

5) Runoff

Total runoff is the amount of surface runoff and groundwater. Surface runoff was calculated by each unit hydrograph and each basin's hourly rainfall distribution. The results of the computer calculation in each basin are shown in Fig. H-8, 9, 10, 11.

6) Estimation of runoff capacity

The runoff capacity for each schemes can be calculated by using the basic factors described in paragraph (1) to (5). The estimated monthly and annual runoff capacities for each schemes are shown below:

(Unit : 10^3 m^3)

Month	Black Right	Black Left	Broad Right	Broad Left
J	280	720	470	430
F	300	770	550	510
M	400	1,040	460	420
A	820	2,120	1,910	1,750
M	1,220	3,140	1,650	1,530
J	820	2,100	630	580
J	820	2,100	1,090	1,010
A	1,050	2,710	1,260	1,160
S	990	2,550	1,710	1,570
O	1,250	3,220	1,960	1,810
N	540	1,380	960	890
D	280	720	370	340
Total	8,770	22,570	13,020	12,000

2.2.6 Pumping drainage plan

1) Design flood

The flood runoff from each area was estimated by the unit hydrograph in Fig. H-8 to H-11. The peak runoff at each pump station is summarized below.

<u>Pump station</u>	<u>Peak runoff</u>
Holland	25.0 m ³ /s
Black River Left	51.5 m ³ /s
Broad River Right	36.4 m ³ /s
Broad River Left	23.0 m ³ /s

2) Drainage requirement

Drainage requirement was determined based on the water balance calculation and the following conditions taking into consideration the growing stage of rice prospected flood season.

- Allowable inundation depth and duration on the lowest paddy field is set at 30 cm and 96 hours respectively.
- Allowable inundation duration is set at 48 hours in case of the depth of more than 30 cm.

The water balance calculation is according to the above-mentioned flood hydrograph and three alternative capacities envisaged. The results of the calculations are shown in Table H-12 and Figs. H-12 to H-15.

Based on the above results, design discharges and peak discharges of the required pumps were decided as follows:

<u>Pump Station</u>	<u>(Unit: m³/s)</u>	
	<u>Design Discharge^{1/}</u>	<u>Peak Discharge^{2/}</u>
Holland	4.5	5.2
Black River Left	7.5	8.7
Broad River Right	6.0	6.7
Broad River Left	4.5	5.0

Note: Pump-up discharge increases with decrease of pump head.

- 1/: Design discharge: Discharge of the design pump head
- 2/: Peak discharge : Discharge of the assumed minimum pump head

Table H-1 BREAKDOWN OF PROJECT AREA

Block	Segment	Upland Area		Swamp Area	Residential Area	Irrigable Area	
		Total Clay Silt Gravel	Herbage Forest Mangrove			Gross	Net
Black Right Bank	Estate Upper (1)	750				550	
	" Lower (2)	650				600	560
	Iacovia (17)	260			260		
Black Left Bank	Y.S. River Left (9)	490	350	140			
	Right (10)	390	340	50			
	Holiday Pen (8)	860	520	90		505	400
Broad River Basin	Styx River (12)	410	400	10		400	300
	Hatfield (7)	310	150			295	220
	Slupe (3)	740	740				
M.Quarters Right	Broad Right (13)	1,290	1,290			1,065	800
	" Left (14)	1,200	1,200			970	800
	Arlington (4)	660	660				
Estuary & M.Quarters Right	Mountainside (6)	760	760				
	Black Estuary (15)	1,460	1,160	300			
	M.Quarters Right (11)	660	660				
Luana	(5)	520				315	
	Black River Town (16)	40			40		
Total		410	1,920	2,160	6,070	290	300
			4,490	6,660		(4,700)	(3,080)

Table H-2 (1/5) AVERAGE CONE INDEX IN EACH 0.5 M LAYER

Site	0-0.5	-1.0	-1.5	-2.0	-2.5	-3.0	-3.5	-4.0	-4.5	-5.0
<u>Black River Left bank</u>										
L.No.5, 100	0.15	0.30	0.54	0.70	0.77	0.92	1.69	1.97	1.69	2.02
200	<u>0.58</u>	0.15	0.82	0.77	0.58	0.89	0.70	0.77	0.70	0.86
300	<u>0.58</u>	0.40	0.70	0.82	1.08	1.26	1.20	1.08	1.08	1.20
L.No.6, 100	0	<u>3.28</u>	7.10							
200	<u>0.58</u>	<u>1.37</u>	1.69	1.58	2.02	0.73	7.10			
300	<u>0.54</u>	<u>1.15</u>	1.69	1.31	1.53	1.64	1.80	7.10		
400	<u>0.54</u>	<u>1.06</u>	1.26	0.86	2.40	7.10				
500	<u>0.65</u>	<u>1.15</u>	1.31	1.48	1.26	1.69	1.48	7.10		
600	<u>0.70</u>	<u>1.06</u>	1.26	1.37	1.37	1.37	1.64	1.86	2.19	2.19
BL.No.2	0.40	<u>0.86</u>	0.92	0.65	0.65	0.74	0.82	0.92	0.58	0.74
BL.No.6	<u>2.07</u>	<u>3.50</u>	7.10							
<u>Styx River</u>										
L.No.11, 100	0	<u>7.10</u>								
200	<u>0.70</u>	<u>1.80</u>	7.10							
300	<u>0.50</u>	<u>1.08</u>	1.31	7.10						
400	0.30	<u>0.50</u>	1.09	7.10						
500	0.15	<u>0.58</u>	1.37	7.10						
SX.No.2	<u>0.50</u>	<u>0.54</u>	0.54	1.64	7.10					
<u>Y.S. River Left bank</u>										
L.No.12, 100	0.40	0	0.86	1.37	1.64	7.10				
200	0.15	0.30	0.70	1.08	1.86	3.11	7.10			
300	0.15	0	0.77	0.82	1.08	1.37	1.86	3.17	7.10	
400	0.30	0.15	0	0.15	0.58	0.98	1.58	2.24	7.10	
500	<u>0.58</u>	<u>0.54</u>	0	0.40	0.64	0.50	0.40	0.92	1.08	0.77

Table H-2 (2/5) AVERAGE CONE INDEX IN EACH 0.5 M LAYER

Site	0-0.5	-1.0	-1.5	-2.0	-2.5	-3.0	-3.5	-4.0	-4.5	-5.0
L.No.13,100	<u>1.04</u>	<u>1.20</u>	1.48	1.20	1.04	1.75	7.10			
200	<u>0.70</u>	<u>0.77</u>	0.98	1.04	1.09	0.82	0.86	0.82	0.86	0.86
300	<u>0.74</u>	<u>0.74</u>	0.74	0.86	1.04	0.65	1.06	1.37	0.92	0.58
400	<u>0.54</u>	<u>0.77</u>	0.89	0.92	1.04	1.37	0.98	0.92	0.70	0.82
490	0.15	<u>0.54</u>	0.82	1.15	1.15	1.20	1.08	0.98	0.74	0.86
YS No.1	<u>3.50</u>	<u>3.17</u>	2.07	1.86	1.69	4.10	7.10			
YS No.2	<u>1.75</u>	<u>1.26</u>	1.15	1.42	1.86	2.62	7.10			
YS No.3	0	0	0.54	7.10						
YS No.4	0	0	0.77	7.10						
BL No.1	<u>0.50</u>	<u>0.77</u>	1.06	0.74	0.98	1.80	2.90	7.10		
BL No.3	<u>0.54</u>	<u>0.98</u>	1.26	1.26	1.53	1.86	2.02	2.90	3.77	7.10
BL No.4	<u>0.54</u>	<u>0.86</u>	1.31	1.04	0.86	1.04	1.08	1.08	1.08	1.26
BL No.5	<u>0.92</u>	<u>1.80</u>	0.98	1.04	1.09	1.09	1.58	3.72	7.10	
L.No.16,100	0	<u>0.50</u>	0.92	2.30	1.69	1.37	1.48	1.37	1.37	2.57
300	<u>0.89</u>	<u>1.08</u>	0.98	1.04	1.09	1.20	1.15	0.89	0.92	0.98
400	<u>0.50</u>	<u>0.70</u>	0.92	0.74	0.70	0.86	0.98	0.86	1.08	1.09
500	<u>0.54</u>	<u>0.74</u>	0.89	0.65	0.86	1.06	0.98	0.89	1.08	1.09
600	0.40	<u>0.58</u>	0.86	0.70	0.89	0.89	0.98	0.82	0.77	0.77
<u>Y.S. River Right-bank</u>										
L.No.2, 50	<u>0.82</u>	<u>0.74</u>	0.89	0.77	0.74	0.77	0.77	0.86	7.10	
100	<u>0.92</u>	<u>1.08</u>	0.92	0.86	0.82	0.77	0.86	0.77	1.04	1.08
200	<u>0.86</u>	<u>0.77</u>	0.82	0.70	0.65	0.74	0.86	0.77	0.70	0.74
250	0.30	<u>0.58</u>	0.50	0.30	0	0.98	0.65	0.40	0.30	0.65
300	0	0	0	0	0.54	0.74	0.74	0.77	0.70	0.92
350	0	0	0.40	0.86	1.20	0.98	1.64	1.26	0.89	1.15
400	0	0	0	0.58	0.65	0.74	0.82	0.70	0.98	0.89
500	0	0	0.58	0.74	0.58	0.77	0.92	0.74	0.77	1.04
L.No.3 20	<u>0.89</u>	<u>0.74</u>	0.54	0	0.71	1.04	1.06	0.92	1.09	1.06
100	0	<u>1.15</u>	1.31	1.42	1.08	1.80	1.31	1.20	1.91	2.40
200	<u>0.58</u>	<u>0.74</u>	1.20	1.26	1.08	0.86	0.86	0.92	1.48	2.02
300	0	0	0.65	0.98	0.82	0.58	0.82	0.89	0.77	0.98
400	0.15	0	1.04	1.48	0.58	0.70	0.77	0.04	1.08	1.53
500	<u>0.54</u>	<u>0.86</u>	1.09	0.89	0.54	0.70	0.74	0.74	0.70	0.74

Table H-2 (3/5) AVERAGE CONE INDEX IN EACH 0.5 M LAYER

Site	0-0.5	-1.0	-1.5	-2.0	-2.5	-3.0	-3.5	-4.0	-4.5	-5.0
L.No.14,100	0	0.30	0.50	0.65	0.15	0.50	0.89	1.09	1.37	1.53
200	0	0	0.58	0.74	0.77	0.77	1.04	0.82	0.82	0.82
300	0	0.30	0.82	0.92	1.58	1.09	1.80	1.58	2.40	2.90
400	0.40	0.40	0.77	1.64	1.75	1.31	1.53	1.31	1.26	1.26
500	0	0	0.65	1.31	0.58	0.74	0.89	1.48	1.64	1.64
M.Q.No.1	0.40	0.30	0.74	0.58	0.50	0.40	0.70	0.58	0.82	0.98
M.Q.No.3	<u>0.65</u>	<u>0.54</u>	0.77	0.54	0.65	0.92	0.89	1.06	0.54	0.89
M.Q.No.4	<u>0.74</u>	<u>0.86</u>	0.89	1.04	0.92	1.08	0.98	1.08	0.65	0.89

Broad River Right bank

L.No.8, 100	0.30	<u>0.92</u>	7.10							
200	0.40	<u>0.74</u>	0.98	1.15	1.69	7.10				
300	<u>0.50</u>	<u>0.58</u>	1.06	0.98	1.86	1.58	4.15	7.10		
400	0	0.03	0.77	1.20	2.24	3.83	7.10			
500	0	0.40	0.82	1.58	7.10					
L.No.9, 100	<u>1.09</u>	<u>2.51</u>	3.93	7.10						
200	<u>1.69</u>	<u>1.69</u>	7.10							
300	<u>0.82</u>	<u>2.40</u>	5.09	7.10						
400	<u>4.70</u>	<u>7.10</u>								
500	0.40	<u>1.04</u>	3.17	7.10						
600	0.40	<u>1.14</u>	7.10							
700	0	0	1.58	7.10						
800	0.15	<u>2.07</u>	7.10							
900	<u>0.50</u>	<u>0.50</u>	0.89	1.31	1.37	2.79	7.10			
L.No.10,100	<u>0.98</u>	<u>1.09</u>	1.48	1.91	3.99	7.10				
200	<u>0.74</u>	<u>1.20</u>	7.10							
300	0.15	<u>0.77</u>	1.09	1.31	7.10					
400	<u>0.58</u>	<u>1.08</u>	1.08	7.10						
500	0.30	<u>0.86</u>	0.86	0.98	1.15	3.17	7.10			
600	0	<u>0.50</u>	0.89	1.08	7.10					

Table H-2 (4/5) AVERAGE CONE INDEX IN EACH 0.5 M LAYER

Site	0-0.5	-1.0	-1.5	-2.0	-2.5	-3.0	-3.5	-4.0	-4.5	-5.0
L.No.15	0	<u>0.50</u>	<u>0.40</u>	<u>0.77</u>	<u>1.08</u>	<u>1.37</u>	<u>1.15</u>	<u>1.42</u>	<u>2.30</u>	<u>7.10</u>
	100	<u>0.89</u>	<u>0.50</u>	<u>0.92</u>	<u>1.42</u>	<u>1.42</u>	<u>1.91</u>	<u>2.79</u>	<u>7.10</u>	
	200	<u>0.77</u>	<u>0.54</u>	<u>1.08</u>	<u>1.31</u>	<u>1.64</u>	<u>1.91</u>	<u>2.46</u>	<u>7.10</u>	
	300	<u>0.54</u>	<u>0.50</u>	<u>1.08</u>	<u>1.15</u>	<u>1.15</u>	<u>7.10</u>			
	400	0	0	<u>3.93</u>	<u>1.04</u>	<u>1.31</u>	<u>7.10</u>			
BR.No.2		<u>0.50</u>	<u>0.65</u>	<u>0.89</u>	<u>1.31</u>	<u>1.48</u>	<u>7.10</u>			
BR.No.4		<u>0.70</u>	<u>0.70</u>	<u>0.89</u>	<u>1.14</u>	<u>1.20</u>	<u>1.15</u>	<u>1.58</u>	<u>7.10</u>	
BR.No.6		<u>1.08</u>	<u>0.92</u>	<u>0.40</u>	<u>7.10</u>					
SX.No.1		<u>0.54</u>	<u>0.40</u>	<u>0.70</u>	<u>1.04</u>	<u>2.02</u>	<u>2.19</u>	<u>7.10</u>		

Broad River Left bank

L.No.17,100		<u>0.89</u>	<u>7.10</u>							
	200	<u>0.92</u>	<u>1.20</u>	<u>7.10</u>						
	300	<u>0.92</u>	<u>1.48</u>	<u>7.10</u>						
	400	<u>0.65</u>	<u>1.06</u>	<u>7.10</u>						
	500	<u>0.74</u>	<u>0.86</u>	<u>1.08</u>	<u>1.31</u>	<u>7.10</u>				
	600	<u>0.58</u>	<u>1.08</u>	<u>7.10</u>						
	700	<u>0.58</u>	<u>0.77</u>	<u>0.65</u>	<u>1.15</u>	<u>7.10</u>				
BR.No.1		<u>0.65</u>	<u>0.77</u>	<u>0.82</u>	<u>0.92</u>	<u>0.98</u>	<u>1.08</u>	<u>1.20</u>	<u>1.31</u>	<u>7.10</u>
BR.No.3		<u>0.70</u>	<u>0.70</u>	<u>1.04</u>	<u>1.09</u>	<u>1.09</u>	<u>1.80</u>	<u>2.13</u>	<u>1.97</u>	<u>3.99</u>
BR.No.5		<u>0.50</u>	<u>0.86</u>	<u>0.70</u>	<u>1.31</u>	<u>0.92</u>	<u>1.42</u>	<u>1.75</u>	<u>1.53</u>	<u>1.58</u>
MS.No.1		<u>0.70</u>	<u>0.89</u>	<u>1.04</u>	<u>1.48</u>	<u>1.69</u>	<u>1.91</u>	<u>2.07</u>	<u>1.97</u>	<u>7.10</u>
MS.No.2		<u>0.86</u>	<u>1.37</u>	<u>0.58</u>	0	<u>0.15</u>	<u>0.65</u>	<u>0.82</u>	<u>7.10</u>	
MS.No.3		<u>0.30</u>	<u>0.70</u>	<u>0.89</u>	<u>1.09</u>	<u>1.06</u>	<u>1.09</u>	<u>7.10</u>		
MS.No.4		<u>0.65</u>	<u>1.20</u>	<u>1.09</u>	<u>1.04</u>	<u>7.10</u>				
AG.No.1		<u>1.42</u>	<u>2.57</u>	<u>2.51</u>	<u>2.30</u>	<u>0.65</u>	<u>7.10</u>			

Middle Quarters River Right bank

L.No.1, 400		<u>0.82</u>	<u>7.10</u>							
	500	<u>0.50</u>	<u>0.92</u>	<u>7.10</u>						

Table H-2 (5/5) AVERAGE CONE INDEX IN EACH 0.5 M LAYER

Site	0-0.5	-1.0	-1.5	-2.0	-2.5	-3.0	-3.5	-4.0	-4.5	-5.0
<u>Middle Quarters River Right bank (Cont'd)</u>										
L.No.1 600	<u>0.89</u>	<u>1.31</u>	1.75	1.69	1.69	7.10				
700	0.15	<u>0.82</u>	1.04	1.37	1.09	1.53	1.97	7.10		
800	0	<u>0.54</u>	0.77	0.74	0.77	0.89	1.15	1.04	0.98	1.09
900	0.15	0.30	0.58	0.54	0.70	0.58	0.58	0.40	0.70	0.98
1,000	0	0.30	0.54	0.54	0.65	0.58	0.70	0.70	0.54	0.89
1,100	<u>0.54</u>	0.15	0.50	0	0.30	0.54	0.65	0.58	0.54	0.70
1,200	0.30	0	0	0.30	0.74	0.50	0.70	0.54	0.70	0.92
1,300	<u>0.50</u>	<u>0.50</u>	0.40	0.40	0	0.40	0.40	0.40	0.40	0.40
MQ.No.2	<u>0.54</u>	0.15	0.54	0.54	0.50	0.65	0.74	0.58	0.70	0.74
MQ.No.7	<u>0.86</u>	<u>0.89</u>	1.06	0.77	0.58	0.65	0.74	0.58	0.82	0.92
<u>Black River Estuary</u>										
L.No.4, 100	0	0	0.40	0.74	0.65	0.77	0.82	0.92	0.74	0.86
197	0.40	<u>0.65</u>	0.74	1.08	2.24	7.10				
BL.No.7	0	0	0.50	0.54	0.30	0.30	0	0.30	0.65	0.98
BL.No.8	<u>0.65</u>	<u>0.98</u>	2.19	1.91	1.08	1.04	0.98	1.42	0.82	1.08
BL.No.9	<u>0.58</u>	0	0.30	0.50	1.69	1.20	0.89	0.82	1.58	0.86
BL.No.10	<u>0.58</u>	<u>0.82</u>	0.74	0.77	0.77	1.09	0.89	0.77	0.86	1.20
BL.No.11	0	0	0	0.15	0	0.50	0	0.30	0	0.30
MQ.No.5	<u>0.65</u>	0.30	0.50	0.40	0.54	0.54	0.40	0.58	0.65	0.77
MQ.No.6	0	0	0.50	0.40	0.54	0.50	0.40	0.50	0.54	0.65
BR.No.7	0	0	0.54	0.65	0.70	0.65	1.04	0.98	7.10	

Table H-3 (1/2) CLASSIFICATION OF BEARING CAPACITY
IN SWAMP AREA

Segment and Survey Site	Number of Survey Datum	Frequency			Number of Eligible Datum	Evalua- tion
		qc>0.5 within 1.0m	qc>1.0 within 2.0m	qc>7.0 within 5.0m		
Black R.						
Left Bank						
Line No. 5	9	3 - 2	3 - 0	3 - 0	2	<u>Eligible 23</u>
Line No. 6	18	6 - 6	6 - 6	6 - 5	17	Survey 33
Spots	4	2 - 2	2 - 1	2 - 1	4	70%
Total	33	11 - 10	11 - 7	11 - 6	23	(Good)
Styx R.						
Both Banks						
Line No. 11	15	5 - 5	5 - 5	5 - 5	15	<u>Eligible 18</u>
Spots	3	1 - 1	1 - 1	1 - 1	3	100%
Total	18	6 - 6	6 - 6	6 - 6	18	(very good)
Y.S. R.						
Left Bank						
Line No. 12	15	5 - 1	5 - 2	5 - 4	7	
Line No. 13	15	5 - 5	5 - 3	5 - 1	9	<u>Eligible 43</u>
Line No. 16	15	5 - 5	5 - 1	5 - 0	6	Survey 69
Spots	24	8 - 6	8 - 8	8 - 7	21	62%
Total	69	23 - 17	23 - 14	23 - 12	43	(No good)
Y.S. R.						
Right Bank						
Line No. 2	24	8 - 4	8 - 1	8 - 1	6	
Line No. 3	18	6 - 4	6 - 4	6 - 0	8	<u>Eligible 19</u>
Line No. 14	15	5 - 0	5 - 2	5 - 0	2	Survey 66
Spots	9	3 - 2	3 - 1	3 - 0	3	29%
Total	66	22 - 10	22 - 8	22 - 1	19	(Bad)

Table H-3 (2/2) CLASSIFICATION OF BEARING CAPACITY
IN SWAMP AREA

Segment and Survey Site	Number		Frequency			Number	
	of Survey Datum	qc>0.5	qc>1.0	qc>7.0	of Eligible Datum	Evalu- ation	
		within 1.0m	within 2.0m	within 5.0m			
Broad R.							
Right Bank							
Line No. 8	15	5 - 3	5 - 5	5 - 5	13		
Line No. 9	27	9 - 8	9 - 9	9 - 9	26	<u>Eligible 82</u>	
Line No. 10	18	6 - 6	6 - 5	6 - 6	17	Survey 87	
Line No. 15	15	5 - 4	5 - 5	5 - 5	14		
Spots	12	4 - 4	4 - 4	4 - 4	12	94%	
Total	87	29 -25	29 -28	29 - 29	82	(Very good)	
Broad R.							
Left Bank							
Line No. 17	21	7 - 7	7 - 7	7 - 7	21	<u>Eligible 43</u>	
Spots	24	8 - 8	8 - 7	8 - 7	22	96%	
Total	45	15 -15	15 -14	15 -14	43	(Very good)	
Black R.							
Estuary							
Spots	30	10 - 4	10 - 2	10 - 2	8	<u>Eligible 8</u> Survey 30 27%	
(Bad)							
M. Quarter R.							
Line No. 1	19	6 - 3	6 - 0	6 - 0	3	<u>Eligible 6</u> Survey 24	
Spots	6	2 - 2	2 - 1	2 - 0	3	25%	
Total	24	8 - 5	8 - 1	8 - 0	6	(Bad)	

Table H-4 PEAT THICKNESS OF EACH SEGMENT

Segment	Total Area ha	Peat Thickness								Remarks
		Less than 3 m		3 m to 6 m		More than 6 m		Max Depth		
		Area	Rate	Area	Rate	Area	Rate			
		ha	%	ha	%	ha	%	m		
Black R. Left Bank	760	608	80	137	18	15	2	7		
Styx R. Both Banks	410	402	98	8	2	0	0	5		
YS R. Right Bank	390	0	0	0	0	390	100	12		
" Left Bank	490	167	34	54	11	269	55	10		
Broad R. Right Bank	1,290	1,135	88	155	12	0	0	4		
" Left Bank	1,200	1,080	90	120	10	0	0	5		
M. Quarter R. Right B	660	46	7	343	52	271	41	10		
Black R. Estuary	1,460	993	68	321	22	146	10	11		
Total	6,660	4,431	67	1,138	17	1,091	16			

Table H-5 MOISTURE RATIO AND IGNITION LOSS

Sample No.	Moisture Ratio		Ignition Loss	Note
	Natural Dry	Complete Dry		
No. 1-300- 0-30	886	1,177	59.7	
-60-90	735	1,048	59.2	
300	768	1,174	37.4	
No. 1-350- 0-30	1,360	1,779	59.8	
90-200	863	1,145	67.2	
300	960	1,197	60.7	
No. 1-400- 0-30	1,196	1,620	62.6	
30-90	1,093	1,267	59.9	
No. 1-500-30-90	791	1,073	36.6	
No. 4-100-30-90	824	1,076	49.0	
No. 6-100- 0-30	829	1,176	44.8	
No. 6-500- 0-30	765	1,431	86.5	
-30-90	460	676	42.7	
No. 9-100-30-90	324	616	78.4	
No. 9-300- 0-30	650	1,497	40.3	
30-90	510	793	51.5	
No. 9-500- 0-30	820	1,304	70.2	
No. 9-700- 0-30	751	988	62.5	
30-90	701	924	76.4	
No. 9-900- 0-30	1,110	1,460	57.7	
30-90	1,079	1,832	53.2	
No. 11-100- 0-50	538	847	24.2	
No. 11-300- 0-50	533	777	67.3	
BL.No. 1 0-30	985	1,194	62.5	
BL.No. 3 0-30	798	1,630	37.0	
30-90	561	1,123	63.8	
BL.No. 5 0-30	548	860	48.1	
BR.No. 2 0-50	547	1,086	71.4	
BR.No. 4 50-100	709	1,190	59.5	
MQ.No. 2 50-100	803	1,650	31.3	
MS.No. 1 0-30	421	1,823	61.5	
MS.No. 3 0-30	373	1,387	65.8	
MS.No. 4 0-30	631	1,319	65.0	
AG.No. 1 0-30	400	709	42.3	
SX.No. 1 0-30	495	1,716	55.3	
Average	735	1,216	56.3	

TABLE H-6 SHRINKAGE OF PEAT SOIL

Survey Site	Long Side		Short Side		Height	
	Length	Ratio	Length	Ratio	Length	Ratio
	mm	%	mm	%	mm	%
	Original		Dimension			
	280		214		98	
Line No. 3,500m	255	8.9	191	10.7	72	26.5
No. 5,200m	207	26.1	171	20.1	68	30.6
No. 6,300m	253	9.6	188	12.1	83	15.3
No. 8,300m	255	8.9	195	8.9	86	12.2
No. 9,500m	243	13.2	183	14.5	68	30.6
No. 11,100m	259	7.5	204	4.7	91	7.1
No. 13,300m	252	10.0	192	10.3	75	23.5
No. 14,300m	255	8.9	185	13.6	82	16.3
No. 15,300m	256	8.6	188	12.1	86	12.2
Average	248	11.4	189	11.7	79	19.4

Table H-7 SELECTION OF RECLAIMABLE LAND

Segment	Bearing Capacity		Soil Property		Settlement		(Unit: %)
	Value	Category	Value	Category	Value	Category	
Black River Right Bank	100	I	IIpl	II	100	I	Suitable
Black River Left Bank	70	III	IVpr	III	80	II	Suitable
Styx River Both Banks	100	I	IVbr	IV	98	I	Suitable
Y.S. River Left Bank							
Upper reaches	78	III	IIIpl	III	100	I	Suitable
Lower reaches	50	V	Vbr	IV-V	52	V	Unsuitable
Total	62	IV	IIIpl-Vbr	III-V	34	V	Unsuitable
Y.S. River Right Bank	29	V	Vbr	V	0	V	Unsuitable
Broad River Right Bank	94	I	IIIr-IVbr	III-IV	88	II	Suitable
Broad River Left Bank	96	I	IVbr	IV	90	I	Suitable
Middle Quarter River Right Bank	25	V	Vbr	V	7	V	Unsuitable
Black River Estuary	27	V	Vbc	V	68	IV	Unsuitable

Table H-8 UNIT DRAINAGE DISCHARGE (IN MAY)

DESCRIPTION	UNIT	BLACK RIVER LEFT			BROAD RIVER BASIN	
		HOLLAND	HATFIELD	FRENCH./HOLIDAY. STYX		
Gross water requirement (Gr) mm/day		7.97	10.00	11.57	12.37	12.1
80% dependable rainfall (R) mm		185	117	117	117	105
ER for paddy field (ER) mm		139	88	88	88	79
(R-ER)/31 day	(ΔR) mm/day	1.48	0.94	0.94	0.94	0.84
Consumptive use (Cu) "		6.5	6.5	6.4	6.4	6.4
Gr + ΔR - ETC (Qlw) "		2.95	4.44	6.11	6.91	6.54
Present Gw in-flow (Gw.p) m ³ /sec		-	-	-	-	1.6
Increased Gw in-flow (Gw.i) "		-	-	-	-	1.9
Differential ¹⁾ (ΔGw) "		-	-	-	-	0.3
- do - (Gw) mm/day		-	-	-	-	1.30
Gr + ΔR - ETC + Gw (Qlw) "		-	-	-	-	7.84
Acreage (A) ha		990	300	500	400	2,000
Unit drainage discharge (Ql) × 10 ⁻⁴ m ³ /sec/ha		3.4	6.9			9.1

Note: 1) Differential in-flow between present and developed stage is recognized to flow into the Project area at the Broad River Basin and remains into the reserved area which is featured by blue-holes.

Table H-9 HOURLY RAINFALL AT HOLLAND STATION

Time	1st day			2nd day			3rd day							
	Hourly Rainfall	Accumulated Rainfall	Runoff Percent	Effective Rainfall	Time	Hourly Rainfall	Accumulated Rainfall	Runoff Percent	Effective Rainfall	Time	Hourly Rainfall	Accumulated Rainfall	Runoff Percent	Effective Rainfall
	1	1.45	1.45	0	0	25	3.00	69.00	50	1.50	49	0.53	204.53	90
2	1.45	2.90	0	0	26	3.00	72.00	50	1.50	50	0.53	205.06	90	0.48
3	1.54	4.44	0	0	27	3.20	75.20	50	1.60	51	0.56	205.62	90	0.50
4	1.63	6.07	0	0	28	3.39	78.59	50	1.70	52	0.59	206.21	90	0.53
5	1.71	7.78	0	0	29	3.59	82.18	50	1.80	53	0.62	206.83	90	0.56
6	1.80	9.58	0	0	30	3.78	85.96	50	1.89	54	0.65	207.48	90	0.59
7	2.05	11.63	10	0.21	31	4.30	90.26	50	2.15	55	0.75	208.23	90	0.68
8	2.30	13.93	10	0.23	32	4.82	95.08	50	2.41	56	0.84	209.07	90	0.76
9	2.55	16.48	10	0.26	33	5.33	100.41	80	4.26	57	0.94	210.01	90	0.85
10	2.80	19.28	10	0.28	34	5.85	106.26	80	4.68	58	1.03	211.04	90	0.93
11	3.78	23.06	10	0.38	35	7.91	114.17	80	6.33	59	1.39	212.43	90	1.25
12	4.77	27.83	10	0.48	36	9.97	124.14	80	7.98	60	1.74	214.17	90	1.57
13	5.75	33.58	30	1.73	37	12.02	136.16	80	9.62	61	2.10	216.27	90	1.89
14	6.73	40.31	30	2.02	38	14.08	150.24	80	11.26	62	2.45	218.72	90	2.21
15	5.59	45.90	30	1.68	39	11.68	161.92	80	9.34	63	2.03	220.75	90	1.83
16	4.44	50.34	50	2.22	40	9.28	171.20	80	7.42	64	1.62	222.37	90	1.46
17	3.30	53.64	50	1.65	41	6.88	178.08	80	5.50	65	1.20	223.57	90	1.08
18	2.15	55.79	50	1.08	42	4.48	182.56	80	3.58	66	0.78	224.35	90	0.70
19	2.01	57.80	50	1.01	43	4.19	186.75	80	3.34	67	0.73	225.08	90	0.66
20	1.87	59.67	50	0.94	44	3.91	190.66	80	3.13	68	0.68	225.76	90	0.61
21	1.72	61.39	50	0.86	45	3.62	194.28	80	2.90	69	0.63	226.39	90	0.57
22	1.58	62.97	50	0.79	46	3.33	197.61	80	2.66	70	0.58	226.97	90	0.52
23	1.52	64.49	50	0.76	47	3.20	200.81	90	2.88	71	0.52	227.49	90	0.47
24	1.51	66.00	50	0.76	48	3.19	204.00	90	2.87	72	0.51	228.00	90	0.46
Total	66.00			17.34		138.00			102.30		24.00			21.64

Estimating Runoff Coefficient $f = 141.28 / 228.0 = 0.62$

Table H-10 HOURLY RAINFALL AT LACOVIA STATION

Time	1st day			2nd day			3rd day							
	Hourly Rainfall	Accumulated Rainfall	Runoff Percent	Effective Rainfall	Time	Hourly Rainfall	Accumulated Rainfall	Runoff Percent	Effective Rainfall	Time	Hourly Rainfall	Accumulated Rainfall	Runoff Percent	Effective Rainfall
1	1.30	1.30	0	0	25	3.65	63.65	50	1.83	49	0.63	227.63	90	0.57
2	1.30	2.60	0	0	26	3.65	67.30	50	1.83	50	0.63	228.26	90	0.57
3	1.39	3.99	0	0	27	3.89	71.19	50	1.95	51	0.68	228.94	90	0.61
4	1.48	5.47	0	0	28	4.12	75.31	50	2.06	52	0.72	229.66	90	0.65
5	1.57	7.04	0	0	29	4.35	79.66	50	2.18	53	0.76	230.42	90	0.68
6	1.65	8.69	0	0	30	4.58	84.24	50	2.29	54	0.80	231.22	90	0.72
7	1.87	10.56	10	0.19	31	5.20	89.44	50	2.60	55	0.91	232.13	90	0.82
8	2.09	12.65	10	0.21	32	5.82	95.26	50	2.91	56	1.02	233.15	90	0.92
9	2.31	14.96	10	0.23	33	6.44	101.70	80	5.15	57	1.13	234.28	90	1.02
10	2.53	17.49	10	0.25	34	7.05	108.75	80	5.64	58	1.23	235.51	90	1.11
11	3.43	20.92	10	0.34	35	9.55	118.30	80	7.64	59	1.66	237.17	90	1.49
12	4.33	25.25	10	0.43	36	12.05	130.35	80	9.64	60	2.09	239.26	90	1.88
13	5.23	30.48	30	1.57	37	14.55	144.90	80	11.64	61	2.52	241.78	90	2.27
14	6.13	36.61	30	1.84	38	17.05	161.95	80	13.64	62	2.95	244.73	90	2.66
15	5.09	41.70	30	1.53	39	14.15	176.10	80	11.32	63	2.45	247.18	90	2.21
16	4.04	45.74	30	1.21	40	11.24	187.34	80	8.99	64	1.95	249.13	90	1.76
17	3.00	48.74	30	0.90	41	8.34	195.68	80	6.67	65	1.45	250.58	90	1.31
18	1.95	50.69	50	0.98	42	5.43	201.11	90	4.89	66	0.95	251.53	90	0.86
19	1.83	52.52	50	0.92	43	5.08	206.19	90	4.57	67	0.89	252.42	90	0.80
20	1.70	54.22	50	0.85	44	4.72	210.91	90	4.25	68	0.83	253.25	90	0.75
21	1.58	55.80	50	0.79	45	4.36	215.27	90	3.92	69	0.77	254.02	90	0.69
22	1.45	57.25	50	0.73	46	4.00	219.27	90	3.60	70	0.70	254.72	90	0.63
23	1.38	58.63	50	0.69	47	3.87	223.14	90	3.48	71	0.65	255.37	90	0.59
24	1.37	60.00	50	0.69	48	3.86	227.00	90	3.47	72	0.63	256.00	90	0.57
Total	60.00			14.35		167.00			126.16		29.00			26.14

Estimating Runoff Coefficient $f = 166.65 / 256 = 0.65$

Table H-11 HOURLY RAINFALL AT BURNT SAVANNA STATION

Time	1st day			2nd day			3rd day						
	Hourly Rainfall	Accumulated Rainfall	Effective Percent Rainfall	Time	Hourly Rainfall	Accumulated Rainfall	Effective Percent Rainfall	Time	Hourly Rainfall	Accumulated Rainfall	Effective Percent Rainfall		
1	1.30	1.30	0	0	2.50	62.50	50	1.25	49	0.52	175.52	80	0.42
2	1.30	2.60	0	0	2.50	65.00	50	1.25	50	0.53	176.05	80	0.42
3	1.39	3.79	0	0	2.67	67.67	50	1.34	51	0.56	176.61	80	0.45
4	1.48	5.47	0	0	2.83	70.50	50	1.42	52	0.59	177.20	80	0.47
5	1.57	7.04	0	0	2.99	73.49	50	1.50	53	0.62	177.82	80	0.50
6	1.65	8.69	0	0	3.15	76.64	50	1.58	54	0.65	178.47	80	0.52
7	1.87	10.56	10	0.19	3.59	80.23	50	1.80	55	0.75	179.22	90	0.60
8	2.09	12.65	10	0.21	4.02	84.25	50	2.01	56	0.84	180.06	80	0.67
9	2.31	14.96	10	0.23	4.45	88.70	50	2.23	57	0.94	181.00	80	0.75
10	2.53	17.49	10	0.25	4.88	93.58	50	2.44	58	1.03	182.03	80	0.82
11	3.43	20.92	10	0.34	6.60	100.18	80	5.28	59	1.39	183.42	80	1.11
12	4.33	25.25	10	0.43	8.31	108.49	80	6.65	60	1.74	185.16	80	1.39
13	5.23	30.48	30	1.57	10.02	118.51	80	8.02	61	2.10	187.26	80	1.68
14	6.13	36.61	30	1.84	11.73	130.24	80	9.38	62	2.45	189.71	80	1.96
15	5.09	41.70	30	1.53	9.73	139.97	80	7.78	63	2.04	191.75	80	1.63
16	4.04	45.74	30	1.21	7.73	147.70	80	6.18	64	1.62	193.37	80	1.30
17	3.00	48.74	30	0.90	5.73	153.43	80	4.58	65	1.20	194.57	80	0.96
18	1.95	50.69	50	0.98	3.73	157.16	80	2.98	66	0.78	195.35	80	0.62
19	1.83	52.52	50	0.92	3.50	160.66	80	2.80	67	0.73	196.08	80	0.58
20	1.70	54.22	50	0.85	3.26	163.92	80	2.61	68	0.68	196.76	80	0.54
21	1.58	55.80	50	0.79	3.02	166.94	80	2.42	69	0.63	197.39	80	0.50
22	1.45	57.25	50	0.73	2.78	169.72	80	2.22	70	0.58	197.97	80	0.46
23	1.38	58.63	50	0.69	2.65	172.37	80	2.12	71	0.52	198.49	80	0.42
24	1.37	60.00	50	0.69	2.63	175.00	80	2.10	72	0.51	199.00	80	0.41
Total	60.00			14.35	115.00			81.94		24.00			19.18

Estimating Runoff Coefficient $f = 115.47 / 199 = 0.58$

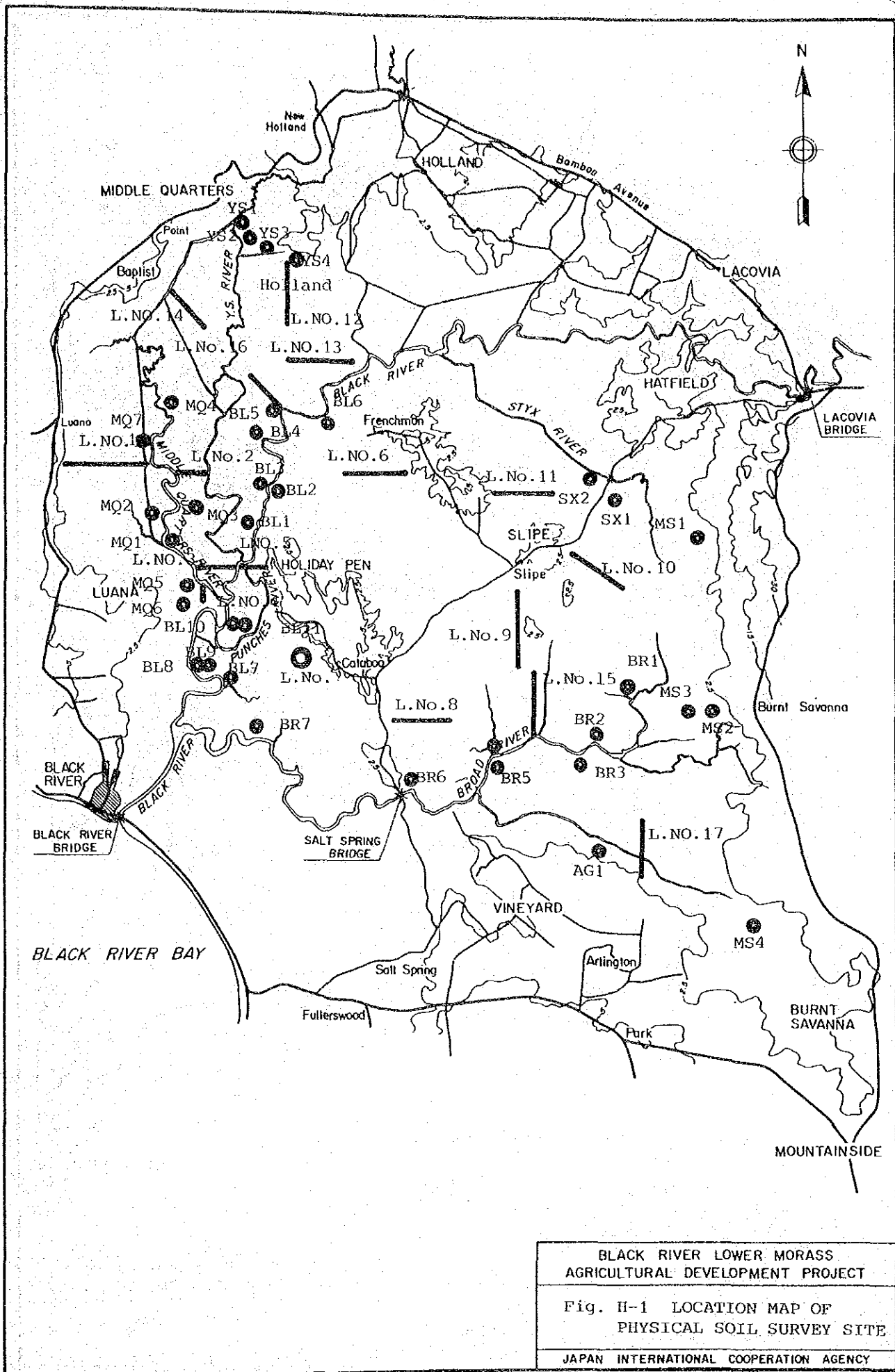
Table H-12 ALTERNATIVE CASE STUDY FOR SPECIFICATIONS OF DRAINAGE PUMPS

Pump Station	Alternative Case	Design Discharge (m ³ /sec)	Peak Discharge (m ³ /sec)	Inundated Duration (hours)	
				GLa.	WLa.
Holland	I: Ø700 mm x 3 sets	3.5	4.0	83	63
	II: Ø700 mm x 4 sets	4.7	5.4	60	44
	III: Ø800 mm x 3 sets	4.5	5.2	61	46
Black River Left	I: Ø700 mm x 5 sets	5.8	6.8	110*	64*
	II: Ø700 mm x 6 sets	7.0	8.1	96	50*
	III: Ø800 mm x 5 sets	7.5	8.7	86	45
Broad River Right	I: Ø700 mm x 4 sets	4.7	5.2	110*	26
	II: Ø700 mm x 5 sets	5.8	6.5	84	0
	III: Ø800 mm x 4 sets	6.0	6.7	75	0
Broad River Left	I: Ø700 mm x 3 sets	3.5	3.9	115*	28
	II: Ø700 mm x 4 sets	4.7	5.2	76	0
	III: Ø800 mm x 3 sets	4.5	5.0	81	0

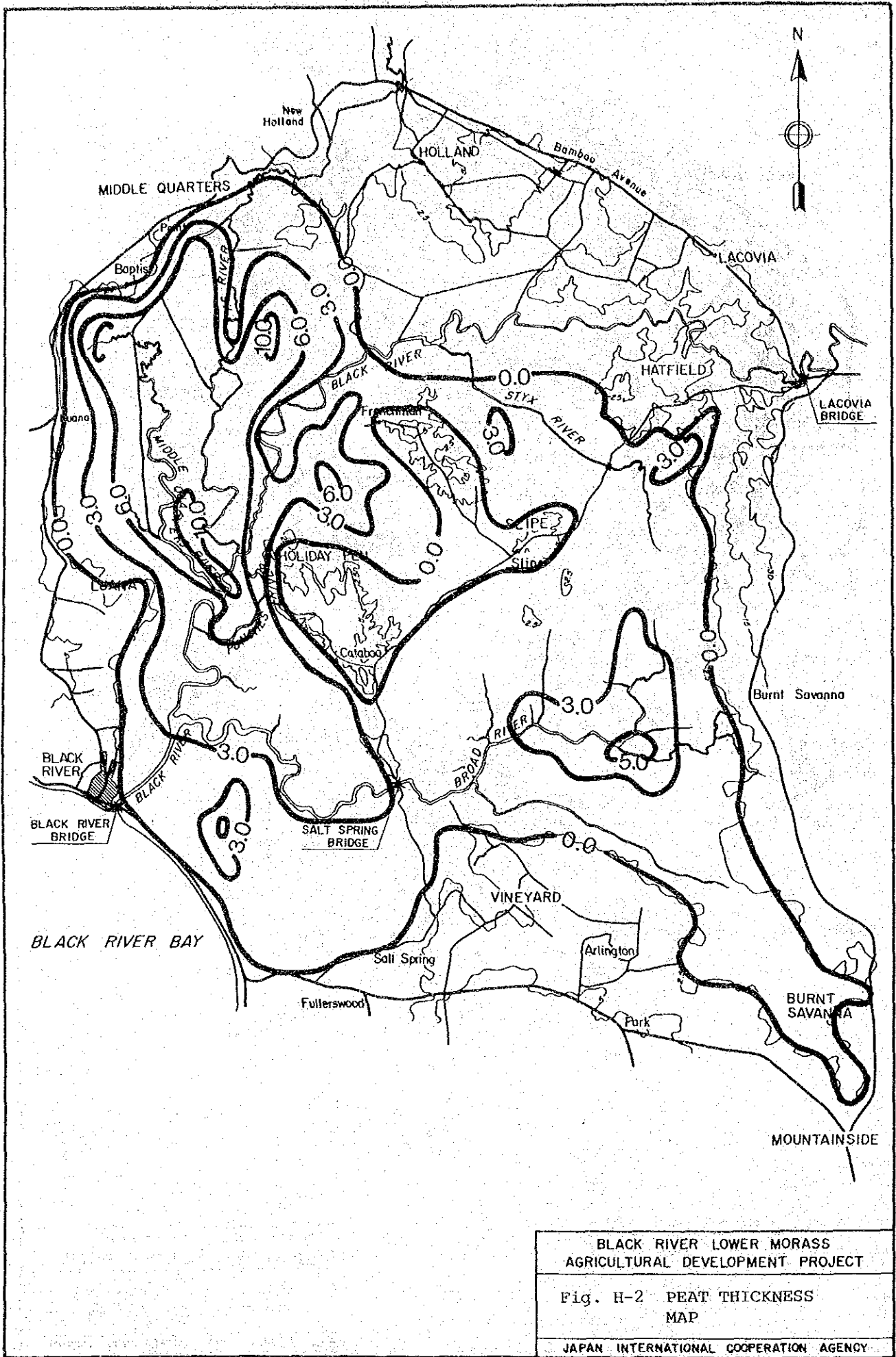
Remarks: WLa.: Inundation duration over Allowable inundation water level.

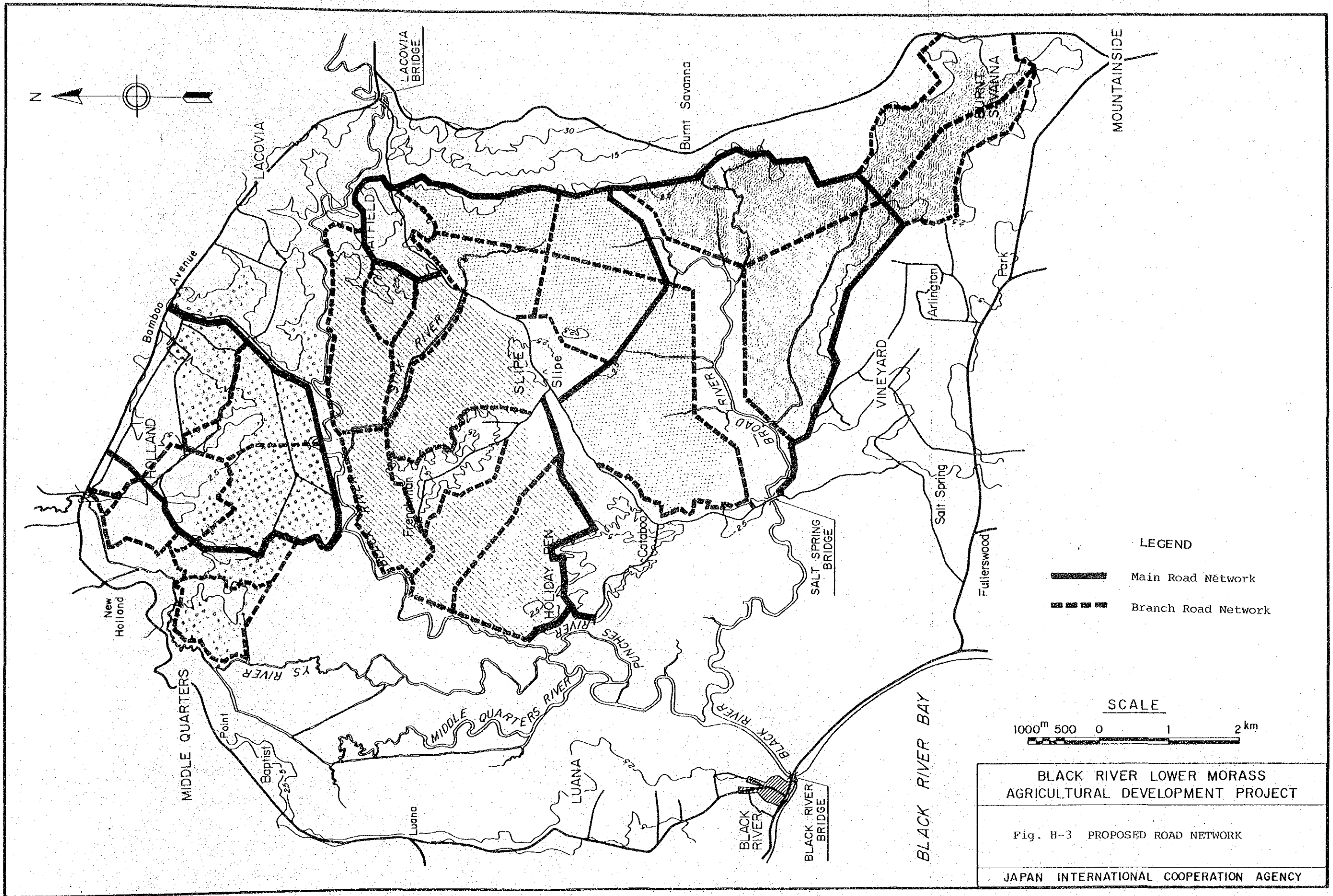
GLa.: Inundation duration over Datum ground elevation.

*: Shortage of pump capacity

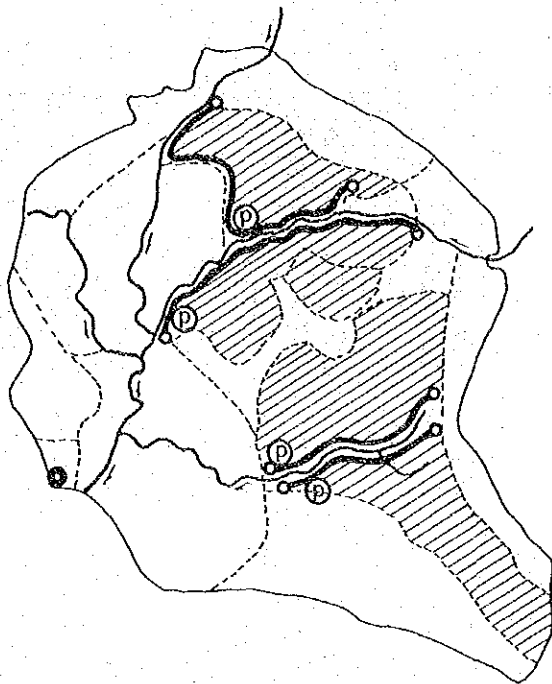


BLACK RIVER LOWER MORASS
 AGRICULTURAL DEVELOPMENT PROJECT
 Fig. H-1 LOCATION MAP OF
 PHYSICAL SOIL SURVEY SITE
 JAPAN INTERNATIONAL COOPERATION AGENCY

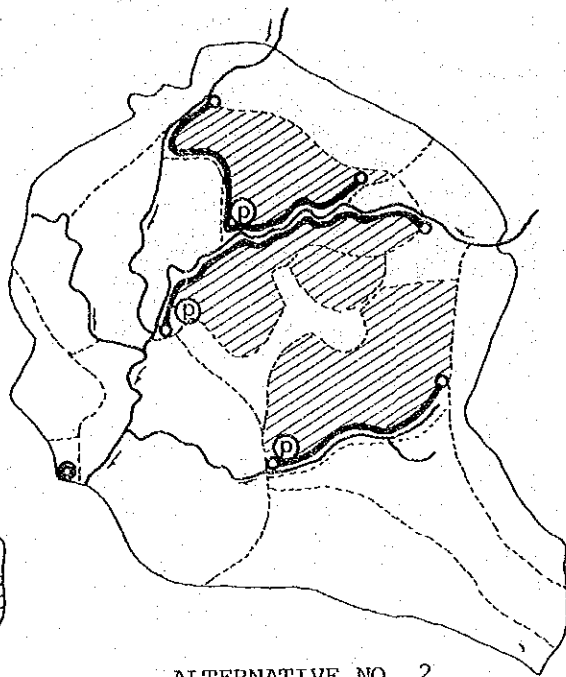




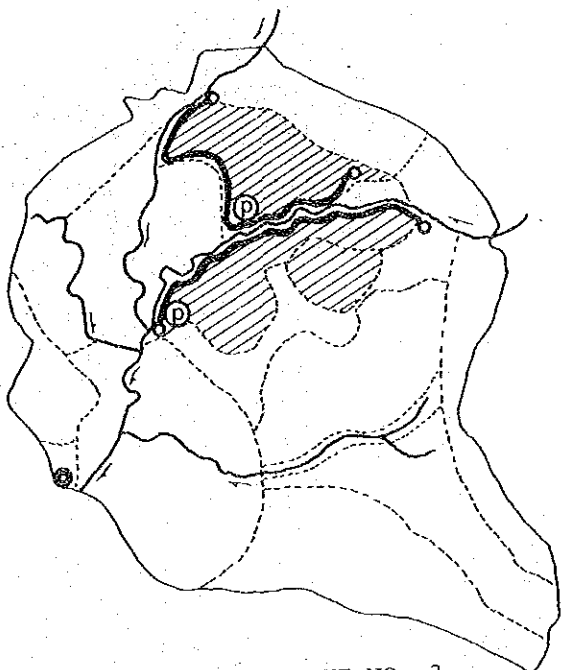
**BLACK RIVER LOWER MORASS
 AGRICULTURAL DEVELOPMENT PROJECT**
 Fig. H-3 PROPOSED ROAD NETWORK
 JAPAN INTERNATIONAL COOPERATION AGENCY



ALTERNATIVE NO. 1



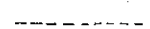

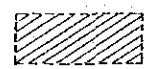


ALTERNATIVE NO. 2



ALTERNATIVE NO. 3

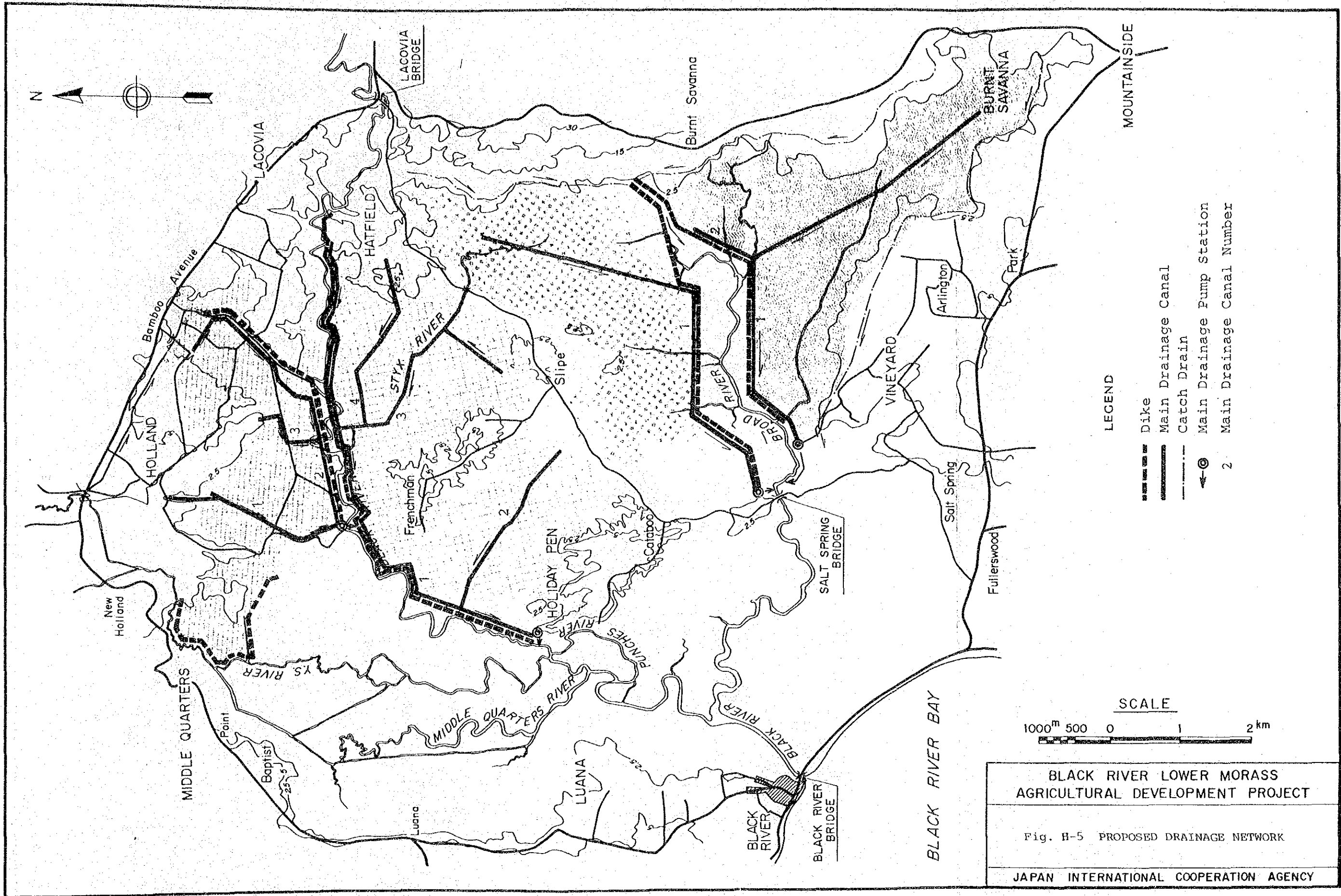
LEGEND

-  RIVER
-  EMBANKMENT
-  SEGMENT BORDER
-  DRAINAGE PUMP STATION
-  SEGMENT PROPOSED DEVELOPMENT

BLACK RIVER LOWER MORASS
AGRICULTURAL DEVELOPMENT PROJECT

Fig. H-4 ALTERNATIVE PLANS

JAPAN INTERNATIONAL COOPERATION AGENCY



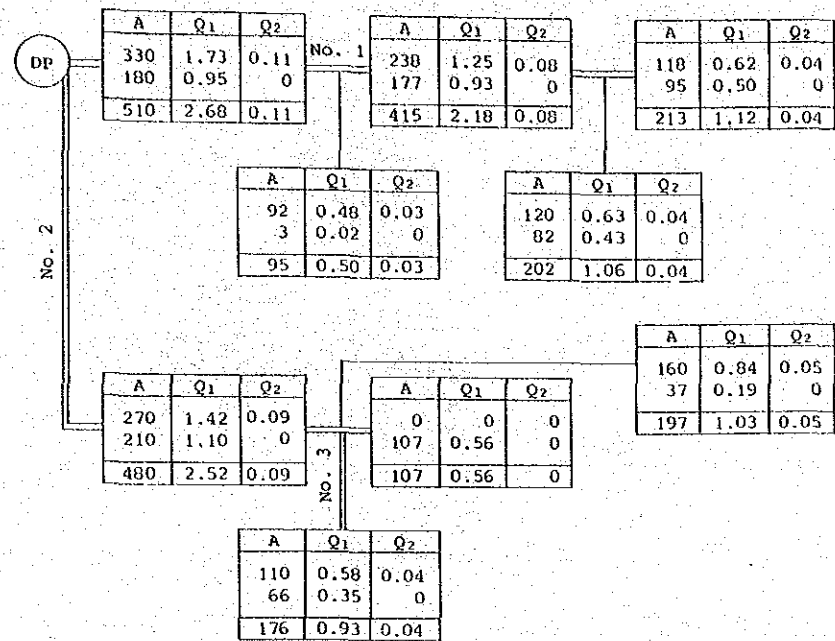
BLACK RIVER LOWER MORASS
 AGRICULTURAL DEVELOPMENT PROJECT

Fig. H-5 PROPOSED DRAINAGE NETWORK

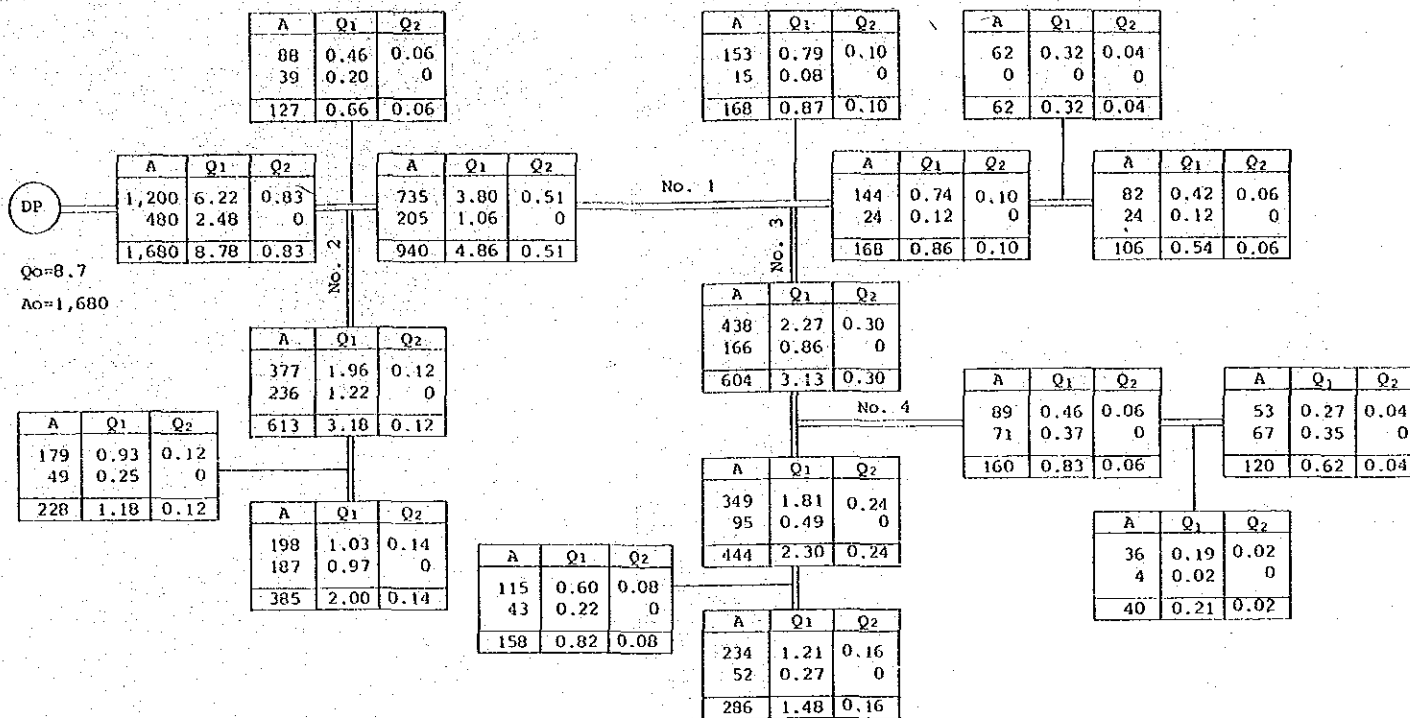
JAPAN INTERNATIONAL COOPERATION AGENCY

HOLLAND AREA

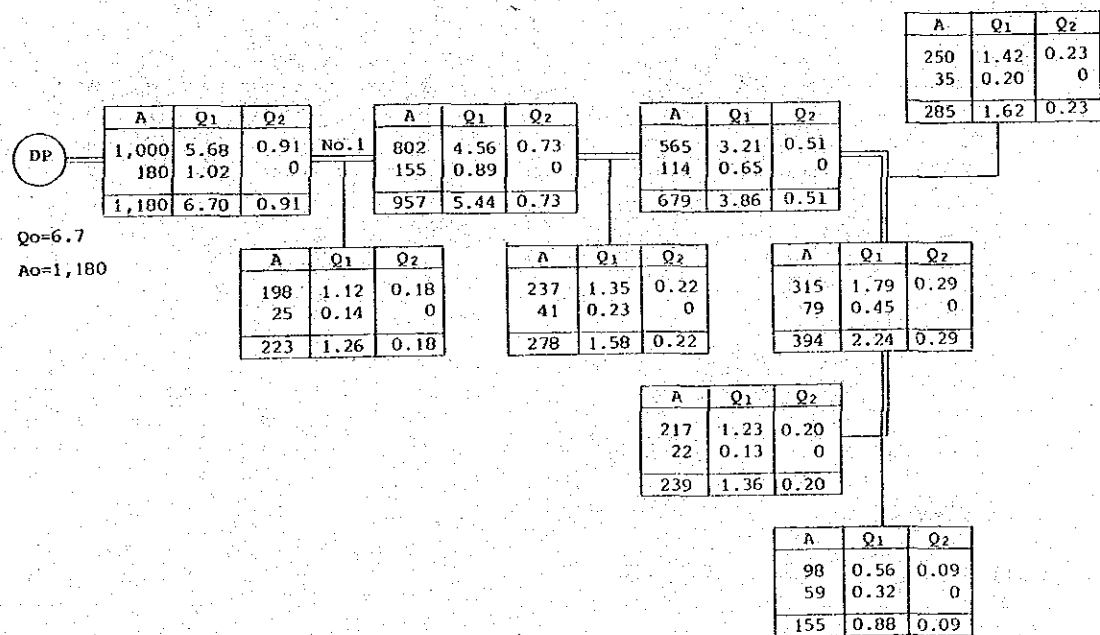
Q₀=5.2
A₀=990



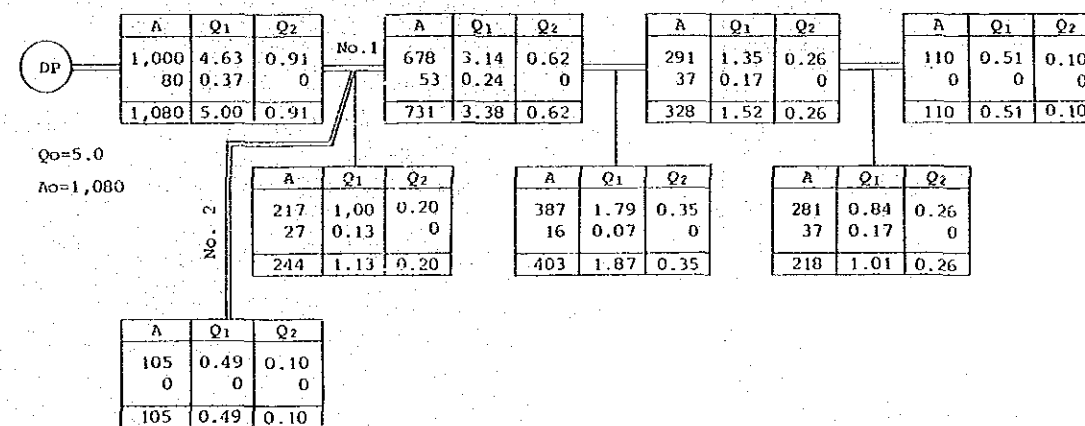
BLACK RIVER LEFT BANK AREA



BROAD RIVER RIGHT BANK AREA



BROAD RIVER LEFT BANK AREA



LEGEND

- 1)

A	Q ₁	Q ₂
Paddy Fields		
Others		
Total		
- 2) A: Water-shed Acreage (ha)
Q₁: Flood Discharge (m³/sec)
Q₂: Low Water Discharge (m³/sec)
- 3)

DP

: Drainage Pump Station
No. 1: Main Drainage Canal and canal Number
 ---: Group of Lateral Drains

Notes

Unit Area Drainage Discharge

$$Q_1 = Q_0 \times (A/A_0) \text{ m}^3/\text{sec}$$

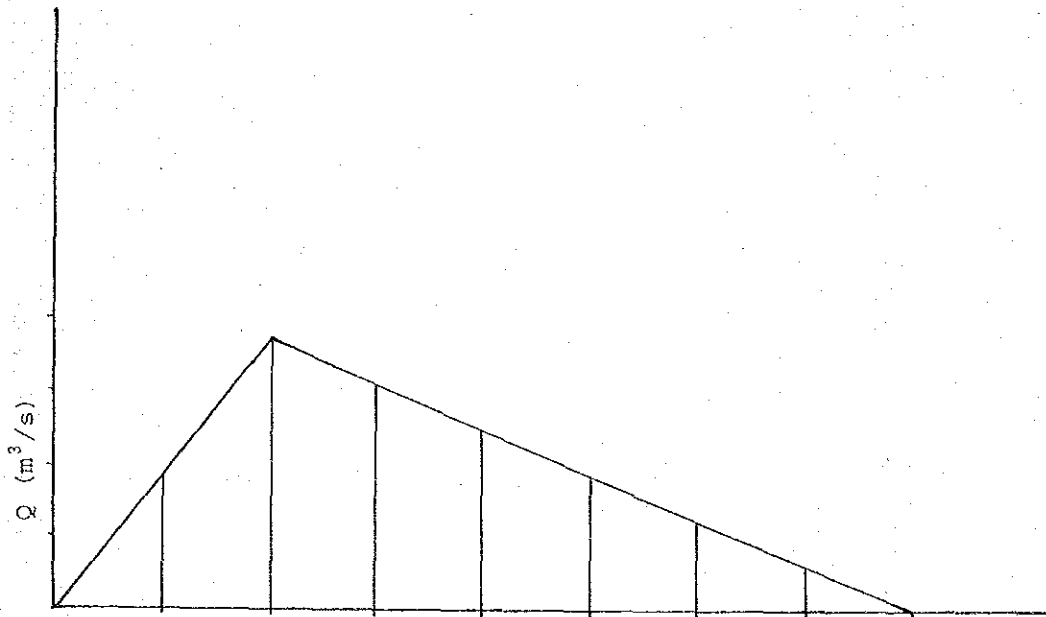
$$Q_2 = 3.4 \times 10^{-4} \text{ m}^3/\text{sec/ha in Holand}$$

- 6.9 x " in Black Left
- 9.1 x " in Broad Right
- 9.1 x " in Broad Left

BLACK RIVER LOWER MORASS
AGRICULTURAL DEVELOPMENT PROJECT

Fig. H-6 DIAGRAM OF PROPOSED DRAINAGE NETWORK

JAPAN INTERNATIONAL COOPERATION AGENCY

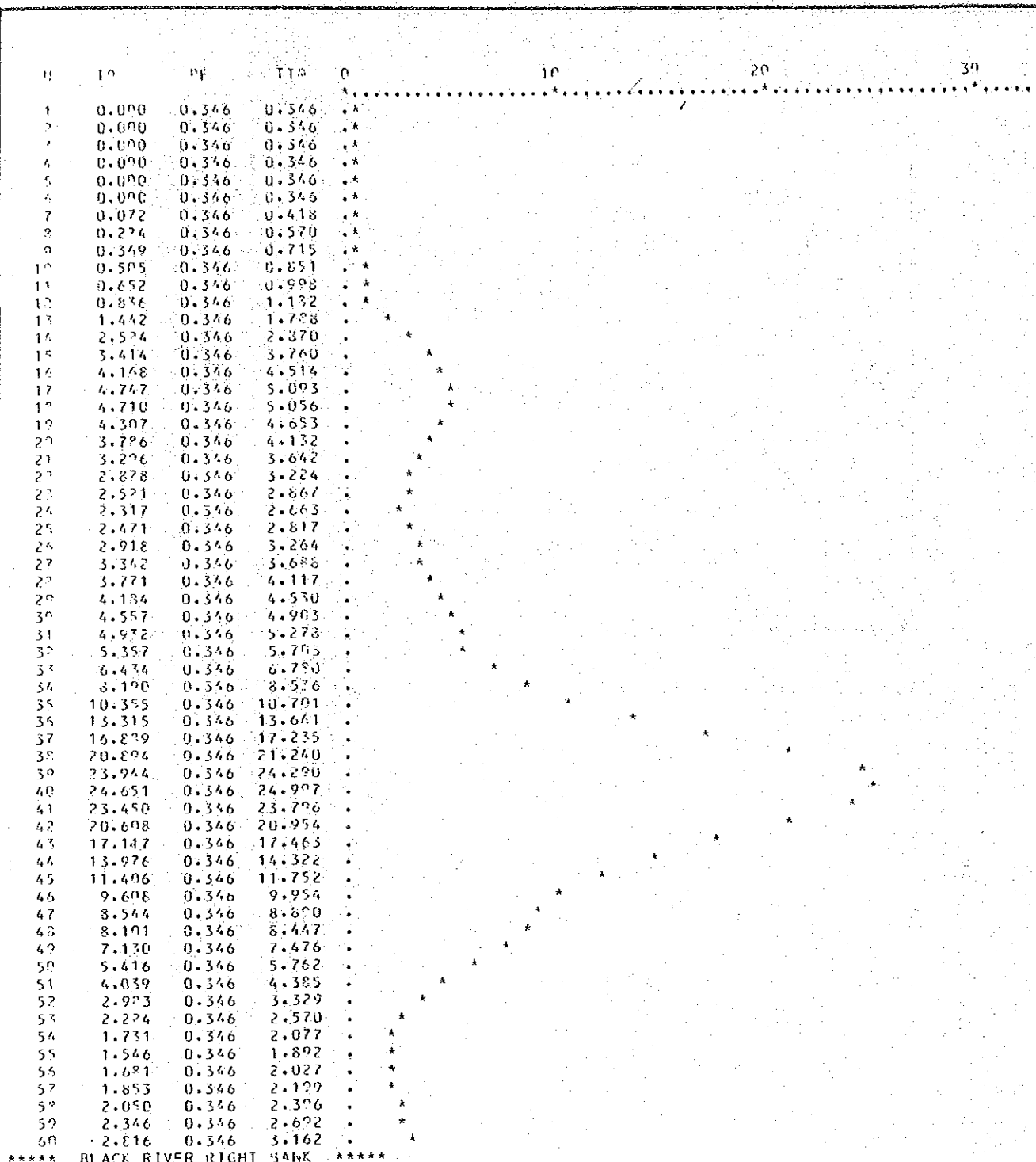


BROAD RIVER LEFT BANK	BROAD RIVER RIGHT BANK	BLACK RIVER LEFT BANK	HOLLAND
0.000	0.000	0.000	0.000
0.375	0.410	0.584	0.345
0.749	0.821	1.168	0.690
0.624	0.684	0.973	0.575
0.500	0.547	0.779	0.460
0.375	0.410	0.584	0.345
0.250	0.274	0.389	0.230
0.125	0.137	0.295	0.115
0.000	0.000	0.000	0.000

BLACK RIVER LOWER MORASS
AGRICULTURAL DEVELOPMENT PROJECT

Fig. H-7 UNIT HYDROGRAPH FOR
EACH BLOCK

JAPAN INTERNATIONAL COOPERATION AGENCY

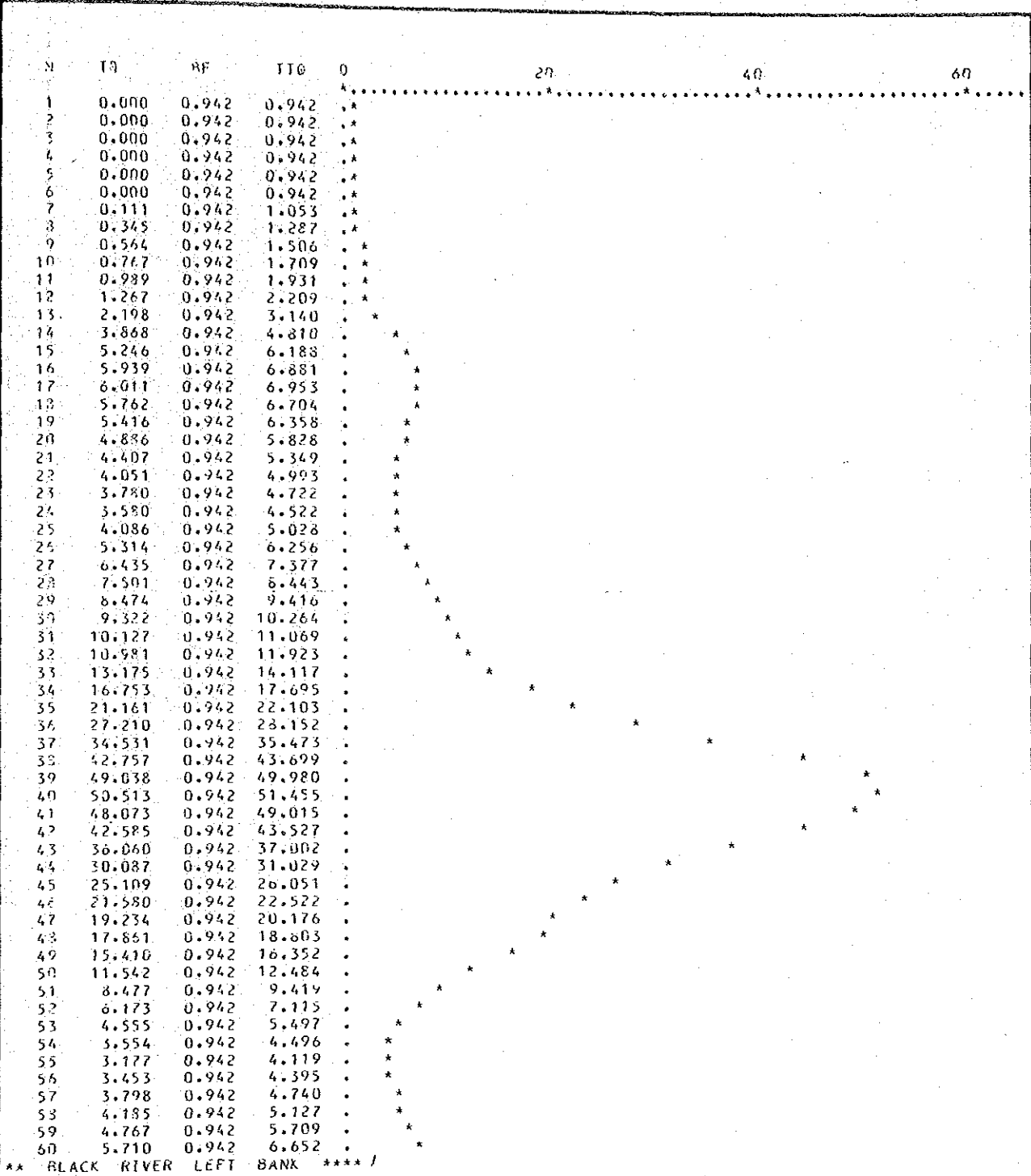


***** BLACK RIVER RIGHT BANK *****

LEGEND

- N - Time
- TQ - Direct Runoff
- BF - Base Flow
- TTQ - Total Runoff Discharge

BLACK RIVER LOWER MORASS AGRICULTURAL DEVELOPMENT PROJECT
Fig. H-8. HYDROGRAPH -BLACK RIVER RIGHT BANK-
JAPAN INTERNATIONAL COOPERATION AGENCY

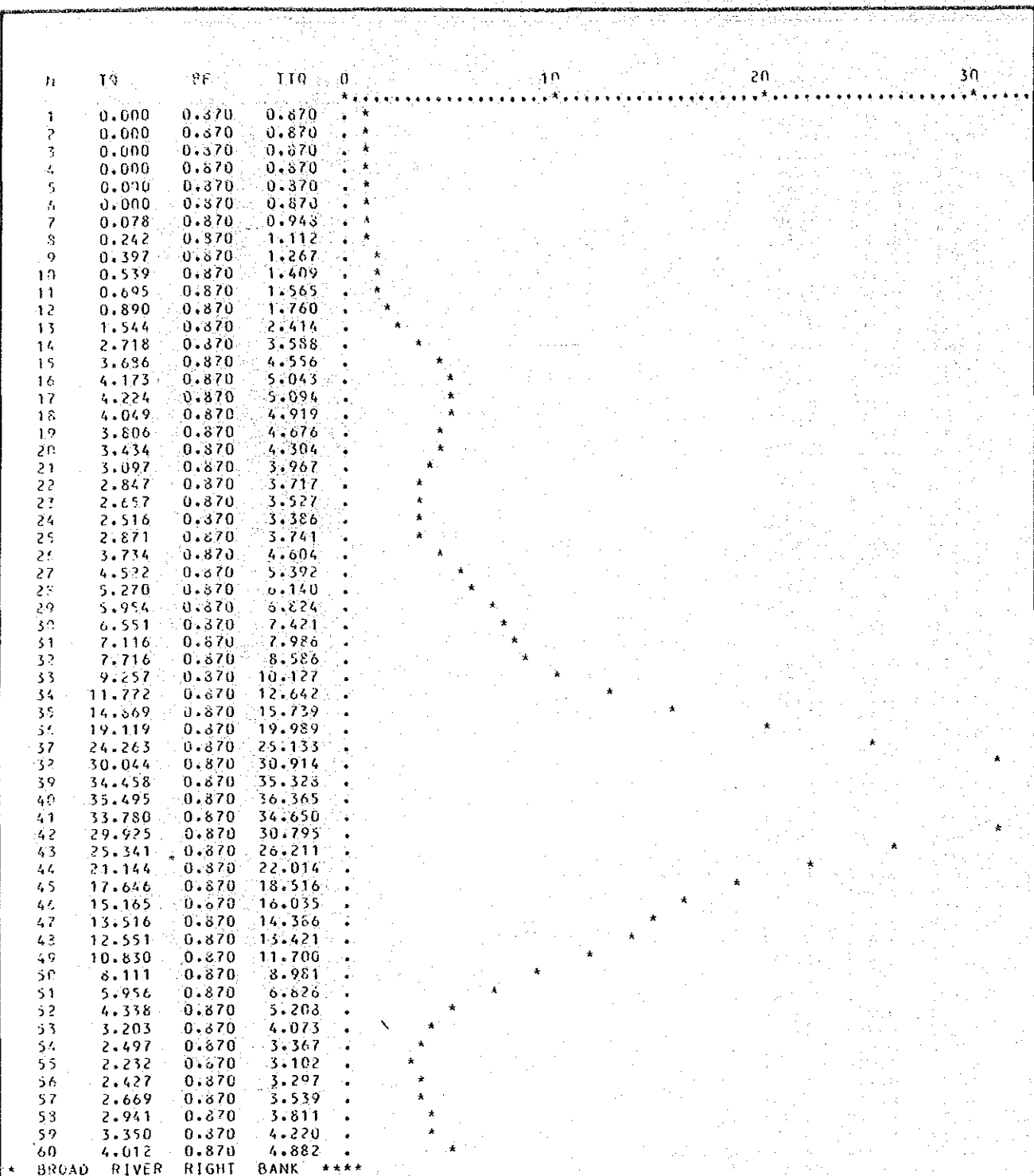


** BLACK RIVER LEFT BANK **** /

LEGEND

- N - Time
- TQ - Direct Runoff
- BF - Base Flow
- TTQ - Total Runoff Discharge

BLACK RIVER LOWER MORASS AGRICULTURAL DEVELOPMENT PROJECT
Fig. H-9 HYDROGRAPH -BLACK RIVER LEFT BANK-
JAPAN INTERNATIONAL COOPERATION AGENCY

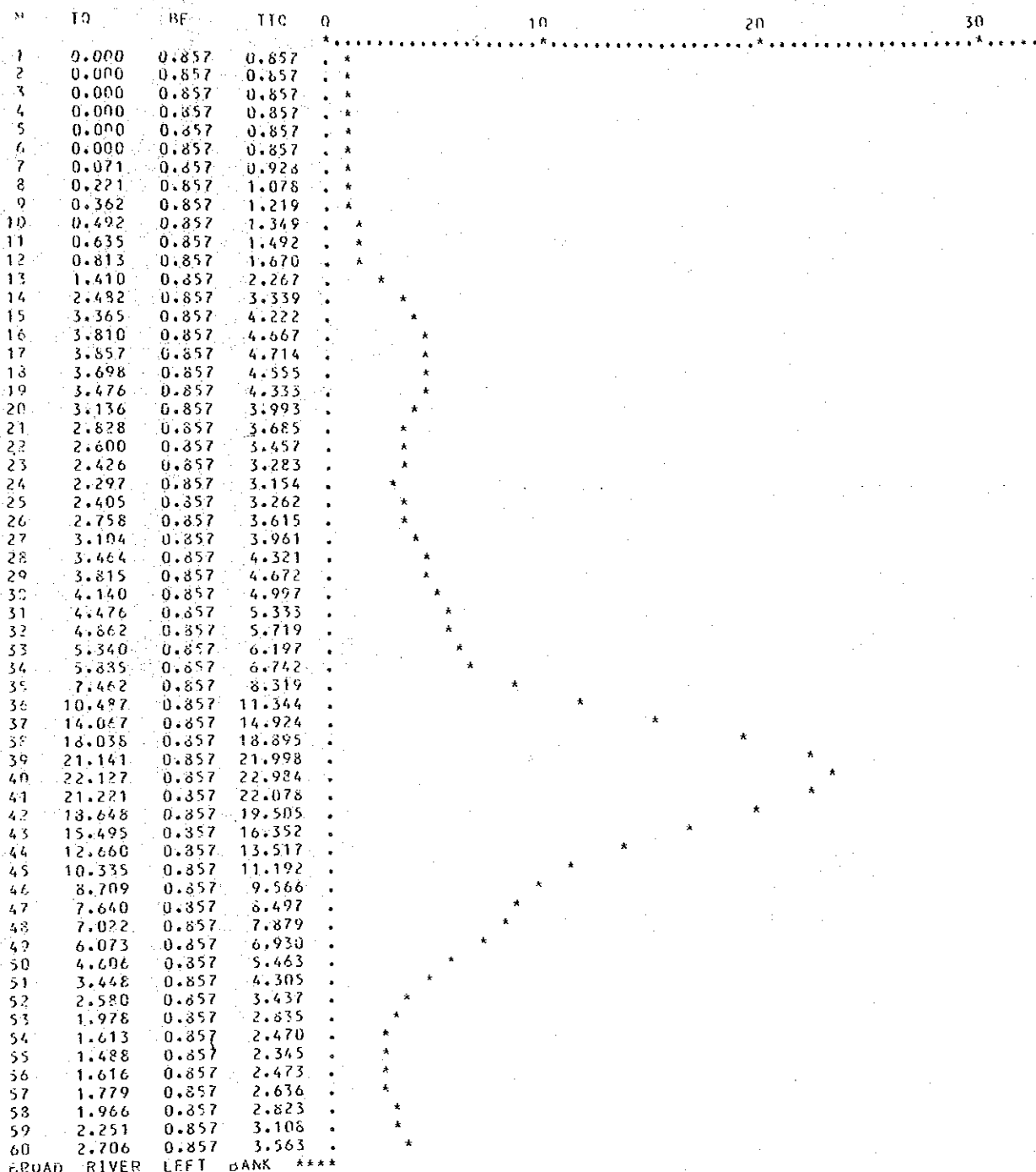


* BROAD RIVER RIGHT BANK ****

LEGEND

- N - Time
- TQ - Direct Runoff
- BF - Base Flow
- TTQ - Total Runoff Discharge

BLACK RIVER LOWER MORASS AGRICULTURAL DEVELOPMENT PROJECT
Fig. H-10 HYDROGRAPH -BROAD RIVER RIGHT BANK-
JAPAN INTERNATIONAL COOPERATION AGENCY



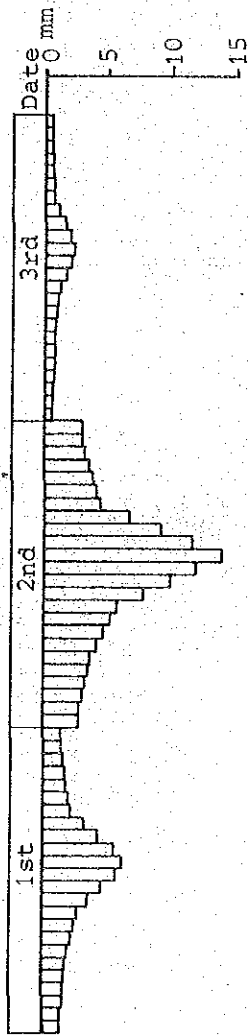
** BROAD RIVER LEFT BANK ****

LEGEND

- N - Time
- TQ - Direct Runoff
- BF - Base Flow
- TTQ - Total Runoff Discharge

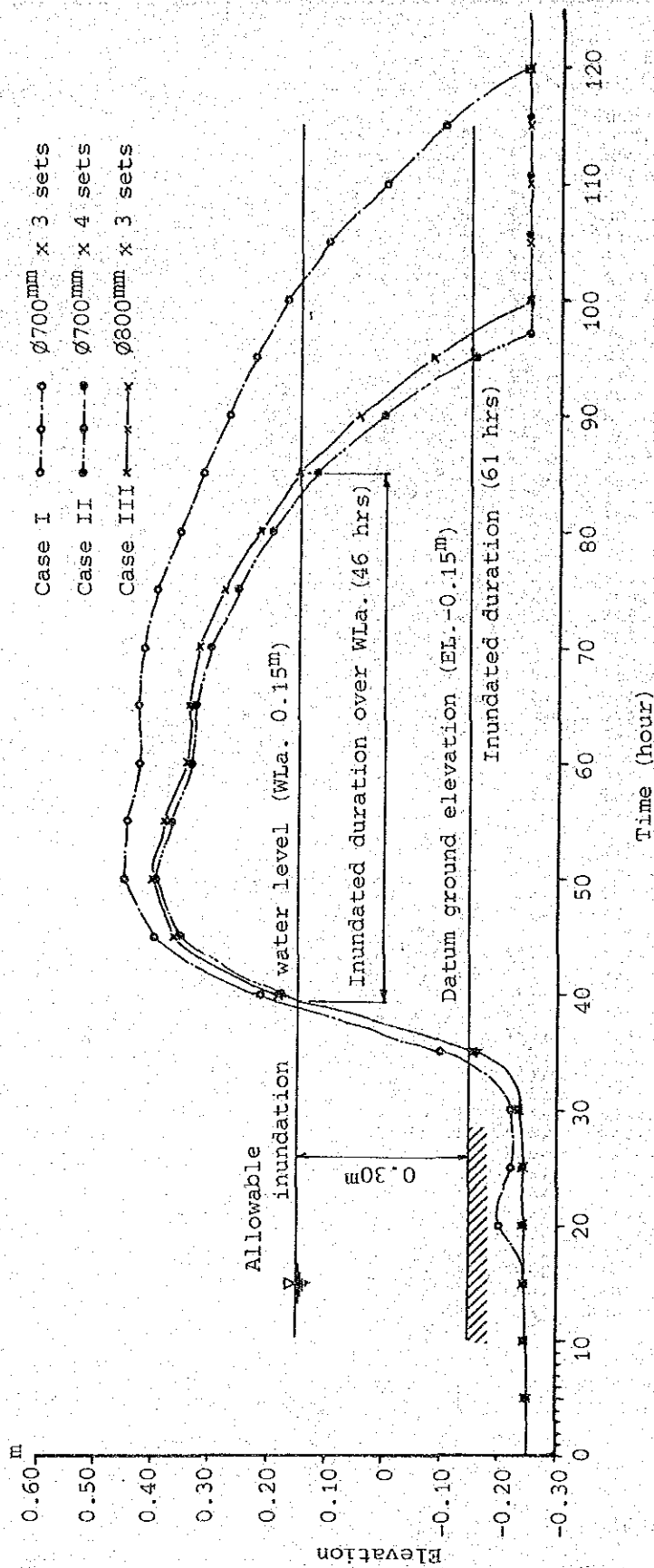
BLACK RIVER LOWER MORASS AGRICULTURAL DEVELOPMENT PROJECT
Fig. H-11 HYDROGRAPH -BROAD RIVER LEFT BANK-
JAPAN INTERNATIONAL COOPERATION AGENCY

Design Rainfall



Alternative Case

- Case I ○---○ $\phi 700\text{mm} \times 3$ sets
- Case II ●---● $\phi 700\text{mm} \times 4$ sets
- Case III ×---× $\phi 800\text{mm} \times 3$ sets

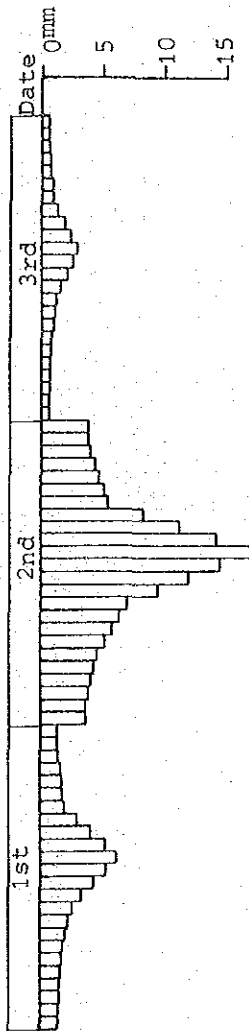


BLACK RIVER LOWER MORASS
AGRICULTURAL DEVELOPMENT PROJECT

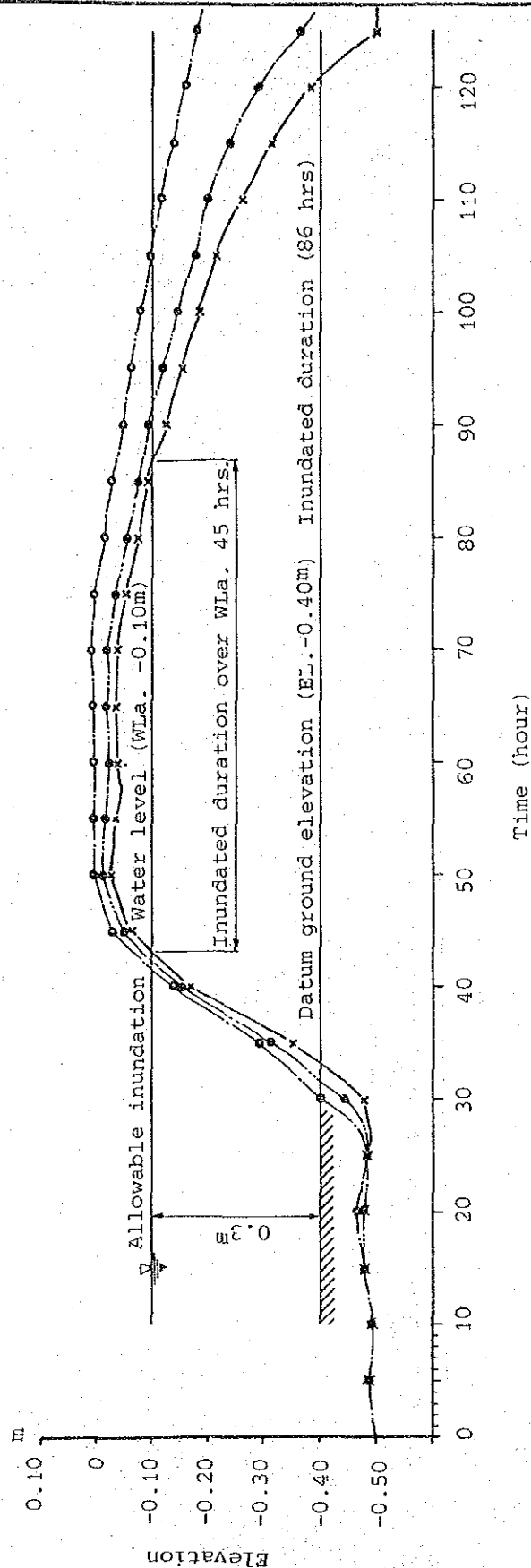
Fig. H-12 INUNDATION CURVE
- HOLLAND AREA -

JAPAN INTERNATIONAL COOPERATION AGENCY

Design Rainfall

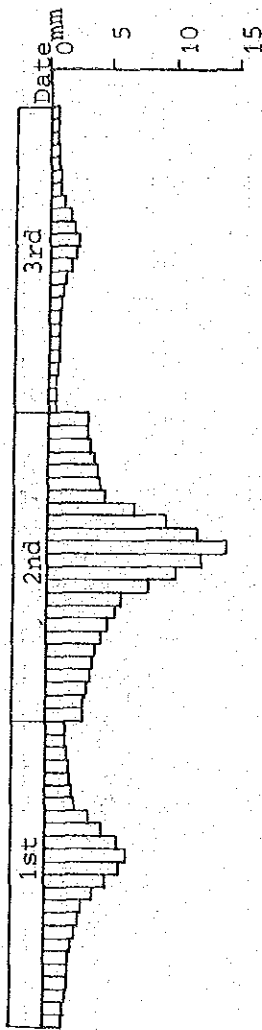


- Alternative Case
- Case I ○---○---○ 700mm x 5 sets
 - Case II ●---●---● 700mm x 6 sets
 - Case III ×---×---× 800mm x 5 sets



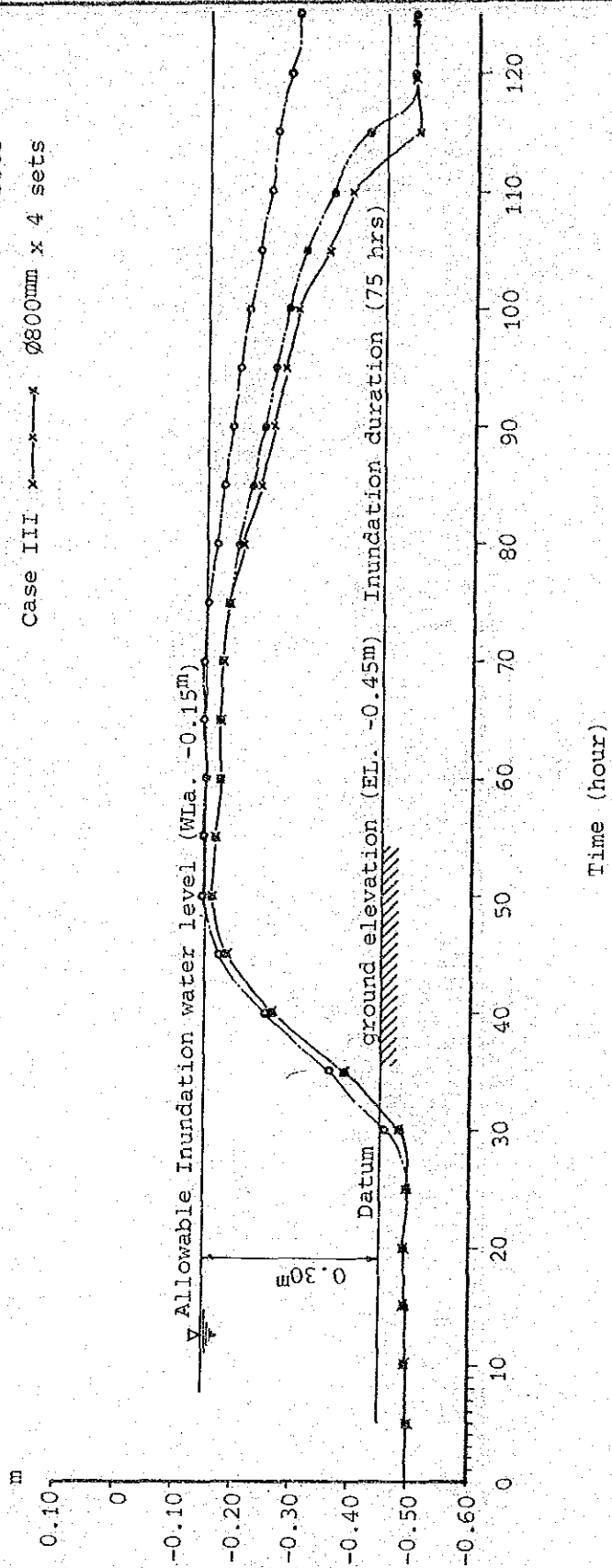
BLACK RIVER LOWER MORASS
 AGRICULTURAL DEVELOPMENT PROJECT
 Fig. H-13 INUNDATION CURVE
 - BLACK RIVER LEFT BANK AREA -
 JAPAN INTERNATIONAL COOPERATION AGENCY

Design Rainfall



Alternative Case

- Case I ○---○ x 4 sets
- Case II ●---● x 5 sets
- Case III ×---× x 4 sets



Elevation

BLACK RIVER LOWER MORASS
 AGRICULTURAL DEVELOPMENT PROJECT
 Fig. H-14 INUNDATION CURVE
 - BROAD RIVER RIGHT BANK AREA -
 JAPAN INTERNATIONAL COOPERATION AGENCY

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ANNEX I

IRRIGATION

ANNEX I

IRRIGATION

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ANNEX I
IRRIGATION

1. PRESENT CONDITION

1.1 Land Use and Existing Irrigation System

The project area of about 11,450 ha located in central south coast of St. Elizabeth parish covers a sugar cane estate, mostly in Holland Estate, pasture of upland grassland and some mixed farming land as well as swamp and forest. The present land use described in Annex G shows that, although about 6,760 ha or 59% of the total project area are covered by swamp and forest, there exist about 2,760 ha or 24% of pasture, 920 ha or 8% of sugar cane, and about 680 ha or 6% of upland crops/pastures mixed farming land and about 330 ha or 3% of other mixed farming land including paddy.

There are no systematic irrigation facilities even for the sugar cane of the Holland Estate which had an intake structure across the Y.S. River about 1.5 km upstream of the Santa Cruz - Black River Highway (Bamboo avenue) crossing. The intake structure and canal were constructed for supplying cooling water to the sugar factory since the late 1920s when it was established. The facilities might be used to supply some irrigation water for sugar cane when necessary. However, at present, they are derelict and not used even for irrigation since the factory was closed in 1981.

1.2 Irrigation Developments Outside the Lower Morass

In Pedro Plain, south of the Lower Morass, an irrigation system, the Hounslow irrigation scheme, is being operated. A successful and advanced irrigation practice has been introduced. At present, 670 ha (1,680 ac) are irrigated by sprinklers from four wells for such upland crops as groundnuts, soya beans, water melons, various kinds of vegetables and so on.

In the Upper Morass of the Black River, about 3,600 ha (9,000 ac) of farmland were developed with the construction of flood protection dikes along the Black River, drainage canal systems and three drainage pump stations by the Black River Upper Morass Development Company Limited (hereinafter called "BRUMDEC"). These constructions were completed in November 1981. Most of the originally designed irrigation facilities have not been constructed.

BRUMDEC commenced rice cultivation in 1981 during construction, and now manages about 2,200 ha (5,515 ac) of paddy fields. Most of the paddy fields are not irrigated systematically but water levels in drainage canals are kept high enough to facilitate sub-surface flow into the fields. Only a limited area including the Elim rice research station located at north-east corner of the Upper Morass is irrigated with water diverted from the Elim River, one of the tributaries of the Black River. Flood irrigation is practised in these paddy fields.

In the Parish of Westmoreland, about 60 km west of Black River, the Meylersfield West Polder Project has been implemented for mechanized small-holders irrigated rice cultivation. The irrigation system and land clearing of about 140 ha (345 ac) were completed by the end of October 1982. Production was commenced in 1983. The total rice cultivated acreage was about 70 ha (180 ac) in 1983 and at present is about 100 ha (250 ac) or three-fourth of total land. Flood irrigation is practised by pumping water from the river and regulating it in a farm pond. Operation and maintenance of irrigation and drainage systems are undertaken by the said project which, however, is facing expensive requirements to prevent irrigation and drainage canals from clogging by weeds. The following shows the expenditures in 1983 and 1984 (until August) for operation and maintenance of both irrigation and drainage systems.

Description	1983 (Jan. - Dec.)	1984 (Jan. - Aug.)
Area planted	70 ha (180 ac)	100 ha (250 ac)
Total Expenditure for O & M	J\$132,000	J\$133,000
Annual Expenditure	J\$132,000	J\$200,000
per unit area	J\$1,900/ha (730 ac)	J\$2,000/ha (800/ac)
for drainage pump	J\$700/ha (270/ac)	J\$810/ha (325/ac)
for Irrigation pump	J\$800/ha (310/ac)	J\$960/ha (385/ac)
for Maintenance of Irrigation canal	J\$400/ha (150/ac)	J\$230/ha (90 ac)

1.3 Existing Development Plan

Technical and economical viabilities of the agricultural development in the Black River Lower Morass were first studied by Grontmy of the Netherlands in 1964 as the Black River Morass Reclamation Project. Since submission of the feasibility report by Grontmy in September 1964, some works have been implemented within the Lower Morass. These have comprised the construction of about 2 km of embankment to divert the Y.S. River and a dredged by-pass channel of the Y.S. River to and along the Middle Quarters River. A bridge across the Styx River at its confluence with the Black River was also constructed at this stage in April 1973. However, neither road nor dike was constructed along the left bank of the Black River. Such construction was suspended in the mid 1970s when efforts were concentrated on the implementation of the Upper Morass Development Project.

Except for some drainage improvement works on the Holland Estate in the 1970s, no other projects have been implemented in the Black River Lower Morass. At present, under the Agro 21 programme, an early development of a part of the Holland Estate for rice cultivation is under study.

2. DEMARCATIION OF AREA FOR IRRIGATION DEVELOPMENT

2.1 Factors to be Considered in the Selection of Area

1) Land suitability classification

Based on the evaluation of land capability, the areas classified in Grade II, III and IV were taken up as the areas for agriculture. In this evaluation, the factors affecting the delineation are soil texture, topography, soil depth, fertility, drainability, soil salinity and acidity and soil physical properties. These are described in detail in Annex D.

2) Present land use

The present land use and vegetation were also taken into account for the delineation, viz., the western marshland sandwiched between the Black River and the Middle Quarters River is intensively used as shrimp fishing area by local fishermen, while the lower basin of the Black River is covered by mangrove forest. Detailed explanation is made in Annexes D and G.

3) Soil physical characteristics

In the project area, a vast marshland composed of peat extends over about 5,100 ha of the lowland. The peat layer is from 1 m to 10 m in depth. The extremely low bearing capacity of these peat soils would require considerable expense for construction of irrigation and drainage infrastructures. In addition, subsidence of soils after implementation could be relatively large due to desiccation and consolidation of soils as well as due to progressive biological oxidation of peat. From these viewpoints, peat soils of more than 4 m depth are excluded from the agricultural development to be proposed. This is explained in detail in Annexes E and H.

4) Peat mining plan area

According to the Environmental Feasibility Study of the Jamaica Peat Resources Utilization Project prepared by Natural Resources Conservation Department (hereinafter "NRCD") in September 1981, a large potential of peats volume is located in the Middle Quarters River basin, which is excluded from the agricultural development area.

5) Ecological considerations

In the Lower Morass noticeable and perculiar herbaceous swamp and swamp forests and precious wildlife are observed. The Black River Morass system offers one of the few diverse and stable wetland habitats in the Caribbean for many forms of wildlife. In order to minimize the environmental impacts on the above, the development area was carefully delineated on particularly in regard to the swamp forest and surroundings of the Broad River. A detailed explanation is given in Annex K.

2.2 Area to be Developed

The area to be developed for the feasibility of the project was selected from the project area of about 11,450 ha taking the above factors into consideration.

For the sake of establishing of efficient irrigation systems, the area to be studied was divided into four sub-areas. These are (1) the Black River right bank bounded by the Middle Quarters River, (2) the Black River left bank bounded by the Lacovia - Cataboo road and the edge of the swamp along the Island of Cataboo and Holiday Pen, (3) the Broad River Basin bounded by the Lacovia - Cataboo - Black River road and the Lacovia - Mountainside - Black River road, (4) the western part of the Middle Quarters River and the estuary of the Black River and Broad River. The fourth sub-area, however, was excluded from the development from the viewpoint of topography, present land use and inadequate irrigation water availability (see Fig. I-1). The respective areas of the proposed sub-areas are as follows:

Area	(Unit: ha)	
	Gross	Net (Acres)
Black River right bank	680	560 (1,400)
Black River left bank	1,200	920 (2,300)
Broad River Basin	2,000	1,600 (4,000)
Estuary - Middle Quarters	-	-
Total	3,880	3,080 (7,700)

A total area of 720 ha is left as it is for the existing Holland Estate, in which sugar cane is presently cultivated in 910 ha (2,275 ac.). As mentioned in the previous Section 2.1, (5) both sides of the Broad River (360 ha) are preserved from the agricultural development.

The location of each sub-area is shown in Fig. I-1 and breakdown of physical area is shown in Table I-1. A detailed explanation of each of the sub-areas is given below.

1) The Black River Right Bank

The right bank area of the Black River, about 2,540 ha, consists of three sub-areas, 260 ha in Lacovia, 1,400 ha in the Holland Estate and 880 ha along the Y.S. River (on both banks). There are nine main soil types in this area, of which five are in upland area of Lacovia and the Holland Estate and four in inundated area along the Y.S. River as shown in Table D-15 in Annex D. Most of the land covered by upland soil (1,580 ha) in the Holland Estate and Lacovia are classified as suitable (Class II) for upland crops as well as for paddy cultivation, while about 390 ha or 40% of wetland in inundated area would be moderately suitable (Class III and IV) for rice cultivation and only 170 ha or 18% are for upland crops. The rest of inundated soils would be marginally suitable or unsuitable for rice cultivation as well as for upland crops.

As Lacovia is a village where mixed culture of trees, grassland or pasture, upland crops, vegetables, etc. in house yards is predominant, no agricultural development was considered. Accordingly, the irrigable area was delineated in the Holland Estate including suitable areas along the Y.S. River.

Holland Estate

Out of 1,900 ha (4,750 ac) of registered acreage, about 200 ha (500 ac) are located outside the project area (north of Bamboo avenue) and about 300 ha (750 ac) are undeveloped swamp and forest lying between the Y.S. River and the Black River, where the soils are only marginally suitable for agricultural development not only from such technical points of view as soil conditions (see Annex D) and soil mechanical

conditions (see Annex E and Annex H) but also from environmental considerations (see Annex K and Annex L). Thus the present arable land of the Holland Estate in the project area was estimated to be 1,400 ha (3,500 ac). Out of 1,400 ha as shown in Table I-2, 910 ha (about 2,300 ac) are under cultivation of sugar cane, 110 ha (about 280 ac) are under a mixed culture of paddy and swampy grass (fallow) and about 180 ha (450 ac) are covered with grasses or in fallow. The remaining 180 ha (450 ac) are swampy grassland lying along the Black River right bank and left bank of the upper reach of the Y.S. River, exclusive of about 20 ha (50 ac) of factory and quarters yards.

The main arable lands of the Holland Estate have three particular characteristics. The elevation is an above El. 3.00 m. About 85% of a gross 540 ha is covered mainly with cane fields (about 460 ha or 85%), some grassland (60 ha or 11%), and factory and quarters yards (20 ha or 4%). This land is gently undulating and its surface slope ranges from 1/500 to 1/30 or 1/200 on an average. These areas would be moderately suitable for irrigated upland crops farming.

There are also about 370 ha of low lying flat land below El. 1.00 m, with only 70 ha or 19% of cane fields and where a mixed culture of rice and swampy grass (fallow) is dominant on 90 ha or 24%. The remainder is occupied by grassland (40 ha or 11%) and swamp (170 ha or 46%). The slope of these areas is quite gentle: less than 1/1,000. These areas would be suitable for paddy cultivation.

In-between above two areas there are about 490 ha lying between El. 1.00 m and El. 3.00 m. About one third of this land is composed of rather steeply sloping strips sandwiched between the elevated and low lying areas. The slopes range from 1/200 to 1/30. The rest is a flat land with gentle surface slopes of about 1/500 on an average. About 380 ha or 78% of this land are cultivated with sugar cane at present, while 90 ha or 18% are grassland or swamp and 20 ha or 4% are paddy field. The flat area in this category would be suitable for irrigated paddy cultivation while the sloped strips would be only moderately suitable for the same purpose.

In general, paddy rice is grown by flood irrigation method. Land suitable for paddy cultivation should be flat and its soils should be reasonably impermeable. Most of the soils in the Holland Estate are classified as clay soil as shown in soil map in Annex D. The irrigable area for rice cultivation was generally delineated within the flat land, excluding the elevated undulating lands above El. 3.0 - 4.0 m and the sloping lands lying below El. 3.00 m where economical land levelling works would require reduction in the size of a farm plot to as small as 0.4 ha (1.0 ac). Thus, the irrigable area delineated is about 680 ha gross (560 ha net), of which present land use is shown below:

Present Land Use	(Unit: ha)		
	Below El. 1.0 m	El. 1.0 - El. 3.0 - El. 4.0 m	Total
Cane fields	70	240	310
Paddy fields	90	20	110
Grass/Pasture	40	50	90
Swamp	160	10	170
Total	360	320	680

Accordingly, the remaining area of 720 ha would be reserved for sugar cane and other crops. The present land use is shown below:

Present Land Use	(Unit: ha)			
	Below El. 1.0 m	El. 1.0 - El. 3.0 - El. 4.0 m	Above 4.0 m	Total
Factory & Quarters	0	0	20	20
Cane fields	0	150	450	600
Grass/Pasture	0	30	60	90
Swamp	10	0	0	10
Total	10	180	530	720

2) The Black River Left Bank

The left bank area of the Black River, about 2,320 ha, consists of four (4) sub-areas, 370 ha of Hatfield, 410 ha of Styx River basin, 800 ha of Frenchman-Holiday Pen and 740 ha of the Island of Slipe and Cataboo.

In Hatfield and Frenchman-Holiday Pen upland area, there are six (6) main soil types. Out of these, five are classified as suitable or moderately suitable (Class II and III) for both upland crops and rice cultivation, with their area of 900 ha or 86% and the rest is marginally suitable with extremely rocky complex. However, the Island of Slipe and Cataboo are village areas where a mixed culture of trees, pastures and partly upland crops is predominant. The irrigable area in such upland is, therefore, delineated mainly in Hatfield.

The Styx River basin and Frenchman-Holiday Pen are wetlands, and three main soil types are observed in the inundated area, except for some forest land. One is mineral soil (clay) observed along the natural levee on the left bank of the Black River. The other two are inundated peat. The whole of this land is classified as moderately suitable (Class III or IV) for rice cultivation but only marginally suitable for upland crops.

The irrigable areas delineated for rice cultivation after planning of the irrigation canal networks totalled about 1,200 ha gross (920 ha net), in the left bank of the Black River as shown below:

Sub-area	(Unit: ha)	
	Gross	Net
Hatfield	300	220
Styx River Basin	400	300
Frenchman-Holiday Pen	500	400
Total	1,200	920

3) Broad River Basin

The Broad River Basin of about 3,910 ha is divided into four sub-areas based on their topographic characteristics, i.e., the Broad River right bank area of about 1,290 ha, the left bank area of about 1,300 ha, a strip of about 760 ha of mountain skirt along the Lacovia-Mountainside road, and the Vineyard - Arlington are of about 560 ha in southern elevated land of the project area. Both right and left bank areas of the Broad River are covered with peat and are classified as moderately suitable for rice cultivation but only marginally suitable for upland crops. On the other hand, in the strip of mountain skirt and Vineyard - Arlington area, there are seven main soil types. About 230 ha in the strip of mountain skirt and 190 ha in Vineyard - Arlington, covered by three out of seven soil types, are classified as suitable for irrigated farming. The suitable land in the strip of mountain skirt was included in the irrigable area of both right and left bank areas of the Broad River. The irrigable area in Vineyard was included under the Pedro Plain Irrigation Project. The irrigable area delineated amounts to about 2,000 ha gross and 1,600 ha net, consisting of 1,000 ha on the right bank and 1,000 ha on the left bank as below:

	(Unit: ha)	
Broad River Basin	Gross	Net
Right Bank	1,000	800
Left Bank	1,000	800
Mountain skirt	included in above	
Vineyard - Arlington	included in Pedro Plain	
Total	2,000	1,600

The above areas exclude the 360 ha set aside for conservation and protection of natural environment.