

3-2-5 Boundary and Initial Value Conditions

According to the previously mentioned facts, the model was assumed as a part of a symmetrical cylinder structure 6 km in diameter, with the Balatoc plug as its center and with no heat or flow transfer from the lateral wall.

Outside of the central area where the mining activities are seen, a recharge of 2.26 mm/day is given. From this amount and within the mining zone, 1.9 mm/day are seeping into the tunnel and remaining 1.9 mm/day are discharging into the neighboring river. As to mine drainage, underground water, including hot water coming from the bottom of the model, amounts to about 13.53 kg/s and 2.72 MW of mass and heat flow respectively. This volume is applicable only to the fan-shaped sector of 15° angle of the cylindrical model, while these values serve as important checkpoints for the calibration of the simulator.

The boundary bottom plane is located at 1500 m.b.s.l., and as mentioned in sect.3.1.5, it is assumed supply 1.05 kg/s at 273°C with a heat flow of 1.375MW in addition to an average 2 HFU of heat flow of the earth's crust. At the beginning of the simulation, a certain supply of recharge was given to a thin weathered zone on the surface, but later on to increase the speed of calculation, this zone was eliminated and recharge was given to the top block of the model.

Atmosphere temperature was fixed at 20°C, and to further simplify the model, the mining area was not considered as part of the model since its permeability must be very large.

On the other hand, this program solves transient initial value problems with appropriate boundary conditions, in our case, a rather stationary condition, an initial value must first be generated. Temperature and pressure distribution are first estimated from existing data on the surface and on the borehole AC-1D. Initial values for temperature distribution used in

simulation are shown in Fig. III-3-6. If estimated values differ from true values, then simulation will consume a long time to reach that value. As to the initial values of pressures, used was natural water pressure according to elevation of the point.

A time step is required for simulation of the system in the transient state, time that is related to the size of the elements and to permeability etc. In the present simulation, and judging from the results of several trials, time steps increasing in geometric progression from 20 days to 1000 years, ended the calculations at the stationary state after more than 10,000 years. The variation of mass and heat flow in the Acupan Mine are given in Fig. III-3-7.

Table III-3-1 Primary physical value of rocks

		Weathered rocks	Basement rocks	Intrusive rocks
Density	kg/m ³	2000.	2700.	2700.
Porosity		.3	.001	.002
Permeability	kx, m ²	1. E-12	7. E-16	7. E-16
"	kz, m ²	1. E-12	7. E-16	4. E-16
Thermal conductivity	W/m°C	2.1	2.7	2.7
Specific heat	J/kg°C	600.	910.	910.

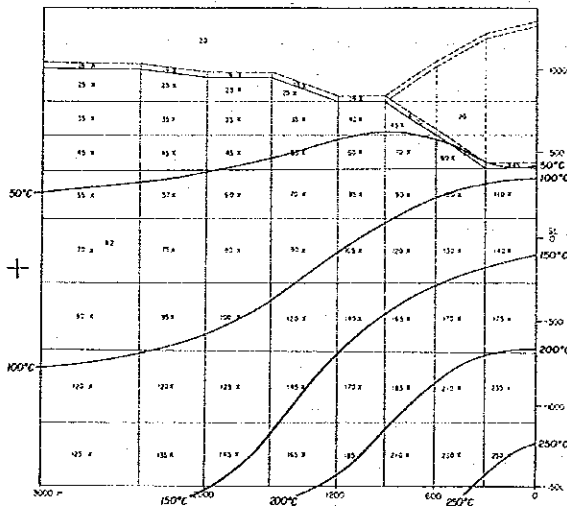


Fig. III-3-6 Estimated primary temperature distribution in °C

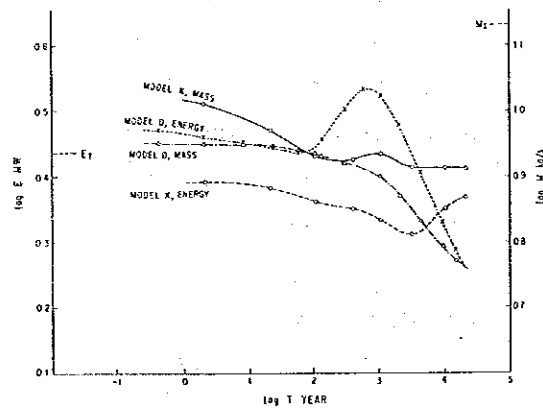


Fig. III-3-7 Variation of mass and heat flow into the Acupan mine in function of time

3-3 Discussion on Results of Simulation

3-3-1 Output

For every cycle of the simulation at the prescribed time step, there is a short printout of the steam condition, rate of the fluid flow across the interface of the elements, total energy change in the elements and so on.

Fig. III-3-8 gives the results of the fluid state in each element after changing the model six times with a time step of 72 and after a calculation time of 14,967 years. This Figure displays calculated temperature T , pressure P , and vapor saturation S based on internal energy E and the fluid density D . Fig. III-3-9 indicates the mass and heat flow of the fluid across the interface. The first three lines, A6G2, A7H3 and A8P4 of this table, indicate values of the underground heat and fluid flow into the Acupan Mine, which are important check values for evaluating the results of simulation. A satisfactory simulation can be obtained by checking various output data and correcting them properly after every running of the model.

In the running of simulation, nine corrections to the model were given, and even after that, the results were not completely satisfactory. However, through all of these calculated results, a deep geothermal structure in the Acupan area can be estimated. Besides the given list of output other data, there are still a lot of other data such as change of convergence of simultaneous equations and change in fluid mass. Some of these are listed in the Appendices.

3-3-2 Considerations of Results

After three trials in calculation by changing the model, produced was a model D that was somewhat close to the lumped parameter model indicated in Fig. III-3-10. Here, on this model, permeability of the upper blocks were enlarged ($1.2 \times 10^{-14} \text{ m}^2$), while those of the lower blocks were rather small ($2.4 \times 10^{-15} \text{ m}^2$).

At the Balatoc plug, in the center of the area, there is vertical fracture with a vertical permeability twice as big as the horizontal fracture.

As previously mentioned, the model considered the recharge at 19°C in such a way as to provide a certain mass flow to the top blocks depending on their surface area. It was also mentioned that a heat flow of 2 HFU was given to the bottom of the model, and in addition, to heat flow of volcanic origin given under the plug.

Under these conditions, the expected values of water flow from the Acupan Mine tunnels are 13.53 Kg./s and 2.72 MW of mass and heat flow respectively. Fig. III-3-11 shows temperature distribution under stationary conditions. From here, it can be seen that a temperature gradient suddenly becoming steep near the Balatoc plug, the same gradient measured in the well AC-1D, reveals a value three times smaller than the calculated value. Fig. III-3-12 indicates a modeling distribution of geothermal fluid, with a total mass flow of 5.86 kg/s and a heat flow of 1.95 MW, both of which are less than the expected values.

For the above reasons it, was therefore necessary to correct distribution of the rocks, their parameters, and boundary condition at depths, in that way preventing seepage of recharge into the underground, increasing of the heat flow up through the plug, and decreasing of the area of upflowing deep hot water. All these steps contribute to making easier the lateral flow of the recharge. Based on those concepts, further repetition of the simulations gave the results indicated in Fig. III-3-13.

No significant differences in permeabilities are given between intrusive rocks and basement rocks. Also, the primary geothermal fluid given to the bottom is caused to decrease radially from the center.

Fig. III-3-14 shows the temperature distribution based on initial values adopted by the previous calculation, after nearly 20,000 years. Here the thermal gradient of deep zones is lower than that of model D, tending to be close to the observed value in AC-1D. On the other hand, the pressure distribution given in Fig. III-3-15 does not directly suggest the geothermal structure.

The distribution of geothermal heat and mass flow are indicated in Figs. III-3-16 and III-3-17 respectively, indicating that mass and heat flow in the Acupan Mine are 8.60 Kg/S and 2.30 MW respectively, and thus showing values closer to the observed values than in the case of model D. Should several more runnings of the simulation be conducted, results closer to the observed values could be obtained.

According to the results obtained from several simulations of the underground geothermal structure of the Acupan area, the following can be summarized:

1. Regardless of whether or not the basement rock is an intrusive rock, the permeability was small in the order of 10^{-15} to 10^{-16}m^2 in spite of the direction.
2. It is concluded that there is no eminent fracture upstream from the deep geothermal fluid. This is inferred from the fact that a strong sealing effect occurred when gold mineral bed formation was formed and volcanic activity was not so prominent to produce an active fault.
3. Upstream movement of the primary geothermal fluid may not be controlled by the Balatoc plug and the geological structure in the NE-SW direction.

It is considered that the flow rate of upstream movement of the geothermal fluid is nearly the same in this area, and within a radius of at least 3 kms it is assumed to be constant.

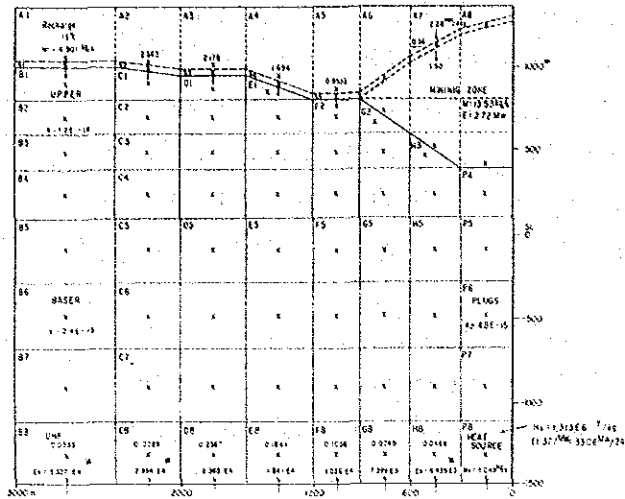


Fig. III-3-10 Simulation model D

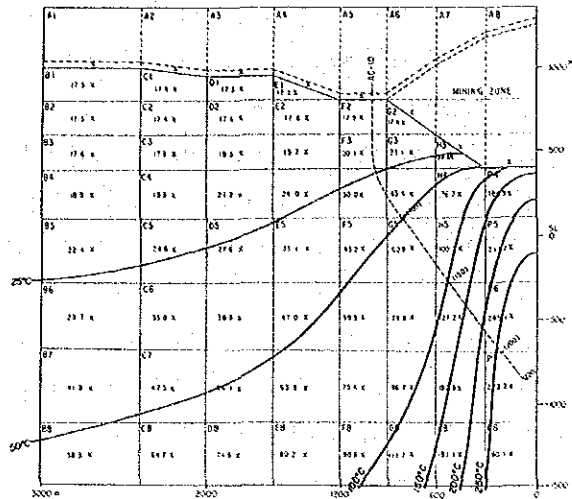


Fig. III-3-11 Temperature distribution for mode D in °C

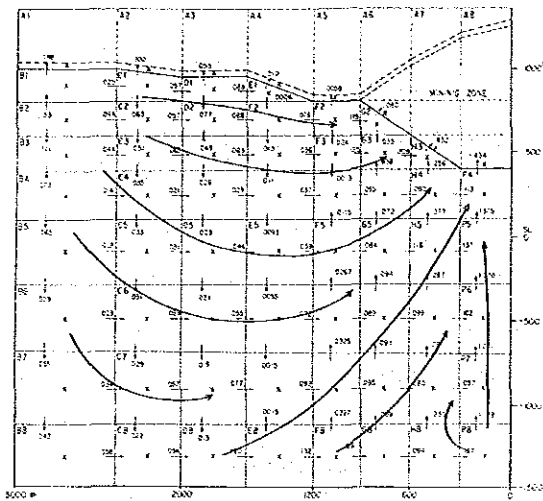


Fig. III-3-12 Heat flow distribution for model D in MW

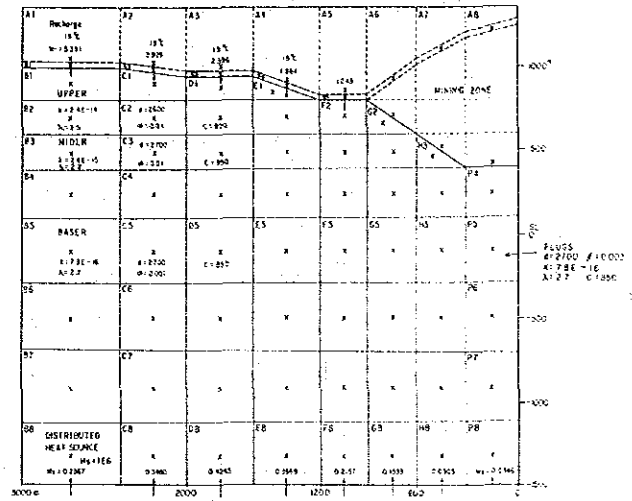


Fig. III-3-13 Simulation model K

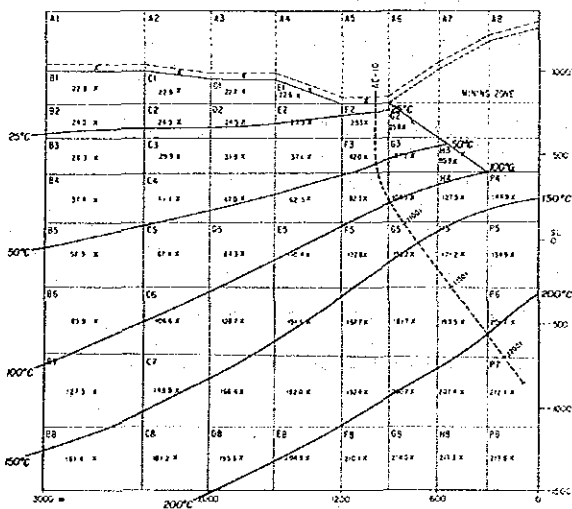


Fig. III-3-14 Temperature distribution (model K) in °C

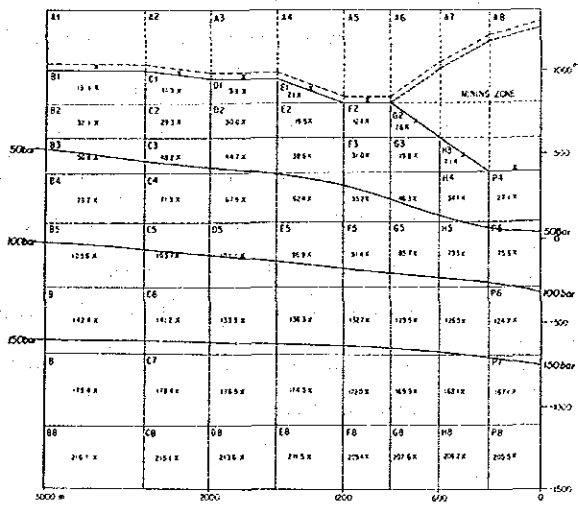


Fig. III-3-15 Pressure distribution (model K) in bar

4. Most of the geothermal heat flow of 33MW found in the Acupan Mine, caused by the hot spring and by drainage of the underground geothermal fluid, is deeply related to development of the Acupan Mine. Before development of the mine, manifestations must have been almost the same as hot springs around the Itogon area.

5. This stage, it is somewhat difficult to assure that there could have been developed high permeability fractures outside of the present simulated zone at depths lower than 1,500 m b.s.l.

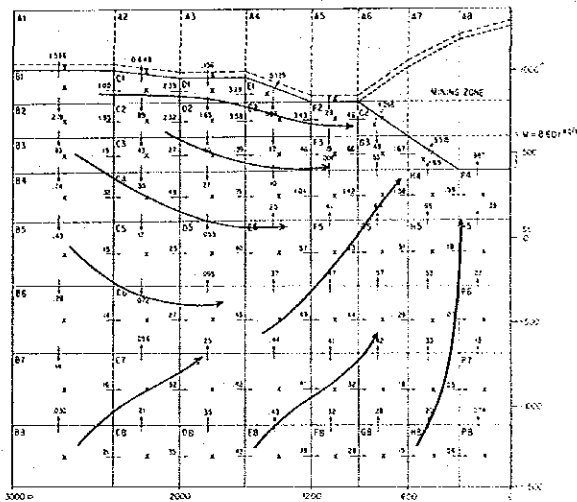


Fig. III-3-16 Heat flow distribution (model K) in MW

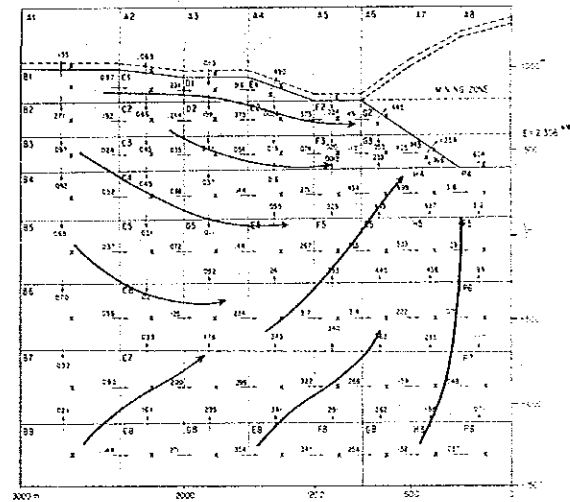


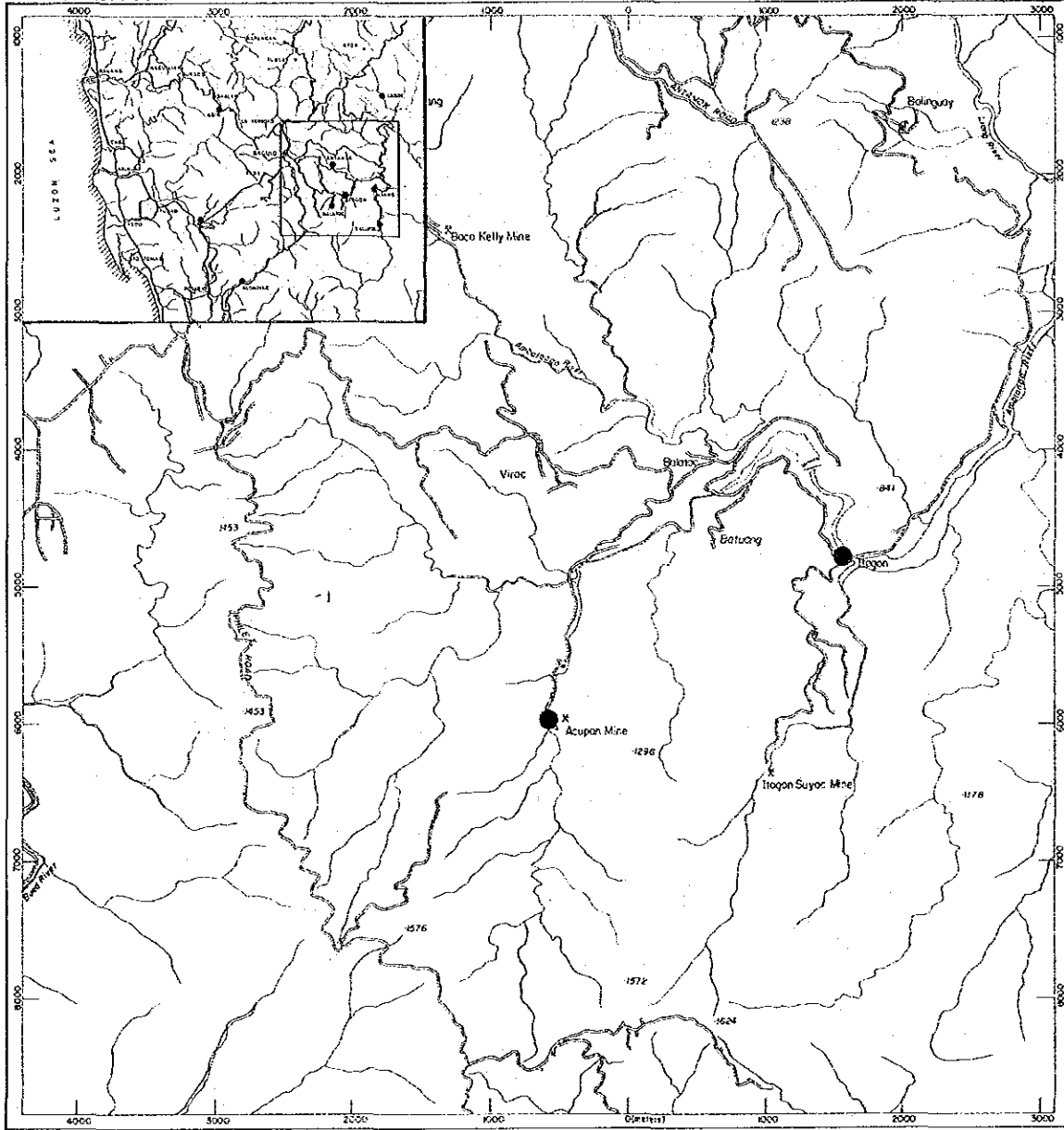
Fig. III-3-17 Mass flow distribution (model K) in kg/s

REFERENCES

1. Pinder G.F., 1979, "State-of-the Art Review of Geothermal Reservoir Modelling"; LBL Report LBL-9093, Lawrence Berkeley Lab., Berkeley, U.S.A.
2. Pruess, K. et al, 1979, "SHAFT 78, A Two Phase Multidimensional Computer Program for Geothermal Reservoir Simulation", LBL Report LBL-8264, Lawrence Berkeley, Lab., Berkeley U.S.A.
3. Pruess, K. et al, 1980, "SHAFT 79, User's Manual" LBL Report LBL-10861, Lawrence Berkeley, Lab., Berkeley U.S.A.

APPENDICES

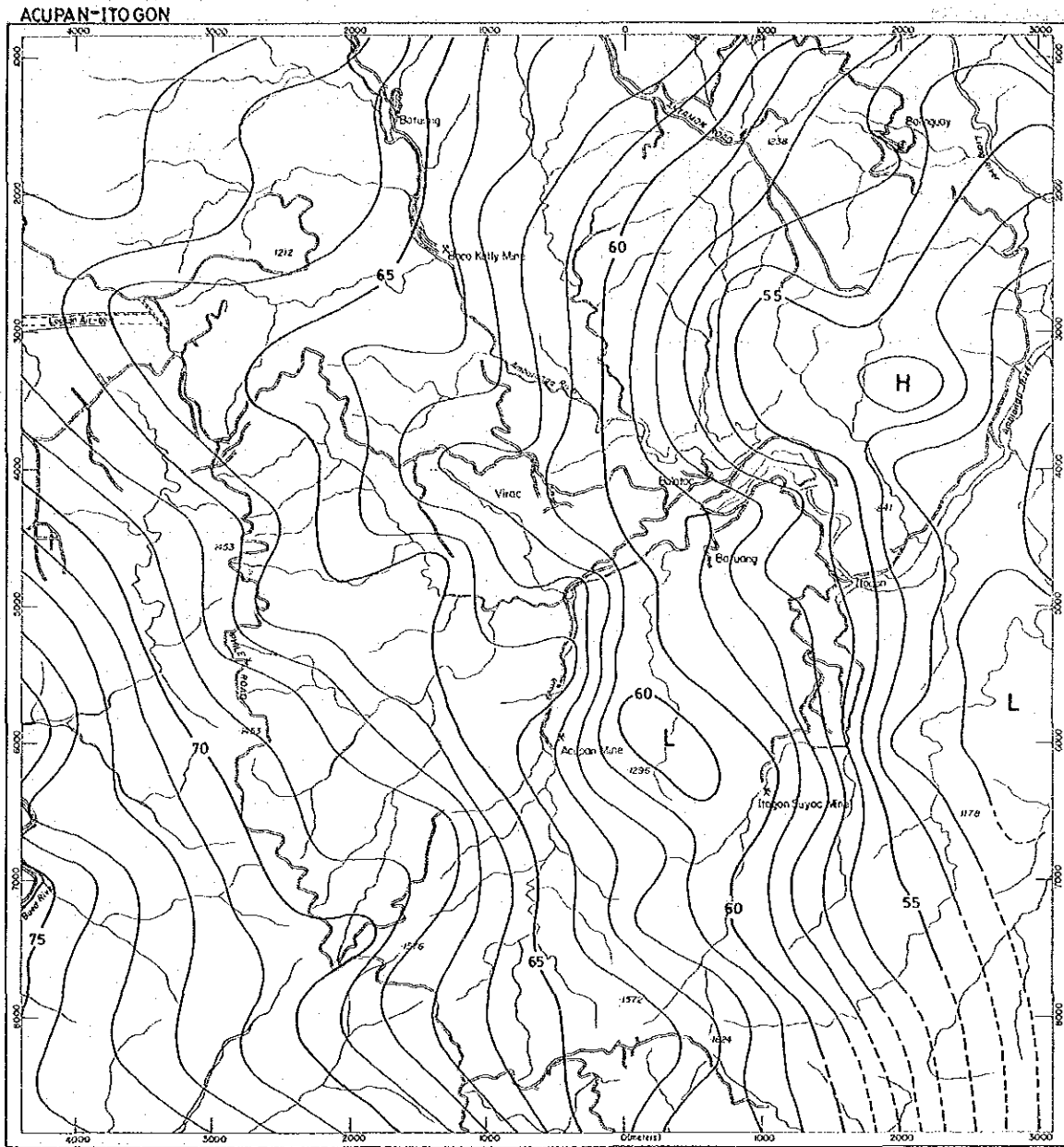
ACUPAN ITOGON



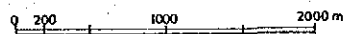
LEGEND

● sample location

App. 1 Location map of spring water samples

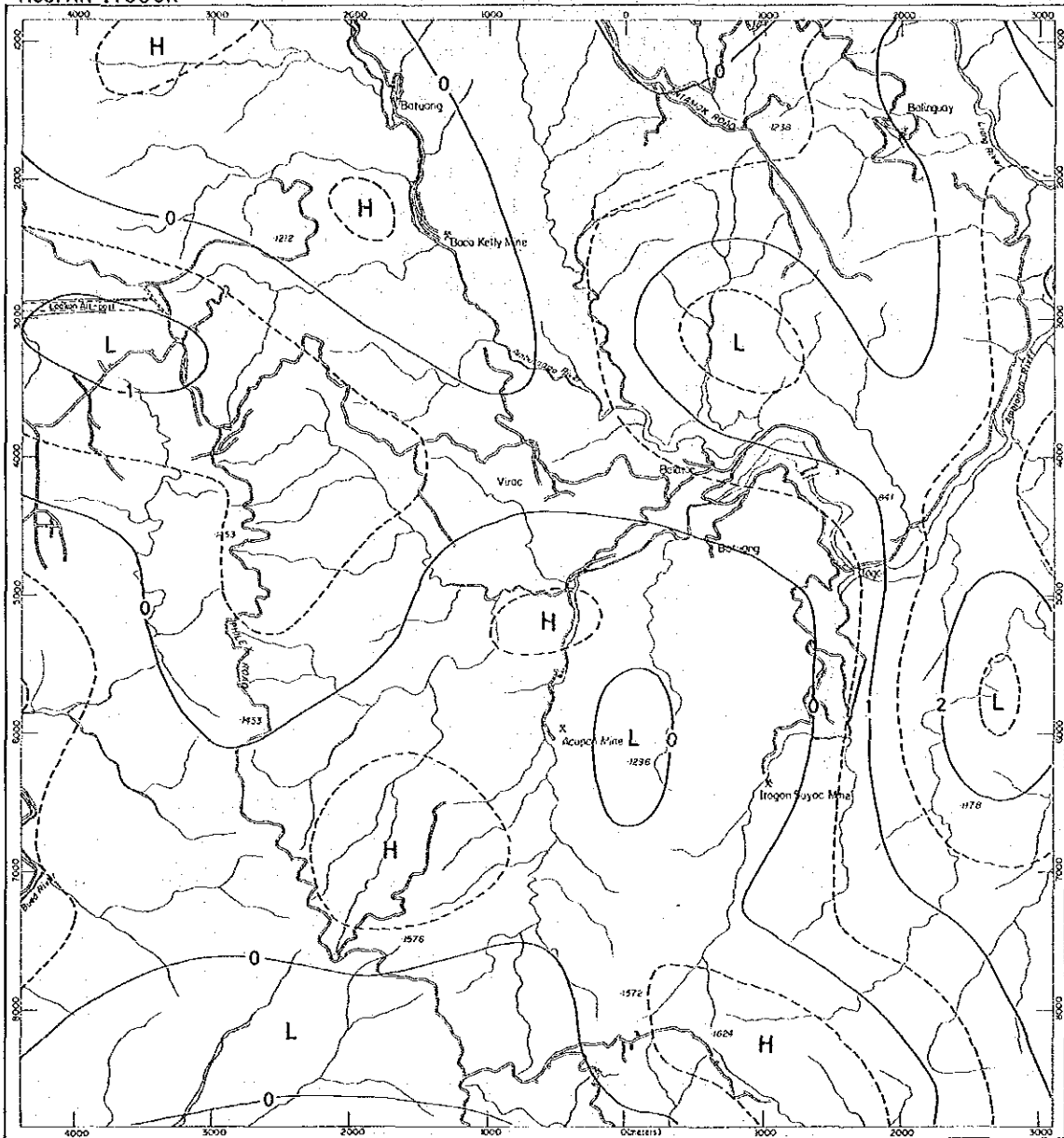


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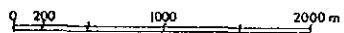


App. 2 Bouguer anomaly map ($\rho = 2.6$)

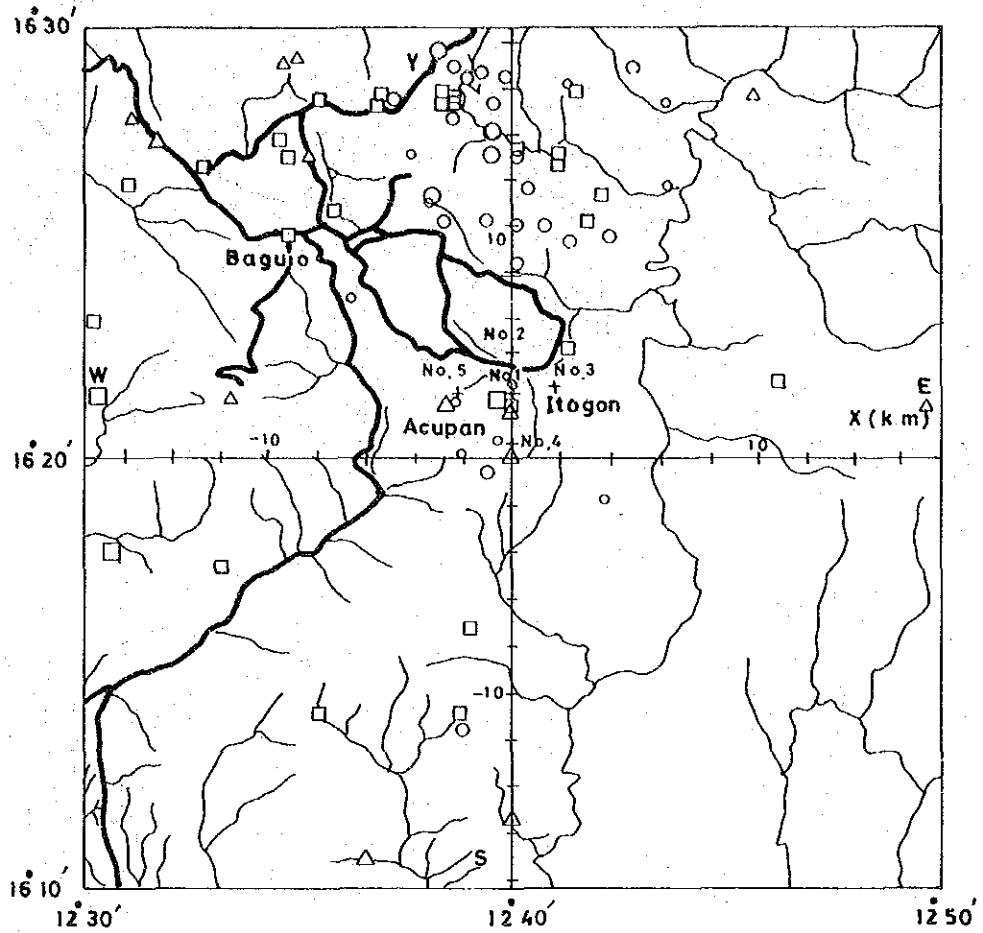
ACUPAN-ITOGON



unit : mgal



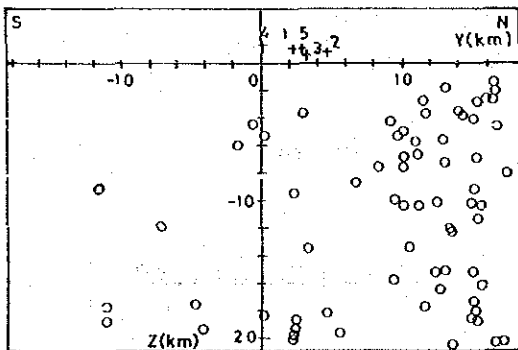
App. 3 Residual map ($\lambda = 0.25 \sim 2.1$)



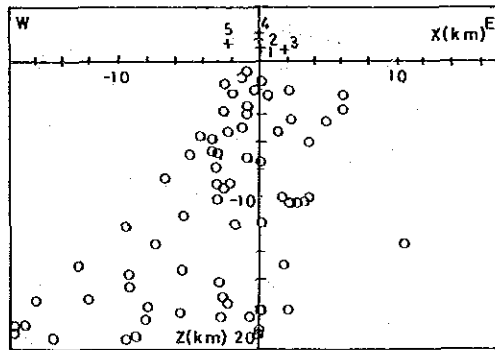
Seismograph

Depth (Z)	Magnitude (M)		
	$0 \leq M < 1$	$1 \leq M < 2$	$2 \leq M < 3$
$0 < Z \leq 10$	○	○	○
$10 < Z \leq 20$	□	□	□
$20 < Z$	△	△	△

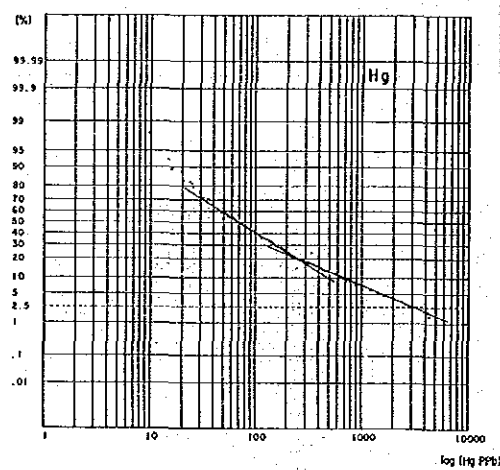
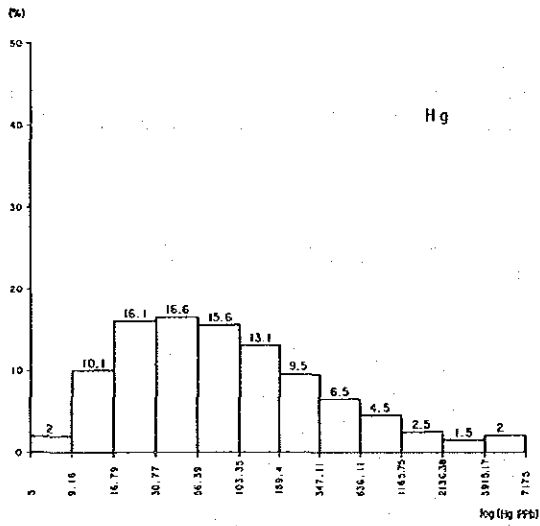
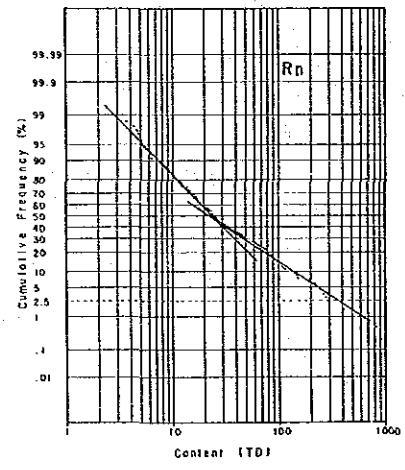
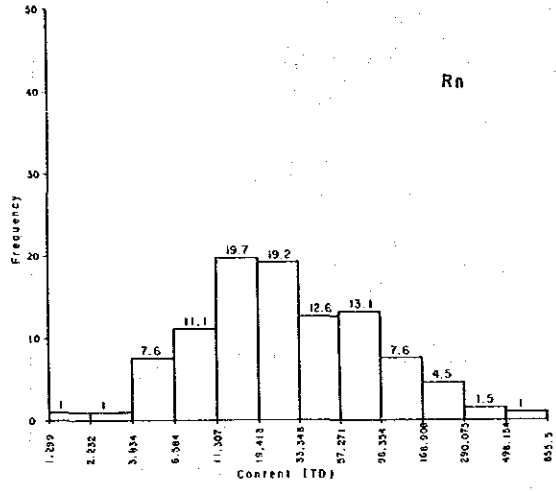
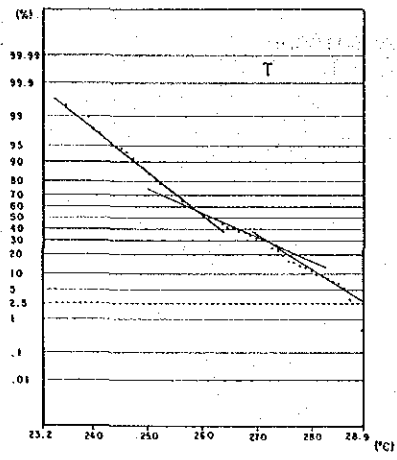
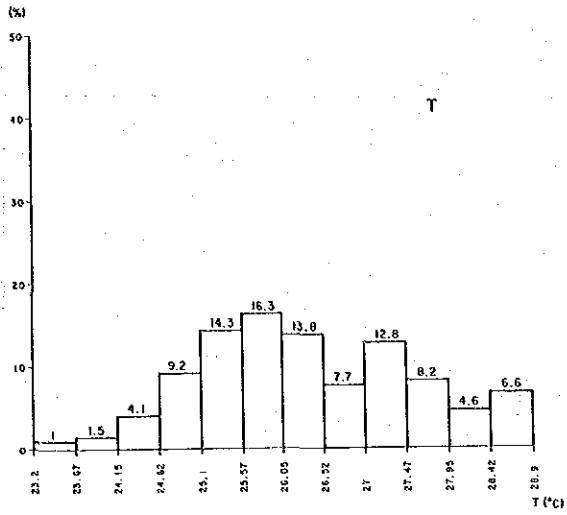
TOTAL



TOTAL

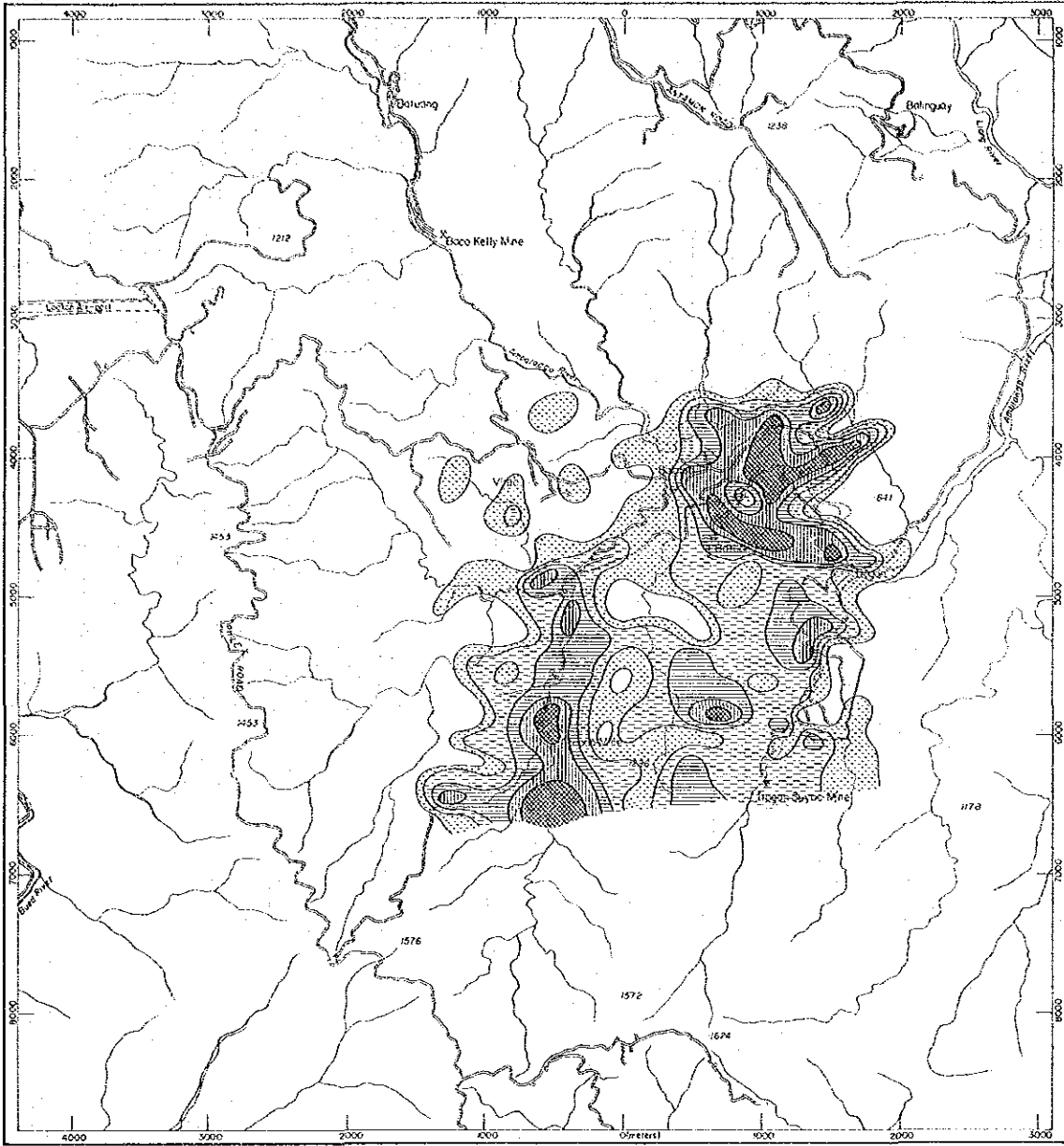


App. 4 Epicentral and hypocentral distribution map of micro earthquakes









App. 5 Histograms and cumulative probability charts for T (°C), Rn (T/30 days, mm²) and Hg (ppb) surveys

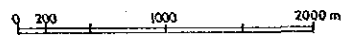
ACUPAN-ITOGON



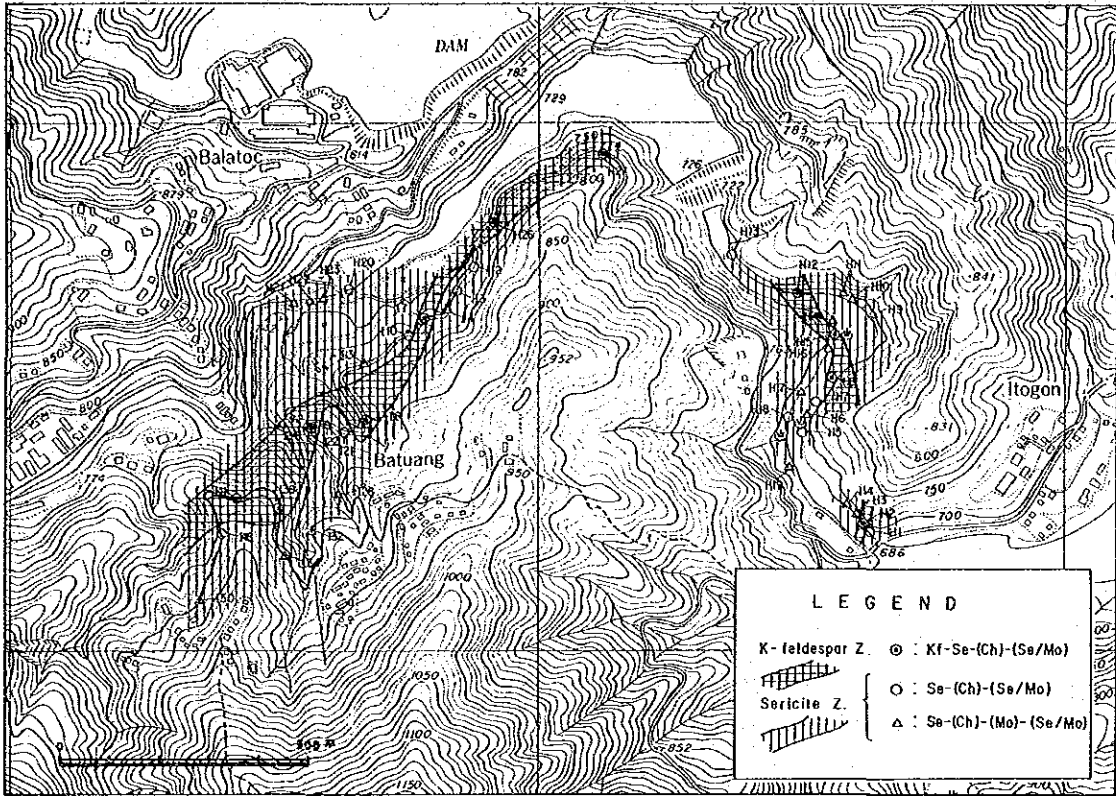
LEGEND

-  956 < Hg
-  478 ~ 955
-  239 ~ 477
-  119 ~ 238
-  59 ~ 118
-  58 > Hg

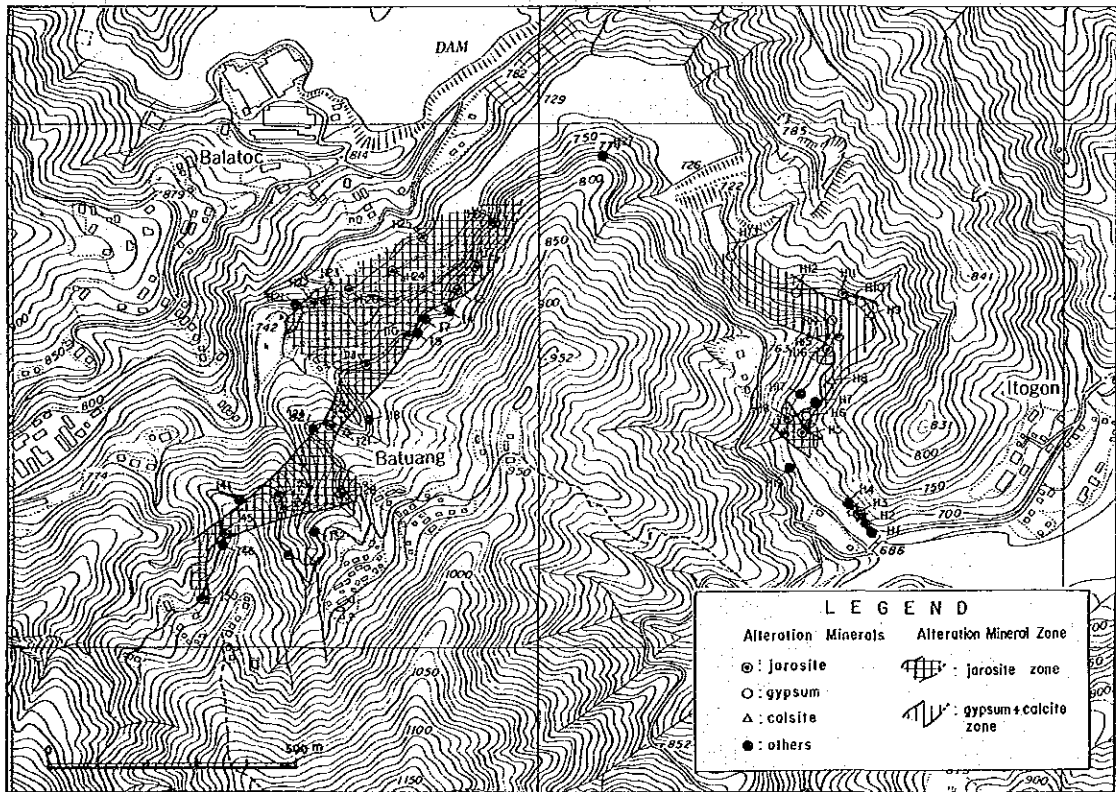
unit : ppb



App. 6 Soil Hg map



App. 10 Distribution of alteration minerals around Itogon plug (1)
(Neutral Hydrothermal Alteration Zone)



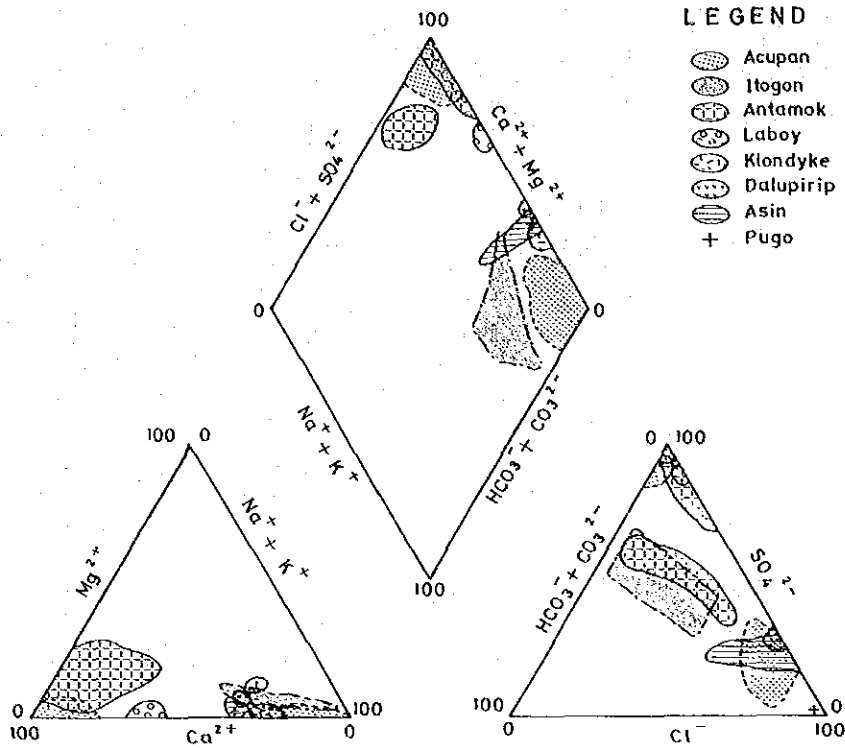
App. 10 Distribution of alteration minerals around Itogon plug (2)
(Jarosite Zone and Gypsum + Calcite Zone)

No.	23	24	25	26	27	28	29	30	31	32	33
Location	Batuang	Batuang	Antemok	Antemok	Acupan	Acupan	Acupan	Acupan	Acupan	Acupan	Acupan
Code	E24	E25	E26	Antamok	Benquet-1	Benquet-2	Benquet-3	Benquet-4	Benquet-5	Benquet-6	Benquet-7
Sampling Date	7, June, '82	7, June, '82	9, June, '82		19, Aug., '77	18, Aug., '77	19, Aug., '77	19, Aug., '77	18, Aug., '77	19, Aug., '77	19, Aug., '77
T (°C)	19.0	18.0	17.5	37.0	79.5	99		72.5	64.5	55	73
pH	5.51	5.30	6.79	3.35	7.84	8.36			8.12	8.05	7.80
Conductivity (µm/cm)	518	647	258	4,653							
Discharge (l/min)	1	0.5	20		40			30	2-3	20	60
Chem. Ana.	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l
Na ⁺	12.6	0.548	14.8	0.644	5.10	0.222	360	15.659	865	37.669	1,245
K ⁺	0.61	0.015	0.73	0.019	0.60	0.015	22.3	0.570	117	2.992	1.28
Ca ⁺⁺	40.0	1.996	49.6	2.475	32.0	1.597	580	18.042	121	6.038	195
Mg ⁺⁺	28.8	2.370	39.6	3.209	7.75	0.638	94.0	7.735	5.4	0.444	0.3
Cl ⁻	7.09	0.200	2.95	0.083	2.36	0.067	613	17.290	1,202	33.504	1,550
SO ₄ ²⁻	230	4.789	247	5.143	52	1.083	2,199	45.786	392	8.162	332
HCO ₃ ⁻	16.5	0.270	22.4	0.367	83.9	1.375			157	2.573	278
CO ₃ ²⁻							2	0.067	10	0.333	
H ₂ CO ₃							6	0.097	3	0.048	
Li					2.40			4.2		7.0	
As										5.9	
B					10.60	0.981	47	4.348	68	6.290	55
SiO ₂	34.1	0.565	39.0	0.649	21.8	0.363	47.6	0.792	177	2.946	295
NH ₄ ⁺										4.910	236
T.S.M (mg/l)	369.7	415.5	205.5		3,926.5		3,092.4		4,154.3		3,530.0
Alkalinity											
Acidity											
Remarks	cold spring	cold spring	stream water	hot spring	hot spring	hot spring	hot spring	hot spring	hot spring	hot spring	hot spring
Reference	B.E.D. (9/Aug/82)	do	do	do	KFTA (Sep/77)	do	do	do	do	do	do

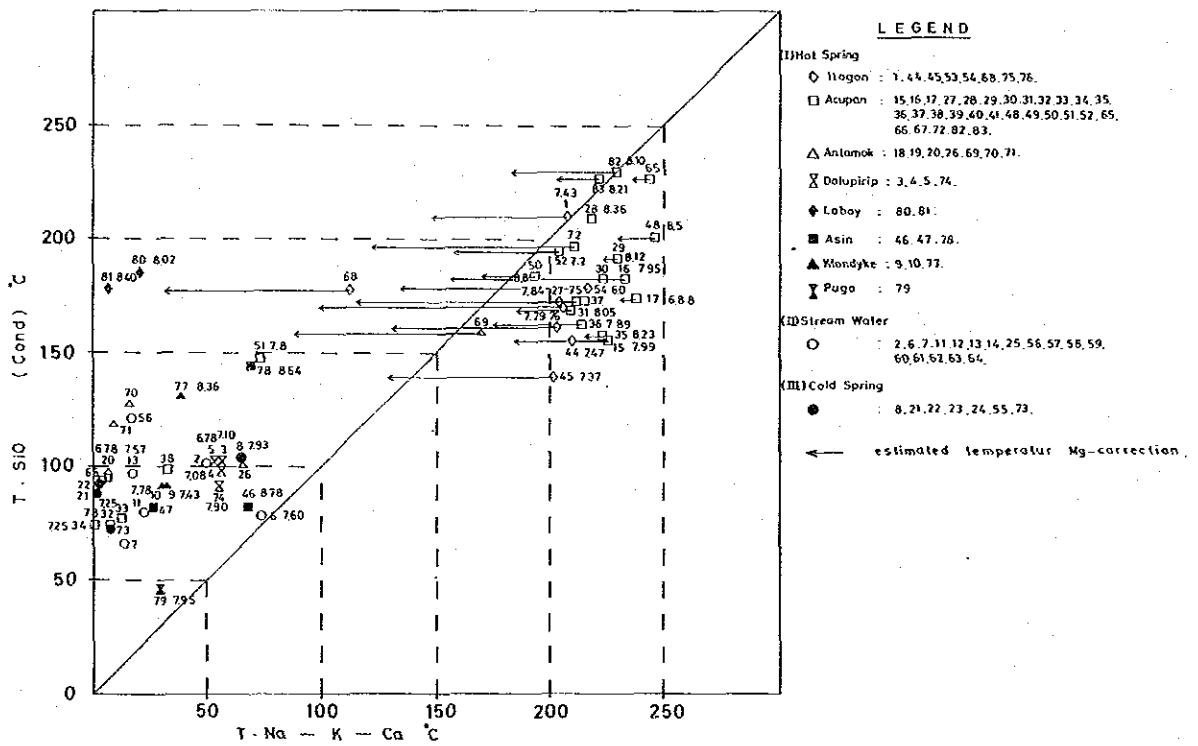
No.	34	35	36	37	38	39	40	41	42	43	44
Location	Acupan	Acupan	Acupan	Acupan	Acupan	Acupan	Acupan	Acupan	Acupan	Acupan	Itogon
Code	Benquet-8	Benquet-9	Benquet-10	Benquet-11	Benquet-12	Benquet-13	Benquet-14	Benquet-15	Benquet-16	Benquet-17	Benquet-18
Sampling Date	19, Aug., '77	20, Aug., '77	20, Aug., '77	20, Aug., '77	20, Aug., '77	20, Aug., '77	20, Aug., '77	20, Aug., '77	20, Aug., '77	20, Aug., '77	19, Aug., '77
T (°C)	57	65	52	97	63	51.5		65	24	43	84
pH	7.25	8.23	7.89		7.57	7.04		7.61	7.75		7.47
Conductivity (µm/cm)											
Discharge (l/min)	5	15	10	<1		8		50	200	20,000	5
Chem. Ana.	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l
Na ⁺	23	1,000	845	36,755	942	40,974	1,041	45,281	85	3,692	32
K ⁺	3.3	0.084	118	3.018	124	3,172	139	3,555	7.2	0.184	2.2
Ca ⁺⁺	425	21,208	50	2,495	98	4,890	119	5,938	312	15,569	505
Mg ⁺⁺	11.0	0.987	1.7	0.140	7.0	0.576	1.3	0.107	2.9	0.239	11.0
Cl ⁻	8	0.226	935	26,373	1,142	32,212	1,760	38,361	12	0.338	6
SO ₄ ²⁻	1,400	29,150	740	15,408	622	12,951	458	10,161	1,000	20,821	1,520
HCO ₃ ⁻	173	2,935	188	3,081	266	4,360		72	1,180	259	4,245
CO ₃ ²⁻	0	0.000	5	0.167	3	0.100		1	0.033	0	0.000
H ₂ CO ₃	21	0.339	3	0.048	8	0.129		4	0.064	58	0.935
Li	0.05		4.4		4.7		5.2		0.10		0.07
As									0.05		0.07
B	<0.05	0.005	31	2,865	45	4,163	55	5,085	0.05	0.005	<0.05
SiO ₂	26	0.433	140	2,330	153	2,546	177	2,946	46	0.766	36
NH ₄ ⁺											0.599
T.S.M (mg/l)	2,071.4	3,056.7	3,410.0		3,350.3		1,542.2		2,429.3		2,388.5
Alkalinity											
Acidity											
Remarks	hot spring	hot spring	hot spring	hot spring	hot spring	hot spring	hot spring	hot spring	hot spring	mine drainage	mine drainage
Reference	KFTA (Sep/77)	do	do	do	do	do	do	do	do	do	do

No.	45	46	47	48	49	50	51	52	53	54	55	
Location	Hogon	Adn	Adn	Acupan	Acupan	Acupan	Acupan	Acupan	Hogon	Hogon	Batang	
Code	Benquet-19	Benquet-20	Benquet-21	BE1-D-1	BE1-D-2	BE1-D-3	BE1-D-4	BE1-D-5	BE1-D-6	BE1-D-7	BE1-D-8	
Sampling Date	19, Aug, '77	21, Aug, '77	21, Aug, '77	25, Oct, '78	25, Oct, '78	25, Oct, '78	25, Oct, '78	25, Oct, '78	25, Oct, '78	25, Oct, '78	26, Oct, '78	
T (°C)	85	70	41	96	87	61	59	79	86	75	20	
pH	7.37	8.78	7.43	8.5	6.8	8.8	7.8	7.7	6.3	6.0	2.7	
Conductivity (µS/cm)				4,113		4,478	1,357	4,267	1,470	7,323	638	
Discharge (l/min)			2.5	60	<6	30	very low	40	70	10	30	
Chem. Ana.	mg/l	m.eq/l	mg/l	m.eq/l	mg/l	m.eq/l	mg/l	m.eq/l	mg/l	m.eq/l	mg/l	m.eq/l
Na ⁺	355	15.441	523	22.749	122	5.307	783	34.058				
K ⁺	56	1.432	11	0.281	1.7	0.043	125	3.197				
Ca ⁺⁺	152	7.585	232	11.078	64	3.194	17.2	0.609				
Mg ⁺⁺	16.0	1.317	N.D.	0.000	5.0	0.411	1.5	0.123				
Cl	233	6.572	635	23.552	200	5.641	984	37.755				
SO ₄ ²⁻	670	33.950	473	9.890	108	2.249	407	8.414				
HCO ₃	347	5.687	26	0.426	170	2.786	382	6.261				
CO ₃ ²⁻	0	0.000	2	0.067	0	0.000						
H ₂ CO ₃	34	0.548	0	0.000	21	0.339						
Li	1.8		0.2		0.1		3.36					
As							2.25					
B	9.5	0.879	9.5	0.879	3.3	0.305	38.9	1.599				
SiO ₂	103	1.714	32	0.533	32	0.533	767	4.444				
NH ₄ ⁺							0.05					
T.S.M (mg/l)	1,975.5		2,135.5		727.0		3,000.6					
Alkalinity												
Acidity												
Remarks	hot spring	hot spring	hot spring	hot spring	hot spring	hot spring	hot spring	hot spring	hot spring	hot spring	cold spring	
Reference	KRTA (Sep.77)	do	do	do	2,900L (Feb.79)	do	do	do	do	do	do	

No.	56	57	58	59	60	61	62	63	64	65	66	
Location	Batang	Batang	Virac	Virac	Virac	Balangay	Hogon	Hogon	Acupan	Acupan	Acupan	
Code	BE1-D-9	BE1-D-10	BE1-D-11	BE1-D-12	BE1-D-13	BE1-D-14	BE1-D-15	BE1-D-16	BE1-D-17	BE1-D-18	BE1-D-19	
Sampling Date	26, Oct, '78	26, Oct, '78	26, Oct, '78	26, Oct, '78	26, Oct, '78	30, Oct, '78	1, Nov, '78	1, Nov, '78	31, Oct, '78			
T (°C)	20	19.5	20	20	20	20	20	20	20	63.7	46.1	
pH	3.9	4.2	7.3	8.2	8.0	8.0	7.4	7.4	7.2			
Conductivity (µS/cm)	532	247	275	224	183	279	104	134	870			
Discharge (l/min)		6,000	600		6,000	6,000	300	400	400	500		
Chem. Ana.	mg/l	m.eq/l	mg/l	m.eq/l	mg/l	m.eq/l	mg/l	m.eq/l	mg/l	m.eq/l	mg/l	m.eq/l
Na ⁺	100	0.435	7.33	0.319	4.0	0.174	4.67	0.203	6.33	0.275	5.67	0.247
K ⁺	0.86	0.022	0.43	0.011	0.29	0.007	0.43	0.011	0.29	0.007	0.43	0.011
Ca ⁺⁺	12.7	0.634	13.0	0.649	42.6	2.126	30.4	1.517	20.0	0.998	47.8	2.385
Mg ⁺⁺	8.75	0.720	9.31	0.765	5.88	0.484	9.69	0.797	7.63	0.628	8.13	0.669
Cl	24.2	0.683	27.8	0.784	3.55	0.100	4.43	0.125	3.55	0.100	3.55	0.100
SO ₄ ²⁻	284	5.913	115	2.354	56.5	1.803	50.9	1.060	33.3	0.693	25.3	0.527
HCO ₃												
CO ₃ ²⁻												
H ₂ CO ₃												
Li												
As											6.75	<0.01
B											5.88	0.544
SiO ₂	74	1.237	59	0.582	24.2	0.403	27.4	0.456	42.1	0.701	49.6	0.826
NH ₄ ⁺	0.049		0.050		0.015		0.140		0.015			
T.S.M (mg/l)	414.5		231.7		238.7		208.7		190.3		285.5	
Alkalinity												
Acidity												
Remarks	stream water	stream water	stream water	stream water	stream water	stream water	stream water	stream water	stream water	stream water	hot spring	hot spring
Reference	BE1-D-10 (Feb.79)	do	do	do	do	do	do	do	do	do	Sarkina F.J. et al. (1979)	do



App. 14 Key diagram for spring water samples



App. 15 Correlation between T_{SiO} and $T_{Na-K-Ca}$

App. 16 List of O/H isotope analyses

Sample No.	Sample Location	Temperature (°C)	Discharge (ℓ/min)	PH	δ D (0/00)	δ ¹⁸ O (0/00)	Remarks
1	AGH-I Drill Hole	66.2	2	7.0	-58.9	-8.6	Nov., '83
2	Ambalanga River	73.8	3	7.0	-59.6	-9.3	"
3	Acupan Mine 2900L	35.9	100	7.0	-66.7	-10.6	"
4	Acupan Mine 2900L	43.5	50	7.0	-70.8	-10.8	"
5	Acupan Mine 2900L	41.7	150 ~ 100	7.0	-70.2	-10.9	"
6	Acupan Mine 2900L	65.0	5	7.5	-57.8	-8.1	"
7	Acupan Mine 2900L	90.0	10	7.5	-56.5	-8.9	"
8	Acupan Mine 2900L	65.0	2	7.0	-55.5	-8.7	"
9	Acupan Mine 3150L	75.0	70	7.5	-55.2	-8.4	"
10	Acupan Mine 3150L	80.0	60 ~ 50	7.5	-64.7	-10.1	"
11	Acupan Mine 3150L	80.0	60 ~ 50	7.0	-68.0	-10.7	"
12	Acupan Mine 3300L	57.1	25	7.0	-57.0	-7.8	"
13	Acupan Mine 3300L	85.8	30 ~ 25	7.5	-59.6	-7.6	"
14	Acupan Mine 2300L	32.8	100 ~ 50	7.0	-68.7	-10.3	"
15	Acupan Mine Drainage Tunnel	73.1	5	7.5	-68.0	-9.5	Sep., '82
IT-1	Itogon Hot Spring	89.5	Total 10	7.7	-67.2	-9.8	"
IT-2	Itogon Hot Spring	62.2		7.8	-67.6	-9.6	"
BA-1	Acupan Mine 3300L	81.0	25	8.1	-62.3	-7.7	"
BA-2	Acupan Mine 3150L	62.1	60 ~ 80	8.2	62.5	-7.6	"
DA-ST	East of Dalupirip stream				-71.0	-10.1	"
PRE	Precipitate at Baguio city				-66.9	-9.9	"
Errors					± 2	± 0.1	"

App. 17 Chemical analyses of water samples on Phase II survey

Sample No.	Sample Location	Temp. (°C)	pH	Na (ppm)	K (ppm)	Ca (ppm)	Mg (ppm)	Li (ppm)	B (ppm)	SiO ₂ (ppm)	SO ₄ ²⁻ (ppm)	HCO ₃ ⁻ (ppm)	Cl ⁻ (ppm)
1	AGH-I, drill hole	66.2	7.53	670	80.0	270	28.0	3.15	31.2	135	554	693	794
2	Ambalanga stream water	73.8	6.66	275	46.5	203	18.0	1.05	2.16	119	1,156	193	85.1
3	Acupan mine 2,900 L	35.9	7.18	15.0	3.5	640	15.0	ND	ND	29.8	1,179	153	7.09
4	" 2,900 L	43.5	7.44	39.0	3.3	680	9.0	ND	ND	32.5	1,630	91.5	7.09
5	" 2,900 L	41.4	7.45	37.5	3.6	650	10.0	ND	ND	32.2	1,584	110	7.09
6	" 2,900 L	65.0	8.23	620	90.0	92.5	7.0	3.05	26.4	214	594	400	581
7	" 2,900 L	70.0	8.09	370	56.0	155	7.0	1.75	13.4	128	881	125	411
8	" 2,900 L	65.0	7.06	220	37.0	430	63.0	1.00	9.41	70.8	1,357	79.3	227
9	" 3,150 L	75.0	8.60	890	120	150	14.0	4.40	43.1	302	385	384	1,191
10	" 3,150 L	85.0	7.35	34.0	3.8	590	5.0	ND	ND	39.7	1,358	81.1	7.09
11	" 3,150 L	80.0	7.87	39.0	6.0	600	14.0	ND	ND	47.2	1,205	67.1	10.6
12	" 3,300 L	57.1	7.59	720	100	260	18.0	3.45	34.6	207	847	270	936
13	" 3,300 L	85.8	8.23	870	115	47.5	6.0	3.50	44.8	280	356	144	1,163
14	" 2,300 L	35.0	7.40	21.5	6.0	430	100	ND	ND	38.0	1,293	58.0	7.09
15	" 2,300 L drainage	73.0	7.85	300	39.5	95.0	10.0	1.00	5.41	153	496	384	70.9

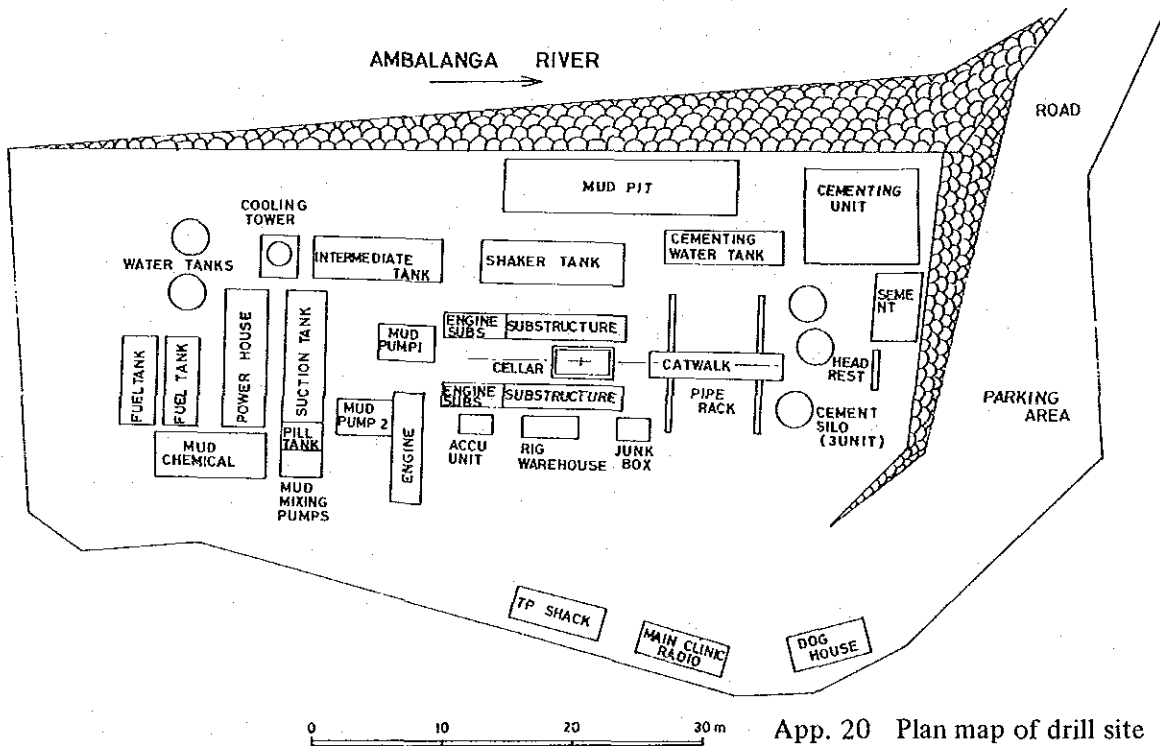
App. 18 List of main machineries

Article	Description	Maker	Quantity	Remarks
Drawworks	NATIONAL 610	NATIONAL	1 set	Hoist load capacity 10 line 180 ton
Engine	D 379	CATERPILLA	2 sets	Diesel engine 500HP/1200rpm
Rotary table	C 275	NATIONAL	1 set	Table opening 27 1/2"
Substructure	Two Section Box on Box	DERRICK SERVICES	1 set	Box:6'Wx9'Hx33'L Casing 180 ton
Derrick	Cantilever type	"	1 set	Height 40m Set back 110Ton
Mud pump No.1	7P-50 Triplex pump	NATIONAL	1 set	Volume 1,900ℓ/min (120kg/cm ³)
Engine	D 379	CATAPILLAR	(1) set	Use one of drawwork's engine
Mud pump No.2	8P-80 Triplex pump	NATIONAL	1 set	Volume 2,300ℓ/min (160kg/cm ³)
Engine	D 398	CATAPILLAR	1 set	Diesel engine 825HP
Mixing pump	5x6R Centrifugal pump	TRW	2 sets	
Engine	motor		2 sets	37KW/set
Mud agitator	34" Impeller	BRANDT	5 units	with 5.5KW motor
Shale shaker	Dust unit	BRANDT	1 unit	with 2.2KW motor (2 sets) Capacity 5,300ℓ/min
Desander	10" x double	SWACO	1 unit	Flow rate 3,780ℓ/min
Desilter	8T4	SWACO	1 unit	Flow rate 4,500ℓ/min
Mud tank (1)	Suction	PNOG	1 unit	Volume 43.5m ³
(2)	Intermediate tank	"	1 unit	Volume 43.5m ³
(3)	Setting tank	"	1 unit	Volume 37.2m ³
Cooling tower	with blower	"	1 unit	with 5.5KW motor
Generator	D 3406	CATAPILLAR	2 sets	Capacity 210KW/440V-60HZ (set)
ROP	21 1/4"-2000	SHAFFER	1 set	API class 2000 (140 kg/cm ²)
	13 5/8"-3000	"	1 set	API class 3000 (210 kg/cm ²)
	13 5/8"-3000	"	1 set	" "
Accumulator unit	T15110-3S	KOOMEY	1 set	with 11KW motor
Water tank		PNOG	2 sets	Volume 37.8m ³ /set
Fuel tank		"	2 sets	Volume 22m ³ /set
Cementing unit	HT-400	HALLIBURTON	1 unit	with diesel engine
Water tank for cementing		PNOG	1 set	Volume 57.2m ³
Mud house		"	1 house	include drilling mud tester
Toolpushers office		"	2 houses	include radio beacon equipment
Warehouse		"	1 set	
Welder		HOBART	1 set	with diesel engine capacity 300A
Crown block	42"x5W, 55"x1W	NATIONAL	1 set	1 1/8" with rope size 1 1/8"
Traveling block	40"x5W	"	1 set	Wire rope size 1 1/8" Capacity 250T/10 line
Water swivel	N-59	"	1 set	
Kelly drive	HDP roller	VARCO	1 set	Hexagonal kelly pin drive type
Kelly cock	6 5/8"	OMSCO	1 set	test pressure 700kg/cm ²
Drilling spool	20"-2000#	CAMERON	1 set	2"-2000 with side valve
	12"-3000#	"	1 set	3"-3000 with side valve

Article	Description	Maker	Quantity	Remarks
Expansion spool	12"-3000x10"-3000	CAMERON	1 set	
Master valve	EIAT-08 10" φ	WKM	1 set	ANSI 900, Gate valve
Side valve	2 1/16 M	"	2 sets	API 3000, Gate valve
Kelly	5 1/4' Hexagon	DRILCO	1	12m length
Core barrel	7 7/8"x4" double core barrel	DIABOART	2	
Drilling recorder	RGD 67D	MARTIN DECKER	1	6 pen type
Directional survey instrument	Sperry sun B		1	include thermal sealed complete and container.
	Totoco (0~8° type)	TOTCO	1	include container
Float valve	4R-G	BAKER	2	
Truck crane		GROVE	1	Capacity 550 ton hydraulic type
Tire loader	FL 220T	Furukawa Industry	1	
Desander pump	Centrifugal	BJ	1	with 37KW motor
Desilter pump	"	"	1	"
Pump for water supply	"	"	1	with 11KW motor
Oxygen cutting installation		VICTOR	2	
Dog house		PNOG	1	
Lighting equipment			1 set	110V

App. 19 Tools list for drilling

Article	Description	Quantity	Pin x Box	Remarks
Drill pipe	5" x 19.5 16/ft	266	4 1/2" IF	R-2, Grade E
"	5" x "	40	"	R-2, Grade G
"	3 1/2" x 13.3 16/ft	10	3 1/2" IF	R-2, Grade E
Tubing pipe	2 7/8"	60	"	R-2
Drill collar	(O.D.) 9 1/2" x (I.D.) 3"	1	7 5/8" REG	4.56m Short drill collar
"	9 1/2" x (I.D.) 3"	3	"	R-2
"	7 3/4" x (2 3/4"~3")	11	6 5/8" REG	"
"	"	4	API NC56	"
"	6 1/2" x 2 1/4"	15	4 1/2" REG	"
Heavy weight drill pipe	5" x 50 16/ft	20	4 1/2" IF	"
Neck stabilizer	26" Blade type	1	7 5/8" REG	
"	26" Roller reamer type	1	"	
"	17 1/2" "	1	"	
"	12 1/4" Blade type	1	6 5/8" REG	Replaceable sleeve type
"	12 1/4" Roller reamer type	1	"	6 point Reamer
"	"	1	"	3 point Reamer
"	8 1/2" Blade type	3	4 1/2" REG	Integral blade type
"	" Roller reamer type	1	"	3 point Reamer
String stabilizer	17 1/2" Blade type	2	7 5/8" REG	I.D. 3"
"	12 1/4" "	5	6 5/8" REG	" 2 2/4"
"	8 1/2" "	4	4 1/2" REG	" 2 5/8" ~ 2 3/4"
Bit sub	26" T.B, 17 1/2" TB	1	7 5/8" REG	O.D. 9 1/2"
"	12 1/4" TB	1	6 5/8" REG	" 7 3/4"
"	8 1/2" TB	1	4 1/2" REG	" 6 1/2"
Shock sub	7 3/4"	2	6 5/8" REG	Hydraulic type
Hydraulic drilling jar	Down ward	2	4 1/2" IF	
"	Upper ward	2	"	
Non-magnetic drill collar	7 3/4" x 2 3/4" x 9.4 m	2	6 5/8" REG	
"	6 1/2" x 2 3/4" x 9.4 m	2	4 1/2" REG	
"	6 1/2" x 2 3/4" x 5.5 m	2	4 1/2" REG	
Dyna drill	7 3/4"	2	6 5/8" REG	include bent sub (orienting key setting)
"	6 1/2"	2	4 1/3" REG	"



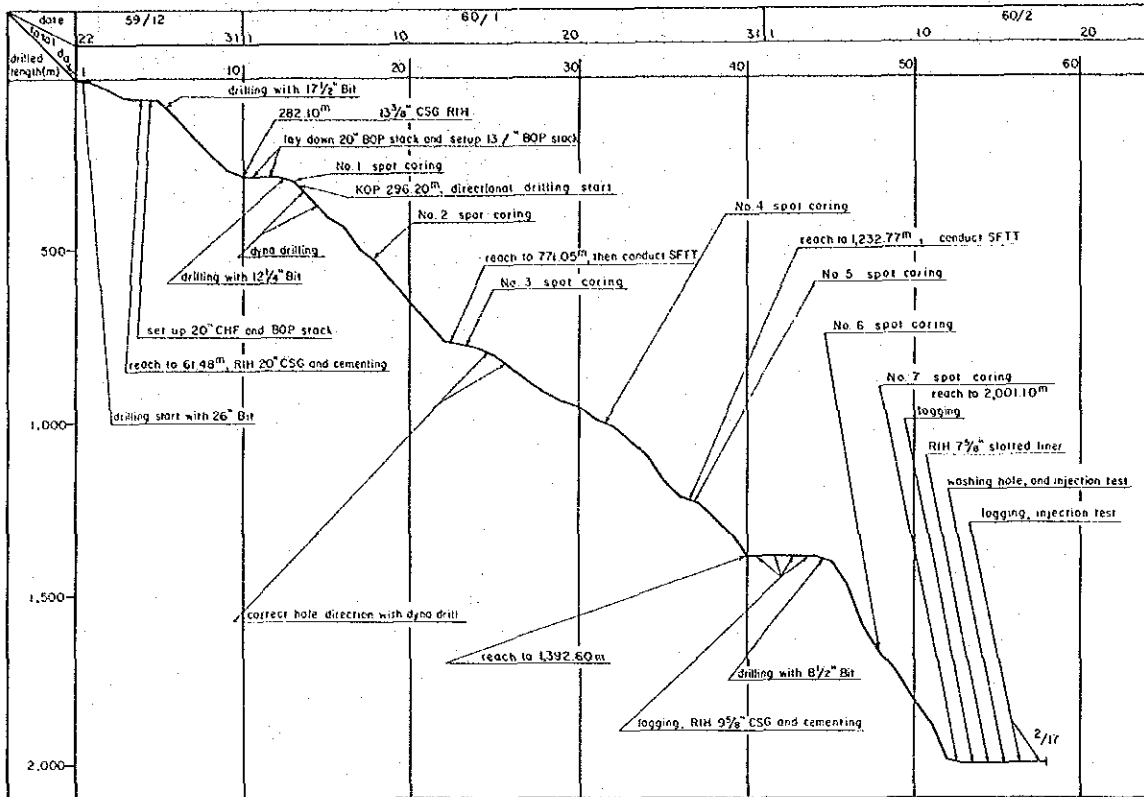
App. 20 Plan map of drill site

drilled length (m)	drilling conditions							bit record															
	weight on bit		maximum hook load (pull)		table revolutions per minute		drilling speed			bit size	nozzle size	drilling time			conditions after used								
	20	40	60	80	100	60	80	100	120			2	4	6	8	10	12	(HOUR)	bit changed depth	No	T	B	G
0																							
100																							
200																							
300																							
400																							
500																							
600																							
700																							
800																							
900																							
1,000																							
1,100																							
1,200																							
1,300																							
1,400																							
1,500																							
1,600																							
1,700																							
1,800																							
1,900																							
2,000																							
1) The drag produced by direction drilling indicated in the following (Maximum, hook load - weight of strings)											1) Not include drill outcement reaming and spot coring 2) Nozzle size indicate quantity x 16/32" ~ 20/32"												

App. 21 Record of drilling
A - 18

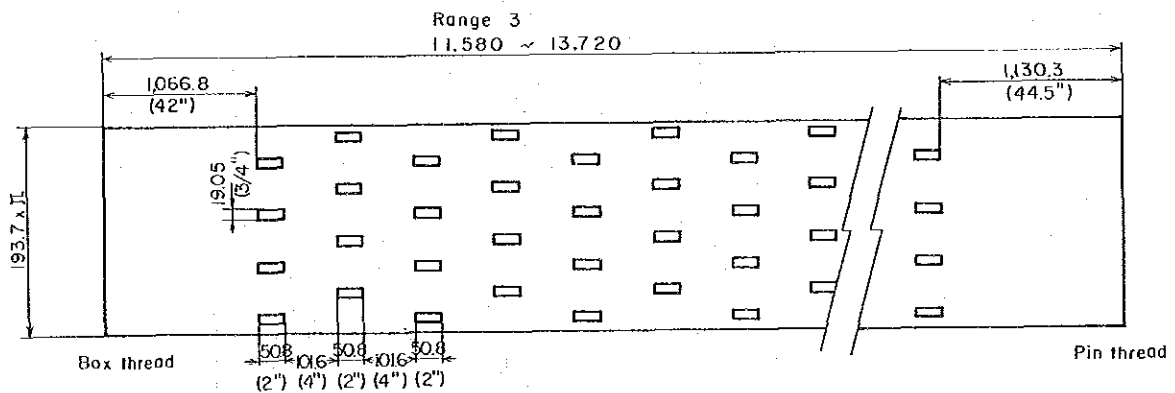
drilled length (m)	discharge mud volume (m ³ /min)		hydraulic pressure (kg/cm ²)					drilling mud temperature (°C)			owayin x wayout		funnel viscosity (sec)			mud character					remarks
	1	2	20	40	60	80	100	20	40	60	40	50	60	PV (CP)	YV (1000)	WL (CC)	Mud wt.	sand content (%)			
																	1.04			bentonite mud water	
																	1.05				
100																	1.04	0.25		fignosulfonate mud	
200																					
300																					
400																					
500																					
600																					
700																					
800																					
900																					
1,000																					
1,100																					
1,200																					
1,300																					
1,400																					
1,500																					
1,600																					
1,700																					
1,800																					
1,900																					
2,000																					

App. 22 Chart of drilling mud



Actual drilling process

App. 23 Chart of drilling process



percentage of slotted area

slotted area $1905 \times 5.08 \times 4 / \text{steps} = 38.71 \text{ cm}^2 / \text{steps}$

average length of casing $65 \text{ steps} \times 15.24 \text{ cm} / \text{steps} + 106.66 \text{ cm} + (113.03 - 5) = 1,205.31 \text{ cm}$

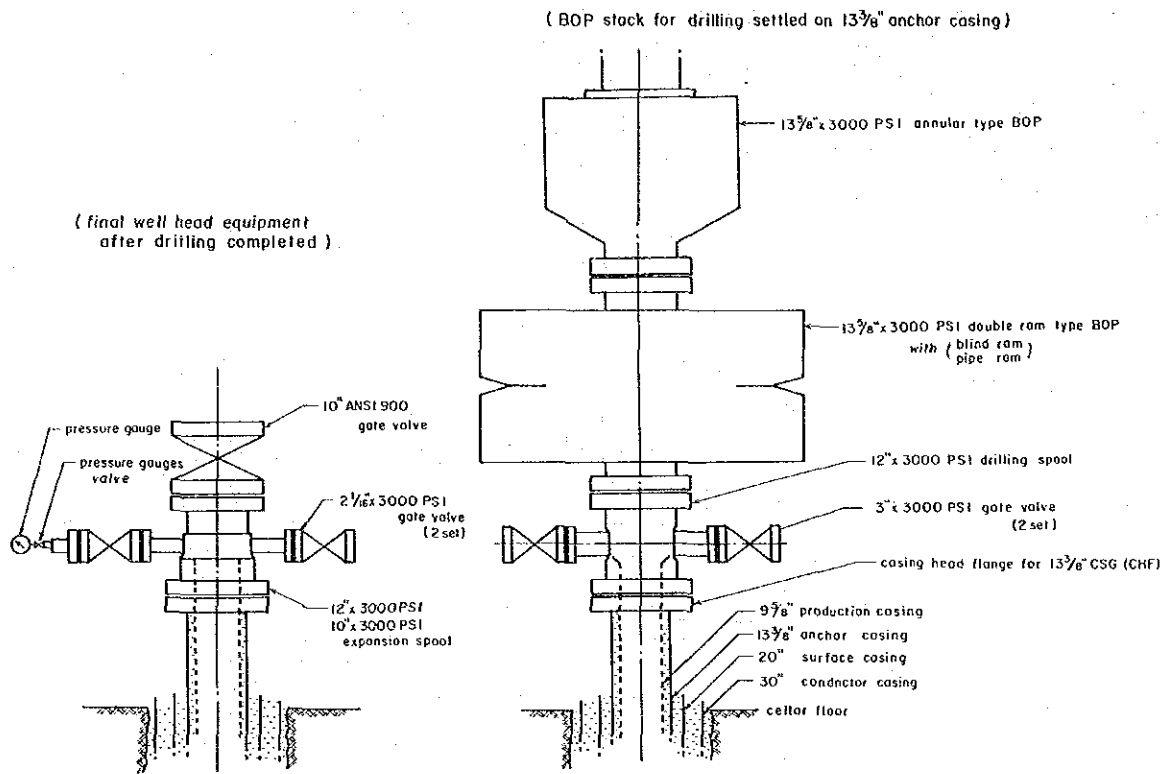
surface area of casing $19.37 \times \pi \times 1,205.31 = 73,309.12 \text{ cm}^2$

slotted area of casing $38.71 \times 65 = 2,516.15 \text{ cm}^2$

percentage of slotted area $2,516.15 \div 73,309.12 = 0.0343$

3.43 %

App. 24 Design of slotted liner casing pipe



App. 25 Well head assemblies

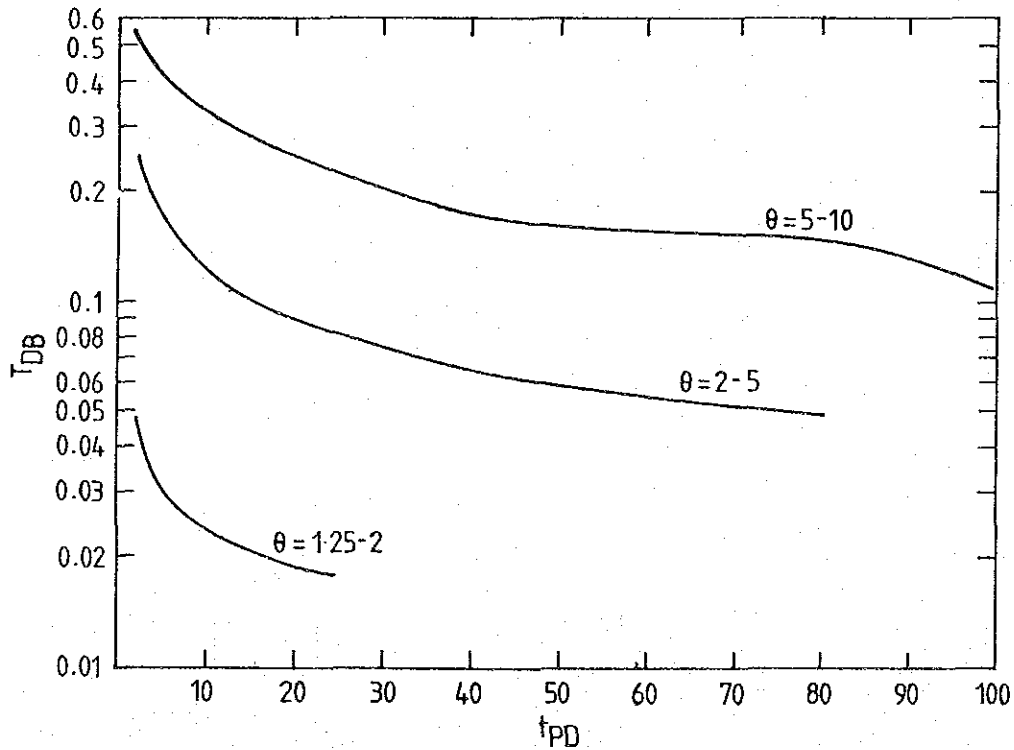
App. 26 List of minerals in sludge samples of the test well (3)

Samples		Zeolite Minerals					Clay Minerals										Sulfate Minerals		Carbonate Minerals			Silica Minerals		Feldspar		Others				Remarks						
No. (m)	division	clinoptilolite	stibite	morcanite	laumontite	laumontite	wairakite	smectite	zeolite	vermiculite	chlorite/saponite	illite/smectite	chlorite	illite	halloysite	kaoline	pyrophyllite	alunite	anhydrite	gypsum	calcite	dolomite	siderite	α -cristobalite	tridymite	quartz	plagioclase	potassium feldspar	pyrite		magnetite			epidote	amphibole	
1875.75	BULK					1	1														1														1	
1878.80	ORTD							+				++	+													+	+	+								
	EG							+				++	+													+										
	HCl							+				+																								
1939.80	BULK					1	1					1	1								1					8	7	1	1					1	1	
1942.85	ORTD					+	+					++	+													+	+	+	+						+	
	EG							+				++	+													+									+	
	HCl							+				+														+									+	
2003.85	BULK					1						2	1								1					9	7	1	1					1		
2009.95	ORTD											++	+												++	+	+	+							+	
	EG											++	+												+										+	
	HCl											+														+										+

LEGEND: a) division of the samples
 BULK: bulk sample
 ORTD: oriented clay sample
 EG: EG treated
 HCl: HCl treated

b) quantity
 ## abundant
 + common
 + a little
 + rare
 ? not clear

c) Quartz Index (QI)
 $QI = I_m \times 100 / I_q$
 I_m : Peak intensity of the mineral in the sample (cps)
 I_q : Peak intensity of the pure quartz (cps)



App. 28 Correction term of Rous et al. (1979), for evaluating temperature recovery

App. 27 Chemical analyses for sludge samples of the test well

Set No.	Sample No.	Depth from	to	SiO ₂ %	TiO ₂ %	Al ₂ O ₃ %	Fe ₂ O ₃ %	MnO %	MgO %	CaO %	Na ₂ O %	K ₂ O %	S %	H ₂ O-% %	ICL %	Total %	As ppm	Au ppm	B ppm	Ba ppm	Be ppm	Co ppm	Cu ppm	Hg ppm	Li ppm	Pb ppm	Rb ppm	Sb ppm	Sr ppm	Zn ppm
1	1	529.2	532.3	53.27	0.51	16.68	7.65	0.17	4.18	7.28	3.68	1.86	0.60	0.10	3.95	99.23	0.5	0.05	4	139	3	8	85	97	7	13	36	0	210	59
2	2	578.0	581.1	55.71	0.66	15.92	6.25	0.24	3.12	5.40	3.19	2.74	2.01	0.15	6.00	99.23	0.9	0.10	3	239	4	6	77	97	9	26	71	0	162	312
3	3	626.8	629.9	50.95	0.59	14.82	7.68	0.51	4.03	6.36	1.58	4.61	2.06	0.06	8.58	99.71	0.0	0.12	3	273	4	11	272	124	12	284	116	1	135	736
4	4	675.6	678.7	55.13	0.86	16.80	6.92	0.16	3.64	7.67	4.10	1.82	0.43	0.10	2.85	99.95	0.0	0.03	3	147	4	8	50	108	6	0	32	0	244	54
5	5	724.4	727.5	54.61	0.67	16.87	6.50	0.19	2.99	7.85	3.64	2.10	0.68	0.14	4.13	99.95	0.0	0.01	2	154	4	8	84	85	6	14	28	0	218	53
6	6	773.2	776.3	58.82	0.59	15.03	4.88	0.16	1.93	6.26	3.76	3.56	0.86	0.24	5.95	100.94	0.5	0.02	1	196	4	26	56	87	6	49	52	0	217	781
7	7	822.0	825.1	63.60	0.36	15.88	3.87	0.12	1.46	5.14	4.20	2.87	0.28	0.17	2.43	99.93	0.3	0.04	1	218	4	4	75	105	3	11	36	1	234	152
8	8	870.8	873.9	52.78	0.71	15.75	7.77	0.27	4.76	8.73	3.24	1.89	0.39	0.07	4.13	100.03	0.6	0.00	2	98	3	10	86	67	7	7	30	1	232	68
9	9	919.6	922.7	52.88	0.70	16.02	7.41	0.23	4.89	8.59	3.71	1.62	0.28	0.10	3.56	99.61	0.5	0.00	2	127	3	10	72	86	8	15	33	0	249	118
10	10	968.4	971.5	53.47	0.74	16.28	7.46	0.21	5.57	8.80	3.24	1.73	0.51	0.10	2.77	100.27	0.5	0.00	3	104	3	11	67	104	6	8	33	0	235	84
11	11	1017.2	1020.2	52.98	0.61	13.04	7.72	0.39	4.20	9.73	1.87	1.33	0.60	0.14	7.66	99.53	0.9	0.03	3	75	3	10	49	87	12	14	33	1	156	115
12	12	1066.0	1069.0	53.96	0.75	16.01	7.77	0.26	5.24	8.41	3.29	1.51	0.40	0.09	3.09	100.29	0.6	0.00	6	129	3	11	72	111	7	10	22	1	255	86
13	13	1114.8	1117.8	52.51	0.75	16.99	7.34	0.18	4.26	8.56	3.97	1.71	0.77	0.05	3.00	99.27	0.3	0.00	8	116	3	10	43	80	5	7	27	0	237	63
14	14	1160.5	1163.6	53.05	0.80	16.35	7.43	0.24	4.63	8.18	3.61	1.84	0.72	0.02	3.64	99.77	0.5	0.00	3	98	3	10	88	90	7	10	22	0	235	107
15	15	1212.4	1215.4	55.81	0.66	15.91	6.80	0.15	3.40	7.15	3.47	1.93	1.14	0.08	4.33	99.61	0.5	0.11	3	154	4	9	165	81	6	8	26	0	230	61
16	16	1261.2	1264.2	54.40	0.60	16.46	6.81	0.26	3.13	7.41	3.34	2.91	1.02	0.11	4.51	99.83	0.4	0.00	6	158	4	8	80	82	8	13	40	0	239	129
17	17	1310.0	1313.0	53.27	0.68	15.91	7.55	0.26	3.74	7.60	3.01	2.54	0.64	0.16	5.25	99.81	0.5	0.02	4	172	3	9	107	84	12	10	44	1	224	212
18	18	1361.8	1364.9	54.17	0.85	16.57	8.37	0.17	3.87	8.10	3.50	2.03	0.93	0.10	2.84	100.47	0.0	0.00	5	132	3	11	72	90	6	8	35	0	259	124
19	19	1407.6	1410.6	55.23	0.79	15.85	7.23	0.23	2.90	7.50	3.12	2.17	1.06	0.12	4.57	99.59	0.4	0.01	4	113	4	7	90	134	10	26	51	2	220	144
20	20	1456.4	1459.4	55.32	0.67	14.95	6.65	0.33	3.80	7.31	2.17	1.84	2.15	0.11	6.15	99.19	0.4	0.01	5	92	4	8	77	90	19	30	43	0	231	243
21	21	1505.2	1508.2	52.74	0.87	15.46	7.37	0.31	3.81	7.75	2.80	2.03	1.65	0.11	6.19	99.33	0.6	0.01	3	157	4	10	139	94	15	33	35	1	257	292
22	22	1553.9	1557.0	55.26	0.53	16.22	5.70	0.16	2.81	6.08	3.59	1.54	1.53	0.11	7.32	99.21	0.5	0.00	2	200	4	8	68	84	13	10	23	1	257	66
23	23	1602.7	1605.8	57.46	0.57	15.23	6.93	0.16	2.85	4.96	1.70	2.45	2.73	0.39	7.23	99.54	0.4	0.01	3	143	3	9	99	35	13	130	60	1	148	886
24	24	1651.5	1654.6	59.58	0.55	15.96	6.12	0.16	2.88	6.29	3.55	1.54	1.19	0.15	4.13	100.76	0.5	0.00	2	164	3	8	67	90	13	11	26	0	209	63
25	25	1700.3	1703.4	59.64	0.47	15.40	5.92	0.15	2.40	5.81	3.15	1.68	0.52	0.19	4.56	99.18	0.3	0.00	3	227	4	7	52	63	13	19	37	1	237	86
26	26	1749.1	1752.2	59.06	0.49	15.29	5.58	0.14	2.52	6.00	3.41	1.75	0.71	0.17	5.04	99.28	0.2	0.00	6	180	4	7	48	64	11	13	37	0	216	58
27	27	1797.9	1801.0	61.81	0.46	15.56	5.15	0.16	2.56	5.41	3.68	1.78	0.59	0.15	3.25	99.82	0.1	0.00	2	249	4	7	49	74	12	10	33	0	244	71
28	28	1846.7	1849.8	60.76	0.48	15.20	4.94	0.08	2.43	5.53	3.15	3.07	1.72	0.13	4.07	99.71	0.3	0.00	3	117	4	7	45	90	10	7	28	1	219	49
29	29	1895.5	1898.6	62.44	0.46	15.37	4.88	0.11	2.45	5.75	3.26	2.05	0.87	0.14	2.88	99.65	0.2	0.00	2	205	4	5	52	64	10	7	33	0	249	54
30	30	1944.3	1947.4	61.36	0.47	15.44	5.71	0.15	2.44	5.79	3.50	2.66	0.62	0.18	2.78	100.30	0.2	0.00	3	246	3	6	48	75	9	6	33	1	246	63
31	31	1993.1	1996.2	60.38	0.47	15.22	6.25	0.15	2.55	5.76	3.40	1.89	0.66	0.21	3.01	99.08	0.3	0.01	4	236	3	8	42	80	13	11	35	0	251	65

App. 29 Records of the static formation temperature test

Test No. 1 (732.8 m)

Measured Drilled Depth : 732.8 m CHF
Vertical Depth : 701 m CHF, Elevation R.S.L. : +120 m

Date : Drill Bit Passing : 11:30, Jan/12, 1985
Circulation Halt : 0:00, Jan/13, 1985
Temp. Log Starting : 3:30, Jan/13, 1985

Cooling Time, T_p : 12.5 hours

Temperature Measured	Time & Date	Recovery Time Δt
62.2 °C	3:45, Jan/13	3.75 hours
63.6	4:15, "	4.25
64.3	4:45, "	4.75
65.0	5:15, "	5.25
65.9	5:45, "	5.75
66.4	6:15, "	6.25
67.0	6:45, "	6.75
67.4	7:15, "	7.25
67.9	7:45, "	7.75
68.4	8:15, "	8.25
68.8	8:45, "	8.75
69.3	9:15, "	9.25
69.8	9:45, "	9.75
70.0	10:00, "	10.00

Apparent Static Temperature T_{ws} : 79.1

Correlation Coefficient : 0.998
Slope of Horner Straight Line, m : 26.4 °C/cycle
Roux Correction Term, t_{pD} : 5.0
Roux Correction Term, T_{pB} : 0.18

Initial Formation Temperature, T_i : 83.8 °C

Table -1 (3) Static Formation Temperature Test

Test No. 3 (1200 m)

Measured Drilled Depth : 1200 m CHF
Vertical Depth : 1052 m CHF, Elevation R.S.L. : -231 m

Date : Drill Bit Passing : 06:30, Jan/26, 1985
Circulation Halt : 01:30, Jan/31, 1985
Temp. Log Starting : 06:33, Jan/31, 1985

Cooling Time, T_p : 115 hours

Temperature Measured	Time & Date	Recovery Time, Δt
82.0 °C	7:21, Jan/31	5.85 hours
91.6	13:07, "	11.62
96.5	20:14, "	18.73
100.1	0:44, Feb/1	23.21

Apparent Static Temperature, T_{ws} : 125.0 °C

Correlation Coefficient : 0.998
Slope of Horner Straight Line, m : 32.6 °C/cycle
Roux Correction Term, t_{pD} : 46
Roux Correction Term, T_{pB} : 0.18

Initial Formation Temperature, T_i : 130.9 °C

Static Formation Temperature Test

Test No. 3 (1400 m)

Measured Drilled Depth : 1400 m CHF
Vertical Depth : 1208 m CHF, Elevation R.S.L. : -387 m

Date : Drill Bit Passing : 22:30, Jan/30, 1985
Circulation Halt : 01:30, Jan/31, 1985
Temp. Log Starting : 06:33, Jan/31, 1985

Cooling Time, T_p : 3.00 hours

Temperature Measured	Time & Date	Recovery Time, Δt
106.4 °C	07:30, Jan/31	6.00 hours
120.0	13:17, "	11.78
125.0	20:27, "	18.95
130.8	01:00, Feb/1	23.50

Apparent Static Temperature, T_{ws} : 138.6 °C

Correlation Coefficient : 0.989
Slope of Horner Straight Line, m : 184.4 °C/cycle
Roux Correction Term, t_{pD} : 1.2
Roux Correction Term, T_{pB} : 0.1

Initial Formation Temperature, T_i : 157.0 °C

Test No. 2 (1207 m)

Measured Drilled Depth : 1200 m CHF
Vertical Depth : 1052 m CHF, Elevation R.S.L. : -231 m

Date : Drill Bit Passing : 16:00, Jan/26, 1985
Circulation Halt : 04:00, Jan/27, 1985
Temp. Log Starting : 09:42, Jan/27, 1985

Cooling Time, T_p : 12.00 hours

Temperature Measured	Time & Date	Recovery Time Δt
86.0 °C	10:50, Jan/27	6.83 hours
90.2	11:00, "	7.00
91.7	11:15, "	7.25
92.8	11:30, "	7.50
93.9	11:45, "	7.75
94.0	12:00, "	8.00
94.6	12:15, "	8.25
94.9	12:30, "	8.50
95.4	12:45, "	8.75
95.9	13:00, "	9.00
96.5	13:15, "	9.25
97.1	13:30, "	9.50
97.6	13:45, "	9.75
97.9	14:00, "	10.00
98.4	14:15, "	10.25
98.7	14:30, "	10.50
99.2	14:45, "	10.75
99.7	15:00, "	11.00
100.2	15:15, "	11.25
100.6	15:30, "	11.50
101.2	15:45, "	11.75
101.6	16:00, "	12.00

Apparent Static Temperature, T_{ws} : 127.7 °C

Correlation Coefficient : 0.971
Slope of Horner Straight Line, m : 86.5 °C/cycle
Roux Correction Term, t_{pD} : 4.8
Roux Correction Term, T_{pB} : 0.18

Initial Formation Temperature, T_i : 143.3 °C

Static Formation Temperature Test

Test No. 3 (1300 m)

Measured Drilled Depth : 1300 m CHF
Vertical Depth : 1131 m CHF, Elevation R.S.L. : -310 m

Date : Drill Bit Passing : 04:00, Jan/29, 1985
Circulation : 01:30, Jan/31, 1985
Temp. Log Starting : 06:33, Jan/31, 1985

Cooling Time, T_p : 45.5 hours

Temperature Measured	Time & Date	Recovery Time, Δt
86.0 °C	7:25, Jan/31	5.92 hours
99.9	13:11, "	11.68
106.8	20:21, "	18.85
111.4	00:52, Feb/1	23.37

Apparent Static Temperature, T_{ws} : 135.8 °C

Correlation Coefficient : 0.998
Slope of Horner Straight Line, m : 52.9 °C/cycle
Roux Correction Term, t_{pD} : 18.2
Roux Correction Term, T_{pB} : 0.1

Initial Formation Temperature, T_i : 141.1 °C

App. 30 Records of temperature recovery test

unit : °C, AC-1D Well, 1985

No.	KT-1	KT-2	KT-3		KT-4	KT-5		
Date	16/Feb	17/Feb	19/Feb	22/Feb	22/Feb	28/Feb	28/Feb	
Elapsed Time*	-	28hrs	73hrs		143hrs	279hrs		
Measured Depth (m CHF)	CHF	-	26	33	(R36)	31	34	
	100	-	38	33	(R38, N38)	36	35	
	200	-	44	45		48	37	
	300	-	46	50	(R48, N55)	53	50	(R53, N53)
	400	-	51	54		59	57	
	500	-	55	59	(R64, N68)	65	64	(R66, N67)
	600	-	60	65		72	70	
	700	-	66	71	(R78, N84)	81	78	(R84, N85)
	800	-	73	80		91	87	
	900	-	80	89		102	98	
	1000	-	89	99		112	110	
	1100	-	97	108		120	121	
	1200	-	104	116		129	129	(R134, N140)
	1300	-	112	124		140	139	
	1400	62	120	134		147	151	
	1500	70	129	143		156	158	
	1600	80	138	152		164	166	
	1700	94	146	160		170	174	
	1800	102	151	166		175	181	(R177, N193)
	1900	110	156	170		181	188	
2000	118	164	176		193	193		
MCD	162	193	199	(R 195, N >200)	197	204		
RD	2019	2019	ND	ND	ND	2018		

* Elapsed Time : Time after halt of 2nd hydrofracturing (20:00, 16/Feb) at MCD

** R.D : Read value of depth meter as MCD

*** () : Temperature from Maximum Thermometer, R : Reverse, N : Normal

Table 2 (2)

^N KT-6	KT-7	KT-8		^N KT-9	KT-10	KT-11	^N KT-12	
2/Mar	2/Mar	7/Mar	7/Mar	7/Mar	12/Mar	18/Mar	20/Mar	20/Mar
328 hrs	330 hrs	19 days		19 days	24 days	30 days	32 days	
-	34	-			39	37	-	
-	35	-			41	38	-	
-	36	37		51	47	46	-	
49.8	45	53		53	53	53	-	
61.9	50	59		61	59	60	59	
68.0	58	66		66	66	66	67	
74.1	65	-			72	74	73	
80.8	75	-			80	82	82	
89.9	84	-			92	92	92	
99.3	94	-			102	103	106	
109.6	107	114	(R112)	115	115	117	118	(R116)
123.6	118	-			126	128	129	
133.8	129	-			137	138	140	
143.5	137	-			144	149	150	
155.2	150	152	(R182)	160	159	160	159	(R121)
165.5	156	165		166	167	166	172	
173.1	166	172		175	173	174	179	(R188)
181.4	173	179	(R188)	184	180	181	189	
188.5	181	187		192	189	189	195	
195.4	187	193		202	195	195	201	
197.4	193	198		207	199	199	209	
205.2	204	208	(R211)	211	209	205	217	(R214)
2021	2020	2021		ND	2025	2022	2020	

**** Kuster Elements ; N : No. 27069, No Mark : No. 10504

App. 31 Records of injection test

Injectivity Test III (Hydrofracturing)

Date : 16/Feb., 1985

Method : Long time injection

Time	Well Head Pressure		Flowrate	
	(psig)	(Mpag)	(SPM)	(l/sec)
8:00	start			
8:30	1200	8.27	76	14.53
9:00	1250	8.62	70	13.38
10:00	1290	8.89	68	13.00
11:00	1300	8.96	68	13.00
12:00	1320	9.10	72	13.76
13:00	1340	9.24	77	14.72
14:00	1330	9.17	76	14.53
15:00	1330	9.17	75	14.34
16:00	1330	9.17	74	14.15
17:00	1320	9.10	73	13.95
18:00	1330	9.17	73	13.95
19:00	1320	9.10	73	13.95
20:00	1320	9.10	73	13.95

Injectivity Test II (Multistage Injection)

Date : 15/Feb., 1985

Method : Pressurizing well injection

Time	Well Head Pressure		Hole Press* (Mpag)	Flowrate	
	(psig)	(Mpag)		(SPM)	(l/sec)
06:00 to 06:30	500	3.45	15.43	14	2.68
06:30 to 07:00	700	4.83	17.10	27	5.31
07:00 to 07:30	950	6.55	18.67	41	7.84
07:30 to 08:00	1100	7.59	19.97	55	10.61

Hole Press. : Measured pressure at drilled depth of 1450 m.

App. 32 Records of pressure drop after inunction test

unit: Mpag, AC-1D Well, 1985

No.	KP-2	KP-3	KP-4	KP-6	KP-7
	Date	17/Feb	19/Feb	23/Feb	2/Mar
Elapsed Time	28 hrs	73 hrs	167 hrs	330 hrs	19 days
CHF	0	0	0	0	0
100	0.32	0	0	0	ND
200	1.33	0.07	0	0	ND
300	2.10	1.40?	0.8	0.55	0.8
400	3.10	1.98	1.7	1.2	1.75
500	3.97	2.88	2.5	2.5	2.75
600	4.85	3.74	3.6	3.4	ND
700	5.63	4.53	4.35	4.2	ND
800	6.42	5.28	4.75	4.75	ND
900	7.10	5.96	5.7	5.68	ND
1000	7.78	6.64	6.4	6.38	6.60
1100	8.44	7.41	7.1	7.05	ND
1200	9.06	8.05	7.75	7.62	ND
1300	9.80	8.70	8.4	8.3	ND
1400	10.42	9.40	9.1	8.83	9.20
1500	11.10	10.05	9.8	9.55	9.95
1600	11.84	10.80	10.3	10.3	10.60
1700	12.50	11.45	10.95	10.9	11.20
1800	13.30	12.40?	11.85	11.77	11.95
1900	13.95	12.81	12.50	12.48	12.60
2000	14.68	13.45	13.20	13.0	13.10
MCD	14.90	13.80	13.40	13.43	13.20
R.D	2019	ND	ND	2020	2021

* Elapsed Time : Time after halt of 2nd hydrofracturing (20:00, 16/Feb) at MCD

** R.D. : Read value of depth meter as MCD

*** ? : Doubtful value

Injectivity Test I (Hydrofracturing)

Date : 15/Feb, 1985

Method : Long time injection

Time	Well Head Pressure		Flowrate	
	(psig)	(MPag)	(SPM)	(l/sec)
15:30	start	-	-	-
15:33	1000	6.90	70	13.38
15:35	1270	8.76	100	19.12
15:40	1320	9.10	97	18.54
15:45	1360	9.38	92	17.59
15:50	1390	9.58	95	18.16
16:00	1400	9.65	92	17.59
16:15	1410	9.72	88	16.82
16:30	1410	9.72	88	16.82
17:00	1410	9.72	88	16.82
18:00	1430	9.86	85	16.25
19:00	1450	10.00	80	15.29
20:00	1450	10.00	80	15.29
21:00	1450	10.00	80	15.29
21:30	1450	10.00	80	15.29

* (psi) : Well head pressure guege (power per inch)

** (SPM): Strokes per minute of pumping.

1 SPM = 3.03 gal/min = 19.12 l/sec

JICA