

7.9.5 Ranking and Evaluation

Scores provided to each proposed route for each sub-criterion are summed up by each major category of criteria; i.e. Isolation, Health, Education and Disparity. Then aggregating them a total score of social impacts is obtained by each proposed route. In this study, equal weight was assigned among sub-criteria and major criteria, viewing that arbitral weighting without any background of the established policies may mislead the judgement.

In ranking the proposed routes by magnitude of social impacts, this Study employed a kind of group ranking method paying attention not to the precise figure of the scores but only to their order of magnitude. Ranking was made as follows:

- Rank A: routes of which scores are higher than the average value
- Rank B: routes of which scores fall into between the average value and 2/3 of the average
- Rank C: routes of which scores are lower than 2/3 of the average value

As summarized in Table 7.9.3, 11 routes fell into Rank A and are deemed to have significant impacts from a social viewpoint.

Table 7.9.1 CRITERIA AND INDICATORS OF
SOCIAL IMPACTS

| | Criteria | Indicators |
|---------|---|---|
| I. | Isolation | |
| I - 1 | Improvement of Access to Amphoe | Per capita savings of average traveling time to Amphoe centers |
| I - 2 | Improvement of Access from Amphoe to Artery Highway | Per capita savings of average traveling time from Amphoe to nearest artery highways |
| I - 3 | Alleviation of Impassability | Duration of impassability a year by disaster |
| II. | Health | |
| II - 1 | Improvement of Access to Hospital | Per capita savings of average traveling time to Amphoe level Hospitals |
| II - 2 | Improvement of Access to Medical Facilities | Per capita savings of average traveling time to medical facilities such as health centers |
| III. | Education | |
| III - 1 | Improvement of Access to Secondary School | Savings per student of average traveling time to secondary schools |
| III - 2 | Improvement of Teacher Intensity | Ratio of University graduate teachers to student; Total number of teachers to student |
| IV. | Disparity | |
| IV - 1 | Alleviation of Income Disparity | Difference between disparity indices* of with project and without project |

* Average of N.E./Per capita crop production value in Influence area

Table 7.9.2

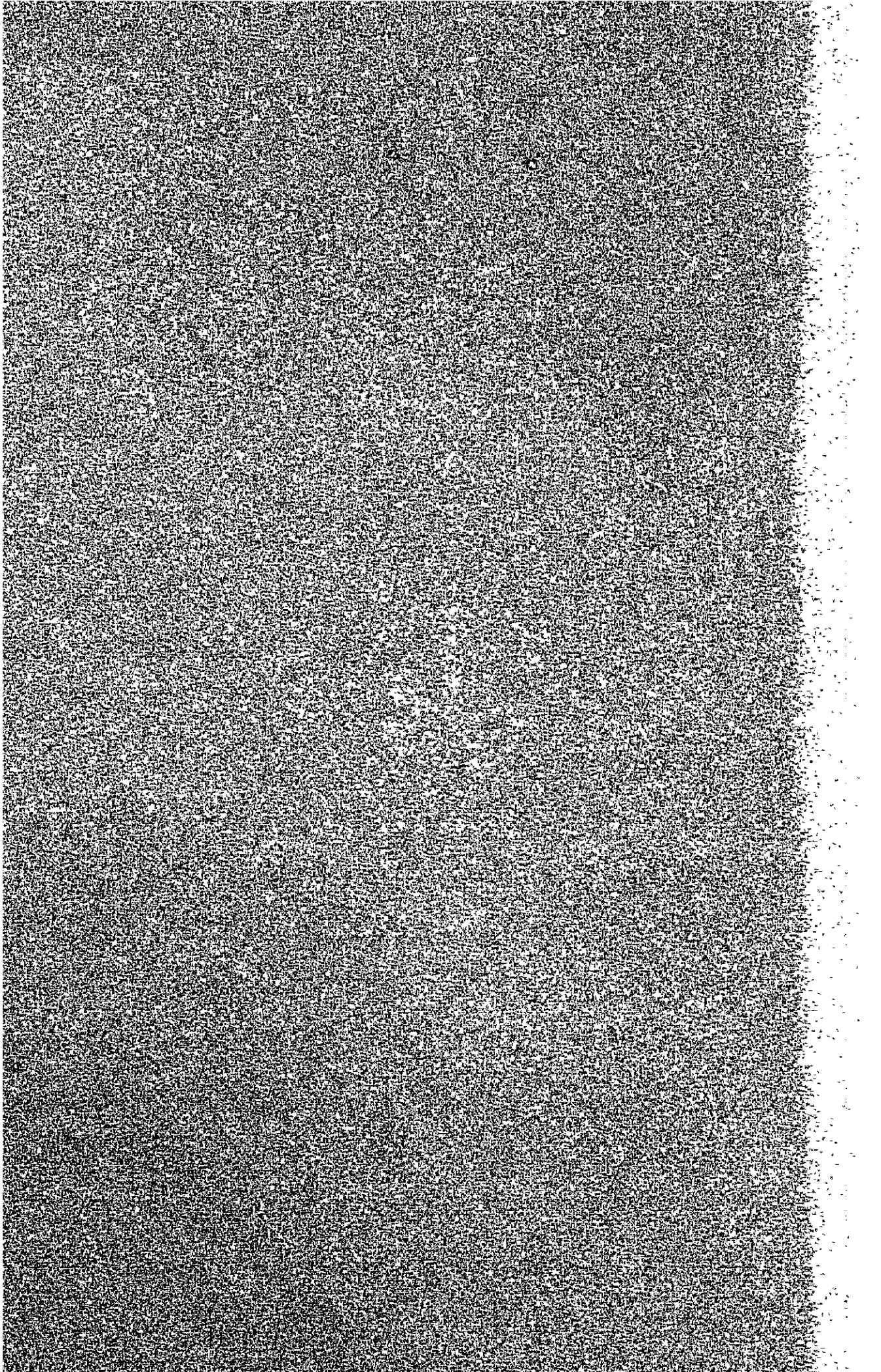
Table 7.9.2 SCORES OF SOCIAL IMPACTS

| Proposed Route | Population 1993 (1,000) | Score | | | | | | | | | | | Total Score |
|----------------|-------------------------|-----------|--------|----------------|-----------|-------------|---------------|-----------|-----------|---------|-----------|-----------|-------------|
| | | Isolation | | | | Health | | | Education | | | Disparity | |
| | | to Amphoe | to Hwy | Im-passability | Sub-Total | to Hospital | to Med. Facil | Sub-Total | to School | Teacher | Sub-Total | | |
| IM - 1 | 29.3 | 100 | 117 | 658 | 876 | 147 | 84 | 231 | 117 | 130 | 247 | 0 | 1376 |
| IM - 2 | 13.2 | 76 | 115 | 0 | 191 | 60 | 60 | 120 | 63 | 85 | 148 | 268 | 727 |
| IM - 3 | 30.0 | 65 | 96 | 108 | 269 | 140 | 76 | 216 | 56 | 66 | 122 | 0 | 608 |
| IM - 4 | 29.3 | 59 | 111 | 108 | 278 | 126 | 44 | 170 | 112 | 100 | 212 | 0 | 660 |
| IM - 5 | 34.3 | 47 | 0 | 0 | 47 | 47 | 32 | 79 | 32 | 74 | 116 | 89 | 331 |
| IM - 6 | 5.8 | 253 | 0 | 0 | 253 | 200 | 344 | 544 | 252 | 85 | 337 | 0 | 1134 |
| IM - 7 | 11.7 | 335 | 100 | 550 | 985 | 265 | 416 | 681 | 361 | 110 | 471 | 161 | 3432 |
| IM - 8 | 23.0 | 76 | 0 | 0 | 76 | 60 | 60 | 120 | 82 | 100 | 182 | 54 | 432 |
| IM - 9 | 32.5 | 59 | 0 | 50 | 109 | 42 | 28 | 70 | 40 | 128 | 168 | 0 | 347 |
| IM - 10 | 39.5 | 41 | 107 | 0 | 148 | 72 | 32 | 104 | 48 | 103 | 151 | 196 | 599 |
| IM - 11 | 8.7 | 153 | 222 | 0 | 375 | 119 | 104 | 223 | 160 | 87 | 247 | 71 | 916 |
| IM - 12 | 22.9 | 115 | 194 | 183 | 492 | 112 | 104 | 216 | 83 | 115 | 198 | 71 | 972 |
| IM - 13 | 18.7 | 79 | 259 | 167 | 505 | 70 | 72 | 142 | 88 | 85 | 173 | 0 | 800 |
| IM - 14 | 12.8 | 133 | 350 | 500 | 983 | 207 | 136 | 343 | 232 | 114 | 346 | 268 | 1940 |
| IM - 15 | 42.4 | 61 | 64 | 0 | 125 | 102 | 40 | 142 | 64 | 75 | 139 | 125 | 531 |
| IM - 16 | 11.1 | 68 | 196 | 0 | 264 | 105 | 180 | 285 | 150 | 114 | 164 | 143 | 956 |
| IM - 17 | 29.5 | 59 | 189 | 0 | 248 | 133 | 84 | 217 | 71 | 74 | 145 | 71 | 681 |
| IM - 18 | 61.3 | 59 | 15 | 108 | 182 | 51 | 60 | 110 | 36 | 102 | 138 | 179 | 610 |
| IM - 19 | 43.2 | 115 | 100 | 33 | 248 | 77 | 40 | 117 | 91 | 110 | 201 | 107 | 673 |
| IM - 20 | 20.1 | 71 | 204 | 0 | 275 | 109 | 116 | 225 | 101 | 91 | 192 | 89 | 781 |
| IM - 21 | 53.3 | 35 | 96 | 0 | 131 | 49 | 56 | 105 | 37 | 105 | 142 | 89 | 467 |
| IM - 22 | 14.9 | 255 | 78 | 0 | 333 | 188 | 204 | 392 | 190 | 176 | 366 | 125 | 1216 |
| IM - 23 | 30.9 | 76 | 100 | 0 | 176 | 86 | 72 | 158 | 25 | 129 | 154 | 0 | 488 |
| IM - 24 | 5.4 | 218 | 100 | 0 | 318 | 167 | 172 | 339 | 135 | 99 | 234 | 0 | 1379 |
| IM - 25 | 44.4 | 79 | 61 | 142 | 282 | 56 | 40 | 96 | 58 | 86 | 144 | 125 | 647 |
| IM - 26 | 39.2 | 53 | 0 | 492 | 545 | 49 | 48 | 97 | 58 | 114 | 172 | 89 | 903 |
| IM - 27 | 36.5 | 44 | 0 | 83 | 127 | 40 | 36 | 76 | 62 | 88 | 150 | 107 | 400 |
| IM - 28 | 46.3 | 56 | 126 | 142 | 324 | 44 | 64 | 108 | 33 | 89 | 122 | 161 | 715 |
| IM - 29 | 71.8 | 35 | 0 | 25 | 60 | 28 | 28 | 56 | 31 | 148 | 179 | 232 | 527 |
| IM - 30 | 48.6 | 41 | 111 | 33 | 185 | 28 | 36 | 64 | 33 | 93 | 126 | 89 | 464 |
| IM - 31 | 62.2 | 56 | 0 | 50 | 106 | 40 | 32 | 72 | 36 | 127 | 163 | 89 | 430 |
| IM - 32 | 24.1 | 82 | 100 | 0 | 152 | 130 | 132 | 262 | 188 | 111 | 299 | 0 | 743 |
| IM - 33 | 22.8 | 165 | 220 | 0 | 385 | 130 | 196 | 326 | 163 | 98 | 261 | 286 | 1258 |

Table 7.9.3 RANKING OF SOCIAL IMPACTS

| Proposed Route | Isolation | Health | Education | Disparity | Overall |
|----------------|-----------|--------|-----------|-----------|---------|
| IM - 1 | A | A | A | C | A |
| IM - 2 | C | C | B | A | B |
| IM - 3 | B | A | C | C | B |
| IM - 4 | B | B | A | C | B |
| IM - 5 | C | C | C | B | C |
| IM - 6 | B | A | A | C | A |
| IM - 7 | A | A | A | A | A |
| IM - 8 | C | C | B | C | C |
| IM - 9 | C | C | B | C | C |
| IM - 10 | C | C | B | A | B |
| IM - 11 | A | A | A | B | A |
| IM - 12 | A | A | B | B | A |
| IM - 13 | A | B | B | C | B |
| IM - 14 | A | A | A | A | A |
| IM - 15 | C | C | C | A | C |
| IM - 16 | B | A | A | A | A |
| IM - 17 | B | A | B | B | B |
| IM - 18 | C | C | C | A | B |
| IM - 19 | B | C | A | A | B |
| IM - 20 | B | A | B | B | B |
| IM - 21 | C | C | B | B | C |
| IM - 22 | A | A | A | A | A |
| IM - 23 | C | B | B | C | C |
| IM - 24 | A | A | A | C | A |
| IM - 25 | B | C | B | A | B |
| IM - 26 | A | C | B | B | A |
| IM - 27 | C | C | B | A | C |
| IM - 28 | A | C | C | A | B |
| IM - 29 | C | C | B | A | C |
| IM - 30 | C | C | C | B | C |
| IM - 31 | C | C | B | B | C |
| IM - 32 | C | A | A | C | B |
| IM - 33 | A | A | A | A | A |

CHAPTER 8
EVALUATION OF PROPOSED LINKS
FOR REHABILITATION



CHAPTER 8
EVALUATION OF PROPOSED LINKS
FOR REHABILITATION

8.1 PROPOSED LINKS

The proposed links for rehabilitation identified in identification process were 28 links, 774 km in total length as given in Table 6.6.1 and also shown in Figure 6.6.1.

8.2 EVALUATION FLOW

Evaluation analyses for rehabilitation links were proceeded laying emphasis on the calculation of overlay thickness and the analysis of VOC savings accrued from roughness improvement of paved road.

Overlay thickness required for the respective proposed links were determined through the comparative studies on thickness analysis employing some deflection criterion curves.

With the object of obtaining data for analysis of benefits and overlay plannings, field surveys on roughness and PSI (Present Serviceability Index) ratings of pavement surface were carried out. Supplemental deflection survey for several links was also conducted to update the rather old data.

Finally, using the calculated rehabilitation costs and benefits, benefit-cost ratio and internal rate of return (IRR) were calculated.

The evaluation flow for the rehabilitation links is shown in Figure 8.2.1.

8.3 ENGINEERING STUDY AND COST ESTIMATES

8.3.1 Field Surveys

1) Deflection Survey

To update the rather old data used for link identification for rehabilitation, field deflection survey was conducted. It was carried out from September to October, 1982. The links subjected to the survey are as follows:

| <u>Link No.</u> | <u>Route - Link</u> | <u>Length (km)</u> |
|-----------------|---------------------|--------------------|
| RH - 5 | 201 - 0100 | 40 |
| - 6 | - 0200 | 25 |
| - 7 | - 0300 | 17 |
| - 8 | - 0400 | 38 |
| -15 | 213 - 0100 | 43 |
| -16 | 214 - 0100 | 28 |
| -17 | - 0200 | 19 |

The surveyed data for the above links were computerized for ready application to pavement design.

2) Roughness Survey

For evaluation and comparison of paved surfaces, roughness survey was conducted. The roughness was measured using a Mays Ride Meter (MRM) installed in a passenger vehicle.

The principle of the MRM instrument is that it measures the displacement of the rear axle of the vehicle relative to its body, thus giving an indirect measurement of roughness in both ways of graphical oscillation chart and roughness summation expressed in figures.

Field survey was carried out for 35 links of proposed links and additional links, totaling about 1,000 km. The roughnesses measured at constant vehicle speed of 60 km/hr were printed on a strip paper together with landmarks and bridge locations and at the same time, they were numerically accumulated every one kilometer basis. Figure 8.3.1 shows typical roughness charts characteristic to respective surface conditions.

Average roughness and analyzed standard deviation for each link is summarized in Table 8.3.1. Measured roughness by every 1 km is graphically shown in Appendix 8.1 together with pavement deflection values.

3) Pavement Condition Survey

In order to correlate the measured roughness with PSI, a condition rating survey for pavement condition was carried out by a panel of engineers. The field work was conducted in November 1982 for 40 sections totaling about 460 km of paved road of asphaltic concrete (AC), surface treatment (ST) and penetration macadam surfaces (PM).

In order to facilitate recognition of pavement deficiencies by the raters, the most common signs of distresses were selected referring to the standard nomenclatures as defined in the HRB Report^{1/} as given in Table 8.3.2.

The condition surveys for all the items described in Table 8.3.2 were carried out by rating their deficiencies in a scale of 0 to 5 listed on the listing form as shown in Figure 8.3.2. The assignment of rating classes with respect to the actual surface conditions were understood among raters prior to the start of ratings through trial practices. The ratings thus obtained by individual rater were analyzed and average rating points and ranges were calculated. They are given in Table 8.3.3.

^{1/}: Standard Nomenclature and Definitions for Pavement Components and Deficiencies. HRB Special Report 113.

4) Roughness - PSI Relationships

In order to correlate roughness with serviceability index, PSI and measured roughness values given in Table 8.3.3 were plotted by surface type. Then following three curves for different surface types were derived referring to the calibration formula introduced in HRB Report^{1/}.

$$PSI = 5.e^{-\left[\frac{\ln(M-M_0)}{8.515}\right]^5}$$

Where M = Measured Roughness Count (mm/km)
M₀ = 1,500 mm/km for A.C.
= 2,500 mm/km for S.T.
= 3,200 mm/km for P.M.

The PSI-roughness relationships are shown in Figure 8.3.3.

8.3.2 Design Standard

Horizontal and vertical alignments of the proposed links for rehabilitation are satisfactorily suitable for the respective design standard of the DOH. Therefore no improvement works of alignments were considered. However, carriageway and roadbed widths were checked through the field surveys and road inventory data. The carriageway and roadbed widths employed in the Study are as follows:

^{1/}: Method for Measuring Serviceability Index with the Mays Ride Meter. HRB Special Report 133.

Road Width by Proposed Link

| Road Class | Proposed Link | Carriageway and Roadbed (m) | | Remarks |
|------------|---------------------|-----------------------------|----------|---|
| | | Existing Width | Improved | |
| P2 | RH-1 | 7/10 | | |
| P3 | PH-2, RH-3 | 6/10 | | |
| S1 | RH-19, RH-20, RH-21 | 7/12 | | |
| S3 | RH-4, RH-5, RH-6 | | | |
| | RH-7, RH-8 | 6/8 | | |
| | RH-9, RH-10, RH-11 | | | |
| | RH-12 | 6/10 | | |
| | RH-13, RH-14 | 5/6 | 6/10 | Reconstruction 7th year ADT (1700 1900) |
| | RH-15, RH-16, RH-17 | 6/9 | | |
| | RH-18 | 6/8 | | |
| F4 | RH-22 | 5/8 | | |
| | RH-23, RH-24 | 6/8 | | |
| | RH-26 | 5/8 | 5.5/9 | Reconstruction |
| | RH-25, RH-27 | 5/7 | | |
| | RH-28 | 5.5/9 | | |

Typical cross sections for overlay and reconstruction works are shown in Figure 8.3.4.

8.3.3 Traffic Analysis

For the analysis of overlay thickness and calculation of rehabilitation benefits, traffic data were analyzed.

1) **Base Traffic and Growth Rate**

Traffic volumes surveyed by the DOH were available for past 10 years (1972 - 1981). Future traffic volumes by vehicle type were forecasted basing on the traffic volumes in 1981.

Growth rates of traffic in the Northeastern Region was adopted from the previous studies^{1/} which was slightly revised from the SRNT studies, as follows:

Traffic Growth Rate (% P.a.)

| <u>Year</u> | <u>Primary Highway</u> | | <u>Secondary Highway</u> | | <u>Provincial Paved Road</u> | |
|-------------|------------------------|----------|--------------------------|----------|------------------------------|----------|
| | <u>P</u> | <u>F</u> | <u>P</u> | <u>F</u> | <u>P</u> | <u>F</u> |
| 1982 - 1987 | 3.8 | 4.9 | 3.8 | 5.2 | 6.6 | 4.5 |
| 1978 - 2001 | 3.8 | 3.8 | 3.8 | 3.8 | 5.5 | 3.6 |

Note: P: Vehicles for passengers
 F: Vehicles for Freights

Forecasted traffic by proposed link is given in Appendix 8.2.

2) ESA^{2/} Conversion Factors

a) Gross Vehicle Weight Distribution

Gross vehicle weight distribution in the Northeastern Region was interpreted from the survey reports^{3/} of the DOH. Location of vehicle weight survey of the DOH is shown in Appendix 8.3.

As loads imposed by passenger cars do not contribute significantly to the structural damage of road pavements, medium and heavy trucks and buses were taken into the analyses. Gross vehicle weight distribution for 6-wheel trucks and 10-wheel trucks are shown in Appendix 8.4.

^{1/} : Increasing Rate of Traffic by Region (1982-2001), DOH.

^{2/} : ESA: Equivalent Standard 8,200 kg Axle Loads.

^{3/} : Loaded vehicle weighing survey-Northeast, Traffic Engineering Office, DOH, 1980.

b) Empty Ratio

For establishing the ESA, the share of unloaded vehicles must be known. According to the DOH's survey as shown in Appendix 8.4, the empty ratio is as unreasonably high as 80 % for 6-wheel trucks and 44 % for 10-wheel trucks.

The results of the Team's O/D Survey revealed that the vehicle empty ratio is around 40 % for 6-wheel trucks and 30 % for 10-wheel trucks as shown below.

Truck Empty Ratio (%)

| Location* | <u>Paved National Road</u> | | <u>Unpaved Provincial Road</u> | |
|-----------|----------------------------|-----------------|--------------------------------|-----------------|
| | <u>6-wheel</u> | <u>10-wheel</u> | <u>6-wheel</u> | <u>10-wheel</u> |
| 1 | 45(133) | 43(105) | | |
| 2 | | | 100(4) | |
| 3 | | | 38(11) | 100(3) |
| 4 | 40(194) | 35(159) | | |
| 5 | | | 46(11) | 67(3) |
| 6 | 35(95) | 31(112) | | |
| 7 | 48(33) | 10(44) | | |
| <hr/> | | | | |
| Weighted | | | | |
| Average | 41 | 33 | 51 | 83 |

() : No. of vehicles interviewed.

* : Location of survey is shown in Appendix 8.3.

From these two survey results, empty ratios for 6-wheel and 10-wheel trucks were decided as follows:

Truck Empty Ratio (%)

| | <u>6-wheel trucks</u> | <u>10-wheel trucks</u> |
|-----------------|-----------------------|------------------------|
| National Road | 40 | 35 |
| Provincial Road | 50 | 50 |

c) Traffic Equivalent Factor

Axle load distribution survey conducted by the DOH shows the share of rear axle(s) load increases as the increase of gross vehicle weight in both 6-wheel trucks and 10-wheel trucks as shown in Appendix 8.5. On the basis of the actual survey results, axle load distribution was calculated as shown in table of Appendix 8.5.

To use the flexible pavement design procedure described later, mixed traffic must be converted to an equivalent number of 8,200 kg single axle load.

To express varying axle loads in terms of a common denominator, it is necessary to develop traffic equivalence factors. The equivalence factors derived at AASHO Road Test were employed in this Study. They are shown in Appendix 8.6.

d) ESA Conversion Factors for Trucks

With the axle loads, axle loads conversion factors and gross vehicle weight distribution, equivalent standard 8,200 kg axle load number (ESA) was calculated for 6-wheel and 10-wheel trucks as given in Table 8.3.4.

e) ESA Conversion Factors for Buses

Average passenger occupancies for buses surveyed during the team's O/D Survey period are as follows:

Average Passenger Occupancies (%)

| Location* No. | Paved National Road | | Unpaved Provincial Road | |
|------------------|---------------------|---------|-------------------------|-------|
| | M / B | H / B | M / B | H / B |
| 1 | 26(21) | 40(114) | | |
| 2 | | | 5(8) | 0 |
| 3 | | | 31(9) | 0 |
| 4 | 19(92) | 38(114) | | |
| 5 | | | 19(8) | 0 |
| 6 | 19(74) | 35(50) | | |
| 7 | 27(38) | 42(16) | | |
| <hr/> | | | | |
| Weighted | | | | |
| Average | 21 | 39 | 19 | |

(): No. of buses interviewed.

* : Location of survey is shown in Appendix 8.3.

On the other hand, PRI study^{1/} indicates that average occupancies of medium and heavy buses are 18 and 27 respectively in the Northeastern Region.

Concerning the axle loading distribution for buses only limited data are available as given in the previous report^{1/}. It derives the ESA conversion factors for heavy buses as 0.61 on the basis of the actual load survey at the Eastern Bus Terminal in Bangkok.

f) Summary of ESA Conversion Factors

Summarizing the foregoing analyses, ESA conversion factors to be used for the Study are given in the following table:

^{1/}: Feasibility Study of Provincial Road Improvement, Louis Berger International, Inc. Dec. 1981.

ESA Conversion Factors

| Class | 6-wheel Truck _{1/} | 10-wheel Truck _{1/} | Heavy Bus |
|------------------|--------------------------------|---------------------------------|--------------|
| National Highway | 0.81 | 1.28 | 0.61 |
| Provincial Road | 0.68 | 0.99 | |

1/: Refer to Table 8.3.4 (a) - (d).

3) Cumulative Numbers of ESA

With the use of the foregoing conversion factors, cumulative numbers of ESA for respective traffic volumes were calculated by proposed link. They are shown in Appendix 8.7, separating past traffics and future traffics in the design period.

8.3.4 Overlay Design

1) Design Deflection

Deflection survey by the DOH has been conducted every 50 meter intervals. The method of deflection measurements is based on the WASHO (Western Association of State Highway Officials) method in principle. The deflection obtained by the WASHO procedures is a rebound deflection.

The deflection readings at the field survey must be corrected for the temperature variations and moisture fluctuations of the subgrade soils which will vary through the year. However, the DOH employs temperature adjustments only. For thicker pavement surfaces, temperature adjustments are made by the following formula in the DOH pavement design:

$$d = 0.0002" (90 - F_t)$$

Where, d : deflection adjustment (inch)

F_t : Pavement temperature ($^{\circ}$ F)

Those adjusted deflection values are treated every 1 km basis, viz, 20 deflection data for 1 km.

Although it is impossible to determine the true population mean and standard deviation deflection of a pavement section, the average and standard deviation obtained from a set of measured data are used to determine deflection values corresponding to the designated probability level. DOH employs the deflection level that only approximately 7 % of the overlay would be underdesigned and subject to distresses. Thus, the DOH has adopted the following value as design deflection in overlay design:

$$D_d = D + 1.5 \sigma$$

Where, D_d : Design deflection
D : Average deflection
 σ : Standard deviation

2) Comparative Studies on Overlay Design

To strengthen the distressed flexible pavements, various kinds of methods of overlay design have been introduced by different organizations. Those methods can be broadly classified into two groups:

- (a) Design method with the use of pavement deflection, and
- (b) Design method by pavement component analysis.

The design methods employed for the comparative analysis in the Study are as follows:

| | | | | |
|------------------|------------------------|---|-----------------------------------|---|
| Design Method | Pavement Deflection | { | Asphalt Institute Method | * |
| | | | Japan Road Associations Method | |
| | | | TRRL** Method | * |
| | | | TRRL Method in the Tropics | * |
| | | | Overlay Thickness Formula by Ruiz | * |
| | Pavement Component | { | Canada Method | |
| | | | California Method | * |
| | | | Asphalt Institute Method | |
| | | | Japan Road Associations Method | |

On the basis of the results of trial overlay designs using the methodologies mentioned above, five methods of them were selected for further comparative studies through the discussions with the DOH.

The selected five methods indicated with * mark are all deflection dependent methods as shown in deflection-life relationship chart (Figure 8.3.5).

The selected methods are briefly explained hereunder;

| Method | Traffics used for the Design | Tolerable Deflection and Thickness Design Charts |
|---|------------------------------|--|
| (A) Asphalt Institute ^{1/} | DTN ^{2/} | refer to Figure 8.3.6 (a) |
| (B) TRRL ^{3/} | ESA | Figure 8.3.6 (b) |
| (C) TRRL Tropics ^{4/} | ESA | Figure 8.3.6 (c) |
| (D) Ruiz's Formula ^{5/} | | Figure 8.3.6 (d) |
| (E) California Division of Highways ^{6/} | ESA TI ^{7/} | Figure 8.3.6 (e) |

** TRRL, Transport and Road Research Laboratory, United Kingdom

Note 1/ : The Asphalt Institute Manual NO. 17

2/ : DTN : Design Traffic Number

3/ : TRRL Report LR 571

4/ : TRRL Report LR 444

5/ : Highway Research Record 129

Ruiz's expression for calculating the necessary overlay thickness:

$$h = \frac{R}{0.434} \cdot \log \frac{D_o}{D_h}$$

Where, h : Overlay thickness (cm)

D_o : Deflection of existing pavement

D_h : Deflection after overlay construction

R : Deflection reduction factor (=12)

6/ : Highway Research Record 129

Percent reduction in deflection: (P)

$$P = \frac{dr - dt}{dr}$$

Where, dr = Design deflection

dt = Tolerable deflection

Increase in Gravel equivalence

Gravel thickness \longrightarrow AC thickness
(factor 1:2)

7/ : TI : Traffic Index

Using these method, overlay thickness computation was carried out for all proposed links every one kilometer basis. The results are shown in Appendix 8.8. Table 8.3.5 shows the computation results for RH-1 link, giving different overlay thicknesses by each method. It is due to the tolerable deflection criterion curves inherent to each design method.

Through the discussions with the DOH, method (E) established by California Division of Highways was employed among the methods owing to its conservative outcomes compared with other methods. This method is also employed by the DOH for pavement design incorporating slight modification to the derivation of traffic analysis.

3) Design of Overlay and Reconstruction

In order to establish the rehabilitation plans and measures, required overlay thickness calculated and roughness conditions together with existing geometric features of road were further refined. As the results, the sections of each link in Table 8.3.6 were deemed necessary to be either overlaid or reconstructed. Those links of RH-7, 8, 11 and 25 are required for neither overlay nor reconstruction during the design period due to their comparatively good deflection conditions. However, those links may be subject to the routine maintenance as the pavement surface deteriorates.

Figure 8.3.7 illustrates the overlay or reconstruction sections by proposed link. Reconstruction sections were introduced due to their considerably thick overlays required or narrow carriageway/roadbed widths.

As the Table 8.3.6 shows, link length required for rehabilitation measures are 468 km in total, 370 km for overlay and 98 km for reconstruction.

8.3.5 Work Quantities and Construction Cost

1) Work Quantity

With the results of overlay and reconstruction designs, work quantities were calculated basing on the typical cross sections shown in Figure 8.3.4. They are given in Appendix 8.9.

2) Construction Cost

Construction unit rates were established as given below, referring to the previous bidding rates in similar projects in Thailand.

Unit Rates For Major Work Items
(Reconstruction and Overlay)

| Work Item | Unit of Quantity | Financial Unit Rate (B) | Tax Component (%) | Remarks |
|--------------------------|------------------|-------------------------|-------------------|----------------------|
| Clearing and Grubbing | ha | 15,000 | 9 | |
| Embankment | m ³ | 45 | 9 | |
| Scarifying (A) | m ² | 20 | 10 | For Asphalt Concrete |
| Scarifying (B) | m ² | 7 | 10 | For DBST |
| Soil Aggregate Subbase | m ³ | 105 | 11 | |
| Crushed Stone Base | m ³ | 370 | 8 | |
| Soil Aggregate Shoulder | m ³ | 105 | 11 | |
| Tack Coat | m ² | 10 | 10 | |
| Asphalt Concrete Surface | | | | |
| T = 40 mm | m ² | 88 | 10 | |
| T = 50 mm | m ² | 110 | 10 | |
| T = 80 mm | m ² | 176 | 10 | |
| T = 100 mm | m ² | 220 | 10 | |
| T = 120 mm | m ² | 264 | 10 | |

Construction costs were calculated by applying unit rates to the respective work items.

Following rates of costs for miscellaneous works, physical contingencies and design/supervision are added to the direct construction cost:

Applied Rates for Cost Estimate

| | Overlay | Reconstruction |
|------------------------------------|---------|----------------|
| Miscellaneous ^{1/} | 3.5 | 7.0 |
| Physical Contingency ^{2/} | 15.0 | 15.0 |
| Design/Supervision ^{2/} | 8.0 | 10.0 |

^{1/} : Rate to construction cost of major work items

^{2/} : Rate to direct construction cost.

Construction cost by proposed link is summarized in Table 8.3.7 and detailed figures are given in Appendix 8.9.

8.4 ESTIMATION OF BENEFIT

8.4.1 Approach

The main benefit accrued from pavement rehabilitation is the savings of vehicle operating costs (VOCs) in case of with project. Valuation of VOCs on paved roads to be rehabilitated was made using the relationship between VOC and surface roughness developed in the Study.

From the PSI-Roughness relationship curves given in Figure 8.3.3, it was assumed that the roughnesses at the beginning stage of newly paved surface and at its terminal serviceability time are respectively 1,500 mm/km (PSI = 5) and 5,500 mm/km ($P_t^{1/} = 2.0$).

As the DOH employs the policy of pavement design for 7-year period, it was also assumed that the terminal serviceability ($P_t = 2.0$) would be brought approximately at 7th year after opening to traffic.

^{1/}: P_t : Terminal Serviceability Index

With these premises, roughness - time relationships for new pavement surface was derived as shown in Figure 8.4.1. In the case of without overlay, roughness in the design period was supposed to increase at the same rate of overlaid case.

8.4.2 Vehicle Operating Costs on Paved Roads

Vehicle operating costs on level tangent paved road mentioned in 7.5.3 are used in the Study, as follows:

Basic Vehicle Operating Costs

| <u>Vehicle</u> | <u>P/C</u> | <u>L/B*</u> | <u>H/B</u> | <u>L/T**</u> | <u>M/T</u> | <u>H/T</u> |
|----------------|------------|-------------|------------|--------------|------------|------------|
| VOCs (B/km) | 1.937 | 3.491 | 5.506 | 2.007 | 3.865 | 6.532 |

Note: * Including Light Bus and Medium Bus.

** Including Pick-up Truck and 4-wheel Truck.

For the purpose of estimation of VOC savings after overlaying in rehabilitation projects, it is required to elaborate a method to value VOC on paved roads more in detail corresponding to surface roughness.

By analyzing the results of the roughness and PSI survey, the previous TRRL'S Kenya Study and the SRNT, the relationship between roughness values and VOCs were derived. As a consequence, the following formula was obtained.

$$C = a \cdot R + b$$

where, C : Vehicle operating costs (B/km)

R : Roughness Value (mm/km)

| <u>Vehicle Type</u> | <u>a (10⁻⁴)</u> | <u>b</u> |
|---------------------|----------------------------|----------|
| P/C | 1.29 | 1.724 |
| L/B | 3.02 | 2.977 |
| H/B | 4.79 | 4.692 |
| L/T | 1.78 | 1.704 |
| M/T | 2.98 | 3.368 |
| H/T | 5.02 | 5.678 |

Using the above formula, VOCs on the existing paved roads to be rehabilitated and also on the overlaid roads were calculated according to their measured roughness values.

8.4.3 Vehicle Operating Costs Savings

VOCs savings were calculated for 7 years after completion of rehabilitation works. Forecasted traffic volumes for 6 types of vehicles as given in Appendix 8.2 were used for the analysis. VOCs savings by proposed link are given in Appendix 8.10.

8.5 ECONOMIC EVALUATION

8.5.1 Approach

Economic evaluation for 24 links out of 28 links originally proposed was performed under the usual benefit-cost analyses.

As work quantities of overlay works and reconstruction are relatively small, benefits were supposed to accrue at year of investment and for 7 years thereafter.

8.5.2 Evaluation and Ranking

The calculated IRR together with link characteristics are summarized in Table 8.5.1. As the table shows, 19 links were feasible in terms of IRR, more than 12 %, and 5 links were less than 12 %.

Following table shows IRR rankings for proposed links. It also shows disbenefits of VOCs savings in case that the project implementation is delayed for two years.

Ranking by IRR

| Link No. | Length (km) | IRR (%) | Amount of Disbenefit ^{1/} (10 ³ B) | Remarks |
|----------|----------------|------------|---|----------------------------|
| RH - 22 | 8 | 118.1 | 8,840 | Overlay |
| RH - 2 | 10 | 91.9 | 10,337 | " |
| RH - 18 | 30 | 82.8 | 27,914 | " |
| RH - 5 | 23 | 69.7 | 18,173 | " |
| RH - 15 | 44 | 56.8 | 28,537 | " |
| RH - 6 | 25 | 48.8 | 14,085 | " |
| RH - 16 | 14 | 43.1 | 7,645 | " |
| RH - 17 | 9 | 34.5 | 3,862 | " |
| RH - 23 | 16 | 34.5 | 13,584 | " |
| RH - 24 | 16 | 29.8 | 14,849 | " |
| RH - 19 | 46 | 28.9 | 40,520 | Overlay/ Reconstruction |
| RH - 4 | 9 | 27.9 | 3,298 | Overlay |
| RH - 20 | 6 | 25.7 | 7,145 | " |
| RH - 26 | 22 | 22.7 | 17,548 | Reconstruction |
| RH - 21 | 13 | 20.7 | 5,507 | Overlay |
| RH - 9 | 7 | 20.3 | 2,084 | " |
| RH - 10 | 5 | 19.6 | 3,302 | Reconstruction |
| RH - 1 | 28 | 13.3 | 7,124 | Overlay |
| RH - 28 | 18 | 13.1 | 3,876 | " |
| RH - 14 | 27 | 11.7 | 20,045 | Reconstruction |
| RH - 3 | 46 | 11.0 | 10,142 | Overlay |
| RH - 12 | 6 | 10.1 | 1,290 | " |
| RH - 13 | 24 | 9.9 | 17,129 | Reconstruction |
| RH - 27 | 16 | 7.3 | 2,518 | Overlay |

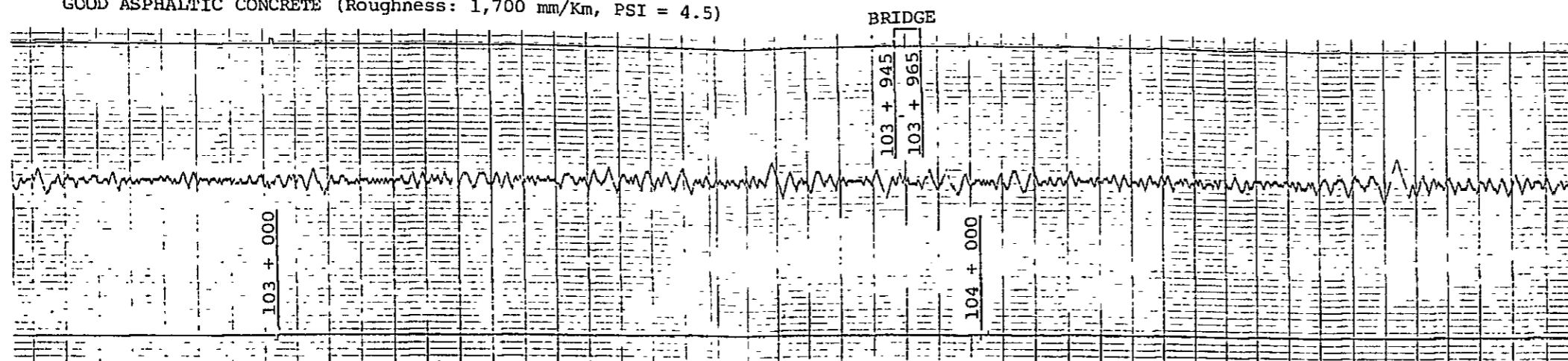
^{1/}: Disbenefits of VOCs Savings due to 2-years delay of implementation.

Figure 8.3.1 TYPICAL ROUGHNESS CHARTS

RH-2 (24-0500)

KP 103 ~ 104

GOOD ASPHALTIC CONCRETE (Roughness: 1,700 mm/Km, PSI = 4.5)

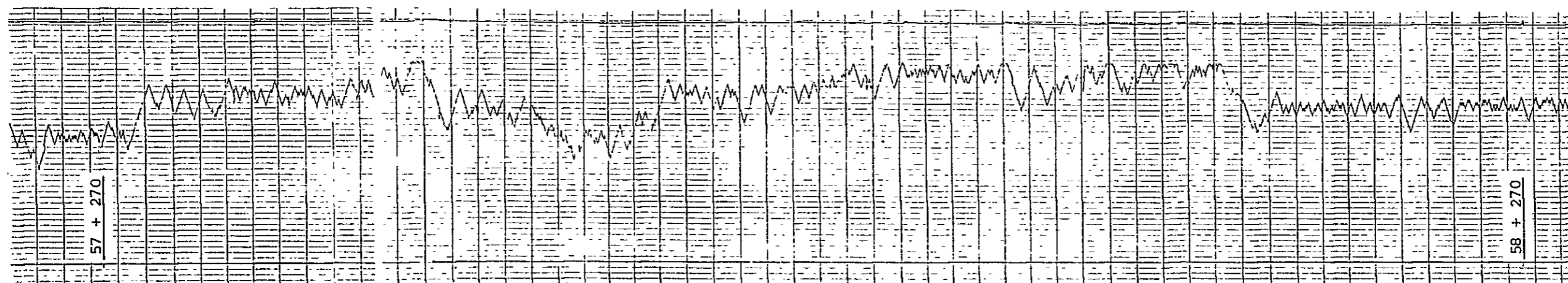


| K.P. | ROUGHNESS (mm/km) |
|------|----------------------|
| 102 | |
| 103 | 1597 |
| 104 | <u>1754</u> |
| 105 | 1744 |
| 106 | 2028 |
| 107 | 1632 |
| 108 | 2099 |
| 109 | 2215 |
| 110 | 1876 |

RH-19 (304-0800)

KP 57 ~ 58

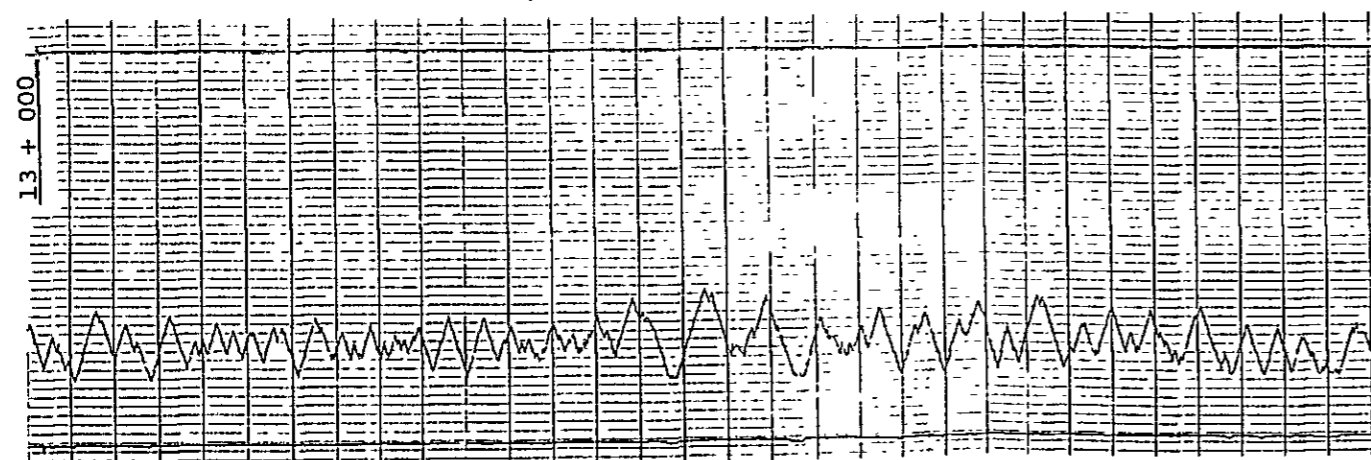
BAD ASPHALTIC CONCRETE (Roughness: 6,400 mm/Km, PSI = 1.9)



RH-13 (208-0100)

KP 13 ~ 14

FAILED SURFACE TREATMENT (Roughness: 5,900 mm/Km, PSI = 2.2)



RH-28 (2175-0100)

KP 0 ~ 1

GOOD SURFACE TREATMENT (Roughness: 2,700 mm/Km, PSI = 4.5)

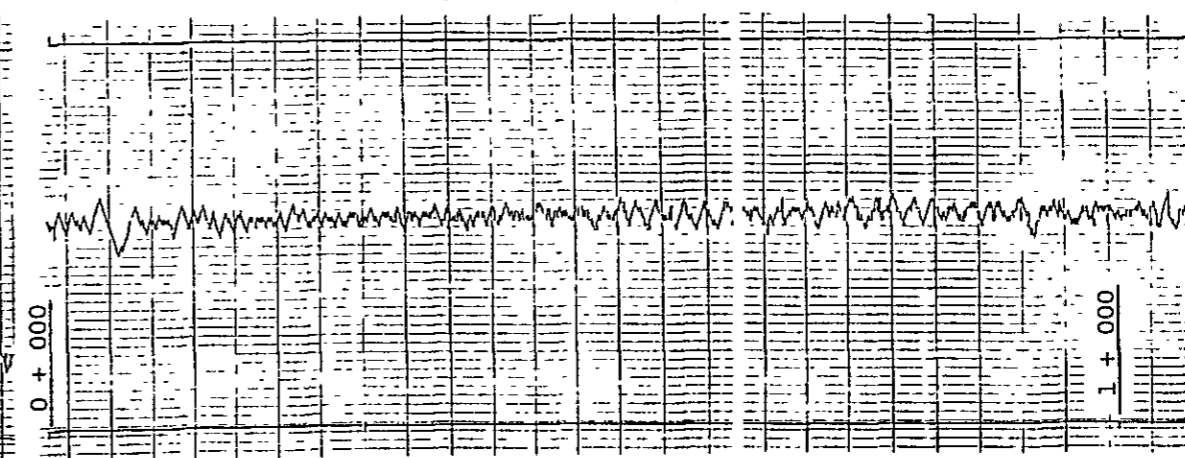


Table 8.3.1 LIST OF MEASURED ROUGHNESS FOR REHABILITATION LINKS

Table 8.3.1

| Route | Proposed Route | | | Origin | Destination | K.P. (Km) - (Km) | Roughness mm/km | | Remarks |
|-------|----------------|--------------|------------------|--------------------------|---------------------------|---------------------|-----------------------|--------------------|--|
| | Link | Surface Type | Link Length (Km) | | | | Average (\bar{R}) | Standard Deviation | |
| 24 | 200* | AC | 42 | J. to A.Chokchai | J. to A.Lamplaimat | 0 - 42 | 2094 | 353 | ** The very high standard deviation is due to the high variation of roughness. It is more proper to divide this link into 3 sections as follows: <u>Section 1 : km 102 - 111</u> $\bar{R} = 1919$ mm/km $S = 336$ mm/km <u>Section 2 : km 111 - 117</u> $\bar{R} = 7575$ mm/km $S = 464$ mm/km <u>Section 3 : km 117 - 138</u> $\bar{R} = 2048$ mm/km $S = 669$ mm/km |
| | 300* | AC | 32 | J. to A.Lamplaimat | J. to C.Buriram | 42 - 74 | 2406 | 509 | |
| | 400 | AC | 28 | A. Nang Rong | A. Prakhon Chai | 74 - 102 | 2637 | 703 | |
| | 500 | AC | 36 | A. Prakhon Chai | A. Prasat | 102 - 138 | 2909 | 2154** | |
| | 600 | AC | 50 | A. Prasat | A. Sangkha | 138 - 188 | 3174 | 1040 | |
| | 1001 | DT | 40 | A. Warin Chamrap | A. Det Udom | 0 - 40 | 2977 | 681 | |
| 201 | 100 | DT | 39 | A. Sikhui | A. Dan Khun Thot | 0 - 39 | 5022 | 1043 | |
| | 200 | DT | 25 | A. Dan Khun Thot | A. Nong Bua Khok | 39 - 64 | 4093 | 573 | |
| | 300 | DT | 17 | A. Nong Bua Khok | A. Chatturat | 64 - 81 | 5277 | 819 | |
| | 400 | DT | 38 | A. Chatturat | A. Chaiyaphum | 81 - 119 | 4888 | 676 | |
| 202 | 301* | PM | 15 | J. to A.Bua Yai | Nakhon Ratchasima 1 Dist. | 51 - 66 | 4897 | 420 | |
| | 400* | PM | 19 | J.B. Sida | J.A. Prathai | 66 - 85 | 5168 | 426 | |
| | 500 | DT | 40 | A. Prathai | A. Phrayakkhamphum Phisai | 10 - 50 | 3754 | 547 | |
| 207 | 100 | DT | 37 | B. Wat | A. Prathai | 448 - 485 | 4553 | 565 | |
| 207 | 202 | DT | 35 | A. Prathai | A. Nong Song Hong | 485 - 498 | 4191 | 667 | |
| 208 | 100 | DT | 31 | A. Tha Phra | A. Kosum Phisai | 0 - 31 | 4296 | 793 | |
| | 200 | DT | 29 | A. Kosum Phisai | C. Maha Sarakham | 31 - 60 | 5026 | 1466 | |
| 213 | 100 | DT | 44 | C. Maha Sarakham | A. Kalasin | 0 - 44 | 4019 | 870 | |
| 214 | 100 | DT | 28 | A. Kalasin | B. Lam Chai | 0 - 28 | 3610 | 513 | |
| | 200 | DT | 19 | A. Lam Chai | C. Roi Et | 28 - 47 | 3661 | 889 | |
| | 800 | PM | 30 | C. Surin | A. Prasat | 0 - 30 | 4238 | 837 | |
| | 900* | PM | 40 | J.R. 24 (A.Prasat) | Chong Chom | 29 - 69 | 3447 | 570 | |
| 219 | 100* | PM | 19 | J.R. 24 (A.Prakhon Chai) | B. Salang Thon | 25 - 44 | 4129 | 549 | |
| | 200* | PM | 25 | B. Saland Thon | J. Buri Ram Dist. Off. | 0 - 25 | 3906 | 657 | |
| 304 | 800 | AC | 46 | A. Buphai | B. Takhop | 55 - 101 | 4164 | 1408 | |
| | 902 | AC | 6 | (Bypass) | A. Pak Thong Chai | 101 - 107 | 4615 | 854 | |
| | 904 | AC | 26 | A. Pak Thong Chai | (Route 2) | 107 - 133 | 2423 | 1170 | |
| 2023 | 100 | PM | 8 | B. Nam Kong | A. Si That | 0 - 8 | 3711 | 523 | |
| 2039 | 101 | DT | 16 | A. Nam Phong | A. Kranuan | 0 - 16 | 4394 | 851 | |
| | 102 | DT | 17 | A. Nam Phong | A. Kranuan | 16 - 33 | 4666 | 699 | |
| 2057 | 100* | AC | 23 | J.R. 2 (A.Ban Phai) | A. Mancha Khiri | 0 - 23 | 1676 | 258 | |
| 2071 | 100 | DT | 28 | A. Chokchai | A. Khonburi | 0 - 28 | 5397 | 572 | |
| 2109 | 100 | DT | 24 | A. Nam Phong | A. Ubolratana Dam | 0 - 24 | 7608 | 1731 | |
| 2160 | 100 | DT | 20 | B. Wat | A. Kong | 0 - 20 | 4638 | 2087 | |
| 2175 | 100 | DT | 34 | B. Wang Hin | A. Chum Phuang | 0 - 34 | 2940 | 554 | |

* Additional roughness survey was carried out to these links.

Table 8.3.2 RATING ITEMS ON PAVEMENT CONDITION SURVEY

| <u>Pavement Deficiency</u> | <u>Description</u> |
|--|--|
| Rutting/Waves | <ul style="list-style-type: none"> ● Longitudinal depressions that form under traffic in the wheel paths and have a minimum length of approximately 6 meters/Longitudinal or transverse undulations in the surface of the pavement, consisting of alternate valleys and crests approximately 60 cm or more apart. |
| Cracking (Longitudinal/ Transverse) | <ul style="list-style-type: none"> ● A crack or break in the pavement surface. (Approximately parallel to centerline/at right angles to centerline) |
| Cracking (Alligator/ Block) | <ul style="list-style-type: none"> ● Interconnected or interlaced cracks forming a series of small polygons that resemble an alligator's hide./ Interconnected cracks forming a series of large polygons usually with sharp corners or angles. |
| Pothole | <ul style="list-style-type: none"> ● Bowl-shape hole of various sizes in the pavement. |
| Bump | <ul style="list-style-type: none"> ● Localized upward displacement of the pavement. |
| Bleeding | <ul style="list-style-type: none"> ● Free bitumen on the surface of the pavement. |
| Shoving | <ul style="list-style-type: none"> ● Displacement or bulging of paving material in the direction of loading or pressure. |
| <u>Other items taken into ratings</u> | |
| Driving Comfort, Speed Change Cycle due to Surface Defects | <ul style="list-style-type: none"> ● Owing to the various pavement deficiencies as indicated above, operating speed is interrupted thus giving discomfort to passengers. |
| Patching | <ul style="list-style-type: none"> ● Partially rehabilitated area with asphaltic materials. |

Figure 8.3.2

Figure 8.3.2 PSI RATING FORM

| THE ROADS DEVELOPMENT STUDY IN THE NORTHEASTERN REGION IN THE KINGDOM OF THAILAND | | PAVEMENT CONDITION RATING | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|---|--|--|---|---|---|---|---|---|---|---|---|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|--|
| FROM : TO : | | DISTRICT ROUTE : LINK : | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| PAVEMENT TYPE : AC <input type="checkbox"/> PM <input type="checkbox"/> ST <input type="checkbox"/> | | DATE : | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RATING 1 Driving Comfort 2 Speed Change Cycle due to surface condition 3 Patching 4 Rutting 5 Longitudinal or Transvers Cracking 6 Alligator Cracking 7 Pot hole 8 Bumping 9 Bleeding 10 Shoving | <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <th style="width: 16.6%;">5</th> <th style="width: 16.6%;">4</th> <th style="width: 16.6%;">3</th> <th style="width: 16.6%;">2</th> <th style="width: 16.6%;">1</th> <th style="width: 16.6%;">0</th> </tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td><td> </td></tr> <tr><td> </td><td> </td><td> </td><td> </td><td> </td><td> </td></tr> </table> | | | | | 5 | 4 | 3 | 2 | 1 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 5 | 4 | 3 | 2 | 1 | 0 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| Summation of Points _____ ÷ 10 = Ride Rating <input style="width: 40px;" type="text"/> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| <u>REMARK</u> | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Table 8.3.3 ROUGHNESS AND PSI

| Route | Section Km | Roughness (mm/Km) | PSI | | | |
|-------------|-------------|----------------------|-----------|-----------|-----------|-----------|
| | | | Average | Range | | |
| AC | 24 - 0200* | 10 - 20 | 1880 | 4.32 | 4.2 ~ 4.5 | |
| | | 25 - 30 | 2656 | 3.30 | 3.2 ~ 3.5 | |
| | 0300* | 45 - 60 | 2508 | 3.58 | 3.1 ~ 3.9 | |
| | | 0400 | 75 - 85 | 2707 | 3.36 | 3.2 ~ 3.6 |
| | | 0500 | 101 - 111 | 1919 | 4.20 | 4.1 ~ 4.4 |
| | 304 - 0800 | 111 - 117 | 7575 | 1.58 | 1.3 ~ 1.7 | |
| | | 120 - 130 | 2111 | 4.00 | 4.0 | |
| | | 57 - 67 | 5823 | 1.80 | 1.7 ~ 1.9 | |
| | | 67 - 73 | 5370 | 2.08 | 1.9 ~ 2.3 | |
| | | 78 - 88 | 3127 | 3.40 | 3.2 ~ 3.6 | |
| | | 88 - 92 | 4476 | 2.72 | 2.6 ~ 2.9 | |
| | | 0902 | 102 - 107 | 4661 | 2.84 | 2.5 ~ 3.1 |
| | 0904 | 115 - 125 | 1698 | 4.42 | 4.3 ~ 4.6 | |
| | 2057 - 0100 | 0 - 23 | 1680 | 4.48 | 4.4 ~ 4.7 | |
| | ST | 201 - 0200 | 45 - 55 | 3858 | 3.46 | 3.4 ~ 3.5 |
| 0300 | | | 70 - 80 | 5850 | 2.82 | 2.7 ~ 3.0 |
| 202 - 0500 | | 14 - 24 | 3761 | 3.70 | 3.5 ~ 3.9 | |
| 207 - 0100 | | 450 - 470 | 4338 | 3.24 | 3.0 ~ 3.3 | |
| | | 0202 | 484 - 498 | 4237 | 3.44 | 3.1 ~ 3.8 |
| 208 - 0100 | | 15 - 25 | 4319 | 2.40 | 2.2 ~ 2.7 | |
| | | 0200 | 35 - 45 | 5173 | 2.16 | 1.9 ~ 2.4 |
| | | 49 - 55 | 6912 | 1.72 | 1.4 ~ 2.3 | |
| 213 - 0100 | | 0 - 10 | 4365 | 3.32 | 3.0 ~ 3.7 | |
| | | 29 - 38 | 3254 | 3.98 | 3.8 ~ 4.1 | |
| 214 - 0100 | | 0 - 10 | 3824 | 3.06 | 2.5 ~ 3.5 | |
| | | 14 - 24 | 3144 | 3.96 | 3.9 ~ 4.2 | |
| | | 0200 | 33 - 45 | 3235 | 3.40 | 3.3 ~ 3.5 |
| 2039 - 0101 | | 0 - 16 | 4395 | 3.04 | 3.0 ~ 3.1 | |
| | | 0102 | 16 - 33 | 4667 | 3.24 | 3.2 ~ 3.4 |
| 2071 - 0100 | | 0 - 28 | 5398 | 2.80 | 2.7 ~ 2.9 | |
| 2109 - 0100 | | 0 - 24 | 7608 | 1.76 | 1.3 ~ 2.0 | |
| 2160 - 0100 | 0 - 10 | 3533 | 2.70 | 2.6 ~ 2.8 | | |
| | 12 - 19 | 5007 | 2.52 | 2.4 ~ 3.0 | | |
| PM | 202 - 0301* | 51 - 66 | 4897 | 3.48 | 3.4 ~ 3.8 | |
| | 214 - 0800 | 10 - 20 | 4378 | 2.73 | 2.6 ~ 2.8 | |
| | | 20 - 25 | 5554 | 2.92 | 2.6 ~ 3.2 | |
| | | 0900 | 30 - 50 | 3472 | 4.10 | 3.8 ~ 4.2 |
| | 219 - 0100* | 43 - 25 | 4152 | 3.54 | 3.4 ~ 3.8 | |
| | | 0200* | 3 - 17 | 3491 | 4.12 | 3.9 ~ 4.2 |
| | | 18 - 23 | 4729 | 3.66 | 3.1 ~ 4.0 | |

* : Those links are not included in the proposed links.

Figure 8.3.3

Figure 8.3.3 PSI VERSUS ROUGHNESS BY SURFACE TYPE

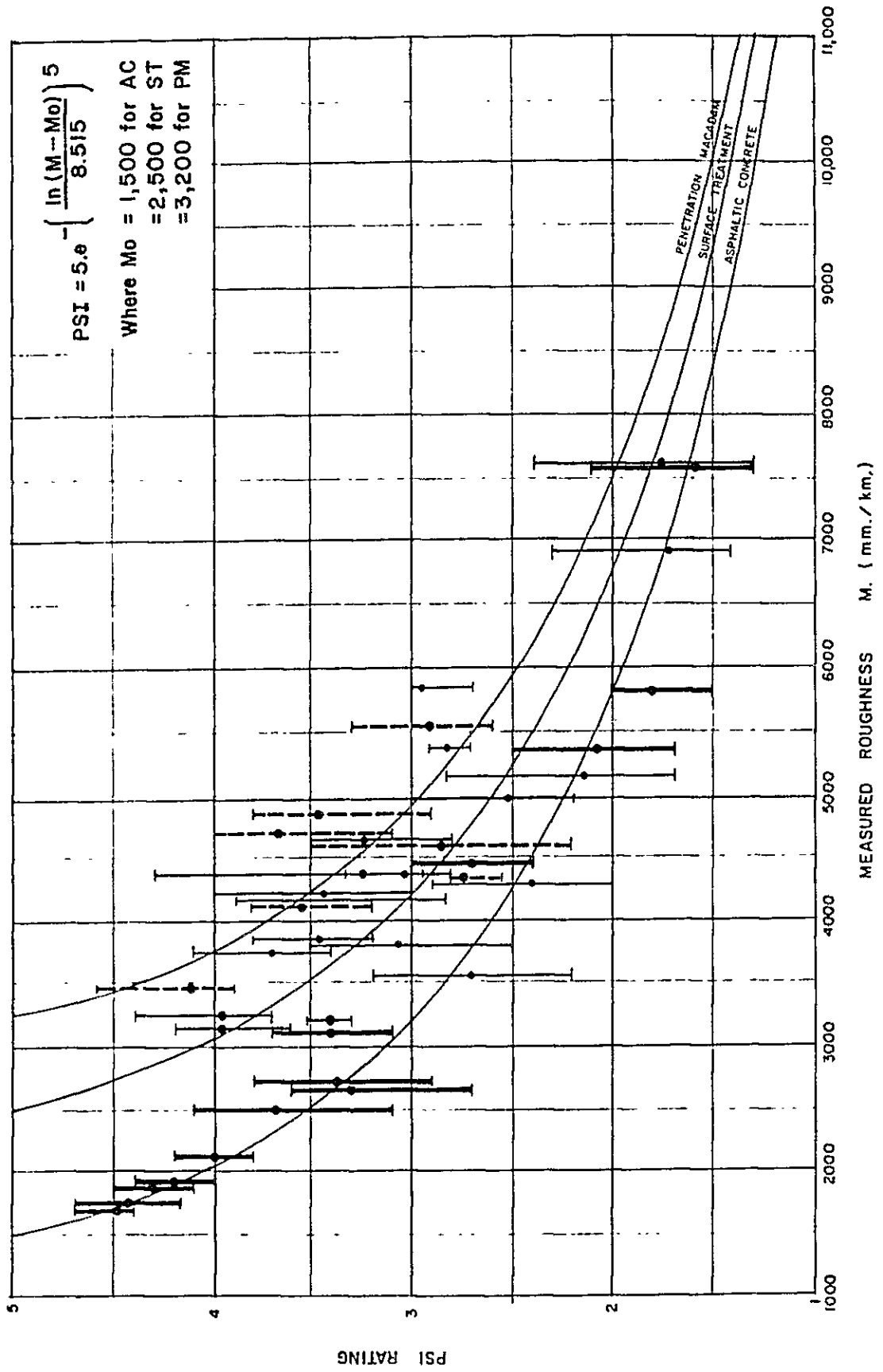
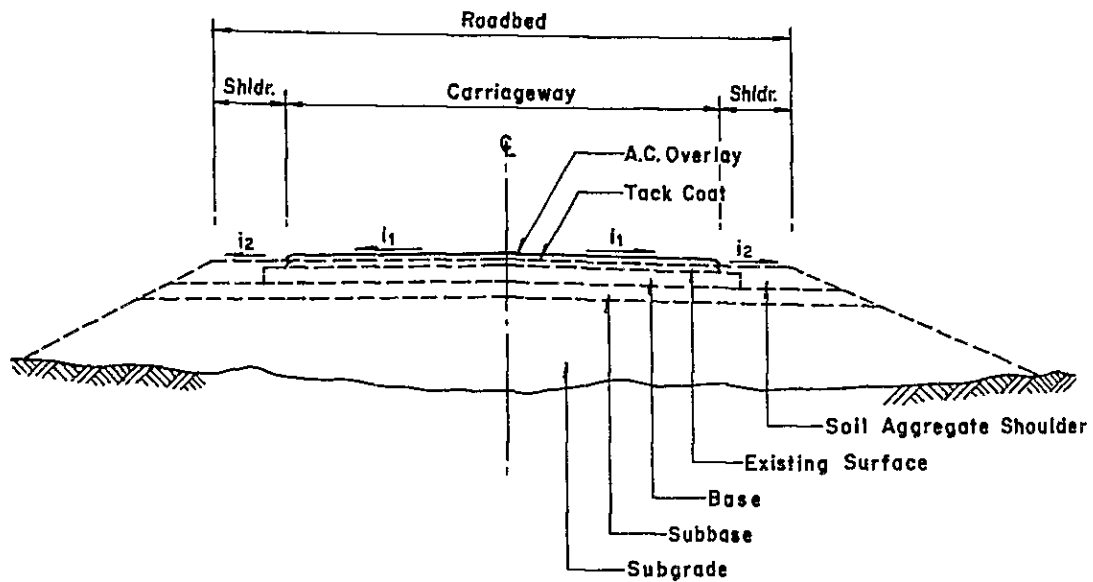


Figure 8.3.4 TYPICAL OVERLAY AND RECONSTRUCTION SECTIONS

OVERLAY



RECONSTRUCTION

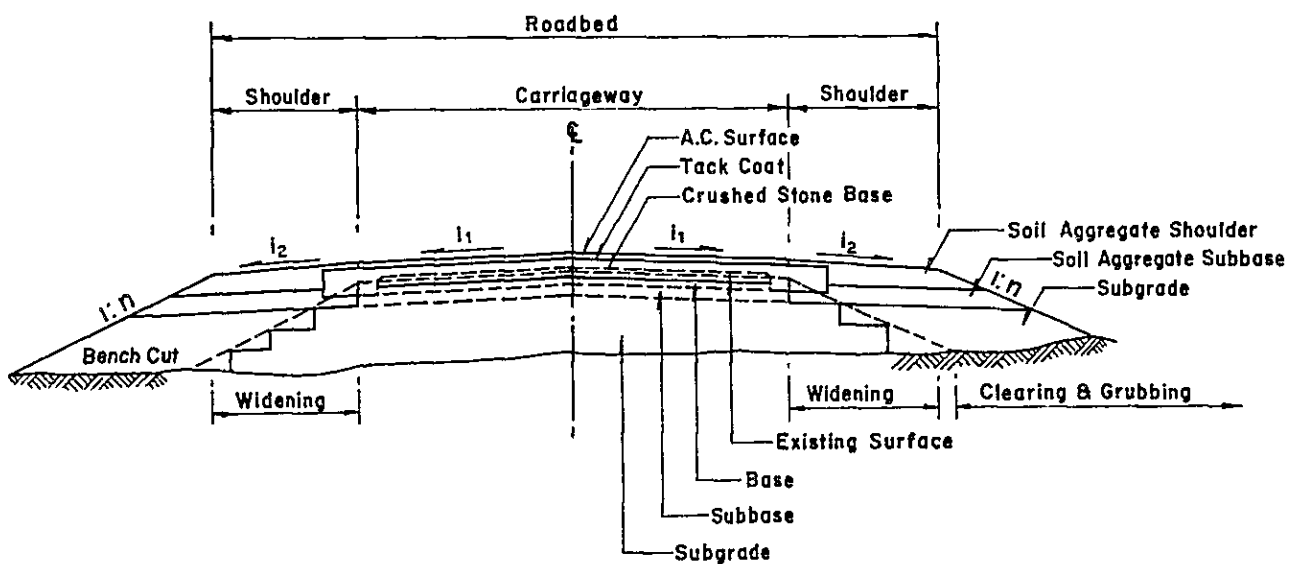


Table 8.3.4(a)Table 8.3.4(a) ESA CONVERSION FACTORS

6-Wheel Trucks (National Road)

| Gross Weight (ton) | Axle load (ton) | | Equivalence Factor | | | Frequency | E S A |
|--------------------|-----------------|-------|--------------------|-------|--------|-----------|--------|
| | Front | Rear | Front | Rear | Total | (%) | Factor |
| 4 | 1.68 | 2.32 | 0.0024 | 0.006 | 0.0084 | 40.0 | 0.336 |
| 5 | 1.95 | 3.05 | 0.0036 | 0.015 | 0.0186 | 1.555 | 0.029 |
| 6 | 2.16 | 3.84 | 0.0048 | 0.038 | 0.0428 | 2.938 | 0.126 |
| 7 | 2.38 | 4.62 | 0.0065 | 0.085 | 0.0915 | 5.187 | 0.475 |
| 8 | 2.56 | 5.44 | 0.0082 | 0.183 | 0.1912 | 7.081 | 1.354 |
| 9 | 2.75 | 6.25 | 0.0103 | 0.335 | 0.3453 | 7.431 | 2.566 |
| 10 | 2.90 | 7.10 | 0.0125 | 0.55 | 0.5625 | 9.330 | 5.248 |
| 11 | 3.08 | 7.92 | 0.0157 | 0.87 | 0.8857 | 6.564 | 5.814 |
| 12 | 3.24 | 8.76 | 0.0190 | 1.35 | 1.369 | 5.360 | 7.338 |
| 13 | 3.45 | 9.55 | 0.025 | 2.00 | 2.025 | 3.626 | 7.343 |
| 14 | 3.64 | 10.36 | 0.030 | 2.90 | 2.93 | 6.226 | 18.242 |
| 15 | 3.77 | 11.23 | 0.035 | 4.15 | 4.185 | 2.077 | 8.692 |
| 16 | 3.87 | 12.13 | 0.040 | 6.00 | 6.04 | 1.383 | 8.353 |
| 17 | 4.01 | 12.99 | 0.045 | 8.30 | 8.345 | 0.344 | 2.871 |
| 18 | 4.14 | 13.86 | 0.053 | 11.10 | 11.153 | 0.381 | 4.249 |
| 19 | 4.33 | 14.67 | 0.064 | 14.20 | 14.264 | 0.277 | 3.951 |
| 20 | 4.52 | 15.48 | 0.078 | 18.20 | 18.278 | 0.245 | 4.478 |
| Total | | | | | | 100 | 81.465 |
| Factor | | | | | | | 0.81 |

Table 8.3.4 (b) ESA CONVERSION FACTORS

6-Wheel Trucks (Provincial Road)

| Gross Weight (ton) | Axle load (ton) | | Equivalence Factor | | | Frequency (%) | E S A Factor |
|--------------------|-----------------|-------|--------------------|-------|--------|---------------|--------------|
| | Front | Rear | Front | Rear | Total | | |
| 4 | 1.68 | 2.32 | 0.0024 | 0.006 | 0.0084 | 50.0 | 0.420 |
| 5 | 1.95 | 3.05 | 0.0036 | 0.015 | 0.0186 | 1.296 | 0.024 |
| 6 | 2.16 | 3.84 | 0.0048 | 0.038 | 0.0428 | 2.448 | 0.105 |
| 7 | 2.38 | 4.62 | 0.0065 | 0.085 | 0.0915 | 4.323 | 0.396 |
| 8 | 2.56 | 5.44 | 0.0082 | 0.183 | 0.1912 | 5.900 | 1.128 |
| 9 | 2.75 | 6.25 | 0.0103 | 0.335 | 0.3453 | 6.192 | 2.138 |
| 10 | 2.90 | 7.10 | 0.0125 | 0.55 | 0.5625 | 7.775 | 4.373 |
| 11 | 3.08 | 7.92 | 0.0157 | 0.87 | 0.8857 | 5.470 | 4.845 |
| 12 | 3.24 | 8.76 | 0.0190 | 1.35 | 1.369 | 4.466 | 6.114 |
| 13 | 3.45 | 9.55 | 0.025 | 2.00 | 2.025 | 3.022 | 6.119 |
| 14 | 3.64 | 10.36 | 0.030 | 2.90 | 2.93 | 5.188 | 15.201 |
| 15 | 3.77 | 11.23 | 0.035 | 4.15 | 4.185 | 1.731 | 7.244 |
| 16 | 3.87 | 12.13 | 0.040 | 6.00 | 6.04 | 1.152 | 6.958 |
| 17 | 4.01 | 12.99 | 0.045 | 8.30 | 8.345 | 0.287 | 2.395 |
| 18 | 4.14 | 13.86 | 0.053 | 11.10 | 11.153 | 0.318 | 3.547 |
| 19 | 4.33 | 14.67 | 0.064 | 14.20 | 14.264 | 0.230 | 3.281 |
| 20 | 4.52 | 15.48 | 0.078 | 18.20 | 18.278 | 0.205 | 3.747 |
| Total | | | | | | 100 | 68.035 |
| Factor | | | | | | | 0.68 |

Table 8.3.4 (c)

Table 8.3.4 (c) ESA CONVERSION FACTORS

10-Wheel Trucks (National Road)

| Gross Weight (ton) | Axle load (ton) | | Equivalence Factor | | | Frequency (%) | E S A Factor |
|--------------------|-----------------|-------|--------------------|--------|--------|---------------|--------------|
| | Front | Rear | Front | Rear | Total | | |
| 8 | 2.83 | 5.17 | 0.0115 | 0.0158 | 0.027 | 35.0 | 0.945 |
| 9 | 2.98 | 6.02 | 0.0138 | 0.027 | 0.041 | 0.163 | 0.007 |
| 10 | 3.08 | 6.92 | 0.0158 | 0.044 | 0.060 | 0.325 | 0.020 |
| 11 | 3.18 | 7.82 | 0.0178 | 0.067 | 0.085 | 0.598 | 0.051 |
| 12 | 3.24 | 8.76 | 0.0188 | 0.103 | 0.122 | 0.761 | 0.093 |
| 13 | 3.32 | 9.68 | 0.0205 | 0.153 | 0.174 | 0.924 | 0.161 |
| 14 | 3.36 | 10.64 | 0.022 | 0.22 | 0.242 | 1.086 | 0.263 |
| 15 | 3.41 | 11.59 | 0.023 | 0.31 | 0.333 | 1.574 | 0.524 |
| 16 | 3.42 | 12.58 | 0.023 | 0.43 | 0.453 | 2.114 | 0.958 |
| 17 | 3.45 | 13.55 | 0.024 | 0.6 | 0.624 | 3.955 | 2.468 |
| 18 | 3.46 | 14.54 | 0.024 | 0.82 | 0.844 | 7.806 | 6.588 |
| 19 | 3.48 | 15.52 | 0.025 | 1.1 | 1.125 | 12.633 | 14.212 |
| 20 | 3.48 | 16.52 | 0.025 | 1.41 | 1.435 | 12.900 | 18.512 |
| 21 | 3.51 | 17.49 | 0.026 | 1.8 | 1.826 | 5.419 | 9.895 |
| 22 | 3.52 | 18.48 | 0.026 | 2.35 | 2.376 | 1.952 | 4.638 |
| 23 | 3.54 | 19.46 | 0.0265 | 3.0 | 3.027 | 2.277 | 6.892 |
| 24 | 3.55 | 20.45 | 0.027 | 3.8 | 3.827 | 2.004 | 7.669 |
| 25 | 3.60 | 21.40 | 0.029 | 4.6 | 4.629 | 2.277 | 10.540 |
| 26 | 3.64 | 22.36 | 0.03 | 5.7 | 5.73 | 2.654 | 15.207 |
| 27 | 3.73 | 23.27 | 0.033 | 6.8 | 6.833 | 1.900 | 12.983 |
| 28 | 3.81 | 24.19 | 0.036 | 8.0 | 8.036 | 0.976 | 7.843 |
| 29 | 3.86 | 25.14 | 0.039 | 9.4 | 9.439 | 0.436 | 4.115 |
| 30 | 3.90 | 26.10 | 0.04 | 11.2 | 11.24 | 0.215 | 2.417 |
| 31 | 3.94 | 27.06 | 0.043 | 13.0 | 13.043 | 0.052 | 0.678 |
| Total | | | | | | 100 | 127.679 |
| Factor | | | | | | | 1.28 |

Table 8.3.4(d) ESA CONVERSION FACTORS

10-Wheel Trucks (Provincial Road)

| Gross Weight (ton) | Axle load (ton) | | Equivalence Factor | | | Frequency (%) | E S A Factor |
|-----------------------|-----------------|-------|--------------------|--------|--------|------------------|-----------------|
| | Front | Rear | Front | Rear | Total | | |
| 8 | 2.83 | 5.17 | 0.0115 | 0.0158 | 0.027 | 50.0 | 1.35 |
| 9 | 2.98 | 6.02 | 0.0138 | 0.027 | 0.041 | 0.125 | 0.005 |
| 10 | 3.08 | 6.92 | 0.0158 | 0.044 | 0.060 | 0.250 | 0.015 |
| 11 | 3.18 | 7.82 | 0.0178 | 0.067 | 0.085 | 0.460 | 0.039 |
| 12 | 3.24 | 8.76 | 0.0188 | 0.103 | 0.122 | 0.585 | 0.071 |
| 13 | 3.32 | 9.68 | 0.0205 | 0.153 | 0.174 | 0.711 | 0.124 |
| 14 | 3.36 | 10.64 | 0.022 | 0.22 | 0.242 | 0.836 | 0.202 |
| 15 | 3.41 | 11.59 | 0.023 | 0.31 | 0.333 | 1.211 | 0.403 |
| 16 | 3.42 | 12.58 | 0.023 | 0.43 | 0.453 | 1.626 | 0.737 |
| 17 | 3.45 | 13.55 | 0.024 | 0.6 | 0.624 | 3.042 | 1.898 |
| 18 | 3.46 | 14.54 | 0.024 | 0.82 | 0.844 | 6.005 | 5.068 |
| 19 | 3.48 | 15.52 | 0.025 | 1.1 | 1.125 | 9.718 | 10.933 |
| 20 | 3.48 | 16.52 | 0.025 | 1.41 | 1.435 | 9.923 | 14.240 |
| 21 | 3.51 | 17.49 | 0.026 | 1.8 | 1.826 | 4.168 | 7.611 |
| 22 | 3.52 | 18.48 | 0.026 | 2.35 | 2.376 | 1.501 | 3.566 |
| 23 | 3.54 | 19.46 | 0.0265 | 3.0 | 3.027 | 1.751 | 5.300 |
| 24 | 3.55 | 20.45 | 0.027 | 3.8 | 3.827 | 1.541 | 5.897 |
| 25 | 3.60 | 21.40 | 0.029 | 4.6 | 4.629 | 1.751 | 8.105 |
| 26 | 3.64 | 22.36 | 0.03 | 5.7 | 5.73 | 2.042 | 11.701 |
| 27 | 3.73 | 23.27 | 0.033 | 6.8 | 6.833 | 1.461 | 9.983 |
| 28 | 3.81 | 24.19 | 0.036 | 8.0 | 8.036 | 0.751 | 6.035 |
| 29 | 3.86 | 25.14 | 0.039 | 9.4 | 9.439 | 0.335 | 3.162 |
| 30 | 3.90 | 26.10 | 0.04 | 11.2 | 11.24 | 0.165 | 1.855 |
| 31 | 3.94 | 27.06 | 0.043 | 13.0 | 13.043 | 0.040 | 0.522 |
| Total | | | | | | 100 | 98.822 |
| Factor | | | | | | | 0.99 |

Figure 8.3.5

DEFLECTION - PAVEMENT LIFE RELATIONSHIP

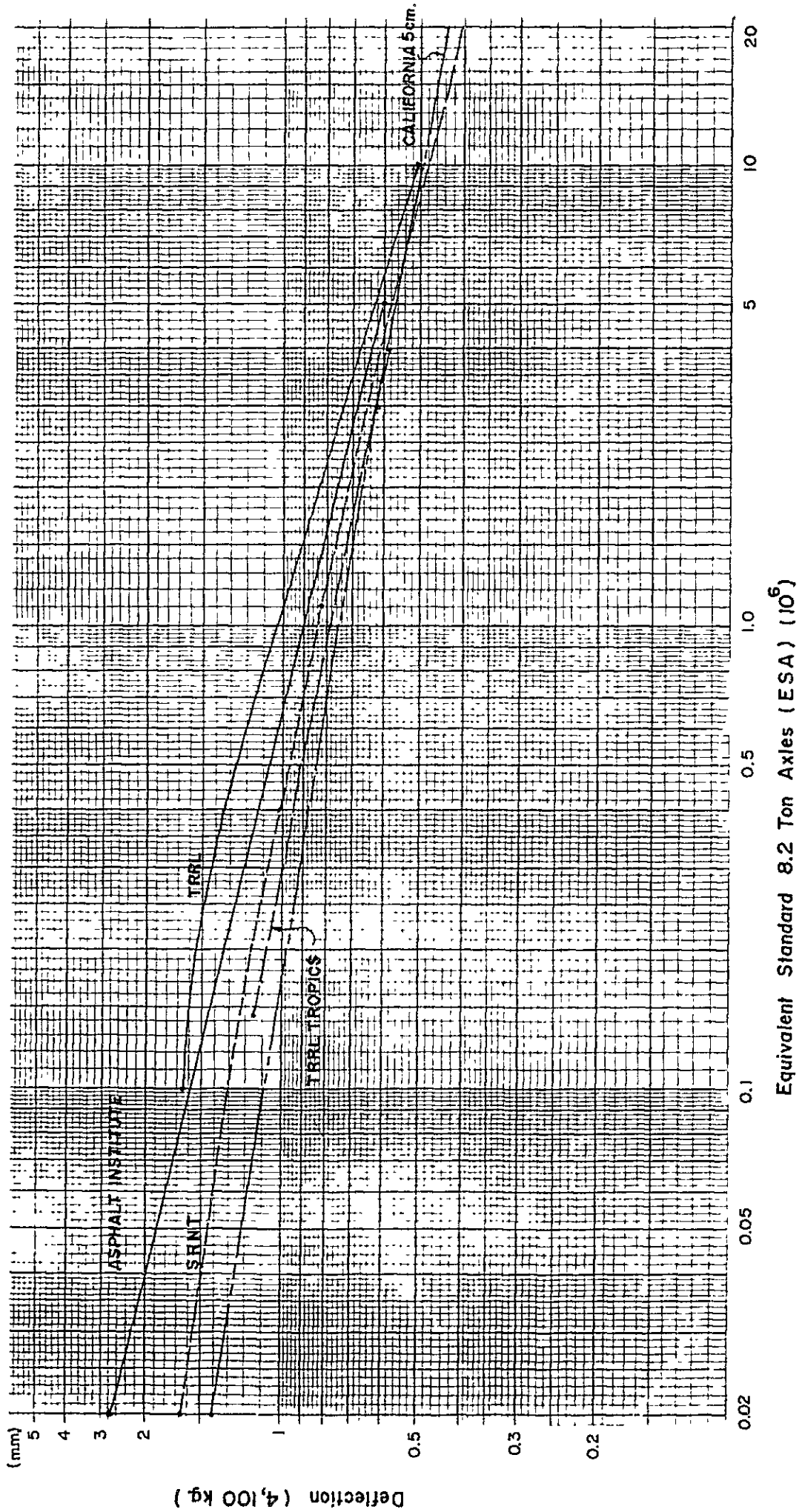
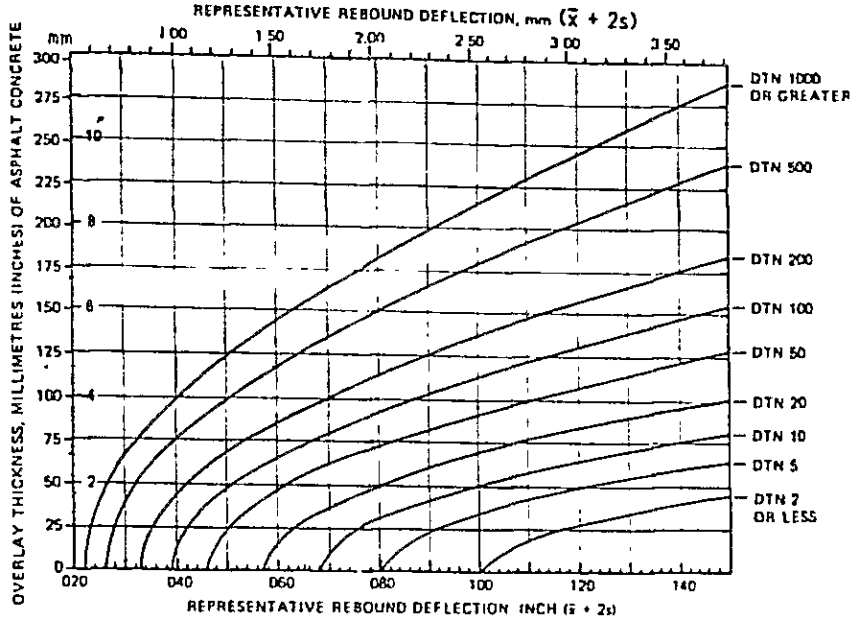
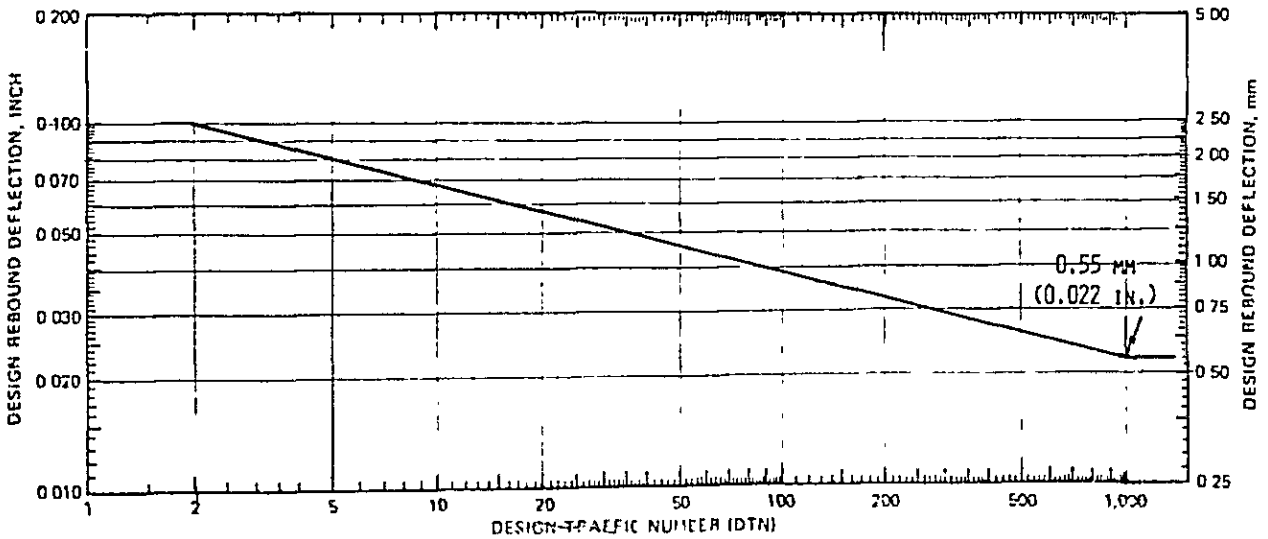


Figure 8.3.6(a) OVERLAY DESIGN -- ASPHALT INSTITUTE METHOD



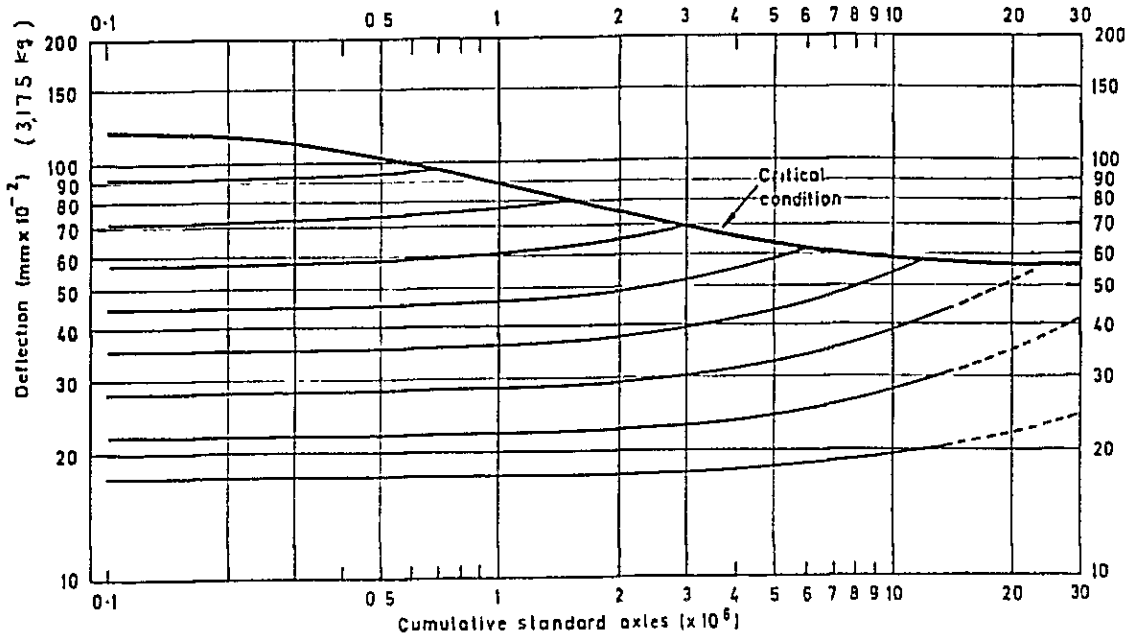
Asphalt concrete overlay thickness required to reduce pavement deflection from a measured to a design deflection value (rebound test).



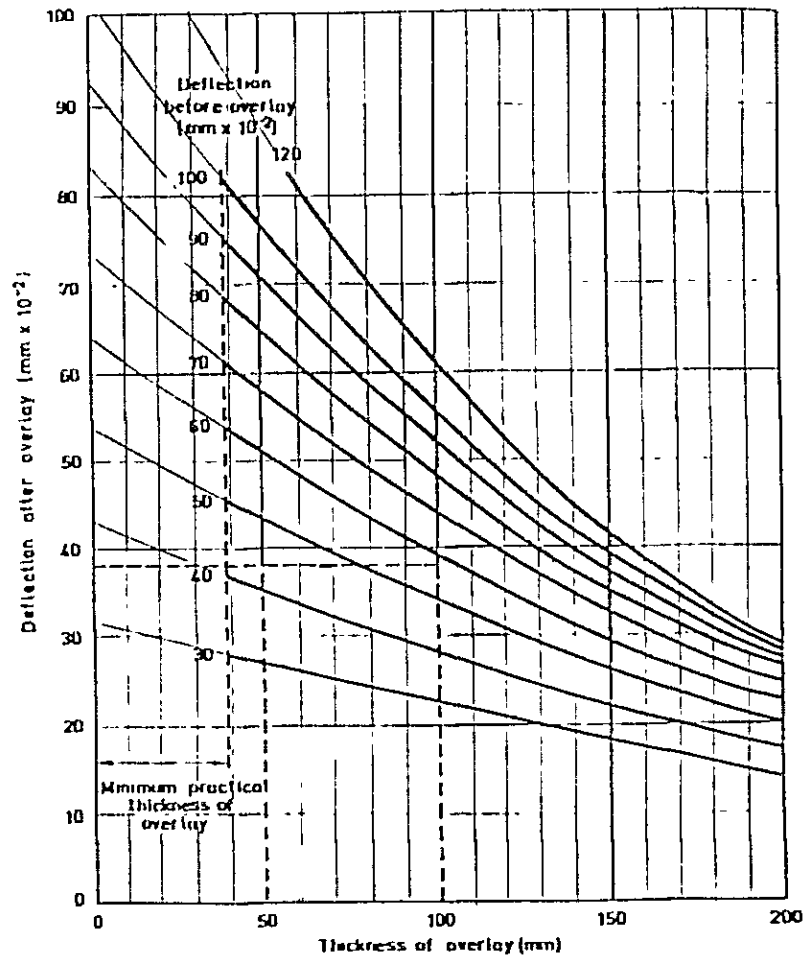
Design Rebound Deflection Chart

Figure 8.3.6(b)

Figure 8.3.6(b) OVERLAY DESIGN -- TRRL METHOD

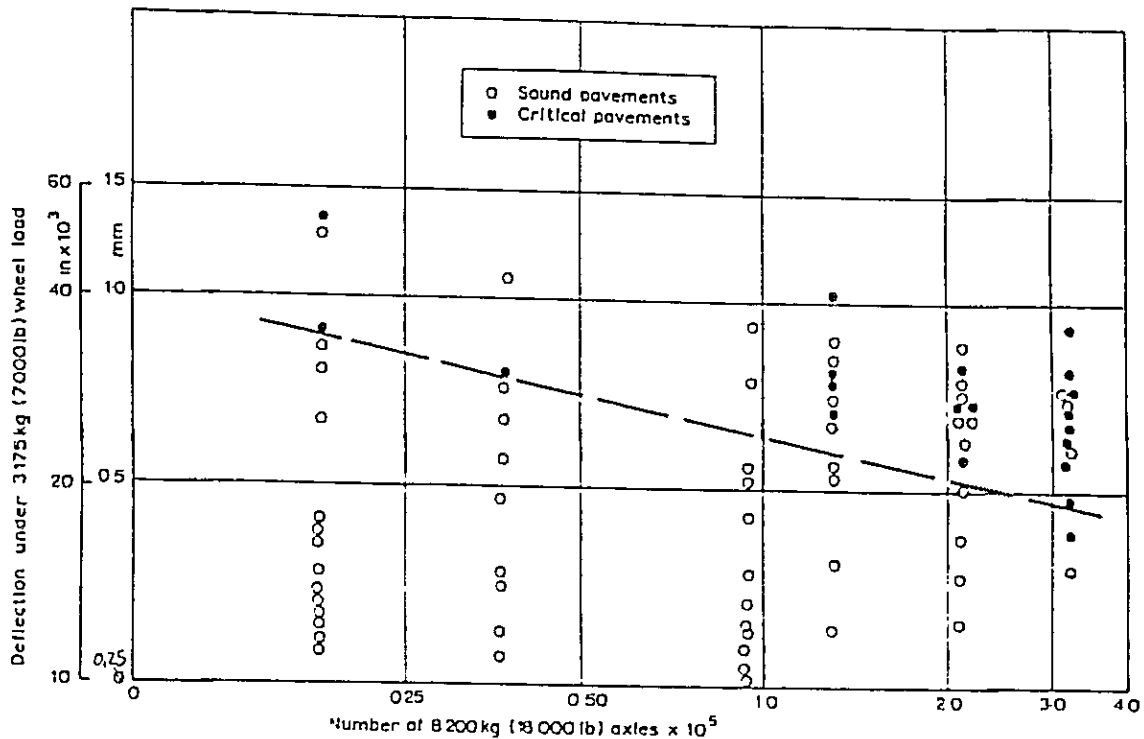


DEFLECTION-LIFE RELATIONSHIPS FOR PAVEMENTS WITH UNBOUND-BASES

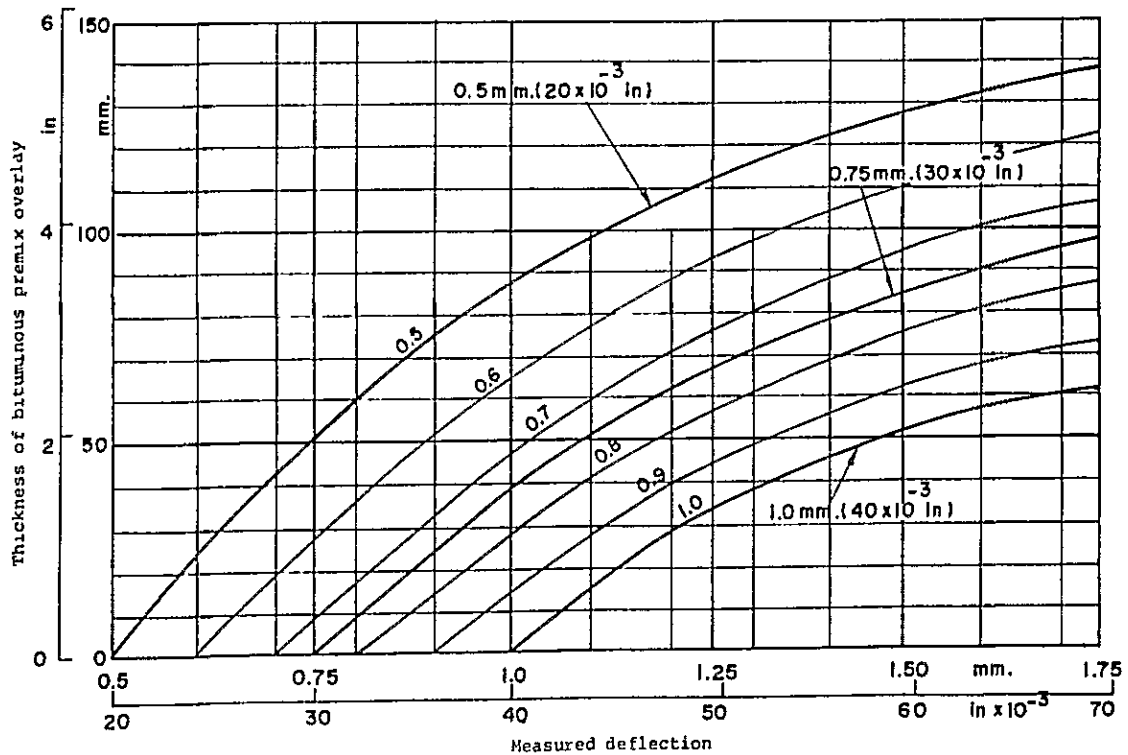


OVERLAY DESIGN CHART

Figure 8.3.6(c) OVERLAY DESIGN -- TRRL METHOD IN THE TROPICS



TENTATIVE DEFLECTION CRITERION CURVE FOR 75-10-100 mm (3 TO 4 in) BITUMEN MACADAM SURFACINGS ON CRUSHED STONE BASES IN A WT TROPICAL ENVIRONMENT



THE THICKNESS OF BITUMINOUS PREMIX OVERLAY REQUIRED TO REDUCE THE DEFLECTION OF A PAVEMENT TO DESIGNATED VALUES

Figure 8.3.6(d)

Figure 8.3.6(d) OVERLAY DESIGN -- RUIZ'S FORMULA

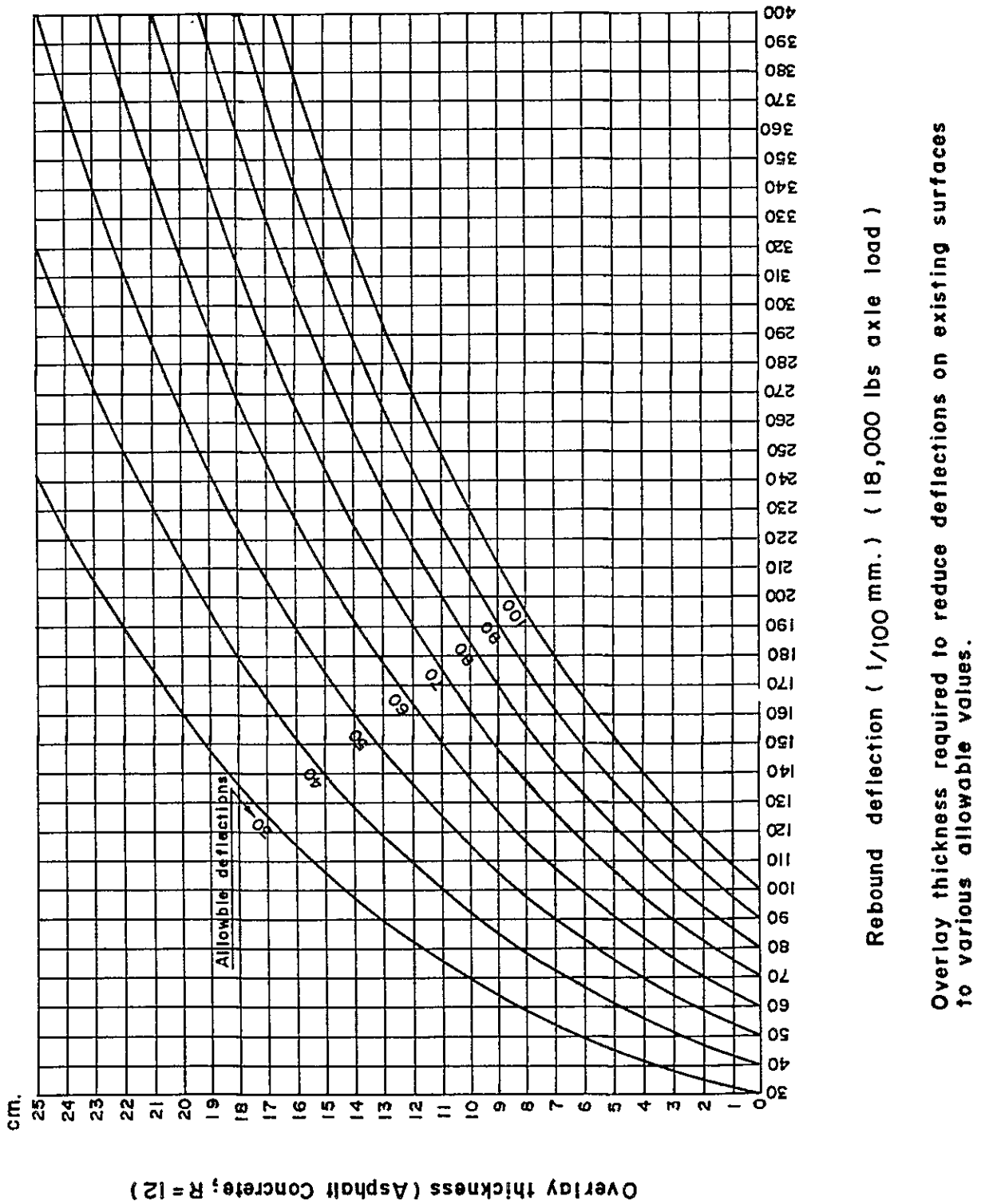
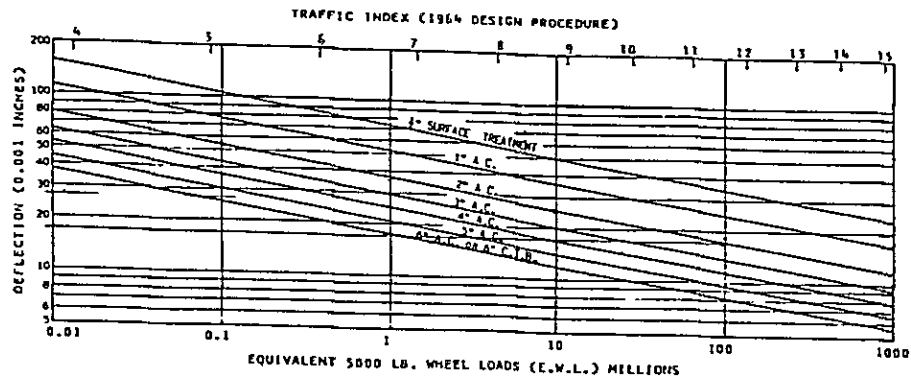
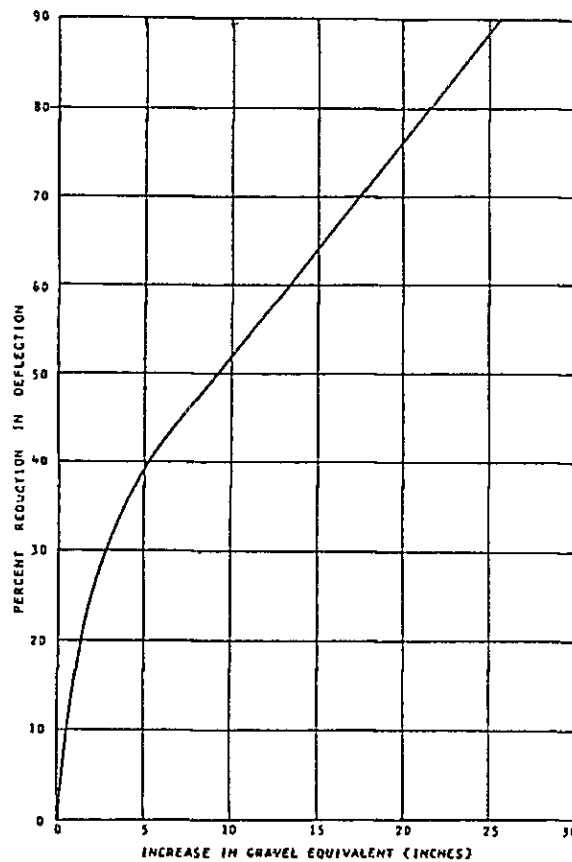


Figure 8.3.6(e) OVERLAY DESIGN -- CALIFORNIA DIVISION OF HIGHWAYS' METHOD



Variation in Tolerable Deflection Based on A.C. Fatigue Tests, California Method of Overlay Design



Reduction in Deflection Resulting from Pavement Reconstruction, California Method of Overlay Design

Table 8.3.5 COMPARATIVE STUDIES ON OVERLAY DESIGN

RH-1(24-0400)

| Section (Km.) - (Km.) | Average Deflection \bar{X} (m.m.) | Standard Deviation σ (m.m.) | Design Deflection $\bar{X} + 1.5\sigma$ (m.m.) | Roughness (10^3 mm/Km.) | | | | | | | | Overlay Thickness (mm) | | | | | Remarks. | |
|--------------------------|---|--|--|----------------------------|---|---|---|---|----|----|----|------------------------|----|----|----|--|----------|--|
| | | | | 0 | 2 | 4 | 6 | 8 | A1 | A2 | B | C | D | E | | | | |
| 74 - 75 | 0.6433 | 0.2704 | 1.0490 | | | | | | | 28 | 45 | 12 | 32 | 30 | 31 | | | |
| 75 - 76 | 0.7241 | 0.2095 | 1.0383 | | | | | | | 26 | 40 | 0 | 31 | 28 | 30 | | | |
| 76 - 77 | 0.7881 | 0.2606 | 1.1790 | | | | | | | 44 | 57 | 30 | 47 | 44 | 49 | | | |
| 77 - 78 | 0.5560 | 0.2330 | 0.9056 | | | | | | | 0 | 23 | * | 13 | 13 | 14 | | | |
| 78 - 79 | 0.5040 | 0.1922 | 0.7922 | | | | | | | 0 | 0 | * | 0 | 0 | 3 | | | |
| 79 - 80 | 0.5394 | 0.2037 | 0.8449 | | | | | | | 0 | 3 | * | 3 | 4 | 8 | | | |
| 80 - 81 | 0.5970 | 0.2038 | 0.9027 | | | | | | | 0 | 19 | * | 12 | 12 | 14 | | | |
| 81 - 82 | 0.6136 | 0.1564 | 0.8433 | | | | | | | 0 | 0 | * | 3 | 4 | 8 | | | |
| 82 - 83 | 0.7940 | 0.1665 | 1.0437 | | | | | | | 27 | 38 | 10 | 32 | 28 | 31 | | | |
| 83 - 84 | 0.5625 | 0.1367 | 0.7675 | | | | | | | 0 | 0 | * | 0 | 0 | 0 | | | |
| 84 - 85 | 0.8525 | 0.1415 | 1.0648 | | | | | | | 30 | 39 | 12 | 34 | 31 | 34 | | | |
| 85 - 86 | 0.7019 | 0.1961 | 0.9960 | | | | | | | 18 | 34 | 0 | 25 | 21 | 24 | | | |
| 86 - 87 | 0.9562 | 0.1740 | 1.2171 | | | | | | | 48 | 56 | 33 | 51 | 47 | 57 | | | |
| 87 - 88 | 0.7802 | 0.1445 | 0.9969 | | | | | | | 18 | 31 | 0 | 25 | 22 | 24 | | | |
| 88 - 89 | 0.7038 | 0.1146 | 0.8758 | | | | | | | 0 | 0 | * | 8 | 9 | 11 | | | |
| 89 - 90 | 0.6090 | 0.1342 | 0.8103 | | | | | | | 0 | 0 | * | 0 | 0 | 4 | | | |
| 90 - 91 | 0.8868 | 0.1601 | 1.1570 | | | | | | | 42 | 51 | 26 | 45 | 42 | 46 | | | |
| 91 - 92 | 0.6376 | 0.0953 | 0.7806 | | | | | | | 0 | 0 | * | 0 | 0 | 2 | | | |
| 92 - 93 | 0.7700 | 0.1607 | 1.0110 | | | | | | | 20 | 34 | 0 | 27 | 25 | 26 | | | |
| 93 - 94 | 0.6913 | 0.1150 | 0.8638 | | | | | | | 0 | 0 | * | 7 | 7 | 10 | | | |
| 94 - 95 | 0.7548 | 0.1105 | 0.9205 | | | | | | | 0 | 13 | 0 | 14 | 13 | 15 | | | |
| 95 - 96 | 0.7370 | 0.3539 | 1.2678 | | | | | | | 53 | 67 | 39 | 56 | 53 | 67 | | | |
| 96 - 97 | 0.6917 | 0.1160 | 0.8658 | | | | | | | 0 | 0 | * | 7 | 8 | 10 | | | |
| 97 - 98 | 0.6539 | 0.1147 | 0.8279 | | | | | | | 0 | 0 | * | 0 | 0 | 7 | | | |
| 98 - 99 | 0.5870 | 0.1466 | 0.8068 | | | | | | | 0 | 0 | * | 0 | 0 | 4 | | | |
| 99 - 100 | 0.5817 | 0.1526 | 0.8107 | | | | | | | 0 | 0 | * | 0 | 0 | 5 | | | |
| 100 - 101 | 0.6327 | 0.1687 | 0.8857 | | | | | | | 0 | 11 | * | 9 | 10 | 12 | | | |
| 101 - 102 | 0.5470 | 0.0602 | 0.6373 | | | | | | | 0 | 0 | * | * | 0 | 0 | | | |

Note;

A1; Asphalt Institute Method
(Design Def. $\bar{X} + 1.5\sigma$)

A2; Asphalt Institute Method
(Design Def. $\bar{X} + 2.0\sigma$)

B; TRRL Method

C; TRRL in the Tropics Method

D; Ruiz's Formula

E; California Method

* Pavement failure within design period is not foreseen.

Table 8.3.6 REHABILITATION MEASURES

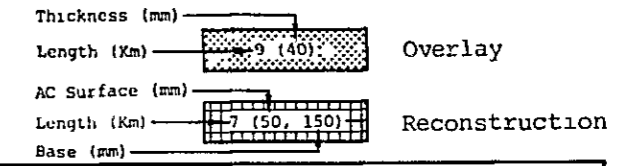
| Link No. | Km.-Km. | Length (Km) | Calculated Thickness ₁ / (mm) | Planned Thickness ₂ / (mm) | Roughness ₁ / (mm/km) | Rehabilitation Measures |
|--------------|-----------|-------------|--|---------------------------------------|----------------------------------|-------------------------|
| RH - 1 | 74 - 102 | 28 | 20 | 40 | 2,620 | Overlay |
| RH - 2 | 102 - 104 | 2 | 14 | 40 | 1,680 | Overlay |
| | 110 - 118 | 8 | 3 | 40 | 6,520 | Overlay |
| RH - 3 | 140 - 186 | 46 | 27 | 40 | 3,170 | Overlay |
| RH - 4 | 26 - 35 | 9 | 7 | 40 | 2,990 | Overlay |
| RH - 5 | 4 - 21 | 17 | 6 | 40 | 5,510 | Overlay |
| | 33 - 39 | 6 | 28 | 40 | 4,770 | Overlay |
| RH - 6 | 39 - 64 | 25 | 32 | 40 | 4,100 | Overlay |
| RH - 7* | | | | | | |
| RH - 8* | | | | | | |
| RH - 9 | 31 - 38 | 7 | 11 | 40 | 3,690 | Overlay |
| RH - 10 | 0 - 5 | 5 | 70 | 50(150) | | Reconstruction |
| RH - 11* | | | | | | |
| RH - 12 | 488 - 494 | 6 | 8 | 40 | 4,070 | Overlay |
| RH - 13 | 7 - 31 | 24 | 38 | 50(250) | 4,350 | Reconstruction |
| RH - 14 | 31 - 58 | 27 | 66 | 50(230) | 5,030 | Reconstruction |
| RH - 15 | 0 - 44 | 44 | 12 | 40 | 4,010 | Overlay |
| RH - 16 | 3 - 12 | 9 | 19 | 40 | 3,770 | Overlay |
| | 23 - 28 | 5 | 42 | 50 | 3,970 | Overlay |
| RH - 17 | 28 - 37 | 9 | 32 | 40 | 4,200 | Overlay |
| RH - 18 | 0 - 30 | 30 | 35 | 40 | 4,240 | Overlay |
| RH - 19 | 55 - 75 | 20 | 126 | 50(300) | 5,330 | Reconstruction |
| | 75 - 101 | 26 | 58 | 50 | 3,310 | Overlay |
| RH - 20 | 101 - 107 | 6 | 129 | 120 | 4,480 | Overlay |
| RH - 21 | 107 - 120 | 13 | 43 | 50 | 2,560 | Overlay |
| RH - 22 | 0 - 8 | 8 | 35 | 40 | 3,710 | Overlay |
| RH - 23 | 0 - 16 | 16 | 72 | 80 | 4,400 | Overlay |
| RH - 24 | 16 - 32 | 16 | 95 | 100 | 4,670 | Overlay |
| RH - 25* | | | | | | |
| RH - 26 | 0 - 22 | 22 | 39 | 50(240) | 7,590 | Reconstruction |
| RH - 27 | 0 - 16 | 16 | 29 | 40 | 4,160 | Overlay |
| RH - 28 | 0 - 7 | 7 | 25 | 40 | 3,040 | Overlay |
| | 14 - 25 | 11 | 32 | 40 | 3,160 | Overlay |
| Total | | 468 | | | | |

Note: 1/ : Figures indicate the average of the section.

2/ : Figures indicate AC thickness for Overlay and AC surface and crushed rock base for Reconstruction.

* : No rehabilitation works are required within the design period.

Figure 8.3.7 OVERLAY/RECONSTRUCTION SECTIONS BY PROPOSED LINK



| Proposed Link No. | Route | Link | Origin | Destination | Length (km) | Length (km) | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-------------------|-------|------|-------------------|-------------------------|-------------|-----------------|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|--|--|--|--|
| | | | | | | 2 | 4 | 6 | 8 | 10 | 12 | 14 | 16 | 18 | 20 | 22 | 24 | 26 | 28 | 30 | 32 | 34 | 36 | 38 | 40 | 42 | 44 | 46 | 48 | | | | |
| RH- 1 | 24 | 400 | A. Nang Rong | A. Prakhon Chai | 28 | K.P. 74 to 102 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH- 2 | 24 | 500 | A. Prakhon Chai | A. Prasat | 36 | K.P. 102 to 138 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH- 3 | 24 | 600 | A. Prasat | A. Sangkha | 50 | K.P. 138 to 188 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH- 4 | 24 | 1001 | A. Warin Chamrap | A. Det Udom | 40 | K.P. 0 to 40 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH- 5 | 201 | 100 | A. Si Khiu | A. Dan Khun Thot | 39 | K.P. 0 to 39 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH- 6 | 201 | 200 | A. Dan Khun Thot | A. Nong Bua Khok | 25 | K.P. 39 to 64 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH- 7 | 201 | 300 | A. Nong Bua Khok | A. Chatturat | 17 | K.P. 64 to 81 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH- 8 | 201 | 400 | A. Chatturat | C. Chaiyaphum | 38 | K.P. 81 to 119 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH- 9 | 202 | 500 | A. Prathai | A. Phayakkhaphum Phisai | 40 | K.P. 10 to 50 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-10 | 206 | 100 | (Route 2) | A. Phimai | 5 | K.P. 0 to 5 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-11 | 207 | 100 | B. Wat | A. Prathai | 37 | K.P. 448 to 485 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-12 | 207 | 202 | A. Prathai | A. Nong Song Hong | 13 | K.P. 485 to 498 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-13 | 208 | 100 | A. Tha Phra | A. Kosum Phisai | 31 | K.P. 0 to 31 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-14 | 208 | 200 | A. Kosum Phisai | C. Maha Sarakham | 29 | K.P. 31 to 60 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-15 | 213 | 100 | C. Maha Sarakham | C. Kalasin | 44 | K.P. 0 to 44 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-16 | 214 | 100 | C. Kalasin | B. Lum Chai | 28 | K.P. 0 to 28 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-17 | 214 | 200 | A. Lam Nam Chi | C. Roi Et | 19 | K.P. 28 to 47 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-18 | 214 | 800 | C. Surin | A. Prasat | 30 | K.P. 0 to 30 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-19 | 304 | 800 | A. Buphai | B. Takhop | 46 | K.P. 55 to 101 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-20 | 304 | 902 | (By Pass) | A. Pak Thong Chai | 6 | K.P. 101 to 107 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-21 | 304 | 904 | A. Pak Thong Chai | (Route 2) | 26 | K.P. 107 to 133 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-22 | 2023 | 100 | B. Nam Kong | A. Si That | 8 | K.P. 0 to 8 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-23 | 2039 | 101 | A. Nam Phong | A. Kranuan | 16 | K.P. 0 to 16 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-24 | 2039 | 102 | A. Nam Phong | A. Kranuan | 17 | K.P. 16 to 33 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-25 | 2071 | 100 | A. Chok Chai | A. Khonburi | 28 | K.P. 0 to 28 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-26 | 2109 | 100 | A. Nam Phong | A. Ubonratana Dam | 24 | K.P. 0 to 24 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-27 | 2160 | 100 | B. Wat | A. Kong | 20 | K.P. 0 to 20 | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| RH-28 | 2175 | 100 | B. Wang Hin | A. Chum Phuang | 34 | K.P. 0 to 34 | | | | | | | | | | | | | | | | | | | | | | | | | | | |

Table 8.3.7 SUMMARY OF REHABILITATION COSTS

| Link No. | Link Length (km) | Rehabilitation Costs | | Remarks |
|----------|------------------|-------------------------------|------------------------------|----------------|
| | | Financial (10 ⁶ B) | Economic (10 ⁶ B) | |
| RH - 1 | 28 | 22.5 | 20.3 | Overlay |
| RH - 2 | 10 | 7.5 | 6.8 | " |
| RH - 3 | 46 | 34.5 | 31.1 | " |
| RH - 4 | 9 | 6.8 | 6.2 | " |
| RH - 5 | 23 | 17.3 | 15.6 | " |
| RH - 6 | 25 | 18.7 | 16.9 | " |
| RH - 9 | 7 | 5.3 | 4.8 | " |
| RH - 10 | 5 | 8.6 | 7.8 | Reconstruction |
| RH - 12 | 6 | 4.5 | 4.1 | Overlay |
| RH - 13 | 24 | 60.0 | 54.4 | Reconstruction |
| RH - 14 | 27 | 65.9 | 59.8 | " |
| RH - 15 | 44 | 33.0 | 29.8 | Overlay |
| RH - 16 | 14 | 11.3 | 10.2 | " |
| RH - 17 | 9 | 6.8 | 6.2 | " |
| RH - 18 | 30 | 22.5 | 20.3 | " |
| RH - 19 | 26 | 29.2 | 26.3 | " |
| - 19 | 20 | 52.9 | 48.0 | Reconstruction |
| RH - 20 | 6 | 15.7 | 14.2 | Overlay |
| RH - 21 | 13 | 13.9 | 12.5 | " |
| RH - 22 | 8 | 5.0 | 4.5 | " |
| RH - 23 | 16 | 24.4 | 22.0 | " |
| RH - 24 | 16 | 29.8 | 26.8 | " |
| RH - 26 | 22 | 42.3 | 38.4 | Reconstruction |
| RH - 27 | 16 | 10.0 | 9.0 | Overlay |
| RH - 28 | 18 | 12.5 | 11.2 | " |
| Total | | 560.9 | | |

Figure 8.4.1

Figure 8.4.1 ROUGHNESS - VOCs RELATIONSHIPS

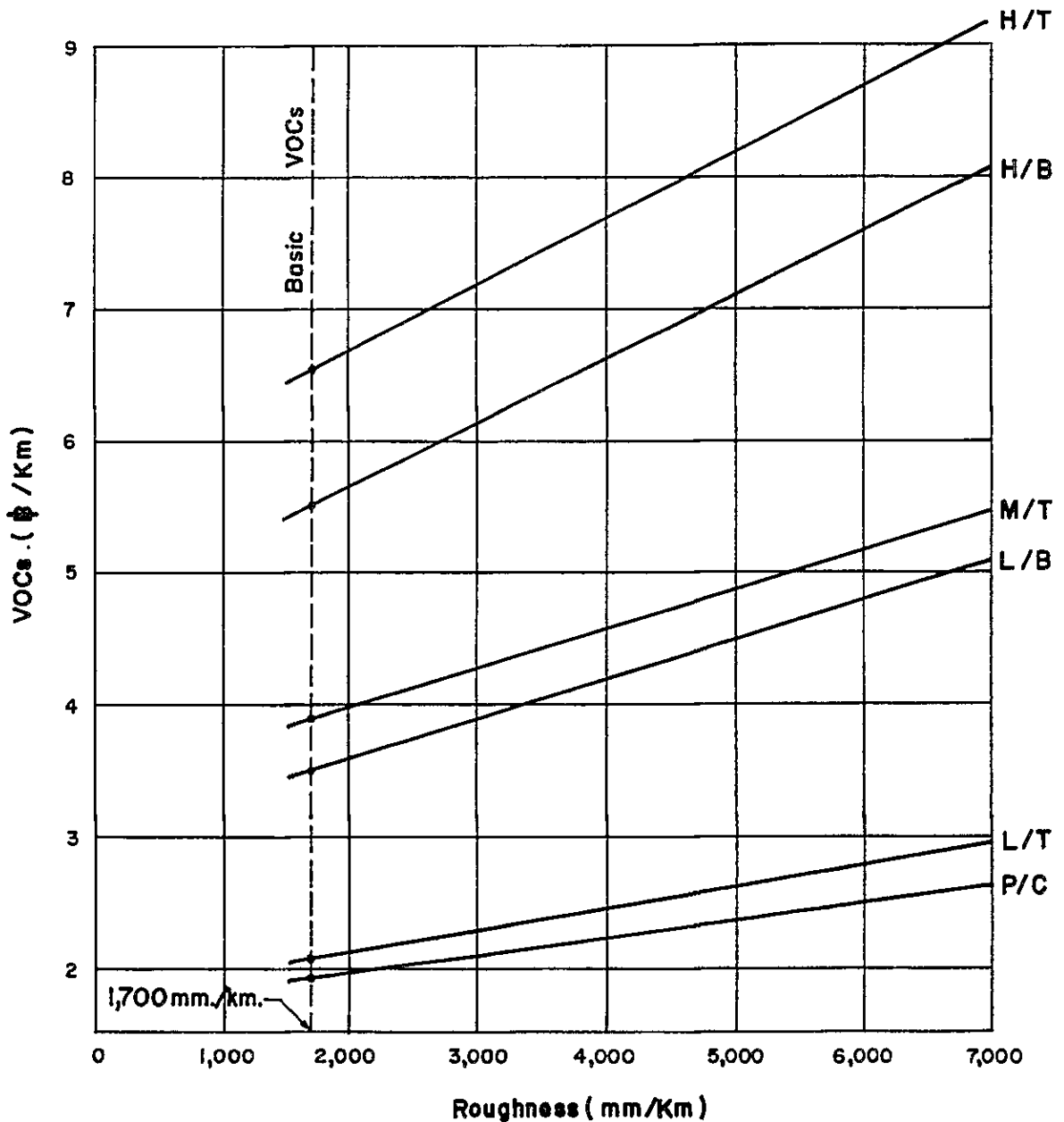
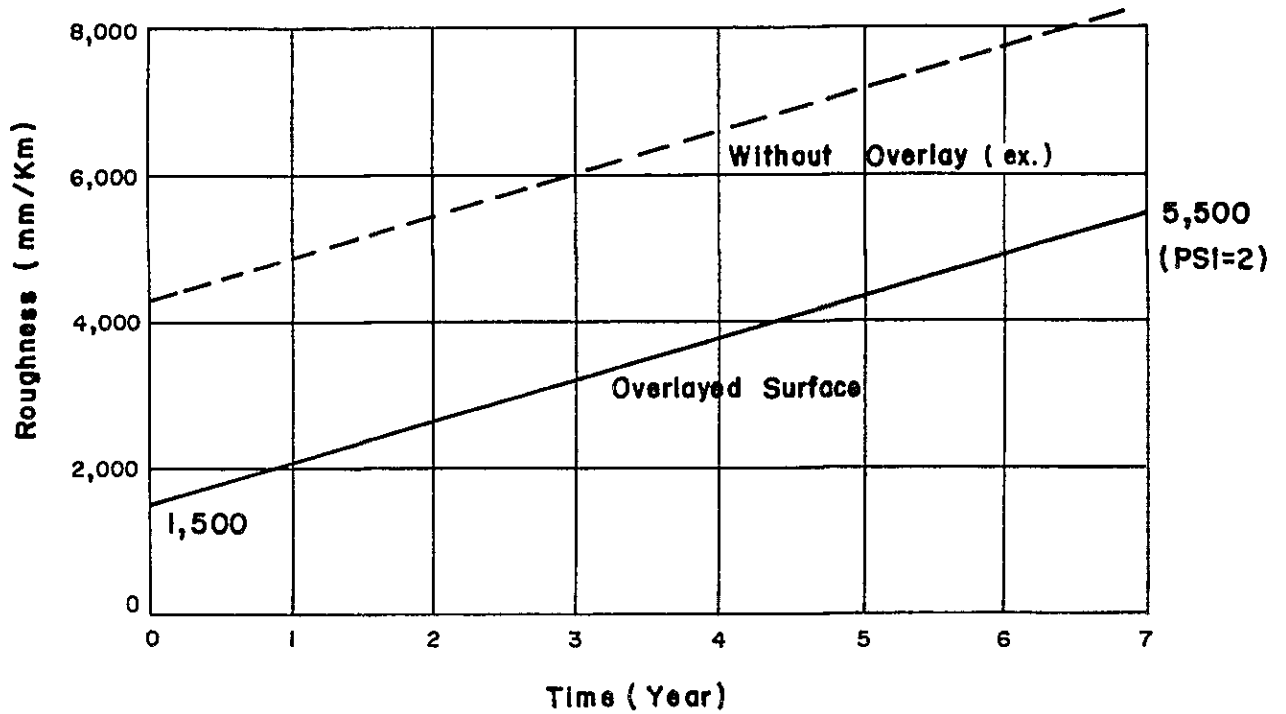
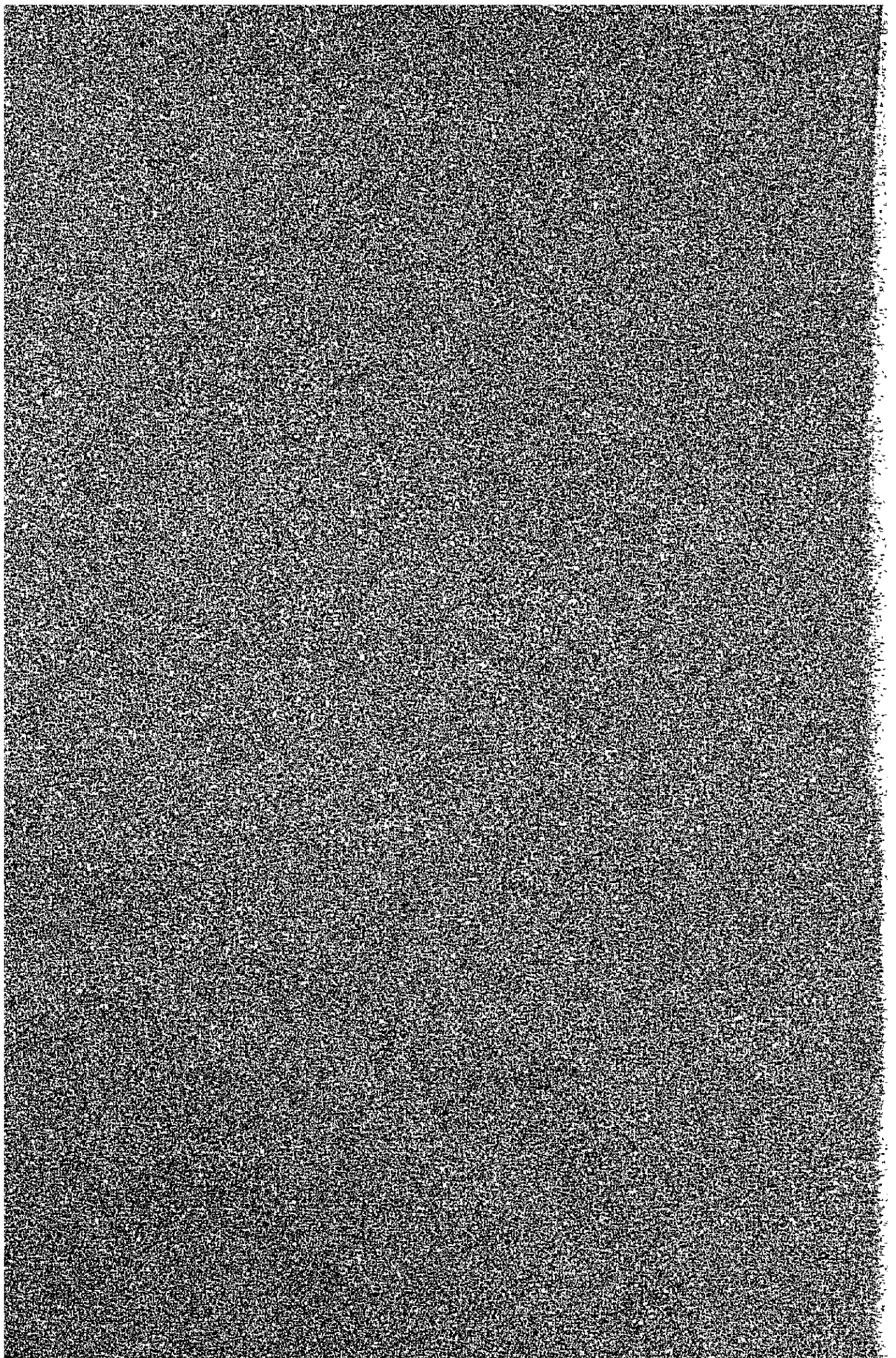


Table 8.5.1 SUMMARY RESULTS OF EVALUATION FOR REHABILITATION LINKS

| Link Number | Route | Link | Surface Type | Proposed Links | | | | ADT (1989) | Length(Km) | | Design Deflection (mm) | Pavement roughness (mm/km) | AC Overlay Thickness (mm) | Reconst. AC-Surface (mm) Base (mm) | Construction Cost (10 ⁶ ฿) | IRR (%) | |
|-------------|-------|------|--------------|------------------|-----------------------------|---------------------------|----------------------|------------|------------|-----------------|------------------------|----------------------------|---------------------------|------------------------------------|---------------------------------------|---------|--|
| | | | | Link Length (Km) | Origin | Destination | Proposed Length (Km) | | Overlay | Recon-struction | | | | | | | |
| RH-1 | 24 | 400 | AC | 28 | A. Nang Rong | A. Prakhon Chai | 28 | 1386 | 28 | - | 0.899 | 2,620 | 40 | | 22.5 | 13.3 | |
| RH-2 | 24 | 500 | AC | 36 | A. Prakhon Chai | A. Prasat | 36 | 1701 | 10 | - | 0.797 | 5,450 | 40 | | 7.5 | 91.9 | |
| RH-3 | 24 | 600 | AC | 50 | A. Prasat | A. Sangkha | 50 | 880 | 46 | - | 1.194 | 3,170 | 40 | | 34.5 | 11.0 | |
| RH-4 | 24 | 1001 | DT | 40 | A. Warin Chamrap | A. Det Udom | 40 | 1662 | 9 | - | 0.849 | 2,990 | 40 | | 6.8 | 27.9 | |
| RH-5 | 201 | 100 | DT | 39 | A. Sikhui | A. Dan Khun Thot | 39 | 1474 | 23 | - | 0.895 | 5,320 | 40 | | 17.3 | 69.7 | |
| RH-6 | 201 | 200 | DT | 25 | A. Dan Khun Thot | A. Nong Bua Khok | 25 | 1427 | 25 | - | 1.046 | 4,100 | 40 | | 18.7 | 48.8 | |
| RH-7 | 201 | 300 | DT | 17 | A. Nong Bua Khok | A. Chatturat | 17 | 1776 | ** | | 0.510 | 5,560 | ** | | | | |
| RH-8 | 201 | 400 | DT | 38 | A. Chatturat | C. Chaiyaphum | 38 | 1776 | ** | | 0.341 | 4,890 | ** | | | | |
| RH-9 | 202 | 500 | DT | 40 | A. Prathai | A. Phrayakkhamphum Phisai | 40 | 849 | 7 | - | 1.005 | 3,690 | 40 | | 5.3 | 20.3 | |
| RH-10 | 206 | 103 | AC | 5 | A. Phimai By Pass | | 5 | 725 | - | 5 | 0.881 | | | 50) 150) | 8.6 | 19.6 | |
| RH-11 | 207 | 100 | DT | 37 | B. Wat | A. Prathai | 37 | 695 | ** | | 0.783 | 4,430 | ** | | | | |
| RH-12 | 207 | 202 | DT | 35 | A. Prathai | A. Khok Chik | 13 | 601 | 6 | - | 0.958 | 4,070 | 40 | | 4.5 | 10.1 | |
| RH-13 | 208 | 100 | DT | 31 | A. Tha Phra | A. Kosum Phisai | 31 | 1912 | - | 24 | 1.126 | 4,350 | | 50) 250) | 60.0 | 9.9 | |
| RH-14 | 208 | 200 | DT | 29 | A. Kosum Phisai | C. Maha Sarakham | 29 | 1722 | - | 27 | 1.316 | 5,030 | | 50) 230) | 65.9 | 11.7 | |
| RH-15 | 213 | 100 | DT | 44 | C. Maha Sarakham | A. Kalasin | 44 | 1742 | 44 | - | 0.882 | 4,010 | 40 | | 33.0 | 56.8 | |
| RH-16 | 214 | 100 | DT | 28 | A. Kalasin | B. Lum Chai | 28 | 1793 | 14 | - | 1.121 | 3,850 | (40-9km) 50-5km) | | 11.3 | 43.1 | |
| RH-17 | 214 | 200 | DT | 19 | A. Lamnamchi | C. Roi Et | 19 | 1118 | 9 | - | 1.166 | 4,200 | 40 | | 6.8 | 34.5 | |
| RH-18 | 214 | 800 | PM | 30 | C. Surin | A. Prasat | 30 | 2249 | 30 | - | 1.035 | 4,240 | 40 | | 22.5 | 82.8 | |
| RH-19 | 304 | 800 | AC | 46 | A. Buphai | B. Takhop | 46 | 2350 | 26 | 20 | 1.476 | 4,180 | 50 | 50) 300) | 82.1 | 28.9 | |
| RH-20 | 304 | 902 | AC | 6 | A. Pak Thong Chai By Pass | | 6 | 2720 | 6 | - | 1.564 | 4,480 | 120 | | 15.7 | 25.7 | |
| RH-21 | 304 | 904 | AC | 26 | A. Pak Thong Chai (Route 2) | | 26 | 2720 | 13 | - | 1.030 | 2,560 | 50 | | 13.9 | 20.7 | |
| RH-22 | 2023 | 100 | PM | 8 | B. Nam Kong | A. Si That | 8 | 3936 | 8 | - | 1.047 | 3,710 | 40 | | 5.0 | 118.1 | |
| RH-23 | 2039 | 101 | DT | 16 | A. Nam Phong | A. Kranuan | 16 | 2016 | 16 | - | 1.339 | 4,400 | 80 | | 24.4 | 34.5 | |
| RH-24 | 2039 | 102 | DT | 17 | A. Nam Phong | A. Kranuan | 17 | 2016 | 16 | - | 1.538 | 4,670 | 100 | | 29.8 | 29.8 | |
| RH-25 | 2071 | 100 | DT | 28 | A. Chokchai | A. Khonburi | 28 | 1108 | ** | | 0.734 | 5,400 | ** | | | | |
| RH-26 | 2109 | 100 | DT | 24 | A. Nam Phong | A. Ubolratana Dam | 24 | 959 | - | 22 | 1.409 | 7,590 | | 50) 240) | 42.3 | 22.7 | |
| RH-27 | 2160 | 100 | DT | 20 | B. Wat | A. Kong | 20 | 442 | 16 | - | 1.397 | 4,160 | 40 | | 10.0 | 7.3 | |
| RH-28 | 2175 | 100 | DT | 34 | B. Wang Hin | A. Chum Phuang | 34 | 1104 | 18 | - | 1.214 | 3,110 | 40 | | 12.5 | 13.1 | |
| Total | | | | | | | 774 | | 370 | 98 | | | | | | | |

(**) Overlay/Reconstruction is not required

CHAPTER 9
PRIORITY RANKING AND PHASING



CHAPTER 9

PRIORITY RANKING AND PHASING

9.1 APPROACH

Listings of the proposed projects ranked by economic viability or social impacts are to be further scrutinized from an overall viewpoint taking also into account policies of the Thai Government.

In determining priority order of the projects for improvement and new construction, an attention is paid to the significance of social impact as well as the economic justification.

Priority or urgency of the proposed project for rehabilitation is judged primarily according to the degree of the existing deterioration, although the economic viability of the investment for rehabilitation is also assessed.

The projects given high priority ranking are classified into Stage I program, and the remained is considered to be included in Stage II program.

9.2 PRIORITY RANKING AND PROPOSED PHASING

9.2.1 Routes for Improvement and New Construction

First, priority of the projects was assessed from the viewpoint of economic viability. As a consequent, 15 routes were picked up to be included into a group of high priority projects. Next, for the remaining 18 routes, further screening was made paying special attention to the routes which have importance from the viewpoint of social impacts. And, 3 routes were chosen to be added into the

priority project group. Eighteen routes thus selected were classified into Stage I program and the remained 15 routes were considered to be included into Stage II. The projects included in the Stage I are recommended to be proceeded with further feasibility studies for earliest implementation.

The process of phasing is illustrated in Figure 9.2.1 and a proposal of a phased project list is presented in Table 9.2.1 and shown in Figure 9.2.2.

9.2.2 Links for Rehabilitation

Out of the identified links of 774 km in total, sections of 468 km was proposed to be urgently rehabilitated. All of the proposed links are judged to be of higher priority in view of the degree of deterioration of the existing pavement. As listed up in Table 9.2.2, they are classified into the Stage I program which are expected to be implemented immediately, within the current five-year-plan period. Those included in Stage I program are shown also in Figure 9.2.3.

The remaining links, 306 km in total, which are judged not required overlay now, are considered to be included into Stage II program.

9.2.3 Proposed Phasing and Fund Requirement

A proposed phasing discussed in the above is summarized in the following table, together with approximate fund requirement:

Summary of Phased Program

| <u>Classification</u> | <u>Number of Project</u> | <u>Length (km)</u> | <u>Fund Requirement (Mn ₪)</u> |
|-------------------------------------|------------------------------|------------------------|------------------------------------|
| Stage I | | | |
| Improvement and New construction | 18 routes | 666.9 | 1,269.8 |
| Rehabilitation (Overlay) | 25 links (20 links) | 468.0 (370.0) | 560.9 (331.2) |
| (Reconstruction) | (5 links) | (98.0) | (229.7) |
| Total of Stage I | - | - | 1,830.7 |
| Stage II | | | |
| Improvement and New Construction | 15 routes | 479.4 | n.a. |
| Rehabilitation | 19 links | 306.0 | n.a. |

Figure 9.2.1

Figure 9.2.1 PROCESS OF PHASING

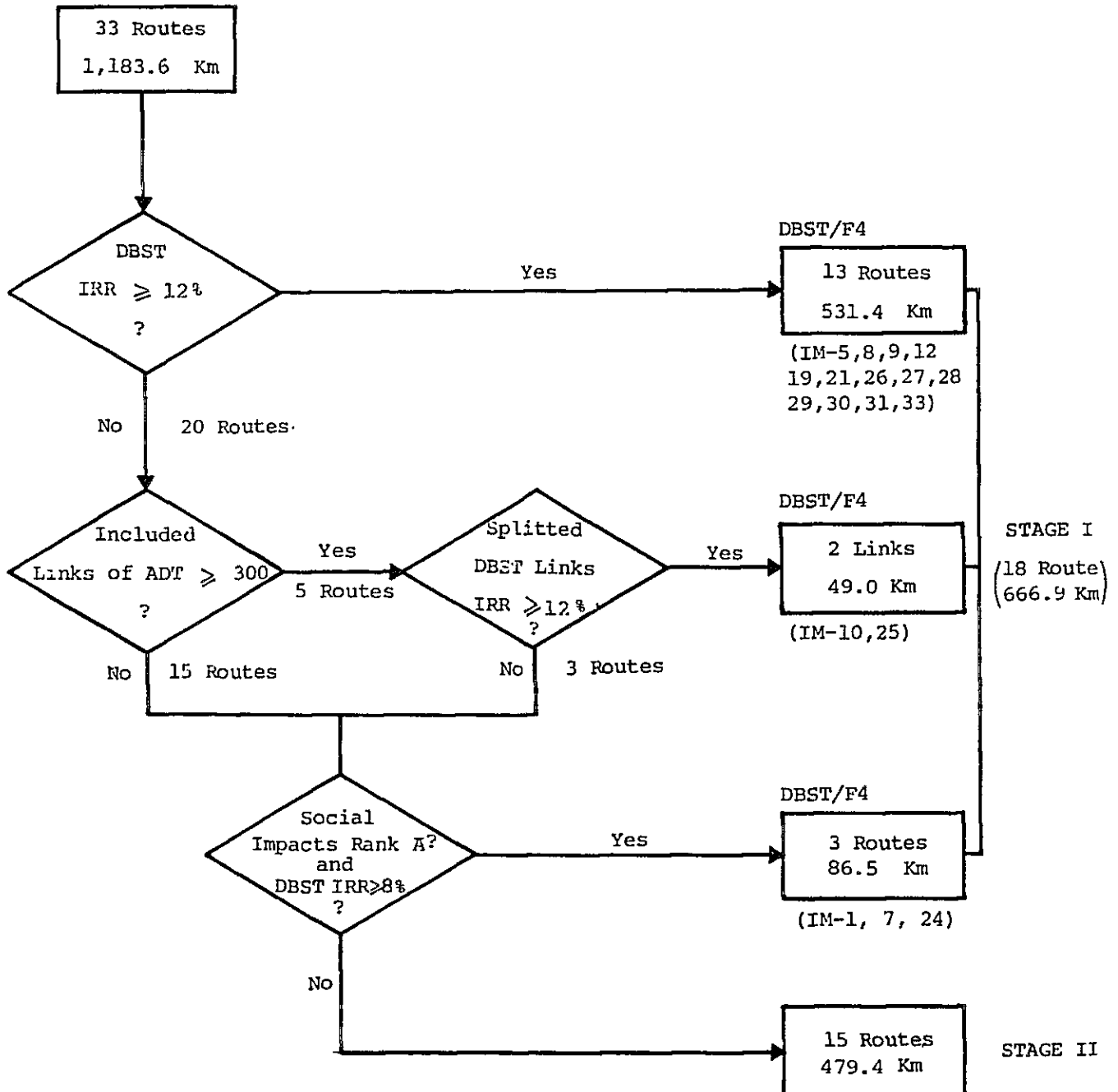


Table 9.2.1 PHASED PROGRAMME (IMPROVEMENT AND NEW CONSTRUCTION)

1) STAGE I

| Pro-posed Route | Origin | Destination | Length (Km) | Road Class | Surface ^{1/} Type | Const. ^{2/} Cost (Mn ฿) | IRR (%) | Social Impacts |
|------------------|----------------------------------|-------------------|-------------|------------|----------------------------|----------------------------------|---------|----------------|
| IM-28 | C. Buri Ram | Lam Chi River | 42.0 | F4 | DBST | 96.1 | 27.0 | B |
| IM-33 | J. R. 2 | A. Chokchai | 51.5 | F4 | DBST | 108.6 | 21.6 | A |
| IM-5 | A. Nam Phong | J. R. 209 | 29.1 | F4 | DBST | 61.5 | 20.0 | C |
| IM-8 | B. Huai Koeng | A. Kumphawapi | 16.7 | F4 | DBST | 27.4 | 18.1 | C |
| IM-19 | A. Selaphum | B. Kham Phon Sung | 46.0 | F4 | DBST | 95.3 | 17.1 | B |
| IM-31 | A. Lamplai Mat | B. Nong Ki | 59.7 | F4 | DBST | 93.1 | 15.1 | C |
| IM-30 | A. Huai Thalaeng | B. Ka Sang | 51.0 | F4 | DBST | 96.4 | 14.6 | C |
| IM-21 | A. T. Phut Phon | A. Khemarat | 65.3 | F4 | DBST | 112.4 | 14.3 | C |
| IM-12 | ^{3/} A. S. Daen Din | A. Song Dao | 18.1 | F4 | DBST | 35.9 | 12.5 | A |
| IM-10 | ^{3/} A. Phen | K. A. Song Khom | 26.0 | F4 | DBST | 45.6 | 12.4 | B |
| IM-26 | ^{3/} B. Non Dang | A. Rattana Buri | 39.5 | F4 | DBST | 74.3 | 11.8 | A |
| IM-25 | ^{3/} A. Maha Chana Chai | A. Kho Wang | 23.0 | F4 | DBST | 39.9 | 11.6 | B |
| IM-29 | A. Prakhon Chai | A. Krasang | 48.0 | F4 | DBST | 95.5 | 11.5 | C |
| IM-27 | B. Nong Khao | A. Chom Phra | 31.1 | F4 | DBST | 52.0 | 11.3 | C |
| IM-9 | A. Nong Han | A. Kumphawapi | 33.4 | F4 | DBST | 72.6 | 11.1 | C |
| IM-24 | B. Na Suang | B. Na Yia | 14.5 | F4 | DBST | 25.7 | 10.6 | A |
| IM-1 | A. Khong | J. R. 2180 | 48.0 | F4 | DBST | 91.5 | 9.6 | A |
| IM-7 | B. Khok Lat | B. Tha Yom | 24.0 | F4 | DBST | 46.0 | 8.1 | A |
| Total of Stage I | | | 666.9 | | | 1,269.8 | | |

2) STAGE II

| Pro-posed Route | Origin | Destination | Length (Km) | Road Class | Surface ^{1/} Type | Const. ^{2/} Cost (Mn ฿) | IRR (%) | Social Impacts | O.O.Y. ^{4/} FYB = 12% | | F5/S.A. ^{5/} | |
|-------------------|-------------------------------|-----------------|-------------|------------|----------------------------|----------------------------------|---------|----------------|--------------------------------|-------|-----------------------|-----|
| | | | | | | | | | DBST | COST | COST | IRR |
| IM-23 | B. Don Chik | B. Nong Rieng | 44.8 | F4 | DBST | 74.2 | 10.7 | C | 1988 | 38.5 | 13.9 | |
| IM-2 | B. Wao | K. A. Na Pho | 9.4 | F4 | DBST | 16.3 | 10.2 | B | 1991 | 8.8 | 12.7 | |
| IM-17 | A. Kuchinarai | B. Nong Rieng | 30.4 | F4 | DBST | 66.1 | 8.7 | B | 1991 | 40.6 | 12.2 | |
| IM-20 | B. Na Hai | A, Kut Khao Pun | 17.2 | F4 | DBST | 32.9 | 8.4 | B | 1992 | 22.3 | 11.0 | |
| IM-18 | C. Kalasin | B. K. Nong Bua | 50.7 | F4 | DBST | 98.2 | 7.5 | B | 1992 | 59.6 | 11.6 | |
| IM-3 | J. R. 2301 | A. Na Chuak | 30.6 | F4 | DBST | 57.8 | 7.4 | B | 1993 | 32.1 | 11.6 | |
| IM-13 | B. Chuam | A. Na Wha | 19.8 | F4 | DBST | 37.5 | 6.6 | B | 1994 | 24.5 | 9.4 | |
| IM-4 | A. Chonnabot | B. Kut Ru | 35.3 | F4 | DBST | 60.6 | 6.2 | B | 1994 | 33.7 | 9.8 | |
| IM-11 | B. Thung Yai | K. A. Thung Fon | 8.3 | F4 | DBST | 18.8 | 5.1 | A | 1996 | 12.4 | 8.8 | |
| IM-15 | A. R. Nakhon | B. Ku Ru Khu | 40.1 | F4 | DBST | 75.4 | 5.1 | C | 1996 | 45.2 | 8.9 | |
| IM-22 | A. Khemarat | B. Hua Saphan | 122.4 | F4 | DBST | 217.1 | 4.5 | A | 1997 | 116.6 | 8.1 | |
| IM-32 | B. Yok Kham | B. Soeng Sang | 29.0 | F4 | DBST | 49.5 | 4.5 | C | 1999 | 29.1 | 9.8 | |
| IM-6 | B. Sok Chan | Ubolratana Dam | 20.3 | F4 | DBST | 62.4 | 4.0 | A | 1999 | 36.0 | 6.2 | |
| IM-14 | J. R. 223 | K. A. Tao Ngai | 12.0 | F4 | DBST | 27.7 | 3.7 | A | 1999 | 18.5 | 5.8 | |
| IM-16 | ^{6/} J. R. 212 | A. Whan Yai | 9.1 | F4 | DBST | 15.2 | 3.0 | A | 1999 | 7.6 | 8.6 | |
| IM-25 | ^{6/} A. Kho Wang | J. R. 2168 | 15.2 | | | | | | | 18.5 | 8.1 | |
| IM-10 | ^{6/} K. A. Song Khom | J. R. 212 | 22.1 | | | | | | | 23.5 | 6.4 | |
| Total of Stage II | | | 516.7 | | | | | | | | | |

Note: ^{1/} DBST : Double Bituminous Surface Treatment
^{2/} Excluding price contingency
^{3/} Section 1 (with ADT more than 300 in the 7th year)
^{4/} Optimum Opening Year : The year when the first year benefit exceeds 12% of total investment
^{5/} S.A. : Soil Aggregate Surfaced
^{6/} Section 2 (with ADT less than 300 in the 7th year)

Figure 9.2.2 PHASED PROGRAM FOR IMPROVEMENT AND NEW CONSTRUCTION

Figure 9.2.2

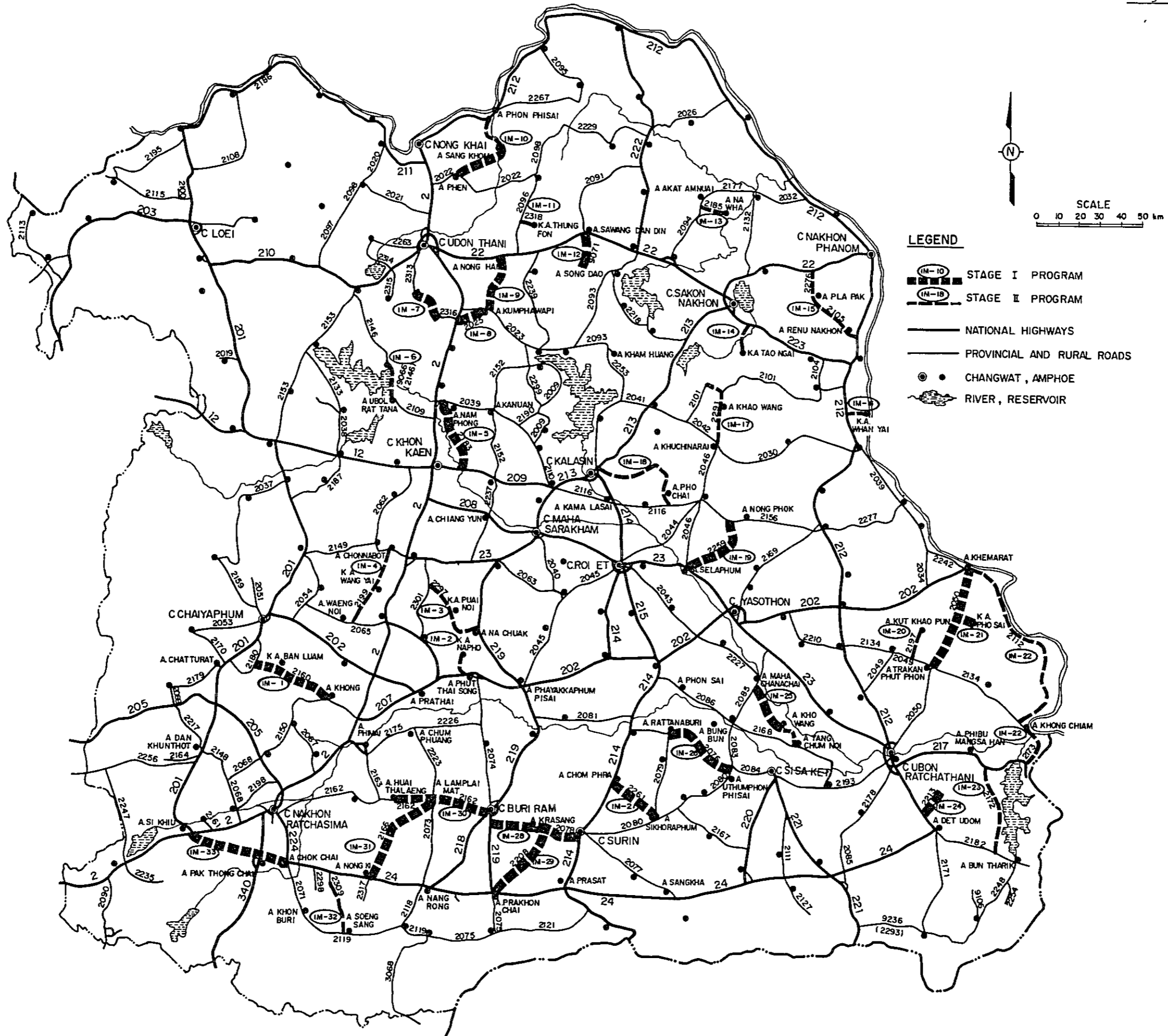
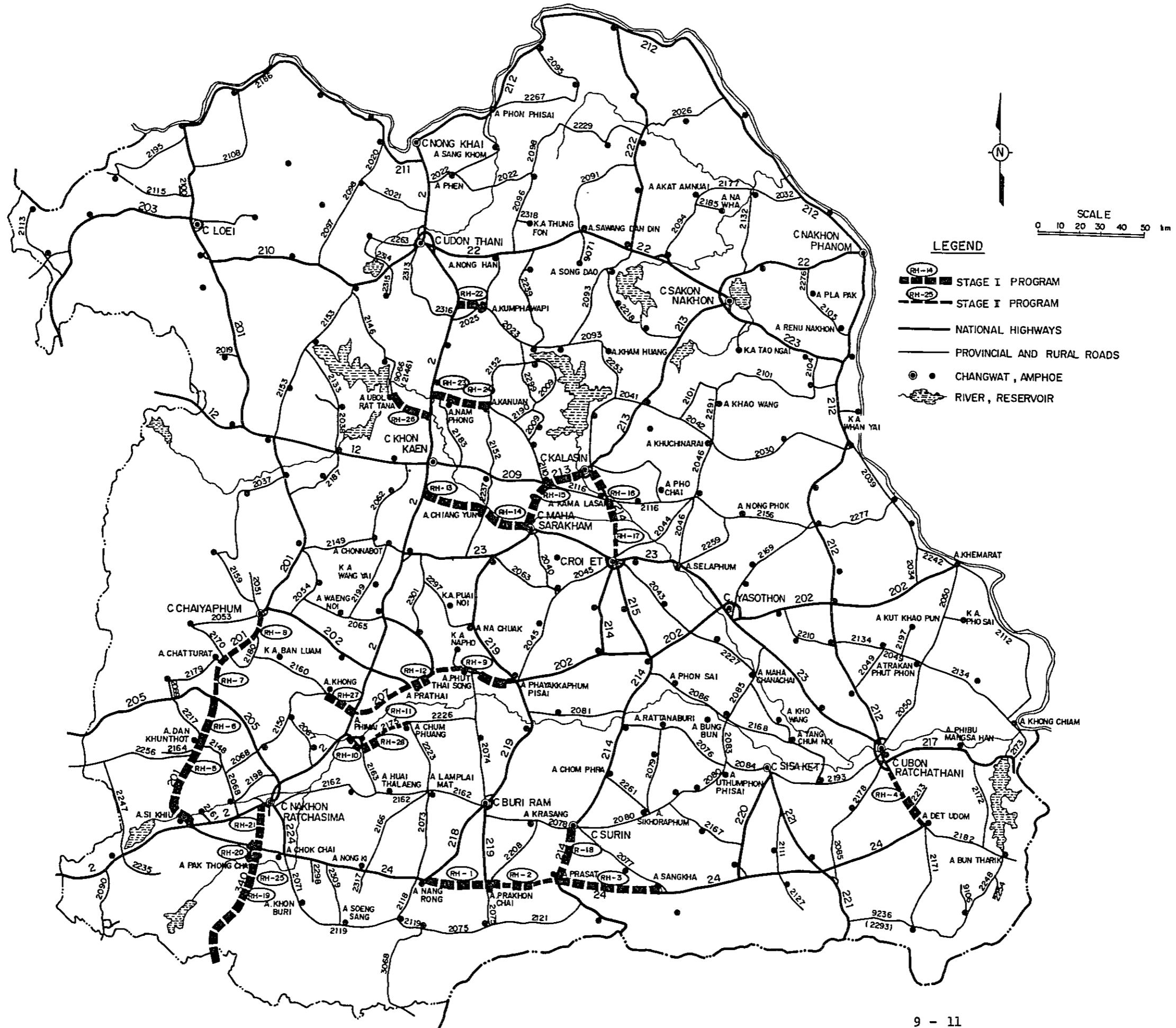


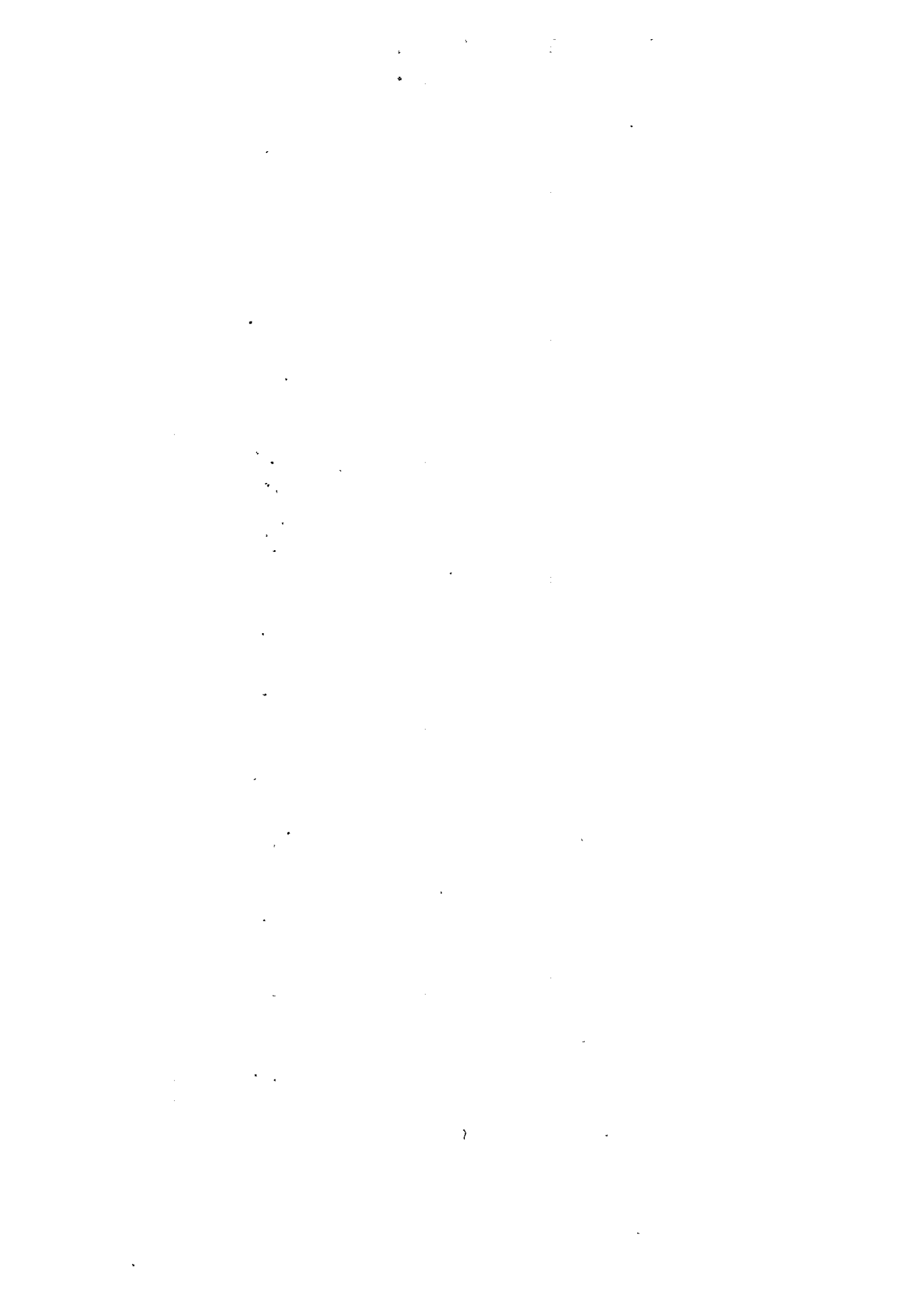
Table 9.2.2 STAGE I PROGRAM FOR REHABILITATION

| Proposed Route | Proposed Link Length (Km) | Const. Cost (Mn Ø) | | IRR (%) |
|-------------------|------------------------------------|-----------------------|----------|------------|
| | | Overlay | Reconst. | |
| RH-22 | 8 | 5.0 | | 118.1 |
| RH-2 | 10 | 7.5 | | 91.9 |
| RH-18 | 30 | 22.5 | | 82.8 |
| RH-5 | 23 | 17.3 | | 69.7 |
| RH-15 | 44 | 33.0 | | 56.8 |
| RH-6 | 25 | 18.7 | | 48.8 |
| RH-16 | 14 | 11.3 | | 43.1 |
| RH-17 | 9 | 6.8 | | 34.5 |
| RH-23 | 16 | 24.4 | | 34.5 |
| RH-24 | 16 | 29.8 | | 29.8 |
| RH-19 (1) | 26 | 29.2 | | 28.9 |
| (2) | 20 | | 52.9 | |
| RH-4 | 9 | 6.8 | | 27.9 |
| RH-20 | 6 | 15.7 | | 25.7 |
| RH-26 | 22 | | 42.3 | 22.7 |
| RH-21 | 13 | 13.9 | | 20.7 |
| RH-9 | 7 | 5.3 | | 20.3 |
| RH-10 | 5 | | 8.6 | 19.6 |
| RH-1 | 28 | 22.5 | | 13.3 |
| RH-28 | 18 | 12.5 | | 13.1 |
| RH-14 | 27 | | 65.9 | 11.7 |
| RH-3 | 46 | 34.5 | | 11.0 |
| RH-12 | 6 | 4.5 | | 10.1 |
| RH-13 | 24 | | 60.0 | 9.9 |
| RH-27 | 16 | 10.0 | | 7.3 |
| Total | 468 | 331.1 | 229.7 | |

Figure 9.2.3 PHASED PROGRAM FOR REHABILITATION

Figure 9.2.3





JICA

10