

IRRI IRRIGATION
RECLAMATION
CONSULTANTS
TOKYO
JAPAN

SUBJECT			
COMPUTED	DATE	CHECKED	DATE

PROJECT
FILE NO.
PAGE OF PAGES

1.3. AREA DE DEMONSTRACAO DO POLDER ITOPAKIRIM

1959 Ave. 10th Area - (80.0 mm > R. > 5.0 mm) - E.R. I.E. - 75.0%
 BABY WIND IRRIGATION REQUIREMENT (Net m³/d) (/)

Date	Area - mm	S.R. mm	h mm	W.S. m³	Actual Net m³/d	Net m³/d
21	0.0	0.0	10.0			
22	12.0	9.6	10.0			
23	0.0	0.0	10.0			
24	0.0	0.0	10.0			
25	0.0	0.0	10.0			
total	12.0	9.6	50.0	20079	26772	.062
26	0.0	0.0	10.0			
27	0.0	0.0	10.0			
28	0.0	0.0	10.0			
29	19.0	14.4	10.0			
30	0.0	0.0	10.0			
31	0.0	0.0	10.0			
total	18.0	14.4	60.0	22663	30219	.058
TOTAL	30.0	24.0		42742	56990	

POND FIELD IRRIGATOR - RUN (Normal) (Normal) (7-7)									
Date	Time	Area	49.7 ha	(10.0 mm > 15.0 mm)	80.0 - 85.0	1.2 - 1.5	75.0	Area	Normal
		mm	mm	mm	mm	mm	mm	mm	mm
1	0.0	0.0	15.0						
2	0.0	0.0	15.0						
3	0.0	0.0	15.0						
4	0.0	0.0	15.0						
5	0.0	0.0	15.0						
total	0.0	0.0	75.0					37275	49700
6	4.1	6.5	15.0						
7	0.0	0.0	15.0						
8	0.0	0.0	15.0						
9	0.6	0.0	15.0						
10	0.0	0.0	15.0						
total	9.7	6.5	75.0					34015	45393
11	0.0	0.0	15.0						
12	21.3	25.0	15.0						
13	17.6	6.1	15.0						
14	0.0	0.0	15.0						
15	0.0	0.0	15.0						
total	38.9	31.1	75.0					21818	29031
16	0.0	0.0	15.0						
17	0.0	0.0	15.0						
18	0.0	0.0	15.0						
19	7.7	6.2	15.0						
20	0.9	0.0	15.0						
total	8.6	6.2	75.0					34194	45591
21	3	0.0	15.0						
22	9	0.0	15.0						
23	4.8	0.0	15.0						
24	0.0	0.0	15.0						
25	0.0	0.0	15.0						
total	5.9	0.0	75.0					37275	49700
26	27.8	19.0	15.0						
27	2.9	0.0	15.0						
28	0.0	0.0	15.0						
29	0.0	0.0	15.0						
30	4	0.0	15.0						
total	27.1	19.0	75.0					27832	37109
total	90.0	62.8						192128	256584

Date	h	mm	mm	mm	mm	Avg. No. Sows/Total
1	0.0	17.0	0.0	0.0	0.0	0.0
2	0.0	17.0	0.0	0.0	0.0	0.0
3	0.0	17.0	0.0	0.0	0.0	0.0
4	0.0	17.0	0.0	0.0	0.0	0.0
5	0.0	17.0	0.0	0.0	0.0	0.0
total	0.0	85.0	0.0	0.0	0.0	56327
6	0.0	17.0	0.0	0.0	0.0	0.0
7	0.0	17.0	0.0	0.0	0.0	0.0
8	0.0	17.0	0.0	0.0	0.0	0.0
9	0.0	17.0	0.0	0.0	0.0	0.0
10	0.0	17.0	0.0	0.0	0.0	0.0
total	0.0	135.0	0.0	0.0	0.0	50881
11	0.0	17.0	0.0	0.0	0.0	0.0
12	0.0	17.0	0.0	0.0	0.0	0.0
13	0.0	17.0	0.0	0.0	0.0	0.0
14	0.0	17.0	0.0	0.0	0.0	0.0
15	0.0	17.0	0.0	0.0	0.0	0.0
total	0.0	85.0	0.0	0.0	0.0	56327
16	0.0	17.0	0.0	0.0	0.0	0.0
17	0.0	17.0	0.0	0.0	0.0	0.0
18	1.6	17.0	0.0	0.0	0.0	0.0
19	0.0	17.0	0.0	0.0	0.0	0.0
20	0.0	17.0	0.0	0.0	0.0	0.0
total	1.6	85.0	0.0	0.0	0.0	56327
21	0.0	17.0	0.0	0.0	0.0	0.0
22	5.5	17.0	4.4	0.0	0.0	0.0
23	0.0	17.0	0.0	0.0	0.0	0.0
24	12.4	17.0	9.9	0.0	0.0	0.0
25	0.2	17.0	0.0	0.0	0.0	0.0
total	13.1	85.0	14.3	0.0	0.0	46851
26	0.0	17.0	0.0	0.0	0.0	0.0
27	0.0	17.0	0.0	0.0	0.0	0.0
28	0.0	17.0	0.0	0.0	0.0	0.0
29	0.0	17.0	0.0	0.0	0.0	0.0
30	0.0	17.0	0.0	0.0	0.0	0.0
31	0.0	17.0	0.0	0.0	0.0	0.0
total	0.0	102.0	0.0	0.0	0.0	67592
TOTAL	43.4	28.7	247655	330209	50691	67592
						130
						108
						108

1960 Acre ft. (Normal) (7.5)

Date	th	Len	(.80 mm > 2)	(.50 mm)	(.25 mm)	(.15 mm)	Agave	Normal	7.5
1	19.0	7.2	15.0	15.0	15.0	15.0	75.0	10	75.0
2	15.0	6.0	15.0	15.0	15.0	15.0	75.0	10	75.0
3	15.0	6.0	15.0	15.0	15.0	15.0	75.0	10	75.0
4	15.0	6.0	15.0	15.0	15.0	15.0	75.0	10	75.0
5	15.0	6.0	15.0	15.0	15.0	15.0	75.0	10	75.0
total	12.2	7.2	67.8	67.8	67.8	67.8	33697	44929	10
6	10.0	5.0	15.0	15.0	15.0	15.0	75.0	10	75.0
7	17.1	13.7	15.0	15.0	15.0	15.0	75.0	10	75.0
8	17.5	13.0	15.0	15.0	15.0	15.0	75.0	10	75.0
9	17.2	13.0	15.0	15.0	15.0	15.0	75.0	10	75.0
10	17.2	13.0	15.0	15.0	15.0	15.0	75.0	10	75.0
total	56.0	43.7	31.3	31.3	31.3	31.3	15556	20741	0.8
11	20.5	24.1	15.0	15.0	15.0	15.0	75.0	10	75.0
12	21.1	24.1	15.0	15.0	15.0	15.0	75.0	10	75.0
13	11.6	9.3	15.0	15.0	15.0	15.0	75.0	10	75.0
14	10.0	8.0	15.0	15.0	15.0	15.0	75.0	10	75.0
15	10.0	8.0	15.0	15.0	15.0	15.0	75.0	10	75.0
total	93.5	74.8	75.0	75.0	75.0	75.0	37275	49700	115
16	0.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
17	0.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
18	0.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
19	0.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
20	0.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
total	0.0	0.0	75.0	75.0	75.0	75.0	37275	49700	115
21	0.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
22	1.5	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
23	0.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
24	0.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
25	3.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
total	3.5	0.0	75.0	75.0	75.0	75.0	37275	49700	115
26	0.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
27	0.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
28	0.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
29	0.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
30	0.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
31	0.0	0.0	15.0	15.0	15.0	15.0	75.0	10	75.0
total	0.0	0.0	90.0	90.0	90.0	90.0	44730	59640	115
TOTAL	165.2	125.7	165632	165632	165632	165632	824843	1091115	

AREA=607 ha DIA PARA "C" DDURING=20 DIA
 =chuva e cultivo. efliciencia de irrigaçao
 de 15-16,550-75%

Normal (92) 10 mm de profundidade
 Asua necessario limbo N1,N2

Agua necesario
 normal

Date	Rain mm	100	150	200	250	300	350	400	450	500	550	600	650	700	750	800	850	900	950	1000	Necessary mm/ha	Total	Necessary mm/ha					
2	0.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	
3	9.5	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
5	0.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
6	17.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
7	0.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
8	13.5	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
9	17.5	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
10	15.5	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
total	70.7	61.0	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763	35763
2	6.9	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
12	4.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
13	0.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
14	35.1	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
15	9.5	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
total	55.0	41.5	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600	17600
2	0.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
17	0.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
18	0.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
19	20.3	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
20	4.7	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0	150.0
total	27.0	17.8	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197	10197
TOTAL	161.6	170.3	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	71568	

IRRIGATION REQUIREMENT (Required) (mm) (mm) (mm) (mm)
 (Normal) (0.75) (1.5) (2.0) (2.5)

1960 Area: 49.7 ha (80.0 mm > R > 5.0 mm) R = 5.0 mm (R = 75.0 mm)

Date	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm	mm
21	21.2	25.0	26.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
22	21.5	26.0	26.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
23	1.2	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
25	20.0	24.0	24.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
total	95.1	75.0	75.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0	50.0
26	11.0	10.4	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
27	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
29	13.7	11.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
total	20.7	21.4	21.4	18.6	18.6	18.6	18.6	18.6	18.6	18.6	18.6	18.6	18.6	18.6	18.6	18.6	18.6	18.6	18.6

121.0 95.4 92.44 92.44 12326 12326

ADDITIONAL IRRIGATION REQUIREMENT (Normal) (C / I)

Date	3 rd Iron	19.7 hr	(490.0 mm > R > 5.0 mm)	80 hr	75.0	Actual	Normal	total
	mm	mm	mm	mm	mm	mm	mm	mm
1	0.0	0.0	15.0					
2	0.0	0.0	15.0					
3	0.0	5.6	15.0					
4	0.0	0.0	15.0					
5	0.0	0.0	15.0					
total	7.0	5.6	75.0	69.1	34492	45989	10	
6	0.0	0.0	15.0					
7	0.0	0.0	15.0					
8	0.0	0.0	15.0					
9	0.0	0.0	15.0					
10	0.0	0.0	15.0					
total	0.0	0.0	75.0	75.0	37275	49700	115	
11	0.0	0.0	15.0					
12	6.1	4.9	15.0					
13	0.0	0.0	15.0					
14	1.1	0.0	15.0					
15	3.3	0.0	15.0					
total	7.5	4.9	75.0	70.1	34840	46453	103	
16	11.0	8.8	15.0					
17	0.0	0.0	15.0					
18	0.0	0.0	15.0					
19	0.0	0.0	15.0					
20	0.0	0.0	15.0					
total	11.0	8.8	75.0	66.2	32901	43869	102	
21	0.0	0.0	15.0					
22	0.0	0.0	15.0					
23	11.2	9.0	15.0					
24	0.0	0.0	15.0					
25	0.0	0.0	15.0					
total	11.2	9.0	75.0	66.0	32802	43736	101	
26	0.0	0.0	15.0					
27	0.0	0.0	15.0					
28	0.0	0.0	15.0					
29	0.0	0.0	15.0					
30	0.0	0.0	15.0					
31	0.0	0.0	15.0					
total	0.0	0.0	90.0	90.0	44730	59640	115	
TOTAL	36.7	28.3			217040	289337		

PADDY FIELD IRRIGATION REQUIREMENT (Normal) (7/60)

1960 Area 5 ch. 49.7 ha (180.0 mu) R > 5.0 mm I.E. = 75.0%
 I.R. mm P mm H mm A qua. m3 Necessario Total m3/5

Date	I.R. mm	P mm	H mm	A qua. m3	Necessario Total m3/5
1	14.5	11.6	15.0		
2	0.0	0.0	15.0		
3	0.0	0.0	15.0		
4	0.0	0.0	15.0		
5	0.0	0.0	15.0		
total	14.5	11.6	75.0	31510	42013 .097
6	0.0	0.0	15.0		
7	0.0	0.0	15.0		
8	0.0	0.0	15.0		
9	0.0	0.0	15.0		
10	7.0	5.6	15.0		
total	7.0	5.6	75.0	34492	45989 .106
11	3.2	0.0	15.0		
12	0.0	0.0	15.0		
13	0.0	0.0	15.0		
14	5.5	4.4	15.0		
15	18.0	14.4	15.0		
total	26.7	18.8	75.0	27931	37212 .036
16	5.7	4.6	15.0		
17	0.0	0.0	15.0		
18	0.0	0.0	15.0		
19	0.0	0.0	15.0		
20	28.0	22.4	15.0		
total	33.7	27.0	75.0	23056	31808 .074
21	49.0	39.2	15.0		
22	0.0	0.0	15.0		
23	0.0	0.0	15.0		
24	0.0	0.0	15.0		
25	0.0	0.0	15.0		
total	49.0	39.2	75.0	17793	23723 .055
26	0.0	0.0	15.0		
27	0.0	0.0	15.0		
28	0.0	0.0	15.0		
29	0.0	0.0	15.0		
30	0.0	0.0	15.0		
31	3.7	0.0	15.0		
total	3.7	0.0	90.0	44730	59640 .115
total	134.6	102.2		180312	240415

PAN IRRIGATION
RECLAMATION
CONSULTANTS
TOKYO
JAPAN

SUBJECT			
COMPUTED	DATE	CHECKED	DATE

PROJECT
FILE NO.
PAGE OF PAGES

1.4. AREA DE DEMONSTRACAO DO POLDER BOA VISTA

PADDY FIELD IRRIGATION REQUIREMENTS (Net of 75%) (75%)

1959 Area = 38.8 ha (180.0 m x 180.0 m) 80% = 31.04 ha 75% = 23.28 ha

Date	Area, mm	Depth, mm	mm	mm	mm	mm	mm	Avg. Net Irrigation Total, mm/s
21	14.5	11.6	10.0	10.0	10.0	10.0	10.0	
22	12.0	9.5	10.0	10.0	10.0	10.0	10.0	
23	0.0	0.0	10.0	10.0	10.0	10.0	10.0	
24	0.0	0.0	10.0	10.0	10.0	10.0	10.0	
25	0.0	0.0	10.0	10.0	10.0	10.0	10.0	
total	26.5	21.2	50.0	28.8	11174	14899		.03%
26	0.0	0.0	10.0	10.0	10.0	10.0	10.0	
27	0.0	0.0	10.0	10.0	10.0	10.0	10.0	
28	0.0	0.0	10.0	10.0	10.0	10.0	10.0	
29	10.0	14.4	10.0	10.0	10.0	10.0	10.0	
30	0.0	0.0	10.0	10.0	10.0	10.0	10.0	
31	0.0	0.0	10.0	10.0	10.0	10.0	10.0	
total	10.0	14.4	60.0	45.6	17693	23590		.04%
total	44.5	35.6			28867	38489		

1959 Aug

PADDO FIELD IRRIGATION RECORD (Nebraska)

(cm/h)

30.8 hd

5.3 mm

11

mm

(10.0 mm > R. > 5.0 mm) 80.0

75.0

Ag. Necessary

Total

m³ m³/h

29100

38800

.090

.092

17033

2271

.053

26694

35593

.092

29100

38800

.090

.067

21728

28971

.067

150234

200312

.067

1 15.0

2 15.0

3 15.0

4 15.0

5 15.0

total 75.0

6 15.0

7 15.0

8 15.0

9 15.0

10 15.0

total 150.0

11 15.0

12 15.0

13 15.0

14 15.0

15 15.0

total 150.0

16 15.0

17 15.0

18 15.0

19 15.0

20 15.0

total 150.0

21 15.0

22 15.0

23 15.0

24 15.0

25 15.0

total 150.0

26 15.0

27 15.0

28 15.0

29 15.0

30 15.0

total 150.0

total 90.2

62.9

1959 Avo 12 th Iron 38.8 ha (80.0 mm > R. > 5.0 mm) 80 1.3 175.0
 Paddy Field Irrigation Requirement (Normal) (C /)

Date	mm	D mm	H mm	I mm	Alc. %	Net mm	Total mm
1	0.0	0.0	17.0				
2	0.0	0.0	17.0				
3	0.0	0.0	17.0				
4	0.0	0.0	17.0				
5	0.0	0.0	17.0				
total	0.0	0.0	85.0			32980	43973
6	0.0	0.0	17.0				
7	0.0	0.0	17.0				
8	1.2	0.0	17.0				
9	18.0	14.4	17.0				
10	0.0	0.0	17.0				
total	19.2	14.4	70.6			32993	50524
11	4.5	0.0	17.0				
12	0.0	0.0	17.0				
13	0.0	0.0	17.0				
14	0.0	0.0	17.0				
15	0.0	0.0	17.0				
total	4.5	0.0	85.0			32980	43973
16	0.0	0.0	17.0				
17	0.0	0.0	17.0				
18	1.6	0.0	17.0				
19	0.0	0.0	17.0				
20	0.0	0.0	17.0				
total	1.6	0.0	85.0			32980	43973
21	0.0	0.0	17.0				
22	5.5	4.4	17.0				
23	0.0	0.0	17.0				
24	12.4	9.9	17.0				
25	2.2	0.0	17.0				
total	18.1	14.3	85.0	70.7		27432	36575
26	0.0	0.0	17.0				
27	0.0	0.0	17.0				
28	0.0	0.0	17.0				
29	0.0	0.0	17.0				
30	0.0	0.0	17.0				
31	0.0	0.0	17.0				
total	0.0	0.0	102.0	102.0		39576	52768
total	43.6	20.7	193340.7			257796	

TANDA FIELD IRRIGATION REQUIREMENT (Revised) (1/3)
(Newspaper)

1960 (Apr 21 to May 25) 39.8 ha (80.0 mm > R > 5.0 mm) * 80% = P.R. I.E. = 75.0%

Date	R. mm	P.R. mm	H mm	N mm	Avg. Necess. mm/s	Total mm
21	31.2	25.0	10.0	10.0	0	0.000
22	32.5	25.0	10.0	10.0	0	0.000
23	1.7	0.0	10.0	10.0	0	0.000
24	0.0	0.0	10.0	10.0	0	0.000
25	30.0	25.0	10.0	10.0	0	0.000
total	95.4	75.0	50.0	50.0	0	0.000
26	13.0	10.4	10.0	10.0	0	0.000
27	0.0	0.0	10.0	10.0	0	0.000
28	0.0	0.0	10.0	10.0	0	0.000
29	13.7	11.0	10.0	10.0	0	0.000
total	26.7	21.4	18.6	40.0	7217	9622
TOTAL	121.8	96.4			7217	9622

1960 Ave 4th Area = 39.8 ha (100.0 mm > R > 5.0 mm) 80% I.E. = 75.0%

Date	Area (ha)	D (mm)	H (mm)	A ₁₀ (mm)	A ₅₀ (mm)	A ₉₀ (mm)	Area (ha)	Area (ha)	Area (ha)
1	0.0	0.0	17.0						
2	0.0	0.0	17.0						
3	0.0	0.0	17.0						
4	0.0	0.0	17.0						
5	0.0	0.0	17.0						
total	0.0	0.0	85.0	3290	43973	102			
6	21.6	17.0	17.0						
7	0.0	17.0	17.0						
8	2.5	0.0	17.0						
9	0.0	0.0	17.0						
10	1.5	0.0	17.0						
total	35.0	21.6	63.4	24599	32799	1076			
11	4.0	0.0	17.0						
12	0.0	0.0	17.0						
13	0.0	0.0	17.0						
14	0.0	0.0	17.0						
15	0.0	0.0	17.0						
total	4.0	0.0	85.0	3290	43973	102			
16	0.0	0.0	17.0						
17	0.0	0.0	17.0						
18	0.0	0.0	17.0						
19	59.8	47.8	17.0						
20	30.0	24.0	17.0						
total	89.8	71.8	85.0	5122	6829	1016			
21	0.0	0.0	0.0						
22	0.0	0.0	0.0						
23	0.0	0.0	0.0						
24	0.0	0.0	0.0						
25	0.0	0.0	0.0						
total	0.0	0.0	0.0	0	0	0.000			
26	0.0	0.0	17.0						
27	0.0	0.0	17.0						
28	0.0	0.0	17.0						
29	0.0	0.0	17.0						
30	0.0	0.0	17.0						
total	0.0	0.0	85.0	3290	43973	102			
TOTAL	128.8	93.4	85.0	12866.1	17154.7				

1960 Ave 5th Iron = 38.8 ha (80.0 m x 5.0 m) 80.0 m x 5.0 m I.P. = 75.0
 Date E.R. P (Ave. Net. Total) (m³/a)

1	14.5	11.6	15.0	15.0
2	0.0	0.0	15.0	15.0
3	0.0	0.0	15.0	15.0
4	0.0	0.0	15.0	15.0
5	0.0	0.0	15.0	15.0
total	14.5	11.6	63.4	24599
6	0.0	0.0	15.0	15.0
7	0.0	0.0	15.0	15.0
8	0.0	0.0	15.0	15.0
9	0.0	0.0	15.0	15.0
10	7.0	5.6	15.0	15.0
total	7.0	5.6	69.4	26927
11	3.2	0.0	15.0	15.0
12	0.0	0.0	15.0	15.0
13	0.0	0.0	15.0	15.0
14	3.5	4.4	15.0	15.0
15	18.0	14.4	15.0	15.0
total	24.7	18.8	56.2	21806
16	5.7	4.6	15.0	15.0
17	0.0	0.0	15.0	15.0
18	0.0	0.0	15.0	15.0
19	0.0	0.0	15.0	15.0
20	0.0	0.0	15.0	15.0
total	5.7	4.6	48.0	18624
21	49.0	39.2	15.0	15.0
22	0.0	0.0	15.0	15.0
23	0.0	0.0	15.0	15.0
24	0.0	0.0	15.0	15.0
25	0.0	0.0	15.0	15.0
total	49.0	39.2	35.8	13990
26	0.0	0.0	15.0	15.0
27	0.0	0.0	15.0	15.0
28	0.0	0.0	15.0	15.0
29	0.0	0.0	15.0	15.0
30	0.0	0.0	15.0	15.0
31	3.7	0.0	15.0	15.0
total	3.7	0.0	90.0	34920
TOTAL	134.6	108.2	90.0	34920
			140766	187689
			29074	24832
			29074	24832
			18521	18521
			46560	46560
			187689	187689

PAN IRRIGATION & RECLAMATION CONSULTANTS TOKYO JAPAN	SUBJECT				PROJECT
	COMPUTED	DATE	CHECKED	DATE	FILE NO.
					PAGE _____ OF _____ PAGES

1.5. AREA DE DEMONSTRACAO DO POLDER PILOT I

PADY FIELD IRRIGATION REQUIREMENTS (Remoto) (7/0)

1959 Aug 10 th Area = 30.9 ha (80.0 mm > R) 5.0 mm * 80.5 = E.R. I.E. = 75.0

Date	A. mm	E. mm	D. mm	mm	mm	mm	mm
21	0.0	0.0	10.0				
22	12.0	9.6	10.0				
23	0.0	0.0	10.0				
24	0.0	0.0	10.0				
25	0.0	0.0	10.0				
total	12.0	9.6	50.0	40.4	12484	16645	.039
26	0.0	0.0	10.0				
27	0.0	0.0	10.0				
28	0.0	0.0	10.0				
29	18.0	14.4	10.0				
30	0.0	0.0	10.0				
31	0.0	0.0	10.0				
total	18.0	14.4	60.0	45.6	14090	18787	.036
TOTAL	30.0	24.0			26574	35432	

1959 Annual PADDY FIELD IRRIGATION REQUIREMENT (Normal) (7/5)

Date	Area (ha)	R.R. (mm)	(50.0 mm > R.R.) (mm)	I.R. (mm)	Area (ha)	Area (ha)	Area (ha)
1	0.0	0.0	15.0	0.0	0.0	0.0	0.0
2	0.0	0.0	15.0	0.0	0.0	0.0	0.0
3	0.0	0.0	15.0	0.0	0.0	0.0	0.0
4	0.0	0.0	15.0	0.0	0.0	0.0	0.0
5	0.0	0.0	15.0	0.0	0.0	0.0	0.0
total	0.0	0.0	75.0	0.0	0.0	0.0	0.0
6	5.1	6.5	15.0	6.5	5.1	5.1	5.1
7	0.0	0.0	15.0	0.0	0.0	0.0	0.0
8	1.0	0.0	15.0	0.0	1.0	1.0	1.0
9	1.6	0.0	15.0	0.0	1.6	1.6	1.6
10	0.0	0.0	15.0	0.0	0.0	0.0	0.0
total	9.7	6.5	75.0	6.5	9.7	9.7	9.7
11	0.0	0.0	15.0	0.0	0.0	0.0	0.0
12	31.3	25.0	15.0	25.0	31.3	31.3	31.3
13	7.6	6.1	15.0	6.1	7.6	7.6	7.6
14	0.0	0.0	15.0	0.0	0.0	0.0	0.0
15	0.0	0.0	15.0	0.0	0.0	0.0	0.0
total	38.9	31.1	75.0	31.1	38.9	38.9	38.9
16	0.0	0.0	15.0	0.0	0.0	0.0	0.0
17	0.0	0.0	15.0	0.0	0.0	0.0	0.0
18	0.0	0.0	15.0	0.0	0.0	0.0	0.0
19	7.7	6.2	15.0	6.2	7.7	7.7	7.7
20	9.9	6.2	15.0	6.2	9.9	9.9	9.9
total	17.6	12.4	75.0	12.4	17.6	17.6	17.6
21	2	0.0	15.0	0.0	2	2	2
22	9	0.0	15.0	0.0	9	9	9
23	4.8	0.0	15.0	0.0	4.8	4.8	4.8
24	0.0	0.0	15.0	0.0	0.0	0.0	0.0
25	0.0	0.0	15.0	0.0	0.0	0.0	0.0
total	5.9	0.0	75.0	0.0	5.9	5.9	5.9
26	23.3	19.0	15.0	19.0	23.3	23.3	23.3
27	2.9	0.0	15.0	0.0	2.9	2.9	2.9
28	0.0	0.0	15.0	0.0	0.0	0.0	0.0
29	0.0	0.0	15.0	0.0	0.0	0.0	0.0
30	4	0.0	15.0	0.0	4	4	4
total	27.1	19.0	75.0	19.0	27.1	27.1	27.1
TOTAL	90.2	62.8	30900	62.8	90.2	90.2	90.2

Area (ha) I.R. (mm) (50.0 mm > R.R.) (mm) I.R. (mm) Area (ha) Area (ha) Area (ha)

30900 .072

21167 28222 .055

13565 18087 .012

21259 20316 .066

23175 30300 .072

17304 23072 .053

119645 159527

ADD: FIELD IRRIGATOR REQUIREMENT (Normal) (1/1)

1959 Apr 12 th Area = 30.9 ha

(80.0 mm > R > 15.0 mm) - E.R. I.E. = 75.0 %

Date	R. mm	S.R. mm	D. mm	H. mm	A.N. mm	A. mm	Net. mm	Total. mm	mm ³ /a
1	0.0	0.0	17.0						
2	0.0	0.0	17.0						
3	0.0	0.0	17.0						
4	0.0	0.0	17.0						
5	0.0	0.0	17.0						
total	0.0	0.0	85.0						35020 .081
6	0.0	0.0	17.0						
7	0.0	0.0	17.0						
8	1.4	0.0	17.0						
9	18.0	14.4	17.0						
10	0.0	0.0	17.0						
total	19.4	14.4	85.0						29007 .067
11	4.5	0.0	17.0						
12	0.0	0.0	17.0						
13	0.0	0.0	17.0						
14	0.0	0.0	17.0						
15	0.0	0.0	17.0						
total	4.5	0.0	85.0						35020 .031
16	0.0	0.0	17.0						
17	0.0	0.0	17.0						
18	1.0	0.0	17.0						
19	0.0	0.0	17.0						
20	0.0	0.0	17.0						
total	1.0	0.0	85.0						35020 .031
21	0.0	0.0	17.0						
22	5.5	4.4	17.0						
23	0.0	0.0	17.0						
24	13.4	9.9	17.0						
25	0.0	0.0	17.0						
total	18.4	14.3	85.0						29128 .057
26	0.0	0.0	17.0						
27	0.0	0.0	17.0						
28	0.0	0.0	17.0						
29	0.0	0.0	17.0						
30	0.0	0.0	17.0						
31	0.0	0.0	17.0						
total	0.0	0.0	102.0						42024 .031
total	42.6	29.7	153975						205299

1960/Avi 11th

50.9 ha (90.0 mm > R > 5.0 mm) 80.5 ha S.R. = 75.0

Date	R ₁ (mm)	S.R. (mm)	D ₁ (mm)	H ₁ (mm)	A ₁ (mm ²)	N ₁ (mm ²)	S ₁ (mm ²)	Total
1	9.0	7.2	15.0					
2	3.0	0.0	15.0					
3	3.0	0.0	15.0					
4	0.0	0.0	15.0					
5	0.0	0.0	15.0					
total	12.2	7.2	75.0	67.8	20950	27931		.065
6	0.0	0.0	15.0					
7	17.1	13.7	15.0					
8	37.5	30.0	15.0					
9	1.2	0.0	15.0					
10	1.2	0.0	15.0					
total	56.0	43.7	75.0	311.3	9672	12195		.030
11	30.5	24.4	15.0					
12	51.1	41.1	15.0					
13	11.6	9.3	15.0					
14	0.0	0.0	15.0					
15	0.0	0.0	15.0					
total	93.5	74.9	75.0	1.2	163	182		.000
16	0.0	0.0	15.0					
17	0.0	0.0	15.0					
18	0.0	0.0	15.0					
19	0.0	0.0	15.0					
20	0.0	0.0	15.0					
total	0.0	0.0	75.0	75.0	23175	30900		.072
21	0.0	0.0	15.0					
22	1.5	0.0	15.0					
23	0.0	0.0	15.0					
24	0.0	0.0	15.0					
25	2.0	0.0	15.0					
total	3.5	0.0	75.0	75.0	23175	30900		.072
26	0.0	0.0	15.0					
27	0.0	0.0	15.0					
28	0.0	0.0	15.0					
29	0.0	0.0	15.0					
30	0.0	0.0	15.0					
31	0.0	0.0	15.0					
total	0.0	0.0	90.0	90.0	27810	37010		.072
total	105.2	125.7			104844	139792		

1960 Acre 3rd Area = 30.7 ha (90.0 mm) > R. > 5.0 mm) 80.2 = 5.71 (1.31 = 75.0)

Date	R ₁ mm	R ₂ mm	D ₁ mm	H ₁ mm	H ₂ mm	A ₁ mm/s	Necessary Total (m/s)
1	0.0	0.0	15.0				
2	0.0	0.0	15.0				
3	7.0	5.6	15.0				
4	0.0	0.0	15.0				
5	0.0	0.0	15.0				
total	7.0	5.6	75.0	69.4	21306	28400	.066
6	0.0	0.0	15.0				
7	0.0	0.0	15.0				
8	0.0	0.0	15.0				
9	0.0	0.0	15.0				
10	0.0	0.0	15.0				
total	0.0	0.0	75.0	75.0	23025	30700	.071
11	0.0	0.0	15.0				
12	6.1	4.0	15.0				
13	0.0	0.0	15.0				
14	1.1	0.0	15.0				
15	0.3	0.0	15.0				
total	7.5	4.0	75.0	70.1	21521	28694	.066
16	11.0	8.8	15.0				
17	0.0	0.0	15.0				
18	0.0	0.0	15.0				
19	0.0	0.0	15.0				
20	0.0	0.0	15.0				
total	11.0	8.8	75.0	66.2	20323	27090	.063
21	0.0	0.0	15.0				
22	0.0	0.0	15.0				
23	11.2	9.0	15.0				
24	0.0	0.0	15.0				
25	0.0	0.0	15.0				
total	11.2	9.0	75.0	66.0	20262	27016	.063
26	0.0	0.0	15.0				
27	0.0	0.0	15.0				
28	0.0	0.0	15.0				
29	0.0	0.0	15.0				
30	0.0	0.0	15.0				
31	0.0	0.0	15.0				
total	0.0	0.0	90.0	90.0	27630	36840	.071
TOTAL	3.7	28.3			134067	178756	

IRRIGATION REQUIREMENT (Normal) (mm)

1960 Area = 30.9 ha (80.0 mm > R > 5.0 mm) 30.3 - 3.1. I.R. = 15.0

Date	D mm	H mm	A mm	Area mm ²	Area mm ²	Total mm ²
1	14.5	13.6	15.0			
2	0.0	0.0	15.0			
3	0.0	0.0	15.0			
4	0.0	0.0	15.0			
5	0.0	0.0	15.0			
total	14.5	11.6	75.0	63.4	19591	26121
6	0.0	0.0	15.0			
7	0.0	0.0	15.0			
8	0.0	0.0	15.0			
9	0.0	0.0	15.0			
10	7.0	5.6	15.0			
total	7.0	5.6	75.0	69.4	21445	28593
11	2.2	0.0	15.0			
12	0.0	0.0	15.0			
13	0.0	0.0	15.0			
14	5.5	4.4	15.0			
15	16.0	14.4	15.0			
total	26.7	18.8	75.0	56.2	17366	23154
16	5.7	4.6	15.0			
17	0.0	0.0	15.0			
18	0.0	0.0	15.0			
19	0.0	0.0	15.0			
20	22.0	22.4	15.0			
total	33.7	27.0	75.0	48.0	14832	19776
21	49.0	39.2	15.0			
22	0.0	0.0	15.0			
23	0.0	0.0	15.0			
24	0.0	0.0	15.0			
25	0.0	0.0	15.0			
total	49.0	39.2	75.0	35.8	11062	14750
26	0.0	0.0	15.0			
27	0.0	0.0	15.0			
28	0.0	0.0	15.0			
29	0.0	0.0	15.0			
30	0.0	0.0	15.0			
31	3.7	0.0	15.0			
total	3.7	0.0	90.0	90.0	27810	37030
total	131.6	102.2			112105	149174

1.6 Traçado do vertedouro

1) Determinação do local

A posição do vertedouro exige considerações a respeito da segurança, devendo ser construído num local completamente separado. O prorrogamento do conduto deve ser curto. No sentido de reduzir a quantidade de terra escavada, é vantajoso construir o vertedouro na margem esquerda, de relevo mais suave. O conduto desempenha ainda as funções de canal recolhedor da água que corre dos declives. Decidimos assim construir o vertedouro de maneira mais racional, na margem esquerda.

2) Determinação da forma

A represa é de pequeno tamanho, e assim a forma do vertedouro deve ser a não-ajustável. Como é ainda uma represa do tipo cheio, é necessário considerar o aspecto da segurança ao se construir o vertedouro em morros. Considerando os aspectos que acabamos de citar, o vertedouro com vala é o mais indicado.

3) Traçado hidráulico

(1) Condições do traçado

quantidade de inundação do traçado	$Q = 17,7 \text{ m}^3/\text{seg.}$
coeficiente de aspereza	$n = 0,015$
profundidade de super-fluxo	$H = 0,50 \text{ m}$
altura da água	$F.W.L = 10,00$
altura da inundação da planta	$H.W.L = 10,50$
altura do dique de super-fluxo	$R.L = 10,00$
altura do leito na entrada	$R.L = 9,50$

(2) secção de super-fluxo

a) deverá ser adotada a seguinte forma na parte da secção de super-fluxo:

$$W \geq H/5$$

W: profundidade na entrada 0,50m

H: profundidade do super-fluxo 0,50m

$$0,50 \geq 0,5/5 = 0,1$$

O.K.

b) Inclinação da parte superior do dique

$$\frac{W}{H} = \frac{0,5}{0,5} = 1,0 \text{ logo, no âmbito de } 0,4 \leq \frac{W}{H} < 2,50$$

neste caso, a inclinação 1: 2/3 é apropriada (segundo o critério do planeamento).

c) Coeficiente da descarga

Segundo o critério do planeamento, $C = 2,16$.

d) Comprimento do ponto mais alto do dique de super-fluxo do dique de super-fluxo

$$Q = C \cdot B \cdot H^{3/2}$$

em que Q: quantidade de água inundada 17,7 m³/seg.

B: comprimento do dique de super-fluxo

$$B = \frac{Q}{C \cdot H^{3/2}} = \frac{17,7}{2,16 \times 0,5^{3/2}} = 23,16 \approx 23,2 \text{ m}$$

e) carga de velocidade dentro do canal d'água de aproximação

carga geral a partir do canal 1,00m aproximação

largura 23,2m descarga $Q = 17,7 \text{ m}^3/\text{seg.}$

se adotamos 10,47 como valor da posição d'água dentro do canal de aproximação,

a profundidade d'água $d = 10,47 - 9,50 = 0,97 \text{ m}$

área do corte seccional $A = 0,97 \times 23,2 = 22,5 \text{ m}^2$

do fluxo

velocidade da corrente

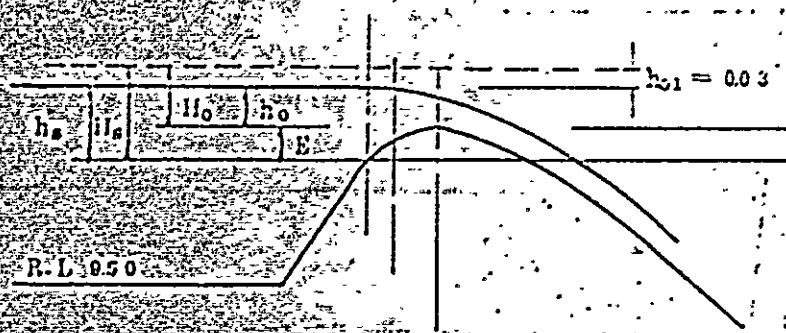
$$V = \frac{Q}{A} = \frac{17,7}{22,5} = 0,787 \text{ (m/sec)}$$

carga de velocidade

$$h_v = \frac{V^2}{2g} = 0,03 \text{ (m)}$$

carga geral $10,97 + 0,03 = 1,00 \text{ m}$

f) Força da secção do corte



Admitimos que

$h_s = 0,53 \text{ m}$

$$h_v/h_s = 0,03/0,53 = 0,057$$

logo, segundo o gráfico

$$E/h_s = 0,057$$

$$E = 0,057 \times 0,53 = 0,030$$

$$h_0 + E = 0,50 + 0,03 = 0,53 = h_s$$

Fig. 3-14 COORDENADAS CRUZADAS DA REPRESA

(na supert. de fronto 2/3, $h_a/h_s = 0,06$) $H_s = 0,53$

X/H _s	0,00	0,05	0,10	0,15	0,20	0,25
X	0	0,027	0,053	0,08	0,106	0,133
Y/H _s	0,00	0,029	0,046	0,054	0,056	0,052
Y	0	0,015	0,024	0,029	0,030	0,026
Elevação	9,970	9,985	9,994	9,999	10,00	9,992
X/H _s	0,30	0,35	0,40	0,45	0,50	0,60
X	0,159	0,186	0,212	0,239	0,265	0,318
Y/H _s	0,045	0,035	0,023	0,006	-0,009	-0,052
Y	0,024	0,019	0,012	0,004	-0,005	0,028
Elevação	9,994	9,989	9,982	9,974	9,965	9,942
X/H _s	0,70	0,80	0,90	1,00	1,20	1,40
X	0,371	0,424	0,477	0,530	0,636	0,742
Y/H _s	-0,105	-0,165	-0,233	-0,307	-0,482	-0,690
Y	-0,056	-0,087	-0,123	-0,163	-0,255	-0,366
Elevação	9,914	9,883	9,847	9,807	9,715	9,604
X/H _s	1,60	1,80	2,00	2,20	2,40	2,50
X	0,848	0,954	1,060	1,166	1,272	1,325
Y/H _s	-0,935	-1,205	-1,506	-1,833	-2,199	-2,399
Y	-0,056	-0,087	-0,123	-0,163	-0,255	-0,366
Elevação	9,474	9,331	9,172	8,999	8,805	8,699

(3) Canal lateral

a) Ambito do leito do canal lateral

O Ambito do leito do canal lateral é tanto melhor quanto mais estreito. Consideramos aqui o contacto com o canal de divisão, admitindo 2,00m.

b) Cálculo hidráulico

Pelo processo básico,

$$Q_x = q \cdot x$$

$$v = \frac{1}{n} x^n$$

$$y = \frac{n+1}{n} \cdot hv = \frac{n+1}{n} \frac{V^2}{2g}$$

em que, Q_x : descarga no ponto x ($m^3 \times \text{seg}$)
 q : descarga no dique, pelo comprimento unitário ($m^3 \times \text{seg}$)
 x : distância da extremidade superior do dique até um ponto arbitrário (m)
 u : velocidade da corrente num ponto arbitrário (m/seg)
 a : coeficiente da velocidade da corrente
 n : índice da velocidade da corrente
 y : distância perpendicular entre o alto do dique a uma inclinação arbitrária e a superfície da água no canal lateral
 h_v : cabeça d'água da velocidade

para uma profundidade de super-fluxo $H = 0,50$, realiza-se um ajustamento de n , a , em que $n = 0,40 \sim 0,80$, a escavação se torna mínima, procurando com calculadora a secção vertical do canal d'água lateral nesse momento.

Como resultado, $n = 0,607$ e $a = 0,3583$, e a fórmula da velocidade da corrente será $V = 0,3583 \times X^{0,607}$.

c) Determinação da inclinação do fundo do canal lateral

A inclinação do fundo do canal lateral será determinada considerando como fundo do canal corrigido a linha reta que liga um ponto 1/10 a partir do terminal do canal lateral e do terminal superior do canal lateral

inclinação do fundo $I = 0,088 = 1/11,36$

d) Profundidade limite do terminal do canal lateral:

$$Q = 1.770 \text{ m}^3/\text{seg} \quad b = 2.00 \text{ m} \quad \bar{m} = 0.60 \text{ f.p.}$$

de profundidade limite, a partir da fórmula simplificada

Altura teórica da
superfície da água

		H.W.L.		F.W.L.	
		Profundidade corrigida do rego			
		Profundidade calculada do rego			
Altura da superfície da água		10300	9951	9516	9086
Valor corrigido		1000	510	100	50
Valor de cálculo		10300	9951	9516	9086
Água inundada		0557	0210	100	50
Distância		232	451	696	928
		1160	1392	1624	1856
		2028	2416	2804	3192

$$b^2 = 2.0^2 = 5.66$$

$$K = Q/b^2 = 17.70/5.66 = 3.13$$

para fazer frente a isto, dc/b , a partir do gráfico,

$$dc/b = 0.84$$

$$dc/b = 0.84$$

$$dc = 0.84 \times 2.00 = 1.600 \text{ m}$$

Por outro lado, como a profundidade na extremidade do canal lateral é de 2,205m, desce a corrente num fluxo ordinário.

e) Rebaixamento da superfície das águas no ponto de transição

Princípios de hidráulica na extremidade do vertedouro

$$I_1 = \dots \quad 1/11,36$$

$$h_1 = \dots \quad 2,205 \text{ m}$$

$$\text{largura do fundo} = 2,0 \text{ m}$$

$$\text{inclinação lat.} \quad 1 : 0,5, 1 : 0,7$$

Área de fluxo em

$$\text{secção cruzada} \quad A_1 = 7,327 \text{ m}^2$$

$$\text{descarga} \quad Q = 17,70 \text{ m}^3/\text{seg.}$$

$$\text{velocidade da} \quad V_1 = 2,416 \text{ m/seg.}$$

corrente

f) Princípios de hidráulica no ponto inicial do canal de diversão

$$I_2 = 1/500$$

$$h_2 = 2.58 \text{ m}$$

$$b = 2.0 \text{ m}$$

$$A_2 = 11.816 \text{ m}^2$$

$$V_2 = 1.498 \text{ m}$$

comprimento da transição = $L = 10,0m$

$$\Delta h_{ge} = f_{ge} \frac{V_1^2 - V_2^2}{2g} + I_m \cdot L + \frac{V_2^2 - V_1^2}{2g}$$

em que, Δh_{ge} : queda da superfície pela extensão

I_m : gradiente hidráulico médio entre os pontos de transição

$$I_m = \frac{I_1 + I_2}{2}$$

f_{ge} : coeficiente de perda com a extensão

forma em linha reta 0,50

$$\Delta h_{ge} = 0,50 \frac{2,416^2 - 1,498^2}{2 \times 9,8} + \frac{0,089 + 0,002}{2} \times 10 + \frac{1,498^2 - 2,416^2}{2 \times 9,8}$$

$$= 0,092 + 0,45 - 0,183 = 0,359 (m)$$

posição d'água no ponto final : 9,212

do vertedouro

altura do leito: 7,007

posição inicial no ponto 9,212 - 0,359 = 8,853

inicial do canal de diversão

altura do leito 8,853 - 2,58 = 6,273

Fig. 3-15 PROCUR

x	S_x	EL	$\frac{D}{\Delta y}$	W.L.	b	s'		
23,20	2,32	7,007		9,212	200	2,205	7,327	1
20,88	2,32	7,208	0,079	9,291	200	2,083	6,769	1
18,56	2,32	7,412	0,087	9,378	200	1,996	6,251	1
16,24	2,32	7,616	0,097	9,475	200	1,859	5,792	12
13,92	2,32	7,820	0,107	9,582	200	1,762	5,387	10
11,60	2,32	8,024	0,112	9,694	200	1,670	5,013	8
9,28	2,32	8,228	0,111	9,805	200	1,577	4,645	7
6,96	2,32	8,432	0,106	9,911	200	1,497	4,270	5
4,64	2,32	8,636	0,097	10,008	200	1,372	3,873	3
2,32	2,32	8,840	0,083	10,091	200	1,251	3,441	1
0	2,32	9,044	0,074	10,165	200	1,121	2,995	0

$Q = 17,70 \text{ m}^3/\text{sec}$ $B = 23,2 (\text{ m. })$

$q = Q/B = \frac{17,70}{23,2} = 0,763 \text{ m}^3/\text{sec}$

$A = bd$ $md^2 = 2 \times d = 0,6 \times d^2$

Fig. 3-15 PROCURA DA SUPERFICIE D'AGUA NO HECO

EL	$\Delta Y:$	W:L	s	z_1	z_2	Q_1	V_1	Q_1+Q_2	$q(Q_1+Q_2)$	V_1+V_2	ΔV	$q_1 V_1 \Delta X$	$\frac{Q_1}{Q_1+Q_2}$	$\frac{z_1+z_2}{2}$	$\frac{Q_1}{Q_1+Q_2} \times \frac{z_1+z_2}{2}$	$\text{D}-\text{Z}$	Erro
7,007		9,212	200	2,205	7,327	17,70	2,416										
7,208	0,079	9,291	200	2,083	6,769	15,93	2,353	33,63	0,054	4,769	0,063	0,242	0,305	0,097	0		
7,412	0,087	9,378	200	1,996	6,251	14,16	2,265	30,09	0,054	4,618	0,088	0,261	0,349	0,087	0		
7,616	0,097	9,475	200	1,859	5,792	12,39	2,139	26,55	0,054	4,404	0,126	0,283	0,409	0,097	0		
7,820	0,107	9,582	200	1,762	5,387	10,62	1,791	23,01	0,055	4,110	0,168	0,306	0,474	0,107	0		
8,024	0,112	9,694	200	1,670	5,013	8,85	1,765	19,47	0,056	3,763	0,206	0,329	0,535	0,112	0		
8,228	0,111	9,805	200	1,577	4,645	7,08	1,524	15,593	0,057	3,289	0,241	0,353	0,594	0,111	0		
8,432	0,106	9,911	200	1,497	4,270	5,31	1,243	12,39	0,058	2,765	0,281	0,381	0,662	0,106	0		
8,636	0,097	10,008	200	1,372	3,873	3,54	0,914	8,85	0,061	2,157	0,329	0,414	0,743	0,097	0		
8,840	0,083	10,091	200	1,251	3,441	1,77	0,514	5,31	0,068	1,423	0,400	0,457	0,857	0,083	0		
9,044	0,074	10,165	200	1,121	2,995	0	0	1,77	0,102	0,514	0,514	0,909	1,923	0,074	0		

$B = 23,2 (m)$

$= 0,763 m^3/sec$

$2 \times d = 0,6 \times d^2$

CALCULO HIDRAULICO

..... RIO RICEIPA

INPUT DATA

FLOOD DISCHARGE MAX DISCHARGE Q-COEFFICIENT SIDE SLOPE ELEVATION DELTA-X
 17.700 2.160 0.600 10.000 10.00
 KIND OF OVERFLOW 0.50

TABLE OF OVERFLOW-H-LENGTH OF WEIR DELTA-H

H (M)	H**3/2	CH**3/2	R (M)	USING-B (M)	QMAX/2B	MAX-H (M)	DELTA-H (M)
0.5	0.3536	0.7637	23.177	23.2	0.381	0.526	0.026

TABLES OF LOWEST SECTION AT SIDE CHANNEL

WATER DEPTH 1.703(M)
 WIDE OF BOTTOM 2.000(M)
 WIDE OF WATER SURFACE ... 7.973(M)
 AREA OF FLOW 5.077(M²)

CONDITION OF END OF SPILLWAY

N	(N+1)/N	Y2	D/B	C	A	V
0.4	3.50	3.497	1.190	2.380	8.160	2.169
0.5	3.00	2.997	1.141	2.282	7.688	2.302
0.6	2.67	2.664	1.105	2.209	7.346	2.409
0.7	2.43	2.426	1.076	2.153	7.086	2.498
0.8	2.25	2.248	1.054	2.108	6.881	2.572

IN CASE OF H= 0.5 (4) B=23.2 (M)

N= 0.4 ((N+1)/N*(Q2/G85))= 3.4965

HA	(N+1)/N	XL	VX	HY	OX	R	A	D	V	D+HY	EL
(M)	(M)	(M)	(M/S)	(M)	(M/S)	(M)	(M)	(M)	(M/S)	(M)	(M)
0.5167	3.50	2.32	0.864	0.133	1.77	2.00	8.160	0.822	2.169	0.955	9.045
		6.64	1.139	0.232	3.54			1.154		1.386	8.614
		6.96	1.340	0.331	5.31			1.396		1.717	8.283
		9.28	1.503	0.404	7.08			1.593		1.997	8.003
		11.60	1.644	0.483	8.85			1.761		2.244	7.756
		13.92	1.768	0.558	10.62			1.909		2.468	7.532
		16.24	1.891	0.632	12.39			2.042		2.674	7.326
		18.56	1.984	0.703	14.16			2.164		2.867	7.133
		20.88	2.080	0.772	15.93			2.276		3.048	6.952
		23.20	2.169	0.840	17.70			2.380		3.220	6.760

N= 0.5 ((N+1)/N*(Q2/G85))= 2.9970

HA	(N+1)/N	XL	VX	HY	OX	B	A	D	V	D+HY	EL
(M)	(M)	(M)	(M/S)	(M)	(M/S)	(M)	(M)	(M)	(M/S)	(M)	(M)
0.5780	3.00	2.32	0.728	0.081	1.77	2.00	7.588	0.947	2.302	1.028	8.972
		6.64	1.030	0.162	3.54			1.250		1.412	8.588
		6.96	1.261	0.243	5.31			1.463		1.707	8.293
		9.28	1.455	0.325	7.08			1.632		1.957	8.043
		11.60	1.628	0.406	8.85			1.774		2.180	7.820
		13.92	1.783	0.487	10.62			1.897		2.384	7.616
		16.24	1.926	0.568	12.39			2.007		2.575	7.425
		18.56	2.058	0.649	14.16			2.107		2.756	7.244
		20.88	2.184	0.730	15.93			2.198		2.928	7.072
		23.20	2.302	0.811	17.70			2.282		3.093	6.907

N= 0.6 ((N+1)/N*(Q2/G85))= 2.6640

HA	(N+1)/N	XL	VX	HY	OX	B	A	D	V	D+HY	EL
(M)	(M)	(M)	(M/S)	(M)	(M/S)	(M)	(M)	(M)	(M/S)	(M)	(M)
0.3653	2.67	2.32	0.605	0.050	1.77	2.00	7.346	1.100	2.609	1.149	8.851
		4.64	0.917	0.114	3.54			1.368		1.483	8.517
		6.96	1.170	0.186	5.31			1.549		1.735	8.265
		9.28	1.390	0.263	7.08			1.670		1.953	8.047
		11.60	1.590	0.344	8.85			1.806		2.149	7.851
		13.92	1.773	0.428	10.62			1.905		2.333	7.667
		16.24	1.945	0.515	12.39			1.993		2.508	7.492
		18.56	2.107	0.604	14.16			2.072		2.676	7.324
		20.88	2.262	0.696	15.93			2.143		2.839	7.161
		23.20	2.409	0.790	17.70			2.209		2.999	7.001

IN CASE OF N= 0.5 (M) R= 23.2 (M)

N= 0.7 (N+1)/N= (Q2/GS) = 2.4262 D/R= 1.076 D= 2.153 (M) V= 2.498 (M/S)

XL (M)	VX (M/S)	HY (M)	QX (M/S)	B (M)	AX (M)	D (M)	D*HY (M)	EL (M)
2.32	0.498	0.031	1.77	2.00	3.552	1.282	1.313	8.587
4.64	0.810	0.081	3.54	2.00	4.372	1.506	1.587	8.413
6.96	1.075	0.163	5.31	2.00	4.938	1.651	1.794	8.206
9.28	1.315	0.274	7.08	2.00	5.383	1.761	1.975	8.025
11.60	1.530	0.293	8.85	2.00	5.756	1.851	2.143	7.857
13.92	1.747	0.378	10.62	2.00	6.079	1.926	2.305	7.695
16.24	1.946	0.469	12.39	2.00	6.367	1.993	2.462	7.538
18.56	2.137	0.566	14.16	2.00	6.627	2.051	2.617	7.383
20.88	2.320	0.667	15.93	2.00	6.866	2.104	2.771	7.229
23.20	2.498	0.773	17.70	2.00	7.085	2.153	2.926	7.074

N= 0.8 (N+1)/N= (Q2/GS) = 2.2478 D/R= 1.056 D= 2.108 (M) V= 2.572 (M/S)

XL (M)	VX (M/S)	HY (M)	QX (M/S)	B (M)	AX (M)	D (M)	D*HY (M)	EL (M)
2.32	0.408	0.019	1.77	2.00	4.342	1.498	1.517	8.483
4.64	0.710	0.058	3.54	2.00	4.987	1.663	1.721	8.279
6.96	0.982	0.111	5.31	2.00	5.408	1.767	1.878	8.122
9.28	1.234	0.175	7.08	2.00	5.729	1.844	2.019	7.981
11.60	1.477	0.251	8.85	2.00	5.990	1.906	2.156	7.844
13.92	1.709	0.335	10.62	2.00	6.213	1.957	2.293	7.707
16.24	1.914	0.429	12.39	2.00	6.407	2.002	2.431	7.569
18.56	2.152	0.532	14.16	2.00	6.581	2.041	2.572	7.428
20.88	2.364	0.642	15.93	2.00	6.737	2.076	2.718	7.282
23.20	2.572	0.760	17.70	2.00	6.881	2.108	2.867	7.133

TABLE OF N-SA,RATIO

N	SA(M2)	RATIO
0.6	48.640	1.031
0.5	47.497	1.007
0.6	47.155	1.000
0.7	47.400	1.005
0.8	48.114	1.020

..... 910/ PIREIRA

(IN CASE OF H= 0.5 (M) D= 23.2 (H)

N=0.607 (H+1)/N=(02/GR5)= 2.6448 D/A= 1.102 D=2.205 (M) A= 7.326 (M2) V= 2.416 (M/S)

WA	(N+1)/N	XL	(M)	VX	(M/S)	HY	(M)	QX	(M ³ /S)	B	(M)	AX	(M2)	D	(M)	DHY	(M)	EI	(M)
0.3583	2.65	2.32	0.597	0.048	1.77	2.00	2.964	1.111	1.160	1.111	1.160	2.964	1.111	1.160	1.160	1.160	8.840		
		6.64	0.910	0.112	3.54		3.892	1.377	1.489	1.377	1.489	3.892	1.377	1.489	1.489	1.489	8.511		
		6.96	1.163	0.183	5.31		5.564	1.556	1.739	1.556	1.739	5.564	1.556	1.739	1.739	1.739	8.261		
		9.28	1.385	0.259	7.08		7.111	1.694	1.953	1.694	1.953	7.111	1.694	1.953	1.953	1.953	8.047		
		11.60	1.586	0.340	8.85		8.579	1.808	2.168	1.808	2.168	8.579	1.808	2.168	2.168	2.168	7.852		
		13.92	1.772	0.424	10.62		10.993	1.906	2.330	1.906	2.330	10.993	1.906	2.330	2.330	2.330	7.670		
		16.24	1.946	0.511	12.39		12.368	1.993	2.504	1.993	2.504	12.368	1.993	2.504	2.504	2.504	7.496		
		18.56	2.110	0.601	14.16		14.16	2.070	2.671	2.070	2.671	14.16	2.070	2.671	2.671	2.671	7.329		
		20.88	2.266	0.694	15.93		15.93	2.140	2.834	2.140	2.834	15.93	2.140	2.834	2.834	2.834	7.166		
		23.20	2.416	0.788	17.70		17.70	2.205	2.993	2.205	2.993	17.70	2.205	2.993	2.993	2.993	7.007		

VERTICAL AREA IN SIDE CHANNEL SPILLWAY 47.155(42)

VELOCITY FORMULA V= 0.3583XL**0.607