

trol must be performed actually on the unit and the suitable chemical injection rate must be decided.

- ii. Change to All Volatile Treatment for drum water treatment. When phosphate is used for the drum water treatment, it is possible that the boiler tube will be attacked by the free caustic. To avoid such condition, Kyushu Electric Power Co. adopts all volatile treatment (AVT) even in the case of the drum type boiler and prevents the damage of material by the water quality. In the adoption of AVT, first the frequency of condenser in-leakage must be minimized.

- (d) Making of monthly report about water analysis (See Table 5C-17)

As an elemental data for monthly report, daily analysis data on every items shall be recorded through one month period. It can be used for checking purposes.



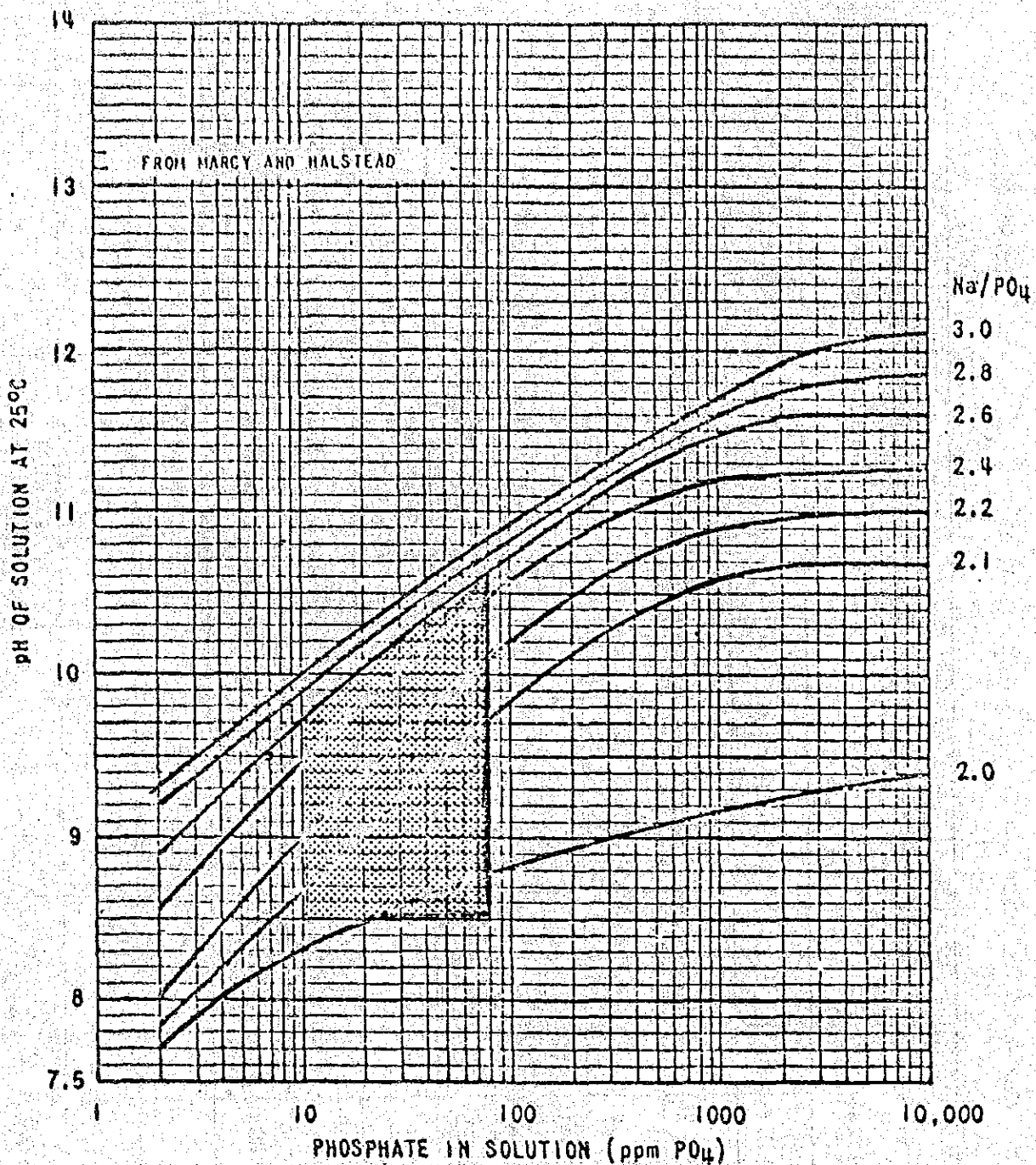


Fig. 5C-3 PH OF ORTHOPHOSPHATE SOLUTIONS HAVING VARIOUS MOL RATIOS OF SODIUM TO PHOSPHATE

Table 5C-13 SYSTEM ANALYSES DATA DONE BY JICA TEAM

(Gardner/Snyder)

Unit	Sample	Time	pH *	Cond. ( $\mu$ S/cm)	Cation Cond. ( $\mu$ S/cm)	Fe (ppb)	Temp. ( $^{\circ}$ C)
S-1	Condensate	Aug. 10	9.3/9.6	9.45	0.83		36
S-2	Condensate	Aug. 10	9.25/ 9.55	8.53	0.45		36
S-1	Condensate	Aug. 11	9.35/ 9.65	10.8	0.85		35
S-2	Condensate	Aug. 11	9.3/ 9.6	10.1	0.41		35
G-1	Condensate	Aug. 11		5.6	0.92		
G-1	Superheated Steam	Aug. 11		5.7	0.95		
G-1	Saturated Steam	Aug. 11		5.8	0.87 ~0.98		
S-1	Ammonex A	Aug. 11		9.8	0.50		
S-1	Ammonex B	Aug. 11		0.58	0.62		
S-2	Ammonex A	Aug. 11		10.2	0.43		
S-2	Ammonex B	Aug. 11		10.2	0.43		
S-2	Ammonex C	Aug. 11		6.2	0.39		
S-1	Condensate	Aug. 12	9.45/ 9.75	13.0	0.99		35
S-2	Condensate	Aug. 12	9.40/ 9.70	12.5	0.33		34
S-1	Condensate	Aug. 13	9.4/9.7	12.0	1.0		36
S-2	Condensate	Aug. 13	9.1/9.4	6.2	0.32		36

\* left/right = at sample temp / at 25 $^{\circ}$ C (by graph)

Table 5C-13 SYSTEM ANALYSES DATA DONE BY JICA TEAM  
(Gardner/Snyder)

Unit	Sample	Time	pH*	Cond. ( $\mu$ S/cm)	Cation Cond. ( $\mu$ S/cm)	Fe (ppb)	Temp ( $^{\circ}$ C)
S-1	Condensate	Aug. 17		9.5	0.34		
S-2	Condensate	Aug. 17		7.2	0.31		
G-1	Condensate	Aug. 18	8.55/9.1	3.5	0.66		48
G-1	Superheated Steam	Aug. 18	8.8/9.1	3.6	0.81		37
G-1	Saturated Steam	Aug. 18	8.85/9.15	3.9	0.65		37
G-1	Boiler Saline	Aug. 18	9.3/	18.0	13.0		35
S-1	Condensate	Aug. 18	9.6/9.9	19.0	0.70		34
S-1	Ammonex B	Aug. 18	9.2/9.9	19.0	0.89		47
S-1	Ammonex C	Aug. 18	9.2/9.9	19.0	0.65		47
S-1	Main Steam	Aug. 18	9.2/9.9	17.4	0.91		45
S-2	Condensate	Aug. 18	9.35/ 9.65	11.0	0.37		36
S-2	Ammonex B	Aug. 18	8.9/9.6	9.0	0.46		52
S-2	Ammonex C	Aug. 18	8.9/9.6	9.0	0.45		51
S-2	Ammonex D	Aug. 18	8.9/9.5	8.8	0.72		45
S-1	Condensate	Aug. 20	9.4/9.7	12.0	0.90		35
G-1	Feedwater	Aug. 23				12	
S-1	Eco Inlet	Aug. 23				20	
S-1	Condensate	Aug. 23				5	
S-2	Eco Inlet	Aug. 23				4	

\* left/right = at sample temp/at 25 $^{\circ}$ C (by graph)

Table 5C-13 SYSTEM ANALYSES DATA DONE BY JICA TEAM

Unit	Sample	Time	pH <sup>*</sup>	Cond. ( $\mu$ S/cm)	Cation Cond. ( $\mu$ S/cm)	Fe (ppb)	Temp (°C)
G-1	Feedwater	Sept. 3	8.8 <sup>**</sup>			8 <sup>**</sup>	
G-1	Condensate	Sept. 3	8.2 <sup>**</sup>			10 <sup>**</sup>	
S-1	Condensate	Sept. 9	9.3/9.6 (9.1) <sup>**</sup>	10.5	0.55		33
S-2	Condensate	Sept. 9	9.1/9.4 (8.7) <sup>**</sup>	7.3	0.38		33
S-1	Condensate	Sept. 9 <sup>***</sup>			0.45		33
S-1	Ammonex B	Sept. 9 <sup>***</sup>		0.19	0.28		53
S-1	Ammonex C	Sept. 9 <sup>***</sup>		0.70	0.70		53

\* left/right = at sample temp/at 25°C

\*\* by NAPOCOR ( Fe analysis = TPTZ Method )

\*\*\* just after H/OH operation of all ammonexs

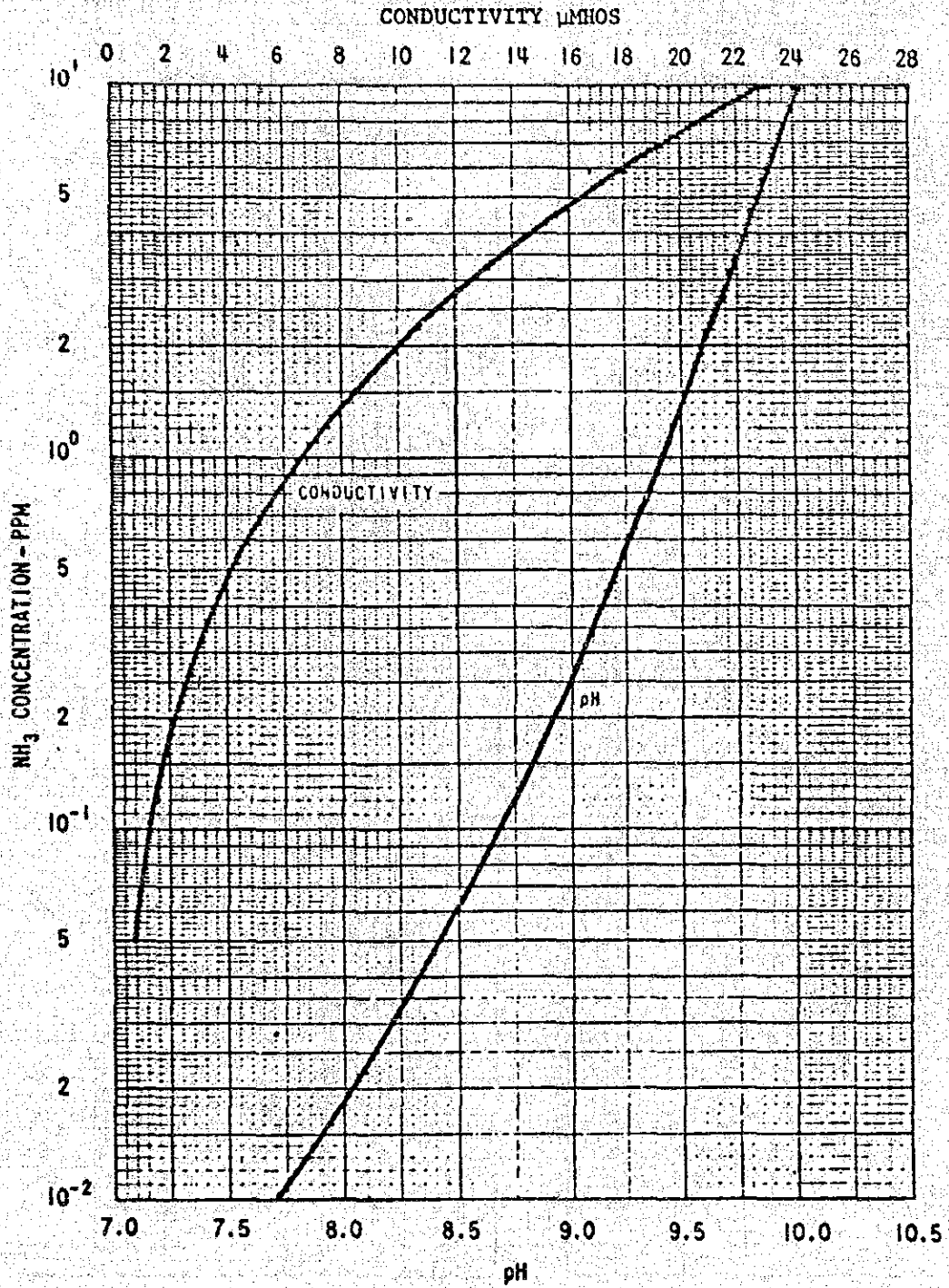
Table 5C-14 SYSTEM ANALYSES DATA DONE BY JICA TEAM (MALAYA)

Unit	Sample	Time	pH*	Cond. ( $\mu$ S/cm)	Cation Cond. ( $\mu$ S/cm)	Temp. ( $^{\circ}$ C)
M-1	Condensate	Aug. 24	8.6/8.9	3.2	0.51	35
M-1	Deaerator Outlet	Aug. 24	8.0/8.3 (8.0)**	2.8	0.46	35
M-1	Ammonex A	Aug. 24		0.38	0.41	40
M-1	Ammonex B	Aug. 24		0.51	0.66	41
M-1	Ammonex C	Aug. 24		0.22	0.32	41
M-1	Ammonex D	Aug. 24		0.33	0.50	42
M-1	Condensate	Aug. 25		1.8	0.49	
M-1	Deaerator Outlet	Aug. 25		2.3	0.36	
M-2	CP Discharge	Aug. 27		3.1	1.6	23
M-2	Eco Inlet	Aug. 27		2.7		
M-2	Boiler Saline	Aug. 27		19	59	
M-1	Deaerator Outlet	Sept. 1			0.55	
M-1	CP Discharge			3.5	0.50	

\* left/right = at sample temp/at 25 $^{\circ}$ C

\*\* Monitor

Fig. 5C-4 VARIATION OF SOLUTION PH AND ELECTRICAL CONDUCTIVITY WITH AMMONIA CONCENTRATION AT 25°C





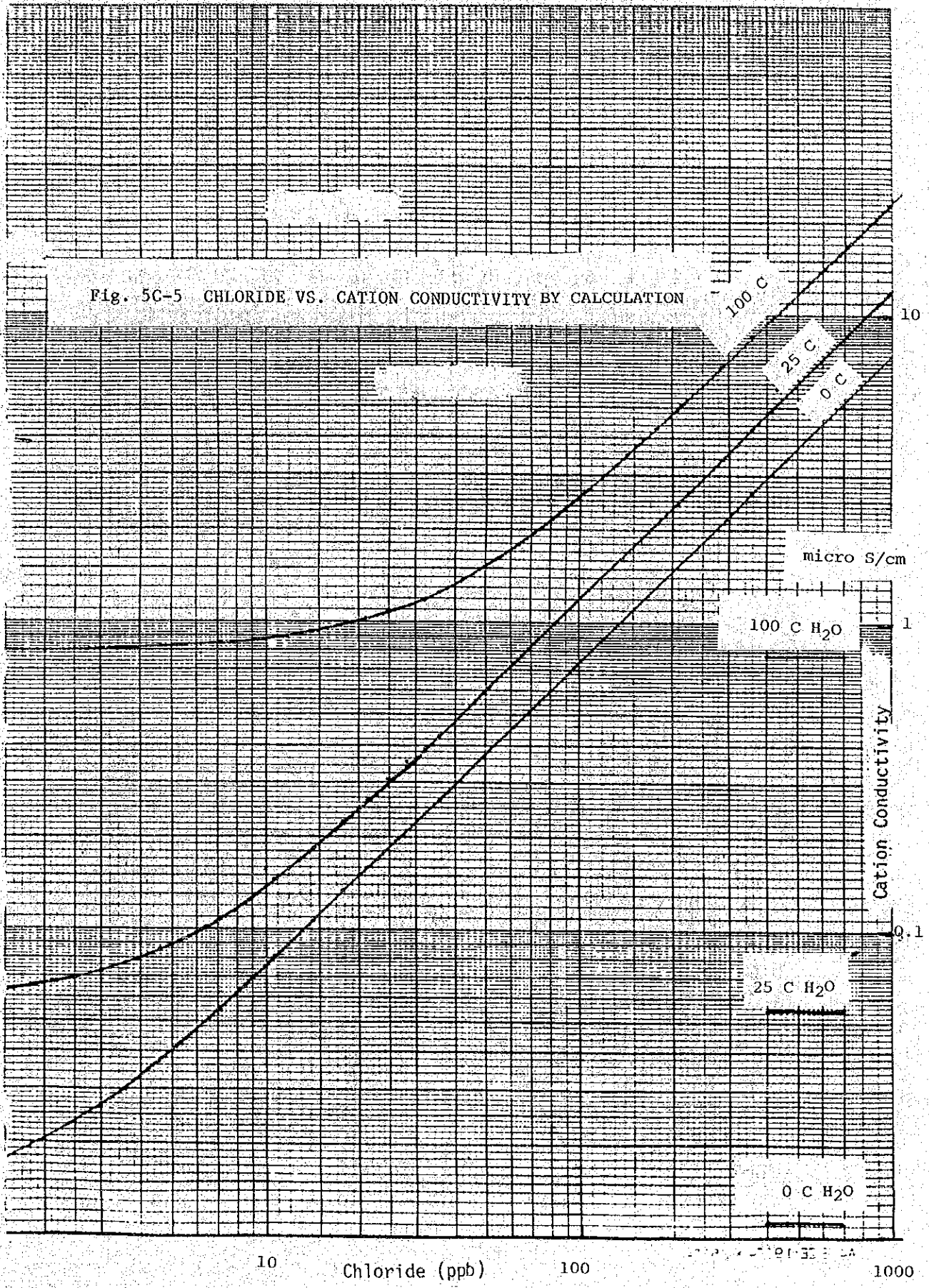


Fig. 5C-5 CHLORIDE VS. CATION CONDUCTIVITY BY CALCULATION

micro S/cm

100 C H<sub>2</sub>O

25 C H<sub>2</sub>O

0 C H<sub>2</sub>O

10

Chloride (ppb)

100

1000

Table 5C-15 DETECTION LIMIT OF WATER ANALYSIS AT GSTP AND MTP

ITEM	ACTUAL		REQUIRED
	GSTP	MTP	
Chloride (ppm as Cl)	0.1 ~ 0.2	0.1 ~ 0.2 with 20mm cell 0.02 ~ 0.04 with 100mm cell	<0.02
Silica (ppm as SiO <sub>2</sub> )	0.03 ~ 0.05	0.02 ~ 0.04	<0.02
Sulfate (ppm as SO <sub>4</sub> )	1 ~ 2	0.5 ~ 1.0	--
Copper (ppm as Cu)	0.005 ~ 0.01	-----	<0.002
Iron (ppm as Fe)	0.02 ~ 0.04	-----	<0.01

Fig. 5C-6 Na AND CATION CONDUCTIVITY AT SNYDER-1  
CONDENSATE DURING CONDENSER IN-LEAKAGE  
(August 16, 1982)

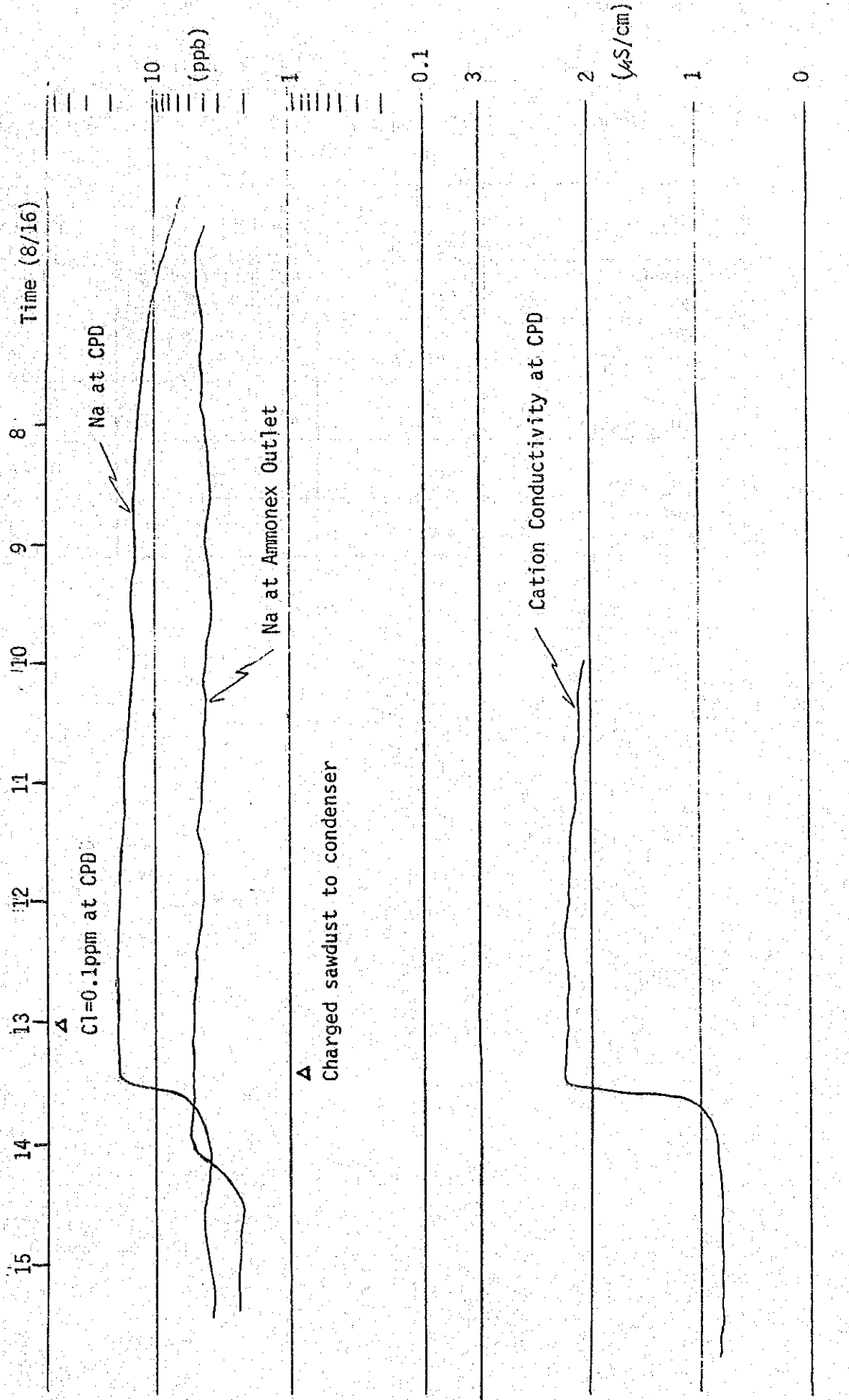


Fig. 5C-7 WATER QUALITY AT MALAYA-2 DURING CONDENSER LEAKAGE

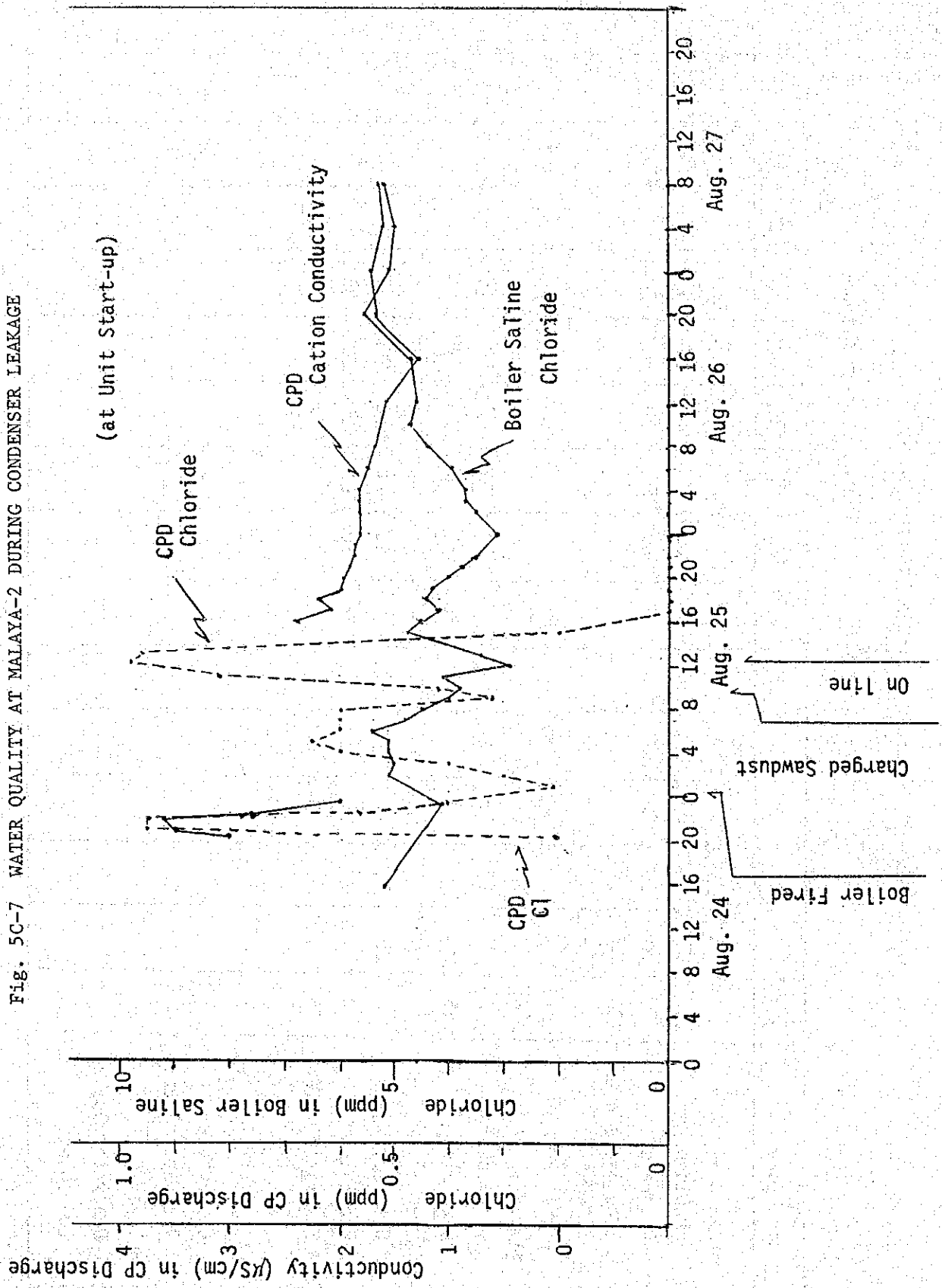
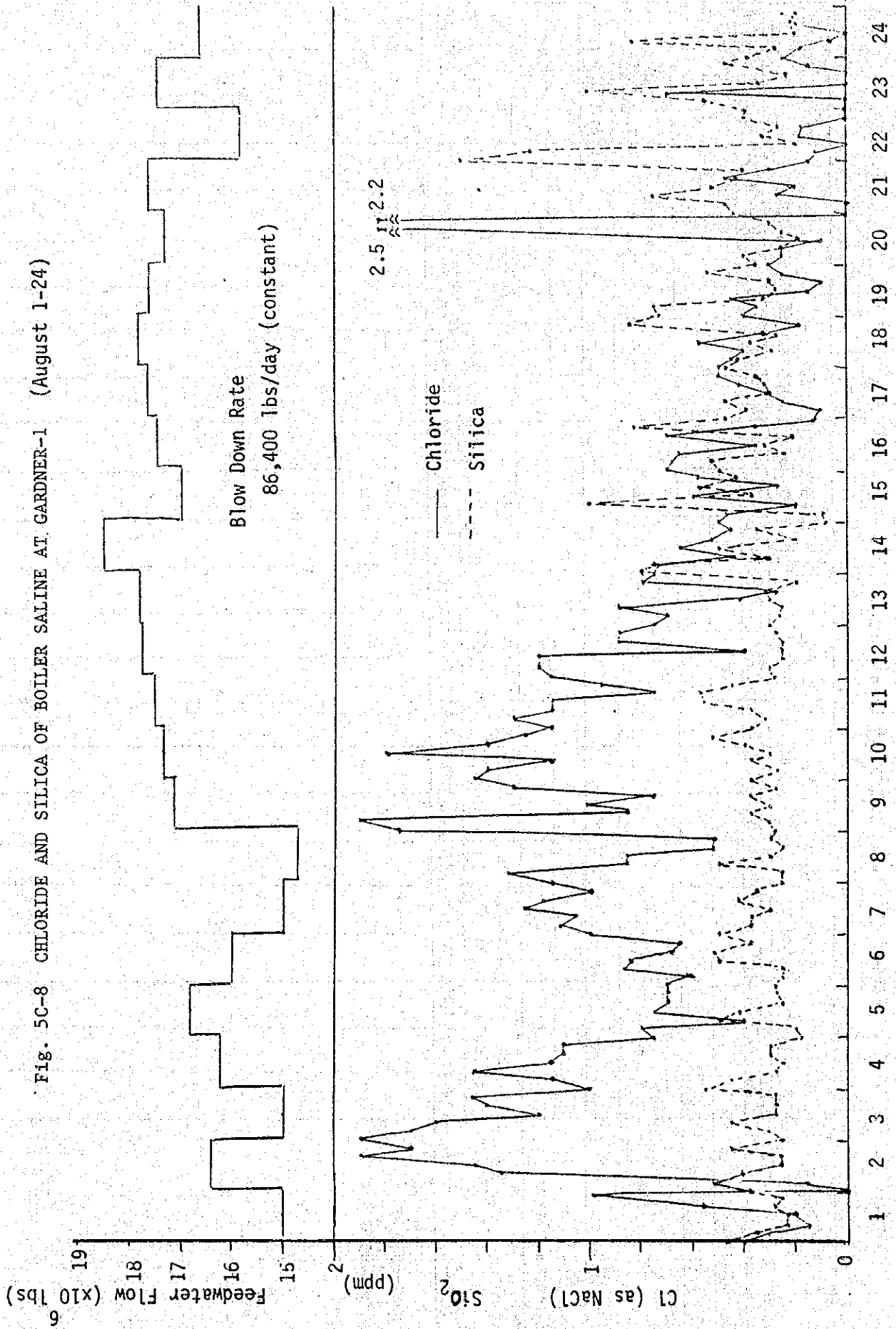




Fig. 5C-8 CHLORIDE AND SILICA OF BOILER SALINE AT GARDNER-1 (August 1-24)





Reference - 5 Limit Value on Water Quality

G-1

Boiler Water LimitsPressure = 1800 psig

Sodium Chloride -----	10 ppm or less
Soluble Phosphate (following 2.6 Na-PO <sub>4</sub> molar ratio) -----	2 to 4 ppm as PO <sub>4</sub>
Silica, SiO <sub>2</sub> -----	0.5 ppm or less
Total Solids -----	100 ppm or less
pH -----	8.9 - 9.25 corresponding to 2 - 4 ppm PO <sub>4</sub>

Feedwater

pH -----	8.6 to 8.9
Dissolved Oxygen -----	0.007 ppm or less
Copper, Cu -----	0.01 ppm or less
Iron, Fe -----	0.02 ppm or less
Hydrazine, N <sub>2</sub> H <sub>4</sub> -----	0.01 - 0.07 ppm
Dardness as CaCO <sub>3</sub> -----	0



G-2, S-1, S-2, M-1Main Steam and Condensate (Siemens)

	<u>Start-up</u>	<u>Normal</u>
Silica, SiO <sub>2</sub> -----	50 ppb or less	20 ppb or less
Total Iron, Fe -----	50 ppb or less	20 ppb or less
Total Copper, Cu -----	10 ppb or less	3 ppb or less
Sodium & Potassium, Na <sup>+</sup> and K <sup>+</sup> -----	20 ppb or less	10 ppb or less
Conductivity (after passing thru cation resin) -----	0.5 micro S/cm equal or less	0.3 micro S/cm equal or less

Economizer Inlet (Hitachi) Normal Operation

pH -----	9.2 - 9.4
Dissolved Oxygen -----	7 ppb (max.)
Silica, SiO <sub>2</sub> -----	20 ppb (max.)
Hydrazine, N <sub>2</sub> H <sub>4</sub> -----	10 - 70 ppb
Total Dissolved Solids -----	50 ppb
Copper, Cu -----	2 ppb
Total Iron, Fe -----	10 ppb
Conductivity -----	0.3 micro S/cm (after passing thru cation resin)

M-2Feedwater

Dissolved Oxygen ----- Preferably zero, and not  
over 0.007 ppm

Hydrogen Ion Value (pH)  
(85°C) ----- Between 8.6 and 8.9 for  
high pressure feedwater  
heater constructed from  
copper alloy tubes, and  
between 9.2 and 9.4 for  
feedwater heater const-  
ructed from steel  
tubes.

Hardness as  $\text{CaCO}_3$  ----- Zero

Total Copper, Cu ----- 0.005 ppm or less

Total Iron, Fe ----- 0.01 ppm or less

Oil ----- Preferably zero

Hydrazine ( $\text{N}_2\text{H}_4$ ) ----- Between 0.01 and 0.03 ppm

Cation Conductivity (25°C) ----- less than 0.3 micro S/cm

Boiler Water

Hydrogen Ion Value (pH) ----- Between 9.5 and 10  
Total Solids ----- Less than 20 ppm  
Phosphoric Acid ( $\text{POa}_3$ ) ----- Between 1 and 3 ppm  
Silica ( $\text{SiO}_2$ ) ----- Preferably less than  
0.3 ppm

### 3) Management

#### a. Result of Survey

Daily laboratory analysis and performance reports about chemical equipment such as demineralizer, ammonex are checked by the chief of shift and submitted to the superintendent. However, it is observed that copies of these reports are not submitted to the Plant Manager, except only in cases of abnormal phenomena. Statistical analysis of the water analyses data, the arrangement and resolution about the water quality log or special test, etc., is scarcely performed which is mainly due to manpower deficiency. Monthly and yearly reports about water quality analysis and chemical consumption are not also submitted. It is also observed that chemistry control is not religiously maintained because of too much paper work being done.

#### b. Recommendation

As the technique pertaining thermal power generating unit advances quickly, chemical management becomes very important. This is also true to geothermal power plants which are already operational and to the nuclear power plant that would soon follow.

Therefore, a central laboratory should be established as the managing organization about chemical works of the power station, in order to do planning and make recommendation for the improvement of chemical techniques and training.

For an effective planning, an initial manpower of 5 to 7 staff members which will take charge of the enumerated tasks below should be established:

- Collection and review of water quality at each unit
- Monthly and yearly reports
- Chemical inspection and material testing during annual outage
- Advices on chemical control pertaining to unit outage
- Presence of trained personnel during chemical cleaning
- Solution of common problems of the chemical section
- Training, observation or education
- Introduction of new technique about chemical treatment (literature, equipment and analysis method)
- Thorough examination of equipment related to chemistry

In the near future, once the central laboratory is operational, an overall manpower of around 20 members should be utilized under the said laboratory to cope with problems which would arise in thermal, geothermal and nuclear power plants. The task includes special water analysis, material corrosion control and analysis, fuel and environmental pollution.

Required instruments for future central laboratory are as follows:

- Electron probe X-ray micro analyzer
- Inductively coupled argon plasma emission spectrophotometer (multi-channel type)
- Ge (Int\*) gamma-ray spectrometer
- Scanning electron microscope
- Fluorescent X-ray analyzer
- X-ray diffractometer
- Atomic absorption spectrophotometer
- Gas chromatography
- Carbon-nitrogen-hydrogen analyzer
- Total nitrogen analyzer
- Ion chromatography (dionex)
- Sulfur analyzer
- Metal microscope

\*Int: Intrinsic (or pure)

The above instruments/equipment are installed at Kyushu Electric Power Research Laboratory.

4) Demineralizera. Specification of Demineralizer

## (a) Raw Water Quality of Demineralizer

Item	Raw Water	Treated Water
Ca <sup>++</sup>	22 ppm as CaCO <sub>3</sub>	
Mg <sup>++</sup>	22 "	
Na <sup>++</sup>	376 "	
Total Cation	420 "	0.1 ppm as CaCO <sub>3</sub>
HCO <sub>3</sub> <sup>-</sup>	307 ppm as CaCO <sub>3</sub>	
Cl <sup>-</sup>	107 "	
SO <sub>4</sub> <sup>--</sup>	6 "	
NO <sub>3</sub> <sup>-</sup>	0 "	
CO <sub>2</sub>	0 "	
SiO <sub>2</sub>	86 "	0.01 ppm as SiO <sub>2</sub>
Total Anion	506 "	0.1 ppm as CaCO <sub>3</sub>
Fe	0.125 ppm as Fe	0.01 ppm as Fe
pH	8.3	7.0

## (b) Raw Water Quality of RO Unit (Tested by ESCO)

Ca <sup>++</sup>	50 ppm	HCO <sub>3</sub> <sup>-</sup>	383 ppm
Mg <sup>++</sup>	25 ppm	Cl <sup>-</sup>	342 ppm
Na <sup>+</sup>	320 ppm	SO <sub>4</sub> <sup>--</sup>	14 ppm
Total Cation		NO <sub>3</sub> <sup>-</sup>	0.6 ppm
pH	7.8	SiO <sub>2</sub>	65 ppm
Fe	0.24 ppm	Total Anion	
Turb.	Nil		
TDS	1198 ppm		

NOTE: Result of raw water quality test submitted by ESCO is inadequate so that total cation and anion cannot be evaluated.

## (c) Designated Values

<u>Location</u>	Gardner	Snyder	Malaya
<u>Manufacturer</u>	Graver	Permutit	Permutit
<u>Cation Exchanger</u>			
Number	3 Units	2 Units	2 Units
Column Size	54" x 13'-6" (1-372mm $\phi$ x 4115mm <sup>H</sup> )	72" x 11' (1829mm $\phi$ x 3353mm <sup>H</sup> )	same
Pressure	100 psi (7kg/cm <sup>2</sup> )	100 psi (7kg/cm <sup>2</sup> )	same
Resin	Re-3 108ft <sup>3</sup>	IR-120 172ft <sup>3</sup>	same
<u>Regenerant</u>			
Up-Flow	66°Be H <sub>2</sub> SO <sub>4</sub> (8lbs/ft <sup>3</sup> )	93% H <sub>2</sub> SO <sub>4</sub> (71bs/ft <sup>3</sup> )	same
Down-Flow	66°Be H <sub>2</sub> SO <sub>4</sub> (10lbs/ft <sup>3</sup> )	93% H <sub>2</sub> SO <sub>4</sub> (112g/L-R)	same
Flow Rate	50 gpm (11.4 m <sup>3</sup> /H)	100 gpm (22.7 m <sup>3</sup> /H)	same
B.T. Capacity	24.2 Kgrain/ft <sup>3</sup> (55.3 g/l-R)	19.6 Kgrain/ft <sup>3</sup> (44.8 g/l-R)	same
Total Capacity	90500 gal (286 m <sup>3</sup> )	136400 gal (516.3 m <sup>3</sup> )	same
<u>Degasifier</u>			
Number	1 Unit	1 Unit	1 Unit same



Anion Exchanger

Number	3 Units	3 Units	3 Units
			same
Column Size	48" x 15'-6" (1219mm $\phi$ x 4724mm <sup>H</sup> )	60" x 9' (1524mm $\phi$ x 2743mm <sup>H</sup> )	same
Pressure	100 psi (7 kg/cm <sup>2</sup> )	100 psi (7 kg/cm <sup>2</sup> )	same
Resin	AE-61 96 ft <sup>3</sup> (2718 lit)	IRA-402 102 ft <sup>3</sup> (2888 lit)	same
Regenerant	100% NaOH 101b/ft <sup>3</sup>	100% NaOH 61b/ft <sup>3</sup>	same
Flow Rate	50 gpm (11.4 m <sup>3</sup> /H)	100 gpm (22.7 m <sup>3</sup> /H)	same
B.T. Capacity	10.7 Kgrain/ft <sup>3</sup> (24.4 g/l-R0)	13.8 Kgrain/ft <sup>3</sup> (31.5 g/l-R)	same
Total Capacity	71000 gal (269 m <sup>3</sup> )	125600 gal (475.4 m <sup>3</sup> )	same

Mixed Bed Polisher

Number	2 Units	2 Units	2 Units
Column Size	36" x 8' (914mm $\phi$ x 2438mm <sup>H</sup> )	42" x 9' (1067mm $\phi$ x 2743mm <sup>H</sup> )	same
Pressure	275 psi (19.3 kg/cm <sup>2</sup> )		
Resin	Anion (AE-61) 11 ft <sup>3</sup> (311 lit)	Anion (IRA-402) 24 ft <sup>3</sup> (679 lit)	same
	Cation (RE-6) 17 ft <sup>3</sup> (481 lit)	Cation (IR-120) 28 ft <sup>3</sup> (792.8 lit)	same

Flow Rate	76 gpm (17.3 m <sup>3</sup> /H)	100 gpm (22.7 m <sup>3</sup> /H)	same same
Total Capacity	1000000 gal (3785 m <sup>3</sup> )	514000 gal (1946 m <sup>3</sup> )	same same
Regenerant	100% NaOH 24 lb/ft <sup>3</sup> (384 g/l-R)	100% NaOH 9 lb/ft <sup>3</sup> (144.2 g/l-R)	same same
	66% H <sub>2</sub> SO <sub>4</sub> 8 lb/ft <sup>3</sup>	(93% H <sub>2</sub> SO <sub>4</sub> same 8 lb/ft <sup>3</sup> )	

Effluent	Total Cation	0.1 ppm as CaCO <sub>3</sub>
	Total Anion	0.1
	SiO <sub>2</sub>	0.01 ppm as SiO <sub>2</sub>
	Fe	0.01 ppm as Fe
	pH	7.0
	Conductivity	0.5 micro S/cm

Note: At Gardner/Snyder Thermal Station, Craver type

Demineralizer treats directly filtered water with a conductivity of 820 micro S/cm and permutit Type of Demineralizer treats blended water with a conductivity of 390 micro S/cm. Blended water comes from RO unit effluent with a conductivity of 170 micro S/cm and deepwell water with a conductivity of 1300 micro S/cm.

b. Result of Survey

(a) Instrumentation of Demineralizers

The instrumentation which are mounted on the control panel of demineralizer are as follows;

i. Gardner Demineralizer (Graver)

## Instruments for Monitoring

Conductivity Meter &amp; Recorder

(Leeds &amp; Northrup) X

pH Meter &amp; Recorder (Leeds &amp; Northrup) X

Flow Meter &amp; Recorder (Foxboro) X

## Control System for Automatic Operation

Stepping Programmer X

## Alarm Unit

Alarm Units X

ii. Snyder Demineralizer (Permutit)

## Instruments for Monitoring

Conductivity Meter &amp; Recorder (Beckman) X

Flow Meter &amp; Recorder (Taylor)

Flow Counter X

## Control System for Automatic Operation

Stepping Programmer X

## Alarm Unit

Alarm Units X

iii. Malaya Demineralizer (Permutit)

## Instruments for Monitoring

Conductivity Meter &amp; Recorder (Beckman) X

Flow Meter &amp; Recorder (Foxboro)

Flow Counter X

## Control System for Automatic Operation

Stepping Programmer X

## Alarm Unit

Alarm Units X

\*Legend            X - - - - - Out of Order  
                     - - - - - Working but necessary  
   to calibrate  
                     0 - - - - - Available

As mentioned above, the monitoring instruments and control system for automatic operation are mostly damaged and all equipments are operated manually. Faulty operations may occur as a result.



In Japan, the demineralizer is usually operated as follows;

Anion Exchanger Outlet

Conductivity            Less than 10 micro S/cm

Silica                    Less than 0.1 ppm as SiO<sub>2</sub>

Mixed Bed Polisher

Conductivity            Less than 0.5 micro S/cm

Silica                    Less than 0.02 ppm as SiO<sub>2</sub>

However, treated water conductivity of Graver demineralizer becomes sometimes higher than the above values.

It is caused by no monitoring of conductivity at anion exchanger and mixed bed polisher outlet, Exhausted points are checked only by Free Mineral Acidity (FMA) (Cation exchanger), SiO<sub>2</sub> (Anion exchanger), SiO<sub>2</sub> and P-alkalinity (Mixed bed polisher) by manual analysis.

(c) Regeneration

Regeneration of demineralizers are carried out as follows:

	<u>Cation Exchanger</u>	<u>Anion Exchanger</u>	<u>Mixed Bed Polisher</u>
Gardner (Graver)	① Down Flow	④ Down Flow	⑦
	② Up Flow	⑤ Down Flow	⑧
	③ Down Flow	⑥ Down Flow	Ordinary
Snyder (Permutit)	① Down Flow	① Down Flow	Method
	② Down Flow	② Down Flow	②
Malaya (Permutit)	① Down Flow	① Down Flow	① Column (No)
	② Down Flow	② Down Flow	

\* Refer to attached operation process; Table 5C-21, 22, 23, 24, 25 and 26.

(d) Regenerants Quantity

Regenerants quantity is checked by dilution flow rate and specific gravity of diluted solution.

Table 5C-19 FILTERED WATER ANALYSIS RECORD

BY

Item#	H-Alk. (ppm as CaCO <sub>3</sub> )	Cl (ppm as NaCl)	SO <sub>4</sub> (ppm as Na <sub>2</sub> SO <sub>4</sub> )	T-Hard (ppm as CaCO <sub>3</sub> )	Ca (ppm as CaCO <sub>3</sub> )	SiO <sub>2</sub> (ppm as SiO <sub>2</sub> )	Conduct (Micro S/cm)	FMA (ppm as CaCO <sub>3</sub> )	
Aug. 1	223	185	9	35	18	66	979	180	G/S TS
2	285	183	16	30	20	68	894	180	
3	340	184	14	40	24	70	970	180	
4	310	170	20	46	20	90	990	180	
5	280	174	12	42	26	65	940	180	
6	290	160	9	48	25	83	990	180	
7	308	185	12	38	24	68	968	180	
8	320	192	12	44	20	72	980	180	
9	300	176	12	40	24	84	974	180	
10	290	184	10	40	16	54	940	190	
11	340	184	12	46	20	65	970	180	
12	320	190	12	46	20	78	-	180	
13	309	188	14	40	28	72	972	180	
14	370	190	10	44	20	60	980	180	
15	260	162	10	34	17	55	900	180	
16	290	170	15	38	20	72	(820)	180	
17	270	182	10	42	24	62	(840)	185	
18	-	-	-	-	-	-	-	-	
19	300	116	12	34	20	42	(800)	190	
19						#4 (1300)		RO Unit Inlet	
19						(170)		RO Unit Outlet	
19						(390)		Permutit Inlet	
Aug. 27 <sup>#1</sup>	138	44	21.9	102	66	80	PH(7.3)	Fe(0.41)	MALAYA
27 <sup>#2</sup>	136	46	21.9	102	58	82.5	PH(7.65)	Fe(0.41)	
27 <sup>#3</sup>	56	24	17.5	64	54	97.5	PH(7.45)	Fe(0.46)	
Aug. City	48 - 43	13 - 15		41 - 46	28 - 32	10.8 - 16	PH(7.3)		TEGEN
River	82 - 76	620 - 580		120 - 118	75 - 80	6.7 - 6.0	PH(7.5)		





Table 5C-21 OPERATION PROCESS OF PRIMARY DEMINERALIZER (GRAVER) GSTP

Cation Exchanger				Anion Exchanger					
Process	Flow Rate	Time	Remarks	Process	Flow Rate	Time	Remarks		
Service	50 gpm			Service	50 gpm				
Back Wash	150 gpm	10 min.		Back Wash	42 gpm	10 min.			
Clouse	-	5 min.		Clouse					
1-st Introduction	Method-1 (Up Flow)		Method-2 (Down Flow)		Caustic Introduction	29.7 gpm + 1.75 gpm (NaOH)	87 min.		
	2 1/2% Acid	45 gpm + 0.7 gpm H <sub>2</sub> SO <sub>4</sub>	31 min	4% Acid				39.2 gpm + 1.0 gpm H <sub>2</sub> SO <sub>4</sub>	29 min
	5% Acid	45 gpm + 1.4 gpm H <sub>2</sub> SO <sub>4</sub>	22.5 min	8% Acid				39.2 gpm + 2.0 gpm H <sub>2</sub> SO <sub>4</sub>	21 min.
	Displacement	45 gpm	10 min	39.2 gpm				125 min.	1.3 m
Fast Rinse	92 gpm	47 min		Displacement	29.7 gpm Heating 110-120°F	23.5 min	2.6 m		
Service	73 gpm			Fast Rinse	73 gpm	54.5 min	15 m		
Remarks				Remarks					

Table 5C-22 MIXED BED POLISHER (GRAVER) GARDNER

Operation Process, Specified Flow Rate, Time, Regenerants

Process	Flow Rate	Time	Remarks
Service	75 gpm		
Sub-Service Wash	21 gpm	10 min.	
Back Wash	25 gpm	10 min.	
Settling	-		
Acid Introduction Acid Displace & Caustic Intro	11.4 gpm +0.355 gpm(H <sub>2</sub> SO <sub>4</sub> ) 5.3 gpm +0.30 gpm(NaOH) 11.4 gpm	25 min.	Heating Temp 110-120°F
Acid Displace Caustic Intro -duction	11.4 gpm 5.3 gpm +0.3 gpm(NaOH)	69 min.	
Drain Unit	-	11.4 min.	
Raise Bed	25 gpm		
Air & Water			
Air Mixing			
Back Flush & Settle & Air			
Slow Fill	5.3 gpm	8 min.	
Fast Fill	41 gpm	3.5 min.	
Through Fill	41 gpm		

Table 5C-23 OPERATION PROCESS OF DEMINERALIZER (PERMUTIT) SNYDER

Cation Exchanger				Anion Exchanger			
Process	Flow Rate (gpm)	Time (min)	Remark	Process	Flow Rate (gpm)	Time (min)	Remarks
Service	100			Service	100		
Back Wash	140	10		Back Wash	40	20	
Settle		5					
1.5% Acid Introduction	250 + 2.15(H <sub>2</sub> SO <sub>4</sub> )	11		4% Caustic Introduction	28 + 1.6	60	Heating Temp 120°F
4% Acid Introduction	90 + 2.15(H <sub>2</sub> SO <sub>4</sub> )	11					
6% Acid Introduction	60 + 2.15(H <sub>2</sub> SO <sub>4</sub> )	16					
Slow Rinse	60	14	3.1 m <sup>3</sup>				
Fast Rinse	250	24	22.7 m <sup>3</sup>	Slow Rinse	28	22	2.3 m <sup>3</sup>
				Fast Rinse	120	68	30.8 m <sup>3</sup>
				40 Micro IS/cm			

Table 5C-24 SNYDER THERMAL STATION  
 OPERATION PROCESS OF PRIMARY  
 DEMINERALIZER (PERMUTIT)

Process	Flow Rate(gpm)	Time(min)	Remarks
Service	100		
Back Wash	33	10	
Settle	—	10	
Heating Anion Resin	10 8.5	15	Heating Temp 120°F
Caustic Introduction & Acid Introduction	10 + 0.6 8.5 + 0.25	60	Heating Temp 120°F
Slow Rinse	10 8.5	15	
Anion Partial Rinse	48		
Cation Partial Rinse	55	15	
Drain	—	15	
Air Mix	150 cfm	20	Air Press 10 psi
Air Mix & Drain	150 cfm	10	
Refill	80	5	
Final Rinse	80	13	
Conductivity Setting			0.5 Micro S/cm

Table 5C-25 MALAYA THERMAL STATION  
OPERATION PROCESS OF PRIMARY DEMINERALIZER (PERMUTIT)

Cation Exchanger				Anion Exchanger			
Process	Flow Rate	Time	Remarks	Process	Flow Rate	Time	Remarks
Service	100 gpm (200 gpm) Max.			Service	100 gpm (200 gpm) Max.		
Back Wash	115 gpm	20 min.		Back Wash	69 gpm	30 min.	
Settle				Settle			
1-st (1% Acid) Introduction	217 gpm + H <sub>2</sub> SO <sub>4</sub> (1%) SG 1.015	20 min.		Caustic (4% NaOH) Introduction	17 gpm + NaOH (4%) SG 1.04	60 min.	
2-nd (4% Acid) Introduction	79 gpm + H <sub>2</sub> SO <sub>4</sub> (4%) SG 1.025	20 min.		Heating Temp. 110-120°F			
3-rd (6% Acid) Introduction	52 gpm + H <sub>2</sub> SO <sub>4</sub> (6%) SG 1.04	20 min.					
Slow Rinse	52 gpm	22 min.					
Rinse	222 gpm		End point 40 TMA 45	Slow Rinse	17 gpm	30 min.	19.3 m <sup>3</sup>
Service	102 gpm			Rinse	102 gpm		23 m <sup>3</sup> End Point P-Alkali Less than 10 ppm
							5102 less than 0.02 ppm

Table 5C-26 MIXED BED POLISHER (PERMUTIT)  
( SNYDER & MALAYA )

Operation Process, Specified Flow Rate, Time and Regenerants

Process	Flow Rate	Time	Remarks
Service	100 gpm		
Back Wash	43 gpm	10min.	
Settling	-	5min.	
Anion Heating	9.7 gpm (Temp. 110-120°F)	15min.	Heating Temp 110-120°F
Regenerant Introduction	Anion (5%NaOH) S.G. 1.05 9.7 gpm + NaOH Cation (5%H <sub>2</sub> SO <sub>4</sub> ) S.G. 1.05 7.1 gpm + H <sub>2</sub> SO <sub>4</sub>	60min.	Heating Temp 110-120°F
Displacement	Anion 9.7 gpm Cation 7.1 gpm	15min.	Heating Temp 110-120°F
Regenerant Rinse	Anion 39 gpm Cation 50 gpm	15 min.	
Final Rinse	69 gpm		Conductivity Less than 0.5 Micro Silica Less than 0.02 ppm

Fig. 5C-9 DEMINERALIZERS SCHEMATIC DIAGRAM

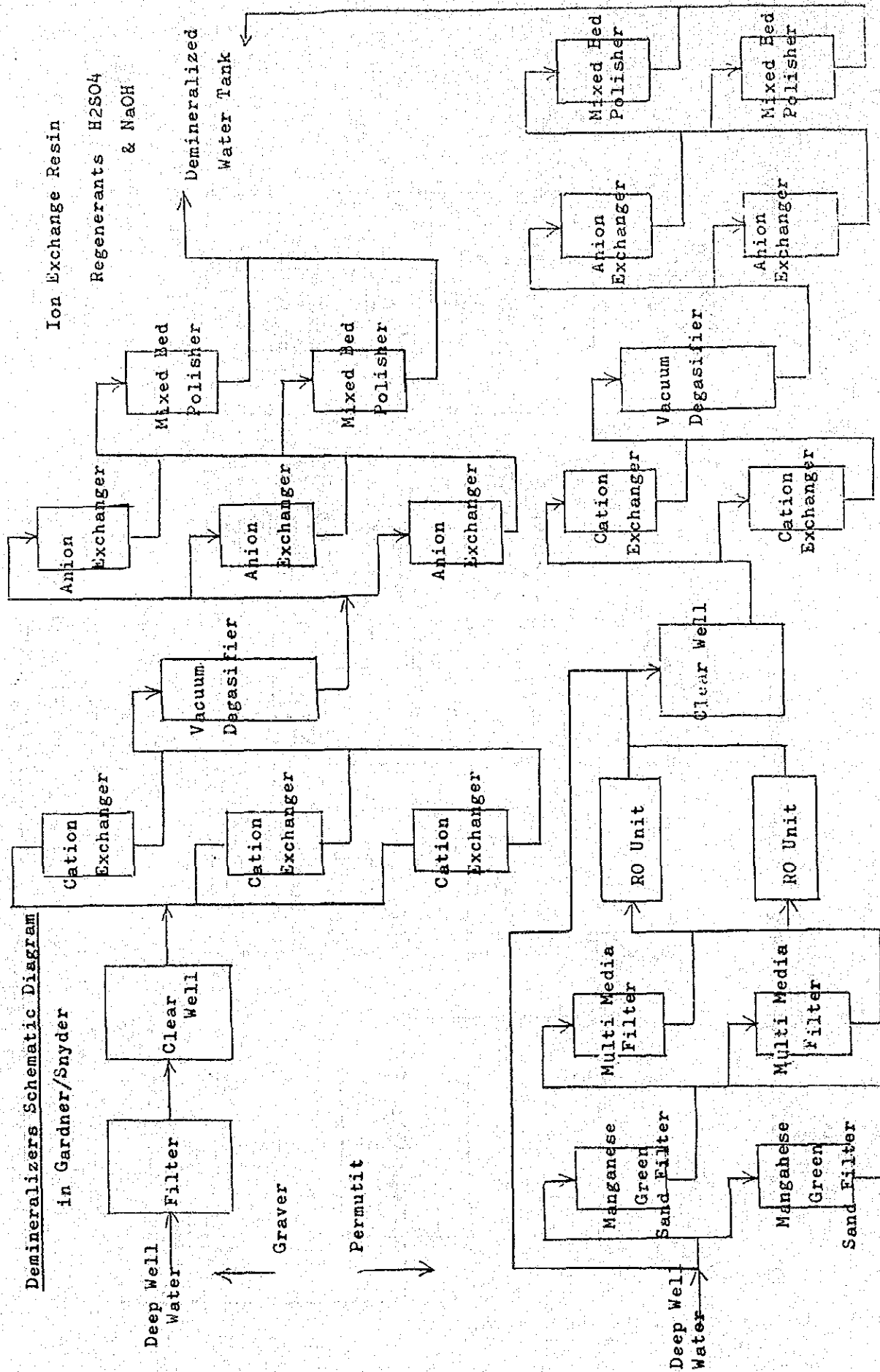




Fig. 5C-10 DEMINERALIZERS SCHEMATIC DIAGRAM (PERMUTIT)

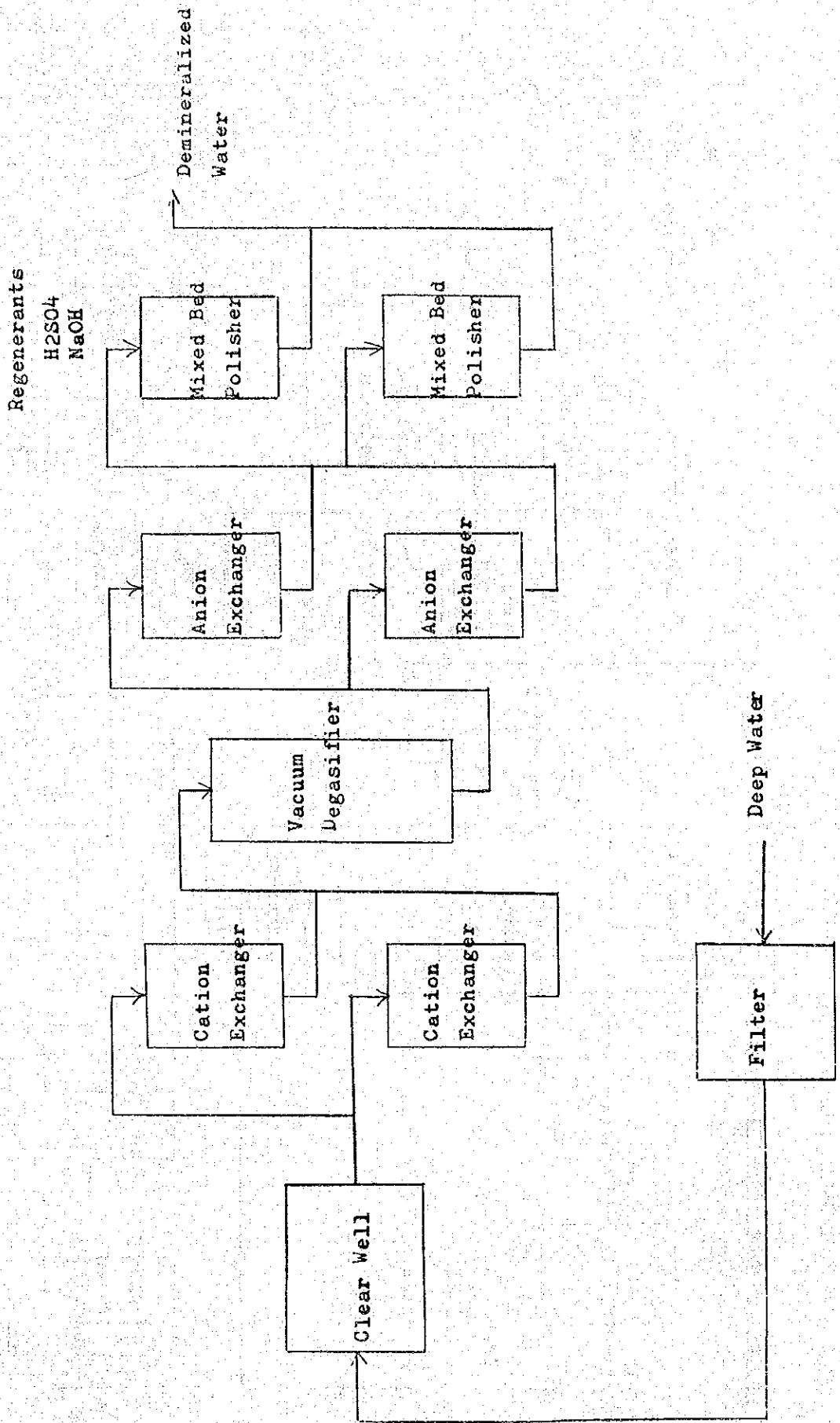


Fig. 5C-11 REVERSE OSMOSIS (RO) UNIT

Manufacturer; Envirogenics System Co.,  
 Location; Snyder Thermal Station

Recovery % 50%

Media; Anthracite (Depth 6")  
 (154mm)

RO Module 2 Sets

Fine Sand (Depth 18")  
 (457mm)

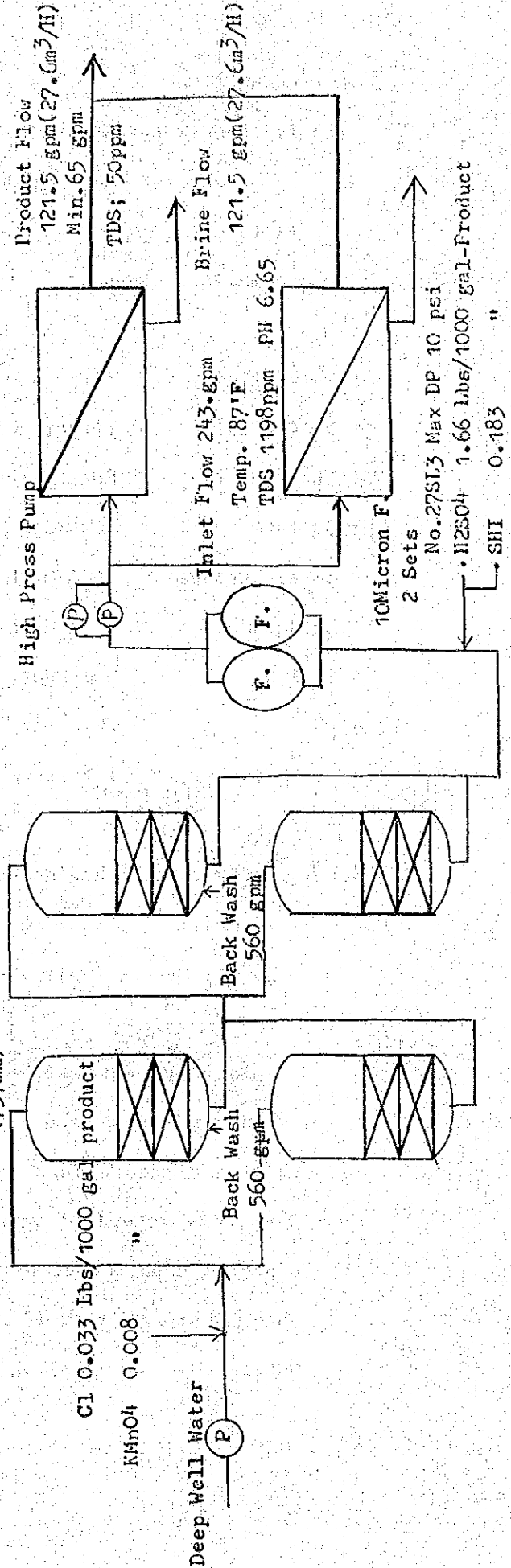
1-st 8 Vessels (4 Elements/Vessel)

Media; Anthracite (Depth 12")  
 (305mm) Multi-media Filter

2-nd 5 Vessels (3 Elements/Vessel)

Manganese Green Sand  
 (Depth 18")  
 (757mm)

Max. Press 420 psi



c. Recommendations

## (a) Filtered Water Analysis Method

According to NAPOCOR thermal station site, filtered water (raw water) is analyzed based on the following methods.

	Method	Unit
* P-Alkalinity	Titrate with N/50 $H_2SO_4$	ppm as $CaCO_3$
* M-Alkalinity	Titrate with N/50 $H_2SO_4$	ppm as $CaCO_3$
* Chloride	Morr Method	ppm as NaCl
* Sulfate	Turbidimetric Method	ppm as $Na_2SO_4$
* Total Hardness	EDTA Method	ppm as $CaCO_3$
* Ca Hardness	EDTA Method	ppm as $CaCO_3$
* Silica	Molybdate Blue Method	ppm as $SiO_2$
* pH	pH Meter	
* Free Mineral Acidity	Titrate with N/50 NaOH	PPM as $CaCO_3$

Note: Refer to attached sheets (Filtered water analysis record.)

No. - - - - - Table 5C-19 and 20.

In above method of analysis items, chloride and sulfate are expressed as NaCl and  $Na_2SO_4$  respectively on this record. This is not suitable because it is thru this record of analysis that we calculate the expected capacity of primary demineralizers by knowing the total cation and total anion of the raw water.

This is to say, the primary demineralizers capacity can be known by the following formula.

\* Expected capacity of primary demineralizer\*

$$A = \frac{B \times C}{D} \times E - F$$

A ;	Expected capacity of demineralizer	(m <sup>3</sup> /cycle)
B ;	Break through capacity of resins	(g as CaCO <sub>3</sub> /1-Resin)
C ;	Resin Volume	(liter)
D ;	Total cation/Total anion	(ppm as CaCO <sub>3</sub> )
E ;	Resin capacity drop %	(1 - %/100)
F ;	Needed water volume for regeneration	(m <sup>3</sup> )

(Displacement & Rinse)

The analysis items and methods of filtered water in Japan are shown below;

	<u>Method-1</u>	<u>Method-2</u>	<u>Method-3</u>
	(JIS-0101)		
Total Hardness(T-H)	Titration with EDTA	Titration with EDTA	
Calcium (Ca)	Titration with EDTA		
Magnesium (Mg)	(T-H) - Ca		
Sodium (Na)	Atomic Absorption	(T-C) - (T-H)	
Total Cation (T-C)	Ca + Mg + Na	M-Alkali + FMA	Conductivity/2
Bicarbonate (HCO <sub>3</sub> )	Titration	Titration	
(M-alkalinity)	with N/50 H <sub>2</sub> SO <sub>4</sub>	with N/50 H <sub>2</sub> SO <sub>4</sub>	
Chloride (Cl)	Morr Method	Free Mineral Acidity (FMA)	
		Titration with N/50 NaOH	
Sulfate (SO <sub>4</sub> )	Turbidimetric Method		
Nitrate (NO <sub>3</sub> )			

Free carbon Dioxide	From graph of	
(CO <sub>2</sub> )	relation of pH	and M-alkalinity
Silica (SiO <sub>2</sub> )	Molybdate Yellow	Molybdate Yellow
Total Anion	HCO <sub>3</sub> + Cl + SO <sub>4</sub>	M-Alkali + FMA
	NO <sub>3</sub> + CO <sub>2</sub> + SiO <sub>2</sub>	CO <sub>2</sub> + SiO <sub>2</sub>
pH	pH meter	pH
Iron (Fe)	Orth-phenanthroline	-
Conductivity	Conductivity	Conductivity meter
(Micro S/cm)		
Turbidity	Spectrophotometer	
Others		
COD	Titration (KMnO <sub>5</sub> )	
TOC	TOC meter	
Frequency of	once a week	once a day
analysis		-

Regarding raw water analysis, JICA team recommends that it should be performed periodically as follows:

Filtered Water (Method-1) Once a week

Filtered Water (Method-2) Once a day

SiO<sub>2</sub> of Anion and Mixed Bed Polisher Outlet

Every 3 hours

In the filtered or raw water supply analysis, expression of results should be unified as  $\text{CaCO}_3$  or its equivalent for easy calculation.

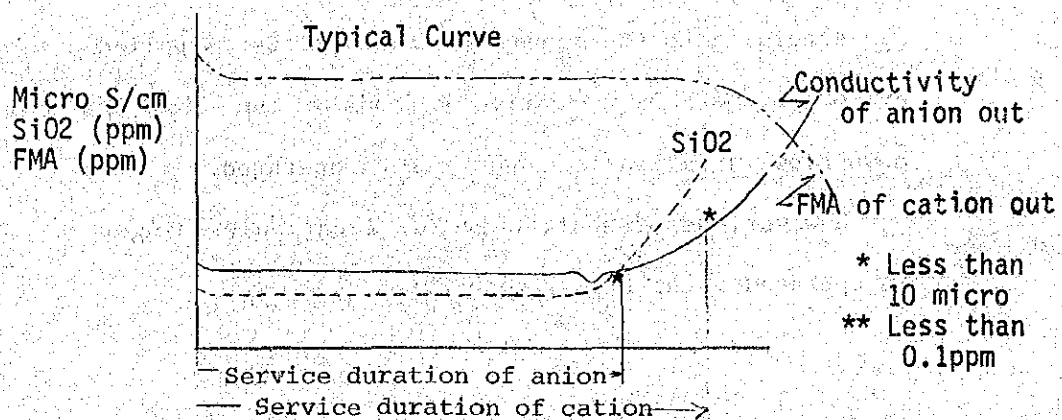
Note: On the attached record of analysis (Table 5C-20), chloride values are higher than FMA (Free Mineral Acidity). Further evaluation of this results shows the probable cause of the big difference in value may be due to the reagent concentrations.

(b) Operation Procedure of Demineralizer

According to NAPOCOR procedure, the exhausting points of cation exchanger and anion exchanger are respectively decided with free mineral acidity and silica value but not on the conductivity value.

However, the conductivity of deionized water is the most important factor when we check the demineralized water quality.

In primary demineralizer, the typical curves of conductivity,  $\text{SiO}_2$  and FMA (Free Mineral Acidity) are shown below.



And when NaOH or NaCl leak at outlet of ion exchanger, the conductivity will be as follows;

CaCO <sub>3</sub>	NaOH	NaCl	HCl
1 ppm	5 micro S/cm	2.5 micro S/cm	8.5 micro S/cm
5 ppm	25 "	13 "	43 "
10 ppm	50 "	25 "	85 "
15 ppm	75 "	38 "	150 "
20 ppm	100 "	40 "	170 "

FMA at the outlet of cation exchanger correspond to NaCl. Conductivity measure is higher in sensitivity than the result of FMA analysis. Monitor continuously by conductivity.

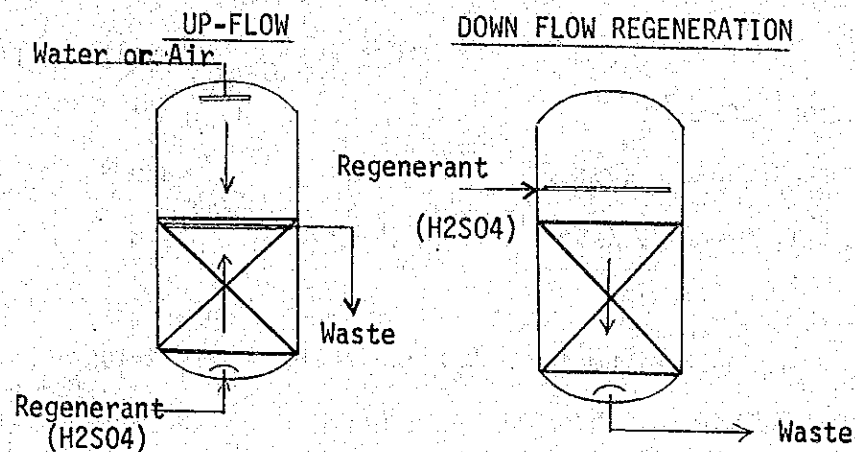
Therefore, JICA team recommends, that the exhausting points of demineralizer should be known by conductivity and conductivity meters which are attached on the control panel should be repaired or replaced immediately. Regarding mixed bed polisher, it is also the same as mentioned above.

(c) Regeneration Method

According to the manual of demineralizer supplied by Graver both regeneration methods of up flow or down flow in cation exchanger can be operated.

However, at present, only No. 2 cation exchanger is operated in up flow regeneration.

When concentration of free mineral acidity ( $\text{Cl}^-$ ,  $\text{SO}_4^-$ ,  $\text{NO}_3^-$ , etc.) in filtered water increase, it is better to employ up flow regeneration in order to keep higher water quality efficient. Also higher capacity will be produced with smaller volume of regenerants.



Therefore, JICA team recommends that up-flow regeneration method should be employed in Gardner (Graver) demineralizer to obtain higher quality of water effluent.

In up-flow regeneration, the most important thing is to avoid resin moving during acid introduction and also of displacement so that water or air is flowed from column top. Regeneration waste collector is installed in upper part of resin layer.

(d) Caustic Introduction & Displacement Temperature

The maximum operating temperature of anion exchange resin in R-OH type is  $60^{\circ}\text{C}$ . "In case of NAPOCOR, it is between  $110^{\circ}\text{F}$  ( $43^{\circ}\text{C}$ ) -  $120^{\circ}\text{F}$  ( $48^{\circ}\text{C}$ )"



The heating temperature should be controlled at  $53 \pm 3^\circ\text{C}$  in order to remove effectively  $\text{SiO}_2$  absorbed in resin layer.

(e) Expected Capacity of Demineralizer

In primary demineralizer, the expected capacity are as follows;

	Gardner (Graver)	Snyder (permutit)	Malaya (permutit)
<u>CATION EXCHANGER</u>			
Resin Volume (liter)	3058	4870	4870
B.T. Capacity (gas ( $\text{CaCO}_3$ /l-R)	55.3	44.8	44.8
Total Cation(ppm as $\text{CaCO}_3$ )	$820/2=410$	$390/2=195$	$450/2=225$
Resin Capacity Drop %	19/100	19/100	19/100
Regene. Water ( $\text{m}^3$ )	18	26	46
Expected Capacity ( $\text{m}^3$ /cycle)	316	880	739
<u>ANION EXCHANGER</u>			
Resin Volume (liter)	2718	2888	2888
B.T. Capacity (gas $\text{CaCO}_3$ /l-R)	24.4	31.5	31.5
Total Anion(ppm as $\text{CaCO}_3$ )	257	97	192
FMA (ppm as $\text{CaCO}_3$ )	180	70	110
$\text{SiO}_2$ (ppm as $\text{CaO}_3$ )	67	17	72
$\text{CO}_2$ (ppm as $\text{CaCO}_3$ )	10	10	10
Resin Capacity Drop %	14/100	14/100	14/100
Regene. Water ( $\text{m}^3$ )	20	33	25
Expected Capacity ( $\text{m}^3$ /cycle)	204	774	382