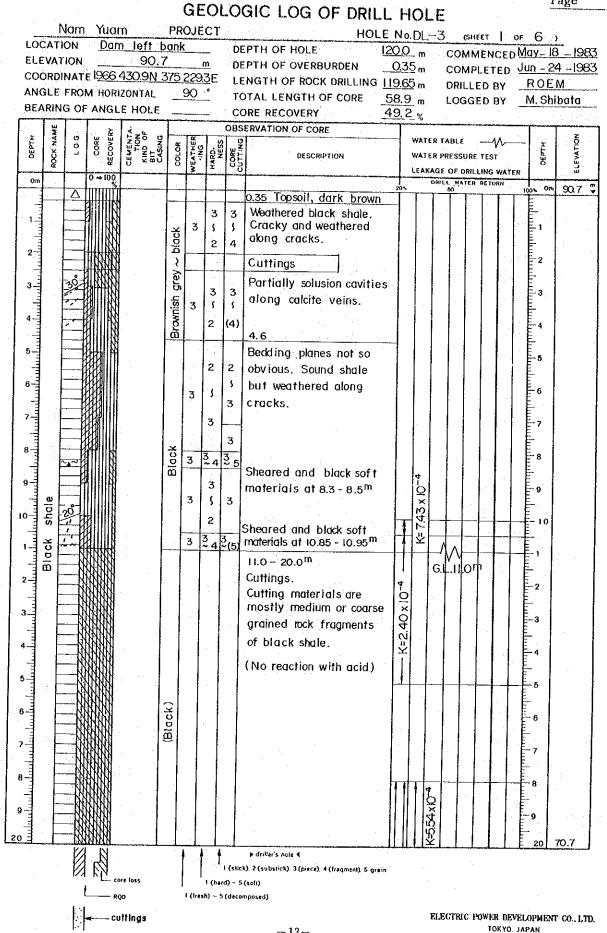




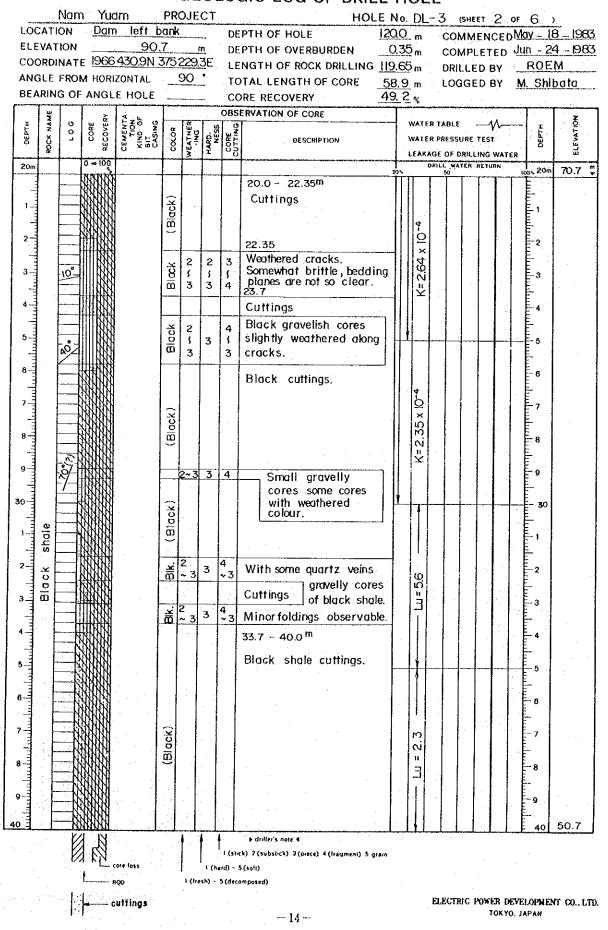


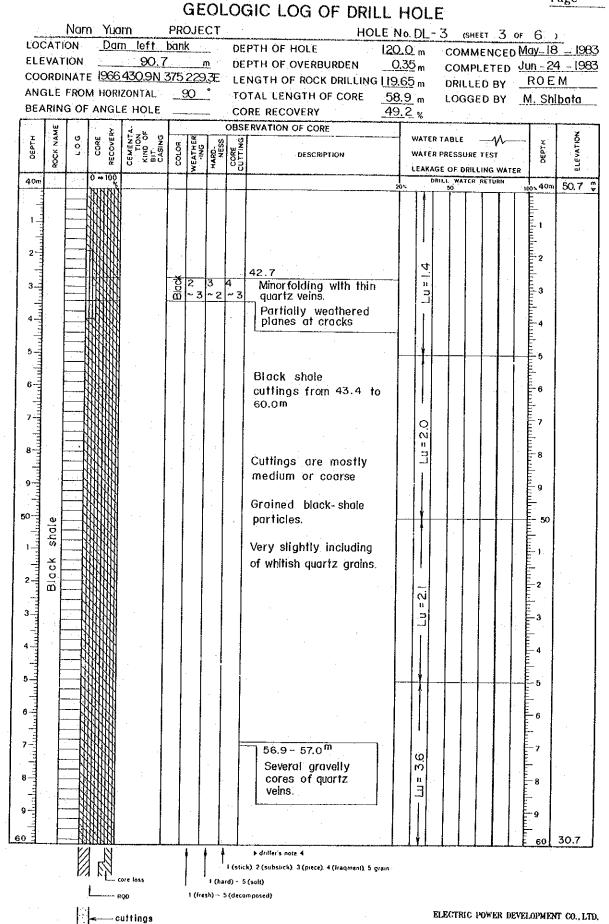






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TOKYO, JAPAN

GEOLOGIC LOG OF DRILL HOLE

.

	Yuam	PROJECT	HOLE N	NOLE No. DL-3 (SHEET 4 OF 6)
LOCATION ELEVATION		bonk	DEPTH OF HOLE	0 m COMMENCED May - 18 - 1983
	90, 1966 4309N	7 <u>m</u> 3752293F		COMPLETED Jun - 24 - 1983
	HORIZONTAL	_90	LENGTH OF ROCK DRILLING 119 TOTAL LENGTH OF CORE 58	1.65 m DRILLED BY ROEM 1.9 m LOGGED BY M.Shibata
BEARING OF	ANGLE HOLE			2_%
			OBSERVATION OF CORE	
DEPTH DCK NAME L O G	CORE RECOVER CEMENT CEMENT TION KIND OF BIT CASING	COLOR WEATHER -iNG HARD-	DESCRIPTION	WATER TABLE
		H W O	85	
60m	0 → 100 אַאַאַעוצוו	<u> </u>		0N 60 100 60m 30.7
		3	Cuttings	
		(Black)		
		1 1 1		
2-1 -02		-X 2 2 2 2 3 2 3 3	4 Black shale, slightly	N 2
3-1		x	weathered along cracks.	
		(Black)	Only gravelly cores.	
4- 9-0		- @	Cuttings	
		11 2 1 3× 1 1	3 Very hard quartz veins and gravelly black shale.	
5		Black and white 2 1 3 3 3 3	4 dire gravely black shale.	
			Cuttings	
		()		
7-		Black)		
		2	67.5 4 Generally gravelly cores	м – – – – – – – – – – – – – – – – – – –
shale	INN	5 3	4 Generally gravelly cores. 3 Minorfolding with thin	
			augrtz veins.	
			Cuttings	-9
		2 3	4 Partially weathered	
		3	3 along cracks.	
		2~33	Cuttings 4	
2			4 Cuttings	m =-2
	ю <u>К</u>	2 3	~ 3 72.8	
	white) 2 3 (3	2 Somewhat long cores are 3 recovered.	
4	and		Cuttings	
			go	
nortz		33	4 Mostly gravelly	
		> 3 1-3		
			3 Calc shale, bedding planes	
7- 0 201			are not so clear .	
shafe		2 dre	Partially flaky.	N
		greenish grey		
Careous Careous Careous		2 3		
9 1 0 1			Somewhat whitish (whitish means rather calcareous)	-9
		S 2 Whity	3	80 10.7
R	<u>N</u>		▶ driller's note 4.	
· · · · · · · · · · · · · · · · · · ·	core loss		J (stick), 2 (substick), 3 (piece), 4 (fragment), 5 grain rð) – 5 (soft)	
. t	RQD	-	s (decomposed)	
i di stati i 🗄	cuttings			ELECTRIC POWER DEVELOPMENT CO., LTD.
Fł			-16-	TOKYO, JAPAN
· · · · · · · · · · · · · · · · · · ·		•		

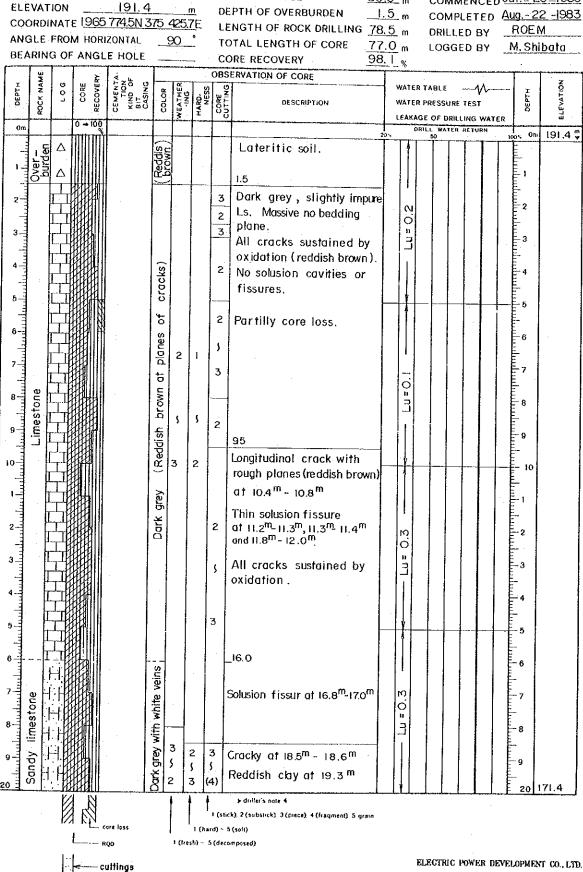
GEOLOGIC LOG OF DRILL HOLE

Nam Yud LOCATION <u>Dan</u> ELEVATION	im PR n left bank 90,7	OJECT	DEPTH OF HOLE DEPTH OF OVERBURDEN	OLE No. DL 120.0 m	-3 (SHEET 5 OF	1ay _ 18	<u> </u>
COORDINATE 1966	430.9N 375	229.3E	LENGTH OF ROCK DRILLIN	<u>0,35</u> m 4G <u>119.65</u> m	COMPLETED	un - 24 ROE	
ANGLE FROM HOR BEARING OF ANGL	E HOLE	<u>.90</u>	TOTAL LENGTH OF CORE	<u>589</u> m 49.2 %	LOGGED BY	<u>M. Shl</u>	<u>bota</u>
		 (OBSERVATION OF CORE			<u> </u>	
DEPTH ROCK NAME L O G CORE RECOVERY	CEMENTA TION KIND OF BIT CASING COLOR	WEATHER ING HARD. NESS	DESCRIPTION	WATER	TABLE	OEPTH -	ELEVATION
80m 0 → 100				201	and the second se	100% 80m	10.7 🖫
	Whity areenish arev	25	Partially slightlysh 2 and slightly flaky. 3 (3)	Гп=0.2		2 1 1 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 1 2 1 2 1 1 2 1 1 2 1 2 1 2 1	
uludiadaulaulaulaulaulauludiad		3	 Rock color gradually cha rather pale greenish. The more greenish the calcareous. Generally sheared partially clayey. 			5 5 7 8 8 9	
00 6 Landrahada 2 Landrahada 4 Landrahada 6 Landrahada 1	Pale grevish light green	$\begin{array}{c} 4 \\ 4 \\ 3 \\ (4) \\ (4) \\ (3) \\ (4) \\ (3) \\ (4) \\ (3) \\ (4) \\ (3) \\ (4) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (3) \\ (4) \\ (3) \\ (3) \\ (3) \\ (3) \\ (4) \\ (3) \\$	 4 Sheared part 3 4 Sheared part 3 4 Sheared part 4 3 Most of cores are brint into small pieces. 4 4 5 Sheared at 94.5 m 7 Pale greenish clay at 95.0 3 4 4 5 5 6 7 7 8 			90 90 1 1 2 2 3 3 4 4 5 6 6 7 7 8 8	-10.7
	I	<u>↓</u> ∮ ∮ ∮	► driller's note 4	<u>i i ! i _</u>	<u>, </u>	100 -	10.7
	are lass	1 1	(stick) 2 (substick), 3 (piece), 4 (fragment), d) = 5 (soft)	5 grain			
1 I	qo uttings	•	(decomposed) 	Ē	LECTRIC POWER DEVI TOKYO, J		° CO., LTD.

LÕ	CATI		<u>Yu</u> Da	am m_left	PR	ÓJE	cr		TH OF HOLE	E N		З (ѕн		or 6 May-18	
٤LI	EVAI	ION		90.1	7		m	DE	PTH OF OVERBUIRDEN	$\cdot \cap \cdot$	25			<u>Jun - 2</u>	
CO	ORDI	NAT	e 1 <u>96</u>	<u>6 430.9N</u>	375	22	<u>3</u> 3E	LE	NGTH OF ROCK DRILLING	196	<u></u>			ROE	
AN	GLE	FRO	N HOP	RIZONTAL		90	•	ŤC			<u>9</u> m		ED BY		
BE1	ARIN	G OF	ANG	LE HOLE						49.	2 %	2000			
	u S	1	ž		1				ERVATION OF CORE	T					
рертн	ROCK NAME	0	CORE	CEMENTA CEMENTA KIND OF BIT	g	u u u	HARD. NESS	ų ž		{	WATER	TABLE		E	ELEVATION
۲ ک	ğ	~	υ ŭ 94	N X N	COLOR	EAT	18ž	CORE CUTTING	DESCRIPTION			PRESSURE		OEPTH	LEVA
100m	+	ļ	0 -+ 100			3	+	-0				E OF DRIL			
100		\mathbf{b}	मामा	1		+	3	3		- 20-	<u> </u>	50	RETURN	100 100 m	-10.7 🖫
				8			3	3						ιĘ	
1-	1	201					~ 2	~2	0					E.	
	shale			N	green		4-5	4-5	Sheared at 101.2~101.4m						
2	ج ا		21		ð		3	2			11			E 2	
	n s	i	81111		pale.	2	5	5			S I				
3	Calcareous		8411				2	3			11			Ē3	
	<u>8</u>				Greyish		4	Ĭ			с L.				
4	ъ			H H	je j		4~3	$ \rightarrow $						E-4	
		\mathbb{Z}		Š.	10	<u> </u>	4-3	-4	Core loss at 104.3-104.7m						
5_		ींगे		8	· . ·	<u> </u>	4-3	4	001 6 1035 01 104.3-104.741					E.	
5 6 7 7				Ъ.					Generally same what						
6-		i 1			green	ŀ			flaky:						
		1			5	н. Т.	3.	3	ridky.					· = 6	
		101			pale -									Ē	
					Ă		4	3	Reconsolidated		2			E7	
					1 E				sheared zone		n			-	
					Greylsth		354	4 5 3	Flaky cores.		1			E 8	
		ilil						2						1	
9-1		IJ			Le	i	2		Somewhat whitish and					· - 9	
					greenish Irey			1	slightly massive clay					<u></u>	
110-	Í		illi		1 Tel		5	5	seam at 111,4 m		╶┼╂┼╌		┼╌╏╶┤		
							3	(3)						E-	
']		lif	4111 II		Whity			,							
							3	3						Ē-	
2-	shale			ĺ		2	<u> </u>		Clay seam at 111.7 ^m and 111.9m		4			2	
	ч Б	1.1				ł	2	21			0				ĺ
3-1	ရှု		翔				\$,	Generally fresh slightly exfoliative along bedding					E-3	
	Calcareous	14	Ħ			İ	'[' [planes,					Ę	.
4	b		Ð				3	2	•					-4	
	8					ł	:								
. 5-		li k	H						Clay seam at 114.7 ^m			++		E-5	
1	- li				5		2	2						E I	
6-	f				green		5	5	Somewhat clayey at 116.0 ^m					E-6	
					1		3 (3)							
7-					pale		Ĩ `	~"						- 7	ł
1	: lí		¥IIII		<u>م</u>	Ę	~2	3		1	0.8			E 1	
8.		1 B			Greyish	F		-			" I			Ĕ.,	
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120	i				Ľ									E 120	- 30.7
		1	N			1	1		> driller's note 4	<u> </u>					
		Ø	5	ence lass) 2 (substick) 3 (piece) 4 (fragment) 5 grain	1					
				core loss				d)~ 5							
di kalenda		, 1	· · ·	RQD		1 (#16	sn}⊷ \$	(dscou	nposéd)						
		ŀ	۹ (cuttings					1		E	LECTRIC		VELOPMEN	Г CO., LTD,
	•	(**')							-18-				FOKYO	, JAPAN	

DEPTH OF HOLE 80.0_m COMMENCED Jul. _ 23_1983 1.5 m COMPLETED Aug. - 22 -1983 DRILLED BY ROEM .<u>77</u>.0 m LOGGED BY <u>98. | "</u> WATER TABLE ELEVATION -----W--DEPTH WATER PRESSURE TEST LEAKAGE OF DRILLING WATER ORILL WATER RETURN 0m 50 · E. 1 2 (N Ö "] - 3 - 4

HOLE NO. DL-4 (SHEET | OF 4)



GEOLOGIC LOG OF DRILL HOLE

Nam Yuam

LOCATION

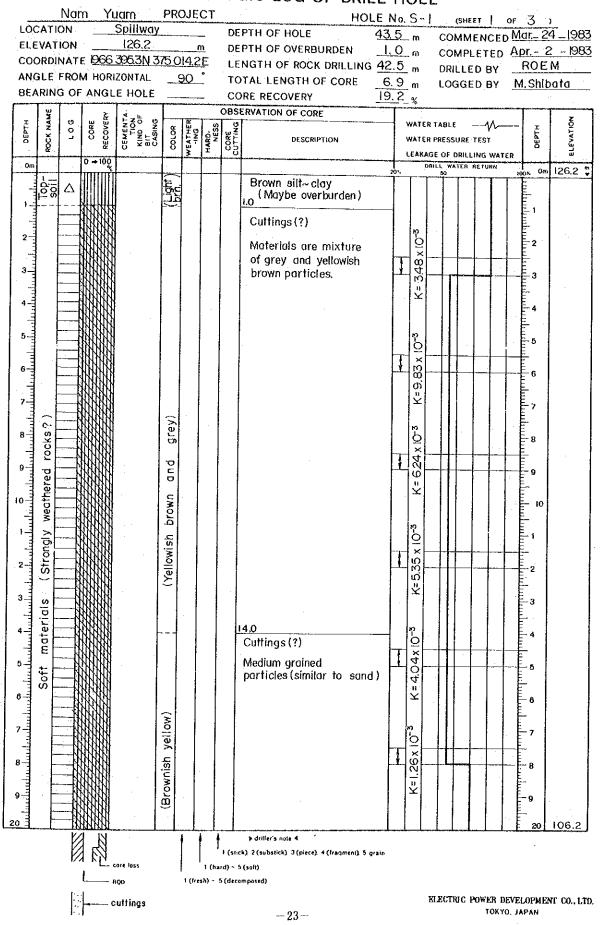
PROJECT

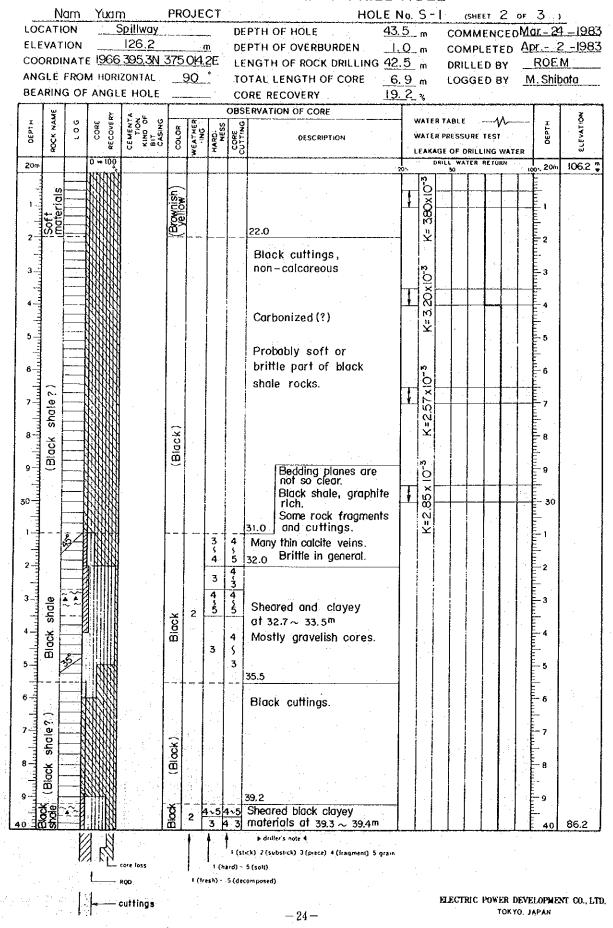
Dam left bank

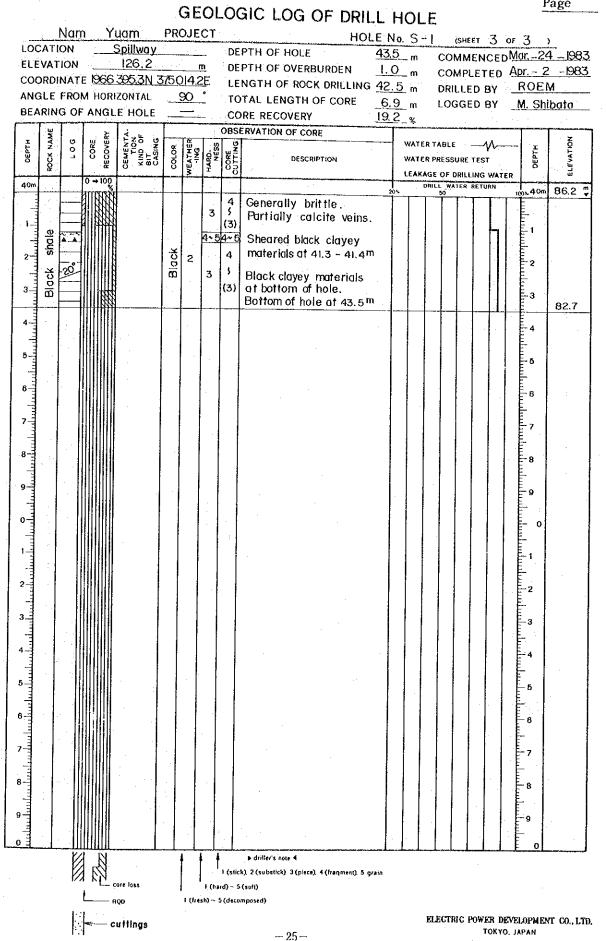
LOCATIC	N	Yuan Dan	n left	bar	OJE	СТ		HOLE BY HOLE	No		4	SHEET AMEN	2 ∘ CED	⊮ 4 Jul 2) <u>3_1983</u>
ELEVATI COORDIN	-	1065	191.4			<u>m</u>		PTH OF OVERBURDEN	1.5	m				<u>Aug - 2</u>	<u>2 - 1983</u>
ANGLE F					<u>+20.</u> 90	-		NGTH OF ROCK DRILLING 7				LED.	- •	ROE	
BEARING					<u></u>	- ·				_ m [_%	LOG	GED	BY	<u>M, Sł</u>	<u>nibata</u>
	Ť	~ ~	<u> </u>	T	-			ERVATION OF CORE	Ť	<u>_ %</u>	17m. m. v			· 	·····
DEPTH ROCK NAME	90 Г 0 С	CORE RECOVERI	CEMENTA TION XIND OF BIT CASING	COLOR	WEATHER	HARD- NESS				WATER		JRE TES		06PTH	ELEVATION
20m		0 → 100 %					<u> </u>		+	Df		ER RETO	-	100 \$ 20m	171.4 🖞
stone				dish brown	3	2	2	Slightly soluble along most of cracks.	Ī						
Sandy limestone			• •	100	1	5 3	۶ 3	Slightly distubed and brittle at 21.5m		00				1	
San L				Dark Dark Dark Dark	-	ľ		23.0		Lu =				113	
Limestone				Light brown	з	3 5 2	3 5 (4)	Slightly brecciated and reconsolidated limestone, partially cracky and brittle. 25.1						uluuluuluu	
				brownish rey	3	3 5	3	Somewhat weathered breccia (inclusions of sandy and shaly breccias)						ц 5 ц 6	
Calcareous breccia						, (4)	(4)	Partially small solusion cavities. Slightly brittle as a whole.		-				ىرىلىيىلىر بىلىيىرل	
							2	28.1 Calcareous shale with sandy part.					:	118 1111 1111	
30							3	Somewhat calcareous as a whole.						9 	
huntunlu • part		R.		grey		3	- I-	Partially small solusion cavities along bedding planes.							
th sandy				greenish	3	5		Sheared and brownish clay at 32.5 m						2	
1 3 3 1 100 110				2				Partially flaky (at shaly part)						113 11-11-11-11-11-11-11-11-11-11-11-11-11-	
Calcareous shale w				yellowish			5	(ur shuny part)							
Calcareous shale w				Light		4	2) - (3) 3	Cracky and weathered along cracks.						-5 	
sandstone			:	ev	2		2 N	ery slightly calcareous nedium grained soundstane		- 2.0-					
sous sone				~dark grey	; . \$ 	5	;	xartially shaly in bands. Partially cracky,	•	" 				8	
				erey. د	3	3	3							- 9 - 40	151.4
	0		re loss				(stick d) ~ 5 i	b driller's note 4), 2 (subslick), 3 (piece), 4 (fraqment), 5 grain (soft)							
· · · · · ·	_] باري	RQ	0		i (fres	ih) ~ 5	(decon	(posed)							
	- -	cul	ltings			•		20		E	LECTRI		r devi Okyo, J		f CO., I.TD.
		÷ 1													

LOCATION ELEVATION COORDINATE ANGLE FROM BEARING OF	Yuam Dam left 191.4 1965 774.5N HORIZONTAL ANGLE HOLE	PROJECT bankm 375 425 7E 90_*	r Di Di Li Ti	EPTH OF HOLE <u>80</u> EPTH OF OVERBURDEN ENGTH OF ROCK DRILLING <u>78</u> OTAL LENGTH OF CORE <u>7</u>	No.DL-4 (SHEET 3 OF 4) 20 m COMMENCED JUL - 23 - 1983 1.5 m COMPLETED AUG - 22 - 1983
DEPTH ROCK NAME L O'G	CORE RECOVERY RECOVERY CEMENTA TION XIND OF BIT CASING	COLOR WEATHER -ING HARD.	w e		WATER TABLE K
00 <		Crey Crey Whity grey with pale greenish thin band	1 2 3 3 5 (2) 3 (2)	Gradually changes. Limestone banded with a few greenish shale. Partially rather massive. Slightly weathered along cracks. Small solusion cavities at 46.9 ^m , 47.8 ^m 49.5 ^m Gradually changes slightly calcareous	DILL WATER RETURN 100,40m 151.4 ** 100,40m 151
	RQO Cuttings	1 (h 1 (lresh) ~	hard) -	ck): 2 (substrick): 3 (piece): 4 (fragment): 5 grain 5 (soft)	ELECTRIC POWER DEVELOPMENT CO., LTD. TOKYO, JAPAN

		N ATI	ON	Yuc Dan	im <u>left b</u> 191,4	PR	OJE	<u>ст</u> —	DE	HOLE N PTH OF HOLE <u>BC</u> PTH OF OVERBURDEN <u>1</u>	10,),Q	DL m	- 4 c	OMN	I EN	CEI	<mark>, Jul. –</mark> 2) 1 <u>3 - 1983</u> 12 - 1983
				e 1965	5774.5N 3	754	125	<u>7</u> E		NGTH OF ROCK DRILLING 78			C D	OMP NILI	LEI FD 1	ED RV	ROE	<u>z - 1300</u> IM
					ZONTAL		90			TAL LENGTH OF CORE 77	7.0	m.						
	BEA	RIN	G OF		E HOLE					DRE RECOVERY <u>98</u>	<u>8. l</u>	%						
	DEPTH	ROCK NAME	r o c	CORE RECOVERY	CEMENTA. TION KINO OF BIT CASING	COLOR	WEATHER	HARD. NESS		DESCRIPTION	·	NATE	· · ·	SLE SSURE F DRIL				ELEVATION
	60m			0 → 100			1		1					WATER	· · · · · · · · · · · · · · · · · · ·			131.4 🖤
	2011 - 2012 - 31 - 40 - 40 - 40 - 40 - 70 - 70 - 70 - 70	(Slightly shoty) Limestone				Grey, partially yellowis brown at cracks	2 2 3 3 3 2 (3) 3 3 2 2	2 2 1 3 $4 \cdot 5$ 2 3 3	2 2 3 3 2 3 4 5 3				DRILL		· · · · · · · · · · · · · · · · · · ·		1000, 6000 1000, 6000, 6000 10000, 6000 1000, 6000 1000, 6000 1000, 6000	131.4 "
	8 7 8 9 9						2 { (3)	3 2 { 1	3 2 (3)	Small fault at 76.2m (dip 50°) Weathered crack at 77.3 ^m		- Lu= 2,5					1 6 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
	, III	÷۴	╤╫	翻					-3				· .					: :
. L .	<u>E 08</u>	<u> </u>		L	core loss RQD cuttings	. .	1 (1)		ard) ~	> driller's note 4 ck) 2 (substick). 3 (piece). 4 (fragment). 5 grain 5 (soft) amposed)		<u>¥</u> 1	ELE	CTRIC	L	ER C	evelopme	111.4 NT CO., LTD.
:		• •	1	1						- 22							O. JAPAN	

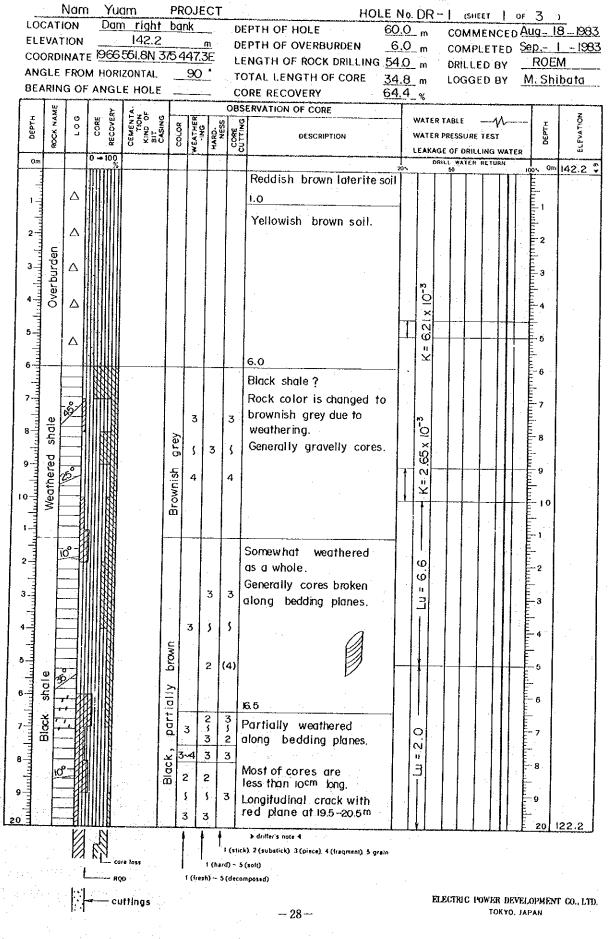


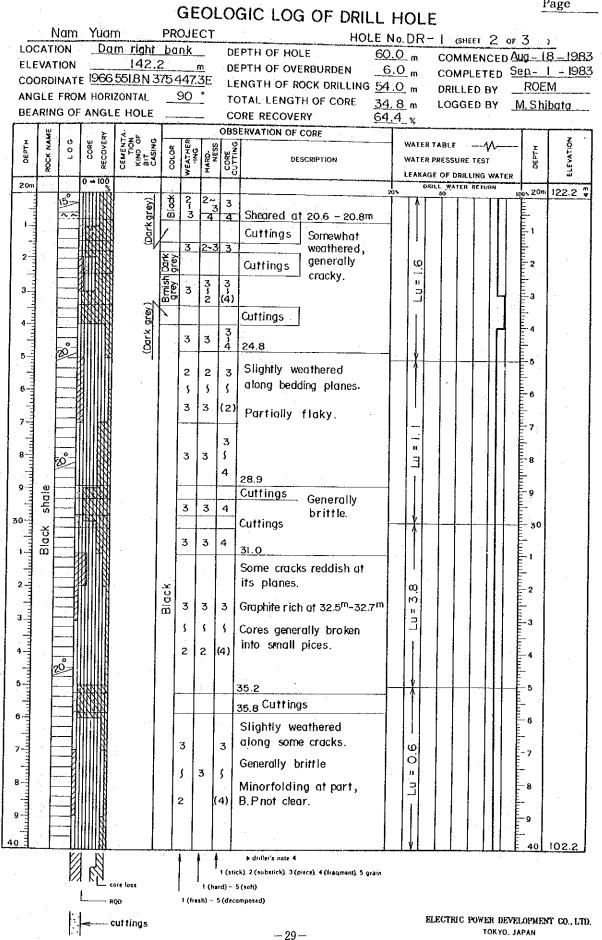


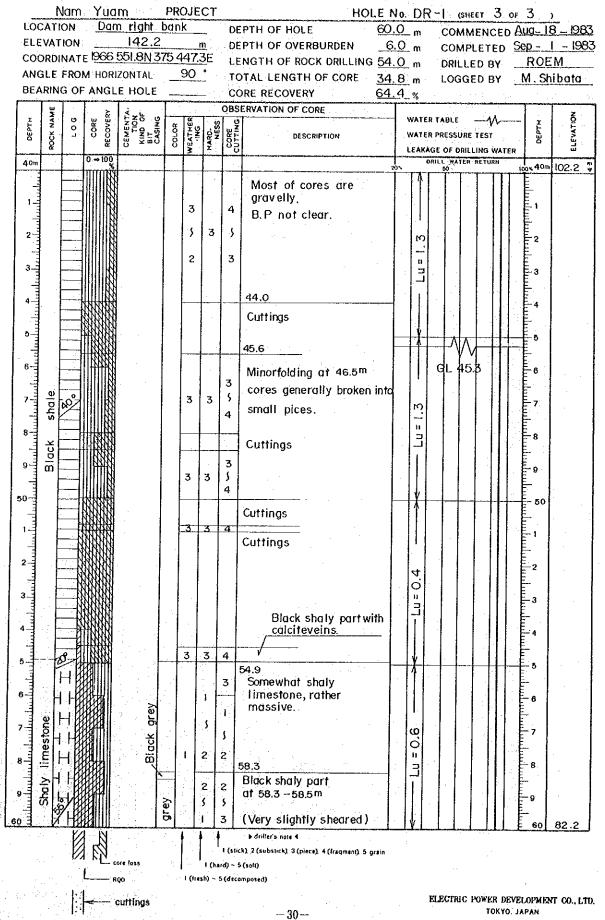


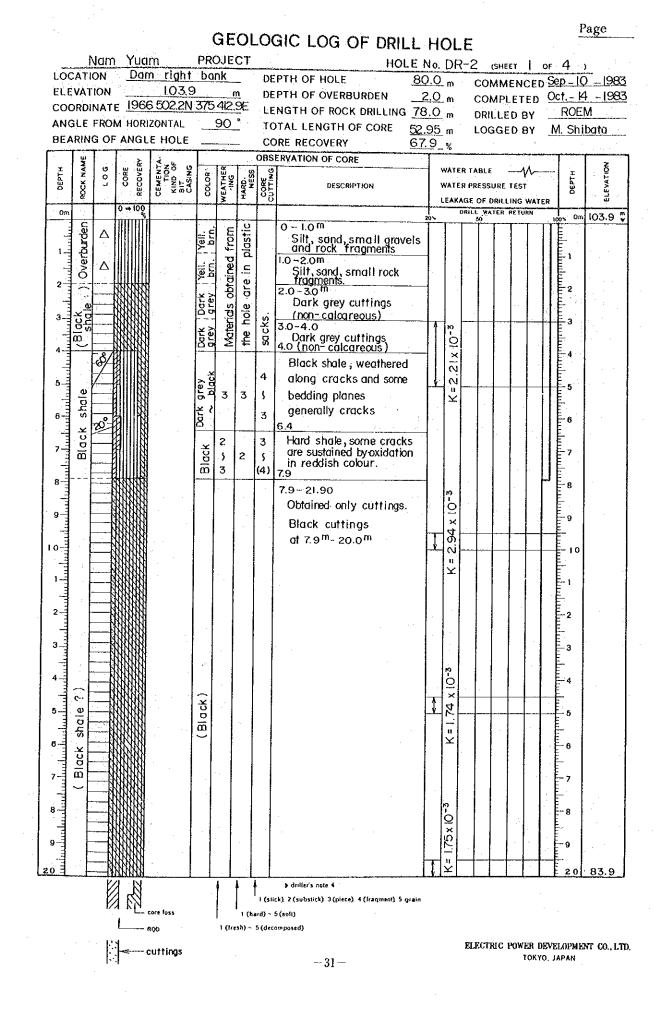
GEOLOGIC LOG OF DRILL HOLE PROJECT Nam Yuam HOLE No. I - I (SHEET | OF 2) Intake LOCATION . _____ 40.0 m DEPTH OF HOLE COMMENCEDMay-18-1983 ELEVATION 143.6 m DEPTH OF OVERBURDEN <u>4.0</u> m COMPLETED JUL -27 - 1983 COORDINATE 1966 516 2N 375 483.6E LENGTH OF ROCK DRILLING 36.0 m DRILLED BY ROEM ANGLE FROM HORIZONTAL 90 * TOTAL LENGTH OF CORE 13.4 m LOGGED BY M. Shibata BEARING OF ANGLE HOLE CORE RECOVERY <u>31. 5 %</u> OBSERVATION OF CORE CEMENTA. TION KIND OF BIT CASING ROCK NAMI RECOVERY ĹŎĠ ELEVATION DEPTH CORE HARD. CORE COLOR WEATHER DEPTH WATER PRESSURE TEST DESCRIPTION LEAKAGE OF DRILLING WATER 100 Ò 0a DRILL WATER RETURN 0n 143.6 🚆 Overburden Δ from 0 to 4.0m E 1 Brown lateritic soil. Δ 2-Overburden (Brown) 2 Δ 3 <u>م</u> 2 4.0 4 4 Brownish grey grey) × Cuttings 5-- 5 (Non-calcareous) ŝ (Grey~ brownish Ч Ч 6-- 6 7 7 ₩ Keo 8.0 Weathered black shale Fault breccia at 8.3m~8.5m Dip. of fault=60° (Thickness 5~6cm) Generally cracky 8 8 3 3 Grey brack 0 2 2 3 9 (4) (4) 9 × m 1.0" 9.5 Core loss 10 зò 10.0 ¥ Brownish grey shale 7 Cuttings (as some as 1 grey) of 4.0m - 8.0m) 2. 2 black (Non - calcareous) (Brownish NO3X 3 (Weathered 3 Ϋ́, 4 |Light grey ∼black: 5.0 Ð 5 4~3 Gravelly cores 3 3 16.0 6 6 Brownish grey cuttings <u>b</u> (Non-colcareous) grey) ā × Brownish 6 ierec 8 8 4 <u>"</u> 19.65 3 4-3 Gravelly cores 3 123.6 20 • drifter's note 4. I (stick), 2 (substick), 3 (piece), 4 (tragment), 5 grain core loss l (hard) ~ 5 (solt) (iresh) ~ 5 (decomposed) - ROD cuttings ELECTRIC POWER DEVELOPMENT CO., LTD. TOKYO, JAPAN -26-

GEOLOGIC LOG OF DRILL HOLE Nam Yuam PROJECT HOLE NO. I - 1 (SHEET 2 OF 2) LOCATION Intake DEPTH OF HOLE 40.0 m COMMENCED May - 18 - 1983 ELEVATION 143.6 DEPTH OF OVERBURDEN m 4.0 m COMPLETED Jul. - 27 - 1983 COORDINATE 1966516.2N 375 483.6E LENGTH OF ROCK DRILLING 36.0 m DRILLED BY ROEM ANGLE FROM HORIZONTAL 90 ° TOTAL LENGTH OF CORE <u>13.4</u> m LOGGED BY M. Shibata BEARING OF ANGLE HOLE CORE RECOVERY <u>31.5 %</u> OBSERVATION OF CORE CEMENTA. TION KIND OF BIT CASING RECOVERY NAM 000 WATER TABLE ELEVATION CORE --W CORE DEPTH COLOR /EATHER HARD. ROCK DESCRIPTION WATER PRESSURE TEST 690 LEAKAGE OF DRILLING WATER $0 \rightarrow 100$ DRILL WATER RETURN 200 100 20m 123.6 🙄 20.0 (Grey) Cuttings ወያ 21.15 1 Gravelly cores of wheathed 22.0 black shale E E 3 .3 22.0 2 Block cuttings (Black) Ľ -3 $\overline{\mathbf{\omega}}$ 24.0 • 4 Weathered black shale. Partially and slightly ñ 5 3 3 brittle. eg eg shale 3 ? 2 Brownish o Weathered along some 6-- 6 bedding planes and cracks. <u>lac</u> 4 (4) m 7 27.4 Ņ lack) Block cuttings h ģ Ξ 8 ٣ď ω 9 9 3 Black shale weathered 5 along cracks and some (4) 30 - 30 bedding plones. 1 Cores are generally cracks) broken into small pieces. 4 2 2 2 Portially minorfolding. 3 (along 11 з (With quartz veins) -3 7 (3) 15 2 4 Generally somewhat cracky - 4 3 brown (4) rocks. Ś shale 2 5 Partially 6 Black 6 3 7~ black, Small solusion cavities ł along calcite veins n 8 8 Grey~ (4)3 at 37.4 m ~ 37.5 m 3 3 2 2 9 0 (4) (4)3 3 3 103.6 ▶ driller's note 4 l (slick), 2 (substick), 3 (piece), 4 (fragment), 5 grain core loss 1 (hard) ~ 5 (solt) 1 (fresh) ~ 5 (decomposed) 800 ELECTRIC POWER DEVELOPMENT CO., LTD. cuttings TOKYO, JAPAN -27-









GEOLOGIC LOG OF DRILL HOLE

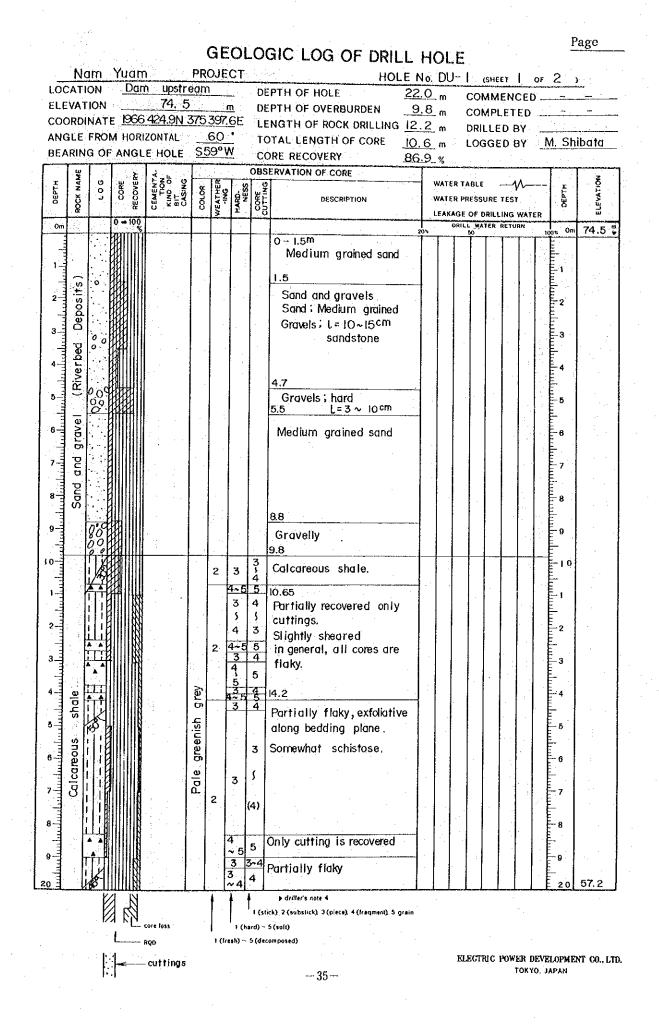
	OCA		N	Yuar Dar	n right	PR b	OJE ank	<u>ст</u>				DF	<u>}-2</u>				of 4) Sep-10) 0 - 1983	à
	LEV			1000	103.9					PTH OF OVERBURDEN 2) CO	омр	LET	ED		4 - 1983	5
					502.2N					NGTH OF ROCK DRILLING 78				81.L.I			RO		
					ZONTAL E HOLE		<u>90</u>				.95		LC	GGI	EDE	<u>3</u> Y	M.Sh	ibata	
Ē				ANGL			-		-		<u>9</u>	%				de 1945-93			1
	ОЕРТН	ROCK NAME	LOG	CORE	CEMENTA. TION KIND OF BIT CASING	COLOR	WEATHER		+	DESCRIPTION		WATE	R TAB	SURE			DEPTH	ELEVATION	
	0m	<u> </u>	·	0 -+ 100		+	3	-	- <u> </u>		1		AGE OF						ł
F	-	=†		WINN				<u> </u>	· ··	Pale green cuttings,	201.	1-		- -	T	T	100 20m	83.9 🛱	ł
	, calc.	< shate			- <u>-</u>	(Pale)				(no reaction with acid)							աստես		
	2-1		\$ 7					i ·	<u> </u>	Weakly schistose,	1	4					1 2		
	Calcareou Calcareou	shale				Whitish greenish grev	2	2	2 5 3	bedding not so clear.		-95 × 10 -					3 		
								3-2	3~4	opper part is semennar		Т Т П							
	سليبيانيسا					grey			2	whitish . Whitish part is rather calcareous than							6	÷	
7	سأسطس					greenish g	1	2	ऽ उ	greenish part .		= 0.6					huut 7		
. 9	الساليبار		, i k 3/1			Whitish g	5	3~ (4)	3 ~4	Slightly sheared around		E					48 11 11 10		
30	سأسبأيت	-				M	2	2	2	28.5 ^m somewhat brittle in part.				\downarrow					
1	يلىسايىسل م 10							۶ 3	। उ	Rother greenish shale.			G	Ц.34	7 .1		սհամա		
2	سطينا ج				-				3 ~4 2	Somewhat flaky due to shearing at 31.7m-32.4m		0.8					2012 1011		
3	Calcareou					ר grey		1 3	5	Generally slightly schistose		- F.							
5	ululu Ca					greenish			3	Little weathered cracks or bedding planes.		Y					E 5		
6	وليسالبونه					Pale		\$ 3 (s (2)				1				8		
7-	يتبليناية	5°						1	2	Weathered crack at 37.2m		0.1			- 				
8-		1					(3)	1	38.2		7					-8	ĺ	
9-			222.22			Greenish)				Cuttings at 38.2 ^m 41.0 ^m							9		
4.0	ŧč,					20						\downarrow						67.0	
<u> </u>		<u></u>	V/	I N		<u> </u>	ł	4. I	. <u> </u>	► driller's note 4		<u>. I . I</u>	ł	. <u>.</u>	ل ــــا		<u> </u>	63.9	
			V					5. ¹	l (stic	ck). 2 (substick). 3 (piece). 4 (fragment). 5 grain									
		• •		1 2 4 1	ore lass	÷ 1	1			5 (soli)						· · ·			
	······			1	oo cuttings	• • •	. (116	*u1 ;	- [d#C(umposed) 32			BLEC	TRIC			EVELOPME 0. japan	NT CO., LTD	5

LOCATION		ight	PRO	JJE		DE			DR-	2 ¢	MEN	3 o ICED	o⊧ 4 Sep_1()
ELEVATION		3.9	76 /		<u>n</u>		PTH OF OVERBURDEN	2.0	m	CON	PLET	red (<u> Oct 14</u>	4 <u>- 1983</u>
							NGTH OF ROCK DRILLING 78	<u>8.0</u>	m		LED		RO	
ANGLE FROM BEARING OF				90			TAL LENGTH OF CORE 52			LOG	GED	BY	M.Sh	i bata
·		IULC	T				DRE RECOVERY <u>67</u>	<u>,9</u>	%					
DEPTH ROCK NAME L O G	NTA:	go g	~	<u>a</u>			ERVATION OF CORE	╡,	WATER	TABLE		۸۸		N N
DEPTH CK NA	CORE RECOVERY CEMENTA	KIND OF BIT CASING	COLOR	WEATHER -ING	HARD. NESS	CORE	DESCRIPTION		NATER		RE TES	уч ЭТ	DEPTI	ELEVATION
8	Ť		õ	Ň	Ĩ	<u>S</u>] 1	EAKAG	E OF DI	NLLING	WATE		11
40m	0 -+ 100						<u> </u>	201	DR	LL WAT	ER RET	URN	100 40m	63.9 🖫
					[Cuttings.		14				Ē	
			Б -				41.0				1		Ē,	
		•	Pale grenish grey		3	3	Slightly flaky due to						Ē'	
2 0 0 0 0			500	2	S.	š	steep foliation.		ω				E.	:
			32		2	(4)	42.7		i				2	
3/			-	<u>-</u> -			Cuttings (Reaction with acid)		n ⊐ '				Ē.	
			ĕĕ				Currings (Reaction with acid)		Ľ				E-3	
			<u>ق</u> م				44.0							
			enist ist		-	3	Somewhat brittle due to	1					: E 4	
State State			E E E E E E E E	22	3	3 5 4	45.0 shearing.						Ē	
			£				Cuttings. (Reaction with acid)		1				5	
			Green				46.0						E.	
			ଁ୍		3	3		1					6	
		ľ			2	3 5 4	Somewhat sheared as a whole						- uu	
	20 II N	ĺ		. l	2 _{~3}	2	ds a whole.	·	0					
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shale		[grey	2	3	3							- 8	
				5	5	5					Ì		<u>.</u>	
9 I SI / I			greenish	<u>'</u>	í I	Ý	Clayed at 49.4m						-9	
e e			ee	1	(4)	4	Clay seam along bedding						Ē	
Calcareou			1				plane at 50.5 m		X	+			50	
			Pale		_	-	· · · · · · · · · · · · · · · · · · ·						Ē	
			0		3	2'	Somewhat more calcareous (whitish)						E-1	
					2	3							E.	
2					-		52.1		ω				2	
- 25 25 10 10	XXXXX		1				Cuttings(Reaction with acid)		0 n				-	
3	<u>XXXXXX</u>	ŀ					53.0		7				E-3	
													E-	
4-						ĺ							<u>-</u> 4	
					3	2	ongituding argate with							
0	祖		. [·.			Longitudinal crack with rough plane at 54.5 ^m		¥	┿		+	- 5	
			rey		5	5	rough hute of ouron		Ϊİ				<u> </u>	
			Ъ.	2									6	
shal					2	3	Colcite veins are						E ·	
7-]	田		greenish				perpendicular to bedding		м				-7	
			Б,	\$	1		planes.		0				Ē.	
Calcareous			Bale	, -					н Э				E-8	
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9 3 1					-	4	504						E-9	
3/1	#						59.4						E.	
		·		<u></u>];	3	<u>~ II</u>			<u>YL</u>				60	43.9
l l				1	† †	1.7-1	þ duller's nate 4 12. 3 Gubabaki 3 Gaiaceil & Gaementi 6, ausia							
E E	1 KZ core la	035		ŀ	1.00		:k) 2 (substick): 3 (piece): 4 (fragment): 5 grain 5 (soft)							
	L ядо			' 1 (fre			(son)							
ŀ.•	4								F	I.E.(TR	C POV	VER DE	VELOPHE	NT CO., LIT
	cut	tings					-33-		-				, JAPAN	
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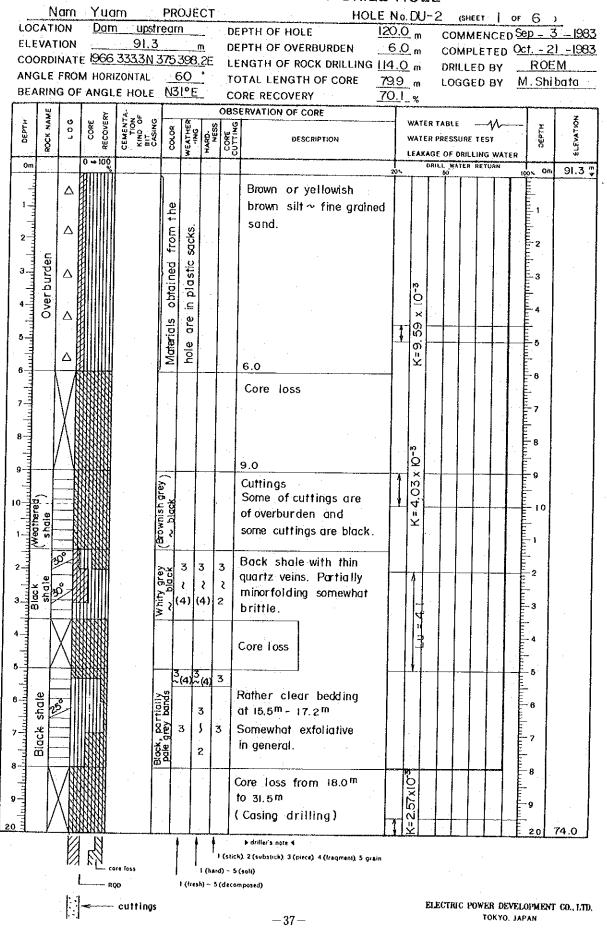
GEOLOGIC LOG OF DRILL HOLE

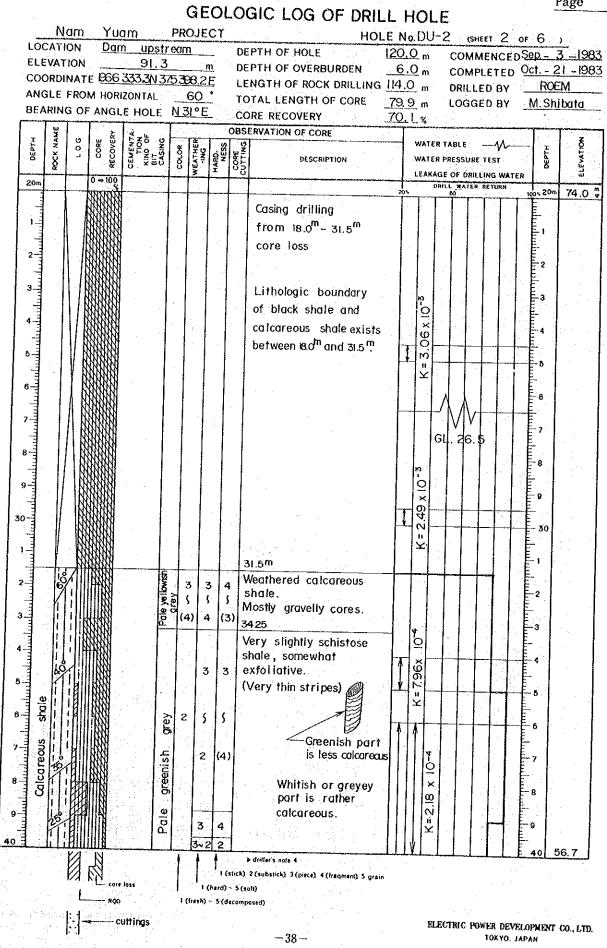
	LOC	CATIC	ΟN .	Dan	m n <u>right</u> 103.9	bar	1K		DE	HOLE N PTH OF HOLE BO PTH OF OVERBURDEN 2	.0	m	C	OMN	AEN	CED	<u>Sep. I</u>	<u>) _ 1983</u>
	ANG	ALE I	FRO	M HORI	502.2N 3		90	•	LE TO	NGTH OF ROCK DRILLING 78 TAL LENGTH OF CORE 521	<u>.0</u> 95	m	D	RILL	ED E	ΒY	ROE	<u>M</u>
			0	T	T	T			OBSI	RE RECOVERY 67.	Т		RTA	9LE		м—	<u>-</u> <u>-</u>	XOL
	DEPTH	ROCK NAME	د د	o core 5 recovery		COLOS	WEATH	HARD	CORE	DESCRIPTION	ι	EAKA	GEC	SSURE F DRIL	LING	WAT	and the second s	ELFVATION
	60m	shale				enish		253	1 5 2	Partially sheared and slightly brittle	20		*	<u>,</u>		Ī		43.9 🚆
		Cdc. sh				Pale greenish gréy	\$ 2	3.	3	623		- 5					11 1 1 1 1 1 1 1 1 1 1	
		Shaly Ilmestone				Pale F grey	1	3	2	Shaly limestone somewhat brittle 63.4 due to shearing		Lu = 0.						
						grey		З	3 5	· · · · · · · · · · · · · · · · · · ·							-1 4	
	2					greenish		_4	2	Sheared and reconsolidated at 65.4 ~ 65.6 ^m		X					5	
	۰. ۱					Pale gr		3	3			4					- 6 	
	4 2 6 2 8 10 10 10 10 10 10 10 10 10 10 10 10 10 1				e e e e e e e e e e e e e e e e e e e		1	<u> </u>		67.6 Somewhat whitish more calcareous shale.		Lu = 0.					1111 1111 1111 1111	
	ر الم م									B.P is not so clear. Clay seam at 69.0m								
	70-1 	shale					5			Core recovery is good in general.		Å					- 70 	
	2 2 1	us sh					2			Weathering is very few.		0.7 -					1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	
	3 10 10 10 10 10 10 10 10 10 10 10 10 10	Calcareou				h grey		2	5			– Lu = (
	4 ilminiti	ບ 				greenish		- 8 - 111			-	Y					- 4 	
	6-1-1 6-1-1					Whity			2	an an an an Arran an Arran Arran an Arran an Arran Arran an Arran an Arran an Arran							6	
	م منابع منابع									Clay seam at 76.4 m		0	- - -		· .		1 1 1 1	
	8 11 11 11 18							••••				" "					-8	
L	30 -							•	•	b driller's note 4							- 80	23.9
					core loss AQO		1 (1/-		ard) -	ck) 2 (substick) 3 (piece) 4 (fragment) 5 grain						• •		•
		1 	•		- cuttings						• .		ELI	CTRIC			EVELOPME 'O, JAPAN	247 CO., LTD.

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Nam	Yuam	- p	ROJE	ст		HOL	.E 1	No. DU-	(SHE	FT 2	ΣΕ 2	`
LOCATION	<u>Bain</u> u	parren	111		DF	PTH OF HOLE	22	Δ		ENCED		<u></u>
ELEVATION		ł. D 👘		m	DE	PTH OF OVERBURDEN	9	8 m	COMP	ETED		
COORDINAT	Ľ	· ·			LΕ	NGTH OF ROCK DRILLING	12	2				
ANGLE FROM				_	то	TAL LENGTH OF CORE	10	6	LOGGE		M Shi	bata
BEARING OF	ANGLE HO	DLE S	<u>59°</u>	V	00.	DRE RECOVERY	86	9 .				Juru
۳. ۲	2 4	<u> </u>			OBS	ERVATION OF CORE		<u>10_ %</u>				<u> </u>
DEPTH ROCK NAME L O G	CORE RECOVERY CEMENTA	CASING	COLOR WEATHER	. %				WATER	TABLE		x	ELEVATION
L C B		C B C B C B C B C B C B C B C B C B C B		HARD- NESS	CUTTING	DESCRIPTION		WATER	RESSURE	TEST	DEPTH	E VA.
	0 -+ 100		<u> }</u>	I	ីបី	; 			E OF DRILL	Concession of the local division of the loca	R	
				· .			2	0×	LL WATER	RETURN	100N 20m	57.2 🗘
dreous 11e	71111	usu.	s s	3	3	Partially minorfolding						
	P	Ne la	2 5	5	5	with calcite veins						
19 <u>2</u> ,50°	IIIIN	0	≫ I I	(4)	- 1						Ē'	
2-1-1-1	HHHN	<u> </u>									Ē.	55.5
						End of hole at 22m						
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Ø.	-8 · · · ·	: .	† . † .	1		driller's note 4						
	Core loss			l (i (hard))		2 (substick) 3 (piece) 4 (frequent) 5 grain	!			÷		
. L.	RQD	. 1	i (fresh)						`			
5 - 5 - ¹ - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1												
	cutting	5				0.0		ELE	TRIC POW		LOPMENT	CO., LTD.
						-36				TOK YO, JA	PAN	
								1.1				





ELEVATION COORDINATE 1966 ANGLE FROM HOR BEARING OF ANG	<u>m upstream</u> 91, 3 n 3333,3N 375 398,2 IZONTAL <u>60</u> LE HOLE <u>N31E</u>	DEPTH OF HOLE DEPTH OF OVERBURDEN 2E LENGTH OF ROCK DRILLING TOTAL LENGTH OF CORE CORE RECOVERY OBSERVATION OF CORE	LL HOLE LE No.DU-2 (SHEET 3 OF 6 120.0 m COMMENCED Sep 3 _6.0 m COMPLETED Oct 2	<u>1 -1983</u> M pata
DEPTH CCK NAME L.O.G C.ORE RECOVERY	CEMENT TION KIND OF BIT CASING COLOR COLOR COLOR	SS SE DESCRIPTION	WATER TABLE X	ÉLE VATION
40m 0 → 100	3	T ~ Q	LEAKAGE OF DRILLING WATER	
	Pale of the second seco	 3 3 4 4 4.5 4 4.5 Greenish grey cuttings 3 3 Greenish grey cuttings Partially quartz veins slightly exfoliative as a whole 45.8^m-46.2^m Cuttings 3 3 3 3 3 4 5 2 (2) 5 5 2 6 49.7 Core loss Brittle 50.2 Core loss partially quartz vei 5 1.05 Core loss 51.65 3 3 Partially weathered cracks or bedding plane \$ 1 \$ 2 (2) Yery hard quartz vein at 55.2^m - 55.3^m From 56^m to 60^m, core box is lost. Driller reports during transportation, the core box was fallen into river 	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	22.1
	1	I (stick) 2 (substick) 3 (piece) 4 (fragment) 5 gr		<u></u>
t R		1 (herd) - 5 (sofi) h) ~ 5 (decomposed) — 39 —	ELECTRIC POWER DEVELOPMENT TOKYO, JAPAN	CO., LTD .

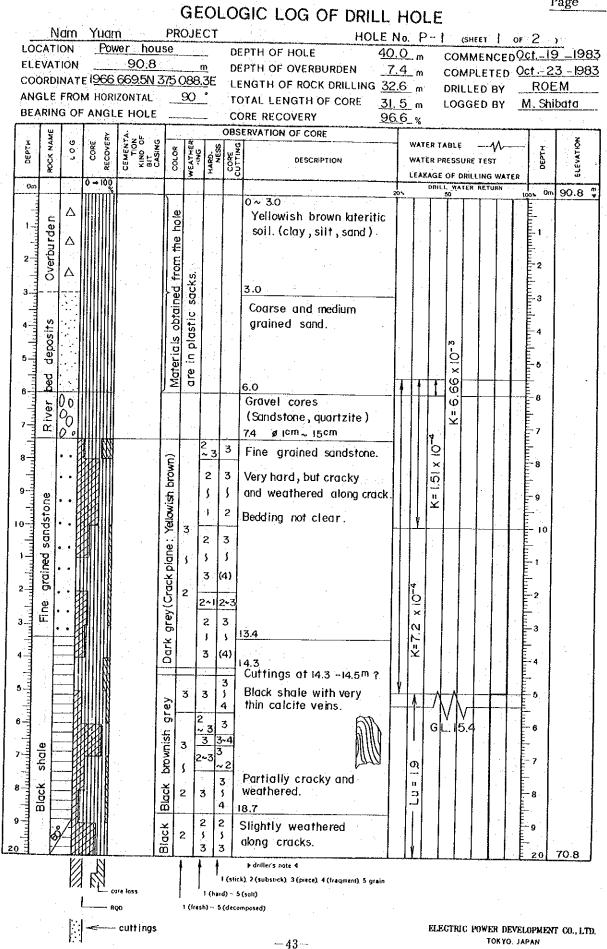
		Na	m	Yuc	าม					-00	GIC LOG OF DRILL			^	0	
	LÕC				am						HOLE N PTH OF HOLE 120	<u>10: DU</u>				<u>)</u> 31983
	ELE	νατ	ION		· .	91.3			m			<u>.0</u> m				<u> -1983</u>
					6 33						NGTH OF ROCK DRILLING		DRIL	LED BY	RO	EM
					RIZON				•	ŢĊ	TAL LENGTH OF CORE 79	.9 m		GED BY	<u>M. Sh</u>	ibata
					GLE F	IOLE						<u> </u>			********	
	E	OCK NAME	U	CORE	NTA.	5° 5		۲,	1.0		ERVATION OF CORE	WATER	TABLE	-1	r	ğ
	рертн	ХX Х	ç	8	CEMENTA	KIND OF BIT CASING	l õj	WEATHER	HARD-	CORE	DESCRIPTION	1	· .	RETEST	DEPTH	ELEVATION
	60m	<u>~</u>		0 ⇒10			+	3	+ <u></u>	00		0		RILLING WA		
	•		ΠŢ		Ň –				+		2 Quartz veins at 60.6 ^m - 60.7 ^m		50		100×604	22.1 🛱
	1		15								and 61.55 - 61.65m					
		shale	1				grey		3	3			•			
	2-	히									Somewhat brecciated				2	
	- 1	Sn					1 s F	2	15	5	in port and brittle.	₹. 				
	3-	- Lec		2			greenísh		la	(4)		"			÷.3	
	3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Calcareous	20.1	3						(47] - - -				
	4	U	150	Ť III			Pall				64.6 m				E 4	
	5-									4	Fault zone with clay and					
	. m	<u>ب</u>	≜ ~				د ک	3	4	\$	breccia and sheared	4				
	6-	zone	â				greenish grey	5		3	rocks.				E-6	
	- Thu	ŧ	田		N		gre	2	3: 5	3	Generally brittle. (Sheared at shaly part)					
	7-1	Fault	Q-11 ?}▲				Pale	- .	4	3	Not sheared at limestone	0.6			E 7	
										~4		u				
	° 11	1								Í	Very slightly weathered	L.			- 8	
	9								2	2	as a whole. Most of cracks somewhat		.			
	The second second second second second second second second second second second second second second second se										weathered.					
	70-						grey		5	5	Slightly banded and shaly.				Ē- 70	
	1	i					p			·	enginity bandou and onary,	11			u.	
		l		2111			rish		,	3						
	2	5					yellowish	3	·	1						
	The second second second second second second second second second second second second second second second se	e /										0				
[3	esto					light					"			-3	
		ĒĽ						\$	2	3 1	Sheared and brecciated					
	4						partially		. F	5	at 73.4 - 73.5 ^m				4	
	2 2 2 1 2 1 2 1 2 2 1 2 2 2 2 2 2 2 2 2	<u>]</u>					Ĕ	z	3 (4)	reconsidated) Weathered a long cracks	· V .				
	The second second second second second second second second second second second second second second second se	5 I					· • ·				Slightly banded				δ	
	6-1	C.		1			grey				with greyish stripes)				-8	
	n	ſ							2	ו ג	imestone					
a a la	7-1						ui ui ui				Partially slightly weathered along cracks or cross	ц.			-7	
							With		S.		joints.				-	
	, il :		- EB	$\Pi \parallel$		· ·	rey		,			E			8	1
	- - -		H				5			3						
		05	個								Clay seam at 79.8 m				9	
80	23	Кİ	111	ШШ И	l <u>.</u>		<u> </u>			ŀ	> driller's note 4	<u> </u>			68	4.8
			0	ß	:		I	ĺ	Ī	l (stic)) 2 (substick). 3 (piece), 4 (fragment), 5 grain					
			1	<u>ا</u> ــــ	core los	s		1 11-1		d) - 5 (dara						
		s.,	.		RQO	nu la l		e 5,17#	ny~ 5	(U#CQ/	nposed)		W 19/100			
•.		н 14 м	ŀ	- 	- cutt	ings					-40	E	LECTRI		EVELOPMEN 0. japan	TT CO., LTD.
			;													
					•			•								

GEOLOGIC LOG OF DRILL HOLE

ς.

LOCATION	91. 1966 333.3N HORIZONTAL	PROJ ostream 3 375 398 60		DI DI DI LI T(PTH OF HOLE 120 PTH OF OVERBURDEN	No. DU-2 <u>).0</u> m 5.0 m . <u>0</u> m 1.9 m	COMMENCED COMMENCED COMPLETED ORILLED BY	ep319
<u> </u>	RECOVERY CEMENTA. KIND OF			OBS	ERVATION OF CORE	· ·	ABLE	DEPTH DEPTH
		Pale grey partially signify yellowish R 4 6 10 - 50	2 5 1 3 5 2 2	2 5 (3) 4 5 3 3	Generally cracky and weathered color along planes of cracks. (No solusion phenomena) (Bedding planes not clear) Clay seam at 84.1m Fresh slightly shaly		L WATER RETURN	2
$\frac{1}{1+1} = \frac{1}{1+1} = \frac{1}$		Grey	2 5	2 5 3	limestone. Partially slightly flaky along bands (One kind of sheared planes ?) Generally massive. (Calcareous contents are rather high)	.0		990
		Yellowish Srey S S S S S S S S S S S S S S S S S S S	2 5 3	3	Weathered part somewhat shaly			3
		bark grey	2 \$ (3)(2	24.0 Shaly limestone ; (Difinition) Rather exfoliative along bedding planes, and rocks color is rather dark grey than the rocks called slighty shaly limestone. Partically somewhat exfoliative. Calc. contents are rather high)	Lu = 0.6		
	RQD			nd) - 5	 > driller's note 4 () 2 (substick), 3 (piece), 4 (fragment), 5 grain (soft) nposed) 	<u> </u>	CTRIC POWER DEVEL	100 - 12.5

	100		am M		am m upst	PR	ĴĴĔ			HOLE IC LOG OF DRILL HOLE	No.		-2)1983
	ELE	VAT	ION	· · ·	91, 3			n.			5.0							1 -1983
					333.3N3					NGTH OF ROCK DRILLING			D	RILL	ED I	BY .	ROE	:M
					IZONTAL		60 31 E				<u>9,9</u> 2,1	<u> </u> m	Ľ	ogg	ED I	BY	<u>M. Shi</u>	bata
ſ		······		<u> </u>		Т				ERVATION OF CORE	T							
	рертн	ROCK NAME	0 0	CORE	CEMENTA TION KIND OF BIT CASING	8	μŰ	S.	N. N	DESCRIPTION		WATE WATE		ale SSURI	/ Trisi	γ Γ	DEPTH	ELFVATION
	ä	SOC.	-	- -	1	COLOR	WEATHER	HARD. NESS	CORE -	DESCRIPTION	1	LEAK	AGE C	F DRIL	LING	WAT		ני דר ש
- li	00m		5	0 ⇒100 रामगा।	 						20	- T-T-		WATER	RETU	18N -	100 10004	- 12.5 🖓
	, nin		4				1	2	2						1			
	11			扣		grey	5	5	5									
	2		Н			2 7 2	2	(3)	(3)				ŀ				12	
	-			翻		Dar	. ·			102.5 ^m		N - N						
	مىرانىيىلىيى ئىيىلىيىلىيى		5	11					3	Exfoliated along bedding planes (sliced cores)		11					<u> </u>	
	1					ds y		3	4	Somewhat weathered						ĺ.	<u>и</u> 1	
Ì	1	-		81111		Ye Ilowish Grey	3	(2)	3	at 104.0m ~ 105.0m Small solusion cavites	-						4	
	5-1	•		ĺ		Ύe			4	at 104.6m	-	¥.				<u> </u>	<u> </u>	
	T	ŀ	25			ark grey		3	4 <u>.</u> 3	Densielle servicelle tate		Î						
	6-1					۵		2	3	Partially very slightly weathered along cracks.							6	
	7									Generally shaly or slightly		5					1 1 1 7	
	m		20							shaly limestone.		0					براييد	
	8-1	Į.								No solusion cavities.		Ē					- 8	
		imestone	ЫÅ							(Partially very slightly exfoliative along							يسله	
	, II II	nes	i i i i				1	2	5	bedding planes)							9	
11		≞	Нł						\$		-	¥.		.				
	1	1	Ô									Î						
	1	Shaly	Н				5	5	(3)									
	2-1	S	IH				·					8					2	· · ·
	عناعينا		H			é				••••••••••••••••••••••••••••••••••••••		Ö						
	3-1	-	ΙH			υĽ			3	· · ·		Ľ					E -3	
	4-1	•	ΗĮ				(2)			· · · · · · · · · · · · · · · · · · ·			-				in a	
	يبطين	Н						•										
· [·	5-1.	1					· .		2			X			-			
	الله الله	H	H						5									
	أعدا		ΗŖ						(3)	· · · ·						ŀ	– – –	
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	n line		╡∦		and Algenting				3			11						· ·
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	inter The	2						k	3)									1
120	<u></u>	<u>. 11</u>	- 11 17	1 N	ا جنوبت		 			> driller's note 4	اب ب	LY.L			Ļ	Ļ	F 150	- 29.8
					core loss					k) 2 (substick) 3 (piece) 4 (fragment) 5 grain					• •	-		
* .		÷			RQD		1 1 (bi			i (soll) Imposed)	· ··							
tyte e		- 12	ľ		- cuttings				•				ELE	CTRIC				NT CO., LTD,
	•		1	1		۰.				-42-						TOKY	D. JAPAN	



TOKYO, JAPAN

Nam Yua LOCATION PO	im wer hou:	PROJ				No.	Р — сян			
ELEVATION	90.8	56	m			<u>).0</u> '.4	m COMN	LETED	$\frac{CT - 12}{CT - 2}$	3 _ 1983
COORDINATE Dee		75 08			NGTH OF ROCK DRILLING 32		m COMP m DRILL		ROE	
ANGLE FROM HOR	ZONTAL	_90) °		TAL LENGTH OF CORE 31				M.Shi	
BEARING OF ANG	LE HOLE	· 				5.6			· · · ·	
, w k					ERVATION OF CORE			**		ž
DEPTH ROCK NAME L O G C ORE RECOVERY	CEMENTA TION KIND OF BIT CASING	COLOR	HARD- NESS	CORE	DESCRIPTION		ATER TABLE	TEST	DEPTH	ELEVATION
	9 X 200	8 8	HARD	85		ł	EAKAGE OF DRIL		ă	EL 12 EL 12
2 0m 0 → 100						20	DRILL WATER	RETURN	100 \$ 2011	70.8 Ţ
		2	2	2	Small solusion cavities along 20.7 colcite veins at 20.7m				E	
1- SAL		-	1.00			1			E,	
				3	Very slightly weathered				E'	
2				2	along bedding planes					
				3	or joints.		<u></u> Ω			
3_		2	2	2	Partially exfoliative		<u>u</u>		E-3	
					along bedding planes.		3		Ē	
3 1 1 1 1 1 1 1 1 1 1 1 1 1			i	3					E-4	
		5	5	5	Some planes of cross joints are smooth.					
5-			1.	2	(with dark greenish		$\frac{1}{1}$	┤┨┦╸	ŧ.	
		,	(3)	2	mineral - chlorite ?)				F	
6		1		5					E-8	
				(3)						
				3			N			[
				5			4		Ē	
									8	
9-0-0		× L		(4)	290					
shale		¥ B			Contained the Access of				-9 ·	
30	1	ភា			Generally few cracks ,		V I I			
				-	partially cross joints				E- 30	
Black				. 1	with calcite veins.					
		1	2	2	No weathering					
2-					at 29.0 - 33.5 ^m	- ı	ŋ			
						- 10	N		Ē	
3 30						I.			-3	
4-				<u> </u>	Cores separated	Ì			4	
			2		along cross joints in parts.					
5-		5		5			{		- 5	
		2		3					- 1	ļ
		<u>a</u>	┟──┝		Anny calcite voine				- 6	
	Block with white honde				Nany calcite veins and ornewhat folding.				-	
	2	2	2	2		In	-1 1 1 1		-7	
8-					Partially small solusiom avities along calcites	. U				
	ŧ		3		eins	-			-8	
9-	, i	(3)	3 (Slightly brittle in general.					
		3							9	
	<u>a</u>	μļ	ļ						40	50.8
		1	1	1 (slark	 Index is note 4 2 (substick): 3 (piece): 4 (fragment), 5 grain 					
<u>к</u> и ку ки ки ки ки ки ки ки ки ки ки ки ки ки	ore losa		1	d) ~ 5	-					
Ĺ R	QD	I (b	resh) - 5							
	cuttings						ELECTRIC I	OWER DEVE	LOPMENT	CO., LTD.
1) I					- 44			TOKYO, J		

A 2 HYDROLOGY

1. Catchment Area of the Damsites

In this study, two damsites, i.e. site A and B were proposed for investigation. Catchment areas of both sites were measured with the available topographical maps (scale: 1/250,000, "Chiangwat Chiang Mai" and "Amphoe Li") published by U.S. Army Map Service, Far East.

Catchment area of Ban Tha Rua G.S. was also measured with the said map.

The catchment areas employed in the study were as follows.

Damsite	A	5,920 km ²
Damsite	в :	5,810 km ²
Ban Tha	Rua G.S.:	5,770 km ²

2. Evapotranspiration

Evapotranspiration was calculated by the following two methods.

(1) Thernthwaite Method

$$E_{PT} = 0.533 \text{ Do } \left(\frac{10tj}{J}\right)^{a}$$

where

$$a = 6.75 \times 10^{-7} J^3 - 7.71 \times 10^{-5} J^2 + 1.79 \times 10^{-2} J + 0.49$$

 $= \sum_{i=1}^{12} \frac{1.514}{5}$

EpT = Monthly average of daily evapotranspiration
 [mm/day]

Do = Daytime ratio i.e. daily daytime/12 hrs

t = Monthly average temperature [°C]

j = Month (1 - 12)

J = Indicator of Month

(2) Blaney and Criddle Method

 $E_{PT} = KCt$

where

E_{PT} = Monthly average evaporation [inch/month]

C = Ratio of monthly daytime to annual daytime

t = Monthly average temperature [°F]

K = Coefficient corresponding to kind of flora

When units are converted to metric system, the equation becomes:

 $E_{PT} = K \cdot C \cdot (45.72^{t} + 812.8)$

In these equations, daytime ratios Do and C were obtained by the following way.

Do; based on the table below, the value at latitude 18° North was interporated.

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C; given by the following figure.

Coefficient for flora (K) is 0.7 corresponding to deciduous forest in semi-dry region(1).

References

Hideaki Nakano, "Forestry Hydrology" p.p.95 - 120, 1980.
 3rd ed. Kyo-ritsu Press.

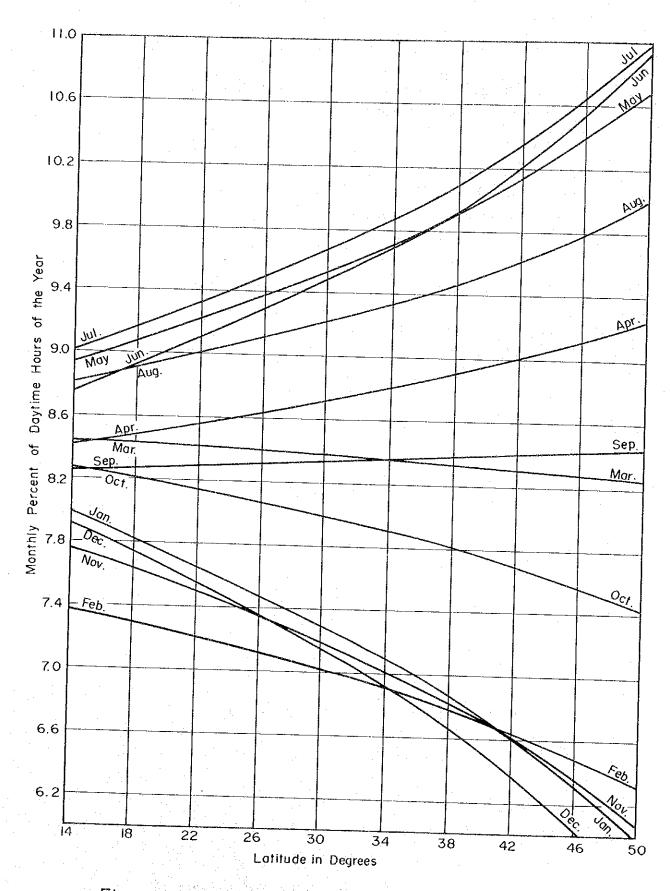


Fig. 2.1 Percent of Annual Sunshine Hours Occurring During the Indicated Month

								·					(Unit:	it: 12	hr/day)
Lat. N. Mon.	10	18*	20	24	26	28	30	32	34	36	38	40	42	4 4	46
JAN	0.965	0.929	0.920	0.899	0.889	0.878	0.867	0.855	0.843	0.830	0.817	0.802	0.787	0.770	0.752
FEB (28)	0.982	0.961	0.956	0.941	0.935	0.929	0.922	0.915	0.908	006*0	0.893	0.884	0.875	0.865	0.855
FEB (29)	0.982	0.961	0.956	0.942	0.936	0.930	0.923	0.916	606.0	0.902	0.894	0.885	0.877	0.867	0.857
MAR	1.003	1.001	1.000	0.997	9.66 0	0.996	0.995	0.994	0.993	0.992	166.0	066.0	0.989	0.988	0.986
APR	1.026	1.044	1.048	1.055	1.060	1.065	1.070	1.076	1.081	1.087	1.093	1.100	1.107	1.115	1.123
MAY	1.045	1.079	1.087	1.104	1.114	1.123	1.134	1.144	1.156	1.167	1.180	1.193	1.208	1.223	2
JUN	1.055	1.096	1.106	1.129	1.141	1.153	1.166	1.180	1.194	1.209	1.225	1.242	1.261	1.280	•
JUL	1.051	1.088	1.097	1.118	1.129	1.140	1.152	1.164	1.177	1.191	1.206	1.221	1.237	•	· · •
AUG	1.034	1.057	1.063	1.077	1.084	1.091	1.098	1.106	1.114	1.123	1.132	1.141	•	.16	
SEP	1.012	1.017	1.018	1.022	1.024	1.025	1.027	1.029	1.031	1.033	1.035	1.037	6		
OCT	066.0	0.975	0.971	0.964	096.0	0.956	0.952	0.947	0.942	0.938	0.932	0.927	0.921	0.915	606-0
NOV	0.970	0.937	0.929	0.913	0.904	0.895	0.885	0.875	0.865	0.854	0.842	0.830	0.817	0.803	0.787
DEC	0.960	616.0	606-0	0.887	0.875	0.863	0.850	0.838	0.824	0.809	0.794	0.778	0.760	0.742	107.0

Note: *; Lat. 18°N. was interporated

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3. Sedimentation

3.1 Geology in the project area

The project area stretches from North to South with distance of 160 km while from West to East with 30 to 50 km width, covering catchment of 6,000 km². In the area, rugged topography in youthfulage is widely seen.

The area is mainly composed of sedimentary rock of Paleozoic and Mesozoic age, and granite of Mesozoic age. The ground is covered in most area by laterite which is generally formed by weathering in humid and high temperature region.

3.2 Sediment

Due to the laterite covering the ground, eroded and flowing material in the river is very fine. In other words, the river flow contains suspended load. On the other hand, since the river gradient is rather mild and river flow is relatively slow, bed material would not be very involved in the flow. Measurement of suspended load has been conducted at three gaging stations along the river. But one gaging station was omitted because it measures on a tributary. Instead, a measurement on the Moei river was taken into account.

(1) Density of sediment deposit

The following equation gives an average density of sediment deposit after t years.

Wav. =
$$W_1 + 0.434 \text{ K} \left[\frac{t}{t-1} (1nt - 1) \right]$$

where

Wav. = Average density of sediment deposit after t years.

 W_1 = Initial density of sediment deposit shown in the table below.

ref.(1)

K = Coefficient

t = Years

	+		+	(1	Jnit	: 1b/ft ³)
Reservoir Operation	(>(Sand).05 mm)		Silt 005 to 05 mm)	(0	Clay .005 mm)
	W1	K	W1	K	W1	K
Sediment always sub- merged or nearly submerged	93	0	65	5.7	30	16.0
Normally a moderate reservoir drawdown	93	0	74	2.7	46	10.7
Normally a consider- able reservoir drawdown	93	0	79	1.0	60	6.0
Reservoir normally emply	93	0	82	0.0	78	0.0

Table 3.1 Initial Density and Coefficient

For a hundred year sedimentation, the following densities were derived

Table	3.2	Average	Density	after	100	years	
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		(U1	iit: gr/cm ³)
Reservoir Operation	Sand	Silt	C1ay
	W100	W100	W100
Sediment always submerged or nearly submerged	1.490	1.185	0.886
Normally a moderate reservoir drawdown	1.490	1,254	1.008
Normally a considerable reservoir drawdown	1.490	1.291	1.113
Reservoir normally empty	1.490	1.313	1.249

In this study stage, no information is available for composition of sediment deposit in Nam Yuam reservoir. Therefore, an average figure of the said densities could be employed, i.e. 1.30 gr/cm^3 .

(2) Estimation of sediment

Using the average density derived above, the suspended load measured in weight at gaging stations was converted to load in volume. At the same time the amount of load was expressed by form of specific discharge.

In addition, bed load was considered, referring other report. The report of Lower Quae Yai Environmental and Ecological Invistigation mentiones 10% of bed load against suspended load in terms of volume, while the Feasibility Study Report of Upper Quae Yai mentiones 20% thereof. In this report, thus, it is decided to consider 20% of bed load against suspended load in terms of volume.

Consequently, following sediments are estimated at each gaging stations.

Sop Han	$(C.A. = 2,496 \text{ km}^2)$	136.2 m ³ /km ² /yr
Ban Tha Rua	$(C.A. = 5,770 \text{ km}^2)$	109.6 m ³ /km ² /yr
Tha Song Yang	$(C.A. = 8,360 \text{ km}^2)$	196.9 m ³ /km ² /yr

Finally the specific sediment discharge of 140 $m^3/km^2/yr$ which is conservatively obtained by enlarging the figure at Sop Han has been adopted in this study. Therefore, the total amount of sediment deposit is estimated to be 82.9x10⁶ m^3

 $140 \ge 5,920 \ge 100 = 82.9 \ge 10^6$ This sediment occupies only 18.6% of total storage volume of the reservoir. Assuming horizontal surface of deposit, sediment level becomes EL.129.0 m.

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4. Generation of Runoff Data by Tank Model

4.1 Purpose

Generation of runoff data of Yuam river aimed to examine reasonability of the runoff data which was actually observed and employed as a basic information in energy computation.

4.2 Observed data utilized in the generation

The observed daily runoff data collected at Ban Tha Rua was available for eleven years from 1970 to 1980, while daily rainfall was observed at Mae Saviang for thirty-one years from 1950 to 1980 and other four observatories, i.e. Ban Tha Rua, Chom Chaeng, Sop Han and Mae La Luang for fourteen years or so.

In the generating process, however, those four rainfall observatories were not taken into consideration because the observing periods are much shorter than of Mae Saviang, and most of the periods are overlapping with the period of runoff data at Ban Tha Rua, thus no point to be used in generating the runoff of Yuam river. Consequently runoff data was generated on the basis of the thirty-one year daily rainfall at Mae Sariang which overlaps for the full period of eleven years of daily runoff at Ban Tha Rua and, in addition, extends twenty years more to the past till 1950.

The generating model, i.e. the tank model, was first adjusted during the overlapping period and then generated the runoff of the river taking the daily rainfall as input.

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4.3 Tank model

1) General

Tank model is one method of runoff analysis, being widely adopted in the world. Tank model applicable to both flood and daily runoff analysis can estimate runoff of a river by taking rainfall as input. Basically the model is composed of several tanks combined each other in series or parallel, each tank of which has outlets in the bottom or side corresponding to seepage to the ground or discharge to a river. The conceptional illustration is given Fig. 4.1(a).

Function of tank model is explained as follows, taking simplest component (one tank with two outlets in the bottom and side) as an example. See Fig. 4.1(b).

In the model, section of all tanks is 1, thus storage volume can be simply expressed by height of the water stored in the tank. All the inputs and outputs are considered in time series and expressed by unit of millimeter (mm).

Rainfall	${x_n}$
Storage	$\{X_n\}$
Discharge	$\{y_n\}$
Seepage	$\{z_n\}$

 $n = 1, 2, 3, \cdots$

The outlets equipped in the side and bottom have respective coefficient α and β adjusting the discharge or seepage rate. The side outlet is usually equipped above the bottom with certain distance H which also enables to adjust the discharge and seepage rate.

The output from the tank can be expressed as follows.

 $y_n = \begin{cases} 0 \\ \alpha(Xn - H) \end{cases}$

if O<Xn<H

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if H≺Xn
```

```
z_n = \beta X n
```

Considering the process in time series, time n and n+1, as shown Fig. 4.1(c), outputs are then expressed in the following way.

```
time n;
```

 $y_n = \alpha (Xn - H)$, since Xn>H in the figure $z_n = \beta Xn$

then

 $X'n = Xn - y_n - z_n$

time n+l;

```
\mathbf{x}_{n+1} = \mathbf{x'}_n + \mathbf{x}_{n+1}
```

```
y_{n+1} = \alpha(X_{n+1} - H)
```

```
z_{n+1} = \beta X_{n+1}
```

then

$$x'_{n+1} = x_{n+1} - y_{n+1} - z_{n+1}$$

This process is repeated afterwards as time proceeds.

In ordinary tank model shown in Fig. 4.1(a), the said tanks are combined each other vertically in series. In such case, discharge to a river is summation of all the output from the side outlets, while output from the bottom outlet is regarded as seepage to the ground, which is trapped in the lower tank.

Structure of the ordinary tank model is also understood on the analogy of real structure of the ground. Fig. 4.2 shows the correspondence between them.

Rainfall falls into the top tank. Lower tanks receive the water coming out of the upper tank through the bottom outlet. On the other hand, a part of water stored in each tank is discharged to a river through the side outlet. This process is seemed resemble to the real structure of the ground shown in left-hand side, figure (a).

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Rainfall falling on the surface of the ground is partially discharged immediately, while the rest seepages to the ground. Outflow from the side outlet of each tank shown in the figure (b) can be considered discharge from each permeable layer of the ground as shown in the figure (a). On the other hand outflow from the bottom outlet of each tank can be thought infiltration from upper permeable layer to lower permeable layer. In the model, outlets of lower tanks are made narrower, i.e. smaller coefficient \triangleleft or β , because discharge rates in real situation are smaller in lower layers.

This model can well reflect variety of discharge pattern resulted from rainfall pattern. For example, continuous rainfall could cause floods, even if the rainfall is less intensified, while highly intensified rainfall could cause floods even if the whole amount of precipitation is small. In this tank model, if the rainfall continues at a rate exceeding the infiltration rate of the bottom outlet of the top tank, storage in the top tank increases gradually and it causes a large amount of discharge from the top tank where side outlet is wide and enables to release water quickly. If the rainfall occured in short period with high intensity, it also causes a large amount of discharge because storage in the top tank increases rapidly and most of the water trapped in the tank is released from the side outlet.

Generally speaking, if the tank model is composed of three or four tanks combined vertically in series, the top tank is considered corresponding to surface runoff, the second tank is to be subsurface flow and the third and fourth tanks are to be base flow. The tank model where each tank has differet discharge rate, \triangleleft and β , is, thus, considered to represent the actual physical characteristics of the phenomenon.

Problem of the tank model is to decide the parameters of the model. As seen in the previous figures, the model

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consists of several tanks and each tank has parameters of outflow rate α and β and the distance of the side outlet from the bottom. These parameters have to be decided by trial and error, namely taking rainfall data as input, the parameters are so adjusted that the model as a whole can generate runoff well-matched to the observed runoff.

2) Tank model considered in the study

Tank model has variety in its structure, reflecting basin condition. Following three types were considered in this study.

- (i) Ordinary series combination of four tanks(ab. ordinary model, see Fig. 4.3(a))
- (ii) Ordinary model equipped with soil moisture function in the top tank(ab. soil moisture model, see Fig. 4.3(b))
- (iii) Parallel combination of four soil moisture models
 (ab. 4 x 4 model, see Fig. 4.3(c))

It is generally said that the ordinary model is suitable for such region that climate is mild and there is moderate rainfall throughout a year rendering the ground always wet. On the other hand, the soil moisture model is said appropriate for such region where long dry season exists and thus the ground becomes dry for certain period in a year. If the dry condition of climate is much severer, the 4x4 model is considered suitable.

All the simulation by these three models had been conducted by computer and the soil moisture model was eventually employed in analysis in this study.

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3) Soil moisture model

Fig. 4.4 shows detail of the soil moisture function equipped in the top tank.

The soil moisture function consists of two components, the primary and the secondary, which have saturation capacity of S1 and S2, respecttively Symbols appearing in the figure have the following meanings.

S1: Saturation Capacity of the primary soil moisture function

S2: Saturation Capacity of the secondary soil moisture function

- XP: Actual Storage in the primary soil moisture function
- XS: Actual Storage in the secondary soil moisture function

XF: Free Water stored above the primary soil moisture function, learing the primary function full.

XA = XP + XF

T1 = K1(1 -
$$\frac{XP}{S1}$$
)
T2 = K2($\frac{XP}{S1} - \frac{XS}{S2}$)

Rainfall is accumulated into XA. If XA is less than S1, whole XA is considered XP. If XA is greater than S1, XP is saturated (XP=S1) and the rest is considered free water (XF=XA-S1). Thus, seepage and discharge from the top tank is caused by the free water XF.

In additrion to the ordinary process of the tank model, this model allows water to move between S1 and S2, and between the top tank and the second tank. It is shown in Fig. 4.4 (3). If S1 portion is not saturated and there is free water left in the second tank, water is supplyed to the S1 portion from the second tank. This water movement is expressed by the equation below.

$$T1 = K1(1 - \frac{XP}{S1})$$

where Kl is a coefficient.

As seen in the equation, water moves only from the second tank to the SI portion in proportion to XP/SI which is relative humidity of the SI portion.

On the other hand, water moves between S1 and S2 portions in a manner expressed by the following equation;

$$T2 = K2(\frac{XP}{S1} - \frac{XS}{S2})$$

If T2 is positive, water moves from the second to the top tank, on the contrary if T2 is negative, water moves from the top to the second tank. This means, in other words, water moves from dry portion to wet portion in proportion to the difference of relative humidities between the two portions.

As described above, the soil moisture function can be controlled by the four parameters, i.e. Sl, S2, Kl, K2.

Fig. 4.5 shows the soil moisture model with the parameters which were finally employed in the analysis. As seen in the figure, there are totally eighteen (18) parameters to be decided. These parameters were decided by trial and error. That is, under certain value of parameters given, runoff was generated by taking Mae Saviang rainfall as input, and hydrograph was then synthesized. Comparing these synthetic hydrograph with the observed hydrograph at Ban Tha Rua, parameters had been adjusted little by little so as to make the synthetic hydrograph more fit to observed.

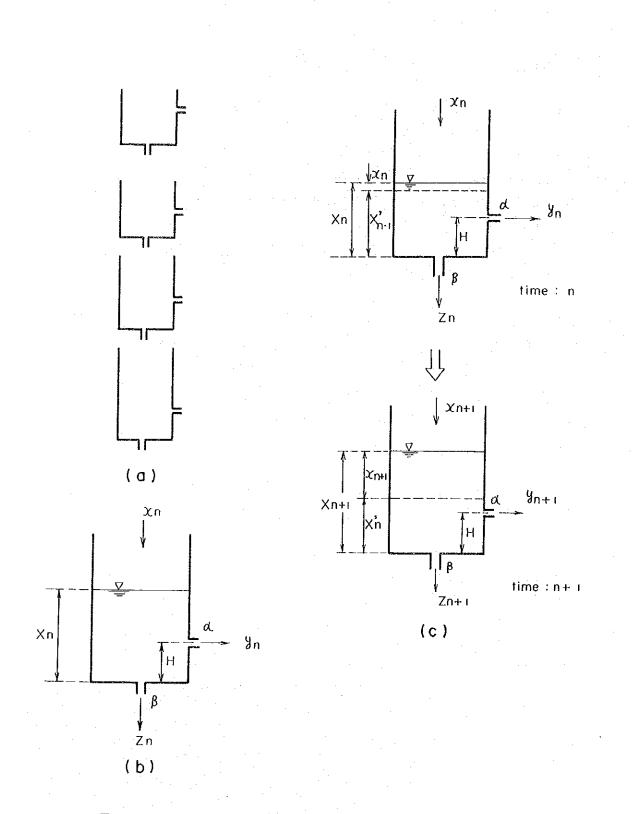
Fig. 4.6 gives the result, where solid line in the observed hydrograph and dot line is the synthetic one.

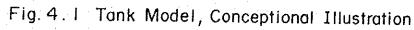
Based on the synthetic hydrograph, periodic feature of Yuam river was studyed by spectlum analysis.

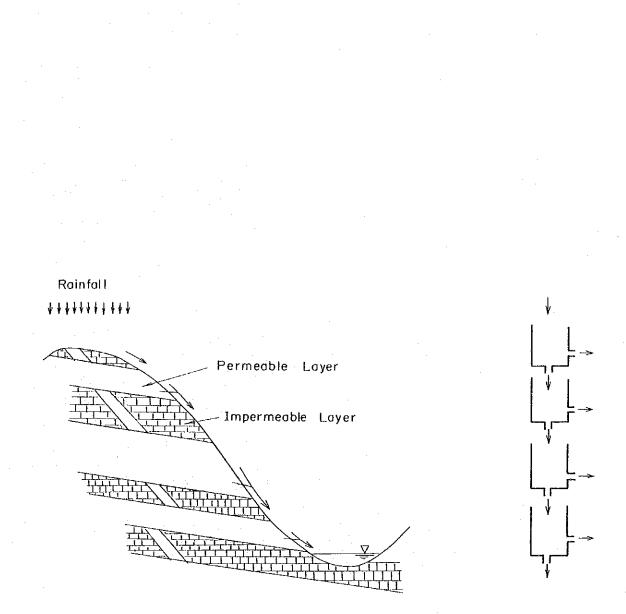
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(a)

(b)

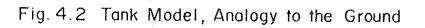
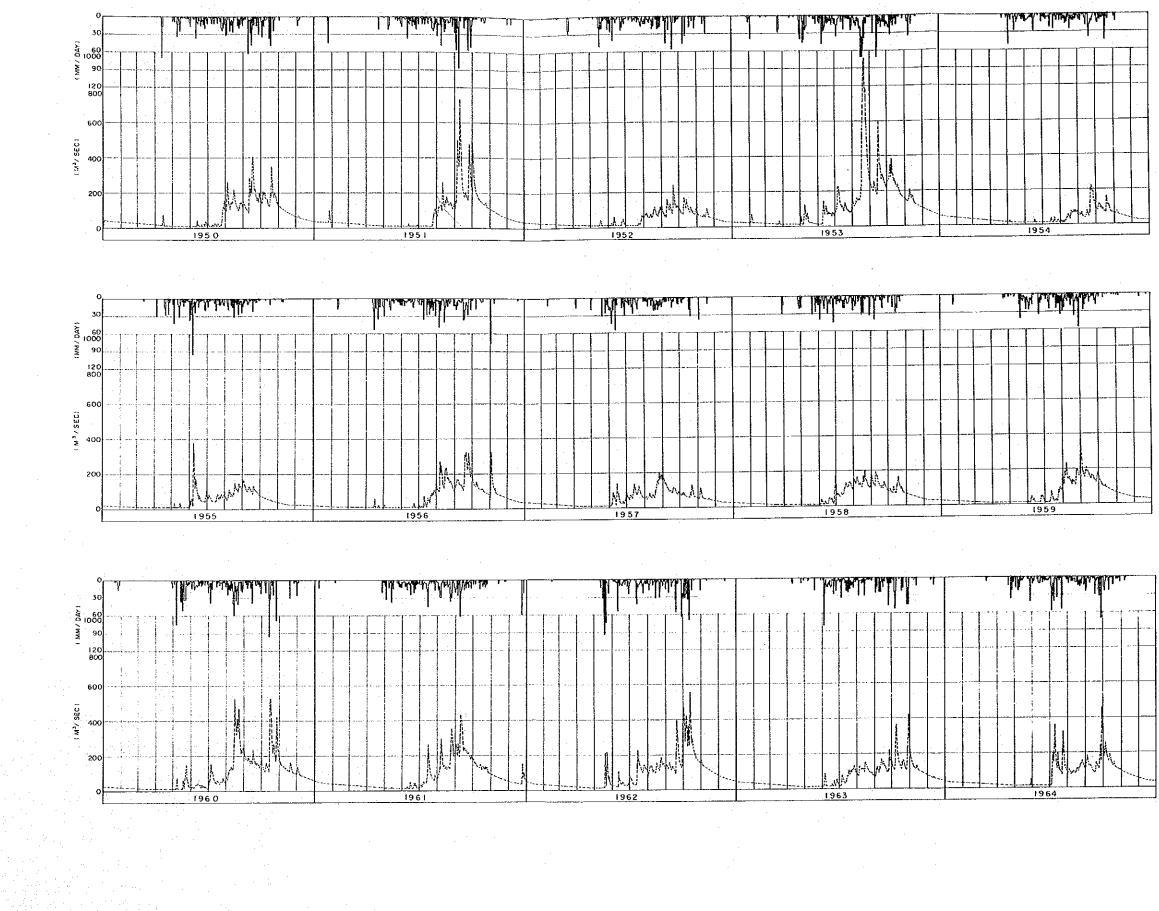


Fig. 4-3 Estimated and Observed Runoff of Yuam River



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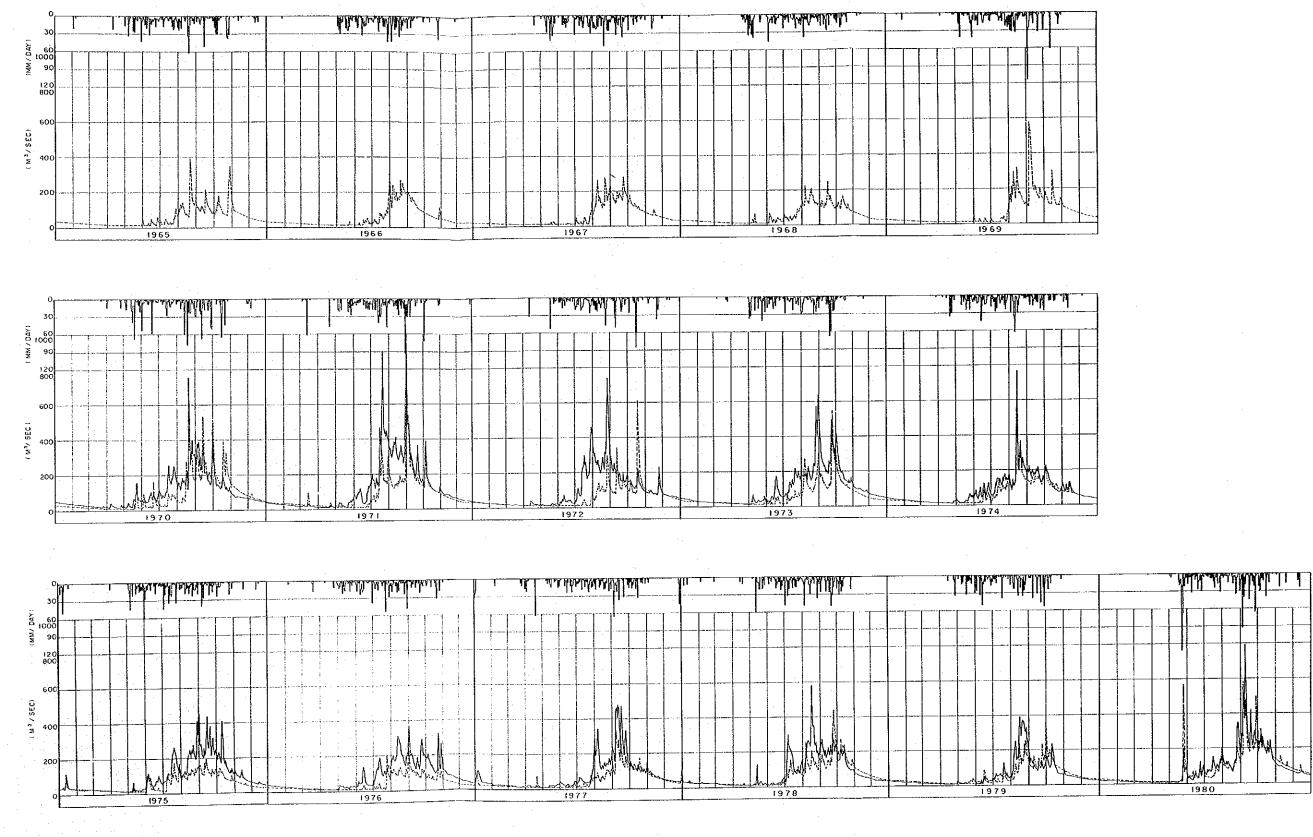
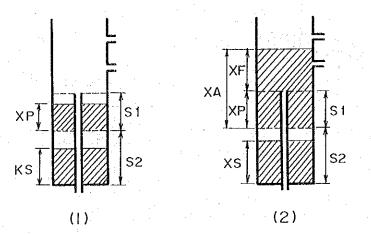
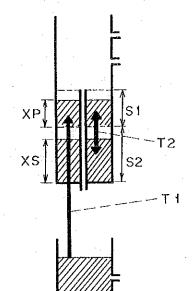


Fig. 4-3 Estimated and Observed Runoff of Yuam River (cont'd.)



- St: Saturation Capacity of the primary soil moisture function
- S2: Saturation Capacity of the secondary soil moisture function
- XP: Actual Storage in the primary soil moisture function

XS : Actual Storage in the secondary soil moisture function



- T1 = K1 $(1 \frac{XP}{S1})$ T2 = K2 $(\frac{XP}{S1} - \frac{XS}{S2})$
 - (3)
- XF : Free Water stored abone the primary soil moisture function, leaving the primary function full.

XA = XP + XF

Fig. 4.4 Detail of Soil Moisture Function

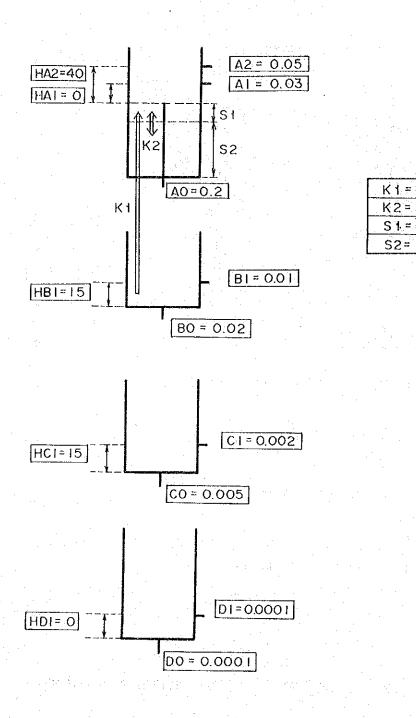


Fig. 4.5 Tank Model Eventually Employed in the Study