### REPUBLIC OF COLOMBIA

# REPORT ON GEOLOGICAL SURVEY OF PIEDRANCHA AREA

PHASE II

LIBRARY

MARCH 1983

JAPAN INTERNATIONAL COOPERATION AGENCY
METAL MINING AGENCY OF JAPAN

705 66.1 MPN 13613

### **PREFACE**

In response to the requirements of the Government of the Republic of Colombia, the Japanese Government has decided to perform collaborative mineral exploration in Piedrancha area located in the southwestern part of the country and has entrusted its performance to the Japan International Cooperation Agency, who has decided to entrust that performance to the Metal Mining Agency of Japan because the subjects of this investigation belongs to a special field of the geological and mineral resources survey.

This investigation was started in 1980 as the first phase. For the third phase plan, the Metal Mining Agency of Japan organized an investigating mission of seven persons to dispatch it to the site from June 14, 1982 to December 12, 1982.

The investigation on the site was completed on schedule by the cooperation of agencies relative to the government of the Republic of Colombia, especially Instituto Nacional de Investigaciones Geologico-Mineras.

This report has collected and arranged the results of the investigation in the third phase to make a part of the final report.

Finally we express our heartiful thanks for the cooperation of the agencies relative to the Government of the Republic of Colombia, and also to the Ministry of Foreign Affairs, Ministry of International Trade and Industry, the Japanese Embassy in Colombia, and all personnel of the companies concerned in the performance of this investigation.

February, 1983

Keisuke Arita

President

Japan International Cooperation Agency

Masayuki Nishiic

Research Anita

Masayuki Nishiie President

Metal Mining Agency of Japan

### CONTENTS

		Page		
PREFACE				
LOCATION MAP				
ABSTRACT	***************************************	i		
INTRODUCTION	***************************************	1		
PARTICULARS				
I	GEOLOGICAL SURVEY.			
	GEOCHEMICAL EXPLORATION	I — 1		
II	DRILLING SURVEY	II 1		
APPENDICES .				
Geologic	al and Geochemical Data			
Drilling	; Data			

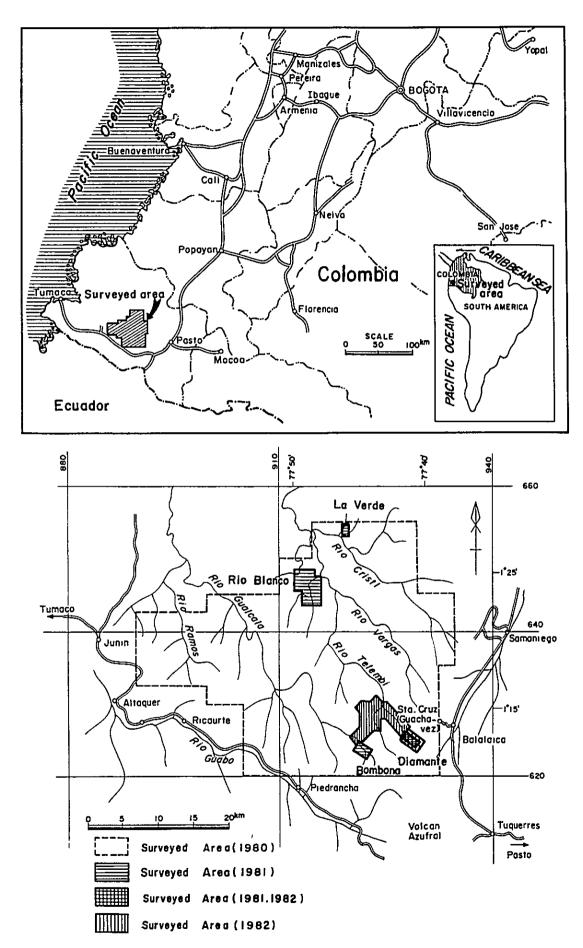


Fig. I-! Location Map of the Surveyed Area

### ABSTRACT

The third phase survey was carried out in and around the mining area of the Diamante Mine, which is auriferous polymetallic vein type ore deposit.

The main purpose of the survey was to obtain the information on the possibility of the existence of ore deposits, by clarifying the relation between the geological structure and the mineralization of the auriferous polymetallic ore deposits, and especially in the Diamante mining area, the survey was aimed to obtain some definite policy for further exploration of the possible ore deposits of the same type as those widely expected in this area, through the precise examination of the ore minerals, in addition to the comprehension of the actual continuity, ore grade and scale of the mineralized area, by carrying out diamond-drilling works in the mineralized zone where main vein type ore deposits are distributed in the Diamante mining area.

The contents of the survey works conducted were geological survey, geochemical exploration and diamond drilling. The geological survey was carried out by mapping along the main river and the main road, describing the details in the route map of the scale of 1/2,000. The total area mapped was about 24 km<sup>2</sup>. The geochemical exploration was carried out by collecting soil samples at the points every 25 meters along the survey lines, which was established with the interval of 125 to 250 meters across the line in the direction of the extension of main ore veins. The soil samples thus collected amounted to as many as 2,256. The diamond drilling was carried out in the mining area of the Diamante mine by locating the drill-holes with approximately 100 meters interval along the extension of the principal ore vein. The total length of the drill holes was 1,335.9 meters with 8 holes.

The principal items of information obtained through the surveys are as follows:

- (1) The rocks distributed in the surveyed area are composed mainly of green volcanic rocks and granodiorite of the Miocene Epoch of Tertiary Period, intruding the former. The intrusive rocks are thought to be a composite intrusive mass, showing two ages of 20 and 6 million years.
- (2) The mineralization is represented by the auriferous poly-metallic fissure-filling type ore deposits contained in the above-mentioned wall rocks.
- (3) The mineralized zones are oriented in the direction of NW-SE and are located in parallel three rows with approximate 3 kilometers interval.
- (4) Each of the mineralized zones has width of several hundred meters, in which several ore veins are found usually. The width of each ore vein is generally under 1 meter and the vein of the largest width ever found in the survey areas is the one in the central part of the main ore vein of the Diamante mining area, which is as wide as 5.6 meters. The lateral extension of the most enriched part of the mineralization is estimated to be 150 to 200 meters, and the depth of this part to be approximately 200 meters. The principal ore minerals composing the ore veins are arsenopyrite and sphalerite. The main gold-silver mineral is electrum. The crystallization of the electrum is thought to have been at the final stage of the crystallization of arsenopyrite. There is a tendency that the gold grade is high in such parts where arsenopyrites are found fairly concentrated.
- (5) As the results of the geochemical exploration conducted, 20 geochemical anomalies have been extracted. The areas represented by the anomalies include every indication of the mineralization represented by the known mineral outcrops and old working tunnels. The distribution of

the anomalies and that of the indications of mineralization are thought to have some intimate relation. Accordingly, it is expected that there would be some fair potentiality of ore deposits in the anomalies where no indication of mineralization has been found yet. Through the realization of this fact, it is thought that further exploration would be warranted in such areas represented by the geochemical anomalies even if no indications have been found at the moment.

According to the above-mentioned results of the surveys in this third phase, the following further investigations would be recommended to be carried out for future perspectives of the mineral exploration in this area.

- (1) Investigation by diamond drilling in the area including the lateral extension and the depth of the known ore deposits as Marina, Desquite, Bombona and so on.
- (2) Exploration of the depth of the very positive anomalies selected by the geochemical exploration conducted in this third phase by such method as trenching and diamond drilling.
- (3) Preliminary feasibility studies for the development of the main mineralized zone in the Diamante mining area, including the study of the minerals and the concentration tests.

## **INTRODUCTION**

### INTRODUCTION

### CONTENTS

	Pag	e
CHAPTER	1. PURPOSE AND OUTLINE OF THE SURVEYS	2
1-1	Outline of the Survey Works	2
1-2	Purpose of the Survey Works	3
CHAPTER	2. OUTLINE OF THE ACTUAL SURVEY WORKS	4
2-1	Area and Term of the Survey Works	4
2-2	Method of the Survey Works	6
2-3	Method of the Analysis	9
2-4	Organization and Members of the Survey Team	1 0

### CHAPTER 1. PURPOSE AND OUTLINE OF THE SURVEYS

### 1-1 Outline of the Survey Works

The main purpose of the survey works carried out in the first phase were the comprehension of the regional geological structure and the extraction of the favorable areas for the mineralization through the geochemical survey by collecting samples of stream sediment. As the results of the survey works five areas with indications of porphyry copper type mineralization associated with the acidic igneous rocks and two areas showing indications of auriferous mineralization have been extracted. Gold ore deposits were found to be divided into two types. The one is milky white quartz vein type and the other is polymetallic vein type abound with sulphide minerals. It has also been clarified that the latter has potentiality of mineralization at the depth, warranting further exploration.

The survey works in the second phase are composed of detailed geological survey accompanied with geochemical exploration for soil in the two favorable areas of La Verde and Rio Blanco selected from the potential areas with indications of porphyry copper type mineralization, in addition to detailed geological survey and geochemical exploration for the investigation of extension of the mineral outcrops in the areas of Diamante and Bombona, where auriferous polymetallic vein type ore deposits are distributed. Also diamond drilling works were carried out in the second phase program in the Diamante mining area.

As the results of these survey works, it has become evident that the mineralized zone is extended with fairly good grade in the area of the Diamante ore deposit as was expected, and that the area of northern extension of the mineralized zone in Bombona and the area including Paraiso area, northeast to it, are quite favorable for the emplacement of the

auriferous ore deposits, left for further exploration. Also a significant information has been obtained as for the soil geochemical exploration that this method is very useful for the extraction of the favorable areas with mineral indication, especially when zinc and arsenic are used for the indicative elements.

In the areas of La Verde and Rio Blanco, alteration zone showing zonal distribution of prophyry copper type and the possibility of emplacement of copper mineralization with the grade of some 0.2 to 0.5% were found through the surveys but no direct mineral indication was discovered, warranting further exploration for higher grade ore deposits.

Therefore, in the third phase of the survey program, geological survey and geochemical exploration in the Diamante-Paraiso-Bombona area and diamond drilling in the area including Diamante ore deposit were to be continued.

### 1-2 Purpose of the Survey Works

The main purpose of the survey works is to clarify the relation between the geological structure and the zone of the mineralization as well as the characteristics of the mineralization, in order to obtain useful direction for further exploration and development of mines in the whole areas in future.

Also, in the works of the diamond drilling in the area including the Diamante ore deposit, the drill holes were programmed to be located in a way to obtain informations of the points with approximately 100 meters interval laterally, which have made it possible to check swell and pinch of the veins, to know variation of intensity of the mineralization and thus to elucidate the feature of the mineralization. These informations would help to proceed further exploration and to study development of the area in future.

### CHAPTER 2. OUTLINE OF THE ACTUAL SURVEY WORKS

### 2-1 Area and Term of the Survey Works

The survey area is located in the central part of the Narino Department, which occupies the southwestern part of the Republic of Colombia.

The area is situated on the western slope of precipitous mountains of the Cordillera Occidental, which runs north to south in the western part of this Republic.

The survey area in this third phase of the program is a triangled area formed by linking Diamante, Paraiso and Bombona, in the southeastern part of the whole project area of  $1,000~{\rm Km}^2$ . It belongs to the Municipalities of Sta. Cruz and Piedrancha, Nariño Department, and the total area is approximately 24  ${\rm Km}^2$ .

The temperature is rather low, because the southern areas of Diamante and Bombona are situated at the altitude of 2,500 to 3,000 meters above sea level and the northern Paraiso area is also located approximately at as high altitude as 2,000 meters above sea level. However, generally they have pretty heavy rainfall and the dry season is only in the period between May and September. Access is hard as there is only horse path in the area, although vehicle road is available up to Guachavez. Therefore, a new road was constructed to the Diamante mine for the transportation of various machines in this phase of the survey program.

The actual works of the geological survey and the geochemical exploration were carried out during the period of 74 days between June 14th and August 26th in 1982, by 6 geologists, 4 from Japan and the other 2 from the Republic.

The diamond drilling was carried out in the mineralized zone including the main Diamante veins, succeeding the second phase of the survey program.

The total length of the drill holes is 1,335.9 meters with 8 holes. In this third phase, a new road for vehicles was constructed for the transportation according to the program, instead of helicopters. The actual works of the diamond drilling was carried out during the period of 152 days between July 5th and December 3rd, by 4 engineers sent from Japan. The schedule of the survey works is shown as following table.

### 1TINERARY

			Geological S	Survey	Drilling Su	rvey
No.	Date	Day	Itinerary	Survey Contents	Itinerary	Survey Contents
1	6/14	М	Tokyo	Travel		
2	15	T	→ Bogota			
3	16	W	Japanese Embassy JICA INGEOMINAS	Courtesy call Work arrangement		
4	17	T	Bogota → Popayan	Travel		
5	18	F		Preparation		
6	19	S	Popayan → Pasto	Travel Foodstuff arrangement		
7	20	S	Pasto → Guachavez			
8	21	M	Diamante Paraiso	Field work		Commencement of road construction
22	7/5	М	*1	n	Tokyo	Travel
23	6	T	11	11	→ Bogota	11
24	7	W	"	19	Japanese Embassy JICA INGEOMINAS	Courtesy call work arrangement
25	8	Т	n	n	Bogota → Guachavez	Travel
26	9	F	o o	D		Preparation
27 1	10	s	n	11	Guachavez → Diamante Diamante	<u>-</u>
			7/19 ∿ 7/25 Guachavez	Compilation	u	11
43 J	7/26		Diamante Bombona	Field work	17	11
57	8/9		n	D	st	ш
58 1	10		Guachavez	Compilation	n	n
62	14	s	Guachavez → Pasto	Travel	11	II .
63	15	S	Pasto → Popayan	11	II .	rt
64 1	16	M	Popayan	Compilation		
70	8/22	S	Popayan → Bogota	Travel	rı	0
71	23	м	INGEOMINAS Japanese Embassy JICA	Verbal explanation of Survey results	п	tt
			8/24 ∿ 8/26	Travel to Japan	17	n
; 141	11/1	M	Leader revisits to	Colombia	n	PT .
147	7	s	Diamante	Core logging	II .	tt
152	12	F	tł	n	11	Termination of drilling work
153	13	S	19		11	Demobilization
166	26	F	Guachavez → Pasto	Travel	Guachavez → Pasto	Travel
167	27	S	Pasto → Popayan	11	Pasto → Popayan	**
168	28	S	Popayan	Compilation	Popayan	
1					12/1 ∿ 12/3	Travel to Japan
179	12/9	T	INGEOMINAS	Interim report		
180	10	F	Bogota	Travel		
182	12	S	→ Tokyo	н		

### 2-2 Method of the Survey Works

The survey works performed in this third phase of the survey program are geological survey, geochemical exploration by soil samples and diamond drilling in Diamante area. The geological survey and the geochemical exploration were carried out in 6 areas (from north, Paraiso area, Desquite area, Delicia area, Bombona northwest area, Gitana area and Diamante area), as indications of mineralization had been found in these areas. The geological survey was composed of mapping along the main river and streams as well as along the main roads, while the geochemical exploration was conducted by collecting soil samples along the cut-lines which are established in almost right angles across the direction of the extension of the mineralized zone (which is approximately N45° E to N60° E). The interval of the cut-lines is 125 to 250 meters and the points for sampling were set every lateral 25 meters along the lines.

Geochemical exploration works were also carried out in other areas than the detailed survey areas, by collecting soil samples with the interval of 50 meters along the ridges and streams, in addition to the geological mapping along the main streams and the main roads.

Easy land survey was carried out with the measuring tapes and simple transit compasses (Ushikata-made) along the survey routes, producing survey maps of the scale of 1 to 2,000. Localities of the sampling points and the details of the geological observation were mapped on this survey map.

These route maps were compiled finally on the topographical map of the scale of 1 to 2,000 or 1 to 5,000.

For the geochemical exploration, three hand-augers and six pairs of hoes were prepared to collect samples from B zone, which had been produced through the weathering of the base rocks. It was pretty hard to collect samples, because the actual points of the sampling went as deep as 70 cm to

320 cm, with the average depth of approximate 160 cm.

The survey team was composed of total 6 or 7 members in a group, that is, 1 or 2 engineers, 1 assistant engineer and 3 helpers with a cook.

For the security in the works and for the smooth administration, a local office was opened in Guachavez, where a jeep was kept in case of the emergency. A wireless was also kept for the communication with Popayan and Bogota offices of INGEOMINAS, as well as with the survey camps for provision and emergency.

The approximate total amounts of the survey works performed in this phase of the program are as follows.

Surveyed area	24	Km <sup>2</sup>
Total length of the routes surveyed	115	Km
Number of samples collected in the		
geochemical exploration	2,256	
Number of thin sections of the rocks	16	
Number of polished sections of the ores	15	
Number of samples for whole rock analysis	5	
Number of samples for age determination	2	
Number of samples for X-ray diffraction	33	
Number of samples for EPMA analysis	5	
Number of samples for chemical analysis (ore)	50	
Number of samples for trace element analysis	33	

The diamond drilling in the second phase was carried out last year with the approximate interval of 200 meters in the northern part of the Diamante old workings.

In the third phase of the program, the interval of the drill holes narrowed and 100 meters interval was employed. The location of the drill holes were extended to about 300 meters south of the Diamante old workings,

covering total length of 800 meters of the ore vein. Thus, various informations on the geology and the ore deposits were obtained successfully.

As the attitude of the ore vein was known to be almost vertical through the results of the diamond drilling in the second phase, the drill holes were planned to be inclined from the southwestern lowland toward the northeastern highland. In this way, many useful informations were obtained on the ore veins at the altitude of about 2,500 meters above sea level, in addition to some other information on the deep part of the same ore vein. At the end of the drilling works, the locations of all the drill holes, including those in the second phase, were surveyed in closing loop with easy transit compasses and measuring tapes, to make the locations of the drill holes plotted precisely.

The cores collected by the diamond drilling works were separated into two groups. The cores in which mineralization was recognized were split into two pieces with diamond cutters. One piece was crushed, milled and analysed, while the other was kept as core samples. The cores in which no mineralization was found were sent to INGEOMINAS, who collected the pieces of cores of the length of about 10 cm at the points of every 10 meters or at every point where different rock appears. These pieces have been kept as the reduced core samples. The amounts of the materials concerning the works of the diamond drilling are as follows.

Number of ore samples for the analysis	80
Number of thin sections of the rocks	16
Number of polished sections of the ores	24
Number of samples for X-ray diffraction	8
Number of samples for EPMA analysis	5
Number of samples for the measurement of	
filling temperature of fluid inclusions	20

### 2-3 Method of Analysis

As for the results of the field surveys, total 15 days of analysis works were held twice in the field, toward the end of July and in the middle of August, when rough survey maps were produced and various problems were picked up for resolution with the members of the counterpart. The chemical analysis of the samples collected in the geochemical exploration were completed at the laboratory of INGEOMINAS with a succeeding temporary interpretation of the assay value. Following statistic treatment and analysis were described in the logging sheets of the scale of 1/200, with the emphasis upon petrographical feature, variety and grade of alteration, conditions of fissilities and states of mineralization.

The informations thus obtained were compiled on the cross sections and were projected on the plan representing the geology and ore deposits at the altitude of 2,500 meters above sea level, and the continuity of the ore vein was examined. Also the results of the measurement of filling temperature of fluid inclusions were plotted on the cross sections for the study of the distribution of temperatures at which the minerals composing the ore vein were formed.

The results of the survey works were roughly conveyed verbally to the counterpart on 23 August with the withdrawal of the members of the geological survey and on 9 December, 1982, when the chief of the team was returning to Japan after completing drilling works. Also, toward the end of January in 1983, when every necessary analysis had been completed a meeting for the technical studies of the results of the survey works was held with two engineers of the counterpart, INGEOMINAS, who visited Japan.

### 2-4 Organization and Members of the Survey Team

Persons in charge of survey planning and negotiation in Japanese side:

Toshio Koizumi Metal Mining Agency

Yozo Baba - do -

Persons in charge of survey planning and negotiation in Colombian side:

Alfonso Lopez Reyna INGEOMINAS General Director

Raul Duran Rodriguez - do - Sub Director

Joaquin Buenaventura - do - Coordinator of Base Metal Project

Humberto Gonzales - do - Regional Director of

Medellin

Members of the survey team in Japanese side:

Junnosuke Oikawa	Chief	MINDECO*
Yoshihiro Nagumo	Member (geology)	- do -
Minoru Saito	- do -	- do -
Shigehisa Fujiwara	- do -	- do -
Kiyotaka Obase	Member (drilling)	- do -
Tadatoshi Nasu	- do -	- do -
Kiyoshi Sakashita	- do -	- do -
Yoshihiro Nagata	- do -	- do -

Members of the survey team in Colombian side:

Abigail Orrego Lopez	Chief	INGEOMINAS	Regional Director of Popayan
Raul Munoz A.	Member (geology)	- do -	Geologist of
Humberto Caballero	- do -	- do -	Medellin Geologist of Medellin

<sup>\*</sup> MINDECO is an abbreviation of Mitsui Mineral
Development Engineering Co., Ltd.

### **PARTICULAR**

# PART I GEOLOGICAL SURVEY-GEOCHEMICAL EXPLORATION

### PART I GEOLOGICAL SURVEY AND GEOCHEMICAL EXPLORATION

### CONTENTS

			Page	3
СНАРТЕ	R 1.	GEOLOGY	I	6
1-1	Outl	ine of the Geology	r-	6
1-2	Gree	n Volcanic Rocks	<b>I</b> —	7
1-3	Shale	e ''''''	I —	7
1-4	Pied	rancha Granodiorite	1-	8
1-5	Geol	ogical Structure	I-1	1
CHAPTE	R 2.	GEOCHEMICAL EXPLORATION	I – 1	2
2-1	India	cative Elements	<b>I</b> -1	2
2-2	Treat	tment of Samples and Method of Chemical Analysis	I — 1	2
2-3	Metho	od of Analysis	I-1	3
2-4	Resu	lts of Analysis ···································	<u>r-1</u>	3
2	-4-1	Results of Calculation	I 1	3
2	-4-2	Selection of Anomalous Values and Division of Grades	I-1	4
2	-4-3	Distribution of Anomalous	I-1	5
СНАРТЕ	R 3.	ORE DEPOSITS	I-2	0
3-1	Out1:	ine of Ore Deposits	I-2	0
3-2	Mine	ralized Zone in the Eastern Area	·I – 2	1
3	-2-1	Diamante Ore Deposit	·I — 2	1
3	<b>-</b> 2-2	Marina Ore Deposit	.I <b>–.</b> 2	2
3	-2-3	Gitana Segunda Ore Deposit	·I — 2	4
3	-2-4	Mineral Indications in the Northwestern Extension of the		
		Gitana Mining Area	·I-2	4
3	-2-5	Descrite Ore Deposit	I 2	2 5

3-3 Mi	neralized Zone in the Central Area	I — 2 6
3-3-1	Mineral Indications in the Paraiso Area	1-26
3-3-2	Delicia Ore Deposit	I — 3 2
3-3-3	Mineral Indication along Q.3	I — 3 3
3-3-4	Mineral Indication at Jarol	I — 3 4
3-4 Mi	neralized Zone in the Western Area	I-35
3-4-1	Mineral Indications in the Northwestern Extension of	
	Bombona Mining Area	I — 3 5
CHAPTER 4.	GENERAL DISCUSSION ON THE MINERALIZED ZONES	I-38
4-1 Re	elation between Geological Structure and Mineralization	I-38
4–2 Re	elation between Igneous Activity and Mineralization	I — 3 9
4-3 Wa	all Rock Alteration	I-41
4-4 01	re Minerals	I-42
4-5 D:	Istribution of Metals in Diamante Mine	I-45
4-6 F	luid Inclusion Study	I-46
4-7 G	enetic Model of Ore Deposit	I — 4 8
CHAPTER 5	. CONCLUSION AND RECOMMENDATION	I — 5 (
5-1 C	onclusion	I-50
5-2 R	ecommendation	I-5
	***************************************	I 6 9
REFERENCE	***************************************	1-0

### LIST OF FIGURES

Fig.	I <b>-1</b>	Location Map of the Surveyed Area
Fig.	I-2	Normative Plagioclase-Alkali Feldspar-Quartz Diagram
Fig.	I <b>-</b> 3	ACF Diagram for Granitic Rocks
Fig.	I-4	Variation Diagram of Granitic Rocks
Fig.	1-5	Log Zn versus Log As Distribution Map
Fig.	1-6-1	Histogram for Granitic Rock
Fig.	1-6-2	Histogram for Shale and Green Volcanic Rock
Fig.	1-6-3	Histogram for All Rock Types
Fig.	I <b>-</b> 7-1	Cumulative Frequency Distribution Curve for Granitic Rock Area
Fig.	I-7-2	Cumulative Frequency Distribution Curve for Shale and Green Volcanic Rock Area
Fig.	I-8	Vein and Sampling Location of Marina Mine
Fig.	I-9	Vein and Sampling Location of Gitana II Mine
Fig.	I-10	Outcrop Sketch Found at the Bank of Q-18 in Bombona-NW Area
Fig.	1-11	Wall Rock Alteration Chart (1)
Fig.	I-12	Wall Rock Alteration Chart (2)
Fig.	I-13	Paragenetic Sequence of Minerals in the Diamante Principal Vein
Fig.	I <b>-1</b> 4	Ag/Au Versus Au Value Diagram from Veins in Diamante-Paraiso-Bombona Area
Fig.	1-15	Prospective Zones extracted after Geochemical Survey in the Diamante-Paraiso-Bombona Area
Fig.	I-16	Longitudinal Section of Diamante Principal Vein for Studying Survey Results
Fig.	I-17	Location of Samples for Fluid-Inclusion Study and their results
Fig.	I-18	Genetic Model for Auriferous Polymetallic Veins in the Surveyed Area

### LIST OF TABLES

Table	I-1	Age Determination of Igneous Rock
Table	1-2	Whole Rock Analysis and Calculation of Normative Minerals
Table	I-3-1	Statistic Data of Soil Samples
Table	I <b>-</b> 3-2	Results of Graphic Analysis
Table	I-4	List of Geochemical Anomalous Zone
Table	I <b>-</b> 5	List of Veins Diamante-Paraiso-Bombona
Table	<b>I-6</b>	Chemical Analysis of Ore Samples in Q.3 Delicia
Table	I-7	Correlation Coefficients among Elements of Ore Vein in

### LIST OF PLATES

PL. I-1	Gelogic Map of Diamante-Paraiso-Bombona Area	1 : 10,000
PL. I-2	Cross Sections of Diamante-Paraiso-Bombona Area	1:10,000
PL. I-3	Geologic Map of Paraiso-Desquite Area	1: 5,000
PL. I-4	Geologic Map of Delicia Area	1: 2,000
PL. 1-5	Geologic Map of Gitana-NW Area	1: 2,000
PL. I-6	Geologic Map of Bombona-NW Area	1: 2,000
PL. I-7	Geologic Map of Diamante-Marina-Gitana Area	1: 2,000
PL. I-8	Geochemical Map of Diamante-Paraiso-Bombona Area	1:10,000
PL. I-9	Geochemical Map of Paraiso-Desquite Area	1: 5,000
PL. I-10	Geochemical Map of Delicia Area	1: 2,000
PL. I-11	Geochemical Map of Gitana-NW Area	1: 2,000
PL. I-12	Geochemical Map of Bombona-NW Area	1: 2,000
PL. I-13	Geochemical Map of Diamante-Marina-Gitana Area	1: 2,000
PL. I-14	Locality Map of Soil and Rock Samples	1:10,000
PL. 1-15	Plan and longitudinal Section of Diamante Principal	Vein 1: 2,000

### CHAPTER 1. GEOLOGY

### 1-1 Outline of Geology

The area surveyed in this third phase of the program is underlain by shale, green volcanic rocks and granodiorites intruding the former two. Although, in some places along the ridges at the southernmost of the surveyed area, there are thin layers of volcanic ashes which are not consolidated yet and are derived from Quaternary volcanic activity, it is impossible to show them on the geological map because they occupy too small areas.

The above-mentioned rocks, except for the Quaternary volcanic ashes, are correlated as follows, according to the Narino quadrangle and its explanation notes by INGEOMINAS (1982).

- \* Shale is to the Dagua Formation (lower or middle Cretaceous)
- \* Green volcanic rocks are to the Diabasico Formation (probably upper Cretaceous)
- \* Granodiorite intrusive mass is to the Piedrancha batholith (Eocene or Miocene)

This correlation does not make good coincidence with the idea shown as a part of the conclusion of the survey report of the first phase of the program, which said as follows:

The Diabasa group is changing rock facies from volcanic rocks prevailing facies to sedimentary rocks from the lower level to the upper level, and the distribution is volcanic rocks in the west part and sedimentary rocks and partly volcanic rocks in the east part, and the general strike of the stratum reveals NNE-SSW. Structurally it represents a synclinorium structure with axis of N-S direction and intruding rock of granodiorite has appeared along the axis extending in a N-S direction.

In order to clarify the reason for this difference, careful observation

of every outcrops and another investigation of the informations already in hand were carried out. However, it was impossible to find out obvious evidences to determine the relation of the strata. Further investigation would be necessary for this point.

### 1-2 Green Volcanic Rocks

The green volcanic rocks are composed of andesitic lava, agglomerate and tuff breccia. The rocks appear in color of green to dark green and are hard generally. The rocks are distributed mainly in the Diamante area and the neighbouring areas to the northwest of it. To mention about the relation of the rocks to the siliceous shale, the green volcanic rocks are thought to be lower stratigraphically than the siliceous shale, according to the results of the survey in the first phase, although no outcrop has been found in this survey area showing any boundary between them.

Under microscope (thin section No. QCPP49, M8021, Q1237) phenocrysts are mainly plagioclase, hornblende and biotite, and the texture is corresponding to that of andesitic volcanic rock. Actionalite and epidote are found as the secondary minerals in the rocks, and it is thought that this would show the rocks were metamorphosed to the green schist facies.

### 1-3 Shale

The shale is siliceous and light grey in color, apparently. In some places it contains thin layers of calcareous shale. As this rock is distributed in the eastern peripheral zone of the Piedrancha granodiorite intrusive body, extensive silicification, in some cases pyritization, is prevailed. Also there are evidences of thermal alteration in this shale. This shale is distributed in the eastern bank area of the middle-stream of Q. La Cruz and along the road between Paraiso and Guachavez.

Under microscope (thin section No. N-43, Q1129, HCA-14), the rock is composed mainly of quartz grains of the size of 0.1 to 0.2 mm. The minerals produced through the thermal alteration are contained. For instances, the calcareous parts include diopside while siliceous parts contain biotite and muscovite.

### 1-4 Piedrancha Granodiorite

This Piedrancha granodiorite is composed of the following three sorts of rocks.

- (1) Fine grained granodiorite.
- (2) Coarse grained granodiorite
- (3) Aplite.

The main part of the Piedrancha granodiorite intrusive mass is composed of (1) and (2), which is distributed occupying most part of the survey area. The aplite shown as(3) is found locally in the form of small dykes intruding the former two. These intrusive rocks are thought to be derived from the magma of the same origin, from the viewpoints of the distribution and the chemical similarity. By the field evidences of intrusion, the sequence of the intrusion of these three rocks is thought to have been (1)-(2)-(3) from the earlier stage to the later. By the result of the age determination by K-Ar isotopic method, the age of the coarse grained granodiorite is  $6.5 \pm 2.7$  million years, which reveals that the intrusion of this granodiorite would have been at the end of Miocene Epoch in Tertiary Period.

The results of the analysis of the whole rock chemical assay of the two samples, RM-6 and F-9, collected in the survey in this third phase program, are shown in Fig. I-2, 3, 4. By Geotimes (1973), these rocks are classified granite or quartz monzonite. On the ACF diagram, they are plotted in the area of the rocks of igneous origin. It has been clarified that the

fine grained granodiorite, represented by the sample F-9, is more basic than the coarse grained granodiorite, RM-6.

### (1) Fine grained granodiorite

The fine grained granodiorite is hollocrystalline, composed mainly of biotite, hornblende, plagioclase and quartz, of the size under 2 mm in diameter. Under microscope, small amounts of apatite, zircon, sphene and magnetite are recognized. The color index, represented by the ratio of the amount of mafic minerals to that of whole minerals, is 25 to 30%, and it appears grey to dark grey. In places, idiomorphic crystals of biotite, about 3 to 4 mm in diameter, are contained where porphyritic texture is recognized. This fine grained granodiorite is distributed predominantly near the ridges along the border between Delicia area and Bombona area. It also is found in places as the xenolithes caught in the coarse grained granodiorite as mentioned in later paragraph. Along the stream Q.3 between Paraiso area and Delicia area, it was observed, when the going-upstream survey was carried out this year, that the coarse grained granodiorite is distributed in the downstream to middle-stream area and that the fine grained granodiorite in the upstream area.

### (2) Coarse grained granodiorite

The color index of the coarse grained granodiorite is 20 to 25%. It is hollocrystalline, composed mainly of hornblende, biotite, plagioclase and quartz of the grain size of 4 to 5 mm in diameter, with such accessory minerals as orthoclase, muscovite, magnetite, apatite, zircon and sphene.

This coarse graine granodiorite, composes the main part of the Piedrancha granodiorite, and is distributed most prevailingly in the survey area.

Along the marginal zone of this coarse grained granodiorite, especially

in the Bombona area, it becomes rather fine grained, and increasingly toward the margin, many xenolithes of the rocks, which contains more mafic minerals and is thought to be of the same origin, are caught in this granodiorite. Sometimes is observed slight lineament (schlieren) produced by hornblende phenocrysts. This lineament has parallel orientation to that of the boundary of the wall of the intrusion. The age of a sample of this coarse grained granodiorite, collected in a Paraiso area, has been determined to be 6.5 million years, which is the youngest of all the measurement values obtained in the Piedrancha On the other hand, the coarse grained granodiorite distributed in the Bombona area (sample No. B.-22) reveals 20.7 million years, which is also grouped into the Piedrancha granodiorite. Therefore, it is thought that coarse grained granodiorite might possibly be a composit complex of the rocks of the same kinds but of the different ages. An evidence for this idea is, as mentioned in the above paragraph (1), that there is an exposure where the coarse grained granodiorite is found to have intruded the fine grained granodiorite, cutting it clearly. Furthermore, through the examination of the ages obtained in 1980 -1982, it has been clarified that the Piedrancha granodiorite is younger than the diorite or the granodiorite intruding the surrounding area of the Piedrancha granodiorite. It can be said there is a tendency that the younger the rocks are, the more acidic they are.

### (3) Aplite

The aplite is leucocratic hollocrystalline intrusive rock. It is distributed in the middle-stream area and in the downstream area of the Q.2 stream and the Q.3, as well as in the downstream area of the Q.12. The width of the dykes varies from 0.1 to 10 meters. The aplite is found to have intruded the siliceous shale and the coarse grained

granodiorite, and it is thought that the aplite would be one of the final products of the acidic igneous activities. No direct relation has been recognized between the aplite and the mineralization.

### 1-5 Geologic Structure

The following three systems of the lineament are recognized to be well developed in this survey area. (1) NW-SE, (2) NE-SW, (3) N-S. In addition to these systems another system of (4) E-W is also recognized slightly. The NW-SE system is most prevalent in the survey area, and is represented by the directions of the main rivers of the ore veins and of the fissures and joints found in the outcropped rocks. The N-S system is also prevalent although it is less frequently found than the NW-SE system. It is represented by the direction of small streams. The NE-SW system is also recognized by the direction of small streams. The E-W system is represented by the direction of joints in rocks in the northern part of the survey area.

As for the sedimentary rocks, it is hard to grasp the whole geologic structure because the area of its distribution are small and because the structure is much complicated owing to the intrusion of igneous rocks.

However, according to the results of the regional geologic mapping in the first phase, it is thought that the sedimentary rocks form isoclinal foldings with the axes of the direction of NNE-SSW. It has been clarified through the analysis of the folding of the strata and the fissure systems that compressed pressure in east and west would have been intensively working to have produced sheared zones of NE-SW system and NW-SE system as well as compressed planes of N-S system and open cracks of E-W system. It is inferred that these systems would have worked at the period of the uplift of the basement, at the time of the intrusion of the igneous rocks, and at the period of the ore mineralization.

Table I - I Age Determination of Igneous Rock

Sample No.	Locality	Rock Name	Mineral	Ar 40	K 40	40Ar R/40K	Age M.Y	Remarks
RM-6	Paraiso	Granodiorite	hornblende	0.000192	0.503	0.000382	6.5 ± 2.7	*1
PD-1088	Diamante	Green volcanic rock	Whole rock 0.000996	966000.0	0.791	0.001259	21.4± 1.5	

 $\star$  l Hornblende concentrate, -80/+200 mesh

Treated with dilute HF and  ${\rm HNO}_3$  to remove alteration.

$$\lambda e = 0.585 \times 10^{-10} / \text{year}$$
  $40 \text{K/K} = 1.2$ 

$$40K/K = 1.22 \times 10^{-4} g/g$$

$$\lambda \beta = 4.72 \times 10^{-10}/\text{year}$$

Age = 
$$\frac{1}{\lambda e + \lambda \beta}$$
 &n  $\left[\frac{\lambda \beta + \lambda e}{\lambda e} \times \frac{Ar}{K} \frac{40}{40} + 1\right]$ 

Table I -2 whole Rock Analysis and Calculation of Normative Minerals

		RM-6	F-9	PD 1088
Sample No.		granodiorite	granodiorite	green volcanic rock
	SiO <sub>2</sub> Weight%	63.22	58.29	52.77
	TiO <sub>2</sub>	0.53	0.66	0.73
Elements	A1203	16.08	16.27	17.61
	Fe <sub>2</sub> 0 <sub>3</sub>	2.49	3.08	4.04
	Fe0	3.44	4.19	4.84
	MnO	0.14	0.16	0.11
	MgO	2.60	3.79	6.03
	Ca0	5.82	6.75	6.03
	Na <sub>2</sub> O	2.93	2.85	4.72
	K20	2.12	1.80	1.31
	P205	0.16	0.22	0.24
	CO2	0.00	0.00	0.00
	H <sub>2</sub> 0 <sup>+</sup>	0.16	0.41	0.53
	H <sub>2</sub> 0 <sup>-</sup>	0.30	0.59	0.12
	Total	99.99	99.06	99.08
	Q	21.34	14.48	0
	OR	12.59	10.85	7.86
	AB	24.91	24.59	40.57
	AN	24.58	26.80	23.36
Normative minerals	Salic Total	83.41	77.13	71.80
	WO-DI	1.41	2.45	2.27
	EN-DI	0.85	1.57	1.59
	FS-DI	0.48	0.72	0.48
	EN-HY	5.65	8.06	8.58
	FS-HY	3.18	3.72	2.60
	FO-OL	0	0	3.59
	FA-OL	0	0	1.19
	MT	3.63	4.55	5.95
	IL	1.01	1.28	1.41
	AP	0.37	0.52	0.56
	Femic Total	16.59	22.87	28.20
D.I = Q + OR + AB		58.83	50.32	48.44
Weight Q		25.58	19.29	0
Percentage AB + Or		44.95	45.95	67.46
	L An	29.47	34.75	32.54

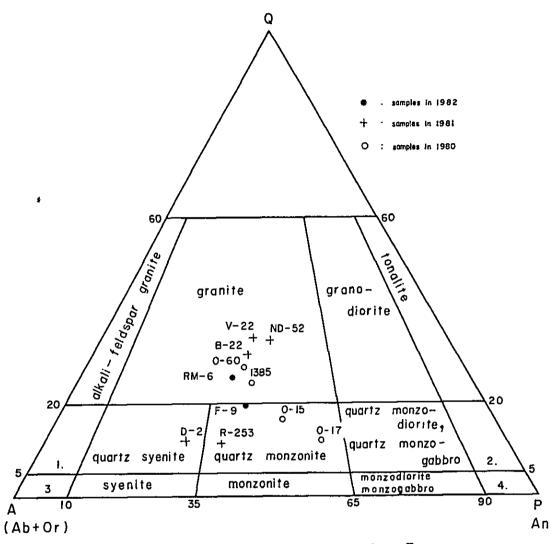


Fig. I-2 Normative Plagioclase (anorthite) — Alkali Feldspars (orthoclase + albite) — Quartz Diagram (Geotimes, 1973)

I. alkali – feldspar quartz syenite
 Quartz diorite, quartz gabbro,
 quartz anorthosite
 3. alkali – feldspar syenite
 4 diorite, gabbro,
 anorthosite

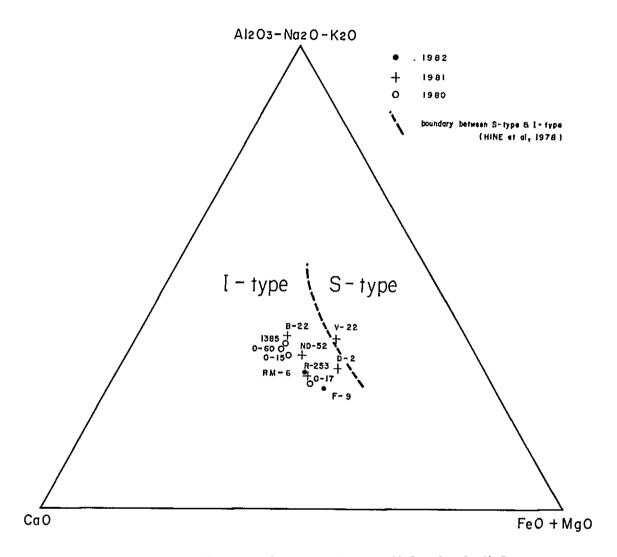


Fig I-3 ACF Diagram (molar ratios, A=Al2O3-Na2O-K2O, C=CaO, F=FeO+MgO) for Granitic Rocks

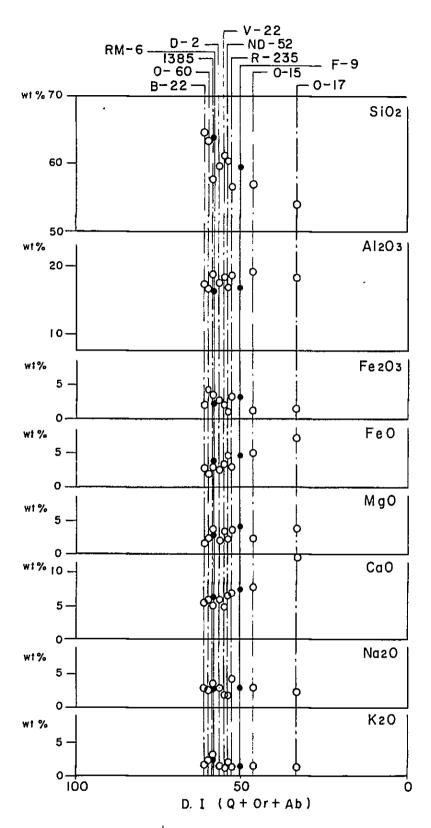


Fig.1-4 Variation Diagram of Granitic Rocks

\_\_\_\_\_; samples in 1982

#### CHAPTER 2. GEOCHEMICAL EXPLORATION

## 2-1 Indicative Elements

The geochemical exploration was carried out with geological survey last year by collecting soil samples in the Diamante area and in some parts of the Bombona area in the second phase of the survey program. For this geochemical exploration, arsenic and zinc were adopted as the indicative elements. The reason why these two elements were employed as the indicative elements for the geochemical exploration was that the known quartz veins in the survey area usually contain arsenopyrite, that sphalerite, though in small amount, is also recognized associated with chalcopyrite and galena, that both arsenic and zinc are known to be easily dispersed, that the chemical analysis is less expensive than that of mercury, gold etc., and that arsenic is employed very often as the indicative element for geochemical exploration for auriferous ore deposits.

As the result of employing these elements, it has been clarified that the distribution of the geochemical anomalies is well corresponding with the area where indications of mineralization are known to be. Considering that the width of ore veins found in this survey area is as narrow as less than 1 meter, the geochemical exploration in this phase was programmed to extract mineralized zones more efficiently by making the intervals of the sampling points narrower and by making use of arsenic and zinc as the indicative elements, which had been proved to be quite useful for this type of geochemical exploration for soil.

## 2-2 Treatment of Samples and Method of Chemical Analysis

All the soil samples totalling 2,256, collected in the works, were left dried naturally at the survey sites or at the base camp. After sieving,

the materials as fine as under 80 mesh were divided into quarters, one of which was sent to the laboratory for chemical analysis. The chemical analysis was carried out at the Bogota central laboratory of INGEOMINAS, by atomic absorption method. The limit of determination in this analysis was 1 ppm. The results of the chemical analysis is shown in Appendices I-1.

## 2-3 Method of Analysis

Geologically, the survey area is underlain by granodiorites, green volcanic rocks and shales. As they are different chemically one another, it is thought that the contents of arsenic and zinc in every sampling point are different according to the difference of basement rocks. Therefore, the results of the chemical analysis were grouped into several categories according to the rock underlying each sampling point, for the statistic treatment of the values.

Taking common logarithms of all the assay values, their average, standard deviation, correlation coefficient etc. were calculated. The histogram and the cumulative frequency curve were prepared. These calculation was performed a computer transaction programmed by MINDECO. Anomalous values were decided by the graphical solution, with the bending points of the cumulative frequency curve to be taken as the threshold, referring the method developed by C. Lepeltier (1969). In the process of the calculation, the values of less than 1 ppm are treated as 0.1 ppm.

## 2-4 Results of Analysis

#### 2-4-1 Results of Calculation

The results of the calculation of the assay values are shown in Table

I-3-1. The average value of arsenic contained in the samples collected

in the area of the coarse grained granodiorite is same as that of the samples

collected in the area of the fine grained granodiorite. Also the average values and the standard deviations of zinc in both of the area are almost same.

The average value of arsenic of the samples collected in the area of the green volcanic rocks is higher by 9 ppm than that of the samples in the granodiorites, while the average value of zinc of the former is higher by 5 ppm than that of the latter. Therefore it is thought that they would belong to different groups. The average values of arsenic and zinc of the samples collected in the area of the shale are pretty high, but because the number of samples is as small as 27, these values are treated in a group with the values of the samples collected in the area of the green volcanic rocks, which have comparatively similar values to those in the shale area. The degree of correlation between arsenic and zinc values is highest (correlation coefficient = 0.55) with the samples collected in the area where the green volcanic rocks are distributed, followed by the samples in the areas of the granodiorites and of the shales. In Fig. I-5, diversion of the correlation is shown, totally and individually with each of the rock types.

## 2-4-2 Selection of Anomalous Values and Division of Grades

It is desirable for the statistical analysis that the number of samples is as large as possible and that the conditions are as simple as possible. Therefore, for the selection of the anomalous values, samples were divided into two categories. The one is a group of the samples collected in the area where the green volcanic rocks and/or the shales are distributed.

Fig. I-6 is a histogram, in which individual and totally treated data are shown.

Normal distribution is not recognized with arsenic, but the peak is

found toward the lower values, which is remarkable especially with the samples in the granodiorite area. On the other hand, the distribution of zinc is almost normal, except for the portion of the lower and higher values.

A cumulative frequency curve was drawn (Fig. I-7) by getting arsenic and zinc values accumulated respectively from the highest. Taking the bending point of the curve to be the threshold, it is decided that the values higher than the threshold are taken to be anomalous. Also, as for arsenic, three grades of anomaly have been established by dividing the distributing areas of the values higher than the threshold into three blocks by logarhythmically equal interval on the figure. They are called strong anomaly, intermediate anomaly and weak anomaly. In case of zinc, two grades, strong anomaly and weak anomaly, are established by the same method except that the division is into two blocks on the figure. The results of these works are shown summarized in Table I-3-2. The proportion of anomalous values of arsenic against the whole is different from that of zinc by several times. For instance, anomalous values of arsenic are 26% in the granodiorite area while those of zinc are 3.5%, as shown in Fig. I-7-1. The tendency is same in the area where the green volcanic rocks or the shales are distributed. It is thought that this fact would reveal the following character of the mineralization. That is to say, arsenic is more aboundantly and more prevailingly distributed in this area compared to zinc, as arsenic would be related to the mineralization, while zinc is concentrated locally. The assay results of the ore are showing that the average value of arsenic and zinc are 0.9% and 0.3% respectively. It is thought from this fact that the mineralization would have carried more arsenic than zinc.

#### 2-4-3 Distribution of Anomalies

Taking the aggregate of anomalous values of arsenic and zinc, as shown

in Table I-3-2, to be anomalous zones, geochemical exploration map has been prepared by plotting the distribution of these anomalous zones. The direction of extension of each anomaly was estimated, on the basis of the information on the directions of the known ore veins and old working tunnels. There are many anomalous zones thus extracted, each of which has the width of several ten to several hundred meters, extending NW-SE, as shown on the geochemical exploration maps. All the anomalous zones are summarized and listed in Table I-4.

The outline of the individual anomalous zone is described in the following.

- (1) Gitana-Marina anomaly: This is a weak anomaly found from the eastern part of the Mina Gitana Segunda to the survey line of D-41. Along this D-41 line, intense anomalies are recognized spots.
- (2) Gitana-NW anomaly: This anomalies is possibly divided into 5 zones. Among them, the most prevailed anomalies, Gitana-NW (A), (B) and (C) zones, are recognized at the north-north-west of the Gitana Primera mine. Three intense anomalies of arsenic of the size of 20 - 40m x 150 - 200m are recognized in the direction of NW-SE. The anomalous zones carry weak to intense zinc anomaly. Granite dyke is found near this geochemical anomaly. In the northwest of the Gitana Primera mine, there is an arsenic anomaly of Gitana-NW (D), which is thought to be a mineral indicated continued from the ore deposit in the mine. The extension of this anomaly is recognized in further northwest. In the south of the (D) zone, another anomaly of arsenic, Gitana-NW (E), is recognized in the direction of NW-SE, with almost same size as that of (D) zone. It is thought that the above-mentioned anomalies would represent mineralization shown by possible parallel veins or continuation of veins extending from those in the Gitana Primera

mining area.

- (3) Desquite anomaly: This is a zinc anomaly of the size of about 700 meters in length with the approximate width of 100 meters, extending from the Desquite mining area. The anomaly is not accompanied with arsenic anomaly, which is different from the conditions of the other anomalies.
- (4) Q. Lulo anomaly: This is the arsenic anomaly related both to the quartz vein found at Q. Lulo and to the ore vein found at Q. La Cruz. Continuity is poor and small anomalies are distributed intermittently.
- (5) San Antonio anomaly: The main part of this anomaly is intermediate and weak anomalous zone of arsenic of the size of 50m by 500m, extending to east-south-east from the San Antonio mine. Small and weak anomalous zones of zinc and arsenic are distributed around the main anomaly.
- (6) San Antomio-S anomaly: This anomaly is represented by the arsenic and zinc anomalies, related to the quartz vein (Jarol indication of mineralization) found in the north-west of the cut-lines, Q.2 and F-6. The intervals of lines in this area are too rough to obtain detailed information.
- (7) San Luis anomaly: This is an arsenic anomaly, about 2 kilometers long with the approximate width of 250 meters, extending in the southeast, to the cut-line of F-1 from the San Luis mine. In places, strong arsenic anomalies are recognized to certain extent along the extension zone of the known ore veins. In many cases, zinc anomalies are distributed in small sizes and are overlapped on the arsenic anomalies.
- (8) San Luis W-1 anomaly: Parallel to the San Luis anomaly in its west, this anomaly is distributed from the cut-line of D-5 to that of F-1. This is an arsenic anomaly and would possibly be linked to the clay vein found along the cut-line of F-3.

- (9) San Luis W-2 anomaly: This anomaly is a strong to weak arsenic anomaly, distributed along the ridge in the west of the San Luis W-1 anomaly. It is thought that the anomaly extends in the direction of NW-SE, but the details of its extension are not certain because the anomaly is located near the boundary of the survey area. A float of pyrite-quartz mass, about 1 meter in diameter, was found along the cut-line of D-6.
- (10) Delicia anomaly: This is an arsenic anomaly, extending in the northwest of the Delicia mine. The width of the anomaly is increased along the cut-lines of F-3E and F-2E. Possibly it would extend about 2 kilometers to the quartz vein found along the cut-line of Q.3N.

  Viewing from the direction of extension, this arsenic anomaly is thought to be the same one as the San Luis W-2. Along the cut-line of F-3, there are high grade points of arsenic and zinc.
- (11) Delicia-NW anomaly: Although parallel to the Delicia anomaly, this anomaly is not continuous in its northern part. Several arsenic anomalies are distributed. It is thought that they are linked in the direction of NW-SE. Possibly it is linked to the anomalous zones found along the cut-lines of F-2E and Q.3, but details are not certain.
- (12) Delicia-W anomaly: This anomaly is composed of anomalous values of arsenic, recognized along the cut-lines, F-3E and F-4E. Because the interval of the lines is too rough, details are not certain.
- (13) Bombona N anomaly: Anomalous arsenic values recognized along the cutlines of F-3W and F-2W are regarded as an anomaly by linking them.

  Direction is in NW-SE and the size is 250 meters by 1,000 meters.

  Especially along the cut-line of F-3W, there are several high grade points of arsenic.
- (14) Bombona NW anomaly: Arsenic anomalous zones widely recognized in the

Bombona-NW area are grouped and taken as three anomalies. Bombona-NW (A) zone is recognized between the right bank of Q. Bombona and Q.17, and composes weak to intermediate anomaly extending intermittently in the direction of NW-SE. No ore veins or ore deposits have been found yet in this anomaly. It is thought that Bombona-NW (B) and (C) anomalies are related to several ore veins as found along Q.18. These anomalies have possibility to extend to further west beyond the cut-line of D-10N, which is located along the western limit of the survey area.

(15) Distribution of anomalous values along streams: In some cases, the samples collected along the streams would show very high assay values. For example, most of the values of the samples along Q.11N, Q.9, Q.3, Q.4 and Q.Bombona are abnormally high. It is thought that the reason would be the contamination by stream water which played great role for the transportation of such element from mines or ore veins located in the upstream area. Therefore, they are not regarded as anomalies.

Table I - 3 - I Statistic Data of Soil Samples

Mother Rock Type	Element	Number of Samples	Mean (ppm)	Minimum Value (ppm)	Maximum Value (ppm)	Standard Value Deviation	Correlation Coefficient
	Zn	1788	36.6	7	850	23.8	^ a.s
C. G	As	1788	2.8	1-	2000+	13.0	0.343
	Zn	101	38.9	11	338	32.5	0.207
F. G	As	101	2.8	1-	2000+	13.6	0.384
G. R	Zn	340	43.8	11	564	31.2	0.552
G. K	As	340	11.9	1-	2000+	25.8	0.332
	Zn	27	62.5	9	820	91.3	0.202
S. H	•As	27	17.7	3	200	40.9	0.293
C. G	Zn	1889	36.7	7	850	24.3	0.045
+ F. G	As	1889	2.8	1-	2000+	13.0	0.345
G. R	Zn	367	44.9	9	820	35.3	0.503
+ S. H	As	367	12.2	1-	2000+	26.9	0.521
411	Zn	2256	37.9	7	850	26.1	0.205
A11	As	2256	3.6	1-	2000+	16.6	0.385

## Abbreviation

C.G. : Coarse grained granodiorite, F.G. : Fine grained granodiorite

G.R.: Green volcanic rock, S.H.: Shale

1- : Less than 1 ppm, 2000+: More than 2000ppm

Table I-3-2 Results of Graphic Analysis

Flores	Threshol		Mother Rock	Туре		
Element		sification nomaly	C. Gd + F. Gd	GR + SH		
	Threshol	d value	t <sub>Zn</sub> = 83 ppm	t <sub>Zn</sub> = 112 ppm		
B.,	Backgrou	ind value	Zn < 83 ppm	Zn < 112 ppm		
Zn	Zn Strong		145 <sup>ppm</sup> ≤ Zn	188 <sup>ppm</sup> ≤ Zn		
	Anomaly	Weak	$83^{\text{ppm}} \leq Z_{\text{n}} < 145^{\text{ppm}}$	112 <sup>ppm</sup> ≤ Zn < 188 <sup>ppm</sup>		
	Threshol	d value	tAs = 6 ppm	tAs = 18 ppm		
	Backgrou	nd value	As < 6 ppm	As < 18 ppm		
As		Strong	98 <sup>ppm</sup> ≤ As	135 <sup>ppm ≤</sup> As		
	Anomaly	Intermediate	24 <sup>ppm</sup> ≤ As < 98 <sup>ppm</sup>	50 <sup>ppm</sup> ≤ As < 135 <sup>ppm</sup>		
		Weak	6 <sup>ppm ≤</sup> As < 24 <sup>ppm</sup>	18 <sup>ppm ≤</sup> As < 50 <sup>ppm</sup>		

C.Gd: coarse grained granodiorite, F.Gd: fine grained granodiorite

G.R : green volcanic rock SH. : shale



Table I-4 List of Geochemical Anomalous Zone

		, , , , , , , , , , , , , , , , , , ,			And		nber of ous Sam		6	Related
	An	nomalous Zone Direction		Width and Length (m)		As			Zn	geology
					S	S+I	S+1+W	S	S+W	Mine, vein
1	Gitana-Marina		N50°W	100 x 1000	1 1		7	1	1	Mina Gitana Segunda Mina Marina
		Gitana-NW (A)	N45°W	30∿120x200+	2	3	6	1	1	
		" (B)	N50°W	100∿200x600+	8	13	28	4	6	Granite dyke
2	a-NW	" (C)	N45°W	50 x 400?			11		2	
	Gitana-NW	" (D)	N55°W	50 x 800?	1	3	8	1	1	Mina Gitana primera
		" (E)	N55°W	70 x 800?		6	11		1	
3		Desquite	N45°W .	100 x 700			3	4	11	Mina Desquite
4	Q. Lulo		N60°W ∿N45°W	200 x 1500?		1	20		3	Quartz vein
5		San Antonio	N70°W	300 x 1600?		4	17		3	Mina San Antonio vein
6	Sa	n Antonio-(S)	N55°W	300? x 2400?	$\angle$	3	23		4	Vein
7		San Luis	N50°W	200∿400x2000+	9	21	60		4	Mina San Luis vein
8	Sa	n Luis-W (1)	N50°W	100~400x1200+	4	13	29	$\angle$	3	
9	Sa	n Luis-W (2)	N35°W	100∿300x 700+	3	14	20		4	
10		Delicia	N55°₩	100~400x2000?	5	19	44	2	5	Mina Delicia vein
11		Delicia - NW	N55°W	400? x 1500?	3	7	17	2	4	
12		Delicia - W	N55°W	100∿200x1000?		1	6		2	
13		Bombona - N	N55°W	250 x 1000+	2	3	12	/	2	
	MN-E	Bombona-NW (A)	N40°W	50~100x1000?	1	6	16	$\angle$	1	
14	Bombona-NW	" (B)	N50°W	200 x 800+	3	16	31	$\angle$	2	vein
L_	Bon	" (C)	N55°W	200 x 800+	5	16	40	2	4	vein

S: Strong anomaly, I: Intermediate anomaly, W: weak anomaly

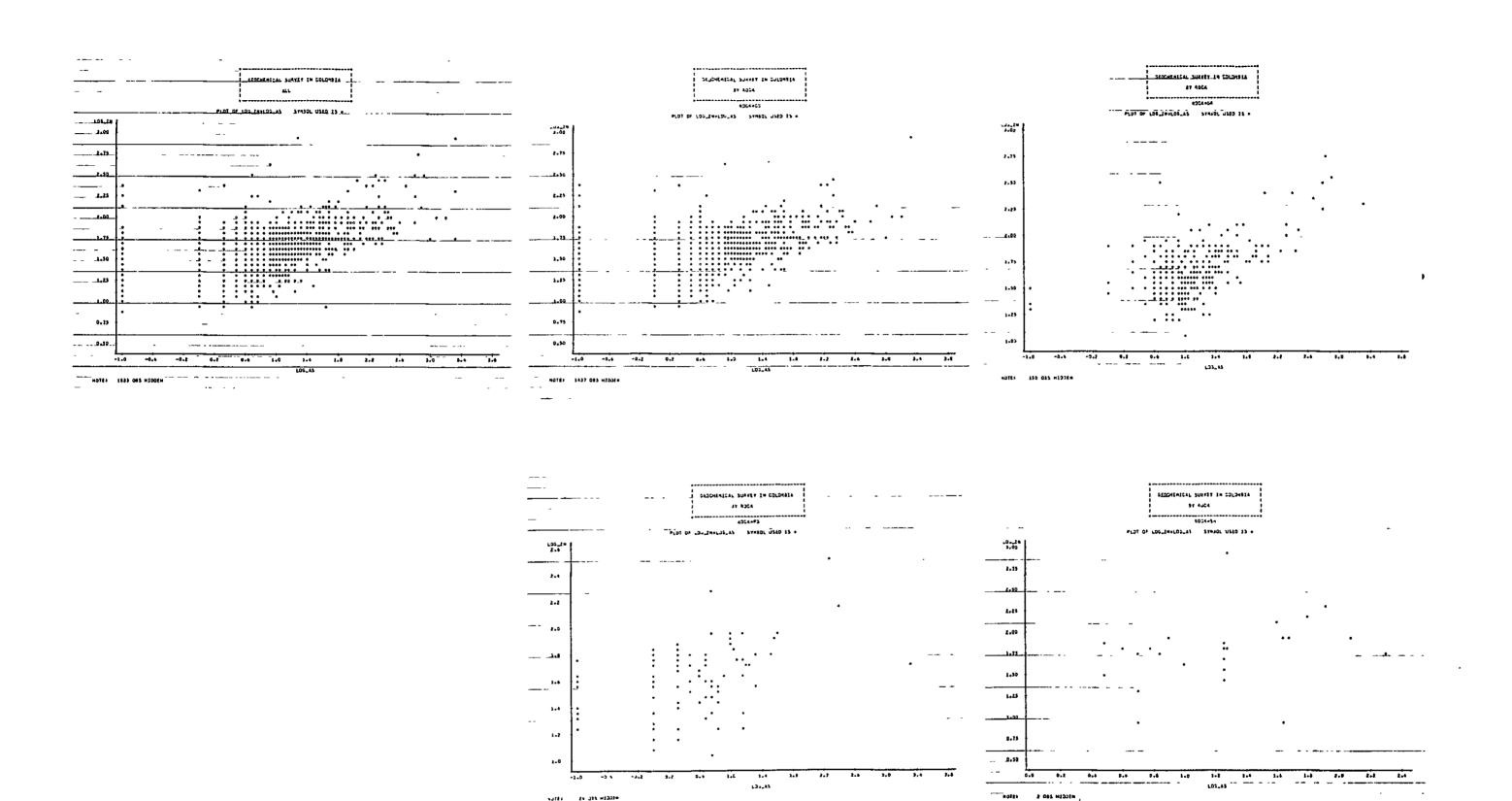
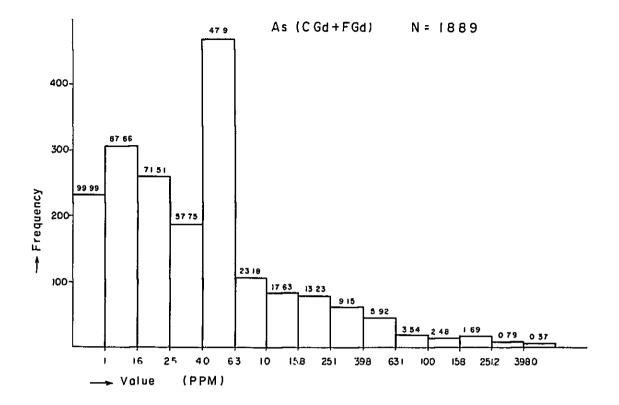


Fig. I-5 Log Zn versus Log As Distribution Map.





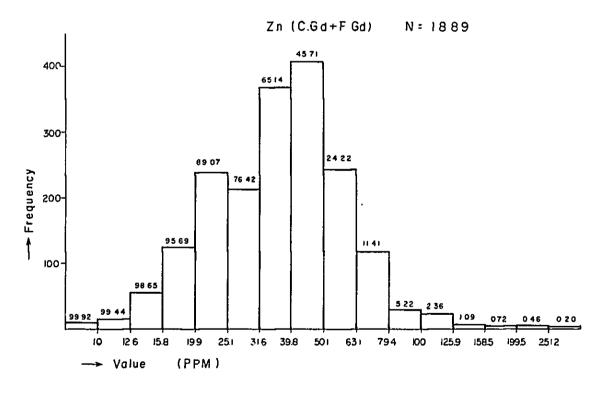
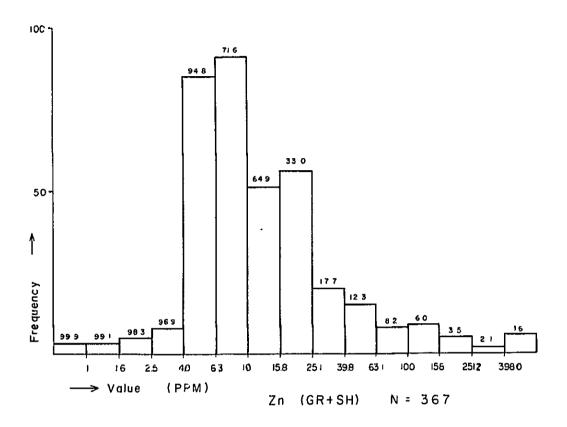


Fig. I-6-1 Histogram for Granitic Rock
(the figures above the column are cumulative frequency percentage)



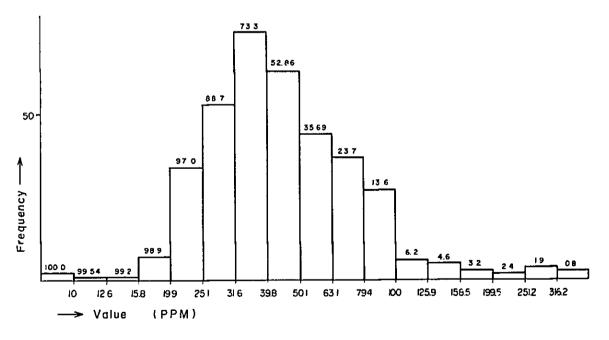
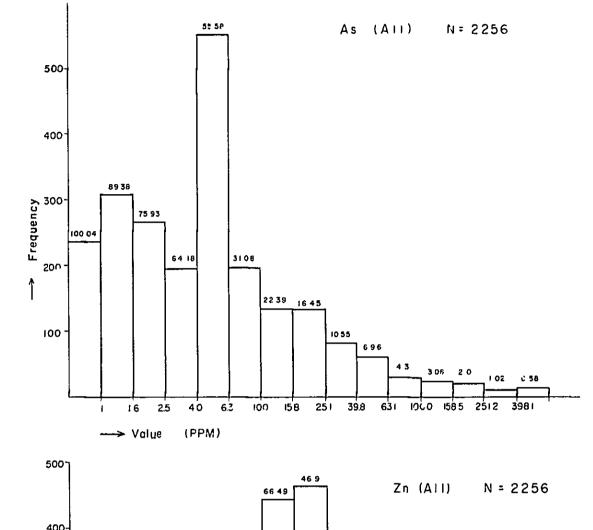


Fig I=6-2 Histogram for Shale and Greem Volcanic Rock (the figures above the column are cumulative frequency percentage)



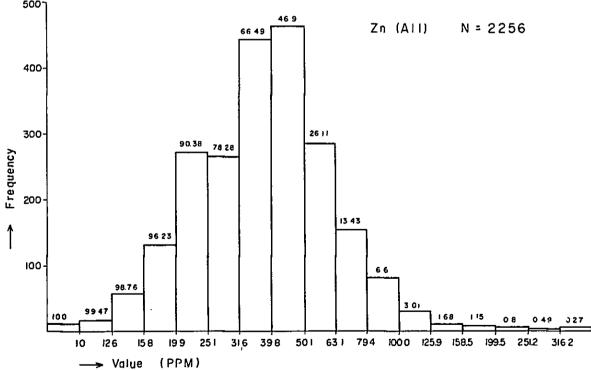


Fig. I-6-3 Histogram for All Rock Types (the figures above the column are cumulative frequency percentage)

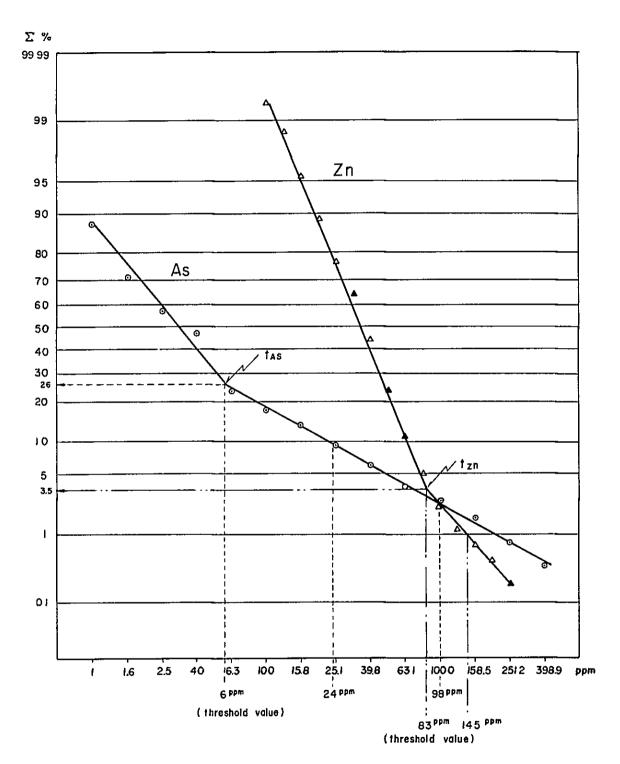


Fig. I-7-I Cumulative Frequency Distribution Curve for Granitic Rock Area

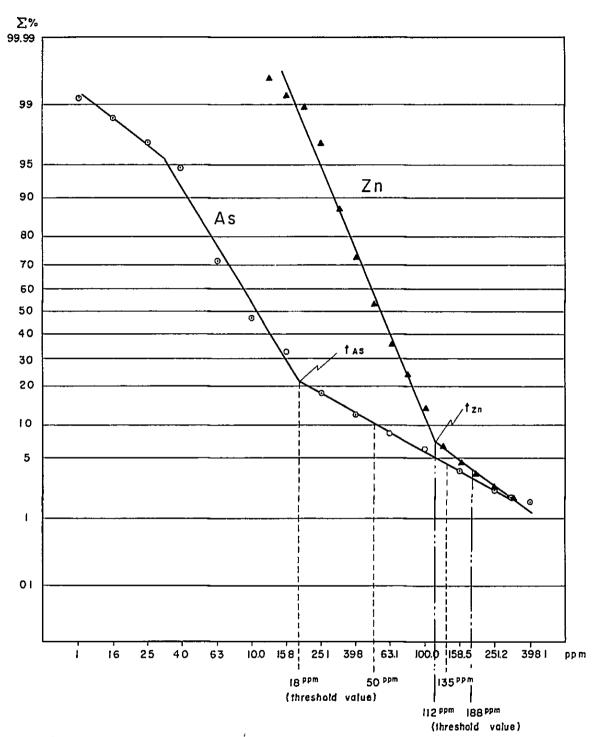


Fig. I-7-2 Cumulative Frequency Distribution Curve for Shale and Green Valcanic Rock Area

#### CHAPTER 3. ORE DEPOSITS

## 3-1 Outline of Ore Deposits

The ore deposits distributed in this survey area is gold ore veins of fissure-filling type. This is the sole type of ore deposits found in this area. The ore veins are emplaced in the green volcanic rocks and in the granodiorites, and are composed of quartz veins associated with pyrite, arsenopyrite, sphalerite and other sulphide minerals. The general trend of the ore veins are NW-SE, and the width of them is mostly 5 cm to 80 cm.

Lateral extension of ore deposits is 100 to 200 meters. In many cases, ore veins are recognized in two or three parallel row, composing a mineralized zone intermittently. There are many known ore deposits in this survey area. By the geochemical exploration carried out in this third phase of the survey program, it has been clarified that there are three mineralized zones extending parallelly in the direction of NW-SE, with the approximate interval of 3 kilometers. The ore deposits and main mineral indications distributed in these mineralized zones are described in the following paragraph. General discussion on the ore deposits are given in Chapter 4.

- (1) Mineralized Zone in the Eastern Area

  Diamante ore deposit, Marina ore deposit, Gitana Segunda ore deposit,

  Mineral indications in the northwestern extension of Gitana mining

  area, Desquite ore deposit.
- (2) Mineralized Zone in the Central Area

  Mineral indications in the Paraiso area, Delicia ore deposit, Mineral
  indication along Q.3, Mineral indication at Jarol.
- (3) Mineralized Zone in the Western Area

  Mineral indications in the northwestern extension of Bombona mining area

3-2 Mineralized Zone in the Eastern Area

In the southern part of this mineralized zone, there are two mineralized zones with the approximate interval of 300 meters. They are Diamante mineralized zone and Marina-Gitana mineralized zone. The northwestern extension of these two mineralized zones has been caught by the geochemical exploration carried out in this third phase. Desquite ore deposit is located approximately 7.5 kilometers to the northwest of area.

## 3-2-1 Diamante Ore Deposit

The Diamante ore deposit is the ore in which the most intense mineralization has been recognized so far in this survey area. It has been worked continuously although in a small scale, for quite a long time.

Preliminary surveys were completed in the first phase of the program.

Detailed geological survey and geochemical exploration were carried out last year with diamond drilling (total length of 757.2m with 7 holes) in the second phase. Also in this third phase of the program, further works of diamond drilling were planned, in order to obtain more detailed information. Actually the diamond drilling of 8 holes was completed with the total length of 1,339.5 meters.

As the results of these works, the following informations have been obtained on the Diamante ore deposit. (cf. PL.I-15)

- (1) The Diamante ore deposit has been worked at Hormiga, Hormiga W,

  Auxiliadora, Diamante, Gualquilia Norte and S, and San Sebastian mines.

  The ore deposit is composed of two ore veins running close to each

  other in parallel in the direction of NW-SE. The extension of them is

  approximately 800 meters. (called Diamante principal vein)
- (2) In the northwest of these two ore veins, the mineral indication caught by the drill hole PD-3 and the ore vein at Homiga mine are continuous

	-	
•		

and the vein at Homiga W mine and that at Auxiliadora mine are also continuous.

- (3) The swell and pinch of the ore vein is remarkable, and intensity of the mineralization is rather dispersed.
- (4) The most enriched portion of the ore vein is found in the inner part of the tunnel, where the vein is widest with high grade ores. The extension to the depth has been caught by the drill holes of PD-6 and PD-10. However, the other portions of the ore vein are generally less wide, 30 to 80 cm, and the extension is approximately 150 to 200 meters.
- (5) The most abundant ore minerals recognized in the ore veins are pyrite and arsenopyrite. They are associated with less amount of sphalerite, chalcopyrite and galena. Tetrahedrite, bismuth-antimony minerals and silver minerals are also recognized though slightly.
- (6) Gold is recognized as electrum in quartz and arsenopyrite as well as in the space among the grains of sulphide minerals. The grain size of electrum is in the order of 0.0X mm.
- (7) The wall rock is composed of tuff breccia and basaltic andesite. The latter is found mainly in the southern part. There seems no genetical relation between wall rock and the enriched portion of the ore vein.

  Sericitization, montmorillonitization and silicification are observed near the ore vein (10 cm to 50 cm).

## 3-2-2 Marina Ore Deposit

The Marina ore deposit is located about 300 meters east of the Diamante main ore vein, and runs in parallel to it. There are many mines on the banks of the small stream. All of them are hand-picking workings and are down to the depth of less than 100 meters below surface. Location of ore veins and sampling points as well as assay values are shown in Fig. I-8. The general

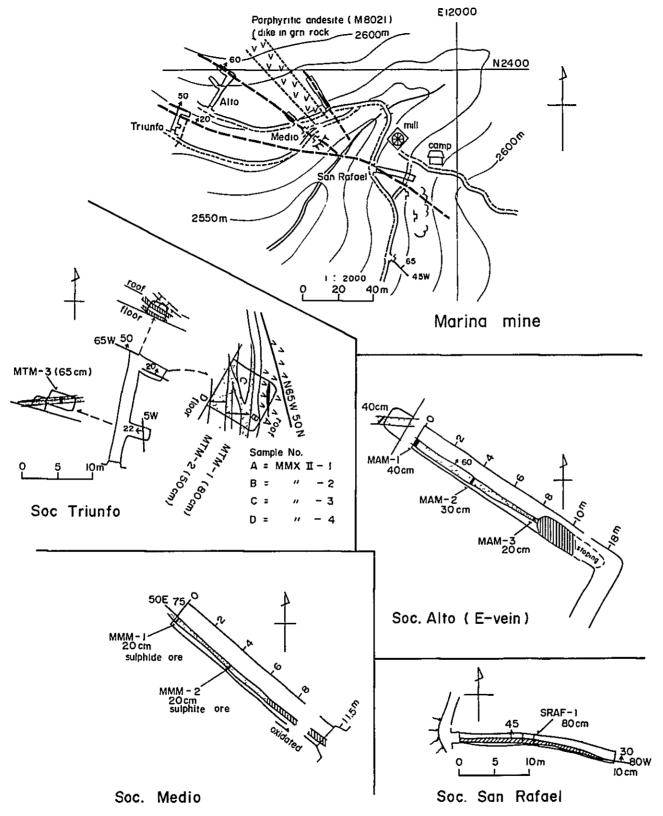


Fig. I - 8 Vein and Sampling Location of Marina Mine

Analysis of ore

- Huly 313						
Sample No.	Au (9/t)	Ag (9/1)	Cu (%)	Pb (%)	Zn (%)	As (%)
MTM- I (80)	tr	tr	1.03	0 0 6	0 09	0 41
MTM-2 (50)	10.8	47	008	0.23	0 59	0.76
MTM- 3	tr	tr	0 0 3	003	0 04	0.39
MAM - I (40)	26	21	005	80.0	0.04	2.32
MAM- 2	2 3	15	011	0 09	0.15	2.12
MAM- 3 (20)	8.2	39	008	107	018	2.67
MMM - 1 (20)	7 2	40	012	0.21	0.90	6 24
MMM- 2 (20)	11.4	112	0.2	0.56	110	613
ARAF-1 (80)	<sup>.X.</sup> ! 7.6	56	0.04	0.40	0 04	9.4

X analyzed in 2nd phase

Study of alteration minerals

Sample No	X-ray	diffrac	tive an	alysis	As	Sb %	Si	Ca	S
	Ser	Mon	Као	Oth	%		%		%
I -II XMM	L	М	S		012	0.03	3463	040	0 01
" –2	L	М	s		0.07	0.02	37.96	0.29	0.01
" -3	С			s?	119	0 03	35.39	0.06	0 05
4	L	L		V	0.39	0.04	2849	057	0.02

Ser Sericite, Mon montmorillonite Kao. Kaolin, Oth : Plagioclase trend of the ore veins is NW-SE, but varies from N 30°W to N 80°W, while the dip of the ore veins varies 20 to 75 degrees to the northeast. The maximum width of the ore veins recognized so far is 130 cm (at the working of Soc. Triunfo), but swelling and pinching are remarkable. Lateral extension of the ore veins is approximately 70 meters and the depth is 10 to 20 meters, so far ascertained. The ore deposit is in clay, oxidized and brown in color in the shallow part but in the inner part of the mine it is quartz vein with sulphide minerals.

The ore grade is as follows.

Au : tr - 17.6 g/t (average 7.5 g/t, 8 samples)

Ag : tr - 112 g/t (average 41 g/t, 8 samples)

Ag/Au ratio : 3.2 - 9.8 (average 6.1, 7 samples)

Cu : less than 0.2%

Pb. Zn : less than 1.1%

As: 0.41 - 9.4% (average 3.74%, 8 samples)

The grade of gold is comparatively high and stable. It is notable that more than 2% of arsenic is detected in auriferous ore vein, usually.

By the observation under microscope, it has been clarified that the ore minerals are mainly pyrite and arsenopyrite with sphalerite, chalcopyrite, galena and tetrahedrite, associated with very small amount of electrum, and that some of the copper minerals are replaced to covelline. Pyrite and arsenopyrite are thought to have been crystallized in early stage. Sphalerite and chalcopyrite are recognized on the corroded surface of the crystals of pyrite and arsenopyrite. Tetrahedrite is the youngest as it is observed to have cut the crystals of sphalerite and chalcopyrite. Electrum is found in aggregation of small grains less than 100 microns in diameter, contained in arsenopyrite grains (MM2A).

#### 3-2-3 Gitana Segunda Ore Deposit

The Gitana Segunda ore deposit is located about 500 meters northwest of the Marina ore deposit, and it is thought that the both ore deposits are in the same mineralized zone. This Gitana Segunda ore deposit has been worked in small scale. Location of the ore veins and sampling points as well as assay values are shown in Fig. I-9. The width of the mineralized zone is approximately 120 meters and four ore veins have been found in it. Gold has been detected from all of the four ore veins where the assay samples were collected in the survey (Au: 2.0 - 11.8 g/t, arithmetic mean of 4 ore veins is 6.3 g/t).

The trend of ore veins is N34° - 50°W, but they have various dip from gentle 45°E to steep 70°E. The width is 10 to 60 cm. In some places it swells up to more than 1 meter, by the observation of the mined out space, but generally the width is about 50 cm. The wall rock is non-stratified green tuff breccia. The ore deposit is composed of one or several quartz veins contained in clayey portion. As the ore veins are situated near the surface, they are white to brown in color, oxidized severely and primary sulphide minerals are rarely observed.

# 3-2-4 Mineral Indications in the Northwestern Extension of the Gitana Mining Area

This area is located at the neighbour of the Diamante mining area investigated in the second phase of the program.

Covered with thick vegetation, rock exposures are limited to along main rivers and streams. Almost whole of the area is underlain by dark green basaltic andesite, although siliceous shales are distributed, occupying small area, in the northwestern corner of this area.

The only indication found in this area is the ore vein in the Gitana

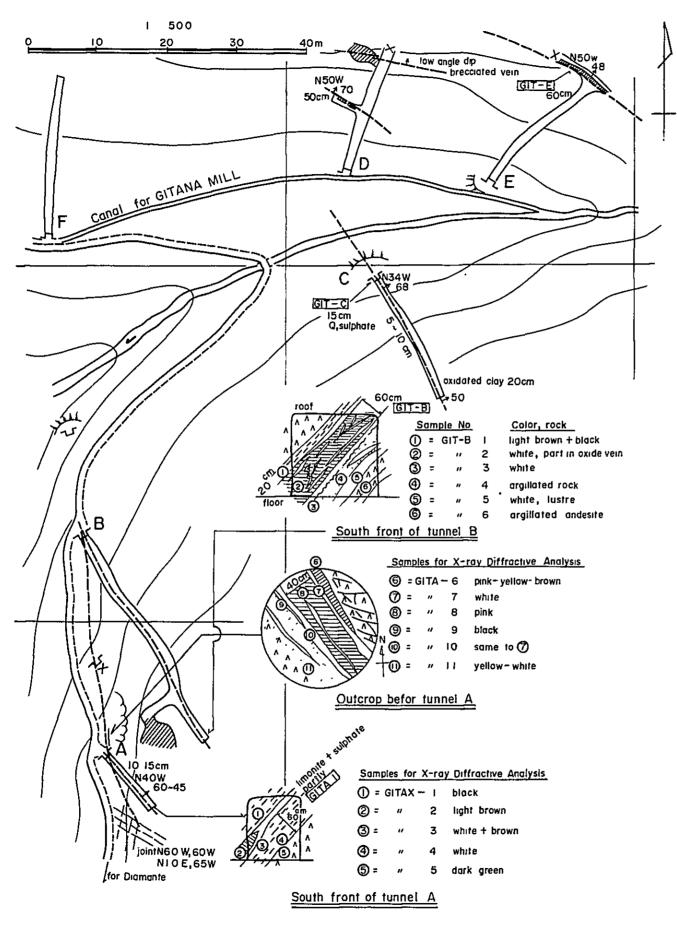


Fig. I-9 Vein and Sampling Location of Gitana II Mine

Analysis of ore

Sample No (width cm)	Au 9/†	Ag 9/1	Cu (%)	Pb (%)	Zn (%)	As (%)
GITA-1 (15)	9.4	53	017	007	007	0.76
GIT - B (60)	2.1	13	0.09	0.04	0.05	1.99
GIT - C	811	114	0.98	0.07	0.14	1.45
GIT - E (60)	20	34	007	005	017	2.07

Study of alteration minerals

Oldey o		411011									
C10	Na	X-ray	diffra	ctive	analysi	s	As	Sb	Si	Ça	S
Sample	No	Ser	Mom	Kao	Ana	Oth	(%)	(%)	(%)	1%)	1%
GTAX -	- 0 1	С		С	S		0.19	0 03	35 60	0 18	002
tı .	02	С	С	L	S		010	0 01	47 46	0 15	001
Ħ	03	V	С		S		800	0 01	4008	008	001
" "	04	V			L		010	0 01	50 98	011	0 005
#	05					М	024	0.04	39 59	2 66	0 03
11	06	С	С	L	s		005	0.03	44 96	0 16	001
tt.	07	С	С		L		0 07	0.02	32 81	0 16	0.0
"	08	s		V	1		009	0.02	41 67	0.16	00
11	09	s				S,M	0.06	0.02	37.33	010	0.0
"	10	С	С	L	L		003	002	71 41	0 22	0.0
n	1 !	С	С	L	s		0.02	0 01	43.83	019	0.005
GITBX ·	- 01	s			T	L	0.36	0 03	42.94	0.26	0.02
u	02	М			s		008	001	5470	010	0 003
"	03	L	М	М	s		019	0.03	2960	0.28	00
"	04			1		M	015	004	39 12	0 40	0.02
"	05	L	М	С	S		006	003	2589	0.32	00
11	06		1			М	021	004	2506	1 72	002

X-ray Diffractive Analysis

V'very much > M: much > C: common > L less >

S scarcely

Ser : Sericite, Mon : montmorillonite, Kao : kao lin

Ana, anatase

Oth: others GITAX-05 --- plagioclase, hornblende,

phlogopite are M, chlorite is S

GITAX-09---- chlorite is S, halloysite is M

GITBX-OI,--- hornblende is S, chlorite and loughlimite are L

GITBX - 04---- loughlinite is M

GITBX-06---hornblende and loughlinite are M.

No. 1 mine, which was described in the report of the survey in the second phase of the program. The width of the vein is 20 cm, the trend is N70°W and the dip is 70°N. Assay results are Au: 1.2 g/t, Ag: 40 g/t, As: 11.7%, and Cu, Pb Zn are less than 0.1% respectively.

By the results of the geochemical exploration carried out in this phase of the program, five anomalies have been detected. (PL. I-11)

Among them, the anomaly 2D is located along the northwestern extension of the above-mentioned ore vein, and it is thought that the area represented by this anomaly would be favorable for the emplacement of ore deposit. It is also thought that the anomalies of 2A and 2B would warrant further exploration as they are superior both in sizes and in grade of values.

#### 3-2-5 Desquite Ore Deposit

The Desquite ore deposit is located on the right bank of the Telembi river in its upstream area. The main access to the ore deposit is horse path, which goes along the east bank of La Cruz river (a branch of Telembi river) after passing the western ridge from Guachavez. The ore deposit has been worked in small scale by underground hand picking, by crushing ore with mill, and by amalgamation. As only a few people are working so intermittently, production is less than 1 ton per day in average. The trend of the ore vein is N40°W and the dip is 70°NE. The width varies 4 to 40 cm. Lateral extension of the ore vein is more than 30 meters. Vertical extension is not certain as the shafts are collapsed and filled with water. The wall rock is argillized and reddish brown in color, owing to the duplication of weathering from the surface and the alteration at the time of mineralization to form the ore veins. The underground is timbered.

The assay results of the three samples collected along the ore vein in the underground are as follows.

Sample No.	Width	Au (g/t)	Ag (g/t)	Cu (%)	Pb(%)	Zn (%)	As(%)
N-9	10 cm	5.1	9	0.00	0.05	0.06	0.03
N-10	15	tr	tr	0.00	0.02	0.03	0.02
N-11	15	tr	tr	0.00	0.03	0.05	0.02

The samples for these assay were collected from gossaneous quartz vein.

The ore minerals are not recognized with naked eyes. A sample N-14 collected from the ore pile was examined under microscope. This sample reveals that sphalerite is left unoxidized. It contains spotted chalcopyrite grains.

By the geochemical exploration, a zinc anomaly has been detected around this ore deposit, extending about 700 meters with approximate width of 100 meters, and it can be said that the distribution of the anomaly is corresponding quite well with that of the ore vein.

## 3-3 Mineralized Zone in the Central Area

## 3-3-1 Mineral Indications in the Paraiso Area

Paraiso is located near the junction of Telembi River and Q. Cerro, where the topographical feature is gentle at the altitude of about 2,000 meters above sea level. The access to Paraiso area is only by the unsealed road 3 to 4 meters wide. Going over the mountain pass 3,200 meters above sea level, from Guachavez, it runs to Eden through Paraiso along the Telembi River. Eden is in the downstream area of Paraiso. As vehicles are not passable along this road, it is necessary to go on foot, which requires about 6 hours from Guachavez to Paraiso. There are three houses along the road, and some cultivated fields where corns and lulo are mainly grown are found in Paraiso area. Also there are some pastures for horses and cows. However, most of the mountainous, land is left as jungles, undeveloped.

Indications of mineralization have been found in the following eight areas. Most of them are only exposures of mineralization, although some of

the mineral indications are known to have been worked.

- (1) San Antonio
- (2) Ruidosa
- (3) San Luis
- (4) Q. Lulo
- (5) Upstream of Q. Oso
- (6) Branch of Q. Oso
- (7) Western end of the geochemical survey line D-6
- (8) Point RM-5 and point RM-2 along the middle-stream of Q.2

  Description on the individual mineral indication is given as follows.
- (1) San Antonio

The ore deposit, situated 1 km west of Paraiso, has been worked most prosperously in this area, and on the gentle eastern slope a depression like basin has been left after the mining, in scale of 90m in east-west and 25m in north-south. The ore vein is observed on the central part of the wall along the north side of the basin. The report of the survey in the second phase of the program says that there are two ore veins of the directions of N5°W and N24°W within the mineralized zone of the approximate width of 300 cm and that the assay results are Au: 4.6 g/t and Ag: 5 g/t (Exposure is not observable in this survey because of the wall collapse). A mill for cleaning ores is found in the vicinity of the outcrop, but it is not operated. White to brown argillized zone about 8 meters wide is seen around the ore veins. Samples (N63 A, B, C) collected from the ore pile were examined under microscope, and the result is that arsenopyrite, magnetite, chalcopyrite and electrum are recognized as the ore minerals, with the secondary minerals of iron hydrates and covelline. Electrum, 20 to 30 microns in diameter, is usually found by itself or along cracks in arsenopyrite grains.

## (2) Ruidosa

This mineral indication is located along a branch stream of Q.1N, about 300 meters southwest of the San Antonio mineral indication. It has been worked in a small scale by hand picking. The ore vein has the width of 2.5 meters. The trend of the ore vein is N40°W and the dip is 50°SW. The assay results are as follows.

The ore vein is composed of severely sericitized and kaolinized white argillaceous vein containing thin quartz veinlets.

A small outcrop of mineralization is found about 130 meters downstream, which has been worked, too. The ore deposit is white argillized vein, 20 cm in width, trending N60°W, with the dip of 10°N. The wall rock is granodiorite, which contains small gossaneous veins. By panning the clay collected from this argillized vein, small grains of gold as well as oxidized pyrite, arsenopyrite, pyrite, magnetite, quartz etc. are detected.

## (3) San Luis

This mineral indication is located about 1.5 kilometers west-south-west of the indication at San Antonio. Three ore veins are observed in the width of 3 meters along the left bank of a stream. A working tunnel as far as 5 meters was driven following the neighbouring two ore veins. Width, trend and dip of the ore veins are as follows.

Ore vein	Width	Trend	Dip	Sample
No. 1 interval	30 cm 80	и30°พ	65°SW	N54 P-SL-1
No. 2 interval	40 150	W°0EN	65°sw	N-56 (100 cm in footwall of No. 2 ore vein)
No. 3	10	N35°W	vertica	1

The assay results are as follows.

Sample	Width	Au (g/t)	Ag (g/t)	Cu(%)	Pb(%)	Zn (%)	As (%)	
P-SL-1	170 cm	4.8	9	-	-	-	-	
N-54	80	tr	tr	0.03	0.14	0.03	0.32	
N-56	100	tr	tr	0.00	0.04	0.03	0.12	

The ore deposit is composed of severely silicified vein the central belt of which is gossaneous and dark brown, while the surrounding outer belt is whitish clay. The outermost part, about 3 cm wide, is also clay in chocolate color. The wall rocks are altered, and many small veins of limonite are contained. By the microscopic observation of the ore samples (N-57A, B, C) chalcopyrite, tetrahedrite, sphalerite, galena, arsenopyrite and pyrite are recognized as ore minerals. The margin zone of galena has been replaced by cerussite, and pyrite has been changed to limonite.

An argillaceous quartz vein, 5 cm wide, of the trend of N30°W and the dip of 30°SW has been found about 200 meters southwest in the direction of extension of the above ore vein. The assay results of the sample collected from the outcrop of this quartz vein are as follows.

Sample Width Au (g/t) Ag (g/t) Cu(%) Pb(%) Zn(%) As(%)
N-51 5 cm tr tr 0.04 0.12 0.05 0.33

Along a stream about 100 meters east of this quartz vein, there is another quartz vein running in parallel. It is argillaceous quartz vein with brownish limonitic gossan, with the width of 50 cm. It trends in N50°W with the dip of 85°NE. The assay results of the sample collected from the outcrop of this quartz vein are as follows.

Sample Width Au (g/t) Ag (g/t) Cu(%) Pb(%) Zn(%) As(%)
N-3 50 cm tr tr 0.01 0.02 0.01 0.02

## (4) Q. Lulo

This mineral indication is located along the small stream flowing in the fields between Guachavez-Eden road and Telembi river. On the floor and along the right bank of this stream four brownish gossaneous quartz veins each of which is 10 cm wide, are observed within the width of 1 meter. White argillization is recognized to the extent of 10 to 30 cm around the quartz vein. The trend of this quartz vein is N65°W and the dip is 80°N. The vein is barren by the assay results shown as follows.

Sample Width Au (g/t) Ag (g/t) Cu(%) Pb(%) Zn(%) As(%)

P-L-1
(whole vein) 120 cm tr tr - - 
N-73 10 tr tr 0.00 0.00 0.00 0.01

## (5) Upstream of Q. Oso

This mineral indication is located on the cutting face of the water path which is introduced from Q. Oso for the mining at the San Antonio mine. Within the width of 7 meters on the exposed surface, three parallel veins are observed. They are 5 to 10 cm wide and are trending N50°W, with the dip of 85°NE. The wall rock is weathered coarse grained granodiorite. The main vein is as wide as 10 cm. To the extent of 30 cm in both the footwall and the hanging wall of this main vein, alteration of the wall rock is recognized. In the neighbouring zone of the ore vein, sericitization is remarkable, while the outer zone is sericite-kaoline zone. Because only slight mineralization is recognized, no sample for assay has been collected.

#### (6) Branch of Q. Oso

This mineral indication is loacted along the stream about 450 meters from Ruidosa, on the southeastern extension of aforementioned San

Antonio and Ruidosa indications. There are two indications. The ore is found as vein on the right bank of the junction of the streams. The width of this vein is 80 cm and the trend is N80°W with the dip of 80°N. The other indication is recognized on the right bank 18 meters upstream from the former. There are two parallel veins. They are 10 cm wide. Their trends are N20°W with the dip of 80°W and N30°W with the dip of 75°W, respectively. Each of them is limonitic gossaneous and argillaceous quartz vein, and whitish clay is recognized to the extent of about 10 cm in the wall rock around the veins. Because of the slight mineralization, no sample has been collected for assay.

- (7) Western end of the geochemical survey line D-6

  This is an indication represented by a gossaneous float containing sulphide minerals, about 1 meter in diameter. This float was found near ridge and it is thought that the site of the original exposure would not be far from the float.
- (8) Along the middle-stream of Q.2 (sample No. RM-5, RM-2)

  Two mineral indications are found along the middle-stream of Q.2.

  The one is located near the Guachavez-Eden road and a short working tunnel is seen excavated toward the west on the left bank of the stream (RM-5). It seems that the tunnel followed an ore vein of E-W trend, but details are not certain because of the heavy weathering.

  The other is found along the stream about 400 meters upstream of the location of the above-mentioned indication. This ore vein is gossaneous and argillaceous quartz vein. It is vertical and is 10 cm wide. Its trend is N45°W (RM-2). The assay results of the samples collected from the respective exposure are barren, as shown below.

Sample	Au(g/t)	Ag(g/t)	Cu(%)	Pb(%)	Zn (%)	As (%)
RM-5	tr	tr	0.01	0.05	0.04	0.04
RM-2 (10cm)	tr	tr	0.00	0.00	0.10	0.01

The geochemically anomalous area detected by the geochemical exploration in the Paraiso area contain all the known mineral indications and ore deposits. It shows that the geochemical anomalies are reflecting mineralizations quite remarkably. Therefore, it is thought that those anomalies where no mineral indication has been found yet (anomaly 8.9 ---PL.I-9) would have high potentiality for the mineralization to be emplaced.

## 3-3-2 Delicia Ore Deposit

The Delicia ore deposit is located about 2 kilometers south of Paraiso, on the left bank of Q.Del Cerro, a branch of the Telembi river. The access to the mine is by the mountain path along the left bank of Q. Del Cerro, after branched from the Guachevez-Eden road.

Geologically, fine grained porphyritic granodiorite is distributed in the high land, while moderate to coarse grained leucocratic granodiorite occupies the low land. The border of the distribution of these two rocks is approximately at the altitude of 2,400 meters above sea level.

There are two old workings with the approximate distance of 100 meters along the small stream. The one old working, located close to D-18, is found in the granodiorite, in which iron oxides are recognized along joints and fissures. It is said that an argillaceous zone containing small quartz veins was worked and that some gold was produced. Although the mineralized zone is said to be running in NW-SE direction with the dip to NE, it is impossible to have a look at the ore vein at present, as it has been mined out. On the floor of the stream about 30 meters upstream from this point, a quartz

vein, 5 cm wide, is found (N-20). Its trend is N70°W with the dip of 40°SW. The assay results of a sample collected from this quartz vein are as follows:

Au(g/t) Ag(g/t) Cu(%) Pb(%) 
$$Zn(%)$$
 As(%)  
tr tr 0.006 0.01 0.01 0.11

The footwall of this quartz vein is white to brown argillaceous zone, 10 to 20 cm thick, and weathered granodiorite appears to the next. There are old trenchings between this quartz vein and the old workings, and several floats of the size of 40 cm in diameter, composed of quartz vein, are observed in the stream.

### 3-3-3 Mineral Indication Along Q.3

Within the width of 40 meters along the right bank of Q.3, four quartz veins carrying limonitic gossan are observed. They are named RM-8B, RM-8A, RM-9 and RM-10 from the downstream. On the left bank about 50 meters upstream from the point of RM-10, a land slide is seen with the approximate width of 8 meters. The site carries gossans of brown iron oxides in whitish clay zone. (This is named RM-11) Trend, dip, width and grade of the quartz veins found along this Q.3 are as follows.

						Assay Results						
		(cm)				Au g/t	Ag g/t	Cu(%)	Pb(%)	Zn (%)	As (%)	
RM-8	RM-8	float	t in st	ream		tr	tr	0.00	0.00	0.00	0.08	
RM-8B	RM-8B	32	N30°W	50°NE	*	tr	tr	0.00	0.00	0.00	0.04	
RM-8B	N-21	6	N30°W	50°NE	**	tr	tr	0.01	0.01	0.03	0.06	
RM-8A	RM-8A	35	N50°W	50°NE	*	tr	tr	0.00	0.00	0.00	0.03	
RM-8A	N-23	20	N50°W	50°ne	**	tr	tr	0.01	0.01	0.03	0.29	
RM-9	RM-9	15	N45°W	vert.		tr	tr	0.02	0.01	0.01	0.17	
RM-10	RM-10	20	N65°W	60°NE	***	2.6	3	0.01	0.01	0.01	0.05	
RM-10	N-26	55	N65°W	60°NE	*	7.3	7	0.01	0.01	0.01	0.07	
RM-11	RM-11	80	N25°W	40°SW		3.0	18	0.00	0.00	0.00	0.02	
RM-11	N-27	200	white	clay zo	one	tr	tr	0.00	0.00	0.00	0.02	
* whole	* whole vein ** both margins *** footwall margin											

Generally, these ore veins are running in NW-SE direction with the dip to NE, and the width is 15 to 55 cm. In most of the veins, marginal belt is composed of brown argillaceous zone and small quartz veins (2 to 3 cm wide) while the central belt is composed of white to yellowish brown clay zone (RM-8A, RM-8B). The wall rock of the ore veins is mostly weathered granodiorite which has not been mineralized. Because of the weathering, it is difficult to determine ore minerals except for brown iron-hydrate, which is thought to have replaced sulphide minerals. Clay minerals are mostly sericite and kaoline. Chlorite is not recognized.

At the approximate altitude of 2,200 meters above sea level along the Q.3N, a branch of Q.3 flowing on the right bank of Q.3, a mineral indication of vein type has been found. The width of this ore vein is 5 cm. Its trend is N60°W with the dip of 65°NE. Composing minerals are pyrite and quartz. The wall rock of the ore vein is granodiorite in which fissilities are well developed in parallel to the ore vein. Almost no alteration associated with mineralization has been recognized in this granodiorite. The assay results of the sample collected from this ore vein are as follows.

width Ag(g/t) Ag(g/t) Cu(%) Pb(%) Zn(%) As(%)
N-32 5 cm 1.8 6 0.00 0.04 0.01 0.69

## 3-3-4 Mineral Indication at Jarol

This mineral indication is located about 250 meters southeast of the junction of the Guachavez-Eden road and the mountain path to Delicia. The indication lies on the floor of a stream flowing toward northwest. It is as wide as a little over 1.2 meters. The trend is N35° to 60°W with the dip of 60°NE. It is composed of white or reddish brown argillaceous vein (N-35). An argillized quartz vein is found at the point 22 meters southeast of the above mineral indication (N-39).

The assay results of the samples collected from these indications are as follows.

As the results of the geochemical exploration, three geochemical a anomalies, 10, 11 and 12 (PL. I-8), are extracted in the area where the central mineralized zone is located. The anomaly 10 includes ore deposits along Q.3, and the northwestern extension is possibly continued to the anomaly 8. The anomaly 11 includes Delicia ore veins in its southeastern part and Q.3 N ore veins in its northwestern part. This anomaly 11 extends approximately 2,000 meters with the width of 400 meters, and it is thought that this anomaly would be quite favorable for the emplacement of ore deposits so as to warrant further exploration. As the size of the anomaly 12 is smaller comparatively, it is better to give priority of exploration to the anomaly 10 and 11.

#### 3-4 Mineralized Zone in the Western Area

# 3-4-1 Mineral Indications in the Northwestern Extension of Bombona Mining Area

This mineral indications occupy a drainage basin of the Bombona River, which is flowing toward the northwest, and are thought to correspond with the northwestern extension of the Bombona mineralization zone, investigated in the second phase of the program.

The land is unfrequented, covered with vegetation of high bomboos and tall trees. Although it is possible to reach the Bombona mine in a little more than 6 hours on the horseback from Guachavez, it is necessary to open a new path by bush-cutting to enter further.

Geologically, the land is underlain by the granodiorite containing about 20% of hypidiomorphic hornblende and biotite, 5 to 10 mm in diameter. Exposure is poor because of thick soil and thick vegetation. No other mineral indications have been recognized than those found at several spots along Q.18, close to the Bombona bajo ore deposit, which were investigated by the survey in the second phase of the program. The ore veins along Q.18 are variably trending from N45°W to EW with the dip of 48°NE to 80°SW, although general trend is NW-SE. Given in Fig. I-10 are the mapped data of the four mineral indications found in the area of middle to upstream of Q.18. These indications are represented by the exposures of vein-type ore deposits. Although an old working tunnel, impossible to step in owing to collapse of the entrance, is found on the other bank of the stream against the mineral indication 3, there is no other exposure of mineralization which seems to have been worked. The indications 1 and 2 are thought to be different portions of the same ore vein, lying on the both banks of a stream. However, their trend and dips are twisted as seen in 1 : N70°W, 80°S and in 2 : N60°W, 50°N. The indications of 3 and 4 are located about 200 meters upstream. They are spaced by 20 meters each other. Trend and dip of the indication 3 are N46°W, B0°NE and those of the indication 4 are N60°W, 48°SW.

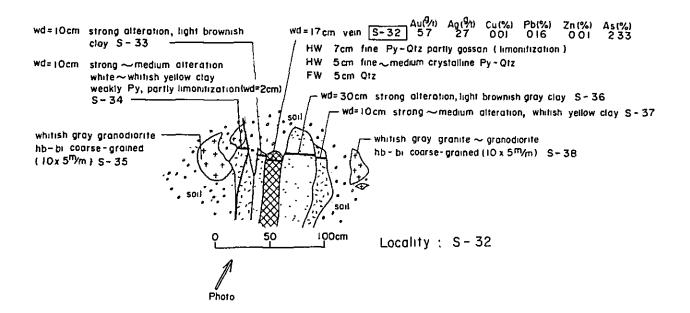
The ores are composed of chalcopyrite-pyrite-quartz vein, but they are gossaneous, reddish brown in color, by oxidation. The ore grades of these mineral indications are as follows.

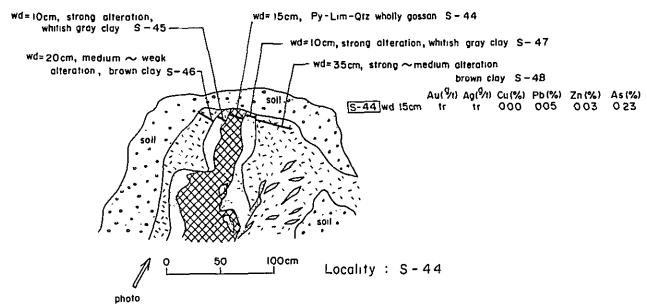
Indi- cation	Sample No.	Width cm	Ag(g/t)	Ag(g/t)	Grade Cu(%)	Pb(%)	Zn (%)	As(%)
1	S-32	15	5.7	27	0.01	0.16	0.01	2.33
2	S-39	35	43.6	1144	0.28	0.44	0.06	3.09
3	S-49	80	0.7	7	0.00	0.01	0.00	0.27
4	S-44	15	tr	tr	0.00	0.05	0.03	0.03

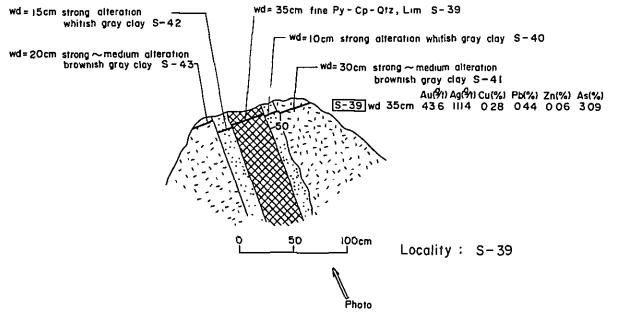


Zonal structure is recognized with the wall rock alteration by the mineralization of the ore veins. It is represented, from the inner part to outer, by white to pale brown clay zone (10 to 30 cm), yellowish clay zone (10 to 50 cm) and weathered granodiorite zone, which are evident with naked eyes. The zonal structure of the minerals is also recognized by the results of the X-ray diffraction of the samples (S-32 to S-38) collected from the mineral indication 1. The structure is symmetrical around the ore vein (S-32). That is, the ore vein and its immediate next zone are rich in sericite. Montrorillonite is associated with sericite except in the ore vein. The outer zone is chloritized to some extent but mostly this zone is composed of non-altered wall rock, bearing fresh hornblende.

As the results of the geochemical exploration in this area, two anomalous zones running in parallel eachother have been extracted. One anomalous zone includes anomaly 14(B) and 14(C), which are along the extension of the known ore veins, while the other anomalous zone includes anomalies 13 and 14(A). It is recommended to start exploration works from the anomalous zone along the extension of the known ore deposits. It is desirable to expand the works to other unexplored areas after obtaining information on the character of ore veins.







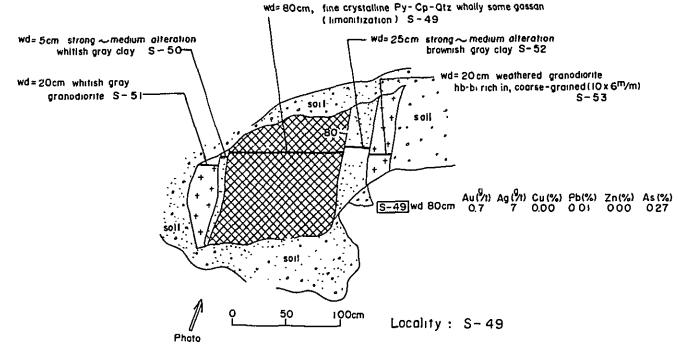


Fig. I-10 Outcrop Sketch Found at the Bank of Q.18 in Bombona Area

Table I-5 List of Veins Diamante-Paraiso-Bombona

Location		Vein				Assay grade							
Name	Position	Strike	Dip	Width (m)	Description	Sample No.	Αυ (g/t)	Ag (g/t)	3.8	Pb (Z)	Žn (X)	As (2)	Remarks
Mina Desquita	D-21A~D21B	NAOW	70N	D.10	Clayey Quartz	N-9	5.1	9	0.00	D.05	0.06	0.03	
		140W	70N	D.15	Clayey Quartz	N-10	tr					0.02	
Desquite	D-23~D-24	N40W N35W	70N 85N	0.15	Clayey Quartz Pyrite Quartz	N-11 S-9	tr	tr	0.00	0.00	0.00	0.04	
needarra .	Q. 6	11.554	03.1		Silicified Shale (grab sample)		tr	tr	0.01	0.00	0.00	0.02	
San Luis	D-3~D-4	N30H	655	0,30		N-53					۱		
" "		N3OH	655	0.80	Clayey	N-54 N-55	tr	tr	0.03	0.14	[0.03	0.32	
n i		WOLE	933	1.00	Clayey	N-56	tr	tr	0.00	0.04	0.03	0.12	
ę,	D-4~D-5	N50W	85N	0.50	Clayey Quartz	N-3	tr	tr	0.01	0.02	0.01	0.02	
San Luis	D-4~D-5	N60E	5 ?	0.30		N-50				•			
(Cristales) San Luis	D-4~D-5	NOON	30s	0.05	Clayey Quartz	N-51	tr	tr	0.04	0.12	0.05	lo. 22 l	
San Antonio	D-5~D-6	N70W	705	****	Black gossan (grab sample)	HCA-1		tr	0.00	0.01	0.00	0.04	
" į		N7OW	705		Purplish clay (grab sample)	HCA-2						1.25	
Prof. Accord	D (4.2.3	N70W N40W	703	0.80	White clay (grab sample)	HCA+3 N-64	tr 6.7	149	0.13	0,00	0.01	0.01	
Ruidosa	D-6^D-7 D-7	N60W	50S 10N	0.20	Clayey	N-66A	0.7	147	0.13	0.37	0.15	0.30	
						S-2							
"						5-3			0.00				
Lulo Paraiso	D-7~D-8 D-8~Q,0sesa	N65W	805 85N	0.10	Clayey Quartz	N-73 N-58	tr	cr	0.00	0.00	0.00	10.01	
LHIETPO	D-8~Q. 1-5	NSOW	80N	0.80		N-67	Ì			1	1	<b>ì</b> i	
						N-68				İ	İ		
						N-69 N-70	i				ŀ		
Paraiso	Q. 1-S	N2OW	508	0.10		N-71							
1212130	Q. 2	N45W	90	0.10	Clayey Quartz	RH-2	tr	tr				0.01	
"	Q. 2	HW	1		Old tunnel	RH-5	tr	tr				0.04	
Delicia	Q Del cerro	N35~60W	60N	1.20	Clayey	N-33	tr	tr	0.04	0.01	0.01	0.16	
				D. 80 D. 15		N-36 N-38	i			ļ			
Delicia		NIOW	40N		Clayey Quartz	N-39	tr	tr				0.06	
: 1	Q. 3	N50W	50N		Gossan (rolling stone)	RM-8						0.08	
		N30M	50N 50N	0.35	Clayey Quarts Clayey Quarts	RH-8A RH-8B		tr				0.03	
n		N459	90	0.15	Clayey Quartz	RH-9	tr	tr	0.02	0.01	0.01	0.17	
"		N65W	60N	0.20	Clayer	RH-10	2.6	3	0.01	0.01	0.01	0.17 0.05 0.02	
"		N25W	40N	0.80	Clayey Quartz	RH-11 MR-11A	3.0	18	0.00	0.00	0 00	0.02	
		N30W	50N	0.06	Clayey Quartz	N-21	tr	tr	0.01	0.01	0.03	0.06	
"		1,50	2011		222)2) 4	N-22				Ī	l		
**		NSOW	50H	0.20	Clayey Quartz	N-23	tr	tr	0.01	0,01	0.03	0.29	
ı. ı		l			'	N-24 N-25	ł			Ì	1	<b>'</b>	
н		N65W	60N	0.55	Clayey	N-26	7.3	7	0.01	0.01	0.01	0.07	
"				2.00	Clayey	N-27	tr	tr	0.00	0.00	0.00	0.02	
	0.3.12	ME D.		(8.0+)		N-32	1.3	6		0.04		1 :	
	Q, 3-N Q, 4	N6OW NW	65N	0.05	Pyrite, Quartz Clayey	N-32 S-16	tr	tr.	0.00	0.01	0.00	0.11	
Mina Delicia	4. 7			0.05	Quartz	N-20	tr	tr	0.06	0.01	0.01	0.11 0.11	
Bombona	Q. 18	N7OW	BOS	0.17	Pyrite, arsenopyrite, Quartz	5-32	5.7 43.6	27 1144	0.01	0.16	0.01	2.33 3.09 0.23	
		N6OW N6OW	50N 48S	0.35 0.15	Pyrite, chalcopyrite, Quartz Clayey Quartz	S-39 S-44	43.0 tr	1144 tr	0.00	0.05	0.03	0.23	
		N46W	80N	0.80	Clayey Quartz		0.7	7	0.00	0.01	0.00	0.27	
Mina Marina	tunnel	N56W		0.40	Arsenopyrite. Quartz	HAH-1	2.6	21	0.05	0.18	0.04	2.32	
	11	NS6W		0.30	Arsonopyrite, Quartz	HAH-2		15 39	0.11	10.09	0.15	2.12	
	11	NSSW NSSW	60N 50N	0.20 D.BO	Arsenopyrite,Quartz Clayey Quartz	HAM-3		11	0.01	0.06	0.09	0,41	ł
	11	N65W	50N	0.50	Clayey Quartz	MTH-2	10.8	47	0.08	0.23	0.59	0,41 2.76	ŀ
	**	NS W	22W	0.65	Clayey Quartz	HTH-3	tr	tr 40	0.03	0.03	0.04	0.39	
		NSOW	75N	0.20	Pyrite-arsonopyrite, Quartz	1001-1 1001-2	11.4	112	0.12	0.54	1.10	6,24	
Gitana	"	NSOW NAOW	75N 60-45N	0.20	Arsenopyrite, Quartz Pyrite, Quartz	GITA-1	9.4	53	0.17	0.07	0.07	6.13 0.76	1
** -	**	NSOW	48N	0.60	Clayey Quartz	GIT-E	2.0	34	0.07	0.05	0.17	2.07	
	1) ()	N34W	68N	0.60	Clayey Quartz	GIT-B		13	0.09	0.04	10.05	1.99	Ì
Gitana-NW	**	W24**	404	0.15	Arsenopyrite, Quartz Pyrite-Arsenopyrite, Quartz	YELA-1 GIT-C		36 114	0.11	0.04	0.06	5.50 14.5 0.05 0.13	
Gitanu Gitana-NV	Q 11-N	N34W N66W	68N 90	D.15	Pyrite-Arsenopyrite, Quartz Clayey Quartz	Q-1116	tr	tr	0.01	0.00	0.00	0.05	
OTC#U#-UM	Q, 11-S	EM	75N	U 3U	Clayey Quartz	Q-11536		tr	0.03	0.02	0.01	0.13	ĺ

Table I -6 Chemical Analysis of Ore Samples in 0.3 Delicia

Assay Value $Au(g/t)$ $Ag(g/t)$ $Cu(x)$ $Au(y)$ $Au(y)$ $Au(y)$ $Au(y)$ $Au(y)$ $Au(y)$	0.00 0.00 0.00 0.08	0.00 0.00 0.00 0.01	0.01 0.01 0.03 0.06	0.00 0.00 0.00 0.03	0.01 0.01 0.03 0.29		0.02 0.01 0.01 0.17	0.01 0.01	0.01 0.01	0.01 0.01
A <u>g/t)</u> <u>Ag(g/t)</u> <u>C</u>	tr	r T	ri Fr	r tr	r tr		r tr	S.		
Remarks Au(	- tr	(1) Whole the vein tr	(2) A part of tr the vein	(1) Whole the vein tr	(2) A part of tr the vein		_ tr	rt of the	c	A part of the vein Whole the vein
Strike, Dip of the vein	I	N30°W, 50°NE	£	N50°W, 50°NE	Ξ	N45°W. Vert		N65°W, 60°NE	N65°W, 60°NE	N65°W, 60°NE " N25°W, 40°SW
Sampling Length	Float ore	32 cm	6 cm	35 сш	20 cm	15 cm		20 cm	20 cm 55 cm	20 cm 55 cm 80 cm
Sample No.	RM-8	RM-8B	N-21	RM-8A	N-23	RM-9		RM-10	RM-10 N-26	RM-10 N-26 RM-11
Locality	RM-8	RM-8B	* *	RM-8A	=	RM-9		RM-10	RM-10	RM-10 " RM-11

#### 4-1 Relation Between Geological Structure and Mineralization

The general trend of the vein-type ore deposits distributed in this survey area is NW-SE, in spite of the differences of the wall rock, may it be the green volcanic rocks or the granodiorites.

The principal directions of the lineament detected through the survey in the first phase of the program are three systems, NW-SE, NE-SW and N-S, of which the mineralization is recognized associated with NW-SE system. By the results of the various survey works carried out in this third phase of the program, especially by the results of the geochemical exploration, are caught many ore veins or mineral indications, which are grouped, as a whole, into three rows of mineralized zones running in parallel in the direction of NW-SE, spaced approximately by 3 kilometers. It is thought that the regional lineament pattern above-mentioned is representing result of the lateral pressure in E-W direction, which would have caused the basement to form combination of a pair of conjugate shear planes (NE and NW systems) and a compressed tension fracture (NS system). It is evident that extensive fault activities were there after the formation of the ore veins, because the ore veins are observed to be cut and dislocated. The stress system of the fault activities is different, to some extent, from the systems aforementioned. It is thought the reason is that the geological structure would have varied to more complicated condition regionally as time went by. Taking as an example for it the Diamante principal mineralized zone, the general trend of which is NW-SE, it can be said that this main mineralized zone has a character of sheared plane, formed by lateral E-W pressure, as the inner-structure of the veins, the series and the branching pattern of the ore veins are revealing it to be left-lateral fault. The ore vein is

composed of a combination of an almost vertical fault plane in N40°W direction and the secondarily formed and gently dipping fault plane in N70°W direction. The mineralization is recognized along these two fault planes and in the space formed in relation to the movement of these planes.

As for the relation of the wall rocks to the width and the continuity of the ore veins, it is possible to compare the Diamante ore deposits lying in the green volcanic rocks with the other ore vein, for instance Bombona ore deposit, lying in the granodiorite. The following two points of difference are noted, on the vein structure, though they would not make so remarkable difference.

- (1) Pinch and swell of the ore veins in the green volcanic rocks are more remarkable and therefore the wide portions of the ore vein would have been easily formed.
- (2) The ore veins found in the granodiorite are comparatively linear and continuous, although not so wide (they have long cycle of pinch and swell).

It seems that sulphide minerals as sphalerite, chalcopyrite, galena, etc. are more abundant in the veins of the Diamante ore deposit. However, as the reason would be the difference of local conditions, it cannot be said that this mineralogical difference would depend upon the difference of wall rocks.

# 4-2 Relation Between Igneous Activity and Mineralization

Viewing from the points that the wall rocks of the vein-type ore deposits are the Piedrancha granodiorite and the green volcanic rocks intruded by the former and that, as above-mentioned, the ore veins are running in specific direction in spite of the difference of the wall rocks, the formation of the ore veins would have been at the period when the physical properties of the granodiorite became almost similar to those of

the surrounding rocks after the intrusion and consolidation. However, it is suggested that the Piedrancha granodiorite would have some relation to the mineralization in the points of their distribution and the variation of the character of the ores, because the gold ore deposits which are distributed along the margin of the granodiorite and in the immediate outer zone of its margin, are observed to have different characteristics locally ---- that is, gold-bearing quartz veins poor in sulphide minerals are distributed in the northeastern part while most of the sulphide rich ore veins are found in the southeastern part of the granodiorite. Through the surveys for these three years, it has been clarified that the Piedrancha granodiorite varies its chemical properties from diorite to granodiorite from early stage to later one, that the diorite would have been a forerunner stretching itself in NE-SW direction, accompanying dissemination of copper and molybdenum and that the Piedrancha granodiorite is distributed in form of intrusive complex, the ages of which are from 6 to 20 million years. As the ore veins found in this survey area are observed to have cut all these intrusive rocks, it is thought that the mineralization would have been at the latest stage of the igneous activities. The granodiorite belongs to the I-type according to the chemical ingredients.

#### 4-3 Wall Rock Alteration

By the X-ray diffraction of the minerals formed by the alteration within the immediate neighbouring area of the ore veins, zonal structure is recognized symmetrically around the ore vein (Fig. I-11).

The samples N58 to N62 and S32 to S38 are collected symmetrically in the wall rocks around the two almost vertical ore veins, which are 15cm and 17 cm wide respectively. The minerals are distributed in the order of sericite-montmorillonite/kaoline-chlorite, from the central zone to the outer. Samples of GITAX 01 - 05 and GITBX 01 - 06 were collected in the underground from the vein-type ore deposit in the wall rock of the green volcanic rocks. Here also is recognized a zonal structure that montmorillonite/kaoline zone is surrounding the sericite zone which is in the center of the mineralization. An example of wall rock alteration in Kammuridake mineralized zone (in the vicinity of the Kushikino mine, Japan) is shown in Fig. I-12, in which the variation of the minerals formed by the alteration in the wall rock are described according to the distance of 0, 5, 20 meters from the ore vein. In this survey area too, sericite and kaolinite are gradually decreasing toward the outer zone, while montmorillonite is most abundant at the point 5 meters apart from the ore vein. Chlorite increases in the outer zone.

To obtain information on the chemical ingredients, Ca, Si, Sb, As and S were analyzed. The results of the analysis are showing that As values are decreasing toward the outer zone, while the maximum value is found in the ore vein, that Ca values have quite reverse tendency to those of As, and that SiO<sub>2</sub> values are high in the ore vein although they are low in the surrounding area. It is evident from the above fact that a sort of devitrification would have occurred with progressive montmorillonitization in the wall rock. Viewing from the variation of minerals formed by the alteration and from the variation of the chemical ingredients, it is evident that wall

rock alteration is confined to fairly narrow zones beside ore vein sitting in the center (within 1 meter from each ore vein in cases of N58 to 62 and S32 to 38).

Wall rock alteration observed in the cores collected through the drilling works for the Diamante main ore veins is as follows. There are severe silicification and sericitization near the ore veins, while montmorillonite is found sporadically. It can be observed with naked eyes that dark colored or dark green colored wall rocks have been turned to pale brown rocks with pale green spots. The width of the altered zone is 10 cm to 1.5 meters from the ore veins composed of quartz and clay.

#### 4-4 Ore Minerals

The most common ore minerals composing the ore veins are pyrite and arsenopyrite, followed by sphalerite. There can be found small amount of chalcopyrite, galena and tetrahedrite. As gold and silver minerals, very small amount of electrum, argentite, polybasite, pyrargyrite, freibergite and silver-bearing lead-bismuth minerals are detected. The gangue minerals are mostly quartz. Calcite veins are observed only in the floats found in the landslide area near the Desquite ore deposit.

As the occurrences of the main ore minerals are described in the survey report of the second phase of the program, occurrences of gold-silver minerals are given here.

According to the EPMA image, the Ag/Au ratio of electrum is low (rich in gold). Electrum is observed to occur in small irregular aggregates, in tabular form and in dendritic form, in the sizes of several to 100 microns. Electrum is associated with idiomorphic arsenopyrite (Sample No. MM2A, D7144: same hereinafter) and rhythmically precipitating quartz (D30B0.3). Often it fills corroded surface of pyrite (ND-17A) and irregular skeleton crystal

of arsenopyrite (MM3). It also occurs in dendritic form in small cracks (N63A). Argentite and polybasite are observed to occur in irregular shape along the crystal margin of pyrite (D6073B). Argentite is observed to compose a thin seams cutting chalcopyrite (PD1376.5). It also is found associated with cerussitization of galena (N57A). Silver-bearing lead-bismuth mineral (Ag-bearing cosalite-galenobismuthinite or gustavite series mineral) has been discovered in the sample No. PD14124.

There are many minerals recognized in the Diamante main ore veins.

Based on the results of microscopic observation, the order of the crystallization of the minerals are inferred early to later stage as follows.

- (1) Pyrite, arsenopyrite, electrum
- (2) Sphalerite, chalcopyrite, galena,
- (3) Argentiferous Pb-Bi mineral, tetrahedrite, pyrite, cerussite, proustite, argentiferous Pb-Bi mineral
- (4) Argentite, pyrargurite

Gangue minerals are mainly quartz and small amount of dolomite is recognized. Arsenopyrite is apt to take idiomorphic form as it is a mineral formed in the early stage of the mineralization. On the corroded and depressed surface of assenopyrite, sphalerite, chalcopyrite and galena are formed. Tetrahedrite occurs as thin seams cutting chalcopyrite and sphalerite and is thought to have been formed in the later stage of the mineralization. Electrum is in most cases associated with arsenopyrite and is thought to be crystallized in the early stage. Argentite and pyrargyrite are observed in fine seams, cutting chalcopyrite formed in the later stage of the mineralization.

It is characteristic that this ore veins are containing zinc of 2 to 3% and copper of 0.2 to 0.4%. In most cases, sphalerite crystale are found to include abundant chalcopyrite dots. Galena is not found so much as a whole but it sometimes contains silver minerals. Tetrahedrite is observed com-

paratively frequently along the rims of sulphide minerals or in the space between grains of minerals. Between the periods of (1)-(2) and (3)-(4), there would have been a brecciation (fault activity), breaking the already-formed crystals. The minerals of the period of (3) and (4) are recognized to have been precipitated filling small cracks formed by the fault activity.

In the Table I-7 are given correlation coefficients of the mutual relation of ingredient elements obtained from the assay results of the ores.

Table I-7 Correlation Coefficients Among Elements of Ore Vein in the Diamante-Paraiso-Bombona Area

	Au	Ag	Cu	Pb	Zn	As
Au	Х	0.82	0.29	0.41	0.11	0.31
Ag	0.82	х	0.30	0.32	-0.02	0.14
Cu	0.29	0.30	х	0.11	0.13	0.33
Pb	0.41	0.32	0.11	х	0.16	0.33
Zn	0.11	-0.02	0.13	0.16	х	0.52
As	0.31	0.14	0.33	0.33	0.52	х

It is noted that in many cases mutual relation of the elements shows positive correlation coefficient. Listed in the following the relation showing high coefficient.

relation coefficient	Eleme	nts	
0.5 - 0.8	Au-Ag	Au-Zn	
0.4	Au-Pb		
0.3	Ag-Pb	Au-As,	Au-Cu
	Ag-Cu	Cu-As,	Pb-As

It is natural that the coefficient of Au-Ag is high because of the important mineral to be electrum. But it is notable that the correlation coefficients

of the elements of Cu and Pb against those of Au and Ag are fairly high, and that, as for the elements of Pb, Zn and Cu, the relations of As-Zn, As-Cu and As-Pb have high correlation coefficient, while there is only low correlation efficient in the relation of those Cu, Pb and Zn elements one another. Taking variations of gold contents against Ag/Au ratio, from the assay results, it is obvious that they are in inverse, proportion, as shown in Fig. I-14. That is, in this survey area, there is a tendency that gold grade of the ore would be low where the Ag/Au ratio is high.

#### 4-5 Distribution of Metals in Diamante Mine

The results of drilling to the principal vein of Diamante Mine and all assay results of samples from abandoned are written in "PL. I-15 Plan and Longitudinal Section of Diamante Principal Vein". Based upon PL. I-15 the following elements were studied and the Fig. I-16, was drawn.

(1) Zoning by ratio of silver and gold

A : Ag/Au = 1 - 5, B : 6 - 15,

C : 16 - 30, D : over 31

- (2) Over 0.3% of Cu
- (3) Over 0.1% of Pb
- (4) Over 2.0% of Zn
- (5) Over 2.0% of As.

At the point where a drilling hole cuts a vein, the width of the vein, where the dip of the vein assumed to be vertical, and its gold content is written in PL. I-15 and only the veins whose width is over 0.25m and gold content is over 3 g/t are drawn with dot on the figure. The following can be pointed out in the Fig. I-16.

(1) Gold-silver ratio of the gold bonanza is in B zone, i.e., between 6 and 15. The area where gold-silver ratio is either over 15 or under 6, shows less gold content in absolute value. High grade gold ore in the adjacent parallel veins, Marina ore deposit and Gitana Segunda ore deposit, show the similar results.

- (2) The zones, where copper content is over 0.3%, are south of the Gualquilia Norte Pit and above 2,550m above sea level in the southern area and Hormiga Pit in the northern area. At the central area, 0.44% of copper is locally seen from the drilling No. PD-5.
- (3) Over 0.1% of Pb is general in the southern area and is in some area at Hormiga Pit and upper part of the central Diamante bonanza.
- (4) Distribution area of Zn over 2.0% generally coincides with the central Diamante bonanza and also is in a small scale at Gualquilia Norte Pit and its lower part, ore cut of the drilling No. PD-14.
- (5) Over 2% of As is in all the area described above (1) to (4) except the area of the zone A of gold-silver ratio and also is at the lower part of Gualquilia Norte Pit, the drilling No. PD-13.

Because the figure reflects the assay results of all the ore samples collected, the vein, which are at least two separate veins are not separately described. Furthermore, minerals are randomly distributed in veins.

Therefore, ore grade of the drilling core tends to reflect irregularity of mineral distribution.

From the indications of the figure and the known features of the ore deposit with the consideration of the above-mentioned irregularity, the genetic model of ore deposits in the area is inferred as follows.

# 4-6 Fluid Inclusion Study

(Purpose) Measurement of homogenizing temperature of fluid inclusions in quartz samples taken from drilling's cores of the Diamante mine has been conducted for studying temperature circumstance when the ore vein had formed. Determination of salinity of aqueous phase also, has been aimed at, however

it was halted because the inclusions were too small to examine.

(Preparation of sample) Twenty quartz samples were collected from drilled core, so as to make representatives for all drilling holes.

Thin sections were made in a thickness of 0.5mm or less polishing one side for microscopic observation.

(Inclusion) Inclusion's grain size is so small in all of the sample as 3 to 15  $\mu$ m, rarely up to 20  $\mu$ m. The shape of inclusions are long or short prismatic, ovoid or like a minus hexagonal crystal. Inclusions are of two phases of gaseous and aqueous. There is no three phases.

(Measurement) Equipment for measurement of temperature is LINKAM-JH600 TYPE which has a temperature rising ratio of +1°C/minute. Ten inclusions from each sample are determinated on an average.

(Results) Sample location and results of temperature measurement are shown in Fig. I-17. Six out of twenty samples did not permit determination of temperature because these inclusions were so fine and scarce to observe. But, it may be noteworthy to say that these samples are in coincidence with barren or very poor gold mineralization part.

Although it is hard to say conclusively on the genetic relation with thus obtained results because of limitted number of samples, the following may enumerate by inference:

- (a) Temperature shows a variation from 188°C to 390°C, making a predominant peak around 345°C and other small peak around 250°C.
- (b) Two examples show different temperatures although they are very close each other. (i.e. CFI-20 and 21, CFI-22 and 23) This may indicate a character of "complex ore vein" which had precipitation of minerals after faulting occurred at the later stage of mineralization.
- (c) When the temperature is high, gold content shows higher value in general. This may coincidence with the results of microscopic observa-

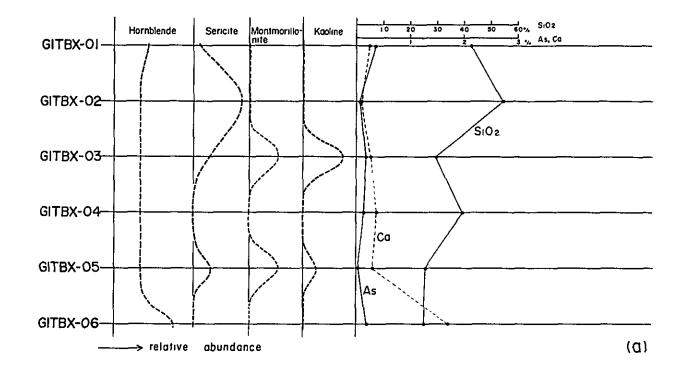
- tion of ores saying that electrum precipitated in the early stage of mineralization.
- (d) In the quartz samples from non-mineralized part, the inclusions are scarce and very fine-grained.

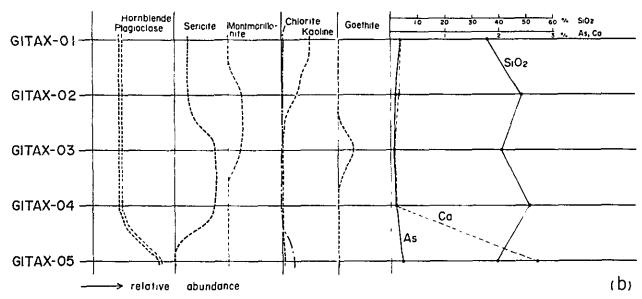
#### 4-7 Genetic Model of Ore Deposit

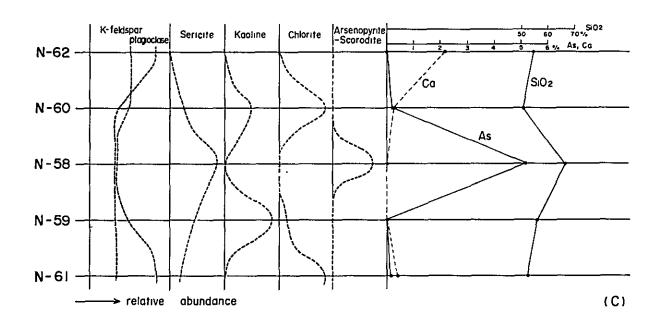
Ore deposits in the area were formed as follows.

- (1) After intrusion and consolidation of Piedrancha granodiorite, due to stress in E-W direction, shear zone was developed in NW direction in this area where the distribution of granodiorite is large. There were developed conjugate faults to NE direction, but only NW shear zones were mineralized in this area.
- (2) The shear zones of several hundred meters wide consists of groups of faults with the same direction. Some of these faults were mineralized. Vein type ore deposits were formed along main pass of ore solution through the shear zone.
- drop, encountering underground water and sudden pH change caused ore solution to crystallize and precipitate many minerals. Contents of each constituent elements of ore solution and physicochemical conditions decide minerals crystallized. The Fig. I-16 shows the zoning pattern of constituent elements in Diamante ore deposit.
- (4) The zoning pattern shows that the Au-Zn-As zone is at the center and surrounded by the Au-Zn-Pb zone and the Pb-Cu-Ag zone and has a shape like a mushroom.
- (5) Mineralized zone of the principal vein of Diamante ore deposit extends about 1,200 meters. However, gold ore zones (Au content: over 3 g/t and zone width: over 25 cm) horizontally extend rather

short, 100m to 200m because veins of the area tend to pinch and to swell. Their vertical extension is also inferred to be about 150m to 200m because their bottom is inferred not below 2,450m above sea level. (On the Fig. I-17, gold ore zone does not exist at south of the center of the figure because the drillings No. PD-11 and PD-12 did not encounter gold ore. The vein structure which was cut by these two drill holes is only an altered fracture zone. The drilling was terminated a few meters beyond cutting the vein structure and there still remains whether no mineralized zone exists beyond the terminated points of these drill holes. Because the principal vein of Diamante ore deposit consists probably of two adjacent parallel veins, there may be the southern extension of the bonanza. The distribution pattern of elements in the area is also easily interpreted that there may be the extension of the bonanza. However, we have not more data around this concerned area and the figure shows no bonanza.)







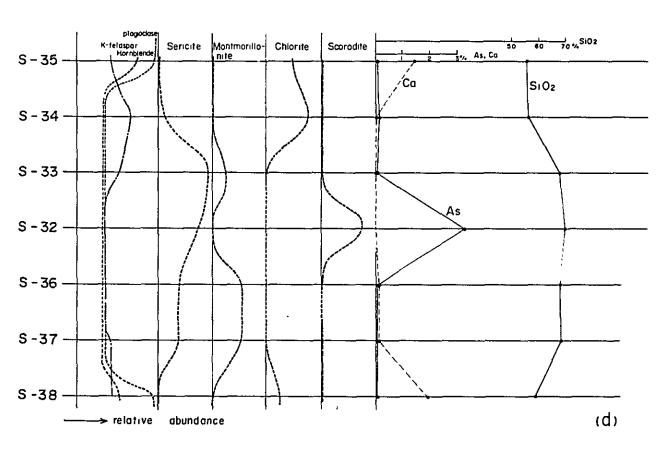
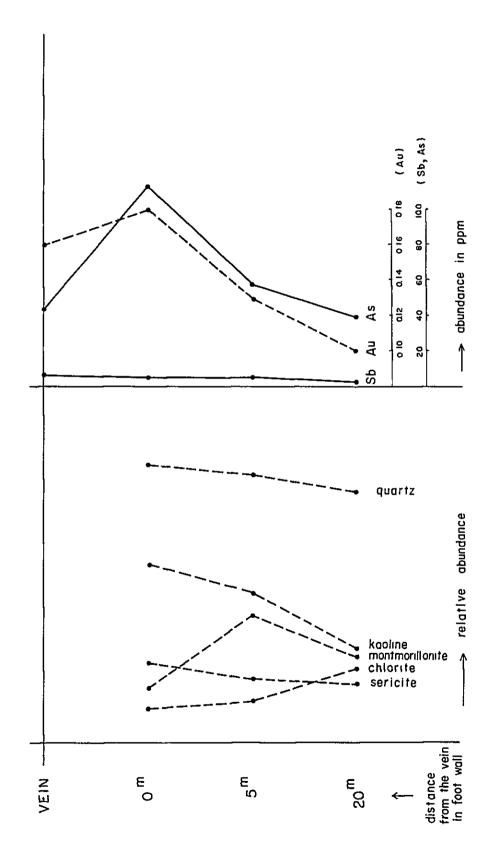


Fig. I-II Wall Rock Alteration Chart

(a)(b) Gitana Mine (c) Paraiso Area (d) Bombona — NW



MMAJ(1981) kushikino area geochemical exploration report (in Japanese)) Kanmuri -dake area, adjacent east of kushikino Au mine Rock Alteration Chart (2) Wall Fig. I- 12 ( after

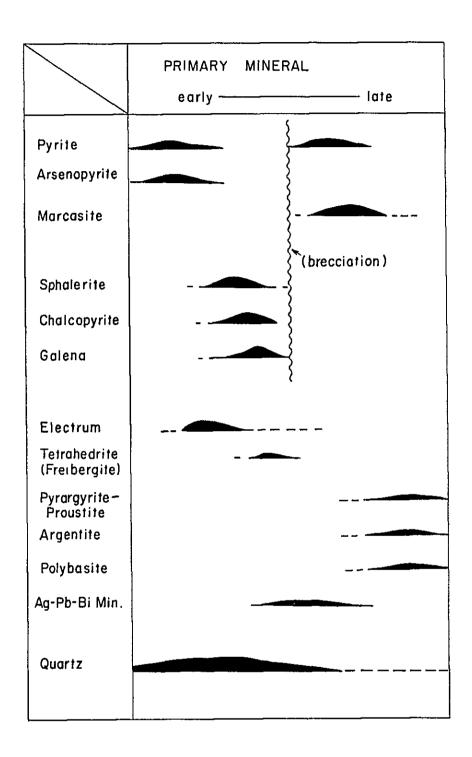


Fig. I-13 Paragenetic Sequence of Minerals in the Diamante Principal Vein



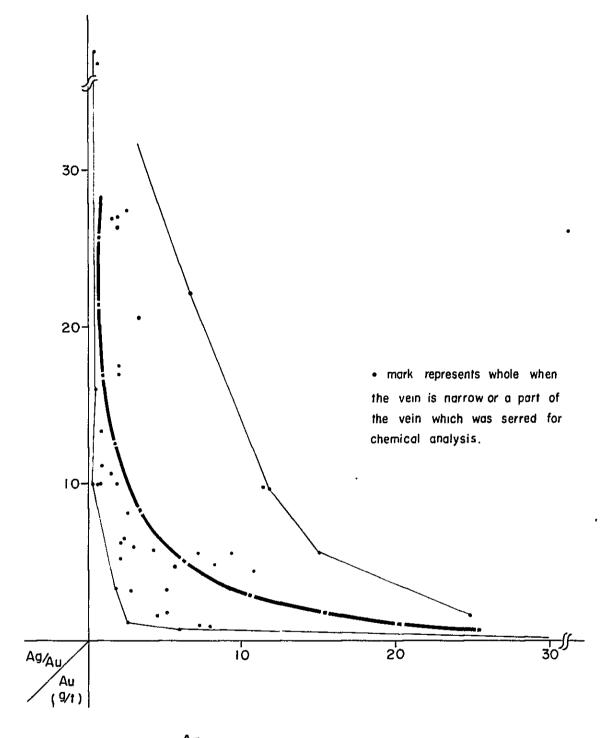


Fig. I-14 Ag/Au Versus Au Value Diagram
from Veins in Diamante — Paraiso — Bombona Area

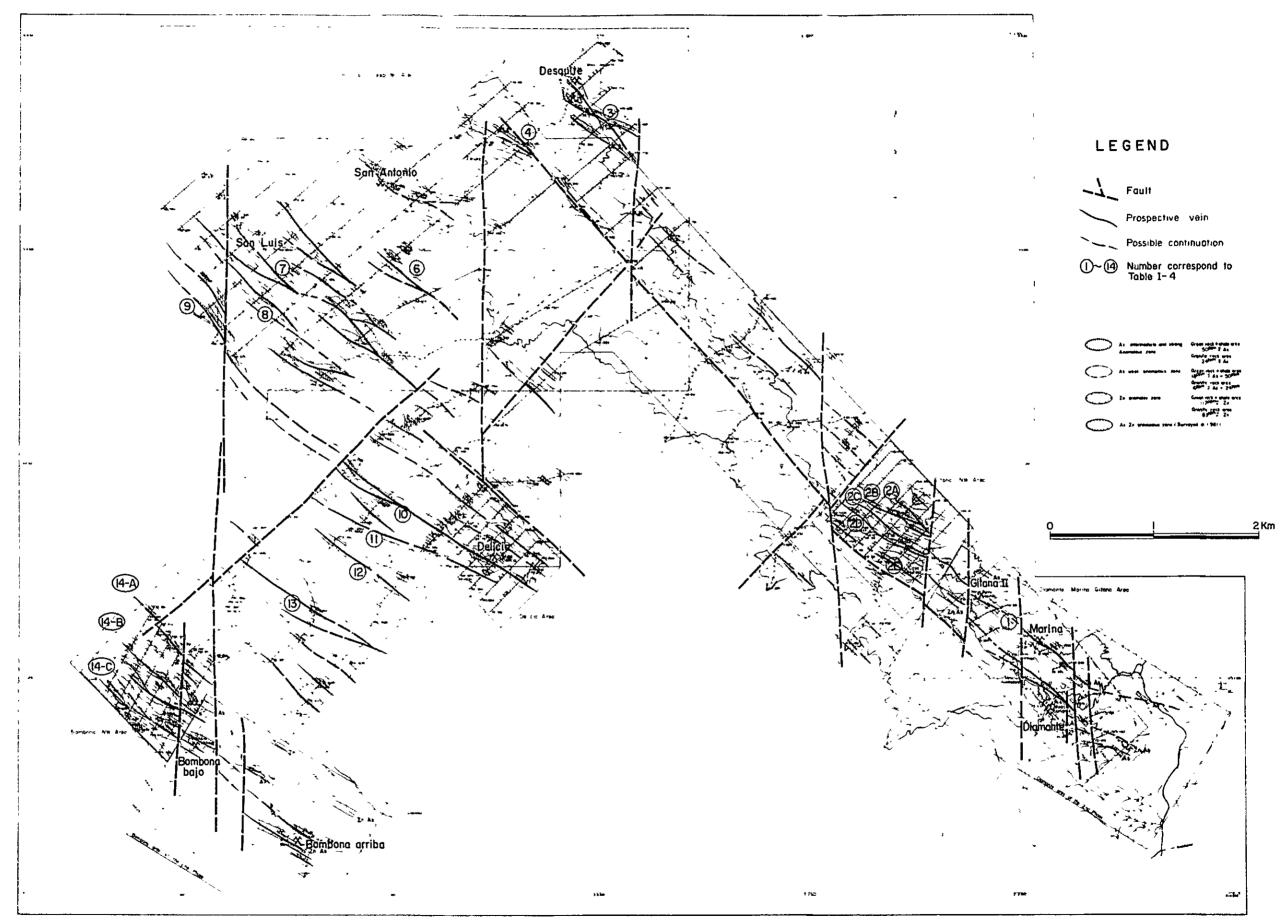


Fig. I – 15 Prospective Zones extracted after Geochemical Survey in the Diamante — Paraiso — Bombona Area

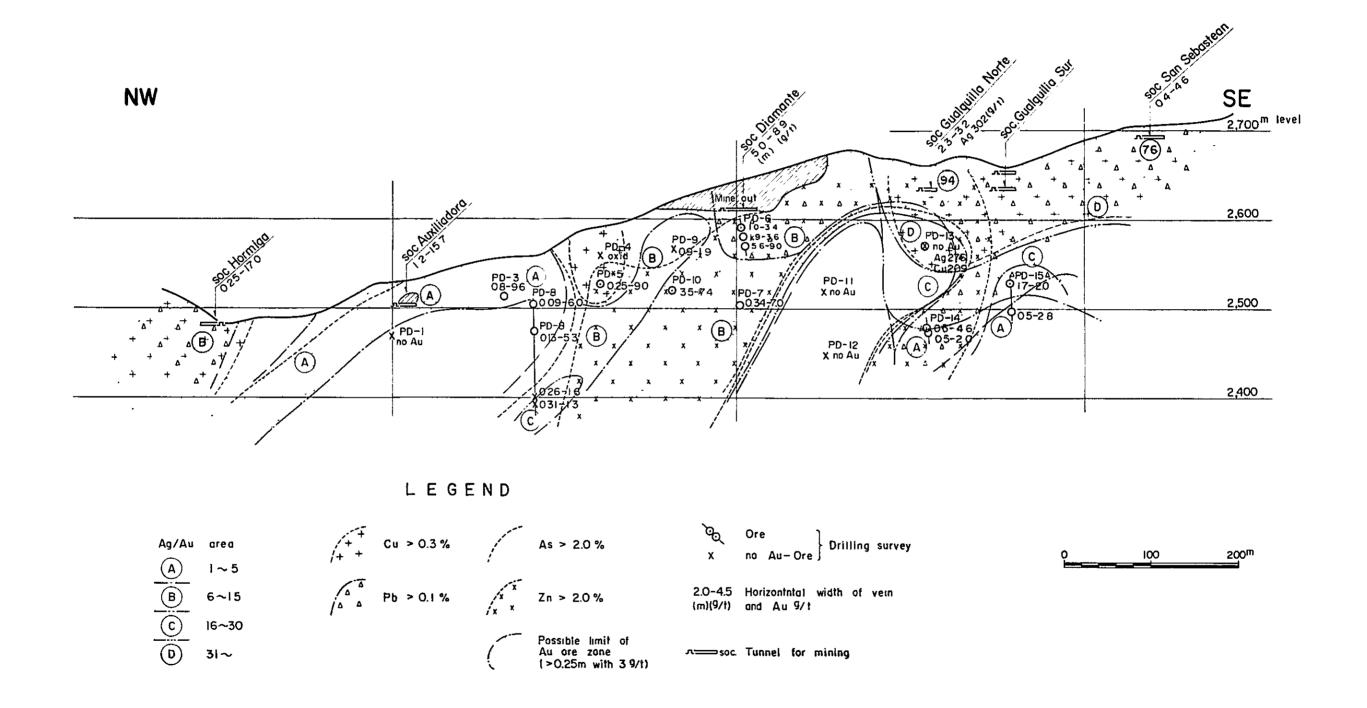


Fig. I - 16 Longitudinal Section of Diamante Principal Vein for Studying Survey Results

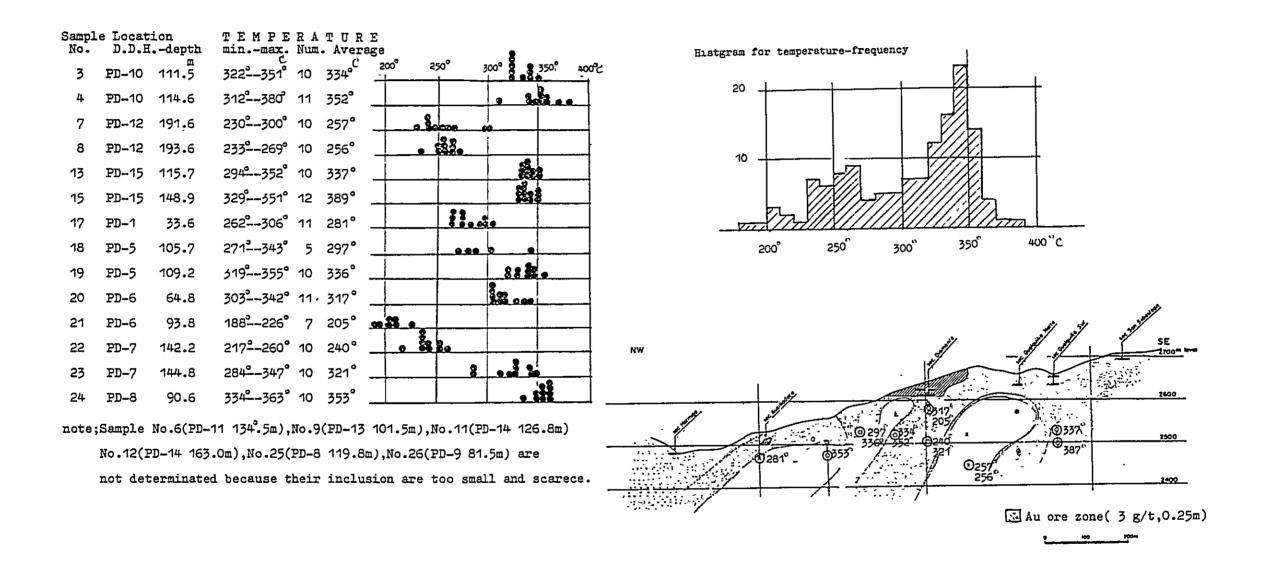


Fig.I-17 Location of Samples for Fluid Inclusion Study and their Results

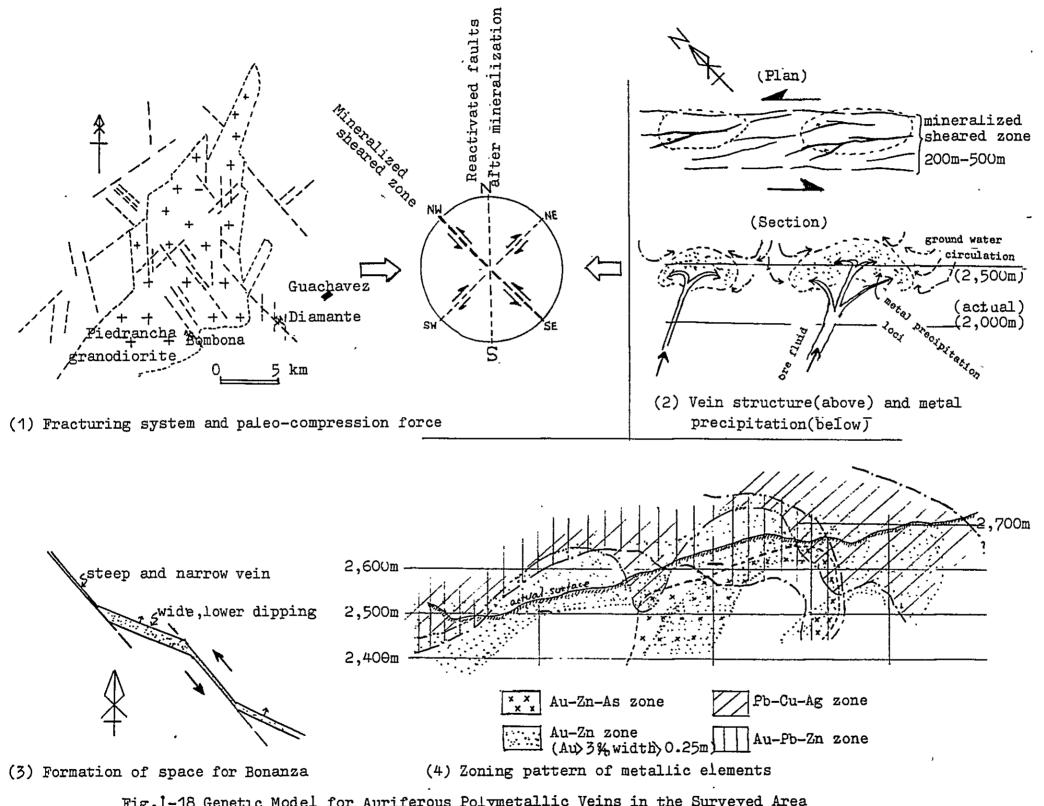


Fig.1-18 Genetic Model for Auriferous Polymetallic Veins in the Surveyed Area

#### CHAPTER 5. CONCLUSION AND RECOMMENDATION

#### 5-1 Conclusion

In this third phase of the program, diamond drilling was carried out for the Diamante main mineralized zone, in addition to the geological survey and the geochemical exploration in Diamante-Paraiso-Bombona area.

The details of the works of diamond drilling are described in Part II.

Including the results of the diamond drilling, the conclusion of the surveys carried out in this phase is as follows.

- (1) Geologically, the rocks distributed in the surveyed area are composed of the green volcanic rocks and the Piedrancha granodiorite intruding the former.
  - The ages of the intrusion are in the range of 6 to 20 million years.
- (2) The mineralization is represented by the fissure-filling polymetallic vein type ore deposits, the wall rock of which are the two aforementioned.
- (3) It has been clarified that the mineralized zones are running in parallel three rows in the NW-SE direction, spaced approximately by interval of 3 kilometers (Three rows are Bombona, San Luis Delicia and Desquite Diamante).
- (4) The mineralized zones are as wide as several hundred meters and in each of them several ore veins are distributed.
- (5) The width of each ore vein is generally small. The maximum width so far recognized in the surveys is 5.6 meters observed in the Diamante main mineralized zone. The lateral extension of enriched portions is as short as 150 to 200 meters, and the depth is inferred to be apporoximately 200 meters, viewing from general attitude of gold ore deposits.

- (6) Gold minerals are composed mainly of electrum. It is thought that its precipitation and crystallization would have been at the final stage of the formation of the arsenopyrite. There is a tendency that gold grade is high where abundant arsenopyrite is recognized.
- (7) It is not likely that there is high correlation coefficient in the relation between the grades of zinc and gold. But locally zinc grade comes up to 10% in some of the enriched portion in the Diamante gold ore vein. Zinc indications are more abundantly found in the Desquite-Diamante mineralized zone than in other two zones.
- (8) By the results of the geochemical exploration carried out by collecting soil samples, as many as 20 geochemical anomalies have been detected.

  There are 10 anomalies out of 20 where mineral indications have been recognized. It is thought that there is possibility for mineral indication to be discovered in these other 10 anomalies.

Following 6 anomalies are thought to be the most favorable areas for the emplacement of ore deposits, viewing from the points of the scale and the individual anomalous values.

Gitana - NW San Luis, San Luis - W
Delicia - NW, Bombona - N, Bombona - NW

# 5-2 Recommendation

There are many gold mines worked in a small scale in this survey area. In most cases, residual gold enrichment zones formed near the surface have been the object of the working. It has been clarified that abundant sulphide ores are still left at the depth of the ore deposit in the Diamante mine. It is expected as well as that workable ore deposits are left at the depth of the other ore veins found in this area. Also it is obvious that many geochemical anomalies extracted by the geochemical exploration would

have high potentiality for the emplacement of gold ore deposits.

It is comparatively easy to construct a new road in this area to the vicinity of Paraiso, as the area is within the reach of Guachavez village.

The area is thought to have favorable geographical conditions for the development of mines with abundant water.

However, it is necessary before the development to carry out sufficient studies and examinations on the methods of the recovery of gold from arsenopyrite, as the ore contains fair amount of arsenopyrite. It is also necessary before the investment for development of mine to grasp clearly the ore reserve and the ore grade by excavating tunnels. Rough feasibility study would be required for the development of mine by investigating problems concerning infrastructure and by carrying out preliminary concentration test.

### References

Baum, W. & Gobel, V.W (1978): Investigations on Metallogeny,

Calc-Alkaline Magmatism, and Related Tectonism in a

Continental Margin Province, Western Cordillera of

Colombia S.A.

Proceedings of Fifth Quadrennial IAGOD Symposium Galviz, J. (1982): Un arco de islas terciario en el occidente Colombiano.

Univ. Nacional (en imprinta)

INGEOMINAS (1982): Mapa Geologico del Departamento de Narino
Escala 1:400,000

Lepeltier, C. (1969): A Simplified Statistic Treatment of Geochemical

Data by Graphical Representation.

Econ. Geol. Vol. 64 p. 538-550

Nagasawa, K. (1981): Clay minerals associated with Au-Ag mineralization (in Japanese)

Mining Geology Special Issue No.10

Perez-Tellez, G. (1980): Evoluci'on geologica de la Subcuenca del Alto Patia, Departmento del Cauca, Colombia.

Geologia Norandina 2 Diciembre 1980

Takenouchi, S. (1981): Fluid inclusion studies of Tertiary gold deposits (in Japanese)

Mining Geology Special Issue Na 10

# PARTICULAR PART I DRILLING SURVEY

# PART II DRILLING SURVEY

CHAPTER 1. DRILLING WORKS	II- 5
1-1 Construction of Roads for Transportation	II- 5
1-2 Drilling Sites and Drilled Length	П- 6
1-3 Construction of Sites	II- 7
1-3-1 Transportation	11- 7
1-3-2 Setting Up	II- 7
1-3-3 Water for Drilling	п— 7
1-4 Drilling	II— 7
1-4-1 PD-8	II— 8
1-4-2 PD-9	П— 9
1-4-3 PD-10	II— 9
1-4-4 PD-11	П-10
1-4-5 PD-12	II1 1
1-4-6 PD-13 ······	II-12
1-4-7 PD-14	II-13
1-4-8 PD-15	II-14
1-5 Mobilization and Demobilization	П—15
1-5-1 Mobilization	II-15
1-5-2 Demobilization	II-1 5
1-6 Drilling Performance Results	П-16
1-6-1 Work Efficiency	II-16
1-6-2 Core Recovery	II-16
CHAPTER 2. GEOLOGY AND MINERALIZATION OF THE DRILL HOLES	II-17
2-1 PD-8	П— 1 7
2_2 PD_9	·∏18

· II — 1 8	***************************************	PD-10	2–3
II-19		PD-11	2-4
II-20	••••••••••••••••••••••••••••••••••••	PD-12	2-5
II-20		PD-13	2-6
II-2 1	***************************************	PD-14	2-7
II2 1	***************************************	PD-15	2-8

## LIST OF FIGURES

Fig.	11-1	Progress Record of Diamond Drilling	PD-8
Fig.	II-2	Progress Record of Diamond Drilling	PD-9
Fig.	11-3	Progress Record of Diamond Drilling	PD-10
Fig.	II-4	Progress Record of Diamond Drilling	PD-11
Fig.	II-5	Progress Record of Diamond Drilling	PD-12
Fig.	II-6	Progress Record of Diamond Drilling	PD-13
Fig.	11-7	Progress Record of Diamond Drilling	PD-14
Fig.	II-8	Progress Record of Diamond Drilling	PD-15
Fig.	II-9	Geological Section for PD-8	
Fig.	II-10	Geological Section for PD-9, PD-10	
Fig.	II-11	Geological Section for PD-11, PD-12	
Fig.	II-12	Geological Section for PD-13, PD-14	
Fig.	II-13	Geological Section for PD-15	

## LIST OF PLATES

PL.	II <b>-</b> 1	Geologic	Drill	Log.	PD-8,	PD-9
PL.	11-2	Geologic	Drill	Log.	PD-10,	PD-11
PL.	11-3	Geologic	Drill	Log.I	PD-12,	PD-13
РΪ	TT-4	Geologic	Dr111	Log.	PD-14	PD-15

#### CHAPTER 1. DRILLING WORKS

### 1-1 Construction of Roads for Transportation

Helicopters were used for the transportation of materials and equipment during the second year, but this year a 3m wide road was constructed for about 15 Km between Guachavez and Diamante Mine. The team leader, who first left with the geological survey team on June 14, borrowed bulldozers from INGEOMINAS, prepared a field camp, procured materials and secured laborers, negotiated with local land owners and related government offices, and partially started road construction. Three drilling members left on July 5 and when they arrived at Guchavez on July 9, they proceeded with work divided into the construction of this main road, the construction of a road for movement and transportation near the mine and the ground levelling for drilling sites. The old road, of which construction had been given up after manually excavating a 2 ~ 4m width 30 to 50 years ago in an attempt to build a motor road along the Telembi River, was used as the main road construction, widening it and levelling the ground. However, a stretch of about 1 Km descending from the opposite bank of the Diamante Mine to the mine was newly excavated.

The local terrain is extremely steep and there is much rain. So, the road construction was, indeed, difficult as frequent collapses occurred during and after its construction and because the road surface did not easily harden. Where the road crossed brooks, the stream were spanned with wooden or stone bridges. Where it crossed marshes, gravel and boulders were used. To ensure smooth transportation of material and equipment, 8-15 temporary workers were posted, whenever necessary to maintain and repair the road.

In April 1982, a regular motor road began to be constructed between

Guachavez and Diamante by the Ministry of Public Works of the Government of Colombia and by the time drilling was completed the road construction had progressed to 4 Km from Guachavez.

## 1-2 Drilling Sites and Drilled Length

The Diamante area is about 10 Km from Guachavez village by a horse path crossing over a pass 3,200m in elevation. The distance takes about three hours to travel on horseback or by foot.

The position (longitude and latitude) of each drilling hole, its elevation and its drilled length are as follows:

Name of hole	Longitude	Latitude	Elevation	Drilled proposed	l length actual	Direction	Dip
PD-8	12,196	1,950	2,564.5	180	180.50	225°	-75°
PD-9	12,208	1,740	2,604.4	130	131.00	45°	-30°
PD-10	12,208	1,740	2,604.4	200	200.50	45°	<b>−</b> 50°
PD-11	12,290	1,619	2,606.6	140	140.50	60°	-40°
PD-12	12,290	1,619	2,606.6	200	200.20	60°	-55°
PD-13	12,377	1,524	2,618.8	120	121.50	60°	-40°
PD-14	12,377	1,524	2,618.8	200	200.20	60°	-60°
PD-15	12,434	1,443	2,624.1	160	161.50	60°	-60°
Total				1,330 1	,335.90		

(\* E 12,000, N 2,000 and elevation 2,500m are used for Station 21 before the pithead of Mina Auxiliadora. Last year, E 2,000 and N 2,000 were used for the same station but a change was made for this year due to an expanded scope of the precision geological survey.)

#### 1-3 Construction of Sites

## 1-3-1 Transportation

Because the construction of the road for motor transport progressed with difficulty, material and equipment were brought by manpower together with self-propelled transportation from the warehouses where they had been stored last year. All transportation between holes was handled by manpower together with a rooper (universal pulling and lifting machine) and self-propelled transportation.

### 1-3-2 Setting Up

Setting up work was started from PD-8. The construction of the mountainous transport route between the drilling sites of PD-8, PD-9 and PD-10, PD-11 and 12, PD-13 and 14, and PD-15, the construction of a 1,600m haul-out route (width: 2m) to the main route and the ground levelling at drilling sites were done manually.

## 1-3-3 Water for Drilling

For holes PD-9 and 10,  $1\frac{1}{2}$  inch polyethylene pipes were laid for 300m with a pump-up height of 10m by HOPE-F pump. For holes PD-8, PD-11, and 12, PD-13 and 14, and PD-15, natural intake was made from a nearby mountain stream, using  $1\frac{1}{2}$  inch and 1-inch polyethylene pipes. The total length of pipes used for this purpose was 1,000m.

## 1-4 Drilling

The top soil was drilled by 101-mm metal crown without using water. When bedrock was hit, drilling was made by the NQ wireline method, inserting and installing one casing pipe after another. For the final caliber, the BQ wireline method was used. The progress of drilling of each hole was as follows:

### 1-4-1 PD-8 (Direction 225°, Inclination -75°)

Drilled length, 180.50m

Core length: 173.50m

Core recovery: 96.1% (excluding top soil)

Day drilling was started: July 15, 1982

Day drilling was completed: July 25, 1982

 $0.00m \sim 4.50m$ 

Waterless drilling was made by 101mm metal crown. Talus sediments were drilled to a depth of 4.50m. With stabilized lithology, NW casing pipe was inserted to 4.50m.

4.50m ∿ 132.80m

Drilling was made by NQ-WL diamond bit, using libonite and bentonite mudwater. The rocks were diabase and agglomerate. At 4.50m ∿ 11.30m, there were many cracks and lost-circulation frequently occurred. So drilling was made while preventing lost-circulation by a Tel-stop. From that depth, the lithology was relatively stabilized and BW casing pipe was inserted to 132.80m. Meanwhile, three mineralized parts were detected and confirmed at 59.10m ∿ 59.45m, 77.90m ∿ 79.30m and 90.20m ∿ 90.70m.

132.80m ∿ 181.50m

Drilling was made by BQ-WL diamond bit, using libonite and bentonite mudwater. The rocks were agglomerate, diabase, quartz veinlets and fracture zone. At 132.80m ∿ 151.50m, the lithology was relatively stabilized. From 151.50m to 180.50m, the lithology was clayey and fractured. The drilling was completed after accomplishing the purpose by drilling to 180.50m, securing the hole wall with libonite mudwater. Meanwhile, four mineralized layers were detected and confirmed at 136.00 ∿ 137.40m, 142.30m ∿ 142.80m, 155.80m ∿ 158.60m and 166.40m ∿ 169.50.

# 1-4-2 PD-9 (Direction 45°, Inclination -30°)

Drilled length: 131.00m

Core length: 103.30m

Core recovery: 85.4% (excluding top soil)

Day drilling was started: July 29

Day drilling was completed: August 7

 $0.00m \sim 9.20m$ 

Waterless drilling was made by 101mm metal crown. A clayey layer was drilled to a depth of 9.20m. When bedrock was hit, NW casing pipe was inserted to 9.20m.

9.20m ∿ 74.20m

Drilling was made by NQ-WL diamond bit, using libonite and bentonite mudwater. The rocks were diabase and agglomerate. At 9.20m ∿ 50.00m lost-circulation and collapse of hole frequently occurred due to a fracture zone with many cracks. So cementation and prevention of lost-circulation were effected as drilling progressed. Then, drilling was made to 74.20m under relatively stabilized lithological conditions. With stabilized lithology, BW casing pipe was inserted to 74.20m.

74.20m ∿ 131.00m

Drilling was made by BQ-WL diamond bit, using libonite and bentonite mudwater. The rocks were agglomerate and clayey zone. With relatively stabilized lithology, drilling was made to 131.00m and completed after accomplishing the purpose. Meanwhile, a mineralized layer was detected and confirmed at  $77.30m \sim 85.30m$ .

### 1-4-3 PD-10 (Direction 45°, Inclination -50°)

Drilled length: 200.50m

Core length: 183.30m

Core recovery: 95.6% (excluding top soil)

Day drilling was started: August 9

Day drilling was completed: August 21

0.00m ∿ 8.70m

Waterless drilling was made by 101mm metal crown. A clayey layer was drilled to a depth of 8.70m. When the bedrock was hit, NW casing pipe was inserted to 8.70m.

8.70m ∿ 120.20m

Drilling was made by NQ-WL diamond bit, using libonite and bentonite mudwater. The rocks were weathered diabase with many cracks, agglomerate and fracture zone. At 8.70m to 17.90m, the hole was enlarged by NW diamond shoebit and NW casing pipe was extended because of the frequent occurrence of cracks and collapses. Then, after the stabilization of lithology, the pipe was inserted to 17.90m.

At 17.90m to 91.70m, the lithology was remarkable for many cracks but drilling was made while preventing lost-circulation. Deeper still, the rocks were agglomerate tuff, quartz veinlets and clayey zone. As lithology became stabilized, BW casing pipe was inserted to 120.20m. Meanwhile, a mineralized layer was detected and confirmed at 105.20m ~ 116.10m.

120.20m ∿ 200.50m

Drilling was made by BQ-WL diamond bit, using libonite and bentonite mudwater. The rocks were agglomerate, shale, diabase and there was a clayey zone. The lithology was relatively stabilized and the boring was completed after drilling to 200.50m and accomplishing the purpose.

### 1-4-4 PD-11 (Direction 60°, Inclination -40°)

Drilled length: 140.50m

Core length: 124.90m

Core recovery: 98.1% (excluding top soil)

Day drilling was started: August 29

Day drilling was completed: September 7

 $0.00m \sim 13.20m$ 

Waterless drilling was made by 101mm metal crown. A clayey layer was drilled for 13.20m. When the bedrock was hit, NW casing pipe was inserted to 13.20m.

13.20m ∿ 83.60m

Drilling was made by NQ-WL diamond bit, using libonite and bentonite mudwater. The rocks were weathered diabase and agglomerate. At 13.20m ~ 20.30m, the hole was enlarged by NW diamond shoebit for cementation because of the frequent occurrence of cracks and collapses, and NW casing pipe was extended to 20.30m and installed. Cracks developed beyond that depth but drilling was made by preventing lost-circulation. When lithology was stabilized at 83.60m, BW casing pipe was inserted to 83.60m.

83.60m ∿ 140.50m

Drilling was made by BQ-WL diamond bit, using libonite and bentonite mudwater. The rocks were agglomerate and diabase and these held a fracture zone between them. The lighology was relatively stabilized and the drilling was completed after drilling to 140.50m and accomplishing the purpose.

Meanwhile, a mineralized layer was detected and confirmed at 131.80m ~ 137.60m.

## 1-4-5 PD-12 (Direction 60°, Inclination -55°)

Drilled length: 200.50m

Core length: 178.20m

Core recovery: 97.4% (excluding top soil)

Day drilling was started: September 12

Day drilling was completed: September 24

 $0.00m \sim 17.20m$ 

Waterless drilling was made by 101mm metal crown. A clayey layer was drilled to a depth of 17.20m and NW casing pipe was inserted.

17.20m ∿ 120.20m

Drilling was made by NQ-WL diamond bit, using libonite and bentonite mudwater. The rocks were agglomerate and held a fracture zone in between. At 17.20m ~ 40.00m, the lithology contained many cracks and lost-circulation and collapses were frequent. So, drilling was made while preventing lost-circulation and carrying out cementation. Later, the lithology was stabilized, and BW casing pipe was inserted to 120.20m.

120.20m ∿ 200.20m

Drilling was made by BQ-WL diamond bit, using libonite and bentonite mudwater. The rocks were agglomerate, diabase and quartz veinlets with sporadic fracture zones. At 165.00m ~ 177.40m, a clayey zone collapsed and rod jamming occurred but drilling was continued while securing the hole wall with libonite mudwater. The drilling was completed after drilling to 200.20m and accomplishing the purpose. Meanwhile, a mineralized layer was detected and confirmed at 178.50m ~ 189.00m

### 1-4-6 PD-13 (Direction 60°, Inclination -40°)

Drilled length: 121.50m

Core length: 104.70m

Core recovery: 93.9% (excluding top soil)

Day drilling was started: October 1

Day drilling was completed: October 8

 $0.00m \sim 10.00m$ 

Waterless drilling was made by 101mm metal crown. A clayey layer was drilled to 10.00mm. There was 2 l/min of spring water. Because of the

collapse of the hole wall, NW casing pipe was inserted to 10.00m.

10.00m ∿ 72.00m

Drilling was made by NQ-WL diamond bit, using bentonite mudwater. The rocks were agglomerate and diabase with a fracture zone inbetween and had many cracks. At 10.00m ~ 20.50m, the hole was enlarged with NW diamond shoebit because of the frequent occurrence of cracks and collapses. NW casing pipe was extended and, as the lithology became stabilized, it was inserted to 20.50m. At 20.50m ~ 72.00m, the rocks had many cracks but drilling was made while preventing lost-circulation. When the lithology was stabilized, BW casing pipe was inserted to 70.00m.

72.00m ∿ 121.50m

Drilling was made by BQ-WL diamond bit, using libonite and bentonite mudwater. The rocks were agglomerate, diabase, quartz veinlets and clay zone. Drilling was continued, using libonite mudwater, though the rocks had many cracks and were clayey and fractured. The drilling was completed after drilling to 121.50m and accomplishing the purpose. Meanwhile, two mineralized layers were detected and confirmed at 76.10m ~ 78.70m and 100.60m ~ 101.80m.

### 1-4-7 PD-14 (Direction 60°, Inclination -60°)

Drilling length: 200.20m

Core length: 184.50m

Core recovery: 98.0% (excluding top soil)

Day drilling was started: October 1

Day drilling was completed: October 23

0.00m ∿ 8,60m

Waterless drilling was made by 101mm metal crown. A clay layer was drilled to 8.60m. There was 2 l/min of spring water. NW casing pipe was

inserted to 8.60m because of collapse of the hole wall.

8.60m ∿ 120.90m

Drilling was made by NQ-WL diamond bit, using libonite and bentonite mudwater. The rocks were weathered diabase and agglomerate and had many cracks. At 8.60m ~ 31.00m, the hole was enlarged by cementation and NW diamond shoebit because of frequent occurrence of cracks and collapses, and NW casing pipe was extended and installed to 12.00m. Later, cracks developed but drilling was made while preventing lost-circulation. Drilling was made to 120.90m and, as the lithology became stabilized, BW casing pipe was inserted to 120.90m.

120.90m ∿ 200.20m

Drilling was made by BQ-WL diamond bit, using libonite and bentonite mudwater. The rocks were agglomerate, diabase and quartz veins and contained fracture zones. Drilling through the many fracture zones that existed was made while securing the hole wall by means of libonite. The drilling was completed after drilling to 200.20m and accomplishing the purpose. Meanwhile, three mineralized layers were detected and confirmed at 123.70m ~ 129.00m, 141.00m ~ 141.70m and 158.30m ~ 164.40m

### 1-4-8 PD-15 (Direction 60°, Inclination -60°)

Drilled length: 161.50m

Core length: 158.30m

Core recovery: 98.6% (excluding top soil)

Day drilling was started: November 1

Day drilling was completed: November 12

 $0.00m \sim 1.00m$ 

Waterless drilling was made by 101mm metal crown. A clay layer was drilled for 1.00m. Then, as the lithology was stabilized, NW casing pipe

was inserted to 1.00m.

1.00m ∿ 96.00m

Drilling was made by NQ-WL diamond bit, using bentonite mudwater. The rocks were agglomerate tuff breccia, agglomerate, shale and diabase. The lithology was stabilized, though with spring water (10  $\ell$ /min), and BW casing pipe was inserted to 96.00m. Meanwhile, a mineralized layer was detected and confirmed at 41.50m  $\sim$  41.90m

96.00m ∿ 161.50m

Drilling was made by BQ-WL diamond bit, using libonite and bentonite mudwater. The rocks were agglomerates, agglomerate tuff breccia, diabase and quartz veins and contained fracture zones. Fracture zones with spring water (10 l/min) developed but drilling was made while securing the hole wall, using libonite. The boring was completed after drilling to 161.50m and accomplishing the purpose. Meanwhile, two mineralized layers were detected and confirmed at 109.90m ~ 122.50m and 147.80m ~ 152.10m.

### 1-5 Mobilization and Demobilization

### 1-5-1 Mobilization

Three to six days were consumed for mobilization and setting up prior to the start of drilling at drill sites of PD-8, PD-9 and 10, PD-11 and 12, PD-13 and 14, and PD-15. Another day or two were necessary to change a inclination at the same place.

## 1-5-2 Demobilization

For demobilization, materials and equipment were transported from Diamante to Guachavez by small four-wheel drive 2-ton trucks. Due to the unfavorable road conditions of the rainy period, accessary tools and equipments were carried on horseback and kept at Guachavez for maintenance.



### 1-6 Drilling Performance Results

### 1-6-1 Work Efficiency

As indicated in AII-12, the total length of drilling holes was 1,335.90m, the drilled length per shift of all drilling work was 5.08m and the drilled length per shift of actual drilling work was 5.64m.

The penetration rate and the rotation speed of the bit were as follows:

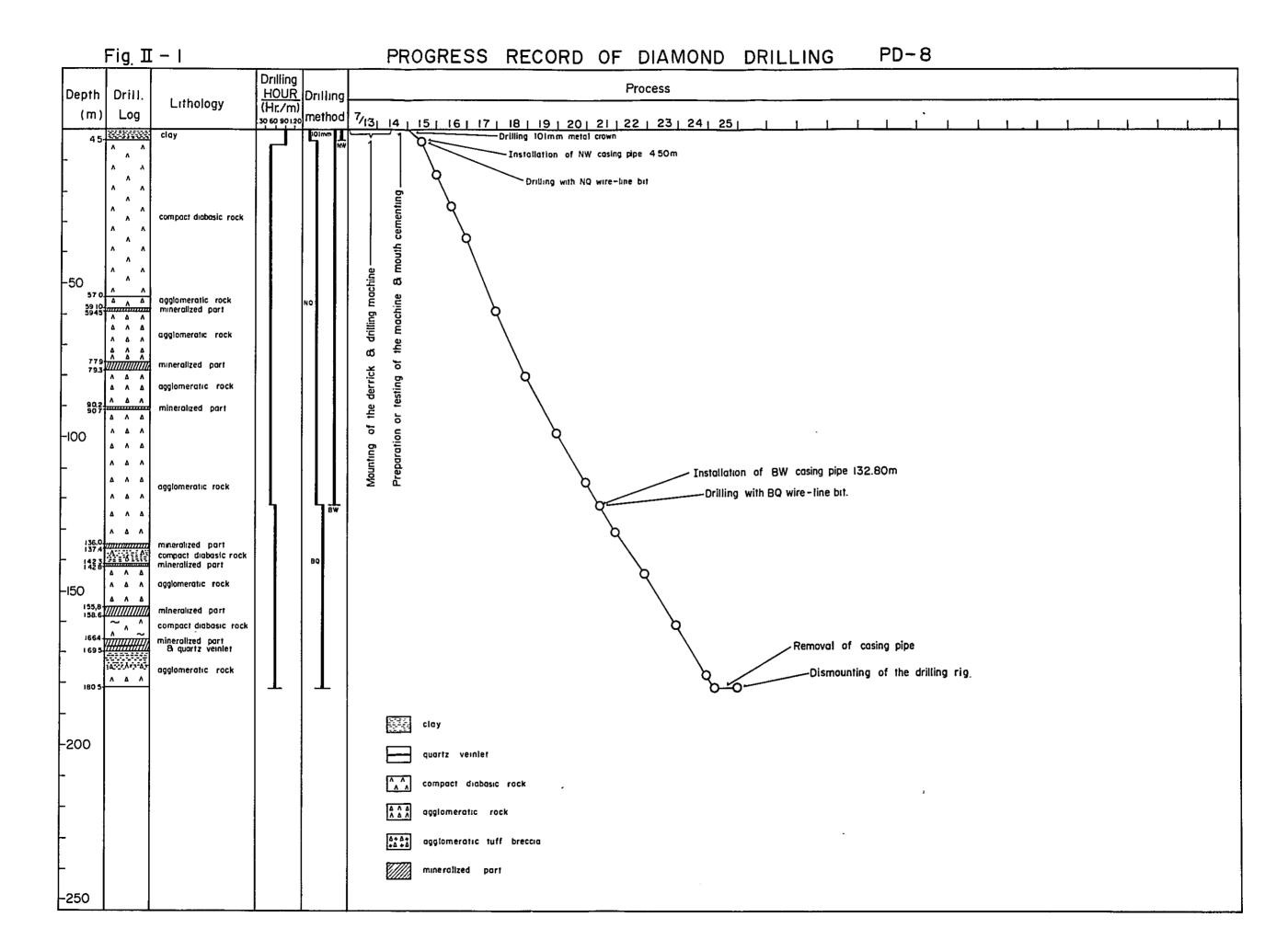
	Penetration rate	Rotation rate			
Hard	$1.0 \sim 2.0$ cm/min	400 ∿ 500 rpm			
Medium	2.0 ∿ 3.0 cm/min	300 ∿ 400 rpm			
Soft	3.0 ∿ 4.0 cm/min	50 ∿ 150 rpm			

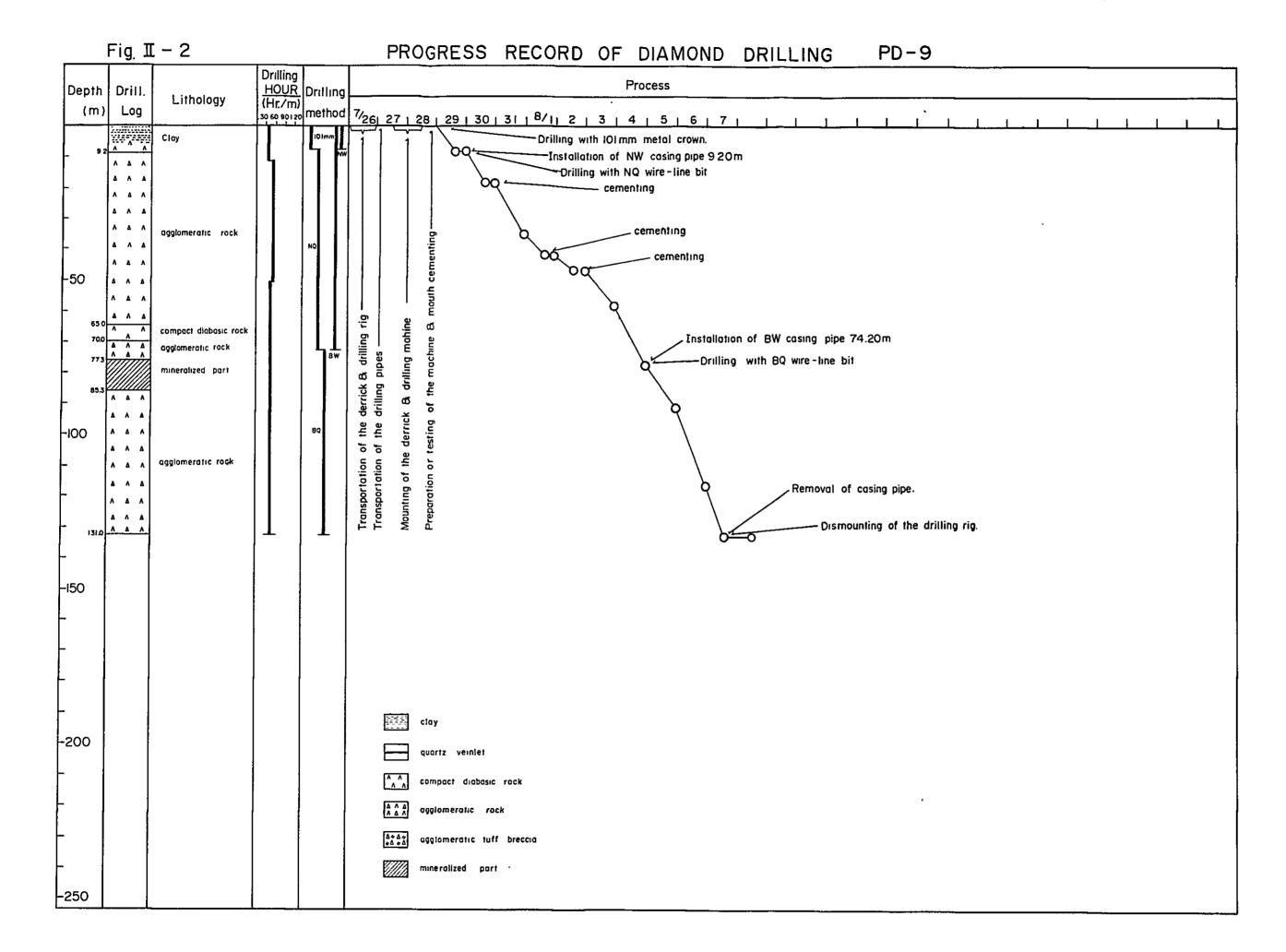
In the above actual drilling results, the drilled length per shift was small because the lithology consisted of fracture zones with many cracks containing clay, generally speaking.

### 1-6-2 Core Recovery

As indicated in AII-12, cores totaling 1,210.70m for a total drilled length of 1,259.30m, excluding 76.60m representing top soil, were recovered.

The average core recovery was 96.1%.

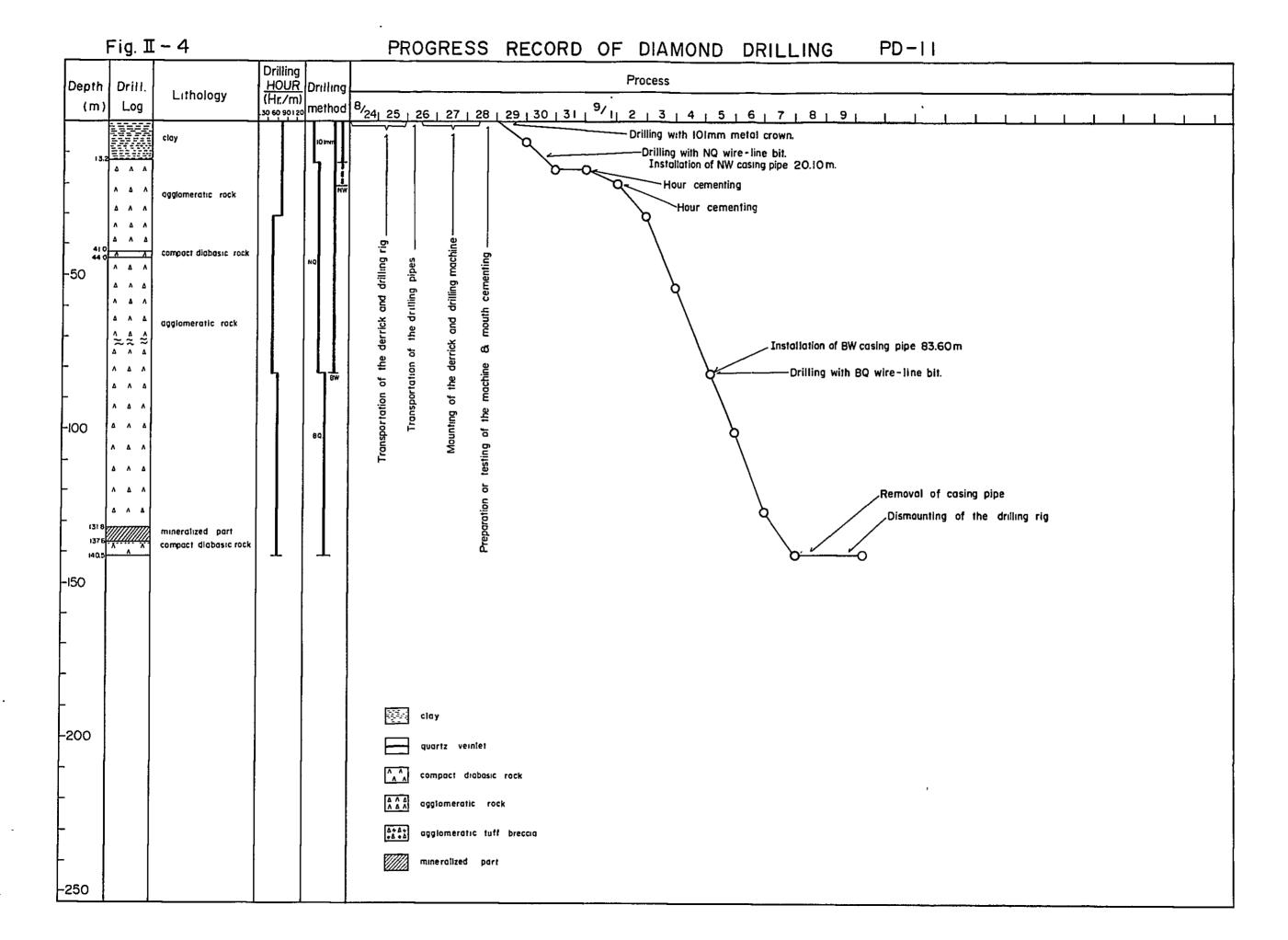


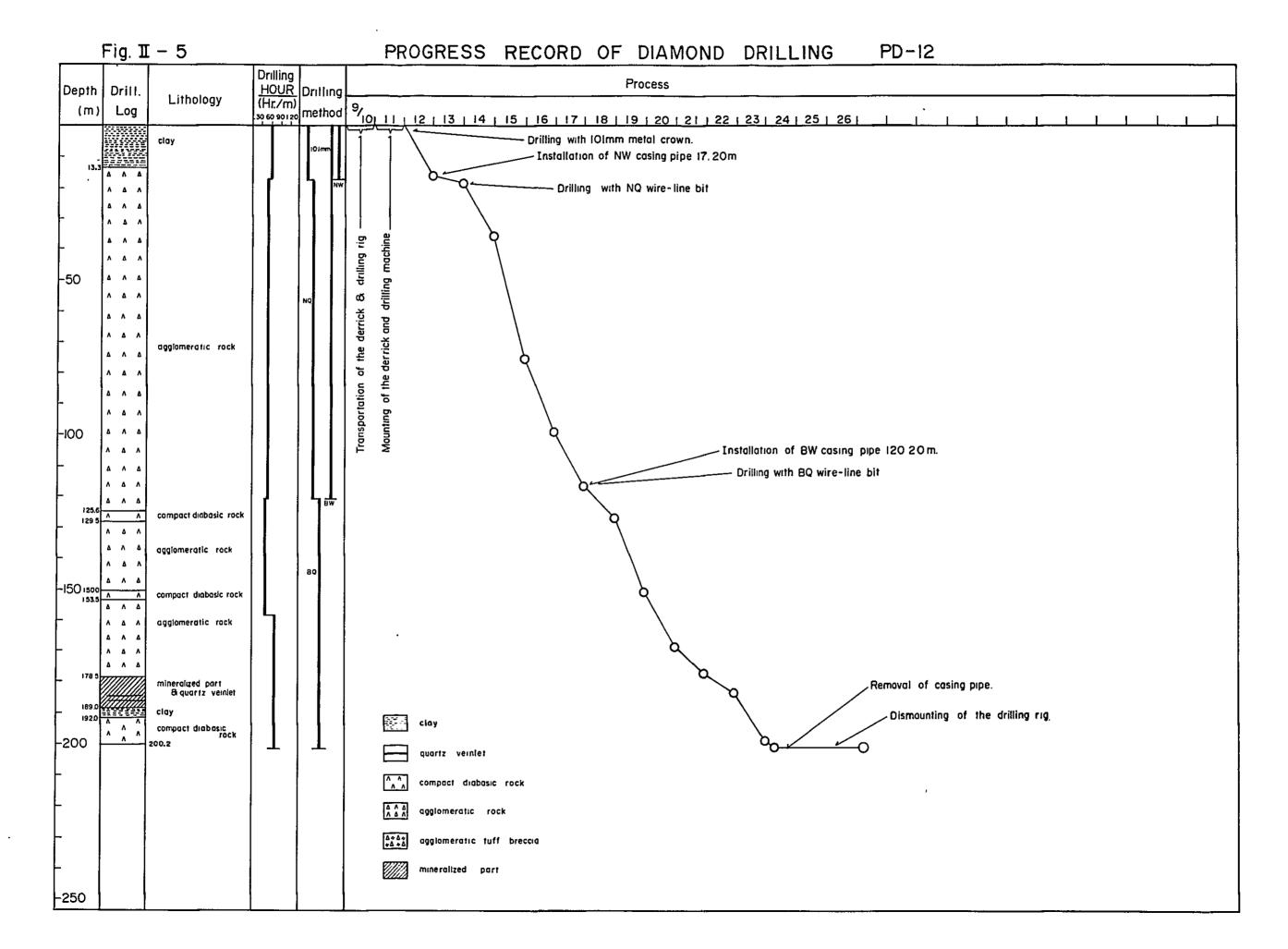


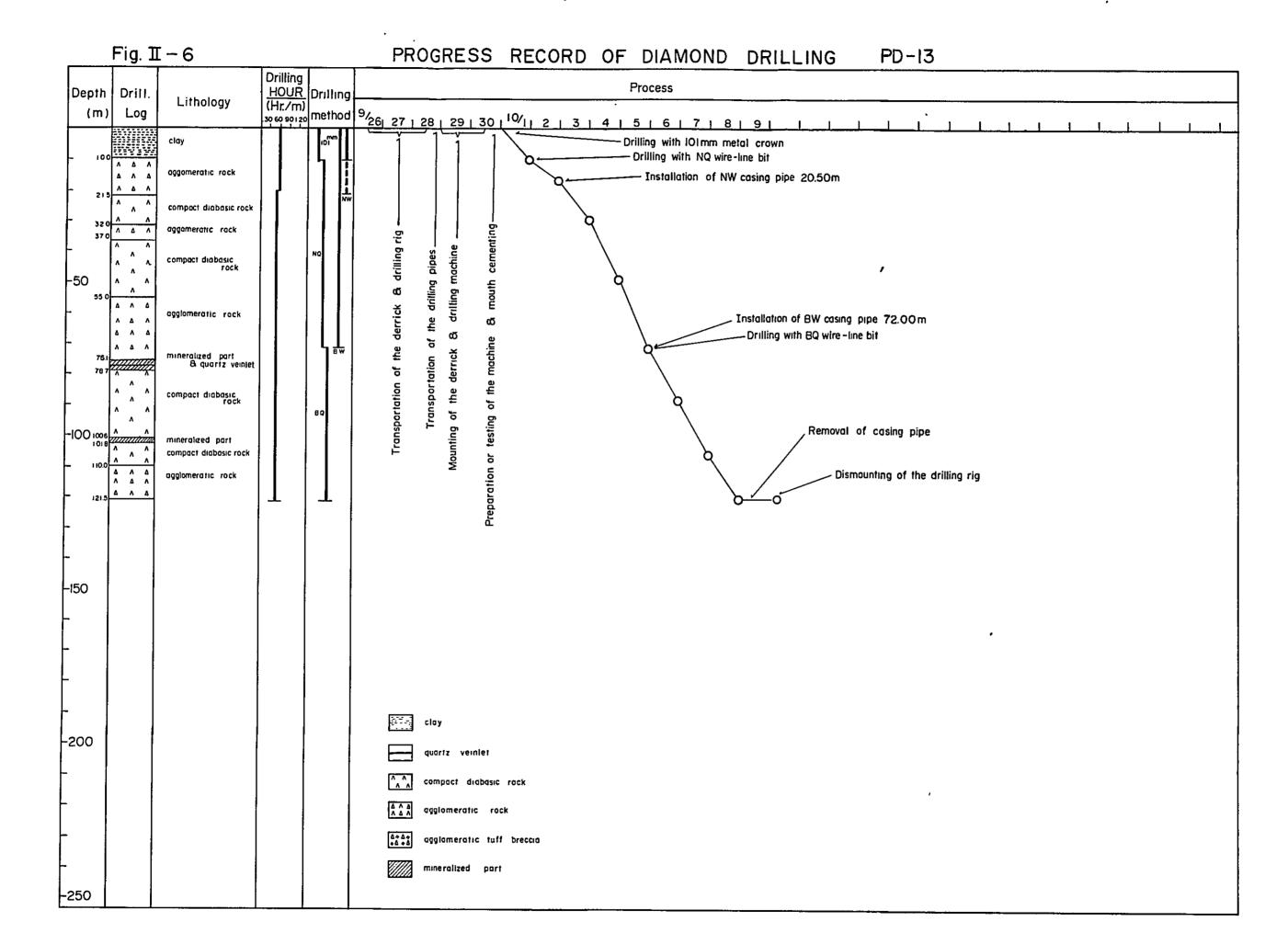
agglomeratic tuff breccia

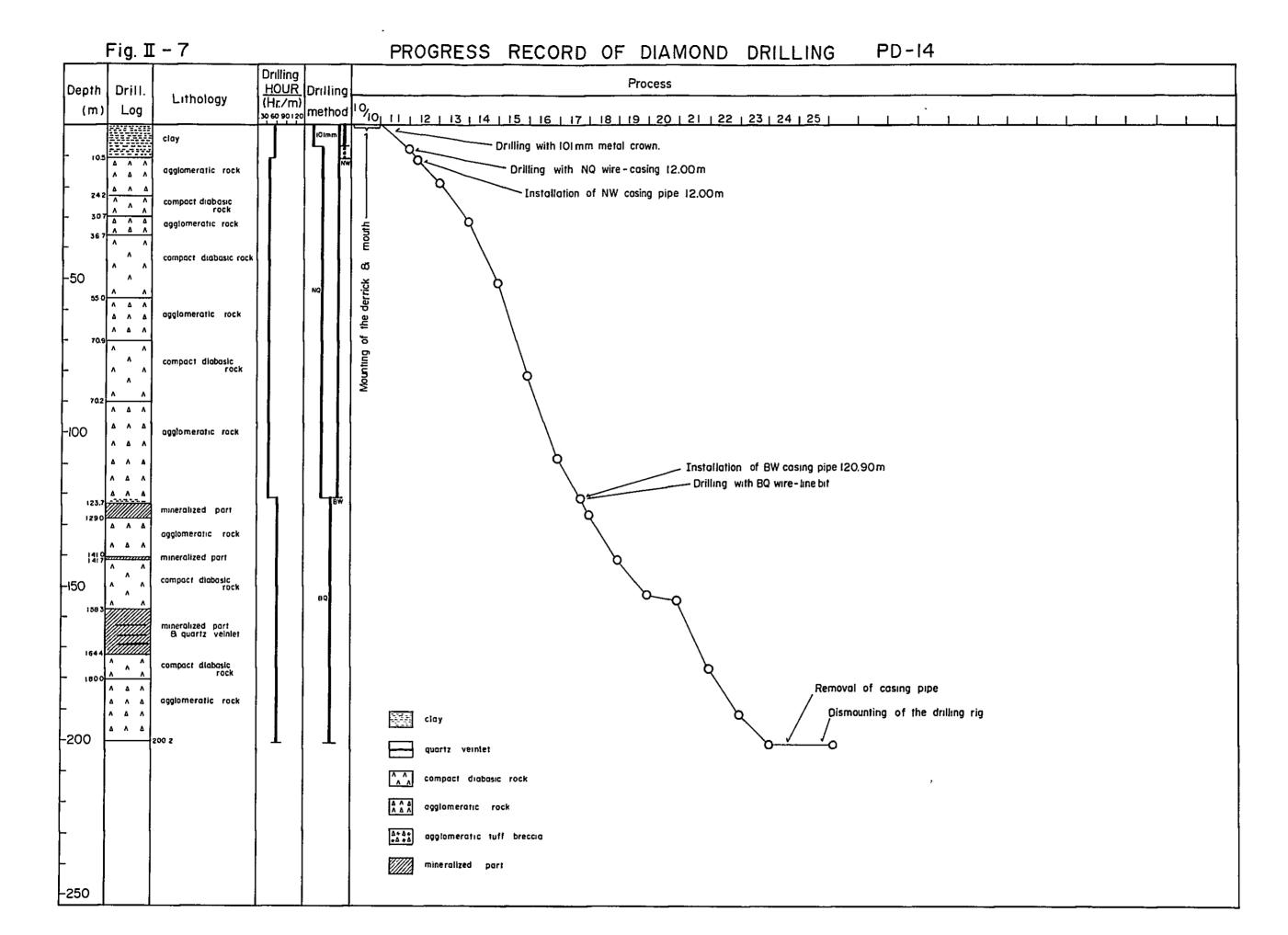
mineralized part

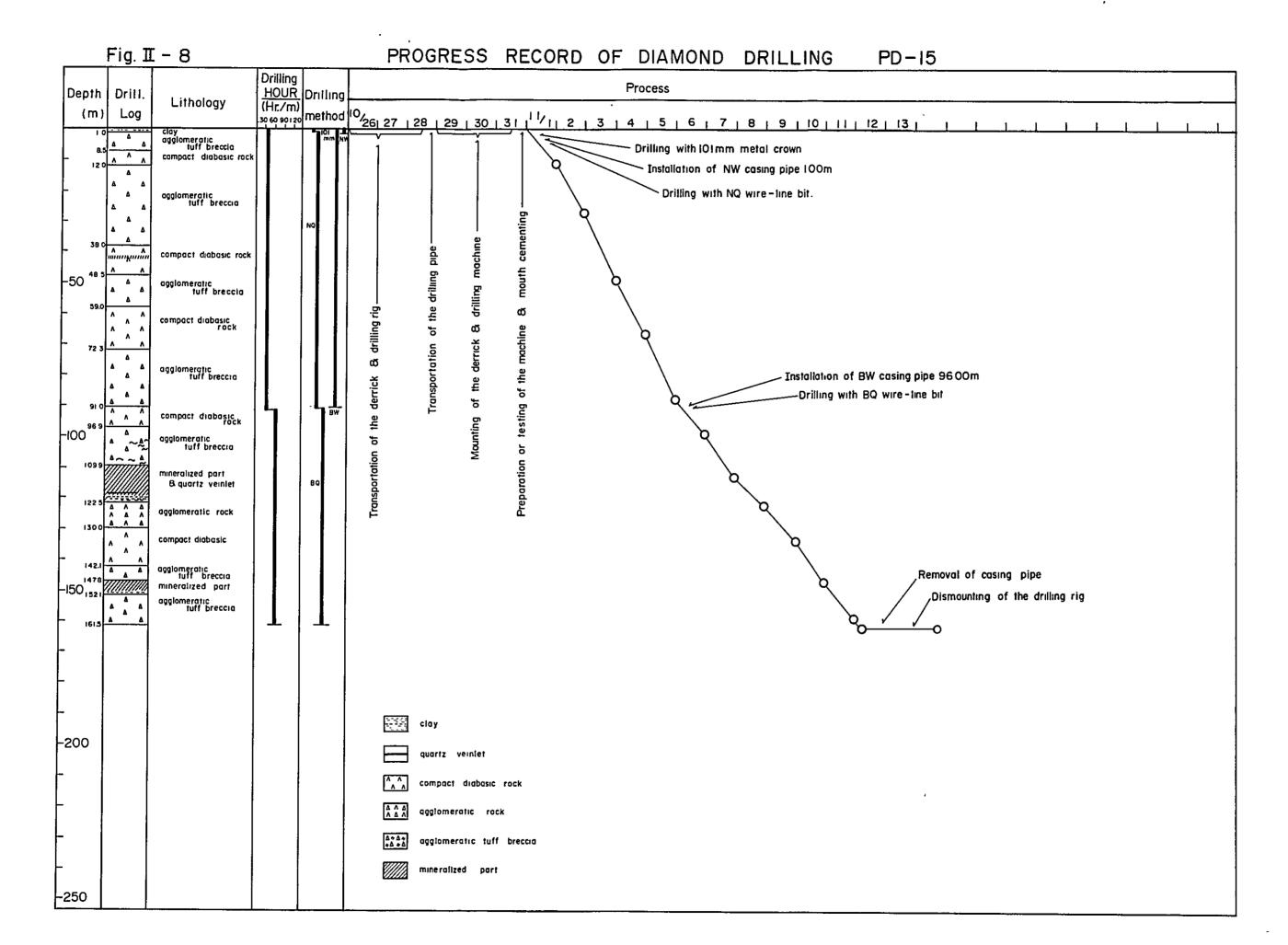
-250











#### CHAPTER 2. GEOLOGY AND MINERALIZATION OF THE DRILL HOLES

- 2-1 PD-8
- (1) Purpose: A vein with a width of 30 cm and Au 9.69 g/t was detected at PD-3, which was drilled in the second phase. But no mineralized zones were found at PD-4 to the south and only veinlets were found at PD-5 bored from the same point. This hole was aimed to see mineralization at the intermediate position.
- (2) Lithology and mineralization: The rocks from the surface to 3.5m were black basaltic andesite but at 3.5m to 14.6m, they were medium-grained diorite. The latter rocks did not outcrop and were not found in other drill holes. They were neither mineralized nor altered and were relatively fresh. From the depth of 14.6m to 58.00m is found a black or dark green cryptocrystalline basaltic andesite that is homogeneous, massive and dense. The flow structure seen at about 25.4m presumably represents lava. From that level to the bottom of the hole is tuff breccia. Fracture zones were found to about 15m but none existed below. Eight veins were found. Of these, veins with ore grades of Au 0.6 g/t or better are as follows:

Footage (drilled	length) m	Au 9∕t	Ag g/t	Cu %	Pb %	Zn %	As %
A . 5 9 1 - 5 9 4	5 (035)	60	4	0.03	001	0.01	0.08
B . 7 7 9 - 7 9 3	(1.40)	1.1	4	0.0 2	0.05	0.07	0.07
C . 9 0 2 - 9 0.7	(050)	5 3	5	< 0.0 1	0.03	0.09	0.5 2
D . 1664 - 167.4	(100)	10	13	0.10	0.03	1.60	2.10
E . 1683 - 1695	(1.20)	1 3	3 7	001	003	0.40	520

The above A, B and C veins are mainly composed of quartz and contain only small quantities of sulfide minerals. The D and E veins are within the same vein structure and, for 5.5m from 165.9m to 171.4m, they are discolored to gray by such alterations as silicification and argillization.

Similarly, altered zones existed at 136.0m - 137.4m, 139.8m - 142.8m and 153.7m - 158.6m and the white clay contained a small quantity of sulfide minerals.

#### 2-2 PD-9

- (1) Purpose: Several high-grade veins exist for a horizontal width of about 20m in the deepest front of the cross cut, Socavon Diamante, located in the approximate center of the mining area of Diamante. Satisfactory results were obtained at PD-6 and PD-7 in the second-year survey of the parts below those veins. But at the PD-4 and PD-5 surveys on the northern extension of the veins, the results were unsatisfactory, as already stated. PD-9 was intended to see mineralization between PD-6, -7 and PD-4, -5.
- (2) Lithology and mineralization: The rocks are tuff breccia all the way to the bottom of the hole at 131.00m. Only at 65m to 85m is there homogeneous andesite lava. Relatively large fracture zones were found at 14.5m 19.7m and 30.1m 39.0m. Also, four fracture zones exist from 115m to the bottom. The breccia has spheric pores, the size of 1 mm to 5 mm, which are filled with quartz, epidote, pyrrhotite and chalcopyrite.

A vein structure was found at 78.0m - 84.7m and a small quantity of sulfide minerals was observed to comprise it along with clay and quartz. However, the gold grade exceeded 1 g/t only at the following position:

78.0 - 79.0 (1.00m) Au 1.9 g/t, Ag 15 g/t, Cu 0.02%, Pb 0.05%
Zn 1.40%, As 9.70%

#### 2-3 PD-10

(1) Purpose: Drilling was carried out at the same point, dipping with a different angle, to see conditions under the above-mentioned PD-9 hole.

(2) Lithology and mineralization: Most rocks are tuff breccia but dense and massive basaltic andesite exist at the depth of 80m, 120m and 183m. As a whole, it is chloritized and also epidotized. The matrix of tuff breccia at about 67.5m contains a black vitreous part of about 0.5mm in thickness, which shows a flow structure.

A vein was mineralized for 10.9m from 105.2m to 116.1m. As a whole, the average grade is Au 5.5 g/t but there are the following two high-grade parts:

This vein is considered to be on the extension of the ore shoot in the Diamante pit since no vein appeared between it and the bottom of the hole, though a small alteration was found there. The continuous grades at places including the above-mentioned two high-grade parts are as follows:

#### 2-4 PD-11

- (1) Purpose: This drilling was planned to survey the vicinity about 100m south of the ore shoot of the Diamante pit with the object of seeing \_\_the southward continuity from this pit.
- (2) Lithology and mineralization: The rocks are tuff breccia with intercalations of lava at 42m and 139m. As a whole, they are epidotized and show many green spots the size of 1 mm to 5 mm.

Mineralized parts were found at 131.8m to 138.0m as cores of sericitized clay and quartz veinlets but the results of analysis did not indicate that they contained gold, silver and other elements. These parts are considered to be on the extension from the principal vein of Diamante.

It is yet to be seen whether the vein will reappear.

#### 2-5 PD-12

- (1) Purpose: This drilling was carried out to see the mineralization under the above-mentioned PD-11.
- (2) Lithology and mineralization: Bedrock was hit at 13.3m. From this depth to 179.8m, the rocks were mainly tuff breccia and this contained five layers, three to six meters thick, of massive basaltic andesite lava between 108.8m and 153.5m.

As for mineralization, 179.8m to 193.6m was found to be a relatively thick altered zone but the results of analysis indicated that Au 0.9 g/t and Ag 10 g/t was present at 186.0m - 187.0m (1.00m) only, and at other levels there was no content of gold and silver and the content of sulfide minerals was small. The altered zone consisted of clay containing quartz fragments.

#### 2-6 PD-13

- (1) Purpose: There is the Gualquilia Norte pit about 200m southeast of the above-mentioned Diamante pit. It has a water-mill ore grinding equipment. Small-scale operation is in progress there, processing pyrite-containing ores mined from the pit. This hole purported to see the conditions under the Gualquilla Norte pit and was planned to survey a point about 100m in a beeline from the survey positions of the foregoing PD-11 and PD-12.
- (2) Lithology and mineralization: The country rock consists of alternate layers of tuff breccia and massive and compact basaltic andesite. The massive andesite includes vitreous parts showing flow structure.

Two lines of vein structure were found at about 76.5m and 100.6m but the results of analysis did not indicate the existence of gold; they just contained some silver and copper.

Footage (drilled length) Au Ag Cu Pb Zn As g/t g/t 
$$\%$$
 % % % 76.5 - 77.0 (0.50) tr 276 2.09 0.03 0.12 0.11

#### 2-7 PD-14

- (1) Purpose: This drilling was carried out to see the mineralization under the above-mentioned PD-13.
- (2) Lithology and mineralization: As in PD-13, alternate layers of tuff breccia and basaltic andesite appear in this hole. Fracture zones are found about 27m, 40m, 74m and 151m.

Veins were discovered at 123.7m - 129.0m, 141.0m - 141.7m and 158.3m - 164.4m. There are argillization and microcrystalline pyrite dissemination. These include fragments of quartz veins, but the results of analysis indicated that only the following two samples contained gold.

Footage (drilled length)	Au g/t	Ag g/t		РЬ %	Zn %	As %
m m m 160.3 - 161.3 (1.00)	4.6	8	0.02	0.04	0.32	0.35
163.3 - 164.4 (1.10)	2.0	35	0.12	0.13	2,56	2.62

### 2-8 PD-15

- (1) Purpose: In the Gualquilia Sur pit being operated in a small scale south of the Diamante principal vein, there is a fairly substantial quartz vein of 30 40cm in width and this vein contains several g/t of gold.

  The PD-15 hole is aimed to see the mineralization under this lode.
- (2) Lithology and mineralization: Alternate layers of tuff breccia and basaltic andesite appear. They are not only chloritized but, as a whole, they are also epidotized.

Four veins were found from the depth of 110m downward and each showed the following values in their analysis:

Footage (drilled length)	Au g/t	Ag g/t	Cu %	Pb %	Zn %	As %
m m m 110.1 - 113.4 (3.30)	2.0	46	0.27	0.12	0.25	0.84
120.8 - 121.4 (0.60)	1.6	43	0.24	0.03	0.64	1.73
147.5 - 148.5 (1.00)	2.8	9	0.00	0.05	0.13	0.26
152.1 = 153.1 (1.00)	0.9	9	0.01	0.03	0.13	1.13

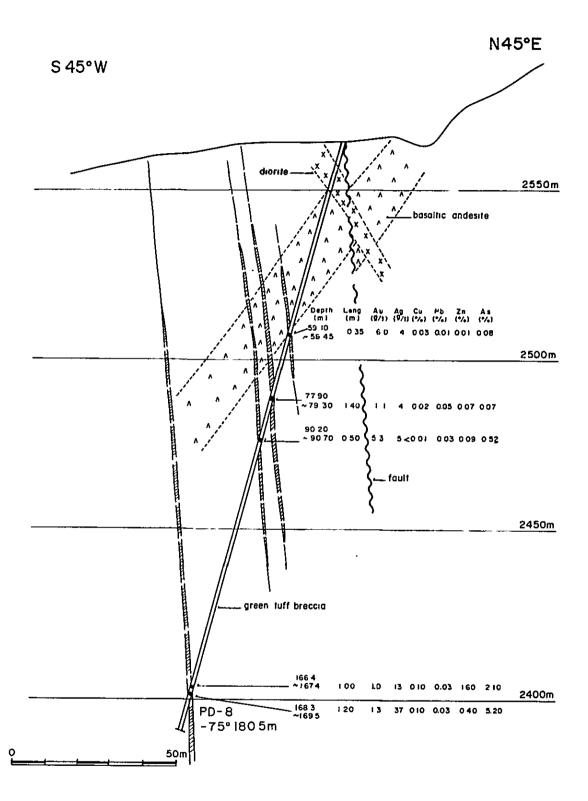


Fig. II - 9 Geological Section for PD - 8

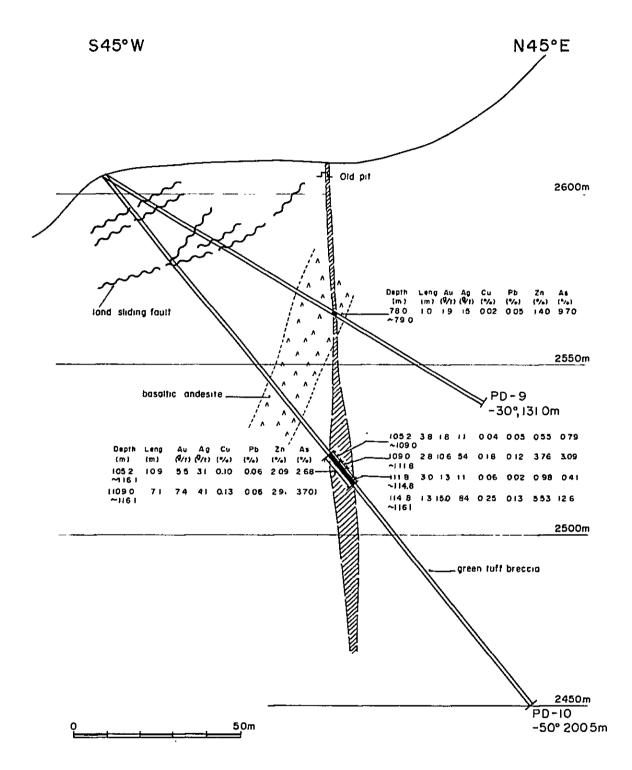


Fig. II - IO Geological Section for PD-9, PD-IO

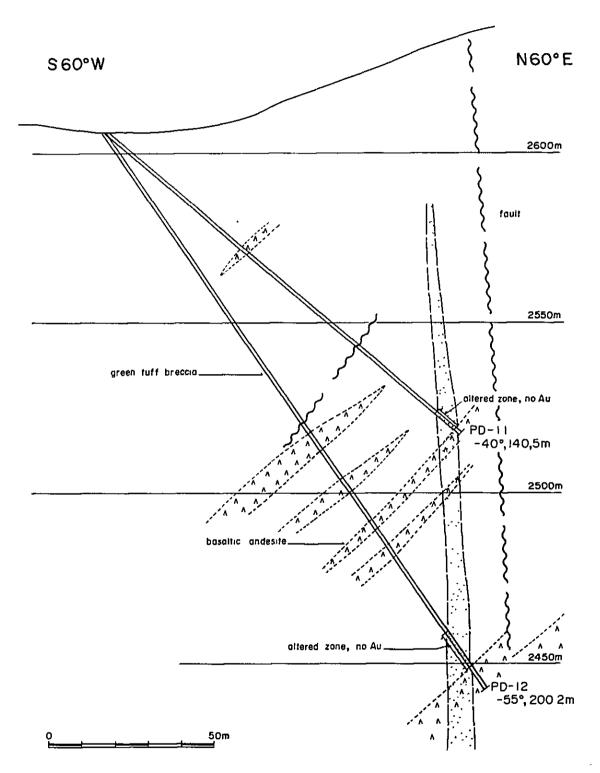


Fig. II – II Geological Section for PD-II, PD-I2

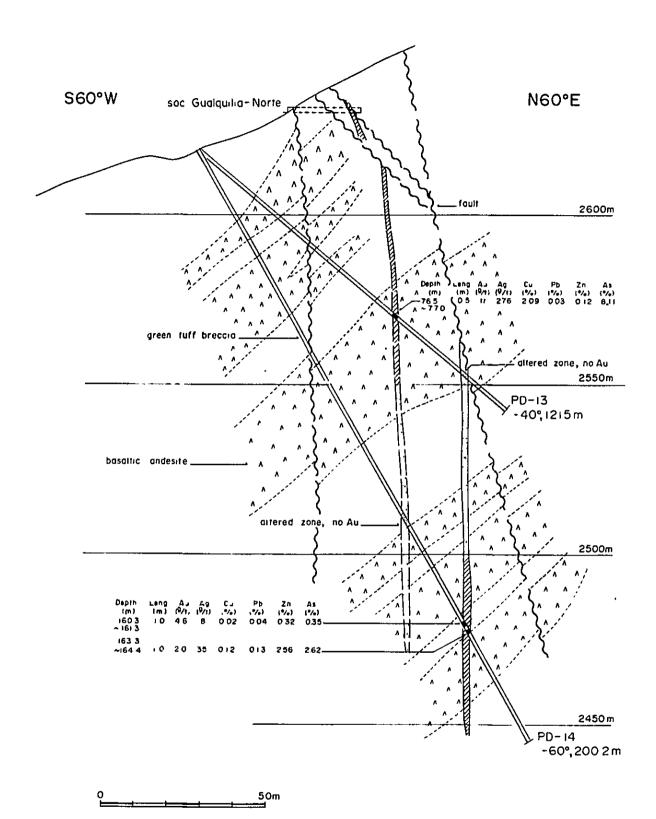


Fig. II - 12 Geological Section for PD-13, PD-14

S60°W N60°E

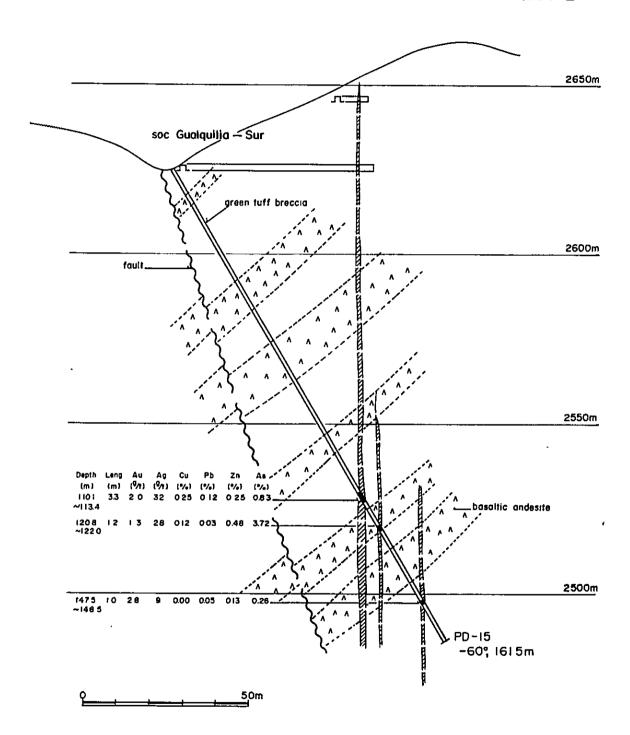


Fig. II - I3 Geological Section for PD- I5

APPENDICES
PART I
GEOLOGICAL AND GEOCHEMICAL
DATA

## LIST OF APPENDICES

- A. I-1 Chemical Analysis of Soil Samples
- A. I-2 Chemical Analysis of Ore Samples
- A. I-3 Chemical Analysis of Altered Rock Samples
- A. I-4 Microscopic Observation of the Thin Sections
- A. I-5 Microscopic Observation of the Polished Sections
- A. I-6 Photomicrographs
- A. I-6-1 Thin Section
- A. I-6-2 Polished Section
- A. I-6-3 EPMA
- A. I-7-1 Summary of X-ray Diffractive Analysis
- A. I-7-2 X-ray Diffraction Chart

## A. I - I Chemical Analysis of Soil Samples

Key to the following tables,

No : sample number area : PA Paraiso

DL Delicia

DQ Desquite

BO Bombona

DA Diamante

GT Gitana

MA Between Paraiso-Gitana

Line : geochemical sampling line

Rock : geology

CG coarse grained granodiorite

FG fine grained granodiorite

GR green volcanic rock

SH shale

Zn, As : assay value in ppm

N	0	AREA	LIHE	RDCA	žH	AS	ND	AREA	LINE	ROCK	ŽH	AS
			***		75	7.0	FS 101	PA	D0 4	£6	29	2.D 13.0
FS FS	2	PA Pa	00 8 00 8	CG CG	28	5.0	FS 102 FS 103	PA Pa	004 004	CG CG	56 63	18.0
FS	3	PA	DOB	C.G	<b>6</b> 0	3.0	FS 104	PA	D0 4	CG	71	10.0
F5	•	PA	DOB	CE	48	0.1	FS 105	PA	D04	CE	84	4.0
FS FS	5	PA Pa	00 B	CG CG	47 28	5.0 4.0	FS 104 FS 107	PA PA	D0 4 D0 4	CG CG	28 40	0.1 0.1
FS	7	PA	DOU	22	37	<b>→•</b> 0	F5 108	PA	004	ČE	42	4.0
FS	8	PA	008	CC	77	10.0	FS 109	PA	DQ 4	55 55 56 56	52	1.0
FS	9	PA	008	CC	36	4.0 2.0	FS 110	PA	D04	CE	49	0.1
FS FS	10 11	PA Pa	008 008	CG CG	31 73	4.0	FS 111 FS 112	PA Pa	D0 4 D0 4	CG CG	45 42	4.0 3.0
F\$	12	PA	800	čĞ	26	3.0	F5 113	PA	004	ČĞ	44	1.0
FS	13	PA	DOB	ÇĞ	48	2.0	F5 114	PA	004	CG	47	0.1
FS FS	14 15	PA PA	DOS DOS	CG CG	74 55	8.0 6.0	FS 115 FS 116	PA PA	DQ 4 DQ 4	CG CG	46	1.0 0.1
FS	16	PA	008	ČĠ	41	5.0	FS 116 FS 117	PA	204	ČĞ	46	1.0
FS	17	PA	000	CG	26	4.0	FS 110.	PÁ	004	ĊG	104	72.0
FS	18	PA	DOB	CG	44 29	5.0	FS 119	PA	004	CG	46	5.0
FS FS	19 20	PA PA	00 B 00 b	CG	43	4.0 3.0	FS 120 FS 121	PA PA	004 004	CG CG	30 67	13.0 2.0
FS	21	PA	008	ČĞ	20	3.0	F5 122	PA	004	ČĞ	32	1.0
FS	22	PA	008	56	20	3.0	F5 123	PA	004	CG	26 52	0.1
FS FS	23 24	PA PA	DO 8	CG CG	41 37	4.0	F5 124 F5 125	PA PA	D0 4	CG CG	52 28	2.0 4.0
FS	25	PÃ	006	čĞ	50	4.0	FS 126	PA	004	ČĞ	58	1.0
F5	26	PA	006	CG	34	4.0	FS 127	PA	D04	CG	50	1.0
15	27	PA	800	CG	31 56	6 + D	FS 128	PA PA	D04	ÇĞ	62 73	0.1 3.0
FS FS	28A 28B	PA PA	D08	CG CG	71	4.0	FS 129 FS 130	PA PA	D0 4 D0 4	CG CG	73 32	1.0
FS	29	PA	D0 P	ÇG	74	3.0	F5 131	PA	D04	CG	69	3.0
FS	30	PA	DOB	56	94	14.0	F5 132	PA	D04	CG	54	6.1
FS FS	31 32	PA PA	008 008	CG CG	43 25	3.0 3.0	FS 133 FS 134	PA PA	D0 4 D0 4	ÇG CG	34 29	0.1 1.0
F 5	33	PA	DDB	56	16	4.0	FS 134 FS 135	PA	D04	CG	30	0.1
FS	34	PA	008	CG	86	4.0	FS 136	PA	D04	t G	120	4.0
FS FS	35 36	PA Pa	DDB DDB	CG CG	84 34	10-0 5-0	FS 137 FS 138	PA PA	DD 4 DO 4	56 56	35 42	0.1 2.0
F\$	37	PA	006	ČĞ	37	6.0	FS 139	PA	004	56	32	1.0
FŠ	38	PA	000	CG	37	5.0	F5 140	PA	004	CG	56	1.0
۴s	39	PA	00 B	CG	34 64	5.0 6.0	FS 141	PA	D04	ÇG CG	49	5.0
F5 F5	40	PA PA	008 008	CG	44	13.0	FS 1+2 FS 1+3	PA PA	004	CG	13 25	0.1 0.1
65	42	PA	909	čě	55	8.0	FS 144	PA	004	CG	71	0.1
F5	4.3	PA	DOF	ÇĢ	25	4.0	F5 145	PA	004	CG	52	0.1 2.0 0.1
F 5	44	PA PA	DQ #	C.	32 38	1.L 7.0	F5 146 F5 147	PA PA	004 004	C G	35 33	0.1
FS	46	PA	DOB	čů	35	1.0	F5 148	PA	UQ4	ČĿ	25	0.1
FS	.47	PA	DO N	ĊĞ	26	1.1	F5 149	PA	804	Ç.	26	0.1
FS	48	PA	DOW	CG	25 21	5.E 4.L	FS 150	PA	004	CC	53	0.1
FS	50	PA PA	50 M	CG CG	20	0.1	FS 151 FS 152	PA PA	DQ4 DQ4	CG CG	45 39	0.1
FS	51	PA	DOB	ČĞ	80	8.0	FS 153	PA	004	CG	54	0.1
FS	52	PA	DOB	CG	41	2.0	F\$ 154	PA	DO 4	CG	43	0.1
FS	53 54	PA Pa	008	CG.	43 34	6.0 5.0	FS 155	PA	D04	۵غ	43	0.1
F5	55	PA	008 008	56 55	30	16.0	FS 156 FS 157	PA PA	DO 4 DO 4	CG CG	25 35	0.1 8.0
F\$	56	PA	DOB	CG	54	43.0	F\$ 158	PA	DO 4	CG	25	0.1
FS	57	PA	D08	ÇĢ	20 36	4.0 6.0	FS 159	PA	D0 4	CG	24	1.0
FS FS	58 59	PA PA	008	CG CG	43	9.0	FS 160 FS 161	PA PA	D0 4 D0 4	CG CG	54 56	0.1
F.S	60	PA	008	CG	44	22.0	FS 162	PA	DQ 4	CG	41	2.0
FS	61	PA	800	CG	80	300-0	FS 163	PA	D04	CG	37	0.1
FS FS	62 63	PA PA	008 008	CG CG	43 100	7.0 265.0	FS 164 FS 165	PA Pa	D0 4 D0 4	ce ce	48 24	2.0 0.1
FS	64	PA	DOS	čč	26	7.0	FS 166	PA	D04	čč	42	0.1
FS	65	PA	DOB	53	66	6.0	FS 167	PA	D04	CG	45	0.1
FS	66 67	PA PA	DO B DO B	CG	42 49	4.0 5.0	F\$ 168	PA PA	004	CG	63 76	5.0 5.0
FS FS	68	PA	DOB	55	51	5.0	FS 169 FS 170	PA	D04 D02	Č6	34	1.0
F\$	69	PA	008	CG	33	0.0	FS 171	PA	200	CG	44	1.0
FS	70	PA	008	CG.	69 49	10.0	FS 172	PA	500	CG	55	5.0
FS FS	71 72	PA Pa	D08	CG	44	4.0	FS 173 FS 174	PA PA	200	CG	37 40	5.0 5.0
FS	73	PA	800	¢G	34	4.0	FS 175	PA	500	CG	33	3.0
FS	74	PA	D0 6	ce	39	3.0	FS 176	PA	D0 2	CG	48	4.0
FS FS	75 76	PA PA	00 a 00 a	CG CG	44 65	13.0 5.0	FS 177 FS 178	PA PA	2005	CG CG	37 38	5.0 0.1
F.5	77	PA	8 00	CG	69	5.0	FS 179	PA	205	ÇG	47	1.0
FS	78	PA	DOB	CG	78	5.0	F5 180	PA	004	ÇG	41	4.0
FS	79	PA	DQ 8	CG	69 73	0.4 0.4	FS 181	PA	002	CG	53	0.1
FS FS	80 81	PA Pa	008	CG CG	64	6.0	FS 182 FS 183	PA PA	200	CG CG	42 43	4.0 0.1
F۵	85	PA	D08	ÇG	65	3.0	FS 184	PA	200	CG	52	5.0
F.S	83	PA	DOS	ce	79	9.0	FS 185	PA	DOS	CG	44	1.0
FS FS	84 85	PA PA	DO 8 DO 8	CG CG	65 77	5.0 5.0	FS 186 FS 187	PA Pa	200	C6 CG	17	2.0 0.1
FS	86	PA	DOS	CG	54	1.0	FS 188	PA	200	CG	32	5.0
FŠ	87	PA	006	CG	52	35.0	FS 189	PA	DQ 5	CG	30	4,0
FS FS FS FS	88	PA PA	D06 D08	CG CG	52 43	48.0 5.0	FS 190	PA	200	CG	49	1.0
F.5	89 90	PA	DOB	CG	36	15.0	FS 191 FS 192	DL DL	FO; FO;	CG CG	61 38	3.D 6.0
FS	91	PA	DOS	CG	34	34.0	FS 193	οĹ	FOI	CG	15	5.0
F.S	92	PA	DO b	CC	35	74.0	F5 194	OL	FO 1	CG	42	4.0
FS FS	93 94	PA PA	D04 D04	EG EG	19 42	3.0 6.0	FS 196	DL	FOI	CG	23	2.0
F.5	95	PA	DO 4	CG	31	4.0	F5 197 F5 198	OL OL	FD1 FD1	CG CG	21 29	1.0 1.0
FS	76	PA	D04	23	66	20.0	FS 199	DL	FO1	CG	21	1.0
FS	97	PA PA	D0 4	CC.	59 30	1.0 1.0	F5 200	ŊL	FOL	CG	32	4.0
FS FS	48	PA	D04	CG CG	45	14.0	F5 201 F5 202	Dr Dr	F01	CG CG	41 10	5.0 5.0
15	160	PA	D0 4	Lu	63	0.1	F5 203	DL	FÖÌ	Č	18	9.0
						i	1					

Section   Sect	h	0	AREA	LINE	RDCA	ZN	A5	P0	AKEA	LINE	ADCK	ZN	AS
10   10   10   10   10   10   10   10	FS	204	DL	FO1	CG	12		F5 307	0L			21	3.0
15   15   15   15   15   15   15   15			DL										
15   150													
15   100								FS 310					
								F3 311					
15	2.7												2.0
15   11						16	1.0						3.0
14	FS							F\$ 315	DL		CG		6.0
12   11	FS	213							DL				4.0
15									<u>D</u> L				25.0
15													780-0
15   216													
15   21													
Section   Sect							18.0						
1.   1.   1.   1.   1.   1.   1.   1.					CG			FS 323	DL		CG	24	13.0
1.													28.0
For   1244								FS 325					
10							84-0	F5 326					2.0
15   221							10.0						
1.5   227   01													
10		227											
1.   1.   1.   1.   1.   1.   1.   1.										03E	FG		5.0
For   100	F۵		ÐL										14.0
S	FS												6.0
F5   233													
S													
S													
Section   Fig.													
F5   237						30	3.0						5.0
Fig.   228				FO1	CG	20	4.0	FS 339	DL	436	FG	53	3.0
F5   240   DL   F01   CC	F۵	238	Dt.		ČĆ								1.0
FS   241	F5	239											
\$\frac{2}{5}\$\$ 242 \text{Cl}\$\$\$ \$\frac{1}{10}\$\$\$ \$\frac{1}{10}\$\$\$ \$\frac{1}{10}\$\$\$ \$\frac{1}{10}\$\$\$ \$\frac{1}{10}\$\$\$\$ \$\frac{1}{10}\$\$\$\$ \$\frac{1}{10}\$												£3	
## 5 244 OL F01 C6 77 2.0 F5 345 OL 200 C6 22 95.0 F5 245 OL 200 C6 32 95.0 F5 245 OL 200 C6 48 5.0 F5 245 OL 200 C6 68 5.0 F5									O.		CU.		
S											23		
5.5         246         DQ         F01         CC         200         Job         F53         347         DL         200         CG         42         5.0           6.5         24.0         DD         22A         CG         313         1.00         F53         348         DL         200         CG         32         3.00           6.5         24.0         DD         22A         CG         30         3.00         F53         348         DL         200         CG         32         2.00         8.00         CG         32         2.00         CG         22A         CG         200         1.00         1												śż	
15   240   DE   22A   CG   SE   SE   SE   SE   SE   SE   SE   S		245			ČC			FS 347		208			6.0
F5   248			99										5.0
S   249													
S													
\$\frac{2}{5}\$ 251 00 22A													2.0
S												24	
1.0													
F5   254				A55			1.0				CG		
## 2526			00		CG			F5 356	υL	cop	CG	52	₹.6
## ## ## ## ## ## ## ## ## ## ## ## ##	FS	255	00	22 A									
## 25 25 26 DD 22A													
## 25													
## ## ## ## ## ## ## ## ## ## ## ## ##													
## 241 00 22A CG 37 1.0 #5 343B DL 20B CG 49 3.0  #\$5 263 00						32	2.0						
#5 202 00							1.0						
E5         263         00         42A         CG         34         3.0         F5         364C         DL         208         CG         30         3.0           F5         264         D0         22A         CG         18         4.0         F5         365         DL         208         CG         89         15.0           F5         266         D0         22A         CG         18         4.0         F5         365         DL         208         CG         31         3.0           F5         266         D0         D24         CG         10         3.0         F5         347         DL         208         CG         31         3.0           F5         260         D0         D24         CG         24         2.0         F5         347         DL         208         CG         31         3.0           F5         271         D0         D24         CG         24         2.0         F5         377         DL         15         CG         91         45.0           F5         271         D0         D24         CG         24         2.0         F5         371         DL						20							
#5 285 00	FŠ		09					FS 363C	ÐL				
65 266 DO 222A CG 16 2.0 F5 346 OL 208 FG 34 3.0 F5 267 DO D24 CG 16 1.0 F5 368 OL 208 CG 31 3.0 F5 268 DO D24 CG 16 1.0 F5 368 OL 208 CG 41 4.0 F5 269 DO D24 CG 18 3.0 F5 369 OL 208 CG 41 4.0 F5 269 DO D24 CG 18 3.0 F5 369 OL 208 CG 41 4.0 F5 269 DO D24 CG 18 3.0 F5 370 OL 15 CG 91 45.0 F5 271 DO D24 CG 24 2.0 F5 370 OL 15 CG 91 45.0 F5 272 DO D24 CG 28 2.0 F5 370 OL 15 CG 91 45.0 F5 273 DO D24 CG 28 1.0 F5 372 OL 15 CG 105 55.0 F5 273 DO D24 CG 28 1.0 F5 372 OL 15 CG 77 85.0 F5 275 DO D24 CG 28 1.0 F5 374 UL 15 CG 77 85.0 F5 275 DO D24 CG 17 1.0 F5 374 UL 15 CG 55 3.0 F5 275 DO D24 CG 17 1.0 F5 374 UL 15 CG 57 285 DF5 275 DO D24 CG 17 1.0 F5 375 UL 15 CG 68 40.0 F5 277 DO D24 CG 17 1.0 F5 375 UL 15 CG 67 77 4.0 F5 277 DO D24 CG 28 1.0 F5 376 UL 15 CG 57 285 DF5 277 DO D24 CG 28 1.0 F5 376 UL 15 CG 67 77 4.0 F5 278 DO D24 CG 28 1.0 F5 376 UL 15 CG 77 4.0 F5 278 DO D24 CG 28 1.0 F5 376 UL 15 CG 77 4.0 F5 278 DO D24 CG 28 1.0 F5 376 UL 15 CG 77 4.0 F5 278 DO D24 CG 28 1.0 F5 378 UL 15 CG 77 4.0 F5 278 DO D24 CG 28 1.0 F5 378 UL 15 CG 77 4.0 F5 278 DO D24 CG 28 1.0 F5 378 UL 15 CG 77 4.0 F5 278 DO D24 CG 38 2.0 F5 378 UL 15 CG 37 2.0 F5 278 DO D24 CG 38 2.0 F5 378 UL 15 CG 37 2.0 F5 278 DO D24 CG 38 2.0 F5 378 UL 15 CG 37 2.0 F5 280 DO D24 CG 47 2.0 F5 378 UL 15 CG 37 2.0 F5 280 DO D24 CG 47 2.0 F5 380 UL 15 CG 37 2.0 F5 281 DO D24 CG 47 2.0 F5 380 UL 15 CG 37 2.0 F5 281 DO D24 CG 47 2.0 F5 380 UL 15 CG 37 2.0 F5 281 DO D24 CG 47 2.0 F5 380 UL 15 CG 37 2.0 F5 281 DO D24 CG 47 2.0 F5 380 UL 15 CG 37 2.0 F5 281 DO D24 CG 47 2.0 F5 380 UL 15 CG 37 2.0 F5 281 DO D24 CG 47 2.0 F5 380 UL 15 CG 37 2.0 F5 281 DO D24 CG 47 2.0 F5 380 UL 15 CG 37 2.0 F5 281 DO D24 CG 47 2.0 F5 380 UL 15 CG 37 2.0 F5 281 DO D24 CG 47 2.0 F5 380 UL 15 CG 47 2.0 F5 281 DO D24 CG 47 2.0 F5 380 UL 15 CG 47 2.0 F5 281 DO D24 CG 47 2.0 F5 380 UL 15 CG 47 2.0 F5 281 DO D24 CG 47 2.0 F5 380 UL 15 CG 47 2.0 F5 380 UL 15 CG 47 2.0 F5 380 UL 15 CG 47 2.0 F5 380 UL 15 CG 47 2.0 F5 380 UL 15 CG 47 2.0 F5 380 UL 15 CG 47 2.0 F5 380 UL 15 CG 47 2.0 F5 380					CG		4.0	FS 364					\$ • 0
## 247 DO				ASS									15.0
S											CC		3.0
#\$ 200 00 024 CG 28 2.0 F5 370 0L 208 CG 50 15.0 F5 270 0D 024 CG 28 2.0 F5 370 0L 15 CG 49 40.0 F5 272 0D 024 CG 39 1.0 F5 370 0L 15 CG 49 40.0 F5 272 0D 024 CG 39 1.0 F5 372 0L 15 CG 49 40.0 F5 273 0D 024 CG 28 1.0 F5 373 0L 15 CG 55 3.0 F5 275 0D 024 CG 28 1.0 F5 375 0L 15 CG 55 3.0 F5 277 0D 024 CG 28 1.0 F5 377 0L 15 CG 55 3.0 F5 277 0D 024 CG 28 1.0 F5 377 0L 15 CG 57 28.0 F5 278 0D 024 CG 28 1.0 F5 377 0L 15 CG 37 28.0 F5 278 0D 024 CG 30 0.1 F5 379 0L 15 CG 37 28.0 F5 279 0D 024 CG 62 0.1 F5 379 0L 15 CG 38 25.0 F5 280 0D 024 CG 44 8.0 F5 379 0L 15 CG 38 25.0 F5 281 0D 024 CG 44 8.0 F5 379 0L 15 CG 38 25.0 F5 283 0D 024 CG 44 8.0 F5 380 0L 15 CG 37 40.0 F5 283 0D 024 CG 44 8.0 F5 380 0L 15 CG 38 25.0 F5 283 0D 024 CG 44 8.0 F5 380 0L 15 CG 37 40.0 F5 283 0D 024 CG 44 8.0 F5 380 0L 15 CG 37 40.0 F5 283 0D 024 CG 44 8.0 F5 380 0L 15 CG 37 40.0 F5 283 0D 024 CG 44 8.0 F5 380 0L 15 CG 38 25.0 F5 283 0D 024 CG 44 8.0 F5 380 0L 15 CG 38 25.0 F5 283 0D 024 CG 46 8.0 F5 380 0L 15 CG 40 76.0 F5 283 0D 024 CG 46 8.0 F5 380 0L 15 CG 40 76.0 F5 283 0D 024 CG 46 8.0 F5 380 0L 15 CG 40 76.0 F5 283 0D 024 CG 46 8.0 F5 380 0L 15 CG 40 76.0 F5 283 0D 024 CG 45 8.0 F5 380 0L 15 CG 40 76.0 F5 283 0D 024 CG 45 8.0 F5 380 0L 15 CG 40 76.0 F5 283 0D 024 CG 45 8.0 F5 380 0L 15 CG 40 76.0 F5 283 0D 024 CG 45 8.0 F5 380 0L 15 CG 40 76.0 F5 283 0D 024 CG 45 8.0 F5 380 0L 15 CG 40 76.0 F5 283 0D 024 CG 45 8.0 F5 380 0L 15 CG 40 76.0 F5 283 0D 024 CG 45 8.0 F5 380 0L 15 CG 40 76.0 F5 283 0D 024 CG 45 8.0 F5 380 0L 15 CG 40 76.0 F5 283 0D 024 CG 45 8.0 F5 380 0L 15 CG 40 76.0 F5 380 0D 15 CG 40 76.0 F5 380 0D 15 CG 40 76.0 F5 380 0D 15 CG 40 76.0 F5 380 0D 15 CG 40 76.0 F5 380 0D 15 CG 40 76.0 F5 380 0D 15 CG 40 76.0 F5 380 0D 15 CG 40 76.0 F5 380 0D 15 CG 40 76.0 F5 380 0D 15 CG 40 76.0 F5 380 0D 15 CG 40 76.0 F5 380 0D 15 CG 40 76.0 F5 380 0D 15 CG 40 76.0 F5 380 0D 15 CG 40 76.0 F5 380 0D 15 CG 40 76.0 F5 380 0D 15 FG 40 40 40 0D 15 CG 40 76.0 F5 380 0D 15 C							1.0						
#\$ 270 00 024 C6 28 2-0 F5 370 01 15 C6 91 45.0 F5 271 00 024 C6 28 1.0 F5 371 01 15 C6 99 40.0 F5 273 00 024 C6 28 1.0 F5 373 01 15 C6 79 85.0 F5 273 00 024 C6 28 1.0 F5 373 01 15 C6 55 35.0 F5 275 00 024 C6 70 84.0 F5 375 01 15 C6 77 88.0 F5 276 00 024 C6 70 84.0 F5 375 01 15 C6 77 88.0 F5 277 00 024 C6 70 84.0 F5 375 01 15 C6 77 88.0 F5 278 00 024 C6 30 1.0 F5 375 01 15 C6 77 88.0 F5 278 00 024 C6 30 1.0 F5 375 01 15 C6 113 25.0 F5 278 00 024 C6 30 1.0 F5 375 01 15 C6 113 25.0 F5 278 00 024 C6 82 0.1 F5 378 01 15 C6 113 25.0 F5 278 00 024 C6 82 0.1 F5 378 01 15 C6 113 25.0 F5 280 00 024 C6 40 1.0 F5 378 01 15 C6 37 88.0 F5 281 00 024 C6 40 1.0 F5 380 01 15 C6 38 25.0 F5 281 00 024 C6 40 1.0 F5 381 01 15 C6 77 80.0 F5 283 00 024 C6 40 1.0 F5 381 01 15 C6 59 50.0 F5 283 00 024 C6 40 1.0 F5 381 01 15 C6 59 50.0 F5 283 00 024 C6 40 1.0 F5 381 01 15 C6 59 50.0 F5 283 00 024 C6 40 1.0 F5 381 01 15 C6 59 50.0 F5 283 00 024 C6 17 1.0 F5 381 01 15 C6 40 76.0 F5 283 00 024 C6 17 1.0 F5 383 01 15 C6 40 76.0 F5 283 00 024 C6 17 1.0 F5 383 01 15 C6 40 76.0 F5 285 00 024 C6 17 1.0 F5 383 01 15 C6 40 76.0 F5 285 00 024 C6 17 1.0 F5 383 01 15 C6 40 76.0 F5 285 00 024 C6 40 40 40 40 40 40 40 40 40 40 40 40 40				DZe	čů		2.0						
#1 271 00 024 C6 39 1.0 F5 372 0L 15 C6 49 40.0  #1 272 00 024 C6 39 1.0 F5 372 0L 15 C6 79 85.0  #5 273 00 024 C6 15 3.0 F5 373 0L 15 C6 79 85.0  #5 274 00 024 C6 17 1.0 F5 375 0L 15 C6 88 40.0  #5 275 00 024 C6 17 1.0 F5 375 0L 15 C6 88 40.0  #5 276 00 024 C6 28 1.0 F5 377 0L 15 C6 88 40.0  #5 277 00 024 C6 28 1.0 F5 377 0L 15 C6 77 4.0  #5 278 00 024 C6 30 1.0 F5 377 0L 15 C6 77 4.0  #5 279 00 024 C6 62 0.1 F5 377 0L 15 C6 113 25.0  #5 280 00 024 C6 62 0.1 F5 379 0L 15 C6 113 25.0  #5 280 00 024 C6 40 1.0 F5 381 0L 15 C6 77 40.0  #5 281 00 024 C6 40 1.0 F5 381 0L 15 C6 77 40.0  #5 282 00 024 C6 40 1.0 F5 381 0L 15 C6 77 40.0  #6 283 00 024 C6 40 1.0 F5 381 0L 15 C6 77 40.0  #6 284 00 024 C6 40 1.0 F5 381 0L 15 C6 77 40.0  #6 285 00 024 C6 40 1.0 F5 381 0L 15 C6 77 40.0  #6 285 00 024 C6 44 6.0 F5 382 0L 15 C6 14 16.0  #6 285 00 024 C6 44 6.0 F5 382 0L 15 C6 14 16.0  #6 285 00 024 C6 45 6.0 F5 383 0L 15 C6 40 76.0  #6 285 00 024 C6 45 6.0 F5 383 0L 15 C6 40 76.0  #6 285 00 024 C6 45 6.0 F5 383 0L 15 C6 40 76.0  #6 286 00 024 C6 45 6.0 F5 383 0L 15 C6 40 76.0  #6 287 00 024 C6 45 6.0 F5 383 0L 15 C6 40 76.0  #6 288 00 024 C6 45 6.0 F5 383 0L 15 C6 40 76.0  #6 288 00 024 C6 45 6.0 F5 383 0L 15 C6 81 40.0  #6 288 00 024 C6 45 6.0 F5 383 0L 15 C6 81 40.0  #6 288 00 024 C6 45 6.0 F5 383 0L 15 C6 81 40.0  #6 289 00 024 C6 45 6.0 F5 383 0L 15 C6 81 40.0  #6 290 00 024 C6 45 6.0 F5 383 0L 15 C6 81 40.0  #6 290 00 024 C6 45 6.0 F5 387 80 03w F6 27 14.0  #6 290 00 024 C6 45 6.0 F5 387 80 03w F6 27 2.0  #6 290 00 024 C6 45 6.0 F5 380 0L 03w F6 37 2.0  #6 290 00 024 C6 45 6.0 F5 380 0L 03w F6 37 2.0  #6 290 00 024 C6 45 6.0 F5 380 0L 03w F6 37 2.0  #6 290 00 024 C6 45 6.0 F5 380 0L 03w F6 37 2.0  #6 290 00 024 C6 45 6.0 F5 380 0L 03w F6 37 2.0  #6 290 00 024 C6 45 6.0 F5 380 0L 03w F6 37 2.0  #6 290 00 024 C6 46 6.0 F5 380 0L 03w F6 37 2.0  #6 290 00 024 C6 46 6.0 F5 380 0L 03w F6 37 2.0  #6 290 00 024 C6 46 6.0 F5 380 0L 03w F6 37 2.0  #6 290 00 00 00 00 00 00 00 00 00 00 00 00 0				924	CG	18	3.0	FS 370	DL	15	CG	91	45.0
F5 273 00 024 C6 39 1-0 F5 373 0L 15 C6 77 85.0 F5 274 0U 024 C6 26 1-0 F5 373 0L 15 C6 77 85.0 F5 275 0U 024 C6 17 1-0 F5 375 0L 15 C6 55 3.0 F5 276 0U 024 C6 17 1-0 F5 375 0L 15 C6 57 28.0 F5 276 0U 024 C6 26 1-0 F5 375 0L 15 C6 57 28.0 F5 277 0U 024 C6 30 1-0 F5 377 0L 15 C6 57 28.0 F5 278 0U 024 C6 30 1-0 F5 377 0L 15 C6 113 25.0 F5 278 0U 024 C6 47 2-0 F5 378 0L 15 C6 37 4.0 F5 378 0L 15 C6 38 25.0 F5 280 0U 024 C6 47 2-0 F5 380 0L 15 C6 38 25.0 F5 281 0U 024 C6 47 2-0 F5 380 0L 15 C6 38 25.0 F5 282 0U 024 C6 44 8-0 F5 382 0L 15 C6 77 40.0 F5 283 0U 024 C6 44 8-0 F5 382 0L 15 C6 59 5.0 F5 284 0U 024 C6 17 1-0 F5 383 0L 15 C6 14 18.0 F5 285 0U 024 C6 17 1-0 F5 383 0L 15 C6 41 18.0 F5 285 0U 024 C6 17 1-0 F5 383 0L 15 C6 63 22.0 F5 285 0U 024 C6 17 1-0 F5 385 0L 15 C6 63 22.0 F5 285 0U 024 C6 17 1-0 F5 385 0L 15 C6 63 22.0 F5 285 0U 024 C6 17 1-0 F5 385 0L 15 C6 63 22.0 F5 285 0U 024 C6 17 1-0 F5 385 0L 15 C6 63 22.0 F5 285 0U 024 C6 17 1-0 F5 385 0L 15 C6 63 22.0 F5 285 0U 024 C6 17 1-0 F5 385 0L 15 C6 63 22.0 F5 285 0U 024 C6 17 1-0 F5 385 0L 15 C6 63 22.0 F5 285 0U 024 C6 17 1-0 F5 385 0L 15 C6 63 22.0 F5 285 0U 024 C6 15 0-1 F5 385 0L 15 C6 81 40.0 F5 287 0U 024 C6 15 0-1 F5 385 0L 15 C6 81 40.0 F5 287 0U 024 C6 15 0-1 F5 385 0L 15 C6 81 40.0 F5 287 0U 024 C6 15 0-1 F5 385 0L 15 C6 81 40.0 F5 287 0U 024 C6 15 0-1 F5 385 0L 15 C6 81 40.0 F5 287 0U 024 C6 15 0-1 F5 385 0L 15 C6 81 40.0 F5 287 0U 024 C6 15 0-1 F5 385 0L 15 C6 81 40.0 F5 287 0U 024 C6 15 0-1 F5 385 0L 15 C6 81 40.0 F5 385 0	F۵	271	04	DZ 4									40.0
F5 274 DU D24 CG 17 1-0 F5 375 UL 15 CG 55 3-0 F5 275 DU D24 CG 17 1-0 F5 375 UL 15 CG 68 40.0 F5 277 DQ D24 CG 40 F5 277 UL 15 CG 68 40.0 F5 277 DQ D24 CG 40 F5 277 UL 15 CG 67 7 4.0 F5 278 DU D24 CG 40 F5 277 UL 15 CG 17 4.0 F5 278 DU D24 CG 40 F5 277 UL 15 CG 17 4.0 F5 278 DU D24 CG 40 F5 277 UL 15 CG 18 5.0 F5 279 DU D24 CG 40 F5 277 UL 15 CG 18 5.0 F5 280 DU D24 CG 40 F5 277 UL 15 CG 18 5.0 F5 280 DU D24 CG 40 F5 277 UL 15 CG 18 5.0 F5 280 DU D24 CG 40 F5 279 UL 15 CG 40 F5 280 DU D24 CG 40 F5 280 DU D24 CG 40 F5 280 DU D24 CG 40 F5 280 DU D24 CG 40 F5 280 DU D24 CG 40 F5 280 DU D24 CG 40 F5 280 DU D24 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 17 1-0 F5 280 DU D25 CG 52 4-0 F5 280 BU D25 CG 55 5-0 F5 280 DU D25 CG 52 5-0 F5 280 BU D25 CG 55 5-0 F5 28	FS	272											
F5 275 DU D24 CG 28 1.0 F5 376 UL 13 CG 66 40.0 F5 277 DQ D24 CG 40 1.0 F5 378 UL 15 CG 67 28.0 CG 113 25.0 CG 113													93.0
F5 276 D0 D24 C6 28 1.0 F5 376 DL 15 C6 37 28.0 F5 277 D0 D24 C6 30 1.0 F5 377 DL 15 C6 77 4.0 F5 278 D0 D24 C6 62 0.1 F5 379 DL 15 C6 48 3.0 F5 279 D0 D24 C6 46 20.1 F5 379 DL 15 C6 48 3.0 F5 280 D0 D24 C6 47 2.0 F5 380 DL 15 C6 38 3.0 F5 281 D0 D24 C6 44 8.0 F5 381 DL 15 C6 77 40.0 F5 281 D0 D24 C6 44 8.0 F5 381 DL 15 C6 39 5.0 F5 283 D0 D24 C6 17 1.0 F5 381 DL 15 C6 39 5.0 F5 283 D0 D24 C6 17 1.0 F5 383 DL 15 C6 14 18.0 F5 283 D0 D24 C6 17 1.0 F5 385 DL 15 C6 14 18.0 F5 285 D0 D24 C6 17 1.0 F5 385 DL 15 C6 63 22.0 F5 285 D0 D24 C6 17 1.0 F5 385 DL 15 C6 63 22.0 F5 285 D0 D24 C6 17 1.0 F5 385 DL 15 C6 63 22.0 F5 285 D0 D24 C6 17 1.0 F5 385 DL 15 C6 63 22.0 F5 285 D0 D24 C6 52 8.0 F5 385 DL 15 C6 81 40.0 F5 385 DL 15 C6 81 40.0 F5 285 D0 D24 C6 52 8.0 F5 387 80 D3w F6 17 14.0 F5 288 D0 D24 C6 52 8.0 F5 387 80 D3w F6 17 14.0 F5 288 D0 D24 C6 52 8.0 F5 387 80 D3w F6 17 14.0 F5 288 D0 D24 C6 52 8.0 F5 387 80 D3w F6 17 14.0 F5 289 D0 D24 C6 15 D01 F5 388 B0 D3w F6 17 14.0 F5 289 D0 D24 C6 15 D01 F5 388 B0 D3w F6 21 5.0 F5 289 D0 D24 C6 15 D01 F5 389 B0 D3w F6 33 5.0 F5 290 D0 D24 C6 25 2.0 F5 388 B0 D3w F6 21 5.0 F5 390 BU D3w F6 63 3.0 F5 290 D0 D24 C6 18 O01 F5 390 BU D3w F6 63 3.0 F5 290 D0 D24 C6 18 O01 F5 390 BU D3w F6 63 3.0 F5 290 D0 D24 C6 18 O01 F5 390 BU D3w F6 63 3.0 F5 290 D0 D24 C6 18 O01 F5 390 BU D3w F6 63 3.0 F5 290 D0 D24 C6 18 O01 F5 390 BU D3w F6 63 3.0 F5 290 D0 D24 C6 18 O01 F5 390 BU D3w F6 63 3.0 F5 290 D0 D24 C6 18 O01 F5 390 BU D3w F6 63 3.0 F6 14 0.0 F5 390 BU D3w F6 63 3.0 F6 14 0.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 390 BU D3w F6 63 3.0 F6 17 2.0 F5 3								63 333					40.0
F5 277 DQ D24 CG 30 1.0 F5 377 UL 15 CG 77 4.0 F5 278 DV D24 CG 40 1.0 F5 378 DL 15 CG 113 25.0 F5 280 DV D24 CG 44 6.0 F5 380 DL 15 CG 48 3.0 F5 280 DV D24 CG 44 6.0 F5 380 DL 15 CG 39 5.0 F5 280 DV D24 CG 44 6.0 F5 381 DL 15 CG 39 5.0 F5 280 DV D24 CG 44 6.0 F5 382 DL 15 CG 40 76.0 F5 285 DV D24 CG 17 1.0 F5 383 DL 15 CG 40 76.0 F5 285 DV D24 CG 17 1.0 F5 384 DL 15 CG 40 76.0 F5 285 DV D24 CG 17 1.0 F5 385 DL 15 CG 40 76.0 F5 285 DV D24 CG 46 6.0 F5 385 DL 15 CG 40 76.0 F5 285 DV D24 CG 17 1.0 F5 385 DL 15 CG 40 76.0 F5 285 DV D24 CG 17 1.0 F5 385 DL 15 CG 63 22.0 F5 286 DV D24 CG 17 1.0 F5 385 DL 15 CG 63 22.0 F5 286 DV D24 CG 17 1.0 F5 385 DL 15 CG 63 22.0 F5 285 DV D24 CG 46 6.0 F5 386 DL 15 CG 63 22.0 F5 287 DV D24 CG 55 CG 52 6.0 F5 386 BV D3W F6 17 14.0 F5 385 F5 287 DV D24 CG 55 CG 52 6.0 F5 386 BV D3W F6 17 14.0 F5 287 DV D24 CG 55 CG 52 6.0 F5 386 BV D3W F6 17 14.0 F5 287 DV D24 CG 55 CG 52 6.0 F5 386 BV D3W F6 17 14.0 F5 287 DV D24 CG 55 CG 52 6.0 F5 386 BV D3W F6 17 14.0 F5 287 DV D24 CG 55 CG 52 CG 55 C							B.C	FS 376					
F3 278 DU D24 CG 62 O-1 F5 378 DL 15 CG 88 3-0 F5 280 DU D24 CL 47 2-0 F5 380 DL 15 CG 88 3-0 F5 281 DU D24 CL 47 2-0 F5 380 DL 15 CG 88 3-0 F5 282 DU D24 CG 44 6-0 F5 381 DL 15 CG 77 40,0 F5 282 DU D24 CG 44 6-0 F5 382 DL 15 CG 77 40,0 F5 283 DU D24 CG 17 1-0 F5 383 DL 15 CG 14 18-0 F5 285 DU D24 CG 17 1-0 F5 385 DL 15 CG 14 18-0 F5 285 DU D24 CG 17 1-0 F5 385 DL 15 CG 40 76-0 F5 285 DU D24 CG 17 1-0 F5 385 DL 15 CG 63 22,0 F5 285 DU D24 CG 17 1-0 F5 385 DL 15 CG 63 22,0 F5 285 DU D24 CG 17 1-0 F5 385 DL 15 CG 63 22,0 F5 286 DU D24 CG 52 8-0 F5 385 DL 15 CG 81 40,0 F5 287 DU D24 CG 52 8-0 F5 385 DL 15 CG 81 40,0 F5 288 DU D24 CG 52 8-0 F5 385 DL 15 CG 81 40,0 F5 289 DU D24 CG 52 8-0 F5 387 80 03w F6 17 14,0 F5 289 DU D24 CG 15 O-1 F5 388 BD 03w F6 17 14,0 F5 289 DU D24 CG 15 O-1 F5 388 BD 03w F6 21 3-0 F5 290 DQ D24 CG 15 O-1 F5 380 BD 03w F6 21 3-0 F5 290 DQ D24 CG 15 O-1 F5 380 BD 03w F6 21 3-0 F5 290 DQ D24 CG 18 O-1 F5 380 BD 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 380 BD 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 380 BD 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 380 BD 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 380 BD 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ D24 CG 18 O-1 F5 390 BU 03w F6 3-0 F5 290 DQ DQ DQ DQ DQ DQ DQ DQ DQ DQ DQ DQ DQ					CG	28	1.0		ÜL	15	CG	77	4.0
F5 279	FS	278	DQ	D2 4	CG			FS 378	OL	15	ÇĞ	113	25.0
F5 280 DU D24 CL 47	FS	279	ρu	D2.4		9.5							5.0
F5 282 DW D24 CG 20 1.0 F5 382 DL 15 CG 59 5.0 F5 283 DW D24 CG 17 1.0 F5 383 DL 15 CG 14 10.0 F5 285 DW D24 CG 17 1.0 F5 385 DL 15 CG 40 76.0 F5 285 DW D24 CG 17 1.0 F5 385 DL 15 CG 63 22.0 F5 286 DW D24 CG 46 8.0 F5 386 DL 15 CG 63 22.0 F5 287 DW D24 CG 52 4.0 F5 387 80 03w FG 17 14.0 F5 288 DW D24 CG 15 0.1 F5 388 BD 03w FG 17 14.0 F5 288 DW D24 CG 15 0.1 F5 388 BD 03w FG 17 14.0 F5 289 DW D24 CG 25 2.0 F5 386 BD 03w FG 21 3.0 F5 290 DW D24 CG 55 2.0 F5 386 BD 03w FG 21 3.0 F5 291 DW D24 CG 55 2.0 F5 387 BD 03w FG 5.0 F5 291 DW D24 CG 55 5.0 F5 390 BU 03w FG 5.5 F5 292 DW D24 CG 55 5.0 F5 390 BU 03w FG 5.5 F5 292 DW D24 CG 53 8.0 F5 390 BU 03w FG 5.5 F5 292 DW D24 CG 53 8.0 F5 390 BU 03w FG 6.3 5.0 F5 293 DW D24 CG 63 8.0 F5 390 BU 03w FG 6.3 5.0 F5 294 DW D24 CG 63 8.0 F5 390 BU 03w FG 6.3 5.0 F5 295 DW D24 CG 63 8.0 F5 390 BU 03w FG 6.3 5.0 F5 296 DW D24 CG 16 0.1 F5 395 BU 03w FG 6.3 5.0 F5 297 DW D24 CG 29 0.1 F5 395 BU 03w FG 6.3 70.0 F5 298 DW D24 CG 29 0.1 F5 395 BU 03w FG 6.7 2.0 F5 299 DW D34 CG 20 2.0 F5 396 BU 03w FG 6.3 70.0 F5 290 DW D35 CG 20 2.0 F5 398 BD 03w FG 6.3 70.0 F5 290 DW D35 CG 20 2.0 F5 398 BD 03w FG 6.3 20.0 F5 290 DW D35 CG 25 0.4 F5 397 BD 03w FG 6.3 10.0 F5 290 DW D35 CG 26 25 0.4 F5 398 BD 03w FG 6.3 10.0 F5 200 DW D35 CG 26 27 F5 398 BD 03w FG 6.3 10.0 F5 200 DW D35 CG 26 27 F5 398 BD 03w FG 6.3 10.0 F5 300 UL 035 CG 19 0.1 F5 402 BD 03w FG 6.3 10.0 F5 300 UL 035 CG 28 1.0 F5 398 BD 03w FG 6.3 10.0 F5 300 UL 035 CG 19 0.1 F5 402 BD 03w FG 6.3 11.0 F5 300 UL 035 CG 28 1.0 F5 402 BD 03w FG 6.3 11.0 F5 300 UL 035 CG 28 1.0 F5 402 BD 03w FG 6.3 11.0 F5 300 UL 035 CG 28 1.0 F5 402 BD 03w FG 6.3 11.0 F5 300 UL 035 CG 28 1.0 F5 402 BD 03w FG 6.3 11.0 F5 300 UL 035 CG 28 2.0 F5 398 BD 03w FG 6.3 11.0 F5 300 UL 035 CG 28 2.0 F5 398 BD 03w FG 6.3 11.0 F5 300 UL 035 CG 28 2.0 F5 398 BD 03w FG 6.3 11.0 F5 300 UL 035 CG 28 2.0 F5 398 BD 03w FG 6.3 11.0 F5 300 UL 035 CG 28 2.0 F5 398 BD 03w FG 6.3 11.0 F5 300 UL 035 CG 28 2.0 F5 398 BD 03w FG 6.3 11.0 F5 300 UL 035 CG 28 2.0 F5 388 BD 03w F	FS	250											25.0
F5 283 DQ D24 CG 17 1.0 F5 383 DL 15 CG 10 76.0 F5 285 DQ D24 CG 17 1.0 F5 385 DL 15 CG 40 76.0 F5 285 DQ D24 CG 17 1.0 F5 385 DL 15 CG 40 76.0 F5 285 DQ D24 CG 46 8.0 F5 386 DL 15 CG 63 22.0 F5 287 DQ D24 CG 52 8.0 F5 387 80 03w FG 17 14.0 F5 288 DQ 024 CG 15 0.1 F5 385 DL 15 CG 81 40.0 F5 288 DQ 024 CG 15 0.1 F5 385 DL 15 CG 81 40.0 F5 288 DQ 024 CG 15 0.1 F5 388 BQ 03w FG 17 14.0 F5 288 DQ 024 CG 15 0.1 F5 388 BQ 03w FG 17 14.0 F5 289 DQ 024 CG 25 2.0 F5 388 BQ 03w FG 21 5.0 F5 289 DQ 024 CG 25 2.0 F5 389 BQ 03w FG 25 5.0 F5 387 BQ 03w FG 26 25 5.0 F5 387 BQ 03w FG 26 35 5.0 F5 291 DQ 024 CG 43 8.0 F5 391 BQ 03w FG 36 3.0 F5 292 DQ 024 CG 43 8.0 F5 391 BQ 03w FG 63 5.0 F5 292 DQ 024 CG 18 0.1 F5 393 BQ 03w FG 63 5.0 F5 293 DQ 024 CG 18 0.1 F5 393 BQ 03w FG 63 5.0 F5 293 DQ 024 CG 18 0.1 F5 393 BQ 03w FG 63 10.0 F5 295 DQ 024 CG 18 0.1 F5 393 BQ 03w FG 63 10.0 F5 295 DQ 024 CG 18 0.1 F5 393 BQ 03w FG 63 10.0 F5 295 DQ 024 CG 25 0.1 F5 395 BQ 03w FG 63 10.0 F5 295 DQ 024 CG 25 0.1 F5 395 BQ 03w FG 77 2.0 F5 295 DQ 024 CG 25 0.1 F5 395 BQ 03w FG 77 2.0 F5 295 DQ 024 CG 25 0.1 F5 395 BQ 03w FG 77 2.0 F5 295 DQ 025 CG 25 0.1 F5 395 BQ 03w FG 77 2.0 F5 295 DQ 025 CG 25 0.1 F5 395 BQ 03w FG 77 2.0 F5 295 DQ 03w FG													
F5 289 DQ D24 CG 17 1.0 F5 385 DL 15 CG 40 76.0 F5 285 DQ D24 CG 17 1.0 F5 385 DL 15 CG 63 22.0 F5 286 DD D24 CG 46 6.0 F5 385 DL 15 CG 63 22.0 F5 288 DQ D24 CG 52 6.0 F5 385 DL 15 CG 63 22.0 F5 288 DQ D24 CG 52 6.0 F5 387 80 03w F6 17 14.0 F5 288 DQ D24 CG 15 0.1 F5 388 80 03w F6 17 14.0 F5 289 DQ D24 CG 25 2.0 F5 388 80 03w F6 21 5.0 F5 289 DQ D24 CG 55 5.0 F5 380 80 03w F6 45 4.0 F5 289 DQ D24 CG 55 5.0 F5 380 80 03w F6 50 55 5.0 F5 290 DQ D24 CG 55 5.0 F5 380 80 03w F6 65 5.0 F5 290 DQ D24 CG 643 80 F5 390 80 03w F6 63 5.0 F5 290 DQ D24 CG 643 80 F5 390 80 03w F6 63 5.0 F5 290 DQ D24 CG 643 80 F5 390 80 03w F6 63 5.0 F5 290 DQ D24 CG 643 80 F5 390 80 03w F6 63 5.0 F5 290 DQ D24 CG 18 0.1 F5 390 80 03w F6 63 5.0 F5 290 DQ D24 CG 18 0.1 F5 390 80 03w F6 63 10.0 F5 290 DQ D24 CG 18 0.1 F5 390 80 03w F6 63 10.0 F5 290 DQ D24 CG 29 0.1 F5 390 80 03w F6 63 10.0 F5 290 DQ D24 CG 30 1.0 F5 390 80 03w F6 63 10.0 F5 290 DQ D24 CG 30 1.0 F5 390 80 03w F6 63 10.0 F5 290 DQ D24 CG 30 1.0 F5 390 80 03w F6 63 10.0 F5 290 DQ D24 CG 30 1.0 F5 390 80 03w F6 63 10.0 F5 290 DQ D24 CG 30 1.0 F5 390 80 03w F6 63 10.0 F5 290 DQ D24 CG 30 1.0 F5 390 80 03w F6 63 10.0 F5 290 DQ D24 CG 30 1.0 F5 390 80 03w F6 63 10.0 F5 290 DQ D34 F6 63 20.0 F5 390 80 03w F6 63 10.0 F5 290 DQ D34 F6 63 20.0 F5 390 80 03w F6 63 10.0 F5 290 DQ D34 F6 63 20.0 F5 390 80 03w F6 63 20.0 F5 390											- CG		
F5 285 DQ D24 CG 46 &0.0 F5 385 DL 15 CG 63 22.0 F5 288 DD D24 CG 52 &0.0 F5 386 DL 15 CG 81 40.0 F5 288 DD D24 CG 52 &0.0 F5 387 80 03w F6 17 14.0 F5 288 DD D24 CG 15 C0.0 F5 387 80 03w F6 17 14.0 F5 288 DD D24 CG 15 C0.0 F5 388 8D 03w F6 21 5.0 F5 289 DW D24 CG 25 2.0 F5 388 8D 03w F6 21 5.0 F5 290 DD D24 CG 58 50 F5 390 8D 03w F6 50 50 F5 291 DD D24 CG 58 50 F5 391 8D 03w F6 50 50 F5 292 DD D24 CG 63 80.0 F5 391 8D 03w F6 50 50 F5 292 DD D24 CG 18 00.1 F5 392 8D 03w F6 63 5.0 F5 293 DD D24 CG 18 00.1 F5 392 8D 03w F6 27 4.0 F5 293 DD D24 CG 18 00.1 F5 393 8D 03w F6 27 4.0 F5 293 DD D24 CG 18 00.1 F5 393 8D 03w F6 67 7 2.0 F5 295 DD D24 CG 18 00.1 F5 395 8D 03w F6 67 7 2.0 F5 295 DD 024 CG 20 0.1 F5 395 8D 03w F6 77 2.0 F5 295 DD 024 CG 20 2.0 F5 395 8D 03w F6 77 2.0 F5 295 DD 038 F6 7					Cr.	17					23		
F5 286 DD D24 CG 52 4.0 F5 386 DL 15 CG 81 40.0 F5 287 DU D24 CG 52 4.0 F5 387 BD O3W FG 17 14.0 F5 288 DW D24 CG 25 2.0 F5 388 BD O3W FG 21 3.0 F5 289 DW D24 CG 25 2.0 F5 388 BD O3W FG 21 3.0 F5 289 DW D24 CG 58 5.0 F5 389 BD O3W FG 5.6 5.0 F5 291 DW D24 CG 6 83 8.0 F5 390 BW O3W FG 5.6 5.0 F5 292 DD D24 CG 6 22 1.0 F5 392 BD O3W FG 6.3 5.0 F5 292 DD D24 CG 18 0.0 F5 391 BD O3W FG 6.3 5.0 F5 292 DD D24 CG 18 0.1 F5 392 BD O3W FG 6.3 5.0 F5 292 DD D24 CG 18 0.1 F5 392 BD O3W FG 6.3 5.0 F5 293 DD D24 CG 18 0.1 F5 393 BD O3W FG 6.3 10.0 F5 295 DW D24 CG 18 0.1 F5 395 BD O3W FG 6.3 10.0 F5 295 DW D24 CG 29 0.1 F5 395 BD O3W FG 6.3 10.0 F5 295 DW D24 CG 30 1.0 F5 395 BD O3W FG 6.3 20.0 F5 295 DW D24 CG 30 1.0 F5 395 BD O3W FG 6.3 20.0 F5 297 DL O3E CG 25 0.1 F5 395 BD O3W FG 6.3 20.0 F5 297 DL O3E CG 25 0.1 F5 395 BD O3W FG 6.3 20.0 F5 299 DL O3E CG 25 0.1 F5 395 BD O3W FG 6.3 20.0 F5 299 DL O3E CG 25 0.1 F5 397 BD O3W FG 6.3 20.0 F5 299 DL O3E CG 25 0.1 F5 397 BD O3W FG 6.3 20.0 F5 299 DL O3E CG 25 0.1 F5 397 BD O3W FG 6.3 20.0 F5 299 DL O3E CG 25 0.1 F5 397 BD O3W FG 6.3 20.0 F5 299 DL O3E CG 25 0.1 F5 397 BD O3W FG 6.3 20.0 F5 299 DL O3E CG 25 0.1 F5 397 BD O3W FG 6.3 20.0 F5 299 DL O3E CG 25 0.1 F5 397 BD O3W FG 6.3 20.0					ČĞ	17	1.0	FS 385					
#5 288 DU 024 CG 15 0-1 F5 388 80 03W FG 17 14.0  #5 288 DU 024 CG 15 0-1 F5 388 80 03W FG 21 5.0  #5 289 DU 024 CG 25 2.0 F5 388 80 03W FG 21 5.0  #5 290 DQ 024 CG 58 5.0 F5 390 80 03W FG 55 5.0  #5 291 DU 024 CG 58 3.0 F5 390 80 03W FG 55 5.0  #5 292 DQ 024 CG 43 8.0 F5 391 80 03W FG 63 5.0  #5 292 DQ 024 CG 22 1.0 F5 392 80 03W FG 63 5.0  #5 293 DQ 024 CG 16 0-1 F5 393 80 03W FG 63 10.0  #5 294 DQ 024 CG 29 0-1 F5 393 80 03W FG 63 10.0  #5 295 DU 024 CG 30 1.0 F5 395 80 03W FG 63 10.0  #5 296 DL 03E CG 20 2.0 F5 395 80 03W FG 77 2.0  #5 297 DL 03E CG 20 2.0 F5 395 80 03W FG 77 2.0  #5 298 DL 03E CG 20 2.0 F5 395 80 03W FG 77 2.0  #5 299 DL 03E CG 25 0.1 F5 397 80 03W FG 77 2.0  #5 299 DL 03E CG 25 0.1 F5 397 80 03W FG 77 2.0  #5 299 DL 03E CG 25 0.1 F5 399 8D 03W FG 53 16.0  #5 300 DL 03E CG 26 2.0 F5 398 8D 03W FG 53 16.0  #5 300 UL 03E CG 19 0-1 F5 402 8D 03W FG 53 16.0  #5 300 UL 03E CG 28 1.0 F5 397 8D 03W FG 53 16.0  #5 300 UL 03E CG 28 1.0 F5 399 8D 03W FG 53 16.0  #5 300 UL 03E CG 28 1.0 F5 399 8D 03W FG 53 16.0  #5 300 UL 03E CG 28 1.0 F5 399 8D 03W FG 53 16.0  #5 300 UL 03E CG 28 1.0 F5 402 8D 03W FG 53 16.0  #5 300 UL 03E CG 28 1.0 F5 402 8D 03W FG 53 16.0  #5 300 UL 03E CG 28 1.0 F5 402 8D 03W FG 53 16.0  #5 300 UL 03E CG 28 1.0 F5 402 8D 03W FG 53 16.0  #5 300 UL 03E CG 28 1.0 F5 402 8D 03W FG 53 16.0  #5 300 UL 03E CG 28 1.0 F5 402 8D 03W FG 53 13.0  #5 300 UL 03E CG 28 1.0 F5 402 8D 03W FG 53 13.0					CG	46		F\$ 386		15	CG	51	40.0
F5 288 DU 024 CC 25 2.0 F5 388 B0 03w F6 21 5.0 F5 289 DU 024 CC 25 2.0 F5 389 B0 03w F6 36 5.0 F5 290 D0 024 CG 56 5.0 F5 391 BU 03w F6 5.6 5.6 F5 291 DU 024 CG 6 3 8.0 F5 391 BU 03w F6 6.3 5.0 F5 292 D0 024 CG 18 0.1 F5 392 BU 03w F6 6.3 5.0 F5 293 D0 024 CG 18 0.1 F5 393 BU 03w F6 6.3 5.0 F5 293 D0 024 CG 18 0.1 F5 393 BU 03w F6 6.7 4.0 F5 293 D0 024 CG 18 0.1 F5 393 BU 03w F6 6.7 2.0 F5 295 D0 024 CG 18 0.1 F5 393 BU 03w F6 77 2.0 F5 295 D0 024 CG 29 0.1 F5 395 BU 03w F6 77 2.0 F5 295 D0 024 CG 29 0.1 F5 395 BU 03w F6 77 2.0 F5 295 D0 024 CG 20 2.0 F5 395 BU 03w F6 77 2.0 F5 295 D0 024 CG 25 0.1 F5 395 BU 03w F6 77 2.0 F5 295 DU 03E CG 25 0.1 F5 395 BU 03w F6 77 2.0 F5 295 DU 03E CG 25 0.1 F5 395 BU 03w F6 77 2.0 F5 295 DU 03E CG 25 0.1 F5 395 BU 03w F6 73 20.0 F5 297 DU 03E CG 25 0.1 F5 395 BD 03w F6 37 20.0 F5 299 DU 03E CG 25 0.1 F5 395 BD 03w F6 37 20.0 F5 299 DU 03E CG 25 0.1 F5 395 BD 03w F6 37 20.0 F5 299 DU 03E CG 25 0.1 F5 395 BD 03w F6 31 20.0 F5 300 DU 03E CG 25 0.1 F5 395 BD 03w F6 31 20.0 F5 300 DU 03E CG 25 0.1 F5 400 BD 03w F6 33 16.0 F5 300 UL 03E CG 38 1.0 F5 400 BD 03w F6 33 12.0 F5 300 UL 03E CG 28 1.0 F5 400 BD 03w F6 34 3.0 F5 300 UL 03E CG 28 1.0 F5 400 BD 03w F6 34 3.0 F5 300 UL 03E CG 28 1.0 F5 400 BD 03w F6 34 3.0 F5 300 DU 03E CG 28 2.0 F5 300 BD 03w F6 34 3.0 F5 300 DU 03E CG 28 2.0 F5 300 BD 03w F6 34 3.0 F5 300 DU 03E CG 28 2.0 F5 300 BD 03w F6 34 3.0 F5 300 DU 03E CG 28 2.0 F5 300 BD 03w F6 34 3.0 F5 300 DU 03E CG 28 2.0 F5 300 BD 03w F6 34 3.0 F5 300 DU 03E CG 28 2.0 F5 300 BD 03w F6 34 3.0 F5 300 DU 03E CG 28 2.0 F5 300 BD 03w F6 34 3.0 F5 300 DU 03E CG 28 2.0 F5 300 BD 03w F6 34 3.0 F5 300 DU 03E CG 28 2.0 F5 300 BD 03w F6 34 3.0 F5 300 DU 03E CG 28 2.0 F5 300 BD 03w F6 34 3.0 F5 300 DU 03E CG 28 2.0 F5 300 BD 03w F6 34 3.0 F5 300 DU 03E CG 28 2.0 F5 300 BD 03w F6 34 3.0 F5 300 DU 03E CG 28 2.0 F5 300 BD 03w F6 34 3.0 F5 300 DU 03E CG 28 2.0 F5 300 DU 03W F			04	D2 4	CG			FS 387	80	03 w	FG	17	14.0
F5 289 DU D24 CG 55 5.0 F5 389 BO 034 F6 45 4.0 F5 290 DQ D24 CG 43 8.0 F5 390 BU 034 F6 55 5.0 F5 291 DQ D24 CG 43 8.0 F5 391 BU 034 F6 63 5.0 F5 292 DQ D24 CG 16 0.1 F5 392 BU 034 F6 63 5.0 F5 293 DQ D24 CG 16 0.1 F5 392 BU 034 F6 63 10.0 F5 294 DQ D24 CG 29 0.1 F5 394 BU 034 F6 63 10.0 F5 295 DQ D24 CG 29 0.1 F5 394 BU 034 F6 63 10.0 F5 295 DQ D24 CG 30 1.0 F5 395 BU 034 F6 63 10.0 F5 295 DQ D24 CG 30 1.0 F5 395 BU 034 F6 77 2.0 F5 296 DL 035 C6 25 0.1 F5 396 BU 034 F6 77 2.0 F5 297 DL 035 C6 25 0.1 F5 396 BU 034 F6 77 20.0 F5 298 DL 035 C6 25 0.1 F5 396 BU 034 F6 77 20.0 F5 298 DL 035 C6 25 0.1 F5 396 BU 034 F6 77 20.0 F5 298 DL 035 C6 25 0.1 F5 397 BU 034 F6 77 20.0 F5 300 DL 035 C6 25 0.1 F5 397 BU 034 F6 53 20.0 F5 301 DL 035 C6 26 2.0 F5 398 BU 034 F6 54 2000.0 F5 301 DL 035 C6 40 2.0 F5 398 BU 034 F6 53 16.0 F5 302 DL 035 C6 28 1.0 F5 402 BU 034 F6 34 12.0 F5 305 DL 035 C6 28 1.0 F5 402 BU 034 F6 34 12.0 F5 305 DL 035 C6 28 1.0 F5 402 BU 034 F6 34 1.0 F5 305 DL 035 C6 28 1.0 F5 402 BU 034 F6 34 1.0 F5 305 DL 035 C6 28 1.0 F5 402 BU 034 F6 77 258.0	FS	288	De	450	ÇG			F5 388		034	F G	21	5.0
F5 291 DU D24 CG A3 8-0 F5 391 80 03w FG 63 3-0 F5 292 DD D24 CG 22 1.0 F5 392 80 03w FG 63 3-0 F5 293 DD D24 CG 18 0.1 F5 393 80 03w FG 44 4.0 F5 293 DD D24 CG 18 0.1 F5 393 80 03w FG 44 4.0 F5 294 DD D24 CG 30 1.0 F5 395 80 03w FG 83 10.0 F5 295 DU D24 CG 30 1.0 F5 395 80 03w FG 83 10.0 F5 295 DU D24 CG 30 1.0 F5 395 80 03w FG 77 2.0 F5 296 DL 03E CG 20 2.0 F5 396 80 03w FG 67 72 2.0 F5 296 DL 03E CG 25 0.1 F5 397 80 03w FG 63 20.0 F5 298 DL 03E CG 25 0.1 F5 397 80 03w FG 63 20.0 F5 298 DL 03E CG 25 0.1 F5 397 80 03w FG 63 20.0 F5 298 DL 03E CG 25 0.1 F5 397 80 03w FG 63 20.0 F5 298 DL 03E CG 25 0.1 F5 397 80 03w FG 63 20.0 F5 298 DL 03E CG 25 0.1 F5 397 80 03w FG 63 20.0 F5 298 DL 03E CG 25 0.1 F5 397 80 03w FG 63 20.0 F5 298 DL 03E CG 25 0.1 F5 398 8D 03w FG 51 20.0 F5 200 DL 03E CG 40 2.0 F5 398 8D 03w FG 51 20.0 F5 300 DL 03E CG 18 70 0.1 F5 400 8D 03w FG 139 258.0 F5 300 DL 03E CG 28 1.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 1.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 1.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 1.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 1.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 300 DL 03E CG 28 2.0 F5 400 8D 03w FG 49 4.0 F5 400 BD 03w FG 49 4.0 F5 400 BD 03w FG 49 4.0 F5 400 BD	FS			D24				F3 389					4.0
F5 292 DD D24 CG 14 0-1 F5 392 ED D3W FG 27 4-0 65 293 DD D24 CG 14 0-1 F5 393 BD D3W FG 44 4-0 65 294 DD D24 CG 29 D-1 F5 395 BD D3W FG 68 10-0 F5 295 DD D24 CG 30 1-0 F5 395 BD D3W FG 77 2-0 F5 295 DD D25 CG 20 2-0 F5 395 BD D3W FG 77 2-0 F5 297 DL D3E CG 20 2-0 F5 395 BD D3W FG 77 2-0 F5 297 DL D3E CG 25 0-1 F5 395 BD D3W FG 77 2-0 F5 298 DD D3E CG 25 0-1 F5 397 BD D3W FG 77 2-0 F5 298 DD D3E CG 25 2-0 F5 398 BD D3W FG 54 2000-0 F5 299 DL D3E CG 25 2-0 F5 398 BD D3W FG 55 35 16-0 F5 300 DL D3E CG 19 0-1 F5 300 BD D3W FG 53 16-0 F5 300 DL D3E CG 19 0-1 F5 400 BD D3W FG 53 16-0 F5 300 DL D3E CG 19 0-1 F5 400 BD D3W FG 53 12-0 F5 300 DL D3E CG 28 1-0 F5 401 BD D3W FG 58 12-0 F5 300 DL D3E CG 28 1-0 F5 402 BD D3W FG 58 12-0 F5 300 DL D3E CG 28 2-0 F5 403 BU D3W FG 58 12-0 F5 300 DL D3E CG 28 2-0 F5 403 BU D3W FG 58 12-0 F5 300 DL D3E CG 28 2-0 F5 403 BU D3W FG 59 49 4-0 F5 300 DL D3E CG 28 2-0 F5 403 BU D3W FG 79 4-0 F5 300 DL D3E CG 28 2-0 F5 403 BU D3W FG 79 4-0 F5 300 DL D3E CG 28 2-0 F5 403 BU D3W FG 79 4-0 F5 300 DL D3E CG 28 2-0 F5 404 BU D3W FG 79 15-0 F5 405 BU D3W FG 79 1					CG								
\$\begin{array}{cccccccccccccccccccccccccccccccccccc					- C6			F3 JV1					
F5 294	7.5				ČĚ								4.0
F5 295 DU 034 CG 30 1.0 F5 395 dU 03w FG 77 2.0 F5 295 296 DL 03E CG 20 2.0 F5 396 BD 03w FG A3 20.0 F5 297 DL 03E CG 25 0.1 F5 397 BD 03w FG A3 20.0 F5 298 DL 03E CG 25 0.1 F5 397 BD 03w FG 37 20.0 F5 298 DL 03E CG 25 2.0 F5 398 BD 03w FG 37 20.0 F5 398 BD 03w FG 31 2000.0 F5 300 DL 03E CG 19 0.1 F5 400 BD 03w FG 139 258.0 F5 301 DL 03E CG 19 0.1 F5 400 BD 03w FG 139 258.0 F5 302 UL 03E CG 28 1.0 F5 402 BD 03w FG 38 12.0 F5 305 DL 03E CG 28 2.0 F5 404 BU 03w FG 34 3.0					ČĠ								
F5 296 DL 03E CG 20 2.0 F5 396 8D 03w FG A3 20.0 F5 297 DL 03E CG 25 0.1 F5 397 BD 03w FG A3 20.0 F5 297 DL 03E CG 25 2.0 F5 398 BD 03w FG 54 2000.0 F5 299 DL 03E CG 26 2.0 F5 398 BD 03w FG 54 2000.0 F5 200 DL 03E CG 19 0.1 F5 390 BD 03w FG 53 16.0 F5 300 DL 03E CG 19 0.1 F5 400 BD 03w FG 139 258.0 F5 301 DL 03E CG 28 1.0 F5 401 BD 03w FG 58 12.0 F5 302 UL 03E CG 28 1.0 F5 402 BD 03w FG 49 4.0 F5 305 DL 03E CG 28 2.0 F5 403 BU 03w FG 34 3.0 F5 305 DL 03E CG 28 2.0 F5 403 BU 03w FG 34 3.0					ÇG	30	1.0						
F5 297 DL 03E C6 25 0.1 F5 397 BD 03W F6 37 20.0 F5 298 BD 03W F6 37 20.0 C0 F5 298 BD 03W F6 35 200 C0 F5 398 BD 03W F6 54 200 C0 F5 300 BD 03W F6 53 16.0 F5 300 DL 03E C6 19 0.1 F5 400 BD 03W F6 139 258.0 F5 301 DL 03E C6 38 4.0 F5 401 BD 03W F6 38 12.0 F5 302 UL 03E C6 28 1.0 F5 402 BD 03W F6 49 4.0 F5 305 DL 03E C6 28 2.0 F5 403 BU 03W F6 49 4.0 F5 305 DL 03E C6 28 2.0 F5 403 BU 03W F6 34 3.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 305 DL 03E C6 28 2.0 F5 404 BU 03W F6 37 258.0 C0 F5 405					CG	20				03w	FG	63	
F5 208 DL 03E CG 26 2-0 F5 398 BD 03w FG 54 2000.05 F5 209 DL 03E CG 10 0-1 F5 300 BD 03w FG 53 16-0 F5 301 DL 03E CG 10 0-1 F5 400 BD 03w FG 130 258.0 F5 301 DL 03E CG 28 4.0 F5 401 BD 03w FG 130 258.0 F5 302 UL 03E CG 28 1.0 F5 402 BD 03w FG 49 4.0 F5 305 DL 03E CG 28 2-0 F5 404 BU 03w FG 34 3.0				03£	CG			FS 397	50	03w		37	20.0
F5 299 DL 03E CG 40 C-0 F5 399 BD 03W FG 53 16-0 F5 300 DL 03E CG 19 0-1 F5 400 BD 03W FG 139 258-0 F5 301 DL 03E CG 28 1-0 F5 402 BD 03W FG 58 12-0 F5 302 UL 03E CG 28 1-0 F5 402 BD 03W FG 49 4-0 F5 305 DL 03E CG 20 0-1 F5 402 BU 03W FG 34 3-0 F5 305 DL 03E CG 28 2-0 F5 403 BU 03W FG 34 3-0 F5 305 DL 03E CG 28 2-0 F5 404 BU 031 CG 71 15-0	47	298			<u> </u>								
FS 301 UL 03E CC 38 4.0 FS 401 80 03W FG 58 12.0 FS 302 UL 03E CG 28 1.0 FS 402 80 03W FG 49 4.0 FS 304 UL 03E CG 20 0.1 FS 403 8U 03W FG 34 3.0 FS 305 UL 03E CG 20 0.1 FS 403 8U 03W FG 34 3.0	FS							F5 340		0311			
F5 302 UL 03E C6 28 1.0 F5 402 80 03w F6 49 4.0 F5 304 DL 03E C6 20 0.1 F5 403 8U 03w F6 34 3.0 F5 305 DL 03E C6 28 2.0 F5 404 8U 031 C6 F1 15.6										DAM			
F5 304 DL 03E CG 20 0.1 F5 403 BU 03W FG 34 3.0 F5 305 DL 03E CG 28 2.0 F5 404 BU 021 CG 71 15.6													12.0
F5 305 DL 03E CG 28 2-U F5 404 BU D11 CG 71 15-0													
						28	2.0	F5 404					15.6
							5 .0	FS 405					6.0

St.   St.	M	u	AREA	LINE	ROCK	ŽH	A.S.	МП	AREA	LINE	RUCA	ŽH	AS
15   16   16   16   16   17   18   18   18   18   18   18   18		404		011	T.G.	40	5.0	33.540	PA	100	CG.	30	1.0
F.   107		407		011	CG	53	12.0	55 521	PA	D0 7			1.6
15													4.0
15   11   10   10   11   12   13   14   15   15   15   15   15   15   15													3.0
25   112   100													3.0 4.0
## 15	FS			D11	ÇG	34	0.1	55 526	PA	007			0.1
Fig.   15													1 +0
Fig.   14													3.0
Fig. 417							0.1						0.1 0.1
25   48	FS	417		011	ÇG	33	0.1	22 233	PA	007	CG	100	35.0
F5   420   800   001   CC							4.0						5.0
## ## ## ## ## ## ## ## ## ## ## ## ##													10.0 6.0
## ## ## ## ## ## ## ## ## ## ## ## ##								55 535	PA				4.0
15	FS	422	90	011				35 536		007	CG		J.0
15   425   80				011				55 537					0-1
\$\frac{1}{2}\$\$ 42\frac{1}{2}\$\$ 80\$  \text{Dil}\$\$  \text{Col}\$\$ 22.0  \text{Sis}\$  \text{Dil}\$\$  \text{Col}\$\$ 32.0  \text{Sis}\$  \text{Dil}\$\$  \text{Col}\$\$ 32.0  \text{Sis}\$  \text{Dil}\$\$  \text{Dil}\$\$  \text{Col}\$\$ 32.0  \text{Sis}\$  \text{Dil}\$\$  \text{Dil}\$\$  \text{Col}\$\$  \text{Dil}\$\$  \text{Dil}\$\$  \text{Dil}\$\$  \text{Dil}\$\$  \text{Dil}\$\$  \text{Dil}\$\$  \text{Dil}\$\$  \text{Dil}\$\$  \text{Dil}\$\$\$  \text{Dil}\$\$\$  \text{Dil}\$\$\$  \text{Dil}\$\$\$\$\$  \text{Dil}\$													0.1 0.1
\$\frac{5}{5} & \frac{28}{8} & \frac{60}{80} & \frac{11}{1} & \frac{6}{6} & \frac{3}{4} & \frac{3}{1} & \frac{1}{6} & \frac{1}{2} & \frac{1}{6}							32.0						0.1
F5   430   80													0.1
## ## ## ## ## ## ## ## ## ## ## ## ##													0.1
15   13    80													0.1 1.6
\$5 432 80 D11 CG 38 2.0 S5 500 PA D07 CG 40							2.D		PA				6.1
\$\frac{\cappa}{\cappa}\$ \text{ais} & \text{u0} & \text{01} & \text{Co} & \text{10} & \text{01} & \text{Co} & \text{10} & \text{10} & \text{02} & \text{10} & \text{02} & \text{10} & \text{02} & \text{02} & \text{02} & \text{02} & \text{02} & \text{02} & \text{03} & \text{03} & \text{03} & \text{02} & \text{03} & \text	F۵	432	90	D11				\$5.546		DG 7	CG	40	0.1
## ## ## ## ## ## ## ## ## ## ## ## ##							46.0						5.0
\$\frac{\cappa}{\cappa}\$ \text{aligned}\$							1.0						1.6 0.1
## ## ## ## ## ## ## ## ## ## ## ## ##				04 w	Fu	32	7.0		24				1.0
15   140   100   104   160   151   152   153   153   154   154   160   160   151   152   153   153   154   154   160   160   154	£5	437	90	04 W	FG			35 558		007	CG	79	1.0
## ## ## ## ## ## ## ## ## ## ## ## ##									PA				0.1
F5 441 80									PA				0.1 0.1
## ## ## ## ## ## ## ## ## ## ## ## ##	FS	441	BU	D4 W	FG	4.7	2.0	55 555	PA	D0 7	CG	44	1.0
## ## ## ## ## ## ## ## ## ## ## ## ##		442	øÜ					\$5 556		007	CG.	38	0.1
F5 449 80 014 CG 35 45.0 S5 590 PA 007 CG 25 F5 449 80 014 CG 55 45.0 S5 590 PA 007 CG 36 F5 447 80 014 CG 38 149.0 S5 590 PA 007 CG 40 PS 448 80 014 CG 114 1.0 S5 591 PA 007 CG 40 PS 448 80 014 CG 114 1.0 S5 591 PA 007 CG 40 PS 449 80 014 CG 114 1.0 S5 591 PA 007 CG 31 PS 449 80 014 CG 114 1.0 S5 591 PA 007 CG 31 PS 449 80 014 CG 114 1.0 S5 591 PA 007 CG 31 PS 449 80 014 CG 114 1.0 S5 591 PA 007 CG 31 PS 449 80 014 CG 114 1.0 S5 591 PA 007 CG 31 PS 449 80 014 CG 114 1.0 S5 591 PA 007 CG 31 PS 449 80 014 CG 31 PS 449 80	-5												1.0 1.0
F5 446 80 D14 C6 35 45.0 35 560 PA D07 C6 41 F5 447 80 D14 C6 35 140.0 35 561 PA D07 C6 41 F5 448 80 U14 C6 13 1 1.1 35 562 PA D07 C6 40							48.0						1.0
#5 4448 80							45.0	\$\$ 560				36	0.1
\$\frac{6}{2}\$ 449\$ \$\frac{6}{80}\$ \$\frac{0}{14}\$ \$\frac{1}{16}\$ \$\													0.1
\$\frac{c}{c}\$ 450									PA				0.1 1.0
\$\frac{F}{F}\$ 452 \$80 \$014 \$Cu \$71 \$160.6\$ \$35 \$565 \$PA \$007 \$Cu \$41 \$15 \$453 \$80 \$014 \$Cu \$93 \$166.4\$ \$33 \$366 \$PA \$007 \$Cu \$42 \$15 \$453 \$80 \$014 \$Cu \$93 \$166.4\$ \$33 \$366 \$PA \$007 \$Cu \$42 \$16 \$453 \$80 \$014 \$Cu \$39 \$166.4\$ \$35 \$366 \$PA \$007 \$Cu \$42 \$16 \$45 \$16 \$16 \$16 \$16 \$16 \$16 \$16 \$16 \$16 \$16	65					59	160.0		PÃ				0.1
F3	F 5										CG	41	0.1
F5 456 80 U14 C6 39 5.0 S5 588 PA D07 C6 21 F5 457 80 U17 C6 23 F5 588 U1 U14 C6 32 6.0 S5 570 PA D07 C6 34 F5 458 80 U14 C6 32 6.0 S5 571 PA D07 C6 33 F5 458 80 U14 C6 22 5 6.0 S5 571 PA D07 C6 33 F5 458 80 U14 C6 22 5 6.0 S5 571 PA D07 C6 33 F5 458 80 U14 C6 22 5 6.0 S5 572 PA D07 C6 33 F5 458 80 U14 C6 23 3.0 S5 572 PA D07 C6 33 F5 458 80 U14 C6 23 3.0 S5 573 PA D07 C6 33 F5 458 80 U14 C6 23 3.0 S5 575 PA D07 C6 35 F5 460 80 U14 C6 18 4.0 S5 576 PA D07 C6 36 F5 460 80 U14 C6 18 4.0 S5 576 PA D07 C6 36 F5 460 80 U14 C6 18 4.0 S5 576 PA D07 C6 36 F5 460 80 U14 C6 18 4.0 S5 576 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 36 F5 460 80 U14 C6 31 5.0 S5 577 PA D07 C6 35 F5 460 PA D07 C6 31 5.0 S5 58 F5 PA D07 C6 35 F5 F5 460 PA D07 C6 31 5.0 S5 58 F5 PA D07 C6 35 F5 F5 460 PA D07 C6 31 5.0 S5 58 F5 PA D07													1.0
F5   455   80													D-1 D-1
FS 485C #U D14 CG 32 8.0 53 971 PA D07 CG 43 FS 487 80 D14 CG 25 6.0 53 972 PA D07 CG 43 FS 487 80 D14 CG 25 6.0 53 973 PA D07 CG 39 FS 488 80 D14 CG 13 1.0 53 576 PA D07 CG 39 FS 489 80 D14 CG 15 1.0 53 576 PA D07 CG 39 FS 489 80 D14 CG 16 4.0 53 576 PA D07 CG 36 FS 489 80 D14 CG 16 4.0 53 576 PA D07 CG 36 FS 480 80 D14 CG 16 4.0 53 576 PA D07 CG 36 FS 481 80 D14 CG 16 4.0 53 576 PA D07 CG 36 FS 481 80 D14 CG 16 4.0 53 576 PA D07 CG 36 FS 481 80 D14 CG 16 CG 17 CG 18 FS 482 80 D14 CG 18				410	Cu	39	1.6		PA				3.0
F3 457 80 014 CG 35 75.0 S5 772 MA 007 CG 43 F5 458 80 014 CG 13 1.0 S5 772 MA 007 CG 37 F5 458 80 014 CG 13 1.0 S5 772 MA 007 CG 37 F5 458 80 014 CG 13 1.0 S5 772 MA 007 CG 37 F5 450 80 014 CG 16 4.0 S5 772 MA 007 CG 36 F5 460 80 014 CG 31 5.0 S5 772 MA 007 CG 36 F5 461 80 014 CG 31 5.0 S5 772 MA 007 CG 36 F5 462 80 014 CG 31 5.0 S5 772 MA 007 CG 36 F5 463 80 014 CG 32 3.0 S5 772 MA 007 CG 36 F5 464 80 014 CG 33 5.0 S5 772 MA 007 CG 46 F5 465 80 014 CG 33 5.0 S5 772 MA 007 CG 46 F5 466 0A 043 GR 47 5.0 S5 972 MA 007 CG 35 F5 468 0A 043 GR 771 10.0 S5 972 MA 007 CC 18 F5 468 0A 0A 043 GR 771 10.0 S5 972 MA 007 CG 46 F5 470 0A 043 GR 770 5.0 S5 978 MA 007 CG 46 F5 471 0A 043 GR 770 5.0 S5 978 MA 007 CG 47 F5 472 0A 043 GR 770 5.0 S5 978 MA 007 CG 47 F5 473 0A 043 GR 770 5.0 S5 978 MA 007 CG 47 F5 474 0A 043 GR 770 5.0 S5 978 MA 007 CG 47 F5 477 0A 044 GR 377 8.0 S5 978 MA 007 CG 37 F5 478 0A 043 GR 770 5.0 S5 978 MA 007 CG 37 F5 478 0A 043 GR 377 8.0 S5 978 MA 007 CG 37 F5 478 0A 043 GR 371 10.0 S5 978 MA 007 CG 37 F5 478 0A 043 GR 372 S.0 S5 978 MA 007 CG 37 F5 478 0A 043 GR 372 S.0 S5 978 MA 007 CG 37 F5 478 0A 043 GR 372 S.0 S5 978 MA 007 CG 37 F5 478 0A 043 GR 372 S.0 S5 978 MA 007 CG 37 F5 478 0A 043 GR 372 S.0 S5 978 MA 007 CG 37 F5 478 0A 044 GR 372 S.0 S5 979 MA 007 CG 37 F5 478 0A 044 GR 372 S.0 S5 979 MA 007 CG 37 F5 478 0A 044 GR 372 S.0 S5 979 MA 007 CG 37 F5 478 0A 044 GR 372 S.0 S5 979 MA 007 CG 37 F5 478 0A 044 GR 372 S.0 S5 979 MA 007 CG 37 F5 480 0A 044 GR 372 S.0 S5 979 MA 007 CG 37 F5 480 0A 044 GR 372 S.0 S5 979 MA 007 CG 37 F5 480 0A 044 GR 372 S.0 S5 979 MA 007 CG 37 F5 478 0A 044 GR 372 S.0 S5 979 MA 007 CG 37 F5 478 0A 044 GR 372 S.0 S5 979 MA 007 CG 37 F5 480 0A 044 GR 372 S.0 S5 979 MA 007 CG 37 F5 480 0A 044 GR 372 S.0 S5 979 MA 007 CG 37 F5 480 0A 044 GR 372 S.0 S5 979 MA 007 CG 37 F5 480 0A 044 GR 372 S.0 S5 979 MA 007 CG 37 F5 480 0A 047 CG 37 F5 55 509 MA 007 CG 39 S.0 S5 500 MA 007 CG 37 F5 55 509 MA 007 CG 37 F5 55 509 M													0-1
F3 487 80 014 C6 25 6.0 55 573 PA 007 C6 39 F5 489 80 014 C6 13 1.0 55 575 PA 007 C6 35 F5 489 80 014 C6 13 1.0 55 575 PA 007 C6 36 F5 480 80 014 C6 15 4.0 55 575 PA 007 C6 36 F5 481 80 014 C6 15 4.0 55 577 PA 007 C6 36 F5 481 80 014 C6 15 4.0 55 577 PA 007 C6 49 F5 483 80 014 C6 24 3.0 55 577 PA 007 C6 49 F5 483 80 014 C6 24 3.0 55 577 PA 007 C6 49 F5 483 80 014 C6 18 6.0 55 577 PA 007 C6 45 F5 484 80 014 C6 18 6.0 55 577 PA 007 C6 51 F5 486 80 014 C6 18 6.0 55 577 PA 007 C6 55 F5 484 80 014 C6 18 6.0 55 577 PA 007 C6 55 F5 484 80 014 C6 18 6.0 55 581 PA 007 C6 55 F5 484 80 014 C6 18 6.0 55 581 PA 007 C6 55 F5 484 80 014 C6 18 6.0 55 581 PA 007 C6 55 F5 484 80 014 C6 18 6.0 55 581 PA 007 C6 55 F5 486 91 PA 007 C6 18 F5 486 91 PA 007 C6 18 F5 486 91 PA 007 C6 81													0.1 0.1
F5 498 80 014 C6 13 1.0 S5 576 PA 007 C0 36 F5 400 80 014 C6 16 4.0 S5 576 PA 007 C0 36 F5 401 80 014 C6 16 4.0 S5 576 PA 007 C0 36 F5 401 80 014 C6 31 5.0 S5 577 PA 007 C0 36 F5 402 80 014 C6 31 5.0 S5 577 PA 007 C6 49 F5 403 80 014 C6 33 5.0 S5 577 PA 007 C6 46 F5 404 80 014 C6 33 5.0 S5 577 PA 007 C6 46 F5 404 80 014 C6 33 5.0 S5 577 PA 007 C6 46 F5 404 80 014 C6 18 40 S5 578 PA 007 C6 51 F5 405 80 014 C6 18 40 S5 578 PA 007 C6 35 F5 404 80 014 C6 18 40 S5 578 PA 007 C6 35 F5 404 80 014 C6 18 40 S5 578 PA 007 C6 35 F5 404 80 014 C6 18 40 S5 578 PA 007 C6 35 F5 404 80 014 C6 18 40 S5 578 PA 007 C6 35 F5 404 80 014 C6 18 40 S5 578 PA 007 C6 35 F5 404 80 014 C6 18 40 S5 578 PA 007 C6 35 F5 404 80 014 C6 18 40 S5 578 PA 007 C6 35 F5 404 80 014 C6 18 40 S5 578 PA 007 C6 81 F5 405 PA 007 C6 81 F5 4							6.0						3.50
ES 400 80 014 CG 16 4.0 SS 576 PA DO7 CG 36 SS 577 PA DO7 CG 36 SS 578 PA DO7 CG 36 SS 578 PA DO7 CG 49 SS 578 PA DO7 CG 49 SS 578 PA DO7 CG 49 SS 578 PA DO7 CG 49 SS 578 PA DO7 CG 49 SS 578 PA DO7 CG 49 SS 578 PA DO7 CG 49 SS 578 PA DO7 CG 49 SS 578 PA DO7 CG 49 SS 578 PA DO7 CG 49 SS 578 PA DO7 CG 49 SS 578 PA DO7 CG 49 SS 578 PA DO7 CG 51 SS				014	CG	13	1.0	35 574		DOT		55	10.0
ES 461 80 014 CG 33 5-0 SS 577 PA 001 CU 38 PS 463 80 014 CG 24 31-0 SS 579 PA D07 CG 49 PS 463 80 014 CG 24 31-0 SS 579 PA D07 CG 26 PS 464 80 014 CG 18 47 5-0 SS 579 PA D07 CG 26 PS 464 80 014 CG 18 47 5-0 SS 579 PA D07 CG 51 PS 465 80 014 CG 18 47 5-0 SS 579 PA D07 CG 51 PS 465 80 014 CG 18 47 5-0 SS 579 PA D07 CG 51 PS 465 DA D43 CR 47 5-0 SS 579 PA D07 CG 81 PS 465 DA D43 CR 71 10-0 SS 579 PA D07 CG 81 PS 467 DA D43 CR 71 10-0 SS 579 PA D07 CG 81 PS 467 DA D43 CR 71 10-0 SS 579 PA D07 CG 81 PS 470 DA D43 CR 71 10-0 SS 579 PA D07 CG 81 PS 470 DA D43 CR 77 S-0 SS 579 PA D07 CG 47 PS 472 DA D43 CR 77 S-0 SS 579 PA D07 CG 37 PA D07 C								55 575					5.0
FS 462 80 014 CG 62 21.0 SS 578 PA DO7 CG 49 FS 464 80 014 CG 33 S.0 SS 578 PA DO7 CG 26 FS 464 80 014 CG 33 S.0 SS 580 PA DO7 CG 26 FS 464 80 014 CG 16 6.0 SS 580 PA DO7 CG 51 FS 466 DA DA3 GR 47 S.0 SS 580 PA DO7 CG 51 FS 466 DA DA3 GR 47 S.0 SS 580 PA DO7 CG 51 FS 466 DA DA3 GR 47 S.0 SS 580 PA DO7 CG 51 FS 466 DA DA3 GR 71 10.0 SS 583 PA DO7 CG 61 FS 468 DA DA3 GR 71 10.0 SS 583 PA DO7 CG 61 FS 468 DA DA3 GR 71 10.0 SS 583 PA DO7 CG 61 FS 468 DA DA3 GR 75 SS 0 SS 584 PA DO7 CG 61 FS 468 DA DA3 GR 75 SS 0 SS 584 PA DO7 CG 61 FS 468 DA DA3 GR 75 SS 0 SS 584 PA DO7 CG 61 FS 468 DA DA3 GR 75 SS 0 SS 584 PA DO7 CG 62 FS 470 DA DA3 GR 75 SS 0 SS 584 PA DO7 CG 64 FS 471 DA DA3 GR 75 SS 0 SS 584 PA DO7 CG 64 FS 471 DA DA3 GR 75 SS 0 SS 584 PA DO7 CG 64 FS 472 DA DA3 GR 75 SS 0 SS 584 PA DO7 CG 77 PA DO7													4.6 10.0
ES 463 BD 014 CG 24 3.0 SS 577 PA D07 CG 26 ES 465 BD 014 CG 16 6.0 SS 577 PA D07 CG 25 ES 465 BD 014 CG 16 6.0 SS 586 PA D07 CG 35 ES 465 BD 014 CG 16 6.0 SS 586 PA D07 CG 35 ES 465 BD 014 CG 16 6.0 SS 586 PA D07 CG 35 ES 467 DA D43 GR 71 10.0 SS 586 PA D07 CG 16 ES ES 467 DA D43 GR 71 10.0 SS 586 PA D07 CG 66 ES ES 467 DA D43 GR 75 SS 585 PA D07 CG 66 ES ES 467 DA D43 GR 75 SS 585 PA D07 CG 66 ES ES 467 DA D43 GR 75 SS 585 PA D07 CG 42 ES 467 DA D43 GR 75 SS 585 PA D07 CG 42 ES 467 DA D43 GR 76 SS 585 PA D07 CG 42 ES 467 DA D43 GR 76 SS 585 PA D07 CG 35 SS 5													1.0
## \$465	FS	463	RC	014									4.0
F5 466 DA DA DA3 GR 47 5.0 55 582 PA U07 CL 186 F5 468 DA DA3 GR 71 10-0 55 583 PA U07 CL 186 F5 468 DA DA3 GR 71 5-0 55 585 PA U07 CL 186 F5 468 DA DA3 GR 75 5.0 55 585 PA U07 CL 187 F5 469 DA DA3 GR 75 5.0 55 585 PA U07 CL 187 F5 470 DA DA3 GR 76 5.0 55 585 PA U07 CL 187 F5 471 DA DA3 GR 770 5.0 55 585 PA U07 CG 44 F5 471 DA DA3 GR 770 5.0 55 586 PA U07 CG 44 F5 472 DA DA3 GR 770 5.0 55 586 PA U07 CG 30 F5 473 DA DA3 GR 115 16.0 55 586 PA U07 CG 32 F5 474 DA DA3 GR 302 5.0 55 590 PA D07 CG 26 F5 475 DA DA4 GR 39 4.0 55 590 PA D07 CG 37 F5 477 DA DA4 GR 39 4.0 55 590 PA D07 CG 47 F5 479 DA DA4 GR 37 4.0 55 590 PA D07 CG 48 F5 479 DA DA4 GR 37 4.0 55 590 PA D07 CG 48 F5 480 DA DA4 GR 32 5.0 55 590 PA D07 CG 48 F5 481 DA DA4 GR 32 5.0 55 590 PA D07 CG 48 F5 483 DA DA4 GR 26 4.0 55 590 PA D07 CG 48 F5 483 DA DA4 GR 32 5.0 55 590 PA D07 CG 48 F5 483 DA DA4 GR 32 5.0 55 590 PA D07 CG 48 F5 483 DA DA4 GR 32 5.0 55 590 PA D07 CG 48 F5 483 DA DA4 GR 32 5.0 55 590 PA D07 CG 48 F5 483 DA DA4 GR 32 5.0 55 590 PA D07 CG 48 F5 483 DA DA4 GR 32 5.0 55 590 PA D07 CG 48 F5 55 500 PA D07 CG 41 1.0 55 500 PA D07 CG 68 F5 55 500 PA D07 CG 29 1.0 55 500 PA D07 CG 45 F5 55 500 PA D07 CG 29 1.0 55 500 PA D07 CG 45 F5 500 PA D07 CG 47 1.0 55 500 PA D07 CG 45 F5 500 PA D07 CG 47 1.0 55 500 PA D07 CG 45 F5 500 PA D07 CG 47 1.0 55 500 PA D07 CG 45 F5 500 PA D07 CG 47 1.0 55 500 PA D07 CG 45 F5 500 PA D07 CG 48 D07 CG 49 D07 CG 45 F5 500 PA D07 CG 47 1.0 55 500 PA D07 CG 45 F5 500 PA D07 CG 47 1.0 55 500 PA D07 CG 45 F5 500 PA D07 CG 47 1.0 55 500 PA D07 CG 45 F5 500 PA D07 CG 47 1.0 55 500 PA D07 CG 45 F5 500 PA D07 CG 47 1.0 55 500 PA D07 CG 55 F5 511 PA D07 CG 47 1.0 55 500 PA D07 CG 55 F5 511 PA D07 CG 47 1.0 55 500 PA D07 CG 55 F5 511 PA D07 CG 47 1.0 55 500 PA D07 CG 55 F5 511 PA D07 CG 51 FA D07 CG 55 F5 511 PA D07 CG 51 FA D07 CG 55 F5 511 PA D07 CG 51 FA D07 CG 55 F5 511 PA D07 CG 51 FA D07 CG 55 F5 511 PA D07 CG 51 FA D07 CG 55 F5 511 PA D07 CG 51 FA D07 CG 55 F5 511 PA D07 CG 51 FA D07 CG 55 F5 511 PA D07 CG 51 FA D07 CG 55 F	FS												9.0 5.0
#\$ 447							5.0						2.0
F5 469 DA D43 GR 55 15.0 53.585 PA D07 CL 82 F5 470 DA D43 GR 79 5.0 55.586 PA D07 CG 44 F5 471 DA D43 GR 70 6.0 55.587 PA D07 CG 79 F5 473 DA D43 GR 115 16.0 55.588 PA D07 CG 39 F5 473 DA D43 GR 115 16.0 55.588 PA D07 CG 32 F5 474 DA D43 GR 115 16.0 55.588 PA D07 CG 32 F5 475 DA D44 UR 51 6.0 55.591 PA D07 CG 25 F5 475 DA D44 GR 39 4.0 55.591 PA D07 CG 37 F5 477 DA D44 GR 39 4.0 55.592 PA D07 CG 37 F5 478 DA D44 GR 37 4.0 55.593 PA D07 CG 42 F5 478 DA D44 GR 37 4.0 55.593 PA D07 CG 64 F5 480 DA D44 GR 37 4.0 55.593 PA D07 CG 65 F5 483 DA D44 GR 32 3.0 55.595 PA D07 CG 48 F5 480 DA D44 GR 32 3.0 55.599 PA D07 CG 65 F5 483 DA D44 GR 32 3.0 55.599 PA D07 CG 65 F5 502 PA D07 CG 32 2.0 55.590 PA D07 CG 65 F5 503 PA D07 CG 32 2.0 55.590 PA D07 CG 65 F5 503 PA D07 CG 32 2.0 55.590 PA D07 CG 65 F5 503 PA D07 CG 32 2.0 55.590 PA D07 CG 65 F5 503 PA D07 CG 32 2.0 55.500 PA D07 CG 65 F5 503 PA D07 CG 29 2.0 55.600 PA D07 CG 65 F5 500 PA D07 CG 29 2.0 55.600 PA D07 CG 65 F5 500 PA D07 CG 29 2.0 55.600 PA D07 CG 65 F5 500 PA D07 CG 29 2.0 55.600 PA D07 CG 65 F5 500 PA D07 CG 29 2.0 55.600 PA D07 CG 65 F5 500 PA D07 CG 29 2.0 55.600 PA D07 CG 65 F5 500 PA D07 CG 29 2.0 55.600 PA D07 CG 33 F5 500 PA D07 CG 33 5.0 55 F6 FA D07 CG 33 5.0 55 FF FA D07 CG 33 5.0 55 FF FA D07 CG 33 5.0 55 FF FA D07 CG 33 5.0 55 FF FA D07 CG 33 5.0 55 FF FA D07 CG 33 5.0 55 FF FA D07 CG 33 5.0 55 FF FA D07 CG 33 5.0 55 FF FA D07 CG 33 5.0 55 FF FA D07 CG 33 5.0 55 FF FA D07 CG 33 5.0 55 FF FA D07 CG 33 5.0 55 FF FA D07 CG 33 5.0 55 FF FA D07 CG 47 1.0					GR	71	10.0		PA				4.0
#55 470 DA D43 GR 79 5.0 55 586 PA D07 CG 44   #55 471 DA D43 GR 70 6.0 55 587 PA D07 CG 79   #54 472 DA D43 GR 87 8.0 55 588 PA D07 CG 30   #54 473 DA D43 GR 302 5.0 55 589 PA D07 CG 30   #55 474 DA D43 GR 302 5.0 55 589 PA D07 CG 32   #55 475 DA D44 GR 39 4.0 55 591 PA D07 CG 13   #55 477 DA D44 GR 39 4.0 55 592 PA D07 CG 24   #55 478 DA D44 GR 37 4.0 55 592 PA D07 CG 24   #55 479 DA D44 GR 37 4.0 55 594 PA D07 CG 24   #55 480 DA D44 GR 32 5.0 55 595 PA D07 CG 26   #56 481 DA D44 GR 32 5.0 55 595 PA D07 CG 41   #56 482 DA D44 GR 32 5.0 55 595 PA D07 CG 41   #57 482 DA D44 GR 32 5.0 55 595 PA D07 CG 41   #57 483 DA D44 GR 32 5.0 55 596 PA D07 CG 41   #57 55 505 PA D07 CG 32 2.0 55 596 PA D07 CG 51   \$55 505 PA D07 CG 29 2.0 55 605 PA D07 CG 33   \$55 505 PA D07 CG 29 2.0 55 605 PA D07 CG 33   \$55 505 PA D07 CG 29 2.0 55 605 PA D07 CG 35   \$55 505 PA D07 CG 29 2.0 55 605 PA D07 CG 35   \$55 505 PA D07 CG 29 2.0 55 605 PA D07 CG 35   \$55 505 PA D07 CG 32 2.0 55 605 PA D07 CG 35   \$55 505 PA D07 CG 37 1.0 55 605 PA D07 CG 35   \$55 505 PA D07 CG 37 1.0 55 605 PA D07 CG 35   \$55 505 PA D07 CG 37 1.0 55 605 PA D07 CG 35   \$55 505 PA D07 CG 37 1.0 55 606 PA D07 CG 35   \$55 505 PA D07 CG 37 1.0 55 606 PA D07 CG 35   \$55 505 PA D07 CG 37 1.0 55 606 PA D07 CG 35   \$55 505 PA D07 CG 37 1.0 55 606 PA D07 CG 35   \$55 505 PA D07 CG 37 1.0 55 607 PA D07 CG 35   \$55 505 PA D07 CG 37 1.0 55 608 PA D07 CG 35   \$55 505 PA D07 CG 37 1.0 55 608 PA D07 CG 35   \$55 505 PA D07 CG 37 1.0 55 608 PA D07 CG 35   \$55 505 PA D07 CG 37 1.0 55 608 PA D07 CG 35   \$55 505 PA D07 CG 37 1.0 55 608 PA D07 CG 37   \$55 505 PA D07 CG 37 1.0 55 608 PA D07 CG 37   \$55 505 PA D07 CG 37 1.0 55 608 PA D07 CG 37   \$55 505 PA D07 CG 37 1.0 55 608 PA D07 CG 37   \$55 505 PA D07 CG 37 1.0 55 608 PA D07 CG 37   \$55 505 PA D07 CG 37 1.0 55 608 PA D07 CG 37   \$55 505 PA D07 CG 37 1.0 55 608 PA D07 CG 37   \$55 505 PA D07 CG 37 1.0 55 608 PA D07 CG 37   \$55 505 PA D07 CG 37 1.0 55 608 PA D07 CG 37   \$55 505 PA D07 CG 37 1.0 55 608 PA D07 CG 37   \$55 505 PA D07 CG 37					GR.		5.0						6.0
F5 471													3.0
F5 472 DA													3.0
F5 473 DA	F.S	472		043	C-4	87	8.0	35 5 pp	₽▲	007	CG	30	4.0
F5 475			DA								Çu		0.1
F5 476 UA D44 GR 39 4.0 S5 592 PA D07 CG 24 F5 477 DA D44 GR 377 4.0 S5 593 PA UD7 CG 24 F5 478 DA D44 GR 377 4.0 S5 593 PA D07 CG 26 F5 479 DA D44 GR 377 4.0 S5 599 PA D07 CG 26 F5 479 DA D44 GR 32 2.0 S5 999 PA D07 CG 26 F5 481 DA D44 GR 32 2.0 S5 999 PA D07 CG 41 F5 481 DA D44 GR 26 4.0 S5 597 PA D07 CG 41 F5 482 DA D44 GR 28 1.0 S5 999 PA D07 CG 41 F5 483 DA D44 GR 28 1.0 S5 999 PA D07 CG 55 B01 PA D07 CG 32 S5 800 PA D07 CG 55 B01 PA D07 CG 35 B05 PA D07 CG 35 S5 809 PA D07 CG 35 S5 809 PA D07 CG 35 S5 809 PA D07 CG 35 S5 809 PA D07 CG 35 S5 809 PA D07 CG 36 B05 S5 500 PA D07 CG 36 B05 S5 500 PA D07 CG 36 B05 S5 500 PA D07 CG 39 1.0 S5 809 PA D07 CG 46 S5 500 PA D07 CG 47 1.0 S5 600 PA D07 CG 45 S5 500 PA D07 CG 47 1.0 S5 600 PA D07 CG 45 S5 511 PA D07 CG 47 1.0 S5 611 PA D07 CG 45 S5 511 PA D07 CG 47 1.0 S5 611 PA D07 CG 45 S5 511 PA D07 CG													1.0 0.1
#\$ 477							4 •D						0.1
F5 470 0A 044 GR 32 5.0 55 595 PA 007 CU 41 1.0 55 602 PA 007 CU 42 F5 503 PA 007 CU 41 1.0 55 505 PA 007 CU 41 1.0 55 505 PA 007 CU 41 1.0 55 505 PA 007 CU 41 1.0 55 505 PA 007 CU 41 1.0 55 505 PA 007 CU 41 1.0 55 606 PA	FS	477	DA	D4.4	GR	45	4.0	55 593	PA	U07	EG	24	0.1
\$\begin{array}{c ccccccccccccccccccccccccccccccccccc							4+0	35 974					12.0
P5 481 DA D44 GR 26 4.0 32 3.0 35 598 PA U07 LU 47 P5 482 DA D44 GR 28 1.0 55 599 PA U07 LU 47 P5 483 DA D44 GR 28 1.0 55 599 PA U07 LU 47 P5 483 DA D44 GR 28 1.0 55 599 PA U07 LU 47 P5 P5 483 DA D44 GR 28 1.0 55 500 PA U07 LU 47 P5 P5 P5 P5 P5 P5 P5 P5 P5 P5 P5 P5 P5													1.0
F5 482				D4.4				55 597					2.6
F5 483 DA D44 GR 28 1.0 55 599 PA 307 CD 22 25 55 500 PA U07 CD 60 55 500 PA U07 CD 60 55 500 PA U07 CD 60 55 500 PA 007 CG 51 55 500 PA 007 CG 29 2.0 55 600 PA 007 CG 33 55 500 PA 007 CG 29 2.0 55 600 PA 007 CG 33 55 500 PA 007 CG 29 2.0 55 600 PA 007 CG 33 55 500 PA 007 CG 39 2.0 55 600 PA 007 CG 25 55 500 PA 007 CG 39 2.0 55 600 PA 007 CG 25 55 500 PA 007 CG 39 2.0 55 600 PA 007 CG 25 55 500 PA 007 CG 39 2.0 55 600 PA 007 CG 25 55 500 PA 007 CG 39 2.0 55 600 PA 007 CG 35 500 PA 007 CG 39 2.0 55 600 PA 007 CG 35 500 PA 007 CG	F۵	482	DA	D4.4	GH	35	3.0	55 598		JU 7		72	10.0
\$\begin{array}{c ccccccccccccccccccccccccccccccccccc	F5	483	DA	D4.4	GR	28	1.0					55	0 - 1
\$\frac{5}{5} \frac{501}{502}  \text{PA} & \text{DO7} & \text{CL} & \frac{41}{1} & \text{1.0} & \frac{55}{5} \frac{602}{55} & \text{PA} & \text{DO7} & \text{CL} & \frac{32}{2} & \text{2.0} & \text{55} \frac{603}{55} & \text{PA} & \text{DO7} & \text{CL} & \frac{32}{29} & \text{2.0} & \text{55} \frac{603}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{29} & \text{1.0} & \text{55} \frac{608}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{29} & \text{1.0} & \text{55} \frac{608}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{27} & \text{1.0} & \text{55} \frac{608}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{27} & \text{1.0} & \text{55} \frac{608}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{27} & \text{1.0} & \text{55} \frac{608}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{24} & \text{0.1} & \text{55} \frac{608}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{29} & \text{20.1} & \text{25} \frac{608}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{29} & \text{20.1} & \text{25} \frac{609}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{29} & \text{20.1} & \text{25} \frac{609}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{29} & \text{20.1} & \text{25} \frac{609}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{29} & \text{20.1} & \text{25} \frac{609}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{29} & \text{20.1} & \text{25} \frac{609}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{29} & \text{20.1} & \text{25} \frac{609}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{29} & \text{20.1} & \text{25} \frac{609}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{29} & \text{20.1} & \text{25} \frac{609}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{27} & \text{20.1} & \text{25} \frac{619}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{27} & \text{20.1} & \text{25} \frac{619}{55} & \text{PA} & \text{DO7} & \text{CL} & \text{27} & \text{25} & \text{21} & \text{20.1} & \text{25} \frac{615}{55} & \text{24} & \text{PA} & \text{DO7} & \text{CL} & \text{27} & \text{25} & \text{21} & 20													P.1
\$5 501 PA D07 CL 32 2.0 \$5 608 PA D07 CG 33 \$5 503 PA D07 CG 66 \$6 \$5 504 PA D07 CG 29 2.0 \$5 608 PA D07 CG 33 \$5 503 PA D07 CG 29 1.0 \$5 608 PA D07 CG 25 \$5 505 PA D07 CG 29 1.0 \$5 608 PA D07 CG 25 \$5 505 PA D07 CG 29 1.0 \$5 608 PA D07 CG 25 \$5 507 PA D07 CG 27 1.0 \$5 608 PA D07 CG 30 \$5 508 PA D07 CG 24 0.1 \$5 608 PA D07 CG 30 \$5 508 PA D07 CG 37 1.0 \$5 608 PA D07 CG 39 \$5 508 PA D07 CG 37 1.0 \$5 608 PA D07 CG 39 \$5 508 PA D07 CG 37 1.0 \$5 608 PA D07 CG 39 \$5 508 PA D07 CG 37 1.0 \$5 608 PA D07 CG 37 1.0 \$5 508 PA D07 CG 27 15 508 PA D						_					ČĞ		18.0
\$5 503	35.5	U1						55 403	PA	D0 7	CG	68	6.0
55 504 PA 007 CG 29 1.0 55 606 PA D07 CG 25 55 505 PA 007 CG 39 2.0 55 606 PA D07 CG 25 55 505 PA 007 CG 27 1.0 55 608 PA D07 CG 30 55 507 PA D07 CG 32 1.0 55 608 PA D07 CG 32 55 507 PA D07 CG 32 1.0 55 608 PA D07 CG 32 1.0 55 608 PA D07 CG 32 1.0 55 608 PA D07 CG 32 1.0 55 610 PA D07 CG 32 55 509 PA D07 CG 45 55 509 PA D07 CG 45 55 510 PA D07 CG 45 55 511 PA D07 CG 47 1.0 55 612 PA D07 CG 27 55 511 PA D07 CG 47 1.0 55 613 PA D07 CG 32 55 512 PA D07 CG 47 1.0 55 613 PA D07 CG 32 55 512 PA D07 CG 47 1.0 55 613 PA D07 CG 32 55 513 PA D07 CG 39 0.1 55 614 PA D07 CG 32 55 514 PA D07 CG 39 0.1 55 615 PA D07 CG 35 515 PA D07 CG 37 0.1 55 516 PA D07 CG 37 0.1 55 516 PA D07 CG 37 0.1 55 516 PA D07 CG 37 0.1 55 516 PA D07 CG 37 0.1 55 516 PA D07 CG 37 0.1 55 518 PA D07 CG 37 0.1 518 PA D07 CG 37 0.1 518 PA D07 CG 37 0.1 518 PA D07 CG 37 0.1 518 PA D07 CG 37 0.1 518 PA D07 CG 37 0.1 518 PA D07 CG 37 0.1 518 PA D07 CG 37 0.1 518 PA D07 CG 37 0.1 518 PA D07 CG 37 0.1 518 PA D07 CG 37 0.1 518 PA D07 CG 37 0.1 518 PA D07 CG 37 0.1 518 P	55 5	03	PA	007	CG	29	5.0		PA	007	ÇĞ	33	5.0 1.0
53 505 PA 007 CG 27 1.0 55 608 PA 007 CG 30 55 507 PA 007 CG 30 55 507 PA 007 CG 32 1.0 55 608 PA 007 CG 32 1.0 55 608 PA 007 CG 32 1.0 55 608 PA 007 CG 32 1.0 55 608 PA 007 CG 32 1.0 55 608 PA 007 CG 32 1.0 55 608 PA 007 CG 32 1.0 55 608 PA 007 CG 32 55 510 PA 007 CG 45 55 510 PA 007 CG 47 1.0 55 611 PA 007 CG 27 55 512 PA 007 CG 47 1.0 55 613 PA 007 CG 32 55 512 PA 007 CG 39 0.1 55 613 PA 007 CG 38 55 513 PA 007 CG 39 0.1 55 615 PA 007 CG 27 55 515 PA 007 CG 33 4 2.0 55 615 PA 007 CG 55 55 515 PA 007 CG 33 55 615 PA 007 CG 35 55 515 PA 007 CG 37 1.0 55 615 PA 007 CG 57 55 515 PA 007 CG 37 1.0 55 615 PA 007 CG 57 55 515 PA 007 CG 37 1.0 55 615 PA 007 CG 57 55 515 PA 007 CG 37 1.0 55 615 PA 007 CG 57 55 515 PA 007 CG 37 1.0 55 616 PA 007 CG 55 55 618 PA 00	35 5	04	PA	007	CG	29	1.0	33 002 35 404	PA	007	CG.		4.0
35 506 PA 007 CC 24 0-1 S5 608 PA D07 CG 39 \$5 507 PA D07 CG 32 1.0 \$5 508 PA D07 CG 32 1.0 \$5 509 PA D07 CG 45 \$5 510 PA D07 CG 40 0-1 S5 610 PA D07 CG 45 \$5 511 PA D07 CG 47 1.0 \$5 512 PA D07 CG 42 0-1 S5 613 PA D07 CG 32 \$5 513 PA D07 CG 42 0-1 S5 613 PA D07 CG 32 \$5 514 PA D07 CG 42 0-1 S5 615 PA D07 CG 27 \$5 515 PA D07 CG 43 4-0 S5 615 PA D07 CG 27 \$5 515 PA D07 CG 43 4-0 S5 615 PA D07 CG 27 \$5 515 PA D07 CG 43 4-0 S5 615 PA D07 CG 27 \$5 515 PA D07 CG 34 2.0 S5 617 PA D07 CG 50 \$5 515 PA D07 CG 34 2.0 S5 617 PA D07 CG 50 \$5 515 PA D07 CG 37 1.0 S5 617 PA D07 CG 50 \$5 515 PA D07 CG 37 1.0 S5 617 PA D07 CG 50	35 5	05	PA	007	CG		2.0	55 607	PA	007	CL	17	0.1
55 510 PA D07 CG 47 1.0 55 612 PA D07 CG 27 55 512 PA D07 CG 27 55 512 PA D07 CG 39 D-1 55 613 PA D07 CG 39 D-1 55 613 PA D07 CG 38 D-1 55 613 PA D07 CG 38 D-1 55 613 PA D07 CG 38 D-1 55 615 PA D07 CG 27 55 515 PA D07 CG 30 37 1.0 55 616 PA D07 CG 50 55 515 PA D07 CG 37 1.0 55 617 PA D07 CG 50 55 515 PA D07 CG 37 1.0 55 618 PA D07 CG 50 55 515 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG	35 5	U6 07						55 608	PA	007	CG	30	0.1
55 510 PA D07 CG 47 1.0 55 612 PA D07 CG 27 55 512 PA D07 CG 27 55 512 PA D07 CG 39 D-1 55 613 PA D07 CG 39 D-1 55 613 PA D07 CG 38 D-1 55 613 PA D07 CG 38 D-1 55 613 PA D07 CG 38 D-1 55 615 PA D07 CG 27 55 515 PA D07 CG 30 37 1.0 55 616 PA D07 CG 50 55 515 PA D07 CG 37 1.0 55 617 PA D07 CG 50 55 515 PA D07 CG 37 1.0 55 618 PA D07 CG 50 55 515 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG 55 55 516 PA D07 CG	\$5.50	08				32		55 409			ÇĞ		3.0
\$5 510 PA D07 C6 47 1.0 \$5 613 PA D07 C6 27 \$5 512 PA D07 C6 27 \$5 512 PA D07 C6 32 \$5 512 PA D07 C6 39 D01 \$5 613 PA D07 C6 38 55 513 PA D07 C6 39 D01 \$5 615 PA D07 C6 28 \$5 513 PA D07 C6 39 D01 \$5 615 PA D07 C6 27 \$5 515 PA D07 C6 30 \$5 515 PA D07 C6 37 \$5 515 PA D07 PA D07 PA D07 PA	35 5	09	PA	<b>007</b>	CG	•3	5.0	55 611					1.0
53 514 PA D07 CG 43 4.0 55 615 PA D07 CG 27 55 515 PA D07 CG 34 2.0 55 616 PA D07 CG 50 50 55 516 PA D07 CG 37 1.0 55 618 PA D07 CG 53	22.2	10	PA	DO 7	CG	4 D	0-1	55 612	PA	DO 7	23	27	3.0
35 514 PA D07 CG 43 4.0 35 615 PA D07 CG 27 55 515 PA D07 CG 34 2.0 35 616 PA D07 CG 50 50 55 516 PA D07 CG 37 1.0 55 618 PA D07 CG 53	77 2	1 I	PA	DD 7	CG CG		1.0	55 613	PA	D07	CG	32	2.0
35 514 PA D07 CG 43 4.0 35 616 PA D07 CG 57 55 516 PA D07 CG 50 55 516 PA D07 CG 50 50 50 617 PA D07 CG 50 50 50 516 PA D07 CG 50 50 50 618 PA D07 CG 50 50 50 618 PA D07 CG 50 50 50 618 PA D07 CG 50 50 50 618 PA D07 CG 50 50 50 618 PA D07 CG 50 50 50 618 PA D07 CG 50 50 50 618 PA D07 CG 50 50 50 618 PA D07 CG 50 50 50 618 PA D07 CG 50 50 618 PA D07 CG 50 50 618 PA D07 CG 50 50 618 PA D07 CG 50 50 618 PA D07 CG 50 50 618 PA D07 CG 50 50 618 PA D07 CG 50 50 618 PA D07 CG 50 50 618 PA D07 CG 50 50 618 PA D07 CG 50 50 618 PA D07 CG 50 50 618 PA D07 CG 50 50 618 PA D07 CG 50 618 PA	55.5	13		007	22		ō.i	55 614 55 616	PA DA		56 CA		2.0 1.0
55 515 PA DO7 CG 34 2-0 55 617 PA DO7 CG 50 55 516 PA DO7 CG 37 1-0 55 618 PA DO7 CG 53	55 5	14	PA	007	CG	43	4.0	33 617			<u> </u>		3.0
35 316 PA DOT CG 37 1-0   55 618 PA DOT CG 53	35 5	15			CG			55 617	PA	007	CG	50	4.0
	33 3	10 17					1.0	55 610	PA	DO 7	CG		2.0
55 516 PA 007 CG 35 2.6 1 44 20 DA 007 PG A1	55 51	16	PA	007	CG	35	2.6	55 619 55 620	PA PA	D0 7	CG CG	36 41	5.0 0.1
55 519 PA DO7 CG 27 2.0 55 821 PA DO7 CG 33	33 51	19											6.0

NU	AREA	LINE	ROCA	ŹN	43	NO.	AREA	LINE	AUCA	ŽH	A5
22 655	PA	DQ 7	CL	42	1.6	22 723	PA	F05	Lu	13	1.6
35 623	PA	D07	Çı	53	5.0	55 724	PA PA	F05	C.C	. 5 . 5	3.G 1.0
55 624 55 625	PA PA	D0 7 D0 7	C u	60 137	10.0 26.0	55 725 55 720	PA	FOS FOS	CG CG	.2	1.0
22 656	PA	003	Cu	33	5.6	55 727	PA	F05	CG	7	2.0
35 627	PA PA	003 003	CG CG	4.3 55	6.U 0.1	55 728 55 729	PA DQ	F05 218	Cr	52	5.0
22 958 27 958	PA	D03	ĔĞ	45	9.1	35 130	Du	216	Ç.	20	1.0
33 640	PA	503	CG	6.3	2.0	55 731	DQ	216	CG CL	4U0	8.0
72 935 72 931	PA PA	E00 E00	Cu Çu	+5 51	0.1 1.6	55 732 55 733	00 00	51 p	ČĠ	1 -3	0.1
55 633	PA	DO 3	CG	42	3.0	55 734	De	216	CL	24.5	0.1
55 634 55 635	PA PA	003 003	CG CG	16 24	3.C	55 735 55 736	00 00	518 518	C¢ Cu	.1 .20	0.1
\$\$ 636	PA	003	Çu	58	5.0	22 131	Du	216	Cu	45	1.0
25 637 86 66	PA PA	D0.3	ÇG Eu	49 25	2.0	55 738 55 739	0 <del>0</del>	216 216	CC CC	15 40	2.0
22 639	PA	D0 7	C to	50	1.0	55 740	50	218	ÇG	`В	<b>5.0</b>
55 640 55 641	PA PA	003 003	Cu Cu	27 42	0.1	55 741 55 742	00 00	51P 51P	CG	19	9.1 5.0
35 642	PA	DQ3	Çü	42	1.6	55 743	Du	216	CG	.9	0.1
55 643 55 644	PA PA	003	CG CG	42 24	1.0	55 144 55 145	Du Du	216 218	C. C.	15	3.0
35 645	PA	507	ÇĞ	38	4.0	33 746	50	218	CL	.3	C-1
55 646	Pá	00.3	Çu	57	é a li	55 747 55 748	89	216	ÇL Cu	13	0.1
55 647 55 648	PA Pa	د ټن د 00	Lu Lu	37 34	( .) 4.L	55 74B 55 749	0 <b>9</b>	216 216	ČĠ	15	6.1
35 64¥	PA	DO 9	Cu	25	1 -1	55 750	0 to	216	ÇG	10	14-0
22 650	PA PA	003 600	CL CL	٠٠ ٠٠	اه 4 اه فرو	55 751 55 752	Du Du	218 D25	CG CL	1) +1	2.0 3.6
\$5 652	PA	003	Cu	24	5 aC	22 153	Ðw	D2 >	Ĺ	135	5.0
25 653	PA PA	003 003	CG CG	27 52	0.1 6.0	>> 1 'A	Do	D25	ć.	+3 +3	4.0
55 654 55 655	PA	003	CG	23	3.6	55 756	84	D25	Ç.G.	57	5.0
22 656	PA	600	CG	36 49	5.0 4.0	55 757 55 758	89 89	D25	CG CG	62 16	4.0 5.0
55 657 55 658	PA PA	DO 3	CG CG	32	1.0	55 759	09	D25	CG-	17	4.0
55 659	PA	(O)	CG	33 35	7.0	55 760 55 761	00 00	025 025	CG CG	47 59	5.0
55 660 55 661	PA PA	003 003	CG	49	7.0	22 195	09	025	ÇL	38	3.0
500 66	PA	DO 3	CG	54	3.0	55 763	DQ	025	CG	35 35	3.0
55 663 55 664	PA PA	D03	CG CG	51 46	8.0 18.0	55 764 55 765	00 00	D25 D25	cc	48	6.0
25 665	PA	003	CG	31	6.0	55 766	00	650	CG	59	4.0
55 666 55 667	PA PA	003 003	CG CG	2 L 3 4	5.6 4.6	55 767 55 768	0 <del>0</del>	025 025	CG CG	37 47	1.0
55 668	PA	DO 3	CG	32	う。し	55 769	DO	D2 5	CG	53	5.0
55 669	PA PA	003 003	CG CG	62 25	5.0 3.E	55 770 55 771	04 04	025 025	CG CG	14	4.0
55 670 55 671	PA	005	CG	51	+	55 774	DQ	025	23	24	4 .C
55 672	PA	500	Cu	30 24	2.0 3.L	55 773 55 774	D6 20	D25	CG CG	30 47	5.C 4.C
55 673	PA PA	D0 4 D0 5	CG	13	5.6	\$\$ 175	20	025	CG	13	€-0
55 675	PA	0.05	CG	45	6.6	55 776	D.	D25	CG CG	28 49	1.6
55 676 55 677	PA PA	00≥ 00≥	CG CG	36 36	2.C	55 778 55 778	74 74	025 025	čů	42	2.0
\$5 678	PA	D05	ĊĿ	33	4 al.	22 136	38	025	Lie	26 37	1.0
55 679 55 680	PA Pa	D05 D05	C G	40	2 o C D o C	55 780 55 781	DC DC	D1 7 U1 7	CG CG	25	4.0
55 681	PA	500≥	ÇG	48	9.6	55 782	DL	017	C.	35	0.5
55 682 55 683	PA Pa	005 005	CG CG	42	1.U	55 783 55 784	DL DL	01 7 01 7	Cu Cu	43 25	5.0 6.1
55 684	PA	005	CG	26	1.6	55 785	ðι	017	Cio	20	4.0
55 685	PA PA	005	CG	32 40	1.0 2.6	55 766 55 787	DL OL	D17 D17	£¢ Ct	10 11	5.6
55 686 55 687	PA	D05	Cu	31	1.0	55 788	UL	017	CG	59	6.1
55 688	PA Pa	D05	CG CG	33 57	). ¢	55 789 55 790	DL DL	D17	EG EG	42 40	0.1 1.0
55 689 55 640	PA	00≥ 200	£G.	44	>.0	55 791	DL	017	CG	45	5.0
55 691	PA PA	D07	CG CG	25 24	4.C	55 793 55 793	OL OL	017 017	CG	+0 +8	1.0
\$\$ 692 55 693	PA	007	CG	27	5.6	22 144	OL	017	Clu	20	4.0
35 694	PA	007	CG	24 39	3.0	55 745 >> 746	DL DL	017 017	CG Eq.	55 85	11.0 56.6
55 695 55 696	PA Pa	D07	CG	34	3.1	22 141	J.L	D1 7	C.G.	43	6.0
33 647	PA	007	CG	<b>31</b>	2.L	55 790	OL OL	017 017	Eŭ Cu	17	U.1 3.0
55 698 55 699	PA MA	D07 F05	Cu CG	47	1.1	22 1AA	OL.	017	CL	10	***
55 7 UC	MA	FQ5	ÇG	4.7	1.1	27 en1	ÐL	DL7	Ču	12	3.0
55 701 55 702	AM AM	F05	Eb Eb	21 46	J 11	22 403 22 605	Jr Jr	017 017	Lu Cu	3 6 5 c	6.0 (.1
22 103	MA	FO^	Lu	•0	6.0	33 bbs	٦L	D) /	LL	16	2.0
55 704	MA	FO3	CL	49	0.1 0.1	51 AU1	DL	01 / D17	c. C.	.s.e 16	7.0
55 705 55 706	AA AA	F0>	CG CG	24	5.0	55 807	ÜĹ	017	ÇĿ	18	1.0
55 707	MA	FO5	CG	28	6.0	55 808	OL	D17	CG CG	- 18	5.0 4.0
55 708 55 709	MA Ma	FOS	CG CG	23 40	5.0 3.0	55 809 55 810	DL OL	D17	ÇG	15	3.0
55 710	AM	FOS	CG	40	0 · 4	55 011	OL.	017	ÇG CU	50 53	13.0
55 711 55 712	PA PA	F05 F05	CG	48 43	3.0 3.0	22 913 27 915	DL DL	D17 F02	23	45	37.0
55 713	PA	FOS	23	48	4.0	55 814	DL	FOZ	CG	23	46.0 0.1
55 714	PA Pa	F05	CG CG	22 45	4.0 1.0	55 815 55 816	DL DL	F02 F02	CG CG	30 47	14.0
55 715 55 716	PA	F03	Ç.G	40	0.1	55 817	OL	FQ2	CG	59	3.0
\$5 717	PA	FOS	CG	10	1.0	55 818 55 819	DL DL	F02	56 23	26 56	3.0 54.0
55 716 55 719	PA PA	FOS FOS	CG CG	+6	0.1	55 820	DL	F02	£6	27	6.0
55 720	PA	FQ\$	CG	, 0 ; 4	0.1 1.0	55 820 55 821 55 822	DL OL	F02	CG	#50 26	0.000\$
55 721 55 722	PA Pa	F05	C.	77	1.0	55 823	٥Ľ	F02	Ç.	15	30.0

NÙ	AREA	LINE	ROCK	ZH	AS	NÜ	AREA	LINE	ROCA	žN	AS
NS 1037	PA	DOS	C G	44	3.0	NS 1140	PA	001	CG	31	3.0
NS 1038	PA	D05	CG	24	2.6	MS 1141	PA	DO 1	CL	33	1.0
NS 1039	PA	005	23	25	5.0	MS 1142	PA Pa	001	CG CG	49 41	3.0
NS 1040 NS 1041	PA PA	005 005	CC	34 30	0.1	NS 1143 NS 1144	PA	00 1 00 1	ÇĞ	71	1.0
MS 1042	PA	D0 5	čč	48	2.0	NS 1145	PA	001	ČĞ	26	5 . D
NS 1043	PA	005	CC	22	3.0	HS 8146	PA	100	Ce	60	1.0
NS 1044	PA	D05	ÇL	*6	15.0	HS 1147	PA PA	DO 1	CP CC	42 40	4.D
NS 1045 NS 1046	PA	005 005	Çu Cu	32 18	3.0 2.L	NS 1148 NS 1147	PA	001	CL	36	2.0
NS 1047	PA	005	CL	>2	2.0	NS 1150	PA	001	ČL	38	3.6
N\$ 1048	PA	400	Ċlo	31	1.6	NS 1151	PA	DO 1	CG	42	5 •0
NS 1049	P.	005	ÇL	46	٠.١	NS 1152 NS 1153	PA Pa	00 L	CG CG	25 48	2.U 2.L
45 1050 45 1051	PA PA	005 005	Çr. El	35	) . L 1 . O	NS 1143	PA	001	CG	32	3.0
NS 1052	PA	D05	čū	20	1.0	HS 1155	PA	340	ČĞ	14	5.0
MS 1053	PA	DO 5	CG	28	1.0	H5 1156	PA	OFE	CG	27	1.0
NS 1054	PA	Do5	CG 23	63 41	2.D 4m.D	NS 1157	PA	09 E	CG CG	30 25	3.0
NS 1055 NS 1056	PA PA	DO 5	ČĞ	61	4.0	NS 1158 NS 1159	PA PA	09£ 09£	ČĞ	17	5.0
NS 1057	PA	005	23	45	3.0	NS 1160	PA	OPE	ČĞ	16	3.0
NS 1058	PA	005	CG	46	1.0	NS 1161	PA	09E	CĢ	24	5.0
NS 1059	PA	005	ee ee	29 34	3.0 1.0	NS 1165	PA	096	CG CG	33 53	17.0 35.0
NS 1060 NS 1061	PA Pa	005 005	CG	30	5.0	NS 1163 NS 1164	PA PA	09E 09E	CG	42	7.0
MS 1062	PA	D05	25	46	76.0	MS 1165	PÃ	09 E	ČĞ	29	13.0
NS 1063	PA	00.5	CG	38	33.0	NS 1100	PA	940	CC	19	4.0
NS 1064	PA	905	CC	72	13.0	NS 1367	PA	09£	ce	27	6.0 5.0
MS 1065 MS 1066	PA PA	005 005	CG CG	61 55	100.0	MS 1166 MS 1169	PA PA	OPE OPE	CG CG	16 17	3.0
NS 1067	PA	D05	čč	56	165.0	NS 1107	PA	09E	čč	21	2.0
HS 1068	PA	DQ 5	CL	43	38.0	HS 1171	PA	09E	CG	50	3.0
NS 1069	PA	005	CC CC	#1 66	50.0 40.0	NS 1172	PA	9 E	CG CG	18 20	1.0
HS 1070 HS 1071	PA	DO5	ÇĞ	46	45.0	NS 1173 NS 1174	PA PA	09 E	ÇĞ	18	3.0
NS 1072	PA	005	¢G.	59	25.0	NS 1175	PA	07E	CG	20	3.0
NS 1073	PA	DO 5	ÇG	51	27.0	NS 1176	PA	OVE	CG	21	8.0
M5 1074	PA	005	CC	37 50	1.0 1.0	HS 1177	PA	09 E 09 E	CG CG	28 13	4.0 5.0
MS 1075 MS 1076	PA PA	005 005	CC.	28	2.0	NS 2178 NS 1179	PA	096	Č	źī	5.0
HS 1077	PA	005	ÇL	38	1.0	NS 1180	PA	09 E	čč	81	4.0
NS 1078	PA	DO 5	CC	35	2.0	NS 1181	PA	09E	Cu	72	1.0
NS 1079	PA	D05	CG	37 76	2.0 2.0	NS 1182	PA PA	09E	CG CG	13 19	2.0
MS 1000 MS 1001	PA PA	D05	ÇĞ	93	1.0	NS 1183 NS 1184	PA	OVE	ce	24	3.0
NS 1082	PA	005	ČĞ	6.0	3.0	NS 1185	PA	OVE	ČĞ	42	5.0
N\$ 1083	PA	D0 5	ÇĢ	40	2.0	N2 1180	PA	940	CG	32	2+0
MS 1084	PA	D05	Cr	37 32	3.0 4.0	MS 1107	PA Pa	04F	CG JJ	27 14	1.0 3.0
MS 1085 MS 1086	PA PA	005	ČG.	27	1.0	NS 1180 NS 1189	PA	09 E	ČĞ	15	ž.u
NS 1088	PA	005	CG	34	1.0	NS 1190	DQ	21 A	CG	31	3.0
RS 1089	PA	D05	çc.	33	1.0	NS 1191	DQ	21 A	ÇG	50	3.0
NS 1090	PA PA	005 005	CG CG	21 ◆9	1.0 3.0	N5 1192	00 09	21A 21A	CG CG	31 44	0.5
NS 1091 NS 1092	PA	005	ČĞ	42	5.0	NS 1193 NS 1194	De	21A	ČĞ	39	1.0
NS 1093	PA	D05	ĊĠ	54	2.0	NS 1395	Du	21A	CG	43	2.0
N5 1094	PA	005	CL	55	5.0	N5 1196	De	214	Ç.	50	1.0
M\$ 1042	PA PA	005 005	CC	36 21	4.0	N5 1197	04 04	A15	CG CG	27 36	5.0 1.0
NS 1046	PA	DO 5	ČL.	2.0	6.1	NS 1146	00	21 A	20	33	3.0
N5 1098	Pa	005	ĊĿ	45	0.1	NS 1200	Ou	214	CG	22	٥. د
H5 1099	PA	D05	ÇG	18	2.0	NZ TS01	Ďυ	214	CG	22	2.0
NS 1100	P.E.	005 005	Ĉlo Clo	26 59	1.0 2.0	NS 1202	Du Du	21A 21A	CL CL	17 31	5.0 3.6
NS 1101	PA	U0 5	Çu	53	2.0	N5 1203 N5 1204	Du	21A	Č	Ĩ,	1.0
NS 1103	PA	DOS	CC	53	1.0	NS 1205	DQ	21A	CG	27	1.0
HS 1104	PA	D05	čc	72	1.0	NS 1206	00	AIS	ÇG	46	5.0
MS 1105	PA	005	CG	67 36	1.0 2.0	NS 1207	DQ	21A	CG	42	2.D 4.0
MS 1106 MS 1107	PA PA	005 005	23	36	2.0	NS 1208	0 <del>0</del>	228 229	CG	17 62	5.0
N\$ 1108	PA	D0 5	CC	27	2.0	MS 1210	96	553	CG	43	1.0
NS 1109	PA	D0 5	ÇG	50	1.0 4.0	NS 1211	00	22 B	ÇG	58	5.0
W2 1110	PA	D05 D05	ÇG	52 38	3.0	NS 1212	DQ	228	ÇG.	5 b 39	1.0
NS 1111	PA PA	U05	ČG	41	1.0	MS 1213 MS 1214	00 00	226 228	CG CG	29	4.0
NS 1113	PA	D0 5	CG	32	2.0	MS 1215	50	226	CG	41	4.0
NS 1114	PA	005	ÇĞ	41	2.0	N2 1519	DQ	228	CG	35	4.0
MS 1115	PA PA	D05	CG	44 43	2.0 4.0	NS 1217	0.6	228	çç	50	4.0
MS 1116 MS 1217	PA	005	Ç	47	4.6	NS 1218	09 09	22 B	CG CG	65 18	4.0
NS 1118	PA	005	CC	44	4.0	NS 1220	DQ	228	CG	24	4.0
NS 1119	PA	DO 5	CG	35	3.0	NS 1221	PG	455	ÇG	24	4.0
NS 1120	PA PA	005 005	¢e ce	75 142	2.0 4.0	NS 1222	00	228	CG CG	46 81	4.0
N2 1121	PA	005	ČĞ	90	2.0	MS 1223 MS 1224	00 00	52 A 55 P	CG	32	12.0
HS 1123	PA	005	CG	52	3.0	NS 1225	Du	220	ÇG	26	3.0
NS 1124	PA	003	CC	+0	1.0	MS 1226	Du	228	CG	64	5.0
NS 1125	PA PA	D05 D05	CG CG	38 43	4.0 3.b	NS 1227	Du	228	€6 CG	26	4.0 4.0
M7 1159	PA PA	005	CC	56	3.0	8551 CH	D4 D4	426 425	CG CG	51 34	4.0 5.0
H5 1128	PA	005	CG	58	4.0	M2 1530	υq	558	čč	33	1.0
NS 1129	PA	DO 5	CC	4.6	4.0	NS 1231	09	855	ÇG	46	1.0
HS 1130	PA	005	CG	56 55	5.0 2.0	NS 1232	Du	655	CG.	63	1.0
NS 1131 NS 1132	PA PA	005 005	CG	46	\$.0	MS 1233 MS 1234	04 04	228 228	CG	33 34	1.0
NS 1133	PA	D05	ÇĞ	45	2.0	NS 1234	06	228	Č	42	4.0
MS 1134	PA	D0 5	CG	86	2.0	MS 1236	Du	228	CG	18	2.0
MS 1135	PA	DO 1	CG	37 54	3.0	NS 1237	Du	458	CG CI	25	3.0 3.0
MS 1136 MS 1137	PA PA	001 001	CC	44	4.0	NS 1238	00	228 228	CP	34 52	5.0
M2 1138	PA	001	ÇG	37	4.0	M5 124D	00	228	čč	50	3.0
NS 1139	PA	001	CG	24	1.0	NS 1241	Du	652	CG	6.6	7.0

NU	AHEA	LIME	RULA	ZH	A5	NO	AREA	LINE	ROCK	ZN	A5
55 824	OL	FO2	CG	19	14.6	55 926	NU	01.0	Çu	**	0.1
22 BSP 22 BS2	DL DL	FO2	CG CL	36 36	15.0 18.0	22 451 22 451	8Ú 80	e 10	Cu	30	0.1
35 827	DL.	F02	č.	9	5.0	33 969	80	U13	Cu Cu	17 37	3.0
22 BSB	DL.	F02	Cu	45	14.0	33 430	80	013	čč	• 6	33.0
55 829	DL	504	16	+1	1-0	55 931	90	D1 5	Ľ.	34	1.0
55 830 55 831	DL OL	FO2 FU2	f6 F6	4 <u>2</u> 70	1.0	55 933 55 933	87 87	013 013	ÇĞ	16 33	1.0
22 935	DL	FOr	FG	59	1.0	25 934	80	213	Cu Cu	35	€.U €.0
SS 833	DL	FOZ	FG	60	1.0	72 472	84	U1 3	Ĺ	36	16.0
55 834	OF	F02	FG	35	5-0	55 436	du	313	<u>t</u> u	117	82.0
55 835 55 836	DL DL	F02	F6 F6	28 37	2.0 1.0	55 437 55 438	60 50	D15	Č C L	44 24	58.0
35 837	υĹ	£05	24	55	0.3	55 939	60	013	Č	32	50.0 19.0
55 835	DL	019	CG	31	2 .0	55 440	80	013	Cu	36	0.1
55 839	DL	019	CG	64	16-0	55 941 55 942	15.0	013	Cu	30	13.0
55 840 55 841	DL DL	D1 A	CG CG	78 28	5.6 38.0	33 746	80 80	n19 e10	C b C b	• 7	0.0
35 642	Or Or	019	čě	17	4.0	35 744	89	ut 1	Ču	26 87	0.01
55 843	JL	D19	Cu	14	4.0	22 242	Bü	011	CG	49	32.0
55 844	DL	D14	Ç.	52	11.0	53 946	#D	U1 1	CL	26	34.0
55 845 55 846	OL OL	D19 D19	CG CG	176 11	0-1 3-0	33 948 33 946	50 50	D11	C G	52	37.0
55 B47	υL	010	čč	10	2.0	55 949	Hu Hu	Die	ČL	16 7 <b>v</b>	3.0 49.0
55 848	ÕL	014	ČĞ	19	0.1	33 950	du	u13	č.	101	1.00.0
55 849	DL	D1 9	Cu	22	4.6	55 451	80	J12	Cu	45	20.0
22 950	DL	D1 4	CC	18	<b>4.0</b>	33 734	èu	-1.	Cu	52	17.6
22 825 22 821	DL DL	019 014	Çu Çu	10 36	5 6 .C	55 453 55 454	<b>4</b> ∿ 80	ule ule	Et.	103 24	3.00%
22 925 22 92	JL	b14	Ču	19	6 .L	55 955	4	JI.	Li	36	4 al 3 al
35 H54	J.	914	Č	35	5.0	22 A29	Ø.	u12	دَن	74	JH4.0
33 855	ul.	u1 ×	Č.	.5 🗸	1 -4	72 951	B.	وإن	Lu	24	4.6
31 056	OL.	۰۱۷	C U	. u	10.L 0.1	77 626	nu an	-113	C.	*6	3 · · ·
55 857 55 858	DF DF	014 014	CG	38	4.0	32 950	80 80	D13	C C C	50 32	30.G 0.4
35 B59	DL	019	CG	27	5.0	55 961	80	013	CG	26	4.0
22 BPO	DL	D1 9	CG	**	13.0	55 965	BD	D13	CG	44	76.0
22 861	DL	D19	Cu	13 53	3.0	55 963	PO.	013	cc.	15	4.0
22 8 <b>63</b> 22 865	OL Di	D19 D19	CG	50	5.0	55 964 55 965	80 80	D13	CG CG	15	4.0 28.0
22 aee	50	D19	čů	43	17.0	33 966	80	013	čĠ	43	5.0
35 865	DL	014	CG	21	5.Q	55 967	#0	013	EG.	28	2.0
55 866	OL.	D1 v	CG	23	1.0	35 968	ep.	013	СĿ	50	19.0
55 867 55 868	DL OL	D1 9 D1 9	ÇG	38 43	0-1 1-0	55 96V 55 970	6U 60	D13 D13	CG CG	50 40	20.0
77 866	ÖL	014	č	65	14.0	55 971	80	013	22	45	0.1
55 H 70	ÐL	015	ČG	54	16.0	55 972	DA	D4Z	ĢĀ	50	5.0
22 931	OL	015	£6	62	90.0	\$5 973	DA	D+5	G#	25	10.0
55 872 55 873	JL JL	015 015	CG CG	42 81	6.0 10.0	35 974 35 975	DA DA	D42	Gr. Gri	24	10.6
35 874	J.	015	ČĢ	48	1.6	33 976	OA.	042	من م	25 22	13.0 9.0
55 875	δĹ	D15	CG	¥3	20.0	55 978	JA	D42	, a	20	0.1
55 876	OL.	015	Cio	85	26.0	35 979	DA	D4 2	Gk	7.3	6.0
27 933	OL OL	015 015	CG.	52 72	128.0	22 880 22 880	.1A	U4 2	54 6 3	30	50-0
55 879 55 879	OL.	015	CG CG	18	3.6	22 485	AÚ AÚ	D41 D41	GH GH	36 60	5.U 50.0
22 980	ÜL	<b>U15</b>	Č.	30	5 -0	55 983	D4	D4 1	Ğĸ	18	17.0
55 681	۵L	<b>∟1</b> >	CC	40	6.0	55 984	O1	D4 I	إنبرا	26	7.0
24 985	JL.	U15	CG CG	38 44	19.G 10.0	22 582	ĐΑ	D4 1	A.	33	6.0
55 a43 55 a64	DL DL	D15	CG	160	46.0	55 986 55 987	UA Un	04 1 04 1	GR GR	564 27	700+0 ++0
22 885	ĎĹ	J15	čũ	39	0-1	55 988	Ú,	U+1	GR	62	10.0
22 886	ВÚ	106	Ču	65	11.C	55 989	U.	041	GK	32	>.0
22 887	Bu	10N	Çu	44	45.0	1					
22 984 22 986	R0 R0	10N 10N	CG Cu	4.3 32	2.0						
22 994	90	10N	CG	26	18.0	MS 1001	PA	DOS	CG	67	2.0
55 891	80	10N	€G	10	5.0	NS 1002	PA	DO 8	53	57	3.0
22 945	aŭ.	10N	ÇG	54	7.0	NS 1003 NS 1004	PA PA	00 <i>6</i>	33 33	16 31	1.0
55 844 55 844	86 8u	10N 10N	66 66	36 34	0-1 0-1	NS 1005	PA	008	čč	45	0.1
35 845	80	10N	LL	30	3.0	NS 1006	PA	D0 5	CG	23	2.0
22 880	BO	104	CG	32	5 *0	NS 1007	PA	DQ 6	CG	32	2.0
55 897	86	10N	Çu	32	1.0	NS 1008 NS 1009	PA PA	008 008	CG GG	19 42	1.0
55 648 55 699	40	10N 10N	CL CL	34 35	1.0 5.0	NS 1010	PA	DOS	ÇĞ	23	0.1
22 ADD	80 80	10M	Cu	33	6 . D	HS 1011	PA	DOS	CG	15	1.0
22 901	an.	10 N	Li	57	£ .0	M2 1012	PA	DO8	CG	12	0.1
27 700	du	10 N	Eu	• 0	1.0	NS 1013 NS 1014	PA PA	DO B	ÇG	57	1.0
55 V63	9	10N	ĩ.	50	56.0	MS 1015	PA	008	CG	29 28	1.0
22 Anv	BĐ BU	1UA 30A	C. U	47	0.1 1.0	MS 1016	PA	008	22	32	2.0
12 APE	9t.	10%	£	•1	i.i	NS 1017	PA	DOS	CG	32	5.0
12 961	841	104	C,	10	1.0	NS 1018	PA	008	ÇĞ	50	2.0
55 9 DB	80	10N	ÇG	34	9.0	NS 1019 NS 1020	PA PA	00 b	CG	31 60	5.0
55 909	80	10N	CG CG	10 29	0.1 0.1	NS 1021	PA	006	CL	17	2.6 1.0
55 910 55 911	BU BU	10M 10M	CG CG	27	4.0	S501 CH	PA	DOR	ÇG	16	2.0
22 615 22 615	5U	10%	CG	36	1.0	HS 1023	PA	DOP	ÇG	52	4.0
55 913	80	10N	CG	34	4.0	NS 1024	PA Pa	006	cc	62	9.0
55 914	80	10N	55	33	ø.0	NS 1025 NS 1026	PA	008 008	CG CG	44	10.0 10.0
55 915	60 60	10N	CG CG	34 24	2.0 1.0	NS 1027	PA	pos	CG	30	4.0
55 916 55 917	80	10 M	CG	24	1.0	NS 1028	PA	DOB	ÇG	50	1.0
55 91 <b>8</b>	80	10M	CG	42	1.0	HS 1029	PA	008	CG	25	6.0
22 616	80	10N	ÇĿ	65	34.0	MS 1030 MS 1031	PA PA	006	Ct.	45	<b>6.0</b>
22 650	50	10M	C.C	32	15.0	MS 1031	PA	DOS DOS	CG	49 116	5.0 24D.0
22 451 22 451	80 80	10N 10H	CG	46 38	' 2.0 1.0	NS 1033	PA	008	čĠ	15	11.0
55 923	BO	013	CG	*8	19.0	NS 1034	PA	DO 5	CG	40	4.0
55 924	θÜ	D13	ÇĞ	>2	80.0	NS 1035	PA	005	CG	47	2.0
55 925	60	013	CC	57	76.0	NS 1036	PA	D05	CG	48	3.0

ND	AREA	LINE	ROCA	ZN	A5	NO	AREA	LINE	AUCA	ZN	AS
NS 1242	DQ	228	ÇĢ.	115	20.6	HS 1344	61	034	(A	81	8.0
NS 1243	٥L	D16	CG	36	1.0	NS 1345	61	D36	GR	30	• • 0
NS 1244 NS 1245	OL OL	D16	CG CG	21 18	4.0 3.0	NS 1346 NS 1347	GT GT	036 036	ÇA ÇA	29 38	6.0 13.0
NS 1246	OF OF	018	CG	110	19.0	NS 1348	61	D36	ÇR	47	15.0
NS 1247	DŁ	D18	CG	27	70.0	HS 1349	GT	936	GR	44	37.0
MS 1248	DL	018	CG	68	1.0	NS 1350	GT	036	GH	36	7.G
NS 1249 NS 1250	DL DL	01s 01s	CG CG	77 49	5.0 21.6	NS 1351	GT GT	D3 6	GH GH	34 27	11.0 6.6
45 1251	DL	Die	Cu	53	15.0	NS 1353	ų į	036	5	34	19.0
NS 1252	υĹ	ula	CG	295	200 at	NS 1354	b ī	U36	GR	24	8.6
NS 1253	UL	U1 6	Cie	20	10.6	NS 1355	GT	036	GR	30	6.0
NS 1254 NS 1255	DL DL	018 D16	ÇG	61 ((	25.C 5.L	NS 1356 NS 1357	67 67	U36	Ca	29 335	800.C
NS 1256	DL	010	CG	41	2.0	NS 1350	Ģī	036	ÇA	73	20.0
NS 1257	DĽ	078	CG	47	11.0	HS 1359	GT	D34	GR	57	4.0
N5 1250	OL.	010	CU	51	6.0	H3 1360	GT	034	LA	67	16.3
N\$ 1259 N\$ 1260	OL OL	D18 D18	CG CG	50 67	10.0	NS 1361 NS 1362	61 61	D36	GA GA	34 21	17.0 9.0
MS 1261	DL	Dia	CG	73	18.0	NS 1363	61	DAP	GR	28	9.0
MS 1262	DL	Dla	55	56	14.0	NS 1364	GT	D36	ĢR	132	60.0
NS 1263	DL	018 D18	CG CG	70 83	320.0 25.0	NS 1365 NS 1366	GT GT	D36	GR GR	99 47	50.0 20.0
NS 1264 NS 1265	DL DL	016	ÇG	74	215.0	NS 1366 NS 1367	GT	D36	GR.	37	15.0
N5 1266	DL	D16	CG	54	4.0	NS 1368	ĢT	D34	GR	26	9.0
MS 1267	DL	016	CG	60	5.0	NS 1369	ωŢ	034	GR	22	6.0
NS 1268 NS 1269	DL DL	018 018	CG	26 49	6.0 6.0	NS 1370 NS 1371	GT GT	D34 D34	GR GR	24 28	5.0 6.0
NS 1270	DL	018	ÇG	47	7.0	NS 1371	GT	034	GR	61	13.0
NS 1271	DL	D18	CG	46	2.0	NS 1373	GT	D34	GR	101	30.0
NS 1272	OL.	018	CG	20 45	5.0 3.0	NS 1374	61	034	GR	61	44.0
NS 1273 NS 1274	OL OL	D18 D18	CG CG	51	2.0	NS 1375 NS 1376	GT GT	D34 D34	GR GR	110 39	12.0 14.0
NS 1275	MA	F06	Cu	44	2.0	NS 1376	GT	034	GR	30	14.0
NS 1276	MA	F06	ÇG	76	2.0	NS 1378	GT	034	CR.	223	500.0
NS 1277	HA	F06	CG	37 47	1.0 3.0	NS 1379	GŤ	034	Ğĸ	125	200.0
NS 1278 NS 1279	AH Am	FO6 FO6	CG CG	29	2.0	NS 1381 NS 1362	6T 61	034 034	GH GH	73 75	38.0 38.0
NS 1280	MA	F06	CG	38	5.0	NS 1383	ĢŤ	034	GH	29	6.0
MS 1261	MA	F06	CC	50	3.0	NS 1384	GT	D34	<b>L</b> AR	31	8.G
M2 1585	AN.	F06	Cu	64 26	3.0 2.0	NS 1385	GT.	U34	LMI.	33	9.0 50.6
NS 1283 NS 1284	MA AM	F06 F06	CG CG	35	3.0	NS 1386	10 10	D34 D34	CR CR	39 195	2000.0
NS 1285	MA	F06	Ċ.	44	55.0	NS 1386	6T	<b>D34</b>	GH	76	170-0
NS 1286	MA	FD6	CG	36	7.0	NS 1389	GT	D34	GH	47	25 6
NS 1287	MA	F06 F06	CG CG	54 40	5.0 10.0	NS 1390	6T	D34 D34	GH GH	32 38	6 C
NS 1288 NS 1289	MA Ma	F06	CG	55	26.0	NS 1391 NS 1393	G T G T	D34	(ju) (ju)	25	9.C
NS 1290	AN	FD6	CG	31	7.0	NS 1394	GT	D34	1.61	33	5 .C
NS 1291	MA	FOb	CG	14	0.1	NS 1395	6T	D34	1	28	6.0
NS 1292	AM AM	F06 F06	CG	37 50	5.0 6.0	NS 1396 NS 1397	61 61	D34 D34	GR GH	46 32	5.0 0.6
NS 1293 NS 1294	MA	F06	CG	30	5.0	NS 1397	GT	03+	GA GA	32 28	5.0
NS 1295	MA	FOb	CG	47	4.0	NS 1399	ψĪ	D3 4	Gk	24	16.0
MS 1296	MA	FO6	CG	52	5.0	NS 1400	G I	D34	Gĸ	34	5.0
NS 1297	MA MA	FO6 FO6	CG Cu	36 30	4.0 4.0	NS 1401 NS 1402	GT GT	D34 D34	GH GH	27 41	15.0
NS 1298 NS 1299	MA	F06	ÇĞ	25	5.0	NS 1402	61 61	U34	LM LM	37	12.6
NS 1300	HA	FD6	ĊĠ	25	J.0	NS 1465	ųΓ	035	GR	11	10.0
NS 1301	AM.	FOA	C.C	24	3-0	NS 1406	GŦ	Läz	6×	23	16,6
N5 1302 N5 1363	MA MA	F06 F06	CC CC	39 47	2.6 3.6	NS 1407	51 61	032 032	u# Gk	31 44	7.C
NS 1303	MA	FUE	Č	28	3.0	NS 1404	Ğ1	032	G#	24	14.0
45 1305	MA	FO <sub>b</sub>	Ĉu	33	7.0	N5 1410	GT	0.75	•	+1	h.l
Nº 1306	MA	4U4	Cu	<i>23</i>	4.C	NS 1411	٥ľ	035	(m	43	17.0
NS 1307	MA	FQ6 FQ6	CG CG	41 37	4.0	MS 1412 MS 1413	61 61	035	ÇA CA	43 45	7.0 13.0
MS 1308 MS 1309	MA MA	FOS	CG	18	4.0	#5 1413   NS 1414	GT GT	735	GH.	33	8.0
MS 1310	AM	FOB	CG	18	1.0	HS 1415	67	D3 2	GR	70	35.0
NS 1311	AM	F06	ÇĞ	42 35	4.0 4.0	NS 1416	GT	D3.5	GR CH	127	20.0 46.0
NS 1312 NS 1313	AN An	FO.6 FO.6	CG	10	4.0	NS 1423	GT GT	D35	GR GR	131 31	9.0
NS 1313	NA NA	F06	26	27	1.0	NS 1424	GT	035	GR.	34	9.0
NS 1315	MA	F06	CG	33	4.0	HS 1425	ĞŤ	035	GR	73	2.0
MS 1316	DL	F07	CG CG	40 51	2.0 9.0	NS 1426	61	250	GH GR	31 29	5.0 6.0
MS 1317 MS 1318	DL DL	F07 F07	CC	59	960.0	NS 1427 NS 1428	GT GT	D32	GR	31	8.0
NS 1319	DL	F07	CG	11	5.0	NS 1429	GT	035	GN	43	5.0
MS 1320	OL	FQ7	CG	17	5.0	NS 1430	GT	D30	GR	17	6.0
NS 1321	DL	F07	CG CG	68 33	6.0 4.0	NS 1431	GT	030	GR GR	33	a.0 3.0
HS 1322 HS 1323	DL DL	F07 F07	CG	33	3.0	MS 1432 MS 1433	GT GT	D30 D30	GR	67 63	5.0
NS 1324	DL DL	F07	CG	46	8.0	NS 1436	61	D30	GR	50	13.0
NS 1325	DL	F07	CG	26	6.0	NS 1437	GT	030	GR	48	10.0
NS 1326	DL	F07	CG	30 20	4.0	H5 1430	GT	030	GR	54 41	35.0
NS 1327 NS 1328	DL DL	F07 F07	CG CG	44	28.0	H5 1439 H5 1440	GT GT	030 030	GH:	57	12.0
N2 1329	OL.	F07	CG	29	3.0	NS 1441	GT	030	CH	43	13.0
NS 1330	OL	F07	C.	37	3.0	HS 1442	ĢĪ	D30	جي	46	5.0
MS 1331	DL	F07	CC.	46 17	4.D 17.0	N\$ 1443	GT	030	GR CR	45	0. b
MS 1332	UL UL	FQ7 F07	CG CG	21	4.0	NS 1444	GT GT	D30	CH CH	60 39	20.0
NS 1333 NS 1334	בונ בונ	Fls	CG	39	2.0	NS 1445 NS 1446	61	D20	Gd	16	6 .O
45 1335	ĢŤ	D36	G#	25	10.0	NS 1447	61	D30	GH	16	+.0
NS 1336	61	036	GH CB	33	0.0	NS 1448	ĢĪ	030	ÇA.	65	6.0
NS 1337 NS 1338	uT GT	D36 D36	ÇJA ÇJA	114 43	9.0	NS 1449 NS 1450	GT GT	D3 0	يامن يائي	46 39	8.0
NS 1339	ĞT	D36	ĢA	78	21.0	NS 1450	GT	030	GR	49	14.0
MS 1340	GŤ	D36	C-M	2>8	110.6	NS 1452	GŦ	D30	GR	76	5.0
NS 1341	GT	D36	GK	310	0.00 0.50	NS 1453	GT	030	GH	59	14.0
NS 1342 NS 1343	GT GT	036 036	G4 G4	58 74	26.0	NS 1454 NS 1455	61 61	D3 C D3 O	GH GH	43 91	1.0
77.2.27.3	Ψ,					1 112 4433	<b>~</b> ,				

10   10   10   10   10   10   10   10	HO	AREA	LIME	ROCK	ZN	A5	NO.	AREA	LINE	ROCK	2.4	AS
	NS 1456			("A			RS 1568		006	CG	41	16.0
	NS 1459											
1,140						340						2.0
10						4.0						0.1
		147										
1,		4.7						DA	006			
1												
1				<b>3</b> 11								
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,		GT	FOb	24	26	16.0						2.0
10   142	NS 1477	41	FOS	2H	9		RS 1503	PA	DOs	EG	125	144.0
15   143	NS 1478	ĢŦ	FOE	54			RS 1584	PA	D0 6	ÇG	69	
15   140							RS 1585					
15   1435   CT								PA				
15   165								PA				1.0
10   10   10   10   10   10   10   10										20		3.0
15   168												
10   10   10   10   10   10   10   10												0.1
15   100						5.0						
10   10   10   10   10   10   10   10												
No   1479   CT					69							
15   1479   CT		GT	F10	244	74	3.0						1.6
15 1499 CT F10 CG 32 4.0		61										
No   1494   CT	NS 1495						RS 1597	PA	LOB	C.	4.6	1.1
S   1000   PA	HP TAAP								AGL			
	NS 1497	G1	F10	CL	25	5.0						
RS   1902   PA												
AS   1500   PA												
\$\$ 1902 PA	AS 1501											
\$5 1500 PA	AS 1502	PA	DO 6	CG	23	5 *0						
\$3 1904 PA	RS 1503											1.0
ST   1508   PA												1.0
Section   Pack   Dock   CC   122						2.0		PA				
Section						1.0		PA				
83 1500 PA 006 CG 51 10 0.1 AS 1610 PA 006 CG 21 1.0 AS 1511 PA 006 CG 21 1.0 AS 1511 PA 006 CG 51 1.0 AS 1511 PA 006 CG 51 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 22 T 1.0 AS 1511 PA 006 CG 23 T 1.0 AS 1511 PA 006 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 AS 1511 PA 001 CG 25 T 1.0 A											49	0.1
## ## ## ## ## ## ## ## ## ## ## ## ##										CG		1.0
## ## ## ## ## ## ## ## ## ## ## ## ##	K2 1204	PA					RS 1611					
1515   PA												0.1
15   15   15   15   15   15   15   15												1.0
S   1514												
S   1315												
S						4.0		PA				
## 1517 PA DOS CG 32		PA	DQ&	Cu		3.0						
No.   1518   PA	AS 1517											
## ## ## ## ## ## ## ## ## ## ## ## ##	KS 1518											
45 1520 PA DOS CC 42 C-1 R5 1622 PA DOS CC 23 D-1 R5 1522 PA DOS CC 23 D-1 R5 1522 PA DOS CC 33 4-0 R5 1623 PA DOS CC 33 D-1 R5 1522 PA DOS CC 33 D-1 R5 1524 PA DOS CC 33 D-1 R5 1524 PA DOS CC 33 D-1 R5 1524 PA DOS CC 34 C-1 R5 1625 PA DOS CC 35 D-1 R5 1524 PA DOS CC 34 C-1 R5 1626 PA DOS CC 35 D-1 R5 1527 PA DOS CC 34 C-1 R5 1626 PA DOS CC 35 D-1 R5 1527 PA DOS CC 34 C-1 R5 1626 PA DOS CC 35 D-1 R5 1527 PA DOS CC 34 C-1 R5 1626 PA DOS CC 37 U-1 R5 1527 PA DOS CC 34 C-1 R5 1626 PA DOS CC 37 U-1 R5 1527 PA DOS CC 38 L-2 R5 1527 PA DOS CC 38 L-2 R5 1527 PA DOS CC 38 L-2 R5 1527 PA DOS CC 38 L-2 R5 1527 PA DOS CC 37 U-1 R5 1527 PA DOS CC 37 U-1 R5 1527 PA DOS CC 37 U-1 R5 1527 PA DOS CC 37 U-1 R5 1531 PA DOS CC 35 D-1 R5 1531 PA DOS CC 35												
\$\$ 1521 PA 006 CG 13 4.0 R\$ 1623 PA 001 CG 23 0.1 R\$ 1523 PA 001 CG 31 0.1 R\$ 1523 PA 006 CG 33 1.0 R\$ 1523 PA 006 CG 34 0.0 R\$ 1523 PA 006 CG 34 0.0 R\$ 1523 PA 007 CG 31 0.1 R\$ 1523 PA 007 CG 31 0.1 R\$ 1523 PA 007 CG 31 0.1 R\$ 1523 PA 007 CG 31 0.1 R\$ 1523 PA 007 CG 31 0.1 R\$ 1524 PA 007 CG 31 0.1 R\$ 1525 PA 007 CG 31 0.1 R\$ 1526 PA 007 CG 31 0.1 R\$ 1526 PA 007 CG 32 0.1 R\$ 1527 PA 007 CG 32												
RS   1522    PA								PA				
No.   1242   PA								PA		CG		
R5   1225   PA						2.0					31	
RS   1527   PA   DOB   CG   43   DOI   RS   1629   PA   DOI   CG   29   U.1												
85 1527 PA						0-1						
## 1920 PA 006 CG 28 1.0 R\$ 1630 PA 001 CG 33 0.1 R\$ 1831 PA 001 CG 31 0.1 R\$ 1831 PA 001 CG 32 1.0 R\$ 1831 PA 001 CG 32 1.0 R\$ 1831 PA 001 CG 32 1.0 R\$ 1831 PA 001 CG 32 1.0 R\$ 1831 PA 001 CG 32 1.0 R\$ 1831 PA 001 CG 32 1.0 R\$ 1831 PA 001 CG 32 1.0 R\$ 1831 PA 001 CG 32 3.0 R\$ 1831 PA 001 CG 38 1.0 R\$ 1833 PA 001 CG 38 1.0 R\$ 1833 PA 001 CG 38 1.0 R\$ 1833 PA 001 CG 38 1.0 R\$ 1833 PA 001 CG 38 1.0 R\$ 1833 PA 001 CG 38 1.0 R\$ 1833 PA 001 CG 38 1.0 R\$ 1833 PA 001 CG 38 1.0 R\$ 1833 PA 001 CG 38 1.0 R\$ 1833 PA 001 CG 38 1.0 R\$ 1833 PA 001 CG 38 1.0 R\$ 1833 PA 001 CG 38 1.0 R\$ 1833 PA 001 CG 40 1.0 R\$ 1831 PA 001 CG 40 1.0 R\$ 1831 PA 001 CG 40 1.0 R\$ 1831 PA 001 CG 40 1.0 R\$ 1831 PA 001 CG 40 1.0 R\$ 1831 PA 001 CG 40 1.0 R\$ 1831 PA 001 CG 40 1.0 R\$ 1831 PA 001 CG 40 1.0 R\$ 1831 PA 001 CG 40 0.1 R\$ 1831 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 001 CG 40 PA 0												
#\$ 1532												
R5 1330  PA												0.1
R5   1331   PA	RS 1530					0.1						
R5   1332   PA	R5 1531		D0 to									
No   1333	42 1235							PA				
RS 1535 PA DOB CC 23 3-0 RS 1636 PA DO1 CG 56 1.0 RS 1535 PA DO6 CG 37 7.6 RS 1637 PA DO1 CG 40 1.0 RS 1537 PA DO6 CG 37 7.6 RS 1638 PA DO1 CG 44 0.1 RS 1537 PA DO6 CG 50 3-0 RS 1639 PA DO1 CG 44 0.1 RS 1537 PA DO6 CG 52 6.0 RS 1639 PA DO1 CG 44 0.1 RS 1538 PA DO6 CG 53 13.6 RS 1640 PA DO1 CG 24 0.1 RS 1536 PA DO6 CG 53 13.6 RS 1640 PA DO1 CG 24 0.1 RS 1540 PA DO6 CG 43 6.0 RS 1641 PA DO1 CG 24 0.1 RS 1540 PA DO6 CG 43 6.0 RS 1641 PA DO1 CG 34 0.1 RS 1540 PA DO6 CG 43 6.0 RS 1644 PA DO1 CG 35 4.0 RS 1540 PA DO6 CG 47 9.6 RS 1644 PA DVW CG 22 4.0 RS 1540 PA DO6 CG 44 4.6 RS 1644 PA DVW CG 22 4.0 RS 1540 PA DO6 CG 44 3.6 RS 1644 PA DVW CG 22 4.0 RS 1540 PA DO6 CG 47 3.6 RS 1644 PA DVW CG 22 4.0 RS 1540 PA DO6 CG 47 3.6 RS 1644 PA DVW CG 11 J.0 RS 1540 PA DO6 CG 47 3.6 RS 1645 PA DVW CG 11 J.0 RS 1540 PA DO6 CG 47 3.6 RS 1647 PA DVW CG 11 J.0 RS 1540 PA DO6 CG 47 3.6 RS 1647 PA DVW CG 11 J.0 RS 1540 PA DO6 CG 47 3.6 RS 1647 PA DVW CG 11 J.0 RS 1540 PA DO6 CG 27 17.6 RS 1647 PA DVW CG 12 20 U.1 RS 1550 PA DO6 CG 31 11.0 RS 1650 PA DVW CG 12 20 U.1 RS 1550 PA DO6 CG 31 11.0 RS 1651 PA DVW CG 25 2.0 RS 1555 PA DO6 CG 31 11.0 RS 1655 PA DVW CG 25 2.0 RS 1555 PA DO6 CG 31 11.0 RS 1657 PA DVW CG 26 26 D.1 RS 1555 PA DO6 CG 34 48.0 RS 1657 PA DVW CG 26 26 D.1 RS 1555 PA DO6 CG 34 10.0 RS 1657 PA DVW CG 26 26 D.1 RS 1555 PA DO6 CG 48 3.0 RS 1657 PA DVW CG 26 26 D.1 RS 1555 PA DO6 CG 48 3.0 RS 1657 PA DVW CG 26 26 D.1 RS 1555 PA DO6 CG 48 3.0 RS 1657 PA DVW CG 26 26 D.1 RS 1555 PA DO6 CG 48 3.0 RS 1657 PA DVW CG 26 27 D.1 RS 1555 PA DO6 CG 48 3.0 RS 1657 PA DVW CG 26 27 D.1 RS 1558 PA DO6 CG 48 3.0 RS 1657 PA DVW CG 26 27 D.1 RS 1558 PA DO6 CG 48 3.0 RS 1657 PA DVW CG 26 27 D.1 RS 1558 PA DO6 CG 48 3.0 RS 1657 PA DVW CG 26 26 D.1 RS 1558 PA DO6 CG 48 3.0 RS 1657 PA DVW CG 26 26 D.1 RS 1558 PA DO6 CG 48 3.0 RS 1657 PA DVW CG 26 26 D.1 RS 1558 PA DO6 CG 48 3.0 RS 1657 PA DVW CG 26 26 D.1 RS 1558 PA DO6 CG 48 3.0 RS 1657 PA DVW CG 26 33 3.0 RS 1560 PA DO6 CG 48 3.0 RS 1666 PA DVW CG 26 33 3.0 RS 1560 PA DO6 CG 48 3.0 RS 1666	K5 1533											
RS 1535 PA 006 CG 37 7.6 RS 1637 PA 001 CG 40 0.1 RS 1537 PA 006 CG 37 7.6 RS 1638 PA 001 CG 47 0.1 RS 1538 PA 006 CG 42 6.0 RS 1638 PA 001 CG 44 0.1 RS 1538 PA 006 CG 42 6.0 RS 1640 PA 001 CG 21 0.1 RS 1540 PA 006 CG 42 6.0 RS 1640 PA 001 CG 21 0.1 RS 1540 PA 006 CG 43 6.0 RS 1641 PA 001 CG 34 0.1 RS 1540 PA 006 CG 43 6.0 RS 1641 PA 001 CG 36 0.1 RS 1540 PA 006 CG 43 6.0 RS 1641 PA 001 CG 46 0.1 RS 1541 PA 006 CG 47 9.6 RS 1642 PA 007 CG 22 4.0 RS 1553 PA 006 CG 47 9.6 RS 1644 PA 07 CG 22 4.0 RS 1554 PA 006 CG 47 9.6 RS 1645 PA 07 CG 22 4.0 RS 1555 PA 006 CG 47 9.6 RS 1646 PA 07 CG 15 5.0 RS 1544 PA 006 CG 44 4.6 RS 1645 PA 07 CG 18 2.0 RS 1544 PA 006 CG 44 4.6 RS 1645 PA 07 CG 18 2.0 RS 1544 PA 006 CG 47 9.6 RS 1645 PA 07 CG 18 2.0 RS 1544 PA 006 CG 42 4.0 RS 1645 PA 07 CG 18 2.0 RS 1544 PA 006 CG 42 4.0 RS 1645 PA 07 CG 18 2.0 RS 1544 PA 006 CG 42 4.0 RS 1645 PA 07 CG 18 2.0 RS 1544 PA 006 CG 42 4.0 RS 1645 PA 07 CG 18 2.0 RS 1544 PA 006 CG 47 1.1 RS 1645 PA 07 CG 18 2.0 RS 1544 PA 006 CG 44 A.1 RS 1649 PA 07 CG 18 2.0 RS 1544 PA 006 CG 44 A.1 RS 1649 PA 07 CG 18 2.0 RS 1544 PA 006 CG 44 A.1 RS 1649 PA 07 CG 18 2.0 RS 1544 PA 006 CG 44 A.1 RS 1649 PA 07 CG 44 C.2 RS 1544 PA 07 CG 44 C												
RS 15350 PA 006 CG 50 3.0 RS 1638 PA 001 CG 47 0.1 RS 1537 PA 006 CG 50 3.0 RS 1638 PA 001 CG 44 0.1 RS 1538 PA 006 CG 50 3.0 RS 1640 PA 001 CG 44 0.1 RS 1530 PA 006 CG 53 13.0 RS 1640 PA 001 CG 21 0.1 RS 1540 PA 006 CG 43 6.0 RS 1641 PA 001 CG 34 0.1 RS 1540 PA 006 CG 43 6.0 RS 1642 PA 001 CG 46 0.1 RS 1541 PA 006 CG 39 B.0 RS 1643 PA 09W CG 35 4.0 RS 1544 PA 006 CG 39 B.0 RS 1644 PA 09W CG 35 4.0 RS 1544 PA 006 CG 44 4.1 RS 1645 PA 09W CG 15 5.0 RS 1544 PA 006 CG 44 4.1 RS 1645 PA 09W CG 11 J.0 RS 1545 PA 006 CG 44 4.1 RS 1645 PA 09W CG 11 J.0 RS 1545 PA 006 CG 44 3.0 RS 1647 PA 09W CG 11 J.0 RS 1545 PA 006 CG 44 3.0 RS 1645 PA 09W CG 11 J.0 RS 1546 PA 006 CG 44 5.1 RS 1645 PA 09W CG 11 J.0 RS 1546 PA 006 CG 44 5.1 RS 1645 PA 09W CG 12 A.0 RS 1546 PA 006 CG 44 5.1 RS 1645 PA 09W CG 12 A.0 RS 1546 PA 006 CG 44 5.1 RS 1645 PA 09W CG 12 A.0 RS 1546 PA 006 CG 44 5.1 RS 1649 PA 09W CG 24 2.0 RS 1546 PA 006 CG 45 BB-1 RS 1649 PA 09W CG 24 2.0 RS 1557 PA 006 CG 38 BB-1 RS 1651 PA 09W CG 25 A.0 RS 1551 PA 006 CG 38 BB-1 RS 1651 PA 09W CG 25 A.0 RS 1555 PA 006 CG 38 BB-1 RS 1652 PA 09W CG 26 A.0 RS 1555 PA 006 CG 38 A8.0 RS 1655 PA 09W CG 26 A.0 RS 1556 PA 006 CG 44 3.0 RS 1659 PA 09W CG 26 A.0 RS 1557 PA 006 CG 44 3.0 RS 1659 PA 09W CG 26 A.0 RS 1558 PA 006 CG 44 3.0 RS 1659 PA 09W CG 6.2 A.0 RS 1557 PA 006 CG 44 3.0 RS 1659 PA 09W CG 6.2 A.0 RS 1558 PA 006 CG 46 3.0 RS 1659 PA 09W CG 6.2 A.0 RS 1557 PA 006 CG 46 3.0 RS 1659 PA 09W CG 6.2 A.0 RS 1558 PA 006 CG 46 3.0 RS 1659 PA 09W CG 6.3 A.0 RS 1558 PA 006 CG 46 3.0 RS 1666 PA 09W CG 6.3 A.0 RS 1558 PA 006 CG 48 3.0 RS 1666 PA 09W CG 6.3 A.0 RS 1566 PA 006 CG 68 A.0 A.0 RS 1666 PA 09W CG 6.3 A.0 RS 1566 PA 006 CG 68 A.0 A.0 RS 1666 PA 09W CG 6.3 A.0 RS 1566 PA 006 CG 68 A.0 A.0 RS 1666 PA 09W CG 6.3 A.0 RS 1566 PA 006 CG 68 A.0 A.0 RS 1666 PA 09W CG 6.3 A.0 RS 1566 PA 006 CG 68 B.0 RS 1666 PA 09W CG 6.3 A.0 RS 1566 PA 006 CG 68 B.0 RS 1666 PA 09W CG 6.3 A.0 RS 1566 PA 006 CG 68 B.0 RS 1666 PA 09W CG 6.3 A.0 RS 1566 PA 006 CG 68 B.0 RS 1666 PA 09W CG 6.3 A.0								PA	DO 1	CG	40	1.0
#\$ 1338 PA 006 CG 42 6.0 R\$ 1640 PA 001 CG 44 0.1 #\$ 1338 PA 006 CG 42 6.0 R\$ 1640 PA 001 CG 34 0.1 #\$ 1340 PA 006 CG 43 6.0 R\$ 1641 PA 001 CG 34 0.1 #\$ 1540 PA 006 CG 43 6.0 R\$ 1642 PA 001 CG 36 0.1 #\$ 1540 PA 006 CG 39 b.0 R\$ 1642 PA 001 CG 36 0.1 #\$ 1540 PA 006 CG 39 b.0 R\$ 1644 PA 07W CG 22 4.0 #\$ 1540 PA 006 CG 47 9.6 R\$ 1644 PA 07W CG 22 4.0 #\$ 1544 PA 006 CG 47 9.6 R\$ 1645 PA 07W CG 22 4.0 #\$ 1544 PA 006 CG 44 4.6 R\$ 1645 PA 07W CG 15 5.0 #\$ 1544 PA 006 CG 44 4.6 R\$ 1645 PA 07W CG 15 5.0 #\$ 1546 PA 006 CG 20 4.6 R\$ 1646 PA 07W CG 16 15 5.0 #\$ 1546 PA 006 CG 27 17.6 R\$ 1648 PA 07W CG 18 2.0 #\$ 1546 PA 006 CG 27 17.6 R\$ 1648 PA 07W CG 18 2.0 #\$ 1546 PA 006 CG 27 17.6 R\$ 1648 PA 07W CG 18 2.0 #\$ 1546 PA 006 CG 27 17.6 R\$ 1648 PA 07W CG 18 2.0 #\$ 1546 PA 006 CG 27 17.6 R\$ 1648 PA 07W CG 18 2.0 #\$ 1546 PA 006 CG 27 17.6 R\$ 1648 PA 07W CG 18 2.0 #\$ 1546 PA 006 CG 27 17.6 R\$ 1648 PA 07W CG 18 2.0 #\$ 1546 PA 006 CG 27 17.6 R\$ 1648 PA 07W CG 18 2.0 #\$ 1546 PA 006 CG 27 17.6 R\$ 1648 PA 07W CG 26 26 0.1 #\$ 1546 PA 006 CG 31 11.6 R\$ 1652 PA 07W CG 26 26 0.1 #\$ 1550 PA 006 CG 31 11.0 R\$ 1652 PA 07W CG 26 25 2.0 #\$ 1550 PA 006 CG 31 11.0 R\$ 1655 PA 07W CG 26 25 2.0 #\$ 1554 PA 006 CG 31 11.0 R\$ 1655 PA 07W CG 26 25 2.0 #\$ 1555 PA 006 CG 54 24.0 R\$ 1657 PA 07W CG 26 26 0.1 #\$ 1555 PA 006 CG 54 24.0 R\$ 1657 PA 07W CG 26 26 0.1 #\$ 1555 PA 006 CG 46 3.0 R\$ 1657 PA 07W CG 26 27 1.0 #\$ 1555 PA 006 CG 46 3.0 R\$ 1659 PA 07W CG 36 1.0 #\$ 1555 PA 006 CG 46 3.0 R\$ 1659 PA 07W CG 36 1.0 #\$ 1555 PA 006 CG 46 3.0 R\$ 1659 PA 07W CG 37 1.0 #\$ 1556 PA 006 CG 46 2.0 R\$ 1660 PA 07W CG 27 1.0 #\$ 1566 PA 006 CG 47 11.0 #\$ 1566 PA 00W CG 27 1.0 #\$ 1566 PA 00W CG 33 A.0							RS 1638		001			
#3 1330 PA							RS 1639					
## 1540 PA 006 CG 43 6.0 ## 1504 PA 001 CG 46 0.1  ## 1540 PA 006 CG 39 8.0 ## 1504 PA 004 CG 35 4.0  ## 1540 PA 006 CG 39 8.0 ## 1504 PA 004 CG 35 4.0  ## 1540 PA 006 CG 47 9.0 ## 1504 PA 004 CG 15 5.0  ## 1540 PA 006 CG 44 4.0 ## 1504 PA 004 CG 15 5.0  ## 1540 PA 006 CG 44 4.0 ## 1504 PA 004 CG 15 5.0  ## 1540 PA 006 CG 44 3.0 ## 1504 PA 004 CG 16 2.0  ## 1540 PA 006 CG 44 3.0 ## 1504 PA 004 CG 18 2.0  ## 1540 PA 006 CG 44 3.0 ## 1504 PA 004 CG 18 2.0  ## 1540 PA 006 CG 47 17.0 ## 1504 PA 004 CC 10 10 3.0  ## 1540 PA 006 CG 27 17.0 ## 1504 PA 004 CC 20 0.1  ## 1540 PA 006 CG 37 ## 1504 PA 004 CC 20 0.1  ## 1550 PA 006 CG 78 48.0  ## 1551 PA 006 CG 31 10.0 ## 1651 PA 004 CG 24 5.0  ## 1552 PA 006 CG 31 10.0 ## 1652 PA 004 CG 25 2.0  ## 1555 PA 006 CG 31 10.0 ## 1653 PA 004 CG 26 25 2.0  ## 1555 PA 006 CG 31 10.0 ## 1653 PA 004 CG 26 26 0.1  ## 1555 PA 006 CG 34 24.0 ## 1655 PA 004 CG 26 26 0.1  ## 1555 PA 006 CG 34 24.0 ## 1650 PA 004 CG 26 26 0.1  ## 1555 PA 006 CG 34 24.0 ## 1650 PA 004 CG 26 0.1  ## 1555 PA 006 CG 34 24.0 ## 1650 PA 004 CG 26 0.1  ## 1555 PA 006 CG 34 24.0 ## 1650 PA 004 CG 26 0.1  ## 1555 PA 006 CG 34 3.0 ## 1650 PA 004 CG 26 0.1  ## 1555 PA 006 CG 34 3.0 ## 1650 PA 004 CG 26 0.1  ## 1556 PA 006 CG 46 3.0 ## 1660 PA 004 CG 26 0.1  ## 1556 PA 006 CG 46 3.0 ## 1660 PA 004 CG 27 11.0  ## 1556 PA 006 CG 46 3.0 ## 1660 PA 004 CG 27 11.0  ## 1560 PA 006 CG 46 2.0 ## 1660 PA 004 CG 27 11.0  ## 1560 PA 006 CG 46 2.0 ## 1660 PA 004 CG 27 11.0  ## 1560 PA 006 CG 46 2.0 ## 1660 PA 004 CG 27 11.0  ## 1560 PA 006 CG 48 2.0 ## 1660 PA 004 CG 25 3.0  ## 1560 PA 006 CG 48 2.0 ## 1660 PA 004 CG 25 3.0  ## 1560 PA 006 CG 48 2.0 ## 1660 PA 004 CG 25 3.0  ## 1560 PA 006 CG 48 2.0 ## 1660 PA 004 CG 25 3.0  ## 1560 PA 006 CG 48 2.0  ## 1560 PA 006 CG 48 2.							R\$ 1640					
#\$ 15-1 PA												
## 154-C PA 006 CG 39 B.D ## 151644 PA 00W CG 22 A.U ## 154-S PA 006 CG 47 9.C ## 164-S PA 00W CG 15 5.0 ## 154-S PA 006 CG 44 4.C ## 164-S PA 00W CG 15 5.0 ## 154-S PA 006 CG 20 4.C ## 165-S PA 00W CG 18 2.0 ## 154-S PA 006 CG 24 3.L ## 154-S PA 00W CG 18 2.0 ## 154-S PA 006 CG 24 3.L ## 154-S PA 00W CG 18 2.0 ## 154-S PA 006 CG 27 17.L ## 154-S PA 00W CG 14 3.0 ## 154-S PA 006 CG 27 17.L ## 154-S PA 00W CG 20 U.1 ## 154-S PA 006 CG 27 17.L ## 154-S PA 00W CG 20 U.1 ## 155-S PA 006 CG 78 48.0 ## 165-S PA 00W CG 24 3.L ## 155-S PA 006 CG 31 10.0 ## 155-S PA 006 CG 31 10.0 ## 155-S PA 006 CG 31 10.0 ## 155-S PA 006 CG 34 24.0 ## 155-S PA 006 CG 34 25.0 ## 155-S PA 006 CG 35 3.0 ## 155-S PA 006 CG 36 3.0 ## 155-S PA 006 CG	#5 15e1									ce		
R\$ 15-3 PA	A5 1542					6.0				CG		
## 1544 PA	RS 1543									-		7.4
#\$ 1505 PA	RS 1544		004	CG	44	4.6			046	C.C.		
HS 1547 PA	95 1595	PA	106	EG		4.0	73 1040 06 1447			E6		3.0
HS 1547 PA	45 1546	PA	006	CC	24	3.6						1.0
No. 1540 PA DOB CL 57 13.C NS 1050 PA DVW CL 25 1.0 D.1 NS 1550 PA DVW CL 25 1.0 D.1 NS 1550 PA DOB CL 34 2.1 NS 1651 PA DVW CL 14 2.1 NS 1551 PA DVW CL 14 2.1 NS 1551 PA DVW CL 14 2.1 NS 1551 PA DVW CL 14 2.1 NS 1552 PA DVW CL 15 2.0 NS 1552 PA DVW CL 15 2.0 NS 1552 PA DVW CL 15 2.0 NS 1555 PA DVW CL 15 2.0 NS 1554 PA DVW CL 15 2.0 NS 1554 PA DVW CL 15 2.0 NS 1554 PA DVW CL 15 2.0 NS 1555 PA	NS 1547		400	CC	27		42 1940			ČL		4.0
#\$ 1549 PA	85 1546					13.0	163 D					
#\$ 1550 PA DO\$ CG 78 48.0 #\$ 1652 PA DO\$ CC 14 2.0 #\$ 1555 PA DO\$ CG 25 2.0 #\$ 1552 PA DO\$ CG 31 10.0 #\$ 1655 PA DO\$ CG 25 2.0 #\$ 1553 PA DO\$ CG 88 100.0 #\$ 1655 PA DO\$ CG 88 1.0 #\$ 1555 PA DO\$ CG 88 1.0 #\$ 1655 PA DO\$ CG 88 1.0 #\$ 1555 PA DO\$ CG 34 48.0 #\$ 1655 PA DO\$ CG 26 D.1 #\$ 1555 PA DO\$ CG 34 48.0 #\$ 1656 PA DO\$ CG 26 D.1 #\$ 1555 PA DO\$ CG 34 48.0 #\$ 1657 PA DO\$ CG 26 D.1 #\$ 1555 PA DO\$ CG 26 3.0 #\$ 1657 PA DO\$ CG 26 D.1 #\$ 1557 PA DO\$ CG 46 3.0 #\$ 1659 PA DO\$ CG 20 1.0 #\$ 1559 PA DO\$ CG 26 D.1 #\$ 1659 PA DO\$ CG 27 D.0 #\$ 1559 PA DO\$ CG 46 3.0 #\$ 1650 PA DO\$ CG 27 D.0 #\$ 1559 PA DO\$ CG 46 3.0 #\$ 1660 PA DO\$ CG 27 D.0 #\$ 1559 PA DO\$ CG 47 11.0 #\$ 1559 PA DO\$ CG 42 7.0 #\$ 1660 PA DO\$ CG 47 11.0 #\$ 1559 PA DO\$ CG 42 7.0 #\$ 1660 PA DO\$ CG 47 11.0 #\$ 1550 PA DO\$ CG 48 230.0 #\$ 1665 PA DO\$ CG 45 3.0 #\$ 1550 PA DO\$ CG 48 230.0 #\$ 1665 PA DO\$ CG 33 3.0 #\$ 1550 PA DO\$ CG 48 230.0 #\$ 1665 PA DO\$ CG 33 3.0 #\$ 1550 PA DO\$ CG 48 230.0 #\$ 1665 PA DO\$ CG 33 3.0 #\$ 1550 PA DO\$ CG 46 230.0 #\$ 1665 PA DO\$ CG 33 3.0 #\$ 1550 PA DO\$ CG 45 2.0 #\$ 110.0 #\$ 1665 PA DO\$ CG 33 3.0 #\$ 1550 PA DO\$ CG 48 230.0 #\$ 1665 PA DO\$ CG 33 3.0 #\$ 1550 PA DO\$ CG 45 2.0 #\$ 110.0 #\$ 1665 PA DO\$ CG 33 3.0 #\$ 1550 PA DO\$ CG 45 2.0 #\$ 110.0 #\$ 1665 PA DO\$ CG 33 3.0 #\$ 1550 PA DO\$ CG 45 2.0 #\$ 110.0 #\$ 1665 PA DO\$ CG 33 3.0 #\$ 1550 PA DO\$ CG 45 2.0 #\$ 110.0 #\$ 1665 PA DO\$ CG 33 4.0 #\$ 1550 PA DO\$ CG 45 2.0 #\$ 110.0 #\$ 1665 PA DO\$ CG 55 3.0 #\$ 1550 PA DO\$ CG 55		PA				150-1	RS 1651					
R\$ 1551 PA 006 CG 78 48.0 R\$ 1653 PA 09W CG 25 2.0 R\$ 1557 PA 006 CG 31 11.0 R\$ 1653 PA 09W CG 68 1.0 R\$ 1555 PA 09W CG 68 1.0 R\$ 1555 PA 09W CG 68 1.0 R\$ 1555 PA 09W CG 68 1.0 R\$ 1555 PA 09W CG 17 1.0 R\$ 1555 PA 09W CG 17 1.0 R\$ 1555 PA 09W CG 17 1.0 R\$ 1556 PA 09W CG 21 17 1.0 R\$ 1556 PA 09W CG 22 1.0 R\$ 1556 PA 09W CG 25 25 1.0 R\$ 1557 PA 006 CG 26 3.0 R\$ 1658 PA 09W CG 20 1.0 R\$ 1558 PA 09W CG 20 1.0 R\$ 1550 PA 09W CG 20 1.0 R\$ 1550 PA 09W CG 27 3.0 R\$ 1550 PA 09W CG 25 3.0 R\$ 1550 PA 09W CG 25 3.0 R\$ 1550 PA 09W CG 25 3.0 R\$ 1550 PA 09W CG 25 3.0 R\$ 1550 PA 09W CG 25 3.0 R\$ 1550 PA 09W CG 25 3.0 R\$ 1550 PA 09W CG 25 3.0 R\$ 1550 PA 09W CG 33 3.0 R\$ 1550 PA 09							45 1652					
RS 1852 PA ODA CG 81 100.0 RS 1854 PA OPW CG 24 3.0 RS 1855 PA OPW CG 88 1.0 RS 1855 PA OPW CG 86 D.1 RS 1855 PA DOA CG 54 29.0 RS 1857 PA OPW CG 26 D.1 RS 1858 PA OPW CG 27 11.0 RS 1858 PA OPW CG 28 D.1 RS 1858 PA OPW CG 20 1.0 RS 1858 PA OPW CG 20 1.0 RS 1858 PA OPW CG 20 1.0 RS 1859 PA OPW CG 20 1.0 RS 1859 PA OPW CG 20 1.0 RS 1859 PA OPW CG 20 1.0 RS 1859 PA OPW CG 20 1.0 RS 1859 PA OPW CG 20 1.0 RS 1859 PA OPW CG 20 1.0 RS 1859 PA OPW CG 27 11.0 RS 1850 PA OPW CG 28 3.0 RS 1850 PA OPW CG 27 11.0 RS 1850 PA OPW CG 27 11.0 RS 1850 PA OPW CG 28 3.0 RS 1850 PA OPW CG 33 3.0 RS 1850 P							NS 1653					2.0
R5 1554 PA DO6 CG 54 24.0 R5 1655 PA D9W CG 68 1.0 R5 1554 PA D06 CG 34 46.0 R5 1657 PA D9W CG 26 D.1 R5 1555 PA D06 CG 54 27.0 R5 1658 PA D9W CG 26 D.1 R5 1557 PA D06 CG 26 3.0 R5 1658 PA D9W CG 26 17 1.0 R5 1557 PA D06 CG 44 3.0 R5 1658 PA D9W CG 27 1.0 R5 1557 PA D06 CG 44 3.0 R5 1659 PA D9W CG 27 1.0 R5 1559 PA D06 CG 44 3.0 R5 1660 PA D9W CG 27 1.0 R5 1559 PA D06 CG 40 19.0 R5 1660 PA D9W CG 27 1.0 R5 1550 PA D06 CG 40 2.0 R5 1661 PA D9W CG 47 11.0 R5 1562 PA D06 CG 42 7.0 R5 1662 PA D9W CG 47 11.0 R5 1562 PA D06 CG 42 7.0 R5 1662 PA D9W CG 47 11.0 R5 1563 PA D06 CG 48 230.0 R5 1664 PA D9W CG 25 3.0 R5 1564 PA D06 CG 48 230.0 R5 1665 PA D9W CG 25 3.0 R5 1564 PA D06 CG 48 230.0 R5 1666 PA D9W CG 33 4.0 R5 1565 PA D06 CG 47 11.0 R5 1666 PA D9W CG 33 4.0 R5 1565 PA D06 CG 48 230.0 R5 1666 PA D9W CG 33 4.0			006				RS 1654	PA	09 w	CG	24	5.0
RS 1555 PA DOB CG 34 48.0 RS 1656 PA D9W CG 17 1.0 RS 1555 PA D0B CG 34 29.0 RS 1658 PA D9W CG 21 1.0 RS 1557 PA D0B CG 26 3.0 RS 1658 PA D9W CG 20 1.0 RS 1558 PA D0B CG 46 3.0 RS 1659 PA D9W CG 20 1.0 RS 1559 PA D0B CG 46 3.0 RS 1659 PA D9W CG 20 1.0 RS 1550 PA D0B CG 46 3.0 RS 1650 PA D9W CG 27 3.0 RS 1550 PA D0B CG 40 19.0 RS 1661 PA D9W CG 67 20.0 RS 1560 PA D9W CG 67 20.0 RS 1561 PA D0B CG 42 7.0 RS 1662 PA D9W CG 47 11.0 RS 1562 PA D0B CG 48 230.0 RS 1664 PA D9W CG 25 3.0 RS 1564 PA D0B CG 48 230.0 RS 1664 PA D9W CG 25 3.0 RS 1564 PA D0B CG 48 230.0 RS 1666 PA D9W CG 25 3.0 RS 1566 PA D0B CG 48 230.0 RS 1666 PA D9W CG 33 3.0 RS 1566 PA D0B CG 48 330.0 RS 1666 PA D9W CG 33 3.0 RS 1566 PA D0B CG 48 330.0 RS 1666 PA D9W CG 33 3.0 RS 1566 PA D0B CG 35 3.0 RS 1566 PA D0B CG 35 3.0 RS 1566 PA D0B CG 35 3.0 RS 1566 PA D0B CG 33 3.0 RS 1566 PA D0B CG 33 3.0 RS 1566 PA D0B CG 33 3.0 RS 1566 PA D0B CG 33 3.0 RS 1566 PA D0B CG 35 35 35 35 35 35 35 35 35 35 35 35 35							RS 1455	PA	QTW	CC	48	1.0
RS 1355 PA DO6 CG 54 27-0 RS 1657 PA DOW CG 26 D.1 RS 1356 PA DO6 CG 26 3.0 RS 1659 PA DOW CG 21 1.0 RS 1358 PA DO6 CG 46 3.0 RS 1659 PA DOW CG 20 1.0 RS 1359 PA DO6 CG 46 3.0 RS 1660 PA DOW CG 27 11.0 RS 1359 PA DO6 CG 40 19-0 RS 1660 PA DOW CG 27 11.0 RS 1350 PA DO6 CG 40 2.0 RS 1661 PA DOW CG 47 11.0 RS 1351 PA DO6 CG 42 7.0 RS 1662 PA DOW CG 47 11.0 RS 1352 PA DO6 CG 56 29-0 RS 1664 PA DOW CG 25 3.0 RS 1356 PA DO6 CG 48 230.0 RS 1665 PA DOW CG 25 3.0 RS 1356 PA DO6 CG 48 230.0 RS 1665 PA DOW CG 35 3.0 RS 1356 PA DO6 CG 48 230.0 RS 1665 PA DOW CG 35 3.0 RS 1356 PA DO6 CG 48 230.0 RS 1665 PA DOW CG 35 3.0 RS 1356 PA DO6 CG 48 230.0 RS 1665 PA DOW CG 35 3.0 RS 1356 PA DO6 CG 48 330.0 RS 1665 PA DOW CG 33 4.0	R5 1554		000	E.F.			I RS 1454			EG		1.0
R5 1557 PA DOS CG 26 3.0 R5 1659 PA OFF CG 27 1.0 R5 1557 PA DOS CG 46 3.0 R5 1659 PA OFF CG 27 1.0 R5 1557 PA DOS CG 40 19.0 R5 1660 PA OFF CG 27 3.0 R5 1550 PA DOS CG 40 2.0 R5 1661 PA OFF CG 47 11.0 R5 1562 PA DOS CG 42 7.0 R5 1662 PA OFF CG 47 11.0 R5 1562 PA DOS CG 42 7.0 R5 1662 PA OFF CG 47 11.0 R5 1562 PA DOS CG 42 30.0 R5 1664 PA OFF CG 25 3.0 R5 1563 PA DOS CG 48 230.0 R5 1665 PA OFF CG 25 3.0 R5 1565 PA OFF CG 25 3.0 R5 1565 PA OFF CG 25 3.0 R5 1565 PA OFF CG 35 1.0 R5 1565 PA OFF CG 35 1.0 R5 1565 PA OFF CG 35 1.0 R5 1565 PA OFF CG 35 3.0 R5 1565 PA OFF	RS 1355		900			29-0	RS 1657			55		0.1
R5 1550 PA DOS CG 46 3.0 R5 1660 PA OSW CG 27 3.0 R5 1550 PA DOS CG 46 230.0 R5 1661 PA OSW CG 67 20.0 R5 1561 PA DOS CG 47 11.0 R5 1562 PA DOS CG 48 230.0 R5 1663 PA OSW CG 25 3.0 R5 1563 PA DOS CG 48 230.0 R5 1664 PA OSW CG 25 3.0 R5 1563 PA DOS CG 48 230.0 R5 1664 PA OSW CG 25 3.0 R5 1564 PA DOS CG 48 230.0 R5 1665 PA OSW CG 36 1.0 R5 1565 PA DOS CG 48 230.0 R5 1665 PA OSW CG 35 3.0 R5 1565 PA DOS CG 48 230.0 R5 1665 PA OSW CG 35 3.0 R5 1566 PA DOSW CG 35 3.0 R5 1667 PA DOSW CG 35 3.0 R5 1566 PA DOSW CG 35 3.0 R5 1667 PA DOSW CG 35 3.0 R5 1566 PA DOSW CG 35 3.0 R5 1667 PA DOSW CG	42 1224					3.6	NS 1658			CE		
## 1559 PA DO6 CG 40 19-0 R5 1662 PA O9W CG 67 11-0 R5 1564 PA D9W CG 47 11-0 R5 1564 PA D9W CG 47 11-0 R5 1564 PA D9W CG 47 11-0 R5 1564 PA D9W CG 45 12-0 R5 1564 PA D9W CG 25 3-0 R5 1564 PA D9W CG 35 3-0 R5 1566 PA D9W CG 35 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 33 3-0 R5 1566 PA D9W CG 35 3-0 R5 1566 PA D9W	AD 1221			ČĚ		3.0	HS 1659		09 W	<u>C</u>		
R5 1950 PA DO6 CG 40 2.0 R5 1662 PA O9W CG 47 11.0 R5 1562 PA DO6 CG 48 29.0 R5 1664 PA D9W CG 25 3.0 R5 1563 PA DO6 CG 48 230.0 R5 1666 PA D9W CG 25 3.0 R5 1565 PA DO6 CG 47 11.0 R5 1666 PA D9W CG 36 1.0 R5 1565 PA DO6 CG 47 11.0 R5 1666 PA D9W CG 36 1.0 R5 1566 PA DO6 CG 47 11.0 R5 1667 PA D9W CG 37 3.0 R5 1566 PA D06 CG 47 11.0 R5 1566 PA D9W CG 37 3.0 R5 1566 PA D06 CG 45 2.0 R5 1566 PA D9W CG 38 3.0 R5 1566 PA D06 CG 45 2.0 R5 1566 PA D9W CG 38 3.0 R5 1566 PA D06 CG 38 3.0 R5 1566 PA D9W CG 38 3.0 R5 1566 PA D9	A3 6770 B1 1880			23		19.0	K5 1660					
R5 1961 PA D06 CG 42 7.0 R5 1643 PA 098 CG 42 12.0 R5 1564 PA 098 CG 25 3.0 R5 1564 PA D06 CG 48 230.0 R5 1664 PA 098 CG 25 3.0 R5 1564 PA D06 CG 48 230.0 R5 1666 PA 098 CG 36 1.0 R5 1566 PA 098 CG 36 1.0 R5 1566 PA 098 CG 51 3.0 R5 1566 PA 098 CG 52 33 4.0 R5 1566 PA 098 CG 52 3.0 R5 1566 PA 098 CG 52 33 4.0 R5 1566 PA 098	RS 1640			ČĞ		2.0	K2 1641					
RS 1562 PA DO6 CG 56 29.0 RS 1664 PA OW CG 25 3.0 RS 1565 PA DO8 CG 69 330.0 RS 1665 PA OW CG 51 3.0 RS 1566 PA DO8 CG 69 330.0 RS 1666 PA OW CG 51 3.0 RS 1566 PA DO8 CG 78 119.0 RS 1667 PA OW CG 51 3.0 RS 1566 PA DO8 CG 45 2.0 RS 1567 PA OW CG 33 4.0 RS 1566 PA DO8 CG 33 3.0 RS 1566 PA DO8 CG 35 3.0 RS 1566 PA DO8 CG 35 3.0 RS 1566 PA DO9 CG 3	25 1441			čč		7.0						
R5 1563 PA DO6 CG 48 230.0 R5 1665 PA DOW CG 36 1.0 R5 1564 PA DO6 CG 78 119.0 R5 1665 PA DOW CG 61 3.0 R5 1566 PA DO6 CG 78 119.0 R5 1667 PA DOW CG 33 4.0 R5 1566 PA DO6 CG 45 2.0 R5 1667 PA DOW CG 56 35 4.0	85 1542					29.0						
R5 1564 PA DO6 CG 69 330.0 R5 1665 PA 09W CG 51 5.0 R5 1565 PA DO6 CG 78 119.0 R5 1666 PA 09W CG 33 4.0 R5 1566 PA DO6 CG 45 2.0 R5 1667 PA D9W CG 33 4.0 R5 1566 PA D06 CG 45 2.0 R5 1666 PA D9W CG 56 3.0						230.0						
R5 1565 PA D06 CG 78 119-0 R5 1667 PA D9H CG 33 4-0 R5 1566 PA D06 CG 45 2-0 R5 1667 PA D9H CG 56 3-0				ÇG		330.0						
R5 1566 PA 006 CG 45 2.0 R5 1666 PA 09W CG 56 3.0		PA	900	CC		114.0						
A. A. A. A. A. A. A. A. A. A. A. A. A. A	RS 1566	PA	D06									
		PA	D06	CG	38	3.0						

NU	AREA	LINE	ROCK	ŽN	45	MO	AREA	LINE	ADDA	£M.	A5
RS 1670	PA	044	CG	67	15.0	RS 1772	DL	014	CC	15	2.0
85 1671	PA	09 w	CG	30	2.0	H5 1773	DL	D1+	C.L	11	5.0
RS 1672	PA	09 W	cc	>2	19.0	MS 1774	DL	D16	çç	17	2.0
45 1673 45 1674	PA Pa	09 M	CG	37 32	0.1 0.1	NS 1775 NS 1776	DL DL	D16 D16	CG CG	13 21	5.6 1.0
H5 1675	PA	09*	Č6	28	0.1	RS 1777	DL	016	čč	28	2.6
H5 1676	PA	09 W	ČĠ	34	2.0	RS 1778	ōī	010	CG	22	3.0
HS 1677	PA	69 w	CG	52	0.1	RS 1779	٥L	016	ÇĞ	22	1.0
AS 1676	PA	094	CG	39 57	3.0 3.0	K\$ 1780	DL	D16	CG	25 29	5.0
MS 1679 RS 1860	PA PA	09 H	CG CG	15	4.0	95 1781 85 1782	OL OL	016 016	CG CG	51	4.0
45 1661	PA	09 w	čč	41	5.0	MS 1783	DL	016	ČĞ	43	0.1
¥S 1682	PA	g9w	CG	17	0.1	RS 1784	ÛL	903	CG	34	35.0
K5 1683	PA	09 w	Çu	19	3.0	RS 1785	ĎΓ	903	CG	>1	3.D
R5 1684	PA PA	09w	ÇG ÇG	11 36	3.0 20.0	RS 1786 RS 1787	ÐL DL	603 603	CG CG	120 68	34.0 35.0
MS 1685 RS 1686	PA	09 w	ČĠ	97	38.0	RS 1785	OL.	903	ČĞ	•7	4.0
R5 1687	PA	09 =	CG	43	36.0	A2 1789	DL	403	CG	43	5.0
45 160B	PA	04=	CG	36	6.0	RS 1790	DL,	903	CG	122	172.0
RS 1689	PA	04 R 04 R	CG CG	78 81	3.0 196.0	RS 1791 RS 1792	DL DL	403 903	CG CG	37 28	14.0
H2 1641 H2 1641	PA	09 M	ÇL	45	100.0	RS 1793	DL.	903	CG	51	32.0
NS 1692	PA	09 W	ČĞ	62	340.0	RS 1794	DL	903	CG	40	29.0
W2 16A3	PA	UPW	cc	49	190.0	A5 1795	ĎΓ	403	CG	54	100.0
85 1694	PA	69 M	CG	76	50.0 0.1	R5 1796	<u>O</u> L	603 600	CG	54 65	39.0 21.0
MS 1695 MS 1696	PA PA	09 m	CG CG	62 62	31.0	45 1797 R5 1798	DL OL	903	CG	110	30.0
45 1697	PA	09#	čč	22	6.0	AS 1799	ÖL	403	CG	iii	35.0
45 1698	PA	69 w	CG	65	0.054	HS 1800	UL	403	CG	103	47.0
RS 1699	ĐŲ	510	Cu	20	3.0	45 1801	DL	903	ÇĞ	115	46.L 43.6
MS 1760 MS 1701	D#	51C	CG CG	64 611	1.0	RS 1802	DL DL	403 403	ÇG CG	141 185	200.C
45 1702	00	216	Cu	44	1.0	RS 1803 RS 1804	OL.	403	CG	225	1+0.0
45 1703	υū	21C	CG	41	2.6	KS 1805	٥L	403	CG	70	1.04
RS 1704	00	21¢	Ce	15	3.0	RS 1806	DŁ	003	Co	52	33.0
RS 1705 RS 1706	94 96	51C	ÇG ÇG	16 16	0.1 1.0	RS 1807	OL OL	903 903	55 53	>4 46	35.0 22.0
AS 1707	DQ	216	CG	22	1.0	RS 1808 RS 1809	OL.	04 E	CG	38	15.0
RS 1708	DQ	216	CG	15	1-0	AS 1810	DĹ	04E	ÇG	25	5.0
HS 1709	00	216	CG	14	2.0	RS 1811	DL	04E	22	23	0.1
RS 1710 RS 1711	DQ DQ	51C 51C	CG	34 73	2.0 1.0	RS 1812	DL	04E	CG CG	20 21	3.0
AS 1712	96	210	čč	38	0.1	RS 1813 RS 1814	DL DL	04 E	ÇĞ	15	3.0
AS 1713	De	21C	CG	18	0.1	AS 1815	OL	04 E	CG	24	25.0
RS 1714	DΨ	21C	CG	27	1.0	RS 1816	PL	04 E	CG	45	11.0
RS 1715 RS 1716	00 00	21C 21C	CG GS	50 97	3.0	MS 1817	DL	04E 04E	CG CG	25 10	6.0 13.0
AS 1717	04	210	23	46	3.0	RS 1818 RS 1817	DL DL	04E	23	61	3.0
R5 1718	09	210	CG	25	0.1	RS 1820	οĩ	DAE	CG	18	6.0
45 1719	Dů	SIC	CG	25	2.0	NS 1921	PL	O+E	CG	21	4.0
RS 1720 RS 1721	00 00	023 023	EG GS	42 52	0.1	85 1828	DL	04 E	CG	23 19	7.0 11.0
AS 1722	Du	023	če	47	4.0	KS 1823 KS 1824	DL DL	04 E	FG	39	0.1
RS 1723	DQ	D23	ČG.	40	3.0	RS 1825	DL	04 E	FG	39	6.0
NS 1724	Du	D2 3	CG	34	1.0	45 1626	OL	04E	FG	40	0.1
KS 1725 RS 1726	04 04	DS 3 DS 3	CG CG	32 16	1.0	#5 1827 #5 1828	DL DL	04 E 04 E	FG FG	22 18	1.0
AS 1727	ŭĢ	023	čč	43	0.1	NS 1829	Ö.	04 E	FG	23	6.0
45 172U	00	D2 3	CG	61	5.0	N2 1630	DL	O4E	FG	19	1.0
RS 1729	00	053	ÇĞ	35	2.0	HS 1831	OL	04 E	Fu	63	3.0
RS 1730 RS 1731	D¥ D¥	D23 D23	66 65	93 17	4.D	AS 1832	OF DF	04 E	FG FG	31 20	3.0
45 173Z	õü	023	ČĠ	33	3.0	RS 1833 RS 1834	OL.	04E	FG	15	1.0
R5 1733	00	D2.3	CG	16	2.0	RS 1635	ĎĹ	AOS	CG	39	5.0
KS 1734	09	023	ČČ	46	2.0	RS 1836	DL	AOS	Cu	23	1.0 0.1
AS 1735 AS 1736	0Q 0Q	023 023	56 56	17 23	2.0 1.0	RS 1837	DL DL	20A 20A	CG Cu	32 19	2.0
RS 1737	00	023	CG	23 16	0.1	K5 1838 R5 1839	ÐL	20A	CG	21	1.0
RS 1738	Du	DZ3	CG	24	1.0	A5 1840	DL	405	CG	47	2.0
AS 1739	DQ	D2 3	CG	61	1.0	RS 1841	DL	20A	CG	15	1.0 2.0
HS 1740 HS 1741	DQ 00	023 023	CG CG	53 30	1.0 1.0	RS 1842 RS 1843	DL DL	A 0 S	CG CG	18 20	1.0
RS 1742	00	023	33	59	2.0	R5 1843	DL	20A	CG	27	0.1
45 1743	De	D2 3	CG	18	2.0	RS 1845	DL	20 A	CG	16	1.0
RS 1744	00	650	66	29	3.0	H5 1846	DL	AGS	CG	18	2.0 0.1
AS 1745 AS 1746	00 04	023 023	25 25	28 28	4.0 0.1	R5 1847	DL DL	A05 A05	CG	15 12	0.1
AS 1747	20	053	CG	47	6.0	MS 1848 MS 1849	DŁ	20A	CG	42	5.0
45 1748	D <b>u</b>	UZ 3	Cu	47	16.0	NS 1650	OL	20A	CG	15	0.1
<b>#5 1749</b>	00	DS 3	Çu	20	7.0	NS 1851	ÐĻ	ADS	CG	24	1.0
45 1750 45 1751	nd Dr	P53	CG CG	40 59	7.0 7.0	HS 1852	DL	20A	CG CG	53 53	1.0 1.0
45 1752	00	023	CG	66	5.0	K\$ 1653 K\$ 1654	DL DL	20A	Cu	16	1.0
45 1753	OL.	010	CG	34	12.0	NS 1855	ÜL	20 a	£lo	5.5	2 .C
45 1754	DL	016	CC	15	3.0	NS 1056	ŊĹ	∠D.a	£6	23	3.0
45 1755 45 1756	DL DL	D16	CG CG	53	4.0 20.0	HS 1857	DL	20A	CG CG	30 43	2.0 5.0
RS 1756 RS 1757 RS 1758 RS 1759 RS 1760	OL.	D16 D16	CG CG	42 38	4_0	45 1858	DL DL	20A 20A	CG	43 32	1.0
AS 1758	DL	D16	CG	17	4.0 1.0	RS 1859 RS 1860	DL.	ZDA	ČG	26	4.0
RS 1759	ÐL	D16	CG	75	5.0	A2 1861	DL	20A	CG	20	1.0
RS 1760 RS 1761	DL	D16	CG	58 41	15.0 9.0	HS 1862	BL	20A	55	27	0-1 1-0
#5 1761 \$5 1762	DL DL	Dia Dia	CC.	18	5.0	R\$ 1863	DL DL	20A 20A	CG CG CG	16 44	1.0
AS 1763	۵L	D16	23 20 20 20	41	16.0	RS 1844 RS 1865	DL	20A	ČĠ	53	2.0
RS 1764	OĻ	D1 6	ÇĢ	30	1.0	RS 1644	OL	20A	CG	40	11.0
RS 1765	DL	016	56	20	2.0 2.0	RS 1867	90	W 50	ÇG	44	1.0
RS 1766 RS 1767	DL DL	D16 D16	CG CG	22 33	0.1	RS 1868	50	05# 05#	FG FG	38 25	2.0
RS 1768	OL.	D16	ĊĢ	14	2.0	RS 1869 RS 1870	60 80	05 M	FG	29	1.0
RS 1769	OL	D16	CG	51	2.0	45 1871	80	W\$0	FG	43	1.0
RS 1770	DL O	016	23 23	21 40	3.0	RS 1872	BQ	05 M	FG FG	20	1.0
RS 1771	DL	D16		40	1.0	RS 1873	80	OZW	FG	19	7 40

Na.	AREA	LINE	RUCK	žH	A5	40	AREA	LINE	ROCA	£H.	43
AS 1874	80	U2 w	FG	12	1.0	45 1976	80	Dia	CL	69	16.0
RS 1875	80	MZG	FG	23	0+1	HS 1977	Bu	D14	Cu	52	5-0
RS 1876	80	02M	FG FG	22 17	1.0 2.0	M5 1978	80	U1 * U1 *	Eu EG	31	7.6
RS 1877 RS 1878	80 80	05 m 05 m	FG	ši	1.0	45 1479 45 1480	8U 80	U1 4	ÇĞ	4.3 2.5	14.0 16.0
RS 1879	80	U2 W	fu	26	0.1	KS 1981	60	01.	EG	33	2.0
A5 1880	80	05A	FG FG	14 52	1 -0 2 -0	RS 1982	80	D14	CG	44	2.0
RS 1881 RS 1882	80 80	02 w	FG	45	15.0	#2 1484 ₩2 1487	8U 8U	014 814	CG CG	49	11.0 17.0
RS 1883	60	02=	FG	15	5 "0	#5 1785	80	D1 4	Ĕ.	52	13.0
RS 1884	60	02 w	FG	14	1.0	H2 1486	60	014	tu	60	12.0
#5 1885 #5 1886	8Q 8Q	02 w 02 w	FG Fb	52 31	17.0 6.0	45 1987 R5 1988	80 80	D1 4 U1 4	fu fu	37 21	0.1
RS 1887	BU	02 m	FG	79	10.0	45 1989	40	01 4	Fu	84	35.6
RS 1888	50	02 <del>u</del>	FL	93	40.0	45 1490	80	01+	£6	e b	7.0
K\$ 1889 K\$ 1890	80 80	02 M	fi. FG	54 61	1.0 1.0	42 1483 42 1483	80 80	014	F.	56 72	11.0
A5 1841	80	02 =	FG	64	1.0	13 1412	••	0.4	- •		****
RS 1892	DG .	02w	FG	44	1.0						
A5 1893	<b>#</b> D	05 m 05 m	FG FG	184 53	6.0 1.0	нь 1	GT	D37	(A	23	3.0
NS 1894 NS 1895	80 80	25 A	FG	70	2.0	47 ₹	ĢT	D3 7	ca.	31	0 - 3
HS 1896	80	010	ÇG	56	30.0	HS 4	6T 6T	D37 D37	GR GR	24 33	12.0
HS 1897	80	010	CG CG	37 19	20.0	HS 5	GT	D3 7	GA	12	40.0
MS 1898 RV 189	80 80	010 010	ČĞ	13	5.0	H\$ 6	ĠŦ	037	GR	79	29.0
R5 1900	80	Dlo	CG	37	21.0	H5 B	GT	037 037	GH GH	51 67	28.0
<b>*5 1901</b>	RO	Dit	ÇG	52	4.0	H5 9 H5 10	GT GT	037	ũ	12	¥.0
MS 1902 MS 1903	BU BU	010 010	€b Lu	78 27	# * £	H5 11	GT	D3 7	€A.	28	31.0
RS 1904	80	<b>D10</b>	ÇG	36	16.0	HZ 12	GT	D37	64	48	23.0
K5 1905	80	616	CG	42	15.0	H5 13 H5 14	GT GT	D37 D37	GA GR	26 22	8.0
MS 1906 MS 1907	8C 6U	01C	23 23	37 48	ن، د ن، د	HS 15	GT	037	GA	25	10.0
45 1400	80	010	ÇĞ	38	28.0	HS 10	GT	037	GH	24	10.0
RS 1909	80	D10	ČĞ	35	13.0	HS 17 HS 18	G1 G1	037 037	GH GH	22 31	9.0
#5 1910 #5 1911	60 60	D10	CG	53 30	48.0 34.0	H5 19	GT	03 7	<b>ال</b> ق	37	10.0
82 1415	BD	010	ČL	30	10.0	H5 20	e.T	037	LA	30	12.0
RS 1913	80	Dic	CG	20	3.0	H2 55	GT GT	03 1 03 7	GM GQ	25 25	5.U 4.L
HS 1914	90	D10	00 03	50 40	33.0 4.0	H5 23	ĞĪ	037	GR	80	80.0
RS 1915 RS 1916	80 80	010	55	19	5.0	н5 24	10	037	G4	35	9.0
AS 1917	80	010	CG	58	55.0	H5 25	GT GT	D37	GA GA	30 +3	10.0 21.0
A5 1916	80	DIG	ÇĞ	42	16.0 42.0	HS 26 HS 27	GT GT	037	GR.	70	28.0
47 1950 47 1918	80 80	D10 D10	Cu Cû	31 43	7.0	H5 28	GT.	037	GA	28	9.0
NS 1921	80	010	ČG	25	10.0	H2 29	GT	017 037	G4 G4	21 39	8.6 14.6
NS 1922	80	010	Ç.C.	15	2 .D 24 .O	н5 30 н5 31	GT GT	D3 7	GA	34	10.0
NS 1923 RS 1924	60 60	010 010	25 23	37 56	66.0	HS 32	61	D37	(en	35	20.5
A5 1925	BQ	010	CG	72	38.0	H2 33	61	037 035	ÇA	46 30	25.6 9.0
45 1926	80	010	cc	18	0.1	H5 34 H5 35	61 61	035	ببئ چئ	39	11.0
45 1927 45 1928	80 80	D10 D10	C b	37 22	1.0	HS 36	ĞŤ	035	جئ	39	46.0
H> 1929	80	010	čč	76	90.0	HS 37	GT	035	ÇQ.	40 37	49.0
47 TA30	θů	010	ÇĻ	94	146.0	H5 3H H5 39	GT GT	035 035	GR GK	66	1.0 36.0
MS 1931 RS 1932	6Q BD	610 610	CG CG	42 38	12.G 1.G	HS 40	ĞŤ	D35	Gal	43	30.0
45 1933	80	012	ČĞ	55	55.0	H5 41	GT	035	<u> </u>	177 33	640.0
RS 1934	#D	D12	CG	58	53.0 36.0	H\$ 42 H\$ 43	GT GT	D35 D35	ᅝ	258	13-C 240.0
A5 1935 A5 1936	60 60	D12	ÇG	50 46	10.0	H5 44	Ğİ	D35	GH	54	120-0
RS 1937	80	210	Su	34	3.0	H5 45	6T	035	(A	67	HO.0
RS 1938	80	DIC	CG	19	4.0	H5 46	GT GT	035 035	64 5-	60 70	48.6
45 1939 45 1940	80 80	01 <i>c</i>	‡G CG	70 104	48.D	H5 48	ĿΤ	035	č=	66	27.6
85 1941	90	016	čč	46	13.0	H\$ 49	Ģī	034	μ.	48	20.6
AS 1942	60	012	CG	27	5.0	H2 21	uT UT	73.2 4.60	سرا 4ن	36 30	10.r 16.i
RS 1943 RS 1944	80 80	D15	ئات ماڻ	87 34	28.0 14.0	H2 55	GT	035	GA	24	4.0
RS 1944 NS 1945	80	012	Clo	32	5.0	HS 53	GT	D35	GH	28	5.0
AS 1946	80	210	22	23	<b>5.0</b>	H\$ 54 H\$ 55	GT GT	035 035	GR GH	34 85	10.0 70.0
RS 1947 RS 1940	80 80	015	CG	74 56	18.0 14.0	HS 54	61	035	CA	57	72.0
45 1949	80	015	CG	32	6.0	HS 57	GT	035	i.a	60	120-0
<b>85 1950</b>	ďU	D1 2	ÇĞ	20	2.0	H3 58	GT GT	035 035	GA GR	36 16	0.01
R5 1951	BD BU	D15	36 36	29 29	35.0 16.0	HS 40	GT	D3.5	ÇR	40	23.0
K7 1423	80 80	DIS	ÇG	39	15.0	H\$ 61	GT	D35	GH	45	7.0
45 1954	đО	D1 €	- 6	37	55.0	54 2H E4 2H	GT GT	03 5 03 5	GM GR	04 32	100.0 14.0
#5 1955 #5 1956	RO.	015 015	C.L.	39 64	12.G 37.0	H3 64	GT	035	GR	15	a .0
45 1956 45 1957	80 90	DIZ	ÇĞ	28	1.0	H\$ 65	ĢŦ	035	GR	25	11.0
N2 1428	84	Dir	26	43	17.0	H\$ 64 H\$ 67	GT GT	035 033	GR GR	29 18	7.0
#5 1959	#G	012	CG CG	35 248	2.0	H5 68	61	033	GA	26	4.0
RS 1940 RS 1941	#0 #0	D12	20	53	180.0	HS 69	61	D33	GR	40	10.6
RS 1962	#O	015	Clo	55	14.0	H5 70	GT GT	D33	GH GH	50	15.0 16.0
R5 1963	80	04 W	FG FG	17	1.0	H5 71 H5 72	61	D33	(A)	36	18.0
RS 1964 RS 1965	80 80	04 W	FG FG	338 59	2.0	H5 73	ĿΤ	033	-	43	24.0
RS 1966	80	04 W	FG	38	6.0	H5 74	ĢÏ	u33	644	23	5.0
RS 1967	80	04 H	FG	34	7.0	HS 75	GT GT	033 033	GR GR	24 39	10.0
RS 1968	B0	04 W	fG Fb	23 11	15.0 6.0	HS 77	61	033	GH	58	15.0
45 1969 85 1970	80 80	04.6	FG	17	7.0	H5 78	GT	033	G-4	73	30.0
RS 1971	80	DAW	FG	18	2.0	HS 80	G1 G1	D33 E10	ija ija	81 38	104.0
RS 1972	8D	D1 4	CG.	69 87	230.0 140.6	H2 B4	61	D33	ᅝ	23	10.D
RS 1973 RS 1974	80 80	D1 + D1 +	CC	60	430.C	H7 83	ĢT	D3.3	<b>ĕ</b> A	37	13.0
R5 1975	80	D14	ČĢ	72	192.0	HS 84	6T	<b>033</b>	, A	99	200.0