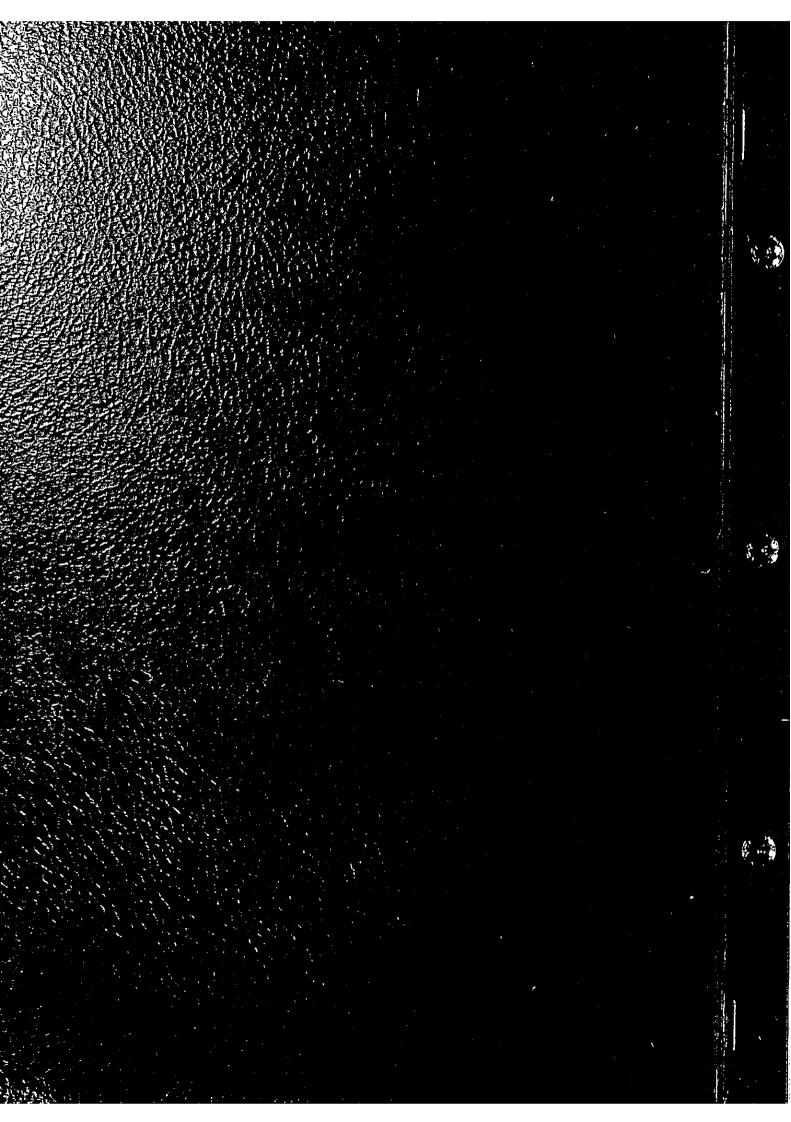
## FEASIBILITY REPORT ON THE MORAGAHAKANDA AGRICULTURAL DEVELOPMENT PROJECT

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Democratic Socialist Republic of Sri Lanka The Ministry of Mahaweli Development

# FEASIBILITY REPORT ON THE MORAGAHAKANDA AGRICULTURAL DEVELOPMENT PROJECT

VOLUME Ⅲ
DOWNSTREAM DEVELOPMENT

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#### Democratic Socialist Republic of Sri Lanka The Ministry of Mahaweli Development

#### FEASIBILITY STUDY REPORT

ON

### THE MORAGAHAKANDA AGRICULTURAL DEVELOPMENT PROJECT

#### VOLUME III :

#### DOWNSTREAM DEVELOPMENT

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October 1979

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ANNEX V: SOIL SURVEY



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#### I Summary and Conclusion

Most of soils in project area is fairly good for agricultural development.

Soil units in project area can be classified into six main groups, that is, Reddish Brown Earths-well drained series, Reddish Brown Earths-imperfecttly drained series, Low Humic Gley soils, Alluvial Soils, Solonetz soils and Rockey and Shallow phase soils.

These former four soil units, which acreage are shown in the following table, are suitable for agricultural development.

Suitability for			Acreage	(Acre)		
Agriculture Development	A/D	D <sub>1</sub> S	D <sub>1</sub> N	D <sub>2</sub>	G	Total
Suitable	15,745	51,920	26,640	14,330	15,460	124,095
Unsuitable	2,165	6,895	1,600	370	7,720	18,750

Table 5-1 Suitability of Soils for Agricultural Development

#### Note

- 1. The above Table shows only acreage of undeveloped area in the proposed project site.
- 2. D1-N area is locating on the west and north side of A/D area.
- 3. The final suitable acreage for agriculture will be changed to the result of topographical survey.

In project area, six main soil units are existing and the cropping potential in each unit are as follows.

#### a) Reddish Brown Earths, well drained series

Very good to good land for upland crops.

All upland crops of dry zone can be grown.

Organic matter should be added.

#### b) Reddish Brown Earths, imperfectly drained series

Very good for lowland rice.

Lowland rice, sugar cane and pastures can be grown.

#### c) Low humic gley soils

Not so good for upland crops.

Only lowland rice can be grown.
(Partly upland crops in Yala Season.)

Drainage would be beneficial.

#### d) Alluvial soils, wellto moderately drained series

Very good to good for cash crops.

Profitable cash crops such as tobacco and vegetables can be grown.

These soils are only existing in  $D_2$  area.

#### e) Alluvial soils, imperfectly drained series

Not so good for upland crops.

Only lowland rice can be grown.

Drainage would be beneficial.

Prevention of flood is necessary.

#### f) Solonetz

Generally very poor to poor.

These Lands are generally unsuitable for crops.

It would be better to abondon these land.

(Generally, leave these soils until determine their salt content by future survey.)

#### g) Shallow and Rocky phase, rock knob plain

These lands are unsuitable for crops, but good for settlement. (household area)

#### h) Erosional Remnants

Generally unsuitable for development.

Acreage of the above soils are given in Table 5-2 in the next page.

Table 5-2 Acreage of Main Soil Units in Underdeveloped Area (Acres)

	A/D	D <sub>1</sub> S /1	$_{\rm D_1N}$ /2	$D_2$	G	Total
Reddish brown earths well drained series	5,510	13,645	12,640	130	7,370	39,295
Reddish brown earths imperfectly drained series	5,215	9,980	6,030	0	5,470	26,695
Low humic gley soils	1,260	25,150	6,030	0	2,050	34,490
Alluvial soils well to moderately drained series	0	0	970	3,650	570	5,190
Alluvial soils imperfectly drained series	3,760	3,145	970	10,550	0	18,425
Solonetz	0	2,825	0	0	0	2,825
Shallow and Rocky phase, rock knob plain and Remnants	2,165	4,070	1,600	370	7,720	15,925
Total	17,910	58,815	28,240	14,700	23,180	142,845
/1,/2: S = South, N =	North					

The soil maps of  $\mathrm{D}_2$  area and undeveloped  $\mathrm{D}_1$  area (west side of A/D area) have not completed yet. The new soil maps of these areas will be completed in future at the Land Use Division by air photo interpretation, which are also not detailed map but valuable for general understanding of the soils.

As time passes after first reclamation, the crop yield decrease rapidly. This phenomena seem to be closely related to the decrease of nutrient content and reduction of soils itself. Therefore, it is most important to improve the drainage condition especially on the poor drained land and need to organize a good extension system relating with the technics of application of chemical fertilizers and organic matters.

#### II Soil Observation and Analysis

#### Number of the Soil Observation Points

Soil observation was done on both developed area and undeveloped area of project site. The number of soil observation points are given in Table 5-3.

Table 5-3 Soil Observation Points

System	A/D	D <sub>1</sub>	D <sub>2</sub>	G	Total
Developed Area	-	47	14	9	70
Undeveloped Area	15	30	15	10	70

#### Soil Analysis

Twenty one soil samples, that is seven samples of developed area and fourteen samples of undeveloped area respectively were analysed.

The purpose of analysing soil samples of developed area is to determine the best soil condition for paddy and upland crops. For this purpose, soil samples were taken from both good and poor paddy as well as upland to compare these soil conditions.

The other purpose of analyzing soil samples of developed area is to know the chemical characteristics of four soil units, such as reddish brown earths, well drained series, reddish brown earths, imperfectly draines series, low humic gley soils and alluvial soils and to check the cropping potential of each soil unit.

This soil analysis was completed at the Soil Science Laboratory, Land Use Division, Irrigation Department of Sri Lanka in compliance with the request made by the Japanese Feasibility Study Team.

The location of soil survey is shown in the DWG. No. 5-1.

#### III Soil Units in Project Area and Their Characteristics

#### Introduction

Soil groups in Sri Lanka are mainly based on their morphology, which shows the main feature of soil profile. Twelve main great soil groups and subgroups are found in the different natural condition of Sri Lanka. (C.R. Panabokke, Ph.D., Soils of Ceylon and fertilizer use, page 67-81, 1967, Metro Printers Ltd.)

An abridge soil map of Ceylon of 1971 which is annexed to the main report shows the main soil groups which occurs in different parts of the island.

Soil maps of undeveloped area in the project area, (system A/D,  $D_1$  and G) have been complied in 1978 on scale of 1 mile to 1 inch Map (1:31,673) by the soil survey staff of the Land Use Division of the Irrigation Department. Soil report showing the cropping potential of these areas has prepared by the Land Use Division.

In these soil maps, we find that soil groups are closely related to the topography of small catchment area. In the project area, four soil units respectively Reddish Brown Earths (well drained) Reddish Brown Earths (imperfectly drained), Low Humic Gley Soils (poor drained) and Alluvial Soils are existing. That is, the most important and extensive soil groups in the project area are the drainage catenary association of Reddish Brown Earths and Low Humic Gley Soils as well as Alluvial soils.

#### Drainage Catena

As above, four main soil units are found in the dry zone, that is, Reddish Brown Earths (well drained), Reddish Brown Earths (imperfectly drained), Low Humic Gley Soils and Alluvial soils. In most of the undulating landscape units of dry zone as well as in the project area, these former three are forming a drainage catena. That is to say, reddish brown earths, well drained, occur in the higher aspect of landscape, reddish brown earths, imperfectly drained, occur middle and lower aspect of landscape, and the low humic gley soils occur in the lower aspect of landscape, as given in Fig. 5-1.

٧

Reddsh brown earths

Yellowish brown earths

Brown brown earths

Low humic gley salts

Rock knob as a salts

Parent meteric

Fig. 5.1 Soil Association or Soil Catena

#### Reddish Brown Earths, well drained

The A horizon is dark brown to dark reddish brown, the B horizon is more red than the A horizon, usually reddish brown to dark red. These red colours of soils indicates the presence of unhydrated iron oxide which can only exist in well drained condition. That is to say, these soils are oxidized very well.

#### Reddish Brown Earths, imperfectly drained

The A and B horizons are dark brown to dark yellow brown. This yellowish colour of soils indicates the presence of hydrate iron oxide which never exist in well drained condition. That is to say, these soils are oxidized not so well.

#### Low Humic Gley Soils

Top soils are brownish gley to gley. This gley colour indicates the presence of ferric iron which can only exist in poor drained condition and reducted condition.

As above, the drainage catena is closely related to landscape unit, drainage condition and soil colour. Moreover, this is closely related to the nature of clay minerals and potentiality of soils. In other words, it is considered that potentiality of soils of project area as well as dry zone is related to a great extent to landscape unit and soil colour.

#### 3.1 Reddish Brown Earths, well drained series

#### 3.1.1 Location

These soils are located on the upper aspect of the slopes, mainly from the ridges to the almost flat aspect.

#### 3.1.2 General description

The modal profile derived from this soil survey is as follows.

#### Horizon A

Depth : Usually 10 - 15 cm

Colour : Dark brown to dark reddish Texture: Sandy loam to sandy clay loam

#### Horizon B

Depth : 90 - 110 cm

Colour : Dark reddish brown to reddish brown

Texture: Sandy clay loam

#### Horizon C

Depth : Deeper that 120 - 150 cm

Colour : Light yellowish brown to pale brown

#### 3.1.3 Physical Characteristics

According to SOGREAN report Vol. III, physical characteristics are as follows.

Bulk Density : 1.5 - 1.630 - 40 % Soil Porosity Available Moisture : Deep phase 100 - 125 mm

> 25 - 50 " Shallow phase

Infiltration rates : Deep phase 5 - 15 cm/hr 25 After 1 hour

3.1.4 Chemical Characteristics

Soil analysis data are given in Table 5-4

Table 5-4 Chemical Characteristics of R.B.E. well drained

				-										
Sample No.:	No.:	НА	E.C.	на	CEC	Ca	Mg	Na	Ж	Org:C%	%N	1	P(Abs	EX.
		1:2.5 1:5		1:2.5	•			•,,,,					Coeff:)	
			m.mhos/	kcl	kcl Meg/	Meg/	Meg/	Meg/	Meg/			wdd		
	_		CB		100g	100g	100g	100g	100g		·			
D <sub>2</sub> D 4	D <sub>2</sub> D 4 78/240	5.90 0.07		4.80	9.62 5.25	5.25	2.49	0.20	0.133	96.0	0.074	Nil	ı	5.74
D <sub>1</sub> D 1		6.10 0.08		5.60	10.03	7.04	2.24	0.16	0.325	1.33	0.099		3 1,300	4.28
$D_1U$ 2	78/232	6.70 0.05		5.50	10.48 7.43	7.43	2.80	0.18	0.112	0.99	0.071	Nil.	ı	3.81
G 5	(poog)	6.90 0.06		5.60	12.89	7.37	4.38	0.18	0.213	0.79	0.157	Nil	3,850	4.80
9 5	78/244	6.50 0.11		5.45	10.96	5.85	2.65	.0.18	1.381	0.58	0.092	4	2,600	3.83
G 1.1	Poor	5.40 0.06		4.70	11.06	6.87	2.48	0.10	0.089	0.77	0.099	m	3,000	5.73
				-								-		

Based on the above data and results of related analysises, the chemical characteristics of this soil in

general will be explained as follows.	5.4 - 7.0	0.6 - 1.3 %	9.6 - 13.0 me/100g	5.0 - 7.4 me/100g	0.1 - 1.4  me/100g	2.0 - 4.4  me/100g
general will be	Ph (H <sub>2</sub> 0)	Organic matter	C.E.C.	Exc. Ca.	×	Mg

#### MODAL PROFILE - REDDISH BROWN EARTH - WELL DRAINED

#### LAND USE DIVISION

#### Soil and Site Description

Location : Bore No. :

Area : Date :

Topography: Photo No.:

Slop : Drainage : Well drained

Land Use :

Site Feature :

Depth	Colour	Texture	Moisture, Structure, Consistence, Cutants, Gravels, Concretion, Pores, Roots, Mottling etc.
0- 4	5 yR 4/2	S1.Scl	Slight organic matter ns & np (w)
4-12	5 yR 4/3	Sc1	SS & Sp (W); mica feldspar; few soft Mn concretion
12-18	5 УR 4/4	Scl	SS & Sp (W); mica feldspar; few soft Mn concretion
28-36	5 УR 4/6	Scl	SS & Sp (W): mica feldspar; few soft Mn concretion
36-40	2.5 yR 4/6	Scl- grscl	SS & Sp (W); mica feldspar; few soft Mn concretion
40-44	2.5 yR 4/6	gr Scl	SS & Sp (W); to S & P (W) few mica, feldspar; Mn stains
44–48	10 R 4/6	gr Scl	S & P (W); mica feldspar; Mn concretion

Remarks :

Classification : R.B.E. - Well drained.

#### 3.2 Reddish Brown Earths, imperfectly drained series

#### 3.2.1 Location

These soils are mostly found in the flat or nearly flat areas which occur on the lower aspect of slopes.

#### 3.2.2 General Description

The model profile derived from this soil survey is as follows.

#### Horizon A

Depth :

Colour : Dark brown to dark yellowish brown

Texture : Sandy clay loam to sandy loam

#### Horizon B

Depth

Colour : Dark yellowish brown to yellowish brown

Texture : Sandy clay loam

#### Horizon C

Depth : 90 - 120 cm

Colour : Yellowish brown

#### 3.2.3 Physical Characteristics

According to SOGREAH report Vol. III, physical characteristics are as follows.

Soil Porosity : 30 - 40 %Available Moisture : 75 - 100 mm

Infiltration rate : Comparatively lower than

RBE well drained series

# 3,2,4 Chemical Characteristics

Soil analysis data are given in Table 5-5

Table 5-5 Chemical Characteristics of R.B.E. imperfectly drained

Sample No.:	PH 1.2 5	1 E.C.	PH 1	CEC	Ca	Mg	Na	Ж	Org: C%	%N	ы	P(Abs	EX.
	+		7:2.3	Meo/	Meo/	Me a /	Mao/	Mpo/			E C	mg/100g	¤
			_	0	1021	ò	io .	0				900+19	
		CH C		100g	100g	100g	100g	100g					
D <sub>2</sub> D 7 78/242	1	6.75 0.96	5.40	8,58 7,08	7,08	1.62	0.10	0.150	99.0	0.079	6	750	3,81
D <sub>1</sub> U 18 78/235	35 6.30	90 0.04	4.90	10.39 7.11	7.11	2.38	0.10	0.151	1.10	0.089	e.	1,750	4.30
G 1.7	6.00	0.07	5.30	10.57 6.90	06.9	3.41	0.18	0.086	0.87	0.092	63	5,400	0.00
D <sub>1</sub> D 10	6.10	.0 0.07	5.50	11.43 6.92	6.92	4.07	0.18	0.125	1.68	1.121	7	ı	5.31
G 16 78/246	6.65	50.05	5.20	10.21 7.04	7.04	1.19	0.15	0.431 1.24	1.24	0.120	က	2,250	5.28
D <sub>1</sub> U 4 78/233	33 6.70	0.23	5.60	19.55	19.55 14.50	6.47	0.34	0.152	1.31	0.082	N11	1,250	4.42
AD 4	6.10	.0 0.04	5.30	5.30 10.31	6.88	3,33	0.18	0.103	1.19	101.0	ო	ł	5.86
	-							-		1			

Based on the above data and results of related analysises, the chemical characteristics of this soil in general will be explained as follows.

Figure 3. 10110WS. From 1.0 (1.0) 6 - 6.8 0.5 0.6 - 1.7 % 0.5 0.6 - 1.7 % 0.5 0.6 0.6 0.6 0.6 0.6 0.7 % 0.8 0.9

1.2 - 6.5 me/100g

#### MODAL PROFILE - REDDISH BROWN EARTHS - IMPERFECTLY DRAINED

#### LAND USE DIVISION

#### Soil and Site Description

Location : Bore No. :

Area : Date :

Topography: Photo No.:

Slope : Drainage : Imperfectly Drained

Land Use :

Site Features :

Depth	Colour	Texture	Moisture, Structure, Consistence, Cutants, Gravels, Concretion, Pores, Roots, Motting etc.
0- 4	10 yR 3/3	S1	Slight organic matter ns & np (w)
4-12	10 yR 4/3	Scl	SS & sp (W) faint mottling; Mottle colour 7.5 R 4/4; few soft Mn Concretion
12-28	10 yR 4/4	Sc1	SS & Sp (W) C ld mottles of colour 7.5 yR 4/4 feldspar few soft Mn Concretion
28-40	10 yR 5/6	Scl	SS & Sp (W) C 2d mottles of colour 7.5 yR 4/4 feldspar few soft Mn Concretion
40-48	10 yR 5/6	Sc1	SS & sp (W) C 2d mottles of colour 7.5 yR 4/4 few Iron Stones, Mn Stains
48-54	10 yR 5/3	Scl- grscl	SS & sp (W) C lp mottles of colour 7.5 yR 4/4 feldspar; Mn Stains

Remarks :

Classification : R.B.E. Imperfectly drained

#### 3.3 Low Humic Gley Soils

#### 3.3.1 Location

These soils are located on the almost the whole extents of valleys.

#### 3.3.2 General Description

The model profile derived from this soil survey is as follows.

#### Horizon A

Depth : 25 - 30 cm

Colour : Dark gley Brown to Brown or bluer

Texture : Loomy sand to sandy Loam

#### Horizon B

Colour : A lighter colour than A horizon strongly mottled or

Pseudo-gley appear

Texture : Sandy clay Loam to Sandy Clay

#### 3.3.3. Physical Characteristics

Soil Porosity : Less than the porosity of RBE

Available Moisture : Usually more than that of RBE

Infiltration rate : Usually less than 5 cm/hr

3.3.4 Chemical Characteristics:

Soil analysis data are given in Table 5-6

Table 5-6 Chemical Characteristics of L.H.G. Soils

.:2.5 1:5 1:2 m.mhos/ kcl 7.05 0.74 6.00	1:2.5 Meg/ 100g 6.00 42.12 6.10 14.22 6.00 10.12 5.10 9.42	Meg/ 100g 25.53 10.40 6.07	Meg/ 100g 14.23 4.72 3.64	Meg/ 100g 4.44 0.31	Meg/ 100g 0.349 0.258	1.47		wdd	Coeff:)	
kc1		Meg/ 100g 25.53 10.40 6.07	Meg/ 100g 14.23 4.72 3.64	Meg/ 100g 4.44 0.31	Meg/ 100g 0.349 0.258	1.47		mdd	-001/	
8		25.53	14.23 4.72 3.64	4.44 0.31 0.36	0.349	1.47			BOOT /Su	H
			3.64	0.31	0.258		0.153	12	ı	8.91
•			3.64	0.36	0.177	1.58	0.075	7	ı	2.91
					1	0,83	0,057	Nil	1,500	2.85
		0.40	2.06	0.13	0.133	66.0	0.077	NII	2,400	3,81
5.80	22.49	13.80	8.78	0.21	0.223	1.80	0.116	NTI ,	ı	5.82
5.40	6.05	2.74	1.82	1.09	0.091	0.05	0.084	1.2	1,150	0.97
4.80	11.14	6.74	3.61	0.20	0.109	0.56	0.076	10	2,600	5.21
5,30	18.05	11.80	4.83	0.26	0.142	1.25	0.138	10	ı	7.39

#### MODAL PROFILE - LOW HUMIC GLEY

#### LAND USE DIVISION

#### Soil and Site Description

Location : Bore No. :

Area : Date :

Topography : Concave bottom Photo No. :

Slop : 0 - 2/1 % Drainage : Poorly drained

Land Use :

Site Feature :

Depth	Colour	Texture	Moisture, Structure, Consistence, Cutants, Gravels, Concretion, Pores, Roots, Motting etc.
0- 4	10 yR 3/2	S1-SC1	Slight organic matter ns & np (W) faint mottles of colour 7.5 yR 4/4
4-14	10 yR 4/3	SC1	C <sub>1</sub> d mottles of colour 7.5 yR 4/4 SS & Sp (W) slightly gleyed 5y 5/1 few soft MN Concretion
14-24	2.5 y 5/2	sc1	Cld mottles to C2d mottles of colour 7.5y 4/4 SS & Sp (W) to S & p Common gleying 5y 5/1 few soft MN concretion
24-40	2.5 y 5/2	SC1-SC	C <sub>1</sub> d to C <sub>2</sub> d mottles of colour 7.5 yR 5/6 Common gleying of colour 2/2 yR 6/2 few soft MN concretion S & p (W)
40-48	5 y 5/1	SC	C <sub>2</sub> d mottles of colour 7.5 yR 5/6 Common gleying; Commons soft MN Concretion S & P (W)

Remarks :

Classification : L.H.G.

#### 3.4 Alluvial Soils

#### 3.4.1 Location

These soils occur in narrow strips along valleys. Especially fairly large amount of these soils is occured in  $\mathbf{D}_2$  area.

#### 3.4.2 General Description

Alluvial soils are developed on recent water laid deposits in which no profile development other than accumulation of some organic matter in A horizon has taken places.

#### 3.4.3 Physical Characteristics

Generally texture of these soils varies from heavy clay to coarse sand. Although these soils which occur in  $\mathbf{D}_2$  area have faily good physical properties.

#### 3.4.4. Chemical Characteristics

Soil analysis data are given in Table 5-7.

Table 5-7 Chemical Characteristics of Alluvial Soils

EX.	Ħ	ı
P(Abs Coeff:)	mg/100 g	4,250
ρι	ppm	25
%N		0.208
Org: C% N%		1.77 0.208
M	Meg/ 100g	4.87 0.23 0.310
Na	Meg/ Meg/ 100g 100g	0.23
Mg	Meg/ 100g	4.87
Ca	Meg/ 100g	14.30
CEC	Meg/ 100g	20.01
PH.	kcl.	5.70
E.C.	m.mhos/ cm	0.09
PH E.C.	1	6.70 0.09
Sample No.:		D <sub>2</sub> U4 78/239
Sam		D2U4

#### MODAL PROFILE - WELL DRAINED TO MOD. - WELL DRAINED

#### LAND USE DIVISION

#### Soil and Site Description

Location : Bore No. :

Area : Date :

Topography : Convex Slope Photo No. :

Slope : 1 - 1 1/2 % Drainage : W. Drained to M. W.

Land Use : Drained

Site Features :

Depth	Colour	Texture	Moisture, Structure, Consistence, Cutants, Gravels, Concretion, Pores, Roots, Mottling etc.
0- 4	10 yR 4/2	S1 to C1	Organic Matter, ns & np (W)
4-18	Varing colour	C1	ns & np (W) to SS & Sp
18-40	10 yR 5/4	C1	SS & Sp (W)
40-48	10 yR 5/3	C1	SS & Sp (W) few soft Mn Concretion

Remarks :

Classification : Alluvium - Well drained to Mod. Well drained.

#### IV Land Classification

It is to be desired that land classification should be done taking account of many factors such as soil factors, Topographic factors and drainage factors as referred in the general land classification specification of U. S. Bureau of Reclamation. However, it is very difficult to classify the land according to the U. S. B. R. specification during this short soil survey period.

However, land classification that is only taking account of soil factors such as texture, depth (limited by gravel, rock or impervious material), salinity, chemical characteristics and permeability seems to be enough to know the datas which showing approximate land potential at present.

Therefore, this simple land classification has been made in this report.

#### 4.1 Cropping Potential of each soil unit

#### 4.1.1 Reddish Brown Earths, well drained series

Very good to good lands on which no limitation are imposed on the choice of crops. On this well drained soil, a wide range of upland crops of the dry zone can be grown, although the cultivation of paddy is not recommended because of high permeability of these soils. (According to the SOGREAH REPORT Vol. III, the average permeability of reddish brown earths is  $K = 1 \times 10^{-5}$  to  $6 \times 10^{-5}$  m/sec, this value is too high comparing with the adequate value that is 3-5 x  $10^{-7}$  m/sec in case of paddy field.

Depending on the depth of these soils the range of crops that can be successfully grown are given in Table 5-8.

Soil structure of reddish brown earths is so weak that the maintenance of soil structure by providing adequate quantities of organic matter is important. This could be succeeded by the application of cattle manure wherever a pattern of mixed farming could be practised; and where sufficient quantities would not be available, it will be definitely beneficial to introduce green manure crops in rotational cropping system.

Table 5-8 Cropping Potential Depending on the Depth of Soils

wn on each soil seasons	YALA	Fruit Crop	as All upland crops of the				Upland rice, sugar cane, Pastures	Lowland rice
Crops that can be grown on each soil during the two seasons	МАНА	Fruit Grop	All upland crops such as Sugar cane, tabacco.	cotton, Chillies, onion, ground nut, Soya Bean, Cowpea, green gram, Turdhal upland rice, maize		Settlement and home- stead areas	Lowland rice, sugar cane, pastures	Lowland rice
Depth to Bed Rock	(Cili)	150	120 - 150	90 - 120	. 06 – 09	09	06	
Depth to Prominent	layer (cm)	120	90 - 120	06 - 09	30 – 60	30	09	
Depth Phase		Very deep	Deep	Moderately	Moderately shallow	shallow	Very deep to Moderatly deep	
Soil Group		Reddish Brown		Well Drained			Reddish Brown Earth, Imperfectly Drained	Low humic gley soil

The optimum water requirement in depth of paddy field is said as 20-30 mm/day in general. In other words, this value in same as  $3-5 \times 10^{-7}$ m/sec in permeability. a Note:

The following table is showing the exchangeable value between permeability and water requirement in depth. 5

## Exchangeable Value between Permeability and Water Requirement in Depth

Permeability k - m/sec	Water requirement in depth mm/day
1 x 10 <sup>-9</sup>	0.1
1 × 10 <sup>-8</sup>	0.9
1 × 10 <sup>-7</sup>	8.6
1 x 10 <sup>-6</sup>	86.4
1 x 10 <sup>-5</sup>	864.0

#### 4.1.2 Reddish brown earths, imperfectly drained series

The choice of crops is limited by dry and wet season, because of low permeability of these soils (According to the SOGEAH report Vol. III, the average permeability of imperfectly drained reddish brown earths is  $K = 1.5 \times 10^{-6}$  to  $9 \times 10^{-6}$  m/s.)

As Soil moisture is so high at wet seasons, only limited crops can be successfully grown on these soils, that is lowland paddy, sugar cane and pastures.

But if adequate surface drainage is provided, some of the other upland crops of dry zone could be cultivated during yala season.

Rice yield on these soil series is highest among the all soil groups that are existing in project area, because these soils are fertile and not so reduced.

But, in a course of time after reclamation the tendency of decrease of yield was found in this survey. The reason of this phenomenon is regarded mainly as the reduction of soils and lowering of its fertilities. Reduction of soils is caused by high soil moisture and lack of air, so drainage should be considered. (This is largely due to poor water management in the upper slopes.)

The depth of these soils are usually deep or moderately deep so that the depth of soilds would not become restricted for root penetration.

#### 4.1.3 Low humic gley soil

The choice of crops is severely limited. Because of low permeability of these soils (According to the SOGREAH report Vol. III the average permeability of Low humic gley soil is  $K = 1.5 \times 10^{-6}$  to  $9 \times 10^{-6}$  m/s.) Soil moisture is too high, so only lowland paddy can be successfully grown on these soils.

In the case of imperfectly drained Reddish Brown Earths, as time passes after reclamation the tendency for decrease in yield was found, too. This would be due to lack of sufficient fertilizer application, but drainage may also be useful on its improvement.

So, drainage would be necessary. Open drains will generally be beneficial for the removal of the drained water.

#### 4.1.4 Alluvial Soils

Drainage of these soils is mostly poor, so that these are best soils suitable for cultivation of lowland rice.

While, there are some well drained to moderately drained alluvial soils mainly in  $\mathrm{D}_2$  area.  $^{/1}$  In this area, the cultivation of paddy is not recommendable because of high permeability of soils. However, the exact distribution of well drained Alluvial soils in  $\mathrm{D}_2$  area is not certain. So, further soil survey is necessary to demarkate the exact distribution of these soils, and to plan the cropping pattern for these area which corresponding to the soil condition.  $^{/2}$ 

Note

/1: Along the bank of the Mahaweli river.

12: An exact demarkation and location of this well drained Alluvial soils is not available during this short survey.

#### 4.1.5 Solodized Solonetz

Very poor to poor lands because of saline or saline - alkaline soil condition. So these lands are normally unsuitable for crops. But these lands could be reclaimed when amelioration of these soils would be possible by provision of chemical amendents, drainage and leaching to remove existing sodium and/or salts and cheap water would be available in excess.

But as these lands are always found on the lower parts of landscape, it would be dofficult to ameliorate these land by provision of drainage and leaching. So on the slightly saline or saline - alkaline lands, only lowland rice could grow, although yields are likely to be smaller.

Therefore, until detailed soil survey to be proceeded and determined the level of salinity in these soils at different locations, it would be better to abandon these lands.

#### 4.1.6 Others

Shallow and Rocky phases and rock knob plain are unsuitable for crops, because these soils restrict to extending root of crops, and thereby yield would be very poor.

However, these lands could be used for settlement, homestead, building sites, communication center and play land.

Erosional remnants is not suitable for agriculture or settlement.

#### 4.2 Cropping Potential of Undeveloped Area

As stated above, cropping potential of each land is depending on soil condition and classified to four types, as follows.

#### (1) Upland crop type

These lands are suitable for upland crops, that is, fruit crop, cotton, chillies, onion, groundnuts, soya bean, cowpea, green gram, turdhal upland rice, maize, sugar cane, tobacco, etc.

However, fruit crops are suitable only on very deep phase, that is, depth to prominent gravel layer is more than 120 cm or depth to bed rock is more than 150 cm.

#### (2) Lowland and Upland Crop Type

These lands are suitable for lowland rice, sugar cane and pastures.

The yield of lowland rice on these lands are highest.

#### (3) Lowland Crop Type

These lands are suitable only for lowland rice.

#### (4) Unsuitable for Crop Type

Cropping potential map annexed with this report the classified by these criteria.

The acreage of each classification corresponding to undeveloped area, that is A/D,  $D_1$ ,  $D_2$  and G respectively is given in Table 5-9.

Table 5-9 Land Use Possibility (Acre)

Area	A/D	D	1	D2	9
Type	(Ac.)	(South)	(Ac.)	(Ac.)	(Ac.)
Upland crop type	5,510	13,645	13,610	3,780	17,940
Lowland and Upland crop type	3,945	086,6	6,030	0	5,470
Lowland crop type	6,290	28,295	7,000	10,550	2,050
Unsuitable to crop type	2,165	7,350	1,600	370	7,720
Total	17,910	59,270	28,240	14,700	23,180

Note: 1. This figure shows the acreage of land use possibility depending on the result of soil survey. The definite suitable acreage for agriculture will be changed by the detailed topographical survey.

 $2..\ \ D_1$  (South & North) and  $D_2$  Area are undeveloped area only.

airphoto interpretation during this short survey period and not checked by This figure was calculated by using the new soil map that is made by detailed field soil survey. m •

#### V Recommendation

#### 5.1 Fertilizer Recommendation

Fertilizer demand of plants varies according to their species. There seems to be tendency of increase fertilizer demand as follows.

Low Demand

Gingelly

Castor

Legume

Such as groundnuts, Soya Bean etc.

Sorghum

Paddy

High Demand Chilly

From a point of view of soil condition, fertilizer recommendation should be different among four main soil units, that is (a) reddish brown earths, well drained series, (b) reddish brown earths, imperfectly drained series, (c) low humic gley soils and (d) alluvial soils. But as shown in Chapter III, IV, the Chemical properties of each soils are not so different among them and it is not necessary to distinguish each other.

Although there would be the tendency that plants on the reddish brown earths, well drained series demand more fertilizer than the others.

According to the Agriculture Research Station of Maha - Illuppallama, crop - wise fertilizer recommendations for Low Country of Dry Zone which are including project area are as follows.

# **Gingelly**

	Super	Phosphate	KCL	Ammonium Sulfate	lb/acre
Basal		112	28		
Top dressing		-	_	<b>1</b> 12	

Soya	bean
------	------

	N	P <sub>2</sub> 0 <sub>5</sub>	к <sub>2</sub> о	1b/acre
With inoculum Basal	10	60	40	
Without inoculum Basal	10	60	40	
Top Dressing after 3 weeks *	3	-	-	
Top Dressing after 11 weeks *	11	-	-	

\*: From Planting

# Maize and Sorghum

	N	P <sub>2</sub> 0 <sub>5</sub>	K20	lb/acre
Basal	15			
Basa1	15	40	25	
Top Dressing after 4 weeks	* 45	-	-	

\*: From Planting

# Cotton

	N	P <sub>2</sub> 0 <sub>5</sub>	K <sub>2</sub> 0	1b/acre
Basal	-	50	33	
Top Dressing after 4 weeks *	22	-	-	

\*: From Germination

# Jute and Kenaf

	N	P205	K20	lb/acre
Basal	-	50	30	
Top Dressing after 3-4 weeks *	11	-	_	
Top Dressing after 8-10 weeks *	11	-	-	

\*: From Germination

#### Bandakka

	N	P205	К20	1b/ acre
Basal	20	60	30	
Top Dressing after 3 weeks *	20	-	-	
Top Dressing after 6 weeks *	20	-	-	

\*: From Planting

## <u>Brinjal</u>

	N	P <sub>2</sub> 0 <sub>5</sub>	К20	lb/acre
Basal	40	100	80	
Top Dressing after 3 weeks *	40	_	-	
Top Dressing after 6 weeks *	40	-	-	

\*: From Planting

## Tomato and Capsicum

	N	P205	К <u>2</u> О	lb/acre
Basal	25	60	25	
Top Dressing after	25		25	

\*: From planting

According to New Fertilizer Recommendations, for Rice Production, October, 1971, Agricultural Information Division, 102, Union Place, Colombo, general fertilizer recommendation for rice production for low - country of dry zone are as follows.

# A) 3 Months Varieties for a yield of - 60 Bushels/Acre

	Quantity of Apply	lb/Acre
Basal; $Mi_X$ ture $V_1$	168	
Top Dressing 2 weeks; Urea	56	
Top Dressing 6-7 weeks; Urea	84	

#### Note:

1. Content of N,P and K of Mixture  $V_1$  is as follows:

N	2.68	%
P <sub>2</sub> 0 <sub>5</sub>	27.4	%
к <sub>2</sub> 0	12.9	Z

2. Timing of top dressing: after sowing

# B) $4 - 4^{1/2}$ Months Varities for a yield of - 80 Bushels/Acre

	Quantity of Apply	lb/Acre
Basal; Mixture V <sub>1</sub>	168	
Top Dressing 2 weeks; Urea / 1	56	
Top Dressing 6 weeks; Urea / 1 or 4 weeks / 2	56	
Top Dressing 10 weeks; Urea / 1 or 8 weeks / 2	. 56	

/1. After sowing.

/2. After transplanting.

According to recent findings at the Maha-Illuppallama Research Station, paddy in well drainied RBE soils require more nitrogen than in imperfectly drained RBE soils.

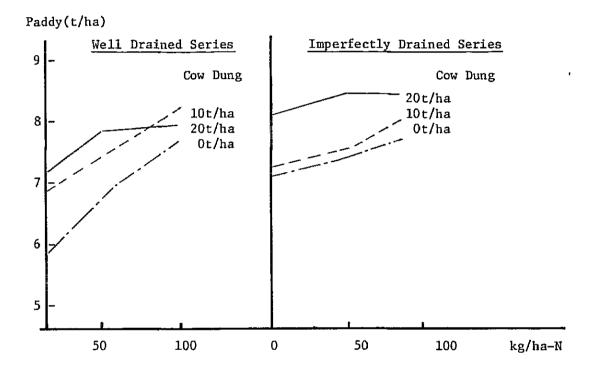
Such information is not available for low humic gley soils. However, inferring from above, it may be said that low humic gley soils would be closen to imperfectly drained RBE soils than the well drained series.

Therefore, the above fertilizer recommendation should be adjusted according to the yield expected and soil characteristics which vary in each field.

#### 5.2 Manuring of Organic Matter

According to Handawela, J, Agricultural Research Station, Maha Illuppallama, the result of nigrogen reponse in Paddy in two drainage members in Reddish Brown Earths is as fig. 5-2.

Fig. 5-2 Nitrogen Respons in Paddy in two Drainage members in RBE.



As shown in Fig. 5-2, manuring respons of cow dung is quite effective, especially in imperfectly drained series.

Manuring of organic matter has advantage not only applying the nutrient of plant but also producing a crumbly soil, which is well drained and well aerated.

In ideal case, manuring 10 t/ha of organic matter is recommended.

## 5.3 Canal Construction and Drainage

According to SOGREAH report Vol. III - Land Classification July, 1972, soil permeability values determined by auger hole method are as follows.

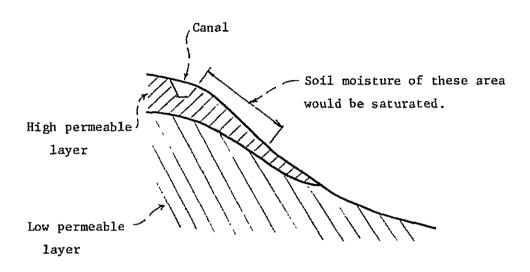
	Condition of lower Horizon and topography	Permeability Values
RBE	GSL to S1 overlying the decomposing Rock	1 x 10 <sup>-5</sup> to 6 x 10 <sup>-5</sup> m/s
RBE	More thicker SCL layers in B Horizon	1 x 10 <sup>-5</sup>
RBE	More sandy and gravelly layer overlying the decomposing Rock	1 × 10 <sup>-4</sup>
RBE Imperfectly drained LHG	SCL to SC layers at depth 3 and 7 feet, Lower aspect of the slope	1.5 x 10 <sup>-6</sup> 9 x 10 <sup>-6</sup>
LHG	Lower aspect of slopes	$6 \times 10^{-6} - 5 \times 10^{-5}$
LHG	SCL to SC without any interlayers of Sand or Gravel	1 × 10 <sup>-6</sup> - 3 × 10 <sup>-6</sup>

The above estimated values of permeability seem to be adequate.

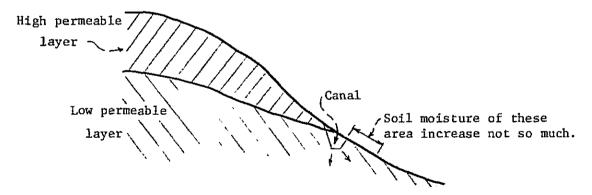
From a point of view of land use, the appropriate canal is better to construct on lower aspect of slope and not higher aspect. Because, if the canal is constructed at the higher aspect of slope, the soil moisture of lower parts of canal will be always so high depending on the high permeability of the soils where canal constructed, that upland crops are unsuitable at this part. (View point from soil sciences.)

However, if the canal is constructed at lower aspect, the soil moisture of lower part of canal would not increase so much depending on the low permeability of the soil where canal is constructed, that lowland paddy is not affected by the high increase of soil moisture.

#### Unrecommendable

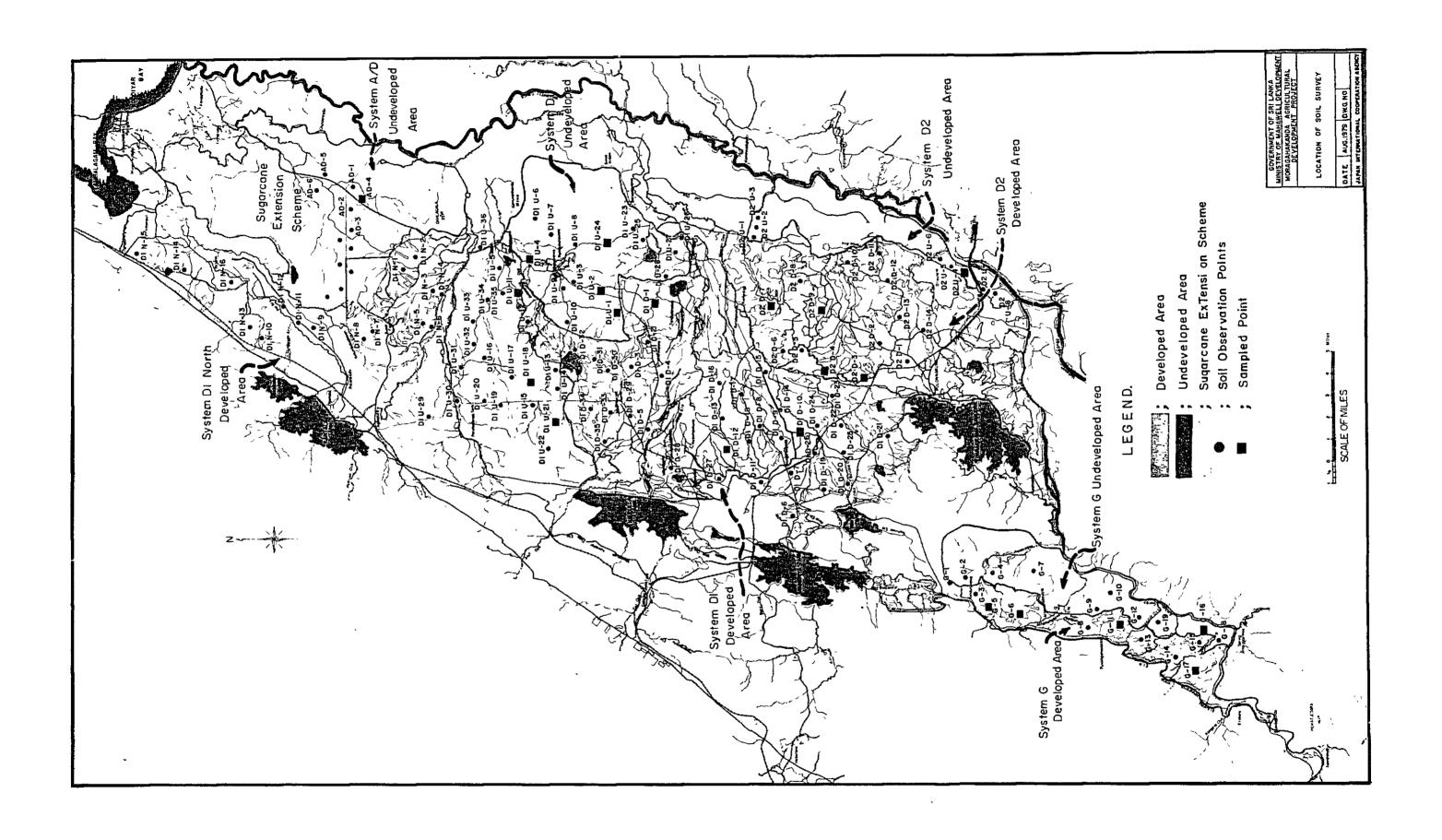


#### Recommendable



Moreover, the lose of water from canal at high aspect of slope is less than that at low aspect.









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# ANNEX VI IRRIGATION AND LAND DEVELOPMENT

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#### I: ENGINEERING STUDIES AND INVESTIGATIONS

#### 1.1 PRESENT IRRIGATION AND DRAINAGE SYSTEMS

#### 1.1.1 Irrigable Area

The area covered by Moragahakanda dam comprises the existing cultivated lands being irrigated by main irrigation canals and a group of tanks following as the starting point Elahera and Amgamedilla headworks intaking water from Amban Ganga and the new land reclaimed by an increase in water supply through the dam.

This region corresponds to Systems  $D_1$ ,  $D_2$ , G and A/D of the Mahaweli Ganga Development; the total area irrigated by the dam covers approximately 1,200 km<sup>2</sup> (460 mile<sup>2</sup>).

As a result of the survey, the area irrigated by the existing tanks and main irrigation canals is summarized in Table 6.1.1. The result indicates that the irrigated area has become larger than that mentioned in the report prepared by M.D.B; this is mainly because, in the previous survey, the area reclaimed without any permission or irrigated by reintaking water has not been included in a part of the irrigated area, but the area irrigated by main tanks only included.

Report System	MDB (1977)	JICA F/S Team
G	4,800 ac	4,800 ac
D <sub>1</sub>	49,400 "	69,100 "
$D_2$	19,000 "	25,000 "
A/D	ı	
Total	73,200 ac (29,600 ha)	98,900 ac (40,000 ha)

Table 6.1.1 Existing Irrigated Area

#### 1.1.2 Irrigation System

The present irrigation system shows that the planting condition realized after completion of Polgolla-Bowatenna Complex in May 1976 is taking a favourable turn in comparison with the previous years. The

planting conditions obtained by conducting local interviews are summarized in Table 6.1.2. In addition, variations in the tank storage capacity before and after completion of the Polgolla-Bowatenna Complex are shown in Figs. 6.1.2 to 6.1.6.

Juding from these data, it is obvious that supplied water has become more abundant; however, it is anticipated that this situation will be slightly deteriorated in the near future, because the newly reclaimed land proposed under the Polgolla-Bowatenna Complex has not yet been completed.

There are some parts suffering from shortage of irrigation water during the Yala season in spite of supplying more irrigation water than projected. This is because that the existing agricultural facilities (irrigation canals and diversion facilities) have old vintage and the dead water caused by their superannuation has become more abundant and also because that due to loosening water supply management surplus water is being intaken on the upstream side.

The reason why the planting condition at Parakrama Samudra is more favourable than the others is that Kalu Ganga, a branch river of Amban Ganga, is abundant in river water discharge and, moreover, irrigation water management is facilitated due to the existence of one tank.

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Table 6.1.2 Existing Irrigation Area

(unit: acs)

System	Scheme	Scheme Acreage under specification		Total
G	Elahera	4,800	-	4,800
	Minneriya	13,500	4,500	18,000
	Giritale	6,200	1,300	7,500
	Kaudulla	10,500	2,500	13,000
	Kantalai			
D <sub>1</sub>	Vendarasan- kulam	20,800	3,100	23,900
	Paravipanchan- kulam			
	Galamuna (Minneri oya)	3,300	1,700	5,000
<u> </u>	Kahambiliya	500	100	600
	Wan Ela	1,000	100	1,100
	(Sub total)	(55,800)	(13,300)	(69,100)
D <sub>2</sub>	Parakrama samudra	19,600	5,400	25,000
A/D	-	-	_	_
	Total	80,200	18,700	98,900
		(32,400 ha)	(7,600 ha)	(40,000 ha)

#### 1.1.3 Drainage System

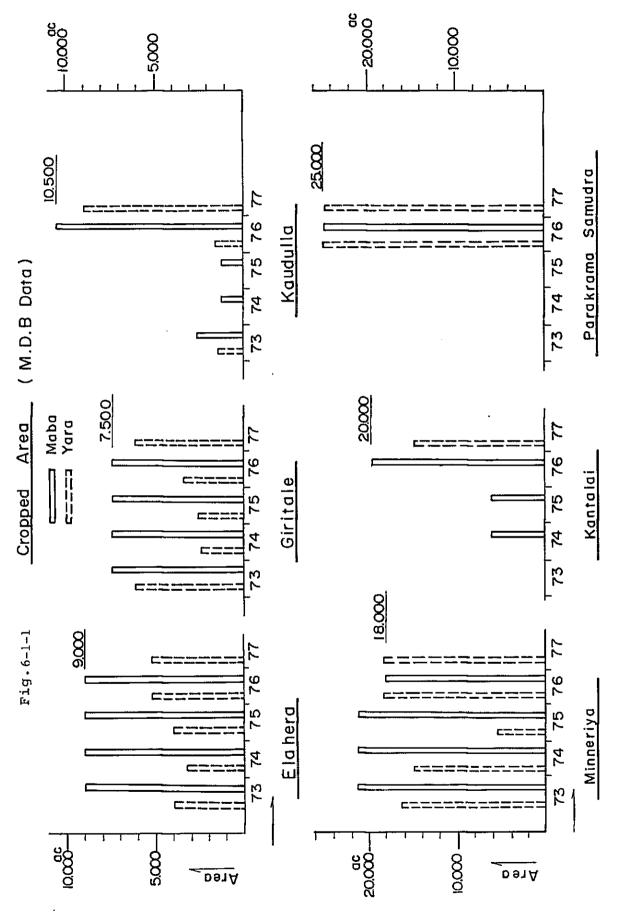
For as the present drainage system, drained water is all flowing down through the drainage canal system consisting of such natural rivers as Aru, Oya and Ganga and mostly flowing into Mahaweli Ganga in the end.

Since there exists almost no embankment along Mahaweli Ganga, but partially, the river is overflooded over a few miles wide during the flood season.

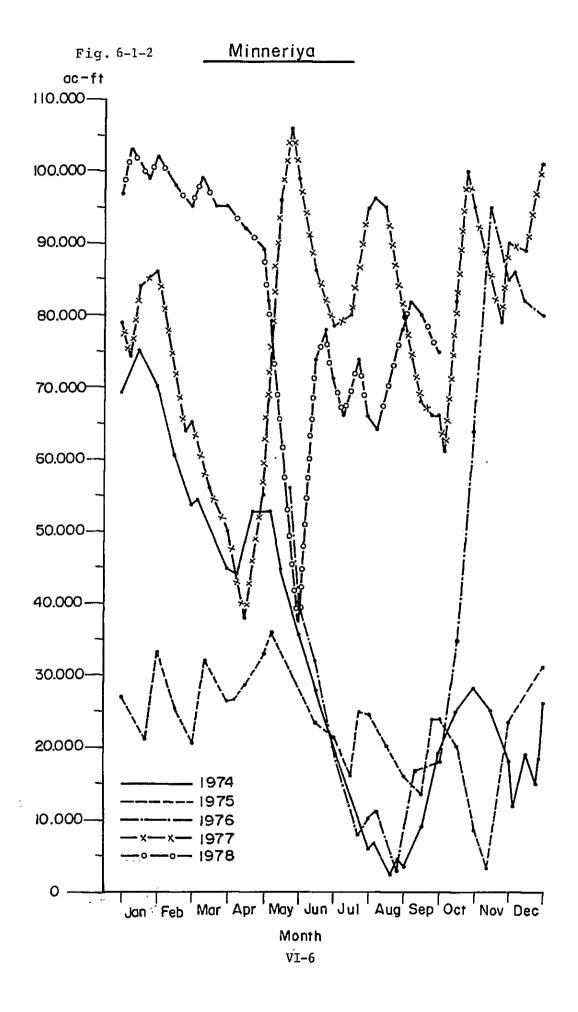
Particularly, System  $D_2$  encircled by rivers is isolated during the flood season and most parts of which are inundated due to its gentle undulations and low lands.

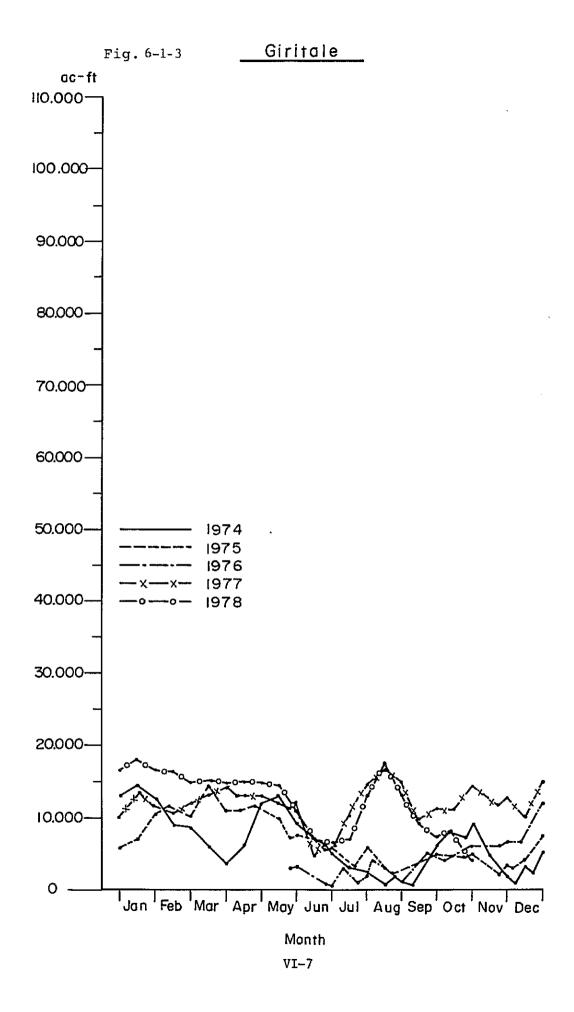
In addition, System A/D is embanked along Mahaweli Ganga; however, draining is not so smooth because of its location near to the river mouth and low lands are inundated.

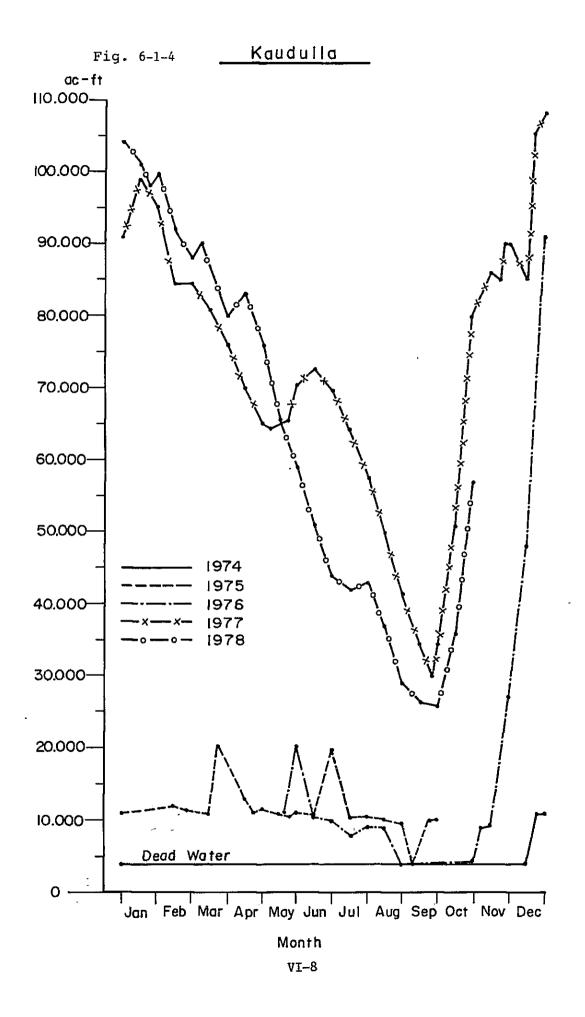
Branch rivers are all naturally formed and overflooded during the Maha season; there are many parts inundated in the vicinity due to mazy river channels and the low flow capacity.

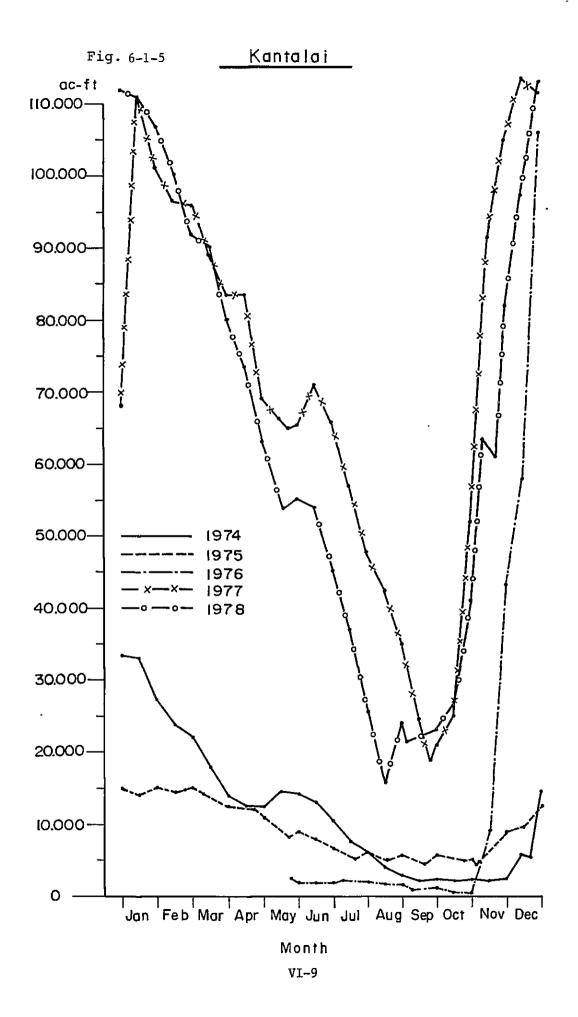


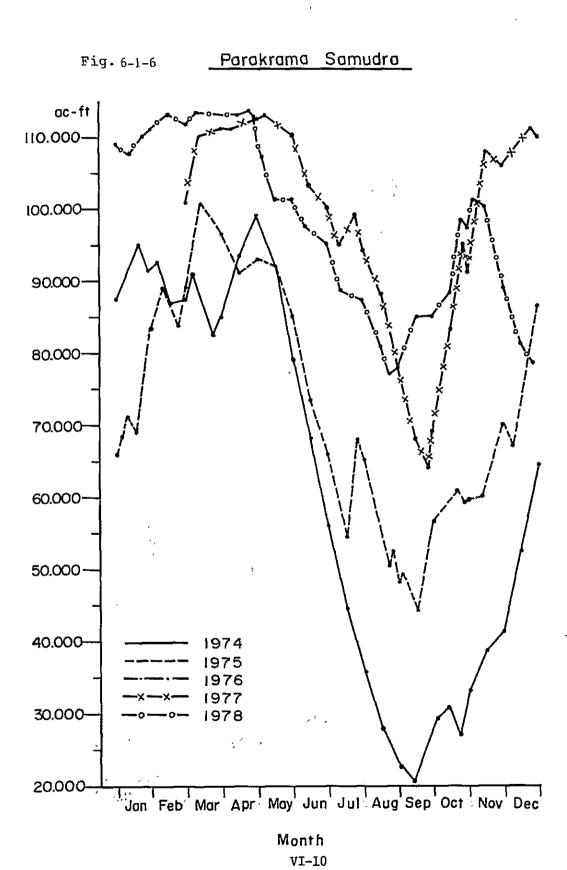
VI-5

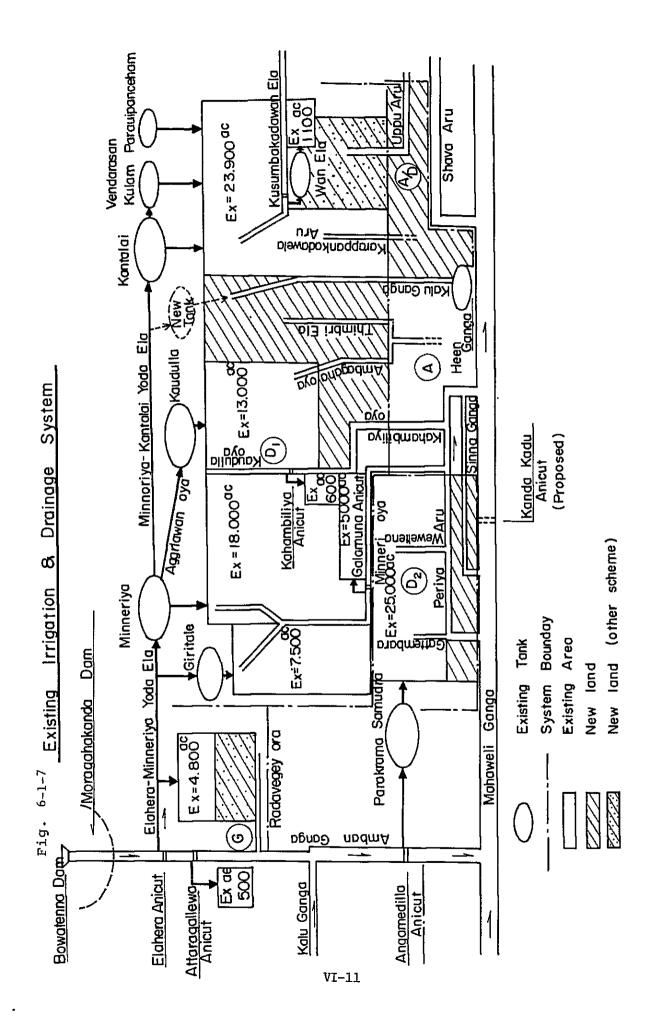












#### 1.1.4 Existing Irrigation Facilities

They mainly consist of tanks, anicuts and some lift-irrigation facilities as follows:

#### (1) Tanks

Besides those shown in Table 6-1-3 below, the details of which have been obtained from Polonnaruwa C.I.E office and I.EE offices at Minneriya (Hingrakgoda) and Kantalai, there are numerous minor tanks which are of much smaller scale in their storage capacities and irrigable areas, hence they have been taken into account supplementarily to the major irrigation schemes in water balance study.

Table 6-1-3 Existing Tank Capacities

		· <del>**</del> · · ·				Availab	
	Name	Capac	ity	Dead (	Storage	Storage	Capacity
		1000 <sup>ac-</sup>	ft <sub>10</sub> 6 <sub>m</sub> 3	1000 <sup>ac-ft</sup>	10 <sup>6</sup> m <sup>3</sup>	1000 <sup>ac-ft</sup>	10 <sup>6</sup> a
	Kaudulla	104.0	128.0	4.5	5.0	99.5	123.0
	Minneriya	110.0	136.0	4.0	5.0	106.0	131.0
	Kantalai	110.0	136.0	4.0	5.0	106.0	131.0
D <sub>1</sub>	Vendarasan Kulan	20.2	25.0	-	-	20.2	25.0
	Giritale	18.8	23.0	0	-	18.8	23.0
	Sub Total	363.0	448.0	12.5	15.0	350.5	433.0
D <sub>2</sub>	Parakkama Samudra	110.0	136.0	15.0	19.0	95.0	117.0
	Total	473.0	584.0	27.5	34.0	445.5	550.0

	Paravipanchan Kulam	T <sub>Q</sub>	5.5	4,500		225 (135.0)		Kantalai area	ft 1430	_	U/S 1 on 3.0 D/S 1 on 2.5	Chate Type Length 120' Crest L 135.0 <sup>MSL</sup> H.F.L 141.15 <sup>MSL</sup>	S111 E 110.0 <sup>MSL</sup>
	Vendarasan hulam	D <sub>1</sub>	4.3	20,200	ı	1,100 (180.0)		Kantalai area	3800 1800		U/S 1 on 2.5 D/S 1 on 2.5	Geusevay Cum Length 50' Crest L 180.04SL H.F.L 183.04SL	5111 E 140.5 <sup>MSL</sup> 1/3'0¢
	Parakrama Samudra	$^{D_2}$	28.0	110,000	15,000	6,275 (194.0)		19,600 (25,000)	mile ft 8 2320	200.0 12.0	U/S 1 on 3.0-2.75 D/S 1 on 2.5-2.0	Matural Spill Length 440' Grest L 195.045L Radial G Length 100' No.10' Crest L 194.045L	B.C. Tower (H.P) 4/42'¢ H.P \$111 U/\$ 169.0 MSL D/\$ 168.23 " 0 350cusec R.C. Tower 1(culver)
Tout	Giritale	D1	9.4	18,000		760 (302.0)	-	6,200 (7,500)	1700 1700	310.0 to 319.0 30.0	U/S 1 on 2.0 D/S 1 on 2.0	Clear vith Length Crest H.F.L	L.B Tower Sluice 1/2'-6''x1'-6" U/S 259.35#SL R.B Tower Sluice 2/4'-0''x32" U/S 264.75#SL
Har of txisting Tank	hantalai	Dı	Kantalai 77.1 Gal OYA 83.0 Aluth OYA 28.0 Total 188.1	110,000	4,000	5,950 (194.5)		20,800 (23,900)	mile ft 2 1584	208.0 to 202.0 45.0	U/S 1 on 3.75-2.0 D/S 1 on 3.0 -2.0	Radial G 10NOS Clear 10/15'x8' vith H.F.L 201.5HSL Length Crest L 194.5HSL Crest Sill L 186.5HSL H.F.L	L.B 2,2'*x' Sill L   52.6 MSL Max.Q 570cusec Area   10,640ac R.B(01d) 2,2'/4' x 21,2' 2,11 L   153.4 MSL Max.Q 440cusec Area   15.0 MSL Sill L   155.7 4 MSL R.B(Hontana) 2,4'* 2,1'2' Sill L   155.7 4 MSL Ax.Q 614Cusec 4/31/2 Bice 4/31/2 Bice 4/31/2 Bice 4/31/2 Bice Area   1.58/3cc
ļ	Minneriya	D <sub>1</sub>	92.6	000'011	7,000	6,300 (307,42)	200	13,500 (18,000)	mile ft 1 3900		U/S 1 on 2 D/S 1 on 3	L.B NO.1(Kantalat) Radial G 2NOS/15'x8' Slide G 2NOS/16'x5' Slil L 294,9HSL L.B NO.2(Kaudulle) Radial G RADS/2CCESCL 307,4HSL SIIL 294,9HSL	Cow(R.B)  Masonary  2/4'-9'x3.0'  269.32HSL  279.73HSL  179.73HSL  279.73HSL  279.73HSL  279.73HSL  279.73HSL  275.0HSL  1/3'x2'-6''  1/3'x2'-6''  1/3'x2'-6''  1/3'x2'-6''
	Kaudulla	D <sub>1</sub>	32.0	104,000	4,500	6,100 (242.0)	550	10,500	mile fr 5 3900	22 73	U/S 1 on 3.0 D/S 1 on 2.5	9 X Q N	Low Level (R. 4) Type R.C. Tower Opening 4' 6 Cast Sill L 210.0'HSL Hight Level (L. B) Hight Level (L. B) 3/3'-9"x5'0 Sill L 215.0
	1ank	Svatem	H11e <sup>2</sup>	AC-ft	=	AC (H.S.L)	¥	AC (H.S.L)	Mile-ft	7. S. P.	u		
Table 6-1-4		ltem	Catchment area	Capacity	Dead storage	Area at F.S.L ( )	Area at Sill	Irrigable area (outside spec)	Bound (Dam) Length	Top Level	Slopes	Sp111	Sluice

;

Table 6-1-5
List of Minor Tanks (Capacity  $30^{ac}$ )

Name of Minor Tanks	Name of Minor Tanks	Capacity	Caltivable Area
		ac-ft	ac
Kaudulla			
	Ambagaswewa	2,102.5	1,188
Parakrama Samudra			
	Kalahagala		30
	Kadawala Wewa	100.0	300
	Amaulunda		108
	Aluth Wewa	150	60
	Kirinatidamanawewa	500	99
	Uradikul <i>e</i> mwewa		30
Giritale			
	Ilukwewa		30
	Gallida	516	177
	Paluwewa	159	50
	Baddepanwiwla	270	70
	Divalamkadawala	313	100
	Pahalasiyambalawewa	110	36
	Wewalawewa	138	40
	Deegannawewa	240	80
	Nikawewa	306	102
	Wijerajawewa	225	75
	Ihalasiyambalawewa	129	33
	Madaymalawewa	300	100

# (2) Anicuts

Besides Elahera and Angamedilla anicuts on the Amban Ganga, there are some anicuts which collect the drainage water flown into the the riverlets such as at Galamuna, Kahambiliya, etc. The particularsof Elahera and Angamedilla Anicuts are shown in Table 6-1-6.

#### (3) Lift Irrigation

Small acreage (19 - 200 ac) in being irrigated by low-head pumps; more than one-half of lift irrigated land is in System G (600 ac) and about 600 ac in other Systems, totalling 1100 ac. Details of lift irrigation schemes will be known from Table 6-1-7.

Table 6 -1-6

Existing Anicut

Item	Unit	Elahera Anicut Amban Ganga Kuda	Anicut Kuda Ganga	Angamedilla Anicut
Catchment Area	M11e <sup>2</sup>			540.0
Length	£t	585.3	105 - 31	0.06
Crest Level	MSL	455.5	455.5	226.4
Scour Gate		je.	Fixed Wheel Gate 2 Nos 10'x 5'	Hand wind 1 Nos 5' x 4'
Sill Level	MSL	1	437.1	216.5
Crest Level of divide wall	MSL	1	442.1	226.91
Head Sluice No. of Opening	٠	É ``	Fixed Wheel Gate 2 Nos II'x 8'	R.C with Gates 2 Nos $10' \times 4'-6"$
Level	MSL	1	439.1	219.2
F.S.L. H.F.L.	MSL	1	447.1	<i>b/s</i> 223.73 230.67
Capable of Discharging	Cusec	ı O	Normal 1,500 Overload 2,000	1,000

Name	Pump St No.	No.of Pump	No.of fore Bay	Acreage under Each fore Bay	Total Acrege
(Kaudulla)					
Stage 1 TR 5	1	1/6" dia	1	32	32
TR 5	2	1/7" 1	1	52	52
				Su	ь.т 84
(Minneriya)					
Stage 3 LB7	3	1/6" dia.	1	22 )	49
LB9	3	1/6" "	1	27 )	7.5
(Giritale)					
LB	6	1/4" dia	1	27	
RB Tract 5	7	1/6† "	3	(30.75) (35.25) 16.50)	82.5
" " 3	7	1/6" dia.	1	45	45
		•		Sub	.т 127.5
(G. System)					
Konduru Stage II	8	1/4" dia	1	30)	
Wewa		2/8" "	2	90) 80)	200
Stage I	9	1/6" dia	1	66)	
J		1/6"	2	32) 62)	158
Bakamuna Stage III	10	1/6" día	1	72 <sup>.</sup>	72
" II	11	1/8"	1	104	104
n I	11	1/6" ,		60	60
				Sub .	T 594
(Minneriya Oya)					
Sunga Wila	12	1/6" dia. 1/6"	) 2	67 18 )	85
(P.P.S.)				6.07	
Dļ Kalinga Ela Unit I	13	1/6" dia.	2	$\binom{0.8}{26}$	00
II	13	1/4"	i	32 )	92
III	14	1/6"	1	26 )	
D2 LB 4	15	1/6" dia	1	48	48
D3	16	1/3" dia.	1	19 Sub	т 159
Total				<u>.</u> ₹	1,098.5 1,100 ac

#### II. PLANS AND STUDIES

# 2.1 Identification of Irrigable Area

The area currently irrigated totalling 98,900 ac (40,000 ha) has been included in its entirety into the irrigable area, together with 19,500 ac (7,900 ha) which will be developed under Polgolla-Bowatenne Complex (10,000 ac or 4,100 ha in System G and 9,500 ac or 3,800 ha in System D1) and the land extending over 34,400 ac (13,900 ha) in Systems D1, D2 and A/D which will be made newly irrigable by constructing the Moragahakanda reservoir, and undeveloped sugar cane area of 1,000 ac (400 ha) in the downstream of Kantalai Tank. The total irrigable area, therefore, would be 153,800 ac (62,200 ha) as is detailed in Table 6-2.-1.

Topographic maps used for identification of the newly reclaimable area were both outdated and incomplete; to cover such gaps coaser maps (1 inch to 1/2 mile = 1/31680) had to be used, as follows:

```
1 inch = 4 chains (1/3168) and 1 inch = 12 chains
System D1
                  (1/9504) in parts
       D2
            .... 1 inch = 1/2 mile (1/31680)
            .... 1 inch = 1/2 mile (1/31680) and 1/10000
       A/D
                  Contours:
         1 inch = 4 chains & 12 chains ....
                                                2 feet
                = 1/2 \text{ mile}
                                               20
                                         ....
         1 "
                = 10000
```

5 meters

Demarkation of the newly reclaimable area(s) has been done somewhat differently between Systems: in System D1, the main canal route was first determined and then the irrigable area has been planimeterd, while in System D2 and A/D for which contours on the maps used were too wide, making it difficult to chalk out the irrigable areas, therefore, the ratio between the gross area and net irrigable area in the adjacent places has been applied for determining the irrigable areas there.

Since development of 19,500 ac under the Polgolla-Bowatenne Complex and 1,000 ac sugarcane field in the downstream of Kantalai Tank should be feasible without the Moragahakanda reservoir, these two areas were first put under the 'Other Schemes' apart from the Project's irrigable area, but as it was found out that the reservoir can make them irrigable together with other new lands, they have been included in the Project benefit area (see Table 6-2-2).

## System D1

The newly irrigable area corresponds to that covered by Stages III and IV of Kaudulla Scheme. Under Kaudula Scheme, it was made 28,000 ac (11,300 ha) but has been revised to 22,400 ac (9,100 ha) by the present study (Stage III = 11,500 ac and Stage IV = 10,900 ac). According to a recent I.D plan (January 1979), the cultivation area in System D1 was estimated at 70 per cent of the total, that is, Stage III 13,715 ac plus Stage IV 13,985 ac = 27,700 ac which seems to be an over-estimation.

#### System D2

The newly reclaimable area is spreading in the downstream of the existing Parakrama Samudra Tank. It is a lowland encircled by the Mahaweli Ganga and the Periya Aru, habitually inundated during Maha season. It was originally estimated at 9,100 ac (3,700 ha) but, as a result of the present survey, it has been identified as net irrigable area 5,400 ac (2,200 ha) out of the gross area of 12,000 ac. This irrigable acreage may be subject to change after the Kandukadu anicut will be completed.

# System A/D

This area was previously included in System A, to be made irrigable by Kandukadu anicut, but has been put in System A/D from water balance, priority and topographic points-of-view. This area is lowly situated and liable to the influences of the Mahaweli Ganga like System D2 area but is now protected by embankment. It was originally planned to irrigate 9,100 ac (3,700 ha) but irrigability has been reduced to 6,600 ac (2,700 ha) as a result of the present survey. There is a plot of land which was developed by the Tobacco Corporation to the extent of 2,000 ac and Heen Ganga Tank has been constructed to irrigate this plot by storing the Kalu Ganga runoff. MDB is planning to develop this land.

		מ	eme)	0	ration				
	(ha)	Remarks	(Other Scheme	EEC/UNDP/FAO Mission	Sugar Corporation				
	Unit ac	Total		14,800 (6,000)	102,000 (41,300)	30,400 (12,300)	6,600 (2,600)	153,800 (62,200)	
gable Area			Sub Total	10,000 (4,100)	32,900 (13,300)	5,400 (2,200)	6,600	54,900 (22,200)	
Proposed Irrigable Area		New Land	Moragahakanda	ı	22,400 (9,100)	5,400 (2,200)	6,600 (2,600)	34,400 (13,900)	
			Other Scheme	10,000 (4,100) * 1,000	(400) 9,500 (3,800)	1	ı	20,500 (8,300)	
		Existing	)	4,800 (1,900)	69,100 (28,000)	25,000 (10,100)	ı	98,900 (40,000)	
able 6-2-1		System		ც	DI	. D2	A/D	Total	

\* under construction

	Tanks or	UNDP/FAO 1968 Report	0 1968	Report	91 1	// NOV / Unautho	1977 NOV MDV Report Unautho		Result Exist-	of Fiel Exist-	ld Surve	ey by F	of Field Survey by F/S Team Exist-		Grogi	Gross Area	Proj	Proposed Area		Irrigable Area	62	
Sya- res	cen (Read Work)	Exist- ing	Hev	Total '		-raised & Pol Comp.	a a	Total		ing out- side spec	Other	ž	Totel	Total Exist-	Other sheme	Nev	Total	Exist- ing under spec	Exist- ing out- side spec	Other	New	Total
ن	Erahera- Minneriya Yoda Ela	4,800	6,200	4,800 6,200 11,000 4,800 6,200	4,800	6,200	ı	11,000	4,800	1	10,000	1	14,800		8,000 23.240	, c	31,200	4,800	'	10,000		14,800
	Giritale	4.,400	t	4,400					6,200	1,300	r	i	7,500	7,500 11,200		•	11,200	6,200	1,300	ŧ		7,500
	Minnerlya	14, 325	ı	14,325					13,500	4,500		1	18,000	18,000 26,300	1	i	26,300	26,300 13,500	4,500	1	•	18,000
	Kaudulla	10,230			49,400	13,800	49,400 13,800 28,000	91,200	10,500	2,500	1	22,400		35,400 25,600		55,700		81,300 10,500	2,500	ı	22,400 35,400	35,40
ជ	-		29,200	29,200 61,660					20,800	3,100	9,500		34,400	34,400 42,800 18,700	18,70		61,500	61,500 20,800 3,100 10.500	3,100	10.500		34,500
	Paravipan- cham										•											
	Galamuna Ani (Minneri Oya	t + =	•	•					3,300	1,700	ı	ı	5,000	005,6	1	ì	6,500	3,300	1,700	•	•	5,000
	Kahambiliya Oya Ani	l nj	ı	•					200	100	•	ı	909	3 1,100	1	•	1,100	200	100	t	ı	909
	Wan Ela	ı	•	1					1,000	100	ι	i	1,100	1,100 2,200	1	ı	2,200	2,200 1,000	100	1	1	1,100
	Sub-Total	51,185 29,200	29,200		80,385 49,400 13,800 28,000	13,800	28,000		55,800	13,300	10,500	22,400	102,000	1115,700	18,70	0 55,700	91,200 55,800 13,300 10,500 22,400 102,000115,700 18,700 55,700190,100 55,800 13,300 10,500 22,400102,000	55,800	13,300	10,500	22,400	102,00
D2	Parakrama Samudra	18,200	9,100		27,300 19,000		9,100	28,100 19,600	19,600	5,400	ı	5,400		30,400 42,000		12,000	12,000 54,000 19,600	19,600	5,400	1	5,400 30,400	30,4
Q/V	Kantalai	ι		1	ţ	t	9,100	9,100	1	ı	2,500	4,100	6,600	•	t	14,400	14,400 14,400	1	ı	.•	6,600	6,600

2.2 Estimation of Irrigation Water Requirements

# 2.2.1 Rainfall and Meteorological Data

Major rainfall and meteorological stations located in and around the project area are illustrated in Fig. 6.2.1. Meteorological stations are as follows:

- (a) Maha-Illuppallama
- (b) Annuradhapura
- (c) Trincomalee

Rainfall stations are as follows:

- (a) Elahera (Bakamuna)
- (b) Polonnaruwa
- (c) Hingurakgoda
- (d) Kantalai

Besides, there are several rainfall stations in and around the project area. But, from recording years observed and location, the typical rainfall stations are above four stations.

Meteorological data of three meteorological stations are shown in Table 6.2.3 - 6.2.6 The mean monthly rainfalls for the last twenty eight (28) years (from 1950 to 1977) recorded at each rainfall stations are shown in Table 6.2.7 - 6.2.10. The meteorological observation at the Kandulla Tank left bank is continued from 1978 by Irrigation Department. As the Kandulla area is located at the centre of the project area, the observed data will be effective meteorological data for the detailed design.

Fig. 6.2.1.

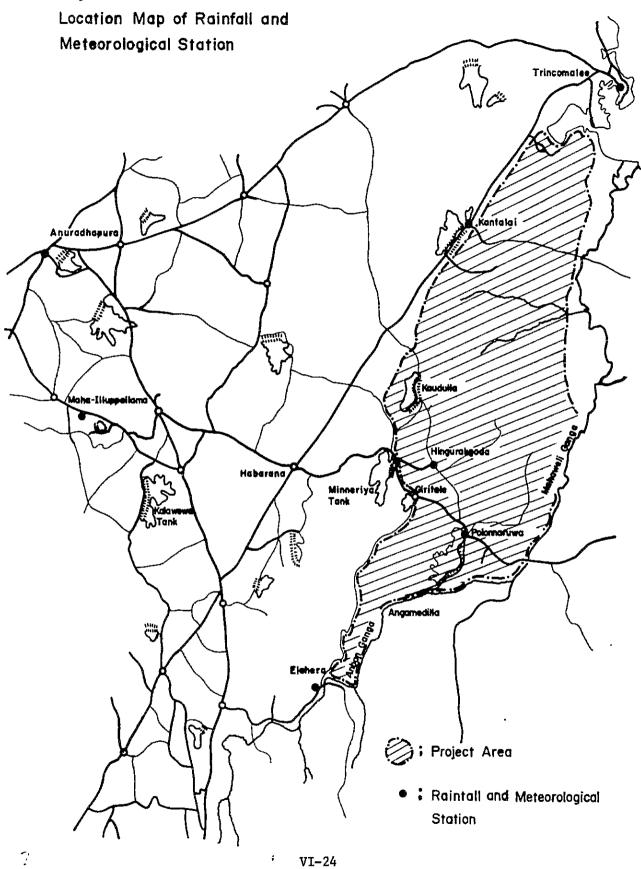


Table 6-2-3

Name	11	Station: MAHA ILLUPPALLAMA		Lat:08°07'N		Long:80°28'E		Barometer:452ft.	452ft.	Anemo	Anemometer:10ft.		1=0830 S.L.S.T.	L.S.T.	11-173	ای		ı	ŀ	
Degree of the control		1	1		Ŀ	70.57	Utahant	1	Moon	Mean	Prevat-		Number	Rain-		Heavi-	No. of	Cloudi-	%.of	No. of
Column   C	Mean Sea	ri ci	יין זיין	Ke1a-	Mean do flo	da41v	Max.		Mind	daily	11mg		oţ				ij.	ness	days	days
The control of the co	rever		arno	) 1 2 1 1 1		1 1 1	remo.	temb.	speed	wind	Mind		rainy						ö	ij
**C         **D         **D <td>Fressu-</td> <td></td> <td>reap.</td> <td>dicy</td> <td>remp.</td> <td>remp.</td> <td>recor-</td> <td>recor</td> <td>at</td> <td>speed</td> <td>direct</td> <td></td> <td>days</td> <td></td> <td></td> <td></td> <td>shine</td> <td></td> <td>thun-</td> <td>80</td>	Fressu-		reap.	dicy	remp.	remp.	recor-	recor	at	speed	direct		days				shine		thun-	80
23.2         88         29.1         20.4         13.3         1.1         6.0         40.4         13.9         7.2         4.7         13.9         1.2         40.4         13.9         1.2 <th< td=""><td>:</td><td></td><td></td><td></td><td></td><td>•</td><td>ded</td><td>qeq</td><td>hour</td><td></td><td>Tou</td><td></td><td></td><td></td><td></td><td></td><td>per day</td><td></td><td>, ,</td><td></td></th<>	:					•	ded	qeq	hour		Tou						per day		, ,	
23.2         88         29.1         20.4         13.3         14.4         6.9         7.2         NE         113.8         9         0         404.6         127.0         7.1         4.7           25.2         70         13.2         13.4         6.6         7.1         NE         51.3         5         6 yrs. 1921         9.0         4.3           23.6         6         31.1         20.4         195.28         19.3         NR         51.3         5         6 yrs. 1922         196.7         4.3           23.7         82         31.4         21.7         38.1         15.9         6.4         6.3         WE         89.7         6         196.7         9.0         4.3           25.7         82         31.4         21.7         38.1         15.9         6.4         6.3         WE         89.7         6         196.7         9.0         4.3           25.3         82         31.4         8.6         5.9         9.9         7         4         9.2         4.1         1.3           25.4         80         32.4         8.6         13.4         12.1         18.2         1.2         1.1         1.1         1.1 </td <td>í</td> <td></td> <td>Ç</td> <td></td> <td>•</td> <td>٥</td> <td>U</td> <td>ູບ</td> <td>kmph.</td> <td>kmph.</td> <td></td> <td>i</td> <td></td> <td></td> <td></td> <td>œ.</td> <td></td> <td></td> <td></td> <td></td>	í		Ç		•	٥	U	ູບ	kmph.	kmph.		i				œ.				
23.8         6         31.1         20.4         36.2         13.4         6.6         7.1         NE         51.3         5         6         yrs.         107.5         8.4         3.8           23.8         6.4         13.4         6.4         6.3         NE         8.7         6         58.0         106.7         9.0         4.3           23.7         8.2         33.4         21.7         36.1         15.9         6.4         6.3         Nar.         89.7         6         28.0         106.7         9.0         4.3           25.2         8.2         13.4         1.2         1.6         13.4         12.1         13.4         12.1         13.6         13.4         12.8         8.7         4.7         193.7	101	١٨٠	23.2	88 5	29.1	20.4		14.4	6.9	7.2	¥ ¥	113.8	6	0 2 yrs.	-	127.0 1921.9	7.1	5.0	н	4
26.1         3.2         3.3.4         21.7         38.1         1.5.9         6.4         6.3         Var.         89.7         6         5.6         285.0         106.7         9.0         3.2           30.2         5.7         4.2         13.4         1.2         1.2         1.8         5.4         6.3         Var.         182.0         1920         1920.5         9.0         4.1         1         4.5         1.4         4.3         4.1         1         4.5         1.4         8.7         6.0         3.7         14.3         8.7         6.0         3.7         14.3         8.7         6.0         3.7         14.3         8.7         6.0         3.7         14.3         8.7         6.0         3.7         14.3         8.7         6.0         3.7         14.3         8.7         8.0         9.3         7         4         4.7         11.1         8.0         8.0         9.3         7         4         4.7         11.1         8.0         8.0         9.3         9.3         9.3         9.3         9.3         9.3         9.3         9.3         9.3         9.3         9.3         9.3         9.3         9.3         9.3         9.3	1012.7	, ,,	23.8	98	31.1	20.4		13.4	9.6	7.1	N N	51.3	'n	0 6 yrs.	_	107.9	8.4	3.8	7	7
26.6         33.6         23.2         19.8         5.8         5.9         Var.         182.9         11         7.1         455.7         143.8         8.7         4.1           29.3         69         33.4         24.4         1965.30         7.9         Var.         193.0         194.1         1.64.1         6.0           29.3         69         32.4         24.4         36.7         20.6         13.4         12.1         5W         99.3         7         4 yrs.         1931         1944.1         6.0           28.9         71         21.0         21.6         13.4         12.1         5W         99.3         7         4 yrs.         1931         1944.1         8.2         5.9           28.9         73         24.0         37.1         21.0         17.9         16.4         5W         30.2         3         17.1         193.1         195.3		, 0.	25.7	82	33.4	21.7		15.9	4.0	6.3	Var.	89.7	9	5.6 1941	285.0 1920	106.7	9.0	3.2	9	4
27.4         80         32.4         36.7         20.6         13.4         12.1         SW         99.3         7         0         347.0         17.7         8.2         5.6           28.8         71         37.1         21.0         13.4         12.1         SW         19.3         4         0         165.9         12.2         5.9           28.9         78         32.2         24.4         37.1         21.0         17.9         16.4         SW         19.3         4         0         165.9         121.9         7.9         6.0           28.5         67         37.2         20.0         17.2         10.9         15.9         17.1         15.8         SW         30.2         3         17.4         92.7         7         6.0           28.6         75         32.9         24.0         36.3         19.9         17.1         15.8         SW         56.9         4         0         217.4         92.7         7         6.0           28.6         63         32.9         24.0         36.3         19.4         17.1         15.8         SW         56.9         4         0         217.4         92.7         7	3 3 3	5.0	26.8	92 69	33.6	23.2	36.6	19.8	5.8	6.8	Var.	182.9	11	7.1 1936	455.7 1921	143.8 1944.1	8.7	6.0	17	H
26.9         3         24.4         37.1         21.0         17.9         16.4         SW         19.3         4         0         165.9         121.9         7.9         6.2           28.5         67.5         67.5         67.1         1953.11         1964.17         18.8         SW         30.2         3         0         181.4         92.7         7.7         6.1           28.5         65         32.9         24.0         37.2         1963.16         17.1         15.8         SW         56.9         4         0         271.4         99.7         7.7         6.0           26.6         76         32.9         24.0         36.3         1965.16         17.1         15.8         SW         56.9         4         0         271.4         99.7         7.7         6.0           26.6         76         32.9         24.0         1965.16         17.1         15.8         SW         226.1         14         78.8         19.7         17.8         6.0           26.8         87         33.1         28.9         8.1         16.0         8.9         SW         226.1         14         97.4         148.8         7.7         5.8	95	2.0	27.4	30	32.4	24.4	36.7	20.6 1971.20	13.4	12.1	A. A.	99.3	,	0 4 yrs.	_	_	8.2	5.6	'n	0
26.6         77         32.5         24.0         37.4         20.8         16.9         15.8         SW         30.2         3         0         217.4         92.7         7.7         6.1           28.6         56.5         55.5         4         0         271.5         89.9         8.1         6.0           26.6         76         36.3         199.9         17.1         15.8         SW         56.9         4         0         271.5         89.9         8.1         6.0           26.6         63         33.1         23.8         195.1         15.8         SW         66.5         4         0         271.5         89.9         8.1         6.0           26.8         75         33.1         23.8         16.7         15.1         15.0         SW         66.5         4         0         271.5         89.9         8.1         6.0           26.0         81         31.7         20.0         17.1         15.0         SW         226.1         14         yrs.         197.1         197.1         197.1         197.1         197.1         197.1         197.1         197.1         197.1         197.1         197.1         197.1	9 2	9.9	26.9	78	32.2	24.4	37.1	21.0 1964.17	17.9	16.4	75 S.	19.3	4	0 7 yrs.	_	121.9 1912.4	7.9	6.2	0	0
26.6         76         32.9         24.0         36.3         19.9         17.1         15.8         SW         56.9         4         0         271.5         89.9         8.1         6.1           28.6         63.6         63         4         0         271.5         89.9         8.1         6.0           28.6         63         4         0         240.4         148.8         7.7         5.8           26.8         56         4         0         340.4         148.8         7.7         5.8           26.0         81         31.7         22.9         137.0         18.5         10.0         8.9         SW         226.1         14         88.9         52.2.2         148.8         7.7         5.8           26.1         72         1959.16         1967.27         10.1         SW         226.1         14         88.9         52.2.2         148.8         6.8         5.6           27.1         73         21.6         1967.2         10.1         8.9         SW         226.1         14         1950.1         145.3         6.1         5.3           26.1         78         36         10.0         8.9	99	80.10	26.6	77	32.5	24.0	37.4		16.9	15.8	75 AS	30.2	ო	0 17 yrs.	-	92.7 1960.11	7.7	6.1	7	0
26.8         75         33.1         23.8         37.2         20.0         17.1         15.0         SM         66.5         4         0         340.4         148.8         7.7         5.8           28.5         6.2         6.2         6.3         84         66.5         4         0         340.4         148.8         7.7         5.8           26.0         81         31.7         12.9         135.1         16.7         8.9         SW         226.1         14         88.9         522.2         148.8         6.8         5.6           27.1         72         1959.16         1967.2         10.1         8.9         SW         226.1         14         88.9         522.2         148.8         6.8         5.6           27.1         72         1959.16         1967.2         10.1         8.9         SW         226.1         14         88.9         522.2         148.8         6.8         5.6           26.1         78         36.0         5.0         5.0         5.0         5.0         5.0         4.0         7.0         7.0         5.2           27.4         88         28.7         21.1         23.2         15.6	9 5	1.6	26.6	25	32.9	24.0	36.3	19.9		15.8	AS AS	56.9	4	0 14 yrs.	_	89.9 1933.11	8.1	6.1	m	0
26.0         81         31.7         22.9         37.0         18.5         10.0         8.9         SW         226.1         14         88.9         522.2         148.8         6.8         5.6           27.1         72.1         1959.16         1967.27         10.1         8.9         SW         226.1         14         88.9         522.2         148.8         6.8         5.6           24.8         86         30.0         21.8         34.9         16.0         5.0         5.5         Var.         253.5         17         61.5         509.8         145.3         6.1         5.2           25.4         88         28.7         21.1         33.2         15.6         6.4         6.5         NE         238.0         14         36.3         1976.4         375.9         5.6         5.3           25.4         78         31.7         22.7         38.1         13.4         10.0         10.2         -1427.5         98         797.0         2499.4         375.9         7.6         5.1           25.7         82         31.7         22.7         38.1         18         18         10         30         71         71         71		6 6 6	26.8	22	33.1	23.8	37.2			15.0	NS AS	66.5	4	0 10 yrs	_	148.8 1974.13	7.7	5.8 8.8	v	0
24.8         86         30.0         21.8         34.9         16.0         5.0         5.5         Var.         253.5         17         61.5         509.8         145.3         6.1         5.2           26.1         78         78         48         197.0         196.2         1927.28         6.1         6.2           23.4         78         28.7         21.1         33.2         15.6         6.4         6.5         NE         238.0         14         36.3         1076.4         375.9         5.6         5.3           25.4         78         78         19.2         1970.5         7.7         NE         1926         1956         1957         1907.15         5.8           25.7         82         31.7         22.7         38.1         13.4         10.0         10.2         -         1427.5         98         797.0         2499.4         375.9         7.6         5.1           27.9         68         11.9         11.9         10.0         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2         10.2		6.0	26.0	81 72	31.7	22.9	37.0		10.0	6.9	AS SW	226.1	14	88.9 1950	-		8.9	5.6	12	7
23.8 88 28.7 21.1 33.2 15.6 6.4 6.5 NE 238.0 14 36.3 1076.4 375.9 5.6 5.3 25.4 78   25.4 78   25.7 62 31.7 22.7 38.1 13.4 10.0 10.2   27.9 68   23 23 23 23 23 23 23 23 18 18 18 10 30 30 71 71 71 71 22 23	25	1.0	24.8	86 87	30.0	21.8	34.9		0.0	5.5	Var. Var.	253.5	17	61.5 1947	_		6.1	5.2	<b>6</b>	п
25.7 62 31.7 22.7 38.1 13.4 10.0 10.2 - 1427.5 98 797.0 2499.4 375.9 7.6 5.1 27.9 68 1957 23 23 23 23 23 23 23 23 23 23 23 23 23	999	12.7	23.8	88	28.7	21.1	33.2		6.4	6.5	N E	238.0	14	36.3 1926		375.9 1907.15		5 S	М	C
23 23 23 23 23 2 3 18 18 10 30 30 71 71 71 22 23	101	7.8	25.7	82 68	31.7	22.7	38.1	13.4	10.0 11.9	10.2	ı	1427.5	98	797.0 1956			7.6	5.1	59	13
	74	m	23	23	23	23	23		18	18	10	30	30	11	וג	<b>z</b>	22	23	<u>ء</u>	۵

Table 6-2-4

	No. of days of fog		o	0	0	0	0	0		0	0	0	o	0	0	0	10
	No. of days of thun- der			7	۵	11	'n	00		71	UT)	in	11	m)	2	\$9	10
	Cloudi- ness (Oct- as)		4.4	3.6	3.0	0. 50 0. 60	5.8	5.7		6.0	9.9	5.7	5.7	5.0	5.0	5.0	25
	No. of hra.of sun- shine per day		7.0	7.8	8.3	4.6	7.9	7.9		7.7	7.4	7.8	4.4	6.2	5.9	7.4	5
į	Heavi- est rain- fall in 24 hrs.	.000	166.4 1963.6	136.9 1922.12	119.4 1919.19	158.8 1955.19	160.8 1932.14	72.6 1906.10		94.0 1938.31	110.7 1965.15	99.1 1914.19	132.8 1924.24	150.6 1920.23	319.5 1948.31	319.5	75
II=1730 S.L.S.T	Rain- fall Wettest wonch	Ė.	\$37.5 1923	195.1 1922	357.4 1936	457.7 1890	1831	176.3 1885		208.0 1910	217.9 1965	349.2 1929	547.1 1902	593.6 1920	927.1 1957	2426.5 1957	105
11=1730	Rain- fall driest month	á	0.8 1916	0 11 yrs.	0 1988 & 1910	13.2 1911	0 3 yrs.	0 10 yrs.		0 24 yrs.	0 8 yrs.	D 8 yrs.	52.1 1870	45.7 1904	62.5 1886	745.2 1956	105
.S. T.	Number of rainy days		12	Ç	7	11	60	4		m	Ŋ	'n	16	19	17	115	30
I*0830 S.L.S.T.	Month- 1y rain- fall	ina,	123.2	53.6	98.8	186.9	93.6	13.5		31.8	46.7	9.69	232,9	248.4	242.3	1447.3	30
	Preval- ling wind direct ion		S S	ENE ENE	២២	AS A	SW	ns Ms		n n	N. N.	NS.	35 AS	Calm NE	N N E		10
Anemometer:-	Mean dialy vind speed	kmph.	0.9	6.3	5.6	5.3	10.3	13.5		12.7	12.7	11.8	7.7	4.5	5.6	80 10.	24
	Mean wind apeed at hour	kmph.	8.0	7.9	7.2	5.3 6.1	11.6 10.9	14.2 15.1		13.2	13.5	12.9	7.6	5.0	5.0 8.8	9.5	25
Barometer: 305ft.	Lowest min. temp. recor- ded	ວ	13.0	12.7 1957.7	14.1 1935.1	18.1 1950.1	20.2 1935.11	21.3 1912.5		20.8 1949.19	20.0 1939.10	20.5 1925.15	1928.28	14.1 1934.13	14.1 1937.6	12.7	65
Baromei	Highest Lowest max. min. temp. recorrect ded ded	ູນ	36.3 1919.9	37.1 1916.29	38.6 1915.1	38.1 1914.24	38.0	37.7 1915.18	1953.1	38.3 1918.22	38.2 1912.10	38.4 1914.17	37.4 1918.1 • 1957.13	34.8 1916.5	33.1 1972.10	38.6	65
18:80°22'E	Mean daily min. temp.	ပ္	20.7	20.7	21.9	23.6	24.6	24.7		24.3	24.2	24.0	23.1	21.9	21.3	22.9	30
Long:8	Mean daily max. temp.	•	28.6	30.7	33.2	33.3	32.7	32.2		32.7	33.0	33.4	31.8	29.9	28.5	31.7	30
Lat:09°21'N	Rela- tive humi- dity	н	22	89 79	85 60	84 71	83 71	79 66		78 64	53	77	83	80 80	91 79	84 69	25
Lat:0	Dry bulb temp.	ņ	23.3	23.9	25.9 30.3	27.4 29.4	27.5	27.3 29.1		26.8 29.0	26.9 29.1	26.9 28.9	26.1 27.4	25.1 26.3	23.8 25.8	25.9	25
Station: ANURADHAPURA	Mean Sea Level Pressurre	đ.	1013.4 1015.2	1012.8 1009.2	1012.2 1008.3	1010.5	1008.2 1005.5	1008,4		1006.5	1008.8 1006.0	1009.7 1006.6	1010.8	1012.2 1009.2	1012.7 1009.7	1010.7 1007.6	22
: ANUR:			-=	- 11	11	111	111	111		11	11	I II	11		- =	11	of irs)
Station	Month	!	January	February	March	Apr11	May	June		July	August	September I	October	Novemver I	December	Annual	Period of Date(lears)

Table 6-2-5

Climatological Table of Observatories in Sri Lanka

stat ion: TRINCOMALEE	NCONVEE	Lat:06°35'N	N, SE.	Long:81	9,51°	Barometi	Barometer: 10ft.		Anemometer:14ft.		1*0830 SLL.S.T.	LL.S.T.		11=1730 S.L.S.T.	. <del>.</del> .				
3	Mean Sea	Drv	Rela-	Mean	Mean do (1)	Highest Lowest	Lowest	Mean	Mean	Prevat-	Month-	Number	Rain-	Rain-	Heavi-	r .	Cloud1-	No. of	No. of
work	re ssur	cemp.	humi- dity	daliy max. temp.	dall) min. temp.	rax. recor- ded	temp. recor-	wind speed at hour	dally wind speed	uing wind direct ion	rain- fall	of rainy days	iall driest month	iali Wettest month	est rain- fall in 24 hrs.	hrs.of sun- per day	ness (Oct- as)	days of thun-	days of fog
	ab.	<b>0</b>	н	ູ	ပ္	<b>.</b>	ů	kmph.	kmph.				mm.		E.				
January 1	1013.7	25.7	78	27.0	24.2	31.7	19.6 1950.3	16.6	18.8	붓끚	210.6	13	0.8 1973	739.6	208.5 1921.9	9.9	5.4	°	o
February I	1013.2	26.2 27.2	77	28.1	24.3	34.3 1915.26	18.3 1947.28	12.4 16.6	14.3	보보	95.2	•	0 6 yrs.	551.4 1965	227.8 1965.14	7.5	4.9		0
March 1	1012.2 1008.8	27.3 28.6	78 1.7	29.9	24.8	37.4 1915.27	19.8 1947.1	8.0 12.2	10.5	N N N D	48.3	'n	0 12 yrs.	282.4 1944	239.0	8.8	3.8	m	0
April I	1000.7	28.5 29.7	77	32.0	25.4	28.6 1956.25	20.9 1943.15	7.9	10.3	St F	76.7	7	o 5 yrs.	237.7 1873	141.0 1955.18	8.9	4,3 5.2	80	a
May I	1008.0	28.9 30.8	72	33.6	26.1	38.7 1915.25	19.4 1920.3	16.7	16.7	MS MS	67.8	9	0 1921 6 1956	434.3 1930	271.5 1930.5	8.0	5.2	9	0
June II	1007.6	28.6 31.2	70 57	33.7	26.2	38.3 1953.2	20.6 1938.25	21.1 19.5	21.8	25 25 25 25	18.5	7	23 yrs.	181.1 1973	79.5	7.7	5.8 6.2	~	0
July I	1008.0	28.0 30.6	71 59	33.7	25.6	38.4 1918.19	21.2 1911.3	19.3 17.2	19.8	AS AS	54.1	4	0 7 vrs.	219.2 1971	99.8 1926.12	7.3	5.7	4	o
August I	1008.3	30.0	71 62	33.5	25.3	37.8 1969.12	20.8 1921.17	18.8 16.3	18.4	as s	102.9	~	0.5 1931	298.2	107.4 1930.28	8.2	5.3	<b>83</b>	٥
September I	1009.3	27.8	71 65	33.5	25.1	37.6 1967.17	21.1 1911.17 6 1948.29	17.5 15.0	16.4	#S	88.9	9	3.0	1901	128.5 1919.15	. 8	5.5 6.3 5.3	60	0
October I	1010.7	27.1	77	31.3	24.3	27.6 1915.16	21.0 1951.8	13.0 13.4	13.4	SK NE	234.7	16	26.2 1974	565.7 1972	154.2	6.9	5.3 6.5	10	0
November I	1011.8	26.4 27.1	81 77	28.7	23.8	35.9 1927.2	18.7 1944.29	10.8 17.1	13.8	SW	355.1	19	54.6 1973	953.5	264.7 1904.19	5.6	5.5	4	0
December I	1012.9	25.9	80 78	27.3	24.0	32.6 1911.3 6 1915.8	19.4 1922.31	17.0 21.3	18.4	NNE	373.9	<b>8</b> 2	56.4 1930	819.9 1948	322.8 1949.17	5.5	5.9 6.1	7	0
Annual I	1010.5	27.4	75 69	21.0	24.9	38.7	18.3	14.9 16.3	16.0	* 1	1726.7	109	886.2 1889	2578.4 1963	322.8	7.4	5.2	98	0
Period of data (yrs.)	30	25	25	30	30	65	65	25	30	10	30	30	107	107	-85	01	25	10	

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ble
Ta

# AVERAGE MONTHLY AND ANNUAL PAN EVAPORATION (M1111meters)

	Jan.	Feb.	Mar.	Apr.	May	Jun.	Jul.	Aug.	Sep.	Oct.	Nov.	Dec.	Anual
°Anuralhapura	118	134	189	174	198	207	220	220	207	143	108	102	2020
Badulla	93	101	143	129	143	138	158	164	159	127	90	78	1523
Batticaloa	133	143	164	183	205	207	220	214	198	164	138	118	2087
Colombo	143	134	180	159	143	144	143	143	138	133	129	133	1722
Diyatalawa	102	115	133	1.14	133	138	158	164	144	112	84	87	1484
Galle	143	148	180	174	174	168	174	180	183	164	138	143	1969
Hambantota	189	193	205	183	180	192	205	205	192	174	153	158	2229
Jaffna	158	162	214	213	245	222	214	198	213	158	129	112	2238
Kankesanturai	164	171	198	207	229	228	214	198	207	158	129	133	2236
Katugastota	174	185	205	174	174	159	164	174	159	143	129	143	1983
Kurunegaia	174	185	214	192	198	168	189	198	183	158	138	143	2140
°Maha Illuppallama	127	157	205	174	205	213	229	220	222	164	123	118	2157
Mannar	158	157	220	198	214	198	1.89	198	192	149	129	133	2135
Nuwara Eliya	118	129	174	138	112	114	102	102	108	93	06	102	1382
Puttalam	164	162	205	168	198	198	189	214	207	149	123	127	2104
Ratnapura	143	162	164	144	133	123	133	143	129	127	114	127	1642
°Trincomalee	164	162	198	207	251	258	282	260	243	174	138	133	2470
Vavuniya	133	134	180	174	190	213	220	220	207	143	123	102	2039

(Unit: inch)

Yala Apr-Sept.	4.26 18.82 19.05 22.62 12.66 15.38 3.57 7.52 4.87 16.95 19.33 20.81 6.82 7.65 17.38 15.98 15.98 15.98 15.98 15.98 11.93	
Maha Oct-Mar.	34.37 74.99 50.46 58.38 67.73 36.50 40.18 40.18 65.32 67.66 64.94 64.94 57.36 57.36 57.36 57.36 57.36 75.38 37.29 39.90 47.66 52.31	
Annual Total	38.63 93.81 69.51 81.00 80.39 51.88 65.74 111.10 49.18 52.67 84.54 72.53 59.02 93.92 64.18 64.18 58.10 47.75 69.61 83.03 74.48 63.64 64.18 64.18 64.18 64.18 64.18 64.18 64.18 64.18 64.18	
Dec.	8.34 11.63 14.34 14.14 7.50 7.50 7.50 12.60 14.01 8.07 8.07 8.07 18.56 9.53 7.60 8.40 8.41 18.56 11.60 11.60 11.56 11.56	
Nov.	6.14 7.37 7.37 13.61 5.84 3.74 3.74 3.74 17.02 19.09 14.45 19.09 14.45 11.36 11.38 11.31 5.36 11.38 11.38 11.38 11.38 11.38 11.38 11.38 11.38 11.38	
Oct.	2.95 6.24 3.89 12.54 8.28 1.13 1.13 1.92 1.92 6.98 3.40 6.98 3.40 6.98 3.40 6.32 7.69 7.69 7.15 11.07 11.07 11.07 11.07 11.07 11.20 6.32 7.69 6.32 7.69 7.69 7.15 7.15 7.15 7.15 7.15 7.15 7.15 7.15	
Sept.	0.84 4.71 1.73 0.05 0.05 0.06 0.08 0.08 0.08 0.08 0.08 0.04 0.08 0.05 0.05 0.05	
Aug.	0.25 3.15 0.35 3.18 1.02 0.59 0.35 4.71 0.35 4.71 0.35 0.35 1.35 0.35 1.35 1.35	
Jul.	0.47 0.73 1.79 0.18 0.18 0.08 0.04 0.04 0.28 6.93 0.04 0.28 0.04 0.28 0.31 1.45	
Jun.	0.34 0.06 0.06 0.05 0.12 0.03 0.96 0.96 0.96 0.25 0.25	
May	1.88 5.27 6.33 6.27 1.42 1.42 1.02 3.75 3.16 6.90 0.09 0.09 0.09 0.09 0.09 0.09 0.09 0.185 1.21 1.21 1.21 1.66	
Apr.	1.29 4.88 8.32 8.32 8.20 8.20 1.37 1.38	
Mar,	5.32 2.53 2.532 12.08 1.93 1.93 3.51 0.45 0.45 0.94 1.72 1.72 1.72 1.72 1.72 1.72 1.72 1.72	
Feb.	5.24 6.70 3.77 3.77 5.64 4.50 4.50 1.03 1.44 8.64 4.70 0.82 0.82 4.70 0.82 1.44 8.64 4.70 0.82 1.44 8.64 4.70 0.82 1.48 1.88	
Jan.	6.38 26.20 17.21 11.80 15.54 17.70 7.42 8.62 6.83 3.27 11.08 9.97 11.05 4.83 16.60 0.93 6.16 8.89 11.05 4.83 11.05 4.83 11.05 6.16 6.16 6.16 6.16 6.16 8.62 7.42 11.05 7.42 11.05 7.42 11.05 7.42 7.42 7.42 7.42 7.42 7.42 7.42 7.42	
Year	1950 51 52 53 54 55 56 60 60 61 65 64 65 67 67 71 72 73	

Monthly Rainfall at Polonnaruwa

, woldstamonopoonoclamonates														(Unit	(Unit: inch)	
65         0.55         2.43         0         3.24         0.71         4.63         6.76         7.03         39.31         32.38         6           87         5.31         0.54         0         2.18         1.63         5.82         2.45         15.12         10.44         70.44         54.96         11.8           88         5.25         3.82         0         2.08         0         4.15         7.05         7.31         8.94         63.71         48.41         11.8         6.64         17.20         76.39         52.72         22.33         5.74         11.8         6.64         17.20         7.26         22.93         5.25         0         2.24         17.86         4.04         5.80         52.93         5.75         1.26         7.24         17.66         9.64         17.70         17.70         18.93         13.72         17.41         17.8         18.93         13.72         17.41         17.4         17.4         15.4         10.4         5.24         17.4         18.94         43.74         18.4         11.7         18.91         19.93         19.93         19.94         11.7         18.91         19.94         19.94         19.94         19.94	•	•	ξ	•	•	May	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.		Maha Oct-Mar.	Yala Apr-Sept.
97         5.13         0.54         0	,	2	ی	,	F	~	_	-	^ ا	1	۷	6 76	7 03		37 38	6 93
88         5.25         3.82         0         2.08         0         4.15         7.05         7.31         8.94         63.71         48.41         115         7.52         22.76         75.39         52.52         23         3.52         2.52         23         4.13         6.05         6.48         4.04         5.86         5.48         4.04         5.80         50.39         31.74         10           3.2         4.13         0.02         4.37         0.48         2.17         0.17         8.82         12.28         11.84         40.4         5.80         50.39         31.74         10           3.5         4.13         0.02         4.37         0.48         2.17         0.17         8.82         12.28         11.84         40.4         5.80         42.74         11         10         6.86         6.86         6.86         6.86         6.86         6.88         10.82         12.74         11         10		, <u>∞</u>	. 6	ı <b>~</b>		ij	· 0		9		2.45	15.12	10.44		54.96	15.48
88         8.45         0         2.91         6.75         1.42         5.24         10.46         9.64         17.20         76.39         52.52         2           33         4,43         0         0         3.58         2.55         0         7.86         7.26         52.76         52.76         17.81         17.81         17.82         17.92         17.91         11.41         17.81         17.82         17.92         17.91         11.71         17.92         17.92	6 5.	7	ij	3	•		0	•		•	7.05	7.31	8.94	63.71	48.41	15.30
3.3         4,43         0         3.58         2.55         0         7.86         7.26         22.76         72.30         61.74         10           2.2         5.03         1.75         0         5.28         6.86         6.48         4.04         5.80         31.97         11           3.4         2.80         5.01         0.048         3.22         0.71         0.58         7.02         24.12         47.98         108.39         95.98         11         11         11         12.3         8.39         15.65         61.25         48.16         13         12         45.16         12.3         49.18         12         12         47.98         108.39         95.98         12         12         47.98         108.39         95.98         12         12         47.98         108.39         95.98         12         12         47.98         108.39         95.98         12         12         47.98         108.39         95.98         10	2 3.	22	2	æ	•		•	•	4.	•	10.46	9.64	17.20	76.39	52.52	23.87
2.2         5.03         1.75         0         5.28         6.86         6.48         4.04         5.80         50.89         31.97         118           3.5         4.13         0.02         4.37         0.48         2.17         0.17         8.82         12.28         11.84         54.08         42.74         118           2.80         5.01         0.09         3.22         0.17         8.82         12.28         11.84         54.08         49.74         118         15.6         12.81         11.84         54.08         49.75         118         15.6         12.33         10.16         57.48         19.81         10.42         57.88         10.82         49.75         118         10.88         10.42         57.88         10.42         57.88         49.75         27.88         49.75         27.88         49.75         27.88         49.75         27.88         49.75         27.88         49.75         27.10         10.99         49.75         49.88         49.75         27.10         10.99         49.75         49.88         49.75         27.10         10.99         49.75         49.75         49.88         49.75         49.88         49.75         49.75         49.88         4	9 3.	34	œ	3	•	0		•	ហ	0	7.86	7.26	22,76	72,30	61.74	10.56
.35         4.13         0.02         4.37         0.48         2.17         0.17         8.82         12.28         11.84         54.08         42.74         11.8           0.8         2.80         5.01         0.09         3.22         0.71         0.58         7.02         24.12         47.98         108.39         95.98         12.5           5.8         3.20         2.37         0.94         1.48         3.98         10.42         5.08         49.75         26.10           5.6         3.00         1.18         0.68         14.62         13.33         10.16         57.48         49.85         10.23         49.75         26.10         37.01         17.01         49.75         26.00         10.99         10.23         10.42         5.08         10.65         8.09         13.73         10.10         10.23         10.23         10.42         5.08         10.23         10.23         10.23         10.21         10.70         10.89         10.23         10.23         10.23         10.23         10.23         10.23         10.23         10.23         10.23         10.23         10.23         10.23         10.23         10.23         10.23         10.23         10.23	7 4.	9	નં	2	•	7	0	0	4	•	6.48	4.04	5.80	50.89	31.97	18.92
2.80         5.01         0.09         3.22         0.71         0.58         7.02         24.12         47.98         108.39         95.98         12           5.6         3.37         0.85         0         6.29         1.23         8.35         8.93         15.65         61.25         48.16         15           5.6         3.20         2.37         0         0.629         1.23         8.35         8.93         15.65         61.25         48.16         15           3.4         1.15         0.85         0         0.36         5.69         13.73         20.21         81.31         70.59         10           8.3         3.77         3.00         0         0.19         1.07         5.00         6.65         8.09         8.75         50.10         37.07         13           1.00         8.12         0.71         5.00         0.36         5.88         0.32         7.41         19.31         17.01         94.97         10           1.00         8.12         0.72         0         0.19         1.07         5.00         6.65         8.09         8.75         50.10         37.01         17           1.00         8.12 <td>94 2.</td> <td>1.1</td> <td>7</td> <td>5</td> <td>•</td> <td></td> <td></td> <td>٧.</td> <td>Τ;</td> <td>•</td> <td>8.82</td> <td>12.28</td> <td>11.84</td> <td>54.08</td> <td>42.74</td> <td>11.34</td>	94 2.	1.1	7	5	•			٧.	Τ;	•	8.82	12.28	11.84	54.08	42.74	11.34
3.20         2.37         0         6.29         1.23         8.35         8.93         15.65         61.25         48.16         1.15         0.85         0         1.18         0.68         14,62         13.33         10.16         57.48         49.75         7         7         2.6         3.89         10.16         57.48         49.75         7         2         2         3.98         10.24         5.08         10.75         5.00         6.65         8.09         8.75         50.10         37.07         13         10.59         10.70         5.00         6.65         8.09         8.75         50.10         37.07         13         10.50         6.65         8.09         8.75         50.10         37.07         13         10.50         6.65         8.09         8.75         50.10         37.07         13         10.50         6.65         8.09         8.75         50.10         37.07         13         10.00         10.00         10.10         10.00         10.00         10.00         10.00         10.00         10.00         10.00         10.00         10.00         10.00         10.00         10.00         10.00         10.00         10.00         10.00         10.00         10.00	4 12.	7	0	. 4	•	0	•	۲,		•	7.02	24.12	47.98	108.39	95.98	12.41
56         3.80         1.15         0.85         0         1.18         0.68         14,62         13.33         10.10         57.48         49.75         76.23         49.75         76.23         49.75         76.23         49.75         76.23         49.75         76.23         49.75         76.23         49.75         76.23         49.75         76.23         49.75         76.23         49.75         76.10         37.07         13         76.23         76.23         76.23         76.23         76.23         76.23         76.21         76.31         76.31         76.31         76.31         76.31         76.31         76.31         76.32         77.10         17         76.32         77.41         19.31         17.01         94.62         77.10         17         10         76.85         37.07         17         10         76.85         37.07         17         17         20.25         10.07         80.75         36.10         37.07         17         10         17         10.05         10         0.02         10         0.02         10         0.02         10         0.02         10         0.02         10         0.02         10         0.02         10         0.02         10	6 3.	6	•		•	t.		0	~	•	8.35	8,93	15.65	$\frac{61.25}{2}$	48.16	13.09 3.00
.34         12.07         6.47         0         5.52         0.94         1.48         3.98         10.42         5.08         76.23         49.75         249           .08         4.55         5.54         0.27         0         0.36         5.69         13.73         20.21         81.31         70.59         10           .08         4.55         5.54         0.27         0         0.19         1.07         5.08         6.65         13.73         20.21         81.31         70.59         10           .00         3.10         0         0         1.07         5.08         0.02         9.50         23.47         22.60         97.11         76.85         20         97.11         76.85         20         97.11         76.85         20         97.11         76.85         20         97.11         76.85         20         97.11         76.85         20         97.11         76.85         20         96         97.11         76.85         20         98         90.29         90.00         90.00         90.00         90.00         90.00         90.00         90.00         90.00         90.00         90.00         90.00         90.00         90.00         90.00 <td>5 0.</td> <td>õ</td> <td>•</td> <td></td> <td>•</td> <td>٠.</td> <td>•</td> <td></td> <td>7</td> <td>• •</td> <td>14.62</td> <td>13.33</td> <td>10.16</td> <td>57.48</td> <td>49.82</td> <td>90'/</td>	5 0.	õ	•		•	٠.	•		7	• •	14.62	13.33	10.16	57.48	49.82	90'/
.08         4.55         5.54         0.27         0         0.36         5.69         13.73         20.21         81.31         70.59         10           .83         3.77         3.00         0         0.19         1.07         5.00         6.65         8.09         8.75         50.10         37.07         13           .00         8.54         1.55         0.07         1.88         0.20         5.28         7.41         19.31         17.01         94.62         77.10         17           .06         3.12         1.51         0         4.08         1.83         2.87         3.47         22.60         97.11         76.85         22.96         30           .36         3.45         0.10         0.10         0.10         0.23         10.02         10.07         80.11         76.85         22.96         30           .38         0.46         0.10         0.01         0.02         10.23         18.37         19.90         62.51         58.01         49.99         19           .80         3.48         0.30         0.60         0.10         0.10         0.10         0.10         0.10         0.10         0.10         0.10 <t< td=""><td>2 16.</td><td>크</td><td>•</td><td>-</td><td>•</td><td>4.</td><td>0</td><td>'n</td><td>ō.</td><td>•</td><td>3.98</td><td>10.42</td><td>5.08</td><td>76.23</td><td>49.75</td><td>76.48</td></t<>	2 16.	크	•	-	•	4.	0	'n	ō.	•	3.98	10.42	5.08	76.23	49.75	76.48
.83         3.77         3.00         0         0.19         1.07         5.00         6.65         8.09         8.75         50.10         37.07         13           .00         8.54         1.55         0.07         1.88         0.20         5.28         7.41         19.31         17.01         94.62         77.10         17           .06         3.12         1.51         0         4.08         1.83         2.87         3.43         22.96         32.96           .06         3.12         1.51         0         5.98         0.02         9.50         23.47         22.60         97.11         76.85         22.96         30           .08         3.44         0.10         0.11         0.20         10.52         10.90         62.51         58.01         43.50         16.61         20.25         10.07         80.11         76.85         20.91         49.90         10         10         10.00         10.10         10.10         10.10         10.10         10.10         10.10         10.10         10.10         10.10         10.10         10.10         10.10         10.10         10.10         10.10         10.10         10.10         10.10         10.10	5 10.	33	•		•	ų			0	•	5.69	13.73	20.21	81.31	70.59	10.72
.00         8.54         1.55         0.07         1.88         0.20         5.28         7.41         19.31         17.01         94.62         77.10         17           .06         3.12         1.51         0         4.08         1.83         2.87         3.43         5.79         6.11         53.89         22.96         30           .90         7.16         6.25         0.85         0         5.98         0.02         9.50         23.47         22.60         97.11         76.85         22.96         30           .36         9.44         0.10         0.10         0.21         4.71         2.05         16.61         20.25         10.07         80.11         76.85         22.96         30           .80         3.45         0.43         0         0         0.03         0.59         10.23         18.37         19.90         62.51         58.01         4           .80         3.88         0.05         0         0.16         1.28         7.46         12.36         82.39         43.66         38.29         52.96         22.96         30.29           .11         10.67         0         0         0.16         1.78         1.76	17 2.	80	•		•	Ō.	0	•	1,07	•	6.65	8.09	8.75	50.10	37.07	13.03
.06         3.12         1.51         0         4.08         1.83         2.87         3.43         5.79         6.11         53.89         22.96         30           .90         7.16         6.25         0.85         0         5.98         0.02         9.50         23.47         22.60         97.11         76.85         22           .36         9.44         0.10         0.10         0.21         4.71         2.05         16.61         20.25         10.07         80.11         76.85         22           .08         3.45         0.00         0         0.01         0.23         18.37         19.90         62.51         58.01         4           .08         3.48         0.05         0         0.16         1.28         7.46         12.36         8.39         43.66         38.29         5           .11         10.67         0         0.16         1.28         7.46         12.36         82.36         60.50         19           .11         10.67         0         0         0.16         1.40         1.40         1.40         11         11         11         11         11         11         11         11         11	24 10.	٠,	•	8	-	5	•	•	0.20	•	7.41	19.31	17.01	94.62	77.10	17.52
.90         7.16         6.25         0.85         0         5.98         0.02         9.50         23.47         22.60         97.11         76.85         20.36         3.47         22.60         97.11         76.85         20.36         3.46         0.00         0.01         4.71         2.05         16.61         20.25         10.07         80.11         63.50         16.51         50.01         4.50         11         63.50         16.61         20.25         10.07         80.11         63.50         16.61         20.25         10.07         80.11         63.50         16.61         20.25         10.07         80.11         62.51         58.01         4.50         10.62         4.30         27.93         69.25         49.99         19         10.60         27.93         69.25         49.99         19         10         20.00         20.20         10.60         20.20         20.20         20.20         20.20         20.20         20.20         20.20         20.20         20.20         20.31         20.31         20.31         99.09         10         20.20         20.33         20.31         8.28         10.23         20.31         30.31         30.31         30.31         8.28         10.20	0 8.	9		90	•	Ŋ	0	•	1.83	•	3,43	5.79	6.11	53.89	22.96	30.93
36         9,44         0.10         0.10         0.21         4.71         2.05         16.61         20.25         10.07         80.11         63.50         16           08         3,45         0.43         0         0.03         0.59         10.23         18.37         19.90         62.51         58.01         4           80         3.88         0.05         0         0.16         1.28         7.46         12.36         8.39         43.66         38.29         5           11         10.67         0         0         0.16         1.28         7.46         12.36         8.39         43.66         38.29         5           11         10.67         0         0         0.16         1.28         7.46         12.36         8.39         43.66         38.29         5         19.90         60.50         26.59         19.90         60.50         26.99         19         60.50         27.93         69.25         49.99         19         19         19         19         19         19         19         19         19         19         19         11         19         19         19         19         19         19         19	15 16.	ξ.	•		•	2		0	5.98	•	9.50	23.47	22.60	97.11	76.85	20.26
.08         3.45         0.43         0         0.03         0.59         10.23         18.37         19.90         62.51         58.01         4.           .80         3.88         0.05         0         0.16         1.28         7.46         12.36         8.39         43.66         38.29         5.           .11         10.67         0         0.16         1.28         7.46         12.36         8.39         43.66         38.29         5.           .11         10.67         0         0.16         1.28         7.49         12.87         82.89         60.50         22.           .32         6.62         1.19         0         0.46         0.10         7.88         7.09         31.42         88.55         63.65         24.           .32         6.62         1.19         0         0.46         0.02         16.03         24.31         22.81         17.14         93.00         65.84         27.           .44         5.70         2.58         0         0.04         0.02         16.03         24.31         17.41         49.47         117.33         79.27         38.           .33         0         0         0.03	52 0.	9	•			ı.	•	•	4.71		16.61	20.25	10.07	80.11		16.61
.80         3.88         0.05         0         0.16         1.28         7.46         12.36         8.39         43.66         38.29         5.           .11         10.67         0         3.80         3.44         1.35         10.62         4.30         27.93         69.25         49.99         19.           .11         10.67         0         3.84         1.35         10.62         4.30         27.93         69.25         49.99         19.           .74         7.75         5.42         3.75         0         4.07         1.40         8.65         19.24         12.87         82.89         60.50         22.           .32         6.62         1.19         0         0.46         0.01         7.88         7.09         31.42         88.55         63.65         24.95         24.91           .75         1.45         3.50         2.60         13.70         1.76         15.05         7.24         15.41         49.47         117.33         79.27         38.           .30         5.70         2.60         1.76         15.05         1.00         7.54         15.41         49.47         117.33         77.67         65.66         12.34 <td>58 4.</td> <td>35</td> <td>•</td> <td></td> <td>•</td> <td>4.</td> <td>0</td> <td>0</td> <td>0.03</td> <td>•</td> <td>10.23</td> <td>18.37</td> <td>19.90</td> <td>62.51</td> <td></td> <td>4.50</td>	58 4.	35	•		•	4.	0	0	0.03	•	10.23	18.37	19.90	62.51		4.50
.11     10.67     0     3.80     3.44     1.35     10.62     4.30     27.93     69.25     49.99     19.24       .74     7.75     5.42     3.75     0     4.07     1.40     8.65     19.24     12.87     82.89     60.50     22.       .32     6.62     1.19     0     5.86     11.13     0.10     7.88     7.09     31.42     88.55     63.65     24.52       .75     1.45     5.21     0     0.46     0.02     16.03     24.31     22.81     17.14     93.00     65.84     27.       .75     1.45     3.50     2.60     13.70     1.76     15.05     7.24     15.41     49.47     117.33     79.27     38.       .30     5.70     2.60     13.70     1.76     15.05     1.00     7.54     9.32     35.60     21.34     14.       .03     7.54     4.97     23.88     27.00     77.67     65.66     12.       .15     2.32     0     1.76     0.68     3.10     4.15     4.97     23.88     27.00     77.67     65.66     12.       .71     7.51     4.78     0.60     2.90     2.50     3.37     8.28     13.52 <td>8 0</td> <td></td> <td>•</td> <td></td> <td>•</td> <td>0</td> <td>0</td> <td>0</td> <td>0.16</td> <td>•</td> <td>7.46</td> <td>12.36</td> <td>8.39</td> <td>43.66</td> <td></td> <td>5.37</td>	8 0		•		•	0	0	0	0.16	•	7.46	12.36	8.39	43.66		5.37
0.74       7.75       5.42       3.75       0       4.07       1.40       8.65       19.24       12.87       82.89       60.50       22.84         6.32       6.62       1.19       0       5.86       11.13       0.10       7.88       7.09       31.42       88.55       63.65       24.65         0       5.44       5.21       0       0.46       0.02       16.03       24.31       22.81       17.14       93.00       65.84       27.7         1.75       1.45       3.50       2.60       13.70       1.76       15.05       7.24       15.41       49.47       117.33       79.27       38.13         1.30       5.70       2.58       0       0.03       5.95       1.00       7.54       9.32       35.60       21.34       14.         8.03       7.54       4.44       0       20.00       3.81       0       8.27       11.24       15.04       91.05       55.26       35.         9.15       4.78       0.19       6.53       3.29       6.09       10.29       26.38       27.00       77.67       65.66       12.         5.71       7.51       4.77       0.60       2.90	37 1	96	ij.	_	-		0	•	3.44	•	10.62	4.30	27.93	69.25		19.26
.32       6.62       1.19       0       5.86       11.13       0.10       7.88       7.09       31.42       88.55       63.65       24.57         .75       1.44       5.21       0       0.46       0.02       16.03       24.31       22.81       17.14       93.00       65.84       27.27         .75       1.45       3.50       2.60       13.70       1.76       15.05       7.24       15.41       49.47       117.33       79.27       38.         .30       5.70       2.58       0       0.03       5.95       1.00       7.54       9.32       35.60       21.34       14.         .03       7.54       4.44       0       20.00       3.81       0       8.27       11.24       15.04       91.05       55.26       35.         .15       2.32       0       1.76       0.68       3.10       4.15       4.97       23.88       27.00       77.67       65.66       12.         .71       7.51       4.78       0.19       6.53       3.29       6.09       10.29       26.38       20.31       99.09       70.70       28.         .37       5.50       2.47       0.60 <t< td=""><td>08 11</td><td><math>\simeq</math></td><td>•</td><td></td><td></td><td></td><td>-</td><td></td><td>4.07</td><td>•</td><td>8.65</td><td>19.24</td><td>12.87</td><td>82.89</td><td></td><td>22.39</td></t<>	08 11	$\simeq$	•				-		4.07	•	8.65	19.24	12.87	82.89		22.39
7.44       5.21       0       0.46       0.02       16.03       24.31       22.81       17.14       93.00       65.84       27.2         30       5.70       2.58       0       0       0.03       5.95       1.00       7.54       94.7       117.33       79.27       38.         30       5.70       2.58       0       0       0.03       5.95       1.00       7.54       9.32       35.60       21.34       14.         03       7.54       4.44       0       20.00       3.81       0       8.27       11.24       15.04       91.05       55.26       35.         15       2.32       0       1.76       0.68       3.10       4.15       4.97       23.88       27.00       77.67       65.66       12.         71       7.51       4.78       0.19       6.53       3.29       6.09       10.29       26.38       20.31       99.09       70.70       28.         37       5.50       2.47       0.60       2.90       2.50       3.37       8.28       13.52       17.37       73.14       55.18       17.	7 76	2	•		•		0	98.	11.13	•	7.88	7.09	31.42	88.55		24.90
.75     1.45     3.50     2.60     13.70     1.76     15.05     7.24     15.41     49.47     117.33     79.27     38.       .30     5.70     2.58     0     0     0.03     5.95     1.00     7.54     9.32     35.60     21.34     14.       .03     7.54     4.44     0     20.00     3.81     0     8.27     11.24     15.04     91.05     55.26     35.26       .15     2.32     0     1.76     0.68     3.10     4.15     4.97     23.88     27.00     77.67     65.66     12.       .71     7.51     4.78     0.19     6.53     3.29     6.09     10.29     26.38     20.31     99.09     70.70     28.       .37     5.50     2.47     0.60     2.90     2.50     3.37     8.28     13.52     17.37     73.14     55.18     17.	ω				•	N	0	94.	0.02	•	24.31	22.81	17.14	93.00		27.16
.30       5.70       2.58       0       0.03       5.95       1.00       7.54       9.32       35.60       21.34       14.         .03       7.54       4.44       0       20.00       3.81       0       8.27       11.24       15.04       91.05       55.26       35.26         .15       2.32       0       1.76       0.68       3.10       4.15       4.97       23.88       27.00       77.67       65.66       12.         .71       7.51       4.78       0.19       6.53       3.29       6.09       10.29       26.38       20.31       99.09       70.70       28.         .37       5.50       2.47       0.60       2.90       2.50       3.37       8.28       13.52       17.37       73.14       55.18       17.	80 4.6	õ	•	ω.		ī.		.70	1.76	•	7.24	15.41	49.47	117.33		38,06
.03 7.54 4.44 0 20.00 3.81 0 8.27 11.24 15.04 91.05 55.26 35. .15 2.32 0 1.76 0.68 3.10 4.15 4.97 23.88 27.00 77.67 65.66 12. .71 7.51 4.78 0.19 6.53 3.29 6.09 10.29 26.38 20.31 99.09 70.70 28. .37 5.50 2.47 0.60 2.90 2.50 3.37 8.28 13.52 17.37 73.14 55.18 17.	2.1	00	•	0		7	0		0.03	•	1.00	7.54	9.32	35.60		14,26
.15 2.32 0 1.76 0.68 3.10 4.15 4.97 23.88 27.00 77.67 65.66 12. .71 7.51 4.78 0.19 6.53 3.29 6.09 10.29 26.38 20.31 99.09 70.70 28. .37 5.50 2.47 0.60 2.90 2.50 3.37 8.28 13.52 17.37 73.14 55.18 17.	83 6.8	Ñ	•	03	•	4	0	8	3.81		8.27	11.24	15.04	91.05		35.79
.71 7.51 4.78 0.19 6.53 3.29 6.09 10.29 26.38 20.31 99.09 70.70 28. .37 5.50 2.47 0.60 2.90 2.50 3.37 8.28 13.52 17.37 73.14 55.18 17.	9.0	.0	•	1.5	•		7.	•	3.10	1.	4.97	23.88		77.67		12.01
.37 5.50 2.47 0.60 2.90 2.50 3.37 8.28 13.52 17.37 73.14 55.18 17	06 1.9	35	•	_	•	•	1	•	3.29	•	10.29	9		60.66		28.39
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	•	9	ë.	7	•	•	•	•	•		•	3.5	•	3	5.	17.96

(Unit: inch)

Annual Maha Yala ıv. Dec. Total Oct-Mar. Apr-Sept.	76       6.56       45.03       33.34       11.69         .45       7.19       74.98       57.79       17.19         .48       7.13       52.73       38.02       14.71         .60       18.31       75.19       50.15       25.04         .48       16.39       61.02       49.03       11.99         .23       6.97       50.48       33.36       17.12         .27       10.49       47.09       40.07       7.02         .90       52.81       111.32       98.59       12.73         .91       8.29       53.57       39.77       13.64         .12       4.10       90.93       60.45       30.48         .12       4.10       90.93       60.45       30.48         .12       4.10       90.93       60.45       14.86         .11       19.72       56.78       43.14       13.64         .10       51.53       36.67       14.86         .11       19.72       51.53       36.45       15.17         .66       8.27       51.53       64.90       22.49         .10       8.36       47.65       36.45       13.99
Oct. Nov	664 7 46 19 28 6 66 6 66 6 66 6 66 6 67 7 77 23 77 23 77 23 77 23 77 23 78 11 89 12 99 12 96 11 96 11 96 11 96 11 97 14 97 15 97 16 97 16 98 11 98 11 98 11 99 11 90 11 9
Sept. Oc	1.85 3.72 3.72 5.48 6.04 6.03 6.03 1.92 7.192 7.193 6.18 6.18 6.18 6.18 6.18 6.18 6.18 6.18
Aug.	3.86 1.25 1.25 1.34 1.45 1.45 1.16 0.05 0.62 0.63 0.63 0.63 0.63 0.63 0.63 0.63 0.63
Jul.	0.22 0.32 1.21 1.21 9.19 3.46 0.03 0.03 0.13 0.27 0.27 0.27 0.27 0.27 0.27 0.27 0.27
Jun.	0.23 0.02 0.02 0.06 0.03 0.16 0.10 0.02 0.02 0.02 0.02 0.03 0.04 0.04 0.05 0.05 0.05 0.05 0.05 0.05
May	5.02 5.99 3.62 0.07 0.05 1.93 0.05 4.48 8.94 4.49 8.94 4.49 8.94 4.49 8.96 0.64 4.49 8.96 1.73 0.64 1.73 0.06 1.73 0.06 1.73 0.06 0.06 0.06 0.06 1.73 0.06 0.06 0.06 0.06 0.06 0.06 0.06 0.0
Apr.	0.74 5.68 4.38 10.19 7.14 7.14 7.14 7.14 9.13 1.33 1.33 1.33 8.13 8.13 8.50 7.69 4.76 4.76 4.76 1.33 8.50 7.39 8.60 7.69 7.69 7.69 7.69 7.69 7.69 7.69 7.69
Mar.	6.48 1.48 1.05 0.61 6.79 0.72 0.72 6.14 4.91 7.24 4.91 7.24 4.91 7.24 7.24 7.24 6.07 6.07 6.07 6.07 6.07 6.07 6.03 6.03 6.03 8.03 6.03 8.03 8.03 8.03 8.03 8.03 8.03 8.03 8
Feb.	3.70 4.17 2.19 1.35 4.90 1.35 4.47 6.44 16.63 8.54 8.54 7.10 0.98 3.64 0.07 2.28 2.25 2.25 0.85
Jan,	5.20 15.89 10.74 10.52 10.74 10.52 6.40 6.40 6.40 7.75 17.93
Year	1950 1950 151 152 160 161 172 173 173 173 174 175 175 176 177 177 178 178 178 178 178 178 178 178

(Unit: inch)

Jan. Feb. Man 2.78 3.18 1.4 18.78 4.20 2.2 16.61 1.30 0.0 9.98 2.46 3.6 12.69 2.10 4.1 13.75 5.41 1.1 5.88 1.97 0.1 4,70 5.24 0.0 3.96 2.75 5.1 6.50 0.65 0.2 9.13 11.24 1.0 16.19 4.73 3.6 10.04 2.19 1.1 14.43 6.42 3.7 4.44 1.27 5.9 2.81 9.69 0.9 9.81 1.86 3.1 1.18 4.40 1.6 6.80 6.77 2.1 6.81 0.53 1.4 4.80 4.94 0 6.80 6.77 2.1 6.81 0.53 1.4 6.81 0.53 1.4 1.21 1.49 0.7 2.26 1.10 1.9 0.75 5.26 2.6										,		
1950 2.78 3.18 1.4 51 18.78 4.20 2.2 52 16.61 1.30 0.0 53 9.98 2.46 3.6 54 12.75 5.41 1.1 55 13.75 5.41 1.1 56 5.88 1.97 0.1 58 3.96 2.75 5.1 59 6.50 0.65 0.2 60 9.13 11.24 1.0 61 16.19 4.73 3.6 62 10.04 2.19 1.1 63 14.43 6.42 3.7 64 444 1.27 5.9 65 6.80 6.77 2.1 71 6.81 0.53 1.4 72 1.21 1.49 0.7 73 0.75 1.33 0.2 74 0.85 0.12 0.0 75 2.26 1.10 1.9 76 0.85 0.12 0.0	Apr.	May	Jun.	Jul.	Aug.	Sept.	Oct.	Nov.	Dec.	Annual Total	Maha Oct-Mar.	Yala Apr-Sept
51 18.78 4.20 2.2 52 16.61 1.30 0.0 53 9.98 2.46 3.6 54 12.69 2.10 4.1 55 13.75 5.41 1.1 56 5.88 1.97 0.1 58 3.96 2.75 5.1 60 9.13 11.24 1.0 61 16.19 4.73 3.6 62 10.04 2.19 1.1 63 14.43 6.42 3.7 64 4.44 1.27 5.9 65 6.80 6.77 2.1 71 6.81 0.53 1.4 72 1.21 1.49 0.7 73 0.75 1.33 0.2 74 0 1.77 5.26 2.6	9.	ω.	0	0	7	2,57	, 7	0	10.71	47.80	33. 79	~
52 16.61 1.30 0.0 53 9.98 2.46 3.6 54 12.69 2.10 4.11 55 13.75 5.41 1.11 56 5.88 1.97 0.1 58 3.96 2.75 5.1 59 6.50 0.65 0.2 60 9.13 11.24 1.0 61 16.19 4.73 3.6 62 10.04 2.19 1.1 63 14.43 6.42 3.7 64 4.44 1.27 5.9 65 2.81 9.69 0.9 66 9.81 1.86 3.1 67 6.80 6.77 2.1 71 6.81 0.53 1.4 72 1.21 1.49 0.7 73 0.75 1.33 0.2 74 0 1.77 5.26 2.6 76 0.85 0.12 0.0	9	9	0	•	1.13	5.68	4			α		
53 9.98 2.46 3.6 54 12.69 2.10 4.11 56 5.88 1.97 0.11 57 4,70 5.24 0.0 58 3.96 2.75 5.11 60 9.13 11.24 1.0 61 16.19 4.73 3.6 62 10.04 2.19 1.1 63 14.43 6.42 3.7 64 4.44 1.27 5.9 65 9.81 1.86 3.1 66 9.81 1.86 3.1 67 1.18 4.40 1.6 68 6.77 2.1 70 6.80 6.77 2.1 71 6.81 0.53 1.4 72 1.21 1.49 0.7 73 0.75 1.33 0.2 74 0 1.91 0.00 75 2.26 1.10 1.99 76 0.85 0.12 0.0	~	2.77	0	•		2.66	. –	Ö				T . (
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7.81 9.69 0.9 9.81 1.86 3.1 1.18 4.40 1.6 5.84 0.11 5.4 4.80 4.94 0 6.80 6.77 2.1 6.81 0.53 1.4 1.21 1.49 0.7 0.75 1.33 0.2 0 2.26 1.10 1.9 0.85 0.12 0.0	Q.	7	0	ᅼ	0.99	3.86			9.7	~;		9.9
2.81 9.69 0.9 9.81 1.86 3.1 1.18 4.40 1.6 5.84 0.11 5.4 4.80 4.94 0 6.80 6.77 2.1 6.81 0.53 1.4 1.21 1.49 0.7 0.75 1.33 0.2 0 1.91 0.0 2.26 1.10 1.9 0.85 0.12 0.0	ထ	7		۲.	∞.	0.35			٥.		~	2.6
9.81 1.86 3.1 1.18 4.40 1.6 5.84 0.11 5.4 4.80 4.94 0 6.80 6.77 2.1 6.81 0.53 1.4 1.21 1.49 0.7 0.75 1.33 0.2 0 1.91 0.0 2.26 1.10 1.9 0.85 0.12 0.0	ij	۲.	0.24	0	œ	1.94		Ŋ	S	~	~	5.9
1.18 4.40 1.6 5.84 0.11 5.4 4.80 4.94 0 6.80 6.77 2.1 6.81 0.53 1.4 1.21 1.49 0.7 0.75 1.33 0.2 0 1.91 0.0 2.26 1.10 1.9 0.85 0.12 0.0	ı.		0	0.28	ო.	4.42			9,2	٠.		8.6
5.84 0.11 5.4 4.80 4.94 0 6.80 6.77 2.1 6.81 0.53 1.4 1.21 1.49 0.7 0.75 1.33 0.2 0 1.91 0.0 2.26 1.10 1.9 0.85 0.12 0.0	7	0		0	ó	2.20		e.	8.4	~	3.4	1.1
6.80 6.77 2.1 6.81 0.53 1.4 1.21 1.49 0.7 0.75 1.33 0.2 0 1.91 0.0 2.26 1.10 1.9 0.85 0.12 0.0	ຕຸ	0	0.10		e.	5.29		ıΩ.	6.1	<u>.</u>	4.	4.0
6.80 6.77 2.1 6.81 0.53 1.4 1.21 1.49 0.7 0.75 1.33 0.2 0 1.91 0.0 2.26 1.10 1.9 0.85 0.12 0.0	∞.	∞		o.	o.	1.57			0	~	2	8.3
6.81 0.53 1.4 1.21 1.49 0.7 0.75 1.33 0.2 0 1.91 0.0 2.26 1.10 1.9 0.85 0.12 0.0 1.77 5.26 2.6	ຕຸ	α	4	۰.	ō	3.74			-			5.9
1.21 1.49 0.7 0.75 1.33 0.2 0 1.91 0.0 2.26 1.10 1.9 0.85 0.12 0.0 1.77 5.26 2.6	Q.	1.85	0.03	2.54	u.	4.81			5.0	<u>~</u> :	.7	'n
0.75 1.33 0.2 0 1.91 0.0 2.26 1.10 1.9 0.85 0.12 0.0 1.77 5.26 2.6	7	4	ō.	9		8.49			0	~:		0.9
0 1.91 0.0 2.26 1.10 1.9 0.85 0.12 0.0 1.77 5.26 2.6	7	-	Ŋ	o.	ú	5.44			0.3		7	9.0
2,26 1.10 1.9 0.85 0.12 0.0 1.77 5.26 2.6	ø	ō	0	∞.	4	4.11			4.1		'n	7.6
1.77 5.26 2.6	Ō.	'n		۲.	õ	1.85			4	_:	6.	3.8
1.77 5.26 2.6	Ŋ		1,50	Τ.	3.03	3.53		ö	5.6	46.23	ι,	~
	∞	1.84		<b>으</b>	ξÜ.	8.60			H		년.	4.9
Mean 6.96 3.38 1.95	4.27	2.21	0.76	2.24	3.59	3.68	7.57	11.62	14.64	62.85	46.22	16.73

#### 2.2.2 Effective Rainfall

The effective rainfall, which is useful for reduction of Irrigation water requirement when the rainfall reached on the soil surface and supplied the soil moisture, vary with natural features, especially rainfall intesity, rainfall, permeability of soils, kind of crops, growing period of crops, condition of farm management. Generally little rainfall is not effective. On the crops, the effective rainfall for paddy different from for upland crops naturally.

In the calculation of the water requirements under the project, effective rainfall is separately computed for lowland paddy and upland crops as follows:

# (1) For as lowland paddy

The following formula is applied to paddy.

 $ER = (R - 1) \times 0.67$ 

ER = 9 inches (228.6 mm) when  $ER \ge 9$  inches.

ER = 0 when  $R \le 1$  inche (25.4 mm)

where ER: effective rainfall, and R: monthly rainfall

## (2) For as upland crops

The effective rainfall for upland crops vary with rainfall, soils, crops and etc.. In this project, it is assumed that effective rainfall for upland crops is computed in terms of the S.C.S. Method adopted by U.S.D.A. (United States, Department of Agriculture's Soil Conservation Service Method).

The effective rainfall is computed by following formula.

 $ER = R \times Ratio (%)$ 

where, ER = effective rainfall

R = monthly rainfall

The ratios of the effective rainfall have been obtained as following Table 6.2.11 by Irrigation and Drainage Pater No. 25, Effective Rainfall, prepared by F.A.O.

(Unit: %)

Table 6.2.11 Ratio of the Effective Rainfall to the Monthly Rainfall

<del></del>					·								
Crops	Month	Jan.	Feb.	Mar.	Apr.	May.	Jun.	Jul.	Aug.	Sep.	Oct.	Nov.	Dec.
Upland	New Land	_	<u> </u>	-	65	75	80	70	75	65	_	_	
Up1	System G	-	50	65	65	75	80	70	-		·	-	_
Sugar (	Cane	60	65	70	65	65	80	70	75	80	65	40	30

# 2.2.3 Method of Calculating Water Requirements

### (1) Definition

The following terminological definitions, which are the same as have been used in the development plans worked out in Asian Development Bank and other international agencies, are used for water requirement.

Evapotranspiration = Evaporation + Transpiration

Water Requirement = Evaporation + Percolation

Irrigation Requirement = Water Requirement + Farm Waste - Effective Rainfall

Farm Turnouts Requirement = Irrigation Requirement + Farm Ditch Loss

Diversion Requirement = Farm Turnouts Requirement + Conveyance Loss

in the Main Canal and Lateral up to Farm

Turnout

## (2) Evapotranspiration

...

Evapotranspiration is calculated by the following formula;

ET = ETo x Crop Factor

where ET: Evapotranspiration

ETo: Reference Evapotranspiration

Monthly Reference Evapotranspiration (ETo), as shown in Table 6.2.12, have been calculated by adopting the Modified Penman Method in reference to the meteorological data obtained at Maha-Illuppallama.

Table 6.2.12 Monthly ETo

									(บ	nit:	inch)	)	
Month	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
ЕТо	4.7	5.0	6.2	5.9	6.4	6.9	7.5	7.6	7.5	6.2	4.3	4.5	72.7

Crop factors are shown in Table 6.2.13.

Table 6.2.13 Crop Factor

Crop and Crop Factor	Initial Stage	Crop Development Stage	Mid Stage	Late Stage
Lowland Rice (135 days) Crop factor	30 days 1.00	40 days 1.15	45 days 1.20	20 days 0.90
Lowland Rice (100 days) Crop factor	20 days 1.00	30 days 1.15	30 days 1.20	20 days 0.90
Lowland Rice (90 days) Crop factor	20 days 1.00	25 days 1.15	30 days 1.20	15 days 0.90
Upland Rice (100 days) (Crop factor	20 days 0.90	30 days 1.00	30 days 1.05	20 days 0.90
Upland Rice (90 days) Crop factor	20 days 0.90	25 days 1.00	30 days 1.05	15 days 0.90
Green Gram (75 days) Crop factor	15 days 0.50	20 days 0.80	25 days 1.05	15 days 0.70
Chillies (150 days) Crop factor	25 days 0.65	25 days 0.85	75 days 1.00	25 days 0.90
Ground Nuts (110 days) Crop factor	20 days 0.65	30 days 0.80	40 days 1.00	20 days 0.80
Soya Bean (105 days) Crop factor	15 days 0.65	20 days 0.85	50 days 1.05	20 days 0.75
Cowpea (90 days) Crop factor	15 days 0.70	25 days 0.90	35 days 1.10	15 days 1.00
Pulses (95 days) Crop factor	15 days 0.50	30 days 0.80	35 days 1.05	15 days 0.50
Cotton (165 days) Crop factor	25 days 0.65	45 days 0.90	55 days 1.05	40 days 0.90

# 2.2.4 Irrigation Efficiency and Losses

- (a) Water requirements for pudding and Land preparation
  Water requirements for pudding have been determined at 7 inches
  (177.8 mm) per crop of paddy, while those for land preparation of
  upland crops at 1.5 inches (38.1 mm).
- (b) Percolation Percolation is assumed to be 6 inches (152.4 mm) per month under the project.
- (c) Irrigation efficiency
  Irrigation efficiency, which is used in estimating irrigation
  requirement for upland crops, is assumed to be 50%.
- (d) Conveyance and diversion losses
  The losses due to conveyance and diversion are combinedly estimated at 30% of the diversion requirement.
- (e) Conveyance loss at Yoda Ela

  The conveyance loss from Elahera and Amgamedilla headworks to each
  of the tanks is estimated at 0.3% per mile.

# 2.2.5 Proposed Cropping Patterns

The proposed cropping patterns under the project are shown in Table 6.2.14 (see Chapter 5, Agricultural Development Plan, Volume-I, Main Report.)

Table 6.2.14 Proposed Cropping Pattern

Remarks		35%	30%	35%
Dec.		_	-	<u>с.</u>
Nov.				
Oct.			1	
Sep.			(egetable(1) 60 days	
Aug.	ys.		Vegeta 60	Vegetable(2)
Jul.	Paddy 105 days	50 days	undnut	Vegeta 60
Jun.	Paddy	Chillies 150 days	Soyabean 105 days or Copsicum or Groundnu	a) Onion)
May		CP	Soyabean 105 days Vor Copsicum or G	Pulses(Cowpea) 75 days (or Onion
Apr.			Soyab (or (	Pulses
Mar.	lys and a second	lys.	ays	8,8
Feb.	Paddy 135 days	Paddy 135 days	Paddy 105 days	Paddv 135 days
Jan.	Paddy	Paddy	Paddy	1 1
Maha-Yala Grop	Puddv~Paddy	Paddy- Chillies	Soya- be an Veg. (1)	Puddy-Pulses
Pattern	lA		-1- -1-	

# 2.2.6 Irrigation Requirements and Diversion Requirements

The crop water requirements have been calculated on the proposed cropping pattern. In the case of excluding the effective rainfall, the irrigation requirements and diversion requirements have been computed as shown in Table 6.2.15 to 6.2.17.

(The amount of the total requirements are based on the relation with the total acreage of each cropping patterns.)

Table 6-2-15

Irrigation Requirements & Diversion Requirements (Newland, System D & A/D)

(excluding Effective Rainfall)

Oct. Nov.	96.6 08.9	 	96.6 08.9	9.72 14.24	810 1,187	4.76 6.97	0.26 1.97				1.09		6.11 8.94	8.74 12.78	728 1,065
Sep.	0.88	1.58	2.46	3.52	293	0.62		1.21			4.83	1.13	7.79	11.14	928
Aug.		12.01	12.01	17.17	1,431			5.00			3.61	4.19	12.80	18.30	1,525
Jul.		14.85	14.85	21.24	1,770			5.25		2.70	;	3.06	11.01	15.74	1,312
Jun.		13.73	13.73	19.63	1,636			4.83	3.77	4.39			12.99	18.58	1,548
Мау		9.76	9.76	13.96	1,163			3.77	4.57	3.73			12.07	17.26	1,438
Apr.		3.50	3.50	5.01	418			3,07	3.44	2.81	•		9.32	13.33	1,111
Mar.	5.91		5.91	8.45	704	4.14	1.89		•		ļ		6.03	8.62	718
Feb.	11.65		11.65	16,66	1,388	8.16	3.50						11.66	16.67	1,389
Jan.	11.55		11.55	16.52	1,377	8.09	3.45		•				11.54	16.50	1,375
Скорв	Lowland Rice: Maha	- do - : Yala	Sub-Total	Div.R. (inches)16.52	1,000Ac Div,R(acft)	Lowland Rice: Maha	n Maha	Chillies	Pulses	Soyabean	Vegetable(1)	- do - (2)	Sub-Total	Div.R. (inches)16.50	1,000Ac Div.R(acft)
Water Req.		1881 uire ent	Кed		oviO nola Tiup			9091	Iupai	ı uo	t de 8	Irri	- 3	-9X	Dive ston quir
Cropping Pattern				9116						я -	פגט	Patt			

Table 6-2-16

Irrigation Requirements & Diversion Requirements (System G)

(excluding Effective Rainfall)

													C1
Total	58.95	52.12	26.98	138.05	196.93	16,411	58.95	23.40	11.78	12.89	107.02	153.03	1,353 12,752
Dec.	11.36			11.36	16.24	1,353	11.36	l .			11.36	16.24	
Nov.	10.90	1		10.90	15.59	1,299	10.90	:			10.90	15.59	1,299
Oct.	12.09			12.09	17.29	1,441	12.09				12.09	17.29	1,020 1,441 1,299
Sep.	8.56		4.33	12.89	18.43	1,536	8,56	į			8,56	12.24	1,020
Aug.	2.34		12.00	14.34	20.51	1,709	2.34				2.34	3.35	279
Jul.		1.10	8.76	9.86	14.10	1,175		3.73			3.73	5.33	444
Jun.		8.69	1.56	10,25	14.66	1,222		4.78	3,77	2,48	11.03	15.77	1,314
Мау		13.36		13.36	19,10	1,592		4.48	4.57	4.07	13.12	18.76	1,311 1,563 1,314
Apr.		12.73		12.73	18,20	1,517		4.13	3,44	3.43	11.00	15.73	1,311
Mar.		10.68		10.68	15.27	1,272		3.65		2.91	6.56	9.38	782
Feb.	3.55	4.98		8.53	12.20	1,017	3.55	2.63			6.18	8.84	737
Jan.	10.15	0.58		10.73	15.34	1,278	10.15				10.15	14.51	1,209
Crops	Lowland Rice: Maha	- do - : Yala	Green Manure Crop	Sub-Total (inches)	Div.R. (inches)15.34	1,000Ac D.R(acft)	Lowland Rice: Maha	Chillies	Pulses	Oil Crops	Sub-Total (inches)	Div.R. (inches)14.51	1,000Ac Div.R(acft)
Water Req.		atto reme			-9X	Dive ainp			oijs reme			-∋И	Dive aton atup
Cropping Water Pattern Req.			A -	ern	1169				я -	ern	Patt		

Table 6-2-17

Irrigation Requirements & Diversion Requirements (Sugar cane)

15,696 131.72 188.35 Total 1,120 1,108 1,270 1,139 1,206 1,299 1,485 1,630 1,752 1,507 1,065 1,115 9:36 13.38 Dec. 18.08 12.78 8.94 Nov. 12.64 Oct. Sept. 9,56 10,12 10,90 12,46 13.68 14.70 21.02 19.56 Aug. 17.82 Jul. 15.59 Jun. 13.67 14.47 May Apr. 15.24 10.66 Mar. 9.30 13.30 Feb. D.R. (inches)13.44 9.40 Jan. 1,000 AC D.R.(ac.ft) Irrigation Requirement (Inches) Item Requirement Diversion

# 2.2.7 Tank-wise Diversion Requirements

The project area is divided into 6 systems in terms of the existing tanks; however, as in Kantalai region further divided into paddy upland and the sugarcane farm managed by the Sugar Coporation, diversion requirements calculation would be made according to the divided 7. The rainfall data used in calculation of tank-wise diversion requirements are as follows:

No.	Tank or System	Rainfall Station
1 2	Parakrama Samudra Minneriya Tank	Polonnaruwa
3 4	Giritale Tank Kaudulla Tank	Hingurakgoda
5 6	Kantalai Tank(Paddy and Upland) Kantalai Tank(Sugarcane)	Kantalai
7	System G	Elahera (Bakamuna)

# 2.2.7.1 Tank-wise Diversion Requirements (Case 1)

In this case (case 1), diversion requirements are computed on the following conditions;

- (a) Existing area; Cropping Pattern A, 97.5%
  - Cropping Pattern B, 2.5%
- (b) New Land : Cropping Pattern A. 80 %
  - Cropping Pattern B, 20 %
- (c) For Elahera region (System G), the cropping patterns used in the report on the Integrated Small Farmer Development Project have been adopted.
- (d) For Kantalai tank, diversion requirements have been determined by summing up the diversion requirements culculated for Kantalai farm managed by the Sugar Corporation (Table 6.2.24) and for paddy and upland (Table 6.2.23).

Table 6-2-18 Irrigation Area in Case 1

	Exis	Existing Area			New Land	
	В – q	P - B	Total	P - A	P - B	Total
Parakrama Samudra	24,375	625	25,000	4,000	1,400	5,400
Minneriya Tank	22,400	009	23,000	1	ı	ł
Giritale "	7,300	200	7,500	1	!	ı
Kandulla "	13,260	340	13,600	21,000	1,400	22,400
Kantalai "	17.160	440	17,600	2,600	4,000	009*9
Kantalai (Sugar Coop)			17,900	1	ŀ	ı
Elahera (System G)	12,400	2,400	14,800	ī	ι	ı

Table 6-2-19

Remarks																													
Кеш																													
Annual Total	337,179	280,351	287,538	262,061	268,984	314,091	301,481	273,654	287,441	302,760	266,961	252,625	312,839	240,430	305,164	318,670	271,963	301,871	322,272	308,548	247,190	<b>√</b> T	287,617	$\Box$	$\overline{}$	229,562	6,7	42,7	253,909
Dec.	25,484	17,207	20,848	7,516	7,516	28,469	13,809	7,516	7,516	17,887	30,217	7,516	21,309	7,516	27,716	7,516	18,105	7,516	22,183	7,516	11,309	7,516	7,516	7,516	19,926	7,516	7,516	7,516	13,829
Nov.	21,855	3,246	20,520	14,865	20,641	28,457	8,457	3,246	16,588	5,908	12,972	4,938	18,627	3,246	24,209	3,246	3,246												11,494
Oct.	15,394	20,685	9,520	1,562	7,554	10,904	5,277	9,593	6,365	0	16,972	12,821	10,491	8,646	18,307	3,736	0	2,083	8,525	1,199	5,662	7,506	0	9,059	24,204	6,559	14,569	1,947	8,541
Sep.	9,975	0	1,610	98	10,198	0	10,145	10,016	9,254	9,985	8,569	10,085	162	74	4,912	10,192	7,027	10,013	9,117	8,925	8,788	10,167	0	0	0	10,198	1,610	0	5,754
Aug.	37,451	41,682	43,699	42,233	39,264	32,091	40,263	43,442	29,438	42,864	43,359	43,699	43,153	43,627	41,156	30,252	33,589	43,688	43,641	36,926	35,270	17,661	43,692	41,340	43,688	35,954	37,819	37,320	38.867
Jul.	52,870	49,460	49,721	37,563	45,816	52,870	52,708	46,753	52,870	52,870	40,765	52,870	52,806	50,241	44,514	52,870	52,799	52,870	52,870	45,243	52,870	39,880	52,715	21,441	52,870	19,780	52,640	38,136	47,203
Jun.	σ,	ີດົ	6	6	o,	ર્જ	်	o,	49,561	ο,	ີດ	e,	່ຕົ	6	°,	ີດົ	ď	6	6	ę,	Ť.	9	5,6	4,	9,5	49,561	7,1	9,4	48.560
May	, 79	,71	, 14	,91	,91	85,	96,	10,	31,953	Į.	,18	,62	, 29	2,	,21	,75	,87	, 75	8	,91	.6	,05	49	.98	6,	<u>.</u> 5	,91	,62	31,059
Apr.	, 91	,65	0		,18	,37	, 69	,12	8,096	,54	0	,61	62		8,302		0	,45	34	0	0	172	,31	12,609	,64		10,366		4.209
Mar.	7.	6,6	4,	6,8	3,6	0,0	8,1	1,4	13,963	1,4	5,7	3	6,9	4,1		4	4,	8,8	~	1,1	1,4	₹,	1,4	٠	0,7	4,3	1,4	O,	15,384
Feb.	ດົ	4	ζ,	့်	'n	<b>\</b>	ထ်	4	35,920	ζ,	•	Ġ	တ်	•	m		7	2,	2	ó	'n	4,	2	'n	ີດ		ζ,	o,	13.980
Jan.	4,	~.	~	2,8	5,8	, 6 3	2,2	3,4	25,917	8,6	8,0	۲,	4	, s	8,7	. – Ţ	1,1	8,0	1,4	3,0	7,0	7,4	4,0	٦,	٦,	0,1	2,2	ິດ	25.965
Year	1950	51	52	53	24	55	56	57	58	59	09		65 I		99	65	99	29	68	69	70	7.7	72	73	74	75	9/	11	Mean

Diversion Requirements for Minneriya Tank

,																													
Remarks																													
Annual Total	245.922	214,618	235,464	205,904	219,828	238,110	239,878	212,264	231,064	223,400	180,858	190,580	235,228	187,146	245,874	194,616	216,166	224,250	239,318	216,272	219,282	2,	220,398	ı,	9	ď,	•	,13	223,414
Dec.	20.222	19,072	19,072	5,732	5,732	19,308	12,868	5,732	17,002	12,862	24,598	5,732	17,002	5,732	22,522	5,732	16,772	5,732	16,772	5,732	8,262	5,732	9,872	5,732	5,732	5,732	5,732	5,732	11,302
Nov.	14.878	2,464	17,178	15,108	17,178	17,638	8,438	2,464	13,498	3,838	2,464	6,828	13,262	2,464	20,398	2,464	2,464	2,464	12,572	8,668	8,438	19,478	2,464	22,238	20,628	11,658	5,908	2,464	10,000
Oct.	13.674	13,904	10,684	0	7,004	15,514	3,136	6,538	11,374	0	7,228	2,016	10,224	11,604	7,464	0	0	0	6,774	0	وق	13,904	0	oʻ	18,504	ર્જ	່ຕົ	0	7,734
Sep.		1,960		3,618	7,054	1,258	7,048	5,264	5,258	5,258	0	6,704	36	0	4,562	•	0	3,376	18	0	4	6,954	0	1,960	2,668	42	6,716	0	3,128
Aug.	27,378	32,364	32,950	29,514	32,134	27,856	32,606	32,112	23,100	32,890	32,600	32,944	28,328	32,860	32,878	25,714	30,700	32,902	28,328	30,228	26,186	30,234	32,944	32,896	32,932	29,520	31,178	31,886	30,649
Jul.	40,416		39,866	25,088	35,606	40,434	40,434	37,028	40,392	40,422	30,166	40,410	40,434	35,842	37,650	40,398	40,422	40,428	40,434	34,426	40,434	39,618	•	•	40,434	•	39,618	•	37,567
Jun.	7	_	΄,	7	~	~	÷	7	~	'n	7,	~	~	7	7	۲,	<u>,</u>	7	۲,	~	o,	7	~	erî	37,666	~	ζ,	ζ,	37,251
May	6	`~	`- <b>`</b>	Ġ	œ.	ິທີ	ô	ó	ຕົ	ó	Ĥ	4	4	ó	ó	ď	o,	ις.	٠Ĉ	ó	ς,	σ,	œ.	√*	16,290	ω	ີຜົ	o,	22,396
Apr.	10.008	1,034	3,618	0	0	0	,20	,86	15	,38	0	45	4,096	,91	, 27	0	,50	68	,15	α	0	0	,45	8,810	4,096	m	78	966'6	3,532
Mar.	6.216	15,416	16,106	16,112	5,532	14,266	16,112	16,112	9,896	16,112	13,806	6,682	11,506	4,836	8,982	16,112	906,9	11,512	8,056	16,112	14,042	14,726	16,112	14,272	16,112	13,346	16,112	14,036	12,684
Feb.	6	26,220	્ષ્	ູ	۷,	ຸ∝ຼ	ന്	7,	25,530	Ů,	6.1	_	ູ້	Ψ)	_ <b>_</b>	,	٥	Г <u>.</u>	O,	3	√,	وآ	,97	,67	29,670	,67	,97	,05	26,418
Jan.	23.9	Ò	6,9	15,8	13,8	14,2	21,8	25,7	16,5	20,9	13,1	9	19	o,	23	26,	20,	31,	22,	27,	24,	17,	28,	31,	31	23,	35,	27,	20,859
Year	1950		52	53	54	55	56	57	58	59	9	61	62	63	99	65	99	67	68	69	70	71	72	73	74	75	9/	77	Mean

Diversion Requirements for Giritale Tank

(Unit : acft)

Remarks																													
Annual Total	188	69,980	77	-	68	79,460	78,221	69,213	75,343	72,845	58,966	62,145	76,701	61,022	79,973	63,459	70,487	73,125	78,036	70,519	71,499	75,737	71,866	7	83,629	48	44	41	72,860
Dec.	•	•	•		•		•	•	5,544	•	•		•		7,344	•	•	•		•	•	•	•	•		. •	•	•	3,684
Nov.	4,851	803	5,601	g,	5,601	5,751	2,751	803	•	1,251		•	4,324	803	6,651	803	803	803	4,099	2,826	2,751	6,351	803	٧,	6,726	∞_	0,	803	3,260
Oct.	45	4,553	,48	0	2,283	5,058	1,022	2,131	3,708	0	2,356	657	3,333	3,783	2,433	0	0	0	2,208	0	,20	53	0	,33	6,033	,50	533	0	2,521
Sep.	1,793	640	2	•	2,303	411	2,301	1,718	1,716	1,716	0	2,188	12	0	•	2,303	0	1,102		0	,71	27	0	640	871	14	2,192	0	096
Aug.	8,926	10,553	10,745	9,623	10,478	9,082	10,632	10,474	7,530	10,725	10,630	10,743	9,236	10,715	10,521	8,383	10,010	10,729	9,236	9,856	8,537	9,858	10,743	10,727	10,739	9,625	10,166	10,397	986,6
Jul.		13,173		_	S	-	13,183	12,071	13,169	13,179	9,832	13,175	13,183	11,684	11,295	13,171	13,179	13,181	13,183	11,222	13,183	12,916	13,183	8,322	13,183	8,614	12,916	12,608	12,213
Jun.	2	•	2,	2	ζ,	•	•	~	12,280	•	•	•	•	•	•	•	•	•		•	•	•	•	•	2,28	•	2,28	2,28	11,708
May	, 24	,62	<b>,</b> 09	,75	,75	,17	,75	,62	7,711	,62	,86	,86	90,	,73	,55	,94	,75	,25	,74	,73	,32	,47	90,	,02	, 31	,16	,73	,56	7,303
Apr.	3,266	338	1,181	0	0	0	•	•	2,334	•	0	800	1,337	950	3,027	0	492	2,182	•	28	0	0	800	•	1,337	12	26	3,262	1,152
Mar.	0	٠ <u>,</u>	2	~	ω,		٦,	~	3,227	€.	τ.Ž	Ţ	_	υ	o,	₹	~	7	ο,	ď	πŽ	ထ	۲,	õ	ୣ	പ്	ς.	ď,	4,136
Feb.	•	•	•		•	•	-	•	8,325	-	-	•	•	•	•	•	•	•	•	•	•	-	•	•	•	•	•	~ ,	8,269
Jan.	w		4	<u>Г</u> ,	п,	Ψ,	٦,	(')	5,398	w	2	~			יניי	~	ω		7	2,	Ç	φ,	ı,	0	. C.J	ω.	Γ,	Ç.	6,755
Year	1950	S	52	53	54	55	56	57	28 2	59	9	-1 -1	9	63	9	65	99	49	89	69	70	7.1	72	73	74	75	9/	7.7	Mean

Remarks 321,418 343,958 371,485 375,911 331,280 374,099 315,285 242,596 289,451 327,236 292,334 384,601 344,146 328,775 303,978 338,147 351,313 342,439 362,708 344,818 376,574 400,738 331,470 360,491 Annual Tota1 8,918 26,316 8,918 12,864 8,918 8,918 26,575 20,194 38,618 8,918 26,632 8,918 35,284 8,918 29,737 29,909 8,918 8,918 30,369 20,251 15,480 8,918 8,918 8,918 8,918 8,918 17,668 Dec. 26,766 27,484 12,998 3,919 10,670 20,500 3,919 31,968 3,919 3,919 26,766 23,547 5,927 3,919 3,919 3,919 19,436 13,113 30,387 3,919 34,728 32,313 21,190 15,617 13,601 3,919 23,087 Nov. 24,032 4,840 3,171 15,897 17,967 11,528 21,732 16,501 21,675 10,752 17,794 11,040 21,617 26,187 11,998 10,551 24,894 15,811 28,803 Oct, 10,729 4,199 8,497 8,406 8,346 8,560 5,084 11,659 2,126 11,651 7,564 107 11,659 3,087 125 5,972 5,521 61 3,087 10,917 Sep. 50,614 51,687 45,984 50,340 51,101 50,005 35,595 51,525 50,888 51,671 44,186 51,429 51,494 39,891 47,933 51,562 44,186 47,202 40,561 47,294 51,684 51,646 48,634 43,394 47,874 Aug. 62,846 62,817 61,985 38,225 62,899 62,902 57,416 62,786 62,873 46,433 62,832 62,893 62,905 61,319 62,910 40,440 55,177 62,910 55,389 38,936 62,910 58,078 62,797 62,867 53,361 52,910 53,331 Jul 58,748 58,672 58,742 58,728 58,748 58,748 748 52,865 58,738 55,135 58,715 58,748 58,748 58,748 52,313 58,748 58,748 58,748 748 58,742 58,685 58,592 58,748 56,264 58,695 58,612 58,748 56,423 Jun, 58 29,792 26,836 34,057 42,328 42,334 39,205 42,334 31,589 36,890 31,437 18,128 37,743 38,870 42,150 42,325 39,815 42,206 42,150 35,032 30,736 28,604 18,347 38,626 25,100 29,183 35,019 May 4,113 1,889 5,796 9,912 12,797 11,385 5,525 10,874 11,595 5,743 4,173 6,817 4,654 2,640 14,270 16,022 14,961 6,787 Apr. 25,235 25,379 22,274 25,379 25,379 15,348 25,379 21,499 22,160 23,022 14,140 10,806 17,934 25,379 18,193 12,473 25,379 22,505 7,443 25,379 19,894 23,968 46,388 46,560 47,451 40,007 28,308 30,780 37,678 42,392 49,981 38,770 11,371 44,491 32,447 49,981 49,981 49,981 46,302 48,975 47,652 45,698 27,359 42,277 49,981 41,319 Feb. 24,886 10,937 21,552 36,469 32,848 38,568 10,937 32,647 20,603 10,937 41,873 48,541 35,636 37,475 34,026 40,149 25,777 27,157 49,547 49,547 22,184 10,937 30,146 42,850 44,000 32,437 Jan. Year 1950 Mean VI-47

Remarks 242,280 207,107 242,303 197,091 257,063 189,843 231,626 235,825 249,001 220,087 230,759 250,281 231,960 249,818 252,380 28,260 228,429 218,298 245,723 23,567 207,376 228,173 86,420 08,707 263,141 268,161 53,251 Annual Total 6,510 9,312 16,171 5,906 11,618 13,099 15,591 20,885 10,452 5,906 16,847 18,335 5,906 18,277 9,659 25,059 5,906 5,906 22,025 5,906 15,997 990,9 5,906 12,384 5,906 19,456 5,906 5,906 10,316 Dec. 9,995 9,692 4,070 12,243 16,513 18,619 14,774 2,261 2,261 11,045 16,281 24,280 2,261 2,261 19,373 2,969 11,084 25,111 21,421 5,133 2,261 2,261 19,991 2,261 2,261 2,261 12,108Nov. 10,747 13,548 18,398 12,505 12,408 8,428 6,206 11,268 1,103 8,351 5,819 10,553 9,375 7,132 299 10,940 11,848 267 18,668 10,437 14,321 Oct. 1,853 7,000 7,273 5,138 8,493 3,371 4,232 6,895 9,674 1,150 6,180 155 2,419 7,733 1,128 5,636 3,982 2,691 485 Sep. 26,529 33,951 35,053 34,339 27,714 30,062 34,354 20,814 23,825 35,053 34,989 25,153 16,830 25,699 30,370 33,358 11,115 28,663 26,220 35,053 32,955 33,216 27,928 7,912 34,267 28,133 19,913 Aug. 38,568 18,418 40,423 36,482 25,493 40,356 40,275 35,300 35,879 37,039 36,204 37,410 40,585 40,793 40,771 36,482 38,592 36,830 38,569 40,793 40,793 30,385 40,793 33,028 Jul. 38,856 39,204 39,204 39,204 39,204 39,204 39,204 39,204 39,000 39,204 39,178 20,924 39,204 34,018 39,204 39,204 37,744 39,136 39,203 27,642 39,068 39,119 38,856 39,204 39,204 Jun. 29,368 29,003 29,035 27,176 21,485 22,694 28,385 25,372 28,884 16,837 24,733 19,730 19,920 24,378 29,368 29,273 29,051 28,575 28,694 21,935 26,559 25,943 22,623 May 5,122 6,074 5,666 12,960 5,462 1,316 7,320 2,721 10,287 10,786 13,008 4,216 3,513 9,880 10,537 3,718 12,349 9,019 5,988 2,177 10,605 Apr. 14,808 17,107 11,967 10,982 16,856 17,107 17,068 11,987 11,755 17,107 8,432 17,107 17,107 17,107 17,107 17,107 690,6 16,759 7,601 2,914 15,890 15,194 14,765 16,238 Mar. 29,390 27,419 33,022 30,781 31,476 25,081 25,410 33,602 13,817 26,395 31,303 23,130 31,940 27,033 33,602 25,989 22,453 33,602 32,655 32,964 31,844 33,409 33,602 28,826 30,221 16,811 Feb. 7,3497,349 8,668 26,154 27,584 22,676 17,595 26,656 33,303 30,869 15,952 10,716 32,897 33,303 7,349 15,836 29,806 25,961 22,096 33,303 32,955 22,271 7,354 16,281 23,95122,077 8 Jan. Year Mean VI-48

Remarks 169,068 73,207 117,490 169,879 117,064 148,761 116,893 98,506 98,634 148,975 108,531 81,612 80,332 132,720 136,758 110,494 146,585 194,409 .82,592 .60,962 43,130 53,155 155,715 190,100 128,880 172,737 41,850 161,901 .25,041 Annual Total 4,761 11,433 9,727 10,495 14,206 8,319 1,920 7,935 8,746 12,201 8,191 5,802 3,754 4,437 Dec. 3,285 6,869 2,261 14,676 11,391 3,200 981 3,616 13,950 9,599 5,546 8,916 2,261 10,153 Nov. 9,386 5,759 13,097 15,358 15,230 24,360 17,961 12,415 12,841 16,851 23,805 9,514 6,314 13,609 12,543 10,879 2,560 8,461 Oct. 22,611 11,988 22,312 27,005 24,402 19,624 20,947 24,914 23,037 17,193 20,563 13,310 18,600 12,799 17,363 25,042 10,708 16,254 30,162 24,744 16,297 23,848 14,974 19,326 18,217 26,024 2,389 18,809 Sep. 15,572 25,597 29,181 26,322 17,150 7,850 11,902 29,181 28,925 24,786 26,024 13,694 2,474 18,430 6,655 26,365 14,462 17,449 20,734 24,232 18,570 15,145 24,573 29,181 Aug. 21,202 4,863 24,488 26,578 21,715 25,085 18,643 21,715 20,222 19,027 15,444 17,491 20,181 26,578 11,177 25,768 26,578 14,548 26,493 19,027 24,829 21,715 Jul. 23,250 21,885 23,251 23,251 22,440 22,909 21,885 17,534 23,251 20,868 23,250 22,995 4,778 23,251 23,251 23,251 23,251 23,251 23,251 22,739 23,251 23,251 23,165 Jun. 14,249 13,907 21,586 19,923 21,288 14,334 20,350 20,435 15,486 17,192 10,537 18,814 5,119 11,945 19,240 11,049 14,804 11,860 8,490 21,587 18,600 15,488 20,478 16,467 May 19,539 8,618 9,812 14,932 18,728 4,053 14,462 9,044 3,968 15,273 5,034 11,305 6,911 5,674 19,752 7,508 17,491 13,396 9,507 6,655 683 8,447 15,572 Apr. 18,430 16,083 22,611 11,817 10,324 19,368 22,312 22,611 7,338 22,099 19,710 11,860 19,240 11,519 19,966 13,310 17,875 22,739 18,430 20,435 21,928 22,525 16,809 22,568 5,077 6,357 16,211 16,941 Mar. 4,863 5,333 14,548 16,809 16,254 13,652 14,036 13,780 1,920 14,377 12,244 18,045 6,741 16,340 19,539 6,143 19,539 11,552 7,636 15,742 16,169 18,387 5,290 11,049 8,191 1,067Feb. 5,034 8,020 9,940 3,413 17,065 5,119 7,764 2,645 2,645 16,979 12,889 14,292 17,875 7,109 12,969 8,703 15,529 20,051 18,131 Jan, Year 1950 Mean 63 64 65 VI-49

ac.ft)	Remarks		
(Unit: ac.	Annual Total	193,163 146,980 161,155 153,295 182,287 182,287 182,287 166,021 169,442 169,442 161,054 161,054 161,054 161,054 161,054 161,054 162,658 162,814 180,561 184,020 184,020 184,020 184,020	1101011
	Dec,	9,939 3,487 3,575 3,783 3,487 3,487 3,487 7,078 3,487 7,078 3,487 9,869 9,869 3,487 5,216 6,294 6,522 6,066	~
	Nov.	11,069 2,808 9,797 3,620 11,422 13,891 2,808 2,808 2,808 2,808 2,808 2,808 2,808 11,986 5,896 5,896 2,808 4,640 17,115 6,354 4,640	19404
(ELAHERA)	Oct.	17,502 13,622 16,391 13,146 11,206 19,654 18,719 4,566 11,911 11,911 11,911 12,068 7,908 7,908 7,908 11,546 10,501 12,546 12,566 12,566 12,566 12,566 13,958 8,572	î
SYSTEM G (E	Sep.	21,495 17,104 15,975 20,631 21,495 17,281 21,495 21,495 21,495 21,495 20,014 21,495 20,014 21,495 20,296 21,495	
FOR	Aug.	21,859 19,319 21,859 18,138 19,284 21,859 21,859 21,859 21,859 21,859 21,859 21,859 21,859 21,859 21,859 21,859 21,859 21,859 21,859 21,859 21,859 21,859 21,859 21,838	0.0.07
DIVERSION REQUIREMENTS	Jul.	15,637 15,637 14,753 14,753 15,637 15,637 15,637 15,637 15,637 15,637 15,637 15,637 15,637 15,637 15,637 15,637 15,637 15,637 15,637	7 I
ION REQU	Jun.	18,301 18,316 18,316 18,316 18,316 18,301	,,
DIVERS	May	22,371 18,044 19,243 23,494 22,960 23,494 23,494 23,494 23,494 23,494 23,494 23,494 23,494 23,494 23,494 23,494 23,494 23,494 23,494 23,494 23,494 23,494	77.7
	Apr.	21,607 17,148 12,891 12,891 12,674 13,038 18,774 16,723 16,723 16,723 16,723 17,741 17,741 17,259 11,078 11,078 11,078 11,078 11,078 11,078 11,078	ו ר
5	Mar.	12,303 12,570 17,657 15,773 16,507 14,552 17,657 17,657 17,092 17,657 17,092 17,657 17,657 17,657 17,657 17,657 17,657 17,653 17,653	17,40C
le 6-2-2	Feb.	8,671 8,135 6,944 10,560 8,593 9,132 12,004 14,331 14,331 10,829 10,289 10,289 11,594 11,594 12,356	~
Table	Jan.	12,409 2,885 2,885 2,885 2,885 11,157 9,214 6,853 15,944 6,853 8,159 2,885 14,226 2,885 12,656 9,430 2,885 12,656 14,226 14,226 14,226 14,226 14,226 14,226 14,226 14,226 14,226 14,226 14,226 14,226 14,226 14,226 14,226 17,885 18,758 18,758 18,758 18,735 18,735 14,061	7,000
	Year	Modern Market Ma	הפמוז

VI-50

# 2.2.7.2 Tank-wise Diversion Requirements (Case 2)

In this case (Case 2), the diversion requirements are computed on the following conditions;

- (a) Existing area and New land

  Cropping Pattern A, 80%

  Cropping Pattern B, 20%
- (b) For Elahera region (System G), the cropping patterns used in the report on the Integrated Small Farmer Development Project have been adopted.
- (c) For Kantalai tank, the diversion requirements have been determined by summing up the diversion requirements culculated for Kantalai farm managed by the Sugar Corporation (Table 6.2.24) and for paddy and upland (Table 6.2.31).

Table 6-2-26 Irrigation Area in Case 2

P-A udra 20,000 k 18,400 6,000	PB				
20,000 18,400 6,000		Total	P-A	P-B	Total
18,400 6,000	5,000	25,000	4,320	1,080	5,400
6,000	4,600	23,000	t	ı	1
	1,500	7,500	ı	1	I
Kaudulla Tank 2,77	2,720	13,600	17,920	4,480	22,400
Kantalai Tank 14,080 3,52	3,520	17,600	5,280	1,320	6,600
Kantalai (Sugar Coop.)		17,900			I
Elabera		14,800			l

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6-2-27 DIVERSION REQUIREMENTS	DIVERSION	DIVERSION	NOI	r requ	IREMENTS		FOR PARAKRAMA SAMUDRA	AMUDRA T	TANK			ac.ft)
Mar.	- 1	Apr.	May	Jun.	Jul.	Aug.	Sep.	0ct.	Nov.	Dec.	Total	Remar
39,824 7,722 1	Н	3,476	31,616	49,309	51,011		12,039	14,531	21,463	25,354	333,833	
16,781		•	36,358	49,309	46,634		0	19,699	2,675	17,145	276,578	
19,517	-	•	27,482	49,309	46,756		2,250	8,756	19,943	20,794	284,205	
		0	36,966	44,992	33,014		243	1,459	14,470	7,418	256,150	
3,708		5,323	36,966	49,309	42,256		12,707	6,627	20,247	7,418		
21,037	•	4,438	33,622	49,309	51,011		0	9,971	27,847	24,394		
18,301		6,992	36,905	40,235	50,524	39,520	12,525	4,621	8,026	13,801	302,286	
21,402	-	10,700	24,781	49,187	43,351		12,160	8,756	2,675	7,418		
14,045	•	9,546	31,677	49,309	51,011		10,944	5,411	15,990	7,418		
21,402		7,783	35,446	48,336	51,011		12,039	0	5,350	17,754		
		0	19,456	49,309	36,662		10,093	16,051	12,343	30,218		
14,045	•	5,655	22,192	49,005	51,011		12,343	12,039	4,438	7,418		
17,085		•	29,792	49,309	50,828		486	9,667	18,118	21,158		
		0	34,291	49,187	47,424		243	7,843	2,675	7,418		
		9,910	34,352	49,309	40,796		5,898	17,510	23,590	27,542		
		0	19,943	48,336	51,011		12,707	3,188	2,675	7,418		
		0	36,845	49,187	50,848		8,390	0	2,675	18,058		
18,908		8,876	36,480	49,309	51,011		12,160	1,702	2,675	6,318		
12,282	-	•	36,905	49,309	51,011		10,883	7,539	7,783	22,010		
		0	36,966	49,309	41,830		10,761	973	27,238	7,418	306,006	
		0	22,557	39,580	51,011		10,457	4,864	2,675	11,126	240,689	
		547	35,446	49,309	35,568		12,586	6,627	20,550	7,418	254,022	
21,402	•	•	23,287	49,309	50,585		0	0	2,675	7,418	284,485	
		4,653	28,272	43,107	18,483		0	8,147	2,675	7,418	258,400	
		•	31,251	49,309	51,011		0	23,347	19,334	19,881	342,486	
		0	25,536	49,309	17,024		12,707	5,716	10,518	7,418	225,204	
	1		,,,,	1	(		0		1	1		

rks

293,543 229,806	279,134
7,418	13,550
2,675	7,870 10,953
2,250 13,619 0 1,702	7,870
2,250	6,671
36,541 36,115	37,914
50,342 33,684	44,526
45,783 49,066	48,034
36,966 24,441	1
12,099 0	4,979 32,259
21,402 10,093	15,426
42,256 39,824	32,109
22,192 42,256 24,788 39,824	25,755 32,109
76	Mean

	Ta	Table 6-2-	.28		DIVER	RSION REQUIREMENTS	UIREMENT	1	FOR MINNERIYA TANK	TANK			(Unit: ac	ac.ft)
ear	Jan.	Feb.	Mar.	Apr.	May	Jun.	Jul.	Aug.	Sep.	Oct.	Nov.	Dec.	Annual Total	Remarks
	23,920	6	•	•	,94	37,306	38,456	25,898	6,	12,834	14,398	20,102	20	
_	•	ô	•	1,794	68	37,076	38,364	31,924	2,7	13,064	2,024	8,952	200,220	
<ul><li>✓</li></ul>	•	σ,	•	•	Π	37,260	37,306	33,350		9,844	16,698	18,952	232,024	
m	S	30,360	16,192	0	2	37,260	20,608	28,474	4,	١.	14,628	5,612	9	
<₹	•	٦,	•	0	,92	37,246	32,246	31,694	9,6	6,164	16,698	5,612	217,948	
S	4,	4,		0	,07	37,306	38,594	26,496	Ļ		17,158	19,228	233,910	
9	ı,	ó		•	,92	32,062	38,594	32,246	ο,	•	7,958	12,788	239,798	
7	'n	'n	16,192	9,706	36	37,168	33,948	31,602	ó	5,658	2,024	5,612	209,024	
8	é	'n		_	,36	37,260	38,272	20,700	9	•	13,018	16,882	227,424	
59	ó	Ę,		•	,32	33,810	38,502	32,890	છ		3,358	12,742	220,800	
0	'n	~		0	5,	37,214	25,806	32,200		•	2,024	24,518	172,178	
Н	•	φ,		3,450	96,	36,938	38,410	33,304	ထ်		6,348	5,612	189,980	
7	•	ထ်		5,336	62,	37,306	38,594	27,048		•	12,742	16,882	231,748	
m	•	6		3,910	41	37,306	32,522	32,660	0	10,764	2,024	5,612	183,586	
<b>_</b> +	ñ	4,		11,316	13	37,306	31,050	32,798	'n	•	19,918	22,402	242,834	
'n	ó,	ó		0	£6,	37,260	38,318	23,874	ο,	0	2,024	5,612	190,210	
۵	ó	-		2,346	,87	37,260	38,502	29,900		0	2,024	16,652	214,406	
_	L,	~		8,326	43	37,122	38,548	32,982	4,	0	2,024	5,612	224,250	
ഹ	2,	1,		8,878	9,	37,306	38,594	27,048		5,934	12,052	16,652	237,038	
~	^	6		949	,41	37,306	30,866	29,348		0	8,188	5,612	212,152	
_	4,	~		0	94	34,730	38,594	24,426	o,	_	7,958	8,142	213,762	
_	~	ŝ		0	,76	36,892	36,938	29,394	8,8	13,064	18,998	5,612	227,516	
~1	တ်			3,450	90,	37,306	38,594	33,304			2,024	9,752	217,718	
m	Ţ,	6		10,810	,56	31,740	20,976	32,936	2,	•	21,758	5,612	236,302	
<u>.</u> +	L,	ο,		5,336	49	37,306	39	33,212	3,5		20,148	5,612	253,555	
٠.	'n	6		276	19,	37,306	7.7	28,520	32	•	11,178	5,612	204,884	
'n	•	•		598	4	37,306	کِ	30,498	8,556	13,064	5,428	5,612	244,676	
_	7,	1,		12,236	54	37,306	5,83	31,326		0	2,024	5,612	223,376	
Mean	19,734	26,421	12,745	4,520	22,051	36,642	34,796	30,002	4,101	7,158	9,530	10,629	219,507	

ac.ft)	Remarks																													
(Unit: a	Annual Total	79,305	55	75,660	9/	71,070	76,275	78,195	68,160	74,160	72,000	56,145	61,950	75,570	59,865	79,185	62,025	69,915	73,125	77,295	69,180	69,705	74,190	70,995	77,055	82,680	66,810	79,785	14,040	69,595
	Dec.	_ ^	•	•	1,830	•	•	_	•	•	•	•	•	•	•	•	•		1,830	•		2,655	•	•	•	•	,83	1,830	, 83	3,648
	Nov.	4,695	099	5,445	4,770	5,445	5,595	2,595	099	4,245	1,095	099	2,070	4,155	099	6,495	099	099	099	3,930	2,670	2,595	6,195	099	7,095	6,570	3,645	1,770	099	3,108
TANK	Oct.	4,185	4,260	3,210	0	2,010	4,785	840	1,845	3,435	0	2,070	540	3,060	3,510	2,160	0	0	0	1,935	0	4,935	4,260	0	3,060	5,760	5,235	4,260	0	2,334
GIRITALE 1	Sep.	2,235	006	15	1,545	3,135	645	3,120	2,160	2,145	2,145	0	2,760	90	0	1,905	3,135	0	1,440	45	0	2,160	2,895	0	006	1,170	105	2,790	0	1,337
FOR	Aug.	8,445	10,410	10,875	9,285	10,335	8,640	10,515	10,305	6,750	10,725	10,500	10,860	8,820	10,650	10,695	7,785	9,750	10,755	8,820	9,570	7,965	9,585	10,860	10,740	10,830	9,300	9,945	21	9,428
IVERSION REQUIREMENTS	Jul.	12,540	12,510	12,165	6,720	10,515	12,585	12,585	11,070	12,480	12,555	8,415	12,525	12,585	10,605	10,125	12,495	12,555	12,570	12,585	10,065	12,585	12,045	12,585	6,840	12,585	80	12,045	89	11,346
RSION RE	Jun.	12,165	4	7	12,150	ζ,	ς,	ó	ς,	ŝ	٠Ĺ	2,	ς,	۲,	ú	ζ,	ζ,	2,	2	ď,	'n	Ξ,	2,	ď	ó	12,165	S,	12,165	2	11,985
DIVE	Мау	85	11,	88	9,105	10,	,17	100,	,31	,62	8,	,18	,81	80,	,94	, 24	, 24	9	,29	9	,94	,15	,12	,56	10,	,72	,74	95	, 65	7,190
	Apr.	4,020	585	1,545	0	0	0	J.	1,	$\infty$	4,	0	Ħ,	۲,	1,275	9,	0	765	7	œί	210	0	0	Ţ,	S	7,	90	195	3,990	1,474
6	Mar.	2,040	o	ς,	5,280	φ	ð	ς,	ς,	ď	ς,	ů	€.1	۲,	τŢ	οž	ď	2	7	ð,	ς,	õ	ω.	ડ્રં	õ	2,	ď	ς,	ī,	4,156
6-2-2	Feb.	8,775																												8,616
Table	Jan.	7,800	4	3	•	n,	a,		د.)	£.3	ω	5	3	٤,	ς,	υ	<u>,</u>	$\infty$	ᅻ	7,	οž	o.	ō	7	u.Ž	വ്	ď	Ļ	Q.	6,754
	Year	1950	21	52	53	53	55	56	57	58	29	09	61	62	63	99	65	99	29	99	69	70	7.1	7.7	73	74	75	92	77	Mean

	Table	le 6-2-30	0		DIVE	VERSION RE	REQUIREMENTS	FOR	KAUDULLA TANK	IANK			(Unit:	ac.ft)
Year	Jan.	Feb.	Mar.	Apr.	May	Jun	Jul.	Aug.	Sep.	Oct.	Nov.	Dec.	Annual Total	Remarks
	37,438 10,800 9,504 24,838 21,600 22,318 34,127 40,246 25,847 32,759 18,576 14,688	7,40,00,4,40,00,4,4	00447 0000 0000 0000 0000 0000 0000 000	922 822 823 932 933	8,07 4,55 0,17 0,17 0,23 0,23 1,53 1,53 1,53	58,391 56,526 56,526 56,526 58,391 56,779 56,182 56,318 56,318 57,816 58,389	60,190 60,046 46,922 0 69,536 52,163 60,406 53,134 59,902 60,262 47,736	40,607 49,967 53,990 39,907 49,607 35,377 50,470 52,917 32,399 51,479 51,479	10,726 4,318 2,762 12,432 15,046 6,320 14,974 10,366 10,295 5,184 8,496	20,087 20,447 11,643 0 9,647 19,203 4,031 8,854 16,487 0 9,216 4,320	22,535 3,167 23,984 20,743 26,135 24,705 12,455 3,167 20,376 5,255 4,464	31,463 29,663 29,126 8,245 8,783 29,736 20,014 8,783 26,424 19,942 32,400	373,428 329,051 348,956 284,450 360,187 347,286 375,316 330,603 353,225 345,611 286,704	
65 67 68 68 69 67 77 77 77	78677999679747	44,640 30,672 37,800 32,400 50,040 42,480 50,040 45,720 45,337 46,337 46,337 48,492	0,74,008,02,02,00,0 0,12,8,02,02,05,1		38,808 42,912 29,952 15,552 43,632 39,816 42,912 34,346 29,376 26,646 38,362 27,510 41,453	58,386 58,392 58,392 58,392 58,320 58,392 58,360 57,744 58,261 58,261 58,261 58,261	60,408 50,904 48,600 59,976 60,264 60,408 48,312 60,408 57,816 60,266 32,741 60,266 32,741 57,677	42,336 51,120 51,336 37,368 48,800 51,624 42,336 46,008 52,014 51,438 51,438 51,438	432 0 9,144 15,048 0 6,912 216 0 10,368 13,896 4,314 5,607 5,607 5,607	14,688 16,848 10,368 0 0 9,288 20,448 20,448 20,48	19,944 3,168 3,168 3,168 3,168 12,816 12,456 29,736 3,159 31,464 17,455 8,475	26,424 8,784 35,064 8,784 26,064 8,784 12,744 8,784 8,764 8,764 8,764	362,730 287,352 380,088 297,792 335,592 351,000 371,016 332,064 336,112 340,002 369,025 369,025 348,848	
Mean	32,419	39,819	19,938	7,113	34,816	57,028	53,534	45,885	6,822	10,968	14,794	17,365	342,223	

 $t_{i-t}$ 

	့ တ		
c.ft)	Remark		
(Unit:ac.ft)	Annual Total	248,680 219,780 252,794 233,170 226,514 206,764 230,382 228,106 249,408 227,426 217,462 207,052 241,664 189,292 241,664 189,292 241,664 257,004 257,004 257,004 257,004 257,004 257,004 257,004 257,004 257,004 257,004 257,004 257,004 257,004 257,004 257,004 257,004 257,820 245,630 257,820 245,630 257,820 245,287 231,798	
$\sim$	Dec.	13,164 24 15,584 21 20,910 25 5,904 22 16,794 20 18,296 23 18,296 23 18,296 22 18,296 22 25,022 21 25,904 22 5,904 22 6,098 24 6,098 24 10,118 22 12,400 25 19,458 26 19,458 26 10,260 23	
(PADDY AND UPLAND CROPS)	Nov.	9,584 4,016 12,244 16,360 18,536 2,130 2,130 2,130 14,664 2,130 2,130 2,130 2,130 2,130 2,130 11,034 2,130 2	
AND UPLA	Oct.	10,598 13,504 18,344 8,422 6,196 11,084 1,162 5,758 10,842 10,358 9,340 3,678 9,340 10,260 11,808 11,808 12,488 12,294 18,586 10,358 10,358	
	Sep.	5,518 6,664 6,680 1,210 3,484 4,356 6,970 5,808 1,790 6,922 1,210 2,420 9,824 6,922 1,210 2,420 2,420 2,420 2,420 2,420 3,242 1,210 1,210 2,420 3,242 1,838 1,	
LAI TANK	Aug	26,330 33,880 35,090 34,266 27,540 27,540 20,570 20,570 34,992 34,992 34,992 34,992 35,090 36,040 36,040 35,090 32,960 32,960 32,960 32,960	
FOR KANTALAI TANK	Jul.	40,608 37,994 18,004 18,004 36,834 40,222 35,804 40,608 40,076 37,170 30,056 40,608 40,608 40,608 40,608 37,170 37,170 37,170 37,170 37,170 37,170 37,170 37,170 38,334 35,042 35,042 35,042	
EMENTS F	Jun.	39,252 39,252 39,252 38,864 39,252 33,252 39,252 39,252 39,252 39,252 39,252 39,252 39,252 39,252 39,252 39,252 39,252 39,252 39,252 39,252 39,252 39,252 39,252 39,252	
REQUIR	May	15,198 24,586 24,298 29,428 29,428 29,330 24,634 29,040 29,040 22,750 21,346 22,748 29,428 28,508 22,668 25,168 25,365	
DIVERSION	Apr.	13,068 1,548 1,548 1,838 3,582 13,262 5,856 6,194 6,194 10,744 1,308 10,744 1,308 10,744 1,536 11,036 11,036 11,036 11,036 12,536 9,098 10,794	
31	Mar.	16,264 14,810 17,036 11,954 10,986 16,794 17,036 17,036 17,036 11,712 7,600 17,036 11,712 17,036 17,036 17,036 17,036 17,036 17,036 17,036 17,036 17,036 17,036 17,036	
Table 6-2-	Feb.	29,330 27,346 32,960 30,734 31,460 25,168 31,702 25,168 31,704 25,378 31,218 23,232 33,154 16,746 31,944 27,104 27,104 27,104 27,104 33,638 32,670 31,375 31,375 31,375	
Ta	Jan.	29,766 7,260 7,260 15,972 10,648 8,712 23,958 27,588 27,588 27,588 27,588 27,260 15,730 7,260 15,730 7,260 22,953 22,922 22,022 22,022 33,396 33,396 31,702	
	Year	1950 1950 51 52 53 53 54 55 66 67 66 67 67 77 77 Mean	

ı	Tab	able 6-2-32		DIVERSION	REQ	UIREMENTS	FOR KAUD	KAUDULLA TANK	(FOR EXISTING	TETING A	AREA)		(Unit:	ac.ft)
Year	Jan.	Feb.	Mar.	Apr.	Мау	Jun.	Jul.	Aug.	Sep.	Oct.	Nov.	Dec.	Annual Total	Remarks
1950	14,143	5,9	, 69	•	,60	$\Box$	73	5,34	4,052	7,588	8,513	11,886	22	
51	,08	5,5	,13	1,060	,27	cn.	89	တ်		7,724	1,196	11,206	õ	
52	<b>80</b>	7,5	, 54	•	2,48	$\Box$	22,059	,71	299	5,820	9,873	11,206	9	
53	,38	7,9	,57	0	6,50	$\Box$	18	Ġ	2,801	a	8,648	3,318	3	
24	,16	4	,31	0	,50	$\mathcal{C}$	19,066		5,684	•	9,873	3,318	128,866	
55	,43	4,6	,45	0	4,82	<b>C</b> 3	22,820	15,666	1,169	Q	10,145	11,369	80	
26	,89	7,9	,57	•	6,50	CTN.	22,820	רט	5,657	√,	4,705	7,560	8	
57	5,20	9,1	,57	•	1,45	ന	20,073	Ç	3,916	u,	1,196	3,318	127,043	
58	,76	o	,87	5,222	3,08	$C_{3}$	22,629		3,889	4	7,697	9,982	133,736	
59	,37	8,9	57	•	1,42	an.	22,765	O.	3,889	0	1,985	7,533	130,551	
9	,01	,6	,37	952	15,	$\alpha$	18,033	19,584	1,958	7,	1,687	12,240	108,310	
61	, 54	1,9	,54	•	4,33	$\boldsymbol{\Box}$	22,821	$\alpha$	3,209	9	4,488	4,651	115,707	
62	,42	6,8	,82		4,66	$\Box$	22,821	r(J)	163	٦,	7,534	9,982	137,029	
63	,08	1,5	,88	2,312	, 21	$\Box$	19,230	5	0	~	1,197	3,318	108,554	
97	3,73	4,2	35	•	1,31	()	18,360	Ġ,	3,454	οž	11,777	13,246	143,585	
65	5,77	2,2	,57		5,87	$\Box$	22,658	• 1	•	0	1,197	3,318	112,498	
99	2,37	8,9	,10	1,387	6,48	$\Box$	22,767	_	0	0	1,197	9,846	126,779	
29	8,36	0,9	, 85	~	5,04	$\Box$	22,794	Q1	2,611	0	1,197	3,318	132,599	
68	3,46	8,0	,78	•	6,32	$\mathbf{c}$	22,821	LJ.	82	3,509	7,126	9,846	140,161	
69	6,18	7,2	,57	381	6,21	$\Box$	18,252		0	0	4,841	3,318	125,446	
70	14,552	10,336	8,351	0	12,974	20,536	22,821	14,443	3,917	8,949	4,706	4,815	126,400	
71	0,20	5,9	,73	0	1,09	ന	21,841	_	, 24	,72	11,234	3,318	134,531	
72	6,49	8,7	, 51	•	0,02	CD.	27	C)	0	0	1,188	5,732	127,968	
73	8,65	7,4	,43	6,362	4,43	vo	12,312	19,361	62	^	12,788	3,298	138,885	
74	8,65	7,4	,51	^	,51	$\alpha$	5	5	2,113	38	11,842	3,298	49,0	
75	3,65	7,4	,86	163	0,35	CT.	74	Ψ	19	43	6,569	3,298	20,4	
9/	8,25	8,7	,51	354	,14	CD.	70	17,925	5,037	•	3,189	3,298	43,8	
77	6,08	8,2	,27	7,202	5,60	$\alpha$	25	18,412		0	1,188	3,298	1,2	
Mean	12,251	15,689	7,515	2,716	13,100	21,643	20,651	17,801	2,439	4,238	5,671	6,576	130,290	

Acft)

(Unit:

Remarks 158,154 150,588 175,755 137,667 180,858 159,841 183,850 162,306 167,551 165,896 186,912 176,247 168,916 143,051 174,626 158,504 150,374 181,387 Annual 165,395 151,396 166,133 .64,687 178,640 183,463 191,276 .94,901 83,920 Total 4,294 4,294 13,271 6,970 18,198 4,435 4,294 4,682 15,207 7,638 4,294 16,087 4,294 11,687 4,471 11,722 4,294 14,151 11,334 4,294 12,214 13,306 6,758 4,294 9,047 4,294 7,462 8,460 Dec. 11,898 13,481 17,670 1,549 1,549 1,549 3,625 1,549 10,665 1,549 14,538 1,549 11,862 1,549 1,549 2,041 8,025 18,234 15,594 8,730 8,905 8,025 7,211 14,010 6,970 3,801 6,970 2,921 Nov. 7,533 7,462 8,588 13,517 10,348 7,533 4,1887,885 7,708 9,821 13,341 5,948 5,419 6,793 2,675 6,125 9,082 8,941 Oct. 2,957 1,760 7,145 5,034 3,802 6,301 4,858 2,534 3,168 5,069 4,224 1,302 5,773 1,337 5,244 2,358 2,605 880 106 387 Sept. 24,218 24,886 18,093 25,520 23,971 24,182 20,240 19,149 24,640 25,520 24,921 20,029 21,789 24,956 14,960 17,177 25,520 25,449 11,933 19,923 20,697 14,326 22,000 18,938 7,885 20,423 5,632 Aug. 29,533 27,632 27,879 13,094 26,365 27,879 29,146 27,033 29,533 29,533 29,533 23,795 29,533 27,879 25,485 29,392 25,907 29,181 26,607 29,252 18,234 21,859 29,533 26,365 July 28,547 28,547 28,547 28,265 28,547 28,547 28,547 24,569 19,817 28,547 28,547 28,547 27,448 28,547 28,265 14,925 28,477 28,547 28,441 28,547 28,547 28,371 28,677 28,547 26,576 28,547 8,477 June 19,395 18,304 18,797 11,053 17,881 17,671 21,402 21,015 12,144 21,331 17,916 21,120 21,120 18,727 19,818 21,155 14,327 21,402 20,733 20,768 20,874 15,910 16,368 15,524 16,544 14,397 18,446 May 7,814 4,259 9,645 3,837 4,505 7,396 2,816 2,007 7,638 8,026 4,457 9,504 1,126 1,337 2,605 4,084 5,491 9,680 3,203 9,117 951 6,617 Apr 11,510 11,828 10,771 12,390 8,694 7,990 112,390 6,583 112,390 6,583 112,390 112,300 112,300 112,300 112,300 112,300 112,300 112,300 112,300 112,300 112,300 112,300 1 9,398 10,771 11,828 12,390 12,390 12,390 11,123 6,195 12,390 10,722 Mar. 16,896 18,832 16,368 24,464 23,760 21,331 19,888 23,971 22,352 18,480 22,000 19,184 19,712 23,232 24,288 24,464 10,032 22,704 24,007 20,969 18,304 24,112 12,179 24,464 23,232 Feb. 19,360 21,648 17,424 19,008 20,064 16,016 5,280 11,616 5,280 5,280 22,492 23,936 17,424 24,288 16,149 16,544 12,848 11,440 11,792 15,016 23,936 18,832 Jan. Year 1950 Mean VI-59

Diversion Requirements for Parakrama Samudra (for Existing Area)

(Unit: Acft)

Remarks																													
Annual Total	274,000	227,450	233,800	210,650	226,150	250,750	249,050	222,600	233,600	248,700	214,400	206,500	254,950	194,250	248,000	195,976	221,750	248,400	265,555	251,650	197,650	208,900	233,950	212,500	281,650	185,200	241,400	192,850	229,724
Dec.	20,850	14,100	17,100	6,100	6,100	19,350	11,350	6,100	6,100	14,600	24,850	6,100	17,400	6,100	22,650	6,100	14,850	5,000	18,100	6,100	9,150	6,100	6,100	6,100	16,350	6,100	6,100	6,100	11,111
Nov.	17,650	2,200	16,400	11,900	16,650	22,900	6,600	2,200	13,150	4,400	10,150	3,650	14,900	2,200	19,400	2,200	2,200	2,200	6,400	22,400	2,200	16,900	2,200	2,200	15,900	8,650	2,200	2,200	9,007
Oct.	11,950	16,200	7,200	1,200	5,450	8,200	3,800	7,200	4,450	0	13,200	006,6	7,950	6,450	14,400	2,626	0	1,400	•	800	•	5,450	0	•	19,200	4,700	11,200	1,400	6,472
Sept.	006'6	0	1,850	200	10,450	0	10,300	10,000	9,000	9,900	8,300	10,150	400	200	4,850	10,450	6,900	10,000	•	8,850	õ	10,350	0	0	0	•	1,850	0	5,782
Aug.	29,750	33,750	36,250	34,350	31,550	24,700	32,500	35,600	22,200	34,950	35,400	36,250	35,250	36,050	33,200	22,900	26,000	36,200	36,100	29,350	27,800	12,400	36,200	33,450	36,200	28,400	30,050	29,700	31,304
July	41,950	38,350	38,450	27,150	34,750	41,950	41,550	35,650	41,950	41,950	30,150	41,950	41,800	39,000	33,550	41,950	41,800	41,950	41,950	34,400	41,950	29,250	41,600	15,200	41,950	14,000	41,400	27,700	36,616
June	40,550	40,550	40,550	37,000	40,550	40,550	33,550	40,450	40,550	39,750	40,550	40,300	40,550	40,450	40,550	39,750	40,450	40,550	40,550	40,550	32,550	40,550	40,550	35,450	40,550	40,550	37,650	40,350	39,517
May	26,000	29,900	22,600	30,400	30,400	27,650	30,350	19,500	26,050	29,150	16,000	18,250	24,500	28,200	28,250	16,400	30,300	30,000	30,350	30,400	18,550	29,150	19,150	23,250	25,700	21,000	30,400	_	25,427
Apr.	10,550	∞_		0	•		5,750	•	•		0	4,650	•	0	8,150	0	0	7,300	•	0	0	450	2,550	12,050	1,950	0	9,950	0	4,079
Mar.	6,350	13,800	16,050	13,850	3,050	17,300	15,050	17,600	11,550	17,600	13,050	11,550	14,050	11,600	0	17,600	7,050	15,550	10,100	17,550	•	7,050	•	•	17,050	•	•	•	12,686
Feb.	32,750	28,250	26,750	29,750	29,000	28,500	31,750	12,000	29,500	34,750	8,000	16,250	31,500	16,500	19,300	8,000	34,750	27,000	34,750	33,500	13,000	28,750	34,750	27,500	32,300	23,000	34,750	75	26,405
Jan.	25,750	•	•	ထ်	ຕົ	ø	•	٧,	Ļ	'n	14,750	7,500	20,000	7,500	23,700	28,000	17,450	31,250	25,750	27,750	22,250	22,500	33,250	34,500	34,500	24,750	18,250	25	21,318
Year	1950	21	52	53	54	55	26	27	58	ĽΩ	9	19 -6	9	63	64	65	99	29	68	69	70	71	72	73	74	75	9/	77	Mean

## 2.2.7.3. Tank-wise Diversion Requirements (Case 3)

In this case (Case 3), the diversion requirements are computed on the following conditions;

- (a) Existing Area only,
- (b) Cropping Pattern A, 97.5% Cropping Pattern B, 2.5%
- (c) For Elahera region (System G), the cropping patterns used in the report on the Integrated Small Farmer Development Project have been adopted. Diversion requirements are shown in Table 6.2.25.
- (d) For Kantalai tank, the diversion requirements have been determined by summing up the diversion requirements culculated for Kantalai farm managed by the Sugar Corporation (Table 6.2.24) and for paddy and upland (Table 6.2.37).
- (e) For Minneriya and Giritale Tank, the diversion requirements are shown in Table 6.2.20 and 6.2.21 as same as Case 1.

(Unit: acft)

Remarks		ı
Annual Total	277,400 231,499 237,350 217,083 227,720 259,489 248,477 225,715 225,715 221,170 208,116 224,272 247,793 264,820 254,527 205,029 214,732 214,732 284,549 189,933 244,757	233,529
Dec.	20,986 14,179 17,173 6,209 6,209 14,738 23,441 11,385 6,209 17,553 6,209 14,918 6,209 6,209 6,209 6,209 6,209 6,209 6,209	11,401
Nov.	18,099 2,789 17,002 12,351 12,351 17,002 12,789 13,529 4,985 10,794 4,187 15,445 2,789 2,789 2,789 17,441 2,789 17,441 2,789 2,789 17,441 2,789 2,789 2,789 2,789 2,789	9,576
Oct.	12,880 17,232 8,050 1,341 6,433 9,188 4,533 8,110 5,455 10,764 3,348 7,331 1,789 7,331 1,789 7,231 1,030 4,864 6,393 6,393 1,202 1,671	7,194
Sept.	7,657 7,657 7,726 7,726 7,670 7,660 6,624 7,661 7,661 7,724 7,724 5,438 7,669 7,724 5,438 7,724 5,438 7,724 1,127 0	4,394
Aug.	31,117 34,431 35,839 32,839 32,537 26,919 35,759 35,759 35,839 35,839 35,839 35,839 35,839 35,839 35,839 35,839 35,835 35,836 36,109 37,109 31,405	34,508
July	43,955 41,431 41,636 43,955 43,955 43,955 43,955 43,955 43,955 43,955 43,955 43,955 43,955 43,955 43,955 43,955 43,955 43,955 43,955 43,955	39,506
June	40,849 40,849	40,117
Мау	26,194 29,188 23,334 29,249 27,594 29,249 20,885 26,318 26,318 28,088 117,881 117,881 28,005 28,005 28,005 28,005 28,005 28,005 28,005 28,005 28,005 28,005 28,005 28,005 28,005 28,005 28,005 28,005 29,249 20,041 28,746 20,041 28,746 20,041 28,746 20,041 28,746 20,041 28,746 20,041 28,746 21,358	25,569
Apr.	10,807 1,959 2,081 2,081 2,531 4,369 7,086 6,269 5,043 5,105 6,433 6,433 1,693 1,693 1,693 1,162 8,067	3,236
Mar.	6,338 13,684 15,959 13,863 17,177 17,177 17,616 11,468 11,468 11,616 6,917 17,616 6,997 17,616 17,616 17,616 17,616 17,616 17,616 17,616 17,616 17,616 17,616	12,637
Feb.	32,672 28,161 26,684 29,039 28,039 28,401 31,913 31,913 34,708 34,708 34,708 34,708 34,708 34,708 34,708 34,708 34,708 35,708 37,708	26,377
Jan.	25,846 7,596 18,800 13,071 15,905 27,544 27,542 27,542 21,315 14,808 23,630 23,630 23,630 23,630 23,630 23,630 24,709 34,409 34,409 24,309	21,354
Year	VI-62 VI-62 VI-62 VI-62 VI-62 VI-62 VI-62	Mean

Diversion Requirements for Kaudulla Tank

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Remarks		
Annual Total	145,265 126,946 139,365 121,766 130,097 140,674 142,020 128,992 106,923 106,923 112,768 139,004 110,723 141,502 141,502 141,502 128,063 129,807 137,438 151,623 125,858 145,994 133,004	131,711
Dec.	11,927 111,243 111,308 3,378 3,378 11,481 7,659 14,598 14,598 14,598 12,378 13,378 13,378 13,378 13,378 13,378 3,378 3,378 3,378 3,378	6,684
Nov.		5,938
Oct.	8,082 8,277 6,301 0 4,129 9,146 1,873 3,825 6,790 6,790 6,073 6,855 4,423 4,423 6,855 6,855 6,040 10,948 8,256 8,256	4,579
Sept.		1,844
Aug.	0H4440H000A444444444	18,137
July		22,116
June		21,194
May	11,35 10,26 10,26 115,90 115,90 11,94 11,9	13,258
Apr.		2,091
Mar.	φομνα4ημνηΗονωμνοωνημφη4ηωνν	7,511
Feb.	ညီလုံ ငှုံ ဟွဲ့ နှံ့ ထွဲ တွဲ့ လွဲ့ ထွဲ နှံ့ ဝပ္ပံုရှိ နှံ့ ပုံ ထွဲ တို့ ထွဲ ငှုံ ဝပ္ပံုစွဲ ငှုံ ငှုံ ဟွဲ့ ထွဲ ခ	15,609
Jan.	444988446444446464464686666666666666666	12,254
Year	1950 521 522 534 544 556 657 657 657 658 657 657 77	Mean

Diversion Requirements for Kantalai Tank

(unit: acft)

Remarks		
Annual Total	183,505 164,827 164,827 167,163 149,517 170,541 138,027 150,797 178,401 141,510 141,510 168,822 161,636 168,822 181,586 185,332 181,586 185,336 187,578 186,586	169,857
Dec.	9,603 11,416 15,266 7,678 4,371 12,329 13,411 4,371 11,711 4,371 11,837 4,488 4,488 4,488 4,488 4,371 11,837 4,371 11,837 4,371 11,837 4,371 7,579	8,531
Nov.	7,388 3,299 12,349 12,349 13,880 17,997 1,963 1,	7,245
Oct.	8,407 10,445 13,972 6,721 5,105 8,787 6,665 4,824 8,548 8,548 9,665 9,686 9,686 9,686 9,686 9,616	5,576
Sept.	3,080 2,951 4,958 3,843 0,659 1,829 2,376 4,059 3,267 1,225 3,986 3,986 4,115 1,397 1,397 1,397 1,397 1,300 1,700	2,040
Aug.	20,492 24,963 25,230 25,160 21,153 6,872 22,588 25,161 16,937 18,777 25,224 24,601 19,589 9,653 14,504 19,922 21,776 20,241 22,776 22,776 22,776 22,776 22,211 22,230 24,355 24,355	21,223
July	30,944 29,716 29,947 15,995 28,847 30,944 21,806 30,944 21,806 30,944 30,944 30,944 30,944 30,944 30,944 30,944 30,946 30,946 30,947 30,946 30,947 30,947 30,947 30,948	28,705
June	28,758 28,758 28,758 28,758 28,758 26,071 28,758 22,247 28,758	27,979
May	12,429 18,122 20,591 20,591 20,582 13,341 20,582 20,582 18,166 19,658 16,920 20,591 16,920 20,591 16,456 18,904 16,456 18,225 18,225 18,225 18,225 18,225	18,467
Apr.	7,605 7,605 1,882 1,882 2,903 3,507 3,119 6,341 1,034 1,034 1,034 1,299 2,803 2,012 1,379 6,499 7,630 7,630 6,384	3,478
Mar.	11,769 12,402 12,402 12,402 12,402 12,402 12,402 12,402 12,149 8,509 8,509 12,402 11,769 11,769 11,769 11,769 11,769 11,769 11,769 11,769 11,769 11,769 11,769	10,698
Feb.	21,371 19,938 22,383 22,383 22,383 18,238 18,238 10,045 10,045 10,045 10,045 10,045 10,045 10,045 10,326 12,223 23,226 12,435 16,326 24,435 16,326 23,746 24,435 18,898 16,326 23,746 24,435 18,898 16,326 23,746 24,435 18,898	20,961
Jan.	21,722 5,348 11,605 7,797 6,307 17,366 19,024 10,024 10,024 11,521 11,521 11,521 11,521 11,680 11,844 23,971 11,621 11,680 11,844 23,971 11,621 23,929 24,224 24,224 22,453	16,201
Year	152 725 727 727 727 727 727 727 727 727 7	Mean

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#### 2.2.8 Results of Water Balance Calculation

As a result of the water balance calculation made for the Moragahakanda dam in consideration of tank-wise water use under the project, the past 28-average value of the success percentage (the ratio of the yield area to the whole cultivated area) has been determined at 90.5% (Table 4.2.38).

For reference, if it is assumed that the water-use facilities (being so superannuated at present) of the existing cultivated land were improved under the situation after completion of the Polgolla-Bowatenna Complex, i.e. Post-Polgolla, then the success percentage would have been estimated at 82.9% by applying the cropping pattern proposed under the project and the projected water requirements to the percentage (Table 6.2.39). In this case, however, the water balance calculation has been made, including System G and the existing proposed site for a programme for increasing sugar production.

Tank		tale	Minne	-		ulla		alai		mudra
	(750	0 ac)		<u>00 ac)</u>		000 ac)		00 ac)		<u>00 ac)</u>
Year	Yala	Maha	<u>Yala</u>	Maha	Yala	Maha	Yala	Maha	Yala	Maha
1950	100	100	100	100	100	100	100	100	100	100
51	100	100	100	100	100	100	100	100	100	100
52	100	100	100	100	100	100	100	100	100	100
53	100	100	49	100	4	100	12	100	18	100
54	100	100	100	100	100	100	100	100	100	100
55	100	100	100	100	100	100	100	100	100	1.00
56	100	100	62	100	0	100	0	100	2	100
57	100	100	100	100	0	100	6	100	28	100
58	100	100	100	100	100	100	1.00	100	100	100
59	100	100	100	100	100	100	100	100	1.00	100
60	100	100	100	100	100	100	100	100	100	100
61	100	100	100	100	100	100	106	100	100	100
62	100	1.00	100	100	100	100	100	100	100	100
63	1.00	100	100	100	100	100	100	100	100	100
64	100	100	100	100	100	100	100	100	100	100
65	100	100	100	100	100	100	100	100	100	100
66	100	100	100	100	100	100	100	100	100	100
67	100	100	100	100	100	100	100	1.00	100	100
68	100	100	100	100	100	1.00	100	100	100	100
69	100	100	100	100	100	100	100	100	100	100
70	100	100	100	100	100	100	100	100	100	100
71	100	100	100	100	100	100	100	100	100	100
72	100	100	100	100	100	100	100	100	100	100
73	100	100	100	100	65	52	88	100	100	100
74	100	100	100	100	0	0	0	54	50	100
75	100	100	100	100	0	1.00	0	100	100	100
76	100	100	0	100	0	100	5	100	29	100
77	100	100	100	100	95	100	96	100	100	100
Mean	100	100	93	100	77	95	79	98	83	100

Table 6-2-39 Success Percentage of Crop Cultivation (Post-Polgolla, after improvement of inflastructures)

Tank	_Giri	tale_	Minne	riya	Kand	ulla _	Kant	alai	PSa	mudr <u>a</u>
Year	Yala	Maha	Yala	Maha	Yala	Maha	Yala	Maha	Yala	Maha
1950	100	100	25	100	100	100	18	100	100	100
51	100	100	100	100	100	100	47	100	63	100
52	100	100	100	100	100	100	99	100	79	100
53	100	100	27	100	0	100	8	100	22	100
54	100	100	100	100	100	100	100	100	49	100
55	100	100	100	100	100	100	100	100	100	100
56	100	100	28	100	0	100	0	1.00	0	100
57	100	100	100	100	100	100	5	100	84	1.00
58	100	100	100	100	100	100	100	100	1.00	100
59	100	100	100	100	100	100	6	100	100	100
60	100	100	100	100	100	100	100	100	100	100
61	100	100	100	100	100	100	39	100	73	100
62	100	100	100	100	100	100	100	100	83	1.00
63	100	100	100	100	100	100	71	100	48	100
64	100	100	100	100	100	100	70	100	57	100
65	100	100	1.00	100	100	100	100	100	100	100
66	100	100	100	100	100	100	14	100	12	100
67	100	100	100	100	100	1.00	0	100	100	100
68	100	100	91	1.00	100	100	16	100	10	100
69	100	100	1.00	100	100	1.00	32	100	61	100
70	100	100	100	100	100	100	100	100	100	100
71	100	1.00	100	1.00	100	100	100	100	100	100
72	100	100	27	100	100	100	0	100	76	100
73	100	100	5	100	51	12	0	60	68	100
74	100	100	100	100	0	100	0	31	84	100
75	100	100	100	100	0	100	0	100	100	100
76	100	1.00	0	100	0	100	0	100	29	100
77	100	100	100	100	100	100	20	100	100	100
Mean	100	100	82	100	80	97	44	96	71	100

2.2.9 Estimation of the Present Success Percentage (Without project)

The success percentage of the existing cultivated land within the project area will be estimated on the following procedures:

- (a) By conducting local interviews by experts including farm management experts and agro-economists, tank-wise success percentages under the situation of Post-Polgolla have been determined at 87.8%;
- (b) Assuming that the infrastructures of the existing entire cultivated land are improved under such a situation as no river discharge control available for Amban Ganga after completion of the Polgolla-Bowatenna Complex and the proposed cropping patterns and the irrigation requirements are applied, the past 28-average value of the success percentage of the yield area to the entire cultivated area including the area, which has already been proposed under the situation of Post-Polgolla, (new lands in System G and a programme for increasing sugar production at Kantalai), has been estimated at 82.9%, while that in 1977 at 86.4% under the situation of the recent Post-Polgolla; and
- (c) Assuming that the success percentage varies proportionally as a result of (1) and (2), the success percentage under the situation of leaving the present infrastructures as they are without any improvements will be estimated as follows:

Success Percentage = 
$$\frac{87.8 \times 82.9}{86.4}$$
 = 84.2

Consequently, the present success percentage will be assumed to be 84.2%.

Success Percentage and Irrigable Area without and with Project Table 6-2-40

With Project 94,100 ac (9,500 ") 153,800 ac 4,800 " 10,000 " 22,400 " 5,400 " 6,600 " 90.5% Post-Polgolla (after improvement of inflastructures) Without Project (Post-Polgolla) (9,500 " (1,000 " 94,100 ac 119,400 ac 10,000 " 4,800 " 82.9% ı 94,100 ac 98,900 ac Existing 4,800 " 84.2% ı & D<sub>2</sub> Sugar Co. Success Percentage A/C Existing  $\mathbf{D}_1$  $^{\mathrm{D}}_{1}$ New Land G Ç Total = Ξ Ξ Irrigable Area

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## 2.2.10 Design Discharge of Irrigation Facilities

Water requirements being estimated on the basis of the proposed cropping patterns is 1,770 ac.ft/month per 1,000 ac under A and 1,312 ac.ft/month under B, culminating to a peak in July. Cropping rates under A and B are 80% and 20%, respectively. No significant effective rainfall is to be hoped for in July. Design water requirements have been calculated as follows:

For each 1,000 ac:

 $1,770 \times 0.8 + 1,312 \times 0.2 = 1,678.0$  ac.ft/month or 54.1 ac.ft/day Which can be converted to:

 $0.0273 \text{ ft}^3/\text{sec/ac} = 36.6 \text{ ac/cusec} \text{ or } 1.91 \text{ 1/sec/ha}$ 

In determining a design crossing to meet the above water requirement, Sri Lankan standard design duties which are given below have been taken into consideration:

		Commanded area	Design duty
(1)	Main canals	below 1,000 ac	40 ac/cusec
	•	1,000 - 5,000 ac	50 "
		above 5,000 ac	60 "
(2)	Branch canals		40 "
(3)	Distributaries		35 "
(4)	Field canals		30 "

As it has been considered somewhat uneconomical to design cross sections of all the canals on the basis of the calculated duty of 36.6 ac/cusec and as the existing canals are regulated by the above standards, it has been decided to adop the following:

- (1) Main and Branch canals .... 40 ac/cusec
- (2) Distributaries .... 35

## III: HYDRAULIC AND STRUCTURAL DESIGN

# 3.1 Irrigation Plan

On the basis of the irrigation plan for both the existing and the new lands as specified in the Main Report, the existing main and branch canals will be imporved and new main and branch canals constructed as follows:

(1)	Improvement of Existing Canals	length (miles)
	System D1	10.18
	System D2	20.80
		30.98
(2)	Construction of New Canals	
	System D1	36.18
	" D2	32.84
	" A/D	21.25
		90.27
(3)	Erahela-Minneriya Yoda Ela	13.5
	(6 - 19.5 miles)	

## New Kalu Ganga Tank

1. Catchment area 6,500 acs (10.2 sq.mis)

2. Capacity 21,600 ac-ft (26.7 milion m3)

3. F.W.L. 190 ft M.S.L.

4. H.F.L. 193.5 ft M.S.L.

5. Area at F.S.L. 1,700 ac

6. Bund

Lenght 2,41 miles (3.88 km)

Top Level 200 ft M.S.L.

Top Width 20 ft

Hirht 2 ft- - -45 ft

Slopes U/S 1 on 2.5 D/S 1 on 2.0

7. Spillway Clear overfall 160 ft

8. Sluice Tower Sluice

## 3.1.1 Irrigation Canals

#### (1) General

The irrigation canals for the purpose of suppling the irrigation water to the proposed irrigation area are consists of newly constructed canals and existing irrigation canals improved to increase the flow capacities. The existing canals to be improved are the Main canal and the Branch canal No. 1 in the Dl irrigation system and the Dl-Main canal, the Dl-North canal and Dl-East canal in the D2 irrigation system.

#### (2) Type of Canal

In principal, irrigation canals are designed as un-lined-earthen canals. However, in the case of improvement existing canals of the Main canal and the Branch canal No.1 in the system D1, they are designed as thin concrete lining in order that the flow capacities of the canals can be increase without large scale widening and the related structures of the canals are able to be used without reconstruction or repairing.

### (3) Design Discharge and Canal Net Work

The design discharge assigned with a command area, the standardized canal types classified by the said discharges, and the diverting discharges of turnouts are summarized in Figs.  $6.3.1\ ilde{to}\ 6.3.3$  and Tables 6.3.4 to 6.3.9.

### (4) Canal Section

The cross section of canal sould be such as carry the required capacity. As a rule, canals for the Project consists of trapezoidal earth canals. The sections of canals to be newly constructed are determined based mainly upon the design standards in the Mahaweli Ganga Irrigation and Hydro-power Survey carried out by UNDP/FAO.

Fig. 6.3.4 shows the relationship of canal sections to discharges for earthen canals and it is used for the canal design.

## a) Velocitiy and Water Depth

## Un-lined canal

Velocities and ratios of bed width to water depth usually range from 1.0 to 3.5 fps. and from 2:1 to 8:1, respectively, depending upon discharges.

For this Project, the permissible velocity is determined 2.7 fps. and the water depth is designed less than 5 ft.

## Thin-concrete lined canal

Lined canals permit higher velocities than un-lined canals. The maximum velocity for the thin-concrete lined canals is determined 5 fps.

#### b) Freeboard

Freeboard in a canal will normally be governed by considerations of the canal size and locaiton, velocity, flooding, wind action, etc. For this Project, the minimum freeboard for the Project is decided as follows.

### i) Earth canal

	$Q \ge 1$	,500	c.f.s	•	3	ft.	0	in.
	$Q \ge 1$	,000	c.f.s	•	2	ft.	6	ins.
	Q <u>&gt;</u>	500	c.f.s	•	2	ft.	0	in.
	Q >	100	c.f.s	•	1	ft.	6	ins
	Q ≥	10	c.f.s	•	1	ft.	3	ins
	Q∑	2	c.f,s		1	ft.	0	in.
ii)	0pen	f1un	ne and	aqueduct	2	ft.	0	in.

# iii) Concrete lined canal

In the lined canals these are the existing canals improved for the Project, the berms of 1/2D+2 ft. width are used at the top of lining to be at about 1 ft. above F.S.L. and the freeboard above the top of the lining is determined as same as earth canals.

### c) Side Slope

The side slopes of canal depend upon the characteristics of the materials in which it is constructed and height of embankment. For the Project, inside slopes of 1:1.5 (vertical to horizontal) and 1:1.0 are determined for the un-lined canals and for the thin-concrete lined canals, respectively, under ordinary conditions.

## d) Bank Top-width and Berm

Since there are no major highways in this area, the canal banks as operation and maitenance roads will also serve as useful communication link for the development of the area. The banks have been classified three types according to their traffic density and road requirements.

On the opposite bank, 4 ft. wide bank has been provided. The typical widths of banks/roadways are as follow.

Type of bank/raod	I	II	III
Road class	11	III	IV
Width of bank (ft)	30	16	12
Width of gravel pavement (ft)	8	8	8
Thickness of gravel (ins)	6	6	6
Width of opposite bank (ft)	4	4	4

Where the berm is to be needed, half the water depth plus two  $\tilde{r}$  feet (0.5d + 2 ft) wide berm has been provided.

# (5) Hydraulic Formula

For the purpose of the hydraulic discharge studies, the Manning formula has been adopted for all canal designs. The formula is as follows.

$$V = \frac{1.486}{n} R^{2/3} S^{1/2}$$

Q = A V

where,

V = velocity of water in fps,

S = slope of energy gradient in feet per foot,

R = hydraulic radius in feet,

n = coefficient of roughness

Q = discharge of canal in c.f.s, and

A = cross-sectional area of water in sq.ft.

The meaning coefficient of roughness 'n' used in the design is as follows.

	n value
Concrete lining	0.015
Concrete block lining	0.017
Earth canal	0.0225
Existing earth canal	0.030 - 0.040
Natural stream	0.040

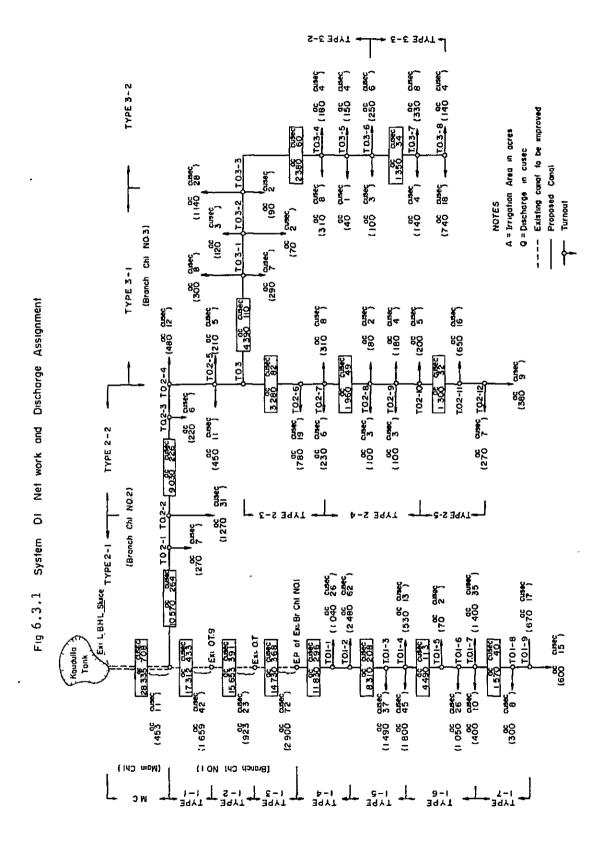
Slope of energy gradient of the canals may range from 0.0002 (1/5,000) to 0.00045 (1/2,200) taking into account topographical conditions and proper velocities.

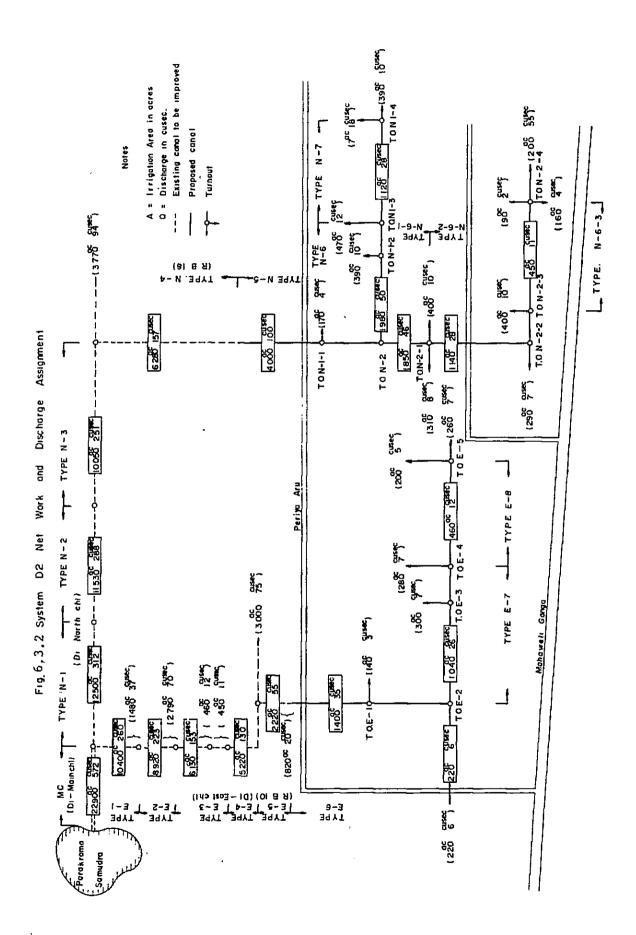
## (6) Standard Cross Section

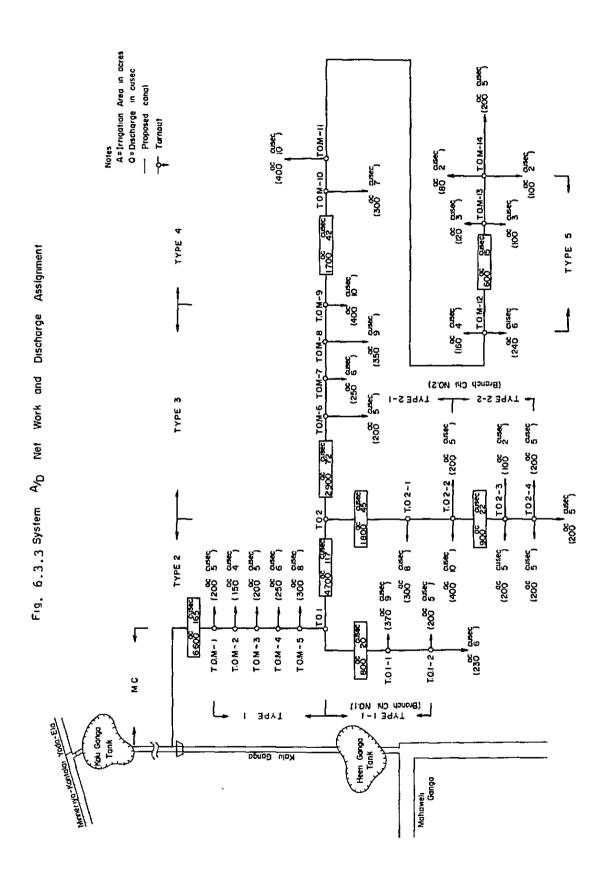
As for the standard cross section, 34 types are designed for the main and branch canals, according to the sectional discharges and the distances' between the turnouts. The numbers of proposed standard cross sections in the three irrigation systems are as follows.

System D1	improvement canal	4 types
	new canal	5 types
System D2	improvement canal	10 types.
	new canal	10 types
System A/D	new canal	5 types

The hydraulic calcultations for determining the standardized cross sections are tabulated in Tables 6.3.10 to 6.3.12. The standard canal sections are illustrated in Figs. 6.3.5 tp 6.3.7.







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Table 6.3.1 Existing Channel Data in System D-1

Chl.Name	Reach	Command Area	Disch.	Grad.	Bed Width	FSD	Prop. Type
	Ml- Ch	Acs	cusec	%	ft	ft	
Main Chl.	0 4 - 2.5	16,000	266.7	0.3	20	4.4	M.C.
	0		-			· · · · · · · · · · · · · · · · · · ·	
Branch Chl.No.1	1 - 36	5,482	137.3	0.3	14	3.6	1-1
	1 - 50	4,427	110.7	0.3	13	3.28	
		3,823	95.6	0.3	12	3.16	
	2 - 27	3,257	81.4	0.3	11	3.03	1-2
	3 - 47	2,900	72.5	0.4	14	2.5	
	4 - 30	883	23.9	0.4	14	2.3	1-3
	4 - 41	-					<del>+</del> -/
	6 - 6.7	756	18,9	0.4	14	2.1	·

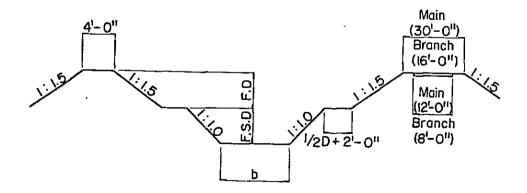


Table 6.3.2 Existing Channel Data in System D-2

Chl.Name	Reach	Command Area	Disch.	Grad.	Bed Width	FSD	Prop. Type
	M1-Ch	Acs	сивес	‰	Ĩt	ft	
D <sub>1</sub> -Main	0 3 - 10	17,500	350.0	0.200	45.0	4.50	M.C.
D <sub>1</sub> -North	0 1 - 0	8,500	175.0	0.252	29.0	3.15	
		8,110	167.0	0.237	28.0	3.07	N-1
	1 - 45	7,770	160.0	0.238	27.6	3.05	
	2 - 28	7,530	155.0	0.238	27.4	3.05	
	3 <b>-</b> 0	7,530	155.0	0.240	26.6	3.00	N-2
	,	7,290	150.0	0.234	26.0	2.97	
	6 <b>-</b> 0 6 <b>-</b> 28	6,050	124.6	0.245	23.4	2.80	N-3
D <sub>1</sub> -North R.B.18	0 4 - 26	2,280	47.0	0.290	13.8	2.13	N-4
D <sub>1</sub> -East	0	9,000	184.0	0.250	30.0	3 <b>.</b> 20	
	1 - 0 2 - 0	7,520	153.7	0.240	30.0	2.99	E-1
	2 <b>-</b> 0 3 <b>-</b> 0	7.070	144.5	0.260	25.5	2.94	E-2
		4,730	96.7	0.260	20.0	2.65	E-3
•	5 - 0 5 - 15	3,820	78 <b>.</b> 0	0.263	18.0	2.45	E-4
D <sub>1</sub> -East R.B.10	0 1 - 15	<b>820</b>	16.7	0.347			E-5

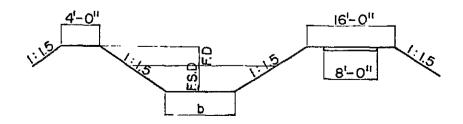


Table 6.3.3 Sectional Discharge and Type & Length of Canal for System D-1 (1)

Canal		Canal Canal		Turnout			
Type	A	Q	L	T.O.	A	_ q	
Main*	28,335	708	4.05				
	,			Exi.T.O.	453	11	
1-1*	17,312	433	1.94	Exi.Dv. (D.S.)	10,570	264	
1 1	11,5,712	477	<b>1</b>	Exi.T.O.	1,055	27	
1 2 0 4	35 652	707	1 OC	-do-	604	15	
1-2*	15,653	391	1.95	-do-	. 566	14	
]				_do-	357	9	
1-3* `	14,730	368	2.24	-do-	2,017	50	
		l.		-do-	127	3	
	İ			-do-	756	19	
1-4	11,830	296	1.50	T.O. 1-1	1,040	26	
	. ]			T.O. 1-2	2,480	62	
1-5	8,310	208	1.75	T.O. 1-3		37	
ļ <b>,</b>	ļ		  -  -	T.O. 1-9	1,490 R 1,800	45	
				1.0. 1-4	ь 530	13	
1-6	4,490	113	2.25				
]				T.O. 1-5	70	2	
				T.O. 1-6	1,050	26	
[		į		T.O. 1-7	L 1,400 R 400	35 10	
1-7	1,570	40	1.25				
				T.O. 1-8	300	8	
	,			T.O. 1-9 (D.S.)	670	17	
				(===•/	600	15	
		ļ					

Notes; A=commanding are in acres
Q=discharge of canal in cusec.
L=canal length in miles
T.O.=turnout
q=offtake discharge in cusec.
\*=existing canal to be improved
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Table 6.3.4 Sectional Discharge and Type & Length of Canal for System D-1 (2)

Canal	Canal				Turnout	
Туре	, A	Q	Ŀ	T.O.	A	q
2-1	10,570	264	3.25	T.O. 2-1	270	7
		205	0.05	T.O. 2-2	1,270	31
2-2	9,030	226	2.25	T.O. 2-3	220	6
	į			T.O. 2-4	. 480	12
				T.O. 2-5	R 450	11
	:				L 210	5
0.7	7 000	00	2 00	T.O. 3	4,390	110
2-3	3,280	82	2.00	(D.S.) T.O. 2-6	780	19
				T.O. 2-7	L 310	8
2-4	1,960	49	2,25	!	R 230	6
2 <b>-</b> 4	1,900	49	2,29	T.O. 2-8	R 100	3
					L 80	2
] 				T.O. 2-9	L 180	4
		,			R 100	3
2~5	1,300	32 32	2.25	T.0.2-10	200	5
(	1,500	ر عر	2.27	T.O.2-11	650	16
	.		· i	T.O.2-12 (D.S.)	270	7
				(1).5.)	380	9

Notes; A=commanding are in acres
Q=discharge of canal in cusec.
L=canal length in miles
T.O.=turnout

q=offtake discharge in cusec.

Table 6.3.5 Sectional Discharge and Type & Length of Canal for System D-1 (3)

Canal		Canal		Turnout			
Type	A	Q	L	T.O.	A	đ	
3-1	4,390	110	1.75	T.O. 3-1	L 300	8	
					R 290	7	
				T.O. 3-2	L 120	3	
					R · 70	2	
		l		T.O. 3-3	L 1,140	28	
7.0	0.700	60	7 05		R 90	2	
3-2	2,380	60	3.25	T.O. 3-4	R 310	8	
:					L 180	4	
				T.O. 3-5	L 150	4	
					R 40	1	
				T.O. 3-6	ь 250	6	
3-3	1,350	34	2 <b>.</b> 25		R 100	3	
	1,770	74	2.27	T.O. 3-7	ъ 330	8	
					R 140	4	
				T.O. 3-8 (D.S.)	140	4	
			: :	( ), ( )	740	18	
	٠						
Total			36.18		28,335	708	

Notes; A=commanding are in acres
Q=discharge of canal in cusec.
L=canal length in miles
T.O.=turnout
q=offtake discharge in cusec.

Table 6.3.6 Sectional Discharge and Type & Length of Canal for System D-2 (1)

Canal Canal			Turnout			
Type	A	Q	Ŀ	T.O.	A	<b>q</b>
M.C.*	22,900	572	<b>3.</b> 19	Exi.T.O.	10,400	260
N-1*	12,500	312	1.85	ļ	-	
N-2*	11,530	288	3.68	-do-	970	24
N-3*	10,050	251	1.01	-do-	1,480	37
N-4*	6,280	157	4.10	-do-	3,770	94
N-5	4,000	100	1.45	-do-	2,280	57
				T.O.N-1-1	170	4
N-6	1,980	50	1.70	T.O.N-2 (D.S.)	1,850	46
N-7	1,120	28	1.60	T.O.N-1-2	390	10
" '	2,220	20	1.00	T.O.N-1-3	470	12
				T.O.N-1-4 (D.S.)	730	18
				(5.5.)	390	10
N-6-1	1,850	46	0.95	T.O.N-2-1	L 400	10
	-				R 310	8
N-6-2	1,140	28	1.27	T.O.N-2-2	290	7
N-6-3	450	11	1.48	T.O.N-2-3	400	10
				T.O.N-2-4	160	4
				(D.S.)	90	2
					200	5

Notes; A=commanding are in acres
Q=discharge of canal in cusec.
L=canal length in miles

T.O.=turnout

q=offtake discharge in cusec.

Table 6.3.7 Sectional Discharge and Type & Length of Canal for System D-2 (2)

Canal	Canal			Turnout			
Type	A	Q	L	T.O.	A	q	
E-1*	10,400	260	1.00	Deri (II o	7 400	20	
E-2*	8,920	223	1.00	Exi.T.O.	1,480	37	
E-3*	6,130	153	2.00	-do-	2,790	70	
E-4*	5,220	130	1.28	-do-	910	23	
E-5*	2,220	55	1.28	-do-	3,000	75	
E-6*	1,400	35	1.50	-do-	820	20	
	_,,,		2.00	T.O. E-1	140	3	
E-7	1,040	26	1 50	T.O. E-2	220	6	
P= !	1,040	. 20	1.50	T.O. E-3	300	7	
	160	7.0	1 00	T.O. E-4	280	7	
E-8	460	12	1.00	T.O. E-5	200	5	
				(D.S.)	260	7	
,					<u>.</u>		
				:			
Total		_	32.84		22,900	572	

Notes; A=commanding are in acres
Q=discharge of canal in cusec.
L=canal length in miles
T.O.=turnout
q=offtake discharge in cusec.

Table 6.3.8 Sectional Discharge and Type & Length of Canal for System A/D (1)

Canal		Canal			Turnout	
Type	A	Q	L	T.O.	A	đ
1	6,600	165	6.80			
				T.O. M-1	200	5
				T.O. M-2	150	4
		-	•	T.O. M-3	200	5
				T.O. M-4	- 250	6
				T.O. M-5	300	8
2	4,700	117	0.75	T.O. 1	800	20
				T.O. 2	1,800	45
3	2,900	72	3.10	(D.S.) T.O. M-6	200	5
				T.O. M-7	250	6
				T.O. M-8	350	9
	7 700	42	1.75	T.O. M-9	400	10
4	1,700	42	1.10	T.O. M-10	300	7
]		i		T.O. M-11	400	10
				T.O. M-12	R 240	6
	600	<b>.</b>	2 75		L 160	4
5	800	15	2.35	T.O. M-13	L 120	3
					R 100	3
				T.O. M-14 (D.S.)	100 80 200	2 2 5

Notes; A=commanding are in acres

Q=discharge of canal in cusec.

L=canal length in miles

T.O.=turnout

q=offtake discharge in cusec.

\*=existing canal to be improved

Table 6.3.9 Sectional Discharge and Type & Length of Canal for System A/D (2)

Gama?		Canal	<u>.</u> .		Turnout	
Canal Type	A	Q	Ŀ	T.O.	A	q.
1-1	800	20	3 <b>.</b> 00	T.O. 1-1 T.O. 1-2 (D.S.)	370 200 230	9 56
2–1	1,800	45	1.00	T.O. 2-1	300	8 :
2–2	900	22	2.50	T.O. 2-2 T.O. 2-3	R 400 L 200 R 200	<b>1</b> 0 5 5
				T.O. 2-4	L 100 200	2
					200 200	5 5
Total			21.25		6,600	165

Notes ; A=commanding are inrac es

Q=discharge of canal in cusec.

L=canal length in miles

T.O.=turnout

q=offtake discharge in cusec.

Fig. 6.3.4 Discharge of Earthen Canals

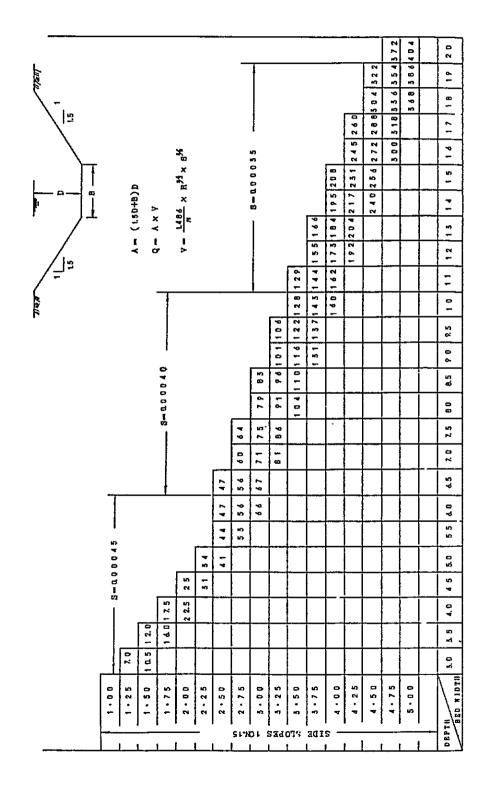
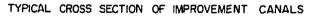
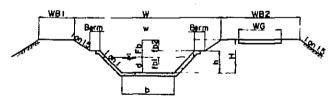


Table 6-3-10Hydraulic Calculation of Standard Cross Section of Irrigation Canal for System D1

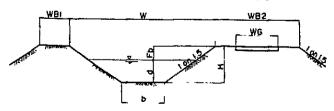
Mgm <sup>2</sup>   Cond   2933d   708   Document   200   1   0   6   08   3   3   586   37   204   263   2629   4   511   7   15   3   17   9   25   505   4.0   30   0   12   0   4   0   2   1   1   1   1   1   1   1   1   1														_	_	_		_	_	_			
Constitution   Cons			_	s	n	486/S	6 (f1)	z	d (11)	Þ/d	A (sq ft)	   P   (f1)	R (f1)	,   <sub>K</sub> 2/3	V (it/sec)	1	1						(mile)
A   173 2   433	Conat	29 335	708	0.0003	0 0 15	17159	20 0	10	6 08	3 3	1586	37 20	4263	5 629	4511	715	3.17	9 25	505	4.0	30 O	12 0	4 05
B   6257   406	Â	17312	433	gt .	"	11	140		55	25	1073	29.56	3629	2 361	4 052	435	2 50	80	41.0	ıt	16 0	8.0	
A   15653 39	۱. · ۱	16257	406	",	11		,"	,,,	5 33	26	103.3	29 O8	3.543	2 324	3 988	411	2 67	"	"	-	2	tı	194
B   15087   377	A	15653	391	4	и	. u	н	п	5 25	27	011	28 85	3.503	2.307	3 958	400	2 25	75	39 5	11			
A   4730  368   00004   1   19613   1   1   467   3   0   187   1927   21   3   2042   1744   307   375   2   33   7.0   380   1   1   1   1   1   1   1   1   1		15087	377	u	, "			,	5.08	28	96.93	28 37	3 416	2 268	3.892	377	2.42	"	41	,,	tt	"	195
C   2566   315		14730	368	0.0004	и	19613		"	467	30	87 19	27 21	3 204	2 174	4 307	375	2 33	7.0	38.0	и	*	Ħ	
1-4   11830   296   2000000   2022   12356   18.0   1 5   4.5   4 0   111 4   34.22   3.254   2   196   2   713   302   1.5   6 0   360   11   11   11.5   1	I-3 B	12713	318	11	и	ŧ	u	н	4 25	33	7756	26.02	2.981	2.071	4 104	318	2 75	.,	0	12		н	2 24
1-5   8310   208	c	12586	315	ч	,, 1			"			[ u	"	"	"	11	"	**	"	"	**	,, !	ls t	
1-6   4490   113   0.0004   113205   9 0   11   35   2 6   4988   21   62   2 307   1746   2 306   115   11   5 0   24 0   11   11   11   12   12   13   15   15   15   15   15   15   15	1-4	11830	296	000038	0.0225	12356	18.0	1.5	4.5	40	1114	34.22	3.254	2 196	2713	302	1,5	6 O	360	tł	4	ti	1.5
1-7 1570 40 20004 " "14010 5.0 " 2.5 2.0 21.88 14 01 1 561 1 346 1 885 41 1.25 3 75 16 25 " " " 1.2 2-1 10570 264 20003 " 12358 16.0 " 45 3 6 102.4 32 22 3.177 2 161 2 670 273 1 5 6.0 340 " " " 3.2 2-2 9030 226 " " " 15 0 " 4.25 3 5 90.84 30.32 2.996 2 078 2 568 2 33 " 5 75 32 25 " " " 2.2 2-3 3280 82 20004 " 1.3209 7 0 " 3 25 2.2 3859 18.72 2 062 1.620 2 140 83 1 25 4 5 205 " 12.0 " 2 0 2 2 4 1960 49 " " " 65 " 2 75 2 4 2922 16 42 1 780 1 469 1.940 57 " 4 0 185 " " 2 2 2 2 2 5 1 300 32 2 2 2 3 1 1 0 1 5 5.0 23 5 " 160 0 " 1 7 2 2 2 2 3 1 4 390 1 10 2 2 2 3 1 4 390 1 10 20004 " 1.3209 8 5 " 3 5 2 4 48.13 21 12 2 2 79 1 732 2 2 8 7 1 1 0 1 5 5.0 23 5 " 160 0 " 17 7 1 2 6 1 1 4 3 1 2 2 2 7 1 1 0 1 5 5.0 23 5 " 160 0 " 17 7 1 2 6 1 1 4 3 1 2 2 2 7 1 1 0 1 5 5.0 23 5 " 160 0 " 17 7 1 2 6 1 1 4 3 1 2 2 2 7 1 1 0 1 5 5.0 23 5 " 160 0 " 17 7 1 2 6 1 1 4 3 1 2 2 2 7 1 1 0 1 5 5.0 23 5 " 160 0 " 17 7 1 2 6 1 1 4 3 1 2 2 2 7 1 1 0 1 5 5.0 23 5 " 160 0 " 17 7 1 2 6 1 1 4 3 1 2 2 2 7 1 1 0 1 5 5.0 23 5 " 160 0 " 17 7 1 2 6 1 1 4 3 1 2 2 2 7 1 1 0 1 5 5.0 23 5 " 160 0 " 17 7 1 2 6 1 1 4 3 1 2 2 2 7 1 1 0 1 5 5.0 23 5 " 160 0 " 17 7 1 2 6 1 1 4 3 1 2 2 2 7 1 1 0 1 5 5.0 23 5 " 160 0 " 17 7 1 2 6 1 1 4 3 1 2 2 2 7 1 1 0 1 5 5.0 23 5 " 160 0 " 17 7 1 2 6 1 1 4 3 1 2 2 2 7 1 1 2 2 2 7 1 1 0 1 5 5 5.0 23 5 " 160 0 " 17 7 1 2 6 1 1 4 3 1 2 2 2 7 1 1 2 6 1 1 4 3 1 2 2 2 7 1 1 2 6 1 1 4 3 1 2 2 2 7 1 1 2 2 2 7 1 1 2 6 1 1 4 3 1 2 2 2 7 1 1 2 6 1 1 4 3 1 2 2 2 7 1 1 2 2 2 7 1 1 2 6 1 1 4 3 1 2 2 2 7 1 1 2 6 1 1 4 3 1 2 2 2 7 1 1 2 2 2 7 1 1 2 6 1 1 4 3 1 2 2 2 7 1 1 2 6 1 1 4 3 1 2 2 2 7 1 1 2 2 7 1 1 2 2 2 7 1 1 2 2 2 7 1 1 2 2 2 7 1 1 2 2 2 7 1 1 2 2 2 7	1-5	63/0	208	11		,,	15 0	ĮĮ.	4.0	3.8	84.00	29 42	2 855	2.013	2 487	209	16	5 5	315	п		10	1.75
2-1 10570 264 20003	1-6	4490	113	0.0004	0	13209	90	4	35	26	4988	21 62	2 307	1 746	2.306	115	"	50	240	0	=	,,	2.25
2-2 9030 226 " " " 15 0 " 4.25 3 5 908430.32 2.996 2078 2 568 2 3 3 " 5 75 3 2 2 5 " " " 2.2 2-3 3280 82 00004 " 1.3209 7 0 " 3 2 5 2 2 3859 18.72 2062 1.620 2 140 8 3 1 2 5 4 5 20 5 " 12.0 " 2 0 2-4 1960 49 " " " 65 " 2 75 2 4 29.22 16 42 1 780 1 469 1.940 5 7 " 4 0 18 5 " " 2 2 2-5 1300 32 00004 " 14010 4 5 " 2 2 5 2.0 1772 12 61 1 405 1.254 1 757 3 1 " 3 5 15 0 " " " 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1-7	1570	40	000048	"	14010	5.0	"	2.5	2.0	21.88	14 ()	1 561	1 346	885	41	1.25	3 75	16 25	11	"	41	1.25
2-3 3260 82 00004 11 13209 7 0 11 3 25 2.2 385918.72 2062 1.6202 140 83 1 25 4 5 205 11 12.0 11 2 0  2-4 1960 49 11 11 11 65 11 2 75 2 4 2922 16 42 1 780 1 469 1.940 5 7 11 4 0 185 11 11 11 2 2  2-5 1300 32 00004 11 14010 4 5 11 2 25 2.0 1772 12 61 1 405 1.254 1 757 31 11 3 5 150 11 11 11 11 11 11 11 11 11 11 11 11 11	2-1	10570	264	0.00035	ь	2356	16.0	н	45	36	102.4	32 22	3.177	2 161	2 670	273	1.5	6.0	340	"		,,	3.25
2-4 1960 49 " " " 65 " 275 24 29221642   780   469   1.940 57 " 40 185 " " " 22 2-5   1300   32   00004 "   14010 45 "   225   2.0   17721261   405   1.254   757   31 "   3 5   150 " " " " " " "   160 "   17 3-1   4390   110   00004 "   13209   85 "   35   24   48.1321   12   2279   1732   287   110   15   5.0   235 "   160 "   17	2-2	9030	226	4	4	,,	15 0	"	4.25	35	9084	30.32	2.996	2 078	2 568	233	"	5 75	32 25	11		и	2.25
2-5   1300   32   00004	2-3	3260	82	0.0004	et	1.3209	7.0	"	3 25	2.2	3859	18.72	2.062	1.620	2 140	83	1 25	45	205	;t	12.0	ıŧ	2 00
3-1 4390 110 00004 " 13209 85 " 35 2 4 48.1321 12 2 2 7 9 1 7 3 2 2 2 8 7 1 1 0 1 5 5.0 2 3 5 " 16 0 " 17	2-4	1960	49	"	Ц	ы	6 5		2 75	2 4	2922	16 42	1 780	I <b>46</b> 9	1.940	57	"	40	18.5	a a	"	11	2 25
7 2 7 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	2-5	1 300	32	0.00045	н	4010	45	"	2 25	2.0	1772	12 61	405	1.254	1 757	31	и	3 5	150		"	н	"
3-2 2390 60 # # # 70 # 275 25 305916921 9091 4941 961 501 254 0 190 # 120 # 22	3-1	4390	110	0.0004	"	1.3209	8 5	н	3 5	2 4	48.13	2! 12	2 2 7 9	ı 732	2 287	110	15	5.0	235	"	16 0	41	1 75
120 13 20 132 132 132 132 132 132 132 132 132 132	3-2	2390	60	#	"	"	70	"	2 75	25	30.59	1692	1 809	1.484	ı 961	60	1.25	4.D	190	11	12.0	и	3 25
3-3   350 34   200043   1   14010 5 0   1   2.25   2.2   18.94   3.11   437   273   784   3.4   1   3.5   15.5   1   1   1   2.2	3-3	1 350	34	000045	16	14010	5 0	61	2.25	2.2	18.84	13.11	I 437	1 273	1 784	34		3.5	15.5	μ.	"	11	2.25

X Existing concils to be improved





TYPICAL CROSS SECTION OF NEW CANALS



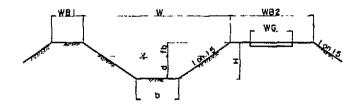
Con	ıl.	fbl	fb2	h	W	Berm
Тур	e	(11)	(fi)	(†1)	(11)	<b>{f1}</b>
Maii Con		1 17	20	7 25	34 5	50
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ľ.,	8	1 17		и 	H	ti
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	٠.	0.92		"		"
	Α	0.83	"	5 5	25 0	4 25
I-3	В	ı 25	и	, #	64	n
	c	u	11	11	11	IJ

Table6-3-11 Hydroulic Calculation of Standard Cross Section for Irrigation Conal for System D2

N-2   1530   288													_	<del></del> -		_			_				
Coval   223   3   2   2   2   2   2   2   2				s	n	48615		Z	d (ft)	Þ/d	A (sq fi)	P (ft)	R (ft)	R <sup>2</sup> /3	V (ft/sed								
N-2   11530   288		22900	572	200020	0.0225	09340	45	15	475	95	2476	62 13	3 985	2514	2 348	581	2 0	6 75	65.25	40	160	80	3 19
N-3 1000 251	N-1	1250d	312	000025	"	E4401	30	u	40	7.5	1440	4442	3 242	2 190	2 287	329	15	5.5	46.5	1)		u	1 85
N-4 6280 157 000000	N-2	11530	288		, , , ,,	u	27	Ħ	41	68	1320	41 42	3 (87	2 166	2 261	298	*	ti	435	u	15	14	3 68
E-1 10400 260 pooces	N-3	10050	251	Ħ	ц	"	26		3 75	69	1186	39.52	3 001	2 080	2 173	258	11	5 25	41 75		#	п	101
E-2 8920 223 " " " 26 " " 7 4 1094 38 62 2832 2002 2090 229 " " 41 0 " " " " 1	N-4	6280	157	0.00030		1 1439	16	, ,,	3.5	4.6	7438	28 62	2 599	1.890	2 162	161	11	50	31.0		<u> </u>	()	4 10
E-3 6130 153 000028	E-I	10400	260	D.00025	"	0443	30	-	, ,	8.6	123.4	4262	2.895	2 031	2 121	262	"	"	45.0	н	- 41	11	10
E-4 5220 130 20002	E-2	8920	223	u	"	. "	26	"	"	74	1094	38 62	2.632	2 002	2.090	229	"	11	410	н	į II	п	"
X	E-3	6130	153	000036	u	10649	22	н	30	73	7950	32 82	2 422	1 804	1921	153	"	45	35.5	4	n	q	20
N-5 4000 100 00040	E-4	5220	130	000029		10711	19	H	"	63	70.50	29 62	2 364	1.775	1 901	134	H.		32.5	"	1)	u	1.28
N-6 1980 50 " " " 6 " 275 22 2784 1592 1.749 1 452 1 9 18 53 1 25 4 0 18.0 " 12.0 " 1 1	E-5	2220	55	000034	"	2303	9	11	2 5	36	3188	18 01	1 769	1 463	1 800	57	1.25	1.25	20.25	A	12.0	,,	. "
N-7   120   28   28   28   28   28   28   28	N-5	4000	100	000040	н	1.3209	H	11	3 25	2 77	45.09	20 72	2 177	1 679	2.218	100	1.5	4 75	23.25	н	16 0	či	1.45
N6-1 1850 46 H H G H 2.5 2 4 2438 15 01 1623 1381 1935 47 H 3.75 17 25 H H H C	N-6	1980	50	"		; . H	6	<b>.</b> .	2 75	22	2784	15 92	1.749	1 452	1918	53	1 25	40	18.0		12.0	11	1.70
N6-2   1   40   28	N-7	1 120	28	0.000	"	14010	45	"	2 25	20	1772	1261	1 405	1 254	1 757	31	н	35	150	13		U	1 60
N6-3 450 11 " " " 35 " 15 23 8625 890809682097871 371 12 " 275 1175 " " " " " 15 16 16 16 16 16 16 16 16 16 16 16 16 16	N6-1	1850	46	"	"	,	6	н	2.5	24	2438	1501	623	1 381	1 935	47	13	3.75	17 25			11	0.95
E-6 1400 35 " " 45 " 25 18 2063 351 526 326 1857 38 " 3.75 15.75 " " " 1	N6-2	1 140	28	"	"	"	45		2 25	20	1772	1261	1 405	254	1 757	31	"	35	150	"	11	H	1 27
	NG-3	450	11	"	-	"	35	"	15	23	8625	8908	09662	0.9787	1 371	12	"	2 75	1175	"	"	"	1.48
E-7 1040 26 " " " 40 " 2.25 " 165512111.37012341728 29 " 35 140 " " " "	E-6	1400	35		"		45	"	25	18	20.63	1351	1 526	1 326	1 857	38	"	3.75	15.75	"	- 41	, n.	15
┠╴╴╿╶╿ <del>┈╎╏┈┼╸┈╎╸┈┤╸┈┼┈┼┈┼┈┈┼┈┈┼┈┈┼┈┈┼┈╸┼┈╸┼┈╸┼┈╸┼</del> ╌ <del>╌┼┈</del> ┼╌╌┼╌┈┼╌┈╅	E-7	1040	26	н	4	н	40	"	2.25		16.59	12 11	1.370	1 234	728	29	"	35	140	"	"	"	15
E-8 460 12 " " " 35 " 15 23 8625 89080968209787 1.371 12 " 2.75 11 75 " " " "	E-8	460	15		"	"	35	н	15	23	8625	8.908	09682	0.9787	1.371	12		2.75	11 75	"	ır	<del></del>	10
	[								i	)		<u> </u>		-				;			<del> </del>	i	

 $\boldsymbol{X}$  Existing canals to be improved

TYPICAL CANAL SECTION



A/D
System
for
Canal
Irrigation
for
Section
Cross
Standard
ō
Catculation
Hydraulic
Table 6-3-12

		IO		ιΩ	Ω			
_1 <b>£</b>	6.8	0.75	3.1	1.75	2.35	3.0	1.0	2.5
₩ œ (£†)	8.0	ш	Ξ	=	=	=	#	=
WB2 (ft)	16.0	=	12.0	=	=	=	21	=
WBI (ft)	4.0	11	. 11	=	=	=	=	=
× (±;	5.25 28.75	24.5	2025	16.75	12.5	3.25 13.75	17.25	13.75
H (#)	5.25	5.0	4.25 2025	3.75	3.0	3.25	3.75	3.25
Fb (ft)	1.5	1	1.25	=	=	=	=	=
0c (c <b>fs</b> )	165	120	75	44	16	23	47	23
V (11/5ec)	2.356	2.324	2.073	1.911	1.486	1.625	1.935	1.625
R2/3	1.907	1.760	1.569	.5931.364   .911		1.2491.1601.625	- 1	1.160
R (#1)	2.634	2.334	1.965	1.593	9.8101.0931.061	1.249	1,623 .38	1.249
م ( <del>1</del>	26.52	22.12	18.32	14.51	9.810	14.00 11.21		11.21
A (sq.ft)	69.8426.52 2.634 1.907 2.356	51.6322.122.3341.7602.324	36.00 18.32 1.965 1.569 2.073	23.13 14.51	10.72	14.00	24.38 15.01	14,0011.21 1.2491.160 1.625
8%	3.5	2.7	2.5	2.2	2.0	=	2.4	2.0
д (#)	3.75	3.5	3.0	2.5	1.75	2.0	2.5	2.0
Z	1.5	=	=	=	=	=	=	=
ф (#)	13.0	9.5	7.5	5.5	3.5	4.0	6.0	0.4
1486 <sub>5</sub> 5	1,2356	13209	=	14010	=	=	Ξ	=
c	2022	3	=	=	=	=	=	=
ဟ	poposs 0,225   13.0	000040	=	000046	=	=	=	=
o (cfs)	165	- 1	72	42	ည	20	45	22
Ac (ac)	9	4 700	2 900	1 700	8	800	- 800	906
Canal	_	N	מו	4	ထ	<u>-</u>	2-1	2-2

TYPICAL CANAL SECTION

