CROP PRODUCTION WITH PROJECT (AVERAGE CROPPING INTENSITY) TABLE G3-16

|   | •   |        | Total    |            |        | Bayongan | an         |       | Capayas  | -          |
|---|---|--------|----------|------------|--------|----------|------------|-------|----------|------------|
|   | Crop                                      | Area   | Yield    | Production | Area   | Yield    | Production | Area  | Yield    | Production |
| - | Rice Field, Irrigated                     | (ha)   | (ton/ha) | (ton)      | (ha) ( | ton/ha)  | (ton)      | (ha)  | (ton/ha) | (ton)      |
|   | (1) Rice, wet season                      | 4,420  | 4.2      | 18,564     | 3,450  | 4.2      | 14,490     | 970   | 4.2      | 4,074      |
|   | (2) Rice, dry season                      | 3,300  | 4.5      | 14,850     | 2,580  | 4.5      | 11,610     | 720   | 4.5      | 3,240      |
|   | Sub-total                                 | 7,720  | -        | 33,414     | 6,030  |          | 26,100     | 1,690 |          | 7,314      |
|   | (3) Beans                                 | 420    | 1.0      | 420        | 330    | 1.0      | 330        | 06    | I.0      | 06         |
|   | (4) Peanut                                | 420    | 1.7      | 714        | 330    | 1.7      | 561        | 06    | 1.7      | 153        |
|   | (5) Feed grains                           | 420    | 2.7      | 1,134      | 330    | 2.7      | 891        | 06    | 2.7      | 243        |
|   | (6) Fruit crops/vegetables                | 420    | 8.9      | 3,738      | 330    | 8<br>9   | 2,937      | 06    | 8.9      | 801        |
|   | <u>Sub-total</u><br>Upland Field, Rainfed | 1,680  |          | 6,006      | 1,320  |          | 4,719      | 360   |          | 1,287      |
|   | (1) Cassava                               | 720    | 14.2     | 10,224     | 590    | 14.2     | 8,378      | 130   | 14.2     | 1,846      |
|   | (2) Sweet potato                          | 480    | 10.8     | 5,184      | 390    | 10.8     | 4,212      | 06    | 10.8     | 972        |
|   | Sub-total                                 | 1,200  |          | 15,408     | 980    |          | 12,590     | 220   |          | 2,818      |
|   | Total                                     | 10,600 |          | 54,828     | 8,330  |          | 43,409     | 2,270 |          | 11,419     |

| Item                           | Total  | San Miguel | Trinidad | <u>Ubay</u> |
|--------------------------------|--------|------------|----------|-------------|
| l. No. of Barangay             | 22     | 5          | 6        | 11          |
| 2. 1980 Population             | 10,870 | 2,878      | 3,215    | 5,777       |
| 3. 1980 No. of Household       | 2,117  | 540        | 496      | 1,081       |
| 4. 1980 No. of farm            | 1,826  | 511        | 410      | 905         |
| 5. 1987 Population (1.6%/year) | 12,086 | 3,200      | 2,463    | 6,423       |
| 6. 2000 Population (0.9%/year) | 13,573 | 3,594      | 2,766    | 7,213       |
| 7. 2000 No. of farm            | 2,280  | 638        | 512      | 1,130       |

TABLE G3-17PROJECTED POPULATION AND NUMBER OF FARM<br/>IN THE PROJECT AREA (2000)

Note: (1) The 1987 and 2000 population were projected on the base of population growth rates indicated in the parenthesis.

> (2) The number of farm households in 2000 was projected on the base of population increase rate from 1980 to 2000.

FARM OPERATION METHOD OF RICE CULTIVATION TABLE G3-18

|     | 8  | ft<br>aal<br>rt)                      |            | ?ower<br>Tiller<br>(Trailer)          |                 | r)<br>t)                                |             |
|-----|--|---------------------------------------|------------|---------------------------------------|-----------------|---|-------------|
| • • | Hauling  | Draft<br>- Animal<br>(Cart)           | -          | Power<br>- Tiller<br>(Traile          |                 | Draft<br>- Animal<br>(Cart)             | -<br>-<br>- |
| •   | Drying   | Sunshine<br>& Dryer                   |            | Sunshine<br>- & Dryer -               |                 | Sunshine                                |             |
|     | Threshing  | Power<br>- Thresher                   |            | Power<br>Thresher                     |                 | Pedal<br>- Thresher                     | •           |
| -   | Harvesting   | Manpower<br>(Sickle)                  | . •        | Manpower<br>(Sickle)                  |                 | Manpower<br>- (Sickle)                  | -           |
|     | Weeding  | Manpower<br>(Rotary<br>Weeder)        |            | Manpower<br>(Rotary<br>Weeder)        |                 | Manpower<br>(Rotary<br>Weeder)          |             |
|     | Spraying   | Manpower<br>(Hand<br>Sprayer)         |            | Manpower<br>(Hand<br>Sprayer)         |                 | Manpower<br>(Hand<br>Sprayer)           |             |
|     | Trans-<br><u>planting</u><br>Animal  | Manpower                              |            | Manpower<br>                          |                 | Manpower                                | -           |
|     | Harrowing Trans-<br>wing <u>&amp; Leveling</u> <u>planti</u><br>4-wheel Tractor + Draft Animal | Draft Animal<br>(Harrow &<br>Leveler) | Tiller     | Power Tiller<br>(Harrow &<br>Leveler) | Power           | Draft Animal<br>(Harrow & -<br>Leveler) | i           |
|     | <u>Plowing</u><br>1. 4-wheel   | 4-wheel.<br>Tractor —<br>(Rotary)     | 2. Power T | Power<br>Tiller -<br>(Plow)           | 3. Animal Power | Draft<br>Animal<br>(Plow)               |             |

The farm operation method of the direct seeded rice is the same as the above method except for the operation of seeding No. of passing of plowing, first harrowing and final harrowing are indicated in Table 1. Note: (1) 5

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CAPACITY AND EFFICIENCY OF MACHINERIES/ANIMAL BY OPERATION

TABLE G3-19 .

| Days<br>Per ha<br>(12)=(9)/(11)<br>(day/ha)          | 8<br>18<br>28<br>2<br>28  | 2.7                                     | 1.3  | 3.8   | 0-9  | 1.0                          | 4.2                          | 0.9                 |                                |
|--|---|---|--|---|--|------------------------------|------------------------------|---------------------|--------------------------------|
| Ope.<br>Hours<br>Per day<br>(11)<br>(hr/day)         | ου ου ου  | ،<br>٥٥                                 | 80   | 80  | 80   | 2                            | 7                            | 16                  |                                |
| Hours<br>per ha<br>(10)=(9)x(8)<br>(ha/hr)           | 66.7<br>14.3<br>3.7   | 21.2                                    | 10.6   | 30.0  | 6 <b>.</b> 8   | 6.7                          | 29.4                         | 14.0                | •<br>•<br>• •                  |
| Ope.<br>Times<br>(11 (11 )                           | ret ped red   | ~                                       | . 2  | 4   | 7  |                              | 1                            | н                   | •<br>•<br>•                    |
| Hours<br>per ha<br>(8)<br>(ha/hr)                    | 66.7<br>14.3<br>3.7   | 10.6                                    | 5.3  | 7.5   | 3.4  | 6.7                          | 43.5                         | 14.0                | ·                              |
| Actual<br>Ope.<br>Capacity<br>(7)*(5)x(6)<br>(ha/hr) | 0.015<br>0.070<br>0.273   | 0.094                                   | 0.190  | 0.134   | 0.294  | 0.150                        | 0,034<br>(0,14 ton)          | 0.071               | 0.11 ton                       |
| Ope.<br>Efficiency<br>(5)<br>(2)                     | 70<br>85<br>85  | 20                                      | 80   | 70  | 80   | 75                           | . 75                         | 80                  | 70                             |
| Field<br>Ope.<br>Capacity<br>(5)=(3)x(4)<br>(ha/hr)  | 0.022<br>0.087<br>0.321   | 0.134                                   | 0.238  | 0.192   | 0.367  | 0.200<br>(0.8 ton)           | 0.046<br>(0.19 ton)          | 0.089               | 0.16 con                       |
| Field<br>Efficiency $\frac{1}{(4)}$                  | 84<br>84<br>78  | 80                                      | 82   | 80  | 82   | 32                           | 80                           | 80                  | 80                             |
| Theoretic<br>Ope.<br>Capacity<br>(3)<br>(ha/hr)      | 0.026<br>0.103<br>0.411   | 0.168                                   | 0.290  | 0.240   | 0.448  | 0.244<br>(1.0 ton)           | 0.058<br>(0.24 ton)          | 0 111<br>(0.50 ton) | 0.2 ton                        |
| Ope<br>Speed (2)<br>(km/hr)                          | 2 6 3 2 | 2.4                                     | 2.9  | 2.4   | 3.2  | ı                            | ι                            | ı                   | 5.5                            |
| Ope.<br>Width<br>(1)<br>(m)                          | 0.12<br>0.24<br>1.58  | 0.7                                     | 1.0  | 1.0   | 1.4  | T.                           | 1                            | Ι.                  | 1                              |
| Operation/Machinery & Animal                         | <ol> <li>Plowing, Carabao W/Plow</li> <li>Plowing, Power Tiller W/Plow</li> <li>Plowing, 4-wheel Tractor</li> <li>W/Rotary</li> </ol>   | 4. First Harrowing, Carabao<br>W/Harrow | 5. First Harrowing, Power Tiller<br>N/Harrow | 6. Final Harrowing, Carabao<br>W/Harrow/Leveler | 7. Final Harrowing, Power<br>Tiller W/Harrow/Leveler | 8. Threshing, Power Thresher | 9. Threshing, Fedal Thresher | 10. Drying, Drier   | 11. Hauling, Carabao with Cart |

Note:

1/... Such losses in the fields as turning of machineries, adjustment of machineries, etc. are deducted

from theoretical capacity. 2/... Such losses happening outside the fields as transportation of machineries between garage and fields. inspection of machineries just before operation (min. 10 minutes), fixing and removal of machineries with putting lubricant oils (min. 30 minutes) etc. from the field operation capacity.

|       |                 |                        |                        | ·                              |                            | ·                            |                           |                              | · · · .               |                         |                       |
|-------|-----------------|------------------------|------------------------|--------------------------------|----------------------------|------------------------------|---------------------------|------------------------------|-----------------------|-------------------------|-----------------------|
|       |                 | <b>F</b> 1             | TABLE G3-20            | 3-20                           | FARM MACH                  | FARM MACHINERY COST          | [-4                       |                              |                       |                         |                       |
|       | · .<br>·        |                        |                        |                                |                            |                              |                           |                              |                       |                         |                       |
| :     |                 | (1)                    | (2)                    | (3)<br>Depre-                  | (4)                        | (5)<br>Other                 | (9)                       | (2)                          | (8)<br>Total          | (6)                     | (10)<br>Fixed         |
| Mé    | Machinery       | Aqui-<br>sition<br>(¥) | Life<br>Span<br>(year) | ciation<br>Cost 1/<br>(₹/year) | Repair<br>Cost<br>(P/year) | Fixed<br>Cost 2/<br>(P/year) | Total<br>Cost<br>(P/year) | Coverage<br>per Unit<br>(ha) | Cost per<br>ha<br>(P) | Area<br>Coverage<br>(%) | Cost<br>per ha<br>(₱) |
| 4-wh  | 4-wheel tractor | 215,000                | . 10                   | 19,350                         | 17,200<br>(8%)             | 2,150                        | 38,700                    | 38,700 l,200 hr/<br>year     | 32/hr                 | 20                      | 24                    |
| Power | Power tiller    | 32,060                 | Ń                      | 5,771                          | 2,565<br>(8%)              | 321                          | 8,657                     | 9.0x1.64/                    | 601                   | 45                      | 270                   |
| Powe  | Power thresher  | 23,125 <u>3</u> /      | 8                      | 2,602                          | 694<br>(3%)                | 231                          | 3,527                     | 30×1.64/                     | 24                    | 75                      | 184                   |
| Peda. | Pedal thresher  | . 650                  | Ŷ                      | 98                             | I                          | 7                            | 105                       | 5.0x1.64/                    | 7                     | 25                      | 7                     |
| Dryer | r               | 16,000                 | œ                      | 1,800                          | 800<br>(5%)                | 160                          | 2,760                     | 2,760 30.0x1.6 <u>4</u> /    | 58                    | 60                      | 35                    |
| Ĥ     | Total           |                        |                        |                                | 1811                       |                              |                           |                              |                       |                         | 515                   |

Note:

 $\frac{1}{2}/ \dots \text{ Computed as (1) x 0.9/(2)}$   $\frac{2}{2}/ \dots \text{ Computed as (1) x 0.01}$   $\frac{3}{2}/ \dots \text{ Price without engine because the engine of hand tractor can be used for thresher}$   $\frac{4}{2}/ \dots \text{ Cropping intensity of rice}$ 

|                     | (7) (8)<br>Area Variable<br>Coverage Cost per ha<br>(7) (P) | 20 24  | 45 77  | 45 30                                      | 45 19  | 75 40                           | 60                  | 383   |
|---------------------|---|--|--|--|--|---------------------------------|---------------------|-------|
|                     | (6)=(5)xl.3<br>Cost Inclu-<br>sive of Oil<br>(P)            | 117.4  | 170.7  | 67.5                                       | 42.8   | 53.2                            | 116.1<br>204.8      |       |
|                     | (5)<br>Cost of<br>Fuel<br>(P)                               | 90.3   | 131.1  | 51.9                                       | 32.9   | 6.04                            | 89.3<br>57.5        |       |
| Y COST              | (4)<br>Unit Cost<br>(P/lit.)                                | 6 • 1  | 6 . I  | 6.1  | 6 • 1<br>6                                       | 6.1                             | 8.5<br>7.5          |       |
| FARM MACHINERY COST | (3)<br>Fuel<br>(lit.)                                       | 14.8   | 21.5   | S. S                                       | 5 . 4  | 6.7                             | G+0 10.5<br>K 21.0  |       |
| FARM                | (2)<br>Fuel<br>Consumption<br>(lit./hr)                     | D. 4.0   | D. 1.5   | D. 0.8                                     | D. 0.8   | D. 1.0                          | G+0.75 G<br>K 1.5 K |       |
| TABLE G3-20         | (1)<br>Ope. hours<br>per ha<br>(hr/ha)                      | 3.7  | er 14.3  | r 10.6                                     | wer 6.8  | 6.7                             | 14.0                |       |
|                     | Operation/Machinery   | <ol> <li>Plowing, 4-wheel<br/>tractor</li> </ol> | <ol> <li>Plowing, Power tiller 14.3</li> <li>+ Plow</li> </ol> | 3. 1st harrowing, power<br>tiller + harrow | 4. Final harrowing, power 6.8<br>tiller + harrow | 5. Threshing, power<br>thresher | 6. Drying, Drier    | Total |

Note: D .... Diesel G .... Gasoline K .... Kerosene

# TABLE G3-21

ANIMAL COST

| Operation          | Requirement<br>(day/ha) | Rate<br>(₽/day) | Amount<br><u>(</u> ₽/ha) | Area<br>Coverage<br>(%) | Amount<br>_(₽) |
|--------------------|-------------------------|-----------------|--------------------------|-------------------------|----------------|
| 1. Plowing         | 7.0                     | 15              | 105                      | 35                      | 37             |
| 2. First harrowing | 2.4                     | 15              | 36                       | 55                      | 20             |
| 3. Final harrowing | 4.8                     | 15              | 72                       | 55                      | 40             |
| 4. Hauling         | 4.5                     | 15              | 68                       | 100                     | 68             |
| Total              | 18.7                    |                 |                          |                         | 165            |

Note: Commodity and distance for hauling work;

| Quantity<br>(ton) | Distance<br>(km)                       |
|-------------------|--|
| 2.0               | 2 km                                   |
| 0.5               | $4 \text{ km} = 2 \text{ km} \times 2$ |
| 8.5               | 1 km                                   |
| 4.1               | $4 \text{ km} = 2 \text{ km} \times 2$ |
| 2.0               | 1 km = 1 km x 2                        |
|                   | (ton)<br>2.0<br>0.5<br>8.5<br>4.1      |

|                                       | man-day/ha)                           | , Future 2/          | Machinery  | ۲<br>د          | 0.1       | 1                   | <u>5</u> |                     | ł                        | 0 °        | 6°0   | 4.0  |             | 0.2                             |      | 0.2       | -<br>-<br>-    | 0.1                  | 0.1             | 0.2       | <b>2•</b> 0     | •                      | l                                     |               | 0 1   | ۰.<br>۲ | ץ ער<br>אין ראיי<br>אין ראיי | )<br>•<br>•       |             | ند<br>ح       | י<br>כ<br>כ                | )<br> <br>    | ;            | Draft animal                                 |
|---------------------------------------|---------------------------------------|----------------------|------------|-----------------|-----------|---------------------|----------|---------------------|--------------------------|------------|---|------|-------------|---------------------------------|------|-----------|----------------|----------------------|-----------------|-----------|-----------------|------------------------|---------------------------------------|---------------|-------|---------|------------------------------|-------------------|-------------|---------------|----------------------------|---------------|--------------|--|
|                                       | (Unit: D                              | W/Project, Future    | Man-day    | C               | Λι<br>5 - |                     | 2-0      |                     |                          |            | (2x) 1.5  | 7.0  |             | 7.2                             | 20.0 | 27.2      | -<br>          | 1.2                  |                 | 2.4       | n, i            | 12.U                   | 0                                     | C<br>7        | 2. C  | 0       | 0<br>0<br>0<br>0             |                   | -<br>-<br>- | ¢             | - r-                       | 8 <u>7 7</u>  |              | •  |
|                                       |                                       | Future 1/            | Animal-day | •               | 0.*T      | ۱.                  | 1•0      |                     | 1                        | 1 t        | - 8<br>- 0  | 14.9 |             | 0.5                             | 1    | 0.5       |                | 4.0                  | 4 0<br>• •      | 8         | 2.0             |                        | l                                     |               | 1 7   | 4.2     | 1 0<br>1 1                   | ;                 |             | с<br>т        | ) e                        | 1.1<br>7<br>7 | t<br>•<br>•  | in the parenthesis                           |
|                                       |                                       | W/Project,           | Man-day    | (<br>-          | 7.1       | ດ I<br>••• (        | 7-7      | (                   | <b>D</b> . U             | (TX)0.4    | (7X)2.1<br>(4x)3.8                                    |      |             | 7.5                             | 20.0 | 27.5      |                | ۲.5                  | ы<br>Ч          | 0         | n<br>in (       | 12.0                   | 0,0                                   | C<br>V<br>F   | 5 - C | - C -   |                              |                   |             | ע<br>רי<br>רי | י<br>י<br>י<br>י<br>י      |               | 7 • • • •    | figures                                      |
| · · · · · · · · · · · · · · · · · · · |                                       | W/O Project, Present |            |                 |           |                     |          |                     |                          |            |   |      |             |                                 | •    |           |                |                      |                 |           | · · ·           |                        | · · · · · · · · · · · · · · · · · · · |               |       |         |                              |                   |             | •             |                            |               |              | Mechanization, $3/$ The                      |
|                                       | · · · · · · · · · · · · · · · · · · · |                      | Operation  | 1. Seed-bedding |           | b. Care of Seedings |          | 2. Land Freparation | a. Cleaning/dike Mending | b. Plowing | c. Breaking/Harrowing<br>J pinel nervering/I and ling | •    | 3. Planting | a. Pulling/Deliver of Seedlings | S    | Sub-total | 4. Fertilizing | a. Basal Fertilizers | b. Top-dressing | Sub-total | 5. Pest Control | 6. Cultivation/Weeding | 7. Irrigation/Drainage                | 8. Harvesting |       |         | C. Intesutus/ Manuowang      | 0 Dest Tarresting | л<br>Э<br>Ч |               | D. Sacning/Liling/Delivery | ans           | IU. LOLAL 2/ | Remarks: $1/\ldots$ Draft animal, $2/\ldots$ |

LABOR REQUIREMENT, RICE, TRANSPLANTED

TABLE G3-22

| ABOR REQUIREMENT, RICE DIRECT SEEDED<br>W/O Project, Present W/Project, Future 1/<br>W/O Project, Fresent W/Project, Future 1/<br>Man-day Animal-day<br>Man-day Animal-day<br>(1x)8.4 8.4<br>(1x)3.8 8.2.7 3.8<br>17.9 14.9<br>0.6<br>3.0 0.5<br>3.0 0.6<br>1.5 0.4<br>1.5 0.4<br>1.7 0.5<br>1.1 0.5 | (Unit: man-day/ha) | W/Project, Future <u>2/</u><br>Man-day Machinery |   | 1 |   | 3.0 | (1x)1.8 1.8 1.8 $(2x)1.3$ 1.3 | 5       | 7.0  | 1         | 2.7 0.2 | _ | -2  |            | 3.5 | 10.0 |            |      | 3.0         |      |   |     | 2.7 0.5 | 53.2 8.4(6.4) |
|--|--------------------|--|---|---|---|-----|-------------------------------|---------|------|-----------|---------|---|-----|------------|-----|------|------------|------|-------------|------|---|-----|---------|---------------|
| LABOR REQUIREMENT, RICE DIRECT<br>W/O Project, Present<br>Man-day Animal-day<br>(1   |                    | lect, Future <u>1</u> /<br>iy <u>Animal-day</u>  | 1 | 1 | 1 |     |                               |         | 14.9 | 1         | 0°2     |   | 0.4 | 40         | 2.0 | ł    | <b>I</b> . | 1    | 1.7         | 5.9  | ļ | ۱ - |         |               |
| LABOR CARACTER CARACT   |                    |  |   | 1 |   | 3.0 | (1x)8.4                       | (4x)3.8 | 17.9 | I         | 0.0     |   | 1,5 | 1.5<br>2.0 | 3.5 | 2.0  |            | 16.0 | 3.4<br>12 6 | 32.0 |   | i c | 0.0<br> | 71.9          |
|  |                    | W/O Projec<br>Man-day                            |   |   |   |     |                               |         |      | Seedlings | 80      |   |     |            |     |      |            |      |             |      |   |     |         |               |

TEMINE μ 2 : parentnesis e L L L C с Н rigures 1 De ) N Mechanization, : 4 anlmal, Urarr ::/i Kenarks:

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of powt-harvesting show draft animal labor requirement 1/: With animal power the parenthesis (Unit: man-day/ha) 3/: Two passings of 2/: Only plowing is 5/: The figures in 4/: Including the mechanized by tractor with tractor with requirment Remarks rotary rotary work 2 Machinery 2 5.6(12.6) 1.0 Future 2.0 2.0 0.5 3.0 2.0 ц П 0 1 2.5 ١ ł ١ ł 1 W/Project, Man-day 12.0 6.0 3.0 10.0 3.0 56.6 о. С 8.6 6.0 ч. С. Ч 12.5 2:0 2x)1.0 4x)4.6 I 1 I ł ł Future 1/ Animal-day 28.9(25.9) 2 0 0 2 3 0 5.9 4.6 18.9 2.0 2.0 0 . 0 1.5 1.0 8.4 ł ł ι 1 ł I ł 1 W/Froject, Man-day  $(2x)\frac{1.5}{3.0}$ 6.0 3.0 21.9 6.0 ы N 10.01 12.5 12.0 69.9 (4x)4.6 (2x)3.0 Ix)8.4 2x)5.9 ł ľ ł I 1 1 I a. Pulling/Deliver of Seedlings Furrowing/Planting/Thinning Harvesting a. Reaping/Plucking/Bundling Final Harrowing/Leveling a. Land Preparation/Sowing Saching/Piling/Delivery Threshing/Winnowing 4/ Cleaning/Bund Mending Operation Breaking/Harrowing Basal Fertilizers Care of Seedings Cultivation/Weeding 7. Irrigation/Drainage b. Hauling/Piling 2. Land Preparation Post Harvesting Top-dressing Seed-bedding Sub-total Sub-total Sub-total Sub-total Sub-total Pest Control Sub-total Fertilizing Plowing a. Drying Planting 10. Total 5/ J ່ວ . 10 . م ۔ م q. ם. ъ, --. م ന . Б 4 . س 8 **ہ** 

LABOR REQUIREMENT, MUNGBEAN

TABLE G3-24

|                                      |              |             |            | ·<br>·         | (Unit: man-day/ha)                    |
|--------------------------------------|--------------|-------------|------------|----------------|---------------------------------------|
| -                                    |              | / 1         |            | 10             | · · · · · · · · · · · · · · · · · · · |
|                                      | W/Project,   | , Future 1/ | W/Project, | t, Future 🖆    |                                       |
| Operation                            | Man-day      | Animal-day  | Man-day    | Machinery      | Remarks                               |
| 1. Seed-bedding                      |              | •           |            |                |                                       |
| a. Land Preparation/Sowing           | İ            | 1           | <b>1</b>   | <b>1</b>       |                                       |
| b. Care of Seedings                  | 1            | I           | I          | . <b>1</b> -   | 1/: With animal                       |
| Sub-total                            | 1            |             | 1          | 1              | power                                 |
| 2. Land Preparation                  |              |             |            |                |                                       |
| a. Cleaning/Bund Mending             | 3.0          | ļ           | 3.0        | 1              | $\frac{2}{2}$ : Only plowing is       |
| b. Plowing                           | (1x)8.4      | 8.4         | ł          | ) e<br>1       |                                       |
| c. Breaking/Harrowing                | (2x)5;9      | 5.9         | (2x)1.0    | )<br>1.0<br>1. | tractor with                          |
|                                      | (2x)4.6      | 4.6         | (2x)4.6    | 4.6            | rotary                                |
| Sub-total                            | 21.9         | 18.9        | 8.6        | 5.6            |                                       |
| 3. Planting                          |              |             |            |                | 3/: Two passings of                   |
| a. Pulling/Deliver of Seedlings      | 1            | 1           | 1.         | ł              | tractor with                          |
| b. Furrowing/Planting/Thinning       | 6.0          | 2.0         | 6.0        | 2.0            | rotary                                |
| Sub-total                            | 6.0          | 2.0         | 6.0        | 2.0            |                                       |
| 4. Fertilizing                       |              |             |            |                | 4/: Including the                     |
| a. Basal Fertilizers                 | ي <b>.</b> 1 | 0.5         | 1.2        | 0.5            | labor requirement                     |
| b. Top-dressing                      | 1.0          | I           | 1°0        | I              | of post harvesting                    |
|                                      | 2.5          | 0.5<br>0    | 2.5        | 0.5            | work                                  |
|                                      | (2x)3.0      | 3.0         | 3.0        | 3.0            |                                       |
| 6. Cultivation/Weeding               | 10.0         | 2.0         | 10.0       | 2.0            | <u>5</u> /: The figures in            |
|                                      | (2x)3.0      | ł           | (2x)3.0    | I              | the parenthesis                       |
| 8. Harvesting                        |              |             |            |                | show draft animal                     |
| a. Reaping/Plucking/Bundling         | 19.0         | I           | 19.0       | ł              | requirement                           |
| b. Hauling/Piling , ,                | 6.2          | 3.1         | 6.2        | л.<br>Ч        |                                       |
| c. Threshing/Winnowing $\frac{4}{-}$ | 30.3         | I           | 30.2       | i              |                                       |
| Sub-total                            | 55.5         | 3 <b>.1</b> | 55.5       | <u>3.1</u>     |                                       |
| 9. Post Harvesting                   |              |             |            |                |                                       |
| a. Drying                            | ı            | ł           | I          | 1              |                                       |
| b. Saching/Piling/Delivery           | I            | I           | I          | 1              |                                       |
| 10. Total 5/                         | 101.9        | 29.5(26.5)  | 88.6       | 16.2(13.2)     |                                       |
|                                      |              |             |            |                |                                       |

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TABLE G3+25

LABOR REQUIREMENT, PEANUT

LABOR REQUIREMENT, CORN

FABLE G3-26

and post-harvesting labor requirement of any harvesting show draft animal the parenthesis (Unit: man-day/ha) Two passings of  $\frac{2}{2}$ : Only plowing is 5/: The figures in Including the rechanized by tractor with 1/: With animal requirement Remarks tractor rotary works power .. // -4] -4] 2 Machinery e 16.6(12.6) 1.0 3.0 2.0 3.0 W/Froject, Future 4.6 5.6 2.0 0.5 0 . . . . 2.0 I I ı 1 ł I 1 Man-day 6.0 0 . 1 10.0 45.0 о. С 8.6 0 9 5 2.5 45.0 79.6 (2x)1.0 (4x)4.6 (2x)<u>3.0</u> (3x)4.5 ١ ۱ ۱ ì ۱ ١ ۱ Animal-day W/Project, Future 1/ 2.0 29.4(26.4) 5.9 4.6 18.9 8.4 in O 2.0 ł I 3.0 0 8 ł ł ł ł 1 Man-day 3.0 6.0 0.0 0.1 10:01 45.0 21.9 1,5 2.5 45.0 92.9 (2x)5.9(2x)3.0(4x)4.6 (3x)4.5 (IX)8.4 1 i ľ L I I ł Pulling/Deliver of Seedlings a. Reaping/Plucking/Bundling 4/ Furrowing/Planting/Thinning Final Harrowing/Leveling a. Land Preparation/Sowing Saching/Piling/Delivery Cleaning/Bund Mending Operation Threshing/Winnowing Breaking/Harrowing Basal Fertilizers Care of Seedings Cultivation/Weeding Irrigation/Drainage Hauling/Piling Land Preparation Top-dressing Post Harvesting Seed-bedding Sub-total Sub-total Sub-total Sub-total Pest Control Sub-total Sub-total Fertilizing Plowing Harvesting a. Drying Planting Ś Total ູ່ . Д . 0 å . م 5 с Ф , a ь. Д ů. а, ÷ 5. с С ŝ 8 0 ຸ ທ 10. 4

|                                       |                  |                     |                  | •           |                                 |
|---------------------------------------|------------------|---------------------|------------------|-------------|---------------------------------|
|                                       | ·                | :                   |                  | ÷           | (Unit: man-day/ha)              |
| · · · · · · · · · · · · · · · · · · · | W/Proiec         | W/Project Puture 1/ | W/Proiect        | + Future 2/ |                                 |
| Operation                             | Man-day          | Animal-day          | Man-day          | Machine     | Remarks                         |
| 1. See-bedding                        |                  |                     |                  |             |                                 |
| a. Land Preparation/Sowing            | 1                | и<br>1<br>1         | Ţ                | 1           |                                 |
| b. Care of Seedings                   | 1                | ı                   | 1                | . 1         | 1/: With animel                 |
| Sub-total                             | .1               | 1                   | l                | ł           | power                           |
| 2. Land Preparation                   |                  |                     |                  |             |                                 |
| a. Claaning/Bund Mending              | 3.0              | 1                   | 3.0              | 1           | 2/: Only plowing is             |
| b. Plowing                            | (1x)8.4          | 8.4                 | (1x) -           | Ì           | mechanized by                   |
| c. Breaking/Harrowing                 | (2x)5.9          | 5.9                 | (2x)1.0          | 1.0 2/      |                                 |
| d. Final Harrowing/Leveling           | (4x)4.6          | 4.6                 | (2x)4.6          | 4.6         |                                 |
|                                       | 21.9             | 18.9                | 8.6              | 5.6         | 3/: Two passings of             |
| 3. Planting                           |                  |                     |                  |             | tractor with                    |
|                                       | ı                | 1                   | 1                | I           | rotary                          |
| b. Furrowing/Planting/Thinning        | 16.0             | I                   | 16.0             | I           |                                 |
|                                       | 16.0             | 1                   | 16.0             | 1           | 4/: Including the               |
| 4. Fertilizing                        |                  |                     |                  |             |                                 |
|                                       | 1.5              | 0.5                 | 1.5              | 0.5         | of post harvesting              |
| b. Top-dressing                       | 1.5              |                     | ب<br>•           | 0.5         | work                            |
|                                       | 3.0              |                     | 0.0<br>8         | 1.0         |                                 |
| 5. Pest Control                       | (8x)1 <u>2.0</u> | 12.0                | (8x)1 <u>2.0</u> | 12.0        | $\overline{5}$ : The figures in |
|                                       | 30.0             | 3°0                 | 30.0             | 3.0         |                                 |
|                                       | (6x)9.0          | 1                   | (6x)9.0          | Į           | show draft animal               |
| 8. Harvesting                         |                  |                     |                  |             | requirement                     |
| a. Reaping/Plucking/Bundling          |                  |                     |                  |             |                                 |
| b. Hauling/Piling                     | 28.0             | 3.0                 | 28.0             | ·3•0        |                                 |
|                                       |                  | c                   | (<br>(           | с<br>с      |                                 |
| Sub-total<br>9. Post Harvesting       | 28.0             | 0.0                 | 28.0             | 3.0         |                                 |
| a. Drying                             | 1                | 1                   | l                | I           |                                 |
| b. Saching/Piling/Delivery            | 12.0             | 3.0                 | 12.0             | 3.0         |                                 |
| Sub                                   | 12.0             | 3.0                 | 12.0             | 3.0         |                                 |
| 10. Total 5/                          | 131.9            | 42.9(30.9)          | 118.6            | 27.6(15.6)  |                                 |

LABOR REQUIREMENT, VEGETABLES (WATER MELON)

TABLE G3-27

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TABLE 63-28

MONTHLY FARM LABOR BALANCE, WITH PROJECT (2000)

|                             | · .  | ÷.      |       |      |        |                         |        |         | (unit | ; tho       | isand m          | an-day]     | )       |  |
|-----------------------------|------|---------|-------|------|--------|-------------------------|--------|---------|-------|-------------|------------------|-------------|---------|--|
| I t em                      | MAY  | JUN     | JUL   | AUG  | SEP    | OCT                     | NOV    | DEC     | JAN   | FEB         | MAR              | APR         | Total   |  |
| A. Labor Requirement        |      |         |       |      |        |                         | . '    |         |       | ÷           |                  |             | 1.1     |  |
| 1. Irrigated area           | 13.0 | 82,2    | 113.7 | 23.2 | 35.5   | 111.9                   | 62.7   | 75.6    | 32.0  | 38.3        | 84.0             | 67.3        | 739.4   |  |
| (1) Rice, Wet season        | 11.0 | 82.2    | 113.7 | 23.2 | 35.5   | 103.5                   | 9.1    |         |       |             |                  |             | 378.2   |  |
| - Transplanted, W/O 1/      | 6.4  | 45.6    | 61.5  | 11.1 | 19,6   | 49.3                    | 1.3    |         |       |             | · .              |             | 194.8   |  |
| - Transplanted, W/ 2/       | 2.4  | 28.9    | 43.3  | 8.9  | 13.3   | 32.9                    | 0.7    |         |       |             |                  |             | 130,4   |  |
| - Direct-seeded, W/O        | 1.6  | 5.3     | 5.8   | 1.8  | 1.5    | 12.8                    | 4 3    |         |       |             | n an an<br>La sa |             | 33.1    |  |
| - Direct-seeded, W/         | 0.6  | 2.4     | 3.1   | 1.4  | 1.1    | 8.5                     | 2.8    |         |       | :           |                  |             | . 19.9  |  |
| (2) Rice, Dry season        |      |         |       |      |        | 8.4                     | 53.6   | 68.5    | 14.1  | 16.5        | 68.9             | 14.6        | 244.6   |  |
| - Transplanted, W/O         |      |         |       |      |        | 4.3                     | 27.8   | 35.1    | 6.1   | 8.4         | 29.2             | 3.5         | 114.4   |  |
| - Transplanted, W/          |      |         |       |      |        | 1.8                     | 17.8   | 24.7    | 4.8   | 5.9         | 19.7             | 2.2         | 76.9    |  |
| - Direct-seeded, W/O        |      |         |       |      |        | 1.7                     | 5.5    | 5.6     | 1.8   | 1.2         | 12.0             | 5.6         | 33.4    |  |
| - Direct-seeded, W/         |      |         |       |      |        | 0.6                     | 2.5    | 3.1     | 1.4   | 1.0         | 8.0              | 3.3         | 19.9    |  |
| (3) Diversified Crops       | 2.0  |         | •     |      |        |                         |        | 7.1     | 17.9  | 21.8        | 15.1             | 52.7        | 116.6   |  |
| - Mingbean                  |      |         |       |      |        |                         |        |         | 3.3   | 4.7         | 4.8              | 6.5         | 19.3    |  |
| - Peanut                    |      |         |       |      |        |                         |        | 3,5     | 4.5   | 2.7         | 1.2              | 18.0        | 29.9    |  |
| - Corn                      |      |         |       |      |        |                         |        | 3.6     | 4.7   | 3.0         | - 1.2            | 14.6        | 27.1    |  |
| - Vegetables                | 2.0  |         |       |      |        | an an the<br>The second |        |         | 5.4   | 11,4        | 7,9              | 13.6        | 40.3    |  |
| 2. Rainfed Upland           | 18.9 | 14.4    | 11.7  | 20.9 | 5.1    | 3.9                     | 4.9    | 1.8     |       |             |                  | 3.7         | 85.3    |  |
| - Cassava                   | 8.1  | 6.9     | 5.4   | 9.6  | 1.2    | 1.0                     | 2.3    |         |       |             |                  | 2.1         | 36.6    |  |
| - Sweet potate              | 5.4  | 3.0     | 2.7   | 4.7  | 3.3    | 2.4                     | 1.0    | 1.8     | •     |             | •                |             | 24.3    |  |
| - Cocomit                   | 5.4  | 4,5     | 3.6   | 6.6  | 0,6    | 0.5                     | 1.6    |         |       | · ·         |                  | 1.6         | 24.4    |  |
| 3. <u>Total (1 + 2)</u>     | 31.9 | 96.6    | 125.4 | 44.1 | 40.6   | 115.8                   | 67.6   | 77.4    | 32.0  | 38.3        | 84.0             | <u>71.0</u> | 824.7   |  |
| 4 Animal Husbandry          | 12.9 | 12.9    | 12.9  | 12.9 | 12.9   | 12.9                    | 12.9   | 12.9    | 12.9  | 12.9        | 12.9             | 12.9        | 154.8   |  |
| 5. Grand Total              | 44.8 | 109.5   | 138.3 | 57.0 | 53.5   | 128.7                   | 80.5   | 90.3    | 44.9  | 51.2        | 96.9             | 83.9        | 979.5   |  |
|                             |      |         |       |      |        |                         |        |         |       |             |                  |             |         |  |
| B. Available Labor<br>Force |      | <b></b> |       |      | (3/ 14 | 3 thous                 | and ma | ni-day) |       |             |                  |             | 1,716.0 |  |
| C. Balance                  | 98.2 | 33.5    | 4.7   | 86.0 | 89.5   | 14.3                    | 62.5   | 52.7    | 98.1  | <u>91.8</u> | 46.1             | 59.1        | 736.5   |  |

Note: 1/ Without mechanization

2/ With mechanization

3/ Estimated at 2,860 farms x 2.0 men x 30 days/month x 25 days/30 days

|  | c                 | Total                  | 378   | 252                                   | 3,240                            | 8,640                          | 5,960                     |
|--|-------------------|------------------------|---|---------------------------------------|----------------------------------|--------------------------------|---------------------------|
|  | Annual Production | per<br>Kind farm       | Fat animals 0.7<br>(two years old)          | Carabao calf 0.7<br>(three years old) | Fat swine 9<br>(6-12 months old) | Piggeries 24<br>(6 months old) | Lumb 22<br>(6 months old) |
| r area                                   |                   | No. of<br>Farm         | 540   | 360                                   | 360                              | 360                            | 180                       |
| PROJEC                                   |                   | Žц                     | <b></b>                                     | F4                                    | : 10                             |                                | : 10                      |
| LIVESTOCK PRODUCTION IN THE PROJECT AREA |                   | Composition of animals | Cow for breeding<br>offspring for fattening | Female carabao for breeding           | Swine for fattening              | Sow<br>offsprings              | Buck<br>Does              |
| TABLE G3-29                              |                   | Type                   | Cow-calf, cattle fattening                  | Carabao-calf                          | Swine fattening                  | Piggeries production           | Goat breeding             |
|  |                   |                        | -1  |                                       | м.                               | 4                              | ۲                         |
|  |                   |                        |   |                                       |                                  |                                |                           |

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LABOR REQUIREMENT OF ANIMAL HUSBANDRY

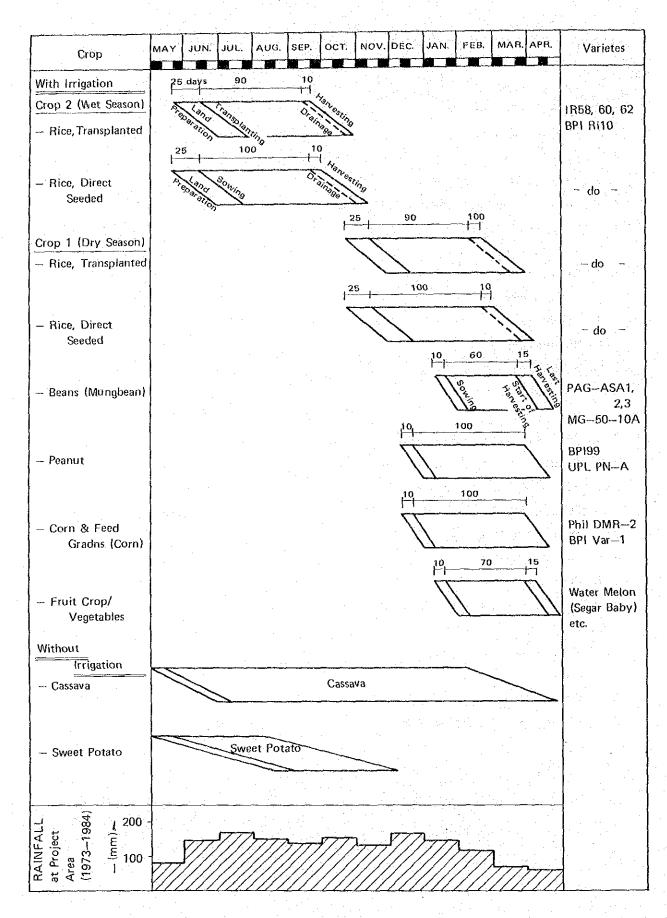
TABLE G3-30

|        |                            | No. of parti-<br>cinating | Labor requi | Labor requirement/Farm | Labor requirement (Total) | ent (Total)     |
|--------|----------------------------|---------------------------|-------------|------------------------|---------------------------|-----------------|
|        | Type                       | farms                     | Per year    | Per month              | Per year                  | Per nonth       |
|        |                            | (no.)                     | (man-day)   | (man-day)              | (1,000 man-day)           | (1,000 man-day) |
| •<br>• | Cow-calf, cattle fattening | (30) 540                  | 93.0        | 7.8                    | 50.2                      | 4.2             |
| 1      | Carabao-calf               | (20) 360                  | 61.6        | 5.1                    | 22.2                      | 1.8             |
| 5      | Swine fattening            | (20) 360                  | 70.0        | 5.8                    | 25.2                      | 2.1             |
| 4      | Piggeries production       | (20) 360                  | 117.0       | 9.8                    | 42.ľ                      | 3.5             |
| Ś      | Goat breeding              | (10) 180                  | 88.6        | 7.4                    | 15.9                      | 1,3             |
|        | Total                      | 1,800                     |             |                        | 155.6                     | 12.9            |
|        |                            |                           |             |                        |                           |                 |

## TABLE G3-31 MAN POWER AND FACILITIES OF PILOT SCHEME

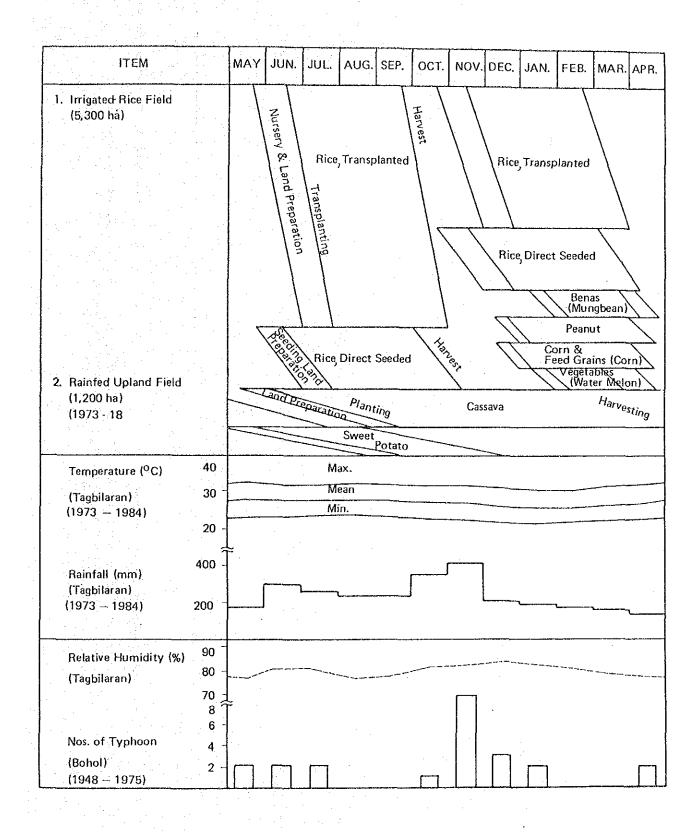
Capacity Item Number 1. Man-power requirement Project manager 1-1 1 1-2 Agronomist 1 1-3 Agricultural engineer 1 1-4 Farm management specialist 1 1-5 Seed technicians 2 1-6 Administrative assistant 1 1-7 Clerk/typist 1 1-8 pump operator 1 1-9 Laborers 20 1-10 Mechanics 1 2. Farm Machinery requirement 2-1 Four-wheel tractor & accessaries 40-50 HP 1 3HP, 5HP, 7-8 HP x 2 4 2-2 Power tiller 18 1 2 2-3 Sprayer (Knapsack-type) 2 l ton/hr 2-4 Powered thresher (IRR1 type) 2 2-5 Dryer (Flat bed type) 2.0 ton bin 600 gallon/min. 2 2-6 Pump & Accessaries (Low-Lift) 2 ton 1 2-7 Service truck 5 2-8 Motor Cycle ł 2-9 Seed cleaner 1 2-10 Sorter and packing machine 1000 kg 1 2-11 Balance (Flat form) 1 2-12 Micellouneous tools & equipment 3. Building  $60 \text{ m}^2$ 1 3-1 Office & Training room  $60 \text{ m}^2$ 1 Warehouse & Machinery Shade 3-2

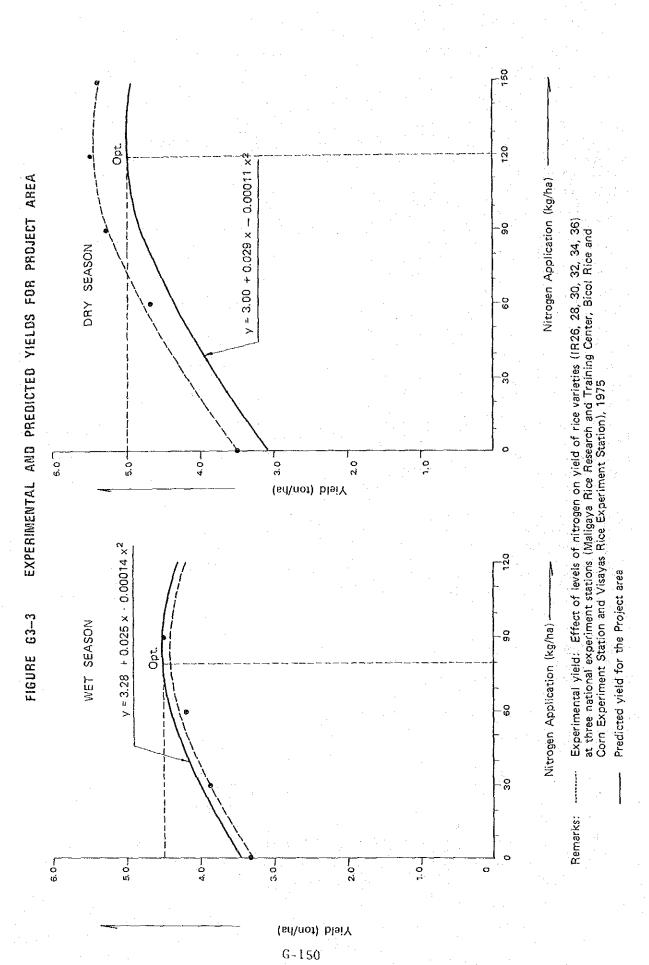
## FIGURE G3-1 PROPOSED CROPPING CALENDAR



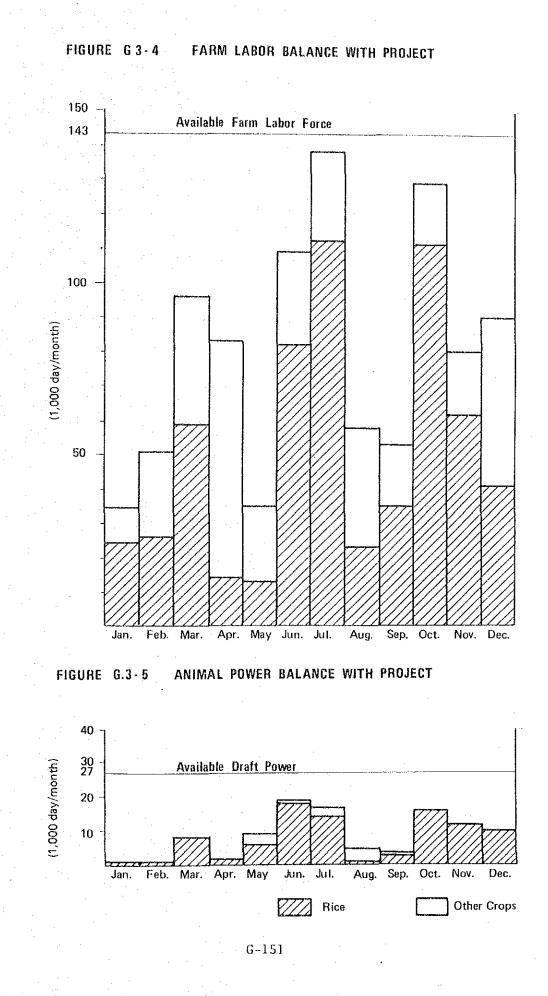
G = 1.48

# FIGURE G3-2 PROPOSED CROPPING PATTERN





0.00



For the analysis of present agriculture and also for the formulation of agricultural development plan, extensive data are collected mostly at the provincial and regional offices of the National Census and Statistics Office (NCSO) of the National Economic Authority (NEDA), the Bureau of Agricultural Economics of the Ministry of Agricultural (MA) and the National Food Authority (NFA) of , as well as at the MA Offices at the municipal to regional levels and Provincial Development Staff Office in Bohol.

Because of the limited time for the data collection, the analysis and planning methods have to be based on the existing data as much as possible. However it was observed that the existing data base have the following weakness in general;

- (i) There is in-consistency among various data sources in such basic data as the present land use, population, number of households and crop production, especially at the Barangay and municipal levels.
- (ii) Few-time-series data are available for the above-said basic data.

One of the reasons for the weakness may be attributed to the unavailability of accurate boundaries among the Barangays and municipalities and also the inadequate data collection systems.

건물 관광 전문 영화

ANNEX H. DAM AND CANALS 

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|            | 나는 이 가 물건 지난 것 수 있는 것 같은 지수는 것을 가지 않는 것을 통했다.            |
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## 1.1 Seismic Analysis

The seismic force must be considered as one of these external forces on dam design. Since there is no standard value of seismic force in the Philippines, it will be determined based on the following analysis.

Analysis of seismic force at the dam site is made by adopting Dr. Okamoto's theory (refer to Earthquake Proof Engineering by Shunzo Okamoto) based on the data of earthquake occured within a radius of about 300 km from the dam site as shown in FIGURE H1-1 (source: Catalogue of Significant Earthquakes (1907~1982) - PAGASA).

According to Okamoto's formula, the maximum seismic acceleration, which is predicted the occurence in the proposed dam site, is given by the following equation.

 $\log_{10} \quad \frac{\alpha}{640} = \frac{D + 40}{100} \ (-0.1036M^2 + 1.7244M - 7.604)$ 

Where,  $\alpha$ : Predicted maximum seismic acceleration (gal-cm/sq.scc)

- D: Distance between the seismic center occured about proposed dam site (km)
- M: Magnitude of seismic center

Also, distance between the seismic center and proposed dam site is estimated as follows:

$$D = \sqrt{A^2 + B^2}$$

Where, A: Distance in the latitude between them

 $A = (Pn - 9.96^{\circ}) \times 111 \text{ km/}\circ$ 

Pn; the latitude of seismic center (°)

9.96°; the latitude of proposed dam site (Bayongan dam)

111; length of latitude per one degree (km/°)

B; Distance in the longitude between them (km)

 $B = (Pe - 124.35^{\circ}) \times 111 \times \cos\left(\frac{9.96 + Pn}{2}\right)$ 

Pe; the longitude of seismic center (°) 124.35°; the longitude of proposed dam site

H-1

As the result of analysis, seismic acceleration at the dam site is estimated to be about 191 Gal in the maximum, while there were earthquakes recorded 83 times with the maximum acceleration of more than one Gal, as shown in TABLE H1-1.

On the other hand for making examination of occurance frequency of earthquake, the estimated seismic accelerations are ploted in the x coordinate with No./year in the y coordinate, as shown in FIGURE H1-2.

Then, for making the earthquake-proof design of the fill dam, the analysis method subjected to the seismic intensity against an earthquake of 100 year probability will be adopted.

Taking into account location of the proposed dam site which belongs to the seismic intensity V in the Philippines (See 3.2.4 b). in the Main Report) and seismicity coefficient in the design of other dams, the coefficient of K = 0.20 will be justified. Therefore, for the design of the Bayongan dam and Capayas dam K = 0.20 is applied as design seismicity coefficient.

### 1.2 Flood Analysis

#### a) Design Flood Discharge

For estimation of design flood discharge in the Philippines, there are useful formulas by B.P.W. These are ranked into four grades of frequency ie. "Extreme", "Rare", "Occasional", and "Frequent". These formulas could substantially correspond to Dr. Creager's formula which is internationally prevailing. (See Annex B.4)

In this study, Design floods of the Bayongan dan Capayas dams will be estimated by B.P.W's formulas as the prime, then verified by other methods such as Creager's formula, Rational Method, survey of historical floods, and meteorological approach through Probable Maximum Precipitation.

Summaries of above studies are shown in TABLE H1-2 (Bayongan)

H-2

TABLE H. 1.-1 SEISMIC ANALYSIS BY DR. OKAMOTO'S FORMULA

| PROJECT NAME       | ; | BOHOL IRRIGATION PROJECT II F/S |
|--------------------|---|---------------------------------|
| LOCATION           | ; | BAYONGAN, SAN-MIGUEL, BOHOL     |
| DAMSITE'S LATITUDE | ; | 9.96(DEGREES)                   |
| DITTO LONGITUDE    | ; | 124.35(DEGREES)                 |
| NUMBER OF DATA ; 8 | 3 | RECORDS ; 1907 TO 1982 = 76 YRS |
|                    |   |                                 |

| NO.   | DATE     | LAT.  | LON.   | MG. | DIST.  | ACC.  | N0./Y  |
|-------|----------|-------|--------|-----|--------|-------|--------|
|       | (M-D-Y)  | (DEG) | (DEG)  |     | (KM)   | (GAL) |        |
| 1     | 03.07.50 | 10.00 | 124.00 | 6.8 | 38.52  | 191.1 | 0.0132 |
| 2     | 09.02.48 | 10.00 | 125.00 | 7.0 | 71.20  | 134.4 | 0.0263 |
| 3     | 10.30.26 | 9.50  | 124.50 | 6.3 | 53.63  | 101.9 | 0.0395 |
| - 4   | 07.19.41 | 10.00 | 124.00 | 5.8 | 38,52  | 89.6  | 0.0526 |
| 5     | 02.04.41 | 9.00  | 124.00 | 6.9 | 113.24 | 67.4  | 0.0658 |
| 6     | 09.21.29 | 10.00 | 125,00 | 6.0 | 71.20  | 51.1  | 0.0789 |
| . 7   | 07.12.11 | 9.00  | 126.00 | 7.8 | 209.73 | 46.3  | 0.0921 |
| 8     | 01.26.56 | 10.00 | 124.00 | 5.0 | 38.52  | 37.3  | 0.1053 |
| 9     | 03.10.75 | 9.60  | 124.10 | 5.2 | 48.42  | 34.2  | 0.1184 |
| 10    | 03.19.52 | 9.50  | 126.50 | 7.8 | 240,69 | 33.4  | 0.1316 |
| 11    | 01.24.48 | 10.50 | 122.00 | 8.2 | 263.61 | 31.7  | 0.1447 |
| 12    | 05.05.25 | 9.50  | 123.00 | 6.8 | 156.27 | 31.2  | 0.1579 |
| 13    | 01.24.48 | 11.00 | 122.00 | 8,2 | 281.28 | 26.6  | 0.1711 |
| 14    | 03.31.55 | 8.00  | 124.00 | 7.3 | 220.92 | 25.5  | 0.1842 |
| 15    | 05.24.31 | 10.00 | 125.50 | 6.3 | 125.80 | 24.7  | 0.1974 |
| 16    | 07.25.42 | 11.50 | 124.50 | 6.8 | 171.72 | 24.6  | 0.2105 |
| 17    | 06.07.47 | 11.50 | 125.00 | 6.9 | 185.06 | 23.5  | 0.2237 |
| 18    | 05.06.65 | 9.60  | 124.10 | 4.9 | 48.42  | 22.6  | 0.2368 |
| 19    | 02.10.57 | 10.25 | 126.00 | 6.8 | 183.16 | 20.6  | 0.2500 |
| 20    | 02.10.57 | 10.00 | 126.00 | 6.7 | 180.43 | 18.2  | 0.2632 |
| 21    | 12.14.77 | 10.00 | 125.30 | 5.8 | 103.95 | 17.4  | 0.2763 |
| 22    | 01.14.82 | 9.99  | 124.23 | 3.4 | 13.54  | 17.1  | 0.2895 |
| .23   | 10.20.42 | 8.50  | 122.50 | 7.3 | 259.51 | 15.8  | 0.3026 |
| 24    | 02.10.57 | 10.00 | 126.00 | 6.6 | 180.43 | 15.3  | 0.3158 |
| 25    | 03.12.15 | 12.00 | 124.00 | 7.0 | 229.63 | 14.5  | 0.3289 |
| 26    | 01.01.19 | 8.00  | 126.00 | 7.4 | 282.95 | 13.7  | 0.3421 |
| 27    | 02.11.57 | 10.00 | 126.00 | 6.5 | 180.43 | 12.7  | 0.3553 |
| 28    | 05.03.82 | 10,03 | 124.44 | 3.1 | 12.54  | 12.5  | 0.3684 |
| 29    | 02.10.57 | 10.25 | 126.00 | 6.5 | 183.16 | 12.1  | 0.3816 |
| 30    | 09.23.73 | 10.35 | 125.30 | 5.7 | 112.46 | 11.7  | 0.3947 |
| 31    | 09.22.40 | 8,00  | 124.00 | 6.8 | 220.92 | 11.5  | 0.4079 |
| 32    | 08.30.24 | 8.50  | 126.50 | 7.3 | 285.92 | 11.4  | 0.4211 |
| 33    | 05.03.43 | 12.50 | 125.50 | 7.4 | 308.49 | 10.1  | 0.4342 |
| 34    | 03.07.50 | 11.00 | 122.50 | 6.8 | 232.59 | 9.6   | 0.4474 |
| 35    | 04.27.19 | 11.00 | 123.00 | 6.4 | 187.19 | 9.2   | 0.4605 |
| 36    | 03.07.50 | 10.50 | 122.25 | 6.8 | 237.10 | 9.0   | 0.4737 |
| 37    | 01.24.31 | 10.00 | 126.00 | 6.3 | 180.43 | 8.5   | 0.4868 |
| 38    | 02.11.57 | 10.00 | 126.00 | 6.3 | 180.43 | 8.5   | 0.5000 |
| · · · |          |       |        |     |        |       |        |

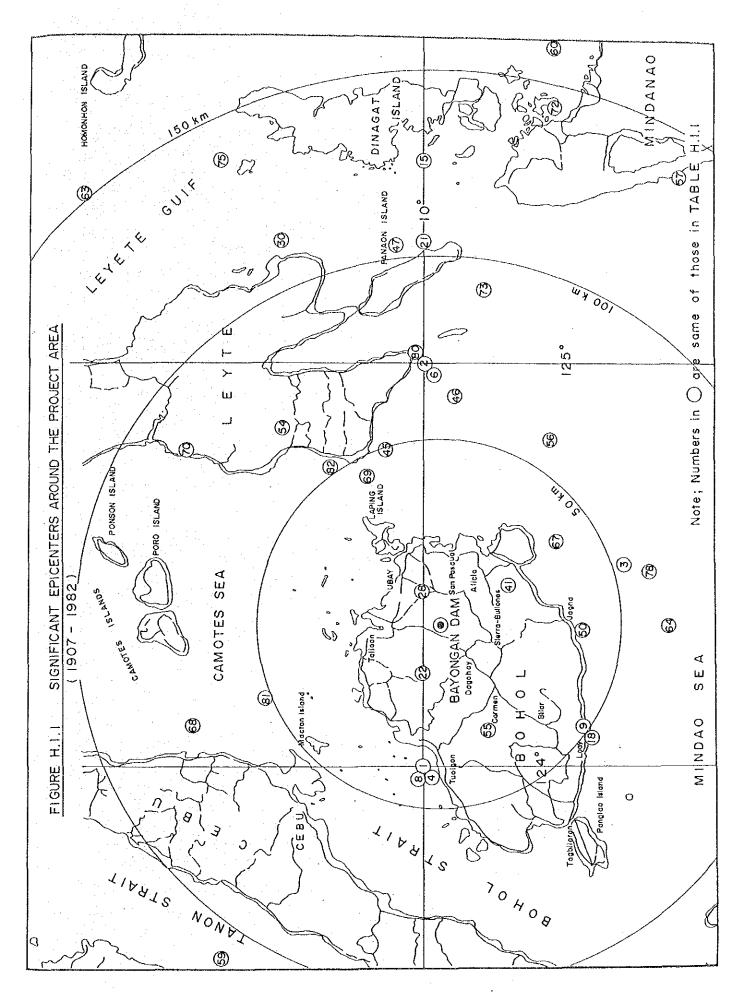
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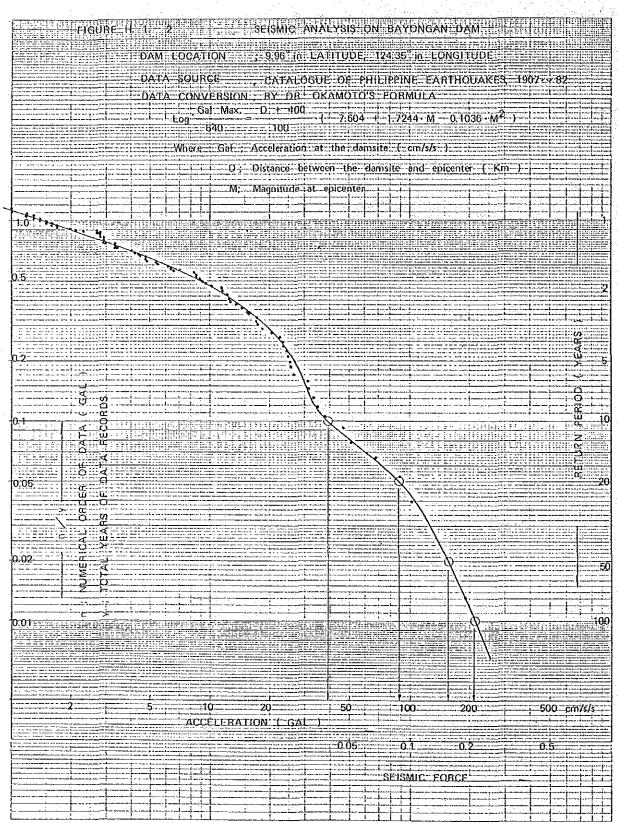
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|      |          |       | 1999 (March 1997) |     | · · · · |             |        |
|------|----------|-------|-------------------|-----|---------|-------------|--------|
| NO.  | DATE     | LAT.  | LON.              | MG. | DIST.   | ACC.        | ND./Y  |
| 1    | (M-D-Y)  | (DEG) | (DEG)             |     | (KM)    | (GAL)       |        |
| .39  | 02.10.57 | 10.50 | 126.50            | 6.8 | 242.38  | 8.3         | 0.5132 |
| 40   | 08.13.36 | 9.00  | 126.50            | 6.8 | 258.39  | 6.5         | 0.5263 |
| 41   | 03.15.80 | 9.79  | 124.45            | 3.1 |         | 6.2         | 0.5395 |
| 42   | 08.18.57 | 12.00 | 124.50            | 6.5 | 227.03  | 5.5         |        |
|      |          | 8.00  | 125.00            | 6.5 | 228.93  | 5.4         | 0.5658 |
| 43   | 04.10.55 |       |                   | 6.5 | 235.17  | 4.8         |        |
| 44   | 07.08.51 | 9.90  | 122.20            |     |         |             |        |
| 45   | 09.16.82 | 10.09 | 124.79            | 4.0 |         | 4.7         | 0.5921 |
| 46   | 05.27.79 | 9.92  | 124.91            | 4.3 | 61.39   |             | 0.6053 |
| 47   | 11.14.81 | 10.07 | 125.29            |     | 103.47  | 4.4         | 0.6184 |
| 48   | 03.31.55 | 8.10  | 123.20            | 6.5 | 241.91  | 4.3         |        |
| 49   | 03.31.55 | 8.10  | 123.20            | 6.5 | 241.91  | 4.3         | 0.6447 |
| 50   | 09.23.82 | 9.60  | 124.34            | 3.6 | 39.97   | 4.1         | 0.6579 |
| . 51 | 11.15.57 | 8.00  | 124.50            | 6.3 | 218.18  | 4.0         | 0.6711 |
| 52   | 11.05.41 | 12.50 | 123.00            | 6.9 | 317.95  | 3.3         | 0.6842 |
| 53   | 02.17.70 | 9.80  | 125.90            | 5.8 | 170.42  | 3.3         | 0.6974 |
| 54   | 07.04.81 | 10.35 | 124.84            | 4.3 | 68.85   | · · · · · · | 0.7105 |
| 55   | 02.05.81 | 9.84  | 124.09            | 3.1 | 31.40   | 3.0         | 0.7237 |
| 56   | 01.16.78 | 9.68  | 124.81            | 4.0 | 59.14   | 2.9         | 0.7368 |
| 57   | 05.01.79 | 9.36  | 125.46            | 5.4 | 138.52  | 2.9         | 0.7500 |
| 58   | 07.13.62 |       | 123.00            | 5.5 | 147.65  | 2.8         | 0.7632 |
| 59   | 09.10.52 | 10.50 | 123.50            |     | 110.52  | 2.8         | 0.7763 |
|      |          |       |                   |     | 159.68  | 2.6         | 0.7895 |
| 60   | 12.12.68 | 9.67  | 125.78            | 5.6 |         | 2.0         |        |
| 61   | 07.13.62 | 10.00 | 122,50            | 6.0 | 202.29  | 2.0         | 0.8026 |
| 62   | 07.12.31 | 12.00 |                   | 6.5 | 270.03  | 2.6         | 0.8158 |
| 63   | 07.12.70 | 10.84 | 125.41            | 5.5 | 151.44  | 2.5         | 0.8289 |
| 64   | 11.25.81 | 9.39  | 124.35            | 4.0 | 63.27   | 2.3         | 0.8421 |
| 65   | 11.25.62 | 11.20 | 124.80            | 5.4 | 146.14  | 2.3         | 0.8553 |
| 66   | 07.08.51 | 11.00 | 122.00            | 6.5 | 281.28  | 2,1         |        |
| 67   | 03.20.81 | 9.67  | 124.56            | 3.2 | 39.54   | 2.0         | 0.8816 |
| 68   | 11.10.75 | 10.57 | 124.10            | 4.1 | 73.01   | 1.7         |        |
| 69   | 09.16.82 | 10.14 | 124.72            | 3.3 | 45.11   | 1.7         | 0.9079 |
| 70   | 10.10.80 | 10.59 | 124.78            | 4.3 | 84.24   | 1.6         | 0.9211 |
| 71   | 06.15.28 | 11.50 | 121.50            | 6.8 | 354.72  | 1.5         | 0.9342 |
| 72   | 12.07.69 | 9.67  | 125.63            | 5.2 | 143.65  | 1.5         | 0.9474 |
| 73   | 12.28.79 | 9.85  | 125.18            | 4,4 | 91.57   | 1.4         | 0,9605 |
| 74   | 04.01.65 | 9.93  | 125.85            | 5.4 | 164.03  | 1.3         | 0.9737 |
| 75   | 01.21.64 | 10.50 | 125.50            | 5.1 | 139.19  | 1.3         | 0.9868 |
| 76   | 03.17.62 | 9.50  | 123.00            | 5.3 | 156.27  | 1.3         |        |
| 77   | 09.13.73 | 9,20  | 126.10            | 5.8 | 209.30  | 1.2         | 1.0132 |
| 78   | 05.03.81 | 9 44  | 124.48            | 3.6 | 59.45   | 1.2         | 1.0263 |
| 79   | 06.12.64 | 11 25 | 124.75            | 5.2 | 149.69  | 1.2         | 1.0395 |
| 80   | 03.06.82 |       |                   |     |         |             |        |
|      |          | 10.01 | 125.06            | 4.0 | 77.81   | 1.0         | 1.0526 |
| 81   | 09.22.77 | 10.39 | 124.17            | 3:3 | 51.62   | 1.0         | 1.0658 |
| 82   | 11.16.82 | 10.23 | 124.74            | 3.3 | 52.10   | 1.0         | 1.0789 |
| 83   | 04.08.77 | 9.04  | 121.82            | 4.4 | 295.20  | 0.0         | 1.0921 |

H-4



H-5



<u>584:28</u> A4 NO.408C

and TABLE H1-3 (Capayas).

## b) Flood Routing

For optimizations of spillway sizes, studies of flood routing are necessary for these spillways which are uncontrolled (gatelless). These studies have been made by using assumed hydrograph and through various sizes of spillways.

Assumption of hydrograph is made by the following empirical equations;

$$\frac{t_{u}}{t_{p}} = \left(\frac{Q_{u}}{Q_{p}}\right)^{0.6} \text{ and } \frac{t_{d}}{t_{p}} = p \cdot \frac{1 - (Q_{d}/Q_{p})}{(Q_{d}/Q_{p})^{0.4}} \frac{1}{(Q_{d}/Q_{p})^{0.4}}$$

where  $t_u$ ; Time (hours) during rising-up the discharge

- $t_p$ ; Travel time (hours) of peak discharge (see the next equation)
- $Q_{\rm U}$ ; Discharge (cu.m/s) at the time of  $t_{\rm H}$
- Q<sub>D</sub>; Peak discharge (cu.m/s)
- $t_{\rm d};$  Time (hours) during drop-down the discharge
  - $t_d = 0$  at  $Q_p$
- $Q_d$ ; Discharge at the time of  $t_d$
- p; Constant p = 1 in normal case

 $t_p = C \cdot A^{0.22} r_e^{-0.35} - 2/$ 

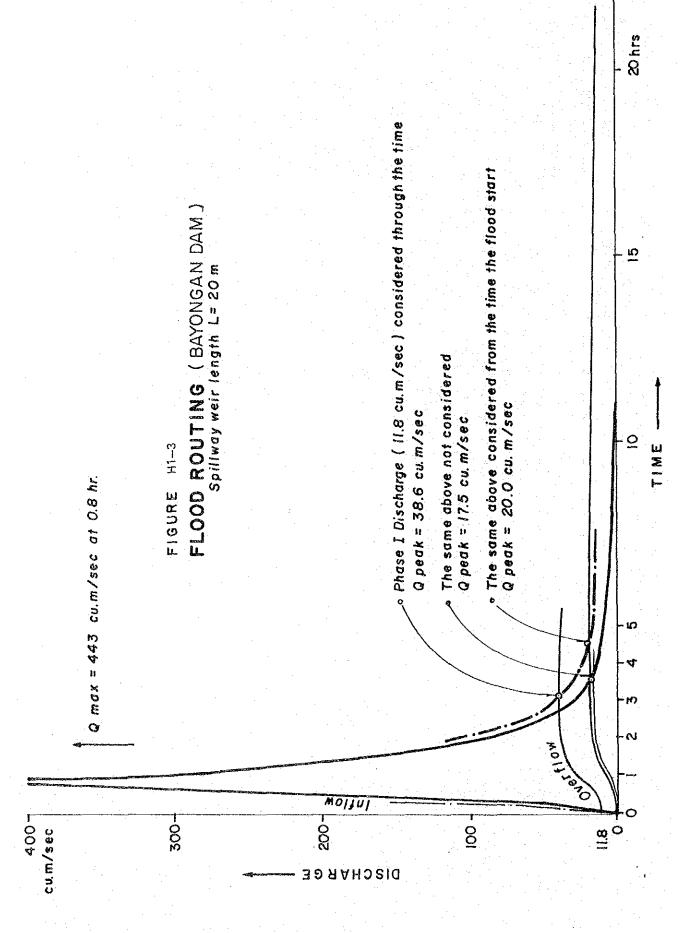
- where C; Constant according to topo-condition
  - c = 290 for well forested area
  - c = 200 for medium forsted or grassland
  - c = 140 for poorly forested or golf links
  - c = 100 for de-forested area
  - c = 65 for plantless city area
  - c = 150 for Bayongan area
  - c = 200 for Capayas area
  - A; Catchment area (sq.km)
  - r<sub>p</sub>; Area mean rainfall intensity (mm/hr)
    - $r_e = 130$  mm/hr for Bayongan area
    - $r_e = 101$  mm/hr for Capayas area
  - Note: 1/: by H. Sugiyama (Kyoto University, not published yet) 2/: by Dr. Kadoya and Fukushima (Kyoto University, 1976)

| C Remarks                 | A; Catchment Area<br>11.2 sq.km                      | Q; in cu.ft/sec<br>A; in sq. mile                  | $f = 0.9$ $rt = \frac{R24}{24} \left(\frac{24}{T}\right)^{0.6}$ $= \frac{403.5}{24} \left(\frac{24}{0.8}\right)^{0.6}$ $f = 150A0.22rt^{-0.35}$ $r = 0.8 hr^{2}$ |   | Meteorological P.N.P may<br>be only about 200 mm/day<br>403.5 $>>$ 200 |                                   |
|---------------------------|--|--|--|---|--|-----------------------------------|
| Equivalent<br>Creager's ( | 100.5  | 100  | 8<br>8<br>9  | 40.7<br>25.9  |  | Flood.                            |
| Max. Discharge            | 443 cu.m/sec or<br>39.6 cu.m/sec/sq.km               | 441 cu.m/sec or<br>39.4 cu.m/sec/sq.km             | 364 cu.m/sec or<br>32.5 cu.m/sec/sq.km   | 2,219 <sup>3/</sup> cu.m/sec or<br>3.80 cu.m/sec/sq.km<br>1.410 <sup>3/</sup> cu.m/sec<br>2.41 cu.m/sec/sq.km |  | the Probable Maximum              |
| Description               | $Q_{\text{max}} = \frac{210 \cdot A}{\sqrt{A + 17}}$ | Qmax =<br>46CA(0.894A <sup>-0.048</sup> )          | Qmax = $\frac{1}{3.6}$ .f.rt.A<br>With the Rainfall data<br>at Dagohoy<br>1957 - 84  | Typhoon "DELILAH:<br>at Nov. 22, 1964<br>Typhoon "NITANG"<br>at Sept. 2, 1984                                 |  | ; Dr. Creager's recommendation as |
| Method                    | B.P.W's<br>Formula<br>(Extreme)                      | Creager's<br>Formula<br>(C = 100) $\underline{1}/$ | Rational<br>Method<br>(R.P = 1,000 yrs)  | From Traces<br>of Historic<br>Floods in<br>Bohol  | From the<br>Probable Maxi-<br>mum Precipitation                        | C = 100 is Dr. Cre                |
| Step                      | The Prime  | Verif. 1   | Veif. 2  | Verif. 3  | Verif. 4   | Note: 1.                          |

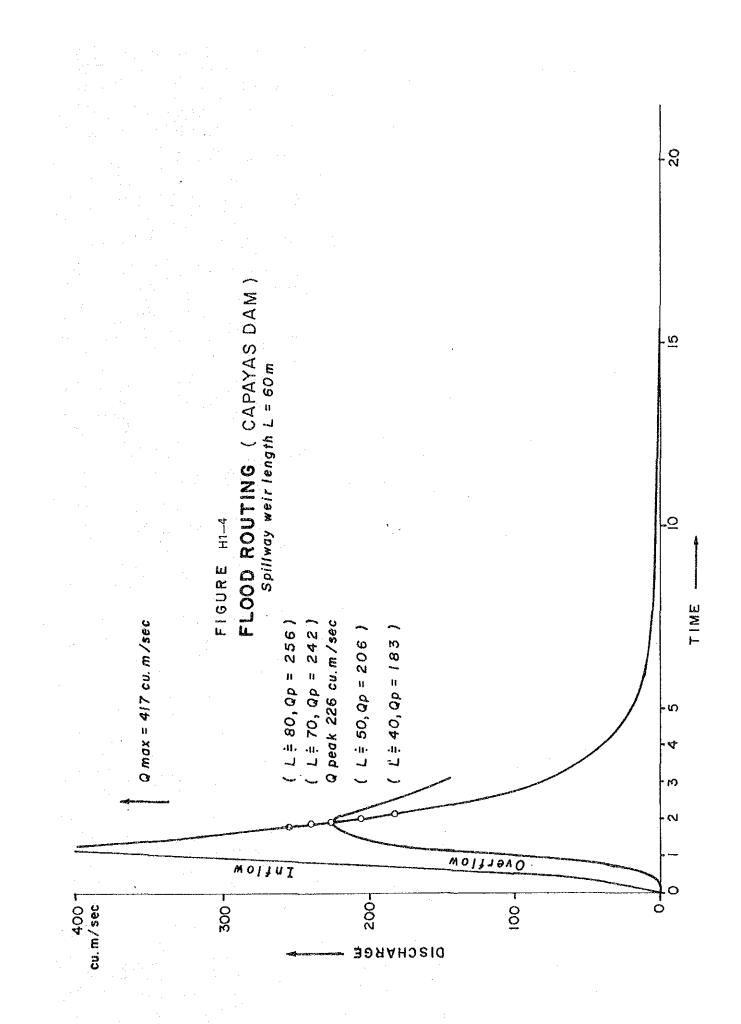
COMPARATIVE ESTIMATION OF DESIGN FLOOD (BAYONGAN)

TABLE H1-2

| Method  | Description   | Max Discharge  | Equivalent<br>Creager 's | Damorke  |
|---|---|--|--------------------------|--|
|   | $Q_{max} = \frac{150 \cdot A}{VA + 13}$   | 1 8 .  | 17                       | A; Catchment Area<br>14.6 sq.km  |
|   | Qmax = 46CA(0.894A-0.048)   | 405 cu.m/ sec or<br>27.7 cu.m/sec/sq.km                | 75                       | Q; in cu.ft/sec<br>A; in sq. mile  |
| l]<br>1,000 yrs)                                | Qmax = $\frac{1}{3.6} \cdot f \cdot r_t \cdot A$<br>With the Rainfall data<br>at Dagohoy<br>1957 - 84 | 369 cu.m/sec or<br>25.3 cu.m/sec/sq.km                 | é,                       | f = 0.9<br>$r_{t} = \frac{R24}{24} \left(\frac{24}{T}\right)^{0.6}$<br>$= \frac{405.5}{24} \left(\frac{24}{1.2}\right)^{0.6}$<br>= 1.01  mm/hr<br>$T = 200A^{0.22}r_{t}^{-0.55}$ |
|   | Typhoon "DELILAH:<br>at Nov. 22, 1964   | 2,219 <sup>3</sup> /cu.m/sec or<br>3.80 cum./sec/sq.km | 40.7                     |  |
|   | Typhoon "NITANG"<br>at Sept. 2, 1984  | l,410 <sup>3/</sup> cu.m/sec<br>2.41 cu.m/sec/sq.km    | 25.9                     |  |
| From the<br>Probably Maxi-<br>mum Precipitation | 1   | ſ  | 1                        | Meteorological P.N.P may<br>be only about 200 mm/day<br>405.5 $\gg$ 200  |



H-10



H-11

Results of flood routings are shown in FIGURE H1-3 (Bayongan) and FIGURE H1-4 (Capayas).

#### 1,3 Hydromechanical Analysis

a) Bayongan Dam

Flow condition of the Bayongan dam spillway at the peak discharge (20 cu.m/s) is summarized in TABLE H1-4.

Discharge capacity of the Bayongan dam intake in various waterhead is shown in FIGURE H1-5. Diversion capacity of the intake tunnel during dam construction is also described in this figure.

b) Capayas Dam

Flow condition of the Capayas dam spillway at the peak discharge (226 cu.m/s) is summarized in TABLE H1-5.

Discharge capacity of the Capayas dam intake in various waterhead is shown in FIGURE H1-6. Diversion capacity of the intake conduit during the dam construction is also described in the figure.

#### 1.4 Stability Analysis

In order to estimate a degree of safety against assumed failure of slope of earth dam, the standard method of slip circle which applies the following equations are generally used.

 $Fs = \frac{\Sigma(C \cdot 1 + (N-Ne) \tan \phi)}{\Sigma(T + Te)} \text{ or }$   $Fs = \frac{\Sigma(C' \cdot 1 + (N-u-Ne) \cdot \tan \phi')}{\Sigma(T + (N-u-Ne) \cdot \tan \phi')}$ 

 $\Sigma(T + Te)$ 

where Fs; Factor of safety

C; Cohesion, on the basis of total stress, of materials on the slip circle (t/sq.m)

C'; Ditto on the basis of effective stress

1; Base length of slice (m)

N; Normal force of slice (t)

Ne; Normal force of seismic load (t)

u; Pore pressure acting on slip circle (t)

 $\phi$ ; Internal friction angle, on the basis of total stress,

of materials on the slip circle (degree)

 $\phi$ '; Ditto on the basis of effective stress

T; Tangential force of slice (t)

Te; Tangential force of seismic load (t)

The factor of safety shall be more than 1.2 in normal case, but in particular case such as rapid drawdown, it could be acceptable if it is more than 1.1.

According to the above equations, a computer program has been originated by the joint effort of the consultant and counterpart so that the office computer system (TRS-80) of PDD, NIA has functioned effectively.

Soil mechanical data applied to these analyses are described in TABLE H1-6 (Bayongan dam) and TABLE H1-7 (Capayas dam).

Results of computations prove that these proposed dam layouts are reasonable, as shown in TABLE H1-8 (Bayongan) and TABLE H1-9 (Capayas).

# FLOW CONDITION OF SPILLWAY

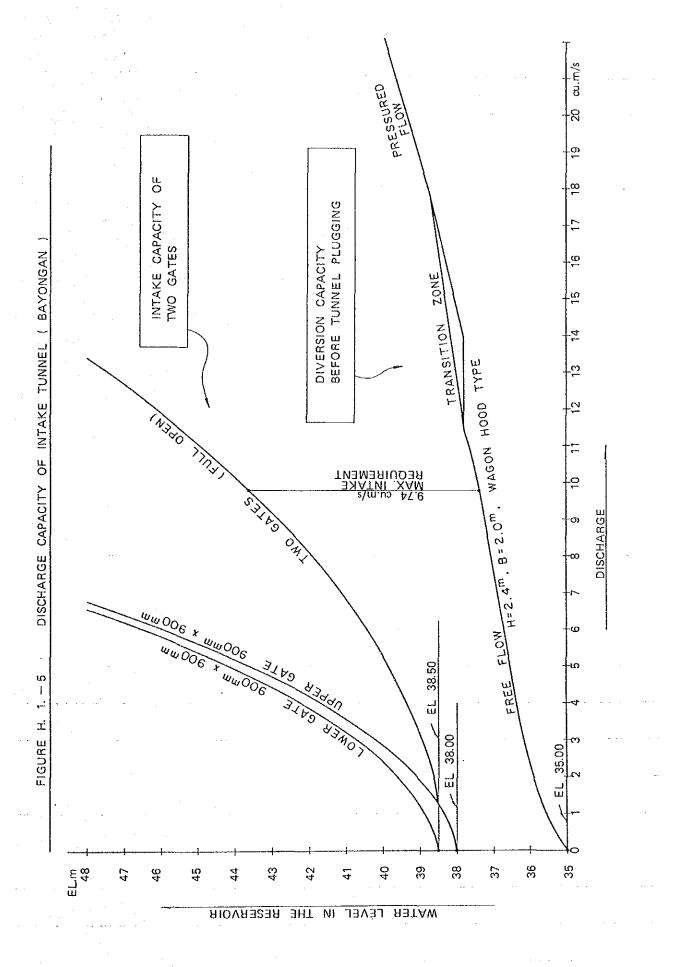
|                              |                      | (Ba          | yongan                                | Dam)                            |        |  |
|------------------------------|----------------------|--------------|---------------------------------------|---------------------------------|--------|--|
|                              |                      |              | Flow                                  |                                 | Froude |  |
| $\frac{\text{Station}}{(m)}$ | $\frac{Bottom}{(m)}$ | Width<br>(m) | $\frac{\text{Depth}}{(\mathfrak{m})}$ | $\frac{\text{Velocity}}{(m/s)}$ | Number | Remarks  |
| 0 + 0.00                     | EL 50.00             | 20           | 0.47                                  | 2.14                            | 1.00   | Crest  |
| 0 + 1.11                     | 49.43                | 20           | 0.22                                  | 4,51                            | 3.06   | Ŷ  |
| 0 + 50.00                    | 48,45                | 10           | 0.49                                  | 4.04                            | 1,84   | $\rangle$ Contraction  |
| 0 + 100.00                   | 47.45                | 5            | 0.93                                  | 4.28                            | 1.41   | ) and the second s |
| 0 + 117.56                   | 45.11                | 5            | 0.49                                  | 8.13                            | 3.70   |  |
| 0 + 130.00                   | 42.00                | . 5          | 0.38                                  | 10.5                            | 5.45   |  |
| 0 + 149.38                   | 39.32                | 5            | 0.37                                  | 10.9                            | 5.76   |  |
| 0 + 240.00                   | 39.60                | 5            | 0.53                                  | 7.54                            | 3,31   |  |
| 0 + 257.93                   | 34.85                | 5            | 0.46                                  | 8.69                            | 4.10   |  |
| 0 + 350.00                   | (19.50)              | 5            | 0.34                                  | 11.9                            | 6,56   | Flip Bucket  |

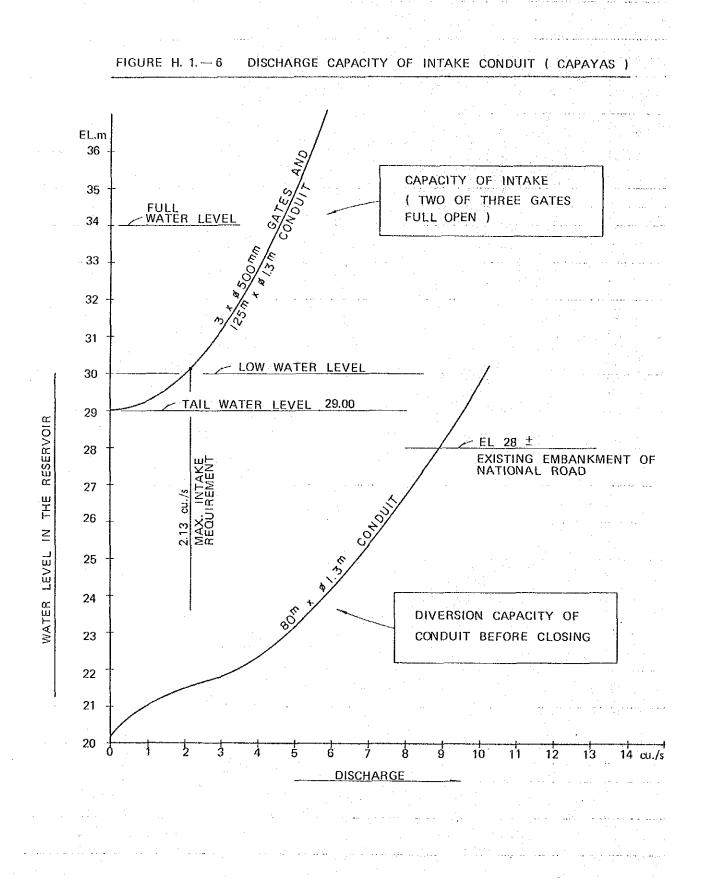
TABLE H1-5

# FLOW CONDITION OF SPILLWAY

# (Capayas Dam)

| Station (m)                                       | Bottom<br>(m)                      | Width<br>(m)       | Flow<br>Depth<br>(m) | Velocity<br>(m/s)    | Froude<br>Number          | <u>Remarks</u>                  |
|---|------------------------------------|--------------------|----------------------|----------------------|---------------------------|---------------------------------|
| CHUTE   |                                    |                    |                      |                      |                           | н<br>- стан                     |
| 0 + 0.00<br>0 + 3.79<br>0 + 13.00                 | EL 34.00<br>31.33<br>31.23         | 60<br>60<br>60     | 1.13<br>0.43<br>0.46 | 3.33<br>8.68<br>8.25 | 1.00<br>4.21<br>3.90      | Crest                           |
| 0 - 60.00<br>0 + 0.00<br>0 + 125.00<br>0 + 200.00 | 30.00<br>27.50<br>26.25<br>(22.50) | 6.5<br>8<br>8<br>8 | 4.33<br>3.33<br>2.35 | 6.52<br>8.48<br>12.0 | -<br>1.00<br>1.48<br>2.51 | Chute<br>Entered<br>Flip Bucket |





SOIL MECHANICAL DATA OF DAM BODY (BAYONGAN)

TABLE H1-6

|               |                           |            |                       |          |               |                             | Iotal Stress Base | ess base   | LTT C                           | Effective Stress Base | s Base             |
|---------------|---------------------------|------------|-----------------------|----------|---------------|-----------------------------|-------------------|------------|---------------------------------|-----------------------|--------------------|
| -,            | Specific Void Dry         | Void       | Dry                   | Moisture | Wet           | Saturated                   |                   |            | -                               |                       | Ratio of           |
| -             | Gravity<br>G <sub>s</sub> | Ratic<br>e | Ratio Density<br>e Yd |          | Density<br>Yt | Density<br>Y <sub>SAt</sub> | Cohesion<br>c     | Ι.F.Α<br>Φ | I.F.A Cohesion I.F.A<br>¢ c' ¢' | I.F.A Pc<br>¢'        | Pore Pressure<br>u |
|               |                           |            | (t/cu.m)              | (%)      | (t/cu.m)      | C                           | (t/sq.m)          | (Degree)   | Degree) (t/sq.m)                | (Degree)              | (%)                |
| Hilly gravel  | 2.6                       | 0,4        | . 1.86                | 10       | 2.05          | 2.14                        | 0                 | 43         | ı                               | I                     | ł                  |
|               | 2.6                       | 0.4        | 1.86                  | 10       | 2.05          | 2.14                        | 0                 | 43         | ŧ                               | I                     |                    |
| Core material | 2.5                       | 0.85       | 1.35                  | 30       | 1.76          | 1.81                        | ı                 | ŧ.         | 10                              | 15                    | 10                 |
|               | 2.55                      | 0.5        | 1.70                  | 15       | 1.96          | 2.03                        | S                 | 40         | 1                               | ł                     | t ·                |
| Dagohoy rock  | 2.65                      | 0.3        | 2.04                  | 0        | 2.04          | 2.27                        | 0                 | 45         | ı                               | ł                     | ł                  |
|               | 2.6                       | 0.25       | 2.08                  | 10       | 2.29          | 2.28                        | 0                 | 45         | ı                               | ı                     | ŧ                  |

Note: G<sub>s</sub>; Based on the soil tests and or on the general informations (see Annex C) e, w, c,  $\phi$ , c',  $\phi$ ', and u; ditto  $\gamma_d = G_s/(1 + e)$ ,  $\gamma_t = \gamma_d.(1 + w/100)$ ,  $\gamma_{sat} = (G_s + e)/(1 + e)$ 

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and the second 
SOIL MECHANICAL DATA OF DAM BODY (CAPAYAS)

TABLE H1-7

|                     |               |            |                                   |              |                         |           |  |              |                |             | しいかん いいくせいく シャー・シント・ド |
|---------------------|---------------|------------|-----------------------------------|--------------|-------------------------|-----------|--|--------------|----------------|-------------|-----------------------|
|                     | Specific      | Void       | Dry                               | Moisture Wet | Wet                     | Saturated |  |              |                |             | Ratio of              |
| Material<br>(Zone)  | Gravity<br>Ge | Ratio<br>e | Gravity Ratio Density<br>Gs. e Yd |              | Content Density<br>w Yt |           | Density Cohesion I.F.A Cohesion I.F.A Ysat C & & C' & C' | Г. Р. А<br>ф | Cohesion<br>c' | I.F.A<br>¢' | Por                   |
|                     |               |            | (t/cu.m)                          | (%)          | (t/cu.m)                |           | (t/sq.m) (Degree) (t/sq.m) (Degree)                      | (Degree)     | (t/sq.m)       | (Degree)    | (%)                   |
| Homogeneous<br>fill | 2.55          | 2.55 0.70  | 1.50                              | 25           | 1.88                    | 16.1      | 3  | 3            | ស              | 10          | 10                    |
| Toe drain           | 2.60          | 0.40       | 2.60 0.40 1.86                    | 10           | 2.05                    | 2.14      | 0  | 43           | I              | J           | <b>1</b>              |
|                     | ۰.            |            |                                   |              |                         |           |  |              |                |             |                       |

tests and or on the general informations [see Annex C] ,  $\gamma_t = \gamma_d (1 + w/100)$ ,  $\gamma_{sat} = (G_s + e)/(1 + e)$ and u; ditto 1105 อ ເຮີ based or  $\gamma d = G_S$  (1) е, w. с, ф NOTE

### TABLE 11.1.-8 (Sheet No.1/8)

### SLOPE STABILITY ANALYSIS

(STANDARD METHOD OF SLICES)

#### BAYONGAN DAM

UPSTREAM SLOPE : 3.25:1

DOWNSTREAM SLOPE: 2.25:1

\*\* MINIMUM FACTOR OF SAFETY \*\*

|   |     | - X -      | OF CENTER           | RADIUS              | FACTO:<br>OF |
|---|-----|------------|---------------------|---------------------|--------------|
| NO.                                     | NO. | ·(M)       | (M)                 | (M)                 | SAFET        |
| ๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛ |     |            | <b>৵</b> ৵৵৵৵৵৵৵৵৵৵ | <u>^</u> ~~~~~~~~~~ | ~~~~~~~      |
|   |     | ** UPSTREA | AM FACE **          |                     |              |
| 1                                       | 41  | 70         | 80                  | 40                  | 1.21         |
| 2                                       | 41  | 70         | 80                  | 40                  | 2.21         |
| 3                                       | 41  | 70         | 80                  | 40                  | 1.21         |
| 4                                       | 41  | 70         | 80                  | 40                  | 1.15         |
| a a de la                               |     | ** DOWNSTR | EAM FACE **         |                     |              |
| 1                                       | 75  | 180        | 80                  | 65                  | 1.50         |
| 2                                       | 86  | 180        | 110                 | 9Ø                  | 2.25         |

Note: With Earthquake (Seismic Force Coefficient, K = .20)

Number of Slip Circles Analyzed for Each Case; Upstream Face - 88 Downstream Face - 87

#### \*\* EXPLANATION \*\*

Case 1 - Reservoir is at Normal Water Level and Seepage is Steady.

Case 2 - End of Construction (there is residual construction pore pressure).

Case 3 - Reservoir is at Intermediate Water Level and Seepage is Steady.

Case 4 - Rapid Drawdown (from normal water level to low water level - there is residual pore pressure).

### TABLE H.1.-8 ( Sheet No.2/8 )

INPUT DATA

COORDINATES OF CENTER OF SLIP CIRCLE (X,Y):

|                              | Vestream | Downstream          |
|------------------------------|----------|---------------------|
| Minimum X - Meters           | 50       | 150                 |
| Maximum X - Meters           | 80       | 180                 |
| Increment of X - Meters      | 10       | 10                  |
| Minimum Y - Meters           | 80       | 80                  |
| Maximum Y - Meters           | 110      | 110                 |
| Increment of Y - Meters      | 10       | iØ                  |
|                              |          | · · · · · · · · · · |
| INCREMENT OF RADIUS - Meters |          | 5                   |
| SLICE THICKNESS - Meters     |          | 2                   |
| SEISMIC FORCE COEFFICIENT, K | •        | 20                  |
|                              |          |                     |

| ZONE  | MOIST<br>DENSITY | SATURATED<br>DENSITY | COHESION                                | ANGLE OF<br>INT. FRIC. | CONST. PORE<br>PRESSURE                 |
|-------|------------------|----------------------|---|------------------------|---|
| NO.   | (T/cu.m.)        | (T/cu.m.)            | (T/sq.m.)                               | (Degrees)              | (Per cent)                              |
| *~~~~ | ~~~~~~~~~~~~~    | ๛๛๛๛๛๛๛๛๛๛๛          | ๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛ | ~~~~~~~~~~~            | ๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛ |
| 1     | 2.05             | 2.14                 | 0.00                                    | 43.0                   | Ø                                       |
| 2     | 2.05             | 2.14                 | 0.00                                    | 43.Ø                   | Ø                                       |
| 3     | 1.76             | i.8i                 | 10.00                                   | 15.0                   | <b>- 1 Ø</b>                            |
| 4     | 2.05             | 2.14                 | 0.00                                    | 43.Ø                   | Ø                                       |
| 5     | 1.96             | 2.03                 | 5.00                                    | 40.0                   | Ø                                       |
| 6     | 2.04             | 2.27                 | 0.00                                    | 45.Ø                   | Ø                                       |
| 7     | 2.29             | 2.28                 | 0.00                                    | 45.0                   | Ø                                       |

\*\* SOIL MECHANICAL DATA OF EACH ZONE \*\*

Note: Zone No. 7 is the roundation.

### TABLE H.1.-8 (Sheet No.3/8)

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SLOPE STABILITY ANALYSIS \*\* بهد جذ

|      |    |      |      | · · ·  |
|------|----|------|------|--------|
| Name | ٥ť | Dami | 'BA' | YONGAN |

.

Location + BOHOL PROVINCE

Type of Dam: EARTHFILL Face of Dam: UPSTREAM Slope : 3.25:1

\*\*\* WITH EARTHQUAKE \*\*\*

|          | C008  | RDINATE      | S OF CENTER      |        | FAC                                    | TORO          | FSAFE                                   | ТΥ          |
|----------|---|--------------|------------------|--------|--|---------------|---|-------------|
| NQ.      |   | ~ X —<br>(M) | - :Y -<br>(M)    | (M)    | CASE 1                                 | CASE 2        | CASE 3                                  | CASE        |
| ~~~~~~   | ~~~~  | ~~~~~~       | ๛๛๛๛๛๛๛๛๛๛๛<br>๛ | ~~~~~~ | ·~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | ~~~~~~~~~     | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | ~~~~~~      |
| 1        |   | 50           | 80               | 45     | 1.28                                   | 2.41          | 1.28                                    | 2.24        |
| 2        |   | 50           | 80               | 50     | i 35                                   | 2.61          |   |             |
| 3        |   | 50           | 80               | 55     |  |               | 1.35                                    | 1.66        |
|          | a sainte de la companya de la |              |                  |        | 1.36                                   | 2.61          | 1.35                                    | 1.54        |
| 4        |   | 50           | 80               | 60     | 1.47                                   | 2.81          | 1.45                                    | 1.66        |
| . 5      |   | 50           | 80               | 65     | 1.52                                   | 2.92          | 1.49                                    | 1.67        |
| at a     |   |              | •                |        | 1.28*                                  | ≥.41×         | 1.28*                                   | 1.50        |
| 6        |   | 50           | 90               | 55     | 1.37                                   | 2.66          | 1.37                                    | .2.07       |
| . 7      |   | 50           | 92               | 60     | 1.34                                   | 2,58          | 1.34                                    | 1.60        |
| . 8      |   | 50           | 90               | 65     | 1.34                                   | 2.56          | 1.33                                    | i.53        |
| 9        |   | 50           | 70               | 70     | 1.44                                   | 2.75          | 1.42                                    | 1.61        |
| 10       |   | 50           | 90               | -75    | 1.49                                   | 2.85          | 1.46                                    | 1.6         |
|          |   |              |                  |        | 1.34*                                  | 2.56*         | 1.33*                                   | i.5         |
|          |   | ·. ·· ·      |                  |        | 1.34*                                  | 2,30*         | 1,00*                                   | 1.1         |
| 11       |   | 50           | 100              | 65     | 1.43                                   | 2.82          | 1.43                                    | 2.0         |
| 12       |   | 50           | 100              | 7Ø     | 1.33                                   | 2.55          | 1.33                                    | 1.54        |
| 13       |   | 50           | 100              | 75     | 1.33                                   | 2,53          | 1.32                                    | 1.4         |
| 14       |   | 50           | 100              | 80     | 1.42                                   | 2.71          | 1.40                                    | 1.5         |
| 15       |   | 50 .         | 100              | 85     | 1,56                                   | 2,85          | 1.53                                    | 1.69        |
|          | 1 - E   |              |                  |        | 1.33*                                  | 2.53*         | 1.32*                                   | 1.4         |
|          |   |              | * .              |        |  | _             |   |             |
| 16       |   | 50           | 110              | 75     | 1.41                                   | 2.77          | 1.41                                    | 1.79        |
| 17       |   | 50           | 110              | 80     | 1.32                                   | 2.51          | 1.33                                    | 1.4         |
| 18       |   | 50           | 110              | 85     | 1.31                                   | 2,50          | 1.31                                    | 1.4         |
| 19       |   | 50           | 110              | 90     | 1.47                                   | 2.74          | 1.46                                    | 1.6         |
| 20       |   | 50           | 110              | 75     | 1.57                                   | 2.93          | 1.53                                    | 1.7         |
|          |   |              | -                |        | 1.31*                                  | 2.50*         | 1.31*                                   | 1.4         |
|          |   | 10           |                  | A 19   | 1 40                                   | 2.75          | 1.40                                    | 1.5         |
| 21       |   | 60           | 80               | 45     | 1.40                                   | 2.62          | 1.35                                    | 1.4         |
| 22       |   | 60           | 80               | 50     | 1.36                                   |               |   | 1 4         |
| 23       |   | 60           | 80               | 55     | 1.36                                   | 2.63          | 1.34                                    |             |
| 24       |   | 60           | 80               | 60     | 1.46                                   | 2.83          | 1.43                                    | 1.5         |
| 25       |   | 60           | 80               | 65     | 1,58<br>1,36*                          | 2.93<br>2.62* | 1.54<br>1.34*                           | 1.7         |
|          |   |              |                  |        | 1.30*                                  |               |   | • •         |
| 26       |   | 60           | 90               | 55     | 1.37                                   | 2.64          | 1.37                                    | 1.4         |
| 27       |   | 60 .         | 90               | 60     | 1.34                                   | 2.56          | 1.33                                    | 1.4         |
| 28       |   | 60           | 90               | 65     | 1.34                                   | 2.57          | 1.32                                    | 1.4         |
| 29       |   | 60           | 90               | 70     | 1.51                                   | 2.82.         | 1.48                                    | 1.6         |
| 30       |   | 60           | 90               | 75     | 1.60                                   | 2.93          | 1.55                                    | . 1.7       |
| <u> </u> |   |              |                  |        | 1.34*                                  | 2.56*         | 1.32*                                   | <b>i.</b> 4 |
|          |   |              |                  |        |  | ~ - <i>i</i>  |   | 1 7         |
| 31       |   | 60           | 100              | 65     | 1.34                                   | 2.56          | 1.35                                    | 1.3         |
| 32       | - '   | 60           | 100              | 70     | 1.32                                   | 2.52          | 1.33                                    | 1.4         |
| 33       | • *   | 60           | 100              | 75     | 1.37                                   | 2.59          | 1.37                                    | 1.4         |
| 34       |   | 60           | 100              | 80     | 1.53                                   | 2.80          | 1.50                                    | 1.6         |
| 35       |   | 60           | 100              | 85     | 1.61                                   | 2.94          | 1.56                                    | 1.7         |

# TABLE H.1.-8 (Sheet No.4/8)

|                 |             | ***               | WITH EART  | THQUAKE **    | *                                       |  | ti she       |
|-----------------|-------------|-------------------|--|---------------|---|--|--------------|
| NANANA<br>IRCLE | COORDINATES | OF CENTER         | RADIUS   | F A C         |   | SAFE   | ~~~~~<br>T Y |
| NQ.             | X           | - Y               |  | ~~~~~~~       | ๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛ | ~~~~~~~~~~~  | ~~~~~~       |
|                 | (M)         | (M)<br>~~~~~~~~~~ | (M)<br>~~~~~~~~  | CASE 1        | CASE 2                                  | CASE 3   | GASE         |
|                 |             |                   |  |               |   |  |              |
|                 |             | · ·               | e<br>Alexandre de la composición de la compo | 1.32*         | 2.52*                                   | 1.33*  | 1.39         |
| 36              | 60          | 110               | 75   | 1,32          | 2.50                                    | 1.36   | 1.35         |
| 30              | 60<br>60    | 110               | 80   | 1.31          | 2.48                                    | 1.33   | 1.37         |
| 38              |             | 110               | 85   | 1.48          | 2.68                                    | 1,47   | 1.58         |
|                 | 60          |                   |  |               |   | and the second |              |
| 39              | 60          | 110               | 70   | 1.55          | 2.79                                    | 1.52   | 1.71         |
| 40              | 60          | 110               | 75   | 1.62          | 2.98                                    | 1.57   | 1.81         |
|                 |             |                   |  | 1.31*         | 2.48*                                   | 1:33*  | 1.35         |
| 41              | 70          | 80                | 40   | 1.21          | 2.21                                    | 1.21   | 1.15         |
| 42              | 70          | 80                | 45   | 1.33          | 2.55                                    | 1.34   | 1.34         |
| 43              | 70          | 80                | 50   | 1.35          | 2.57                                    | 1.33   | 1.39         |
| 44              | 70          | - 80              | 55   | 1.35          | 2.64                                    | 1.34   | 1.44         |
|                 |             |                   |  | 20.00         |   | · · · ·  |              |
| 45              | 70          | 80                | 60   | 1.63          | 2.87                                    | 1.57   | 1.7          |
| 46              | 70          | 80                | 65   | 1.69          | 3.14                                    | 1.63   | 1.80         |
|                 |             |                   |  | 1.21*         | 2.21*                                   | 1.21*  | 1.15         |
| 47              | 70          | 90                | 50   | 1.21          | 2.22                                    | 1.29   | 1.15         |
| 48              | 70          | 90                | 55   | 1.31          | 2.48                                    | 1.34   | 1.30         |
| 49              | 70          | 90                | 60   | 1.32          | 2.54                                    | 1.33   | 1.3          |
| 50              | 70          | 90                | 65   | 1.55          | 2.82                                    |  |              |
|                 |             |                   |  |               |   | 1.52   | 1.6          |
| 51              | 70          | 90<br>80          | 70   | 1.58          | 2.81                                    | 1.53   | 1.7          |
| 52              | 70          | 90                | 75   | 1.67<br>1.21* | 3.10<br>2.22*                           | 1.61   | 1.19         |
|                 |             |                   |  |               |   |  |              |
| 53              | 70          | 100               | 60   | 1.21          | 2.22                                    | 1.38   | 1.15         |
| 54              | 70          | 100               | - 65   | 1.29          | 2.44                                    | 1.35   | 1.30         |
| 55              | 70          | 100               | 79   | 1.50          | 2.71                                    | 1.51   | 1.54         |
| 56              | 70          | 100               | 75   | 1.50          | 2.77                                    | 1.48   | 1.6          |
| 57              | 70          | 100               | 80   | 1.59          | 2,86                                    | 1.55   | 1.75         |
| 58              | 70          | 100               | 85   | 1.68          | 3.20                                    | 1.64   | 1.90         |
|                 |             |                   |  | 1.21*         | 2.22*                                   | 1.35*  | 1.1          |
| 80              | 78          | 110               |  |               |   |  |              |
| 59              | 70          | 110               | 70   | 1.21          | 2.23                                    | 1.44   | 1.1          |
| 60              | 70          | 110               | 75   | 1.40          | 2.54                                    | 1.48   | 1.4          |
| 61              | 70          | 110               | 80   | 1.51          | 2.73                                    | i.52   | 1.60         |
| 62              | 70          | 110               | 85   | 1,53          | 2.83                                    | 1.51   | 1.6          |
| 63              | 70          | 11Ø               | 90   | 1.60          | 2.91                                    | 1.57   | 1.8          |
| 54              | 70          | 110               | 95   | 1.69          | 3.29                                    | 1.67   | 2.04         |
|                 |             |                   |  | 1.21*         | 2.23*                                   | 1.44*  | 1.1          |
| 65              | 80          | 80                | 40   | i.23          | 2.27                                    | •  | 1.18         |
| 66              | 80          | 80                | 40   | 1.23          |   | 1.37   |              |
| 57              | 80          |                   |  |               | 2.45                                    | 1.34   | 1.30         |
|                 |             | 80                | 50   | 1.60          | 2.87                                    | 1.57   | 1.67         |
| 68<br>( 0       | . 80        | 80                | 55   | 1.61          | 2.98                                    | 1.56   | 1.74         |
| 69<br>77        | 80          | 80                | 60   | 1.65          | 3.04                                    | 1.60   | 1.87         |
| 70              | 80          | 80                | 65   | 1.76          | 3.54                                    | 1.73   | 2.1          |
|                 |             |                   | · .  | 1.23*         | 2.27*                                   | 1.34*  | 1.18         |
| 71              | 80          | 92                | 50   | 1.23          | 2.26                                    | 1.42   | 1.20         |
|                 |             |                   |  |               |   |  |              |

TABLE H.1.-8 ( Sheet No.5/8 )

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|      | · · · · |   |      |     |  |  |  |
|------|---------|---|------|-----|--|--|--|
| UPST | REA     | м | <br> | ÷ . |  |  |  |

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| Page | З |
|------|---|
|      |   |

| or a i namin |   |                                    |  |  |  |                        | Page   |
|--------------|---|------------------------------------|--|--|--|------------------------|--------|
|              |   | **)                                | WITH EAR                                     | THQUAKE **                             | *  |                        |        |
|              | COORDINATES                               |                                    |  | FAC                                    | TORO   |                        |        |
|              | (พิ)                                      | (M)                                | (M)  | CASE 1                                 | CASE 2                                       | ~~~~~~~~~~~<br>CASE `3 | čase   |
| ๛๛๛๛๛๛๛      | ۵، به | 2 M2 | <u>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,</u> | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | <u>~~~~~~~~</u> ~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | ~~~~~~                 | ~~~~~~ |
| 73           | 80  | 90                                 | 60   | 1.57                                   | 2.86   | 1.57                   | 1.68   |
| 74           | 80  | 90                                 | 65   | 1.61                                   | 2,99   | 1.58                   | 1.80   |
| 75           | 80.                                       | 90                                 | 70   | 1.64                                   | 3.04   | 1.59                   | 1,92   |
| 76           | 80  | 90                                 | 75   | 1.77                                   | 3.68   | 1.76                   | 2.20   |
| · ·          | · · ·                                     |                                    |  | 1.23*                                  | 2.26*  | 1.42*                  | 1.20   |
| 77           | 80  | 100                                | 60   | 1.24                                   | 2.27   | 1.46                   | 1.26   |
| 79           | 80  | 100                                | 65   | 1.58                                   | 2.75   | 1.63                   | 1.65   |
| 79           | 80  | 100                                | 70   | 1.60                                   | 2.93   | 1.60                   | 1.01   |
| 90           | 80  | 100                                | 75   | 1.62                                   | 3.06   | 1.60                   | 1.87   |
| 91           | 80  | 100                                | 80   | 1.65                                   | 3,12   | 1.61                   | 1.07   |
| 82           | 80  | 100                                | 85   | 1.79                                   | 3.81   | 1.80                   | 2.28   |
| ÷            | :   |                                    |  | 1.24 <del>×</del>                      | 2.27*  | 1.46*                  | 1.26   |
| 83           | 80  | 110                                | 70   | 1.64                                   | 2,69   | 1.83                   | 1.69   |
| 84           | 80  | 110                                | 75   | 1.57                                   | 2.87   | 1.63                   | 1.65   |
| 95           | 80  | 110                                | 80   | 1.63                                   | 2.99   | 1.64                   | 1.83   |
| 86           | 80  | 110                                | 85   | 1.65                                   | 3.18   | 1.65                   | 1.95   |
| 87           | 80  | 110                                | 90   | 1.67                                   | 3.20   | 1.64                   | 2.07   |
| 88           | 80  | 110                                | 75   | 1.83                                   | 3,94   | 1.84                   | 2.36   |
| 54           |   | * * ×                              | 1 - A  | 1,57*                                  | 2.69*  | 1.63*                  | 1.68   |

Note: \* - Minimum factor of safety in every center of slip circle.

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II-23

### TABLE H.1.-8 (Sheet No.6/8)

#### SLOPE STABILITY ANALYSIS \* \* $\times \times$

| Name  | ٥f   | Dami | BAYON | SAN     | •  |
|-------|------|------|-------|---------|----|
| Locat | tior | i i  | BOHOL | PROVINC | E) |

Type of Dam: EARTHFILL Face of Dam: DOWNSTREAM Slope : 2.25:1

والأخاص أعاصوا والم

\*\*\* WITH EARTHQUAKE \*\*\* A.----

2 2 2 2 2 2

| IRCLE<br>NO. | COORDINATES<br>- X -                        | OF CENTER   | RADIUS      | FACTOR OF SAFETY                        |              |  |
|--------------|---|-------------|-------------|---|--------------|--|
| NO.          | (M)   | (M)         | (M)         | CASE 1                                  | CASE :       |  |
| ~~~~~~       | <i>๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛</i> | ~~~~~~~~~   | ~~~~~~~~~~~ | ๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛ |              |  |
| 1            | 150   | 80          | 40          | 2.75                                    | 3.37         |  |
| 2            | 150   | 80          | 45          | 2.34                                    | 2.83         |  |
| 3            | 150   | 80          | 50          | 2.24                                    | 2.59         |  |
| 4            | 150   | 80          | 55          | 2.24                                    | 2.50         |  |
| 5            | 150   | 80          | 60          | 2.11                                    | 2.53         |  |
| 6            | 150   | 80          | 65          | 2.20                                    | 3.06         |  |
| 4            | 100   |             |             | 2.11*                                   | 2.50         |  |
|              |   | .*          |             |   |              |  |
| 7            | 150   | 90          | 45          | 17.32                                   | 20.57        |  |
| 8            | 150   | 90          | 50          | 2.85                                    | 3.51         |  |
| 9            | 150   | 90          | 55          | 2.36                                    | 2.80         |  |
| 10           | 150   | 90          | 50          | 2.27                                    | 2.63         |  |
| 11           | 150   | 92)         | 65          | 2.25                                    | 2.57         |  |
| 12           | 150   | 90          | 70          | 2.15                                    | 2.67         |  |
| 13           | 150   | 90          | 75          | 2.21                                    | 3.21         |  |
|              |   |             |             | 2.15*                                   | 2.57         |  |
| . 14         | 150   | 100         | 55          | 6.31                                    | 7.61         |  |
| 15           | 150   | 100         | 60          | 2.69                                    | 3,34         |  |
| 16           | 150   | 100         | 65          | 2.36                                    | 2.83         |  |
| 17           | 150   | 100         | 70          | 2.27                                    | 2.69         |  |
| 18           | 150   | 100         | 75          | 2.24                                    | 2.65         |  |
| 19           | 150   | 100         | 80          | 2,14                                    | 2.75         |  |
| 20           | 150   | 100         | 85          | 2.22                                    | 3.33         |  |
|              | 130   |             | 32          | 2.14*                                   | 2.65         |  |
| 21           | 150   | 110         | 45          | 4 70                                    | 5 70         |  |
| 21           |   |             | 65          | 4.70                                    | 5.78         |  |
|              | 150   | 110         | 70          | 2.71                                    | 3.33         |  |
| 23           | 150   | 110         | 75          | 2.38                                    | 2.87         |  |
| 24<br>25     | 150   | 110         | 80          | 2.33                                    | 2.82         |  |
|              | 150   | 110         | 85          | 2.29                                    | 2.77         |  |
| 26<br>27     | 150<br>150                                  | 110<br>110  | 90          | 2.17                                    | 2.88         |  |
| <u>,</u>     | 1, 1, 43                                    | 110 .       | 95          | 2.24                                    | 3.46<br>2.77 |  |
|              |   |             |             |   |              |  |
| 28           | 160   | 80          | 40          | 14.52                                   | 17.27        |  |
| 29           | 160   | 80          | 45          | 2.54                                    | 3.12         |  |
| 30           | 160   | 80          | 50          | 2.14                                    | 2.65         |  |
| 31           | 160   | 80          | 55          | 2.03                                    | 2,40         |  |
| 32           | 160   | 80          | 60          | 1.91                                    | 2.37         |  |
| 33           | 160   | 80          | 65          | 1.87                                    | 2,52         |  |
|              |   |             | • • • •     | 1.87*                                   | 2.37         |  |
| 34           | 160   | φØ          | 50          | 6.51                                    | 7.81         |  |
| 35           | 160   | 90          | 55 .        | 2.41                                    | 2.97         |  |
| 36           | 160   | - <b>90</b> | 60          | 2.13                                    | 2.57         |  |
| 37           | 160   | 90          | 65          | 2.07                                    | 2.40         |  |

# TABLE H.1.-8 (Sheet No.7/8)

| DOWNSTREA   |   |                |            |  | Pagg   |
|---|---|----------------|------------|--|--------|
| ****  | ๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛ | *** WITH EART! |            | <sup>᠊</sup> ᠖ᡧᢣᡀ᠊᠙ᡧᠺᡁᡪᢋᠺᢦᡐ <b>ᠺᢧ</b> ᡕᢧᠬᢧ | ~~~~~  |
| CIRCLE<br>NO.   | COORDINATE                              | S OF CENTER    | RADIUS     | FACTOR OF                                  |        |
|   | (M)                                     | (M)            | (M)        | CASE 1                                     | CASE   |
|   |   |                | ~~~~~~~~~~ | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~     | nnninn |
| 38  | 15Ø                                     | 90             | 70         | 1.70                                       | 2.2    |
| 39  | 160                                     | 90             | 75         | 1.90                                       | 2.6    |
| t de la composición d | •                                       |                |            | 1.90*                                      | 2,3    |
| 40  | 160                                     | 100            | 60         | 3,93                                       | 4.7    |
| 41  | 160                                     | 100            | 65         | 2.33                                       | 2.8    |
| 42  | 160                                     | 100            | 70         | 2.12                                       | 2.5    |
| 43  | 160                                     | 100            | 75         | 2.07                                       | 2.4    |
| 44  | 160                                     | 100            | 80         | 1.93                                       | 2.4    |
| 45  | 160                                     | 100            | 85         | 1,93                                       | 2.7    |
|   |   |                |            | 1.93*                                      | 2.4    |
| 46  | 160                                     | 110            | 70         | 3,47                                       | , -    |
| 47  | 160                                     | 110            | 75         | 2,31                                       | 4.2    |
| 48  | 160                                     | 110            | 80         | 2.31                                       | 2.5    |
| 49  | 160                                     | 110            | 85         | 2.10                                       | 2.4    |
| 50  | 160                                     | 110            | 8J<br>70   | 1.96                                       | 2.5    |
| 51  | 160                                     | 110            | 75<br>75   | 1.94                                       | 2.8    |
|   |   |                |            | 1.94*                                      | 2.4    |
|   |   |                |            |  |        |
| 52<br>53  | 170                                     | 80             | 45         | 5.07                                       | 6.1    |
|   | 170                                     | 80             | 50         | 2.38                                       | 2.9    |
| 54<br>55  | 170<br>170                              | - 80<br>80     | 55<br>60   | 1.88                                       | 2.0    |
| 56  | 170                                     | 80             | 65         | 1.66                                       | 2.4    |
| 20  |   | 00             |            | 1.66*                                      | 2      |
| · .   | 4 7 8                                   |                | ~ ~        | 4 97                                       |        |
| 57  | 170                                     | 90             | 55         | 4.03                                       | 4.9    |
| 58  | 170                                     | 90             | . 60       | 2.16                                       | 2.4    |
| 59<br>60  | 170                                     | 60<br>60       | 65<br>70   | 1.75                                       | 2.1    |
| 51  | .170<br>170                             | 90<br>90       | 75         | 1.76                                       | 2.4    |
| D1 .  | 170                                     | 70             | 4.5        | 1.66*                                      | 2.2    |
|   |   |                |            |  |        |
| 62  | 170                                     | 100            | 65         | 3.39                                       | 4.     |
| 63  | 170                                     | 100            | 70         | 2.17                                       | 2.0    |
| 64 .  | 170                                     | 100            | 75         | 1.95                                       | 2.1    |
| 65.   | 170                                     | 100            | 80<br>85   | 1.69                                       | 2.4    |
| 66 .  | 170                                     | 100            |            | 1.69*                                      | 2.1    |
|   |   |                |            | `  | _      |
| 67  | 170                                     | 110            | 75         | 2.79                                       | 3.4    |
| 68  | 170                                     | 110            | 80         | 2.13                                       | 2.6    |
| 69  | 170                                     | 110            | 85         | 1 98                                       | 2.0    |
| - 70  | 170                                     | 110            | 90<br>85   | 1.77                                       | .2.1   |
| 71  | 170                                     | 110            | 95         | 1.67<br>1.67*                              | 2.4    |
|   |   |                |            |  |        |
| 72  | 180                                     | 80             | 50         | 3.42                                       | 4.     |
| 73  | 180                                     | 80             | 55         | 2.15                                       | 2.0    |
| 74  | 180                                     | 80             | 60         | 1.63                                       | 2.3    |

| <u> </u> | FABLE | H.1 | 8 | ( | Sheet | No.8/ | '8 | ) |  |
|----------|-------|-----|---|---|-------|-------|----|---|--|
|----------|-------|-----|---|---|-------|-------|----|---|--|

| DONNST   | n n le 'n M |   |   |  |   |   |   |   |   |  |
|----------|-------------|---|---|--|---|---|---|---|---|--|
| DOMINO I | RC.MOL      | ٠ | ٦ |  | ٠ | • | • | ٠ | • |  |

Page 3

|         |   | *** WITH EART                             | HQUAKE ***  |           |          |
|---------|---|---|-------------|-----------|----------|
| ~~~~~~~ | เฉล่างการการการการการการการการการการการการการก  | เฉลุลุลลุลลุลลุลลุลลุลลุลลุลลุลลุลลุลลุลล | ~~~~~~~~~~~ |           | ~~~~~~~~ |
| CIRCLE  | COORDINATES   | B OF CENTER                               | RADIUS      | FACTOR OF | SAFETY   |
| NO.     | X   | - Y -                                     |             | ~~~~~~~   | ~~~~~~   |
|         | (M)   | (M)                                       | (M)         | CASE 1    | CASE 2   |
| ~~~~~~~ |   | www.www.www.ww                            | ~~~~~~~~~   | ~~~~~~    | ~~~~~~   |
|         |   |   |             |           |          |
| 75      | 180   | 80  | 65          | 1.50      | 2.48     |
|         |   | · .                                       |             | 1.50*     | 2.35*    |
|         | e de la competition d | · .                                       |             |           |          |
| 76      | 180   | 90  | 60          | 3.11      | 3,80     |
| 77      | 180   | 90  | <u>م</u>    | 2.08      | 2.58     |
| 78      | 180   | 90  | 70          | 1.59      | 2.29     |
| 79      | 180   | 90  | 75          | 1.53      | 2.46     |
|         |   |   |             | 1.53*     | 2.29*    |
|         | · · · · · · · · · · · · · · · · · · ·   |   | -           |           |          |
| 66      | 180   | 100                                       | 70          | 2,83      | 3.46     |
| 91      | 180   | 100                                       | 75          | 1.97      | 2.44     |
| 82      | 180   | 100                                       | 80          | 1.60      | 2.27     |
| 83      | 180   | 100                                       | 85          | 1.56      | 2,45     |
|         |   |   |             | 1.56*     | 2.27*    |
|         | 1.1   |   |             |           |          |
| 84      | 190   | 110                                       | 80          | 2.50      | 3.06     |
| 85      | 180   | 110                                       | 85          | 1,98      | 2,46     |
| 86      | 180   | 110                                       | 90          | 1.61      | 2.25     |
| 97      | 180   | i 10                                      | 95          | 1.56      | 2.44     |
|         |   | . •                                       |             | 1.56*     | 2.25*    |
|         |   |   |             |           |          |

Note: \* - Minimum factor of safety in every center of slip circle.

٠.

# SLOPE STABILITY ANALYSIS

(STANDARD METHOD OF SLICES)

### CAPAYAS DAM

UPSTREAM SLOPE : 3:1

DOWNSTREAM SLOPE: 2:1

# \*\* MINIMUM FACTOR OF SAFETY \*\*

| <br>~~~~~ | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | 21/2/21/21/21/21/21/21/21/21/21/21/21/21 |   |         |              |
|-----------|---|--|---|---------|--------------|
| CASE      | CIRCLE                                  | COORDINATES O                            | F CENTER                                | RADIUS  | FACTOR       |
| NO.       | NO.                                     | (M)                                      | (M)                                     | (M)     | OF<br>SAFETY |
| ~~~~      | *******                                 | ๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛  | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | <u></u> | ~~~~~~~~     |
|           | · · · · ·                               | ** UPSTREAM                              | FACE **                                 |         |              |
| <br>1     | 45                                      | 35                                       | 50                                      | 24.75   | 1.65         |
| 2         | 34                                      | 30                                       | 55                                      | 29.75   | 2.06         |
| З         | 45                                      | 35                                       | 50                                      | 24.75   | 1,56         |
| . 4       | 45                                      | 35                                       | 50                                      | 24.75   | 1.92         |
|           |   | ** DOWNSTREA                             | ⁴ FACE ★★                               |         |              |
| 1         | 29                                      | 65                                       | 55                                      | 29.75   | 1.50         |
| 2         | 25                                      | 65                                       | 50                                      | 24.75   | 1.71         |
|           |   |  |   |         |              |

**ᡧᡐᡐᡧᢤᡧ᠔ᡧᡐᡐᡐᡐᡐᡐᡐ᠔ᡧᡐᡐᢑ᠔ᡧ᠔ᢌᡐᡆ᠔᠔᠗ᡧ᠔᠔᠔᠔᠔᠔᠔᠔᠔᠔᠔᠔᠔᠔᠔᠔᠔᠔᠔᠔** 

Note: With Earthquake (Seismic Force Coefficient, K = .20)

Number of Slip Circles Analyzed for Each Case: Upstream Face - 65 Downstream Face - 49

#### \*\* EXPLANATION \*\*

.

| Case | i | ļ | Reservoir is at Normal Water Level and Seepage is Steady.                                      |
|------|---|---|--|
| Case | 2 |   | End of Construction (there is residual construction pore pressure).                            |
| Case | 3 |   | Reservoir is at Intermediate Water Level and Seepage is<br>Steady.                             |
| Case | 4 |   | Rapid Drawdown (from normal water level to low water level - there is residual pore pressure). |

# TABLE H.1.-9 ( Sheet No.2/7 )

INPUT DATA

COORDINATES OF CENTER OF SLIP CIRCLE (X,Y):

| •                          |     | Vrstre | am D                                     | )ownstrea | 1.Π1 |
|----------------------------|-----|--------|--|-----------|------|
| Minimum X - Meters         |     | 1.5    | ·<br>· · · ·                             | 60        |      |
| Maximum X - Meters         |     | 4Ø     |  | 80        |      |
| Increment of X - Meters    |     | 5      |  | 5         |      |
| Minimum Y - Meters         | · · | 40     |  | 40        |      |
| Maximum Y - Meters         |     | 55     | an a | 55        | -    |
| Increment of Y - Meters    |     | 5      |  | 5         |      |
|                            |     |        |  |           |      |
| INCREMENT OF RADIUS - Met: | 202 |        | 2.50                                     | · ·       |      |
| SLICE THICKNESS - Meter/s  |     |        | 1.00                                     |           | • •  |
| SEISMIC FORCE COEFFICIENT  | к   | · *    | .20                                      |           |      |
|                            |     |        |  |           |      |

### \*\* SOIL MECHANICAL DATA OF EACH ZONE \*\*

| ONE              | MOIST<br>DENSITY | SATURATED<br>DENSITY | COHESION  | ANGLE OF<br>INT. FRIC.                  | CONST. POR |
|------------------|------------------|----------------------|-----------|---|------------|
| NO,              | (T/cu.m.)        | (T/:u.m.)            | (T/sq.m.) | (Degrees)                               | (Per cent  |
| , <u>0</u> 00000 |                  | ~~~~~~~~~~~          |           | ๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛ | ~~~~~~~~~~ |
| Ø                | 1.00             | 1.00                 | 0.00      | 0.0                                     | Ø          |
| 1                | 1.88             | 1.91                 | 5.00      | 10.0                                    | 10         |
| 2                | 2.05             | 2.14                 | 0.00      | 43.0                                    | Ø          |
| з                | 0.00             | 0.00                 | 0,00      | 0.0                                     | Ø          |

# TABLE H.1.-9 ( Sheet No.3/7 )

# \*\* SLOPE STABILITY ANALYSIS \*\*

| Name of Dam: CAPAYAS      |  | Type of | Dam  | EARTHEILL |
|---------------------------|--|---------|------|-----------|
| Location   BOHOL PROVINCE |  | Face of | Dam: | UPSTREAM  |
|                           |  | Slope   | 1    | 3:1       |

# \*\*\* WITH EARTHQUAKE \*\*\*

| CIRCLE<br>NO. | COORDINATES | RDINATES OF CENTER RADIUS |         | FACTOR OF SAFETY                       |        |               |   |  |
|---------------|-------------|---------------------------|---------|--|--------|---------------|---|--|
|               | (M)         | (M)                       | (M)     | CASE 1                                 | CASE 2 | CASE 3        | CASE 4                                  |  |
|               |             |                           |         | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ |        | ~~~~~~~~~~    | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ |  |
| 1             | 15          | 40                        | 14.75   | 6.97                                   | 6.15   | . 6, 97       | 9.77                                    |  |
|               |             |                           |         | 6.97*                                  | 6.15*  | 6.97*         | 9.77*                                   |  |
|               |             |                           |         |  |        |               | -                                       |  |
| 2             | 15          | 45                        | 19.75   | 6.34                                   | 5.60   | 6.34          | 8,43                                    |  |
|               |             |                           |         | 6.34*                                  | 5.60*  | 6.34*         | 8.43*                                   |  |
| З             | 15          | 50                        | 24,75   | 5.56                                   | 4.93   | 5,56          | 6.79                                    |  |
| 5             | 1.4         | 50                        | 24.73   | 5.56*                                  | 4.93*  | 5.56*         | 6.79*                                   |  |
| •             |             |                           | · •     |  |        |               |   |  |
| 4             | 15          | 55                        | 29.75   | 4.97                                   | 4.42   | 4.86          | 5.67                                    |  |
|               | •           |                           | •       | 4.97*                                  | 4.42*  | 4.86*         | 5.67*                                   |  |
| 5             | 20          | 40                        | 12.25   | 14.66                                  | 12,61  | 14.66         | 18.80                                   |  |
| л<br>6        | 20          | 40                        | 14.75   | 4.18                                   | 3.83   | 4.18          | 4:95                                    |  |
| U             | 20          | 10                        |         | 4.18*                                  | 3.83*  | 4.18*         | 4.95*                                   |  |
|               |             |                           | ••      |  |        |               |   |  |
| 7             | 20          | 45                        | 17.25   | 11.17                                  | 9.67   | 11,19         | 12.37                                   |  |
| 8             | 20          | 45                        | 19.75   | 3.82                                   | . 3,49 | 3.67          | · 4.20                                  |  |
|               | · · · ·     |                           |         | 3.82*                                  | 3.49*  | 3.67*         | 4、20*                                   |  |
| Ģ             | 20          | 50                        | 22,25   | 9.07                                   | 7.88   | 8,87          | 9.20                                    |  |
| 10            | 20          | 50                        | 24,75   | 3.43                                   | 3.15   | 3.16          | 3.59                                    |  |
|               |             |                           | 2.14.12 | 3.43*                                  | 3.15*  | 3.16*         | 3.59*                                   |  |
|               |             |                           |         |  |        |               |   |  |
| 11            | 20          | 55                        | 27.25   | 7.64                                   | 6.66   | 7.01          | 7.35                                    |  |
| 12            | . 20        | 55                        | 29.75   | 3.17                                   | 2.99   | 2.87          | 3.29                                    |  |
|               |             |                           |         | 3.17*                                  | 2.99*  | 2.97*         | 3.29*                                   |  |
| 13            | 25          | 40                        | 12.25   | - 5.53                                 | 4.99   | 5,23          | 5.32                                    |  |
| 14            | 25          | 40                        | 14.75   | 3.09                                   | 2.94   | 2.80          | 3.14                                    |  |
|               |             |                           |         | 3,09*                                  | 2,94*  | 2,80*         | 3.14*                                   |  |
| 1 m           |             | 45 .                      | 17.25   | 4.99                                   | 4.48.  | 4.40          | 4.63                                    |  |
| 15            | 25          | 45                        | 19.75   | 2,69                                   | 2.63   | 2.41          | 2.73                                    |  |
| 10            | 2.3         | -t J                      | 17.(2)  | 2.69*                                  | 2.63*  | 2.41*         | 2.73*                                   |  |
|               |             |                           | · .     |  |        |               | 21.03                                   |  |
| 17            | 25          | 50                        | 19.75   | 25.30                                  | 21.53  | 21.98<br>3.71 | 4.02                                    |  |
| 18            | 25          | 50                        | 22.25   | 4.26<br>2.41                           | 2.45   | 2.18          | 2.50                                    |  |
| 19            | , 25        | 50                        | 24.75   | 2,41*                                  | 2.45*  |               | 2.50*                                   |  |
|               | -<br>•      |                           | . •     |  | -      |               |   |  |
| . 20          | 25          | 55                        | 24.75   | 16.22                                  | 13.88  | 12.82         | 13.49                                   |  |
| 21            | 25          | 55                        | 27,25   | 3.68                                   | 3.61   | 3.25          | 3.60                                    |  |
| 22            | 25          | 55                        | 29,75   | 2.21                                   | 2.32   | 2.03          | 2.35<br>2.35*                           |  |
| · · ·         | · · · ·     |                           |         | 2.21*                                  | 2.32*  | 2.03*         | *دد.×                                   |  |
| 23            | 30          | 40                        | 9.75    | 8.49                                   | 7.49   | 6.72          | 7.21                                    |  |
|               |             |                           |         |  |        |               |   |  |

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| TABLE | H.19 | (Sheet | No.4/ | 7:) |
|-------|------|--------|-------|-----|
|-------|------|--------|-------|-----|

|              |       | .*                |   |   |  |  | an a  |   |
|--------------|-------|-------------------|---|---|--|--|---|---|
|              |       |                   |   |   |  |  |   |   |
|              |       |                   | TABLE H.1                               | 9 (She                                  | et No.4/7                              | ) ka s                                   |   |   |
| PSTREA       | м     |                   |   | •                                       |  | an a |   | Page  |
| •            |       | . •               | **                                      | * WITH EAR                              | THOUAKE **                             |  |   |   |
| ~~~~         |       | ******            |   | ๛๛๛๛๛๛๛๛๛                               | ~~~~~~~~~                              | งสลุ่นกล่างกลาง                          |   |   |
| IRCLE<br>NO: |       | RDINATS<br>· X    | ES OF CENTE                             | R RADIUS                                |  | TOR 0                                    |   |   |
|              |       | (M)               | (M)                                     | (M)                                     | CASE 1                                 |  | CASE 3  |   |
| ~~~~~        | ~~~~~ | ~~~~              | ๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛ | .~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | <u></u>                                  | ~~~~~~~~~   | <u>un un u</u> |
| 24           |       | 30                | 40                                      | 12.25                                   | 3.50                                   | 3.45                                     | 2,98  | 3.27  |
| 25           |       | 30                | 40                                      | 14.75                                   | 2.34                                   | 2.49                                     | 2.08  | 2.35  |
|              |       | •                 |   |   | 2.34*                                  | 2,49*                                    | 2.08*   | 2.35  |
| 26           |       | 30                | 45                                      | 14.75                                   | 6.62                                   | 6.15                                     | 5.29  | 5.90  |
| 27           |       | 30                | 45                                      | 17.25                                   | 3.06                                   | 3.16                                     | 2.68  | 3.02  |
| 28           |       | 30                | 45                                      | 19.75                                   | 2.03<br>2.03*                          | 2.24                                     | 1.85<br>1.85*   | 2.15  |
|              |       |                   | -                                       |   | ⊷.u0≭                                  | <u> </u>                                 | X • O J *   |   |
| 29           |       | 30                | 50                                      | 19.75                                   | 5.58                                   | 5.60                                     | 4.72  | 5.40  |
| 30           |       | 30                | 50                                      | 22.25                                   | 2.61                                   | 2.81                                     | 2.35  | 2.69  |
| 31           |       | 30                | 50                                      | 24.75                                   | 1.87<br>1.87*                          | 2.12<br>2.12*                            | 1.73<br>1.73*   | 2.04  |
| •            |       |                   | · .                                     |   |  |  |   |   |
| 32           |       | 30                | 55                                      | 24.75                                   | 4.66                                   | 4.93                                     | 4.10  | 4.77  |
| 33           |       | 30                | 55                                      | 27.25                                   | 2.41                                   | 2.68<br>2.06                             | 2.21  | 2.56  |
| 34           |       | 30                | 55                                      | 29.75                                   | 1.78<br>1.78*                          | 2.06*                                    | 1.00  | 1.98  |
|              |       |                   | 1                                       |   |  |  |   |   |
| 35           |       | 35                | 40                                      | 9.75                                    | 4.10                                   | 4.47                                     | 3.51  | 4.28  |
| 26           |       | 35                | 40                                      | 12.25                                   | 2.54                                   | 2.94<br>2.30                             | 2.28  | 2.76  |
| 37           |       | 35                | 40                                      | 14.75                                   | 1.90<br>1.90*                          | 2.30*                                    | 1.74  | 2.12  |
|              |       |                   |   |   |  |  | 10.01   | 4   |
| 38<br>38     |       | 35<br>35          | 45<br>45                                | 12.25<br>14.75                          | 11.42<br>3.36                          | 12.61<br>3.82                            | 10.24<br>3.04   | 12.45   |
| 40           |       | 35                | 45                                      | 17.25                                   | 2.17                                   | 2,58                                     | 2.00  | 2.41  |
| 41           |       | 35                | 45                                      | 17.75                                   | 1.74                                   | 2.15                                     | 1.63  | 1.98  |
|              |       |                   |   |   | 1.74*                                  | 2.15*                                    | 1.53*   | 1.98  |
| 42           |       | 35                | 50                                      | 17.25                                   | 8.33                                   | 9.67                                     | 7.86  | 9.5   |
| 43           |       | 35                | 50                                      | 19.75                                   | 3.01                                   | 3.53                                     | 2.80  | 3.40  |
| 44           |       | 35                | 50                                      | 22.25                                   | 2.03                                   | 2.46                                     | 1.90  | 2.3   |
| 45           |       | 35                | 50                                      | 24.75                                   | 1.65<br>1.65*                          | 2.08<br>2.08*                            | 1.56<br>1.56*   | 1.92  |
|              |       |                   |   |   |  |  |   |   |
| 46           |       | 35                | 55                                      | 22.25                                   | 6.39                                   | 7.61                                     | 6.17  | 7.5   |
| 47<br>48     |       | 35<br>35          | 55<br>55                                | 24.75<br>27.25                          | 2.83<br>2.01                           | 3.40<br>2.49                             | 2.66<br>1.90  | 3.2   |
| 49           |       | 35                | 55                                      | 27.75                                   | 1.66                                   | 2.14                                     | 1.58  | 1.9   |
|              |       |                   | н                                       |   | 1.66*                                  | 2.14*                                    | 1.58*   | 1.9   |
| 50           |       | 40                | 40                                      | 0.75                                    |  | 7 2 /                                    | ~ ~~  |   |
| 51           |       | 40                | 40                                      | 9.75<br>12.25                           | 2.74<br>2.09                           | 3,56<br>2,80                             | 2.73<br>2.02  | 3.4   |
| 52           |       | 40                | 40                                      | 14.75                                   | 1.75                                   | 2.43                                     | 1.68  | 2.2   |
|              |       |                   |   | t.                                      | 1.75*                                  | 2.43¥                                    | 1.68*   | 2.2   |
| 53           |       | 40                | 45                                      | 12.25                                   | 3.97                                   | 5.05                                     | 4.02  | 5.0   |
| -54          |       | 40                | 45                                      | 14.75                                   | 2.54                                   | 3.31                                     | 2.51  | 3.19  |
| 55           | . *   | 4Ø                | 45                                      | 17.25                                   | 1.93                                   | 2.61                                     | 1.87  | 2.44  |
| 56           |       | 40                | 45                                      | 19.75                                   | 1.66                                   | 2,35                                     | 1.60  | 2.14  |
|              |       |                   | •                                       | e transformation.                       |  |  | ана стана<br>Спортана<br>Спортана   |   |
|              |       | -                 | •                                       |   | · . ·                                  |  | 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - 1997 - | . • •   |
|              |       |                   | н.<br>Н                                 |   |  |  |   |   |
| ÷.,          |       | 1 <sup>90</sup> e |   | H-30                                    |  |  |   |   |
|              |       |                   |   | n-30                                    |  | · · ·                                    | La de la construcción de la constru |   |

# Таріт TABLE H.1.-9 ( Sheet No.5/7 )

Page 3

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| NO.      |  | DINATI<br>X - | ES OF | CENTE  | R RADIUS      | F A C                                  | $\begin{array}{ccc} T & O & R & O \\ \sim $ | F SAFE                                 | T Y   |
|----------|--|---------------|-------|--------|---------------|--|--|--|-------|
|          |  | (M)           |       | (M)    | (M)           | CASE 1                                 | CASE 2   | CASE 3                                 | CASE  |
| ~~~~~~~  | ~~~~·  | ~~~~~         |       | ~~~~~~ | ᠔ᠬᡐᡐᡐᡐᡐᡐᡆᠥᠧᡧᢦ | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | www.www.www.   | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | ~~~~~ |
|          |  |               | ·     | · •    |               | 1.66*                                  | 2.35×  | 1.60*                                  | 2.14  |
| 5.7      |  | 40            |       | 50     | 17.25         | 4 00                                   | 5.16   | 4.04                                   | 5,14  |
| 58       | ·  | 40            |       | 50     | 19.75 .       | 2.40                                   | 3.19   | 2.38                                   | 3.07  |
| 59       |  | 40            |       | 50     | 22,25         | 1.94                                   | 2.68   | 1.88                                   | 2.50  |
| 60       |  | 40            |       | 50     | 24,75         | 1.68                                   | 2.42   | 1.62                                   | 2.18  |
|          |  |               |       | •      |               | 1.68*                                  | 2.42*  | 1.62*                                  | 2.18  |
| 61       |  | 40            |       | 55     | 19.75         | 18.27                                  | 22.96  | 18.27                                  | 23.01 |
| 62       |  | 40            |       | 55     | 22,25         | 3.80                                   | 4.97   | 3.83                                   | 4,95  |
| 63       | · · · · ·  | 40            |       | 55     | 24.75         | 2.45                                   | 3.31   | 2.42                                   | 3,18  |
| 64       |  | 40            |       | 55     | 27.25         | 1,97                                   | 2,79   | 1,92                                   | 2,59  |
| 65       |  | 40            |       | 55     | 29.75         | 1.74                                   | 2.56   | 1.68                                   | 2.30  |
| 1 - A.L. | 1. 1   |               | 1     |        |               | 1.74*                                  | 2.56*  | 1.68*                                  | 2.30  |
|          | 1997 - 19 |               | ·     |        |               |  |  |  |       |

Note: \* - Minimum factor of safety in every center of slip circle.

| Name of Da<br>Location                       | INI CAPAYAS<br>I BOHOL PRO | VINCE                                   |  | e of Dam; E/<br>e of Dam; D(<br>pe ; 2) | WNSTREA |
|--|----------------------------|---|--|---|---------|
|  | *                          | ** WITH EARTH                           | 1@UAKE ***                             |   |         |
| CIRCLE                                       | COORDINATES                | OF CENTER                               | RADIUS                                 | FACTOR OF                               |         |
| NO.  | - X -<br>(M)               | - Y -<br>(M)                            | (M)                                    | CASE 1                                  | CASE    |
| <u>~~</u> ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | ᠈᠕᠕᠕᠕᠕᠕᠕᠕᠕᠕᠕᠕              | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ |         |
| 1  | 60                         | 40                                      | 9.75                                   | 2.57                                    | 2.9     |
| 2  | 60                         | 40                                      | 12.25                                  | 1.78                                    | 2.2     |
| з.   | 60                         | 40                                      | 14.75                                  | 1.58                                    | 1.8     |
|  | · .                        |   |  | 1.58*                                   | 1.9     |
| 4  | 60                         | 45                                      | 12.25                                  | 4.10                                    | 4.8     |
| 5  | 60                         | 45                                      | 14.75                                  | 2.34                                    | 2.7     |
| 6  | 60                         | 45                                      | 17.25                                  | 1.88                                    | 2.1     |
| 7  | 60                         | 45                                      | 19.75                                  | 1.53                                    | i.8     |
|  |                            |   |  | 1.53*                                   | 1.8     |
| 9  | 60                         | 50                                      | 17.25                                  | 3.82                                    | 4.6     |
| 9<br>9                                       | 60                         | 50                                      | 19.75                                  | 2.36                                    | 2.8     |
| 10   | 60                         | 50                                      | 22.25                                  | 1.85                                    | 2.1     |
| 11   | 60                         | 50                                      | 24.75                                  | 1.55                                    | 1.8     |
| * *  | 0.5                        |   |  | 1.55*                                   | 1.8     |
| 12   | 60                         | 55                                      | 22.25                                  | 3.60                                    | 4 4     |
| 13   | 60                         | 55                                      | 24.75                                  | 2.33                                    | 2.8     |
| 14   | 60                         | 55                                      | 27.25                                  | 1.89                                    | 2.2     |
| 15   | 60                         | 55                                      | 29.75                                  | 1.59                                    | 1.7     |
|  |                            |   |  | 1.59*                                   | 1.9     |
| 16   | 65                         | 40                                      | 9.75                                   | 4.63                                    | 5.2     |
| 17   | 65                         | 40                                      | 12.25                                  | 2.33                                    | 2.4     |
| 18   | 65                         | 40                                      | 14.75                                  | 1.70                                    | 1.8     |
|  |                            |   |  | 1.70*                                   | 1.8     |
| 19   | 65                         | 45                                      | 14.75                                  | 3.50                                    | 3.9     |
| 20   | 65                         | 45                                      | 17.25                                  | 1.95                                    | 2.10    |
| 21   | 65                         | 45                                      | 19.75                                  | 1.57                                    | 1.7     |
|  |                            | · · · · ·                               |  | 1.57*                                   | 1.7     |
| 22   | 65                         | 50                                      | 17.25                                  | 23.80                                   | 27.7    |
| 23   | 65                         | 50                                      | 19.75                                  | 2.85                                    | 3.2     |
| 24   | 65                         | 50                                      | 22.25                                  | 1.86                                    | 2.0     |
| 25   | 65                         | 50                                      | 24.75                                  | 1.51                                    | i.7     |
|  |                            |   | · ·                                    | 1.51*                                   | 1.7     |
| 26   | 65                         | 55                                      | 22.25                                  | 8.51                                    | 10 0    |
| 27   | 65                         | 55                                      | 24.75                                  | 2.65                                    | 3.0     |
| 28   | 65                         | 55                                      | 27.25                                  | 1.81                                    | 2.0     |
| 29   | 65                         | 55                                      | 29.75                                  | 1.50                                    | 1.7     |
|  |                            | ·<br>· ·                                |  | 1.50*                                   | 1.7     |
| 30   | 70                         | 40                                      | 12.25                                  | 3.30                                    | 3.6     |
|  | 70                         | 40                                      | 14.75                                  | 2.15                                    | 2.2     |

# TABLE H.1.-9 ( Sheet No.6/7 )

# TABLE H.1.-9 (Sheet No.7/7)

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DOWNSTREAM.....

. . .

| <u> </u> | NO.     | COORDINATES            |                          | RADIUS                       | FACTOR O     |         |
|----------|---------|------------------------|--------------------------|------------------------------|--------------|---------|
|          | NOL     | (M)                    | - Y -<br>(M)             | (M)                          | CASE 1       | CASE    |
|          | ~~~~~~~ | <b>ᡣᡣᡧ᠕᠕᠕᠕᠕᠕᠕᠕᠕</b> ᠕᠕ | ᡣᡐᡧᠦᡐᡐᡐᡐᡐ <u>ᡐ</u> ᡐᡐᡐᡐᡐ | ᡃᢑ <b>ᡧᠬ᠅ᡧᠣ᠊ᠧᡊ</b> ᠈ᡧ᠕᠈ᠺᢧᡢᢖᡒ | ᠃ᠬ᠔ᠬᠬᡧᡳᡡᡐᡐᡐᡇ | ~~~~~~~ |
|          |         |                        |                          |                              | 2.15*        | 2,26    |
|          | 32      | 70                     | 45                       | 17.25                        | 2.89         | 3.09    |
|          | .33 .   | 70                     | 45                       | 19,75                        | 1.84         | 1.96    |
|          |         |                        |                          |                              | 1.84*        | 1,96    |
|          | 34      | 7Ø                     | 50                       | 19.75                        | 12.54        | 14.63   |
|          | 35      | 70                     | 50                       | 22.25                        | 2.43         | 2.62    |
|          | 36      | 70                     | 50                       | 24.75                        | 1.67         | i.8i    |
|          |         | •                      |                          |                              | 1.67*        | 1.81    |
| . 1      | 37      | 70                     | 55                       | 24.75                        | 4.59         | 7.68    |
|          | 38      | 70                     | 55                       | 27,25                        | 2,14         | 2.33    |
|          | 39      | 70                     | 55 <sup>°</sup>          | 29.75                        | 1.59         | 1.76    |
|          |         |                        |                          |                              | 1.59*        | 1.76    |
|          | 40      | 75                     | 40                       | 14,75                        | 2.41         | 2.80    |
|          |         | ·                      |                          |                              | 2.41*        | 2.80    |
|          | 41      | 75                     | .45                      | 17.25                        | 17.33        | 22,56   |
|          | 42      | 75                     | 45                       | 19.75                        | 2.41         | 2.62    |
|          |         | •                      |                          |                              | 2.41*        | 2,62    |
|          | 43      | 75                     | 50                       | 22,25                        | 7.52         | 8.77    |
|          | 44      | . 75                   | 50                       | 24.75                        | 2.20         | 2.35    |
| •        |         |                        |                          |                              | 2.20*        | 2.35    |
|          | 45      | 75                     | 55                       | 27,25                        | 4.70         | 5,48    |
|          | 46      | 75                     | 55                       | 29.75                        | 1.93         | 2.08    |
|          |         |                        |                          |                              | 1.93*        | 2.08    |
|          | 47      | 80                     | 45                       | 19.75                        | 2.78         | 3.32    |
|          |         |                        | 7                        |                              | ≥.78*        | 3.32    |
|          | 48      | 80                     | 50                       | 24.75                        | 3.49         | 4,12    |
|          |         |                        |                          |                              | 3.49*        | 4.12    |
|          | 49      | 80                     | 55                       | 29.75                        | 3.05         | 3.57    |
|          | -       | • •                    |                          |                              | J.05*        | 3.57    |

Note: \* - Minimum factor of safety in every center of slip circle.

#### CHAPTER II CANALS

#### 2,1 General

The project area is located in an undulated hilly area with elevetion of 40 m to 5 m and is incised by narrow valleys developed along the streams flowing down from south to north. The soils in the project area are composed of Ubay soil series which characterized by slightly coarse-textured surface soil underlaid by loamy or clayey but gravelly subsoils.

Irrigation canal systems are planned to take water directly from the proposed reservoirs and to distribute the irrigation water to existing paddy field expanded along the streams and hilly area to be reclaimed. In connection with irrigation canal system, drainage system is also provided using the existing streams. The Bayongan and Capayas dams are proposed as a water source of the project and main irrigation canals start these dam outlets to make up its distribution networks in the project area. Based on the topography and location of water sources, the project area is divided by the Soom -Bayan river into two irrigation systems, namely, Bayongan and Capayas.

Under these concepts, the Bayongan and Capayas systems are planned to cover an area of 4,140 ha with 112 service units and of 1,160 ha with 33 service units, respectively. Service unit of each irrigation system is demarcated by an area of 25 ha in minimum, 50 ha in maximum and about 36 ha on the average.

#### 2.2 Irrigation Canal System

#### 2.2.1 Function and Requirement of Canal

The proposed irrigation canal systems consist of main, lateral and sub-lateral canals. The layout of these canals is planned with understanding their respective functions and requirements.

Two main canals of Bayongan and Capayas are planned to secure the proper water distribution in the project area. The functions

of main canal are to convey irrigation water most economically and effectively from each dam to the proposed lateral canals.

The functions of lateral and sub-lateral canals are to deliver irrigation water from main canal and/or lateral canal to the head portions of service units. To facilitate an efficient water managemont, service units should preferably be supplied only from lateral or sub-lateral canals.

2.2.2 Canal Alignment

Prior to the field survey of irrigation canal route, preliminary canal alignment is made on a scale of 1/4,000 topographic maps. Modification of preliminary canal alignment was conducted on the said maps in accordance with the proposed land use, allowing service by gravity system and result of field survey.

The main irrigation canal to cover the Bayongan system area is placed between the Bayongan dam outlet and the Capayas reservoir and runs through a flat hilly area with the elevation of 40 m to 35 m. The water level of main canal is 37 m at the Bayongan dam outlet and the 34 m at the terminal point of main canal in the Capayas reservoir. Total length of the Bayongan main canal is designed at 12.45 km with maximum design discharge of 7.54 cu·m/sec. in crop maintenance period and of 9.74 cu·m/sec. in land soaking period.

The main irrigation canal to cover the Capayas system starts from the Capayas dam outlet and reaches near Ubay. The canal alignment is placed at the moderately undulated area having the elevation of 30 m to 25 m. The Capayas main canal is planned at the total length of 3.27 km with maximum design discharge at 1.65 cu·m/sec. for crop maintenance period and 2.13 cu·m/sec. for land soaking period.

Both of the main canals run mostly along the ridge area of hill and cross only a few streams. Canals are constructed with cut and fill portion and excavated materials can be used for filling materials. The alignment of lateral and sub-lateral irrigation canals are selected to run at the higher place of hilly area in order to cover service units as much as possible by the gravity system. 30 lines of lateral and sub-lateral canal with total length of 87.73 km are planned with a design discharge of 3.15 cu.m/sec. in maximum. The lateral and sub-lateral alignments can run also the flat hilly area with structures crossing a few streams.

The size of service area commanded by a lateral canal is designed from 160 ha to 1,700 ha consisting of 5 to 46 service units.

The diagram of irrigation networks is formed in accordance with the irrigation water requirement, demarcation of each service unit, proposed lateral canal alignment and irrigation systems.

Proposed irrigation canal alignment, irrigation system in lateral canalwise and proposed irrigation canal features are shown in FIGURE H2-1, FIGURE H2-2 and TABLE H2-1, respectively.

2.2.3 Design of Irrigation Canal

Trapezoidal cross section are designed for all the proposed canals. Design criteria prevailing in NIA are mainly adopted for the design of canal and related structures.

1) Design discharge

Design discharge for all the irrigation canals and related structures are obtained in compliance with the peak irrigation water requirement of 1.422 l/sec/ha in crop maintenance period. During the land soaking period, the peak irrigation water requirement is estimated at 1.837 l/sec/ha and excessive irrigation water compared with the crop maintenance period will be delivered using the canal freeboard.

2) Velocity

The maximum and the minimum permissible velocity are determined so as not to give the erosion and deterioration and not to allow the sedimentation and the growth of aquaplant and

moss in canals. Considering the above basic requirements, the canal velocities are determined as follows;

|                      | Max.       | <u>Min.</u> |
|----------------------|------------|-------------|
| Concrete Lined Canal | 1.0 m/sec. | 0.5 m/sec.  |
| Earth Canal          | 0.8 11     | 0.3 "       |

3) Roughness Coefficient

The Manning's Formula is used for determination of hydraulic properties of canals. Following roughness coefficient, "n" is applied;

|                      | Roughness   |
|----------------------|-------------|
|                      | Coefficient |
| Concrete Lined Canal | 0.015       |
| Earth Canal          | 0.025       |

#### 4) Freeboard

The freeboard in canals is determined as 40 percent of the water depth with the minimum of 0.30 m whichever is bigger.

5) Canal base width/water depth (B/h) ratio

The ratio of canal base width and water depth is used at 1 for concrete lined canal of which discharge is less than 4 cu·m/sec. and 2 for earth canal and concrete lined canal with discharge more than 4 cu·m/sec.

6) Side Slope

The inside slope of 1:1 is adopted for concrete lined canal with discharge less than 4 cu m/sec. and 1:1.5 for other size of canals. The outside slopes of 1:1.5 for embankment portion and 1:1 for cutting portion are used taking into account the soil conditions.

7) Berm Width

Berm width is taken with same length as canal height.

8) Lining of Canal

All the main canals with the total length of 15.72 km are lined with 10 cm thickness of plain concrete to check seepage

from the canal banks and bottom and to protect the canal section against erosion.

Twenty three types of canal section are proposed for the irrigation canal system. Hydraulic properties of each type are shown in attached drawing in main report.

2.2.4 Related Structures

A number of related structures are essential for full functions of canal. These structures are classified into measurement, distribution, regulation, conveyance and protection purpose.

1) Distributing and Measuring Structure

Head Regulator and Turnout are provided as a distributing structures of canals.

Head Regulator is installed to divert irrigation water from main canal to lateral canal. Neyrpic Orifice Module (so called "Distributor") is provided as a measuring divice of Head Regulator. The distributor is so designed as to be capable of constantly delivering a predetermined rate of flow regardless variations in the upstream water level.

Turnout is constructed for the diversion of irrigation water from lateral canal to sub-lateral canal or lateral canal and/or sublateral canal to service unit. As a measuring divice, constant head orifice is furnished at the inlet portion of turnout.

Following distributing structures are designed for canal systems;

|                     | Head Regulator<br>(places) | Turnout<br>(places) |
|---------------------|----------------------------|---------------------|
| Bayongan System     | ·                          |                     |
| Main canal          | 6                          | -                   |
| Lateral/Sub-lateral | -                          | 126                 |
| Capayas System      |                            | • •                 |
| Main canal          | 3                          | e e e               |
| Lateral/Sub-lateral | -                          | 36                  |
| Total               | 9                          | 162                 |

#### 2) Regulating Structure

Check and drops are provided for regulating of water level in the canal. A check is provided at the just downstream of distributing structure to maintain the required water level during the period of partial flow in the canal. There are three types of check; (1) check cum duckbill weir, (2) check cum drop and (3) check gate only. Type (1) of check cum duckbill weir is furnished in main canal in order to secure the function of distributor. Type (2) and (3) are installed in lateral and/or sub-lateral canal according to the site conditions.

To dissipate the excess energy in canals, vertical drops of 1.5 m or 1.0 m in water surface are provided for the canal design. Regulating structures required for the project are tabulated below;

|                     | Check            |     |     | Drop     |  |
|---------------------|------------------|-----|-----|----------|--|
|                     | $\overline{(1)}$ | (2) | (3) | (places) |  |
| Bayongan System     |                  |     |     |          |  |
| Main                | 5                | -   | -   |          |  |
| Lateral/Sub-lateral | -                | 44  | 13  | 84       |  |
| Capayas System      |                  |     |     |          |  |
| Main                | 2                | -   | -   | 1        |  |
| Lateral/Sub-lateral | -                | .4  | 8   | 28       |  |
| Total               | 7                | 48  | 21  | 113      |  |

3) Conveyance Structure

Crossing structures such as bridge, pipe crossing and syphon are installed to convey the irrigation water over or under road, rivér and stream. Pre-cast concrete pipe is used for crossing structures with a canal discharge of less than 1.0  $cu \cdot m/sec.$  and the concrete bridges for a discharge of more than 1.0  $cu \cdot m/sec.$  due to decrease the head losses of irrigation canals.

For the syphon barrel, pre-cast concrete pipe is also used because of the design discharge estimated less than 1.0 cu·m/sec. Following conveyance structures are designed for the project;

|  |          | ipe Crossing<br>(places) | <u>Syphon</u><br>(places)   |
|--|----------|--------------------------|---|
| Bayongan System<br>Main<br>Lateral/Sub-lateral | 11<br>18 | 105                      | 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - 1000 - |
| Capayas System<br>Main<br>Lateral/Sub-lateral  | 4        | 35                       | -2  |
| Total  | 33       | 140                      | 2   |

4) Protecting Structures

Spillway of the side channel overflow type will be provided in the canal to spill the excess water in the canal.

Cross drains are constructed across the irrigation canals at the places where the canals run across depressed place or natural streams. Protecting structures required for the project are tabulated below:

|                     | <u>Spillway</u><br>(places) | Cross Drain<br>(places) |
|---------------------|-----------------------------|-------------------------|
| Bayongan System     |                             |                         |
| Main                | 3                           | 18                      |
| Lateral/Sub-lateral | 1                           | 57                      |
| Capayas System      | 1                           |                         |
| Main                | 1                           | 10                      |
| Lateral/Sub-lateral | 2                           | 40                      |
| Total               | 7                           | 125                     |

2.3 Drainage Canal Systems

2.3.1 Function and Requirement of Canal

The functions of drainage canals are to drain out water in fields and to lead the water to drain outlets. The layout of the irrigation system and the topography of the related area are the main factors for determining the location of the drainage canal. Existing natural streams or depressed places are used for the drainage canal as much as possible.

2.3.2 Canal Alignment

Many natural streams flowing down from the south to the north

direction will be available for the main drainage canal. These streams are situated at the lowest place in the project area and will have a sufficient drainage capacity. The lateral drainage system will not be required generally because the irrigation water or rain water comes down to the paddy field formed along the slope of hill by the plot to plot irrigation method and reach the streams. The lateral drainage canal will be planned at the lower area where natural river course is indistinct and/or drain water from the proposed service units has to lead to existing stream due to set up a new irrigation system. Total length of drainage canals is proposed at 49.0 km with 49 lines in the project area. Design discharge and canal gradient vary from 0.87 cu.m/sec. to 0.09 cu.m/sec. and from 1/3,000 to 1/750, respectively.

Drainage diagram is planned in compliance with location of existing stream, demarcation of drainage area, drainage unit requirement and irrigation canal alignment.

2.3.3 Design of Drainage Canal

The design discharge of drainage canals is estimated at 5.61 1/sec/ha based on the rainfall record with a frequency of 5 years. Manning's Formura is used for hydrauric calculation with a roughness coefficient of 0.04. Drainage canals are designed trapezoidal in shape with inside slopes of 1:1 and base width to water depth ratio of 1.0. To prevent erosion and sedimentation in the canals, permissible velocity is taken at 0.3 m/sec. in minimum and 0.8 m/sec. in maximum.

2.3.4 Related Structure

Regulating and conveyance structures are provided in the canals as related structure of the drainage canal.

Drop is installed to regulate the water surface in the canals that have steeper slopes than those needed to reach permissible velocities. Road crossing with pipe barrel is furnished at the place where existing road crosses the drainage canal. Drain outlets at the terminal point of canals will also be provided. Required regulating and conveyance structures are tabulated below;

| <u>Structures</u> | Bayongan system<br>(places) | Capayas system<br>(places) | <u>Total</u><br>(places) |
|-------------------|-----------------------------|----------------------------|--------------------------|
| Road Crossing     | 63                          | 16                         | 79                       |
| Drop              | 178                         | 28                         | 206                      |
| Drain Cutlet      | 43                          | 6                          | 49                       |

2.4 Operation & Maintenance Road

Operation and maintenance road is planned along the irrigation canals except sections where existing road runs in parallel. O & M road will be constructed on one bank 6.0 m wide roadway having 4.5 m wide gravel surfacing of 20 cm thickness for main canal and 4.0 m wide roadway having 3.0 m wide gravel surfacing of 20 cm thickness for lateral and sub-rateral canals.

Required O & M road in each system is shown below;

|                 | Along Main<br>Canal | Along Lateral/<br>Sub-lateral Canal |
|-----------------|---------------------|-------------------------------------|
| Bayongan System | 9.90 km             | 52.0 km                             |
| Capayas System  | 2.60                | 16.0                                |

|                        | 1.<br>                |           | ·               | · •    |                  |
|------------------------|-----------------------|-----------|-----------------|--------|------------------|
| System                 | <u>Canal</u> <u>C</u> | anal Name | Commanding Area | Length | Remarks          |
|                        |                       |           |                 |        |                  |
| Bayongan               | Main                  | B.M.C.    | 4,140 ha        | 12.45  | km               |
|                        | Lateral               | LAT BA    | 645             | 6.42   |                  |
|                        | S-Lateral             | LAT BA-1  | 284             | 3.10   |                  |
|                        | ditto                 | LAT.BA-2  | 41              | 0,55   |                  |
|                        | Lateral               | LAT.BB    | 441             | 5.37   |                  |
|                        | S-Lateral             | LAT.BB-1  | 37              | 0.80   |                  |
|                        | ditto                 | LAT BB-2  | 153             | 2.53   |                  |
|                        | Lateral               | LAT.BC    | 658             | 6.20   |                  |
|                        | S-Lateral             | LAT.BC-1  | 151             | 1.85   |                  |
|                        | ditto                 | LAT.BC-la | 60              | 0.69   |                  |
|                        | Lateral               | LAT BD    | 355             | 4.96   |                  |
|                        | S-Lateral             | LAT.BD-1  | 100             | 1.47   |                  |
|                        | ditto                 | LAT BD-2  | 75              | 1.24   | ÷                |
| • . •                  | Lateral               | LAT.BE    | 324             | 2,60   |                  |
|                        | S-Lateral             |           | 189             | 3.30   |                  |
| a stalina.<br>La t     | Lateral               | LAT.BF    | 1,717           | 13.18  |                  |
|                        | S-Lateral             |           | 198             | 4.57   |                  |
| •                      | ditto                 | LAT.BF-2  | 68              | 0.55   |                  |
| , *                    |                       | LAT.BF-3  | 222             | 3.47   |                  |
|                        | ditto                 | LAT.BF-4  | 149             | 1.35   |                  |
|                        | ditto                 | LAT.BF-5  | 76              | 0.80   | Total Length     |
|                        | ditto                 | LAT.BF6   | 73              | 1.00   | Main 12.45 km    |
|                        | ditto                 | LAT.BF-7  | 126             |        | Lateral 38.73 km |
| ta t<br>A a secondaria | ditto                 | LAT.BF-8  | 39              | 0.95   | Sub-Lat 30.14 km |
|                        | ditto                 | LAT.BF-9  | 34              | 0.80   | Total 81.32 km   |
|                        | arceo                 |           | <i></i>         |        |                  |
| Capayas                | Main                  | C.M.C     | 1,160           | 3.27   |                  |
|                        | Lateral               | LAT.CA    | 163             | 2.53   |                  |
|                        | ditto                 | LAT.CB    | 597             | 7.35   | Total Length     |
|                        | S-Lateral             | LAT.CB-1  | 63              | 1.20   | Main 3.27 km     |
|                        | Lateral               | LAT.CC    | 400             | 3.98   | Lateral 13.86 km |
|                        | S-Lateral             | LAT.CC-1  | 66              | 2.60   | Sub-Lat 5.00 km  |
|                        | ditto                 | LAT.CC-2  | 71              | 1.20   | Total 22.13 km   |
| 1                      |                       |           | • -             |        |                  |

TABLE H2-1 PROPOSED IRRIGATION CANAL FEATURES

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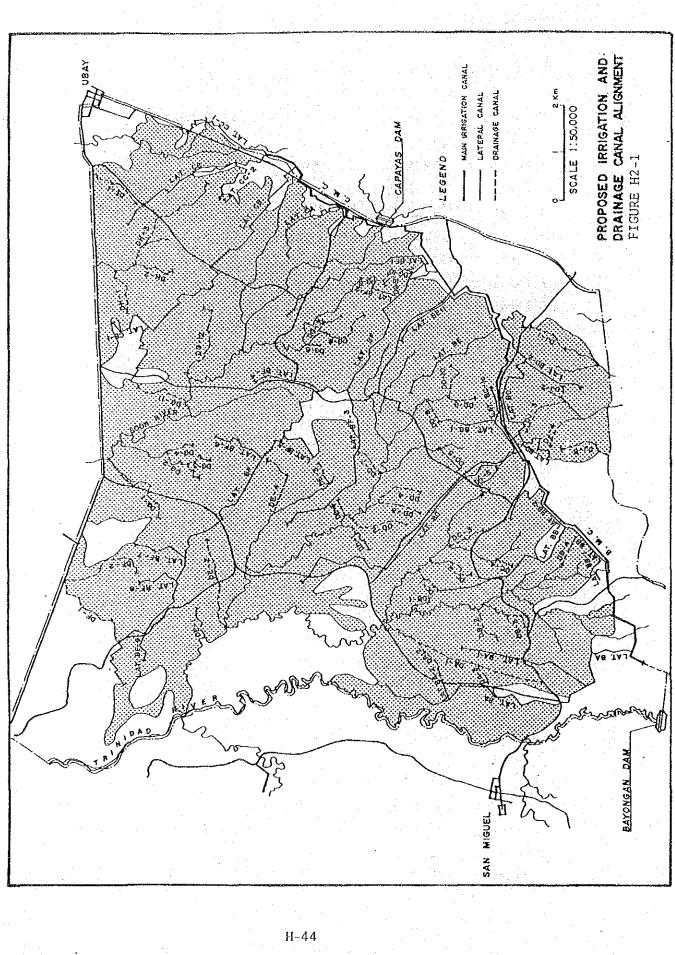
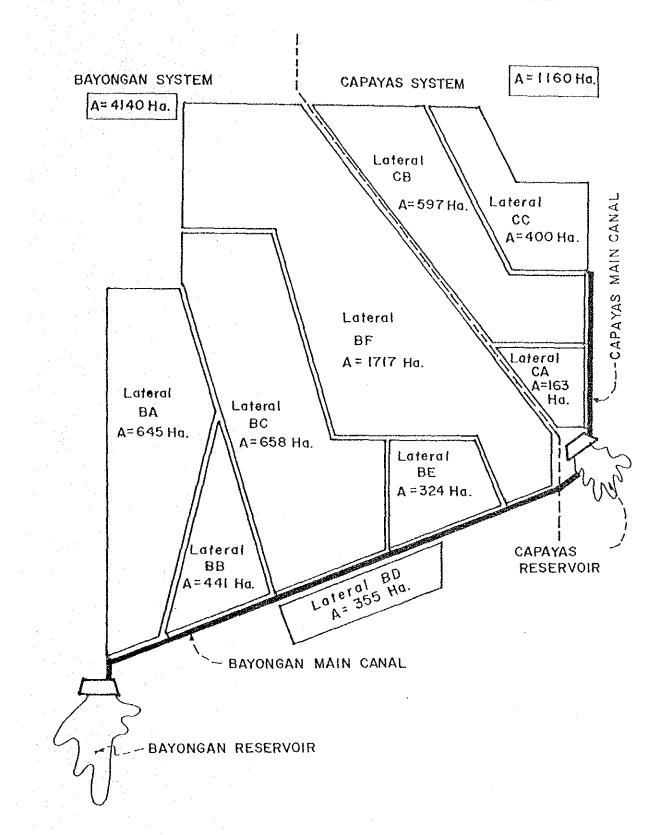


FIGURE H2-2 IRRIGATION SYSTEM IN LATERAL CANAL



# ANNEX I. ON-FARM DEVELOPMENT AND WATER MANAGEMENT

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CHAPTER I ON-FARM DEVELOPMENT

1.1 Land Development

a) General

Land development in hilly area is an essential component of the project. Total 3,600 hectares of Class-I land with land slope less than three percent is proposed to be developed to paddy field by the project component, while 1,200 hectares of Class-II land with land slope three to five percent is assumed to be developed to upland farm.

As to the farm development of the Class II land after the project, beneficical farmers would desire to reclaime paddy as following background. In this connection, necessary countermeasures to cope with this possibility should be taken before the project, as it will cause an additional water demand.

- Under the poor land resources and population pressure, farmers in Bohol Island have reclaimed a great number of paddy terraces even on the steep slope so much as irrigation water is avairable.
- Paddy terrace development on the sloped land will be quite attrective for farmers at the standpoint of erosion control of soil and better farm management expected.

- Class-I land of rotation area is not evenly distributed in size to each property lot.

- In case of communal irrigation project, farmers have expanded their paddy terraces by themselves very soon after the water is avairable.
- Voluntary reclamation of land by farmers themselves is never prohibited by NIA.

Demand for additional water supply by farmers to reclamated paddy after the project will be an important subject of Farmers Irrigatars' Associations to be dissolved by themselves. Because, the concern with NIA regarding water scepply will be how to answer irrigation requirement of the system area in exchange for collectible irrigation fee.

I-1

b) Proposed Criteria of Land Development

Paddy reclamation in hilly area will be planned by contour terracing method which is most commonly carried out in such undulated hills as in the project area. The dimension of paddy to be developed by the project is proposed as follows:

- Standard width of terrace will be 20 meters.

- The minimum and maximum widths of terrace will be 10 meters and 30 meters respectively.

- The Maximum length of one plot of paddy will be 100 meters.

- The maximum hight of terrace will be 60 centimeters.

- Side slope of terrace on cut and fill sections will be 1 : 1.

In order to obtain adequate soil depth availrable for crop production, deep plowing by means of heavy equipment will be planned as required.

Proposed paddy land with a large size will be divided into irrigation units with one to one and a half hectares in size in order to make a terminal irrigation unit for rotational irrigation practice. Plot to plot irrigation will be planned within each irrigation unit. Farm turnouts and internal ditches are constructed as required at the expense of beneficial farmers.

As layout of on-farm facilities is influential in figuring the land reclamation plan, the layout of on-farm facilities should be planned in connection with the land development plan. As a rule, a land development plan is more adjustable in the layout of terracing than the routing of on-farm facilities.

Right of way of on-farm facilities should be established prior to the commencement of land development works. The line of right of way shoul be protected so as not to be destroyed by the development works. 1.2 On-Farm Development

a) Design Criteria of On-Farm Facilities

Standard design and design criteria of on-farm facilities are shown in FIGURE OF-3, OF-4 attached to MAIN REPORT and as follows:

Unit discharge:

For irrigation requirement2.183 l/sec/haFor drainage requirement5.61 l/sec/ha

Flow formular :

Mannings' open channel formular is used to determine the ditch elements

Coefficent of roughness :

n = 0.03 for main farm ditch

n = 0.04 for supplementary farm ditch and farm drain

Allowable maximum velocity :

1.0 m/s for farm ditches 0.7 m/s for farm drain

Inside and outside slopes :

1 : 1 for cut section and fill section

Profile slope of ditches :

0.001 for main farm ditch at the minimum

Elements of ditches : unit: cm

| Item         | MFD | SFD | Farm Draiw |
|--------------|-----|-----|------------|
| Berm width   | 40  | 35  | 30         |
| Bottom width | 40  | 30  | 30 min     |
| Free board   | 15  |     | . 20       |

Note: Total depth of supplementary farm ditch is determined to be 30 cm.

#### b) On-Farm Facilities

On-farm facilities are planned based on NIA criteria with regard to on-farm facilities adding some proposed modifications aiming at better water management by farmers' group. The on-farm facilities are outlined as follows:

### 1) Turnout

The turnout point will be selected along lateral/sub-lateral canals based on the physical condition of rotation area to be convenient to supply water for all rotation units.

When the rotation area extends along lateral canal or a ridge line with long span, the turnout point will be selected around the middle section of rotation area so as to covey water evenly to each rotation units.

2) Main Farm Ditch

The main farm ditch is planned to convey water from the turnout to each supplementary farm ditch through division box. No direct turnout from the main farm ditch to farm lots is designed.

The division box is composed of two wing type checks; one is provided at the head of the supplementary farm ditch and the other is just at the downstream across the main farm ditch.

Two checks are designed to provide a fixed proportional division of flow in accordance with respective size of service area commanded by each check. The standard trapezoidal (Cipolletti) weirs are installed in checks at each overflow section as shown in FIGURE OF-4 attached at MAIN REPORT.

The dimension of two weirs is determined in accordance with the size of each service area. A temporary alternation in diversion rate of flow can be accommodated by means of stop logs, while the permanent correction of diveision flow due to change of service area is accomplised by replacing of corresponding weirs.

3) Supplementary Farm Ditch

The supplementary farm ditches are planned in each rotation area with the purpose of distributing water to farm lots in each rotation area. The route of supplementary farm ditch is selected along ridge line or across the terraces depending on the local conditions. As much as possible, supplementary farm ditch should not be constructed on fill section, but on cut section considering probable erosion problem after the project.

The supplementary farm ditch planned along hilly area will be designed for irrigation only in view of protecting the subgrade from scouring by drainage water.

### 4) Farm Drains

Farm drains are planned along the present paddy field as required so as to remove excess water from the paddy field. The farm drain can be used for the irrigation purpose of the present paddy field.

### 5) Farm Road

Farm road is planned for better farm management of the community, and operation and maintainance of on-farm facilities. In this connection, farm road is connected with public road or farm road adjacent to rotation area.

The total width of farm road is assumed to be three meters in view of future requirement for public transportation, machanized farm management and operation and maintainance work of on-farm facilities.

1.3 Typical Layout for On-Farm Development

a) General Description of Sample Areas

Layout of on-farm development was planned at selected two sample areas in the project area based on the topographic maps of 1: 2,000 in scale. One sample area (area "A") commanded by the Capayas system is located at Barangay Tuburan, and the other sample area (area "B") commanded by the Bayongan system is located at Barangay Hambabawran.

### 1) Sample area "A"

The sample area "A" is extended on the sloped area in which hilly areas and paddy fields are alternated. As the paddy field is branched into four tributaries within the area, the hills in the area is separated into three blocks.

The drainage water through the sample area is concentrated to the paddy fields, and the size of drainage area amounts to 87 hectares at the lowest end of the sample area. However as the drainage system of the area branches into four major tributaries, the drainage water causes less problems in the area.

The route of lateral canal C-B transits across the drainage area about one and a half kilometers in span along the rotation area. The average ground slope of proposed reclamation area is estimated to be two percent.

Although no avairable cadastal map of the rotation area authorized by the Government, the property lines in the rotation area were followed by the field survey. The number of farms in the sample area was 12.

2) Sample Area "B"

The sample area is shaped a head land. Several ridge lines are branched off from the main ridge in the middle to both ways. The area is located at the tail end of lateral canal B-E.

Proposed reclamation area is extended on the hills which have average ground slope of two percent. Paddy fields have been developed on the depressed areas and along narrow depressions which have relatively steep profile slopes.

I - 6

As the sample area had been bought by the Government and sold to farmers after divided into lots, each farm lot is shaped of regular size with 200 by 150 meters length apurtenanted an additional right of way for farm road along one side line of each lot.

Although no available cadastal map was obtained in the field survey, the property lines were followed in the field survey. The number of the property lots related to proposed land development amounts to 27.

b) Layout of On-Farm Facilities

As a result of home works based on the topographic maps, proposed routes of irrigation and drainage ditches are not followed along the property line except only limited sections. On the contrary, proposed farm roads are able to confirm property lines.

Farm lots with relatively large size were divided into irrigation units to have one to one and a half hectares in size. Internal ditches between supplementary farm ditch and the irrigation units were planned as required.

The layouts of on-farm development in two sample area are shown in FIGURE OF-1 and OF-2 attached to MAIN REPORT. And the quantities of on-farm facilities are shown in TABLE I-1 and I-2.

TABLE 11-1

SUMMARY OF ON-FARM FACILITIES IN SAMPLE AREA "A"

|                      |         |           | Rot | ation  | Unit                         |              |
|----------------------|---------|-----------|-----|--------|------------------------------|--------------|
| Item                 | Unit    | 1         | 2   | 3      | 4                            | <u>Total</u> |
| Gross area           | ha      |           |     |        | n in sea e se<br>Se sea e se | 50.6         |
| Irrigated area       | ha      | 7.0       | 8.8 | 7.9    | 5.9                          | 29.6         |
| No. of irrigation un | it unit | 6         | 8   | 6      | 6                            | 26           |
| Main farm ditch      | m       | -         | · - | -<br>- | -                            | 510          |
| Supplementary        | m       | 840       | 330 | 280    | 480                          | 1,930        |
| farm ditch           |         | . · · · · |     |        |                              |              |
| Farm drain           | m       | 1,040     | 270 | 650    | 660                          | 2,620        |
| Farm road            | m       |           |     |        |                              | 2,280        |
| Division box         | unit    | ]         | L I |        | ĺ.                           | 2            |
| Check and drop       | unit    | 4         | 1   | 2      | 3                            | 10           |
| Road crossing        | unit    | 2         | 1   | 2      | 3                            | 8            |
|                      |         |           |     |        | •                            |              |

TABLE I1-2

SUMMARY OF ON-FARM FACILITIES IN SAMPLE AREA "B"

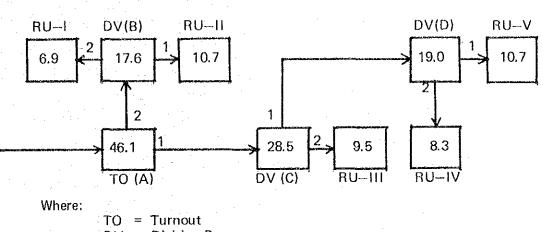
|                             |      |     | Ro   | tation | Unit |      |       |
|-----------------------------|------|-----|------|--------|------|------|-------|
| Item                        | Unit | 1   | 2    | 3      |      | 5    | Total |
| Gross area                  | ha   |     |      |        | · ·  |      | 64.4  |
| Irrigated area              | ha   | 6.9 | 10.6 | 9.5    | 8.4  | 10.7 | 46.1  |
| No. of irrigation unit      | unit | 6   | 8    | 7      | 8    | 9    | 38    |
| Main farm ditch             | m    | -   | -    | · · ·  | -    | -    | 720   |
| Supplementary<br>farm ditch | m    | 210 | 700  | 310    | 450  | 390  | 2,060 |
| Farm drain                  | m    | 50  | 100  | 620    | 440  | 350  | 1,560 |
| Farm road                   | m    |     |      |        |      | •.   | 1,520 |
| Division box                | unit |     | 1    | 1      |      | 1    | 3     |
| Check and drop              | unit |     | 2    | 2      | 3    |      | 7     |
| Road crossing               | unit | 1   | 3    | 3      | 2    | 5    | 14    |

c) Typical Design of Division Box.

In order to materialize the design process of water distribution structure of on-farm facilities, the typical design was carried out at sample area "B". The schimatic chart of the water diversion structure is shown in FIGURE 11-3.

TABLE I1-3 shows the dimension of devision weirs at sample area "B" corresponding to the schimatic chart as shown in FIGURE I1-3.





DV = Division Box

RU-= Rotation Unit - Number

TABLE 11-3 DIMENSION OF DIVERSION WEIR FOR DIVERSION SYSTEM OF SAMPLE AREA "B"

(Unit: ha)

|                                       |                |      | Number | of Weir |
|---------------------------------------|----------------|------|--------|---------|
| Division box                          | Item           | Unit | 1      | 2       |
| Α                                     | Service area   | ha   | 28.5   | 17.6    |
|                                       | Length of weir | cm   | 40.0   | 24.7    |
| В                                     | Service area   | ha   | 10.7   | 6.9     |
|                                       | Length of weir | cm   | 40.0   | 24.7    |
| · · · · · · · · · · · · · · · · · · · | Service area   | ha   | 19.0   | 9.5     |
|                                       | Length of weir | Cm   | 40.0   | 20.0    |
| D                                     | Service area   | hà   | 10.7   | 8.3     |
|                                       | Length of weir | Cm   | 40.0   | 31.0    |
|                                       |                |      |        |         |

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2,1 Water Management Structure

a) General

The Phase II irrigation system will be integrated by the Bohol irrigation system after the Phase II project in accordance with rules and regulations of NIA. Two zone offices will be founded for operation and maintainance of two irrigation systems; one is Zone I for Phase I system, and the other is Zone II for Phase II system. The responsibility for the Bohol irrigation system and Zone I office concerned with Zone II system are as follows:

- Bohol irrigation System:

The irrigation superintendent of Bohol Irrigation System is responsible for operation and management of entire irrigation systems, who will supervise two irrigation systems of Phase I and Phase II through each zone engineer.

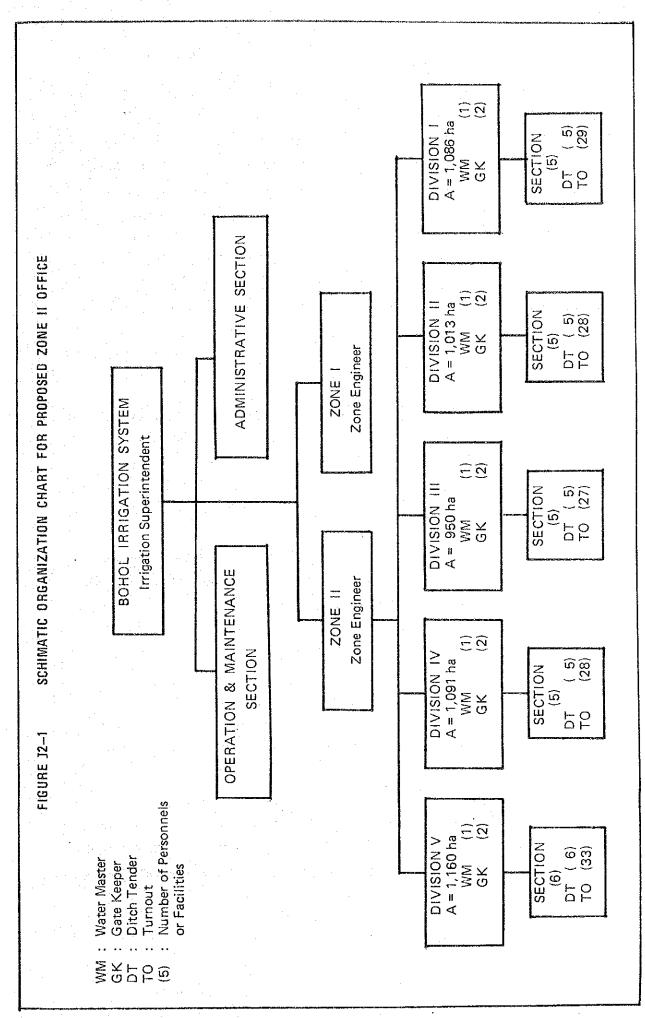
~ Zone I Office:

Zone I engineer is responsible for operation and management of Phase I system as well as necessary water management works to deliver surplus water to Phase II system through the Phase I main canal.

b) Structure and Activities of Zone II Office

Zone engineer is responsible for operation and management of Phase II system, who Prepares operation plan, carries out day-to-day water management of major irrigation facilities and supervises water management of lateral/sub-lateral canals through water masters in their operation divisions.

Proposed organization of Zone II office is shown in FIGURE I2-1, and the activities of Zone II office with regard to water management of Phase II system are outlined as follows:



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### 1) Zone II Office

The operation and maintainance group headed by a zone engineer is responsible for preparation of operation plan, water management of major irrigation facilities as well as reservoir operation. Two groups of gate keepers, one is for the Bayongan system and the other is for the Capayas system, are in charge of water control for two systems of Bayongan and Capayas.

The water management group headed by a supervising water management technologist (SWMT) is responsible for water management of lateral/ sub-lateral canals, who supervises water masters in their operation divisions.

### 2) Operation Division

The system of Phase II is divided into five operation divisions; each operation division is to be under the direct supervision of water master. NIA will construct working stations of each water master in the middle of the division area in accordance with the regulations and rules of NIA. Average size of the operation division is 1,000 hectares.

Each water master is responsible for operation and management of lateral/sub-lateral canals commanded by his operation division, who directs two gate keepers and five to six ditch tenders. He prepares cropping calender, conducts water distribution works and renders technical advices to Farmer Irrigators' Group regarding water management on on-farm level.

The gate keepers carried out day-to-day water management for lateral canals under the direct supervision of water master in accordance with water distribution schedule.

The organization of the operation division is assumed to be turned over to corresponding Formers Irrigators' Association together with the responsibility for operation and maintainance of lateral/sub-lateral canal in accordance with the present strategy of NIA regarding operation and maintainance of National Irrigation Systems.

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### 3) Operation Section

The service area of each operation division is divided into operation sections with an average service area of 200 hectares under the direct supervision of each ditch tender. The operation division will be one of the terminal units for irrigated farm management to cooperate with each other.

The operation section will control four to seven rotation areas. Ditch tender will supervise water distribution control for each rotation area through Farmer Irrigators' Groups and renders them necessary technical assistance.

### 2.2 Operation Plan

### a) Cropping Calendar

Cropping calendar of rotation areas is prepared by each water master based on proposed planting area and cropping schedule collected from each Farmer Irrigators' Group. Annual planting date and order of each rotation area within operation section will be shifted intentionally according to timetable.

The cropping calendar of each operation division is formally determind by the Zone II office and transmitted to each Farmer Irrigators' Association through water masters in accordance with operation rule.

### b) Operation Plan

Water masters prepare water distribution plan of each rotation area based on the cropping calendar and arrange it at each lateral canal in order to make use distribution guide for day-to-day water management.

Water supply plan from main canal to each lateral is determined by Zone II office in accordance with capacity of stored water in the Bayongan reservoir. The guide line with regard to water supply plan based on the capacity of stored water in the Bayongan reservoir is outlined in Main Report at 4.4.4 Reservoir Operation Rule. Water supply plan based on the guide line is as follows:

- If the capacity of stored water in the Bayongan reservoir is exceeding the volume of guide line, the water supply plan will be fixed up in accordance with the proposed cropping calendar.

On the contrary, when stored water in the reservoir is less than the guide line, the water supply plan will be determined by the discounted rate of water supply evenly to all lateral canal in accordance with the deficit capacity of water in the Bayongan reservoir.

Zone II office will prepare detailed plan for water supply of each lateral canal in accordance with available water. And each water master will arrange water distribution plan in his division to be conformed to the allocated discharge at each lateral canal.

Water supply schedule will be revised time to time by Zone II office based on water balance in the Bayongan reservoir, volume of effective rainfall and demand of irrigation water informed from water master.

2.3. Water Management Practice

a) General

Water resources once stored in the reservoir is delivered to a farm lot through following route of irrigation canals/ditches; main canal, lateral canal, sub-lateral, main farm ditch and supplementary farm ditch. Operation of these canal systems are carried out by NIA and Farmers Organizations.

According to proposed water management rule, structures concerned with operation of those irrigation canals/ditches are as follows:

- Zone II office is responsible for reservoirs and main canals.

Operation divisions are responsible for lateral/sub-lateral canals, however it is to be turned over to respective Farmer Irrigators' Associations.

Main farm ditches are responsible for Farmer Irrigators' Groups.

Supplementary farm ditches are left to Terminal Unit Group.

b) Water Distribution Control

In order to distribute water satisfactorily to all farm lots, adequate water distribution management is required at each irrigation system. In this connection, water control and measurement facilities of each irrigation system are designed to be associated with relative importance of each system.

There are five to six in number of water distribution facilities between reservoir to farm lot. Discharge through these facilities except farm turnout is computed by hydraulic equations from dimension of flow such as sectional area of orifice, water depth, span of flow, differential of water head. Accordingly, flow through these facilities can be obtained by means of table or graph which is specially prepared for the convenience of operation personnel.

The water distribution facilities of respective canal system and dimensions of flow required of water measurement are as follows:

Intake structure of reservoir is provided with sluice gate, discharge through it is obtained from water level of reservoir and sectional area of orifice.

Diversion structure of main canal to lateral canal is provided with Neyrpic orifice module, the division flow is directly measured by total span of flow.

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- Diversion structure of lateral canal to sub-lateral canal is provided with constant head orifice in accordance with NIA standard. Discharge through the orifice is obtained by sectional area of measuring orifice and differential of waterhead through the measuring orifice.
- Turnout of lateral/sub-lateral canal to rotation area is provided with constant head orifice in accordance with NIA standard.
- Division box is used for division of water from main farm ditch to supplementary farm ditch. The division box is provided with no control gate, but is designed to divert flow of main farm ditch into two flows in proportion to the size of each service area.
- Farm ternout is provided along supplementary farm ditch in order to divert water to a farm lot. No measurement facility nor permanent control facilities are provided for farm turnout. The distribution control within rotation unit is conducted by cooperation of beneficial farmers.

c) Water Management of Major Facilities

Water managements of the Bayongan system and the Capayas system are carried out independently so far as the Capayas system has enouth water in the reservoir or from the river. When the Capayas system has insufficient water in the system, necessary water is delivered from the Bayongan reservoir through the Bayongan main canal.

In case the Bayongan system waste water from main canal to the Capayas reservoir is mostly rufused for the Capayas system as far as the reservoir can afford empty capacity in the reservoir. However, as water resources of the Capayas system to be wasted through the Capayas reservoir amount to about 40 percent annually, the empty capacity in the Capayas reservoir should be managed as much as possilbe by operation of the Bayongan reservoir. BY day to day operation, check water level should be kept during operation period and even temporally discontinuance period due to rainfall or other cause. The stored water in canal section is efficient not only to protect canal lining against uplift power, but also to shorten time lag caused at the beginning of operation as well as to decrease waste water due to time lag of operation.

d) Water Management of Lateral System

The most important requirement for water management of lateral canal/sub-lateral canal is to assure Farmers Irrigators' Groups of even water distribution of supplied water from main canal. In this connection systematic water distribution control will be conducted by full time gate operators as proposed before.

As capacity of lateral canal is tapering from the head to terminal end, supplied water from main canal should be distributed correctly in accordance with operation schedule, any misoperation cause of surplus water in the canal span might endanger canal section in the lower rank of span or flooding of rotation area located at the terminal end.

In addition, water balance between operation sections should be maintained at the standpoint of even water distribution as well as canal safty. To this end, proposed water measurement section along canal is selected between two operation sections. The canal check or canal drop located just at the downstream of the terminal turnout of operation section is desirable for the purpose.

e) Water Management for On-Farm Level

Planting schedule of a rotation area is assumed to be carried out simultaneously in all rotation units during the period of five to ten days in accordance with the cropping calendar. Based on the understanding, diversion rate of water at the head of each supplementary farm ditch is determined to be proportional to the size of each service: area. As no water control facilities is provided at each division point, complaint regarding water distribution will be diminished compared with manual control system.

In the course of water management, basic unbalance of water requirement between present paddy field and proposed paddy will be cleared. The excessive water for present paddy could be used of water source for paddy extension within rotation area after formally qualified by the Fermer Irrigators' Association concerned.

As stated above, farm lots will be divided into irrigation unit with one to one and a half hectare in size, more intensive irrigated farming is expected in each irrigation unit. Appropriate water management method of each irrigation unit should be aquired by each farmers themselves.

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# ANNEX J. PROJECT IMPLEMENTATION PROGRAM AND COST ESTIMATE

ANNEX J PROJECT IMPLEMENTATION PROGRAM AND COST ESTIMATE

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### CHAPTER I PROJECT IMPLEMENTATION PROGRAM

1.1 Project Implementation

1.1.1. Executing Agency of the Project

The excuting agency of the project will be the National Irrigation Administration (NIA), which has a sufficient capability and deep experience in carrying out the detailed design, construction of civil works and operation and maintenace of the completed facilities of the project.

NIA will execute the detailed design for major project facilities recruiting a consulting firm, the construction contracting with a competent contractor and the operation and maintenance guiding the farmer's association.

The organization of NIA is shown in FIGURE 6-1 of Main Report. In this organization, the detailed design works are carried out by the design and speciffication division, construction by the construction division and operation and maintenance by the O/M division.

### 1.1.2 Financing

The foreign currency portion of the project will be financed by the international financing institute while the local currency portion will be appropriated by the Philippine Government.

1.1.3 Construction Mode

A qualified contractor to construct the civil works of the project will be also selected by the international competitive bidding. The on-farm works except land leveling works will be made by the farmers association newly established in service area under the technical guidance by the NIA O/M division.

Of course some complicated works such as turnout, drop and crossing structers might be constructed by NIA administration to provide

construction equipment and materials except labor force.

The operation and maintenance works of the project facilities will be made directly by NIA O/M staff together with the farmer's association. The NIA will provide necessary equipments of O/M prior to compeletion of the construction works.

### 1,1.4 Preperatory Works

Preparatory works are composed of survey and investigation works for the detailed design stage and site facilities for administration of the project implementation.

Though the topographical map with scale of 1 : 4,000 covering the whole project area and geological investigations at the proposed dam site which had been provided during the Feasibility Study will be useful.

Therefore, additional survey and investigation works necessary for the detail design will be limited to the items as follows:

|    | Item                            | <u>Unit</u> | Quantities |
|----|---------------------------------|-------------|------------|
|    |                                 |             |            |
| 1. | Topographical Survey            |             |            |
|    | Bayangan dam profile *          | km          | 4.0        |
|    | Capayas dam profile *           | km          | 3.0        |
|    | Canal alignment profile         | km          | 160.0      |
|    |                                 |             |            |
| 2. | Geological Investigation        |             |            |
|    | Core drilling at Bayongan dam   | m           | 100.0      |
|    | Core drilling at Capayas dam    | m           | 100.0      |
|    | Test pit at Bayongan dam        | place       | 5          |
|    | Test pit at Capayas dam         | place       | 5          |
|    | Laboratory test of dam material | L.S         | 1          |
|    | Corn penetration test at canal  | place       | 150        |
|    | Sand & gravel test              | L.S         | 1          |

Note: \* Survey works of both dams including dam, spillway and intake axis profile.

The site facilities for the project administration will be completed by NIA before commencement of the project construction and consist of the following buildings.

|                     | and the second |            |
|---------------------|--|------------|
| Item                | <u>Unit</u>  | Quantities |
| Main office         | sq∙m   | 400        |
| Staff residence     | sq•m   | 800        |
| Guest house         | sq∙m   | 200        |
| Equipment warehouse | sq⋅m   | 200        |
| Office supplies and |  |            |
| furnitures          | L.S  | 1          |
|                     |  |            |

### 1.1.5 Administration Office

The organization of NIA office is proposed as shown in FIGURE 6-2 of Main Report, taking into consideration administrative and engineering works at the project site office during construction period. Machinery and equipments for the administration are as follows:

| <u>Item</u> <u>l</u>  | Jnit      | Quantities |
|-----------------------|-----------|------------|
| Jeep type of vehicles | Nos       | 6          |
| Motorcycle            | <u>†1</u> | 6          |
| Theodrite             | 11        | 2          |
| Level                 | <b>11</b> | 2          |
| Current meter         | н         | 2          |
| Radio set             | н         | 1          |
| Walkie-Tolie          | n         | 10         |
| Automatic rain gauge  | If        | 1          |
| Personal computer     | "         | 1          |
|                       |           |            |

### 1.1.6 Consulting services

Consulting services including local experts are required for the detailed design and construction supervision as well as bid evaluation. The total man-months for foreign and local experts are shown as follows:

|                                  |                             |                    | · -                       |                               |
|----------------------------------|-----------------------------|--------------------|---------------------------|-------------------------------|
| Expert                           | Foreign<br><u>Man-Month</u> | Local<br>Man-Month | Total<br><u>Man-Month</u> | NIA Staff<br><u>Man-Month</u> |
| 1. Detailed design stage         | · ·                         | -<br>              | int<br>                   | •                             |
| Project director                 | 1                           |                    | 1                         | -                             |
| Project Manager                  | 12                          | -                  | 12                        |                               |
| Dam engrs.                       | 10                          | 6                  | 16                        | 10                            |
| Irrigation engrs.                | 10                          | 6                  | 16                        | 10                            |
| On farm development engrs.       | -                           | 4                  | 4                         | 20                            |
| Hydrologist                      | 4                           | _                  | 4                         | 3                             |
| Hydraulic structure engrs.       | 10                          | 6                  | 16                        | 10                            |
| Engineering geologist            | 3                           |                    | . <b>3</b>                | 5                             |
| Soil mechanist                   | 3                           | ·;                 | 3                         | 5                             |
| Mechanical engr.                 | 3                           | -                  | 3                         | -                             |
| Topo-Surveyor                    | -                           | <u>-</u> *         |                           | 25                            |
| Cost estimator                   | 3                           | · - ·              | 3                         | 3                             |
| Specification specialist         | 4                           | -                  | 4                         | 4                             |
| Specialist as required           | 5                           | 3                  | 8                         | -                             |
| Home support engr.               | 2                           |                    | 2                         | -                             |
| Total                            | 70                          | 25                 | 95                        | 95                            |
| 2. Construction supervision stag | je                          |                    | :                         |                               |
| Project director                 | 2                           |                    | 2                         |                               |
| Resident engr.                   | 36                          | , <del>-</del> .   | 36                        |                               |
| Design engr.                     | 8                           | 4                  | 12                        | н.<br>Н                       |
| Dam engr.                        | 30                          | 18                 | 48                        |                               |
| Canal engr.                      | -                           | 36                 | 36                        |                               |
| Mechanical engr.                 | 4                           |                    | 4                         |                               |
| Tender Evaluation Expert         | 3                           | · · · - · · ·      | 3                         | •                             |
| Specialist as required           | 4                           | 2                  | 6                         |                               |
| Home support engr.               | 3                           | · · -              | 3                         |                               |
| Total                            | 90                          | 60                 | 150                       |                               |
|                                  |                             |                    |                           |                               |

# 1.1.7 Land Acquisition and Compensation

Land aquisition in the reservoir and along the canal alignment will be undertaken by NIA before starting of construction works.

The detail is shown as follows:

| Item                  | <u>Unit</u> | Quantities |
|-----------------------|-------------|------------|
| 1. Bayogan system     |             |            |
|                       |             |            |
| (1) Bayogan reservoir |             |            |
| Mountain area         | ha          | 36         |
| Waste area            | , B. A.     | 145        |
| Coconuts area         | ti          | 43         |
| Paddy fields          | 17          | 34         |
| Up-land               | *1          | 92         |
| Residential house     | houses      | 30         |
| Housing site          | ha          | 30         |
| (2) Canal system      |             |            |
| Wast area             | ha          | 10         |
| Cultural area         | 17          | 85         |
| (3) Resettlment       | family      | 30         |
|                       | -           |            |
| 2. Capayas system     |             |            |
|                       |             |            |
| (1) Capayas reservoir |             |            |
| Mountain area         | ha          | 20         |
| Waste area            | 11          | 80         |
| (2) Canal system      |             |            |
| Waste area            | ha          | 3          |
| Cultivated area       | n           | 23         |
|                       |             | -<br>-     |

### 1.2 Construction Plan

### 1.2.1 General Construction Method

a) Temporary works

The contractor's camp office, access road, tentative diversion of the river for dam construction, provision of borrow area, drainage during construction etc., will be made as temporary works by the contractor.

b) Working hours and days

The construction works are planned to be carried out one shift with net working hour of 6.5 hr/day and 25 working day/month except the embankment and fill of earth works which will be carried out with 15 to 20 working days per month due to suspension by rainfall.

c) Available Construction Material at Site

i) Earth material in Capayas Dam

The Capayas dam is planned with a homogeneous earth type dam and requires the embankment volume of about 230,000 cu.m. The embankment earth materials are mostly collected from the borrow area near dam axis and with a transporting distance less than 200 m and are selected from the excavated materials of dam foundation, spillway and intake structures.

ii) Earth Material in Bayongan Dam

The Bayongan dam is planned with a center core type earth dam and requires the impervious core materials of about 274,000 cu.m. This embankment materials are collected form the borrow area located at hilley area with elevation of 40 to 60 m in the left bank of dam site. The material is easily taken by bulldozer pushing along the slope and transported to the embankment site within a distance of about 300 m. The material in borrow area has a high field moisture content due to high ground water level, so that trenches along the slope of borrow area should be provided during construction period to make ground water level lower and get optimum field moisture content for core material.

### iii) Filter Material in Both Dams

Filter materials are consisting of sand and gravel with a designed grain size distribution. This material is not found near both damsited of Capayas and Bayongan, but at place along the Hinlayagan river 9 km far from both damsites.

The deposit of sand and gravel materials in the river is extending over 3 km long and 30 m wide, and will be sufficient for the embankment of filter zones with total volume of about 99,000 cu.m combining both dams.

### iv) Shell Material in Bayongan Dam

The shell material in the Bayongan dam is found at the borrow area located at the upstream hilly area and 2 km far from the damsite. This material consisting of weathered rock, sand and gravel including silt and clay materials and most suitable for the shell embankment material having a function of semipervious zone. This semi-pervious material is used for both shell zones on the upstream and the downstream.

The exacavated material from dam foundation, spillway and intake structures will be also available for the downstream shell zone mixing with semi-pervious material taken from the borrow area as mentioned in the above.

### v) Rock Material

Rock material is used for the riprap on the upstream slope and also for the toe embankment at the downstream dam.

The rock material should be hard and solid to protect dams from errosion in the reservoir and to fullfil a function to release seepage water through dambody smoothly at the por-

tion, so that the rock material should be collected from the Dagohoy quarry site.

Since the Capayas dam is of small scale as compared with the

Bayongan dam the riprap material and the toe material are not required so hard and solid. The riprap material is expected to be taken from the quarry site near the damsite and the toe material from the borrow area having a coarse random material at the upstream.

vi) Concrete Aggregate

Concrete aggregate material such as sand and gravel is collected at the deposited area of the Hinlayagan river, where the filter material is also taken.

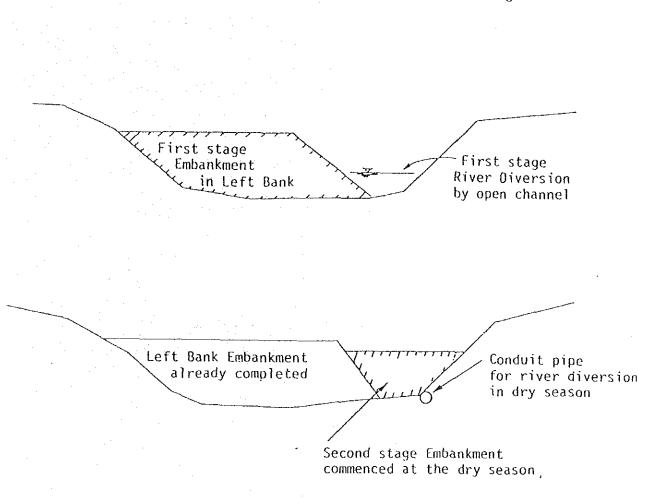
- vii) Embankment Material of Canal The excavated material in canal is sufficiently available for the embankment material.
- 1.2.2 Construction Method of Bayongan Dam
  - a) Work Volume

The work volume of the Bayongan dam construction is as follows.

|                           |           | · · · · · · · · · · · · · · · · · · · |
|---------------------------|-----------|---------------------------------------|
| Stripping                 | 72,000    | cu.m.                                 |
| Trench Excavation         | 31,000    | cu.m.                                 |
| Dam Embankment            | 1,126,000 | cu.m.                                 |
| Spillway Excavation       | 80,000    | cu.m.                                 |
| Spillway Concrete         | 1,800     | cu.m.                                 |
| Intake Tunnel             | 320       | m.                                    |
| Intake Excavation         | 27,000    | cu.m.                                 |
| Intake Concrete           | 1,000     | cu.m.                                 |
| Gate & Valve Installation | L.S.      |                                       |
|                           |           |                                       |

b) Dam Embankment Works

Dam embankment is made for core, filter and shell zone after stripping of all dam foundation and excavation of core trench. The dam embankment is commenced at the left bank diverting river water at the right bank with an open channel and then the right bank embankment should be performed in the dry year diverting a small discharge into the conduit pipe installed in



the foundation of right bank as shown in the following FIGURE.

The embankment material is transported from each borrow area and compacted under the following criteria;

| Zone   | Spreading<br><u>Thickness</u> | Number of<br><u>Pass</u> | Compaction<br>Equipment  |
|--------|-------------------------------|--------------------------|--------------------------|
| Core   | 20 cm                         | 8                        | Tamping Roller 8-10 Ton  |
| Filter | 30 cm                         | 5                        | Vibrating Roller 3-5 Ton |
| Shell  | 30 cm                         | 5                        | -ditto- 8-10 Ton         |

The embankment progress is planned as follows ;

|        | Embankment     | Performance         | Construction |
|--------|----------------|---------------------|--------------|
| Zone   | Volume         | <u>Per Month</u>    | Period       |
|        |                |                     |              |
| Core   | 274,000 (cu.m) | 8,000 (cu.m/month)  | 32 (month)   |
| Filter | 98,000 (cu.m)  | 3,500 (cu.m/month)  | 28 (month)   |
| Shell  | 760,000 (cu.m) | 30,000 (cu.m/month) | 24 (month)   |

The performance of embankment works are planned as follows ;

| · . ·   | Distance fro | m Performonce                              |
|---------|--------------|--|
| Zone    | Borrow Area  | <u>Per Month</u>                           |
| · · · · |              |  |
| Core    | 500 m        | 70 cu.m/hrx7.0hr/dayx22 days = 10,000 cu.m |
| Filter  | 9,000 m      | 20 cu.m/hrx7.0hr/dayx25 days = 3,500 cu.m  |
| Shell   | 2,000 m      | 90 cu.m/hrx7.0hr/dayx25 days x2 units      |

= 30,000 cu.m

c) Spillway Works

The spillway works in the Bayongan dam is of a scale with excavation of 80,000 cu.m and concrete of 1,800 cu.m and can be carried out at any time without any interruption of the other works such as dam embankment and intake structure works.

The concrete works will be made at the section of chute and overflow weir separately and with the concrete mixing plant provided at the weir site and the concrete pump. The concrete conveying pipe of concrete pump is installed along the chute of spillway.

d) Intake Works

The intake works are consisting of tunnel with a section area of 9.5 sq.m and intake works placing the gate and valve at the right abutment slope. Construction period will be about one year.

The following construction schedule is considered :

| works   |                  | <u>1</u> <u>2</u> | 34 | 56       | 78 | 9 10 | ) 11 | 12 |
|---------|------------------|-------------------|----|----------|----|------|------|----|
| Excavat | tion 320m        | <u> </u>          |    | <u> </u> |    |      |      |    |
| Invert  | Concrete 320m    | 9 - 1 - F         |    | <u> </u> |    |      |      |    |
| Area &  | Side Concrete 32 | Om                |    |          | Ē  | ***  |      |    |

The intake works consisting of the inclined concrete base where spindles of gate are placed and intake structure where gates are installed will be made in parallel with the tunnel works or a little later than tunnel works.

The gate itself will be installed at the end of dam construction stage before storaging water in the reservoir. 'The detailed construction schedule is shown in FIGURE 6-3 of Main Report.

1.2.3 Construction Method of Capayas Dam

a) Work Volume

The work volume of the Capayas dam construction is as follow:

| Stripping             | 36,000  | cu.m |
|-----------------------|---------|------|
| Trench Excavation     | 16,000  | cu.m |
| Dam Embankment Volume | 233,000 | cu.m |
| Spilway Excavation    | 26,000  | cu.m |
| Spilway Concrete      | 2,600   | cu,m |
| Intake Excavation     | 9,500   | cu.m |
| Intake Concrete       | 850     | cu.m |
| Outlet Gate           | L.S     |      |

#### b) Dam Embankment

A homogeneous earthfill type dam is designed so that any available material from the borrow area located in the upstream of reservoir can be used.

After providing the river diversion with an open channel at the right bank and completion of excavation, the embankment is commenced from the river bed section. The dam embankment criteria are the same as mentioned in the Bayongan dam.

The section of both side banks except the river bed is emban-

ked with only 5 to 10 m height as the dike, so that this section embankment can be made at any time.

c) Spillway and Intake Structures

The construction works of spillway and intake structures can be made in parallel with the embankment works. The only river diversion provided at the right bank should be made at the beginning stage of construction.

- 1.2.4 Irrigation and Drainage Canals
  - a) Work Volume

The work volume of irrigation and drainage canals is calculated as follows:

| . • | Item                          | Bayo      | ngan system                              | <u>Capayas system</u>                 | <u>Total</u> |
|-----|-------------------------------|-----------|--|---------------------------------------|--------------|
| (1) | Main Irrigation               | Canal     | • * * · · ·                              |                                       | ·            |
|     | Stripping (cu                 | •m)       | 9,500                                    | 5,700                                 | 15,200       |
|     | Excavation (cu                | .m) · ·   | 271,300                                  | 8,400                                 | 279,700      |
|     | Embankment (cu                | .m)       | 12,000                                   | 7,400                                 | 19,400       |
|     | Concrete Lining               | (cu.m)    | 11,900                                   | 1,500                                 | 13,400       |
|     | Struc. concrete               | (cu.m)    | 600                                      | 100                                   | 700          |
|     | Gate (pl                      | ace)      | 22                                       | 4                                     | 26           |
|     |                               |           |  |                                       |              |
| (2) | Lateral Irrigat               | ion Canal | an a | · · · · · · · · · · · · · · · · · · · |              |
|     | Stripping (cu                 | .m)       | 60,500                                   | 27,300                                | 87,800       |
|     | Excavation (cu                | .m)       | 172,100                                  | 26,800                                | 198,900      |
|     | Embankment (cu                | .m)       | 132,000                                  | 74,100                                | 206,100      |
|     | Struc.Concrete(               | cu.m)     | 2,000                                    | 600                                   | 2,600        |
|     | Turnout Gate (p<br>& Division | lace)     | 179                                      | 47                                    | 226          |
| (3) | Drainage Canal                |           |  |                                       | •            |
|     | Excavation (cu                | .m)       | 18,500                                   | 24,500                                | 43,000       |
|     | Embankment (cu                | .m)       | 500                                      | 300                                   | 800          |
|     | Reinforced Conc               | rete (cu. | n) 2,000                                 | 500                                   | 2,500        |
|     | Grouted Masonry               | (cu.m)    | 700                                      | 200                                   | 900          |
| 1.1 |                               |           |  |                                       |              |

#### b) Canal Works

The most of canal alignment is located at the top of hill with a flat area, so that excavation and fill of earth works are only made by bulldozer without any transportation such as dump truck. The concrete lining works are made by dividing into several working sections and placed by the mixer with small capacity for each section.

#### 1.2.5 On-farm Development Works

#### a) Work Volume

Two model areas of 200 ha in total were selected for the typical design of on-farm works in the project area. On the basis of the results of this design, the work volume of on-farm works is estimated. The on-farm works consists of land leveling, farm roads, farm ditches, drains and its related structures. Required areas of on-farm works are tabulated below:

|    | Item                  | <u>Bayogan</u> system | <u>Capayas system</u> | <u>Total</u> |
|----|-----------------------|-----------------------|-----------------------|--------------|
|    |                       |                       |                       |              |
| 1. | Land leveling works(h | a) 2,910              | 690                   | 3,600        |
| 2. | On-farm works (ha)    | 4.140                 | 1.160                 | 5,300        |

b) Land Leveling

Land leveling including plowing of cutting portion is made using the bulldozer for the existing upland field and grass land having a slope of 2 % on the average.

c) On-farm Facilities

These works will be carried out by the farmer's association under administration of the NIA office.

# 1.2.6 Construction Schedule of Civil Works

The construction schedule of Phase II project will be determined taking into consideration construction schedule of Phase I, since irrigation water is delivered to the proposed Bayongan reservoir through the main canal constructed during phase I of the project.

The construction works of Phase II will be commenced one year before the completion of construction work in Phase I of the project.

The construction of the Capayas system will be finished with construction period of about one year, because the Capayas service area would be developed as model agriculture area in early stage of the Phase II project.

The Bayongan system will be completed within three years from the beginning of the construction stage.

The summary of construction schedule is shown in FIGURE 6-3 of Main Report.

#### 1.3 Implementation Schedule of the Project

The construction of the major works will be commenced from about three years after completion of the Feasibility Study taking into consideration the loan procedures, detailed design and tendering for contract.

The construction of major works will be completed within about one and a half years for the Capayas system and about three years for the Bayongan system.

The on-farm works will be commenced in parallel with the major works to supply the water immediately after completion of the major works.

The implementation program for the project is shown in FIGURE 6-4 of Main Report.

# CHAPTER II COST ESTIMATION

2.1 Conditions of Cost Estimation

The project cost is estimated under the following conditions.

(1) The civil works are constructed on the contract basis.

The construction machinery and equipment required for construction will be provided by the contractors. Therefore, only depreciation costs of machinery and equipment are included to the estimated project cost.

- (2) The project cost is composed of construction cost and associated cost. Components of the project cost are shown in FIGURE J2-1.
- (3) The exchange rate between Philippine Pesos and U.S.Dollar; U.S. \$ 1.00 = 18.0 Philippines Pesos
- (4) The physical contigency related to the construction and associated cost is set at 15 % of the direct cost. The price contigency is assumed as follow.

| · ·  |                  | (unit: %)      |
|------|------------------|----------------|
| Year | Foreign Currency | Local Convency |
| • •  |                  |                |
| 1986 | 9.0              | 20.0           |
| 1987 | 9.0              | 20.0           |
| 1988 | 9.0              | 15.0           |
| 1989 | 7.5              | 10.0           |
| 1990 | 6.0              | 8.0            |
| 1991 | 6.0              | 8.0            |
| 1992 | 6.0              | 8.0            |
|      |                  |                |

2.2 Construction Cost

#### 2.2.1 Basic Rate

The basic rate of labor, material and construction equipment is estimated in the prevailing rate in the Philippines. Detailed basic rate is shown in TABLE J2-1 through J2-7.

## 2.2.2 Unit Cost

Unit cost of construction work is calculated, according to the proporsed work items which are designed by construction method since the construction is made on the contract basis, the overhead of 25 % against the unit rate is considered. Summerized unit cost is shown in TABLE J2-8 and detailed data are shown in Data book of the Report.

# 2.2.3 Construction Cost

The construction cost is divided into the foreign and local currency portions. The local currency portion is estimated on the basis of the current prices in Manila as of May,1985 and the foreign currency portion is estimated on the CIF prices at Manila. Construction cost is estimated based on unit cost for individual working items. The summary is shown TABLE J2-9 and breakdown is shown in TABLE J2-10 to J2-13.

2.3 Associated Cost

Associated cost is composed of five items, such as on-farm development cost, land acquisition & compensation cost, engineering & administration cost, 0 & M equipment cost and pilot farm cost.

Breakdown of each item is shown in TABLE J2-14 to J2-18.

2.4 Project Cost

2.4.1 Project Cost

The project cost is estimated at  $\cancel{V}$  659 million of which  $\cancel{V}$  401 millon is foreign currency and  $\cancel{V}$  258 million is local currency. The summary of the project cost is shown in Main Report TABLE 5-5.

#### 2.4.2 Annual Disbursement Schedule

The annual disbursement schedule is estimated on the basis of the project inplementation schedule, and the summary is as follows:

| Annua       | l Disbursement | Program |              |
|-------------|----------------|---------|--------------|
|             |                | · . (   | unit:1000 ₽) |
| <u>Year</u> | <u>F/C</u>     | L/C     | <u>Total</u> |
| 1987        | 25,300         | 7,800   | 33,100       |
| 1988        | 10,100         | 10,100  | 20,200       |
| 1989        | 83,200         | 59,600  | 142,800      |
| 1990        | 110,500        | 73,000  | 183,500      |
| 1991        | 128,000        | 80,800  | 208,800      |
| 1992        | 43,900         | 26,700  | 70,600       |
| Total       | 401,000        | 258,000 | 659,000      |

Details are shown in TABLE J2-19.

2.5 Operation and Maintenance Cost

The operation and maintenace cost annualy required for the project is composed of the salaries of 0 & M organization staff and the cost of operation and maintenance of 0 & M equipment and facilities. The operation and maintenance cost is estimated at  $\not$  592 per ha. Breakdown of 0 & M cost is shown in TABLE J2-20.

2.6 Replacement Cost

Some of the facilities, especially mechanical works have shorter useful life than the project life and require replacement within the project useful life. The following table shows the useful life and replacement costs of the mechanical works.

|                | · .                | (unit: 1000 ₽)   |
|----------------|--------------------|------------------|
| <u>Item</u>    | <u>Useful Life</u> | Replacement Cost |
| Gate           | 25 years           | 3,854            |
| 0 & M equipmen | t 10 years         | 7,100            |

2.7 Pilot Farm Cost

Cost of pilot farm constructed in the Capayas service area is estimated at  $\cancel{P}$  3,800,000. Detailed breakdown is shown in TABLE J2-21.

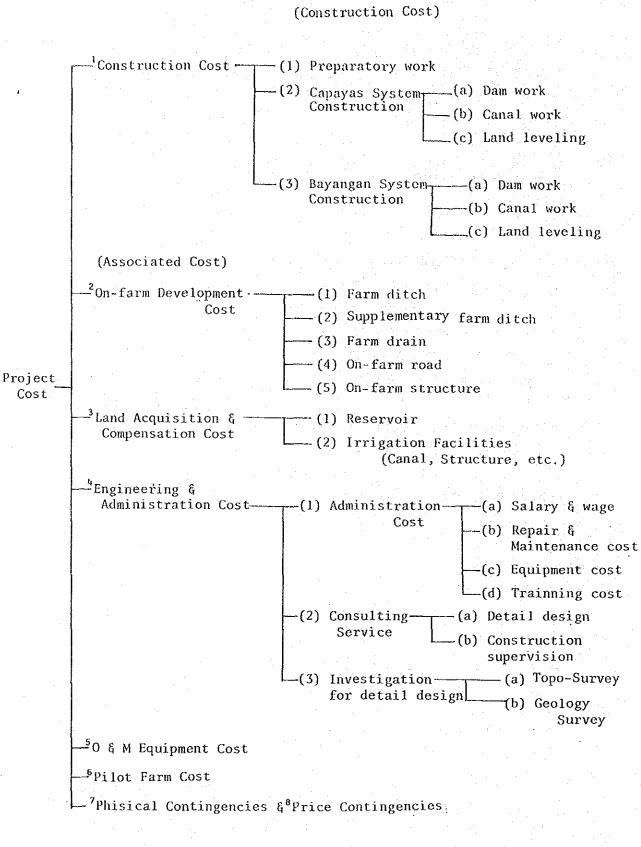


FIGURE J2-1 PROJECT COST COMPONENT

TABLE J2-1 LABOUR RATES (as of 1985)

|                           | Rates/Day |
|---------------------------|-----------|
|                           |           |
| Laborer                   | 50,00     |
| Skilled-Laborer           | 58.00     |
| General Foreman           | 84.00     |
| Carpenter                 | 65.00     |
| SR Carpenter              | 74.00     |
| Head, Carpenter           | 79.00     |
| SR Mason                  | 69,00     |
| Head, Mason               | 74.00     |
| Steelman                  | 65.00     |
| Head, Steelman            | 74.00     |
| Welder                    | 65,00     |
| C.E. AIDE                 | 65.00     |
| Driver, (Light Equipment) | 65.00     |
| Driver, (Heavy Equipment) | 74.00     |
| Driver, (General)         | 69,00     |
| Mechanic                  | 65.00     |
| Master Mechanic           | 74.00     |
| Electrician               | 65.00     |
| Driller                   | 74.00     |
| Blaster                   | 178.00    |
| Plumber                   | 61.00     |
| Batch plant               | 65.00     |
| Watchman                  | 58.00     |
| Janitor                   | 50.00     |
| Surveyor                  | 97.00     |

|                              |                | Total   | Compor | ient- | Unit C                        | Unit: )<br>ost |
|------------------------------|----------------|---|--------|-------|-------------------------------|----------------|
| Description                  | Unit           | Unit Cost   | F.C    | L.C   | F.C                           | L.C            |
| teinforced Bar               | kg             | 10.5  | 80     | 20    | 8.5                           | 2.0            |
| ail, Bolt and Nut            | kg             | 18.0  | 80     | 20    | 14.5                          | 3.5            |
| pecial Gasoline              | l              | 9.0   | 80     | 20    | 7.5                           | 1.5            |
| asolin                       | ł              | 8.5   | 80     | 20    | 7.0                           | 1.5            |
| Diesel                       | £              | 6.5   | 80     | 20    | 5.5                           | 1.0            |
| ubricating Oil               | R              | 30.0  | 80     | 20    | 24.0                          | 6.0            |
| Cement (1 Bag 0.40 kg)       | Bag            | 50.0  | 60     | 40    | 30.0                          | 20.0           |
| einforced Concrete Pipe (1") |                | an an taon taon taon taon taon taon taon  |        |       |                               |                |
| ø450 (18")                   | p.c.           | 360.0   | 60     | 40    | 215.0                         | 145.0          |
| ø600 (24 <sup>11</sup> )     | p.c.           | 400.0   | 60     | 40    | 240.0                         | 160.0          |
| ø750 (30'')                  | p.c.           | 500.0   | 60     | 40    | 300.0                         | 200.0          |
| ø900 (36'')                  | 0.c.           | 650.0   | 60     | 40    | 390.0                         | 260.0          |
| ø1000                        | p.c.           | an a  | 60     | 40    |                               |                |
| ø1300                        | p.c.           | 900.0   | 60     | 40    | 540.0                         | 360.0          |
| oncrete Hollow Block         | 11.1           | n an an an an Arrange.<br>An an an Arrange an Arr |        |       |                               |                |
| 4' x 8' x 16'                | p.c.           | 3.0   | 60     | 40    | 2.0                           | 1.0            |
| 6' x 8' x 16'                | p.c.           | 4.0   | 60     | 40    | 2.5                           | 1.5            |
| lasting ( Dynamite           | kg             | 32.0  | 80     | 20    | 26.0                          | 6.0            |
| laterial E A.N.F.O           | kg             | 30.0  | 80     | 20    | 24.0                          | 6.0            |
| E Detanator                  | p.c.           | 21.0  | 80     | 20    | 17.0                          | 4.0            |
| E Fuse                       | m              | 10.5  | 80     | 20    | 8.5                           | 2.0            |
| umber                        | bd.ft*         | 8.0   | 0      | 100   | 0                             | 8.0            |
| lywood 1/4 x 4 x 8           | p.c.           | 68.0  | 0      | 100   | 0                             | 68.0           |
| $1/2 \times 4 \times 8$      | p.c.           | 145.0   | 0      | 100   | <sup>1</sup> · · · · <b>0</b> | 145.0          |
| od                           | m <sup>2</sup> | 1.2   | 0      | 100   | ын а то <mark>о</mark> то     | 1.2            |

TABLE J2-2 UNIT COST OF CONSTRUCTION MATERIAL (1)

\* 1 bd.ft x 1.0 feet x 1.0 feet x 10 inch x 0.0023 cu.m

TABLE J2-3 UNIT COST OF CONSTRUCTION MATERIAL (2)

|                |          |                  |           | - Un     | it;₿   |
|----------------|----------|------------------|-----------|----------|--------|
| Description    | Unit     | Total            | Comporner |          | t Cost |
| Description    | 01110    | <u>Unit Cost</u> | F.C: L.C. | F.C.     | L.C.   |
| Drilling { Rod | <br>p.c. | 1,103.00         | 80 20     | 883.0    | 220.0  |
| Bid            | р.с.     | 1,545.00         | 80 20     | 1,236.0  | 309.   |
| E Sleaves      | p.c.     | 625.00           | 80 20     | 500.0    | 125.   |
| Small Gate     |          |                  |           |          |        |
| 600 x 600mm    | p.c.     | 3,800.00         | 80 20     | 3,040.0  | 760.   |
| 800 x 800mm    | p.c.     | 4,400.00         | 80 20     | 3,520.0  | 880.   |
| 1200 x 1200mm  | p.c.     | 12,000.00        | 80 20     | 9,600.0  | 2,400. |
| 1600 x 1400mm  | p.c.     | 16,000.00        | ·80 20    | 12,800.0 | 3,200. |
| 1600 x 1600mm  | p.c.     | 17,000.00        | 80 20     | 13,600.0 | 3,400. |
| H-Beam         | kg       | 18.00            | 80 20     | 15.0     | 3.     |
| L-Beam         | kg       | 13.00            | 80 20     | 11.0     | 2.     |

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LAND ACQUISITION AND COMPENSATION COST

|  |          |           |            |      | ι         | lnit;₽   |
|--|----------|-----------|------------|------|-----------|----------|
|  |          | Total     | Compornent |      | Unit Cost |          |
| Description  | Unit     | Unit Cost | F.C.       | L.C. | F.C.      | L.C.     |
| Mauntain Area  | ha       | 4,000     | 0          | 100  | 0         | 4,000.0  |
| Waste Area   | ha       | 6,000     | 0          | 100  | 0         | 6,000.0  |
| Cultivated Area  | ha       | 10,000    | 0          | 100  | 0         | 10,000.0 |
| Housing  | 1 house  | 20,000    | 0          | 100  | 0         | 20,000.0 |
| Housing Site   | 1 house  | 2,400     | 0          | 100  | 0         | 2,400.0  |
| Resettlement Cost<br>(Hauling charge and<br>allowance) | l family | 6,000     | 0          | 100  | 0         | 6,000.0  |

TABLE J2-4 ADOPTED PROPORTION OF FOREIGN AND LOCAL COMPORNENT

|     | Description                       | Foreign<br>Compornent | Local<br>Compornent |
|-----|-----------------------------------|-----------------------|---------------------|
| 1.  | Cement                            | 60 <sup>(%)</sup>     | 40 <sup>(%)</sup>   |
| 2.  | Reinforced Bar                    | 80                    | 20                  |
| 3.  | Fuel and Oil                      | 80                    | 20                  |
| 4.  | Equipment for Construction        | 80                    | 20                  |
| 5.  | Equipment for Agriculture         | 70                    | 30                  |
| 6.  | Truck & vehicle                   | 70                    | 30                  |
| 7.  | Blasting Materials                | 80                    | 20                  |
| 8.  | Steel Gate & Steel Structure      | 80                    | 20                  |
| 9.  | Lumber                            | 0                     | 100                 |
| 10, | Labour                            | 0                     | 100                 |
| 11. | Land Acquisition and Compensation |                       | 100                 |
| 12. | Taxes and Bonding Charges         | 0                     | 100                 |
| 13. | Contractors Profit                | 50                    | 50                  |
| •   |                                   |                       |                     |

The source: Tariff and Customs Code 1982 Vol 1

# TABLE J2-5 HIRING RATE AND FUEL CONSUMPTION (Per Hr)

|                       | · .                           |          | Capital | Hiring | Equipmen | nt Rate | Fuel             |
|-----------------------|-------------------------------|----------|---------|--------|----------|---------|------------------|
| Fquipment             |                               |          | Cost    | Rate   | F/C      | L/C     | Con-<br>sumption |
|                       |                               |          | x1000   | x0,001 |          | ······  | (१)              |
| Bulldozer             | 21t                           | 200 p.s. | 1,997   | 0.345  | 550      | 140     | 21               |
| Bulldozer (with Rippo | er) 21t                       | 200 p.s. | 2,220   | 0.353  | 630      | 160     | 21               |
| Bulldozer             | 15t                           | 150 p.s. | 1,268   | 0,345  | 350      | 90      | 16               |
| Bulldozer             | 11t                           | 108 p.s. | 977     | 0.345  | 270      | 70      | 11               |
| Bulldozer             | 8t                            | 86 p.s.  | 746     | 0.433  | 260      | 70      | 9                |
| Backhoe shovel        | $1.0^{m^3}$                   | 175 p.s. | 2,614   | 0,292  | 610      | 150     | 19               |
| Backhoe shovel        | 0.6 <sup>m<sup>3</sup></sup>  | 108 p.s. | 1,440   | 0.292  | * 340    | 80      | 12               |
| Backhoe shovel        | 0.35 <sup>m<sup>3</sup></sup> | 78 p.s.  | 951     | 0.308  | 230      | 60      | 9                |
| Wheel loader          | 1,70 <sup>m<sup>3</sup></sup> |          | 1,020   | 0.374  | 310      | 80      | 8                |
| Wheel loader          | 1,20 <sup>m<sup>3</sup></sup> |          | 617     | 0.374  | 190      | 50      | 6                |
| Tunnel muck loader    | 0.35 <sup>m<sup>3</sup></sup> | \$       | 1,097   | 0.450  | 400      | 100     |                  |
| Dump truck            | llt                           | 314 p.s. | 690     | 0.303  | 170      | 40      | 11               |
| Dump truck            | 4t                            | 160 p.s. | 243     | 0.385  | 80       | 20      | 6                |
| Truck                 | 6.5t                          | 175 p.s. | 294     | 0.361  | 90       | 20      | 6                |
| Truck                 | 4.5t                          | 164 p.s. | 229     | 0.385  | 70       | 20      | 6                |
| Water Lorry           | 4t                            | 155 p.s. | 373     | 0.336  | 100      | 30      | 6                |
| Truck crane           | 15t                           | 230 p.s. | 1,808   | 0.239  | 350      | 90      | 9                |
| Truck crane           | 20t                           | 230 p.s. | 2,031   | 0.239  | 390      | 100     | 9                |
| Road Roller           | 8~10t                         | 90 p.s.  | 518     | 0,355  | 150      | 40      | 6                |
| Vibrating Roller      | 8~10t                         | 105 p.s. | 1,123   | 0.479  | 430      | 110     | 11               |
|                       | 3~5t <sup>.</sup>             | 23 p.s.  | . 310   | 0.479  | 120      | 30      | 3                |
| Tamping Roller        | 8~15t                         |          | 523     | 0.321  | 130      | 30      |                  |
| Tamping Roller        | 3~ 5t                         | _        | 223     | 0.321  | 60       | 10      |                  |
| Motor Grader          | 1. = 2.511                    | 76 p.s.  | 740     | 0.356  | 210      | 50      | 5                |
| Motor Grader          | L = 3.1H                      | 110 p.s. | 883     | 0.356  | 250      | 60      | 7                |
|                       |                               |          |         |        |          |         |                  |

TABLE J2-6 HIRING RATE AND FUEL CONSUNPTION (Per hr or Day)

|                                  | · · · ·                                   |   |                      |                        |                   | Unit: | Y                   |
|----------------------------------|---|---|----------------------|------------------------|-------------------|-------|---------------------|
|                                  |   |   | Capital              | Hiring                 | Equipment         | Rate  | Fuel                |
| Equipment                        |   | ar an<br>Thair an | Cost                 | Rate                   | F/C               | L/C   | Con-<br>sumption    |
| Compressor                       | 10.5m³/mii                                | (per day)<br>1 105 p.s.                               | 321 <sup>×1000</sup> | 2.500 <sup>x0.00</sup> | <sup>)1</sup> 640 | 160   | 26 <sup>2/day</sup> |
| Compressor                       | 7.Om <sup>3</sup> /min                    | (per day)<br>75 p.s.<br>(per day)                     | 243                  | 2,500                  | 490               | 120   | 191                 |
| Compressor                       | 9.5m³/min                                 | (per day)<br>46 p.s.<br>(per day)                     | 124                  | 2,500                  | 250               | 60    | 12"                 |
| Compressor                       | 20m³/min                                  | 28 p.s.<br>(per day)                                  | 103                  | 2.500                  | 206               | 52    | .7"                 |
| Generator                        | 15 kw                                     | 22 p.s.<br>(per day)                                  | 75                   | 2,231                  | 1 30              | 30    | 6"                  |
| Generator                        | 45 kw                                     | 58 p.s.<br>(per day)                                  | 222                  | 1,987                  | 350               | 90    | 15 <sup>11</sup>    |
| Generator                        | 75 kw                                     | 93 p.s.<br>(per day)                                  | 250                  | 1.987                  | 400               | 100   | 23"                 |
| Generator 1                      | 00 kw                                     | 120 p.s.<br>(per day)                                 | 351                  | 1,987                  | 560               | 140   | 30"                 |
| Drainage pump ø80m/m             | H-10M                                     | 2.2 kw<br>(per day)                                   | 12                   | 3.194                  | 30                | 10    |                     |
| Drainage pump \$110m/m           | H-20M                                     | ll kw<br>(per day)                                    | 35                   | 3,194                  | 90                | 20    |                     |
| Furbin pump ø100m/m              | -<br>-<br>-                               | 7.5 kw<br>(per day)                                   | 37                   | 3.194                  | 90                | 20    |                     |
| later pump ∮50m/m                | ta an | 1.7 kw<br>(per day)                                   | 14                   | 3,750                  | 42                | 11    | 1. P.               |
| ater pump ø100m/m                |   | 3.7 kw<br>(per day)                                   | 15                   | 3.750                  | 50                | 10    | · · .               |
| later pump ǿ150m/m               | 9 /min                                    | 7.5 kw<br>(per day)                                   | 22                   | 3.750                  | 66                | 17    | · ·                 |
| routing pump 15 ~ 34             | 0~7                                       | 2.2 kw<br>(per day)                                   | 44                   | 3.648                  | 130               | 30    |                     |
| routing mixer 2001               |   | 5.5 kw  | 37                   | 3.648                  | 110               | 30    |                     |
| Concrete plant 0.5m <sup>3</sup> | 26m <sup>3</sup> /h                       | 4.1 kw<br>(per day)                                   | 817                  | 0.463                  | 300               | 80    |                     |
| Concrete mixer 0.5m <sup>3</sup> |   | 3.5 kw  | 817                  | 0.463                  | 300               | 80    |                     |
| Concrete pump car 20 p           |   | 80 p.s.   | 814                  | 0.413                  | 270               | 70    | 6                   |
| fruck mixer 3.0 m <sup>3</sup>   |   | 220 p.s.  | 529                  | 0.360                  | 150               | 40    | 8                   |
| Crawler Drill (10m cla           |   | · · ·   | 618                  | 0.479                  | 240               | 60    | :                   |
| land Rammer 20kg (per            | 4   |   | 15                   | 4.808                  | 60                | 10    | at a                |
| Drifter for tunnel 30            | ~ •                                       |   | 20                   | 4.808                  | 80                | 20    | ·.· · ·             |
| lassifier 105cm x 75             | · ·                                       | 3.7 kw  | 697                  | 0.210                  | 120               | 30    |                     |
|                                  | x 480                                     | 22 kw   | 599                  | 0.225                  | 110               | 30    | •                   |
| Belt conveyer 45cm x             | 15m                                       | 2.2 kw<br>(per day)                                   | 114                  | 0.230                  | 20                | 10    |                     |
| ibrator 45 m/m                   | •   | 5.0 p.s.  | 13                   | 4.028                  | 40                | 10    | 1                   |
| ater pipe 100m/m                 |   |   | 0.3                  | 2:713                  | 0.7               | 0.2   |                     |
| ggregate Hopper                  |   |   | 34                   | 2.639                  | 72                | 18    |                     |

TABLE J2-7FUEL CONSUMPTION OF EQUIPMENT (Per Hr)

| Equipment         | Fuel Consumption  |
|-------------------|-------------------|
| Bulldozer         | 0.105 (l/p.s./hr) |
| Backhoe           | 0.110             |
| Wheel Loader      | 0.080             |
| Dump Truck        | 0.035             |
| Fruck             | 0.036             |
| Motor Grader      | 0.067             |
| Road Roller       | 0.065             |
| Vibrating Roller  | 0.109             |
| Concrete Pump Car | 0.072             |
| Water Lorry       | 0.036             |
| Truck Crane       | 0.040             |
| Other Equipment   | 0.050             |

J-25

1.1

|   |                | <u> </u> | payas S  | vstem          |              | nit : P<br>yangan                        |        |
|---|----------------|----------|----------|----------------|--------------|--|--------|
| Description of works  | Unit           | B/C      | L/C      | Total          |              | 1./C                                     | Total  |
|   |                |          |          |                | <u></u>      |  |        |
| Dam Construction  |                |          | <u> </u> | 21             | 22           | 9  | 71     |
| . Stripping   | cu.m           | 15       | 6        |                |              | 1  | 31     |
| . Earth excavation in trench & intake   | <b>u</b> []    |          | 8        | 27             | 25           | 10                                       | 35     |
| . Soft Rock Excavation in Trench &<br>Intake  | <b>t</b> 4     | - 35     | 15       | 50             | 45           | 18                                       | 63     |
| . Earth Excavation in Spillway  | .11            | 19       | 8        | 27             | 40           | 16                                       | S6     |
| . Soft Rock Excavation in Spillway  | 11             | 35       | 15       | 50             | 64           | 25                                       | . 89   |
| . Core material transportation  | щ              | -        | -        | · · ·          | 25           | 10                                       | 35     |
| . " compaction  |                | -        |          | -              | 17           | 7  | 24     |
| . Shell material transportation   | <b>11</b><br>  |          |          | -              | 27           | 11                                       | 38     |
| " compaction  |                |          | -        | <u> </u>       | 11           | 4  | 15     |
| . Filter material transportation  | , <b>H</b>     | 67       | 26       | • 93           | 67           | 26                                       | 93     |
| . " compaction  | . **           | 15       | . 7      | 22             | 15           | 7  | 22     |
| . Riprap material transportation  | . <u>1</u>     | 102      | 42       | 144            | 102          | 42                                       | 144    |
| " compaction  | . <b>61</b>    | 6        | 2        | 8              | 6            | 2  | 8      |
| . Earth material transportation   | **             | 17       | 7        | 24             | · · ·        | · · -                                    |        |
| . " compaction  | 11             | 12       | 5        | 17             |              | -  |        |
| . Toe Material excavation &   | 14             | 19       | 7        | 26             | 11 - 14<br>1 | -  | · -    |
| transportation  | -<br>-         |          | ÷        |                |              | an a |        |
| . <sup>11</sup> Compaction  | 11             | 10       | 5        | 15             |              |  | · · ·  |
| . Tunnel excavation of Intake   | ч              |          | · -      | <del>-</del> . | 436          | 221                                      | 657    |
| . Tunnel steel Support  | set            | · _      | 1        |                | 3,694        | 1,358                                    | 5,057  |
| . Tunnel Concrete canal   | cu.m           | -        | -        | - 3            | 1,172        | 783                                      | 1,955  |
| . Tunnel Grout  | cu.m           | · . ~    |          | . <b>-</b>     | 1,796        | 776                                      | 1,572  |
| . Drilling of Grout Holes   | hole           | · _      | · -      | <u>ئ</u>       | 55           | 34                                       | - 89   |
| . Intake concrete (class A)   | cu.m           | 741      | 696      | 1,437.         | 735          | 677                                      | 1,412  |
| . Spillway concrete ( " )   | <b>с</b> і     | 741      | 696      | 1,437          | 731          | 629                                      | 1,360  |
| Canal Construction  |                |          |          |                |              |  |        |
| . Stripping   | cu.m           | .6       | . 2      | 8              | 6            | 2  | ŧ      |
| . Canal Excavation  |                | 29       | 13       | 42             | 29           | 13                                       | 4      |
| . Excavation at side borrow area  | <b>1</b> 4 ·   | 8        | 3        | 11             | 8            | 3  | . 1    |
| . Canal fill compaction   | . <del>1</del> | 16       | 8        | 24             | 16           | . 8                                      | 24     |
| . Back fill at canal  | 11             | 13       | . 7      | 20             | 13           | . 7                                      | 20     |
| . Lining concrete   | 17             | 834      | 576      | 1,410          | 834          | 576                                      | 1,410  |
| . Structure concrete  | 11             | 92.4     | 1,174    | -2,098         |              | 1,174                                    | 2,09   |
| · Structure Concrete  |                | 541      |          | 2,000          |              | -,                                       |        |
| On-farm Construction  |                |          |          |                |              |  |        |
| . Farm Ditch (16.2m/ha)   | ha             | 421      | 218      | 639            | 421          | 218                                      | 639    |
| . Supplementary Farm Ditch (50.9m/ha)   | <b>1</b> 1     | 1,170    | \$33     | 1,703          | 1,170        | 533                                      | 1,70   |
| . Farm Drain (14.1m/ha)   | . 11           | 127      | 62       | 189            | 127          | . 62                                     | 189    |
| . Farm Road (46.2m /ha)   | ••             | 369      | 180      | 549            | 369          | 180                                      | 545    |
| . On-farm Structures  | ••             | 471      | 309      | 780            | 471          | 309                                      | 780    |
| . Land leveling   |                | 2,820    | 1,097    | 3,917          | 2,820        | 1,097                                    | 3,91   |
| Deep plawing  | ••             | 581      | 195      | 776            | 581          | 195                                      | 770    |
| . Ridge Preparation   |                | 760      | 476      | 1,226          | 760          | 476                                      | 1,220  |
| Common Unite Rate   |                |          | · .      |                |              |  |        |
| . Rainforced Bar  | t              | 11,119   | 4,337    | 15 451         | 11 110       | A 77-                                    | 10 40  |
| <ul> <li>A set of the set of</li></ul> |                | 22       |          | 15,456         | 1 - E        | 1. I.                                    | 15,450 |
| . Back Fill   | cu.m           | 22       | 9        | 31             | 22           | 9  | 31     |
|   |                |          |          |                |              |  |        |
|   | J-26           | 1.1      |          |                | 6 A.         |  |        |

# TABLE J2-8 MAJOR UNIT RATE

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|                  |        | TABLE J2-9     |         | CONSTRUCTION COST | N COST          |                       |         |                |         |
|------------------|--------|----------------|---------|-------------------|-----------------|-----------------------|---------|----------------|---------|
|                  |        |                |         |                   |                 | ·<br>·<br>· · · · · · |         | (Unit : P'000) | (000)   |
|                  | ů      | Capayas System | E       | <i>в</i>          | Bayongan System | tem                   |         | Total          |         |
| Description      | F/C    | L/C            | Total   | F/C               | L/C             | Total                 | F/C     | L/C            | Total   |
| Preparatory Work | 200    | 400            | 006     | 1,500             | 1,500           | 2,800                 | 2,000   | 1,700          | 5,700   |
|                  |        |                |         |                   |                 |                       |         |                |         |
| Temporary work   | 861    | 487            | 1,348   | 10,600            | 4,460           | 15,060                | 11,461  | 4,947          | 16,408  |
| - Dam            | 8,963  | 3,695          | 12,658  | 57,431            | 23,052          | 80,483                | 66, 394 | 26,747         | 93,141  |
| - Spillway       | 5,250  | 3,095          | 8,345   | 7,239             | 3,508           | 10,747                | 12,489  | 6,603          | 19,092  |
| - Intake         | 1,826  | 1,023          | 2,849   | 5,830             | 2,780           | 8,610                 | 7,656   | 5,803          | 11,459  |
| Sub Total        | 16,900 | 8,300          | 25,200  | 81,100            | 33,800          | 114,900               | 98,000  | 42,100         | 140,100 |
| Canal Work       |        |                |         |                   | •               |                       |         |                |         |
| - Temporary work | 204    | 172            | 376     | 505               | 534             | 1,437                 | 1,107   | 706            | 1,813   |
| - Main Canal     | 2,871  | 1,386          | 4,257   | 24,007            | 12,724          | 36,731                | 26,878  | 14,110         | 40,988  |
| - Lateral Canal  | 4,312  | 2,188          | 6,500   | 14,881            | 8,014           | 22,895                | 19,193  | 10,202         | 29,395  |
| - Drainage Canal | 1,313  | 854            | 2,167   | .2,909            | 2,428           | 5,337                 | 4,222   | 3,282          | 7,504   |
| Sub Total        | 8,700  | 4,600          | 13, 300 | 42,700            | 23,700          | 66,400                | 51,400  | 28,300         | 79,700  |
| On-Farm          |        |                |         |                   |                 |                       |         |                | ·       |
| - Land Leveling  | 3,000  | 1,300          | 4, 300  | 12,700            | 5,400           | 18,100                | IS, 700 | 6,700          | 22,400  |
| Total            | 29,100 | 14,600         | 43,700  | 138,000           | 64,200          | 202,200               | 167,100 | 78,800         | 245,900 |
|                  |        |                |         |                   |                 |                       |         |                |         |

TABLE J2-9 CONSTRUCTION COST

Remarks 800 1,600 600 200 400 Total Amount (p\*000) L/C 320 240 640 400 80 F/C 480 960 360 120 1 2,000 3,000 1,000 400 2,000 Total Unit Rate L/C 1,200 800 800 400 400 F/C 1,200 1,200 1,800 . 600 Quantity 400 800 200 200 sq.m sq.m sq. n Unit sq.m L.S Facilities for Construction Supervision Equipment warehouse Description of Item . Staff Residence . Guest House Preparatory works . Main Office . Furniture

TABLE J2-10 CONSTRUCTION COST ESTIMATION FOR PREPARATORY WORK

J-28

Total

3,600 )

1,680

(1,920

|  | 14             | 3 )x0.05  | <br>   |   | · · · · · · · · · · · · · · · · · · ·   |  |  |
|--|----------------|---|--|---|---|--|--|
|  | Remarks        | { 1 + 2 +   |  |   |   |  |  |
| ĒM                                       | ))<br>Total    | 1,348<br>1,348  | 756<br>270<br>300  | 7,749<br>366  | 2,477<br>2,477<br>33<br>603<br>12,658 )   | 567<br>250<br>3,737<br>2,627<br>720<br>8,345<br>8,345  | 230<br>50<br>113<br>1,222<br>851   |
| YAS SYSTEM                               | Amount (P1000  | 487<br>487  | 216<br>80<br>90  | 2,268   | 30<br>717<br>10<br>176<br>176<br>3,695  | 168<br>75<br>14<br>14<br>737<br>144<br>144<br>3,095  | 2 2 2 4 1 5 8<br>2 3 5 4 1 5 8<br>3 3 2 7 9 9 7 8  |
| FOR CAPA                                 | Amo<br>F/C     | 861<br>861  | 540<br>190<br>210  | 5,481<br>258  | 1,760<br>23<br>427<br>(8,963  | 399<br>175<br>1,927<br>1,890<br>1,890<br>250<br>(5,250   | 162<br>35<br>71<br>630<br>612  |
| LIMATION                                 | Total          |   | 27<br>27<br>27   | 04 di   | 152<br>152<br>41  | 27<br>50<br>31<br>1,437<br>15,456<br>2,000   | 27<br>50<br>51,451<br>1,451<br>1,451<br>1,457  |
| COST ES1                                 | it Rate<br>L/C |   | \$\$<br>\$<br>\$   |   | 44 5<br>74 4<br>75  | 8<br>15<br>896<br>4,337<br>400   | 4<br>15<br>73<br>75<br>75<br>75<br>75<br>75<br>75<br>75<br>75<br>75<br>75<br>75<br>75<br>75  |
| CONSTRUCTION COST ESTIMATION FOR CAPAYAS | E/C            |   | 505<br>11 11 11  | 56 70<br>11 56  | 108<br>108<br>29  | 19<br>30<br>741<br>11,119<br>1,600   | 19<br>35<br>22<br>914<br>741<br>119  |
|  | Quantity       |   | 36,000<br>10,000   | 189,000<br>21,500   | 16, 300<br>800  | 21,000<br>5,000<br>1,500<br>2,600<br>360   | 8,500<br>1,000<br>1,000<br>850<br>55   |
| TABLE J2-11(1)                           | Unit           | н<br>   | er no<br>cr m  | = = :   | = = =   | cu.m<br><br>Ton<br>sq.m  | си. н<br>си. н<br>си. н<br>си. н<br>сол  |
| TAB                                      | on of Item     |   | ų,   | it by Excavated   | ent<br>cment<br>(5%)  | on<br>vation<br>A<br>(S%)  | ition<br>ccavation<br>δe φ 1300mm<br>iss A<br>Sar  |
|  | Description    | <ol> <li>Capayas Dam<br/>(1) Temporary works<br/>Sub Total</li> </ol> | <pre>(2) Dam works Stripping Earth Excavation Cort Provision</pre> | Earth Embankment<br>Earth Embankment by Excavated<br>Material | Filter Embankment<br>Riprap Embankment<br>Toe Rock Embankment<br>Miscellaneous (5%<br>Sub Total | <pre>(3) Spillway<br/>Earth Excavation<br/>Soft Rock Excavation<br/>Backfill<br/>Concrete Class A<br/>Rainforced Bar<br/>Bridge<br/>Miscellaneous (5%)<br/>Sub Total</pre> | <ul> <li>(4) Intake<br/>Earth Excavation<br/>Soft Rock Excavation<br/>Backfill<br/>Concrete pipe φ 1500mm<br/>Concrete Class A<br/>Rainforced Bar</li> </ul> |

TABLE J2-11(2) CONSTRUCTION COST ESTIMATION FOR CAPAYAS SYSTEM

| F/C<br>49,040<br>66<br>29<br>16<br>24<br>23<br>23<br>23<br>324<br>324      | 777<br>777<br>2<br>13<br>8<br>11<br>9   | 817<br>817<br>355<br>355<br>355<br>355<br>355<br>355<br>355<br>355<br>355<br>35  | F/C<br>F/C<br>(1,87<br>87<br>87<br>((16,900<br>((16,900<br>(16,900<br>(16,900<br>(16,900<br>(16,900<br>(16,900<br>(16,900<br>(16,900<br>(16,900<br>(16,900<br>(16,900<br>(16,900<br>(16,900)<br>24<br>(1,82<br>(1,82<br>(1,82<br>(1,82<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>(1,82)<br>( | CC L/C L/C L/C L/C L/C L/C L/C 264 1 2526 1,023 326 1,023 900 8,300 8,300 8,300 8,300 8,300 8,300 8,300 8,300 8,300 8,300 8,300 8,300 8,100 96 48 15 | Total<br>50<br>2,849 )<br>25,200 ))<br>376 )<br>376 )<br>355<br>144       | Remarks<br>( 5 + 6 + 7 )x2%   |
|--|---|--|---|--|---|---|
| 49,040<br>6<br>6<br>26<br>24<br>24<br>24<br>24<br>324<br>924               |   | 817<br>8817<br>8817<br>812<br>812<br>812<br>812<br>812<br>812<br>812<br>812<br>812<br>817<br>817<br>817<br>817<br>817<br>817<br>817<br>817<br>817<br>817 | 49<br>(1,826<br>((16,900<br>((16,900<br>204<br>(204<br>34<br>244<br>36<br>34<br>2   |  | 50<br>136<br>2,849 )<br>25,200 ))<br>376 )<br>376 )<br>144<br>144         | ►<br>+<br>\$  |
| 11<br>119<br>119<br>119<br>119<br>119<br>119                               | م با ه<br>ا ه با ه ا  | 2 3 3 4 7 8<br>2 1 0 4 8<br>2 1 0 4 8  | 87<br>87<br>87<br>87<br>87<br>204<br>(16,900<br>(204<br>244<br>34<br>34<br>25<br>34   | N N  | 136<br>2,849 )<br>25,200 ))<br>376 )<br>376 )<br>144<br>144<br>149        | ►   |
| 11<br>119<br>119<br>119<br>119<br>119<br>119                               | ر با ۳۵ م<br>۱۳۵۱ م   | 2 4 2 2 8<br>8 4 2 8<br>9 1 0 1 0 1 0  | ((16,900<br>204<br>34<br>34<br>34<br>2<br>2   | <ul> <li>N</li> <li>1</li> </ul>   | 25,200 ))<br>376 )<br>376 )<br>355<br>144<br>49                           | ۲<br>ب<br>ب   |
| 11<br>119<br>119<br>119<br>119<br>119<br>119<br>119<br>119<br>119          | م با ه<br>ا ه با ه ا  | 3 3 2 4 8<br>3 3 5 4 8<br>3 5 4 8  | 2000<br>2000<br>2000<br>2000<br>2000<br>2000<br>2000<br>200   | 172<br>172<br>109<br>15  | 376<br>376<br>353<br>144<br>49  | r<br>+<br>\$  |
| 22<br>16<br>11<br>119<br>119<br>119<br>119                                 | 2 2 8 1 8 1<br>1 8 1 8 1<br>1 8 1 8 1<br>1 8 1 8 | 4 2 2 4 8<br>2 4 2 8 4<br>0 1 2 4 8  | 、<br>202<br>202<br>202<br>202<br>202<br>202<br>202<br>202<br>202<br>20  | 172<br>172<br>112<br>109<br>15   | 376<br>376<br>353<br>353<br>144<br>49                                     | <ul> <li>►</li> <li>↓</li> <li>↓</li> <li>↓</li> <li>↓</li> <li>↓</li> </ul>  |
| 26<br>24<br>24<br>24<br>24<br>24<br>22<br>24<br>22<br>24<br>21<br>11<br>11 | 2 2 2 2 7 5 7 5 5 5 5 5 5 5 5 5 5 5 5 5   | 8<br>35<br>31<br>31<br>31<br>31<br>31<br>32<br>31<br>31<br>31<br>31<br>31<br>31<br>31<br>31<br>31<br>31<br>31<br>31<br>31                                | )<br>00<br>00<br>00<br>00<br>00<br>00<br>00<br>00<br>00<br>00<br>00<br>00<br>00   | 172<br>11<br>109<br>15   | 144<br>49<br>49   | <<br>►<br>►   |
| 6<br>16<br>22<br>832<br>832<br>924<br>111119                               | 2 2 2 2 1 3 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5   | 42<br>835<br>35<br>35<br>35  | ы<br>14<br>14<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10   | 101<br>109<br>158<br>158   | 35 35<br>144<br>49  | ·<br>· · · · ·  |
| 6<br>16<br>24<br>22<br>834<br>924<br>11<br>119                             | 12 12 12 12 12 12 12 12 12 12 12 12 12 1  | 42<br>31<br>35<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10   | 88<br>84<br>84<br>80<br>84<br>80<br>84<br>80<br>84<br>80<br>84<br>80<br>84<br>80<br>84<br>80<br>84<br>80<br>84<br>80<br>84<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80<br>80  | 11<br>109<br>158<br>158  | 353<br>353<br>144<br>49   |   |
| 29<br>16<br>24<br>22<br>834<br>924<br>1119                                 | 11 °13  | 42<br>335<br>42<br>35<br>42<br>24<br>24<br>24<br>24<br>24<br>24<br>24<br>24<br>24<br>24<br>24<br>24  | 244<br>96<br>34<br>2  | 109<br>48<br>15  | 353<br>144<br>49  |   |
| 16<br>24<br>23<br>834<br>924<br>11,119                                     | ° ដី ទំ   | 24<br>35<br>31<br>31   | 96<br>34<br>2   | 15   | 144<br>49   |   |
| 24<br>22<br>834<br>924<br>11-119   | ii o j  | 35<br>31<br>710  | 34  | 15   | 49  |   |
| 22<br>834<br>924<br>11.119   | ດ   | 31   | 64  |  |   |   |
| 834<br>924<br>11.119   |   | 017  | •   | ₽~ <b>€</b> `  |   |   |
| 924<br>11.119  |   | ) + F<br>+ F<br>+ F  | 1,284   | 887  | 2,171   |   |
|  | 1,1,4<br>1,277  | 2,098  | 74  | 71 X<br>   | 204<br>26   |   |
|  | •   |  | ער מ<br>חייני<br>חייני  |  |   |   |
| 100  | 1<br>2<br>4<br>7<br>7<br>7<br>7   | 2000 ° 4   | 1<br>1<br>1<br>1  | † 0<br>† ¥   | 125   | •   |
| ,<br>N   | , n   | 201  | 285   | 00   | 16  |   |
| 319  | 144   | 463  | 64  | 29   | 93  |   |
| 352  | 163   | 515  | 35  | 16   | 51  |   |
| 616  | 2.74  | 890  | 62  | 27   | 83  |   |
| 1  | ľ   |  | 542-  | 28   | 570   |   |
| 3,125  | 781   | 3,906  | 13  | m  | 16  |   |
| •  | • •   |  |   | 66   | 203   |   |
|  |   |  | · ·   | 1,386  | 4,257.)   | 2   |
| •  | i.  |  |   | -  |   |   |
| و  | 5   | 20   | 162   | 54   | 216   |   |
| 29   | Ч   | 42   | 754   | 338  | 1 092   |   |
| 16<br>74   | ° =   | 24<br>75   | 520   | 160<br>794   | 480   |   |
|  |   | 0 5 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7  | 2 4 6 6 6<br>2 4 4 6 7<br>1 1 8<br>2 1 2<br>1 1 8<br>2 1 2<br>1 1 8<br>2 1 2<br>2 1 2 1  | 6<br>6<br>29<br>13<br>24<br>11<br>35<br>1<br>24<br>11<br>35<br>1   | 157<br>6 2 8 162<br>1, 29<br>16 13<br>29 13<br>24 754<br>1, 296<br>1, 296 | 157       157       66       4,         6       2       8       162       54       1,         29       13       42       754       538       1,         26       13       42       754       538       1,         29       13       42       754       538       1,         24       11       35       1,296       594       1, |

Remarks S 2,703 536 852 209 4,300 )) 42,800 ))) 13,300 )) 6,500 2,167 326 133 Total 1.55 46 675 586 629 124 217 104 CONSTRUCTION COST ESTIMATION FOR CAPAYAS SYSTEM Amount (7'000) 131 195 293 101 104 2,188 287 352 352 87 87 41 4,600 854 757 135 328 80 49 1,300 14,200 117 27 11 L/C 92 33 35 35 35 35 35 29 55 106 45 205 ( 4,312 1,946 401 524 129 (( 3,000 641 7 277 89 150 106 (1,313 (( 8,700 (((28,500 F/C 42 31 2,098 15,456 1,088 515 2,098 15,456 1,088 135 10 10 463 515 3,906 4,340 Total 3,917 776 1,236 ъ 144 163 781 868 1,174 4,337 457 163 1,174 437 1,097 195 476 δ S S S L/C Unit Rate 22 924 11,119 651 96 29 22 924 11,119 651 352 319 352 3,125 3,125 2,820 581 760 F/C 5,000 5,000 58,500 700 300 Quantity 300 300 200 300 690 690 100 22,100 TABLE J2-11(3). ц 4 134 Ton sq.m ш.н си.н Unit set. ha ha Description of Item Structural concrete Reinforced Bar Grouted Riprap RC-pipe ø600mm Miscellaneous 5% Sub Total Structural concrete Miscellaneous (5%) Deep plawing Ridge preparation Miscellaneous 5% Drainage Canal Earth Excavation Backfill Reinforced Bar Grouted Riprap Grand Total Sodding RC-pipe \$450 " \$600 Gate 0.5x1.0 0.7x1.0 Land Leveling Gravel Paving Sub Total 3. Land Leveling Total Backfill Tota1 Ð ł

|                                  |        |                |        |            |             |          | · · · ·                |              |                 |     |
|----------------------------------|--------|----------------|--------|------------|-------------|----------|------------------------|--------------|-----------------|-----|
| Descrintion of Item              | lhit   | Ouantitv       | Unit   | t Rate     |             | Amount   | unt () 1000)           |              | Remarks         |     |
|                                  | 2      | (              | F/C    | L/C        | Total       | F/C      | L/C                    | Total        | CV TOTICA       |     |
|                                  |        |                |        |            |             |          |                        |              |                 | 1.  |
| 1. Dam Works                     |        |                |        | •          |             | c        |                        |              | ר<br>פ<br>ר     | Ļ   |
| (1) jemporary works<br>Sub Total |        |                |        |            |             | ( 10,600 | 4,400                  | 15,060 )     | ( + + + + ) XU. | 4   |
| (2) Dom Mowles                   |        |                |        |            |             | •        | •                      | •<br>•<br>•  |                 | ۰.  |
| Celetan Voice                    | E<br>E | 72 000         | 22     | σ          | 12          | 1 5,84   | 64.8                   | ,<br>1<br>1  | • •             | •   |
| Earth Excavation                 | = ;;;  | 19,000         | 25     | n OI       | 20 F        | 475      | 190                    | 5, 10<br>665 |                 |     |
| Soft Rock Excavation             | 11     | 12,000         | 4S     | 18         | 63          | 540      | 216                    | 756          |                 |     |
| Core Embankment                  | F      | 274,000        | 42     | 17         | 59          |          | <u>ہ</u>               | 6,16         |                 |     |
| Filter Embankment                | τ.     | 98,000         | 82     | 33         | 115         | . n      |                        | 1,27         |                 |     |
| Up Stream Shell Embankment       |        | 432,000        | 38     | 15         | 53          |          | - T                    | 22,896       | •               |     |
| Down Stream Shell from           | Ŧ      | 219,000        | 38     | 15         | 53          | 8,32     | . <sup>с</sup> ,       | 1,60         |                 |     |
| Dam Borrow site                  |        | •              |        |            |             | •        |                        | •            |                 |     |
| Down Stream Shell by             | :      | 56,000         | 11     | 4          | 15          | 616      | 224                    | 840          |                 |     |
| Excavated Material               | •      | •              |        |            |             |          |                        |              |                 |     |
| Riprap Embankment                | , E    | 40,000         | 108    | 44         | 152         | 4,320    | 1,760                  | 6,080        |                 | •   |
| Toe Rock Embankment              | F      | 2,000          | 29     | 12         | 41          | 232      | 96                     | 328 (        |                 |     |
| Sodding                          | sq.m   | 33,000         | ю      | ŝ          | 10          | 165      | 165                    | 330          |                 |     |
| Miscellaneous 10%                | I      | •              |        |            |             | ி        | 2,096                  | •            |                 |     |
| Sub Total                        |        |                |        |            |             | 4        | 02                     | 80,483)      |                 |     |
| (3) Spillway                     |        | ی<br>۹۰ م<br>۹ |        |            |             | 1.<br>1. |                        | ہ<br>جی ا    |                 |     |
| Earth Excavation                 | cu.m   | 56,000         | 40     | . 16       | 56          | 24       | 896                    | •            | •               | . * |
| Soft Rock Excavation             |        | 24,000         | 64     | 25         | 89          | 5.5      | 600                    | 2,136        |                 | •   |
| Backfill                         | ÷      | 2,000          | . 22   | ġ.         | 31          | 44       | 18                     |              |                 |     |
| Structural Concrete, Class A     | ÷      | 1,800          | 731    | 629        | -           | 1,316    | 1,132                  | 2,448        | -               |     |
| Reinforced Bar                   | Ton    | 117            | 11,119 | 4,337      | 15,456      | 1,301    | 507                    | 1,808        | ·<br>· ·        | *   |
| bridge                           | SQ.B   | 06             | ۰,     | 400        |             | 144      | 36                     | 180          | •               |     |
| Miscellaneous 10%                | L.S    |                |        |            | - ".<br>- " | 30       |                        |              |                 |     |
| Sub Total                        |        | •              |        |            | •           | (7,239   | 3,508                  | 10,747)      | 2               |     |
| (4) Intake                       |        |                |        |            |             |          |                        |              |                 |     |
| Earth Excavation                 | cu.m   | 16,000         | 25     | 10         | 35          | 400      | 160                    | 560          |                 | . • |
| Soft Rock Excavation             | •      | 11,000         | 45     | 8          | 63          | 495      | 198                    | 693          |                 | •   |
| Backfill                         | , I 1  | 1,000          | . 22   | <u></u> б. | 31          | 22       | თ                      | 31           |                 |     |
| Tunnel Excavation                | :      | 2,500          | 436    | 221        |             | 060°T    | 55<br>2<br>2<br>2<br>3 | 1,643        |                 | •   |
| Tunnel Support                   | set    | 267            | 3,694  | 1,358      |             | 986      | 363                    | •            |                 | •   |
| Structural Concrete Class A      | cu.m.  | 160            | 735    | 677        | •           | 118      | 108                    | 226          |                 |     |
| Tunnel concrete                  |        | 850            |        | 776        | r~1         | 687      | 660                    | 1,337        |                 |     |
| Reinforced Bar                   | Ton    | . 66           | 11,119 | 4,337      | •           | 734      | 286                    | 62           |                 | •   |

TABLE J2-12(1) CONSTRUCTION COST ESTIMATION FOR BAYONGAN SYSTEM

TABLE J2-12(2) CONSTRUCTION COST ESTIMATION FOR BAYONGAN SYSTEM

(4+5+6)x0.02 Remarks ŀĄ 114,900 )) 8,610.) 1,437 ) 1,749. 36,731 39 167 28 183 391 12,138 7,228 3,144 S 540 I,479 Total 276 840 180 232 1,695 484 16,77 Amount (P'000) L/C 2,780 253 33,800 100 534 470 90 72 747 296 19 3,757 92 5 6,854 48 131 156 606 12,724 121 2,237 1,048 'n 67 81 100 179 400 179 530 ( 903 ( 5,830 184 370 370 584 584 160 160 363 4,991 2,096 (( 81,100 57 8,381 9,925 .,183 .,614 ,143 F/C 24,007 50,980 91,240 27,917 10,000 68 1.955 1,410 2,098 15,456 1,088 135 463 15,653 1,600 2 4 0 2 4 0 Total 3242 54 783 1,960 1,960 2,085 2,000 3,145 320 576 1,174 4,337 144 0 M 00 39 437 r/c Unit Rate 1,172 49,020 89,280 25,852 8,000 12,503 1,280 11,119 16 29 16 ы N 96 319 651 F/C 11 300 4,000 18,000 500 Quantity 60,500 172,100 131,000 9,500 289,000 11,500 500 430 85 ŝ 2 15 924 11,900 403 Holes cu. n sq.m u.n sq.m set set r.S ۳. ۳. ۲. ສ. ກິ Unit L.S Ton set set ÷ Ξ = ÷ Stripping Earth Excavatíon Fill by Excavated Material Fill by Excavated Material Tunnel Grouting Clossure Gate 2.8x2.2m Intake Gate 0.9x0.9m Outlet Plag by Stop Log Description of Item Structural Concrete Reinforced Bar Grouted Riprap Tunnel Grout Hole Miscellaneous 10% Sub Total Miscellaneous 5% Earth Excavation 1.5x1.5 Lining Concrete Sodding R.C. Pipe Ø250 Canal Works
 Temporary works Control House Gravel Paving Lateral Canal Sub Total Distributor (2) Main Canal Stripping Backfill Total Bridge Gate છ

TABLE J2-12(3) CONSTRUCTION COST ESTIMATION FOR BAYONGAN SYSTEM

Remarks (((,,005,921))) 18,100 )) 66,400 )) 11, 398 2, 258 3, 597 847 5,337 1,091 762 258 778 16 L, 220 464 476 247 2,727 Total 979 602 47 3,645 Amount (P\*000) 62,900 187 5,400 1,526 152 393 1,053 610 306 2,428 23,700 382 8,014 1,526 152 3,192 567 1,385 1,385 ъ В 49 241 82 1.16 C L 8,206, 1,691 2,212 2,212 ((( 136,600 1,201 389 586 2,592 610 415 537 456 139 (.( 42,700 (( 12,700 317 381 198 709 1,201 389 176 (2,909 (14,881 Ц F/C 3,917 776 1,226 31 2,098 15,456 1,088 1,088 2,098 15,456 1,088 515 Total 10 463 515 5,906 4,340 31 31 1,174 4,337 437 39 144 163 781 868 1,174 4,337 437 163 1,097 195 476 9 13 r/C Unit Rate 29 22 924 11,119 651 352 22 924 11,119 651 96 2,820 581 760 319 352 3,125 3,472 F/C Quantity 27,000 122,000 1,300 1,300 122 122 18,500 500 1,300 35 700 500 2,910 2,910 1,500 1,300 35 Unit cu.m cu.m sq.m m.uo cu.m Ton Ton set E : = = E ца г : Description of Item Structural Concrete Reinforced Bar Structural Concrete Miscellaneous 5% Ridge Preparation Miscellaneous 5% Miscellaneous 5% (4) Drainage Canal Earth Excavation Grouted Riprap R.C. Pipe \$600 R.C. Pipe \$450 ø600 Reinforced Bar Grouted Riprap Grand Total Land Leveling Deep Plawing Gravel Paving Gate 0.5x1.0 " 0.7x1.0 Land Leveling Sub Total Sub Total Backfill Total Sodding Backfill Total F ы.