

**REPUBLIC OF THE UNION OF MYANMAR
MINISTRY OF CONSTRUCTION
DEPARTMENT OF BRIDGE**

**DETAILED DESIGN STUDY ON
THE BAGO RIVER BRIDGE
CONSTRUCTION PROJECT**

FINAL REPORT ATTACHMENTS

**VOLUME II DESIGN REPORT
Part V Flyover Bridge**

DECEMBER 2017

JAPAN INTERNATIONAL COOPERATION AGENCY (JICA)

NIPPON KOEI CO., LTD.

ORIENTAL CONSULTANTS GLOBAL CO., LTD.

METROPOLITAN EXPRESSWAY COMPANY LIMITED.

CHODAI CO., LTD.

NIPPON ENGINEERING CONSULTANTS CO., LTD.

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01-PC BRIDGE

02-STEEL BRIDGE

03-SUBSTRUCTURE AND FOUNDATION

01-PC BRIDGE




01-1-PC-I GIRDER BRIDGE
(AF1-PF2)

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1.1 DESIGN CONDITION

ROAD GRADE	:	Equivalent to CLASS 4-1
BRIDGE TYPE	:	2 span continuous PC-I girder bridge with composite deck (PC plate and RC deck)
BRIDGE LENGTH	:	L = 60.000 m
SPAN LENGTH	:	L = 28.801 + 28.851 m (ON CL)
WIDTH OF THE ROAD	:	TOTAL 12.750 m L = 0.500 + 5.500 + 0.750 + 5.500 + 0.500 m
HORIZONTAL ALIGNMENT	:	A=150 ~ R=420 ~ A=150
LONGITUDINAL SLOPE	:	3.00 % 
SECTION SLOPE	:	LEFT : 3.45 % ~ 4.00 % ~ 3.34 %  RIGHT : 3.45 % ~ 4.00 % ~ 3.34 % 
ANGLE OF SKEW	:	90°00'00"
PAVEMENT	:	ASPHALT PAVEMENT t= 80 mm
SLAB	:	REINFORCED CONCRETE t= 170 mm
PLATE	:	PRESTRESS CONCRETE PLATE t= 100 mm
LIVE ROAD	:	AASHTO HL=93
DESIGN STANDARD	:	AASHTO LRFD BRIDGE DESIGN 2014(LIVE ROAD) Specifications for highway bridges(Japan Road Association) 1 Common matters,3 Concrete bridges,5 seismic design (April 2012)

1.2 MATERIALS STRENGTH

1) CONCRETE

		(N/mm ²)				
		MAIN GIRDER	CROSS BEAM	RC SLAB	PC PLATE	COUPLING CONCRETE
DESIGN STANDARD STRENGTH OF CONCRETE		40.00	30.00	30.00	40.00	30.0
BENDING COMPRESSIVESTRESS	IMMEDIATELY AFTER PRESTRESSING	19.00	14.00	----	19.00	----
	OTHERS	14.00	11.00	10.00	15.00	10.00
BENDING TENSILE STRESS	IMMEDIATELY AFTER PRESTRESSING	-1.50	-1.20	----	-1.50	----
	DEAD LOAD	0.0	0.0	----	----	----
	DESIGN LOAD	-1.50	-1.20	----	0.0	----
	TEMPERATURE CHANGE	-2.00	----	----	----	----
MEAN SHEAR STRESS CONCRETE CAN CARRY		0.55	0.45	----	----	----
MAXIMUM MEAN CONCRETE SHEAR STRESS		5.30	4.00	----	----	----
ALLOWABLE DIAGONEL TENSILE STRESS (Case where shear force or torsional moment)	DEAD LOAD	-1.00	-0.80	----	----	----
	LIVE LOAD	-2.00	-1.70	----	----	----
ALLOWABLE DIAGONEL TENSILE STRESS (Case where both shear force and torsional moment)	DEAD LOAD	-1.30	-1.10	----	----	----
	LIVE LOAD	-2.50	-2.20	----	----	----

2) PC STRAND

		(N/mm ²)		
		MAIN GIRDER	CROSS BEAM	PC PLATE
PRESTRESSING STEEL TYPE		SWPR7BL 7S15.2mm	SWPR7BL 4S15.2mm	SWPR7AL 1S9.3mm
TENSILE STRENGTH		1850	1850	1700
YIELD POINT		1600	1600	1450
ALLOWABLE TENSILE STRESS	DURING PRESTRESSING	1440	1440	1305
	IMMEDIATELY AFTER PRESTRESSING	1295	1295	1190
	AT COMPOSITION OF SLAB	1110	----	----
	DESIGN LOAD	1110	1110	1020

3) REINFORCING STEEL

		(N/mm ²)			
		MAIN GIRDER	CROSS BEAM	RC SLAB	COUPLING CONCRETE
STEEL TYPE		SD345	SD345	SD345	SD345
YIELD POINT		345	345	345	345
ALLOWABLE TENSILE STRESS	DEAD LOAD	----	----	100	100
	DESIGN LOAD	180	200	140	160
	COLLISION LOAD	----	----	300	----
	WIND LOAD	----	----	175	----

1.3 DESIGN CONSTANT

1) CONCRETE

		MAIN GIRDER	CAST IN PLACE	PC PLATE
YOUNG'S MODULUS	DESIGN LOAD (N/mm ²)	3.10×10^4	2.80×10^4	3.10×10^4
	IMMEDIATELY AFTER PRESTRESSING (N/mm ²)	2.92×10^4	2.58×10^4	2.92×10^4
CREEP COEFFICIENT	NUMBER OF DAYS FOR DECK CONSTRUCTION	90	----	----
	NUMBER OF CONSTRUCTION DAYS FOR BRIDGE SURFACE	120	----	----
	DESIGN LOAD	2.60	2.60	3.00
	DURING DECK CONSTRUCTION	1.70	----	----
	BRIDGE SURFACE	1.65	----	----
DRYING SHRINKAGE OF CONCRETE	DURING DECK CONSTRUCTION	4.0×10^{-5}	----	----
	DESIGN LOAD	20.0×10^{-5}	20.0×10^{-5}	20.0×10^{-5}
UNIT WEIGHT (kN/mm ³)		24.5	24.5	24.5

2) PC STRAND(MAIN GIRDER)

		1	2
YOUNG'S MODULUS	N/mm ²	2.00×10^5	2.00×10^5
SLIP	mm	4.0	4.0
RELAXATION	%	2.5	2.5
FRICTION COEFFICIENT	1/m	0.004	0.004
	1/rad	0.300	0.300
AREA	mm ²	970.900	970.900
UNIT WEIGHT	kg/m	7.707	7.707
DIAMETER OF SHEATH	mm	60.0	60.0
DECREASE RATIO BY ANCHOR	%	0.0	0.0

3) PC STRAND(CROSS BEAM)

YOUNG'S MODULUS	N/mm ²	2.00×10^5
SLIP	mm	4.0
RELAXATION	%	2.5
FRICTION COEFFICIENT	1/m	0.004
AREA	mm ²	554.800
UNIT WEIGHT	kg/m	4.404
DIAMETER OF SHEATH	mm	45.0
DECREASE RATIO BY ANCHOR	%	0.0

4) PC STRAND(PC PLATE)

		BETWEEN MAIN GIRDERS	
YOUNG'S MODULUS		N/mm ²	2.00 × 10 ⁵
RELAXATION	BEFORE PRESTRESSING	%	1.5
	AFTER PRESTRESSING	%	1.5
	EXTRA COEFFICIENT OF HIGH TEMPERATURE	%	1.0
AREA		mm ²	51.610
UNIT WEIGHT		kg/m	0.405

1. 5 Dimension

1) Dimension of Main Girder

Girder Height : 1900.00 ~ 1900.00 mm

【Change of Web Width (mm)】

Span	End of Girder (Left Side)			End of Girder (Right Side)		
	Ending Point of Changing Web Width	Starting Point of Changing Web Width	Web Width	Ending Point of Changing Web Width	Starting Point of Changing Web Width	Web Width
1	1000.0	4000.0	700.0	4000.0	1000.0	700.0
2	1000.0	4000.0	700.0	4000.0	1000.0	700.0

2) Dimension of Cross Beam

【Interval of Cross Beam on Left Girder (m)】

Span	Number of Intermediate Cross Beams	CB1~CB2	CB2~CB3
1	1	15.088	15.088
2	1	15.106	15.106

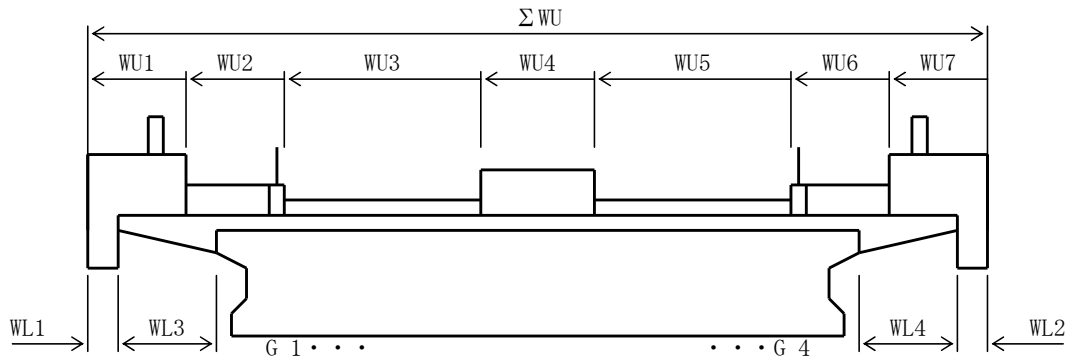
【Interval of Cross Beam on Right Girder (m)】

Span	Number of Intermediate Cross Beams	CB1~CB2	CB2~CB3
1	1	14.715	14.715
2	1	14.747	14.747

【Dimension of Cross Beam (m)】

Span	Cross Beam Width	Cross Beam Width (Left Side)	Cross Beam Width (Right Side)
1	0.300	0.900	0.950
2	0.300	0.950	0.900

【Cross Section】



【m】

	ΣWU	WU1	WU2	WU3	WU4	WU5	WU6	WU7
1	12.750	0.500	0.000	5.500	0.750	5.500	0.000	0.500
2	12.750	0.500	0.000	5.500	0.750	5.500	0.000	0.500
3	12.750	0.500	0.000	5.500	0.750	5.500	0.000	0.500

	ΣWU	WL1	WL2	WL3	WL4
1	3.502	0.000	0.000	0.339	0.604
2	3.502	0.000	0.000	0.340	0.604
3	3.502	0.000	0.000	0.338	0.606

2. 1 Load Intensity

1) Load Intensity

(1) Bridge Surface Loads

< 1 >

Load Type		Load Intensity	Load Location	
			Left End of Girder Side	Right End of Girder Side
Selfweight of Kerb	Left	8.900 kN/m	0.180 m	0.180 m
	Right	8.650 kN/m	0.180 m	0.180 m
Selfweight of Concrete Barrier	Left	0.600 kN/m	0.125 m	0.125 m
	Right	0.600 kN/m	0.125 m	0.125 m
Selfweight of Sidewalk	Left	0.000 kN/m ²		
	Right	0.000 kN/m ²		
Selfweight of Handrail	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Kerb	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Pavement	Left	2.170 kN/m ²		
	Right	2.240 kN/m ²		
Selfweight of Median		8.590 kN/m ²		
Selfweight of Additional Object	1	0.110 kN/m	0.075 m	0.075 m
	2	0.110 kN/m	12.675 m	12.675 m

< 2 >

Load Type		Load Intensity	Load Location	
			Left End of Girder Side	Right End of Girder Side
Selfweight of Kerb	Left	8.790 kN/m	0.180 m	0.180 m
	Right	8.960 kN/m	0.180 m	0.180 m
Selfweight of Concrete Barrier	Left	0.600 kN/m	0.125 m	0.125 m
	Right	0.600 kN/m	0.125 m	0.125 m
Selfweight of Sidewalk	Left	0.000 kN/m ²		
	Right	0.000 kN/m ²		
Selfweight of Handrail	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Kerb	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Pavement	Left	2.150 kN/m ²		
	Right	2.630 kN/m ²		
Selfweight of Median		8.710 kN/m ²		
Selfweight of Additional Object	1	0.110 kN/m	0.075 m	0.075 m
	2	0.110 kN/m	12.675 m	12.675 m

Condition of Load

Calculation of Bridge Surface Loads

(AF1-PF1)

① Unit Weight

PC · RC Concrete	$\gamma_1 = 24.5 \text{ kN/m}^3$
Concrete	$\gamma_2 = 23.0 \text{ kN/m}^3$
Asphalt Pavement	$\gamma_3 = 22.5 \text{ kN/m}^3$

② Bridge Surface Loads

- Pavement on Left Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = 1/2 \times (0.107 + 0.084) = 0.096 \text{ m}$$

(Thickness of Leveling Concrete)

$$t_c = 0.096 - 0.080 = 0.016 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.016 \times 23.0 = \underline{\underline{2.17 \text{ kN/m}^2}}$$

- Pavement on Right Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = 1/2 \times (0.110 + 0.087) = 0.099 \text{ m}$$

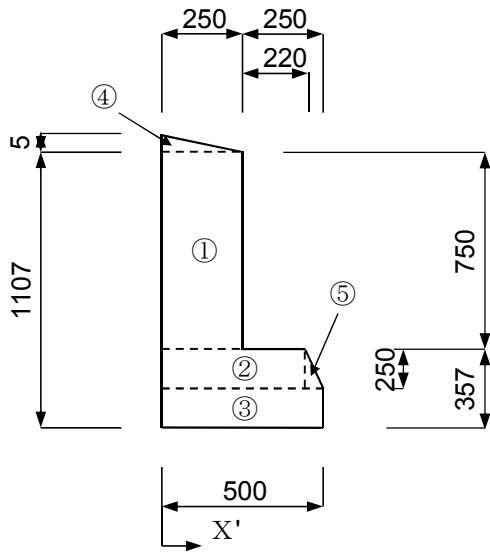
(Thickness of Leveling Concrete)

$$t_c = 0.099 - 0.080 = 0.019 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.019 \times 23.0 = \underline{\underline{2.24 \text{ kN/m}^2}}$$

• Concrete Barrier (Left Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.107	0.500	0.0535	0.250	0.01338
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3629		0.0663

Load Location

$$X' = 0.0663 / 0.3629$$

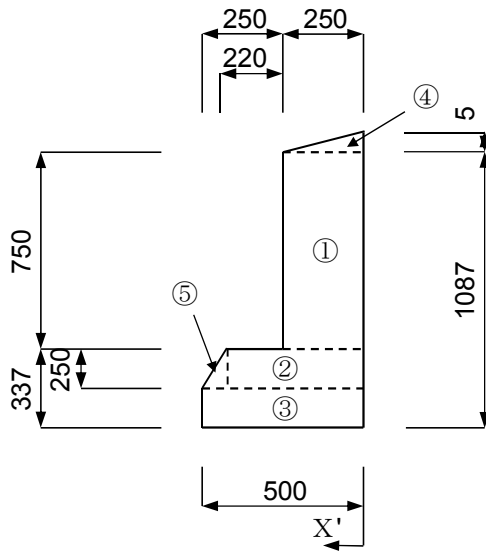
$$= \underline{0.180 \text{ m}}$$

Load Intensity

$$P = 0.3629 \times 24.5$$

$$= \underline{8.90 \text{ kN/m}}$$

• Concrete Barrier (Right Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.087	0.500	0.0435	0.250	0.01088
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3529		0.0638

Load Location

$$X' = 0.0638 / 0.3529$$

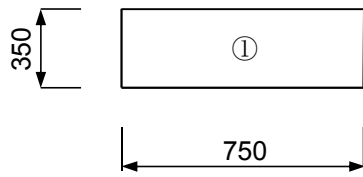
$$= \underline{0.180 \text{ m}}$$

Load Intensity

$$P = 0.3529 \times 24.5$$

$$= \underline{8.65 \text{ kN/m}}$$

• Median



a) Load Intensity and Load Location

		H	B	A
①	□	0.3500	0.7500	0.2625
				<u>0.2625</u>

Load Location

X' = On CL

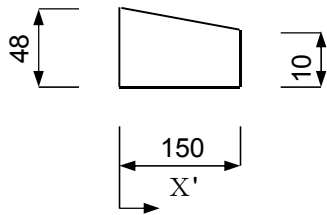
Load Intensity

$$P = 0.2625 \times 24.5 = \underline{6.44 \text{ kN/m}}$$

$$W = 6.4400 / 0.750 = \underline{8.59 \text{ kN/m}^2}$$

• Left Drain Duct

※Loaded as Selfweight of Additional Object 1



Load Location

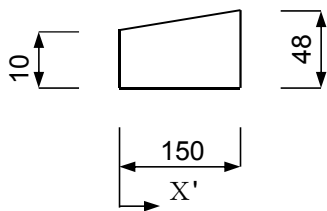
$X' = 75\text{mm}$ inside beginning of Left Kerb

Load Intensity

$$P = 1/2 \times (0.048 + 0.010) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Right Drain Duct

※Loaded as Selfweight of Additional Object 2



Load Location

$X' = 75\text{mm}$ inside beginning of Right Kerb

Load Intensity

$$P = 1/2 \times (0.010 + 0.048) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Handrail

※Loaded as Concrete Barrier

Load Location

$X' = 125\text{mm}$ inside beginning of Right and Left Kerb

Load Intensity

$$P = 0.60 = \underline{0.60 \text{ kN/m}}$$

Condition of Load

Calculation of Bridge Surface Loads

(PF1-PF2)

① Unit Weight

PC · RC Concrete	$\gamma_1 = 24.5 \text{ kN/m}^3$
Concrete	$\gamma_2 = 23.0 \text{ kN/m}^3$
Asphalt Pavement	$\gamma_3 = 22.5 \text{ kN/m}^3$

② Bridge Surface Loads

- Pavement on Left Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = 1/2 \times (0.098 + 0.091) = 0.095 \text{ m}$$

(Thickness of Leveling Concrete)

$$t_c = 0.095 - 0.080 = 0.015 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.015 \times 23.0 = \underline{\underline{2.15 \text{ kN/m}^2}}$$

- Pavement on Right Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = 1/2 \times (0.119 + 0.112) = 0.116 \text{ m}$$

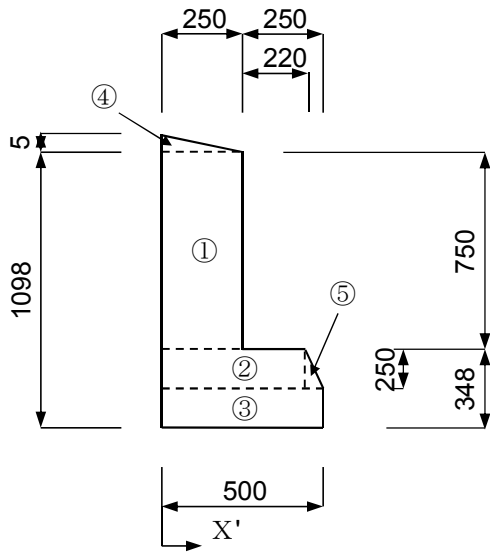
(Thickness of Leveling Concrete)

$$t_c = 0.116 - 0.080 = 0.036 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.036 \times 23.0 = \underline{\underline{2.63 \text{ kN/m}^2}}$$

• Concrete Barrier (Left Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.098	0.500	0.0490	0.250	0.01225
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3584		0.0652

Load Location

$$X' = 0.0652 / 0.3584$$

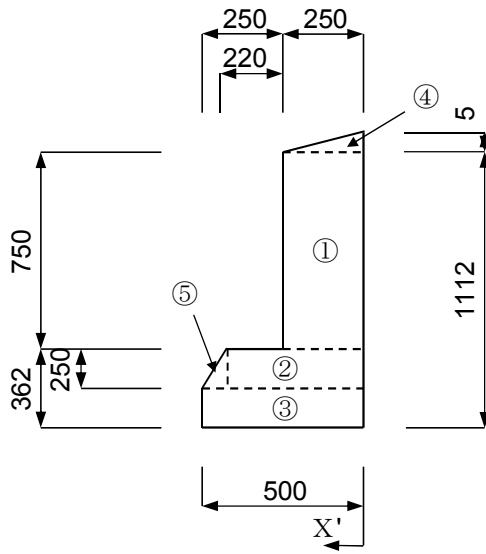
$$= \underline{0.180 \text{ m}}$$

Load Intensity

$$P = 0.3584 \times 24.5$$

$$= \underline{8.79 \text{ kN/m}}$$

• Concrete Barrier (Right Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.112	0.500	0.0560	0.250	0.01400
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3654		0.0669

Load Location

$$X' = 0.0669 / 0.3654$$

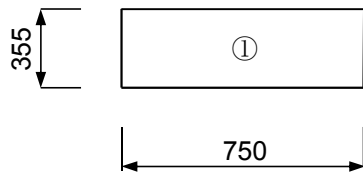
$$= \underline{0.180 \text{ m}}$$

Load Intensity

$$P = 0.3654 \times 24.5$$

$$= \underline{8.96 \text{ kN/m}}$$

• Median



a) Load Intensity and Load Location

	H	B	A
① □	0.3550	0.7500	0.2663
			0.2663

Load Location

X' = On CL

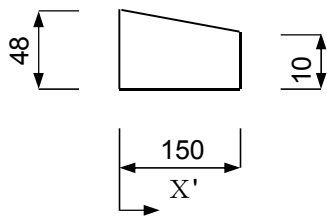
Load Intensity

$$P = 0.2663 \times 24.5 = \underline{\underline{6.53 \text{ kN/m}}}$$

$$W = 6.5300 / 0.750 = \underline{\underline{8.71 \text{ kN/m}^2}}$$

• Left Drain Duct

※Loaded as Selfweight of Additional Object 1



Load Location

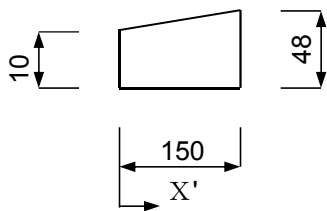
$X' = 75\text{mm}$ inside beginning of Left Kerb

Load Intensity

$$P = 1/2 \times (0.048 + 0.010) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Right Drain Duct

※Loaded as Selfweight of Additional Object 2



Load Location

$X' = 75\text{mm}$ inside beginning of Right Kerb

Load Intensity

$$P = 1/2 \times (0.010 + 0.048) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Handrail

※Loaded as Concrete Barrier

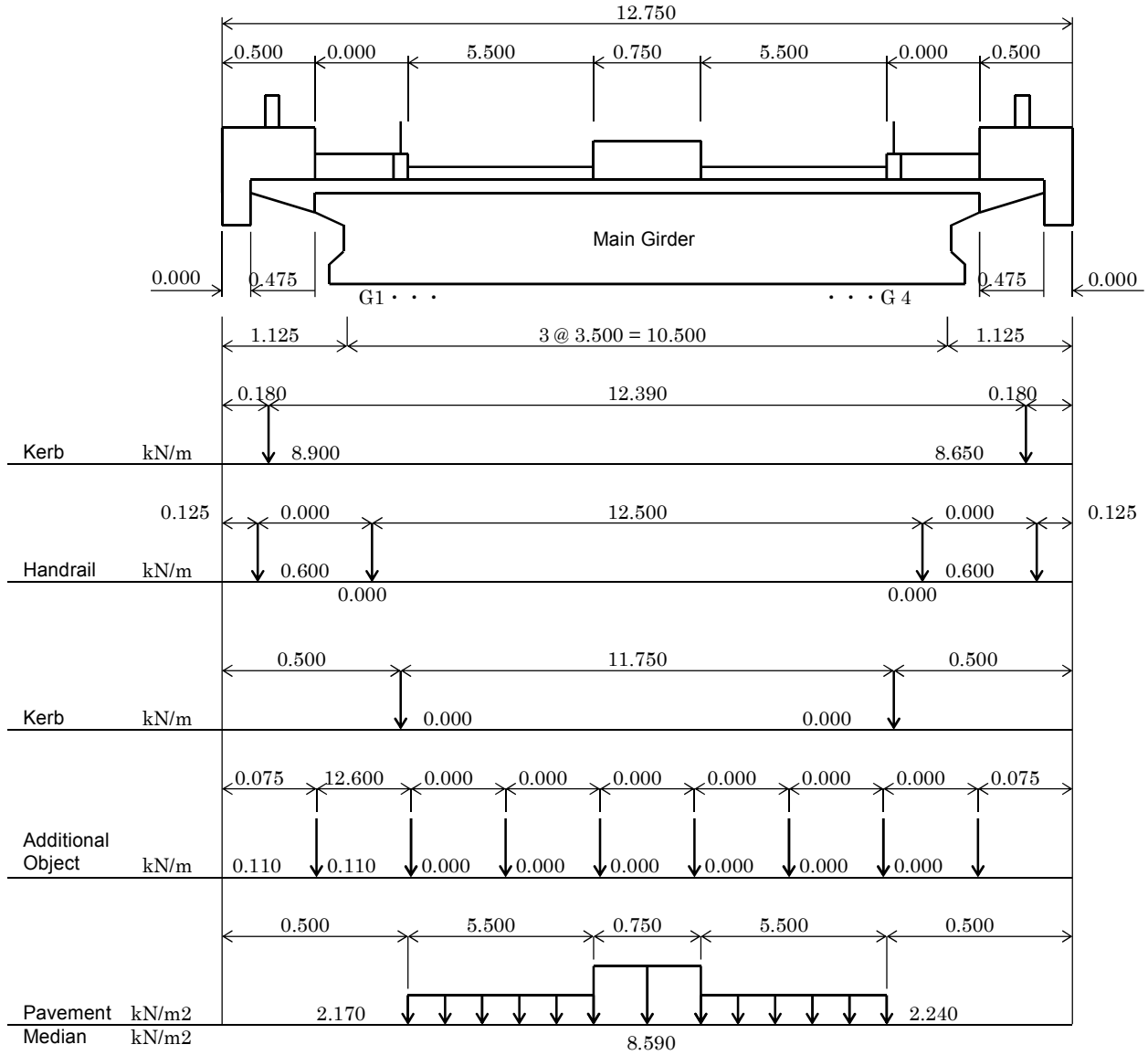
Load Location

$X' = 125\text{mm}$ inside beginning of Right and Left Kerb

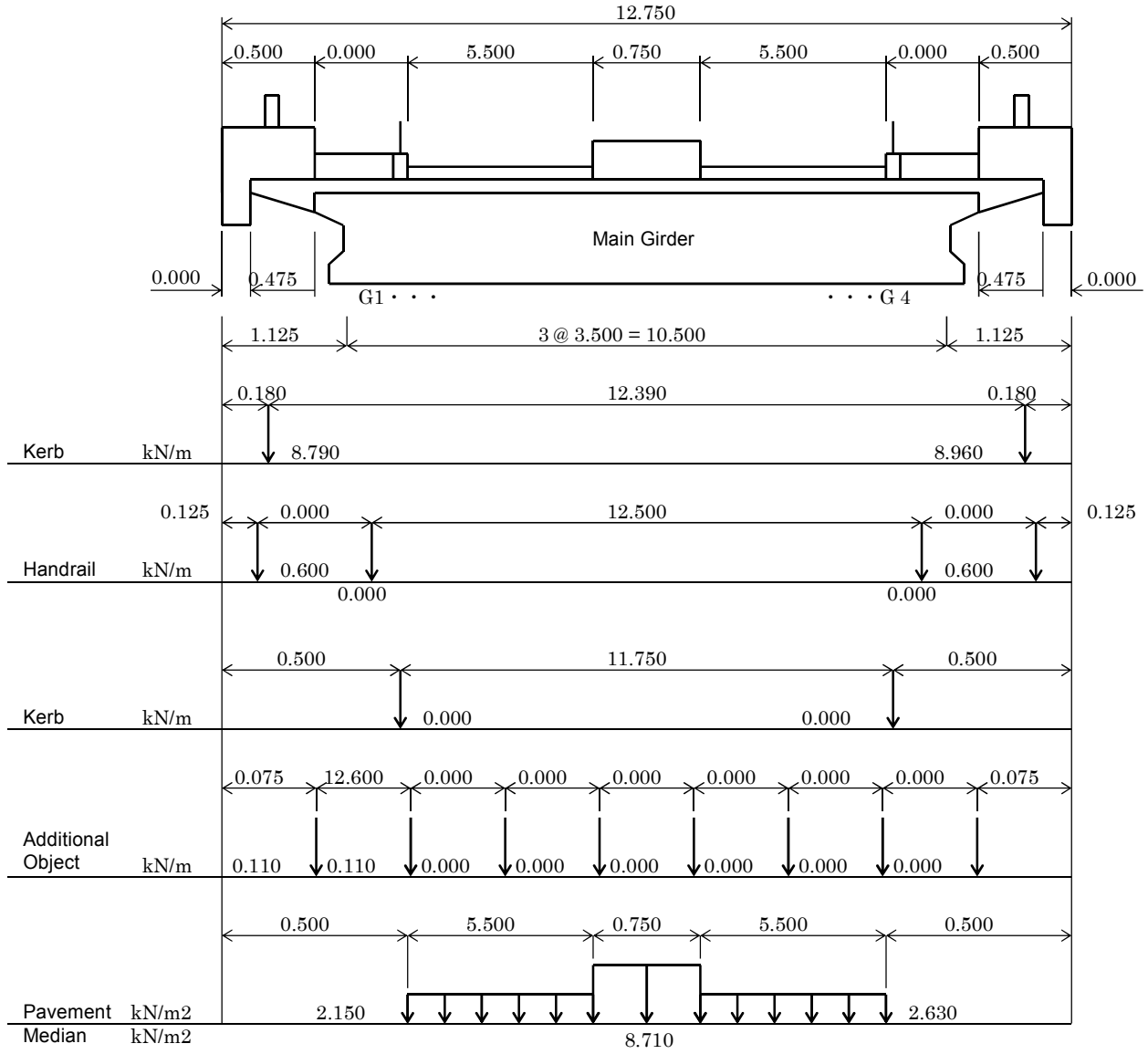
Load Intensity

$$P = 0.60 = \underline{0.60 \text{ kN/m}}$$

Load Intensity (Bridge Surface Loads_AF1-PF1)



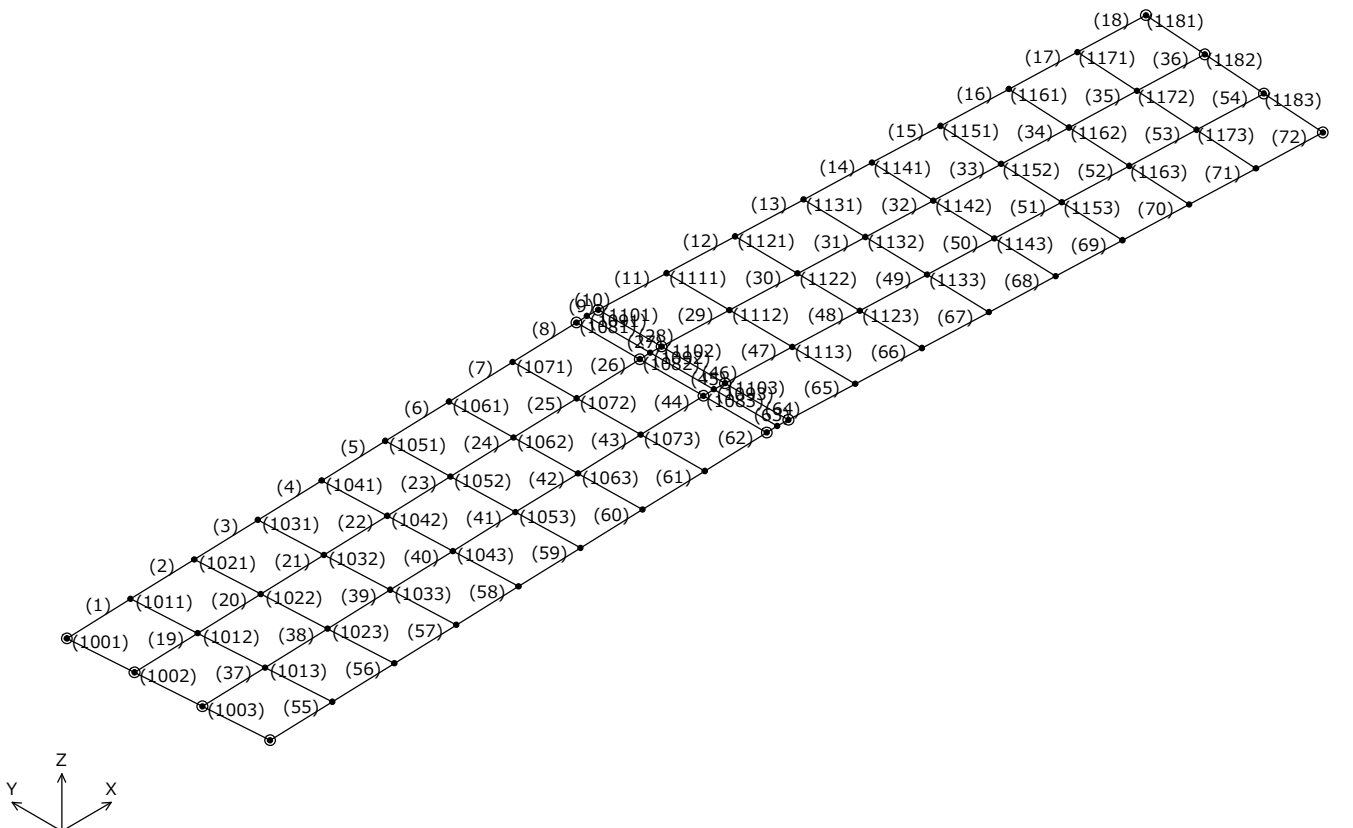
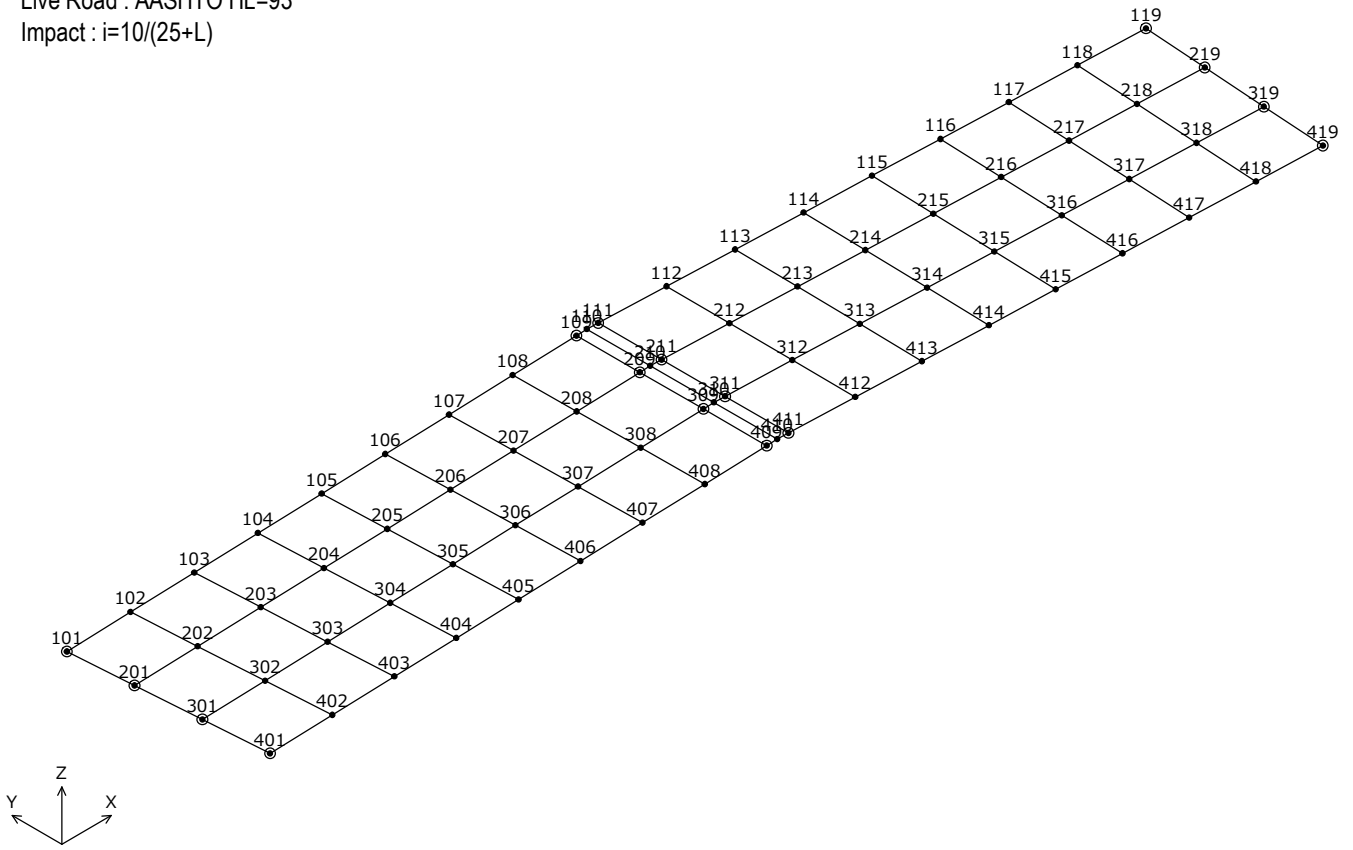
Load Intensity (Bridge Surface Loads_PF1-PF2)

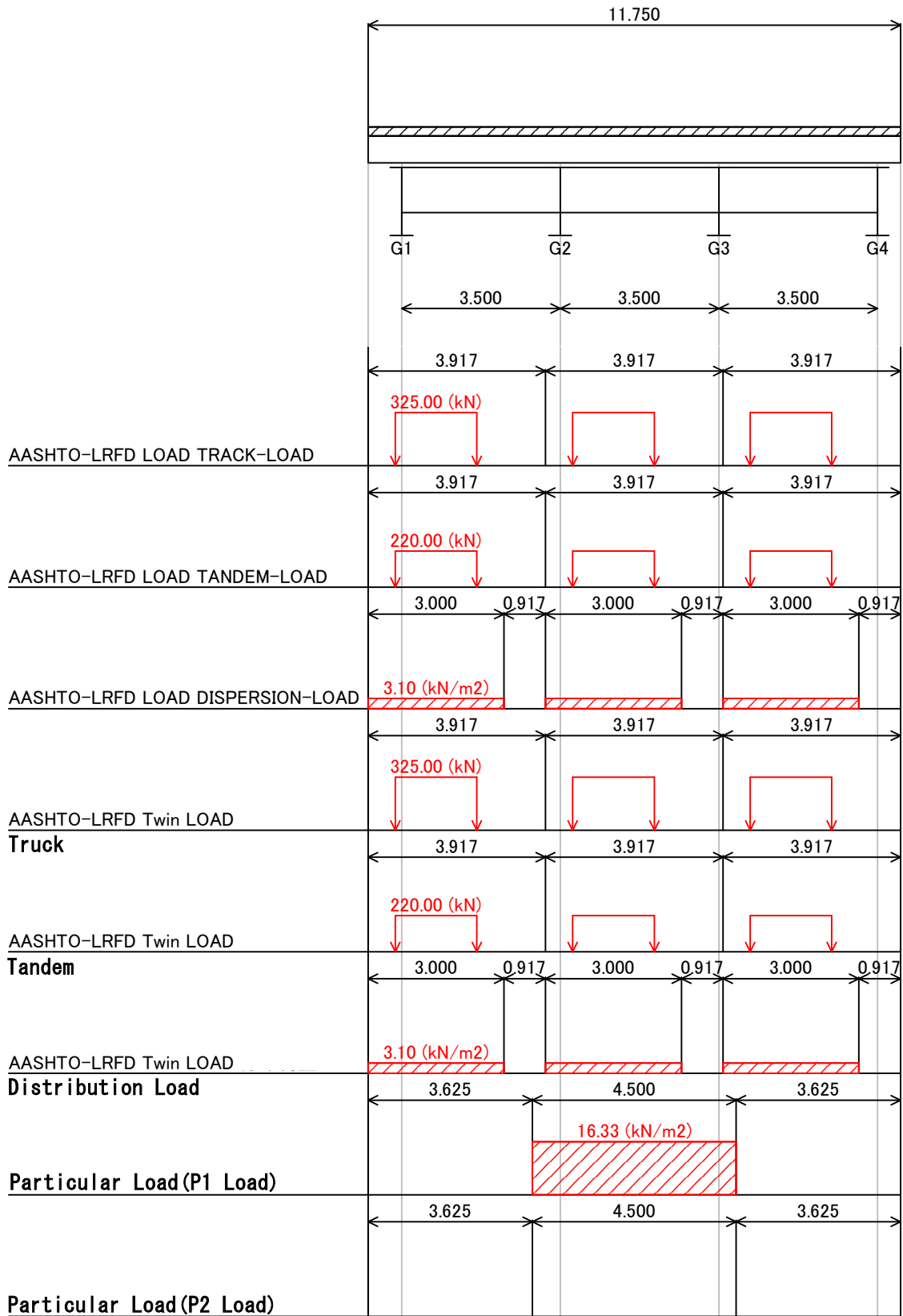


(2) Live Road

Live Road : AASHTO HL=93

Impact : $i=10/(25+L)$

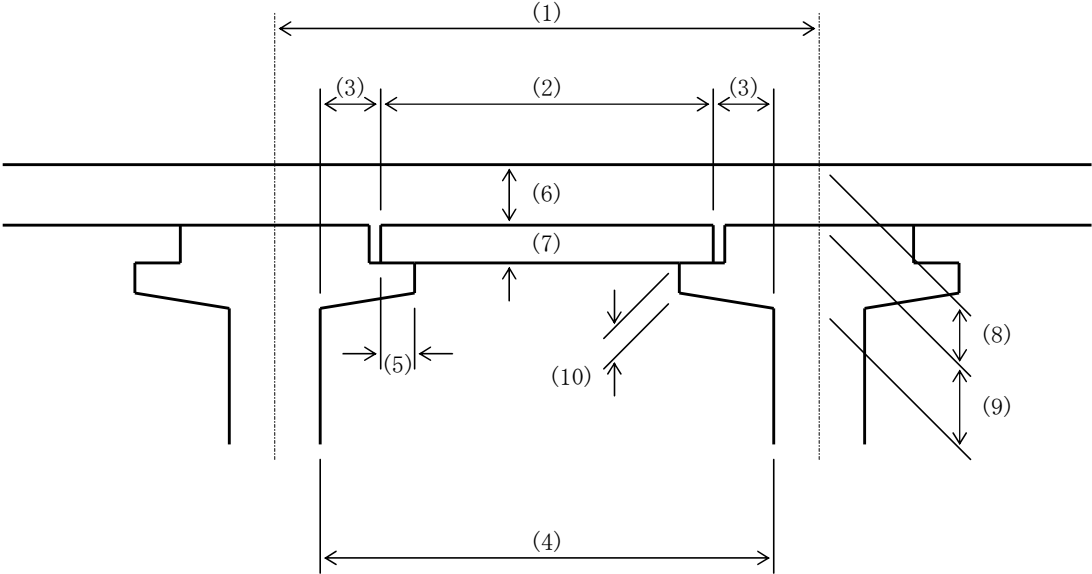




3 Design of Deck Slab

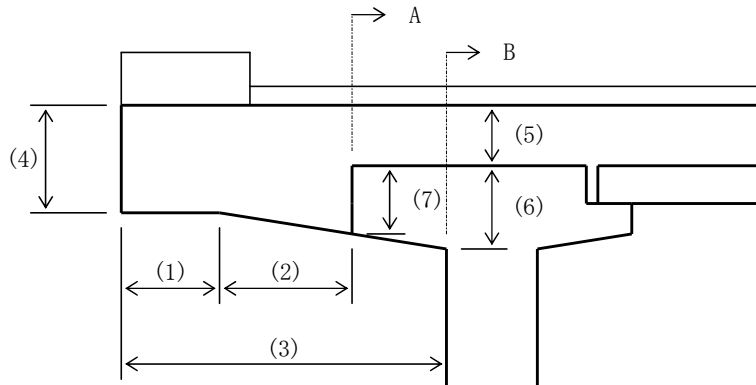
3.1 Dimension

1) Deck Slab between Girders



		1st Span		2nd Span	
		End of Girder	Center of Girder	Center of Girder	End of Girder
(1)	m	3.500	3.500	3.500	3.500
(2)	m	2.380	2.380	2.380	2.380
(3)	m	0.210	0.450	0.450	0.210
(4)	m	2.800	3.280	3.280	2.800
(5)	m	0.090	0.090	0.090	0.090
Span Length of PC Plate		2.260	2.260	2.260	2.260
(6)	mm	170.0	170.0	170.0	170.0
(7)	mm	100.0	100.0	100.0	100.0
(6)+(7)	mm	270.0	270.0	270.0	270.0
(8)	mm	170.0	170.0	170.0	170.0
(9)	mm	255.6	300.0	300.0	255.6
(10)	mm	100.0	100.0	100.0	100.0

2) Deck Slab outside of Girders



			1st Span		2nd Span	
			End of Girder	Center of Girder	Center of Girder	End of Girder
Left Side	(1)	m	0.000	0.000	0.000	0.000
	(2)	m	0.607	0.607	0.607	0.607
	(3)	m	0.907	1.147	1.147	0.907
	(4)	mm	250.0	250.0	250.0	250.0
	(5)	mm	170.0	170.0	170.0	170.0
	(6)	mm	255.6	300.0	300.0	255.6
	(7)	mm	200.0	200.0	200.0	200.0
Right Side	(1)	m	0.000	0.000	0.000	0.000
	(2)	m	0.607	0.607	0.607	0.607
	(3)	m	0.907	1.147	1.147	0.907
	(4)	mm	250.0	250.0	250.0	250.0
	(5)	mm	170.0	170.0	170.0	170.0
	(6)	mm	255.6	300.0	300.0	255.6
	(7)	mm	200.0	200.0	200.0	200.0

3) Calculation of Prestressing of PC Plate

		Unit	
Name of PC Strand			1S9.3
Material of PC Strand			SWPR7AL
Area of PC Strand		mm ² /no.	51.61
Number of PC Strand		No.	15
Creep Coefficient			3.00
Drying Shrinkage of Concrete		×10 ⁻⁵	25.00
Relaxation	Before Prestressing	%	1.50
	Extra Coefficient of High Temperature	%	1.00
	After Prestressing	%	1.50
Prestressing Stress σ_{pi}		N/mm ²	1225.00
Allowable Value		N/mm ²	1305.00

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Left End of Girder Side

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item		Unit	Allowable Value	Result	
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5	9.17	○
	Bottom of PC Plate	N/mm ²		~19.0	8.343
	Max×0.6	N/mm ²	8.343	5.502	○
Bending stress of PC plate	Top of PC Plate	N/mm ²	0	10.579	○
	Bottom of PC Plate	N/mm ²		~15.0	3.686
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11	3.479	○
	Bottom of RC Deck	N/mm ²		-0.799	○
	Top of PC Plate	N/mm ²	0	8.354	○
	Bottom of PC Plate	N/mm ²		~15.0	1.356
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305	1225	○
	Immediately After Prestressing	N/mm ²	1190	1131.097	○
	Effective Prestressing Force	N/mm ²	1020	921.338	○
Axial stress of PC plate		N/mm ²	10	8.756	○

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.555	○	140	73.604	○	
Edge of PC Plate	Positive Moment	10	3.843	○	140	59.714	○
	Negative Moment	10	3.743	○	140	78.38	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	8.659	○	140	100.221	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	0.56	○
Tensile Stress of Reinforcement Bar	140	27.98	○

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Left End of Girder Side

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	8.23	○
	D+L	10	0.314	○	140	8.23	○
	D+L+CO	15	2.151	○	300	56.373	○
	D+L+W	12.5	0.459	○	175	12.028	○
	D+W	12.5	0.604	○	175	15.827	○
Supporting for Deck	D	-----	-----	--	100	13.197	○
	D+L	10	3.525	○	140	101.529	○
	D+L+CO	15	4.977	○	300	143.358	○
	D+L+W	12.5	3.641	○	175	104.871	○
	D+W	12.5	0.69	○	175	19.881	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	8.07	○
	D+L	10	0.308	○	140	8.07	○
	D+L+CO	15	2.145	○	300	56.213	○
	D+L+W	12.5	0.453	○	175	11.868	○
	D+W	12.5	0.598	○	175	15.667	○
Supporting for Deck	D	-----	-----	--	100	12.972	○
	D+L	10	3.517	○	140	101.304	○
	D+L+CO	15	4.969	○	300	143.133	○
	D+L+W	12.5	3.633	○	175	104.646	○
	D+W	12.5	0.682	○	175	19.656	○

Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	1.857	○	140	67.16	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	1.857	○	140	67.16	○

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Center of Span

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item		Unit	Allowable Value	Result	
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5	9.17	○
	Bottom of PC Plate	N/mm ²		~19.0	8.343
	Max×0.6	N/mm ²	8.343	5.502	○
Bending stress of PC plate	Top of PC Plate	N/mm ²	0	10.584	○
	Bottom of PC Plate	N/mm ²		~15.0	3.691
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11	4.153	○
	Bottom of RC Deck	N/mm ²		-0.954	○
	Top of PC Plate	N/mm ²	0	8.187	○
	Bottom of PC Plate	N/mm ²		~15.0	0.649
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305	1225	○
	Immediately After Prestressing	N/mm ²	1190	1131.097	○
	Effective Prestressing Force	N/mm ²	1020	921.936	○
Axial stress of PC plate		N/mm ²	10	8.756	○

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.523	○	140	77.599	○	
Edge of PC Plate	Positive Moment	10	6.597	○	140	102.499	○
	Negative Moment	10	3.225	○	140	67.529	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	9.958	○	140	115.254	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	1.002	○
Tensile Stress of Reinforcement Bar	140	55.499	○

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Center of Span

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	8.228	○
	D+L	10	0.314	○	140	8.228	○
	D+L+CO	15	2.151	○	300	56.371	○
	D+L+W	12.5	0.459	○	175	12.027	○
	D+W	12.5	0.604	○	175	15.825	○
Supporting for Deck	D	-----	-----	--	100	16.718	○
	D+L	10	2.463	○	140	75.749	○
	D+L+CO	15	3.698	○	300	113.734	○
	D+L+W	12.5	2.563	○	175	78.813	○
	D+W	12.5	0.743	○	175	22.845	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	8.07	○
	D+L	10	0.308	○	140	8.07	○
	D+L+CO	15	2.145	○	300	56.213	○
	D+L+W	12.5	0.453	○	175	11.868	○
	D+W	12.5	0.598	○	175	15.667	○
Supporting for Deck	D	-----	-----	--	100	16.863	○
	D+L	10	2.468	○	140	75.895	○
	D+L+CO	15	3.703	○	300	113.879	○
	D+L+W	12.5	2.567	○	175	78.958	○
	D+W	12.5	0.748	○	175	22.991	○

Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	2.293	○	140	82.905	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	2.293	○	140	82.905	○

<Design of Deck: Summary for Calculation Results of Stress>

2nd Span, Center of Span

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item		Unit	Allowable Value	Result	
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5 ~ 19.0	9.17	○
	Bottom of PC Plate	N/mm ²		8.343	○
	Max×0.6	N/mm ²	8.343	5.502	○
Bending stress of PC plate	Top of PC Plate	N/mm ²	0 ~ 15.0	10.586	○
	Bottom of PC Plate	N/mm ²		3.694	○
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11	4.187	○
	Bottom of RC Deck	N/mm ²		-0.962	○
	Top of PC Plate	N/mm ²	0 ~ 15.0	8.181	○
	Bottom of PC Plate	N/mm ²		0.617	○
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305	1225	○
	Immediately After Prestressing	N/mm ²	1190	1131.097	○
	Effective Prestressing Force	N/mm ²	1020	922.32	○
Axial stress of PC plate		N/mm ²	10	8.756	○

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.539	○	140	78.077	○	
Edge of PC Plate	Positive Moment	10	6.65	○	140	103.329	○
	Negative Moment	10	3.245	○	140	67.945	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	9.958	○	140	115.254	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	1.002	○
Tensile Stress of Reinforcement Bar	140	55.499	○

<Design of Deck: Summary for Calculation Results of Stress>

2nd Span, Center of Span

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	8.157	○
	D+L	10	0.311	○	140	8.157	○
	D+L+CO	15	2.148	○	300	56.3	○
	D+L+W	12.5	0.456	○	175	11.956	○
	D+W	12.5	0.601	○	175	15.755	○
Supporting for Deck	D	-----	-----	--	100	16.596	○
	D+L	10	2.459	○	140	75.627	○
	D+L+CO	15	3.694	○	300	113.611	○
	D+L+W	12.5	2.559	○	175	78.69	○
	D+W	12.5	0.739	○	175	22.723	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	8.272	○
	D+L	10	0.316	○	140	8.272	○
	D+L+CO	15	2.153	○	300	56.415	○
	D+L+W	12.5	0.461	○	175	12.071	○
	D+W	12.5	0.606	○	175	15.87	○
Supporting for Deck	D	-----	-----	--	100	17.298	○
	D+L	10	2.482	○	140	76.329	○
	D+L+CO	15	3.717	○	300	114.314	○
	D+L+W	12.5	2.582	○	175	79.393	○
	D+W	12.5	0.762	○	175	23.425	○

Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	2.293	○	140	82.905	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	2.293	○	140	82.905	○

<Design of Deck: Summary for Calculation Results of Stress>

2nd Span, Right End of Girder Side

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item		Unit	Allowable Value	Result	
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5	9.17	○
	Bottom of PC Plate	N/mm ²		~ 19.0	8.343
	Max×0.6	N/mm ²	8.343	5.502	○
Bending stress of PC plate	Top of PC Plate	N/mm ²	0	10.581	○
	Bottom of PC Plate	N/mm ²		~ 15.0	3.688
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11	3.503	○
	Bottom of RC Deck	N/mm ²		-0.805	○
	Top of PC Plate	N/mm ²	0	8.35	○
	Bottom of PC Plate	N/mm ²		~ 15.0	1.332
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305	1225	○
	Immediately After Prestressing	N/mm ²	1190	1131.097	○
	Effective Prestressing Force	N/mm ²	1020	921.618	○
Axial stress of PC plate		N/mm ²	10	8.756	○

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.569	○	140	73.994	○	
Edge of PC Plate	Positive Moment	10	3.87	○	140	60.135	○
	Negative Moment	10	3.763	○	140	78.796	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	8.659	○	140	100.221	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	0.56	○
Tensile Stress of Reinforcement Bar	140	27.98	○

<Design of Deck: Summary for Calculation Results of Stress>

2nd Span, Right End of Girder Side

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	8.159	○
	D+L	10	0.311	○	140	8.159	○
	D+L+CO	15	2.148	○	300	56.302	○
	D+L+W	12.5	0.456	○	175	11.958	○
	D+W	12.5	0.601	○	175	15.756	○
Supporting for Deck	D	-----	-----	--	100	13.093	○
	D+L	10	3.521	○	140	101.424	○
	D+L+CO	15	4.974	○	300	143.254	○
	D+L+W	12.5	3.637	○	175	104.766	○
	D+W	12.5	0.687	○	175	19.777	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	8.272	○
	D+L	10	0.316	○	140	8.272	○
	D+L+CO	15	2.153	○	300	56.415	○
	D+L+W	12.5	0.461	○	175	12.071	○
	D+W	12.5	0.606	○	175	15.87	○
Supporting for Deck	D	-----	-----	--	100	13.302	○
	D+L	10	3.529	○	140	101.633	○
	D+L+CO	15	4.981	○	300	143.463	○
	D+L+W	12.5	3.645	○	175	104.975	○
	D+W	12.5	0.694	○	175	19.986	○

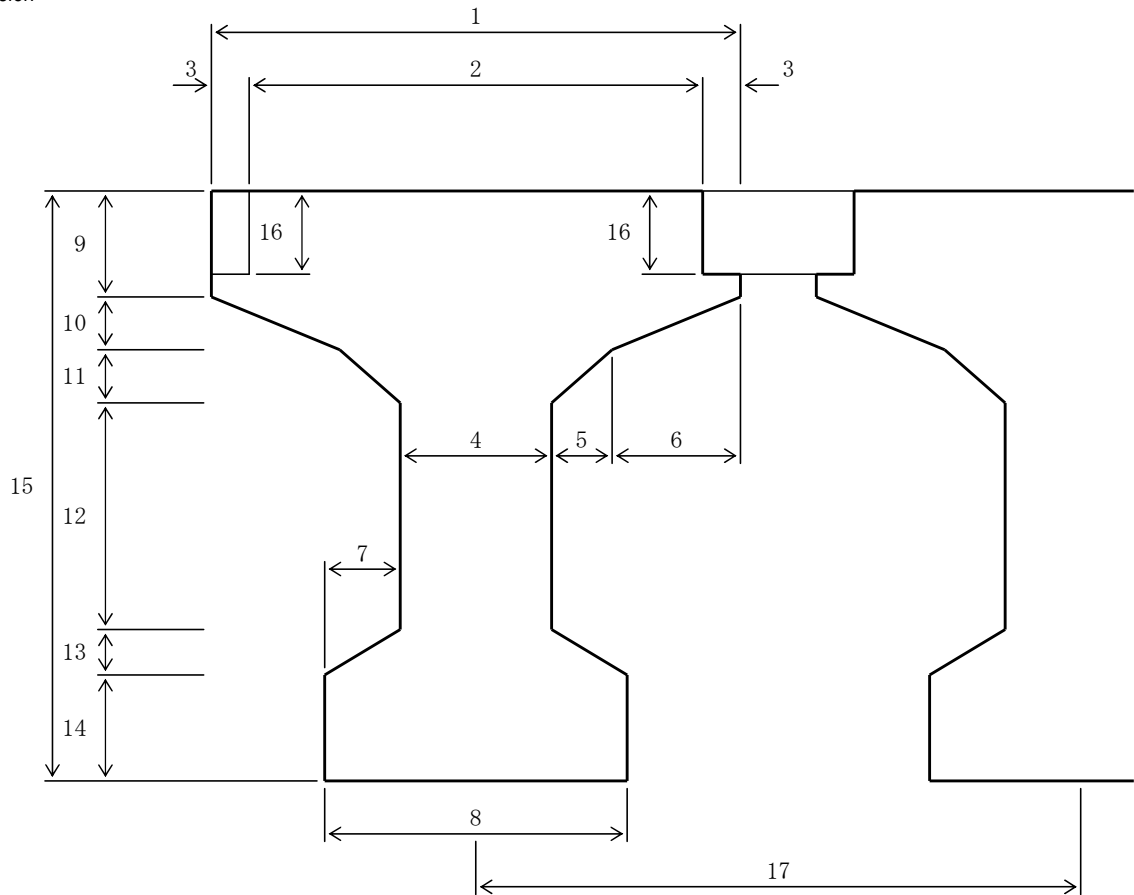
Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	1.857	○	140	67.16	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	1.857	○	140	67.16	○

4 Design of Main Girder

4.1 Dimension and PC Strand Arrangement

1) Dimension



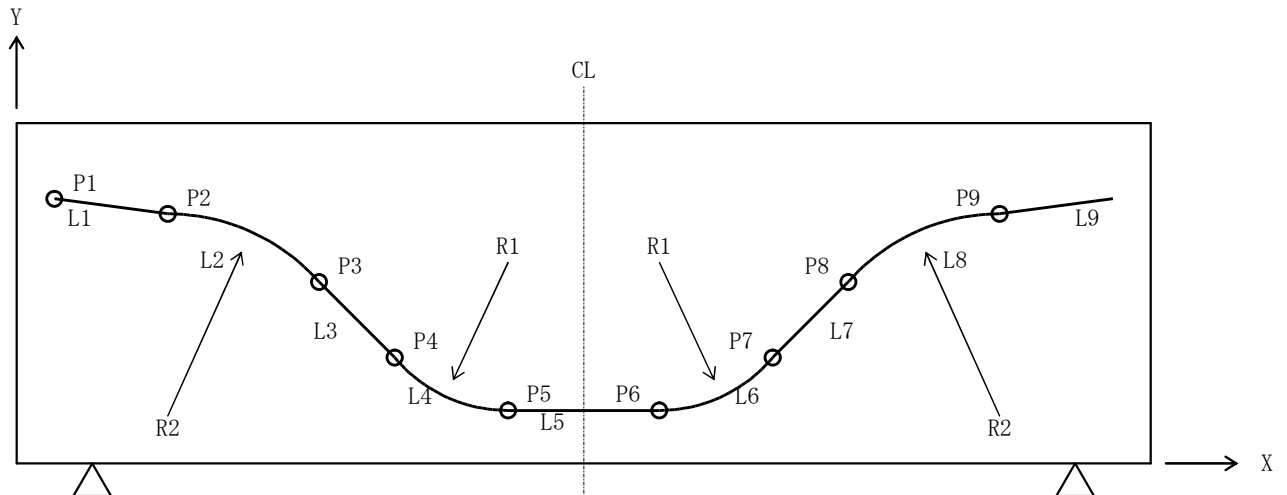
(Unit: mm)

	1st Span			2nd Span		
	End of Girder (Left)	Center Span	End of Girder (Right)	End of Girder (Left)	Center Span	End of Girder (Right)
1	1300.0	1300.0	1300.0	1300.0	1300.0	1300.0
2	1060.0	1060.0	1060.0	1060.0	1060.0	1060.0
3	120.0	120.0	120.0	120.0	120.0	120.0
4	700.0	220.0	700.0	700.0	220.0	700.0
5	0.0	0.0	0.0	0.0	0.0	0.0
6	300.0	540.0	300.0	300.0	540.0	300.0
7	0.0	240.0	0.0	0.0	240.0	0.0
8	700.0	700.0	700.0	700.0	700.0	700.0
9	200.0	200.0	200.0	200.0	200.0	200.0
10	55.6	100.0	55.6	55.6	100.0	55.6
11	0.0	0.0	0.0	0.0	0.0	0.0
12	1444.4	1150.0	1444.4	1444.4	1150.0	1444.4
13	0.0	250.0	0.0	0.0	250.0	0.0
14	200.0	200.0	200.0	200.0	200.0	200.0
15	1900.0	1900.0	1900.0	1900.0	1900.0	1900.0
16	100.0	100.0	100.0	100.0	100.0	100.0
17	3500.0	3500.0	3500.0	3500.0	3500.0	3500.0

2) PC Strand Arrangement

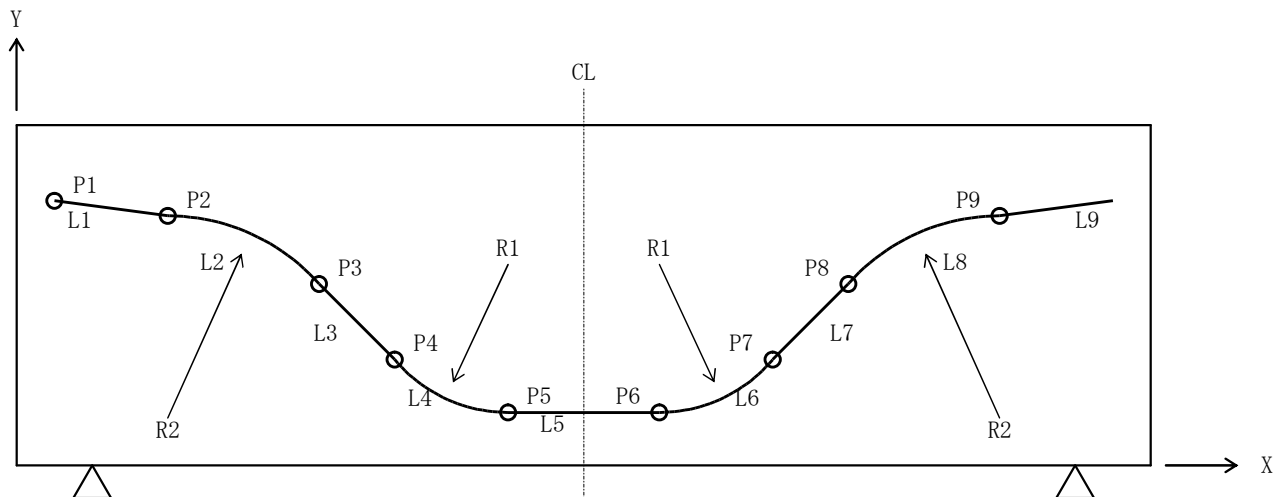
<1st Span>

PC Strand No.		1	2	3	4	5
Number of PC Strand		1	1	1	1	1
Coordinate (mm)	P1 X	-----	-----	-----	-----	-----
	Y	-----	-----	-----	-----	-----
	P2 X	-----	-----	-----	-----	-----
	Y	-----	-----	-----	-----	-----
	P3 X	200.0	200.0	200.0	200.0	200.0
	Y	1650.0	1300.0	950.0	600.0	250.0
	P4 X	13119.0	10730.4	8341.8	4706.9	1710.7
	Y	406.0	286.0	166.0	166.0	144.4
	P5 X	14077.5	11688.9	9300.2	5665.3	2408.3
	Y	360.0	240.0	120.0	120.0	120.0
	P6 X	16197.8	18071.0	19944.2	22794.8	25616.5
	Y	360.0	240.0	120.0	120.0	120.0
P7 X	17416.5	19289.7	21162.9	24013.4	26575.0	
Y	434.5	314.5	194.5	194.5	166.0	
P8 X	26708.6	26708.6	26708.6	26708.6	26968.8	
Y	1575.5	1225.5	875.5	525.5	204.0	
P9 X	27927.3	27927.3	27927.3	27927.3	27927.3	
Y	1650.0	1300.0	950.0	600.0	250.0	
P1 [~] X	29727.3	29727.3	29727.3	29727.3	29727.3	
Y	1650.0	1300.0	950.0	600.0	250.0	
Angle	α (L) (R)	5°30'0" 0°0'0"	5°30'0" 0°0'0"	5°30'0" 0°0'0"	5°30'0" 0°0'0"	4°0'0" 0°0'0"
Radius (m)	R2 (L)	-----	-----	-----	-----	-----
	R1 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (R)	10.000	10.000	10.000	10.000	10.000
	R2 (R)	10.000	10.000	10.000	10.000	10.000
Angle	β (L) (R)	----- 7°0'0"	----- 7°0'0"	----- 7°0'0"	----- 7°0'0"	----- 5°30'0"
Length of PC Strand (m)	L1	-----	-----	-----	-----	-----
	L2	-----	-----	-----	-----	-----
	L3	12.979	10.579	8.179	4.528	1.514
	L4	0.960	0.960	0.960	0.960	0.698
	L5	2.120	6.382	10.644	17.129	23.208
	L6	1.222	1.222	1.222	1.222	0.960
	L7	9.362	7.475	5.587	2.715	0.396
	L8	1.222	1.222	1.222	1.222	0.960
	L9	1.800	1.800	1.800	1.800	1.800
	Total	29.664	29.639	29.614	29.576	29.536



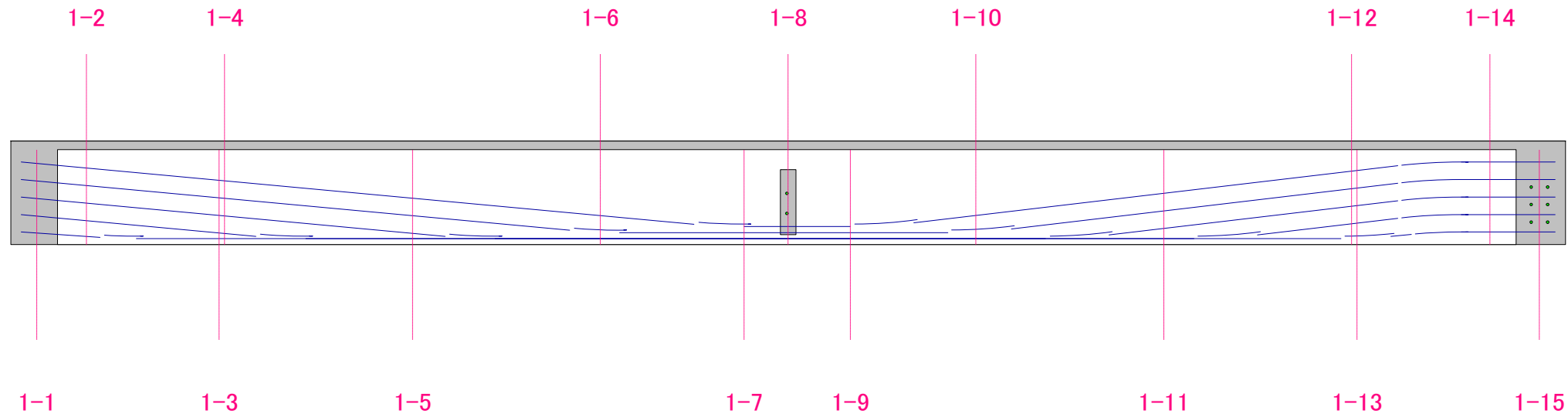
<2nd Span>

PC Strand No.		1	2	3	4	5
Number of PC Strand		1	1	1	1	1
Coordinate (mm)	P1 X	200.0	200.0	200.0	200.0	200.0
	Y	1650.0	1300.0	950.0	600.0	250.0
	P2 X	2000.0	2000.0	2000.0	2000.0	2000.0
	Y	1650.0	1300.0	950.0	600.0	250.0
	P3 X	3218.7	3218.7	3218.7	3218.7	2958.5
	Y	1575.5	1225.5	875.5	525.5	204.0
	P4 X	12510.8	10637.6	8764.4	5913.8	3352.3
	Y	434.5	314.5	194.5	194.5	166.0
	P5 X	13729.5	11856.3	9983.1	7132.5	4310.8
	Y	360.0	240.0	120.0	120.0	120.0
	P6 X	15895.2	18283.9	20672.5	24307.4	27564.4
	Y	360.0	240.0	120.0	120.0	120.0
	P7 X	16853.7	19242.3	21630.9	25265.8	28262.0
	Y	406.0	286.0	166.0	166.0	144.4
	P8 X	29772.7	29772.7	29772.7	29772.7	29772.7
	Y	1650.0	1300.0	950.0	600.0	250.0
	P9 X	-----	-----	-----	-----	-----
	Y	-----	-----	-----	-----	-----
P10 X	-----	-----	-----	-----	-----	
Y	-----	-----	-----	-----	-----	
Angle	α (L)	0°0'0"	0°0'0"	0°0'0"	0°0'0"	0°0'0"
	(R)	5°30'0"	5°30'0"	5°30'0"	5°30'0"	4°0'0"
Radius (m)	R2 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (R)	10.000	10.000	10.000	10.000	10.000
	R2 (R)	-----	-----	-----	-----	-----
Angle	β (L)	7°0'0"	7°0'0"	7°0'0"	7°0'0"	5°30'0"
	(R)	-----	-----	-----	-----	-----
Length of PC Strand (m)	L1	1.800	1.800	1.800	1.800	1.800
	L2	1.222	1.222	1.222	1.222	0.960
	L3	9.362	7.475	5.587	2.715	0.396
	L4	1.222	1.222	1.222	1.222	0.960
	L5	2.166	6.428	10.689	17.175	23.254
	L6	0.960	0.960	0.960	0.960	0.698
	L7	12.979	10.579	8.179	4.528	1.514
	L8	-----	-----	-----	-----	-----
	L9	-----	-----	-----	-----	-----
	Total		29.710	29.685	29.660	29.621



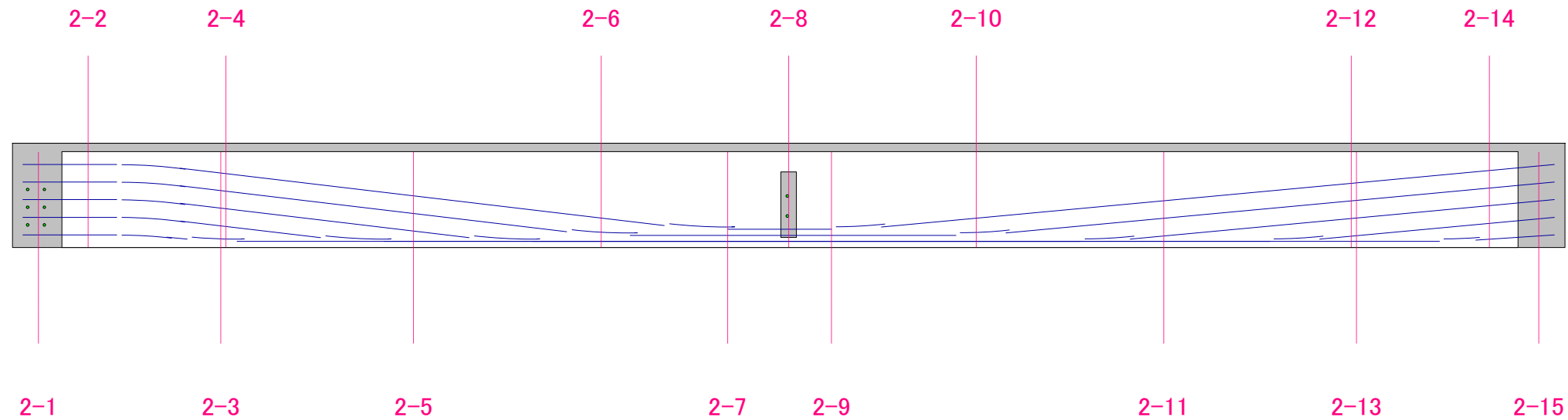
4.4 Summary for Calculation Results of Stress

1) AF1-PF2



		Unit	Allowable Value	Cross Section Number		
Calculation for Bending Moment				[1- 7]	[1- 8]	[1- 9]
				Bent up Point(Left)	Center of Span	Bent up Point(Right)
Bending Stress of Concrete						
Immediately After Prestressing	N/mm ²	-1.5 ~ 19.00	Top of Main Girder	0.76	0.80	0.78
			Bottom of Main Girder	15.09	14.99	14.94
During Deck Construction	"	-1.5 ~ 14.00	Top of Main Girder	6.30	6.36	6.28
			Bottom of Main Girder	7.08	6.96	6.98
Dead Load	"	≤ 10.00	Top of Deck	2.97	3.04	3.03
		0 ~ 14.00	Top of Main Girder	5.44	5.51	5.49
			Bottom of Main Girder	2.67	2.45	2.39
Design Load	"	≤ 10.00	Top of Deck max	4.50	4.54	4.48
			Top of Deck min	2.61	2.65	2.61
		-1.5 ~ 14.00	Top of Main Girder(max)	6.70	6.75	6.68
			Bottom of Main Girder(max)	-0.89	-1.05	-0.99
			Top of Main Girder(min)	5.14	5.19	5.14
		Bottom of Main Girder(min)	3.51	3.35	3.37	
Stress of PC Strand	N/mm ²	Pmax ≤ 1110		1048	1045	1036
Ultimate Load	----	F ≥ 1.0		1.16	1.16	1.18
Calculation for Shear Force				[1- 2]	[1- 3]	[1- 14]
				Near a Support of girder(Left)	Change point of Web Width(Left)	Near a Support of girder(Right)
Shear Stress of Design Load	kN			0.55	1.29	0.97
Compressive Strength to Failure	----	F ≥ 1.0		3.92	1.83	3.19
Diagonal Tensile Stress	Dead Load	N/mm ²	≥ -1	-0.04	-0.12	-0.22
	Design Load	"	≥ -2	-0.16	-0.49	-0.39

2) PF1-PF2



		Unit	Allowable Value	Cross Section Number		
Calculation for Bending Moment				[2- 7]	[2- 8]	[2- 9]
				Bent up Point(Left)	Center of Span	Bent up Point(Right)
Bending Stress of Concrete						
Immediately After Prestressing	N/mm ²	-1.5 ~ 19.00	Top of Main Girder	0.79	0.82	0.78
			Bottom of Main Girder	14.92	14.97	15.07
During Deck Construction	"	-1.5 ~ 14.00	Top of Main Girder	6.31	6.39	6.33
			Bottom of Main Girder	6.95	6.92	7.05
Dead Load	"	≤ 10.00	Top of Deck	3.07	3.08	3.01
		0 ~ 14.00	Top of Main Girder	5.53	5.55	5.47
			Bottom of Main Girder	2.30	2.36	2.58
Design Load	"	≤ 10.00	Top of Deck max	4.52	4.58	4.54
			Top of Deck min	2.65	2.69	2.64
		-1.5 ~ 14.00	Top of Main Girder(max)	6.72	6.79	6.74
			Bottom of Main Girder(max)	-1.08	-1.14	-0.98
			Top of Main Girder(min)	5.18	5.23	5.18
		Bottom of Main Girder(min)	3.28	3.26	3.43	
Stress of PC Strand	N/mm ²	P _{max} ≤ 1110		1037	1047	1050
Ultimate Load	----	F ≥ 1.0		1.17	1.15	1.16
Calculation for Shear Force				[2- 2]	[2-13]	[2-14]
				Near a Support of girder(Left)	Change point of Web Width(Right)	Near a Support of girder(Right)
Shear Stress of Design Load	kN			0.97	1.28	0.55
Compressive Strength to Failure	----	F ≥ 1.0		3.20	1.84	3.91
Diagonal Tensile Stress	Dead Load	N/mm ²	≥ -1	-0.22	-0.12	-0.04
	Design Load	"	≥ -2	-0.40	-0.49	-0.16

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[1- 1]		[1- 2]		[1- 3]	
Interval from beginning of Girder		-----	0.500		1.450		4.000	
Immediately After Prestressing	Top of Main Girder	-1.5	2.971	○	2.771	○	3.781	
	Bottom of Main Girder	~19.00	5.077	○	6.016	○	11.160	
During Deck Construction	Top of Main Girder	-1.5	2.819	○	3.207	○	5.823	
	Bottom of Main Girder	~14.00	4.817	○	5.018	○	7.575	
Dead Load	Top of Deck	≤10.00	0.275	○	0.548	○	1.388	
	Top of Main Girder	0	2.120	○	2.482	○	4.321	
	Bottom of Main Girder	~14.00	4.786	○	4.694	○	5.873	
Design Load1	Top of Deck	Max	0.275	○	0.821	○	2.276	
		Min	≤10.00	0.274	○	0.523	○	1.292
	Top of Main Girder	Max	-1.5	2.120	○	2.719	○	5.053
		Min	~14.00	2.120	○	2.461	○	4.243
	Bottom of Main Girder	Max	~14.00	4.786	○	4.190	○	3.779
		Min	~14.00	4.786	○	4.740	○	6.097
Design Load2 Temperature Rise	Top of Deck	Max	≤11.50	0.793	○	1.346	○	2.780
		Min	≤11.50	0.793	○	1.048	○	1.796
	Top of Main Girder	Max	-2	1.264	○	1.866	○	4.159
		Min	~16.10	1.263	○	1.607	○	3.349
	Bottom of Main Girder	Max	~16.10	5.260	○	4.627	○	3.994
		Min	~16.10	5.260	○	5.178	○	6.312
Design Load3 Temperature Drop	Top of Deck	Max	≤11.50	0.793	○	1.346	○	2.780
		Min	≤11.50	0.793	○	1.048	○	1.796
	Top of Main Girder	Max	-2	1.264	○	1.866	○	4.159
		Min	~16.10	1.263	○	1.607	○	3.349
	Bottom of Main Girder	Max	~16.10	5.260	○	4.627	○	3.994
		Min	~16.10	5.260	○	5.178	○	6.312
Design Load4 Support sinking	Top of Deck	Max	≤10.00	0.275	○	0.821	○	2.276
		Min	≤10.00	0.274	○	0.523	○	1.292
	Top of Main Girder	Max	-1.5	2.120	○	2.719	○	5.053
		Min	~14.00	2.120	○	2.461	○	4.243
	Bottom of Main Girder	Max	~14.00	4.786	○	4.190	○	3.779
		Min	~14.00	4.786	○	4.740	○	6.097
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	≤11.50	0.793	○	1.346	○	2.780
		Min	≤11.50	0.793	○	1.048	○	1.796
	Top of Main Girder	Max	-2	1.264	○	1.866	○	4.159
		Min	~16.10	1.263	○	1.607	○	3.349
	Bottom of Main Girder	Max	~16.10	5.260	○	4.627	○	3.994
		Min	~16.10	5.260	○	5.178	○	6.312
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	≤11.50	0.793	○	1.346	○	2.780
		Min	≤11.50	0.793	○	1.048	○	1.796
	Top of Main Girder	Max	-2	1.264	○	1.866	○	4.159
		Min	~16.10	1.263	○	1.607	○	3.349
	Bottom of Main Girder	Max	~16.10	5.260	○	4.627	○	3.994
		Min	~16.10	5.260	○	5.178	○	6.312

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1- 4]		[1- 5]		[1- 6]		
Interval from beginning of Girder		-----	4.116		7.732		11.348		
Immediately After Prestressing	Top of Main Girder	-1.5	3.725	○	2.197	○	0.993	○	
	Bottom of Main Girder	~19.00	11.238	○	13.449	○	15.059	○	
During Deck Construction	Top of Main Girder	-1.5	5.836	○	6.136	○	6.108	○	
	Bottom of Main Girder	~14.00	7.565	○	7.454	○	7.551	○	
Dead Load	Top of Deck	≤10.00	1.413	○	2.118	○	2.623	○	
	Top of Main Girder	0	4.343	○	4.887	○	5.143	○	
	Bottom of Main Girder	~14.00	5.819	○	4.516	○	3.640	○	
Design Load1	Top of Deck	Max	2.325	○	3.515	○	4.172	○	
		Min	1.315	○	1.923	○	2.332	○	
	Top of Main Girder	Max	5.093	○	6.038	○	6.421	○	
		Min	-1.5	4.262	○	4.726	○	4.903	○
	Bottom of Main Girder	Max	~14.00	3.672	○	1.246	○	0.030	○
		Min		6.051	○	4.973	○	4.318	○
Design Load2 Temperature Rise	Top of Deck	Max	2.830	○	4.097	○	4.829	○	
		Min	≤11.50	1.820	○	2.504	○	2.988	○
	Top of Main Girder	Max	4.201	○	5.209	○	5.653	○	
		Min	-2	3.370	○	3.897	○	4.136	○
	Bottom of Main Girder	Max	~16.10	3.882	○	1.279	○	-0.110	○
		Min		6.260	○	5.006	○	4.178	○
Design Load3 Temperature Drop	Top of Deck	Max	2.830	○	4.097	○	4.829	○	
		Min	≤11.50	1.820	○	2.504	○	2.988	○
	Top of Main Girder	Max	4.201	○	5.209	○	5.653	○	
		Min	-2	3.370	○	3.897	○	4.136	○
	Bottom of Main Girder	Max	~16.10	3.882	○	1.279	○	-0.110	○
		Min		6.260	○	5.006	○	4.178	○
Design Load4 Support sinking	Top of Deck	Max	2.325	○	3.515	○	4.172	○	
		Min	≤10.00	1.315	○	1.923	○	2.332	○
	Top of Main Girder	Max	5.093	○	6.038	○	6.421	○	
		Min	-1.5	4.262	○	4.726	○	4.903	○
	Bottom of Main Girder	Max	~14.00	3.672	○	1.246	○	0.030	○
		Min		6.051	○	4.973	○	4.318	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	2.830	○	4.097	○	4.829	○	
		Min	≤11.50	1.820	○	2.504	○	2.988	○
	Top of Main Girder	Max	4.201	○	5.209	○	5.653	○	
		Min	-2	3.370	○	3.897	○	4.136	○
	Bottom of Main Girder	Max	~16.10	3.882	○	1.279	○	-0.110	○
		Min		6.260	○	5.006	○	4.178	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	2.830	○	4.097	○	4.829	○	
		Min	≤11.50	1.820	○	2.504	○	2.988	○
	Top of Main Girder	Max	4.201	○	5.209	○	5.653	○	
		Min	-2	3.370	○	3.897	○	4.136	○
	Bottom of Main Girder	Max	~16.10	3.882	○	1.279	○	-0.110	○
		Min		6.260	○	5.006	○	4.178	○

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1- 7]		[1- 8]		[1- 9]		
Interval from beginning of Girder		-----	14.078		14.964		16.198		
Immediately After Prestressing	Top of Main Girder	-1.5	0.764	○	0.799	○	0.778	○	
	Bottom of Main Girder	~19.00	15.089	○	14.989	○	14.935	○	
During Deck Construction	Top of Main Girder	-1.5	6.298	○	6.359	○	6.280	○	
	Bottom of Main Girder	~14.00	7.084	○	6.960	○	6.980	○	
Dead Load	Top of Deck	≤10.00	2.970	○	3.036	○	3.034	○	
	Top of Main Girder	0	5.436	○	5.512	○	5.486	○	
	Bottom of Main Girder	~14.00	2.665	○	2.446	○	2.387	○	
Design Load1	Top of Deck	Max	4.498	○	4.537	○	4.484	○	
		Min	2.605	○	2.648	○	2.614	○	
	Top of Main Girder	Max	6.697	○	6.750	○	6.683	○	
		Min	-1.5	5.135	○	5.191	○	5.139	○
	Bottom of Main Girder	Max	~14.00	-0.891	○	-1.048	○	-0.988	○
		Min		3.513	○	3.350	○	3.366	○
Design Load2 Temperature Rise	Top of Deck	Max	5.211	○	5.269	○	5.242	○	
		Min	≤11.50	3.318	○	3.379	○	3.371	○
	Top of Main Girder	Max	5.976	○	6.045	○	5.999	○	
		Min	-2	4.415	○	4.486	○	4.455	○
	Bottom of Main Girder	Max	~16.10	-1.163	○	-1.362	○	-1.363	○
		Min		3.242	○	3.035	○	2.991	○
Design Load3 Temperature Drop	Top of Deck	Max	5.211	○	5.269	○	5.242	○	
		Min	≤11.50	3.318	○	3.379	○	3.371	○
	Top of Main Girder	Max	5.976	○	6.045	○	5.999	○	
		Min	-2	4.415	○	4.486	○	4.455	○
	Bottom of Main Girder	Max	~16.10	-1.163	○	-1.362	○	-1.363	○
		Min		3.242	○	3.035	○	2.991	○
Design Load4 Support sinking	Top of Deck	Max	4.498	○	4.537	○	4.484	○	
		Min	≤10.00	2.605	○	2.648	○	2.614	○
	Top of Main Girder	Max	6.697	○	6.750	○	6.683	○	
		Min	-1.5	5.135	○	5.191	○	5.139	○
	Bottom of Main Girder	Max	~14.00	-0.891	○	-1.048	○	-0.988	○
		Min		3.513	○	3.350	○	3.366	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	5.211	○	5.269	○	5.242	○	
		Min	≤11.50	3.318	○	3.379	○	3.371	○
	Top of Main Girder	Max	5.976	○	6.045	○	5.999	○	
		Min	-2	4.415	○	4.486	○	4.455	○
	Bottom of Main Girder	Max	~16.10	-1.163	○	-1.362	○	-1.363	○
		Min		3.242	○	3.035	○	2.991	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	5.211	○	5.269	○	5.242	○	
		Min	≤11.50	3.318	○	3.379	○	3.371	○
	Top of Main Girder	Max	5.976	○	6.045	○	5.999	○	
		Min	-2	4.415	○	4.486	○	4.455	○
	Bottom of Main Girder	Max	~16.10	-1.163	○	-1.362	○	-1.363	○
		Min		3.242	○	3.035	○	2.991	○

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1-10]		[1-11]		[1-12]		
Interval from beginning of Girder		-----	18.579		22.195		25.811		
Immediately After Prestressing	Top of Main Girder	-1.5	1.113	○	2.974	○	5.668	○	
	Bottom of Main Girder	~19.00	14.439	○	12.169	○	8.601	○	
During Deck Construction	Top of Main Girder	-1.5	6.209	○	6.840	○	7.640	○	
	Bottom of Main Girder	~14.00	7.004	○	6.336	○	5.182	○	
Dead Load	Top of Deck	≤10.00	2.930	○	2.812	○	2.595	○	
	Top of Main Girder	0	5.438	○	5.779	○	6.108	○	
	Bottom of Main Girder	~14.00	2.455	○	2.210	○	1.840	○	
Design Load1	Top of Deck	Max	4.228	○	3.718	○	2.962	○	
		Min	2.445	○	2.207	○	1.781	○	
	Top of Main Girder	Max	6.508	○	6.525	○	6.410	○	
		Min	-1.5	5.038	○	5.280	○	5.439	○
	Bottom of Main Girder	Max	~14.00	-0.569	○	0.088	○	0.972	○
		Min		3.585	○	3.630	○	3.765	○
Design Load2 Temperature Rise	Top of Deck	Max	5.036	○	4.605	○	3.930	○	
		Min	≤11.50	3.253	○	3.094	○	2.749	○
	Top of Main Girder	Max	5.866	○	5.947	○	5.898	○	
		Min	-2	4.396	○	4.703	○	4.927	○
	Bottom of Main Girder	Max	~16.10	-1.063	○	-0.596	○	0.088	○
		Min		3.091	○	2.946	○	2.881	○
Design Load3 Temperature Drop	Top of Deck	Max	5.036	○	4.605	○	3.930	○	
		Min	≤11.50	3.253	○	3.094	○	2.749	○
	Top of Main Girder	Max	5.866	○	5.947	○	5.898	○	
		Min	-2	4.396	○	4.703	○	4.927	○
	Bottom of Main Girder	Max	~16.10	-1.063	○	-0.596	○	0.088	○
		Min		3.091	○	2.946	○	2.881	○
Design Load4 Support sinking	Top of Deck	Max	4.228	○	3.718	○	2.962	○	
		Min	≤10.00	2.445	○	2.207	○	1.781	○
	Top of Main Girder	Max	6.508	○	6.525	○	6.410	○	
		Min	-1.5	5.038	○	5.280	○	5.439	○
	Bottom of Main Girder	Max	~14.00	-0.569	○	0.088	○	0.972	○
		Min		3.585	○	3.630	○	3.765	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	5.036	○	4.605	○	3.930	○	
		Min	≤11.50	3.253	○	3.094	○	2.749	○
	Top of Main Girder	Max	5.866	○	5.947	○	5.898	○	
		Min	-2	4.396	○	4.703	○	4.927	○
	Bottom of Main Girder	Max	~16.10	-1.063	○	-0.596	○	0.088	○
		Min		3.091	○	2.946	○	2.881	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	5.036	○	4.605	○	3.930	○	
		Min	≤11.50	3.253	○	3.094	○	2.749	○
	Top of Main Girder	Max	5.866	○	5.947	○	5.898	○	
		Min	-2	4.396	○	4.703	○	4.927	○
	Bottom of Main Girder	Max	~16.10	-1.063	○	-0.596	○	0.088	○
		Min		3.091	○	2.946	○	2.881	○

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[1-13]		[1-14]		[1-15]	
Interval from beginning of Girder		-----	25.927		28.477		29.427	
Immediately After Prestressing	Top of Main Girder	-1.5	5.758	○	3.827	○	3.065	
	Bottom of Main Girder	~19.00	8.471	○	4.286	○	4.504	
During Deck Construction	Top of Main Girder	-1.5	7.659	○	4.187	○	2.884	
	Bottom of Main Girder	~14.00	5.142	○	3.410	○	4.298	
Dead Load	Top of Deck	≤10.00	2.585	○	1.795	○	1.390	
	Top of Main Girder	0	6.112	○	3.988	○	3.093	
	Bottom of Main Girder	~14.00	1.830	○	1.426	○	2.352	
Design Load1	Top of Deck	Max	2.937	○	1.877	○	1.397	
		Min	1.754	○	0.471	○	-0.181	
	Top of Main Girder	Max	6.402	○	4.059	○	3.099	
		Min	-1.5	5.429	○	2.844	○	1.725
	Bottom of Main Girder	Max	~14.00	0.995	○	1.275	○	2.340
		Min		3.795	○	3.867	○	5.141
Design Load2 Temperature Rise	Top of Deck	Max	3.907	○	2.963	○	2.509	
		Min	≤11.50	2.724	○	1.557	○	0.930
	Top of Main Girder	Max	5.892	○	3.691	○	2.758	
		Min	-2	4.919	○	2.475	○	1.385
	Bottom of Main Girder	Max	~16.10	0.105	○	0.677	○	1.761
		Min		2.905	○	3.270	○	4.563
Design Load3 Temperature Drop	Top of Deck	Max	3.907	○	2.963	○	2.509	
		Min	≤11.50	2.724	○	1.557	○	0.930
	Top of Main Girder	Max	5.892	○	3.691	○	2.758	
		Min	-2	4.919	○	2.475	○	1.385
	Bottom of Main Girder	Max	~16.10	0.105	○	0.677	○	1.761
		Min		2.905	○	3.270	○	4.563
Design Load4 Support sinking	Top of Deck	Max	2.937	○	1.877	○	1.397	
		Min	≤10.00	1.754	○	0.471	○	-0.181
	Top of Main Girder	Max	6.402	○	4.059	○	3.099	
		Min	-1.5	5.429	○	2.844	○	1.725
	Bottom of Main Girder	Max	~14.00	0.995	○	1.275	○	2.340
		Min		3.795	○	3.867	○	5.141
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	3.907	○	2.963	○	2.509	
		Min	≤11.50	2.724	○	1.557	○	0.930
	Top of Main Girder	Max	5.892	○	3.691	○	2.758	
		Min	-2	4.919	○	2.475	○	1.385
	Bottom of Main Girder	Max	~16.10	0.105	○	0.677	○	1.761
		Min		2.905	○	3.270	○	4.563
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	3.907	○	2.963	○	2.509	
		Min	≤11.50	2.724	○	1.557	○	0.930
	Top of Main Girder	Max	5.892	○	3.691	○	2.758	
		Min	-2	4.919	○	2.475	○	1.385
	Bottom of Main Girder	Max	~16.10	0.105	○	0.677	○	1.761
		Min		2.905	○	3.270	○	4.563

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2

Cross Section NumberNo.	Unit	Allowable Value	[1- 1]		[1- 2]		[1- 3]	
Interval from beginning of Girder								
				0.500		1.450		4.000
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1163	○	1166	○	1173	○
Effective Prestressing Force (*1)	N/mm ²	1110	1103	○	1104	○	1090	○
Effective Prestressing Force (*2)	N/mm ²	1110	1031	○	1029	○	992	○
max	N/mm ²	1110	1031	○	1031	○	1009	○
Ultimate Load	-----	1.00	999.9	○	5.66	○	2.01	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1- 4]		[1- 5]		[1- 6]	
Interval from beginning of Girder								
				4.116		7.732		11.348
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1174	○	1193	○	1196	○
Effective Prestressing Force (*1)	N/mm ²	1110	1090	○	1097	○	1092	○
Effective Prestressing Force (*2)	N/mm ²	1110	992	○	1005	○	1003	○
max	N/mm ²	1110	1009	○	1044	○	1058	○
Ultimate Load	-----	1.00	1.96	○	1.36	○	1.21	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1- 7]		[1- 8]		[1- 9]	
Interval from beginning of Girder								
				14.078		14.964		16.198
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1176	○	1172	○	1166	○
Effective Prestressing Force (*1)	N/mm ²	1110	1071	○	1068	○	1062	○
Effective Prestressing Force (*2)	N/mm ²	1110	988	○	985	○	978	○
max	N/mm ²	1110	1048	○	1045	○	1036	○
Ultimate Load	-----	1.00	1.16	○	1.16	○	1.18	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1-10]			[1-11]		[1-12]	
Interval from beginning of Girder					18.579			22.195	
Stress of PC Strand									
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○	
Immediately After Prestressing	N/mm ²	1295	1162	○	1171	○	1158	○	
Effective Prestressing Force (*1)	N/mm ²	1110	1061	○	1082	○	1082	○	
Effective Prestressing Force (*2)	N/mm ²	1110	972	○	987	○	982	○	
max	N/mm ²	1110	1021	○	1013	○	986	○	
Ultimate Load	-----	1.00	1.25	○	1.42	○	2.00	○	

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1-13]			[1-14]		[1-15]	
Interval from beginning of Girder					25.927			28.477	
Stress of PC Strand									
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○	
Immediately After Prestressing	N/mm ²	1295	1157	○	1103	○	1099	○	
Effective Prestressing Force (*1)	N/mm ²	1110	1081	○	1045	○	1043	○	
Effective Prestressing Force (*2)	N/mm ²	1110	981	○	969	○	969	○	
max	N/mm ²	1110	984	○	967	○	966	○	
Ultimate Load	-----	1.00	2.03	○	4.15	○	2.41	○	

*1:During DeckConstruction *2:Design Load

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[1- 1]	[1- 2]	[1- 3]	
Interval from beginning of Girder			-----	0.500	1.450	4.000	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.55 ○ 1.29 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.03 ○ -0.11 ○	
	Neutral Axis before Composition			-----	--	-0.04 ○ -0.10 ○	
	Neutral Axis after Composition			-----	--	-0.04 ○ -0.12 ○	
	Base of Lower Flange			-----	--	0.00 ○ -0.06 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.14 ○ -0.46 ○	
				Min	-----	--	-0.03 ○ -0.09 ○
	Neutral Axis before Composition			Max	-----	--	-0.14 ○ -0.47 ○
				Min	-----	--	-0.03 ○ -0.09 ○
	Neutral Axis after Composition			Max	-----	--	-0.16 ○ -0.49 ○
				Min	-----	--	-0.04 ○ -0.10 ○
	Base of Lower Flange			Max	-----	--	-0.02 ○ -0.33 ○
				Min	-----	--	0.00 ○ -0.05 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 -- 24.04 --	
	D16	cm	-----	-----	--	31.62 -- 37.68 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 -- 9.22 --	
Compressive Strength to Failure (Suc/Shu)			1.00	-----	--	3.92 ○ 1.83 ○	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	--	----- -- 1.00 ○	
	D16			-----	--	----- -- 1.00 ○	
	D19			-----	--	----- -- 1.15 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.55 ○ 1.29 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.03 ○ -0.11 ○	
	Neutral Axis before Composition			-----	--	-0.04 ○ -0.10 ○	
	Neutral Axis after Composition			-----	--	-0.04 ○ -0.12 ○	
	Base of Lower Flange			-----	--	0.00 ○ -0.06 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.14 ○ -0.46 ○	
				Min	-----	--	-0.03 ○ -0.09 ○
	Neutral Axis before Composition			Max	-----	--	-0.14 ○ -0.47 ○
				Min	-----	--	-0.03 ○ -0.09 ○
	Neutral Axis after Composition			Max	-----	--	-0.16 ○ -0.49 ○
				Min	-----	--	-0.04 ○ -0.10 ○
	Base of Lower Flange			Max	-----	--	-0.02 ○ -0.33 ○
				Min	-----	--	0.00 ○ -0.05 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 -- 24.04 --	
	D16	cm	-----	-----	--	31.62 -- 37.68 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 -- 0.00 --	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[1- 4]	[1- 5]	[1- 6]				
Interval from beginning of Girder			-----	4.116	7.732	11.348				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.26	Δ	0.90	Δ	0.73	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.11	○	-0.05	○	-0.04	○	
	Neutral Axis before Composition			-0.10	○	-0.04	○	-0.04	○	
	Neutral Axis after Composition			-0.11	○	-0.05	○	-0.04	○	
	Base of Lower Flange			-0.06	○	-0.03	○	-0.03	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.45	○	-0.22	○	-0.14	○
				Min	-0.09	○	-0.01	○	0.00	○
	Neutral Axis before Composition			Max	-0.46	○	-0.27	○	-0.20	○
				Min	-0.08	○	-0.01	○	0.00	○
	Neutral Axis after Composition			Max	-0.48	○	-0.25	○	-0.17	○
				Min	-0.09	○	-0.02	○	0.00	○
	Base of Lower Flange			Max	-0.33	○	-0.26	○	-0.25	○
				Min	-0.05	○	-0.01	○	0.00	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	24.48	--	40.00	--	40.00	--	
	D16	cm	-----	38.37	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	9.06	--	5.26	--	2.33	--	
Compressive Strength to Failure (Suc/Shu)		-----	1.00	1.85	○	2.46	○	3.52	○	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.00	○	1.018	○	1.32	○	
	D16			1.00	○	1.222	○	1.63	○	
	D19			1.16	○	1.471	○	2.00	○	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.26	Δ	0.90	Δ	0.73	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.11	○	-0.05	○	-0.04	○	
	Neutral Axis before Composition			-0.10	○	-0.04	○	-0.04	○	
	Neutral Axis after Composition			-0.11	○	-0.05	○	-0.04	○	
	Base of Lower Flange			-0.06	○	-0.03	○	-0.03	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.45	○	-0.22	○	-0.14	○
				Min	-0.09	○	-0.01	○	0.00	○
	Neutral Axis before Composition			Max	-0.46	○	-0.27	○	-0.20	○
				Min	-0.08	○	-0.01	○	0.00	○
	Neutral Axis after Composition			Max	-0.48	○	-0.25	○	-0.17	○
				Min	-0.09	○	-0.02	○	0.00	○
	Base of Lower Flange			Max	-0.33	○	-0.26	○	-0.25	○
				Min	-0.05	○	-0.01	○	0.00	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	24.48	--	40.00	--	40.00	--	
	D16	cm	-----	38.37	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[1- 7]	[1- 8]	[1- 9]	
Interval from beginning of Girder			-----	14.078	14.964	16.198	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.66 Δ	0.54 ○	0.58 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.03 ○	-0.02 ○	-0.01 ○	
	Neutral Axis before Composition			-0.04 ○	-0.02 ○	-0.01 ○	
	Neutral Axis after Composition			-0.04 ○	-0.02 ○	-0.01 ○	
	Base of Lower Flange			-0.03 ○	-0.02 ○	-0.01 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.12 ○	-0.08 ○	-0.02 ○
				Min	-0.01 ○	-0.03 ○	-0.10 ○
	Neutral Axis before Composition			Max	-0.16 ○	-0.12 ○	-0.02 ○
				Min	0.00 ○	-0.02 ○	-0.11 ○
	Neutral Axis after Composition			Max	-0.14 ○	-0.09 ○	-0.03 ○
				Min	-0.01 ○	-0.03 ○	-0.11 ○
	Base of Lower Flange			Max	-0.19 ○	-0.23 ○	-0.03 ○
				Min	0.00 ○	-0.02 ○	-0.08 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.34 --	0.61 --	1.98 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	5.13 ○	4.44 ○	3.76 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.784 ○	----- --	1.40 ○	
	D16			2.259 ○	----- --	1.74 ○	
	D19			2.839 ○	----- --	2.17 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.66 Δ	0.54 ○	0.58 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.03 ○	-0.02 ○	-0.01 ○	
	Neutral Axis before Composition			-0.04 ○	-0.02 ○	-0.01 ○	
	Neutral Axis after Composition			-0.04 ○	-0.02 ○	-0.01 ○	
	Base of Lower Flange			-0.03 ○	-0.02 ○	-0.01 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.12 ○	-0.08 ○	-0.02 ○
				Min	-0.01 ○	-0.03 ○	-0.10 ○
	Neutral Axis before Composition			Max	-0.16 ○	-0.12 ○	-0.02 ○
				Min	0.00 ○	-0.02 ○	-0.11 ○
	Neutral Axis after Composition			Max	-0.14 ○	-0.09 ○	-0.03 ○
				Min	-0.01 ○	-0.03 ○	-0.11 ○
	Base of Lower Flange			Max	-0.19 ○	-0.23 ○	-0.03 ○
				Min	0.00 ○	-0.02 ○	-0.08 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[1-10]	[1-11]	[1-12]
Interval from beginning of Girder			-----	18.579	22.195	25.811
Shear Force						
Shear Stress	Design Load	N/mm ²	0.55	0.53 ○	0.62 △	0.86 △
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00 ○	0.00 ○	0.00 ○
	Neutral Axis before Composition			0.00 ○	0.00 ○	0.00 ○
	Neutral Axis after Composition			0.00 ○	0.00 ○	0.00 ○
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○
Diagonal Tensile Stress	Base of Upper Flange	Max	-2.00	-0.02 ○	-0.01 ○	0.00 ○
		Min		-0.09 ○	-0.12 ○	-0.22 ○
	Neutral Axis before Composition	Max		-0.03 ○	-0.01 ○	0.00 ○
		Min		-0.08 ○	-0.11 ○	-0.21 ○
	Neutral Axis after Composition	Max		-0.02 ○	-0.01 ○	0.00 ○
		Min		-0.09 ○	-0.12 ○	-0.23 ○
	Base of Lower Flange	Max		-0.03 ○	-0.02 ○	0.00 ○
		Min		-0.06 ○	-0.08 ○	-0.14 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	39.85 --	24.16 --
	D16	cm	-----	40.00 --	40.00 --	37.86 --
	D19	cm	-----	40.00 --	40.00 --	40.00 --
Axial Reinforcement Bar Volume	cm ²	-----	2.90 --	5.56 --	9.18 --	
Compressive Strength to Failure (Suc/Shu)	-----	1.00	2.95 ○	2.21 ○	1.77 ○	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	1 ○	1.00 ○
	D16			-----	1.177 ○	1.00 ○
	D19			-----	1.394 ○	1.14 ○
Shear Force + Torsion						
Shear Stress	Design Load	N/mm ²	0.55	0.53 ○	0.62 △	0.86 △
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00 ○	0.00 ○	0.00 ○
	Neutral Axis before Composition			0.00 ○	0.00 ○	0.00 ○
	Neutral Axis after Composition			0.00 ○	0.00 ○	0.00 ○
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○
Diagonal Tensile Stress	Base of Upper Flange	Max	-2.50	-0.02 ○	-0.01 ○	0.00 ○
		Min		-0.09 ○	-0.12 ○	-0.22 ○
	Neutral Axis before Composition	Max		-0.03 ○	-0.01 ○	0.00 ○
		Min		-0.08 ○	-0.11 ○	-0.21 ○
	Neutral Axis after Composition	Max		-0.02 ○	-0.01 ○	0.00 ○
		Min		-0.09 ○	-0.12 ○	-0.23 ○
	Base of Lower Flange	Max		-0.03 ○	-0.02 ○	0.00 ○
		Min		-0.06 ○	-0.08 ○	-0.14 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	39.85 --	24.16 --
	D16	cm	-----	40.00 --	40.00 --	37.86 --
	D19	cm	-----	40.00 --	40.00 --	40.00 --
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[1-13]	[1-14]	[1-15]				
Interval from beginning of Girder			-----	25.927	28.477	29.427				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.85	Δ	0.97	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	-0.08	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.22	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.17	○	-----	--	
	Base of Lower Flange			0.00	○	-0.07	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	-0.07	○	-----	--
				Min	-0.21	○	-0.26	○	-----	--
	Neutral Axis before Composition			Max	0.00	○	-0.20	○	-----	--
				Min	-0.21	○	-0.39	○	-----	--
	Neutral Axis after Composition			Max	0.00	○	-0.16	○	-----	--
				Min	-0.22	○	-0.39	○	-----	--
	Base of Lower Flange			Max	0.00	○	-0.07	○	-----	--
				Min	-0.14	○	-0.07	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	24.03	--	20.18	--	-----	--	
	D16	cm	-----	37.67	--	31.63	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	9.22	--	9.43	--	-----	--	
Compressive Strength to Failure (Suc/Shu)			-----	1.00	1.76	○	3.19	○	-----	--
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1	○	1.023	○	-----	--	
	D16			1	○	1.023	○	-----	--	
	D19			1.141	○	1.073	○	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.85	Δ	0.97	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	-0.08	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.22	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.17	○	-----	--	
	Base of Lower Flange			0.00	○	-0.07	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	-0.07	○	-----	--
				Min	-0.21	○	-0.26	○	-----	--
	Neutral Axis before Composition			Max	0.00	○	-0.20	○	-----	--
				Min	-0.21	○	-0.39	○	-----	--
	Neutral Axis after Composition			Max	0.00	○	-0.16	○	-----	--
				Min	-0.22	○	-0.39	○	-----	--
	Base of Lower Flange			Max	0.00	○	-0.07	○	-----	--
				Min	-0.14	○	-0.07	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	24.03	--	20.18	--	-----	--	
	D16	cm	-----	37.67	--	31.63	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1- 1]	[1- 2]	[1- 3]	
Interval from beginning of Girder			-----	0.500	1.450	4.000	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.47 ○ 1.16 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.03 ○ -0.11 ○	
	Neutral Axis before Composition			-----	--	-0.04 ○ -0.10 ○	
	Neutral Axis after Composition			-----	--	-0.04 ○ -0.11 ○	
	Base of Lower Flange			-----	--	0.00 ○ -0.06 ○	
Diagonal Tensile Stress Design Load	Base of Upper Flange	N/mm ²	-2.00	Max	-----	--	-0.11 ○ -0.39 ○
				Min	-----	--	-0.04 ○ -0.12 ○
	Neutral Axis before Composition	Max		-----	--	-0.11 ○ -0.40 ○	
		Min		-----	--	-0.04 ○ -0.11 ○	
	Neutral Axis after Composition	Max		-----	--	-0.12 ○ -0.42 ○	
		Min		-----	--	-0.05 ○ -0.12 ○	
	Base of Lower Flange	Max		-----	--	-0.01 ○ -0.27 ○	
		Min		-----	--	-0.01 ○ -0.06 ○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 -- 27.84 --	
	D16	cm	-----	-----	--	31.62 -- 40.00 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 -- 7.96 --	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.47 ○ 1.16 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.03 ○ -0.11 ○	
	Neutral Axis before Composition			-----	--	-0.04 ○ -0.10 ○	
	Neutral Axis after Composition			-----	--	-0.04 ○ -0.11 ○	
	Base of Lower Flange			-----	--	0.00 ○ -0.06 ○	
Diagonal Tensile Stress Design Load	Base of Upper Flange	N/mm ²	-2.50	Max	-----	--	-0.11 ○ -0.39 ○
				Min	-----	--	-0.04 ○ -0.12 ○
	Neutral Axis before Composition	Max		-----	--	-0.11 ○ -0.40 ○	
		Min		-----	--	-0.04 ○ -0.11 ○	
	Neutral Axis after Composition	Max		-----	--	-0.12 ○ -0.42 ○	
		Min		-----	--	-0.05 ○ -0.12 ○	
	Base of Lower Flange	Max		-----	--	-0.01 ○ -0.27 ○	
		Min		-----	--	-0.01 ○ -0.06 ○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 -- 27.84 --	
	D16	cm	-----	-----	--	31.62 -- 40.00 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 -- 0.00 --	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	-----	--	999.999 ○ 999.999 ○	
Strength against Diagonal Densile Failure(Mus/Mtu)	D13	-----	1.00	-----	--	999.999 ○	
	D16	-----		-----	--	999.999 ○	
	D19	-----		-----	--	999.999 ○	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1- 4]	[1- 5]	[1- 6]				
Interval from beginning of Girder			-----	4.147	7.794	11.441				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.14	Δ	0.89	Δ	0.55	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.10	○	-0.03	○	-0.02	○	
	Neutral Axis before Composition			-0.09	○	-0.03	○	-0.02	○	
	Neutral Axis after Composition			-0.10	○	-0.03	○	-0.02	○	
	Base of Lower Flange			-0.05	○	-0.02	○	-0.01	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.38	○	-0.22	○	-0.08	○
				Min	-0.11	○	-0.03	○	-0.02	○
	Neutral Axis before Composition			Max	-0.38	○	-0.27	○	-0.12	○
				Min	-0.10	○	-0.03	○	-0.02	○
	Neutral Axis after Composition			Max	-0.40	○	-0.25	○	-0.10	○
				Min	-0.11	○	-0.03	○	-0.02	○
	Base of Lower Flange			Max	-0.26	○	-0.29	○	-0.25	○
				Min	-0.06	○	-0.02	○	-0.01	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	29.05	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	7.63	--	5.14	--	0.00	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.14	Δ	0.89	Δ	0.55	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.10	○	-0.03	○	-0.02	○	
	Neutral Axis before Composition			-0.09	○	-0.03	○	-0.02	○	
	Neutral Axis after Composition			-0.10	○	-0.03	○	-0.02	○	
	Base of Lower Flange			-0.05	○	-0.02	○	-0.01	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.38	○	-0.22	○	-0.08	○
				Min	-0.11	○	-0.03	○	-0.02	○
	Neutral Axis before Composition			Max	-0.38	○	-0.27	○	-0.12	○
				Min	-0.10	○	-0.03	○	-0.02	○
	Neutral Axis after Composition			Max	-0.40	○	-0.25	○	-0.10	○
				Min	-0.11	○	-0.03	○	-0.02	○
	Base of Lower Flange			Max	-0.26	○	-0.29	○	-0.25	○
				Min	-0.06	○	-0.02	○	-0.01	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	29.05	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	-	
	D16			999.999	○	999.999	○	-----	-	
	D19			999.999	○	999.999	○	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1- 7]	[1- 8]	[1- 9]				
Interval from beginning of Girder			-----	14.078	15.088	16.446				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.20	o	0.04	o	0.36	o	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.01	o	0.00	o	0.00	o	
	Neutral Axis before Composition			-0.01	o	0.00	o	0.00	o	
	Neutral Axis after Composition			-0.01	o	0.00	o	0.00	o	
	Base of Lower Flange			-0.01	o	0.00	o	0.00	o	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.01	o	0.00	o	0.00	o
				Min	-0.01	o	0.00	o	-0.03	o
	Neutral Axis before Composition	Max		-0.01	o	0.00	o	0.00	o	
		Min		-0.01	o	0.00	o	-0.06	o	
	Neutral Axis after Composition	Max		-0.01	o	0.00	o	0.00	o	
		Min		-0.01	o	0.00	o	-0.04	o	
	Base of Lower Flange	Max		-0.01	o	-0.01	o	0.00	o	
		Min		-0.02	o	0.00	o	-0.31	o	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.20	o	0.04	o	0.36	o	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.01	o	0.00	o	0.00	o	
	Neutral Axis before Composition			-0.01	o	0.00	o	0.00	o	
	Neutral Axis after Composition			-0.01	o	0.00	o	0.00	o	
	Base of Lower Flange			-0.01	o	0.00	o	0.00	o	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.01	o	0.00	o	0.00	o
				Min	-0.01	o	0.00	o	-0.03	o
	Neutral Axis before Composition	Max		-0.01	o	0.00	o	0.00	o	
		Min		-0.01	o	0.00	o	-0.06	o	
	Neutral Axis after Composition	Max		-0.01	o	0.00	o	0.00	o	
		Min		-0.01	o	0.00	o	-0.04	o	
	Base of Lower Flange	Max		-0.01	o	-0.01	o	0.00	o	
		Min		-0.02	o	0.00	o	-0.31	o	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	o	999.999	o	999.999	o	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	-----	-	-----	-	
	D16	-----		-----	-	-----	-	-----	-	
	D19	-----		-----	-	-----	-	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1-10]	[1-11]	[1-12]				
Interval from beginning of Girder			-----	18.735	22.381	26.028				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.53	○	0.66	△	0.89	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	-0.01	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	0.00	○	0.00	○
				Min	-0.08	○	-0.13	○	-0.23	○
	Neutral Axis before Composition			Max	0.00	○	0.00	○	0.00	○
				Min	-0.11	○	-0.15	○	-0.25	○
	Neutral Axis after Composition			Max	0.00	○	0.00	○	0.00	○
				Min	-0.09	○	-0.14	○	-0.25	○
	Base of Lower Flange			Max	0.00	○	0.00	○	0.00	○
				Min	-0.24	○	-0.17	○	-0.20	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	36.21	--	24.27	--	
	D16	cm	-----	40.00	--	40.00	--	38.05	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	2.97	--	6.12	--	9.13	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.53	○	0.66	△	0.89	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	-0.01	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	0.00	○	0.00	○
				Min	-0.08	○	-0.13	○	-0.23	○
	Neutral Axis before Composition			Max	0.00	○	0.00	○	0.00	○
				Min	-0.11	○	-0.15	○	-0.25	○
	Neutral Axis after Composition			Max	0.00	○	0.00	○	0.00	○
				Min	-0.09	○	-0.14	○	-0.25	○
	Base of Lower Flange			Max	0.00	○	0.00	○	0.00	○
				Min	-0.24	○	-0.17	○	-0.20	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	36.21	--	24.27	--	
	D16	cm	-----	40.00	--	40.00	--	38.05	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	999.999	○	999.999	○	
	D16			-----	-	999.999	○	999.999	○	
	D19			-----	-	999.999	○	999.999	○	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1-13]	[1-14]	[1-15]				
Interval from beginning of Girder			-----	26.176	28.725	29.675				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.89	Δ	0.98	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	-0.09	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.22	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.19	○	-----	--	
	Base of Lower Flange			0.00	○	-0.06	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	-0.10	○	-----	--
				Min	-0.23	○	-0.28	○	-----	--
	Neutral Axis before Composition			Max	0.00	○	-0.21	○	-----	--
				Min	-0.25	○	-0.40	○	-----	--
	Neutral Axis after Composition			Max	0.00	○	-0.19	○	-----	--
				Min	-0.25	○	-0.40	○	-----	--
	Base of Lower Flange			Max	0.00	○	-0.05	○	-----	--
				Min	-0.20	○	-0.07	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	23.99	--	20.18	--	-----	--	
	D16	cm	-----	37.60	--	31.63	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	9.24	--	9.52	--	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.89	Δ	0.98	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	-0.09	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.22	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.19	○	-----	--	
	Base of Lower Flange			0.00	○	-0.06	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	-0.10	○	-----	--
				Min	-0.23	○	-0.28	○	-----	--
	Neutral Axis before Composition			Max	0.00	○	-0.21	○	-----	--
				Min	-0.25	○	-0.40	○	-----	--
	Neutral Axis after Composition			Max	0.00	○	-0.19	○	-----	--
				Min	-0.25	○	-0.40	○	-----	--
	Base of Lower Flange			Max	0.00	○	-0.05	○	-----	--
				Min	-0.20	○	-0.07	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	23.99	--	20.18	--	-----	--	
	D16	cm	-----	37.60	--	31.63	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	-----	--	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	--	
	D16			999.999	○	999.999	○	-----	--	
	D19			999.999	○	999.999	○	-----	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[2-1]		[2-2]		[2-3]		
Interval from beginning of Girder		-----	0.500		1.450		4.000		
Immediately After Prestressing	Top of Main Girder	-1.5	3.066	○	3.829	○	5.762	○	
	Bottom of Main Girder	~19.00	4.503	○	4.284	○	8.466	○	
During Deck Construction	Top of Main Girder	-1.5	2.885	○	4.190	○	7.667	○	
	Bottom of Main Girder	~14.00	4.297	○	3.407	○	5.132	○	
Dead Load	Top of Deck	≤10.00	1.387	○	1.795	○	2.593	○	
	Top of Main Girder	0	3.090	○	3.989	○	6.123	○	
	Bottom of Main Girder	~14.00	2.358	○	1.425	○	1.806	○	
Design Load1	Top of Deck	Max	1.393	○	1.876	○	2.946	○	
		Min	≤10.00	-0.185	○	0.471	○	1.764	○
	Top of Main Girder	Max	-1.5	3.096	○	4.060	○	6.412	○
		Min	~14.00	1.722	○	2.844	○	5.441	○
	Bottom of Main Girder	Max	~14.00	2.346	○	1.274	○	0.972	○
		Min	~14.00	5.148	○	3.867	○	3.770	○
Design Load2 Temperature Rise	Top of Deck	Max	≤11.50	2.505	○	2.963	○	3.916	○
		Min	≤11.50	0.926	○	1.557	○	2.734	○
	Top of Main Girder	Max	-2	2.755	○	3.692	○	5.902	○
		Min	~16.10	1.381	○	2.476	○	4.931	○
	Bottom of Main Girder	Max	~16.10	1.767	○	0.676	○	0.082	○
		Min	~16.10	4.570	○	3.269	○	2.879	○
Design Load3 Temperature Drop	Top of Deck	Max	≤11.50	2.505	○	2.963	○	3.916	○
		Min	≤11.50	0.926	○	1.557	○	2.734	○
	Top of Main Girder	Max	-2	2.755	○	3.692	○	5.902	○
		Min	~16.10	1.381	○	2.476	○	4.931	○
	Bottom of Main Girder	Max	~16.10	1.767	○	0.676	○	0.082	○
		Min	~16.10	4.570	○	3.269	○	2.879	○
Design Load4 Support sinking	Top of Deck	Max	≤10.00	1.393	○	1.876	○	2.946	○
		Min	≤10.00	-0.185	○	0.471	○	1.764	○
	Top of Main Girder	Max	-1.5	3.096	○	4.060	○	6.412	○
		Min	~14.00	1.722	○	2.844	○	5.441	○
	Bottom of Main Girder	Max	~14.00	2.346	○	1.274	○	0.972	○
		Min	~14.00	5.148	○	3.867	○	3.770	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	≤11.50	2.505	○	2.963	○	3.916	○
		Min	≤11.50	0.926	○	1.557	○	2.734	○
	Top of Main Girder	Max	-2	2.755	○	3.692	○	5.902	○
		Min	~16.10	1.381	○	2.476	○	4.931	○
	Bottom of Main Girder	Max	~16.10	1.767	○	0.676	○	0.082	○
		Min	~16.10	4.570	○	3.269	○	2.879	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	≤11.50	2.505	○	2.963	○	3.916	○
		Min	≤11.50	0.926	○	1.557	○	2.734	○
	Top of Main Girder	Max	-2	2.755	○	3.692	○	5.902	○
		Min	~16.10	1.381	○	2.476	○	4.931	○
	Bottom of Main Girder	Max	~16.10	1.767	○	0.676	○	0.082	○
		Min	~16.10	4.570	○	3.269	○	2.879	○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[2- 4]		[2- 5]		[2- 6]		
Interval from beginning of Girder		-----	4.122		7.743		11.365		
Immediately After Prestressing	Top of Main Girder	-1.5	5.667	○	2.974	○	1.120	○	
	Bottom of Main Girder	~19.00	8.603	○	12.168	○	14.427	○	
During Deck Construction	Top of Main Girder	-1.5	7.647	○	6.854	○	6.232	○	
	Bottom of Main Girder	~14.00	5.174	○	6.320	○	6.974	○	
Dead Load	Top of Deck	≤10.00	2.605	○	2.834	○	2.961	○	
	Top of Main Girder	0	6.119	○	5.801	○	5.470	○	
	Bottom of Main Girder	~14.00	1.816	○	2.160	○	2.382	○	
Design Load1	Top of Deck	Max	2.972	○	3.740	○	4.260	○	
		Min	1.792	○	2.230	○	2.478	○	
	Top of Main Girder	Max	6.421	○	6.548	○	6.542	○	
		Min	-1.5	5.452	○	5.304	○	5.071	○
	Bottom of Main Girder	Max	~14.00	0.946	○	0.035	○	-0.646	○
		Min		3.737	○	3.576	○	3.508	○
Design Load2 Temperature Rise	Top of Deck	Max	3.940	○	4.627	○	5.068	○	
		Min	≤11.50	2.760	○	3.117	○	3.286	○
	Top of Main Girder	Max	5.909	○	5.970	○	5.900	○	
		Min	-2	4.939	○	4.726	○	4.429	○
	Bottom of Main Girder	Max	~16.10	0.063	○	-0.649	○	-1.140	○
		Min		2.853	○	2.892	○	3.014	○
Design Load3 Temperature Drop	Top of Deck	Max	3.940	○	4.627	○	5.068	○	
		Min	≤11.50	2.760	○	3.117	○	3.286	○
	Top of Main Girder	Max	5.909	○	5.970	○	5.900	○	
		Min	-2	4.939	○	4.726	○	4.429	○
	Bottom of Main Girder	Max	~16.10	0.063	○	-0.649	○	-1.140	○
		Min		2.853	○	2.892	○	3.014	○
Design Load4 Support sinking	Top of Deck	Max	2.972	○	3.740	○	4.260	○	
		Min	≤10.00	1.792	○	2.230	○	2.478	○
	Top of Main Girder	Max	6.421	○	6.548	○	6.542	○	
		Min	-1.5	5.452	○	5.304	○	5.071	○
	Bottom of Main Girder	Max	~14.00	0.946	○	0.035	○	-0.646	○
		Min		3.737	○	3.576	○	3.508	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	3.940	○	4.627	○	5.068	○	
		Min	≤11.50	2.760	○	3.117	○	3.286	○
	Top of Main Girder	Max	5.909	○	5.970	○	5.900	○	
		Min	-2	4.939	○	4.726	○	4.429	○
	Bottom of Main Girder	Max	~16.10	0.063	○	-0.649	○	-1.140	○
		Min		2.853	○	2.892	○	3.014	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	3.940	○	4.627	○	5.068	○	
		Min	≤11.50	2.760	○	3.117	○	3.286	○
	Top of Main Girder	Max	5.909	○	5.970	○	5.900	○	
		Min	-2	4.939	○	4.726	○	4.429	○
	Bottom of Main Girder	Max	~16.10	0.063	○	-0.649	○	-1.140	○
		Min		2.853	○	2.892	○	3.014	○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[2- 7]		[2- 8]		[2- 9]		
Interval from beginning of Girder		-----	13.730		14.987		15.995		
Immediately After Prestressing	Top of Main Girder	-1.5	0.792	○	0.815	○	0.778	○	
	Bottom of Main Girder	~19.00	14.915	○	14.968	○	15.072	○	
During Deck Construction	Top of Main Girder	-1.5	6.308	○	6.391	○	6.326	○	
	Bottom of Main Girder	~14.00	6.945	○	6.922	○	7.050	○	
Dead Load	Top of Deck	≤10.00	3.071	○	3.075	○	3.006	○	
	Top of Main Girder	0	5.525	○	5.553	○	5.474	○	
	Bottom of Main Girder	~14.00	2.301	○	2.356	○	2.583	○	
Design Load1	Top of Deck	Max	4.521	○	4.577	○	4.536	○	
		Min	2.651	○	2.687	○	2.643	○	
	Top of Main Girder	Max	6.722	○	6.793	○	6.736	○	
		Min	-1.5	5.178	○	5.234	○	5.175	○
	Bottom of Main Girder	Max	~14.00	-1.075	○	-1.141	○	-0.978	○
		Min		3.278	○	3.257	○	3.427	○
Design Load2 Temperature Rise	Top of Deck	Max	5.279	○	5.309	○	5.249	○	
		Min	≤11.50	3.409	○	3.419	○	3.356	○
	Top of Main Girder	Max	6.038	○	6.088	○	6.016	○	
		Min	-2	4.495	○	4.529	○	4.454	○
	Bottom of Main Girder	Max	~16.10	-1.451	○	-1.456	○	-1.249	○
		Min		2.902	○	2.943	○	3.157	○
Design Load3 Temperature Drop	Top of Deck	Max	5.279	○	5.309	○	5.249	○	
		Min	≤11.50	3.409	○	3.419	○	3.356	○
	Top of Main Girder	Max	6.038	○	6.088	○	6.016	○	
		Min	-2	4.495	○	4.529	○	4.454	○
	Bottom of Main Girder	Max	~16.10	-1.451	○	-1.456	○	-1.249	○
		Min		2.902	○	2.943	○	3.157	○
Design Load4 Support sinking	Top of Deck	Max	4.521	○	4.577	○	4.536	○	
		Min	≤10.00	2.651	○	2.687	○	2.643	○
	Top of Main Girder	Max	6.722	○	6.793	○	6.736	○	
		Min	-1.5	5.178	○	5.234	○	5.175	○
	Bottom of Main Girder	Max	~14.00	-1.075	○	-1.141	○	-0.978	○
		Min		3.278	○	3.257	○	3.427	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	5.279	○	5.309	○	5.249	○	
		Min	≤11.50	3.409	○	3.419	○	3.356	○
	Top of Main Girder	Max	6.038	○	6.088	○	6.016	○	
		Min	-2	4.495	○	4.529	○	4.454	○
	Bottom of Main Girder	Max	~16.10	-1.451	○	-1.456	○	-1.249	○
		Min		2.902	○	2.943	○	3.157	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	5.279	○	5.309	○	5.249	○	
		Min	≤11.50	3.409	○	3.419	○	3.356	○
	Top of Main Girder	Max	6.038	○	6.088	○	6.016	○	
		Min	-2	4.495	○	4.529	○	4.454	○
	Bottom of Main Girder	Max	~16.10	-1.451	○	-1.456	○	-1.249	○
		Min		2.902	○	2.943	○	3.157	○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[2-10]		[2-11]		[2-12]	
Interval from beginning of Girder		-----	18.608		22.230		25.851	
Immediately After Prestressing	Top of Main Girder	-1.5	1.002	○	2.200	○	3.726	
	Bottom of Main Girder	~19.00	15.046	○	13.447	○	11.237	
During Deck Construction	Top of Main Girder	-1.5	6.132	○	6.151	○	5.844	
	Bottom of Main Girder	~14.00	7.522	○	7.437	○	7.555	
Dead Load	Top of Deck	≤10.00	2.655	○	2.142	○	1.426	
	Top of Main Girder	0	5.176	○	4.911	○	4.357	
	Bottom of Main Girder	~14.00	3.564	○	4.461	○	5.787	
Design Load1	Top of Deck	Max	4.207	○	3.541	○	2.339	
		Min	2.365	○	1.947	○	1.328	
	Top of Main Girder	Max	6.456	○	6.064	○	5.108	
		Min	-1.5	4.937	○	4.751	○	4.276
	Bottom of Main Girder	Max	~14.00	-0.051	○	1.186	○	3.637
		Min		4.240	○	4.916	○	6.018
Design Load2 Temperature Rise	Top of Deck	Max	4.863	○	4.122	○	2.845	
		Min	≤11.50	3.022	○	2.529	○	1.834
	Top of Main Girder	Max	5.689	○	5.235	○	4.216	
		Min	-2	4.170	○	3.922	○	3.384
	Bottom of Main Girder	Max	~16.10	-0.191	○	1.219	○	3.847
		Min		4.100	○	4.950	○	6.228
Design Load3 Temperature Drop	Top of Deck	Max	4.863	○	4.122	○	2.845	
		Min	≤11.50	3.022	○	2.529	○	1.834
	Top of Main Girder	Max	5.689	○	5.235	○	4.216	
		Min	-2	4.170	○	3.922	○	3.384
	Bottom of Main Girder	Max	~16.10	-0.191	○	1.219	○	3.847
		Min		4.100	○	4.950	○	6.228
Design Load4 Support sinking	Top of Deck	Max	4.207	○	3.541	○	2.339	
		Min	≤10.00	2.365	○	1.947	○	1.328
	Top of Main Girder	Max	6.456	○	6.064	○	5.108	
		Min	-1.5	4.937	○	4.751	○	4.276
	Bottom of Main Girder	Max	~14.00	-0.051	○	1.186	○	3.637
		Min		4.240	○	4.916	○	6.018
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	4.863	○	4.122	○	2.845	
		Min	≤11.50	3.022	○	2.529	○	1.834
	Top of Main Girder	Max	5.689	○	5.235	○	4.216	
		Min	-2	4.170	○	3.922	○	3.384
	Bottom of Main Girder	Max	~16.10	-0.191	○	1.219	○	3.847
		Min		4.100	○	4.950	○	6.228
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	4.863	○	4.122	○	2.845	
		Min	≤11.50	3.022	○	2.529	○	1.834
	Top of Main Girder	Max	5.689	○	5.235	○	4.216	
		Min	-2	4.170	○	3.922	○	3.384
	Bottom of Main Girder	Max	~16.10	-0.191	○	1.219	○	3.847
		Min		4.100	○	4.950	○	6.228

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[2-13]		[2-14]		[2-15]		
Interval from beginning of Girder		-----	25.973		28.523		29.473		
Immediately After Prestressing	Top of Main Girder	-1.5	3.785	○	2.772	○	2.971	○	
	Bottom of Main Girder	~19.00	11.156	○	6.015	○	5.077	○	
During Deck Construction	Top of Main Girder	-1.5	5.831	○	3.209	○	2.819	○	
	Bottom of Main Girder	~14.00	7.566	○	5.016	○	4.817	○	
Dead Load	Top of Deck	≤10.00	1.399	○	0.551	○	0.275	○	
	Top of Main Girder	0	4.334	○	2.486	○	2.120	○	
	Bottom of Main Girder	~14.00	5.844	○	4.687	○	4.786	○	
Design Load1	Top of Deck	Max	2.288	○	0.825	○	0.275	○	
		Min	1.304	○	0.526	○	0.274	○	
	Top of Main Girder	Max	5.065	○	2.723	○	2.120	○	
		Min	-1.5	4.256	○	2.464	○	2.120	○
	Bottom of Main Girder	Max	~14.00	3.749	○	4.184	○	4.786	○
		Min		6.067	○	4.734	○	4.786	○
Design Load2 Temperature Rise	Top of Deck	Max	2.791	○	1.350	○	0.793	○	
		Min	≤11.50	1.807	○	1.051	○	0.793	○
	Top of Main Girder	Max	4.172	○	1.869	○	1.263	○	
		Min	-2	3.362	○	1.611	○	1.263	○
	Bottom of Main Girder	Max	~16.10	3.965	○	4.621	○	5.260	○
		Min		6.283	○	5.171	○	5.260	○
Design Load3 Temperature Drop	Top of Deck	Max	2.791	○	1.350	○	0.793	○	
		Min	≤11.50	1.807	○	1.051	○	0.793	○
	Top of Main Girder	Max	4.172	○	1.869	○	1.263	○	
		Min	-2	3.362	○	1.611	○	1.263	○
	Bottom of Main Girder	Max	~16.10	3.965	○	4.621	○	5.260	○
		Min		6.283	○	5.171	○	5.260	○
Design Load4 Support sinking	Top of Deck	Max	2.288	○	0.825	○	0.275	○	
		Min	≤10.00	1.304	○	0.526	○	0.274	○
	Top of Main Girder	Max	5.065	○	2.723	○	2.120	○	
		Min	-1.5	4.256	○	2.464	○	2.120	○
	Bottom of Main Girder	Max	~14.00	3.749	○	4.184	○	4.786	○
		Min		6.067	○	4.734	○	4.786	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	2.791	○	1.350	○	0.793	○	
		Min	≤11.50	1.807	○	1.051	○	0.793	○
	Top of Main Girder	Max	4.172	○	1.869	○	1.263	○	
		Min	-2	3.362	○	1.611	○	1.263	○
	Bottom of Main Girder	Max	~16.10	3.965	○	4.621	○	5.260	○
		Min		6.283	○	5.171	○	5.260	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	2.791	○	1.350	○	0.793	○	
		Min	≤11.50	1.807	○	1.051	○	0.793	○
	Top of Main Girder	Max	4.172	○	1.869	○	1.263	○	
		Min	-2	3.362	○	1.611	○	1.263	○
	Bottom of Main Girder	Max	~16.10	3.965	○	4.621	○	5.260	○
		Min		6.283	○	5.171	○	5.260	○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Cross Section NumberNo.	Unit	Allowable Value	[2- 1]		[2- 2]		[2- 3]	
Interval from beginning of Girder								
				0.500		1.450		4.000
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1099	○	1103	○	1157	○
Effective Prestressing Force (*1)	N/mm ²	1110	1043	○	1045	○	1081	○
Effective Prestressing Force (*2)	N/mm ²	1110	969	○	969	○	981	○
max	N/mm ²	1110	966	○	967	○	984	○
Ultimate Load	-----	1.00	2.41	○	4.15	○	2.03	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2- 4]		[2- 5]		[2- 6]	
Interval from beginning of Girder								
				4.122		7.743		11.365
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1158	○	1171	○	1162	○
Effective Prestressing Force (*1)	N/mm ²	1110	1082	○	1082	○	1061	○
Effective Prestressing Force (*2)	N/mm ²	1110	983	○	988	○	972	○
max	N/mm ²	1110	986	○	1014	○	1022	○
Ultimate Load	-----	1.00	1.99	○	1.42	○	1.24	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2- 7]		[2- 8]		[2- 9]	
Interval from beginning of Girder								
				13.730		14.987		15.895
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1166	○	1172	○	1176	○
Effective Prestressing Force (*1)	N/mm ²	1110	1062	○	1068	○	1071	○
Effective Prestressing Force (*2)	N/mm ²	1110	979	○	986	○	989	○
max	N/mm ²	1110	1037	○	1047	○	1050	○
Ultimate Load	-----	1.00	1.17	○	1.15	○	1.16	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2-10]	[2-11]	[2-12]
Interval from beginning of Girder			18.608	22.230	25.851
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	1320	1320
Immediately After Prestressing	N/mm ²	1295	1196	1193	1174
Effective Prestressing Force (*1)	N/mm ²	1110	1092	1097	1090
Effective Prestressing Force (*2)	N/mm ²	1110	1003	1005	993
max	N/mm ²	1110	1059	1045	1010
Ultimate Load	-----	1.00	1.21	1.36	1.95

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2-13]	[2-14]	[2-15]
Interval from beginning of Girder			25.973	28.523	29.473
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	1320	1320
Immediately After Prestressing	N/mm ²	1295	1173	1166	1163
Effective Prestressing Force (*1)	N/mm ²	1110	1090	1104	1103
Effective Prestressing Force (*2)	N/mm ²	1110	992	1029	1031
max	N/mm ²	1110	1009	1031	1031
Ultimate Load	-----	1.00	2.00	5.64	999.90

*1:During DeckConstruction *2:Design Load

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2- 1]	[2- 2]	[2- 3]		
Interval from beginning of Girder			-----	0.500	1.450	4.000		
Shear Force								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.88 Δ	0.84 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.08 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.22 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.18 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.07 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.22 ○	-0.20 ○	
				Min	-----	--	-0.08 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.44 ○	-0.24 ○
				Min	-----	--	-0.18 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.39 ○	-0.22 ○
				Min	-----	--	-0.16 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.14 ○	-0.24 ○
				Min	-----	--	-0.04 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 --	23.46 --	
	D16	cm	-----	-----	--	31.63 --	36.77 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	7.66 --	9.45 --	
Compressive Strength to Failure (Suc/Shu)			1.00	-----	--	3.49 ○	1.76 ○	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	--	1.12 ○	1.00 ○	
	D16			-----	--	1.12 ○	1.00 ○	
	D19			-----	--	1.176 ○	1.13 ○	
Shear Force + Torsion								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.88 Δ	0.84 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.08 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.22 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.18 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.07 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.22 ○	-0.20 ○	
				Min	-----	--	-0.08 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.44 ○	-0.24 ○
				Min	-----	--	-0.18 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.39 ○	-0.22 ○
				Min	-----	--	-0.16 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.14 ○	-0.24 ○
				Min	-----	--	-0.04 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 --	23.46 --	
	D16	cm	-----	-----	--	31.63 --	36.77 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 --	0.00 --	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2- 4]	[2- 5]	[2- 6]	
Interval from beginning of Girder			-----	4.092	7.684	11.275	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.84 Δ	0.60 Δ	0.48 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis after Composition			0.00 ○	0.00 ○	0.00 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.20 ○	-0.10 ○	-0.07 ○
				Min	0.00 ○	-0.01 ○	-0.03 ○
	Neutral Axis before Composition			Max	-0.24 ○	-0.13 ○	-0.09 ○
				Min	0.00 ○	-0.01 ○	-0.03 ○
	Neutral Axis after Composition			Max	-0.22 ○	-0.12 ○	-0.08 ○
				Min	0.00 ○	-0.01 ○	-0.03 ○
	Base of Lower Flange			Max	-0.24 ○	-0.16 ○	-0.14 ○
				Min	0.00 ○	-0.01 ○	-0.02 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	23.55 --	36.15 --	40.00 --	
	D16	cm	-----	36.91 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	9.41 --	6.13 --	3.40 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	1.77 ○	2.24 ○	3.06 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.00 ○	1 ○	----- --	
	D16			1.00 ○	1.147 ○	----- --	
	D19			1.14 ○	1.367 ○	----- --	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.84 Δ	0.60 Δ	0.48 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis after Composition			0.00 ○	0.00 ○	0.00 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.20 ○	-0.10 ○	-0.07 ○
				Min	0.00 ○	-0.01 ○	-0.03 ○
	Neutral Axis before Composition			Max	-0.24 ○	-0.13 ○	-0.09 ○
				Min	0.00 ○	-0.01 ○	-0.03 ○
	Neutral Axis after Composition			Max	-0.22 ○	-0.12 ○	-0.08 ○
				Min	0.00 ○	-0.01 ○	-0.03 ○
	Base of Lower Flange			Max	-0.24 ○	-0.16 ○	-0.14 ○
				Min	0.00 ○	-0.01 ○	-0.02 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	23.55 --	36.15 --	40.00 --	
	D16	cm	-----	36.91 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2- 7]	[2- 8]	[2- 9]				
Interval from beginning of Girder			-----	13.730	14.867	15.656				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.52	○	0.47	○	0.62	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.01	○	0.00	○	-0.03	○	
	Neutral Axis before Composition			-0.01	○	0.00	○	-0.03	○	
	Neutral Axis after Composition			-0.01	○	0.00	○	-0.03	○	
	Base of Lower Flange			-0.01	○	0.00	○	-0.03	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.07	○	-0.03	○	-0.01	○
				Min	-0.03	○	-0.07	○	-0.11	○
	Neutral Axis before Composition			Max	-0.11	○	-0.05	○	-0.01	○
				Min	-0.02	○	-0.07	○	-0.12	○
	Neutral Axis after Composition			Max	-0.09	○	-0.04	○	-0.01	○
				Min	-0.03	○	-0.07	○	-0.12	○
	Base of Lower Flange			Max	-0.20	○	-0.10	○	-0.01	○
				Min	-0.02	○	-0.05	○	-0.08	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	2.41	--	0.80	--	0.00	--		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	4.05	○	5.02	○	5.49	○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	--	-----	--	1.92	○	
	D16			-----	--	-----	--	2.43	○	
	D19			-----	--	-----	--	3.05	○	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.52	○	0.47	○	0.62	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.01	○	0.00	○	-0.03	○	
	Neutral Axis before Composition			-0.01	○	0.00	○	-0.03	○	
	Neutral Axis after Composition			-0.01	○	0.00	○	-0.03	○	
	Base of Lower Flange			-0.01	○	0.00	○	-0.03	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.07	○	-0.03	○	-0.01	○
				Min	-0.03	○	-0.07	○	-0.11	○
	Neutral Axis before Composition			Max	-0.11	○	-0.05	○	-0.01	○
				Min	-0.02	○	-0.07	○	-0.12	○
	Neutral Axis after Composition			Max	-0.09	○	-0.04	○	-0.01	○
				Min	-0.03	○	-0.07	○	-0.12	○
	Base of Lower Flange			Max	-0.20	○	-0.10	○	-0.01	○
				Min	-0.02	○	-0.05	○	-0.08	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	0.00	--	0.00	--	0.00	--		

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2-10]	[2-11]	[2-12]	
Interval from beginning of Girder			-----	18.459	22.050	25.642	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.70 Δ	0.89 Δ	1.26 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.03 ○	-0.05 ○	-0.11 ○	
	Neutral Axis before Composition			-0.03 ○	-0.05 ○	-0.10 ○	
	Neutral Axis after Composition			-0.03 ○	-0.05 ○	-0.11 ○	
	Base of Lower Flange			-0.02 ○	-0.03 ○	-0.06 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00 ○	-0.01 ○	-0.09 ○
				Min	-0.15 ○	-0.24 ○	-0.48 ○
	Neutral Axis before Composition			Max	0.00 ○	-0.02 ○	-0.09 ○
				Min	-0.14 ○	-0.22 ○	-0.41 ○
	Neutral Axis after Composition			Max	0.00 ○	-0.02 ○	-0.09 ○
				Min	-0.15 ○	-0.25 ○	-0.48 ○
	Base of Lower Flange			Max	0.00 ○	-0.02 ○	-0.06 ○
				Min	-0.09 ○	-0.13 ○	-0.24 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	25.21 --	
	D16	cm	-----	40.00 --	40.00 --	39.51 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.95 --	4.14 --	8.79 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	3.62 ○	2.49 ○	1.86 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.462 ○	1.092 ○	1.00 ○	
	D16			1.778 ○	1.298 ○	1.00 ○	
	D19			2.165 ○	1.55 ○	1.18 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.70 Δ	0.89 Δ	1.26 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.03 ○	-0.05 ○	-0.11 ○	
	Neutral Axis before Composition			-0.03 ○	-0.05 ○	-0.10 ○	
	Neutral Axis after Composition			-0.03 ○	-0.05 ○	-0.11 ○	
	Base of Lower Flange			-0.02 ○	-0.03 ○	-0.06 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00 ○	-0.01 ○	-0.09 ○
				Min	-0.15 ○	-0.24 ○	-0.48 ○
	Neutral Axis before Composition			Max	0.00 ○	-0.02 ○	-0.09 ○
				Min	-0.14 ○	-0.22 ○	-0.41 ○
	Neutral Axis after Composition			Max	0.00 ○	-0.02 ○	-0.09 ○
				Min	-0.15 ○	-0.25 ○	-0.48 ○
	Base of Lower Flange			Max	0.00 ○	-0.02 ○	-0.06 ○
				Min	-0.09 ○	-0.13 ○	-0.24 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	25.21 --	
	D16	cm	-----	40.00 --	40.00 --	39.51 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2-13]	[2-14]	[2-15]				
Interval from beginning of Girder			-----	25.734	28.284	29.234				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.28	Δ	0.55	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.12	○	-0.03	○	-----	--	
	Neutral Axis before Composition			-0.11	○	-0.04	○	-----	--	
	Neutral Axis after Composition			-0.12	○	-0.04	○	-----	--	
	Base of Lower Flange			-0.06	○	-0.01	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.09	○	-0.03	○	-----	--
				Min	-0.49	○	-0.15	○	-----	--
	Neutral Axis before Composition			Max	-0.10	○	-0.04	○	-----	--
				Min	-0.42	○	-0.14	○	-----	--
	Neutral Axis after Composition			Max	-0.10	○	-0.04	○	-----	--
				Min	-0.49	○	-0.16	○	-----	--
	Base of Lower Flange			Max	-0.07	○	-0.01	○	-----	--
				Min	-0.25	○	-0.02	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	24.70	--	20.18	--	-----	--	
	D16	cm	-----	38.71	--	31.62	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	8.98	--	0.00	--	-----	--	
Compressive Strength to Failure (Suc/Shu)			1.00	1.84	○	3.91	○	-----	--	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1	○	1.423	○	-----	--	
	D16			1	○	1.423	○	-----	--	
	D19			1.166	○	1.481	○	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.28	Δ	0.55	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.12	○	-0.03	○	-----	--	
	Neutral Axis before Composition			-0.11	○	-0.04	○	-----	--	
	Neutral Axis after Composition			-0.12	○	-0.04	○	-----	--	
	Base of Lower Flange			-0.06	○	-0.01	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.09	○	-0.03	○	-----	--
				Min	-0.49	○	-0.15	○	-----	--
	Neutral Axis before Composition			Max	-0.10	○	-0.04	○	-----	--
				Min	-0.42	○	-0.14	○	-----	--
	Neutral Axis after Composition			Max	-0.10	○	-0.04	○	-----	--
				Min	-0.49	○	-0.16	○	-----	--
	Base of Lower Flange			Max	-0.07	○	-0.01	○	-----	--
				Min	-0.25	○	-0.02	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	24.70	--	20.18	--	-----	--	
	D16	cm	-----	38.71	--	31.62	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2- 1]	[2- 2]	[2- 3]		
Interval from beginning of Girder			-----	0.500	1.450	4.000		
Shear Force								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.96 Δ	0.84 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.09 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.22 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.18 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.06 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.26 ○	-0.21 ○	
				Min	-----	--	-0.10 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.39 ○	-0.22 ○
				Min	-----	--	-0.21 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.39 ○	-0.22 ○
				Min	-----	--	-0.19 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.07 ○	-0.17 ○
				Min	-----	--	-0.05 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 --	25.61 --	
	D16	cm	-----	-----	--	31.63 --	40.00 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	8.92 --	8.65 --	
Shear Force + Torsion								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.96 Δ	0.84 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.09 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.22 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.18 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.06 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.26 ○	-0.21 ○	
				Min	-----	--	-0.10 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.39 ○	-0.22 ○
				Min	-----	--	-0.21 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.39 ○	-0.22 ○
				Min	-----	--	-0.19 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.07 ○	-0.17 ○
				Min	-----	--	-0.05 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 --	25.61 --	
	D16	cm	-----	-----	--	31.63 --	40.00 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 --	0.00 --	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	-----	--	999.999 ○	999.999 ○	
Strength against Diagonal Densile Failure(Mus/Mtu)	D13	-----	1.00	-----	--	999.999 ○	999.999 ○	
	D16			-----	--	999.999 ○	999.999 ○	
	D19			-----	--	999.999 ○	999.999 ○	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2- 4]	[2- 5]	[2- 6]				
Interval from beginning of Girder			-----	4.152	7.803	11.455				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.84	Δ	0.62	Δ	0.48	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.21	○	-0.11	○	-0.06	○
				Min	-0.01	○	0.00	○	0.00	○
	Neutral Axis before Composition	Max		-0.22	○	-0.13	○	-0.09	○	
		Min		0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition	Max		-0.23	○	-0.13	○	-0.08	○	
		Min		0.00	○	0.00	○	0.00	○	
	Base of Lower Flange	Max		-0.18	○	-0.15	○	-0.24	○	
		Min		0.00	○	0.00	○	0.00	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	25.81	--	39.27	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	8.59	--	5.65	--	2.43	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.84	Δ	0.62	Δ	0.48	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.21	○	-0.11	○	-0.06	○
				Min	-0.01	○	0.00	○	0.00	○
	Neutral Axis before Composition	Max		-0.22	○	-0.13	○	-0.09	○	
		Min		0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition	Max		-0.23	○	-0.13	○	-0.08	○	
		Min		0.00	○	0.00	○	0.00	○	
	Base of Lower Flange	Max		-0.18	○	-0.15	○	-0.24	○	
		Min		0.00	○	0.00	○	0.00	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	25.81	--	39.27	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Densile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	-	
	D16			999.999	○	999.999	○	-----	-	
	D19			999.999	○	999.999	○	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2- 7]	[2- 8]	[2- 9]				
Interval from beginning of Girder			-----	13.730	15.106	16.134				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.31	○	0.18	○	0.22	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	-0.01	○	-0.01	○	
	Neutral Axis before Composition			0.00	○	-0.01	○	-0.01	○	
	Neutral Axis after Composition			0.00	○	-0.01	○	-0.01	○	
	Base of Lower Flange			0.00	○	-0.01	○	-0.01	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.03	○	0.00	○	-0.01	○
				Min	0.00	○	-0.01	○	-0.01	○
	Neutral Axis before Composition	Max		-0.03	○	0.00	○	-0.01	○	
		Min		0.00	○	-0.01	○	-0.02	○	
	Neutral Axis after Composition	Max		-0.03	○	0.00	○	-0.01	○	
		Min		0.00	○	-0.01	○	-0.02	○	
	Base of Lower Flange	Max		-0.03	○	0.00	○	-0.01	○	
		Min		0.00	○	-0.01	○	-0.18	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.31	○	0.18	○	0.22	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	-0.01	○	-0.01	○	
	Neutral Axis before Composition			0.00	○	-0.01	○	-0.01	○	
	Neutral Axis after Composition			0.00	○	-0.01	○	-0.01	○	
	Base of Lower Flange			0.00	○	-0.01	○	-0.01	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.03	○	0.00	○	-0.01	○
				Min	0.00	○	-0.01	○	-0.01	○
	Neutral Axis before Composition	Max		-0.03	○	0.00	○	-0.01	○	
		Min		0.00	○	-0.01	○	-0.02	○	
	Neutral Axis after Composition	Max		-0.03	○	0.00	○	-0.01	○	
		Min		0.00	○	-0.01	○	-0.02	○	
	Base of Lower Flange	Max		-0.03	○	0.00	○	-0.01	○	
		Min		0.00	○	-0.01	○	-0.18	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	-----	-	-----	-	
	D16	-----	1.00	-----	-	-----	-	-----	-	
	D19	-----	1.00	-----	-	-----	-	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2-10]	[2-11]	[2-12]				
Interval from beginning of Girder			-----	18.758	22.409	26.060				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.56	Δ	0.87	Δ	1.20	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.02	○	-0.03	○	-0.10	○	
	Neutral Axis before Composition			-0.02	○	-0.03	○	-0.09	○	
	Neutral Axis after Composition			-0.02	○	-0.03	○	-0.10	○	
	Base of Lower Flange			-0.01	○	-0.02	○	-0.05	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.02	○	-0.03	○	-0.10	○
				Min	-0.08	○	-0.21	○	-0.42	○
	Neutral Axis before Composition			Max	-0.02	○	-0.03	○	-0.09	○
				Min	-0.13	○	-0.26	○	-0.42	○
	Neutral Axis after Composition			Max	-0.02	○	-0.03	○	-0.10	○
				Min	-0.10	○	-0.24	○	-0.45	○
	Base of Lower Flange			Max	-0.01	○	-0.02	○	-0.05	○
				Min	-0.24	○	-0.27	○	-0.30	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	26.06	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.09	--	4.91	--	8.51	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.56	Δ	0.87	Δ	1.20	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.02	○	-0.03	○	-0.10	○	
	Neutral Axis before Composition			-0.02	○	-0.03	○	-0.09	○	
	Neutral Axis after Composition			-0.02	○	-0.03	○	-0.10	○	
	Base of Lower Flange			-0.01	○	-0.02	○	-0.05	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.02	○	-0.03	○	-0.10	○
				Min	-0.08	○	-0.21	○	-0.42	○
	Neutral Axis before Composition			Max	-0.02	○	-0.03	○	-0.09	○
				Min	-0.13	○	-0.26	○	-0.42	○
	Neutral Axis after Composition			Max	-0.02	○	-0.03	○	-0.10	○
				Min	-0.10	○	-0.24	○	-0.45	○
	Base of Lower Flange			Max	-0.01	○	-0.02	○	-0.05	○
				Min	-0.24	○	-0.27	○	-0.30	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	26.06	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	999.999	○	
	D16			999.999	○	999.999	○	999.999	○	
	D19			999.999	○	999.999	○	999.999	○	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2-13]	[2-14]	[2-15]				
Interval from beginning of Girder			-----	26.212	28.762	29.712				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.23	Δ	0.50	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.11	○	-0.03	○	-----	--	
	Neutral Axis before Composition			-0.10	○	-0.04	○	-----	--	
	Neutral Axis after Composition			-0.11	○	-0.04	○	-----	--	
	Base of Lower Flange			-0.06	○	0.00	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.11	○	-0.04	○	-----	--
				Min	-0.44	○	-0.12	○	-----	--
	Neutral Axis before Composition			Max	-0.10	○	-0.04	○	-----	--
				Min	-0.44	○	-0.12	○	-----	--
	Neutral Axis after Composition			Max	-0.11	○	-0.04	○	-----	--
				Min	-0.46	○	-0.14	○	-----	--
	Base of Lower Flange			Max	-0.06	○	-0.01	○	-----	--
				Min	-0.30	○	-0.02	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	25.48	--	20.18	--	-----	--	
	D16	cm	-----	39.95	--	31.62	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	8.70	--	0.00	--	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.23	Δ	0.50	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.11	○	-0.03	○	-----	--	
	Neutral Axis before Composition			-0.10	○	-0.04	○	-----	--	
	Neutral Axis after Composition			-0.11	○	-0.04	○	-----	--	
	Base of Lower Flange			-0.06	○	0.00	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.11	○	-0.04	○	-----	--
				Min	-0.44	○	-0.12	○	-----	--
	Neutral Axis before Composition			Max	-0.10	○	-0.04	○	-----	--
				Min	-0.44	○	-0.12	○	-----	--
	Neutral Axis after Composition			Max	-0.11	○	-0.04	○	-----	--
				Min	-0.46	○	-0.14	○	-----	--
	Base of Lower Flange			Max	-0.06	○	-0.01	○	-----	--
				Min	-0.30	○	-0.02	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	25.48	--	20.18	--	-----	--	
	D16	cm	-----	39.95	--	31.62	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	-----	--	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	-----	-	-----	--	
	D16			999.999	○	-----	-	-----	--	
	D19			999.999	○	-----	-	-----	--	

5 Design of Intermediate Cross Beam

(1) Parameters

<1st Span>

	Unit	Bending Moment (Maximum)	Bending Moment (Minimum)	
CB 2				
Length between End of Girders	Lb	cm	328.0	328.0
Web Width	Bw	cm	22.0	22.0
Width of Cross Beam	Bc	cm	30.0	30.0
Thickness of Deck	Hs	cm	17.0	17.0
Height of Cross Beam (before Composition of Deck)	Hb	cm	130.0	130.0
Height of Cross Beam (after Composition of Deck)	Ha	cm	187.0	187.0
Interval of Cross Beam	Lt	cm	1404.0	1404.0

<2nd Span>

	Unit	Bending Moment (Maximum)	Bending Moment (Minimum)	
CB 2				
Length between End of Girders	Lb	cm	328.0	328.0
Web Width	Bw	cm	22.0	22.0
Width of Cross Beam	Bc	cm	30.0	30.0
Thickness of Deck	Hs	cm	17.0	17.0
Height of Cross Beam (before Composition of Deck)	Hb	cm	130.0	130.0
Height of Cross Beam (after Composition of Deck)	Ha	cm	187.0	187.0
Interval of Cross Beam	Lt	cm	1406.7	1406.7

(2) Calculation of Prestressing

1) Arrangement of PC Strand

(1) Parameter of PC Strand

	Unit	Parameters
Name of PC Strand		4S15.2, SWPR7BL
Area of PC Strand	mm ² /no.	554.80
Amount of Set	mm	4.0
Reduction Rate of Anchor	%	0.000
Friction Coefficient	1/m	0.0040
Creep Coefficient		2.60
Drying Shrinkage	×10 ⁻⁵	20.00
Relaxation	%	2.5
Prestressing Stress	N/mm ²	1250.000
(Considering Friction Coefficient)	N/mm ²	1250.000
Allowable Value	N/mm ²	1440.000

(2) Arrangement of PC Strand

<1st Span>

Item		Unit	Maximum Bending Moment	Minimum Bending Moment
CB 2				
How to Prestressing			From One Side	
Length of PC Strand		m	10.720	10.720
1st	Position	mm	400	400
	Number	No.	1	1
2nd	Position	Mm	800	800
	Number	No.	1	1

<2nd Span>

Item		Unit	Maximum Bending Moment	Minimum Bending Moment
CB 2				
How to Prestressing			From One Side	
Length of PC Strand		m	10.720	10.720
1st	Position	mm	400	400
	Number	No.	1	1
2nd	Position	mm	800	800
	Number	No.	1	1

<Design of Cross Beam : Summary for Calculation Results of Stress>

1st Span : Cross Beam (CB2)

Item		Unit	Allowable Value	Mmax		Mmin	
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	-0.36	○	-0.39	○
	Bottom of Deck			-0.24	○	-0.26	○
Dead Load	Top of Cross Beam	N/mm ²	0 ~ 11.0	2.28	○	2.29	○
	Bottom of Cross Beam			4.55	○	4.62	○
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	0.52	○	-0.91	○
	Bottom of Deck			0.35	○	-0.61	○
Dead Load	Top of Cross Beam	N/mm ²	0 ~ 11.0	2.18	○	2.34	○
	Bottom of Cross Beam			2.21	○	6.01	○
Ultimate Load		-----	1	1.79	○	1.64	○
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1440	1250	○	1250	○
	Immediately After Prestressing	N/mm ²	1295	1175	○	1175	○
	Effective Prestressing Force	N/mm ²	1110	1024	○	1024	○

2nd Span : Cross Beam (CB2)

Item		Unit	Allowable Value	Mmax		Mmin	
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	-0.36	○	-0.39	○
	Bottom of Deck			-0.24	○	-0.26	○
Dead Load	Top of Cross Beam	N/mm ²	0 ~ 11.0	2.28	○	2.29	○
	Bottom of Cross Beam			4.53	○	4.63	○
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	0.53	○	-0.92	○
	Bottom of Deck			0.35	○	-0.61	○
Dead Load	Top of Cross Beam	N/mm ²	0 ~ 11.0	2.18	○	2.35	○
	Bottom of Cross Beam			2.19	○	6.01	○
Ultimate Load		-----	1	1.79	○	1.64	○
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1440	1250	○	1250	○
	Immediately After Prestressing	N/mm ²	1295	1175	○	1175	○
	Effective Prestressing Force	N/mm ²	1110	1024	○	1024	○

<Design of Cross Beam : Summary for Calculation Results of Stress>

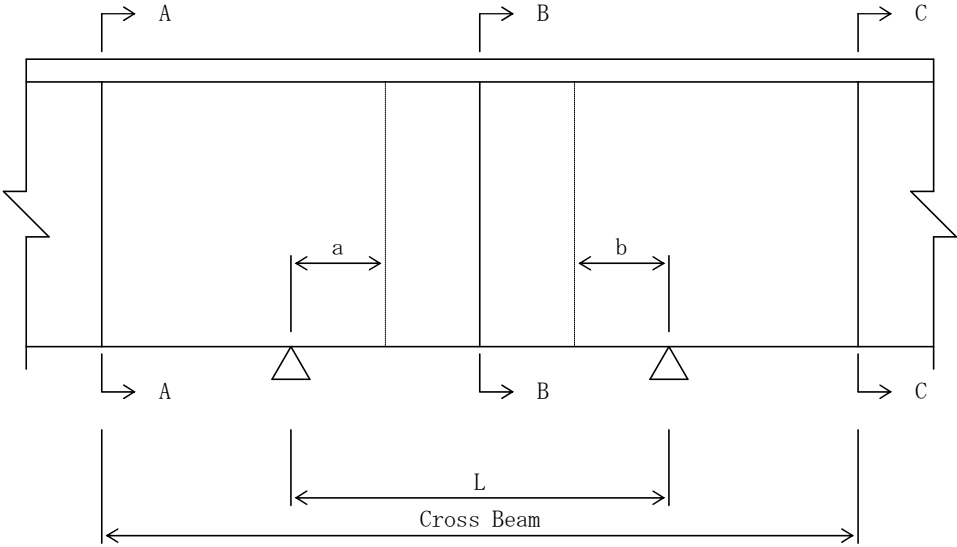
1st Span : Cross Beam (CB2)

Item	Unit	Allowable Value	Smax	Smin	Tmax	Tmin					
Shear Force											
Shear Stress	Design Load	N/mm ²	0.45	0.69	Δ	0.48	Δ	0.12	○	0.17	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	-0.02	○	-0.02	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	-0.17	○	-0.18	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Suc/Shu	-	1.00	2.71	○	3.89	○	12.52	○	9.86	○
Strength against Diagonal Densile Failure	D13	-	1.00	1.00	○	1.49	○	----	--	----	--
	Sus/Shu	D16	-	1.00	1.00	○	1.84	○	----	--	----
Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.00	○	0.00	○	0.00	○	0.00	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	0.00	○	0.00	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	0.00	○	0.00	○	0.00	○	0.00	○
Shear Force + Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.69	Δ	0.48	Δ	0.12	○	0.17	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-1.10	-0.02	○	-0.02	○	0.00	○	0.00	○
	Design Load	N/mm ²	-2.20	-0.17	○	-0.18	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Muc/Mtu	-	1.00	999.999	○	999.999	○	1000.00	○	999.999	○
Strength against Diagonal Densile Failure	D13	-	1.00	999.999	○	999.999	○	----	--	----	--
	Mus/Mtu	D16	-	1.00	999.999	○	999.999	○	----	--	----
Amount of Diagonal Tension Re-bar	cm ²	----	10.28	--	6.00	--	6.00	--	6.00	--	
Axial Reinforcement Bar Volume	cm ²	----	5.57	--	1.01	--	0.00	--	0.00	--	

2nd Span : Cross Beam (CB2)

Item	Unit	Allowable Value	Smax	Smin	Tmax	Tmin					
Shear Force											
Shear Stress	Design Load	N/mm ²	0.45	0.68	Δ	0.48	Δ	0.18	○	0.11	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	-0.02	○	-0.02	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	-0.17	○	-0.18	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Suc/Shu	-	1.00	2.72	○	3.89	○	9.71	○	12.65	○
Strength against Diagonal Densile Failure	D13	-	1.00	1.00	○	1.49	○	----	--	----	--
	Sus/Shu	D16	-	1.00	1.00	○	1.84	○	----	--	----
Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.00	○	0.00	○	0.00	○	0.00	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	0.00	○	0.00	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	0.00	○	0.00	○	0.00	○	0.00	○
Shear Force + Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.68	Δ	0.48	Δ	0.18	○	0.11	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-1.10	-0.02	○	-0.02	○	0.00	○	0.00	○
	Design Load	N/mm ²	-2.20	-0.17	○	-0.18	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Muc/Mtu	-	1.00	999.999	○	999.999	○	1000.00	○	999.999	○
Strength against Diagonal Densile Failure	D13	-	1.00	999.999	○	999.999	○	----	--	----	--
	Mus/Mtu	D16	-	1.00	999.999	○	999.999	○	----	--	----
Amount of Diagonal Tension Re-bar	cm ²	----	10.23	--	6.00	--	6.00	--	6.00	--	
Axial Reinforcement Bar Volume	cm ²	----	5.54	--	1.02	--	0.00	--	0.00	--	

6 Design of Coupling Concrete
Dimension



Unit: m

L	1.200
a	0.500
b	0.500

<Connection of Cross beam : Summary for Calculation Results of Stress>

1st Span~2nd Span, Main Girder Number: G1(Negative Moment) G4(Positive Moment)

Item		Unit	Allowable Value	Negative Moment						Positive Moment		
				A-A		B-B		C-C		B-B		
Re-bar Volume	1st Layer	Diameter	mm	-----	D19	--	D19	--	D19	--	D22	--
		Number	Number	-----	16	--	16	--	16	--	12	--
	2nd Layer	Diameter	mm	-----	D19	--	D19	--	D19	--	D22	--
		Number	Number	-----	16	--	16	--	16	--	12	--
Bending Stress (Dead Load)												
Bending Tensile Stress of Reinforcement Bar		N/mm ²	100	-80.12	○	-73.90	○	-80.15	○	95.77	○	
Bending Stress (Design Load)												
Bending Stress of Concrete		N/mm ²	10	1.53	○	1.53	○	1.53	○	2.18	○	
Bending Tensile Stress of Reinforcement Bar		N/mm ²	160	41.37	○	41.37	○	41.37	○	109.04	○	
Bending Stress (Temperature Load)												
Bending Stress of Concrete		N/mm ²	11.5	1.90	○	1.53	○	1.90	○	2.99	○	
Bending Tensile Stress of Reinforcement Bar		N/mm ²	184	51.19	○	41.37	○	51.23	○	149.80	○	
Ultimate Load		-----	1.00	1.37	○	1.55	○	1.37	○	2.85	○	

7 Calculation of Reaction Force

7.1 Reaction Force for Each Girder

<1st Span, Left>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	348.939	342.005	339.517	341.351
Cast-in-place Concrete	D2	312.629	430.185	427.634	304.118
Weight of Bridge Surface	D3	155.436	133.624	130.103	144.839
Subtotal: DT1=D1+D2+D3		817.004	905.814	897.254	790.308
Live Load LT	Max	316.170	303.730	304.430	320.980
	Min	-65.180	-29.940	-28.870	-67.760
Subtotal: DT2 =DT1+LT+SW	Max	1133.174	1209.544	1201.684	1111.288
	Min	751.824	875.874	868.384	722.548
Creep CR		97.215	94.869	97.067	111.118
Drying Shrinkage SH		-8.204	-9.254	-9.329	-9.079
Temperature Range		21.331	24.060	24.255	23.605
Dead Load: DT1+CR+SH		906.015	991.429	984.992	892.347
Total: DT2+CR +SH+T+SD	Max	1243.516	1319.219	1313.677	1236.932
	Min	862.166	985.549	980.377	848.192

<1st Span, Right>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	348.946	342.012	339.524	341.358
Cast-in-place Concrete	D2	326.736	454.033	451.482	318.701
Weight of Bridge Surface	D3	236.817	212.143	210.857	241.897
Subtotal: DT1=D1+D2+D3		912.499	1008.188	1001.863	901.956
Live Load LT	Max	537.160	473.330	463.700	514.040
	Min	-245.000	-162.940	-146.050	-213.350
Subtotal: DT2 =DT1+LT+SW	Max	1449.659	1481.518	1465.563	1415.996
	Min	667.499	845.248	855.813	688.606
Creep CR		-97.486	-95.530	-97.821	-111.957
Drying Shrinkage SH		8.207	9.244	9.317	9.055
Temperature Range		-21.336	-24.034	-24.223	-23.543
Dead Load: DT1+CR+SH		823.220	921.902	913.359	799.054
Total: DT2+CR +SH+T+SD	Max	1339.044	1371.198	1352.836	1289.551
	Min	556.884	734.928	743.086	562.161

<2nd Span, Left>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	349.317	342.467	340.071	342.007
Cast-in-place Concrete	D2	326.677	454.507	452.050	319.589
Weight of Bridge Surface	D3	230.039	221.809	238.534	286.238
Subtotal: DT1=D1+D2+D3		906.033	1018.783	1030.655	947.834
Live Load LT	Max	537.660	473.690	465.120	515.530
	Min	-245.110	-162.290	-145.720	-212.450
Subtotal: DT2 =DT1+LT+SW	Max	1443.693	1492.473	1495.775	1463.364
	Min	660.923	856.493	884.935	735.384
Creep CR		-96.812	-94.032	-96.097	-109.996
Drying Shrinkage SH		8.192	9.250	9.324	9.084
Temperature Range		-21.299	-24.049	-24.241	-23.617
Dead Load: DT1+CR+SH		817.413	934.001	943.882	846.922
Total: DT2+CR +SH+T+SD	Max	1333.774	1383.642	1384.761	1338.835
	Min	551.004	747.662	773.921	610.855

<2nd Span, Right>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	349.309	342.460	340.064	342.000
Cast-in-place Concrete	D2	312.667	430.659	428.202	304.941
Weight of Bridge Surface	D3	151.890	138.205	143.023	166.011
Subtotal: DT1=D1+D2+D3		813.866	911.324	911.289	812.952
Live Load LT	Max	315.870	303.700	304.890	321.560
	Min	-65.220	-29.790	-28.730	-67.180
Subtotal: DT2 =DT1+LT+SW	Max	1129.736	1215.024	1216.179	1134.512
	Min	748.646	881.534	882.559	745.772
Creep CR		97.083	94.693	96.851	110.834
Drying Shrinkage SH		-8.194	-9.240	-9.312	-9.060
Temperature Range		21.304	24.023	24.210	23.555
Dead Load: DT1+CR+SH		902.755	996.777	998.828	914.726
Total: DT2+CR +SH+T+SD	Max	1239.929	1324.500	1327.928	1259.841
	Min	858.839	991.010	994.308	871.101

7.2 Reaction Force for Pier and Abutment

Unit: kN

		1	2	3
Weight of Girder	D1	1371.812	2745.702	1373.833
Cast-in-place Concrete	D2	1474.566	3103.775	1476.469
Weight of Bridge Surface	D3	564.002	1878.334	599.129
Subtotal: DT1=D1+D2+D3		3410.380	7727.811	3449.431
Live Load LT	Max	1021.120	1963.620	1021.720
	Min	-103.030	0.000	-102.430
Subtotal: DT2 =DT1+LT+SW	Max	4431.500	9691.431	4471.151
	Min	3307.350	7727.811	3347.001
Creep CR		400.269	-799.731	399.461
Drying Shrinkage SH		-35.866	71.673	-35.806
Temperature Range		93.251	-186.342	93.092
Dead Load: DT1+CR+SH		3774.783	6999.753	3813.086
Total: DT2+CR +SH+T+SD	Max	4889.154	8777.031	4927.898
	Min	3765.004	6813.411	3803.748

7.3 Horizontal Force

Horizontal Force(PF1、 PF2fix)

(kN)

	PF1	PF2
Prestressing	-266	344
Drying Shrinkage	-275	356
Temperature(+)	251	-331
Temperature(-)	-251	331
Dead Load	-540	700
Temperature+15°C	-290	370
Temperature-15°C	-791	1031
Temperature+40°C	128	-181
Temperature-40°C	-1208	1582

8 Design of Cross Beam at End of Girder

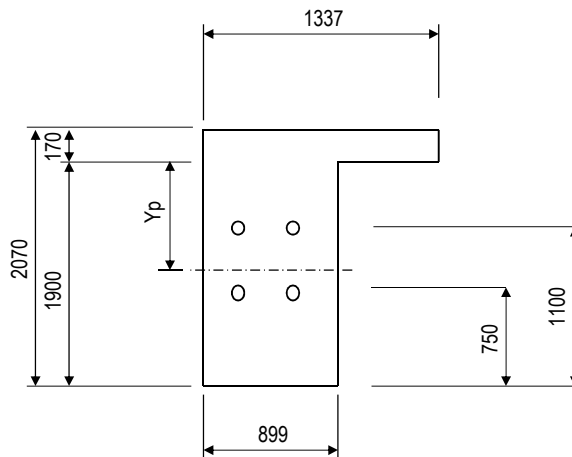
8.1 For Bending Moment

1) Calculation of Bending Moment

(kN·m)

		Bending Moment	
		max	min
Dead Load	(Md)	-84.24	-84.24
Live Load	(ML)	320.31	-159.80
Total	(M)	236.07	-244.04

2) Dimension



3) Calculation of Prestressing

Type of PC strand 4S15.2 SWPR19L

Area of PC strand 554.8 mm²

Number of PC strand 4

(N/mm²)

	Tensile Stress of PC strand	
	Allowable Value	Result
During Prestressing	1440	1250
Immediately after Prestressing	1295	1151
Under Effective Prestressing Force	1110	1056

4) Combined Flexural Stress

(N/mm²)

		Bending Moment(Max)		Bending Moment(Min)	
		Top	Bottom	Top	Bottom
Dead Load		-0.12	0.12	-0.12	0.12
Live Load		0.44	-0.47	-0.22	0.23
Prestressing		1.26	1.48	1.26	1.48
Total	Dead Load	1.14	1.60	1.14	1.60
	Live Load	1.58	1.13	0.92	1.83
Allowable Value		$0.00 \leq \sigma \leq 12.0$			





01-2-PC-I GIRDER BRIDGE
(PF5-PF7)

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END 81

1.1 DESIGN CONDITION

ROAD GRADE	:	Equivalent to CLASS 4-1
BRIDGE TYPE	:	2 span continuous PC-I girder bridge with composite deck (PC plate and RC deck)
BRIDGE LENGTH	:	L = 60.000 m
SPAN LENGTH	:	L = 28.851 + 28.852 m (ON CL)
WIDTH OF THE ROAD	:	TOTAL 12.750 m L = 0.500 + 5.500 + 0.750 + 5.500 + 0.500 m
HORIZONTAL ALIGNMENT	:	R=320 ~ A=130
LONGITUDINAL SLOPE	:	0.50 %  ~ 0.20 % 
SECTION SLOPE	:	LEFT : 6.00 % ~ 3.86 %  RIGHT : 6.00 % ~ 3.79 % 
ANGLE OF SKEW	:	PF5,PF6 : 90°00'00" PF7 : 92°29'51"
PAVEMENT	:	ASPHALT PAVEMENT t= 80 mm
SLAB	:	REINFORCED CONCRETE t= 170 mm
PLATE	:	PRESTRESS CONCRETE PLATE t= 100 mm
LIVE ROAD	:	AASHTO HL=93
DESIGN STANDARD	:	AASHTO LRFD BRIDGE DESIGN 2014(LIVE ROAD) Specifications for highway bridges(Japan Road Association) 1 Common matters,3 Concrete bridges,5 seismic design (April 2012)

1.2 MATERIALS STRENGTH

1) CONCRETE

		(N/mm ²)				
		MAIN GIRDER	CROSS BEAM	RC SLAB	PC PLATE	COUPLING CONCRETE
DESIGN STANDARD STRENGTH OF CONCRETE		40.00	30.00	30.00	40.00	30.0
BENDING COMPRESSIVESTRESS	IMMEDIATELY AFTER PRESTRESSING	19.00	14.00	----	19.00	----
	OTHERS	14.00	11.00	10.00	15.00	10.00
BENDING TENSILE STRESS	IMMEDIATELY AFTER PRESTRESSING	-1.50	-1.20	----	-1.50	----
	DEAD LOAD	0.0	0.0	----	----	----
	DESIGN LOAD	-1.50	-1.20	----	0.0	----
	TEMPERATURE CHANGE	-2.00	----	----	----	----
MEAN SHEAR STRESS CONCRETE CAN CARRY		0.55	0.45	----	----	----
MAXIMUM MEAN CONCRETE SHEAR STRESS		5.30	4.00	----	----	----
ALLOWABLE DIAGONEL TENSILE STRESS (Case where shear force or torsional moment)	DEAD LOAD	-1.00	-0.80	----	----	----
	LIVE LOAD	-2.00	-1.70	----	----	----
ALLOWABLE DIAGONEL TENSILE STRESS (Case where both shear force and torsional moment)	DEAD LOAD	-1.30	-1.10	----	----	----
	LIVE LOAD	-2.50	-2.20	----	----	----

2) PC STRAND

		(N/mm ²)		
		MAIN GIRDER	CROSS BEAM	PC PLATE
PRESTRESSING STEEL TYPE		SWPR7BL 7S15.2mm	SWPR7BL 4S15.2mm	SWPR7AL 1S9.3mm
TENSILE STRENGTH		1850	1850	1700
YIELD POINT		1600	1600	1450
ALLOWABLE TENSILE STRESS	DURING PRESTRESSING	1440	1440	1305
	IMMEDIATELY AFTER PRESTRESSING	1295	1295	1190
	AT COMPOSITION OF SLAB	1110	----	----
	DESIGN LOAD	1110	1110	1020

3) REINFORCING STEEL

		(N/mm ²)			
		MAIN GIRDER	CROSS BEAM	RC SLAB	COUPLING CONCRETE
STEEL TYPE		SD345	SD345	SD345	SD345
YIELD POINT		345	345	345	345
ALLOWABLE TENSILE STRESS	DEAD LOAD	----	----	100	100
	DESIGN LOAD	180	200	140	160
	COLLISION LOAD	----	----	300	----
	WIND LOAD	----	----	175	----

1.3 DESIGN CONSTANT

1) CONCRETE

		MAIN GIRDER	CAST IN PLACE	PC PLATE
YOUNG'S MODULUS	DESIGN LOAD (N/mm ²)	3.10×10^4	2.80×10^4	3.10×10^4
	IMMEDIATELY AFTER PRESTRESSING (N/mm ²)	2.92×10^4	2.58×10^4	2.92×10^4
CREEP COEFFICIENT	NUMBER OF DAYS FOR DECK CONSTRUCTION	90	----	----
	NUMBER OF CONSTRUCTION DAYS FOR BRIDGE SURFACE	120	----	----
	DESIGN LOAD	2.60	2.60	3.00
	DURING DECK CONSTRUCTION	1.70	----	----
	BRIDGE SURFACE	1.65	----	----
DRYING SHRINKAGE OF CONCRETE	DURING DECK CONSTRUCTION	4.0×10^{-5}	----	----
	DESIGN LOAD	20.0×10^{-5}	20.0×10^{-5}	20.0×10^{-5}
UNIT WEIGHT (kN/mm ³)		24.5	24.5	24.5

2) PC STRAND(MAIN GIRDER)

		1	2
YOUNG'S MODULUS	N/mm ²	2.00×10^5	2.00×10^5
SLIP	mm	4.0	4.0
RELAXATION	%	2.5	2.5
FRICTION COEFFICIENT	1/m	0.004	0.004
	1/rad	0.300	0.300
AREA	mm ²	970.900	970.900
UNIT WEIGHT	kg/m	7.707	7.707
DIAMETER OF SHEATH	mm	60.0	60.0
DECREASE RATIO BY ANCHOR	%	0.0	0.0

3) PC STRAND(CROSS BEAM)

YOUNG'S MODULUS	N/mm ²	2.00×10^5
SLIP	mm	4.0
RELAXATION	%	2.5
FRICTION COEFFICIENT	1/m	0.004
AREA	mm ²	554.800
UNIT WEIGHT	kg/m	4.404
DIAMETER OF SHEATH	mm	45.0
DECREASE RATIO BY ANCHOR	%	0.0

4) PC STRAND(PC PLATE)

		BETWEEN MAIN GIRDERS	
YOUNG'S MODULUS		N/mm ²	2.00 × 10 ⁵
RELAXATION	BEFORE PRESTRESSING	%	1.5
	AFTER PRESTRESSING	%	1.5
	EXTRA COEFFICIENT OF HIGH TEMPERATURE	%	1.0
AREA		mm ²	51.610
UNIT WEIGHT		kg/m	0.405

1. 5 Dimension

1) Dimension of Main Girder

Girder Height : 1900.00 ~ 1900.00 mm

【Change of Web Width (mm)】

Span	End of Girder (Left Side)			End of Girder (Right Side)		
	Ending Point of Changing Web Width	Starting Point of Changing Web Width	Web Width	Ending Point of Changing Web Width	Starting Point of Changing Web Width	Web Width
1	1000.0	4000.0	700.0	4000.0	1000.0	700.0
2	1000.0	4000.0	700.0	4000.0	1000.0	700.0

2) Dimension of Cross Beam

【Interval of Cross Beam on Left Girder (m)】

Span	Number of Intermediate Cross Beams	CB1~CB2	CB2~CB3
1	1	14.682	14.682
2	1	14.587	14.587

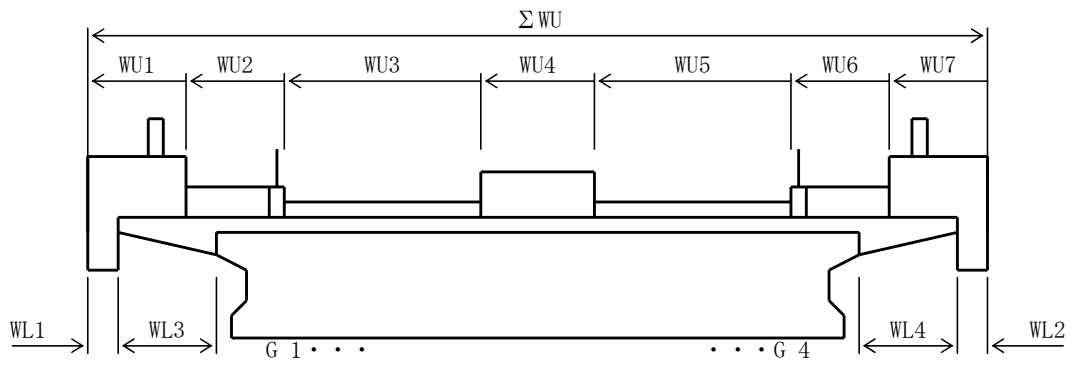
【Interval of Cross Beam on Right Girder (m)】

Span	Number of Intermediate Cross Beams	CB1~CB2	CB2~CB3
1	1	15.174	15.174
2	1	15.277	15.277

【Dimension of Cross Beam (m)】

Span	Cross Beam Width	Cross Beam Width (Left Side)	Cross Beam Width (Right Side)
1	0.300	0.900	0.950
2	0.300	0.950	0.900

【Cross Section】



【m】

	ΣWU	WU1	WU2	WU3	WU4	WU5	WU6	WU7
1	12.750	0.500	0.000	5.500	0.750	5.500	0.000	0.500
2	12.750	0.500	0.000	5.500	0.750	5.500	0.000	0.500
3	12.763	0.500	0.000	5.506	0.751	5.505	0.000	0.500

	ΣWU	WL1	WL2	WL3	WL4
1	3.508	0.000	0.000	0.623	0.314
2	3.508	0.000	0.000	0.648	0.289
3	3.517	0.000	0.000	0.617	0.302

2. 1 Load Intensity

1) Load Intensity

(1) Bridge Surface Loads

< 1 >

Load Type		Load Intensity	Load Location	
			Left End of Girder Side	Right End of Girder Side
Selfweight of Kerb	Left	8.590 kN/m	0.180 m	0.180 m
	Right	9.750 kN/m	0.190 m	0.180 m
Selfweight of Concrete Barrier	Left	0.600 kN/m	0.125 m	0.125 m
	Right	0.600 kN/m	0.125 m	0.125 m
Selfweight of Sidewalk	Left	0.000 kN/m ²		
	Right	0.000 kN/m ²		
Selfweight of Handrail	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Kerb	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Pavement	Left	2.610 kN/m ²		
	Right	3.300 kN/m ²		
Selfweight of Median		9.320 kN/m ²		
Selfweight of Additional Object	1	0.110 kN/m	0.075 m	0.075 m
	2	0.110 kN/m	12.675 m	12.675 m

< 2 >

Load Type		Load Intensity	Load Location	
			Left End of Girder Side	Right End of Girder Side
Selfweight of Kerb	Left	9.140 kN/m	0.180 m	0.180 m
	Right	9.570 kN/m	0.180 m	0.190 m
Selfweight of Concrete Barrier	Left	0.600 kN/m	0.125 m	0.125 m
	Right	0.600 kN/m	0.125 m	0.125 m
Selfweight of Sidewalk	Left	0.000 kN/m ²		
	Right	0.000 kN/m ²		
Selfweight of Handrail	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Kerb	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Pavement	Left	3.000 kN/m ²		
	Right	3.000 kN/m ²		
Selfweight of Median		9.680 kN/m ²		
Selfweight of Additional Object	1	0.110 kN/m	0.075 m	0.075 m
	2	0.110 kN/m	12.675 m	12.675 m

Condition of Load

Calculation of Bridge Surface Loads

(PF5-PF6)

① Unit Weight

PC · RC Concrete	$\gamma_1 = 24.5 \text{ kN/m}^3$
Concrete	$\gamma_2 = 23.0 \text{ kN/m}^3$
Asphalt Pavement	$\gamma_3 = 22.5 \text{ kN/m}^3$

② Bridge Surface Loads

- Pavement on Left Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = 1/2 \times (0.082 + 0.148) = 0.115 \text{ m}$$

(Thickness of Leveling Concrete)

$$t_c = 0.115 - 0.080 = 0.035 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.035 \times 23.0 = \underline{\underline{2.61 \text{ kN/m}^2}}$$

- Pavement on Right Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = 1/2 \times (0.112 + 0.177) = 0.145 \text{ m}$$

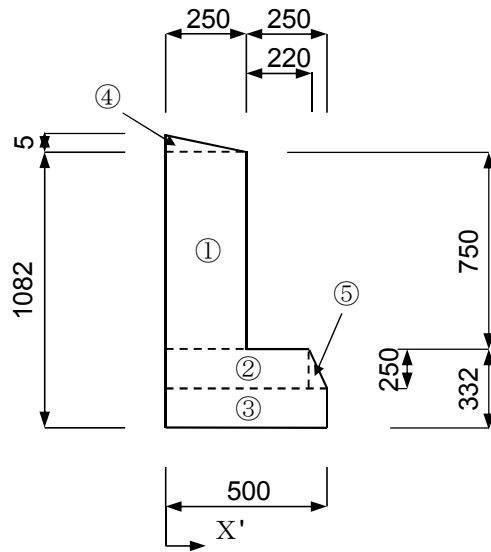
(Thickness of Leveling Concrete)

$$t_c = 0.145 - 0.080 = 0.065 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.065 \times 23.0 = \underline{\underline{3.30 \text{ kN/m}^2}}$$

• Concrete Barrier (Left Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.082	0.500	0.0410	0.250	0.01025
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3504		0.0632

Load Location

$$X' = 0.0632 / 0.3504$$

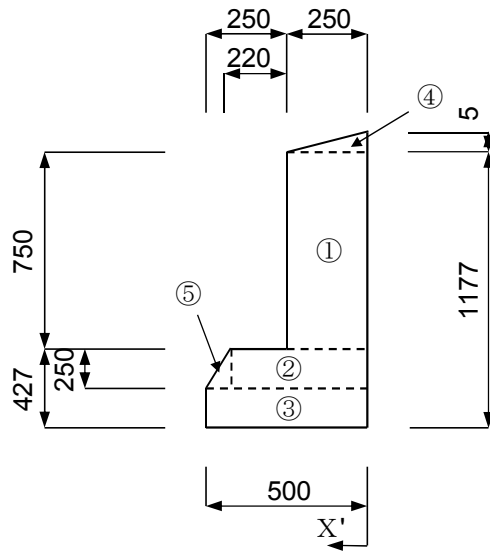
$$= \underline{0.180 \text{ m}}$$

Load Intensity

$$P = 0.3504 \times 24.5$$

$$= \underline{8.59 \text{ kN/m}}$$

• Concrete Barrier (Right Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.177	0.500	0.0885	0.250	0.02213
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3979		0.0750

Load Location

$$X' = 0.0750 / 0.3979$$

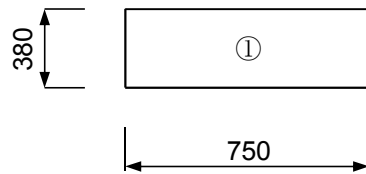
$$= \underline{0.190 \text{ m}}$$

Load Intensity

$$P = 0.3979 \times 24.5$$

$$= \underline{9.75 \text{ kN/m}}$$

• Median



a) Load Intensity and Load Location

	H	B	A
① □	0.3800	0.7500	0.2850
			0.2850

Load Location

X' = On CL

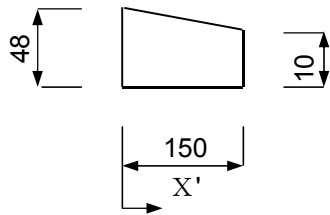
Load Intensity

$$P = 0.2850 \times 24.5 = \underline{\underline{6.99 \text{ kN/m}}}$$

$$W = 6.9900 / 0.750 = \underline{\underline{9.32 \text{ kN/m}^2}}$$

• Left Drain Duct

※Loaded as Selfweight of Additional Object 1



Load Location

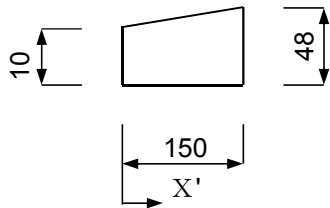
$X' = 75\text{mm}$ inside beginning of Left Kerb

Load Intensity

$$P = 1/2 \times (0.048 + 0.010) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Right Drain Duct

※Loaded as Selfweight of Additional Object 2



Load Location

$X' = 75\text{mm}$ inside beginning of Right Kerb

Load Intensity

$$P = 1/2 \times (0.010 + 0.048) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Handrail

※Loaded as Concrete Barrier

Load Location

$X' = 125\text{mm}$ inside beginning of Right and Left Kerb

Load Intensity

$$P = 0.60 = \underline{0.60 \text{ kN/m}}$$

Condition of Load

Calculation of Bridge Surface Loads

(PF6-PF7)

① Unit Weight

PC · RC Concrete	$\gamma_1 = 24.5 \text{ kN/m}^3$
Concrete	$\gamma_2 = 23.0 \text{ kN/m}^3$
Asphalt Pavement	$\gamma_3 = 22.5 \text{ kN/m}^3$

② Bridge Surface Loads

- Pavement on Left Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = 1/2 \times (0.127 + 0.163) = 0.145 \text{ m}$$

(Thickness of Leveling Concrete)

$$t_c = 0.145 - 0.080 = 0.065 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.065 \times 23.0 = \underline{\underline{3.30 \text{ kN/m}^2}}$$

- Pavement on Right Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = 1/2 \times (0.127 + 0.162) = 0.145 \text{ m}$$

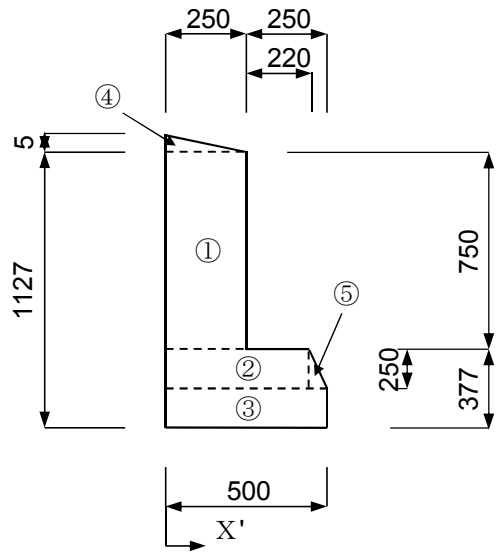
(Thickness of Leveling Concrete)

$$t_c = 0.145 - 0.080 = 0.065 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.065 \times 23.0 = \underline{\underline{3.30 \text{ kN/m}^2}}$$

• Concrete Barrier (Left Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.127	0.500	0.0635	0.250	0.01588
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3729		0.0688

Load Location

$$X' = 0.0688 / 0.3729$$

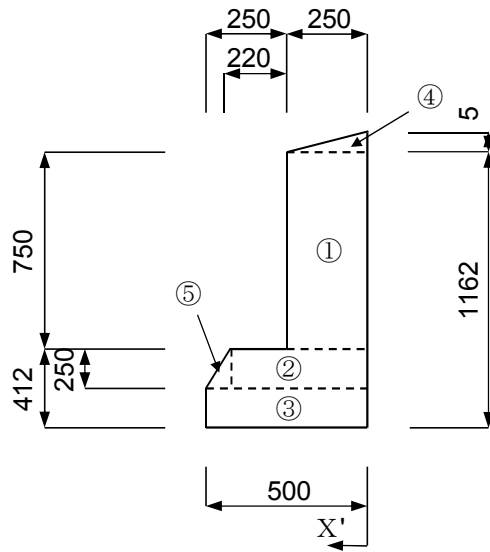
$$= \underline{0.180 \text{ m}}$$

Load Intensity

$$P = 0.3729 \times 24.5$$

$$= \underline{9.14 \text{ kN/m}}$$

• Concrete Barrier (Right Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.162	0.500	0.0810	0.250	0.02025
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3904		0.0732

Load Location

$$X' = 0.0732 / 0.3904$$

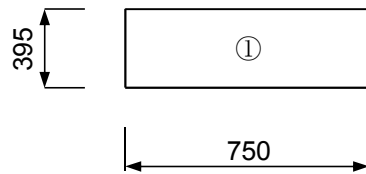
$$= \underline{0.190 \text{ m}}$$

Load Intensity

$$P = 0.3904 \times 24.5$$

$$= \underline{9.57 \text{ kN/m}}$$

• Median



a) Load Intensity and Load Location

	H	B	A
① □	0.3950	0.7500	0.2963
			0.2963

Load Location

X' = On CL

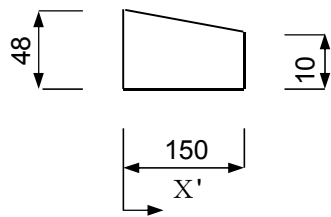
Load Intensity

$$P = 0.2963 \times 24.5 = \underline{\underline{7.26 \text{ kN/m}}}$$

$$W = 7.2600 / 0.750 = \underline{\underline{9.68 \text{ kN/m}^2}}$$

• Left Drain Duct

※Loaded as Selfweight of Additional Object 1



Load Location

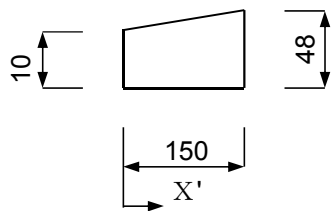
$X' = 75\text{mm}$ inside beginning of Left Kerb

Load Intensity

$$P = 1/2 \times (0.048 + 0.010) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Right Drain Duct

※Loaded as Selfweight of Additional Object 2



Load Location

$X' = 75\text{mm}$ inside beginning of Right Kerb

Load Intensity

$$P = 1/2 \times (0.010 + 0.048) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Handrail

※Loaded as Concrete Barrier

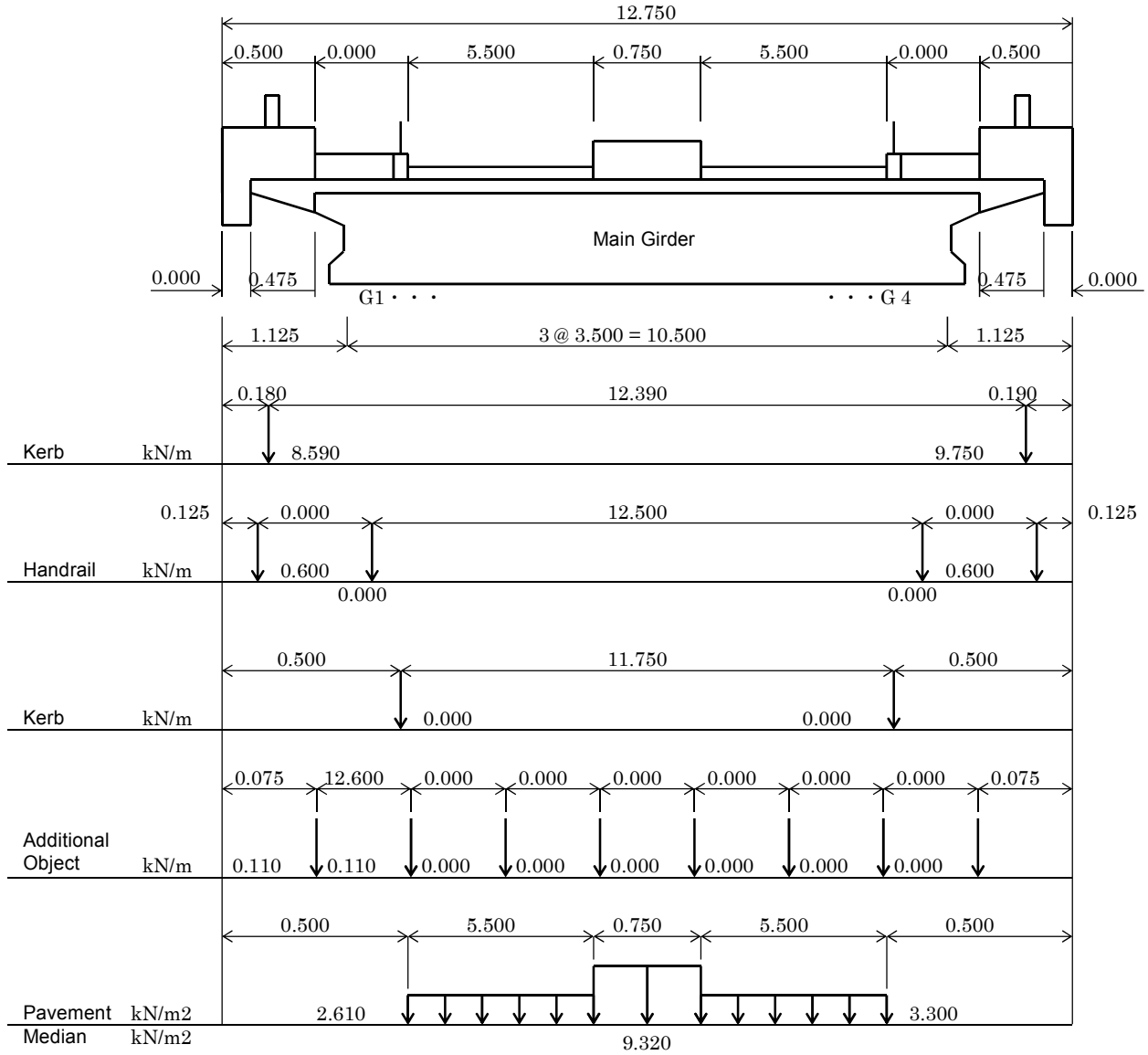
Load Location

$X' = 125\text{mm}$ inside beginning of Right and Left Kerb

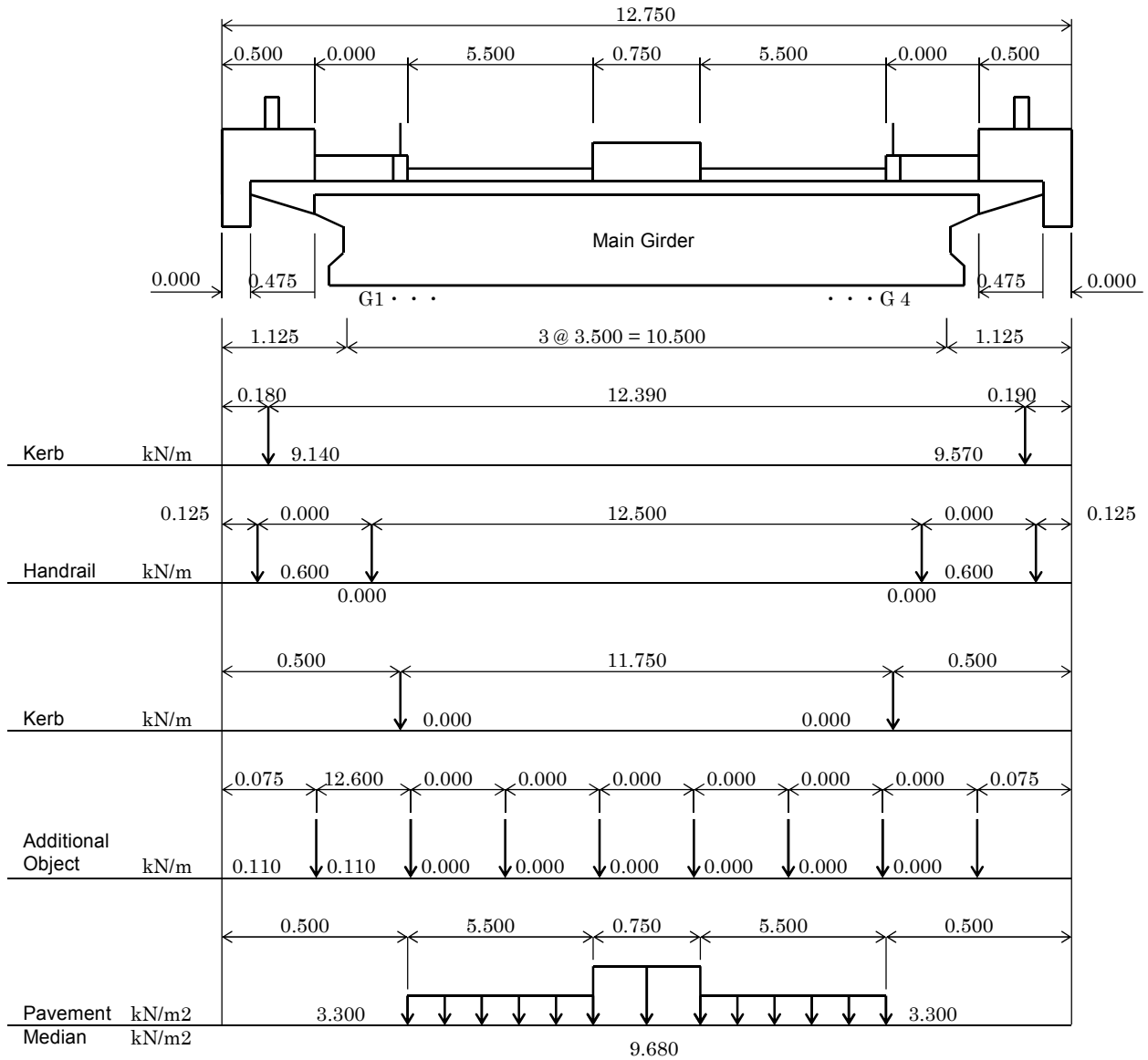
Load Intensity

$$P = 0.60 = \underline{0.60 \text{ kN/m}}$$

Load Intensity (Bridge Surface Loads_PF5-PF6)



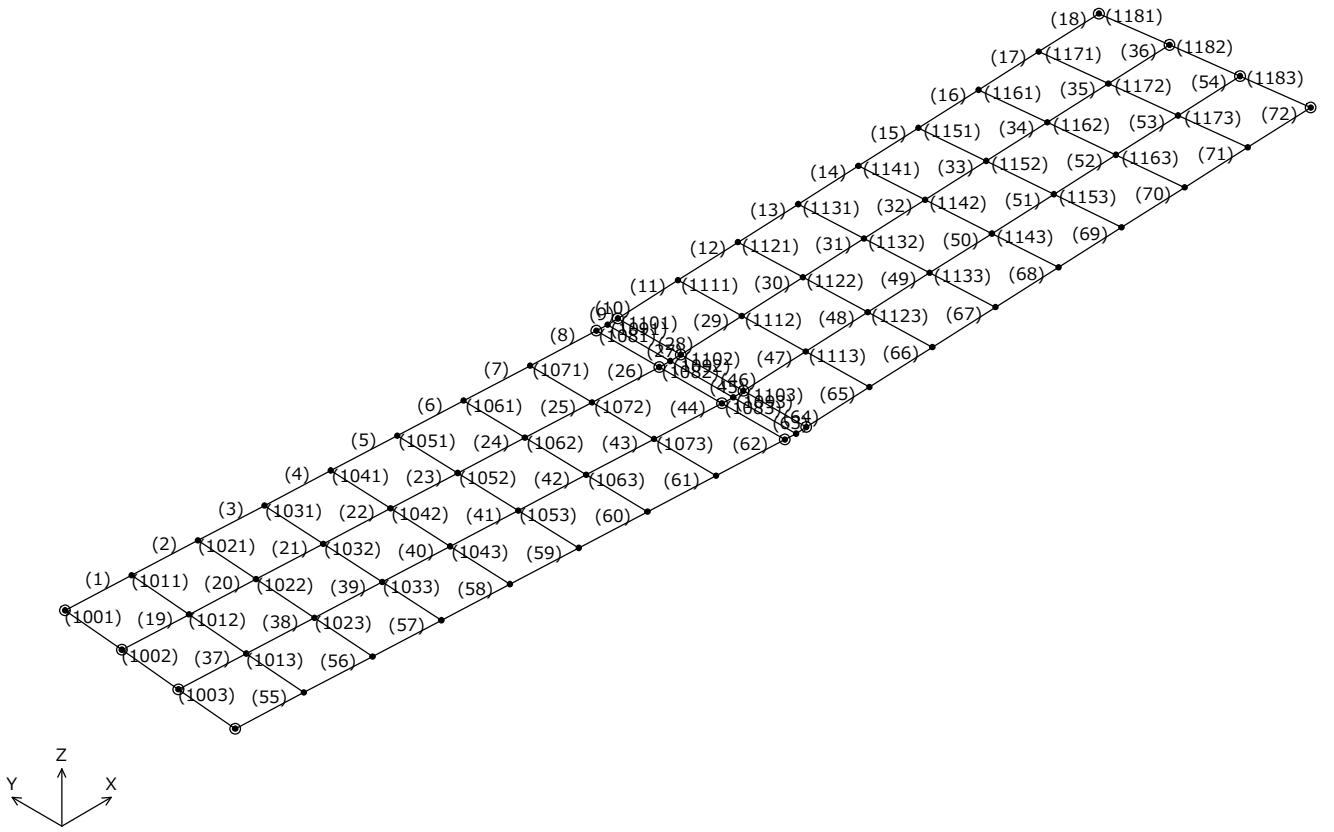
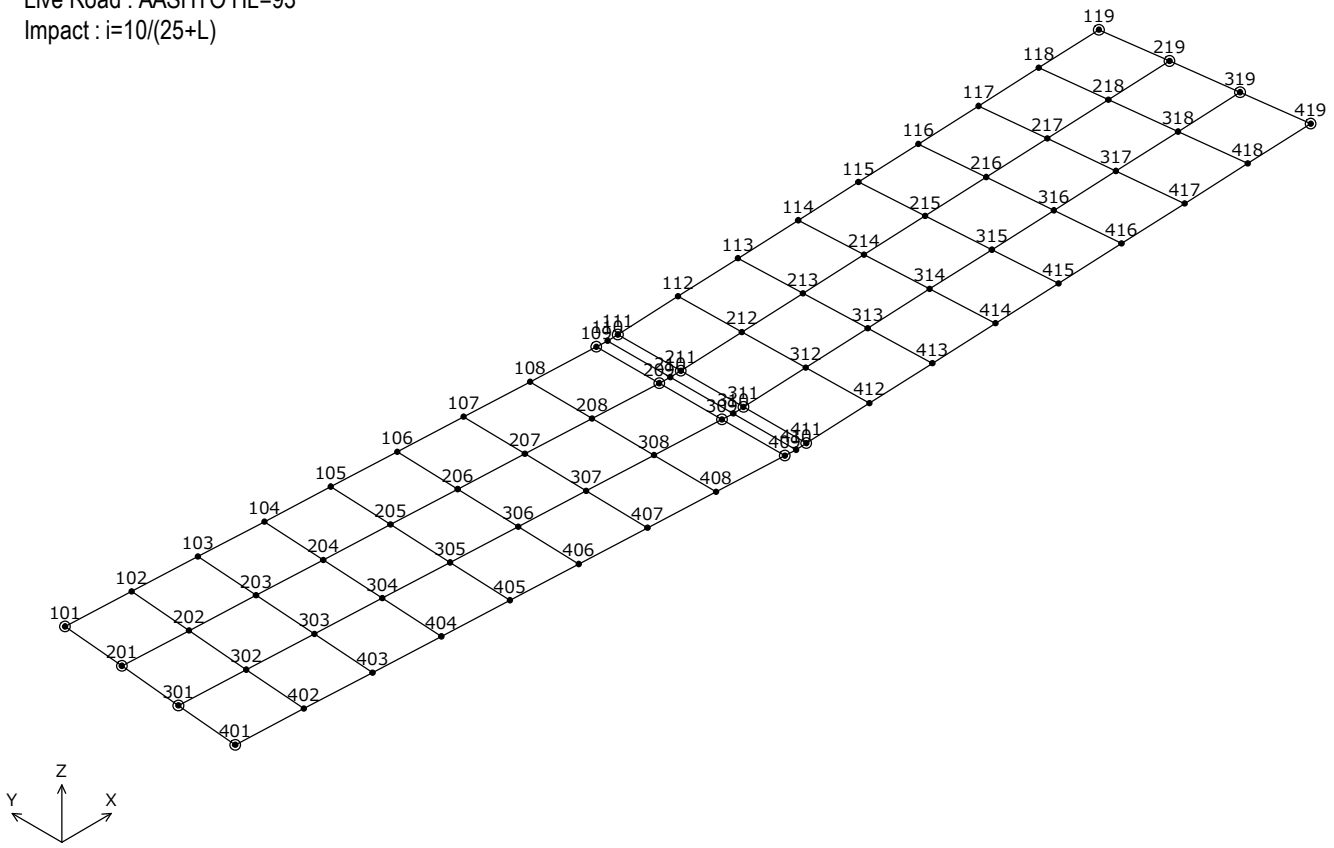
Load Intensity (Bridge Surface Loads_PF6-PF7)

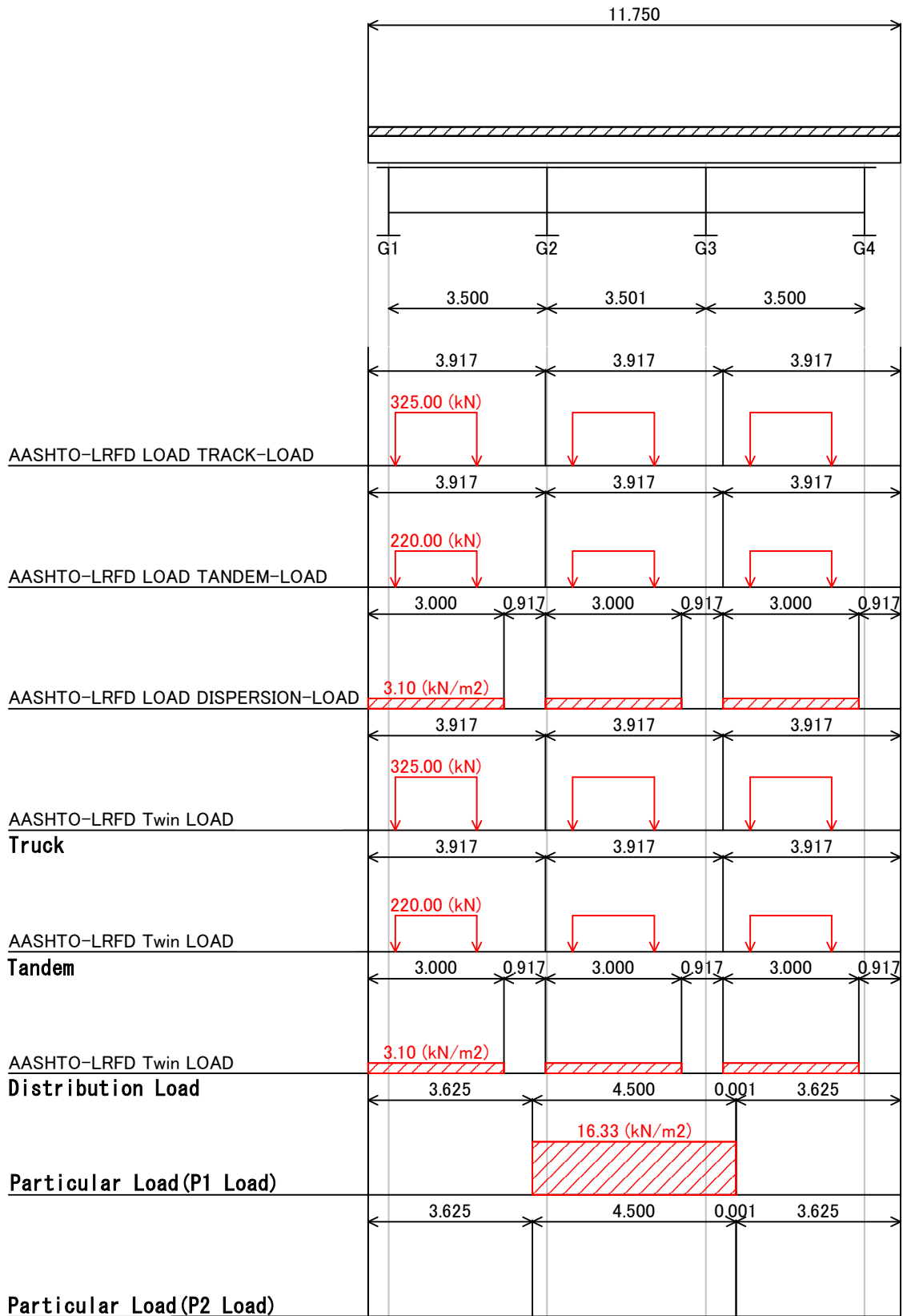


(2) Live Road

Live Road : AASHTO HL=93

Impact : $i=10/(25+L)$

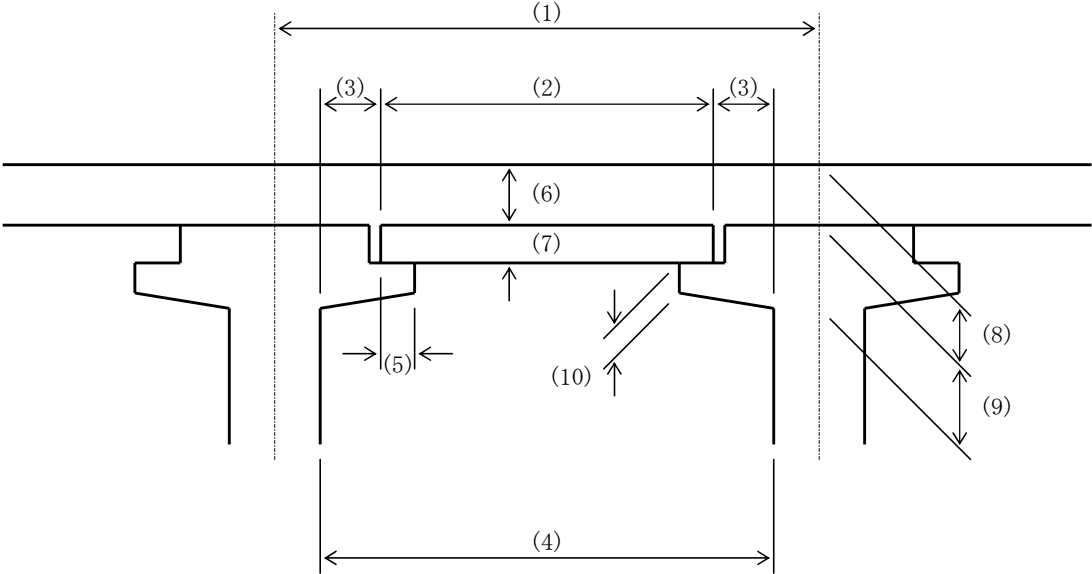




3 Design of Deck Slab

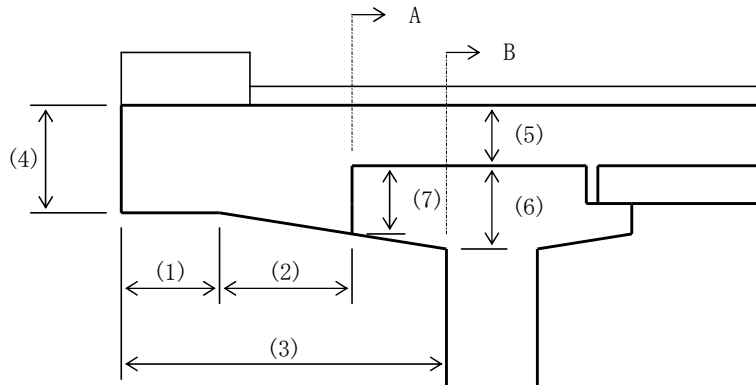
3.1 Dimension

1) Deck Slab between Girders



		1st Span		2nd Span	
		End of Girder	Center of Girder	Center of Girder	End of Girder
(1)	m	3.500	3.500	3.500	3.500
(2)	m	2.380	2.380	2.380	2.380
(3)	m	0.210	0.450	0.450	0.210
(4)	m	2.800	3.280	3.280	2.800
(5)	m	0.090	0.090	0.090	0.090
Span Length of PC Plate		2.260	2.260	2.260	2.260
(6)	mm	170.0	170.0	170.0	170.0
(7)	mm	100.0	100.0	100.0	100.0
(6)+(7)	mm	270.0	270.0	270.0	270.0
(8)	mm	170.0	170.0	170.0	170.0
(9)	mm	255.6	300.0	300.0	255.6
(10)	mm	100.0	100.0	100.0	100.0

2) Deck Slab outside of Girders



			1st Span		2nd Span	
			End of Girder	Center of Girder	Center of Girder	End of Girder
Left Side	(1)	m	0.000	0.000	0.000	0.000
	(2)	m	0.648	0.648	0.648	0.648
	(3)	m	0.948	1.188	1.188	0.948
	(4)	mm	250.0	250.0	250.0	250.0
	(5)	mm	170.0	170.0	170.0	170.0
	(6)	mm	255.6	300.0	300.0	255.6
	(7)	mm	200.0	200.0	200.0	200.0
Right Side	(1)	m	0.000	0.000	0.000	0.000
	(2)	m	0.647	0.647	0.647	0.647
	(3)	m	0.947	1.187	1.187	0.947
	(4)	mm	250.0	250.0	250.0	250.0
	(5)	mm	170.0	170.0	170.0	170.0
	(6)	mm	255.6	300.0	300.0	255.6
	(7)	mm	200.0	200.0	200.0	200.0

3) Calculation of Prestressing of PC Plate

		Unit	
Name of PC Strand			1S9.3
Material of PC Strand			SWPR7AL
Area of PC Strand	mm ² /no.		51.61
Number of PC Strand	No.		15
Creep Coefficient			3.00
Drying Shrinkage of Concrete		×10 ⁻⁵	25.00
Relaxation	Before Prestressing	%	1.50
	Extra Coefficient of High Temperature	%	1.00
	After Prestressing	%	1.50
Prestressing Stress σ_{pi}		N/mm ²	1225.00
Allowable Value		N/mm ²	1305.00

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Left End of Girder Side

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item	Unit	Allowable Value	Result
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5
	Bottom of PC Plate	N/mm ²	~19.0
	Max×0.6	N/mm ²	8.343
Bending stress of PC plate	Top of PC Plate	N/mm ²	0
	Bottom of PC Plate	N/mm ²	~15.0
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11
	Bottom of RC Deck	N/mm ²	11
	Top of PC Plate	N/mm ²	0
	Bottom of PC Plate	N/mm ²	~15.0
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305
	Immediately After Prestressing	N/mm ²	1190
	Effective Prestressing Force	N/mm ²	1020
Axial stress of PC plate	N/mm ²	10	

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.592	○	140	74.665	○	
Edge of PC Plate	Positive Moment	10	3.917	○	140	60.859	○
	Negative Moment	10	3.797	○	140	79.511	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	8.659	○	140	100.221	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	0.56	○
Tensile Stress of Reinforcement Bar	140	27.98	○

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Left End of Girder Side

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	8.904	○
	D+L	10	0.34	○	140	8.904	○
	D+L+CO	15	2.177	○	300	57.047	○
	D+L+W	12.5	0.485	○	175	12.702	○
	D+W	12.5	0.63	○	175	16.501	○
Supporting for Deck	D	-----	-----	--	100	13.854	○
	D+L	10	3.942	○	140	113.551	○
	D+L+CO	15	5.395	○	300	155.381	○
	D+L+W	12.5	4.058	○	175	116.893	○
	D+W	12.5	0.713	○	175	20.538	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	9.709	○
	D+L	10	0.37	○	140	9.709	○
	D+L+CO	15	2.208	○	300	57.852	○
	D+L+W	12.5	0.515	○	175	13.507	○
	D+W	12.5	0.66	○	175	17.306	○
Supporting for Deck	D	-----	-----	--	100	15.057	○
	D+L	10	3.975	○	140	114.505	○
	D+L+CO	15	5.428	○	300	156.334	○
	D+L+W	12.5	4.092	○	175	117.847	○
	D+W	12.5	0.755	○	175	21.741	○

Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	1.932	○	140	69.85	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	1.93	○	140	69.784	○

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Center of Span

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item		Unit	Allowable Value	Result	
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5	9.17	○
	Bottom of PC Plate	N/mm ²		~19.0	8.343
	Max×0.6	N/mm ²	8.343	5.502	○
Bending stress of PC plate	Top of PC Plate	N/mm ²	0	10.591	○
	Bottom of PC Plate	N/mm ²		~15.0	3.699
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11	4.245	○
	Bottom of RC Deck	N/mm ²		-0.975	○
	Top of PC Plate	N/mm ²	0	8.171	○
	Bottom of PC Plate	N/mm ²		~15.0	0.561
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305	1225	○
	Immediately After Prestressing	N/mm ²	1190	1131.097	○
	Effective Prestressing Force	N/mm ²	1020	922.979	○
Axial stress of PC plate		N/mm ²	10	8.756	○

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.565	○	140	78.898	○	
Edge of PC Plate	Positive Moment	10	6.742	○	140	104.756	○
	Negative Moment	10	3.279	○	140	68.659	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	9.958	○	140	115.254	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	1.002	○
Tensile Stress of Reinforcement Bar	140	55.499	○

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Center of Span

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	8.893	○
	D+L	10	0.339	○	140	8.893	○
	D+L+CO	15	2.176	○	300	57.036	○
	D+L+W	12.5	0.484	○	175	12.692	○
	D+W	12.5	0.629	○	175	16.49	○
Supporting for Deck	D	-----	-----	--	100	17.242	○
	D+L	10	2.541	○	140	78.134	○
	D+L+CO	15	3.776	○	300	116.118	○
	D+L+W	12.5	2.64	○	175	81.197	○
	D+W	12.5	0.76	○	175	23.37	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	9.709	○
	D+L	10	0.37	○	140	9.709	○
	D+L+CO	15	2.208	○	300	57.852	○
	D+L+W	12.5	0.515	○	175	13.507	○
	D+W	12.5	0.66	○	175	17.306	○
Supporting for Deck	D	-----	-----	--	100	19.295	○
	D+L	10	2.606	○	140	80.143	○
	D+L+CO	15	3.841	○	300	118.128	○
	D+L+W	12.5	2.706	○	175	83.207	○
	D+W	12.5	0.827	○	175	25.422	○

Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	2.367	○	140	85.595	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	2.365	○	140	85.53	○

<Design of Deck: Summary for Calculation Results of Stress>

2nd Span, Center of Span

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item		Unit	Allowable Value	Result	
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5	9.17	○
	Bottom of PC Plate	N/mm ²		~19.0	8.343
	Max×0.6	N/mm ²	8.343	5.502	○
Bending stress of PC plate	Top of PC Plate	N/mm ²	0	10.591	○
	Bottom of PC Plate	N/mm ²		~15.0	3.699
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11	4.245	○
	Bottom of RC Deck	N/mm ²		-0.975	○
	Top of PC Plate	N/mm ²	0	8.171	○
	Bottom of PC Plate	N/mm ²		~15.0	0.561
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305	1225	○
	Immediately After Prestressing	N/mm ²	1190	1131.097	○
	Effective Prestressing Force	N/mm ²	1020	922.979	○
Axial stress of PC plate		N/mm ²	10	8.756	○

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.565	○	140	78.898	○	
Edge of PC Plate	Positive Moment	10	6.742	○	140	104.756	○
	Negative Moment	10	3.279	○	140	68.659	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	9.958	○	140	115.254	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	1.002	○
Tensile Stress of Reinforcement Bar	140	55.499	○

<Design of Deck: Summary for Calculation Results of Stress>

2nd Span, Center of Span

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	9.289	○
	D+L	10	0.354	○	140	9.289	○
	D+L+CO	15	2.192	○	300	57.432	○
	D+L+W	12.5	0.499	○	175	13.088	○
	D+W	12.5	0.644	○	175	16.886	○
Supporting for Deck	D	-----	-----	--	100	17.912	○
	D+L	10	2.562	○	140	78.804	○
	D+L+CO	15	3.798	○	300	116.788	○
	D+L+W	12.5	2.662	○	175	81.867	○
	D+W	12.5	0.782	○	175	24.04	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	9.582	○
	D+L	10	0.366	○	140	9.582	○
	D+L+CO	15	2.203	○	300	57.725	○
	D+L+W	12.5	0.511	○	175	13.381	○
	D+W	12.5	0.656	○	175	17.179	○
Supporting for Deck	D	-----	-----	--	100	19.088	○
	D+L	10	2.599	○	140	79.937	○
	D+L+CO	15	3.834	○	300	117.921	○
	D+L+W	12.5	2.699	○	175	83.001	○
	D+W	12.5	0.82	○	175	25.216	○

Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	2.367	○	140	85.595	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	2.365	○	140	85.53	○

<Design of Deck: Summary for Calculation Results of Stress>

2nd Span, Right End of Girder Side

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item		Unit	Allowable Value	Result	
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5	9.17	○
	Bottom of PC Plate	N/mm ²		8.343	○
	Max×0.6	N/mm ²	8.343	5.502	○
Bending stress of PC plate	Top of PC Plate	N/mm ²	0	10.585	○
	Bottom of PC Plate	N/mm ²		3.692	○
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11	3.545	○
	Bottom of RC Deck	N/mm ²		-0.814	○
	Top of PC Plate	N/mm ²	0	8.343	○
	Bottom of PC Plate	N/mm ²		1.292	○
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305	1225	○
	Immediately After Prestressing	N/mm ²	1190	1131.097	○
	Effective Prestressing Force	N/mm ²	1020	922.098	○
Axial stress of PC plate		N/mm ²	10	8.756	○

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.592	○	140	74.665	○	
Edge of PC Plate	Positive Moment	10	3.917	○	140	60.859	○
	Negative Moment	10	3.797	○	140	79.511	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	8.659	○	140	100.221	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	0.56	○
Tensile Stress of Reinforcement Bar	140	27.98	○

<Design of Deck: Summary for Calculation Results of Stress>

2nd Span, Right End of Girder Side

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	9.302	○
	D+L	10	0.355	○	140	9.302	○
	D+L+CO	15	2.192	○	300	57.445	○
	D+L+W	12.5	0.5	○	175	13.101	○
	D+W	12.5	0.645	○	175	16.9	○
Supporting for Deck	D	-----	-----	--	100	14.482	○
	D+L	10	3.964	○	140	114.179	○
	D+L+CO	15	5.416	○	300	156.009	○
	D+L+W	12.5	4.08	○	175	117.521	○
	D+W	12.5	0.735	○	175	21.166	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	9.582	○
	D+L	10	0.366	○	140	9.582	○
	D+L+CO	15	2.203	○	300	57.725	○
	D+L+W	12.5	0.511	○	175	13.381	○
	D+W	12.5	0.656	○	175	17.179	○
Supporting for Deck	D	-----	-----	--	100	14.88	○
	D+L	10	3.969	○	140	114.329	○
	D+L+CO	15	5.422	○	300	156.158	○
	D+L+W	12.5	4.085	○	175	117.671	○
	D+W	12.5	0.749	○	175	21.564	○

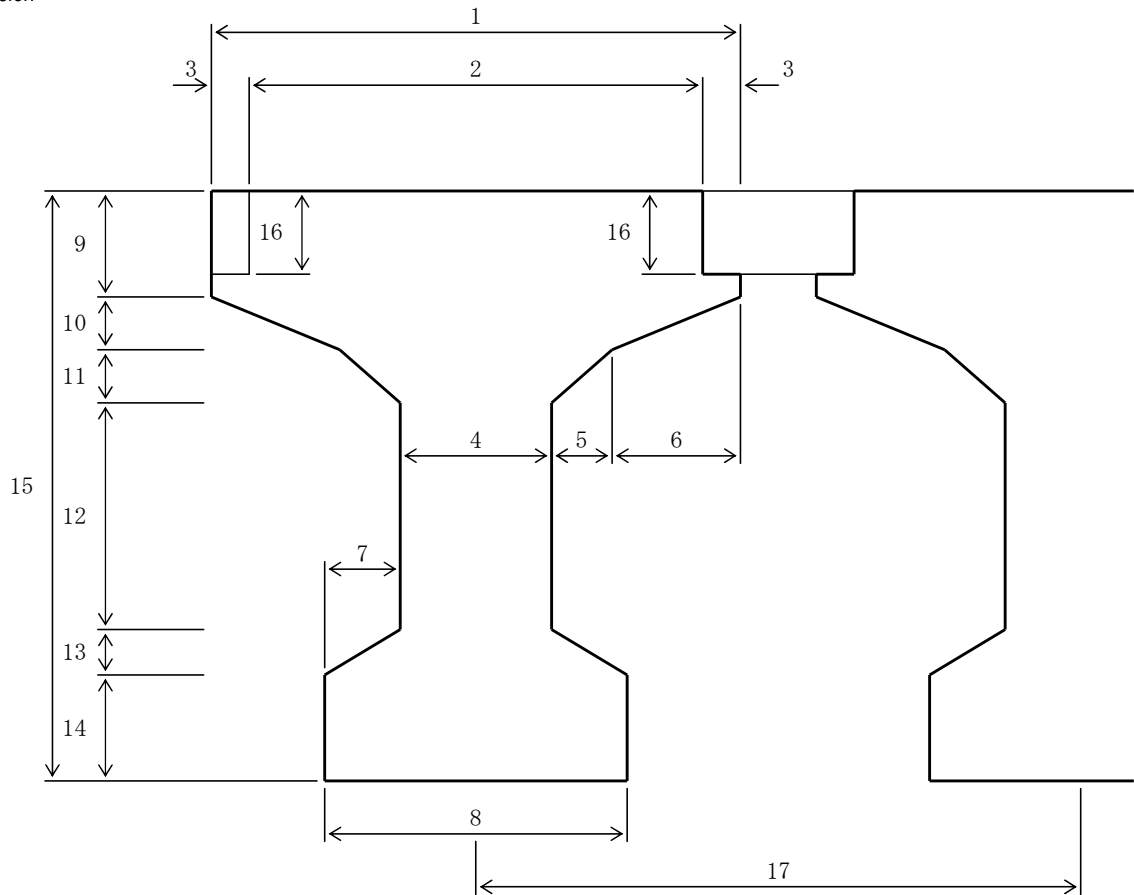
Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	1.932	○	140	69.85	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	1.93	○	140	69.784	○

4 Design of Main Girder

4.1 Dimension and PC Strand Arrangement

1) Dimension



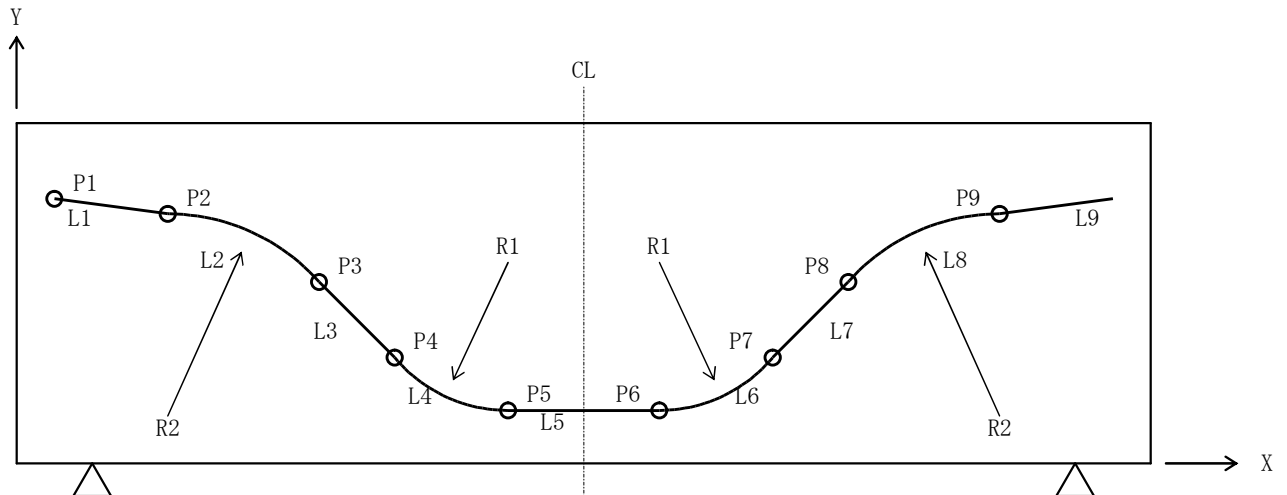
(Unit: mm)

	1st Span			2nd Span		
	End of Girder (Left)	Center Span	End of Girder (Left)	Center Span	End of Girder (Left)	Center Span
1	1300.0	1300.0	1300.0	1300.0	1300.0	1300.0
2	1060.0	1060.0	1060.0	1060.0	1060.0	1060.0
3	120.0	120.0	120.0	120.0	120.0	120.0
4	700.0	220.0	700.0	700.0	220.0	700.0
5	0.0	0.0	0.0	0.0	0.0	0.0
6	300.0	540.0	300.0	300.0	540.0	300.0
7	0.0	240.0	0.0	0.0	240.0	0.0
8	700.0	700.0	700.0	700.0	700.0	700.0
9	200.0	200.0	200.0	200.0	200.0	200.0
10	55.6	100.0	55.6	55.6	100.0	55.6
11	0.0	0.0	0.0	0.0	0.0	0.0
12	1444.4	1150.0	1444.4	1444.4	1150.0	1444.4
13	0.0	250.0	0.0	0.0	250.0	0.0
14	200.0	200.0	200.0	200.0	200.0	200.0
15	1900.0	1900.0	1900.0	1900.0	1900.0	1900.0
16	100.0	100.0	100.0	100.0	100.0	100.0
17	3500.0	3500.0	3500.0	3500.2	3500.2	3500.2

2) PC Strand Arrangement

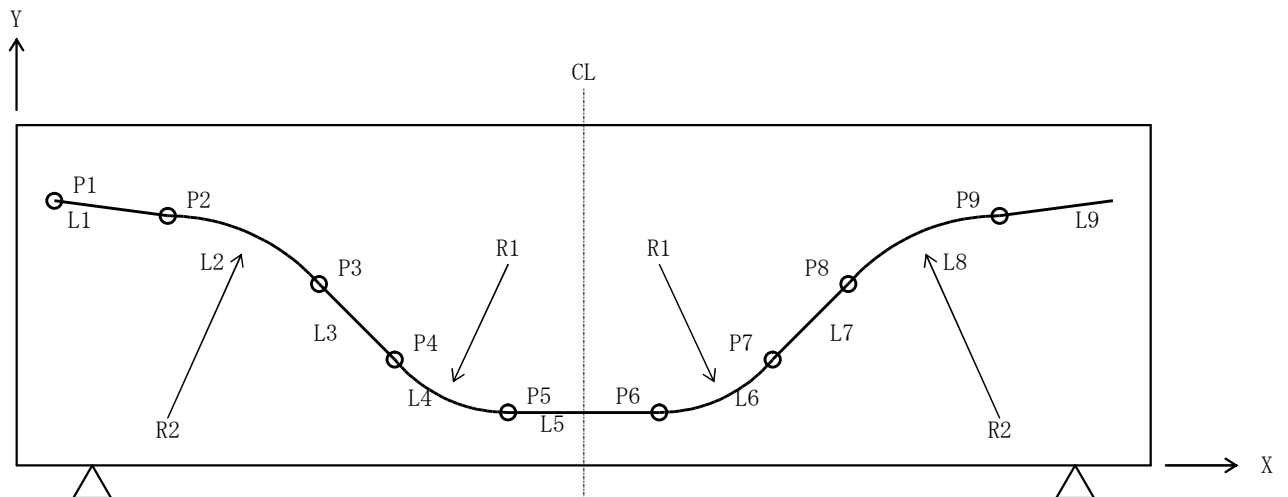
<1st Span>

PC Strand No.		1	2	3	4	5
Number of PC Strand		1	1	1	1	1
Coordinate (mm)	P1 X	-----	-----	-----	-----	-----
	Y	-----	-----	-----	-----	-----
	P2 X	-----	-----	-----	-----	-----
	Y	-----	-----	-----	-----	-----
	P3 X	200.0	200.0	200.0	200.0	200.0
	Y	1650.0	1300.0	950.0	600.0	250.0
	P4 X	13119.0	10730.4	8341.8	4706.9	1710.7
	Y	406.0	286.0	166.0	166.0	144.4
	P5 X	14077.5	11688.9	9300.2	5665.3	2408.3
	Y	360.0	240.0	120.0	120.0	120.0
P6 X	16290.4	18163.6	20036.8	22887.4	25709.1	
Y	360.0	240.0	120.0	120.0	120.0	
P7 X	17509.1	19382.3	21255.5	24106.1	26667.6	
Y	434.5	314.5	194.5	194.5	166.0	
P8 X	26801.2	26801.2	26801.2	26801.2	27061.4	
Y	1575.5	1225.5	875.5	525.5	204.0	
P9 X	28019.9	28019.9	28019.9	28019.9	28019.9	
Y	1650.0	1300.0	950.0	600.0	250.0	
P1 [~] X	29819.9	29819.9	29819.9	29819.9	29819.9	
Y	1650.0	1300.0	950.0	600.0	250.0	
Angle	α (L) (R)	5°30'0" 0°0'0"	5°30'0" 0°0'0"	5°30'0" 0°0'0"	5°30'0" 0°0'0"	4°0'0" 0°0'0"
Radius (m)	R2 (L)	-----	-----	-----	-----	-----
	R1 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (R)	10.000	10.000	10.000	10.000	10.000
	R2 (R)	10.000	10.000	10.000	10.000	10.000
Angle	β (L) (R)	7°0'0" -----	7°0'0" -----	7°0'0" -----	7°0'0" -----	5°30'0" -----
Length of PC Strand (m)	L1	-----	-----	-----	-----	-----
	L2	-----	-----	-----	-----	-----
	L3	12.979	10.579	8.179	4.528	1.514
	L4	0.960	0.960	0.960	0.960	0.698
	L5	2.213	6.475	10.737	17.222	23.301
	L6	1.222	1.222	1.222	1.222	0.960
	L7	9.362	7.475	5.587	2.715	0.396
	L8	1.222	1.222	1.222	1.222	0.960
	L9	1.800	1.800	1.800	1.800	1.800
	Total	29.757	29.732	29.707	29.669	29.629



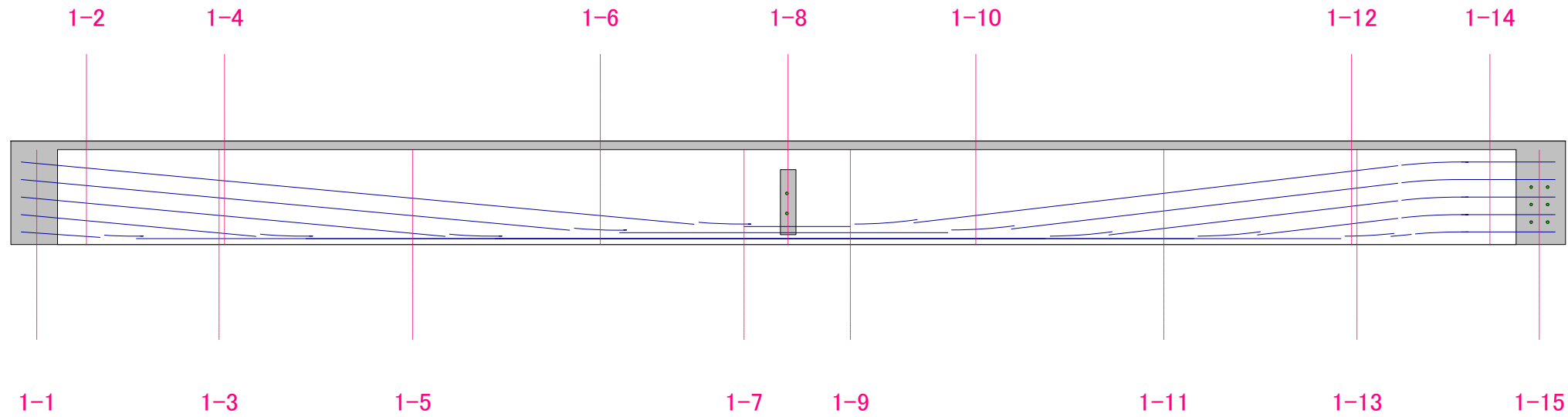
<2nd Span>

PC Strand No.		1	2	3	4	5
Number of PC Strand		1	1	1	1	1
Coordinate (mm)	P1 X	200.0	200.0	200.0	200.0	200.0
	Y	1650.0	1300.0	950.0	600.0	250.0
	P2 X	2000.0	2000.0	2000.0	2000.0	2000.0
	Y	1650.0	1300.0	950.0	600.0	250.0
	P3 X	3218.7	3218.7	3218.7	3218.7	2958.5
	Y	1575.5	1225.5	875.5	525.5	204.0
	P4 X	12510.8	10637.6	8764.4	5913.8	3352.3
	Y	434.5	314.5	194.5	194.5	166.0
	P5 X	13729.5	11856.3	9983.1	7132.5	4310.8
	Y	360.0	240.0	120.0	120.0	120.0
P6 X	16016.0	18404.6	20793.3	24428.1	27685.2	
Y	360.0	240.0	120.0	120.0	120.0	
P7 X	16974.4	19363.1	21751.7	25386.6	28382.7	
Y	406.0	286.0	166.0	166.0	144.4	
P8 X	29893.5	29893.5	29893.5	29893.5	29893.5	
Y	1650.0	1300.0	950.0	600.0	250.0	
P9 X	-----	-----	-----	-----	-----	
Y	-----	-----	-----	-----	-----	
P10 X	-----	-----	-----	-----	-----	
Y	-----	-----	-----	-----	-----	
Angle	α (L)	0°0'0"	0°0'0"	0°0'0"	0°0'0"	0°0'0"
	(R)	5°30'0"	5°30'0"	5°30'0"	5°30'0"	4°0'0"
Radius (m)	R2 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (R)	10.000	10.000	10.000	10.000	10.000
	R2 (R)	-----	-----	-----	-----	-----
Angle	β (L)	7°0'0"	7°0'0"	7°0'0"	7°0'0"	5°30'0"
	(R)	-----	-----	-----	-----	-----
Length of PC Strand (m)	L1	1.800	1.800	1.800	1.800	1.800
	L2	1.222	1.222	1.222	1.222	0.960
	L3	9.362	7.475	5.587	2.715	0.396
	L4	1.222	1.222	1.222	1.222	0.960
	L5	2.287	6.548	10.810	17.296	23.374
	L6	0.960	0.960	0.960	0.960	0.698
	L7	12.979	10.579	8.179	4.528	1.514
	L8	-----	-----	-----	-----	-----
	L9	-----	-----	-----	-----	-----
	Total		29.831	29.805	29.780	29.742



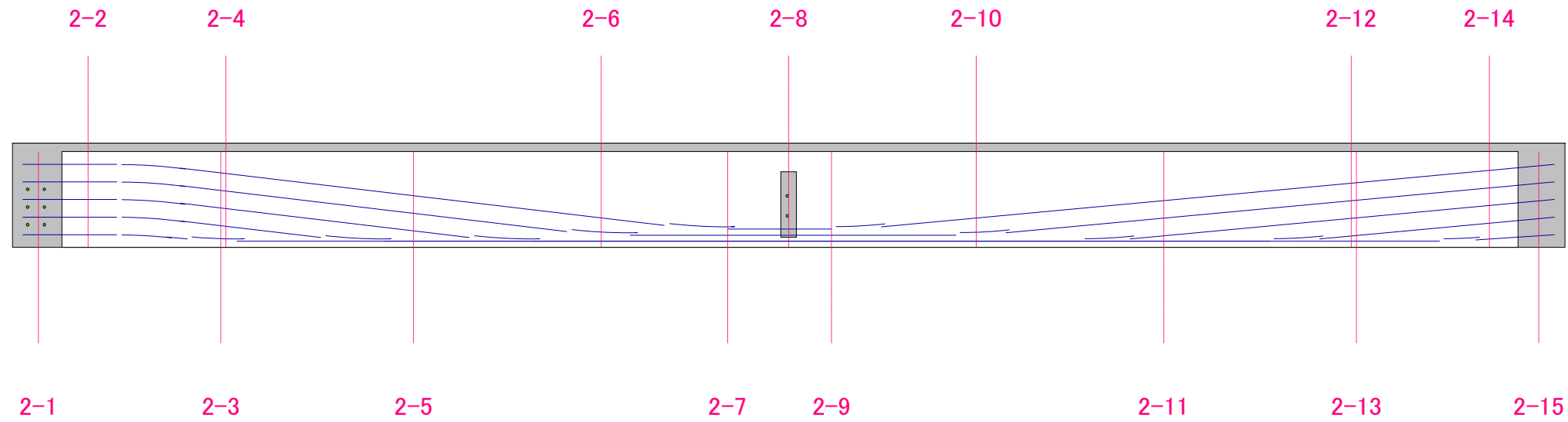
4.4 Summary for Calculation Results of Stress

1) PF5-PF6



		Unit	Allowable Value	Cross Section Number		
Calculation for Bending Moment				[1- 7]	[1- 8]	[1- 9]
				Bent up Point(Left)	Center of Span	Bent up Point(Right)
Bending Stress of Concrete						
Immediately After Prestressing	N/mm ²	-1.5 ~ 19.00	Top of Main Girder	0.79	0.83	0.81
			Bottom of Main Girder	15.05	14.95	14.89
During Deck Construction	"	-1.5 ~ 14.00	Top of Main Girder	6.35	6.42	6.34
			Bottom of Main Girder	7.02	6.88	6.91
Dead Load	"	≤ 10.00	Top of Deck	2.82	2.86	2.81
		0 ~ 14.00	Top of Main Girder	5.32	5.38	5.31
			Bottom of Main Girder	3.05	2.88	2.93
Design Load	"	≤ 10.00	Top of Deck max	4.37	4.38	4.27
			Top of Deck min	2.45	2.47	2.39
		-1.5 ~ 14.00	Top of Main Girder(max)	6.60	6.63	6.52
			Bottom of Main Girder(max)	-0.55	-0.65	-0.48
			Top of Main Girder(min)	5.02	5.06	4.96
		Bottom of Main Girder(min)	3.90	3.80	3.92	
Stress of PC Strand	N/mm ²	P _{max} ≤ 1110		1054	1051	1041
Ultimate Load	----	F ≥ 1.0		1.16	1.16	1.19
Calculation for Shear Force				[1- 2]	[1- 3]	[1- 14]
				Near a Support of girder(Left)	Change point of Web Width(Left)	Near a Support of girder(Right)
Shear Stress of Design Load	kN			0.55	1.28	1.05
Compressive Strength to Failure	----	F ≥ 1.0		3.85	1.81	3.01
Diagonal Tensile Stress	Dead Load	N/mm ²	≥ -1	-0.04	-0.11	-0.24
	Design Load	"	≥ -2	-0.17	-0.49	-0.44

2) PF6-PF7



		Unit	Allowable Value	Cross Section Number		
Calculation for Bending Moment				[2- 7]	[2- 8]	[2- 9]
				Bent up Point(Left)	Center of Span	Bent up Point(Right)
Bending Stress of Concrete						
Immediately After Prestressing	N/mm ²	-1.5 ~ 19.00	Top of Main Girder	0.83	0.86	0.82
			Bottom of Main Girder	14.86	14.91	15.03
During Deck Construction	"	-1.5 ~ 14.00	Top of Main Girder	6.38	6.47	6.40
			Bottom of Main Girder	6.85	6.82	6.96
Dead Load	"	≤ 10.00	Top of Deck	2.88	2.94	2.89
		0 ~ 14.00	Top of Main Girder	5.39	5.46	5.40
			Bottom of Main Girder	2.76	2.71	2.88
Design Load	"	≤ 10.00	Top of Deck max	4.35	4.46	4.44
			Top of Deck min	2.46	2.55	2.53
		-1.5 ~ 14.00	Top of Main Girder(max)	6.60	6.71	6.68
			Bottom of Main Girder(max)	-0.65	-0.83	-0.73
			Top of Main Girder(min)	5.04	5.14	5.10
		Bottom of Main Girder(min)	3.75	3.62	3.73	
Stress of PC Strand	N/mm ²	P _{max} ≤ 1110		1043	1053	1057
Ultimate Load	----	F ≥ 1.0		1.18	1.15	1.15
Calculation for Shear Force				[2- 2]	[2-13]	[2-14]
				Near a Support of girder(Left)	Change point of Web Width(Right)	Near a Support of girder(Right)
Shear Stress of Design Load	kN			1.06	1.30	0.56
Compressive Strength to Failure	----	F ≥ 1.0		2.98	1.80	3.82
Diagonal Tensile Stress	Dead Load	N/mm ²	≥ -1	-0.24	-0.12	-0.04
	Design Load	"	≥ -2	-0.45	-0.50	-0.17

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[1- 1]		[1- 2]		[1- 3]	
Interval from beginning of Girder		-----	0.500		1.450		4.000	
Immediately After Prestressing	Top of Main Girder	-1.5	2.971	○	2.773	○	3.788	
	Bottom of Main Girder	~19.00	5.077	○	6.014	○	11.151	
During Deck Construction	Top of Main Girder	-1.5	2.819	○	3.211	○	5.838	
	Bottom of Main Girder	~14.00	4.817	○	5.014	○	7.557	
Dead Load	Top of Deck	≤10.00	0.275	○	0.554	○	1.399	
	Top of Main Girder	0	2.120	○	2.490	○	4.339	
	Bottom of Main Girder	~14.00	4.786	○	4.681	○	5.852	
Design Load1	Top of Deck	Max	0.275	○	0.829	○	2.291	
		Min	≤10.00	0.275	○	0.529	○	1.304
	Top of Main Girder	Max	2.120	○	2.727	○	5.073	
		Min	-1.5	2.120	○	2.468	○	4.260
	Bottom of Main Girder	Max	~14.00	4.786	○	4.177	○	3.751
		Min		4.786	○	4.728	○	6.078
Design Load2 Temperature Rise	Top of Deck	Max	0.793	○	1.354	○	2.794	
		Min	≤11.50	0.793	○	1.054	○	1.806
	Top of Main Girder	Max	1.263	○	1.874	○	4.179	
		Min	-2	1.263	○	1.615	○	3.366
	Bottom of Main Girder	Max	~16.10	5.260	○	4.614	○	3.967
		Min		5.260	○	5.165	○	6.294
Design Load3 Temperature Drop	Top of Deck	Max	0.793	○	1.354	○	2.794	
		Min	≤11.50	0.793	○	1.054	○	1.806
	Top of Main Girder	Max	1.263	○	1.874	○	4.179	
		Min	-2	1.263	○	1.615	○	3.366
	Bottom of Main Girder	Max	~16.10	5.260	○	4.614	○	3.967
		Min		5.260	○	5.165	○	6.294
Design Load4 Support sinking	Top of Deck	Max	0.275	○	0.829	○	2.291	
		Min	≤10.00	0.275	○	0.529	○	1.304
	Top of Main Girder	Max	2.120	○	2.727	○	5.073	
		Min	-1.5	2.120	○	2.468	○	4.260
	Bottom of Main Girder	Max	~14.00	4.786	○	4.177	○	3.751
		Min		4.786	○	4.728	○	6.078
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	0.793	○	1.354	○	2.794	
		Min	≤11.50	0.793	○	1.054	○	1.806
	Top of Main Girder	Max	1.263	○	1.874	○	4.179	
		Min	-2	1.263	○	1.615	○	3.366
	Bottom of Main Girder	Max	~16.10	5.260	○	4.614	○	3.967
		Min		5.260	○	5.165	○	6.294
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	0.793	○	1.354	○	2.794	
		Min	≤11.50	0.793	○	1.054	○	1.806
	Top of Main Girder	Max	1.263	○	1.874	○	4.179	
		Min	-2	1.263	○	1.615	○	3.366
	Bottom of Main Girder	Max	~16.10	5.260	○	4.614	○	3.967
		Min		5.260	○	5.165	○	6.294

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1- 4]		[1- 5]		[1- 6]		
Interval from beginning of Girder		-----	4.127		7.755		11.382		
Immediately After Prestressing	Top of Main Girder	-1.5	3.726	○	2.202	○	1.011	○	
	Bottom of Main Girder	~19.00	11.236	○	13.445	○	15.034	○	
During Deck Construction	Top of Main Girder	-1.5	5.853	○	6.166	○	6.156	○	
	Bottom of Main Girder	~14.00	7.545	○	7.420	○	7.492	○	
Dead Load	Top of Deck	≤10.00	1.427	○	2.106	○	2.548	○	
	Top of Main Girder	0	4.362	○	4.884	○	5.089	○	
	Bottom of Main Girder	~14.00	5.795	○	4.572	○	3.850	○	
Design Load1	Top of Deck	Max	2.344	○	3.514	○	4.113	○	
		Min	1.328	○	1.909	○	2.254	○	
	Top of Main Girder	Max	5.116	○	6.045	○	6.379	○	
		Min	-1.5	4.280	○	4.722	○	4.846	○
	Bottom of Main Girder	Max	~14.00	3.635	○	1.276	○	0.203	○
		Min		6.028	○	5.033	○	4.534	○
Design Load2 Temperature Rise	Top of Deck	Max	2.850	○	4.096	○	4.769	○	
		Min	≤11.50	1.834	○	2.490	○	2.910	○
	Top of Main Girder	Max	4.225	○	5.216	○	5.612	○	
		Min	-2	3.389	○	3.893	○	4.079	○
	Bottom of Main Girder	Max	~16.10	3.845	○	1.309	○	0.063	○
		Min		6.238	○	5.067	○	4.394	○
Design Load3 Temperature Drop	Top of Deck	Max	2.850	○	4.096	○	4.769	○	
		Min	≤11.50	1.834	○	2.490	○	2.910	○
	Top of Main Girder	Max	4.225	○	5.216	○	5.612	○	
		Min	-2	3.389	○	3.893	○	4.079	○
	Bottom of Main Girder	Max	~16.10	3.845	○	1.309	○	0.063	○
		Min		6.238	○	5.067	○	4.394	○
Design Load4 Support sinking	Top of Deck	Max	2.344	○	3.514	○	4.113	○	
		Min	≤10.00	1.328	○	1.909	○	2.254	○
	Top of Main Girder	Max	5.116	○	6.045	○	6.379	○	
		Min	-1.5	4.280	○	4.722	○	4.846	○
	Bottom of Main Girder	Max	~14.00	3.635	○	1.276	○	0.203	○
		Min		6.028	○	5.033	○	4.534	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	2.850	○	4.096	○	4.769	○	
		Min	≤11.50	1.834	○	2.490	○	2.910	○
	Top of Main Girder	Max	4.225	○	5.216	○	5.612	○	
		Min	-2	3.389	○	3.893	○	4.079	○
	Bottom of Main Girder	Max	~16.10	3.845	○	1.309	○	0.063	○
		Min		6.238	○	5.067	○	4.394	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	2.850	○	4.096	○	4.769	○	
		Min	≤11.50	1.834	○	2.490	○	2.910	○
	Top of Main Girder	Max	4.225	○	5.216	○	5.612	○	
		Min	-2	3.389	○	3.893	○	4.079	○
	Bottom of Main Girder	Max	~16.10	3.845	○	1.309	○	0.063	○
		Min		6.238	○	5.067	○	4.394	○

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1- 7]		[1- 8]		[1- 9]		
Interval from beginning of Girder		-----	14.078		15.010		16.290		
Immediately After Prestressing	Top of Main Girder	-1.5	0.792	○	0.831	○	0.807	○	
	Bottom of Main Girder	~19.00	15.054	○	14.947	○	14.894	○	
During Deck Construction	Top of Main Girder	-1.5	6.354	○	6.422	○	6.336	○	
	Bottom of Main Girder	~14.00	7.017	○	6.884	○	6.909	○	
Dead Load	Top of Deck	≤10.00	2.820	○	2.861	○	2.811	○	
	Top of Main Girder	0	5.323	○	5.380	○	5.314	○	
	Bottom of Main Girder	~14.00	3.048	○	2.882	○	2.927	○	
Design Load1	Top of Deck	Max	4.365	○	4.377	○	4.274	○	
		Min	2.453	○	2.468	○	2.385	○	
	Top of Main Girder	Max	6.598	○	6.632	○	6.521	○	
		Min	-1.5	5.020	○	5.057	○	4.963	○
	Bottom of Main Girder	Max	~14.00	-0.547	○	-0.648	○	-0.478	○
		Min		3.903	○	3.795	○	3.918	○
Design Load2 Temperature Rise	Top of Deck	Max	5.077	○	5.109	○	5.032	○	
		Min	≤11.50	3.165	○	3.200	○	3.144	○
	Top of Main Girder	Max	5.877	○	5.927	○	5.838	○	
		Min	-2	4.299	○	4.352	○	4.280	○
	Bottom of Main Girder	Max	~16.10	-0.817	○	-0.962	○	-0.855	○
		Min		3.633	○	3.481	○	3.541	○
Design Load3 Temperature Drop	Top of Deck	Max	5.077	○	5.109	○	5.032	○	
		Min	≤11.50	3.165	○	3.200	○	3.144	○
	Top of Main Girder	Max	5.877	○	5.927	○	5.838	○	
		Min	-2	4.299	○	4.352	○	4.280	○
	Bottom of Main Girder	Max	~16.10	-0.817	○	-0.962	○	-0.855	○
		Min		3.633	○	3.481	○	3.541	○
Design Load4 Support sinking	Top of Deck	Max	4.365	○	4.377	○	4.274	○	
		Min	≤10.00	2.453	○	2.468	○	2.385	○
	Top of Main Girder	Max	6.598	○	6.632	○	6.521	○	
		Min	-1.5	5.020	○	5.057	○	4.963	○
	Bottom of Main Girder	Max	~14.00	-0.547	○	-0.648	○	-0.478	○
		Min		3.903	○	3.795	○	3.918	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	5.077	○	5.109	○	5.032	○	
		Min	≤11.50	3.165	○	3.200	○	3.144	○
	Top of Main Girder	Max	5.877	○	5.927	○	5.838	○	
		Min	-2	4.299	○	4.352	○	4.280	○
	Bottom of Main Girder	Max	~16.10	-0.817	○	-0.962	○	-0.855	○
		Min		3.633	○	3.481	○	3.541	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	5.077	○	5.109	○	5.032	○	
		Min	≤11.50	3.165	○	3.200	○	3.144	○
	Top of Main Girder	Max	5.877	○	5.927	○	5.838	○	
		Min	-2	4.299	○	4.352	○	4.280	○
	Bottom of Main Girder	Max	~16.10	-0.817	○	-0.962	○	-0.855	○
		Min		3.633	○	3.481	○	3.541	○

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1-10]		[1-11]		[1-12]		
Interval from beginning of Girder		-----	18.637		22.265		25.892		
Immediately After Prestressing	Top of Main Girder	-1.5	1.127	○	2.974	○	5.666	○	
	Bottom of Main Girder	~19.00	14.415	○	12.169	○	8.605	○	
During Deck Construction	Top of Main Girder	-1.5	6.254	○	6.866	○	7.653	○	
	Bottom of Main Girder	~14.00	6.945	○	6.306	○	5.168	○	
Dead Load	Top of Deck	≤10.00	2.609	○	2.305	○	1.862	○	
	Top of Main Girder	0	5.184	○	5.370	○	5.506	○	
	Bottom of Main Girder	~14.00	3.213	○	3.391	○	3.557	○	
Design Load1	Top of Deck	Max	3.919	○	3.217	○	2.231	○	
		Min	2.119	○	1.692	○	1.041	○	
	Top of Main Girder	Max	6.265	○	6.121	○	5.809	○	
		Min	-1.5	4.779	○	4.865	○	4.832	○
	Bottom of Main Girder	Max	~14.00	0.159	○	1.255	○	2.685	○
		Min		4.355	○	4.827	○	5.498	○
Design Load2 Temperature Rise	Top of Deck	Max	4.727	○	4.104	○	3.198	○	
		Min	≤11.50	2.927	○	2.580	○	2.009	○
	Top of Main Girder	Max	5.623	○	5.544	○	5.297	○	
		Min	-2	4.137	○	4.288	○	4.319	○
	Bottom of Main Girder	Max	~16.10	-0.334	○	0.571	○	1.801	○
		Min		3.862	○	4.143	○	4.614	○
Design Load3 Temperature Drop	Top of Deck	Max	4.727	○	4.104	○	3.198	○	
		Min	≤11.50	2.927	○	2.580	○	2.009	○
	Top of Main Girder	Max	5.623	○	5.544	○	5.297	○	
		Min	-2	4.137	○	4.288	○	4.319	○
	Bottom of Main Girder	Max	~16.10	-0.334	○	0.571	○	1.801	○
		Min		3.862	○	4.143	○	4.614	○
Design Load4 Support sinking	Top of Deck	Max	3.919	○	3.217	○	2.231	○	
		Min	≤10.00	2.119	○	1.692	○	1.041	○
	Top of Main Girder	Max	6.265	○	6.121	○	5.809	○	
		Min	-1.5	4.779	○	4.865	○	4.832	○
	Bottom of Main Girder	Max	~14.00	0.159	○	1.255	○	2.685	○
		Min		4.355	○	4.827	○	5.498	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	4.727	○	4.104	○	3.198	○	
		Min	≤11.50	2.927	○	2.580	○	2.009	○
	Top of Main Girder	Max	5.623	○	5.544	○	5.297	○	
		Min	-2	4.137	○	4.288	○	4.319	○
	Bottom of Main Girder	Max	~16.10	-0.334	○	0.571	○	1.801	○
		Min		3.862	○	4.143	○	4.614	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	4.727	○	4.104	○	3.198	○	
		Min	≤11.50	2.927	○	2.580	○	2.009	○
	Top of Main Girder	Max	5.623	○	5.544	○	5.297	○	
		Min	-2	4.137	○	4.288	○	4.319	○
	Bottom of Main Girder	Max	~16.10	-0.334	○	0.571	○	1.801	○
		Min		3.862	○	4.143	○	4.614	○

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1-13]		[1-14]		[1-15]		
Interval from beginning of Girder		-----	26.020		28.569		29.519		
Immediately After Prestressing	Top of Main Girder	-1.5	5.765	o	3.829	o	3.065	o	
	Bottom of Main Girder	~19.00	8.463	o	4.284	o	4.504	o	
During Deck Construction	Top of Main Girder	-1.5	7.673	o	4.191	o	2.884	o	
	Bottom of Main Girder	~14.00	5.125	o	3.406	o	4.299	o	
Dead Load	Top of Deck	≤10.00	1.842	o	0.894	o	0.431	o	
	Top of Main Girder	0	5.503	o	3.207	o	2.254	o	
	Bottom of Main Girder	~14.00	3.567	o	3.080	o	4.048	o	
Design Load1	Top of Deck	Max	2.195	o	0.976	o	0.438	o	
		Min	1.003	o	-0.444	o	-1.157	o	
	Top of Main Girder	Max	5.793	o	3.278	o	2.260	o	
		Min	-1.5	4.813	o	2.050	o	0.872	o
	Bottom of Main Girder	Max	~14.00	2.732	o	2.929	o	4.036	o
		Min		5.553	o	5.547	o	6.867	o
Design Load2 Temperature Rise	Top of Deck	Max	3.165	o	2.062	o	1.550	o	
		Min	≤11.50	1.973	o	0.643	o	-0.045	o
	Top of Main Girder	Max	5.283	o	2.910	o	1.920	o	
		Min	-2	4.303	o	1.682	o	0.532	o
	Bottom of Main Girder	Max	~16.10	1.841	o	2.331	o	3.458	o
		Min		4.662	o	4.949	o	6.289	o
Design Load3 Temperature Drop	Top of Deck	Max	3.165	o	2.062	o	1.550	o	
		Min	≤11.50	1.973	o	0.643	o	-0.045	o
	Top of Main Girder	Max	5.283	o	2.910	o	1.920	o	
		Min	-2	4.303	o	1.682	o	0.532	o
	Bottom of Main Girder	Max	~16.10	1.841	o	2.331	o	3.458	o
		Min		4.662	o	4.949	o	6.289	o
Design Load4 Support sinking	Top of Deck	Max	2.195	o	0.976	o	0.438	o	
		Min	≤10.00	1.003	o	-0.444	o	-1.157	o
	Top of Main Girder	Max	5.793	o	3.278	o	2.260	o	
		Min	-1.5	4.813	o	2.050	o	0.872	o
	Bottom of Main Girder	Max	~14.00	2.732	o	2.929	o	4.036	o
		Min		5.553	o	5.547	o	6.867	o
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	3.165	o	2.062	o	1.550	o	
		Min	≤11.50	1.973	o	0.643	o	-0.045	o
	Top of Main Girder	Max	5.283	o	2.910	o	1.920	o	
		Min	-2	4.303	o	1.682	o	0.532	o
	Bottom of Main Girder	Max	~16.10	1.841	o	2.331	o	3.458	o
		Min		4.662	o	4.949	o	6.289	o
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	3.165	o	2.062	o	1.550	o	
		Min	≤11.50	1.973	o	0.643	o	-0.045	o
	Top of Main Girder	Max	5.283	o	2.910	o	1.920	o	
		Min	-2	4.303	o	1.682	o	0.532	o
	Bottom of Main Girder	Max	~16.10	1.841	o	2.331	o	3.458	o
		Min		4.662	o	4.949	o	6.289	o

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 3

Cross Section NumberNo.	Unit	Allowable Value	[1- 1]		[1- 2]		[1- 3]	
Interval from beginning of Girder								
				0.500		1.450		4.000
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1163	○	1166	○	1173	○
Effective Prestressing Force (*1)	N/mm ²	1110	1103	○	1104	○	1090	○
Effective Prestressing Force (*2)	N/mm ²	1110	1031	○	1029	○	993	○
max	N/mm ²	1110	1031	○	1031	○	1011	○
Ultimate Load	-----	1	1000	○	6	○	2	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1- 4]		[1- 5]		[1- 6]	
Interval from beginning of Girder								
				4.127		7.755		11.382
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1174	○	1193	○	1196	○
Effective Prestressing Force (*1)	N/mm ²	1110	1090	○	1097	○	1091	○
Effective Prestressing Force (*2)	N/mm ²	1110	994	○	1008	○	1006	○
max	N/mm ²	1110	1012	○	1048	○	1064	○
Ultimate Load	-----	1	2	○	1	○	1	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1- 7]		[1- 8]		[1- 9]	
Interval from beginning of Girder								
				14.078		15.010		16.290
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1176	○	1172	○	1166	○
Effective Prestressing Force (*1)	N/mm ²	1110	1071	○	1068	○	1062	○
Effective Prestressing Force (*2)	N/mm ²	1110	991	○	988	○	981	○
max	N/mm ²	1110	1054	○	1051	○	1041	○
Ultimate Load	-----	1	1	○	1	○	1	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1-10]	[1-11]	[1-12]
Interval from beginning of Girder			18.637	22.265	25.892
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	1320	1320
Immediately After Prestressing	N/mm ²	1295	1162	1171	1159
Effective Prestressing Force (*1)	N/mm ²	1110	1060	1082	1082
Effective Prestressing Force (*2)	N/mm ²	1110	973	988	981
max	N/mm ²	1110	1024	1013	984
Ultimate Load	-----	1	1	2	2

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1-13]	[1-14]	[1-15]
Interval from beginning of Girder			26.020	28.569	29.519
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	1320	1320
Immediately After Prestressing	N/mm ²	1295	1157	1103	1099
Effective Prestressing Force (*1)	N/mm ²	1110	1081	1045	1043
Effective Prestressing Force (*2)	N/mm ²	1110	980	968	967
max	N/mm ²	1110	982	965	963
Ultimate Load	-----	1	2	3	2

*1:During DeckConstruction *2:Design Load

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[1- 1]	[1- 2]	[1- 3]	
Interval from beginning of Girder			-----	0.500	1.450	4.000	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.55 Δ 1.28 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.03 ○ -0.11 ○	
	Neutral Axis before Composition			-----	--	-0.04 ○ -0.10 ○	
	Neutral Axis after Composition			-----	--	-0.04 ○ -0.11 ○	
	Base of Lower Flange			-----	--	-0.01 ○ -0.06 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.14 ○ -0.46 ○	
				Min	-----	--	-0.03 ○ -0.09 ○
	Neutral Axis before Composition			Max	-----	--	-0.15 ○ -0.47 ○
				Min	-----	--	-0.03 ○ -0.09 ○
	Neutral Axis after Composition			Max	-----	--	-0.17 ○ -0.49 ○
				Min	-----	--	-0.04 ○ -0.09 ○
	Base of Lower Flange			Max	-----	--	-0.02 ○ -0.33 ○
				Min	-----	--	0.00 ○ -0.05 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 -- 23.25 --	
	D16	cm	-----	-----	--	31.62 -- 36.45 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	-----	--	0.19 -- 9.53 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	-----	--	3.85 ○ 1.81 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	--	1.402 ○ 1.00 ○	
	D16			-----	--	1.402 ○ 1.00 ○	
	D19			-----	--	1.459 ○ 1.14 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.55 Δ 1.28 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.03 ○ -0.11 ○	
	Neutral Axis before Composition			-----	--	-0.04 ○ -0.10 ○	
	Neutral Axis after Composition			-----	--	-0.04 ○ -0.11 ○	
	Base of Lower Flange			-----	--	-0.01 ○ -0.06 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.14 ○ -0.46 ○	
				Min	-----	--	-0.03 ○ -0.09 ○
	Neutral Axis before Composition			Max	-----	--	-0.15 ○ -0.47 ○
				Min	-----	--	-0.03 ○ -0.09 ○
	Neutral Axis after Composition			Max	-----	--	-0.17 ○ -0.49 ○
				Min	-----	--	-0.04 ○ -0.09 ○
	Base of Lower Flange			Max	-----	--	-0.02 ○ -0.33 ○
				Min	-----	--	0.00 ○ -0.05 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 -- 23.25 --	
	D16	cm	-----	-----	--	31.62 -- 36.45 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	-----	--	0.00 -- 0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[1- 4]	[1- 5]	[1- 6]				
Interval from beginning of Girder			-----	4.127	7.755	11.382				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.26	Δ	0.87	Δ	0.68	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.10	○	-0.04	○	-0.02	○	
	Neutral Axis before Composition			-0.10	○	-0.04	○	-0.03	○	
	Neutral Axis after Composition			-0.11	○	-0.04	○	-0.03	○	
	Base of Lower Flange			-0.06	○	-0.02	○	-0.02	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.44	○	-0.21	○	-0.12	○
				Min	-0.08	○	-0.01	○	0.00	○
	Neutral Axis before Composition			Max	-0.46	○	-0.25	○	-0.17	○
				Min	-0.08	○	-0.01	○	0.00	○
	Neutral Axis after Composition			Max	-0.47	○	-0.23	○	-0.15	○
				Min	-0.09	○	-0.01	○	0.00	○
	Base of Lower Flange			Max	-0.33	○	-0.24	○	-0.21	○
				Min	-0.05	○	-0.01	○	0.00	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	23.76	--	40.00	--	40.00	--	
	D16	cm	-----	37.24	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	9.33	--	5.14	--	2.03	--		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	1.84	○	2.48	○	3.64	○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.00	○	1.026	○	1.36	○	
	D16			1.00	○	1.231	○	1.68	○	
	D19			1.15	○	1.482	○	2.07	○	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.26	Δ	0.87	Δ	0.68	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.10	○	-0.04	○	-0.02	○	
	Neutral Axis before Composition			-0.10	○	-0.04	○	-0.03	○	
	Neutral Axis after Composition			-0.11	○	-0.04	○	-0.03	○	
	Base of Lower Flange			-0.06	○	-0.02	○	-0.02	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.44	○	-0.21	○	-0.12	○
				Min	-0.08	○	-0.01	○	0.00	○
	Neutral Axis before Composition			Max	-0.46	○	-0.25	○	-0.17	○
				Min	-0.08	○	-0.01	○	0.00	○
	Neutral Axis after Composition			Max	-0.47	○	-0.23	○	-0.15	○
				Min	-0.09	○	-0.01	○	0.00	○
	Base of Lower Flange			Max	-0.33	○	-0.24	○	-0.21	○
				Min	-0.05	○	-0.01	○	0.00	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	23.76	--	40.00	--	40.00	--	
	D16	cm	-----	37.24	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	0.00	--	0.00	--	0.00	--		

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[1- 7]	[1- 8]	[1- 9]	
Interval from beginning of Girder			-----	14.078	15.010	16.290	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.59 Δ	0.45 ○	0.69 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.02 ○	-0.01 ○	-0.02 ○	
	Neutral Axis before Composition			-0.02 ○	-0.01 ○	-0.03 ○	
	Neutral Axis after Composition			-0.02 ○	-0.01 ○	-0.03 ○	
	Base of Lower Flange			-0.02 ○	-0.01 ○	-0.02 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.09 ○	-0.05 ○	-0.01 ○
				Min	-0.02 ○	-0.04 ○	-0.14 ○
	Neutral Axis before Composition			Max	-0.12 ○	-0.08 ○	-0.01 ○
				Min	-0.01 ○	-0.04 ○	-0.14 ○
	Neutral Axis after Composition			Max	-0.11 ○	-0.07 ○	-0.01 ○
				Min	-0.02 ○	-0.05 ○	-0.15 ○
	Base of Lower Flange			Max	-0.13 ○	-0.14 ○	-0.01 ○
				Min	-0.01 ○	-0.03 ○	-0.10 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	1.28 --	2.82 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	5.00 ○	4.08 ○	3.44 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.742 ○	----- --	1.28 ○	
	D16			2.205 ○	----- --	1.60 ○	
	D19			2.77 ○	----- --	1.98 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.59 Δ	0.45 ○	0.69 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.02 ○	-0.01 ○	-0.02 ○	
	Neutral Axis before Composition			-0.02 ○	-0.01 ○	-0.03 ○	
	Neutral Axis after Composition			-0.02 ○	-0.01 ○	-0.03 ○	
	Base of Lower Flange			-0.02 ○	-0.01 ○	-0.02 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.09 ○	-0.05 ○	-0.01 ○
				Min	-0.02 ○	-0.04 ○	-0.14 ○
	Neutral Axis before Composition			Max	-0.12 ○	-0.08 ○	-0.01 ○
				Min	-0.01 ○	-0.04 ○	-0.14 ○
	Neutral Axis after Composition			Max	-0.11 ○	-0.07 ○	-0.01 ○
				Min	-0.02 ○	-0.05 ○	-0.15 ○
	Base of Lower Flange			Max	-0.13 ○	-0.14 ○	-0.01 ○
				Min	-0.01 ○	-0.03 ○	-0.10 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[1-10]	[1-11]	[1-12]				
Interval from beginning of Girder			-----	18.637	22.265	25.892				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.65	Δ	0.76	Δ	1.04	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.01	○	-0.01	○	-0.03	○	
	Neutral Axis before Composition			-0.01	○	-0.01	○	-0.02	○	
	Neutral Axis after Composition			-0.01	○	-0.01	○	-0.03	○	
	Base of Lower Flange			-0.01	○	-0.01	○	-0.02	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.13	○	-0.19	○	-0.32	○
	Neutral Axis before Composition			Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.12	○	-0.16	○	-0.28	○
	Neutral Axis after Composition			Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.14	○	-0.19	○	-0.32	○
	Base of Lower Flange			Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.08	○	-0.10	○	-0.17	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	33.24	--	20.87	--	
	D16	cm	-----	40.00	--	40.00	--	32.71	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	3.83	--	6.67	--	10.62	--		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	2.75	○	2.08	○	1.66	○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.13	○	1	○	1.00	○	
	D16			1.368	○	1.107	○	1.00	○	
	D19			1.659	○	1.312	○	1.08	○	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.65	Δ	0.76	Δ	1.04	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.01	○	-0.01	○	-0.03	○	
	Neutral Axis before Composition			-0.01	○	-0.01	○	-0.02	○	
	Neutral Axis after Composition			-0.01	○	-0.01	○	-0.03	○	
	Base of Lower Flange			-0.01	○	-0.01	○	-0.02	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.13	○	-0.19	○	-0.32	○
	Neutral Axis before Composition			Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.12	○	-0.16	○	-0.28	○
	Neutral Axis after Composition			Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.14	○	-0.19	○	-0.32	○
	Base of Lower Flange			Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.08	○	-0.10	○	-0.17	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	33.24	--	20.87	--	
	D16	cm	-----	40.00	--	40.00	--	32.71	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	0.00	--	0.00	--	0.00	--		

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[1-13]	[1-14]	[1-15]				
Interval from beginning of Girder			-----	26.020	28.569	29.519				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.03	Δ	1.05	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.02	○	-0.12	○	-----	--	
	Neutral Axis before Composition			-0.02	○	-0.24	○	-----	--	
	Neutral Axis after Composition			-0.03	○	-0.22	○	-----	--	
	Base of Lower Flange			-0.02	○	-0.05	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.01	○	-0.11	○	-----	--
				Min	-0.32	○	-0.35	○	-----	--
	Neutral Axis before Composition			Max	-0.01	○	-0.22	○	-----	--
				Min	-0.28	○	-0.41	○	-----	--
	Neutral Axis after Composition			Max	-0.01	○	-0.20	○	-----	--
				Min	-0.32	○	-0.44	○	-----	--
	Base of Lower Flange			Max	-0.01	○	-0.04	○	-----	--
				Min	-0.16	○	-0.06	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	20.76	--	18.26	--	-----	--	
	D16	cm	-----	32.54	--	28.63	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume	cm ²	-----	10.68	--	11.11	--	-----	--		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	1.65	○	3.01	○	-----	--		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1	○	1	○	-----	--	
	D16			1	○	1	○	-----	--	
	D19			1.075	○	1.012	○	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.03	Δ	1.05	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.02	○	-0.12	○	-----	--	
	Neutral Axis before Composition			-0.02	○	-0.24	○	-----	--	
	Neutral Axis after Composition			-0.03	○	-0.22	○	-----	--	
	Base of Lower Flange			-0.02	○	-0.05	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.01	○	-0.11	○	-----	--
				Min	-0.32	○	-0.35	○	-----	--
	Neutral Axis before Composition			Max	-0.01	○	-0.22	○	-----	--
				Min	-0.28	○	-0.41	○	-----	--
	Neutral Axis after Composition			Max	-0.01	○	-0.20	○	-----	--
				Min	-0.32	○	-0.44	○	-----	--
	Base of Lower Flange			Max	-0.01	○	-0.04	○	-----	--
				Min	-0.16	○	-0.06	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	20.76	--	18.26	--	-----	--	
	D16	cm	-----	32.54	--	28.63	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume	cm ²	-----	0.00	--	0.00	--	-----	--		

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1- 1]	[1- 2]	[1- 3]	
Interval from beginning of Girder			-----	0.500	1.450	4.000	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.47 ○ 1.11 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.03 ○ -0.08 ○	
	Neutral Axis before Composition			-----	--	-0.03 ○ -0.07 ○	
	Neutral Axis after Composition			-----	--	-0.03 ○ -0.08 ○	
	Base of Lower Flange			-----	--	0.00 ○ -0.04 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.11 ○ -0.39 ○	
				Min	-----	--	-0.03 ○ -0.08 ○
	Neutral Axis before Composition			Max	-----	--	-0.11 ○ -0.36 ○
				Min	-----	--	-0.03 ○ -0.06 ○
	Neutral Axis after Composition			Max	-----	--	-0.12 ○ -0.40 ○
				Min	-----	--	-0.03 ○ -0.07 ○
	Base of Lower Flange			Max	-----	--	-0.01 ○ -0.23 ○
				Min	-----	--	0.00 ○ -0.03 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 -- 30.08 --	
	D16	cm	-----	-----	--	31.62 -- 40.00 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 -- 7.37 --	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.47 ○ 1.11 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.03 ○ -0.08 ○	
	Neutral Axis before Composition			-----	--	-0.03 ○ -0.07 ○	
	Neutral Axis after Composition			-----	--	-0.03 ○ -0.08 ○	
	Base of Lower Flange			-----	--	0.00 ○ -0.04 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.11 ○ -0.39 ○	
				Min	-----	--	-0.03 ○ -0.08 ○
	Neutral Axis before Composition			Max	-----	--	-0.11 ○ -0.36 ○
				Min	-----	--	-0.03 ○ -0.06 ○
	Neutral Axis after Composition			Max	-----	--	-0.12 ○ -0.40 ○
				Min	-----	--	-0.03 ○ -0.07 ○
	Base of Lower Flange			Max	-----	--	-0.01 ○ -0.23 ○
				Min	-----	--	0.00 ○ -0.03 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 -- 30.08 --	
	D16	cm	-----	-----	--	31.62 -- 40.00 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 -- 0.00 --	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	-----	--	999.999 ○ 999.999 ○	
Strength against Diagonal Densile Failure(Mus/Mtu)	D13	-----	1.00	-----	--	----- - 999.999 ○	
	D16			-----	--	----- - 999.999 ○	
	D19			-----	--	----- - 999.999 ○	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1- 4]	[1- 5]	[1- 6]				
Interval from beginning of Girder			-----	4.045	7.591	11.136				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.11	Δ	0.69	Δ	0.45	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.08	○	-0.02	○	0.00	○	
	Neutral Axis before Composition			-0.06	○	-0.02	○	0.00	○	
	Neutral Axis after Composition			-0.08	○	-0.02	○	0.00	○	
	Base of Lower Flange			-0.04	○	-0.01	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.38	○	-0.15	○	-0.06	○
				Min	-0.07	○	-0.02	○	0.00	○
	Neutral Axis before Composition			Max	-0.36	○	-0.15	○	-0.07	○
				Min	-0.06	○	-0.02	○	0.00	○
	Neutral Axis after Composition			Max	-0.40	○	-0.16	○	-0.07	○
				Min	-0.07	○	-0.02	○	0.00	○
	Base of Lower Flange			Max	-0.23	○	-0.12	○	-0.07	○
				Min	-0.03	○	-0.01	○	0.00	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	30.40	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	7.29	--	2.63	--	0.00	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.11	Δ	0.69	Δ	0.45	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.08	○	-0.02	○	0.00	○	
	Neutral Axis before Composition			-0.06	○	-0.02	○	0.00	○	
	Neutral Axis after Composition			-0.08	○	-0.02	○	0.00	○	
	Base of Lower Flange			-0.04	○	-0.01	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.38	○	-0.15	○	-0.06	○
				Min	-0.07	○	-0.02	○	0.00	○
	Neutral Axis before Composition			Max	-0.36	○	-0.15	○	-0.07	○
				Min	-0.06	○	-0.02	○	0.00	○
	Neutral Axis after Composition			Max	-0.40	○	-0.16	○	-0.07	○
				Min	-0.07	○	-0.02	○	0.00	○
	Base of Lower Flange			Max	-0.23	○	-0.12	○	-0.07	○
				Min	-0.03	○	-0.01	○	0.00	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	30.40	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	-	
	D16			999.999	○	999.999	○	-----	-	
	D19			999.999	○	999.999	○	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1- 7]	[1- 8]	[1- 9]				
Interval from beginning of Girder			-----	14.078	14.681	15.634				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.12	○	0.03	○	0.27	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	-0.02	○
	Neutral Axis before Composition	Max		-0.01	○	0.00	○	0.00	○	
		Min		0.00	○	0.00	○	-0.03	○	
	Neutral Axis after Composition	Max		-0.01	○	0.00	○	0.00	○	
		Min		0.00	○	0.00	○	-0.02	○	
	Base of Lower Flange	Max		0.00	○	0.00	○	0.00	○	
		Min		0.00	○	0.00	○	-0.04	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.12	○	0.03	○	0.27	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	-0.02	○
	Neutral Axis before Composition	Max		-0.01	○	0.00	○	0.00	○	
		Min		0.00	○	0.00	○	-0.03	○	
	Neutral Axis after Composition	Max		-0.01	○	0.00	○	0.00	○	
		Min		0.00	○	0.00	○	-0.02	○	
	Base of Lower Flange	Max		0.00	○	0.00	○	0.00	○	
		Min		0.00	○	0.00	○	-0.04	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	-----	-	-----	-	
	D16	-----	1.00	-----	-	-----	-	-----	-	
	D19	-----	1.00	-----	-	-----	-	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1-10]	[1-11]	[1-12]				
Interval from beginning of Girder			-----	18.227	21.772	25.317				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.37	○	0.48	○	0.82	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			-0.01	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.01	○	0.00	○	0.00	○
				Min	-0.05	○	-0.08	○	-0.22	○
	Neutral Axis before Composition			Max	-0.01	○	0.00	○	0.00	○
				Min	-0.05	○	-0.07	○	-0.21	○
	Neutral Axis after Composition			Max	-0.01	○	0.00	○	0.00	○
				Min	-0.05	○	-0.08	○	-0.23	○
	Base of Lower Flange			Max	-0.01	○	0.00	○	0.00	○
				Min	-0.05	○	-0.06	○	-0.14	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	26.18	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	1.25	--	3.78	--	8.47	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.37	○	0.48	○	0.82	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			-0.01	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.01	○	0.00	○	0.00	○
				Min	-0.05	○	-0.08	○	-0.22	○
	Neutral Axis before Composition			Max	-0.01	○	0.00	○	0.00	○
				Min	-0.05	○	-0.07	○	-0.21	○
	Neutral Axis after Composition			Max	-0.01	○	0.00	○	0.00	○
				Min	-0.05	○	-0.08	○	-0.23	○
	Base of Lower Flange			Max	-0.01	○	0.00	○	0.00	○
				Min	-0.05	○	-0.06	○	-0.14	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	26.18	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	-----	-	999.999	○	
	D16			-----	-	-----	-	999.999	○	
	D19			-----	-	-----	-	999.999	○	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1-13]	[1-14]	[1-15]				
Interval from beginning of Girder			-----	25.363	27.913	28.863				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.79	Δ	0.95	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	-0.10	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.20	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.18	○	-----	--	
	Base of Lower Flange			0.00	○	-0.05	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	-0.09	○	-----	--
				Min	-0.21	○	-0.28	○	-----	--
	Neutral Axis before Composition			Max	0.00	○	-0.18	○	-----	--
				Min	-0.19	○	-0.37	○	-----	--
	Neutral Axis after Composition			Max	0.00	○	-0.16	○	-----	--
				Min	-0.21	○	-0.38	○	-----	--
	Base of Lower Flange			Max	0.00	○	-0.04	○	-----	--
				Min	-0.13	○	-0.06	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	27.03	--	20.18	--	-----	--	
	D16	cm	-----	40.00	--	31.63	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	8.20	--	8.69	--	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.79	Δ	0.95	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	-0.10	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.20	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.18	○	-----	--	
	Base of Lower Flange			0.00	○	-0.05	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	-0.09	○	-----	--
				Min	-0.21	○	-0.28	○	-----	--
	Neutral Axis before Composition			Max	0.00	○	-0.18	○	-----	--
				Min	-0.19	○	-0.37	○	-----	--
	Neutral Axis after Composition			Max	0.00	○	-0.16	○	-----	--
				Min	-0.21	○	-0.38	○	-----	--
	Base of Lower Flange			Max	0.00	○	-0.04	○	-----	--
				Min	-0.13	○	-0.06	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	27.03	--	20.18	--	-----	--	
	D16	cm	-----	40.00	--	31.63	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	-----	--	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	--	
	D16			999.999	○	999.999	○	-----	--	
	D19			999.999	○	999.999	○	-----	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[2-1]		[2-2]		[2-3]		
Interval from beginning of Girder		-----	0.501		1.451		4.000		
Immediately After Prestressing	Top of Main Girder	-1.5	3.066	○	3.831	○	5.771	○	
	Bottom of Main Girder	~19.00	4.503	○	4.282	○	8.455	○	
During Deck Construction	Top of Main Girder	-1.5	2.886	○	4.195	○	7.686	○	
	Bottom of Main Girder	~14.00	4.297	○	3.402	○	5.109	○	
Dead Load	Top of Deck	≤10.00	0.424	○	0.894	○	1.861	○	
	Top of Main Girder	0	2.248	○	3.209	○	5.525	○	
	Bottom of Main Girder	~14.00	4.061	○	3.078	○	3.516	○	
Design Load1	Top of Deck	Max	0.431	○	0.976	○	2.213	○	
		Min	≤10.00	-1.165	○	-0.445	○	1.022	○
	Top of Main Girder	Max	-1.5	2.254	○	3.279	○	5.814	○
		Min	~14.00	0.865	○	2.051	○	4.835	○
	Bottom of Main Girder	Max	~14.00	4.048	○	2.928	○	2.684	○
		Min	~14.00	6.881	○	5.547	○	5.503	○
Design Load2 Temperature Rise	Top of Deck	Max	≤11.50	1.543	○	2.062	○	3.184	○
		Min	~16.10	-0.053	○	0.642	○	1.992	○
	Top of Main Girder	Max	-2	1.914	○	2.911	○	5.304	○
		Min	~16.10	0.525	○	1.683	○	4.325	○
	Bottom of Main Girder	Max	~16.10	3.470	○	2.329	○	1.793	○
		Min	~16.10	6.303	○	4.949	○	4.611	○
Design Load3 Temperature Drop	Top of Deck	Max	≤11.50	1.543	○	2.062	○	3.184	○
		Min	~16.10	-0.053	○	0.642	○	1.992	○
	Top of Main Girder	Max	-2	1.914	○	2.911	○	5.304	○
		Min	~16.10	0.525	○	1.683	○	4.325	○
	Bottom of Main Girder	Max	~16.10	3.470	○	2.329	○	1.793	○
		Min	~16.10	6.303	○	4.949	○	4.611	○
Design Load4 Support sinking	Top of Deck	Max	≤10.00	0.431	○	0.976	○	2.213	○
		Min	~14.00	-1.165	○	-0.445	○	1.022	○
	Top of Main Girder	Max	-1.5	2.254	○	3.279	○	5.814	○
		Min	~14.00	0.865	○	2.051	○	4.835	○
	Bottom of Main Girder	Max	~14.00	4.048	○	2.928	○	2.684	○
		Min	~14.00	6.881	○	5.547	○	5.503	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	≤11.50	1.543	○	2.062	○	3.184	○
		Min	~16.10	-0.053	○	0.642	○	1.992	○
	Top of Main Girder	Max	-2	1.914	○	2.911	○	5.304	○
		Min	~16.10	0.525	○	1.683	○	4.325	○
	Bottom of Main Girder	Max	~16.10	3.470	○	2.329	○	1.793	○
		Min	~16.10	6.303	○	4.949	○	4.611	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	≤11.50	1.543	○	2.062	○	3.184	○
		Min	~16.10	-0.053	○	0.642	○	1.992	○
	Top of Main Girder	Max	-2	1.914	○	2.911	○	5.304	○
		Min	~16.10	0.525	○	1.683	○	4.325	○
	Bottom of Main Girder	Max	~16.10	3.470	○	2.329	○	1.793	○
		Min	~16.10	6.303	○	4.949	○	4.611	○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[2- 4]		[2- 5]		[2- 6]		
Interval from beginning of Girder		-----	4.137		7.774		11.410		
Immediately After Prestressing	Top of Main Girder	-1.5	5.666	○	2.975	○	1.139	○	
	Bottom of Main Girder	~19.00	8.607	○	12.169	○	14.395	○	
During Deck Construction	Top of Main Girder	-1.5	7.665	○	6.888	○	6.291	○	
	Bottom of Main Girder	~14.00	5.155	○	6.280	○	6.896	○	
Dead Load	Top of Deck	≤10.00	1.884	○	2.351	○	2.674	○	
	Top of Main Girder	0	5.529	○	5.415	○	5.247	○	
	Bottom of Main Girder	~14.00	3.503	○	3.285	○	3.065	○	
Design Load1	Top of Deck	Max	2.252	○	3.263	○	3.986	○	
		Min	1.064	○	1.741	○	2.186	○	
	Top of Main Girder	Max	5.832	○	6.167	○	6.330	○	
		Min	-1.5	4.856	○	4.913	○	4.845	○
	Bottom of Main Girder	Max	~14.00	2.631	○	1.148	○	0.007	○
		Min		5.441	○	4.714	○	4.201	○
Design Load2 Temperature Rise	Top of Deck	Max	3.220	○	4.150	○	4.794	○	
		Min	≤11.50	2.032	○	2.629	○	2.994	○
	Top of Main Girder	Max	5.320	○	5.589	○	5.688	○	
		Min	-2	4.344	○	4.336	○	4.203	○
	Bottom of Main Girder	Max	~16.10	1.747	○	0.463	○	-0.487	○
		Min		4.557	○	4.030	○	3.708	○
Design Load3 Temperature Drop	Top of Deck	Max	3.220	○	4.150	○	4.794	○	
		Min	≤11.50	2.032	○	2.629	○	2.994	○
	Top of Main Girder	Max	5.320	○	5.589	○	5.688	○	
		Min	-2	4.344	○	4.336	○	4.203	○
	Bottom of Main Girder	Max	~16.10	1.747	○	0.463	○	-0.487	○
		Min		4.557	○	4.030	○	3.708	○
Design Load4 Support sinking	Top of Deck	Max	2.252	○	3.263	○	3.986	○	
		Min	≤10.00	1.064	○	1.741	○	2.186	○
	Top of Main Girder	Max	5.832	○	6.167	○	6.330	○	
		Min	-1.5	4.856	○	4.913	○	4.845	○
	Bottom of Main Girder	Max	~14.00	2.631	○	1.148	○	0.007	○
		Min		5.441	○	4.714	○	4.201	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	3.220	○	4.150	○	4.794	○	
		Min	≤11.50	2.032	○	2.629	○	2.994	○
	Top of Main Girder	Max	5.320	○	5.589	○	5.688	○	
		Min	-2	4.344	○	4.336	○	4.203	○
	Bottom of Main Girder	Max	~16.10	1.747	○	0.463	○	-0.487	○
		Min		4.557	○	4.030	○	3.708	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	3.220	○	4.150	○	4.794	○	
		Min	≤11.50	2.032	○	2.629	○	2.994	○
	Top of Main Girder	Max	5.320	○	5.589	○	5.688	○	
		Min	-2	4.344	○	4.336	○	4.203	○
	Bottom of Main Girder	Max	~16.10	1.747	○	0.463	○	-0.487	○
		Min		4.557	○	4.030	○	3.708	○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[2- 7]		[2- 8]		[2- 9]		
Interval from beginning of Girder		-----	13.730		15.047		16.016		
Immediately After Prestressing	Top of Main Girder	-1.5	0.831	○	0.856	○	0.815	○	
	Bottom of Main Girder	~19.00	14.860	○	14.914	○	15.026	○	
During Deck Construction	Top of Main Girder	-1.5	6.382	○	6.473	○	6.401	○	
	Bottom of Main Girder	~14.00	6.851	○	6.822	○	6.963	○	
Dead Load	Top of Deck	≤10.00	2.883	○	2.938	○	2.894	○	
	Top of Main Girder	0	5.387	○	5.459	○	5.397	○	
	Bottom of Main Girder	~14.00	2.761	○	2.707	○	2.884	○	
Design Load1	Top of Deck	Max	4.349	○	4.459	○	4.444	○	
		Min	2.459	○	2.547	○	2.529	○	
	Top of Main Girder	Max	6.596	○	6.714	○	6.676	○	
		Min	-1.5	5.036	○	5.136	○	5.096	○
	Bottom of Main Girder	Max	~14.00	-0.649	○	-0.834	○	-0.725	○
		Min		3.750	○	3.617	○	3.733	○
Design Load2 Temperature Rise	Top of Deck	Max	5.108	○	5.191	○	5.156	○	
		Min	≤11.50	3.218	○	3.279	○	3.241	○
	Top of Main Girder	Max	5.914	○	6.009	○	5.954	○	
		Min	-2	4.354	○	4.431	○	4.374	○
	Bottom of Main Girder	Max	~16.10	-1.028	○	-1.149	○	-0.993	○
		Min		3.372	○	3.302	○	3.465	○
Design Load3 Temperature Drop	Top of Deck	Max	5.108	○	5.191	○	5.156	○	
		Min	≤11.50	3.218	○	3.279	○	3.241	○
	Top of Main Girder	Max	5.914	○	6.009	○	5.954	○	
		Min	-2	4.354	○	4.431	○	4.374	○
	Bottom of Main Girder	Max	~16.10	-1.028	○	-1.149	○	-0.993	○
		Min		3.372	○	3.302	○	3.465	○
Design Load4 Support sinking	Top of Deck	Max	4.349	○	4.459	○	4.444	○	
		Min	≤10.00	2.459	○	2.547	○	2.529	○
	Top of Main Girder	Max	6.596	○	6.714	○	6.676	○	
		Min	-1.5	5.036	○	5.136	○	5.096	○
	Bottom of Main Girder	Max	~14.00	-0.649	○	-0.834	○	-0.725	○
		Min		3.750	○	3.617	○	3.733	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	5.108	○	5.191	○	5.156	○	
		Min	≤11.50	3.218	○	3.279	○	3.241	○
	Top of Main Girder	Max	5.914	○	6.009	○	5.954	○	
		Min	-2	4.354	○	4.431	○	4.374	○
	Bottom of Main Girder	Max	~16.10	-1.028	○	-1.149	○	-0.993	○
		Min		3.372	○	3.302	○	3.465	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	5.108	○	5.191	○	5.156	○	
		Min	≤11.50	3.218	○	3.279	○	3.241	○
	Top of Main Girder	Max	5.914	○	6.009	○	5.954	○	
		Min	-2	4.354	○	4.431	○	4.374	○
	Bottom of Main Girder	Max	~16.10	-1.028	○	-1.149	○	-0.993	○
		Min		3.372	○	3.302	○	3.465	○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[2-10]		[2-11]		[2-12]	
Interval from beginning of Girder		-----	18.684		22.320		25.957	
Immediately After Prestressing	Top of Main Girder	-1.5	1.025	○	2.206	○	3.728	
	Bottom of Main Girder	~19.00	15.013	○	13.441	○	11.235	
During Deck Construction	Top of Main Girder	-1.5	6.196	○	6.191	○	5.866	
	Bottom of Main Girder	~14.00	7.442	○	7.391	○	7.530	
Dead Load	Top of Deck	≤10.00	2.616	○	2.157	○	1.456	
	Top of Main Girder	0	5.155	○	4.934	○	4.391	
	Bottom of Main Girder	~14.00	3.696	○	4.456	○	5.726	
Design Load1	Top of Deck	Max	4.184	○	3.569	○	2.376	
		Min	2.323	○	1.961	○	1.357	
	Top of Main Girder	Max	6.449	○	6.098	○	5.148	
		Min	-1.5	4.914	○	4.772	○	4.310
	Bottom of Main Girder	Max	~14.00	0.042	○	1.152	○	3.559
		Min		4.378	○	4.915	○	5.959
Design Load2 Temperature Rise	Top of Deck	Max	4.840	○	4.150	○	2.882	
		Min	≤11.50	2.979	○	2.542	○	1.863
	Top of Main Girder	Max	5.682	○	5.268	○	4.256	
		Min	-2	4.147	○	3.943	○	3.418
	Bottom of Main Girder	Max	~16.10	-0.098	○	1.185	○	3.768
		Min		4.238	○	4.949	○	6.168
Design Load3 Temperature Drop	Top of Deck	Max	4.840	○	4.150	○	2.882	
		Min	≤11.50	2.979	○	2.542	○	1.863
	Top of Main Girder	Max	5.682	○	5.268	○	4.256	
		Min	-2	4.147	○	3.943	○	3.418
	Bottom of Main Girder	Max	~16.10	-0.098	○	1.185	○	3.768
		Min		4.238	○	4.949	○	6.168
Design Load4 Support sinking	Top of Deck	Max	4.184	○	3.569	○	2.376	
		Min	≤10.00	2.323	○	1.961	○	1.357
	Top of Main Girder	Max	6.449	○	6.098	○	5.148	
		Min	-1.5	4.914	○	4.772	○	4.310
	Bottom of Main Girder	Max	~14.00	0.042	○	1.152	○	3.559
		Min		4.378	○	4.915	○	5.959
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	4.840	○	4.150	○	2.882	
		Min	≤11.50	2.979	○	2.542	○	1.863
	Top of Main Girder	Max	5.682	○	5.268	○	4.256	
		Min	-2	4.147	○	3.943	○	3.418
	Bottom of Main Girder	Max	~16.10	-0.098	○	1.185	○	3.768
		Min		4.238	○	4.949	○	6.168
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	4.840	○	4.150	○	2.882	
		Min	≤11.50	2.979	○	2.542	○	1.863
	Top of Main Girder	Max	5.682	○	5.268	○	4.256	
		Min	-2	4.147	○	3.943	○	3.418
	Bottom of Main Girder	Max	~16.10	-0.098	○	1.185	○	3.768
		Min		4.238	○	4.949	○	6.168

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[2-13]		[2-14]		[2-15]		
Interval from beginning of Girder		-----	26.094		28.644		29.594		
Immediately After Prestressing	Top of Main Girder	-1.5	3.794	○	2.774	○	2.971	○	
	Bottom of Main Girder	~19.00	11.144	○	6.013	○	5.077	○	
During Deck Construction	Top of Main Girder	-1.5	5.850	○	3.213	○	2.819	○	
	Bottom of Main Girder	~14.00	7.543	○	5.011	○	4.817	○	
Dead Load	Top of Deck	≤10.00	1.425	○	0.562	○	0.274	○	
	Top of Main Girder	0	4.365	○	2.497	○	2.120	○	
	Bottom of Main Girder	~14.00	5.789	○	4.667	○	4.786	○	
Design Load1	Top of Deck	Max	2.319	○	0.836	○	0.275	○	
		Min	1.330	○	0.536	○	0.274	○	
	Top of Main Girder	Max	5.100	○	2.735	○	2.120	○	
		Min	-1.5	4.287	○	2.476	○	2.120	○
	Bottom of Main Girder	Max	~14.00	3.685	○	4.161	○	4.786	○
		Min		6.014	○	4.713	○	4.786	○
Design Load2 Temperature Rise	Top of Deck	Max	2.821	○	1.361	○	0.793	○	
		Min	≤11.50	1.833	○	1.061	○	0.793	○
	Top of Main Girder	Max	4.206	○	1.882	○	1.263	○	
		Min	-2	3.393	○	1.622	○	1.263	○
	Bottom of Main Girder	Max	~16.10	3.901	○	4.599	○	5.260	○
		Min		6.230	○	5.151	○	5.260	○
Design Load3 Temperature Drop	Top of Deck	Max	2.821	○	1.361	○	0.793	○	
		Min	≤11.50	1.833	○	1.061	○	0.793	○
	Top of Main Girder	Max	4.206	○	1.882	○	1.263	○	
		Min	-2	3.393	○	1.622	○	1.263	○
	Bottom of Main Girder	Max	~16.10	3.901	○	4.599	○	5.260	○
		Min		6.230	○	5.151	○	5.260	○
Design Load4 Support sinking	Top of Deck	Max	2.319	○	0.836	○	0.275	○	
		Min	≤10.00	1.330	○	0.536	○	0.274	○
	Top of Main Girder	Max	5.100	○	2.735	○	2.120	○	
		Min	-1.5	4.287	○	2.476	○	2.120	○
	Bottom of Main Girder	Max	~14.00	3.685	○	4.161	○	4.786	○
		Min		6.014	○	4.713	○	4.786	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	2.821	○	1.361	○	0.793	○	
		Min	≤11.50	1.833	○	1.061	○	0.793	○
	Top of Main Girder	Max	4.206	○	1.882	○	1.263	○	
		Min	-2	3.393	○	1.622	○	1.263	○
	Bottom of Main Girder	Max	~16.10	3.901	○	4.599	○	5.260	○
		Min		6.230	○	5.151	○	5.260	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	2.821	○	1.361	○	0.793	○	
		Min	≤11.50	1.833	○	1.061	○	0.793	○
	Top of Main Girder	Max	4.206	○	1.882	○	1.263	○	
		Min	-2	3.393	○	1.622	○	1.263	○
	Bottom of Main Girder	Max	~16.10	3.901	○	4.599	○	5.260	○
		Min		6.230	○	5.151	○	5.260	○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3

Cross Section NumberNo.	Unit	Allowable Value	[2- 1]		[2- 2]		[2- 3]	
Interval from beginning of Girder								
				0.501		1.451		4.000
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1099	○	1103	○	1157	○
Effective Prestressing Force (*1)	N/mm ²	1110	1043	○	1045	○	1081	○
Effective Prestressing Force (*2)	N/mm ²	1110	967	○	968	○	980	○
max	N/mm ²	1110	963	○	965	○	982	○
Ultimate Load	-----	1	2	○	3	○	2	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2- 4]		[2- 5]		[2- 6]	
Interval from beginning of Girder								
				4.137		7.774		11.410
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1159	○	1171	○	1161	○
Effective Prestressing Force (*1)	N/mm ²	1110	1082	○	1082	○	1060	○
Effective Prestressing Force (*2)	N/mm ²	1110	981	○	988	○	975	○
max	N/mm ²	1110	984	○	1015	○	1026	○
Ultimate Load	-----	1	2	○	1	○	1	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2- 7]		[2- 8]		[2- 9]	
Interval from beginning of Girder								
				13.730		15.047		16.016
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1166	○	1172	○	1176	○
Effective Prestressing Force (*1)	N/mm ²	1110	1062	○	1068	○	1071	○
Effective Prestressing Force (*2)	N/mm ²	1110	982	○	990	○	993	○
max	N/mm ²	1110	1043	○	1053	○	1057	○
Ultimate Load	-----	1	1	○	1	○	1	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2-10]	[2-11]	[2-12]
Interval from beginning of Girder			18.684	22.320	25.957
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	1320	1320
Immediately After Prestressing	N/mm ²	1295	1196	1193	1174
Effective Prestressing Force (*1)	N/mm ²	1110	1091	1098	1090
Effective Prestressing Force (*2)	N/mm ²	1110	1007	1009	994
max	N/mm ²	1110	1066	1050	1012
Ultimate Load	-----	1	1	1	2

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2-13]	[2-14]	[2-15]
Interval from beginning of Girder			26.094	28.644	29.594
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	1320	1320
Immediately After Prestressing	N/mm ²	1295	1173	1166	1163
Effective Prestressing Force (*1)	N/mm ²	1110	1090	1104	1103
Effective Prestressing Force (*2)	N/mm ²	1110	994	1029	1031
max	N/mm ²	1110	1011	1031	1031
Ultimate Load	-----	1	2	6	1000

*1:During DeckConstruction *2:Design Load

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2- 1]	[2- 2]	[2- 3]		
Interval from beginning of Girder			-----	0.501	1.451	4.000		
Shear Force								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	1.06 Δ	1.05 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.13 ○	-0.03 ○	
	Neutral Axis before Composition			-----	--	-0.24 ○	-0.03 ○	
	Neutral Axis after Composition			-----	--	-0.22 ○	-0.03 ○	
	Base of Lower Flange			-----	--	-0.05 ○	-0.02 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.35 ○	-0.33 ○	
				Min	-----	--	-0.12 ○	-0.01 ○
	Neutral Axis before Composition			Max	-----	--	-0.43 ○	-0.29 ○
				Min	-----	--	-0.23 ○	-0.01 ○
	Neutral Axis after Composition			Max	-----	--	-0.45 ○	-0.33 ○
				Min	-----	--	-0.21 ○	-0.01 ○
	Base of Lower Flange			Max	-----	--	-0.06 ○	-0.18 ○
				Min	-----	--	-0.05 ○	-0.01 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	17.89 --	20.45 --	
	D16	cm	-----	-----	--	28.05 --	32.05 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	11.34 --	10.84 --	
Compressive Strength to Failure (Suc/Shu)			1.00	-----	--	2.98 ○	1.64 ○	
Strength against Diagonal Densile Failure(Sus/Shu)	D13		1.00	-----	--	1 ○	1.00 ○	
	D16		1.00	-----	--	1 ○	1.00 ○	
	D19		1.00	-----	--	1.004 ○	1.07 ○	
Shear Force + Torsion								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	1.06 Δ	1.05 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.13 ○	-0.03 ○	
	Neutral Axis before Composition			-----	--	-0.24 ○	-0.03 ○	
	Neutral Axis after Composition			-----	--	-0.22 ○	-0.03 ○	
	Base of Lower Flange			-----	--	-0.05 ○	-0.02 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.35 ○	-0.33 ○	
				Min	-----	--	-0.12 ○	-0.01 ○
	Neutral Axis before Composition			Max	-----	--	-0.43 ○	-0.29 ○
				Min	-----	--	-0.23 ○	-0.01 ○
	Neutral Axis after Composition			Max	-----	--	-0.45 ○	-0.33 ○
				Min	-----	--	-0.21 ○	-0.01 ○
	Base of Lower Flange			Max	-----	--	-0.06 ○	-0.18 ○
				Min	-----	--	-0.05 ○	-0.01 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	17.89 --	20.45 --	
	D16	cm	-----	-----	--	28.05 --	32.05 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 --	0.00 --	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2- 4]	[2- 5]	[2- 6]				
Interval from beginning of Girder			-----	4.137	7.774	11.410				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.06	Δ	0.78	Δ	0.67	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.03	○	-0.01	○	-0.01	○	
	Neutral Axis before Composition			-0.03	○	-0.01	○	-0.01	○	
	Neutral Axis after Composition			-0.03	○	-0.01	○	-0.01	○	
	Base of Lower Flange			-0.02	○	-0.01	○	-0.01	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.33	○	-0.19	○	-0.14	○
				Min	-0.01	○	0.00	○	-0.01	○
	Neutral Axis before Composition			Max	-0.29	○	-0.16	○	-0.13	○
				Min	-0.01	○	0.00	○	-0.01	○
	Neutral Axis after Composition			Max	-0.34	○	-0.19	○	-0.15	○
				Min	-0.01	○	0.00	○	-0.01	○
	Base of Lower Flange			Max	-0.18	○	-0.11	○	-0.09	○
				Min	-0.01	○	0.00	○	-0.01	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	20.57	--	32.61	--	40.00	--	
	D16	cm	-----	32.24	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	10.78	--	6.80	--	3.96	--	
Compressive Strength to Failure (Suc/Shu)			-----	1.00	○	2.06	○	2.73	○	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.00	○	1	○	1.12	○	
	D16			1.00	○	1.1	○	1.36	○	
	D19			1.07	○	1.303	○	1.65	○	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.06	Δ	0.78	Δ	0.67	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.03	○	-0.01	○	-0.01	○	
	Neutral Axis before Composition			-0.03	○	-0.01	○	-0.01	○	
	Neutral Axis after Composition			-0.03	○	-0.01	○	-0.01	○	
	Base of Lower Flange			-0.02	○	-0.01	○	-0.01	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.33	○	-0.19	○	-0.14	○
				Min	-0.01	○	0.00	○	-0.01	○
	Neutral Axis before Composition			Max	-0.29	○	-0.16	○	-0.13	○
				Min	-0.01	○	0.00	○	-0.01	○
	Neutral Axis after Composition			Max	-0.34	○	-0.19	○	-0.15	○
				Min	-0.01	○	0.00	○	-0.01	○
	Base of Lower Flange			Max	-0.18	○	-0.11	○	-0.09	○
				Min	-0.01	○	0.00	○	-0.01	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	20.57	--	32.61	--	40.00	--	
	D16	cm	-----	32.24	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2- 7]	[2- 8]	[2- 9]	
Interval from beginning of Girder			-----	13.730	15.047	16.016	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.70 Δ	0.50 ○	0.60 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.02 ○	-0.01 ○	-0.02 ○	
	Neutral Axis before Composition			-0.03 ○	-0.01 ○	-0.03 ○	
	Neutral Axis after Composition			-0.03 ○	-0.01 ○	-0.02 ○	
	Base of Lower Flange			-0.02 ○	-0.01 ○	-0.02 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.14 ○	-0.07 ○	-0.01 ○
				Min	-0.01 ○	-0.04 ○	-0.09 ○
	Neutral Axis before Composition			Max	-0.15 ○	-0.07 ○	-0.01 ○
				Min	-0.01 ○	-0.06 ○	-0.13 ○
	Neutral Axis after Composition			Max	-0.15 ○	-0.08 ○	-0.01 ○
				Min	-0.01 ○	-0.05 ○	-0.11 ○
	Base of Lower Flange			Max	-0.10 ○	-0.05 ○	-0.01 ○
				Min	-0.01 ○	-0.11 ○	-0.14 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	2.86 --	0.93 --	0.00 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	3.43 ○	4.26 ○	5.08 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.271 ○	----- --	1.88 ○	
	D16			1.588 ○	----- --	2.35 ○	
	D19			1.976 ○	----- --	2.92 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.70 Δ	0.50 ○	0.60 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.02 ○	-0.01 ○	-0.02 ○	
	Neutral Axis before Composition			-0.03 ○	-0.01 ○	-0.03 ○	
	Neutral Axis after Composition			-0.03 ○	-0.01 ○	-0.02 ○	
	Base of Lower Flange			-0.02 ○	-0.01 ○	-0.02 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.14 ○	-0.07 ○	-0.01 ○
				Min	-0.01 ○	-0.04 ○	-0.09 ○
	Neutral Axis before Composition			Max	-0.15 ○	-0.07 ○	-0.01 ○
				Min	-0.01 ○	-0.06 ○	-0.13 ○
	Neutral Axis after Composition			Max	-0.15 ○	-0.08 ○	-0.01 ○
				Min	-0.01 ○	-0.05 ○	-0.11 ○
	Base of Lower Flange			Max	-0.10 ○	-0.05 ○	-0.01 ○
				Min	-0.01 ○	-0.11 ○	-0.14 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2-10]	[2-11]	[2-12]	
Interval from beginning of Girder			-----	18.684	22.320	25.957	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.70 Δ	0.88 Δ	1.28 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.03 ○	-0.04 ○	-0.11 ○	
	Neutral Axis before Composition			-0.03 ○	-0.04 ○	-0.10 ○	
	Neutral Axis after Composition			-0.03 ○	-0.04 ○	-0.11 ○	
	Base of Lower Flange			-0.02 ○	-0.03 ○	-0.06 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00 ○	-0.01 ○	-0.09 ○
				Min	-0.13 ○	-0.21 ○	-0.46 ○
	Neutral Axis before Composition			Max	0.00 ○	-0.01 ○	-0.08 ○
				Min	-0.18 ○	-0.26 ○	-0.46 ○
	Neutral Axis after Composition			Max	0.00 ○	-0.01 ○	-0.09 ○
				Min	-0.15 ○	-0.24 ○	-0.49 ○
	Base of Lower Flange			Max	0.00 ○	-0.01 ○	-0.05 ○
				Min	-0.23 ○	-0.25 ○	-0.32 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	23.56 --	
	D16	cm	-----	40.00 --	40.00 --	36.92 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	2.15 --	5.26 --	9.41 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	3.62 ○	2.47 ○	1.82 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.343 ○	1.018 ○	1.00 ○	
	D16			1.661 ○	1.222 ○	1.00 ○	
	D19			2.05 ○	1.471 ○	1.14 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.70 Δ	0.88 Δ	1.28 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.03 ○	-0.04 ○	-0.11 ○	
	Neutral Axis before Composition			-0.03 ○	-0.04 ○	-0.10 ○	
	Neutral Axis after Composition			-0.03 ○	-0.04 ○	-0.11 ○	
	Base of Lower Flange			-0.02 ○	-0.03 ○	-0.06 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00 ○	-0.01 ○	-0.09 ○
				Min	-0.13 ○	-0.21 ○	-0.46 ○
	Neutral Axis before Composition			Max	0.00 ○	-0.01 ○	-0.08 ○
				Min	-0.18 ○	-0.26 ○	-0.46 ○
	Neutral Axis after Composition			Max	0.00 ○	-0.01 ○	-0.09 ○
				Min	-0.15 ○	-0.24 ○	-0.49 ○
	Base of Lower Flange			Max	0.00 ○	-0.01 ○	-0.05 ○
				Min	-0.23 ○	-0.25 ○	-0.32 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	23.56 --	
	D16	cm	-----	40.00 --	40.00 --	36.92 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2-13]	[2-14]	[2-15]				
Interval from beginning of Girder			-----	26.094	28.644	29.594				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.30	Δ	0.56	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.12	○	-0.03	○	-----	--	
	Neutral Axis before Composition			-0.11	○	-0.04	○	-----	--	
	Neutral Axis after Composition			-0.12	○	-0.04	○	-----	--	
	Base of Lower Flange			-0.07	○	-0.01	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.10	○	-0.03	○	-----	--
				Min	-0.48	○	-0.15	○	-----	--
	Neutral Axis before Composition			Max	-0.09	○	-0.04	○	-----	--
				Min	-0.48	○	-0.15	○	-----	--
	Neutral Axis after Composition			Max	-0.10	○	-0.04	○	-----	--
				Min	-0.50	○	-0.17	○	-----	--
	Base of Lower Flange			Max	-0.05	○	-0.01	○	-----	--
				Min	-0.33	○	-0.02	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	23.04	--	20.18	--	-----	--	
	D16	cm	-----	36.12	--	31.62	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	9.62	--	0.40	--	-----	--	
Compressive Strength to Failure (Suc/Shu)			-----	1.00	○	3.82	○	-----	--	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1	○	1.391	○	-----	--	
	D16			1	○	1.391	○	-----	--	
	D19			1.133	○	1.448	○	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.30	Δ	0.56	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.12	○	-0.03	○	-----	--	
	Neutral Axis before Composition			-0.11	○	-0.04	○	-----	--	
	Neutral Axis after Composition			-0.12	○	-0.04	○	-----	--	
	Base of Lower Flange			-0.07	○	-0.01	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.10	○	-0.03	○	-----	--
				Min	-0.48	○	-0.15	○	-----	--
	Neutral Axis before Composition			Max	-0.09	○	-0.04	○	-----	--
				Min	-0.48	○	-0.15	○	-----	--
	Neutral Axis after Composition			Max	-0.10	○	-0.04	○	-----	--
				Min	-0.50	○	-0.17	○	-----	--
	Base of Lower Flange			Max	-0.05	○	-0.01	○	-----	--
				Min	-0.33	○	-0.02	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	23.04	--	20.18	--	-----	--	
	D16	cm	-----	36.12	--	31.62	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2- 1]	[2- 2]	[2- 3]	
Interval from beginning of Girder			-----	0.501	1.451	4.000	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.95 Δ	0.78 Δ
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.11 ○	-0.01 ○
	Neutral Axis before Composition			-----	--	-0.22 ○	0.00 ○
	Neutral Axis after Composition			-----	--	-0.19 ○	0.00 ○
	Base of Lower Flange			-----	--	-0.05 ○	0.00 ○
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.28 ○	-0.20 ○
				Min	-----	--	-0.11 ○
	Neutral Axis before Composition	Max		-----	--	-0.37 ○	-0.18 ○
		Min		-----	--	-0.20 ○	0.00 ○
	Neutral Axis after Composition	Max		-----	--	-0.38 ○	-0.20 ○
		Min		-----	--	-0.18 ○	0.00 ○
	Base of Lower Flange	Max		-----	--	-0.06 ○	-0.13 ○
		Min		-----	--	-0.04 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 --	27.55 --
	D16	cm	-----	-----	--	31.63 --	40.00 --
	D19	cm	-----	-----	--	40.00 --	40.00 --
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	8.71 --	8.05 --
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.95 Δ	0.78 Δ
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.11 ○	-0.01 ○
	Neutral Axis before Composition			-----	--	-0.22 ○	0.00 ○
	Neutral Axis after Composition			-----	--	-0.19 ○	0.00 ○
	Base of Lower Flange			-----	--	-0.05 ○	0.00 ○
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.28 ○	-0.20 ○
				Min	-----	--	-0.11 ○
	Neutral Axis before Composition	Max		-----	--	-0.37 ○	-0.18 ○
		Min		-----	--	-0.20 ○	0.00 ○
	Neutral Axis after Composition	Max		-----	--	-0.38 ○	-0.20 ○
		Min		-----	--	-0.18 ○	0.00 ○
	Base of Lower Flange	Max		-----	--	-0.06 ○	-0.13 ○
		Min		-----	--	-0.04 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 --	27.55 --
	D16	cm	-----	-----	--	31.63 --	40.00 --
	D19	cm	-----	-----	--	40.00 --	40.00 --
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 --	0.00 --
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	-----	--	999.999 ○	999.999 ○
Strength against Diagonal Densile Failure(Mus/Mtu)	D13	-----	1.00	-----	--	999.999 ○	999.999 ○
	D16			-----	--	999.999 ○	999.999 ○
	D19			-----	--	999.999 ○	999.999 ○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2- 4]	[2- 5]	[2- 6]	
Interval from beginning of Girder			-----	4.022	7.544	11.065	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.78 Δ	0.58 Δ	0.35 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.01 ○	0.00 ○	0.00 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	-0.01 ○	
	Neutral Axis after Composition			0.00 ○	0.00 ○	0.00 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.20 ○	-0.11 ○	-0.04 ○
				Min	0.00 ○	0.00 ○	-0.01 ○
	Neutral Axis before Composition			Max	-0.19 ○	-0.11 ○	-0.05 ○
				Min	0.00 ○	0.00 ○	-0.01 ○
	Neutral Axis after Composition			Max	-0.20 ○	-0.12 ○	-0.05 ○
				Min	0.00 ○	0.00 ○	-0.01 ○
	Base of Lower Flange			Max	-0.13 ○	-0.10 ○	-0.06 ○
				Min	0.00 ○	0.00 ○	-0.01 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	27.59 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	8.03 --	4.99 --	1.27 --	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.78 Δ	0.58 Δ	0.35 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.01 ○	0.00 ○	0.00 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	-0.01 ○	
	Neutral Axis after Composition			0.00 ○	0.00 ○	0.00 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.20 ○	-0.11 ○	-0.04 ○
				Min	0.00 ○	0.00 ○	-0.01 ○
	Neutral Axis before Composition			Max	-0.19 ○	-0.11 ○	-0.05 ○
				Min	0.00 ○	0.00 ○	-0.01 ○
	Neutral Axis after Composition			Max	-0.20 ○	-0.12 ○	-0.05 ○
				Min	0.00 ○	0.00 ○	-0.01 ○
	Base of Lower Flange			Max	-0.13 ○	-0.10 ○	-0.06 ○
				Min	0.00 ○	0.00 ○	-0.01 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	27.59 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	0.00 --	0.00 --	0.00 --	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999 ○	999.999 ○	999.999 ○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999 ○	999.999 ○	-----	
	D16			999.999 ○	999.999 ○	-----	
	D19			999.999 ○	999.999 ○	-----	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2- 7]	[2- 8]	[2- 9]				
Interval from beginning of Girder			-----	13.730	14.587	15.096				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.24	○	0.13	○	0.11	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	-0.01	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	-0.01	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.02	○	0.00	○	0.00	○
				Min	0.00	○	-0.01	○	0.00	○
	Neutral Axis before Composition			Max	-0.02	○	0.00	○	0.00	○
				Min	0.00	○	-0.01	○	-0.01	○
	Neutral Axis after Composition			Max	-0.02	○	0.00	○	0.00	○
				Min	0.00	○	-0.01	○	0.00	○
	Base of Lower Flange			Max	-0.01	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	-0.01	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.24	○	0.13	○	0.11	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	-0.01	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	-0.01	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.02	○	0.00	○	0.00	○
				Min	0.00	○	-0.01	○	0.00	○
	Neutral Axis before Composition			Max	-0.02	○	0.00	○	0.00	○
				Min	0.00	○	-0.01	○	-0.01	○
	Neutral Axis after Composition			Max	-0.02	○	0.00	○	0.00	○
				Min	0.00	○	-0.01	○	0.00	○
	Base of Lower Flange			Max	-0.01	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	-0.01	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	-----	-	-----	-	
	D16	-----	1.00	-----	-	-----	-	-----	-	
	D19	-----	1.00	-----	-	-----	-	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2-10]	[2-11]	[2-12]				
Interval from beginning of Girder			-----	18.109	21.630	25.152				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.42	○	0.80	△	1.14	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	-0.03	○	-0.09	○	
	Neutral Axis before Composition			0.00	○	-0.02	○	-0.08	○	
	Neutral Axis after Composition			0.00	○	-0.02	○	-0.09	○	
	Base of Lower Flange			0.00	○	-0.01	○	-0.04	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	-0.02	○	-0.09	○
				Min	-0.05	○	-0.20	○	-0.41	○
	Neutral Axis before Composition			Max	0.00	○	-0.02	○	-0.07	○
				Min	-0.07	○	-0.21	○	-0.38	○
	Neutral Axis after Composition			Max	0.00	○	-0.02	○	-0.09	○
				Min	-0.06	○	-0.22	○	-0.42	○
	Base of Lower Flange			Max	0.00	○	-0.01	○	-0.04	○
				Min	-0.08	○	-0.18	○	-0.25	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	28.91	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	4.04	--	7.67	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.42	○	0.80	△	1.14	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	-0.03	○	-0.09	○	
	Neutral Axis before Composition			0.00	○	-0.02	○	-0.08	○	
	Neutral Axis after Composition			0.00	○	-0.02	○	-0.09	○	
	Base of Lower Flange			0.00	○	-0.01	○	-0.04	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	-0.02	○	-0.09	○
				Min	-0.05	○	-0.20	○	-0.41	○
	Neutral Axis before Composition			Max	0.00	○	-0.02	○	-0.07	○
				Min	-0.07	○	-0.21	○	-0.38	○
	Neutral Axis after Composition			Max	0.00	○	-0.02	○	-0.09	○
				Min	-0.06	○	-0.22	○	-0.42	○
	Base of Lower Flange			Max	0.00	○	-0.01	○	-0.04	○
				Min	-0.08	○	-0.18	○	-0.25	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	28.91	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Densile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	999.999	○	999.999	○	
	D16			-----	-	999.999	○	999.999	○	
	D19			-----	-	999.999	○	999.999	○	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2-13]	[2-14]	[2-15]				
Interval from beginning of Girder			-----	25.174	27.724	28.674				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.14	Δ	0.48	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.10	○	-0.04	○	-----	--	
	Neutral Axis before Composition			-0.08	○	-0.03	○	-----	--	
	Neutral Axis after Composition			-0.09	○	-0.04	○	-----	--	
	Base of Lower Flange			-0.04	○	0.00	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.09	○	-0.04	○	-----	--
				Min	-0.41	○	-0.12	○	-----	--
	Neutral Axis before Composition			Max	-0.07	○	-0.03	○	-----	--
				Min	-0.38	○	-0.11	○	-----	--
	Neutral Axis after Composition			Max	-0.09	○	-0.04	○	-----	--
				Min	-0.42	○	-0.13	○	-----	--
	Base of Lower Flange			Max	-0.04	○	0.00	○	-----	--
				Min	-0.25	○	-0.01	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	28.67	--	20.18	--	-----	--	
	D16	cm	-----	40.00	--	31.62	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	7.73	--	0.00	--	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.14	Δ	0.48	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.10	○	-0.04	○	-----	--	
	Neutral Axis before Composition			-0.08	○	-0.03	○	-----	--	
	Neutral Axis after Composition			-0.09	○	-0.04	○	-----	--	
	Base of Lower Flange			-0.04	○	0.00	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.09	○	-0.04	○	-----	--
				Min	-0.41	○	-0.12	○	-----	--
	Neutral Axis before Composition			Max	-0.07	○	-0.03	○	-----	--
				Min	-0.38	○	-0.11	○	-----	--
	Neutral Axis after Composition			Max	-0.09	○	-0.04	○	-----	--
				Min	-0.42	○	-0.13	○	-----	--
	Base of Lower Flange			Max	-0.04	○	0.00	○	-----	--
				Min	-0.25	○	-0.01	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	28.67	--	20.18	--	-----	--	
	D16	cm	-----	40.00	--	31.62	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	-----	--	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	-----	-	-----	--	
	D16			999.999	○	-----	-	-----	--	
	D19			999.999	○	-----	-	-----	--	

5 Design of Intermediate Cross Beam

(1) Parameters

<1st Span>

	Unit	Bending Moment (Maximum)	Bending Moment (Minimum)	
CB 2				
Length between End of Girders	Lb	cm	328.0	328.0
Web Width	Bw	cm	22.0	22.0
Width of Cross Beam	Bc	cm	30.0	30.0
Thickness of Deck	Hs	cm	17.0	17.0
Height of Cross Beam (before Composition of Deck)	Hb	cm	130.0	130.0
Height of Cross Beam (after Composition of Deck)	Ha	cm	187.0	187.0
Interval of Cross Beam	Lt	cm	1421.0	1421.0

<2nd Span>

	Unit	Bending Moment (Maximum)	Bending Moment (Minimum)	
CB 2				
Length between End of Girders	Lb	cm	328.0	328.0
Web Width	Bw	cm	22.0	22.0
Width of Cross Beam	Bc	cm	30.0	30.0
Thickness of Deck	Hs	cm	17.0	17.0
Height of Cross Beam (before Composition of Deck)	Hb	cm	130.0	130.0
Height of Cross Beam (after Composition of Deck)	Ha	cm	187.0	187.0
Interval of Cross Beam	Lt	cm	1424.7	1424.7

(2) Calculation of Prestressing

1) Arrangement of PC Strand

(1) Parameter of PC Strand

	Unit	Parameters
Name of PC Strand		4S15.2, SWPR7BL
Area of PC Strand	mm ² /no.	554.80
Amount of Set	mm	4.0
Reduction Rate of Anchor	%	0.000
Friction Coefficient	1/m	0.0040
Creep Coefficient		2.60
Drying Shrinkage	×10 ⁻⁵	20.00
Relaxation	%	2.5
Prestressing Stress	N/mm ²	1250.000
(Considering Friction Coefficient)	N/mm ²	1250.000
Allowable Value	N/mm ²	1440.000

(2) Arrangement of PC Strand

<1st Span>

Item		Unit	Maximum Bending Moment	Minimum Bending Moment
CB 2				
How to Prestressing			From One Side	
Length of PC Strand		m	10.720	10.720
1st	Position	mm	400	400
	Number	No.	1	1
2nd	Position	mm	800	800
	Number	No.	1	1

<2nd Span>

Item		Unit	Maximum Bending Moment	Minimum Bending Moment
CB 2				
How to Prestressing			From One Side	
Length of PC Strand		m	10.723	10.723
1st	Position	mm	400	400
	Number	No.	1	1
2nd	Position	mm	800	800
	Number	No.	1	1

<Design of Cross Beam : Summary for Calculation Results of Stress>

1st Span : Cross Beam (CB2)

Item		Unit	Allowable Value	Mmax		Mmin	
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	-0.38	○	-0.40	○
	Bottom of Deck			-0.25	○	-0.27	○
Dead Load	Top of Cross Beam	N/mm ²	0	2.28	○	2.29	○
	Bottom of Cross Beam			~ 11.0	4.58	○	4.64
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	0.45	○	-0.85	○
	Bottom of Deck			0.30	○	-0.57	○
Dead Load	Top of Cross Beam	N/mm ²	0	2.19	○	2.34	○
	Bottom of Cross Beam			~ 11.0	2.40	○	5.83
Ultimate Load		-----	1	1.96	○	1.68	○
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1440	1250	○	1250	○
	Immediately After Prestressing	N/mm ²	1295	1175	○	1175	○
	Effective Prestressing Force	N/mm ²	1110	1024	○	1024	○

2nd Span : Cross Beam (CB2)

Item		Unit	Allowable Value	Mmax		Mmin	
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	-0.36	○	-0.40	○
	Bottom of Deck			-0.24	○	-0.27	○
Dead Load	Top of Cross Beam	N/mm ²	0	2.28	○	2.29	○
	Bottom of Cross Beam			~ 11.0	4.54	○	4.64
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	0.47	○	-0.85	○
	Bottom of Deck			0.31	○	-0.57	○
Dead Load	Top of Cross Beam	N/mm ²	0	2.19	○	2.34	○
	Bottom of Cross Beam			~ 11.0	2.34	○	5.84
Ultimate Load		-----	1	1.93	○	1.68	○
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1440	1250	○	1250	○
	Immediately After Prestressing	N/mm ²	1295	1175	○	1175	○
	Effective Prestressing Force	N/mm ²	1110	1024	○	1024	○

<Design of Cross Beam : Summary for Calculation Results of Stress>

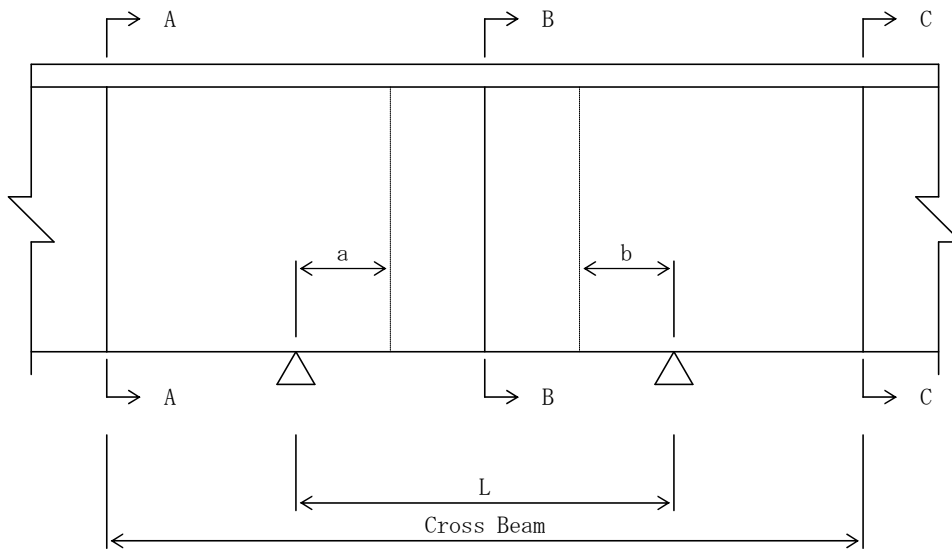
1st Span : Cross Beam (CB2)

Item	Unit	Allowable Value	Smax	Smin	Tmax	Tmin					
Shear Force											
Shear Stress	Design Load	N/mm ²	0.45	0.68	Δ	0.46	Δ	0.17	○	0.12	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	-0.02	○	-0.02	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	-0.17	○	-0.16	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Suc/Shu	-	1.00	2.81	○	4.14	○	9.76	○	12.76	○
Strength against Diagonal Densile Failure	D13	-	1.00	1.00	○	1.59	○	----	--	----	--
	Sus/Shu	D16	-	1.00	1.01	○	1.96	○	----	--	----
Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.00	○	0.00	○	0.00	○	0.00	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	0.00	○	0.00	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	0.00	○	0.00	○	0.00	○	0.00	○
Shear Force + Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.68	Δ	0.46	Δ	0.17	○	0.12	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-1.10	-0.02	○	-0.02	○	0.00	○	0.00	○
	Design Load	N/mm ²	-2.20	-0.17	○	-0.16	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Muc/Mtu	-	1.00	999.999	○	999.999	○	1000.00	○	999.999	○
Strength against Diagonal Densile Failure	D13	-	1.00	999.999	○	999.999	○	----	--	----	--
	Mus/Mtu	D16	-	1.00	999.999	○	999.999	○	----	--	----
Amount of Diagonal Tension Re-bar	cm ²	----	9.74	--	6.00	--	6.00	--	6.00	--	
Axial Reinforcement Bar Volume	cm ²	----	5.27	--	0.52	--	0.00	--	0.00	--	

2nd Span : Cross Beam (CB2)

Item	Unit	Allowable Value	Smax	Smin	Tmax	Tmin					
Shear Force											
Shear Stress	Design Load	N/mm ²	0.45	0.68	Δ	0.45	○	0.11	○	0.18	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	-0.02	○	-0.02	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	-0.17	○	-0.16	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Suc/Shu	-	1.00	2.81	○	4.17	○	12.79	○	9.61	○
Strength against Diagonal Densile Failure	D13	-	1.00	1.00	○	----	--	----	--	----	--
	Sus/Shu	D16	-	1.00	1.01	○	----	--	----	--	----
Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.00	○	0.00	○	0.00	○	0.00	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	0.00	○	0.00	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	0.00	○	0.00	○	0.00	○	0.00	○
Shear Force + Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.68	Δ	0.45	○	0.11	○	0.18	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-1.10	-0.02	○	-0.02	○	0.00	○	0.00	○
	Design Load	N/mm ²	-2.20	-0.17	○	-0.16	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Muc/Mtu	-	1.00	999.999	○	999.999	○	1000.00	○	999.999	○
Strength against Diagonal Densile Failure	D13	-	1.00	999.999	○	----	--	----	--	----	--
	Mus/Mtu	D16	-	1.00	999.999	○	----	--	----	--	----
Amount of Diagonal Tension Re-bar	cm ²	----	9.75	--	6.00	--	6.00	--	6.00	--	
Axial Reinforcement Bar Volume	cm ²	----	5.28	--	0.46	--	0.00	--	0.00	--	

6 Design of Coupling Concrete
Dimension



Unit: m

L	1.200
a	0.500
b	0.500

<Connection of Cross beam : Summary for Calculation Results of Stress>

1st Span~2nd Span, Main Girder Number: G4(Negative Moment) G1(Positive Moment)

Item		Unit	Allowable Value	Negative Moment						Positive Moment		
				A-A		B-B		C-C		B-B		
Re-bar Volume	1st Layer	Diameter	mm	-----	D19	--	D19	--	D19	--	D22	--
		Number	Number	-----	16	--	16	--	16	--	12	--
	2nd Layer	Diameter	mm	-----	D19	--	D19	--	D19	--	D22	--
		Number	Number	-----	16	--	16	--	16	--	12	--
Bending Stress (Dead Load)												
Bending Tensile Stress of Reinforcement Bar		N/mm ²	100	-4.19	○	5.36	○	-3.89	○	49.42	○	
Bending Stress (Design Load)												
Bending Stress of Concrete		N/mm ²	10	4.54	○	4.54	○	4.54	○	1.27	○	
Bending Tensile Stress of Reinforcement Bar		N/mm ²	160	122.32	○	122.32	○	122.32	○	63.44	○	
Bending Stress (Temperature Load)												
Bending Stress of Concrete		N/mm ²	11.5	4.79	○	4.54	○	4.82	○	2.09	○	
Bending Tensile Stress of Reinforcement Bar		N/mm ²	184	129.05	○	122.32	○	129.94	○	104.79	○	
Ultimate Load		-----	1	1.04	○	1.12	○	1.03	○	4.36	○	

7 Calculation of Reaction Force

7.1 Reaction Force for Each Girder

<1st Span, Left>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	340.656	339.639	342.933	350.701
Cast-in-place Concrete	D2	303.224	427.759	431.134	314.097
Weight of Bridge Surface	D3	150.985	150.499	168.009	202.782
Subtotal: DT1=D1+D2+D3		794.865	917.897	942.076	867.580
Live Load LT	Max	321.730	304.940	303.710	315.600
	Min	-67.510	-28.650	-30.040	-65.520
Subtotal: DT2 =DT1+LT+SW	Max	1116.595	1222.837	1245.786	1183.180
	Min	727.355	889.247	912.036	802.060
Creep CR		87.227	70.930	67.833	68.782
Drying Shrinkage SH		-9.234	-9.324	-9.226	-7.986
Temperature Range		24.010	24.243	23.988	20.763
Dead Load: DT1+CR+SH		872.858	979.503	1000.683	928.376
Total: DT2+CR +SH+T+SD	Max	1218.598	1308.686	1328.381	1264.739
	Min	829.358	975.096	994.631	883.619

<1st Span, Right>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	340.669	339.651	342.946	350.713
Cast-in-place Concrete	D2	317.836	451.621	454.995	328.195
Weight of Bridge Surface	D3	257.523	245.574	265.559	301.974
Subtotal: DT1=D1+D2+D3		916.028	1036.846	1063.500	980.882
Live Load LT	Max	512.760	463.910	476.950	540.140
	Min	-205.700	-143.670	-167.200	-254.440
Subtotal: DT2 =DT1+LT+SW	Max	1428.788	1500.756	1540.450	1521.022
	Min	710.328	893.176	896.300	726.442
Creep CR		-85.640	-70.030	-69.046	-71.669
Drying Shrinkage SH		9.297	9.336	9.210	7.998
Temperature Range		-24.171	-24.273	-23.945	-20.791
Dead Load: DT1+CR+SH		839.685	976.152	1003.664	917.211
Total: DT2+CR +SH+T+SD	Max	1328.274	1415.789	1456.669	1436.560
	Min	609.814	808.209	812.519	641.980

<2nd Span, Left>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	338.733	339.068	343.687	352.806
Cast-in-place Concrete	D2	316.991	451.047	455.775	329.021
Weight of Bridge Surface	D3	325.889	291.881	286.897	300.415
Subtotal: DT1=D1+D2+D3		981.613	1081.996	1086.359	982.242
Live Load LT	Max	511.490	463.600	477.980	542.050
	Min	-207.200	-143.510	-166.640	-252.740
Subtotal: DT2 =DT1+LT+SW	Max	1493.103	1545.596	1564.339	1524.292
	Min	774.413	938.486	919.719	729.502
Creep CR		-89.468	-72.012	-66.399	-65.299
Drying Shrinkage SH		9.232	9.331	9.220	7.919
Temperature Range		-24.005	-24.261	-23.972	-20.589
Dead Load: DT1+CR+SH		901.377	1019.315	1029.180	924.862
Total: DT2+CR +SH+T+SD	Max	1388.862	1458.654	1483.188	1446.323
	Min	670.172	851.544	838.568	651.533

<2nd Span, Right>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	338.720	339.056	343.675	352.794
Cast-in-place Concrete	D2	301.984	427.186	431.914	314.522
Weight of Bridge Surface	D3	185.699	172.859	177.701	199.949
Subtotal: DT1=D1+D2+D3		826.403	939.101	953.290	867.265
Live Load LT	Max	321.350	304.220	302.570	314.500
	Min	-64.830	-28.840	-29.760	-64.870
Subtotal: DT2 =DT1+LT+SW	Max	1147.753	1243.321	1255.860	1181.765
	Min	761.573	910.261	923.530	802.395
Creep CR		87.881	71.112	67.612	68.187
Drying Shrinkage SH		-9.294	-9.343	-9.204	-7.930
Temperature Range		24.165	24.291	23.929	20.618
Dead Load: DT1+CR+SH		904.990	1000.870	1011.698	927.522
Total: DT2+CR +SH+T+SD	Max	1250.505	1329.381	1338.197	1262.640
	Min	864.325	996.321	1005.867	883.270

7.2 Reaction Force for Pier and Abutment

Unit: kN

		1	2	3
Weight of Girder	D1	1373.929	2748.273	1374.245
Cast-in-place Concrete	D2	1476.214	3105.481	1475.606
Weight of Bridge Surface	D3	672.275	2275.712	736.208
Subtotal: DT1=D1+D2+D3		3522.418	8129.466	3586.059
Live Load LT	Max	1021.890	1965.700	1019.460
	Min	-102.880	0.000	-102.630
Subtotal: DT2 =DT1+LT+SW	Max	4544.308	10095.166	4605.519
	Min	3419.538	8129.466	3483.429
Creep CR		294.772	-589.563	294.792
Drying Shrinkage SH		-35.770	71.543	-35.771
Temperature Range		93.004	-186.007	93.003
Dead Load: DT1+CR+SH		3781.420	7611.446	3845.080
Total: DT2+CR +SH+T+SD	Max	4896.314	9391.139	4957.543
	Min	3771.544	7425.439	3835.453

7.3 Horizontal Force

Horizontal Force(PF5、 PF6fix)

(kN)

	PF5	PF6
Prestressing	-192	121
Drying Shrinkage	-199	125
Temperature(+)	201	-128
Temperature(-)	-201	128
Dead Load	-391	246
Temperature+15°C	-190	119
Temperature-15°C	-592	374
Temperature+40°C	145	-94
Temperature-40°C	-928	586

8 Design of Cross Beam at End of Girder

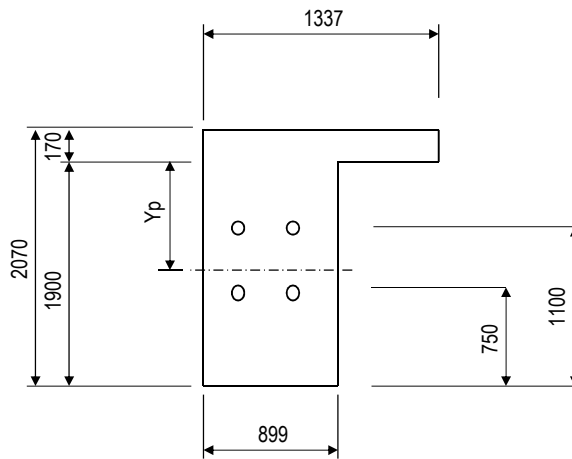
8.1 For Bending Moment

1) Calculation of Bending Moment

(kN·m)

		Bending Moment	
		max	min
Dead Load	(Md)	-81.62	-78.85
Live Load	(ML)	320.89	-160.86
Total	(M)	239.27	-239.71

2) Dimension



3) Calculation of Prestressing

Type of PC strand 4S15.2 SWPR19L
 Area of PC strand 554.8 mm²
 Number of PC strand 4

(N/mm²)

	Tensile Stress of PC strand	
	Allowable Value	Result
During Prestressing	1440	1250
Immediately after Prestressing	1295	1151
Under Effective Prestressing Force	1110	1056

4) Combined Flexural Stress

(N/mm²)

	Bending Moment(Max)		Bending Moment(Min)		
	Top	Bottom	Top	Bottom	
Dead Load	-0.11	0.12	-0.11	0.12	
Live Load	0.44	-0.47	-0.22	0.24	
Prestressing	1.26	1.48	1.26	1.48	
Total	Dead Load	1.15	1.60	1.15	1.60
	Live Load	1.59	1.13	0.93	1.84
Allowable Value	$0.00 \leq \sigma \leq 12.0$				





01-3-PC-I GIRDER BRIDGE
(PF7-PF11)

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END 132

1.1 DESIGN CONDITION

ROAD GRADE	:	Equivalent to CLASS 4-1
BRIDGE TYPE	:	4 span continuous PC-I girder bridge with composite deck (PC plate and RC deck)
BRIDGE LENGTH	:	L = 120.000 m
SPAN LENGTH	:	L = 28.798 + 28.800 + 28.800 + 28.800 m
WIDTH OF THE ROAD	:	TOTAL 12.750 m L = 0.500 + 5.500 + 0.750 + 5.500 + 0.500 m
HORIZONTAL ALIGNMENT	:	A=130 ~ R=∞
LONGITUDINAL SLOPE	:	0.72 % 
SECTION SLOPE	:	LEFT : 3.83 % ~ 2.00 %  RIGHT : 3.77 %  ~ 2.00 % 
ANGLE OF SKEW	:	PF7 : 92°29'51" PF8 : 90°07'09" PF9,PF10,PF11 : 90°00'00"
PAVEMENT	:	ASPHALT PAVEMENT t= 80 mm
SLAB	:	REINFORCED CONCRETE t= 170 mm
PLATE	:	PRESTRESS CONCRETE PLATE t= 100 mm
LIVE ROAD	:	AASHTO HL=93
DESIGN STANDARD	:	AASHTO LRFD BRIDGE DESIGN 2014(LIVE ROAD) Specifications for highway bridges(Japan Road Association) 1 Common matters,3 Concrete bridges,5 seismic design (April 2012)

1.2 MATERIALS STRENGTH

1) CONCRETE

		(N/mm ²)				
		MAIN GIRDER	CROSS BEAM	RC SLAB	PC PLATE	COUPLING CONCRETE
DESIGN STANDARD STRENGTH OF CONCRETE		40.00	30.00	30.00	40.00	30.0
BENDING COMPRESSIVESTRESS	IMMEDIATELY AFTER PRESTRESSING	19.00	14.00	----	19.00	----
	OTHERS	14.00	11.00	10.00	15.00	10.00
BENDING TENSILE STRESS	IMMEDIATELY AFTER PRESTRESSING	-1.50	-1.20	----	-1.50	----
	DEAD LOAD	0.0	0.0	----	----	----
	DESIGN LOAD	-1.50	-1.20	----	0.0	----
	TEMPERATURE CHANGE	-2.00	----	----	----	----
MEAN SHEAR STRESS CONCRETE CAN CARRY		0.55	0.45	----	----	----
MAXIMUM MEAN CONCRETE SHEAR STRESS		5.30	4.00	----	----	----
ALLOWABLE DIAGONEL TENSILE STRESS (Case where shear force or torsional moment)	DEAD LOAD	-1.00	-0.80	----	----	----
	LIVE LOAD	-2.00	-1.70	----	----	----
ALLOWABLE DIAGONEL TENSILE STRESS (Case where both shear force and torsional moment)	DEAD LOAD	-1.30	-1.10	----	----	----
	LIVE LOAD	-2.50	-2.20	----	----	----

2) PC STRAND

		(N/mm ²)		
		MAIN GIRDER	CROSS BEAM	PC PLATE
PRESTRESSING STEEL TYPE		SWPR7BL 7S15.2mm	SWPR7BL 4S15.2mm	SWPR7AL 1S9.3mm
TENSILE STRENGTH		1850	1850	1700
YIELD POINT		1600	1600	1450
ALLOWABLE TENSILE STRESS	DURING PRESTRESSING	1440	1440	1305
	IMMEDIATELY AFTER PRESTRESSING	1295	1295	1190
	AT COMPOSITION OF SLAB	1110	----	----
	DESIGN LOAD	1110	1110	1020

3) REINFORCING STEEL

		(N/mm ²)			
		MAIN GIRDER	CROSS BEAM	RC SLAB	COUPLING CONCRETE
STEEL TYPE		SD345	SD345	SD345	SD345
YIELD POINT		345	345	345	345
ALLOWABLE TENSILE STRESS	DEAD LOAD	----	----	100	100
	DESIGN LOAD	180	200	140	160
	COLLISION LOAD	----	----	300	----
	WIND LOAD	----	----	175	----

1.3 DESIGN CONSTANT

1) CONCRETE

		MAIN GIRDER	CAST IN PLACE	PC PLATE
YOUNG'S MODULUS	DESIGN LOAD (N/mm ²)	3.10×10^4	2.80×10^4	3.10×10^4
	IMMEDIATELY AFTER PRESTRESSING (N/mm ²)	2.92×10^4	2.58×10^4	2.92×10^4
CREEP COEFFICIENT	NUMBER OF DAYS FOR DECK CONSTRUCTION	90	----	----
	NUMBER OF CONSTRUCTION DAYS FOR BRIDGE SURFACE	120	----	----
	DESIGN LOAD	2.60	2.60	3.00
	DURING DECK CONSTRUCTION	1.70	----	----
	BRIDGE SURFACE	1.65	----	----
DRYING SHRINKAGE OF CONCRETE	DURING DECK CONSTRUCTION	4.0×10^{-5}	----	----
	DESIGN LOAD	20.0×10^{-5}	20.0×10^{-5}	20.0×10^{-5}
UNIT WEIGHT (kN/mm ³)		24.5	24.5	24.5

2) PC STRAND(MAIN GIRDER)

		1	2
YOUNG'S MODULUS	N/mm ²	2.00×10^5	2.00×10^5
SLIP	mm	4.0	4.0
RELAXATION	%	2.5	2.5
FRICTION COEFFICIENT	1/m	0.004	0.004
	1/rad	0.300	0.300
AREA	mm ²	970.900	970.900
UNIT WEIGHT	kg/m	7.707	7.707
DIAMETER OF SHEATH	mm	60.0	60.0
DECREASE RATIO BY ANCHOR	%	0.0	0.0

3) PC STRAND(CROSS BEAM)

YOUNG'S MODULUS	N/mm ²	2.00×10^5
SLIP	mm	4.0
RELAXATION	%	2.5
FRICTION COEFFICIENT	1/m	0.004
AREA	mm ²	554.800
UNIT WEIGHT	kg/m	4.404
DIAMETER OF SHEATH	mm	45.0
DECREASE RATIO BY ANCHOR	%	0.0

4) PC STRAND(PC PLATE)

		BETWEEN MAIN GIRDERS	
YOUNG'S MODULUS		N/mm ²	2.00 × 10 ⁵
RELAXATION	BEFORE PRESTRESSING	%	1.5
	AFTER PRESTRESSING	%	1.5
	EXTRA COEFFICIENT OF HIGH TEMPERATURE	%	1.0
AREA		mm ²	51.610
UNIT WEIGHT		kg/m	0.405

1. 5 Dimension

1) Dimension of Main Girder

Girder Height : 2000.00 ~ 2000.00 mm

【Change of Web Width (mm)】

Span	End of Girder (Left Side)			End of Girder (Right Side)		
	Ending Point of Changing Web Width	Starting Point of Changing Web Width	Web Width	Ending Point of Changing Web Width	Starting Point of Changing Web Width	Web Width
1	1000.0	4000.0	700.0	4000.0	1000.0	700.0
2	1000.0	4000.0	700.0	4000.0	1000.0	700.0
3	1000.0	4000.0	700.0	4000.0	1000.0	700.0
4	1000.0	4000.0	700.0	4000.0	1000.0	700.0

2) Dimension of Cross Beam

【Interval of Cross Beam on Left Girder (m)】

Span	Number of Intermediate Cross Beams	CB1~CB2	CB2~CB3
1	1	14.899	14.899
2	1	14.900	14.900
3	1	14.900	14.900
4	1	14.900	14.900

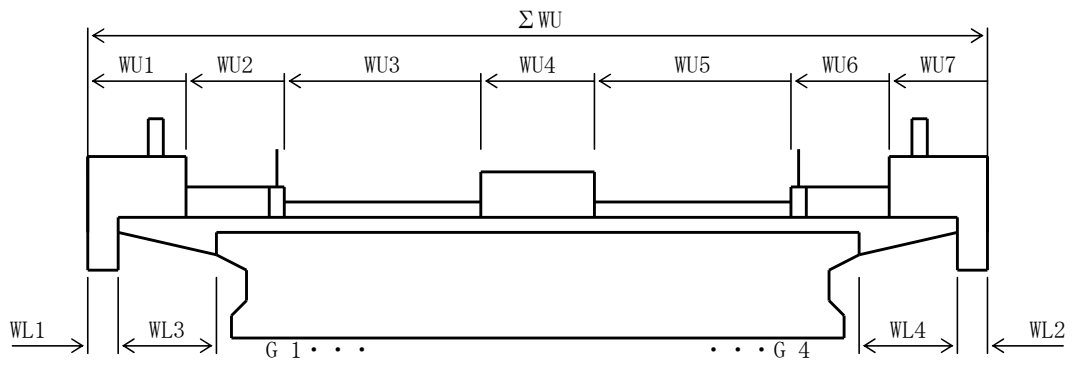
【Interval of Cross Beam on Right Girder (m)】

Span	Number of Intermediate Cross Beams	CB1~CB2	CB2~CB3
1	1	14.899	14.899
2	1	14.900	14.900
3	1	14.900	14.900
4	1	14.900	14.900

【Dimension of Cross Beam (m)】

Span	Cross Beam Width	Cross Beam Width (Left Side)	Cross Beam Width (Right Side)
1	0.300	0.900	1.000
2	0.300	1.000	1.000
3	0.300	1.000	1.000
4	0.300	1.000	0.900

【Cross Section】



【m】

	ΣWU	WU1	WU2	WU3	WU4	WU5	WU6	WU7
1	12.762	0.500	0.000	5.505	0.751	5.505	0.000	0.500
2	12.750	0.500	0.000	5.500	0.750	5.500	0.000	0.500
3	12.750	0.500	0.000	5.500	0.750	5.500	0.000	0.500
4	12.750	0.500	0.000	5.500	0.750	5.500	0.000	0.500
5	12.750	0.500	0.000	5.500	0.750	5.500	0.000	0.500

	ΣWU	WL1	WL2	WL3	WL4
1	3.500	0.000	0.000	0.487	0.475
2	3.500	0.000	0.000	0.479	0.471
3	3.500	0.000	0.000	0.475	0.475
3	3.500	0.000	0.000	0.475	0.475
3	3.500	0.000	0.000	0.475	0.475

2. 1 Load Intensity

1) Load Intensity

(1) Bridge Surface Loads

< 1 >

Load Type		Load Intensity	Load Location	
			Left End of Girder Side	Right End of Girder Side
Selfweight of Kerb	Left	9.020 kN/m	0.180 m	0.180 m
	Right	11.630 kN/m	0.200 m	0.200 m
Selfweight of Concrete Barrier	Left	0.600 kN/m	0.125 m	0.125 m
	Right	0.600 kN/m	0.125 m	0.125 m
Selfweight of Sidewalk	Left	0.000 kN/m ²		
	Right	0.000 kN/m ²		
Selfweight of Handrail	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Kerb	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Pavement	Left	4.150 kN/m ²		
	Right	6.610 kN/m ²		
Selfweight of Median		12.190 kN/m ²		
Selfweight of Additional Object	1	0.110 kN/m	0.075 m	0.075 m
	2	0.110 kN/m	12.686 m	12.675 m

< 2 >

Load Type		Load Intensity	Load Location	
			Left End of Girder Side	Right End of Girder Side
Selfweight of Kerb	Left	8.570 kN/m	0.180 m	0.180 m
	Right	8.690 kN/m	0.180 m	0.180 m
Selfweight of Concrete Barrier	Left	0.600 kN/m	0.125 m	0.125 m
	Right	0.600 kN/m	0.125 m	0.125 m
Selfweight of Sidewalk	Left	0.000 kN/m ²		
	Right	0.000 kN/m ²		
Selfweight of Handrail	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Kerb	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Pavement	Left	3.070 kN/m ²		
	Right	3.180 kN/m ²		
Selfweight of Median		10.790 kN/m ²		
Selfweight of Additional Object	1	0.110 kN/m	0.075 m	0.075 m
	2	0.110 kN/m	12.675 m	12.675 m

< 3 >

Load Type		Load Intensity	Load Location	
			Left End of Girder Side	Right End of Girder Side
Selfweight of Kerb	Left	8.570 kN/m	0.180 m	0.180 m
	Right	8.570 kN/m	0.180 m	0.180 m
Selfweight of Concrete Barrier	Left	0.600 kN/m	0.125 m	0.125 m
	Right	0.600 kN/m	0.125 m	0.125 m
Selfweight of Sidewalk	Left	0.000 kN/m ²		
	Right	0.000 kN/m ²		
Selfweight of Handrail	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Kerb	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Pavement	Left	3.070 kN/m ²		
	Right	3.070 kN/m ²		
Selfweight of Median		10.790 kN/m ²		
Selfweight of Additional Object	1	0.110 kN/m	0.075 m	0.075 m
	2	0.110 kN/m	12.675 m	12.675 m

< 4 >

Load Type		Load Intensity	Load Location	
			Left End of Girder Side	Right End of Girder Side
Selfweight of Kerb	Left	8.570 kN/m	0.180 m	0.180 m
	Right	8.570 kN/m	0.180 m	0.180 m
Selfweight of Concrete Barrier	Left	0.600 kN/m	0.125 m	0.125 m
	Right	0.600 kN/m	0.125 m	0.125 m
Selfweight of Sidewalk	Left	0.000 kN/m ²		
	Right	0.000 kN/m ²		
Selfweight of Handrail	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Kerb	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Pavement	Left	3.070 kN/m ²		
	Right	3.070 kN/m ²		
Selfweight of Median		10.790 kN/m ²		
Selfweight of Additional Object	1	0.110 kN/m	0.075 m	0.075 m
	2	0.110 kN/m	12.675 m	12.675 m

Condition of Load

Calculation of Bridge Surface Loads

(PF7-PF8)

① Unit Weight

PC · RC Concrete	$\gamma_1 = 24.5 \text{ kN/m}^3$
Concrete	$\gamma_2 = 23.0 \text{ kN/m}^3$
Asphalt Pavement	$\gamma_3 = 22.5 \text{ kN/m}^3$

② Bridge Surface Loads

- Pavement on Left Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = 1/2 \times (0.117 + 0.247) = 0.182 \text{ m}$$

(Thickness of Leveling Concrete)

$$t_c = 0.182 - 0.080 = 0.102 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.102 \times 23.0 = \underline{4.15 \text{ kN/m}^2}$$

- Pavement on Right Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = 1/2 \times (0.247 + 0.330) = 0.289 \text{ m}$$

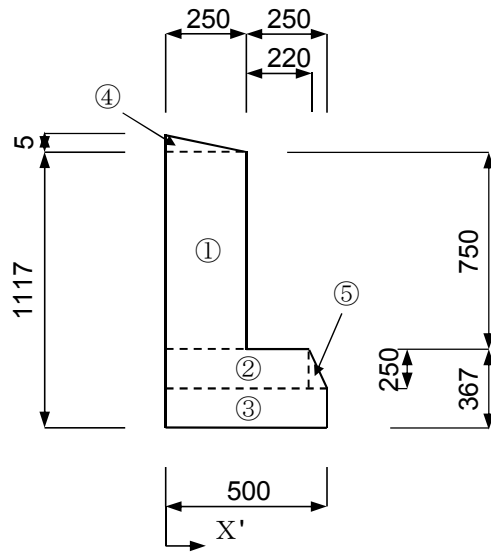
(Thickness of Leveling Concrete)

$$t_c = 0.289 - 0.080 = 0.209 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.209 \times 23.0 = \underline{6.61 \text{ kN/m}^2}$$

• Concrete Barrier (Left Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.117	0.500	0.0585	0.250	0.01463
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3679		0.0675

Load Location

$$X' = 0.0675 / 0.3679$$

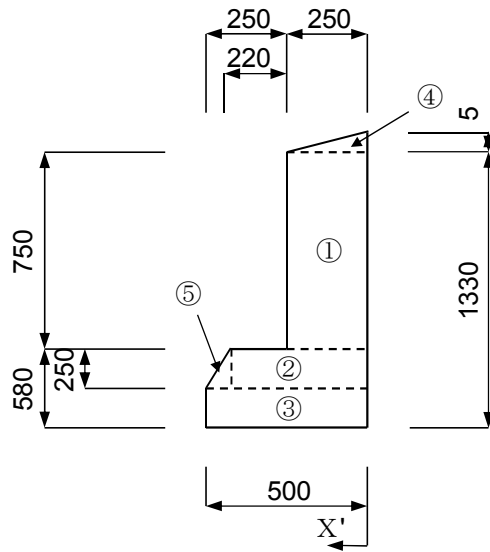
$$= \underline{0.180 \text{ m}}$$

Load Intensity

$$P = 0.3679 \times 24.5$$

$$= \underline{9.02 \text{ kN/m}}$$

• Concrete Barrier (Right Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.330	0.500	0.1650	0.250	0.04125
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.4744		0.0942

Load Location

$$X' = 0.0942 / 0.4744$$

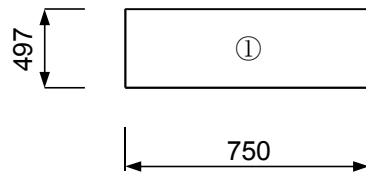
$$= \underline{0.200 \text{ m}}$$

Load Intensity

$$P = 0.4744 \times 24.5$$

$$= \underline{11.63 \text{ kN/m}}$$

• Median



a) Load Intensity and Load Location

	H	B	A
① □	0.4970	0.7500	0.3728
			0.3728

Load Location

X' = On CL

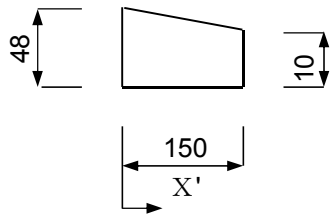
Load Intensity

$$P = 0.3728 \times 24.5 = \underline{\underline{9.14 \text{ kN/m}}}$$

$$W = 9.1400 / 0.750 = \underline{\underline{12.19 \text{ kN/m}^2}}$$

• Left Drain Duct

※Loaded as Selfweight of Additional Object 1



Load Location

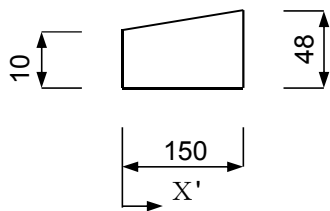
$X' = 75\text{mm}$ inside beginning of Left Kerb

Load Intensity

$$P = 1/2 \times (0.048 + 0.010) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Right Drain Duct

※Loaded as Selfweight of Additional Object 2



Load Location

$X' = 75\text{mm}$ inside beginning of Right Kerb

Load Intensity

$$P = 1/2 \times (0.010 + 0.048) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Handrail

※Loaded as Concrete Barrier

Load Location

$X' = 125\text{mm}$ inside beginning of Right and Left Kerb

Load Intensity

$$P = 0.60 = \underline{0.60 \text{ kN/m}}$$

Condition of Load

Calculation of Bridge Surface Loads

(PF8-PF9)

① Unit Weight

PC · RC Concrete	$\gamma_1 = 24.5 \text{ kN/m}^3$
Concrete	$\gamma_2 = 23.0 \text{ kN/m}^3$
Asphalt Pavement	$\gamma_3 = 22.5 \text{ kN/m}^3$

② Bridge Surface Loads

- Pavement on Left Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = 1/2 \times (0.080 + 0.190) = 0.135 \text{ m}$$

(Thickness of Leveling Concrete)

$$t_c = 0.135 - 0.080 = 0.055 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.055 \times 23.0 = \underline{\underline{3.07 \text{ kN/m}^2}}$$

- Pavement on Right Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = 1/2 \times (0.190 + 0.090) = 0.140 \text{ m}$$

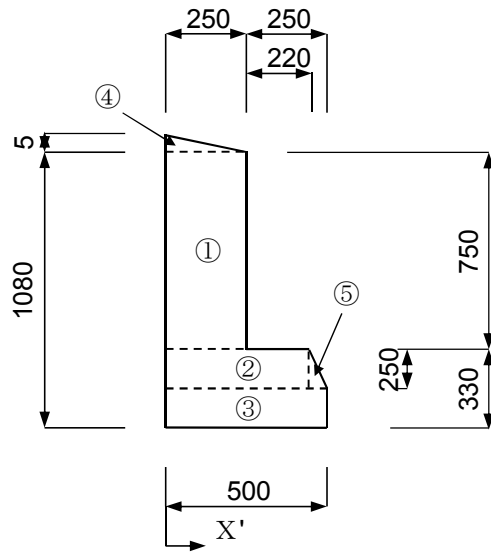
(Thickness of Leveling Concrete)

$$t_c = 0.140 - 0.080 = 0.060 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.060 \times 23.0 = \underline{\underline{3.18 \text{ kN/m}^2}}$$

• Concrete Barrier (Left Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.080	0.500	0.0400	0.250	0.01000
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3494		0.0629

Load Location

$$X' = 0.0629 / 0.3494$$

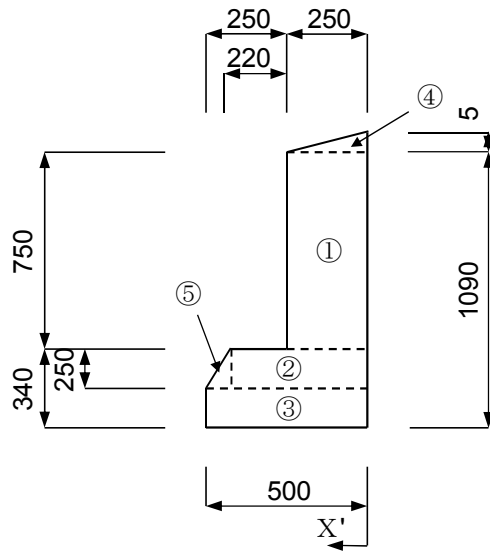
$$= \underline{0.180 \text{ m}}$$

Load Intensity

$$P = 0.3494 \times 24.5$$

$$= \underline{8.57 \text{ kN/m}}$$

• Concrete Barrier (Right Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.090	0.500	0.0450	0.250	0.01125
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3544		0.0642

Load Location

$$X' = 0.0642 / 0.3544$$

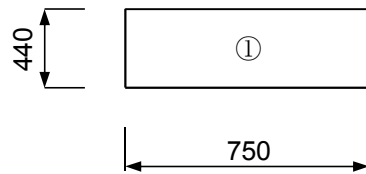
$$= \underline{0.180 \text{ m}}$$

Load Intensity

$$P = 0.3544 \times 24.5$$

$$= \underline{8.69 \text{ kN/m}}$$

• Median



a) Load Intensity and Load Location

		H	B	A
①	□	0.4400	0.7500	0.3300
				0.3300

Load Location

X' = On CL

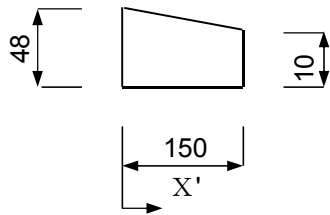
Load Intensity

$$P = 0.3300 \times 24.5 = \underline{8.09 \text{ kN/m}}$$

$$W = 8.0900 / 0.750 = \underline{10.79 \text{ kN/m}^2}$$

• Left Drain Duct

※Loaded as Selfweight of Additional Object 1



Load Location

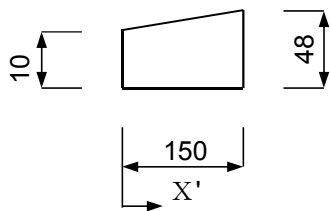
$X' = 75\text{mm}$ inside beginning of Left Kerb

Load Intensity

$$P = 1/2 \times (0.048 + 0.010) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Right Drain Duct

※Loaded as Selfweight of Additional Object 2



Load Location

$X' = 75\text{mm}$ inside beginning of Right Kerb

Load Intensity

$$P = 1/2 \times (0.010 + 0.048) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Handrail

※Loaded as Concrete Barrier

Load Location

$X' = 125\text{mm}$ inside beginning of Right and Left Kerb

Load Intensity

$$P = 0.60 = \underline{0.60 \text{ kN/m}}$$

Condition of Load

Calculation of Bridge Surface Loads

(PF9-PF11)

① Unit Weight

PC · RC Concrete	$\gamma_1 = 24.5 \text{ kN/m}^3$
Concrete	$\gamma_2 = 23.0 \text{ kN/m}^3$
Asphalt Pavement	$\gamma_3 = 22.5 \text{ kN/m}^3$

② Bridge Surface Loads

- Pavement on Left Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = \frac{1}{2} \times (0.080 + 0.190) = 0.135 \text{ m}$$

(Thickness of Leveling Concrete)

$$t_c = 0.135 - 0.080 = 0.055 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.055 \times 23.0 = \underline{\underline{3.07 \text{ kN/m}^2}}$$

- Pavement on Right Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = \frac{1}{2} \times (0.190 + 0.080) = 0.135 \text{ m}$$

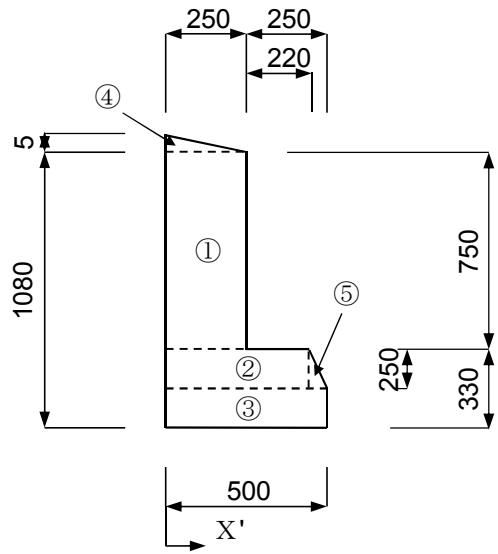
(Thickness of Leveling Concrete)

$$t_c = 0.135 - 0.080 = 0.055 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.055 \times 23.0 = \underline{\underline{3.07 \text{ kN/m}^2}}$$

• Concrete Barrier (Left Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.080	0.500	0.0400	0.250	0.01000
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3494		0.0629

Load Location

$$X' = 0.0629 / 0.3494$$

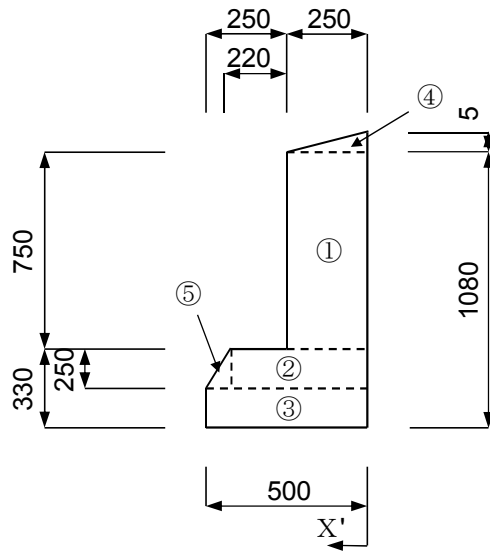
$$= \underline{0.180 \text{ m}}$$

Load Intensity

$$P = 0.3494 \times 24.5$$

$$= \underline{8.57 \text{ kN/m}}$$

• Concrete Barrier (Right Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.080	0.500	0.0400	0.250	0.01000
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3494		0.0629

Load Location

$$X' = 0.0629 / 0.3494$$

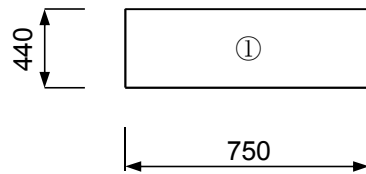
$$= \underline{0.180 \text{ m}}$$

Load Intensity

$$P = 0.3494 \times 24.5$$

$$= \underline{8.57 \text{ kN/m}}$$

• Median



a) Load Intensity and Load Location

	H	B	A
① □	0.4400	0.7500	0.3300
			0.3300

Load Location

X' = On CL

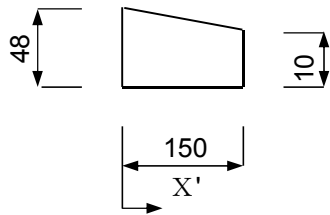
Load Intensity

$$P = 0.3300 \times 24.5 = \underline{8.09 \text{ kN/m}}$$

$$W = 8.0900 / 0.750 = \underline{10.79 \text{ kN/m}^2}$$

• Left Drain Duct

※Loaded as Selfweight of Additional Object 1



Load Location

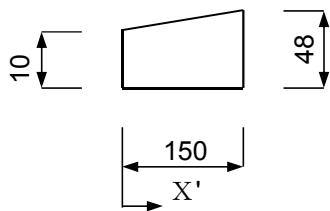
$X' = 75\text{mm}$ inside beginning of Left Kerb

Load Intensity

$$P = 1/2 \times (0.048 + 0.010) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Right Drain Duct

※Loaded as Selfweight of Additional Object 2



Load Location

$X' = 75\text{mm}$ inside beginning of Right Kerb

Load Intensity

$$P = 1/2 \times (0.010 + 0.048) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Handrail

※Loaded as Concrete Barrier

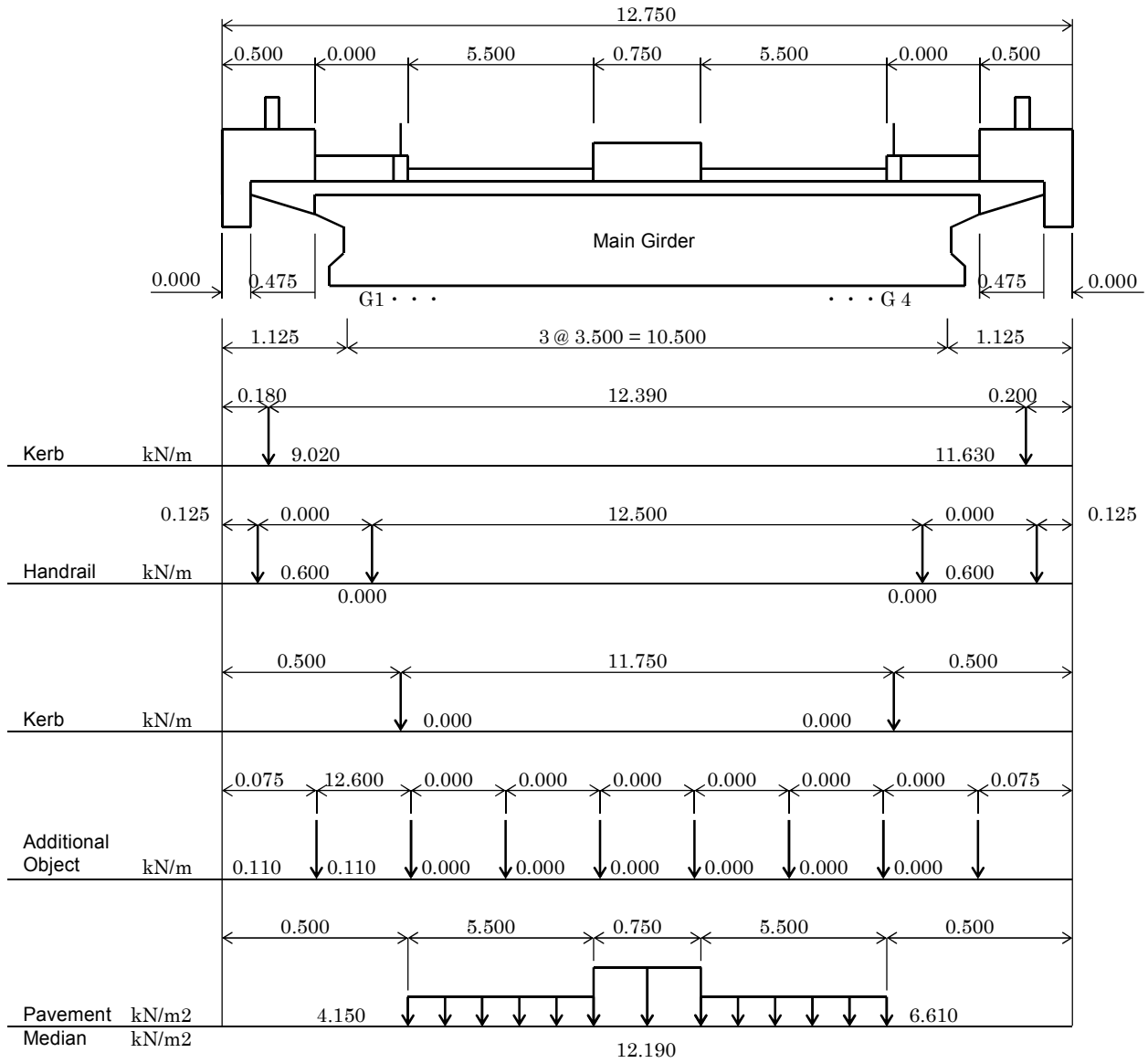
Load Location

$X' = 125\text{mm}$ inside beginning of Right and Left Kerb

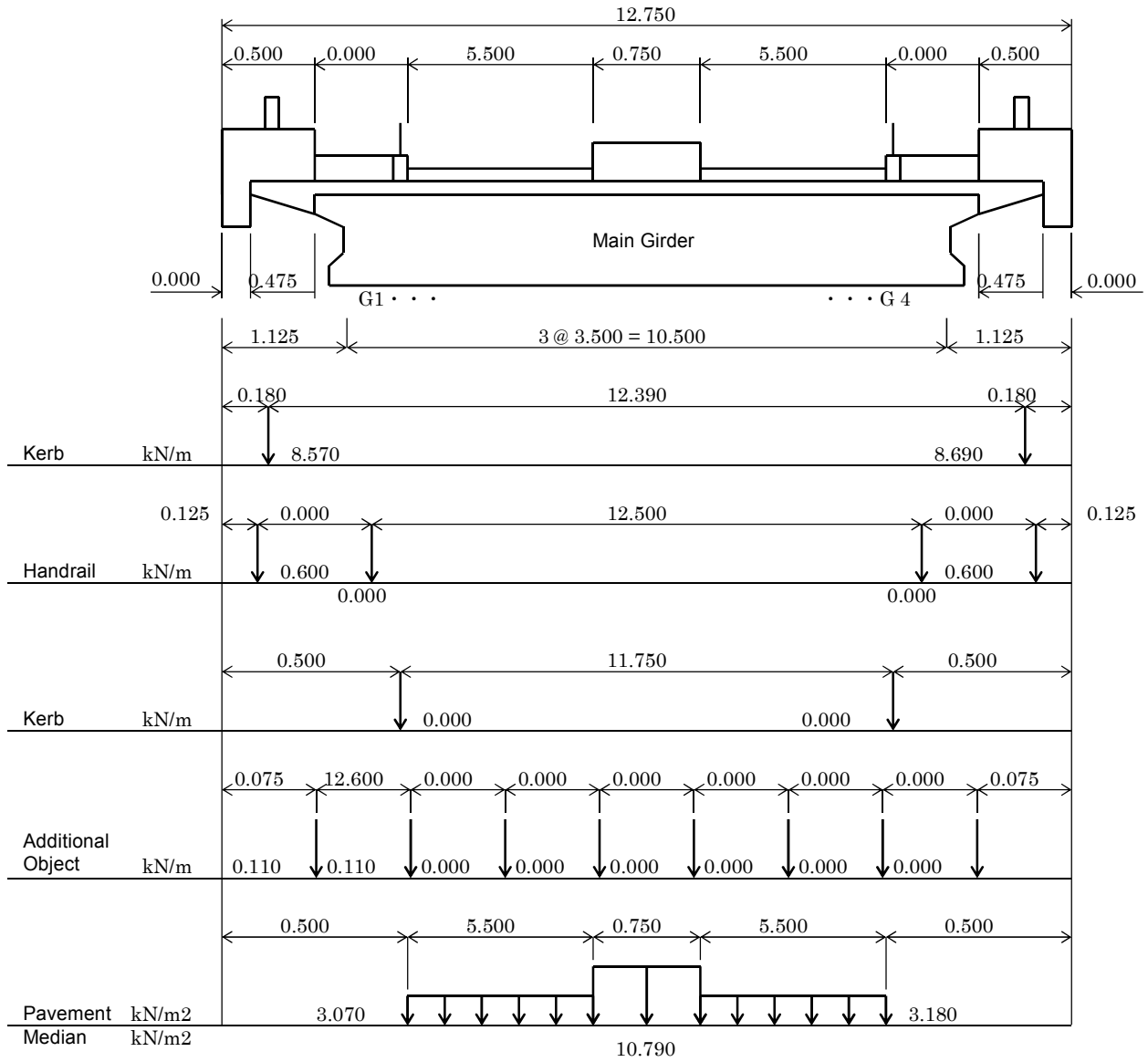
Load Intensity

$$P = 0.60 = \underline{0.60 \text{ kN/m}}$$

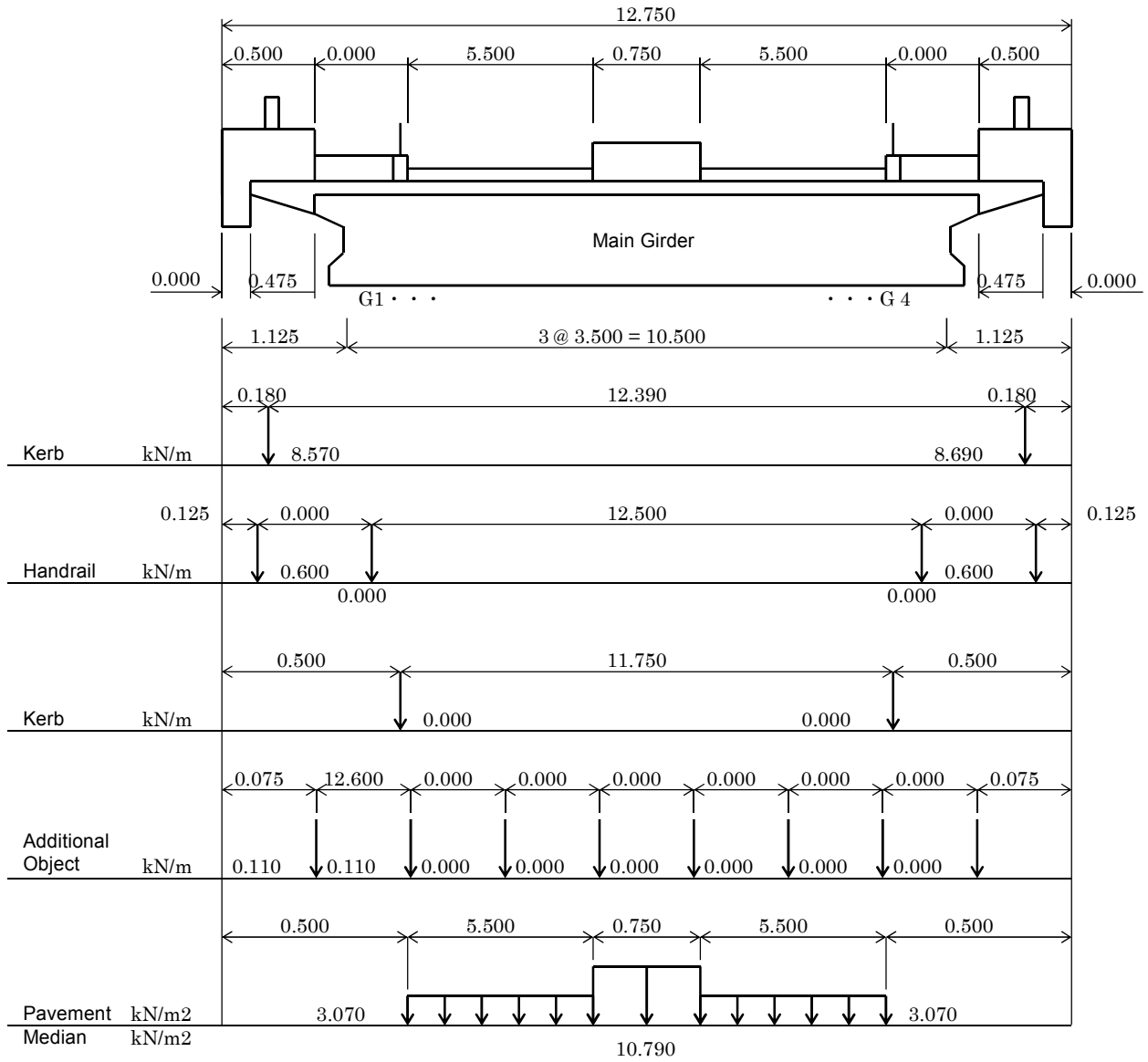
Load Intensity (Bridge Surface Loads_PF7-PF8)



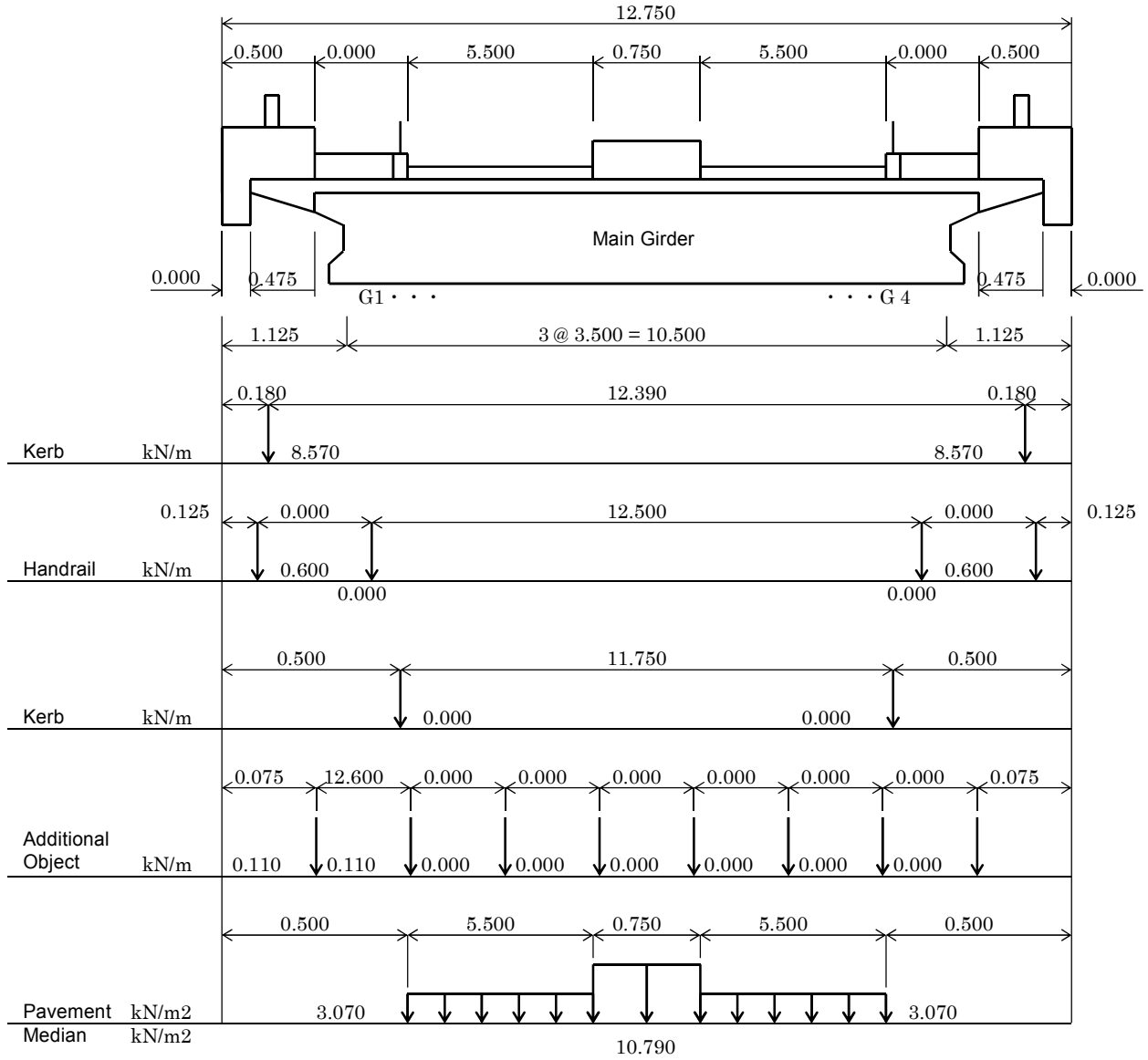
Load Intensity (Bridge Surface Loads_PF8-PF9)



Load Intensity (Bridge Surface Loads_PF9-PF10)



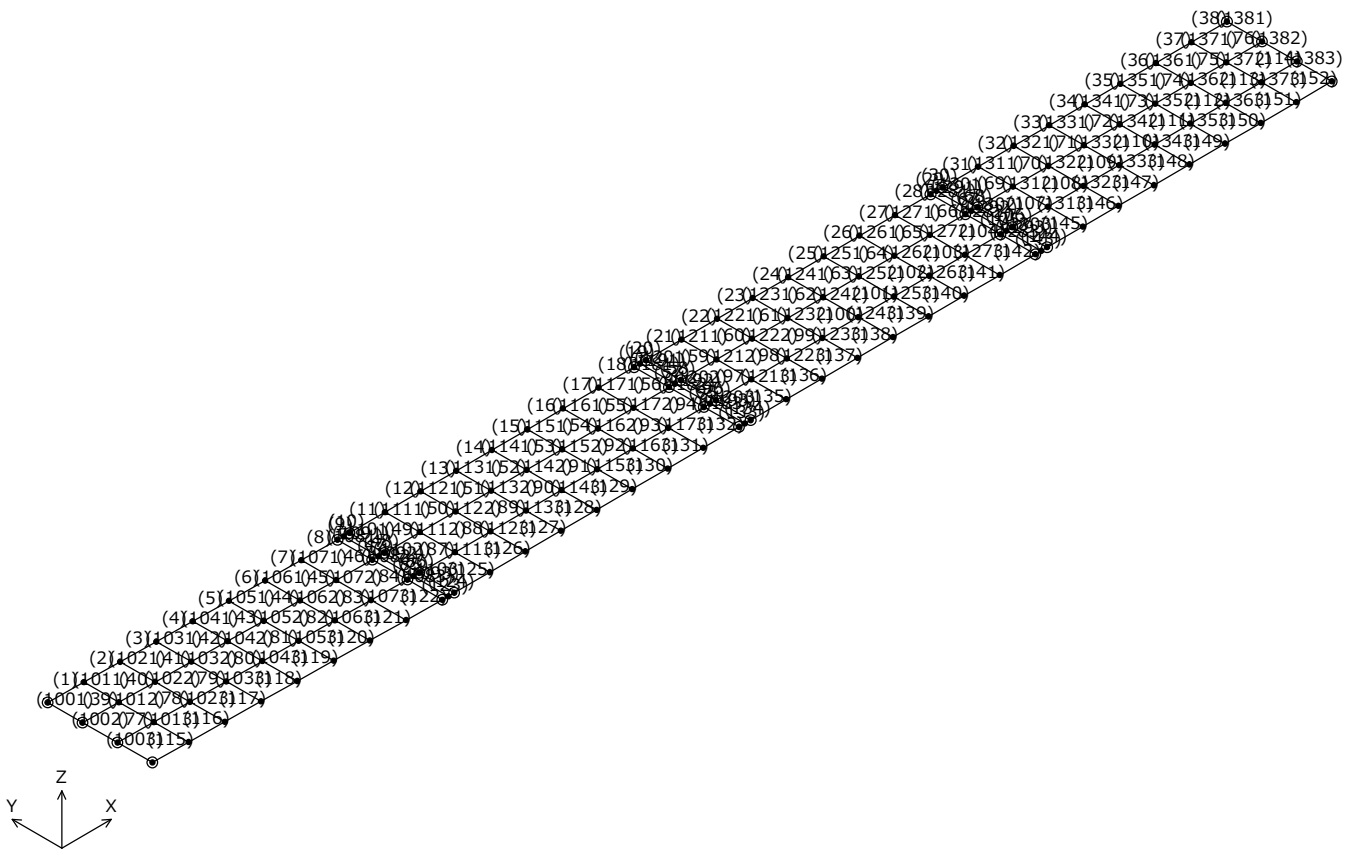
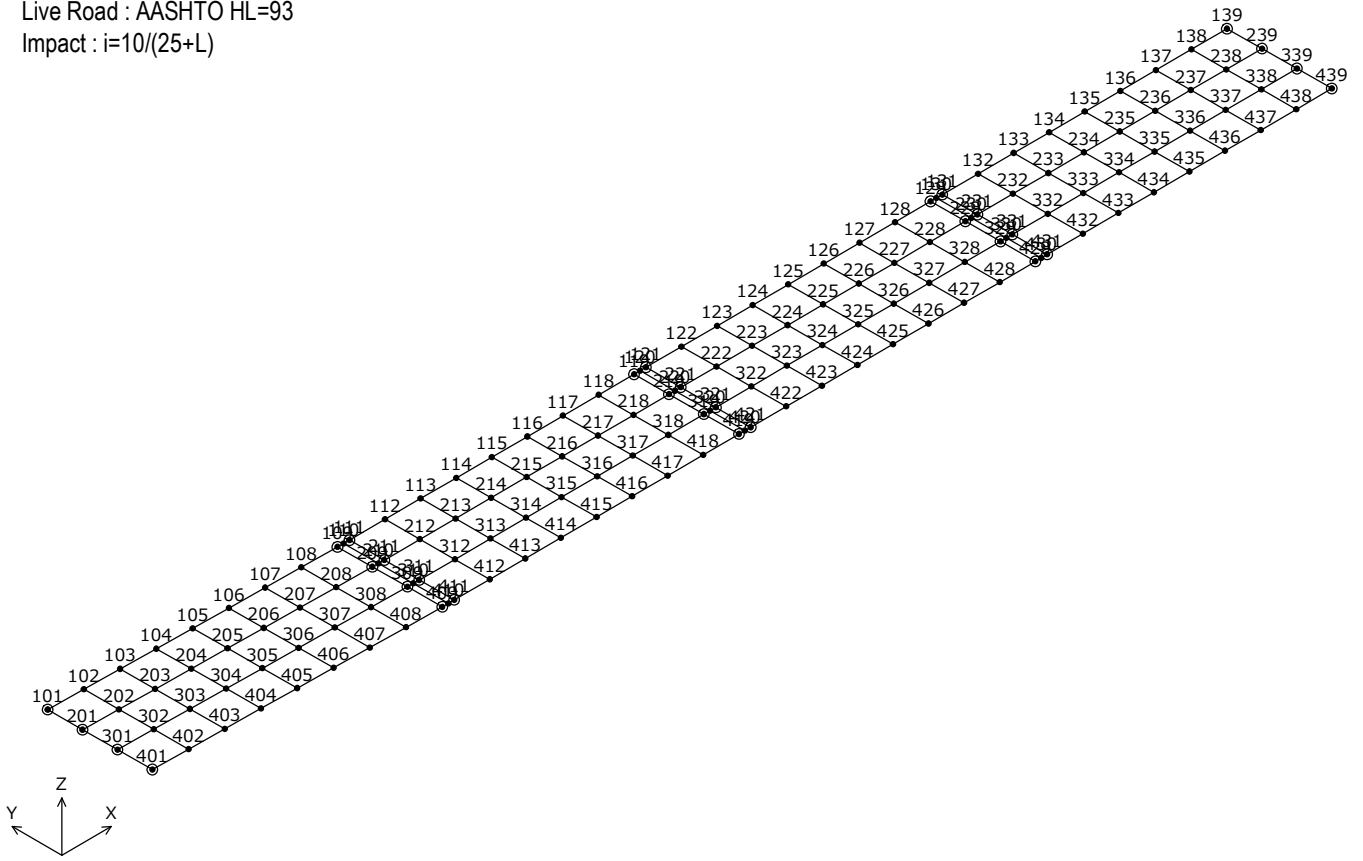
Load Intensity (Bridge Surface Loads_PF10-PF11)

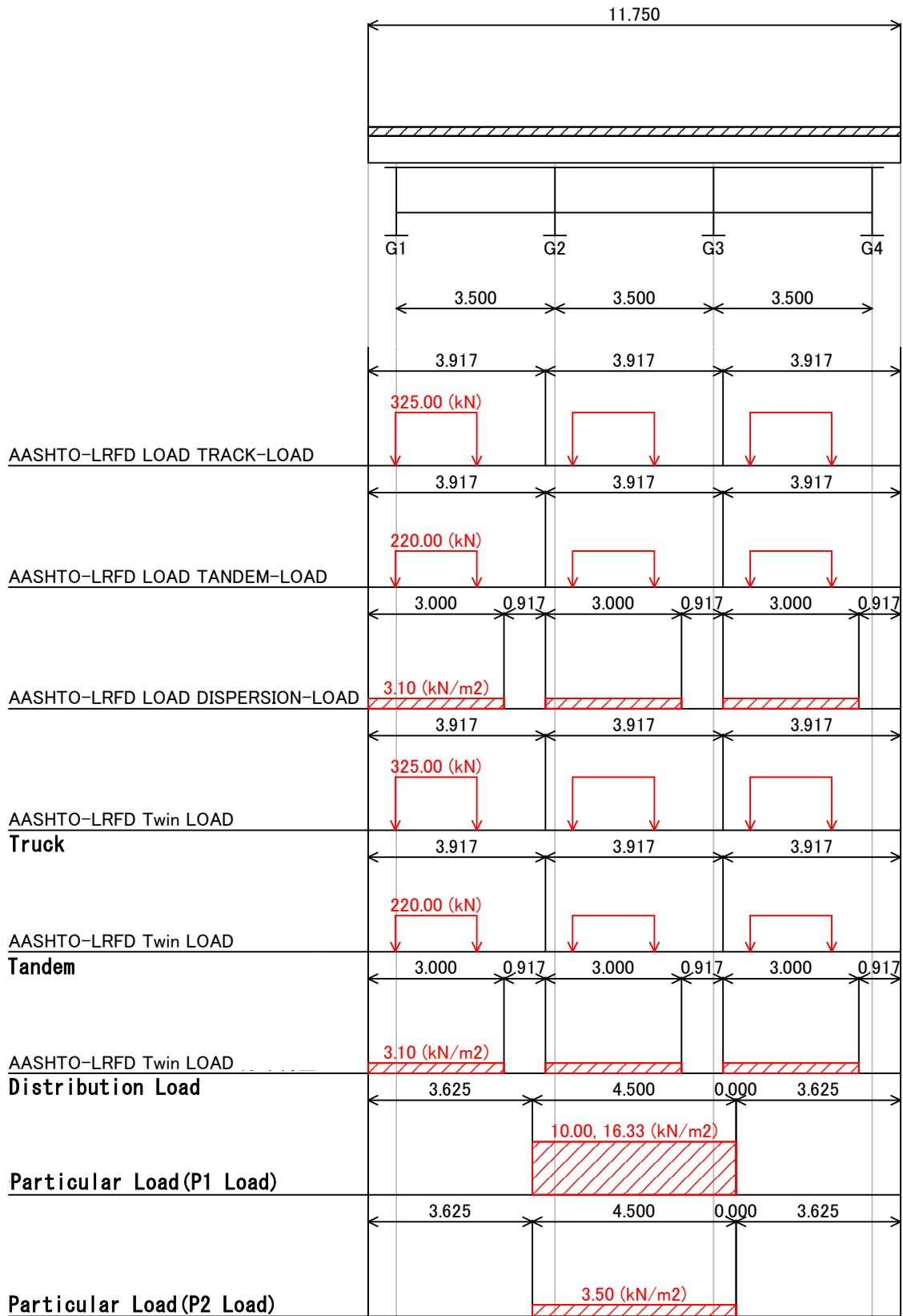


(2) Live Road

Live Road : AASHTO HL=93

Impact : $i=10/(25+L)$

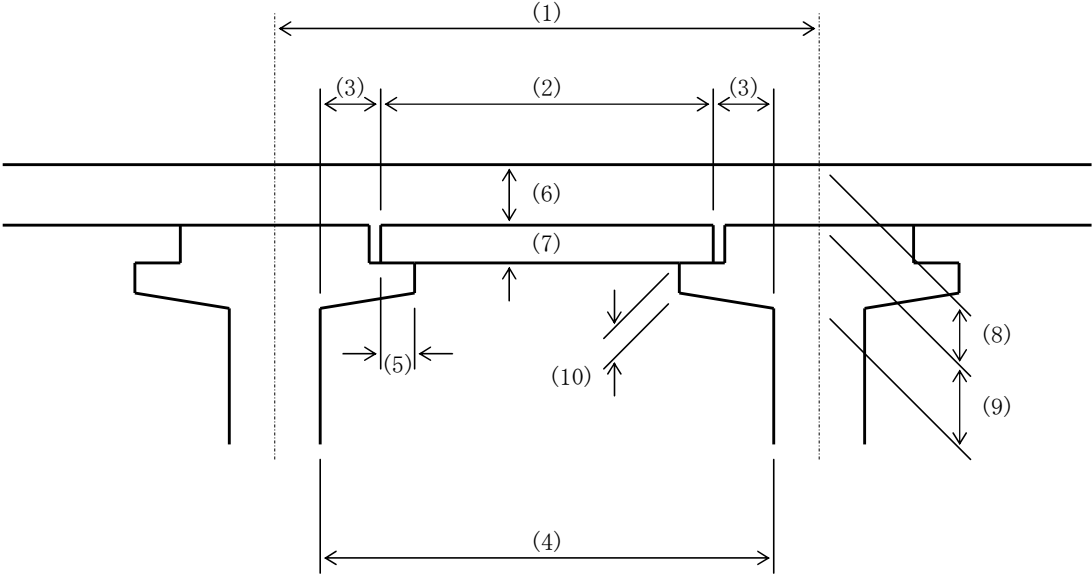




3 Design of Deck Slab

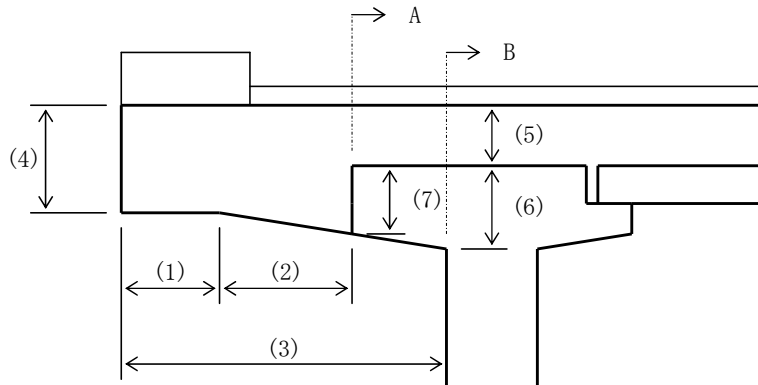
3.1 Dimension

1) Deck Slab between Girders



		1st Span		4th Span
		End of Girder	Center of Girder	Center of Girder
(1)	m	3.500	3.500	3.500
(2)	m	2.380	2.380	2.380
(3)	m	0.210	0.450	0.450
(4)	m	2.800	3.280	3.280
(5)	m	0.090	0.090	0.090
Span Length of PC Plate		2.260	2.260	2.260
(6)	mm	170.0	170.0	170.0
(7)	mm	100.0	100.0	100.0
(6)+(7)	mm	270.0	270.0	270.0
(8)	mm	170.0	170.0	170.0
(9)	mm	255.6	300.0	300.0
(10)	mm	100.0	100.0	100.0

2) Deck Slab outside of Girders



			1st Span		4th Span
			End of Girder	Center of Girder	Center of Girder
Left Side	(1)	m	0.000	0.000	0.000
	(2)	m	0.484	0.484	0.475
	(3)	m	0.784	1.024	1.015
	(4)	mm	250.0	250.0	250.0
	(5)	mm	170.0	170.0	170.0
	(6)	mm	255.6	300.0	300.0
	(7)	mm	200.0	200.0	200.0
Right Side	(1)	m	0.000	0.000	0.000
	(2)	m	0.626	0.626	0.475
	(3)	m	0.926	1.166	1.015
	(4)	mm	250.0	250.0	250.0
	(5)	mm	170.0	170.0	170.0
	(6)	mm	255.6	300.0	300.0
	(7)	mm	200.0	200.0	200.0

3) Calculation of Prestressing of PC Plate

		Unit	
Name of PC Strand			1S9.3
Material of PC Strand			SWPR7AL
Area of PC Strand		mm ² /no.	51.61
Number of PC Strand		No.	15
Creep Coefficient			3.00
Drying Shrinkage of Concrete		×10 ⁻⁵	25.00
Relaxation	Before Prestressing	%	1.50
	Extra Coefficient of High Temperature	%	1.00
	After Prestressing	%	1.50
Prestressing Stress σ_{pi}		N/mm ²	1225.00
Allowable Value		N/mm ²	1305.00

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Left End of Girder Side

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item	Unit	Allowable Value	Result
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5
	Bottom of PC Plate	N/mm ²	~19.0
	Max×0.6	N/mm ²	8.343
Bending stress of PC plate	Top of PC Plate	N/mm ²	0
	Bottom of PC Plate	N/mm ²	~15.0
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11
	Bottom of RC Deck	N/mm ²	11
	Top of PC Plate	N/mm ²	0
	Bottom of PC Plate	N/mm ²	~15.0
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305
	Immediately After Prestressing	N/mm ²	1190
	Effective Prestressing Force	N/mm ²	1020
Axial stress of PC plate	N/mm ²	10	

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.707	○	140	77.98	○	
Edge of PC Plate	Positive Moment	10	4.147	○	140	64.431	○
	Negative Moment	10	3.966	○	140	83.041	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	8.659	○	140	100.221	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	0.56	○
Tensile Stress of Reinforcement Bar	140	27.98	○

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Left End of Girder Side

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	5.77	○
	D+L	10	0.22	○	140	5.77	○
	D+L+CO	15	2.057	○	300	53.913	○
	D+L+W	12.5	0.365	○	175	9.569	○
	D+W	12.5	0.51	○	175	13.367	○
Supporting for Deck	D	-----	-----	--	100	10.797	○
	D+L	10	1.4	○	140	40.323	○
	D+L+CO	15	2.852	○	300	82.152	○
	D+L+W	12.5	1.516	○	175	43.665	○
	D+W	12.5	0.607	○	175	17.481	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	10.172	○
	D+L	10	0.388	○	140	10.172	○
	D+L+CO	15	2.225	○	300	58.315	○
	D+L+W	12.5	0.533	○	175	13.971	○
	D+W	12.5	0.678	○	175	17.769	○
Supporting for Deck	D	-----	-----	--	100	16.433	○
	D+L	10	3.831	○	140	110.346	○
	D+L+CO	15	5.283	○	300	152.176	○
	D+L+W	12.5	3.947	○	175	113.688	○
	D+W	12.5	0.803	○	175	23.117	○

Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	1.634	○	140	59.09	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	1.892	○	140	68.406	○

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Center of Span

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item		Unit	Allowable Value	Result	
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5	9.17	○
	Bottom of PC Plate	N/mm ²		8.343	○
	Max×0.6	N/mm ²	8.343	5.502	○
Bending stress of PC plate	Top of PC Plate	N/mm ²	0	10.615	○
	Bottom of PC Plate	N/mm ²		3.726	○
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11	4.53	○
	Bottom of RC Deck	N/mm ²		-1.041	○
	Top of PC Plate	N/mm ²	0	8.122	○
	Bottom of PC Plate	N/mm ²		0.286	○
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305	1225	○
	Immediately After Prestressing	N/mm ²	1190	1131.097	○
	Effective Prestressing Force	N/mm ²	1020	926.235	○
Axial stress of PC plate		N/mm ²	10	8.756	○

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.697	○	140	82.954	○	
Edge of PC Plate	Positive Moment	10	7.196	○	140	111.805	○
	Negative Moment	10	3.447	○	140	72.189	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	9.958	○	140	115.254	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	1.002	○
Tensile Stress of Reinforcement Bar	140	55.499	○

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Center of Span

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	5.77	○
	D+L	10	0.22	○	140	5.77	○
	D+L+CO	15	2.057	○	300	53.913	○
	D+L+W	12.5	0.365	○	175	9.569	○
	D+W	12.5	0.51	○	175	13.367	○
Supporting for Deck	D	-----	-----	--	100	14.428	○
	D+L	10	2.143	○	140	65.917	○
	D+L+CO	15	3.379	○	300	103.902	○
	D+L+W	12.5	2.243	○	175	68.981	○
	D+W	12.5	0.668	○	175	20.556	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	10.159	○
	D+L	10	0.388	○	140	10.159	○
	D+L+CO	15	2.225	○	300	58.302	○
	D+L+W	12.5	0.533	○	175	13.958	○
	D+W	12.5	0.678	○	175	17.756	○
Supporting for Deck	D	-----	-----	--	100	20.153	○
	D+L	10	2.604	○	140	80.077	○
	D+L+CO	15	3.839	○	300	118.061	○
	D+L+W	12.5	2.703	○	175	83.141	○
	D+W	12.5	0.855	○	175	26.28	○

Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	2.07	○	140	74.836	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	2.327	○	140	84.152	○

<Design of Deck: Summary for Calculation Results of Stress>

4th Span, Center of Span

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item		Unit	Allowable Value	Result	
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5	9.17	○
	Bottom of PC Plate	N/mm ²		~19.0	8.343
	Max×0.6	N/mm ²	8.343	5.502	○
Bending stress of PC plate	Top of PC Plate	N/mm ²	0	10.59	○
	Bottom of PC Plate	N/mm ²		~15.0	3.697
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11	4.225	○
	Bottom of RC Deck	N/mm ²		-0.97	○
	Top of PC Plate	N/mm ²	0	8.174	○
	Bottom of PC Plate	N/mm ²		~15.0	0.58
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305	1225	○
	Immediately After Prestressing	N/mm ²	1190	1131.097	○
	Effective Prestressing Force	N/mm ²	1020	922.752	○
Axial stress of PC plate		N/mm ²	10	8.756	○

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.556	○	140	78.616	○	
Edge of PC Plate	Positive Moment	10	6.711	○	140	104.266	○
	Negative Moment	10	3.267	○	140	68.414	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete		Tensile Stress of Reinforcement Bar			
	Allowable Value	Result	Allowable Value	Result		
Center of RC Deck	10	9.958	○	140	115.254	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	1.002	○
Tensile Stress of Reinforcement Bar	140	55.499	○

<Design of Deck: Summary for Calculation Results of Stress>

4th Span, Center of Span

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	5.392	○
	D+L	10	0.206	○	140	5.392	○
	D+L+CO	15	2.043	○	300	53.535	○
	D+L+W	12.5	0.351	○	175	9.191	○
	D+W	12.5	0.496	○	175	12.99	○
Supporting for Deck	D	-----	-----	--	100	13.776	○
	D+L	10	2.099	○	140	64.554	○
	D+L+CO	15	3.334	○	300	102.538	○
	D+L+W	12.5	2.199	○	175	67.618	○
	D+W	12.5	0.647	○	175	19.904	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	5.392	○
	D+L	10	0.206	○	140	5.392	○
	D+L+CO	15	2.043	○	300	53.535	○
	D+L+W	12.5	0.351	○	175	9.191	○
	D+W	12.5	0.496	○	175	12.99	○
Supporting for Deck	D	-----	-----	--	100	13.776	○
	D+L	10	2.099	○	140	64.554	○
	D+L+CO	15	3.334	○	300	102.538	○
	D+L+W	12.5	2.199	○	175	67.618	○
	D+W	12.5	0.647	○	175	19.904	○

Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	2.053	○	140	74.245	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	2.053	○	140	74.245	○

<Design of Deck: Summary for Calculation Results of Stress>

4th Span, Right End of Girder Side

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item		Unit	Allowable Value	Result	
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5	9.17	○
	Bottom of PC Plate	N/mm ²		8.343	○
	Max×0.6	N/mm ²	8.343	5.502	○
Bending stress of PC plate	Top of PC Plate	N/mm ²	0	10.584	○
	Bottom of PC Plate	N/mm ²		3.691	○
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11	3.531	○
	Bottom of RC Deck	N/mm ²		-0.811	○
	Top of PC Plate	N/mm ²	0	8.345	○
	Bottom of PC Plate	N/mm ²		1.306	○
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305	1225	○
	Immediately After Prestressing	N/mm ²	1190	1131.097	○
	Effective Prestressing Force	N/mm ²	1020	921.933	○
Axial stress of PC plate		N/mm ²	10	8.756	○

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.584	○	140	74.435	○	
Edge of PC Plate	Positive Moment	10	3.901	○	140	60.61	○
	Negative Moment	10	3.785	○	140	79.265	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	8.659	○	140	100.221	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	0.56	○
Tensile Stress of Reinforcement Bar	140	27.98	○

<Design of Deck: Summary for Calculation Results of Stress>

4th Span, Right End of Girder Side

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	5.392	○
	D+L	10	0.206	○	140	5.392	○
	D+L+CO	15	2.043	○	300	53.535	○
	D+L+W	12.5	0.351	○	175	9.191	○
	D+W	12.5	0.496	○	175	12.99	○
Supporting for Deck	D	-----	-----	--	100	10.212	○
	D+L	10	1.14	○	140	32.822	○
	D+L+CO	15	2.592	○	300	74.651	○
	D+L+W	12.5	1.256	○	175	36.164	○
	D+W	12.5	0.587	○	175	16.896	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	5.392	○
	D+L	10	0.206	○	140	5.392	○
	D+L+CO	15	2.043	○	300	53.535	○
	D+L+W	12.5	0.351	○	175	9.191	○
	D+W	12.5	0.496	○	175	12.99	○
Supporting for Deck	D	-----	-----	--	100	10.212	○
	D+L	10	1.14	○	140	32.822	○
	D+L+CO	15	2.592	○	300	74.651	○
	D+L+W	12.5	1.256	○	175	36.164	○
	D+W	12.5	0.587	○	175	16.896	○

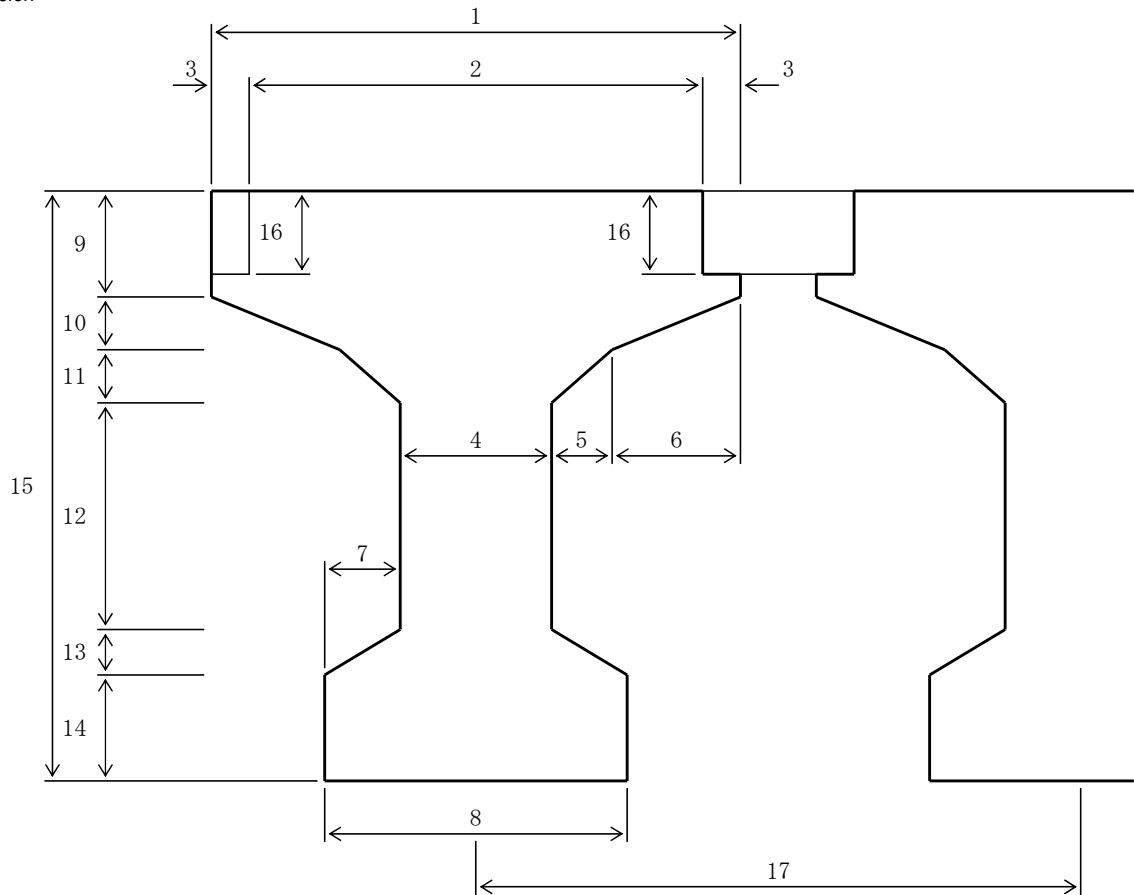
Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	1.618	○	140	58.5	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	1.618	○	140	58.5	○

4 Design of Main Girder

4.1 Dimension and PC Strand Arrangement

1) Dimension



(Unit: mm)

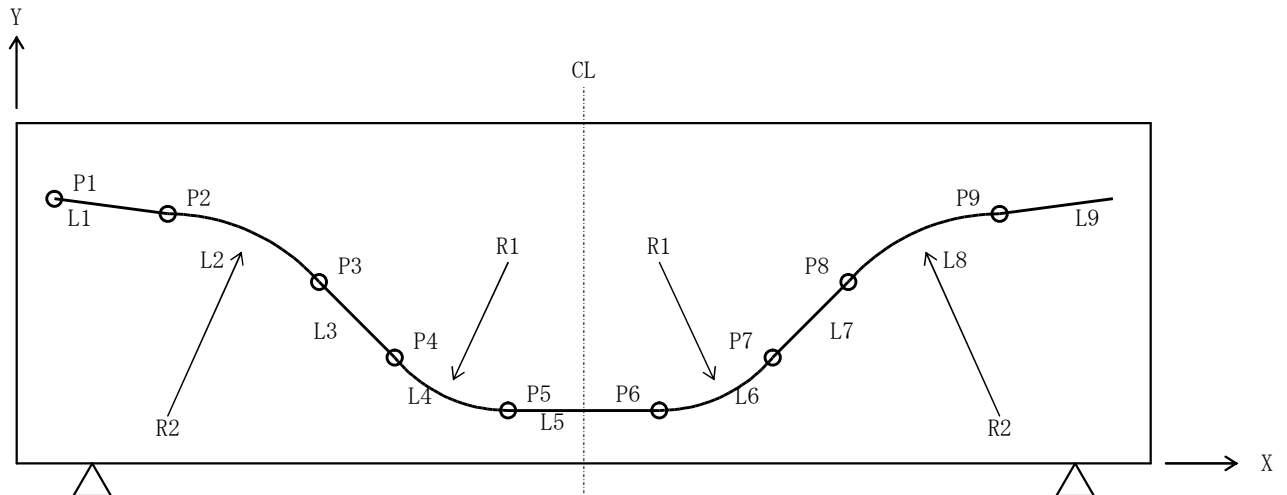
	1st Span			2nd Span		
	End of Girder (Left)	Center Span	End of Girder (Right)	End of Girder (Left)	Center Span	End of Girder (Right)
1	1300.0	1300.0	1300.0	1300.0	1300.0	1300.0
2	1180.0	1180.0	1180.0	1060.0	1060.0	1060.0
3	120.0	120.0	120.0	120.0	120.0	120.0
4	700.0	220.0	700.0	700.0	220.0	700.0
5	0.0	0.0	0.0	0.0	0.0	0.0
6	300.0	540.0	300.0	300.0	540.0	300.0
7	0.0	240.0	0.0	0.0	240.0	0.0
8	700.0	700.0	700.0	700.0	700.0	700.0
9	200.0	200.0	200.0	200.0	200.0	200.0
10	55.6	100.0	55.6	55.6	100.0	55.6
11	0.0	0.0	0.0	0.0	0.0	0.0
12	1494.4	1200.0	1494.4	1494.4	1200.0	1494.4
13	0.0	250.0	0.0	0.0	250.0	0.0
14	250.0	250.0	250.0	250.0	250.0	250.0
15	2000.0	2000.0	2000.0	2000.0	2000.0	2000.0
16	100.0	100.0	100.0	100.0	100.0	100.0
17	3499.4	3499.4	3499.4	3500.0	3500.0	3500.0

	3rd Span			4th Span		
	End of Girder (Left)	Center Span	End of Girder (Right)	End of Girder (Left)	Center Span	End of Girder (Right)
1	1300.0	1300.0	1300.0	1300.0	1300.0	1300.0
2	1060.0	1060.0	1060.0	1060.0	1060.0	1060.0
3	120.0	120.0	120.0	120.0	120.0	120.0
4	700.0	220.0	700.0	700.0	220.0	700.0
5	0.0	0.0	0.0	0.0	0.0	0.0
6	300.0	540.0	300.0	300.0	540.0	300.0
7	0.0	240.0	0.0	0.0	240.0	0.0
8	700.0	700.0	700.0	700.0	700.0	700.0
9	200.0	200.0	200.0	200.0	200.0	200.0
10	55.6	100.0	55.6	55.6	100.0	55.6
11	0.0	0.0	0.0	0.0	0.0	0.0
12	1494.4	1200.0	1494.4	1494.4	1200.0	1494.4
13	0.0	250.0	0.0	0.0	250.0	0.0
14	250.0	250.0	250.0	250.0	250.0	250.0
15	2000.0	2000.0	2000.0	2000.0	2000.0	2000.0
16	100.0	100.0	100.0	100.0	100.0	100.0
17	3500.0	3500.0	3500.0	3500.0	3500.0	3500.0

2) PC Strand Arrangement

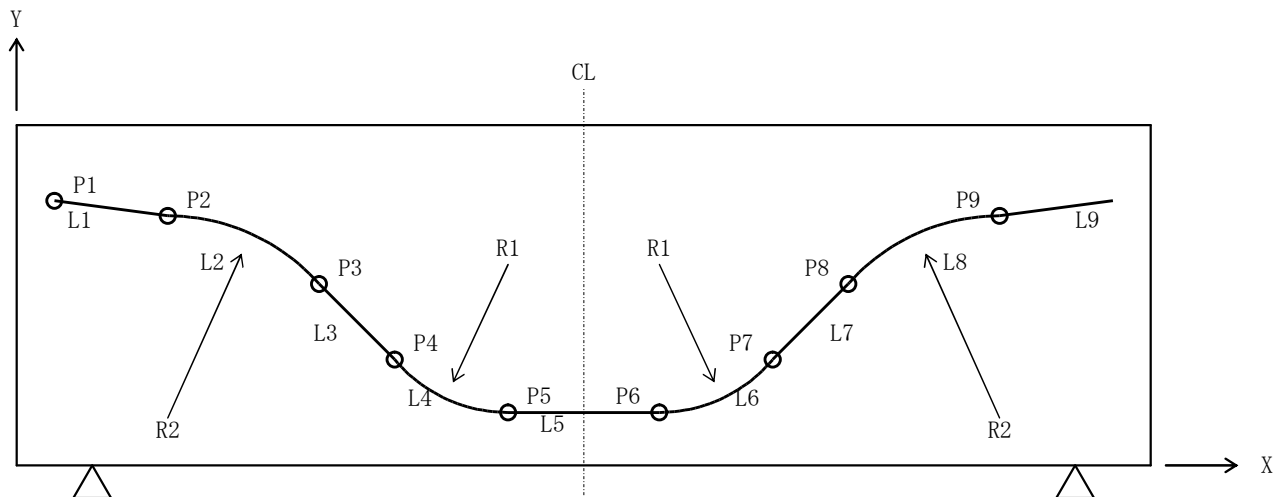
<1st Span>

PC Strand No.		1	2	3	4	5
Number of PC Strand		1	1	1	1	1
Coordinate (mm)	P1 X	-----	-----	-----	-----	-----
	Y	-----	-----	-----	-----	-----
	P2 X	-----	-----	-----	-----	-----
	Y	-----	-----	-----	-----	-----
	P3 X	200.0	200.0	200.0	200.0	200.0
	Y	1750.0	1400.0	1050.0	700.0	350.0
	P4 X	12903.8	10715.5	8527.2	5197.1	2730.7
	Y	414.8	294.8	174.8	174.8	150.8
	P5 X	13949.0	11760.7	9572.4	6242.4	3515.3
	Y	360.0	240.0	120.0	120.0	120.0
	P6 X	15928.8	17675.8	19422.8	22081.4	24448.5
	Y	360.0	240.0	120.0	120.0	120.0
P7 X	17234.1	18981.1	20728.1	23386.6	25406.9	
Y	445.6	325.6	205.6	205.6	166.0	
P8 X	26492.5	26492.5	26492.5	26492.5	26839.3	
Y	1664.4	1314.4	964.4	614.4	304.0	
P9 X	27797.8	27797.8	27797.8	27797.8	27797.8	
Y	1750.0	1400.0	1050.0	700.0	350.0	
P1 [~] X	29597.8	29597.8	29597.8	29597.8	29597.8	
Y	1750.0	1400.0	1050.0	700.0	350.0	
Angle	α (L)	6°0'0"	6°0'0"	6°0'0"	6°0'0"	4°30'0"
	(R)	0°0'0"	0°0'0"	0°0'0"	0°0'0"	0°0'0"
Radius (m)	R2 (L)	-----	-----	-----	-----	-----
	R1 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (R)	10.000	10.000	10.000	10.000	10.000
	R2 (R)	10.000	10.000	10.000	10.000	10.000
Angle	β (L)	-----	-----	-----	-----	-----
	(R)	7°30'0"	7°30'0"	7°30'0"	7°30'0"	5°30'0"
Length of PC Strand (m)	L1	-----	-----	-----	-----	-----
	L2	-----	-----	-----	-----	-----
	L3	12.774	10.573	8.373	5.025	2.539
	L4	1.047	1.047	1.047	1.047	0.785
	L5	1.980	5.915	9.850	15.839	20.933
	L6	1.309	1.309	1.309	1.309	0.960
	L7	9.338	7.576	5.814	3.133	1.439
	L8	1.309	1.309	1.309	1.309	0.960
	L9	1.800	1.800	1.800	1.800	1.800
	Total	29.557	29.530	29.503	29.461	29.416



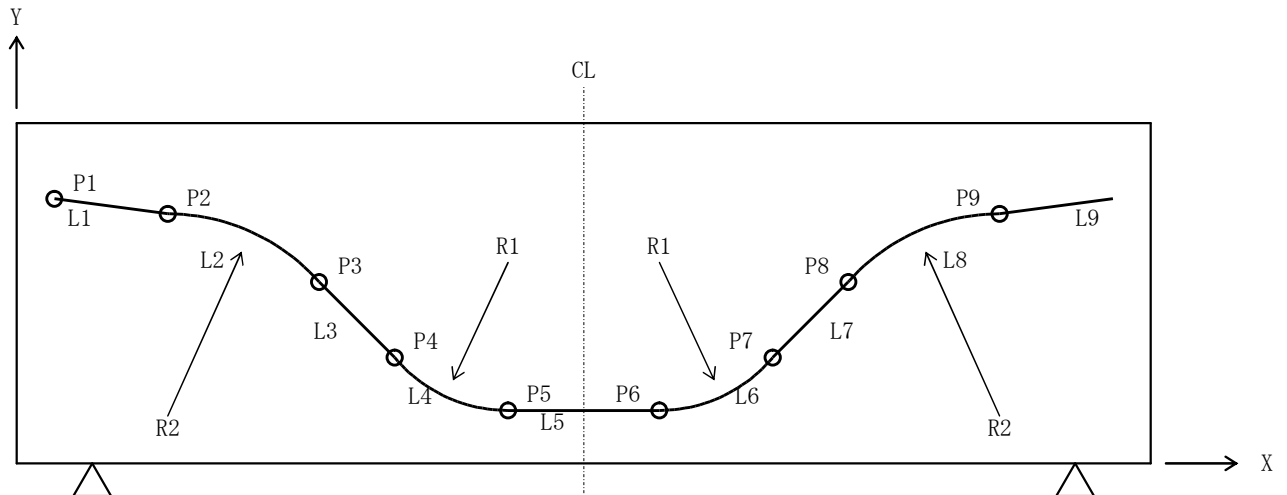
<2nd Span>

PC Strand No.		1	2	3	4	5
Number of PC Strand		1	1	1	1	1
Coordinate (mm)	P1 X	200.0	200.0	200.0	200.0	200.0
	Y	1750.0	1400.0	1050.0	700.0	350.0
	P2 X	2000.0	2000.0	2000.0	2000.0	2000.0
	Y	1750.0	1400.0	1050.0	700.0	350.0
	P3 X	3305.3	3305.3	3305.3	3305.3	2958.5
	Y	1664.4	1314.4	964.4	614.4	304.0
	P4 X	12563.7	10816.7	9069.7	6411.1	4390.9
	Y	445.6	325.6	205.6	205.6	166.0
	P5 X	13869.0	12121.9	10374.9	7716.4	5349.3
	Y	360.0	240.0	120.0	120.0	120.0
	P6 X	15931.0	17678.0	19425.1	22083.6	24450.7
	Y	360.0	240.0	120.0	120.0	120.0
	P7 X	17236.3	18983.3	20730.3	23388.8	25409.1
	Y	445.6	325.6	205.6	205.6	166.0
	P8 X	26494.7	26494.7	26494.7	26494.7	26841.5
	Y	1664.4	1314.4	964.4	614.4	304.0
	P9 X	27800.0	27800.0	27800.0	27800.0	27800.0
	Y	1750.0	1400.0	1050.0	700.0	350.0
P10 X	29600.0	29600.0	29600.0	29600.0	29600.0	
Y	1750.0	1400.0	1050.0	700.0	350.0	
Angle	α (L)	0°0'0"	0°0'0"	0°0'0"	0°0'0"	0°0'0"
	(R)	0°0'0"	0°0'0"	0°0'0"	0°0'0"	0°0'0"
Radius (m)	R2 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (R)	10.000	10.000	10.000	10.000	10.000
	R2 (R)	10.000	10.000	10.000	10.000	10.000
Angle	β (L)	7°30'0"	7°30'0"	7°30'0"	7°30'0"	5°30'0"
	(R)	7°30'0"	7°30'0"	7°30'0"	7°30'0"	5°30'0"
Length of PC Strand (m)	L1	1.800	1.800	1.800	1.800	1.800
	L2	1.309	1.309	1.309	1.309	0.960
	L3	9.338	7.576	5.814	3.133	1.439
	L4	1.309	1.309	1.309	1.309	0.960
	L5	2.062	5.556	9.050	14.367	19.101
	L6	1.309	1.309	1.309	1.309	0.960
	L7	9.338	7.576	5.814	3.133	1.439
	L8	1.309	1.309	1.309	1.309	0.960
	L9	1.800	1.800	1.800	1.800	1.800
	Total		29.575	29.545	29.514	29.469



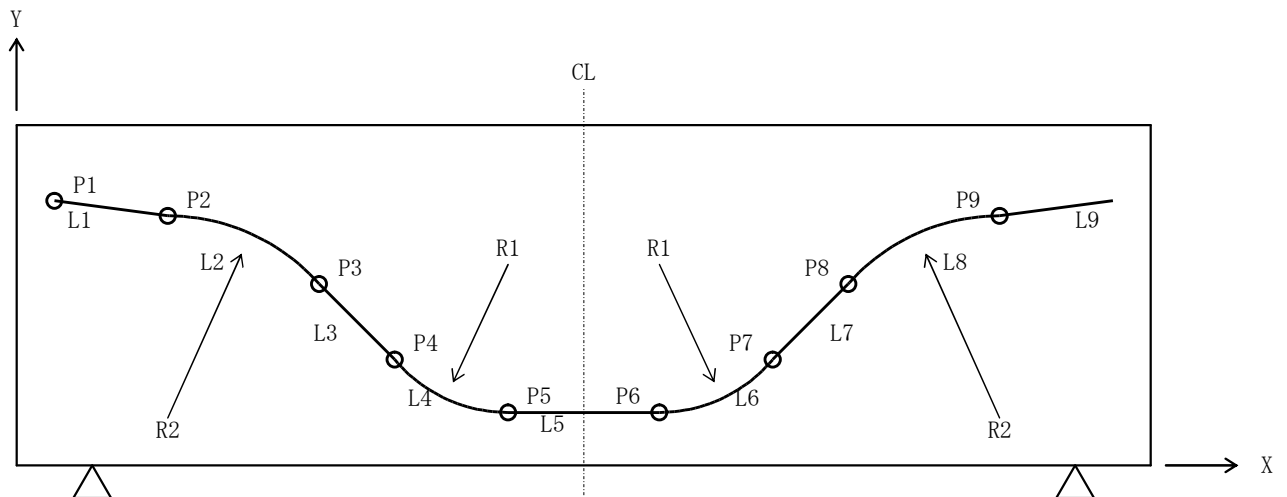
<3rd Span>

PC Strand No.		1	2	3	4	5
Number of PC Strand		1	1	1	1	1
Coordinate (mm)	P1 X	200.0	200.0	200.0	200.0	200.0
	Y	1750.0	1400.0	1050.0	700.0	350.0
	P2 X	2000.0	2000.0	2000.0	2000.0	2000.0
	Y	1750.0	1400.0	1050.0	700.0	350.0
	P3 X	3305.3	3305.3	3305.3	3305.3	2958.5
	Y	1664.4	1314.4	964.4	614.4	304.0
	P4 X	12563.7	10816.7	9069.7	6411.1	4390.9
	Y	445.6	325.6	205.6	205.6	166.0
	P5 X	13869.0	12121.9	10374.9	7716.4	5349.3
	Y	360.0	240.0	120.0	120.0	120.0
	P6 X	15931.0	17678.1	19425.1	22083.6	24450.7
	Y	360.0	240.0	120.0	120.0	120.0
	P7 X	17236.3	18983.3	20730.3	23388.9	25409.1
	Y	445.6	325.6	205.6	205.6	166.0
	P8 X	26494.7	26494.7	26494.7	26494.7	26841.5
	Y	1664.4	1314.4	964.4	614.4	304.0
	P9 X	27800.0	27800.0	27800.0	27800.0	27800.0
	Y	1750.0	1400.0	1050.0	700.0	350.0
P10 X	29600.0	29600.0	29600.0	29600.0	29600.0	
Y	1750.0	1400.0	1050.0	700.0	350.0	
Angle	α (L) (R)	0°0'0" 0°0'0"	0°0'0" 0°0'0"	0°0'0" 0°0'0"	0°0'0" 0°0'0"	0°0'0" 0°0'0"
Radius (m)	R2 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (R)	10.000	10.000	10.000	10.000	10.000
	R2 (R)	10.000	10.000	10.000	10.000	10.000
Angle	β (L) (R)	7°30'0" 7°30'0"	7°30'0" 7°30'0"	7°30'0" 7°30'0"	7°30'0" 7°30'0"	5°30'0" 5°30'0"
	Length of PC Strand (m)	L1	1.800	1.800	1.800	1.800
L2		1.309	1.309	1.309	1.309	0.960
L3		9.338	7.576	5.814	3.133	1.439
L4		1.309	1.309	1.309	1.309	0.960
L5		2.062	5.556	9.050	14.367	19.101
L6		1.309	1.309	1.309	1.309	0.960
L7		9.338	7.576	5.814	3.133	1.439
L8		1.309	1.309	1.309	1.309	0.960
L9		1.800	1.800	1.800	1.800	1.800
Total			29.575	29.545	29.514	29.469



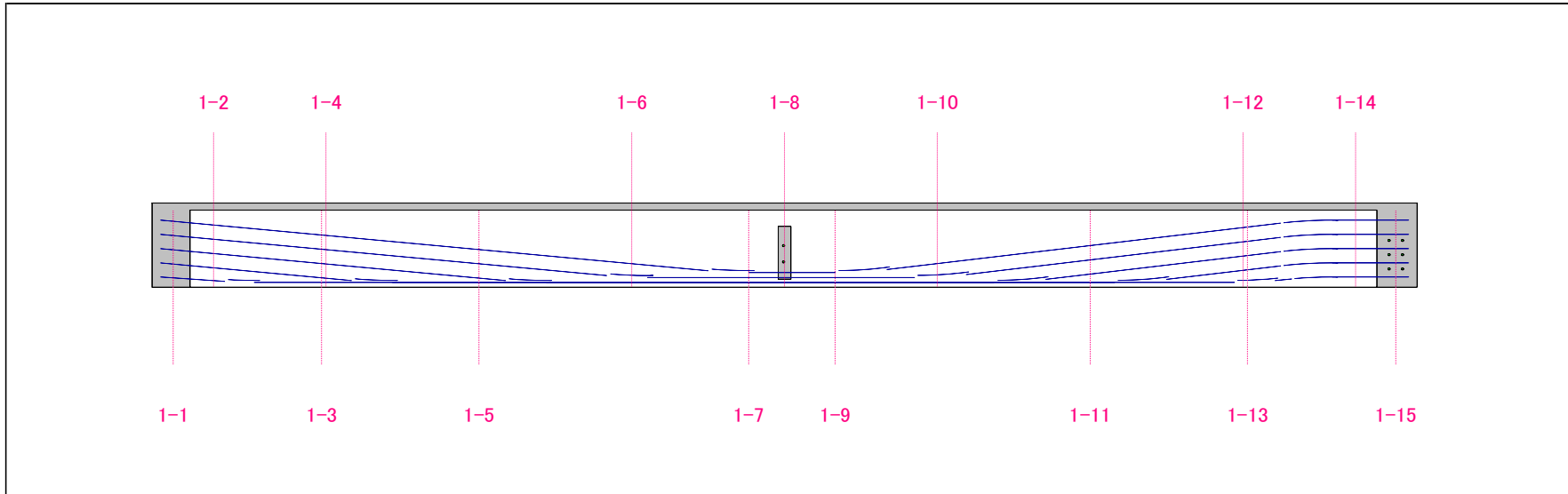
<4th Span>

PC Strand No.		1	2	3	4	5
Number of PC Strand		1	1	1	1	1
Coordinate (mm)	P1 X	200.0	200.0	200.0	200.0	200.0
	Y	1750.0	1400.0	1050.0	700.0	350.0
	P2 X	2000.0	2000.0	2000.0	2000.0	2000.0
	Y	1750.0	1400.0	1050.0	700.0	350.0
	P3 X	3305.3	3305.3	3305.3	3305.3	2958.5
	Y	1664.4	1314.4	964.4	614.4	304.0
	P4 X	12563.7	10816.7	9069.7	6411.1	4390.9
	Y	445.6	325.6	205.6	205.6	166.0
	P5 X	13869.0	12121.9	10374.9	7716.4	5349.3
	Y	360.0	240.0	120.0	120.0	120.0
P6 X	15851.0	18039.3	20227.6	23557.6	26284.7	
Y	360.0	240.0	120.0	120.0	120.0	
P7 X	16896.2	19084.5	21272.9	24602.9	27069.3	
Y	414.8	294.8	174.8	174.8	150.8	
P8 X	29600.0	29600.0	29600.0	29600.0	29600.0	
Y	1750.0	1400.0	1050.0	700.0	350.0	
P9 X	-----	-----	-----	-----	-----	
Y	-----	-----	-----	-----	-----	
P10 X	-----	-----	-----	-----	-----	
Y	-----	-----	-----	-----	-----	
Angle	α (L)	0°0'0"	0°0'0"	0°0'0"	0°0'0"	0°0'0"
	(R)	6°0'0"	6°0'0"	6°0'0"	6°0'0"	4°30'0"
Radius (m)	R2 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (R)	10.000	10.000	10.000	10.000	10.000
	R2 (R)	-----	-----	-----	-----	-----
Angle	β (L)	7°30'0"	7°30'0"	7°30'0"	7°30'0"	5°30'0"
	(R)	-----	-----	-----	-----	-----
Length of PC Strand (m)	L1	1.800	1.800	1.800	1.800	1.800
	L2	1.309	1.309	1.309	1.309	0.960
	L3	9.338	7.576	5.814	3.133	1.439
	L4	1.309	1.309	1.309	1.309	0.960
	L5	1.982	5.917	9.853	15.841	20.935
	L6	1.047	1.047	1.047	1.047	0.785
	L7	12.774	10.573	8.373	5.025	2.539
	L8	-----	-----	-----	-----	-----
	L9	-----	-----	-----	-----	-----
	Total		29.559	29.532	29.505	29.464



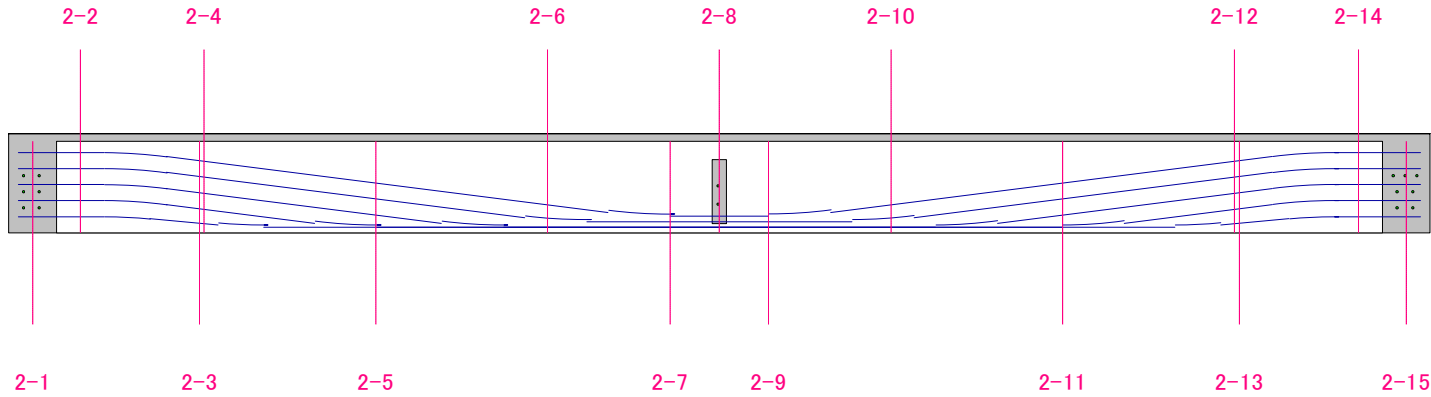
4.4 Summary for Calculation Results of Stress

1) PF7-PF8



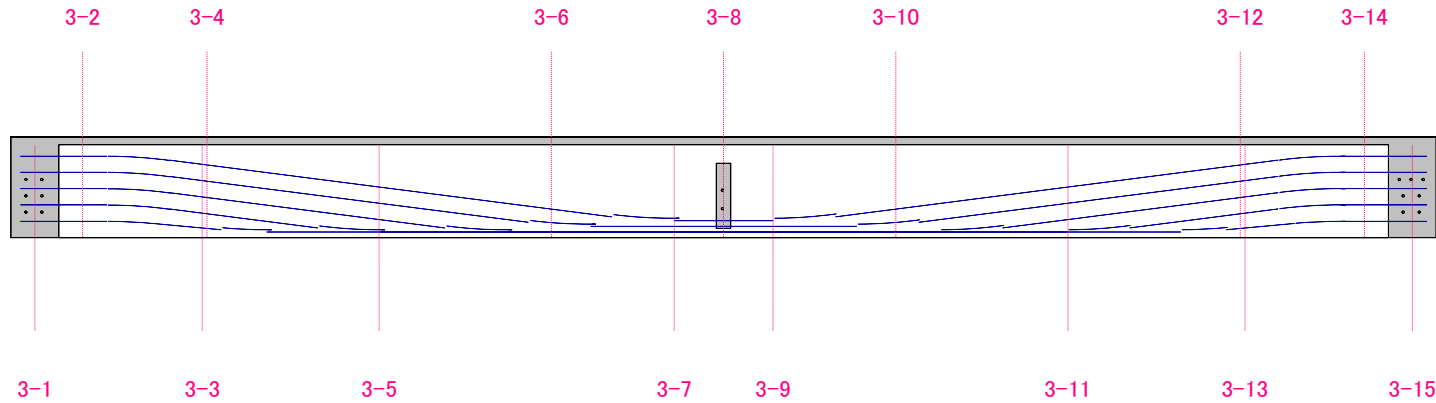
		Unit	Allowable Value	Cross Section Number		
Calculation for Bending Moment				[1- 7]	[1- 8]	[1- 9]
				Bent up Point(Left)	Center of Span	Bent up Point(Right)
Bending Stress of Concrete						
Immediately After Prestressing	N/mm ²	-1.5~19.00	Top of Main Girder	0.64	0.68	0.67
			Bottom of Main Girder	13.98	13.88	13.83
During Deck Construction	"	-1.5~14.00	Top of Main Girder	4.71	4.77	4.73
			Bottom of Main Girder	7.97	7.86	7.85
Dead Load	"	≦ 10.00	Top of Deck	3.21	3.21	3.19
		0~14.00	Top of Main Girder	5.17	5.19	5.16
			Bottom of Main Girder	2.52	2.44	2.44
Design Load	"	≦ 10.00	Top of Deck max	4.96	4.94	4.86
			Top of Deck min	2.72	2.69	2.65
		-1.5~14.00	Top of Main Girder(max)	6.66	6.67	6.59
			Bottom of Main Girder(max)	-1.22	-1.27	-1.15
			Top of Main Girder(min)	4.75	4.75	4.71
Bottom of Main Girder(min)	3.58	3.56	3.58			
Stress of PC Strand	N/mm ²	Pmax ≦ 1110		1063	1058	1051
Ultimate Load	-----	F ≧ 1.0		1.10	1.11	1.13
Calculation for Shear Force				[1- 2]	[1- 3]	[1-14]
				Near a Support of girder(Left)	Change point of Web Width(Left)	Near a Support of girder(Right)
Shear Stress of Design Load	kN			0.59	1.34	1.15
Compressive Strength to Failure	-----	F ≧ 1.0		3.58	1.72	2.74
Diagonal	Dead Load	N/mm ²	≧ -1	-0.07	-0.17	-0.32
Tensile Stress	Design Load	"	≧ -2	-0.20	-0.56	-0.55

2) PF8-PF9



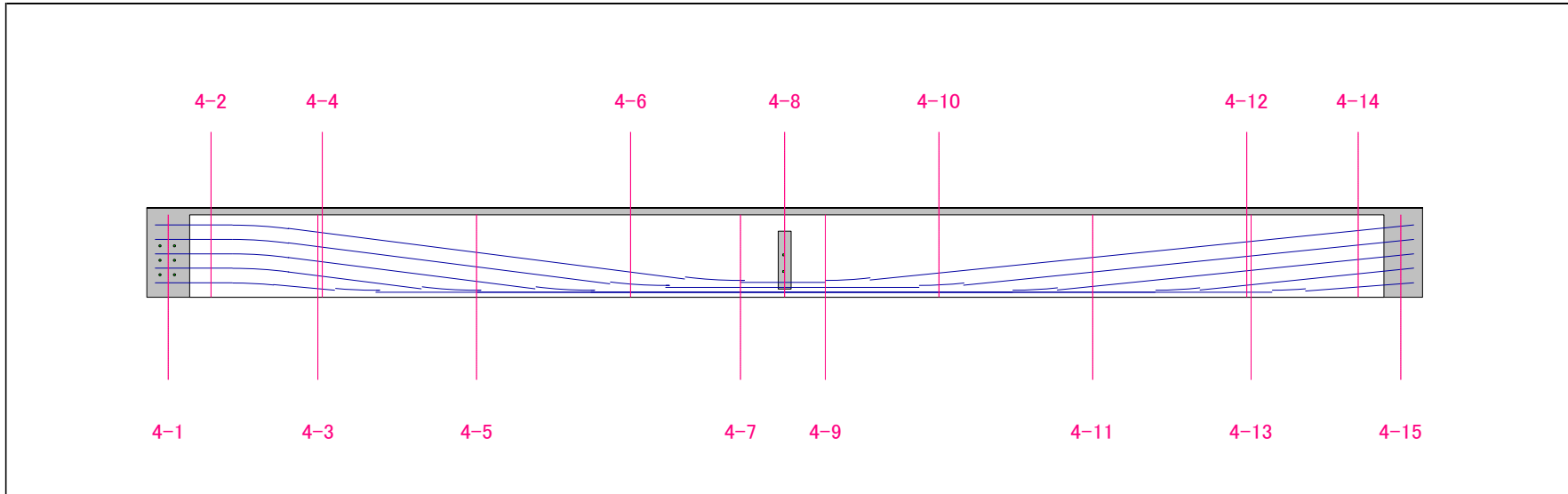
		Unit	Allowable Value	Cross Section Number		
Calculation for Bending Moment				[2- 7]	[2- 8]	[2- 9]
				Bent up Point(Left)	Center of Span	Bent up Point(Right)
Bending Stress of Concrete						
Immediately After Prestressing	N/mm ²	-1.5~19.00	Top of Main Girder	0.79	0.83	0.79
			Bottom of Main Girder	13.20	13.09	13.20
During Deck Construction	"	-1.5~14.00	Top of Main Girder	5.85	5.93	5.85
			Bottom of Main Girder	6.24	6.10	6.24
Dead Load	"	≦ 10.00	Top of Deck	2.45	2.49	2.46
		0~14.00	Top of Main Girder	4.87	4.93	4.88
			Bottom of Main Girder	2.98	2.83	2.96
Design Load	"	≦ 10.00	Top of Deck max	3.58	3.63	3.60
			Top of Deck min	2.10	2.16	2.13
		-1.5~14.00	Top of Main Girder(max)	5.83	5.89	5.84
			Bottom of Main Girder(max)	0.46	0.30	0.43
			Top of Main Girder(min)	4.57	4.64	4.59
	Bottom of Main Girder(min)	3.76	3.58	3.71		
Stress of PC Strand	N/mm ²	Pmax ≦ 1110		992	991	994
Ultimate Load	-----	F ≧ 1.0		1.35	1.34	1.34
Calculation for Shear Force				[2- 2]	[2-13]	[2-14]
				Near a Support of girder(Left)	Change point of Web Width(Right)	Near a Support of girder(Right)
Shear Stress of Design Load	kN			1.02	0.72	0.91
Compressive Strength to Failure	-----	F ≧ 1.0		3.18	1.91	3.62
Diagonal	Dead Load	N/mm ²	≧ -1	-0.23	0.00	-0.22
Tensile Stress	Design Load	"	≧ -2	-0.43	-0.17	-0.45

3) PF9-PF10



		Unit	Allowable Value	Cross Section Number		
Calculation for Bending Moment				[3- 7]	[3- 8]	[3- 9]
				Bent up Point(Left)	Center of Span	Bent up Point(Right)
Bending Stress of Concrete						
Immediately After Prestressing	N/mm ²	-1.5~19.00	Top of Main Girder	0.79	0.83	0.79
			Bottom of Main Girder	13.20	13.09	13.20
During Deck Construction	"	-1.5~14.00	Top of Main Girder	5.85	5.93	5.85
			Bottom of Main Girder	6.24	6.10	6.24
Dead Load	"	≤ 10.00	Top of Deck	2.56	2.60	2.56
		0~14.00	Top of Main Girder	4.96	5.01	4.96
			Bottom of Main Girder	2.77	2.62	2.76
Design Load	"	≤ 10.00	Top of Deck max	3.70	3.74	3.70
			Top of Deck min	2.22	2.25	2.20
		-1.5~14.00	Top of Main Girder(max)	5.92	5.98	5.92
			Bottom of Main Girder(max)	0.24	0.09	0.24
			Top of Main Girder(min)	4.67	4.72	4.65
	Bottom of Main Girder(min)	3.54	3.40	3.57		
Stress of PC Strand	N/mm ²	Pmax ≤ 1110		997	994	996
Ultimate Load	----	F ≥ 1.0		1.32	1.31	1.33
Calculation for Shear Force				[3- 2]	[3-13]	[3-14]
				Near a Support of girder(Left)	Change point of Web Width(Right)	Near a Support of girder(Right)
Shear Stress of Design Load	kN			0.92	0.73	1.00
Compressive Strength to Failure	----	F ≥ 1.0		3.58	1.87	3.25
Diagonal	Dead Load	N/mm ²	≥ -1	-0.23	0.00	-0.23
Tensile Stress	Design Load	"	≥ -2	-0.46	-0.18	-0.42

4) PF10-PF11



		Unit	Allowable Value	Cross Section Number		
Calculation for Bending Moment				[4- 7]	[4- 8]	[4- 9]
				Bent up Point(Left)	Center of Span	Bent up Point(Right)
Bending Stress of Concrete						
Immediately After Prestressing	N/mm ²	-1.5~19.00	Top of Main Girder	0.64	0.65	0.62
			Bottom of Main Girder	13.89	13.94	14.04
During Deck Construction	"	-1.5~14.00	Top of Main Girder	5.71	5.76	5.69
			Bottom of Main Girder	6.88	6.88	7.00
Dead Load	"	≤ 10.00	Top of Deck	2.52	2.54	2.50
		0~14.00	Top of Main Girder	4.86	4.90	4.84
			Bottom of Main Girder	3.39	3.39	3.54
Design Load	"	≤ 10.00	Top of Deck max	3.86	3.92	3.91
			Top of Deck min	2.22	2.26	2.24
		-1.5~14.00	Top of Main Girder(max)	6.00	6.07	6.03
			Bottom of Main Girder(max)	0.40	0.32	0.41
			Top of Main Girder(min)	4.61	4.66	4.62
	Bottom of Main Girder(min)	4.06	4.02	4.12		
Stress of PC Strand	N/mm ²	Pmax ≤ 1110		1039	1046	1049
Ultimate Load	-----	F ≥ 1.0		1.26	1.24	1.24
Calculation for Shear Force				[4- 2]	[4-13]	[4-14]
				Near a Support of girder(Left)	Change point of Web Width(Right)	Near a Support of girder(Right)
Shear Stress of Design Load	kN			1.00	1.12	0.49
Compressive Strength to Failure	-----	F ≥ 1.0		3.16	1.92	4.02
Diagonal	Dead Load	N/mm ²	≥ -1	-0.23	-0.08	-0.03
Tensile Stress	Design Load	"	≥ -2	-0.42	-0.39	-0.14

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 4

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1- 1]		[1- 2]		[1- 3]		
Interval from beginning of Girder		-----	0.500		1.500		4.000		
Immediately After Prestressing	Top of Main Girder	-1.5	3.248	○	3.050	○	3.865	○	
	Bottom of Main Girder	~19.00	4.312	○	5.267	○	9.954	○	
During Deck Construction	Top of Main Girder	-1.5	3.086	○	3.347	○	5.317	○	
	Bottom of Main Girder	~14.00	4.097	○	4.463	○	7.253	○	
Dead Load	Top of Deck	≤10.00	0.377	○	0.799	○	1.873	○	
	Top of Main Girder	0	2.324	○	2.786	○	4.598	○	
	Bottom of Main Girder	~14.00	4.147	○	3.876	○	4.544	○	
Design Load1	Top of Deck	Max	0.377	○	1.063	○	2.713	○	
		Min	≤10.00	0.377	○	0.765	○	1.751	○
	Top of Main Girder	Max	2.324	○	3.019	○	5.312	○	
		Min	-1.5	2.324	○	2.756	○	4.494	○
	Bottom of Main Girder	Max	~14.00	4.147	○	3.408	○	2.720	○
		Min		4.147	○	3.935	○	4.809	○
Design Load2 Temperature Rise	Top of Deck	Max	0.947	○	1.635	○	3.250	○	
		Min	≤11.50	0.947	○	1.338	○	2.288	○
	Top of Main Girder	Max	1.512	○	2.206	○	4.448	○	
		Min	-2	1.512	○	1.943	○	3.630	○
	Bottom of Main Girder	Max	~16.10	4.588	○	3.815	○	2.937	○
		Min		4.588	○	4.342	○	5.025	○
Design Load3 Temperature Drop	Top of Deck	Max	0.947	○	1.635	○	3.250	○	
		Min	≤11.50	0.947	○	1.338	○	2.288	○
	Top of Main Girder	Max	1.512	○	2.206	○	4.448	○	
		Min	-2	1.512	○	1.943	○	3.630	○
	Bottom of Main Girder	Max	~16.10	4.588	○	3.815	○	2.937	○
		Min		4.588	○	4.342	○	5.025	○
Design Load4 Support sinking	Top of Deck	Max	0.377	○	1.063	○	2.713	○	
		Min	≤10.00	0.377	○	0.765	○	1.751	○
	Top of Main Girder	Max	2.324	○	3.019	○	5.312	○	
		Min	-1.5	2.324	○	2.756	○	4.494	○
	Bottom of Main Girder	Max	~14.00	4.147	○	3.408	○	2.720	○
		Min		4.147	○	3.935	○	4.809	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	0.947	○	1.635	○	3.250	○	
		Min	≤11.50	0.947	○	1.338	○	2.288	○
	Top of Main Girder	Max	1.512	○	2.206	○	4.448	○	
		Min	-2	1.512	○	1.943	○	3.630	○
	Bottom of Main Girder	Max	~16.10	4.588	○	3.815	○	2.937	○
		Min		4.588	○	4.342	○	5.025	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	0.947	○	1.635	○	3.250	○	
		Min	≤11.50	0.947	○	1.338	○	2.288	○
	Top of Main Girder	Max	1.512	○	2.206	○	4.448	○	
		Min	-2	1.512	○	1.943	○	3.630	○
	Bottom of Main Girder	Max	~16.10	4.588	○	3.815	○	2.937	○
		Min		4.588	○	4.342	○	5.025	○

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 4

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1- 4]		[1- 5]		[1- 6]		
Interval from beginning of Girder		-----	4.100		7.699		11.299		
Immediately After Prestressing	Top of Main Girder	-1.5	3.815	○	2.134	○	0.858	○	
	Bottom of Main Girder	~19.00	10.020	○	12.356	○	13.984	○	
During Deck Construction	Top of Main Girder	-1.5	5.313	○	5.015	○	4.633	○	
	Bottom of Main Girder	~14.00	7.263	○	7.844	○	8.317	○	
Dead Load	Top of Deck	≤10.00	1.903	○	2.728	○	3.124	○	
	Top of Main Girder	0	4.618	○	5.059	○	5.109	○	
	Bottom of Main Girder	~14.00	4.494	○	3.348	○	2.907	○	
Design Load1	Top of Deck	Max	2.762	○	4.121	○	4.794	○	
		Min	1.777	○	2.474	○	2.739	○	
	Top of Main Girder	Max	5.349	○	6.246	○	6.533	○	
		Min	-1.5	4.511	○	4.843	○	4.781	○
	Bottom of Main Girder	Max	~14.00	2.629	○	0.346	○	-0.674	○
		Min		4.766	○	3.894	○	3.731	○
Design Load2 Temperature Rise	Top of Deck	Max	3.301	○	4.724	○	5.460	○	
		Min	≤11.50	2.316	○	3.077	○	3.405	○
	Top of Main Girder	Max	4.486	○	5.438	○	5.779	○	
		Min	-2	3.648	○	4.036	○	4.028	○
	Bottom of Main Girder	Max	~16.10	2.842	○	0.422	○	-0.732	○
		Min		4.979	○	3.971	○	3.673	○
Design Load3 Temperature Drop	Top of Deck	Max	3.301	○	4.724	○	5.460	○	
		Min	≤11.50	2.316	○	3.077	○	3.405	○
	Top of Main Girder	Max	4.486	○	5.438	○	5.779	○	
		Min	-2	3.648	○	4.036	○	4.028	○
	Bottom of Main Girder	Max	~16.10	2.842	○	0.422	○	-0.732	○
		Min		4.979	○	3.971	○	3.673	○
Design Load4 Support sinking	Top of Deck	Max	2.762	○	4.121	○	4.794	○	
		Min	≤10.00	1.777	○	2.474	○	2.739	○
	Top of Main Girder	Max	5.349	○	6.246	○	6.533	○	
		Min	-1.5	4.511	○	4.843	○	4.781	○
	Bottom of Main Girder	Max	~14.00	2.629	○	0.346	○	-0.674	○
		Min		4.766	○	3.894	○	3.731	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	3.301	○	4.724	○	5.460	○	
		Min	≤11.50	2.316	○	3.077	○	3.405	○
	Top of Main Girder	Max	4.486	○	5.438	○	5.779	○	
		Min	-2	3.648	○	4.036	○	4.028	○
	Bottom of Main Girder	Max	~16.10	2.842	○	0.422	○	-0.732	○
		Min		4.979	○	3.971	○	3.673	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	3.301	○	4.724	○	5.460	○	
		Min	≤11.50	2.316	○	3.077	○	3.405	○
	Top of Main Girder	Max	4.486	○	5.438	○	5.779	○	
		Min	-2	3.648	○	4.036	○	4.028	○
	Bottom of Main Girder	Max	~16.10	2.842	○	0.422	○	-0.732	○
		Min		4.979	○	3.971	○	3.673	○

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 4

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1- 7]		[1- 8]		[1- 9]		
Interval from beginning of Girder		-----	13.949		14.899		15.929		
Immediately After Prestressing	Top of Main Girder	-1.5	0.644	○	0.681	○	0.670	○	
	Bottom of Main Girder	~19.00	13.981	○	13.880	○	13.833	○	
During Deck Construction	Top of Main Girder	-1.5	4.712	○	4.768	○	4.729	○	
	Bottom of Main Girder	~14.00	7.973	○	7.858	○	7.847	○	
Dead Load	Top of Deck	≤10.00	3.209	○	3.210	○	3.186	○	
	Top of Main Girder	0	5.171	○	5.194	○	5.162	○	
	Bottom of Main Girder	~14.00	2.520	○	2.444	○	2.442	○	
Design Load1	Top of Deck	Max	4.959	○	4.944	○	4.863	○	
		Min	2.717	○	2.690	○	2.654	○	
	Top of Main Girder	Max	-1.5	6.662	○	6.673	○	6.592	○
		Min	~14.00	4.751	○	4.751	○	4.709	○
	Bottom of Main Girder	Max	~14.00	-1.224	○	-1.267	○	-1.146	○
		Min	~14.00	3.575	○	3.556	○	3.580	○
Design Load2 Temperature Rise	Top of Deck	Max	≤11.50	5.672	○	5.674	○	5.612	○
		Min	~16.10	3.430	○	3.420	○	3.403	○
	Top of Main Girder	Max	-2	5.949	○	5.974	○	5.909	○
		Min	~16.10	4.037	○	4.052	○	4.026	○
	Bottom of Main Girder	Max	~16.10	-1.381	○	-1.460	○	-1.378	○
		Min	~16.10	3.418	○	3.363	○	3.348	○
Design Load3 Temperature Drop	Top of Deck	Max	≤11.50	5.672	○	5.674	○	5.612	○
		Min	~16.10	3.430	○	3.420	○	3.403	○
	Top of Main Girder	Max	-2	5.949	○	5.974	○	5.909	○
		Min	~16.10	4.037	○	4.052	○	4.026	○
	Bottom of Main Girder	Max	~16.10	-1.381	○	-1.460	○	-1.378	○
		Min	~16.10	3.418	○	3.363	○	3.348	○
Design Load4 Support sinking	Top of Deck	Max	≤10.00	4.959	○	4.944	○	4.863	○
		Min	~14.00	2.717	○	2.690	○	2.654	○
	Top of Main Girder	Max	-1.5	6.662	○	6.673	○	6.592	○
		Min	~14.00	4.751	○	4.751	○	4.709	○
	Bottom of Main Girder	Max	~14.00	-1.224	○	-1.267	○	-1.146	○
		Min	~14.00	3.575	○	3.556	○	3.580	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	≤11.50	5.672	○	5.674	○	5.612	○
		Min	~16.10	3.430	○	3.420	○	3.403	○
	Top of Main Girder	Max	-2	5.949	○	5.974	○	5.909	○
		Min	~16.10	4.037	○	4.052	○	4.026	○
	Bottom of Main Girder	Max	~16.10	-1.381	○	-1.460	○	-1.378	○
		Min	~16.10	3.418	○	3.363	○	3.348	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	≤11.50	5.672	○	5.674	○	5.612	○
		Min	~16.10	3.430	○	3.420	○	3.403	○
	Top of Main Girder	Max	-2	5.949	○	5.974	○	5.909	○
		Min	~16.10	4.037	○	4.052	○	4.026	○
	Bottom of Main Girder	Max	~16.10	-1.381	○	-1.460	○	-1.378	○
		Min	~16.10	3.418	○	3.363	○	3.348	○

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 4

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[1-10]		[1-11]		[1-12]	
Interval from beginning of Girder		-----	18.499		22.098		25.698	
Immediately After Prestressing	Top of Main Girder	-1.5	1.075	○	3.020	○	5.940	
	Bottom of Main Girder	~19.00	13.276	○	10.968	○	7.177	
During Deck Construction	Top of Main Girder	-1.5	4.822	○	5.825	○	7.300	
	Bottom of Main Girder	~14.00	7.695	○	6.623	○	4.660	
Dead Load	Top of Deck	≤10.00	3.066	○	2.686	○	1.993	
	Top of Main Girder	0	5.153	○	5.402	○	5.565	
	Bottom of Main Girder	~14.00	2.504	○	2.658	○	2.942	
Design Load1	Top of Deck	Max	4.487	○	3.604	○	2.396	
		Min	2.533	○	2.125	○	1.222	
	Top of Main Girder	Max	6.364	○	6.184	○	5.908	
		Min	-1.5	4.699	○	4.925	○	4.910
	Bottom of Main Girder	Max	~14.00	-0.539	○	0.682	○	2.066
		Min		3.645	○	3.866	○	4.617
Design Load2 Temperature Rise	Top of Deck	Max	5.282	○	4.466	○	3.327	
		Min	≤11.50	3.328	○	2.988	○	2.153
	Top of Main Girder	Max	5.721	○	5.598	○	5.379	
		Min	-2	4.055	○	4.339	○	4.382
	Bottom of Main Girder	Max	~16.10	-0.871	○	0.203	○	1.432
		Min		3.313	○	3.386	○	3.982
Design Load3 Temperature Drop	Top of Deck	Max	5.282	○	4.466	○	3.327	
		Min	≤11.50	3.328	○	2.988	○	2.153
	Top of Main Girder	Max	5.721	○	5.598	○	5.379	
		Min	-2	4.055	○	4.339	○	4.382
	Bottom of Main Girder	Max	~16.10	-0.871	○	0.203	○	1.432
		Min		3.313	○	3.386	○	3.982
Design Load4 Support sinking	Top of Deck	Max	4.487	○	3.604	○	2.396	
		Min	≤10.00	2.533	○	2.125	○	1.222
	Top of Main Girder	Max	6.364	○	6.184	○	5.908	
		Min	-1.5	4.699	○	4.925	○	4.910
	Bottom of Main Girder	Max	~14.00	-0.539	○	0.682	○	2.066
		Min		3.645	○	3.866	○	4.617
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	5.282	○	4.466	○	3.327	
		Min	≤11.50	3.328	○	2.988	○	2.153
	Top of Main Girder	Max	5.721	○	5.598	○	5.379	
		Min	-2	4.055	○	4.339	○	4.382
	Bottom of Main Girder	Max	~16.10	-0.871	○	0.203	○	1.432
		Min		3.313	○	3.386	○	3.982
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	5.282	○	4.466	○	3.327	
		Min	≤11.50	3.328	○	2.988	○	2.153
	Top of Main Girder	Max	5.721	○	5.598	○	5.379	
		Min	-2	4.055	○	4.339	○	4.382
	Bottom of Main Girder	Max	~16.10	-0.871	○	0.203	○	1.432
		Min		3.313	○	3.386	○	3.982

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 4

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1-13]		[1-14]		[1-15]		
Interval from beginning of Girder		-----	25.798		28.298		29.298		
Immediately After Prestressing	Top of Main Girder	-1.5	6.032	○	4.111	○	3.323	○	
	Bottom of Main Girder	~19.00	7.060	○	3.536	○	3.775	○	
During Deck Construction	Top of Main Girder	-1.5	7.346	○	4.345	○	3.149	○	
	Bottom of Main Girder	~14.00	4.600	○	2.833	○	3.594	○	
Dead Load	Top of Deck	≤10.00	1.969	○	0.656	○	-0.003	○	
	Top of Main Girder	0	5.567	○	3.087	○	1.980	○	
	Bottom of Main Girder	~14.00	2.959	○	3.148	○	4.354	○	
Design Load1	Top of Deck	Max	2.363	○	0.909	○	0.244	○	
		Min	1.184	○	-0.615	○	-1.536	○	
	Top of Main Girder	Max	5.902	○	3.311	○	2.199	○	
		Min	-1.5	4.899	○	1.967	○	0.621	○
	Bottom of Main Girder	Max	~14.00	2.103	○	2.700	○	3.933	○
		Min	4.666	○	5.393	○	6.965	○	
Design Load2 Temperature Rise	Top of Deck	Max	3.296	○	1.955	○	1.317	○	
		Min	2.116	○	0.432	○	-0.463	○	
	Top of Main Girder	Max	5.375	○	2.917	○	1.833	○	
		Min	-2	4.372	○	1.573	○	0.254	○
	Bottom of Main Girder	Max	~16.10	1.464	○	2.274	○	3.522	○
		Min	4.027	○	4.967	○	6.554	○	
Design Load3 Temperature Drop	Top of Deck	Max	3.296	○	1.955	○	1.317	○	
		Min	2.116	○	0.432	○	-0.463	○	
	Top of Main Girder	Max	5.375	○	2.917	○	1.833	○	
		Min	-2	4.372	○	1.573	○	0.254	○
	Bottom of Main Girder	Max	~16.10	1.464	○	2.274	○	3.522	○
		Min	4.027	○	4.967	○	6.554	○	
Design Load4 Support sinking	Top of Deck	Max	2.363	○	0.909	○	0.244	○	
		Min	1.184	○	-0.615	○	-1.536	○	
	Top of Main Girder	Max	5.902	○	3.311	○	2.199	○	
		Min	-1.5	4.899	○	1.967	○	0.621	○
	Bottom of Main Girder	Max	~14.00	2.103	○	2.700	○	3.933	○
		Min	4.666	○	5.393	○	6.965	○	
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	3.296	○	1.955	○	1.317	○	
		Min	2.116	○	0.432	○	-0.463	○	
	Top of Main Girder	Max	5.375	○	2.917	○	1.833	○	
		Min	-2	4.372	○	1.573	○	0.254	○
	Bottom of Main Girder	Max	~16.10	1.464	○	2.274	○	3.522	○
		Min	4.027	○	4.967	○	6.554	○	
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	3.296	○	1.955	○	1.317	○	
		Min	2.116	○	0.432	○	-0.463	○	
	Top of Main Girder	Max	5.375	○	2.917	○	1.833	○	
		Min	-2	4.372	○	1.573	○	0.254	○
	Bottom of Main Girder	Max	~16.10	1.464	○	2.274	○	3.522	○
		Min	4.027	○	4.967	○	6.554	○	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 4

Cross Section NumberNo.	Unit	Allowable Value	[1- 1]		[1- 2]		[1- 3]	
Interval from beginning of Girder								
				0.500		1.500		4.000
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1164	○	1168	○	1177	○
Effective Prestressing Force (*1)	N/mm ²	1110	1106	○	1107	○	1097	○
Effective Prestressing Force (*2)	N/mm ²	1110	1037	○	1036	○	1010	○
max	N/mm ²	1110	1037	○	1038	○	1027	○
Ultimate Load	-----	1.00	999.90	○	4.68	○	1.79	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1- 4]		[1- 5]		[1- 6]	
Interval from beginning of Girder								
				4.100		7.699		11.299
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1177	○	1197	○	1199	○
Effective Prestressing Force (*1)	N/mm ²	1110	1097	○	1106	○	1098	○
Effective Prestressing Force (*2)	N/mm ²	1110	1010	○	1026	○	1020	○
max	N/mm ²	1110	1028	○	1067	○	1079	○
Ultimate Load	-----	1.00	1.75	○	1.24	○	1.12	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1- 7]		[1- 8]		[1- 9]	
Interval from beginning of Girder								
				13.949		14.899		15.929
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1176	○	1172	○	1167	○
Effective Prestressing Force (*1)	N/mm ²	1110	1075	○	1071	○	1067	○
Effective Prestressing Force (*2)	N/mm ²	1110	1000	○	996	○	990	○
max	N/mm ²	1110	1063	○	1058	○	1051	○
Ultimate Load	-----	1.00	1.10	○	1.11	○	1.13	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1-10]	[1-11]	[1-12]
Interval from beginning of Girder			18.499	22.098	25.698
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	1320	1320
Immediately After Prestressing	N/mm ²	1295	1164	1174	1157
Effective Prestressing Force (*1)	N/mm ²	1110	1067	1089	1084
Effective Prestressing Force (*2)	N/mm ²	1110	987	1002	989
max	N/mm ²	1110	1037	1028	991
Ultimate Load	-----	1.00	1.20	1.43	2.35

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1-13]	[1-14]	[1-15]
Interval from beginning of Girder			25.798	28.298	29.298
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	1320	1320
Immediately After Prestressing	N/mm ²	1295	1156	1104	1099
Effective Prestressing Force (*1)	N/mm ²	1110	1084	1047	1044
Effective Prestressing Force (*2)	N/mm ²	1110	989	971	971
max	N/mm ²	1110	990	969	967
Ultimate Load	-----	1.00	2.41	2.49	1.55

*1:During DeckConstruction *2:Design Load

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 4(Shear Force Max)

Cross Section Number			Allowable Value	[1- 1]	[1- 2]	[1- 3]	
Interval from beginning of Girder			-----	0.500	1.500	4.000	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.59 Δ 1.34 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.06 ○ -0.16 ○	
	Neutral Axis before Composition			-----	--	-0.06 ○ -0.15 ○	
	Neutral Axis after Composition			-----	--	-0.07 ○ -0.17 ○	
	Base of Lower Flange			-----	--	-0.01 ○ -0.10 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.16 ○ -0.51 ○	
				Min	-----	--	-0.05 ○ -0.13 ○
	Neutral Axis before Composition			Max	-----	--	-0.18 ○ -0.55 ○
				Min	-----	--	-0.05 ○ -0.12 ○
	Neutral Axis after Composition			Max	-----	--	-0.20 ○ -0.56 ○
				Min	-----	--	-0.06 ○ -0.14 ○
	Base of Lower Flange			Max	-----	--	-0.03 ○ -0.44 ○
				Min	-----	--	-0.01 ○ -0.08 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 -- 20.37 --	
	D16	cm	-----	-----	--	32.03 -- 31.93 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	-----	--	1.98 -- 11.42 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	-----	--	3.58 ○ 1.72 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	--	1.313 ○ 1.00 ○	
	D16			-----	--	1.313 ○ 1.00 ○	
	D19			-----	--	1.371 ○ 1.07 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.59 Δ 1.34 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.06 ○ -0.16 ○	
	Neutral Axis before Composition			-----	--	-0.06 ○ -0.15 ○	
	Neutral Axis after Composition			-----	--	-0.07 ○ -0.17 ○	
	Base of Lower Flange			-----	--	-0.01 ○ -0.10 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.16 ○ -0.51 ○	
				Min	-----	--	-0.05 ○ -0.13 ○
	Neutral Axis before Composition			Max	-----	--	-0.18 ○ -0.55 ○
				Min	-----	--	-0.05 ○ -0.12 ○
	Neutral Axis after Composition			Max	-----	--	-0.20 ○ -0.56 ○
				Min	-----	--	-0.06 ○ -0.14 ○
	Base of Lower Flange			Max	-----	--	-0.03 ○ -0.44 ○
				Min	-----	--	-0.01 ○ -0.08 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 -- 20.37 --	
	D16	cm	-----	-----	--	32.03 -- 31.93 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	-----	--	0.00 -- 0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 4(Shear Force Max)

Cross Section Number			Allowable Value	[1- 4]	[1- 5]	[1- 6]				
Interval from beginning of Girder			-----	4.100	7.699	11.299				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.31	Δ	0.84	Δ	0.54	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.15	○	-0.04	○	-0.01	○	
	Neutral Axis before Composition			-0.14	○	-0.04	○	-0.01	○	
	Neutral Axis after Composition			-0.16	○	-0.04	○	-0.01	○	
	Base of Lower Flange			-0.10	○	-0.03	○	-0.01	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.49	○	-0.20	○	-0.08	○
				Min	-0.13	○	-0.01	○	-0.01	○
	Neutral Axis before Composition	Max		-0.53	○	-0.26	○	-0.12	○	
		Min		-0.12	○	-0.01	○	-0.01	○	
	Neutral Axis after Composition	Max		-0.54	○	-0.24	○	-0.10	○	
		Min		-0.13	○	-0.01	○	-0.01	○	
	Base of Lower Flange	Max		-0.43	○	-0.30	○	-0.20	○	
		Min		-0.08	○	-0.01	○	0.00	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	20.73	--	40.00	--	40.00	--	
	D16	cm	-----	32.49	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	11.23	--	5.48	--	1.40	--	
Compressive Strength to Failure (Suc/Shu)		-----	1.00	1.74	○	2.47	○	3.91	○	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.00	○	1.021	○	-----	--	
	D16			1.00	○	1.223	○	-----	--	
	D19			1.08	○	1.471	○	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.31	Δ	0.84	Δ	0.54	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.15	○	-0.04	○	-0.01	○	
	Neutral Axis before Composition			-0.14	○	-0.04	○	-0.01	○	
	Neutral Axis after Composition			-0.16	○	-0.04	○	-0.01	○	
	Base of Lower Flange			-0.10	○	-0.03	○	-0.01	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.49	○	-0.20	○	-0.08	○
				Min	-0.13	○	-0.01	○	-0.01	○
	Neutral Axis before Composition	Max		-0.53	○	-0.26	○	-0.12	○	
		Min		-0.12	○	-0.01	○	-0.01	○	
	Neutral Axis after Composition	Max		-0.54	○	-0.24	○	-0.10	○	
		Min		-0.13	○	-0.01	○	-0.01	○	
	Base of Lower Flange	Max		-0.43	○	-0.30	○	-0.20	○	
		Min		-0.08	○	-0.01	○	0.00	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	20.73	--	40.00	--	40.00	--	
	D16	cm	-----	32.49	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 4(Shear Force Max)

Cross Section Number			Allowable Value	[1- 7]	[1- 8]	[1- 9]	
Interval from beginning of Girder			-----	13.949	14.899	15.929	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.39 ○	0.47 ○	0.57 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00 ○	0.00 ○	-0.01 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	-0.01 ○	
	Neutral Axis after Composition			0.00 ○	0.00 ○	-0.01 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	-0.01 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.04 ○	-0.01 ○	-0.01 ○
				Min	-0.03 ○	-0.07 ○	-0.10 ○
	Neutral Axis before Composition			Max	-0.07 ○	-0.02 ○	-0.01 ○
				Min	-0.03 ○	-0.07 ○	-0.11 ○
	Neutral Axis after Composition			Max	-0.05 ○	-0.02 ○	-0.01 ○
				Min	-0.03 ○	-0.08 ○	-0.11 ○
	Base of Lower Flange			Max	-0.16 ○	-0.06 ○	-0.03 ○
				Min	-0.02 ○	-0.05 ○	-0.08 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.80 --	1.88 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	5.55 ○	4.35 ○	3.84 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	-----	1.42 ○	
	D16			-----	-----	1.78 ○	
	D19			-----	-----	2.21 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.39 ○	0.47 ○	0.57 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00 ○	0.00 ○	-0.01 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	-0.01 ○	
	Neutral Axis after Composition			0.00 ○	0.00 ○	-0.01 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	-0.01 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.04 ○	-0.01 ○	-0.01 ○
				Min	-0.03 ○	-0.07 ○	-0.10 ○
	Neutral Axis before Composition			Max	-0.07 ○	-0.02 ○	-0.01 ○
				Min	-0.03 ○	-0.07 ○	-0.11 ○
	Neutral Axis after Composition			Max	-0.05 ○	-0.02 ○	-0.01 ○
				Min	-0.03 ○	-0.08 ○	-0.11 ○
	Base of Lower Flange			Max	-0.16 ○	-0.06 ○	-0.03 ○
				Min	-0.02 ○	-0.05 ○	-0.08 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 4(Shear Force Max)

Cross Section Number			Allowable Value	[1-10]	[1-11]	[1-12]
Interval from beginning of Girder			-----	18.499	22.098	25.698
Shear Force						
Shear Stress	Design Load	N/mm ²	0.55	0.58 Δ	0.85 Δ	1.04 Δ
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00 ○	-0.03 ○	-0.04 ○
	Neutral Axis before Composition			0.00 ○	-0.02 ○	-0.03 ○
	Neutral Axis after Composition			0.00 ○	-0.02 ○	-0.04 ○
	Base of Lower Flange			0.00 ○	-0.02 ○	-0.02 ○
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00 ○	-0.02 ○
				Min	-0.12 ○	-0.24 ○
	Neutral Axis before Composition			Max	0.00 ○	-0.01 ○
				Min	-0.10 ○	-0.21 ○
	Neutral Axis after Composition			Max	0.00 ○	-0.01 ○
				Min	-0.12 ○	-0.24 ○
	Base of Lower Flange			Max	0.00 ○	-0.01 ○
				Min	-0.07 ○	-0.15 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	30.80 --	19.67 --
	D16	cm	-----	40.00 --	40.00 --	30.83 --
	D19	cm	-----	40.00 --	40.00 --	40.00 --
Axial Reinforcement Bar Volume	cm ²	-----	3.57 --	7.55 --	11.83 --	
Compressive Strength to Failure (Suc/Shu)	-----	1.00	2.77 ○	2.01 ○	1.59 ○	
Strength against Diagonal Tensile Failure(Sus/Shu)	D13	-----	1.00	1.162 ○	1 ○	1.00 ○
	D16			1.399 ○	1.076 ○	1.00 ○
	D19			1.688 ○	1.273 ○	1.05 ○
Shear Force + Torsion						
Shear Stress	Design Load	N/mm ²	0.55	0.58 Δ	0.85 Δ	1.04 Δ
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00 ○	-0.03 ○	-0.04 ○
	Neutral Axis before Composition			0.00 ○	-0.02 ○	-0.03 ○
	Neutral Axis after Composition			0.00 ○	-0.02 ○	-0.04 ○
	Base of Lower Flange			0.00 ○	-0.02 ○	-0.02 ○
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00 ○	-0.02 ○
				Min	-0.12 ○	-0.24 ○
	Neutral Axis before Composition			Max	0.00 ○	-0.01 ○
				Min	-0.10 ○	-0.21 ○
	Neutral Axis after Composition			Max	0.00 ○	-0.01 ○
				Min	-0.12 ○	-0.24 ○
	Base of Lower Flange			Max	0.00 ○	-0.01 ○
				Min	-0.07 ○	-0.15 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	30.80 --	19.67 --
	D16	cm	-----	40.00 --	40.00 --	30.83 --
	D19	cm	-----	40.00 --	40.00 --	40.00 --
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 4(Shear Force Max)

Cross Section Number			Allowable Value	[1-13]	[1-14]	[1-15]				
Interval from beginning of Girder			-----	25.798	28.298	29.298				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.06	Δ	1.15	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.05	○	-0.20	○	-----	--	
	Neutral Axis before Composition			-0.04	○	-0.32	○	-----	--	
	Neutral Axis after Composition			-0.05	○	-0.31	○	-----	--	
	Base of Lower Flange			-0.03	○	-0.08	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.02	○	-0.17	○	-----	--
				Min	-0.37	○	-0.45	○	-----	--
	Neutral Axis before Composition			Max	-0.02	○	-0.30	○	-----	--
				Min	-0.31	○	-0.50	○	-----	--
	Neutral Axis after Composition			Max	-0.02	○	-0.28	○	-----	--
				Min	-0.36	○	-0.55	○	-----	--
	Base of Lower Flange			Max	-0.01	○	-0.08	○	-----	--
				Min	-0.20	○	-0.09	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	19.29	--	14.74	--	-----	--	
	D16	cm	-----	30.24	--	23.10	--	-----	--	
	D19	cm	-----	40.00	--	33.32	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	12.06	--	14.51	--	-----	--	
Compressive Strength to Failure (Suc/Shu)			-----	1.00	1.58	○	2.74	○	-----	--
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1	○	1	○	-----	--	
	D16			1	○	1	○	-----	--	
	D19			1.039	○	1	○	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.06	Δ	1.15	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.05	○	-0.20	○	-----	--	
	Neutral Axis before Composition			-0.04	○	-0.32	○	-----	--	
	Neutral Axis after Composition			-0.05	○	-0.31	○	-----	--	
	Base of Lower Flange			-0.03	○	-0.08	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.02	○	-0.17	○	-----	--
				Min	-0.37	○	-0.45	○	-----	--
	Neutral Axis before Composition			Max	-0.02	○	-0.30	○	-----	--
				Min	-0.31	○	-0.50	○	-----	--
	Neutral Axis after Composition			Max	-0.02	○	-0.28	○	-----	--
				Min	-0.36	○	-0.55	○	-----	--
	Base of Lower Flange			Max	-0.01	○	-0.08	○	-----	--
				Min	-0.20	○	-0.09	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	19.29	--	14.74	--	-----	--	
	D16	cm	-----	30.24	--	23.10	--	-----	--	
	D19	cm	-----	40.00	--	33.32	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1- 1]	[1- 2]	[1- 3]	
Interval from beginning of Girder			-----	0.500	1.500	4.000	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.44 ○ 1.03 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.03 ○ -0.07 ○	
	Neutral Axis before Composition			-----	--	-0.03 ○ -0.06 ○	
	Neutral Axis after Composition			-----	--	-0.03 ○ -0.07 ○	
	Base of Lower Flange			-----	--	0.00 ○ -0.04 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.10 ○ -0.33 ○	
				Min	-----	--	-0.03 ○ -0.07 ○
	Neutral Axis before Composition			Max	-----	--	-0.10 ○ -0.32 ○
				Min	-----	--	-0.03 ○ -0.06 ○
	Neutral Axis after Composition			Max	-----	--	-0.11 ○ -0.35 ○
				Min	-----	--	-0.03 ○ -0.07 ○
	Base of Lower Flange			Max	-----	--	-0.02 ○ -0.23 ○
				Min	-----	--	-0.01 ○ -0.04 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 -- 31.61 --	
	D16	cm	-----	-----	--	32.03 -- 40.00 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 -- 7.36 --	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.44 ○ 1.03 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.03 ○ -0.07 ○	
	Neutral Axis before Composition			-----	--	-0.03 ○ -0.06 ○	
	Neutral Axis after Composition			-----	--	-0.03 ○ -0.07 ○	
	Base of Lower Flange			-----	--	0.00 ○ -0.04 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.10 ○ -0.33 ○	
				Min	-----	--	-0.03 ○ -0.07 ○
	Neutral Axis before Composition			Max	-----	--	-0.10 ○ -0.32 ○
				Min	-----	--	-0.03 ○ -0.06 ○
	Neutral Axis after Composition			Max	-----	--	-0.11 ○ -0.35 ○
				Min	-----	--	-0.03 ○ -0.07 ○
	Base of Lower Flange			Max	-----	--	-0.02 ○ -0.23 ○
				Min	-----	--	-0.01 ○ -0.04 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 -- 31.61 --	
	D16	cm	-----	-----	--	32.03 -- 40.00 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 -- 0.00 --	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	-----	--	999.999 ○ 999.999 ○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	--	----- - 999.999 ○	
	D16			-----	--	----- - 999.999 ○	
	D19			-----	--	----- - 999.999 ○	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1- 4]	[1- 5]	[1- 6]				
Interval from beginning of Girder			-----	4.100	7.699	11.299				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.01	Δ	0.69	Δ	0.40	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.07	○	-0.01	○	0.00	○	
	Neutral Axis before Composition			-0.06	○	-0.01	○	0.00	○	
	Neutral Axis after Composition			-0.07	○	-0.01	○	0.00	○	
	Base of Lower Flange			-0.04	○	-0.01	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.32	○	-0.15	○	-0.05	○
				Min	-0.07	○	-0.01	○	0.00	○
	Neutral Axis before Composition			Max	-0.31	○	-0.16	○	-0.06	○
				Min	-0.06	○	-0.01	○	0.00	○
	Neutral Axis after Composition			Max	-0.34	○	-0.16	○	-0.06	○
				Min	-0.07	○	-0.01	○	0.00	○
	Base of Lower Flange			Max	-0.23	○	-0.15	○	-0.07	○
				Min	-0.03	○	-0.01	○	0.00	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	32.18	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	7.23	--	3.49	--	0.00	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.01	Δ	0.69	Δ	0.40	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.07	○	-0.01	○	0.00	○	
	Neutral Axis before Composition			-0.06	○	-0.01	○	0.00	○	
	Neutral Axis after Composition			-0.07	○	-0.01	○	0.00	○	
	Base of Lower Flange			-0.04	○	-0.01	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.32	○	-0.15	○	-0.05	○
				Min	-0.07	○	-0.01	○	0.00	○
	Neutral Axis before Composition			Max	-0.31	○	-0.16	○	-0.06	○
				Min	-0.06	○	-0.01	○	0.00	○
	Neutral Axis after Composition			Max	-0.34	○	-0.16	○	-0.06	○
				Min	-0.07	○	-0.01	○	0.00	○
	Base of Lower Flange			Max	-0.23	○	-0.15	○	-0.07	○
				Min	-0.03	○	-0.01	○	0.00	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	32.18	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	-	
	D16			999.999	○	999.999	○	-----	-	
	D19			999.999	○	999.999	○	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1- 7]	[1- 8]	[1- 9]			
Interval from beginning of Girder			-----	13.949	14.899	15.929			
Shear Force									
Shear Stress	Design Load	N/mm ²	0.55	0.16	○	0.05	○	0.33	○
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○
	Base of Lower Flange			0.00	○	0.00	○	0.00	○
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	○	0.00	○	0.00	○
				Min	○	0.00	○	-0.03	○
	Neutral Axis before Composition	Max		○	0.00	○	0.00	○	
		Min		○	0.00	○	-0.05	○	
	Neutral Axis after Composition	Max		○	0.00	○	0.00	○	
		Min		○	0.00	○	-0.04	○	
	Base of Lower Flange	Max		○	0.00	○	0.00	○	
		Min		○	0.00	○	-0.08	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--
	D16	cm	-----	40.00	--	40.00	--	40.00	--
	D19	cm	-----	40.00	--	40.00	--	40.00	--
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--
Shear Force + Torsion									
Shear Stress	Design Load	N/mm ²	0.55	0.16	○	0.05	○	0.33	○
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○
	Base of Lower Flange			0.00	○	0.00	○	0.00	○
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	○	0.00	○	0.00	○
				Min	○	0.00	○	-0.03	○
	Neutral Axis before Composition	Max		○	0.00	○	0.00	○	
		Min		○	0.00	○	-0.05	○	
	Neutral Axis after Composition	Max		○	0.00	○	0.00	○	
		Min		○	0.00	○	-0.04	○	
	Base of Lower Flange	Max		○	0.00	○	0.00	○	
		Min		○	0.00	○	-0.08	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--
	D16	cm	-----	40.00	--	40.00	--	40.00	--
	D19	cm	-----	40.00	--	40.00	--	40.00	--
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	-----	-	-----	-
	D16	-----	1.00	-----	-	-----	-	-----	-
	D19	-----	1.00	-----	-	-----	-	-----	-

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1-10]	[1-11]	[1-12]				
Interval from beginning of Girder			-----	18.499	22.098	25.698				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.43	○	0.47	○	0.68	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	0.00	○	0.00	○
				Min	-0.06	○	-0.08	○	-0.16	○
	Neutral Axis before Composition			Max	-0.01	○	0.00	○	0.00	○
				Min	-0.07	○	-0.07	○	-0.14	○
	Neutral Axis after Composition			Max	-0.01	○	0.00	○	0.00	○
				Min	-0.07	○	-0.08	○	-0.16	○
	Base of Lower Flange			Max	0.00	○	0.00	○	0.00	○
				Min	-0.09	○	-0.06	○	-0.10	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	29.72	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	1.96	--	3.59	--	7.83	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.43	○	0.47	○	0.68	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	0.00	○	0.00	○
				Min	-0.06	○	-0.08	○	-0.16	○
	Neutral Axis before Composition			Max	-0.01	○	0.00	○	0.00	○
				Min	-0.07	○	-0.07	○	-0.14	○
	Neutral Axis after Composition			Max	-0.01	○	0.00	○	0.00	○
				Min	-0.07	○	-0.08	○	-0.16	○
	Base of Lower Flange			Max	0.00	○	0.00	○	0.00	○
				Min	-0.09	○	-0.06	○	-0.10	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	29.72	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	-----	-	999.999	○	
	D16	-----	1.00	-----	-	-----	-	999.999	○	
	D19	-----	1.00	-----	-	-----	-	999.999	○	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1-13]	[1-14]	[1-15]				
Interval from beginning of Girder			-----	25.798	28.298	29.298				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.70	Δ	0.98	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	-0.11	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.23	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.21	○	-----	--	
	Base of Lower Flange			0.00	○	-0.06	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	-0.12	○	-----	--
				Min	-0.17	○	-0.30	○	-----	--
	Neutral Axis before Composition	Max		0.00	○	-0.21	○	-----	--	
		Min		-0.15	○	-0.40	○	-----	--	
	Neutral Axis after Composition	Max		0.00	○	-0.20	○	-----	--	
		Min		-0.17	○	-0.41	○	-----	--	
	Base of Lower Flange	Max		0.00	○	-0.05	○	-----	--	
		Min		-0.11	○	-0.08	○	-----	--	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	29.00	--	20.44	--	-----	--	
	D16	cm	-----	40.00	--	32.03	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	8.02	--	9.67	--	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.70	Δ	0.98	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	-0.11	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.23	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.21	○	-----	--	
	Base of Lower Flange			0.00	○	-0.06	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	-0.12	○	-----	--
				Min	-0.17	○	-0.30	○	-----	--
	Neutral Axis before Composition	Max		0.00	○	-0.21	○	-----	--	
		Min		-0.15	○	-0.40	○	-----	--	
	Neutral Axis after Composition	Max		0.00	○	-0.20	○	-----	--	
		Min		-0.17	○	-0.41	○	-----	--	
	Base of Lower Flange	Max		0.00	○	-0.05	○	-----	--	
		Min		-0.11	○	-0.08	○	-----	--	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	29.00	--	20.44	--	-----	--	
	D16	cm	-----	40.00	--	32.03	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	-----	--	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	--	
	D16	-----		999.999	○	999.999	○	-----	--	
	D19	-----		999.999	○	999.999	○	-----	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[2-1]		[2-2]		[2-3]	
Interval from beginning of Girder		-----	0.500		1.500		4.000	
Immediately After Prestressing	Top of Main Girder	-1.5	3.413	○	4.219	○	6.224	
	Bottom of Main Girder	~19.00	3.729	○	3.488	○	7.018	
During Deck Construction	Top of Main Girder	-1.5	3.229	○	4.549	○	7.931	
	Bottom of Main Girder	~14.00	3.554	○	2.677	○	4.132	
Dead Load	Top of Deck	≤10.00	0.346	○	0.809	○	1.696	
	Top of Main Girder	0	2.334	○	3.300	○	5.518	
	Bottom of Main Girder	~14.00	3.745	○	2.804	○	3.301	
Design Load1	Top of Deck	Max	0.489	○	0.995	○	2.063	
		Min	≤10.00	-1.000	○	-0.329	○	0.951
	Top of Main Girder	Max	-1.5	2.460	○	3.463	○	5.828
		Min	~14.00	1.144	○	2.301	○	4.891
	Bottom of Main Girder	Max	~14.00	3.494	○	2.465	○	2.470
		Min	~14.00	6.106	○	4.876	○	4.985
Design Load2 Temperature Rise	Top of Deck	Max	≤11.50	1.519	○	2.010	○	
		Min	≤11.50	0.029	○	0.686	○	
	Top of Main Girder	Max	-2	2.051	○	3.036	○	
		Min	~16.10	0.735	○	1.874	○	
	Bottom of Main Girder	Max	~16.10	3.098	○	2.030	○	
		Min	~16.10	5.710	○	4.441	○	
Design Load3 Temperature Drop	Top of Deck	Max	≤11.50	1.519	○	2.010	○	
		Min	≤11.50	0.029	○	0.686	○	
	Top of Main Girder	Max	-2	2.051	○	3.036	○	
		Min	~16.10	0.735	○	1.874	○	
	Bottom of Main Girder	Max	~16.10	3.098	○	2.030	○	
		Min	~16.10	5.710	○	4.441	○	
Design Load4 Support sinking	Top of Deck	Max	≤10.00	0.489	○	0.995	○	
		Min	≤10.00	-1.000	○	-0.329	○	
	Top of Main Girder	Max	-1.5	2.460	○	3.463	○	
		Min	~14.00	1.144	○	2.301	○	
	Bottom of Main Girder	Max	~14.00	3.494	○	2.465	○	
		Min	~14.00	6.106	○	4.876	○	
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	≤11.50	1.519	○	2.010	○	
		Min	≤11.50	0.029	○	0.686	○	
	Top of Main Girder	Max	-2	2.051	○	3.036	○	
		Min	~16.10	0.735	○	1.874	○	
	Bottom of Main Girder	Max	~16.10	3.098	○	2.030	○	
		Min	~16.10	5.710	○	4.441	○	
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	≤11.50	1.519	○	2.010	○	
		Min	≤11.50	0.029	○	0.686	○	
	Top of Main Girder	Max	-2	2.051	○	3.036	○	
		Min	~16.10	0.735	○	1.874	○	
	Bottom of Main Girder	Max	~16.10	3.098	○	2.030	○	
		Min	~16.10	5.710	○	4.441	○	

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[2- 4]		[2- 5]		[2- 6]		
Interval from beginning of Girder		-----	4.100		7.700		11.300		
Immediately After Prestressing	Top of Main Girder	-1.5	6.127	○	3.091	○	1.096	○	
	Bottom of Main Girder	~19.00	7.137	○	10.982	○	13.173	○	
During Deck Construction	Top of Main Girder	-1.5	7.892	○	6.616	○	5.764	○	
	Bottom of Main Girder	~14.00	4.183	○	5.888	○	6.659	○	
Dead Load	Top of Deck	≤10.00	1.706	○	2.018	○	2.250	○	
	Top of Main Girder	0	5.507	○	5.062	○	4.739	○	
	Bottom of Main Girder	~14.00	3.310	○	3.687	○	3.602	○	
Design Load1	Top of Deck	Max	2.083	○	2.832	○	3.321	○	
		Min	0.974	○	1.472	○	1.822	○	
	Top of Main Girder	Max	5.824	○	5.750	○	5.645	○	
		Min	-1.5	4.889	○	4.601	○	4.377	○
	Bottom of Main Girder	Max	~14.00	2.458	○	1.864	○	1.216	○
		Min		4.966	○	4.910	○	4.554	○
Design Load2 Temperature Rise	Top of Deck	Max	3.014	○	3.742	○	4.209	○	
		Min	≤11.50	1.905	○	2.382	○	2.710	○
	Top of Main Girder	Max	5.289	○	5.197	○	5.074	○	
		Min	-2	4.353	○	4.048	○	3.806	○
	Bottom of Main Girder	Max	~16.10	1.727	○	1.192	○	0.599	○
		Min		4.235	○	4.238	○	3.936	○
Design Load3 Temperature Drop	Top of Deck	Max	3.014	○	3.742	○	4.209	○	
		Min	≤11.50	1.905	○	2.382	○	2.710	○
	Top of Main Girder	Max	5.289	○	5.197	○	5.074	○	
		Min	-2	4.353	○	4.048	○	3.806	○
	Bottom of Main Girder	Max	~16.10	1.727	○	1.192	○	0.599	○
		Min		4.235	○	4.238	○	3.936	○
Design Load4 Support sinking	Top of Deck	Max	2.083	○	2.832	○	3.321	○	
		Min	≤10.00	0.974	○	1.472	○	1.822	○
	Top of Main Girder	Max	5.824	○	5.750	○	5.645	○	
		Min	-1.5	4.889	○	4.601	○	4.377	○
	Bottom of Main Girder	Max	~14.00	2.458	○	1.864	○	1.216	○
		Min		4.966	○	4.910	○	4.554	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	3.014	○	3.742	○	4.209	○	
		Min	≤11.50	1.905	○	2.382	○	2.710	○
	Top of Main Girder	Max	5.289	○	5.197	○	5.074	○	
		Min	-2	4.353	○	4.048	○	3.806	○
	Bottom of Main Girder	Max	~16.10	1.727	○	1.192	○	0.599	○
		Min		4.235	○	4.238	○	3.936	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	3.014	○	3.742	○	4.209	○	
		Min	≤11.50	1.905	○	2.382	○	2.710	○
	Top of Main Girder	Max	5.289	○	5.197	○	5.074	○	
		Min	-2	4.353	○	4.048	○	3.806	○
	Bottom of Main Girder	Max	~16.10	1.727	○	1.192	○	0.599	○
		Min		4.235	○	4.238	○	3.936	○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[2- 7]		[2- 8]		[2- 9]		
Interval from beginning of Girder		-----	13.869		14.900		15.931		
Immediately After Prestressing	Top of Main Girder	-1.5	0.789	○	0.833	○	0.790	○	
	Bottom of Main Girder	~19.00	13.199	○	13.089	○	13.198	○	
During Deck Construction	Top of Main Girder	-1.5	5.847	○	5.926	○	5.849	○	
	Bottom of Main Girder	~14.00	6.244	○	6.102	○	6.241	○	
Dead Load	Top of Deck	≤10.00	2.449	○	2.491	○	2.463	○	
	Top of Main Girder	0	4.868	○	4.928	○	4.879	○	
	Bottom of Main Girder	~14.00	2.980	○	2.830	○	2.960	○	
Design Load1	Top of Deck	Max	3.583	○	3.630	○	3.600	○	
		Min	2.096	○	2.155	○	2.127	○	
	Top of Main Girder	Max	5.828	○	5.892	○	5.840	○	
		Min	-1.5	4.570	○	4.644	○	4.594	○
	Bottom of Main Girder	Max	~14.00	0.459	○	0.298	○	0.434	○
		Min		3.763	○	3.578	○	3.707	○
Design Load2 Temperature Rise	Top of Deck	Max	4.457	○	4.498	○	4.463	○	
		Min	≤11.50	2.970	○	3.023	○	2.990	○
	Top of Main Girder	Max	5.245	○	5.305	○	5.248	○	
		Min	-2	3.987	○	4.057	○	4.003	○
	Bottom of Main Girder	Max	~16.10	-0.126	○	-0.275	○	-0.128	○
		Min		3.179	○	3.004	○	3.145	○
Design Load3 Temperature Drop	Top of Deck	Max	4.457	○	4.498	○	4.463	○	
		Min	≤11.50	2.970	○	3.023	○	2.990	○
	Top of Main Girder	Max	5.245	○	5.305	○	5.248	○	
		Min	-2	3.987	○	4.057	○	4.003	○
	Bottom of Main Girder	Max	~16.10	-0.126	○	-0.275	○	-0.128	○
		Min		3.179	○	3.004	○	3.145	○
Design Load4 Support sinking	Top of Deck	Max	3.583	○	3.630	○	3.600	○	
		Min	≤10.00	2.096	○	2.155	○	2.127	○
	Top of Main Girder	Max	5.828	○	5.892	○	5.840	○	
		Min	-1.5	4.570	○	4.644	○	4.594	○
	Bottom of Main Girder	Max	~14.00	0.459	○	0.298	○	0.434	○
		Min		3.763	○	3.578	○	3.707	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	4.457	○	4.498	○	4.463	○	
		Min	≤11.50	2.970	○	3.023	○	2.990	○
	Top of Main Girder	Max	5.245	○	5.305	○	5.248	○	
		Min	-2	3.987	○	4.057	○	4.003	○
	Bottom of Main Girder	Max	~16.10	-0.126	○	-0.275	○	-0.128	○
		Min		3.179	○	3.004	○	3.145	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	4.457	○	4.498	○	4.463	○	
		Min	≤11.50	2.970	○	3.023	○	2.990	○
	Top of Main Girder	Max	5.245	○	5.305	○	5.248	○	
		Min	-2	3.987	○	4.057	○	4.003	○
	Bottom of Main Girder	Max	~16.10	-0.126	○	-0.275	○	-0.128	○
		Min		3.179	○	3.004	○	3.145	○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[2-10]		[2-11]		[2-12]		
Interval from beginning of Girder		-----	18.500		22.100		25.700		
Immediately After Prestressing	Top of Main Girder	-1.5	1.101	○	3.100	○	6.141	○	
	Bottom of Main Girder	~19.00	13.167	○	10.971	○	7.121	○	
During Deck Construction	Top of Main Girder	-1.5	5.773	○	6.635	○	7.921	○	
	Bottom of Main Girder	~14.00	6.648	○	5.866	○	4.150	○	
Dead Load	Top of Deck	≤10.00	2.300	○	2.120	○	1.860	○	
	Top of Main Girder	0	4.778	○	5.154	○	5.662	○	
	Bottom of Main Girder	~14.00	3.526	○	3.507	○	2.983	○	
Design Load1	Top of Deck	Max	3.379	○	2.952	○	2.296	○	
		Min	1.927	○	1.660	○	1.228	○	
	Top of Main Girder	Max	5.691	○	5.858	○	6.030	○	
		Min	-1.5	4.462	○	4.766	○	5.130	○
	Bottom of Main Girder	Max	~14.00	1.124	○	1.643	○	1.998	○
		Min		4.357	○	4.535	○	4.411	○
Design Load2 Temperature Rise	Top of Deck	Max	4.230	○	3.787	○	3.114	○	
		Min	≤11.50	2.778	○	2.496	○	2.047	○
	Top of Main Girder	Max	5.089	○	5.242	○	5.399	○	
		Min	-2	3.860	○	4.150	○	4.499	○
	Bottom of Main Girder	Max	~16.10	0.589	○	1.137	○	1.521	○
		Min		3.821	○	4.030	○	3.934	○
Design Load3 Temperature Drop	Top of Deck	Max	4.230	○	3.787	○	3.114	○	
		Min	≤11.50	2.778	○	2.496	○	2.047	○
	Top of Main Girder	Max	5.089	○	5.242	○	5.399	○	
		Min	-2	3.860	○	4.150	○	4.499	○
	Bottom of Main Girder	Max	~16.10	0.589	○	1.137	○	1.521	○
		Min		3.821	○	4.030	○	3.934	○
Design Load4 Support sinking	Top of Deck	Max	3.379	○	2.952	○	2.296	○	
		Min	≤10.00	1.927	○	1.660	○	1.228	○
	Top of Main Girder	Max	5.691	○	5.858	○	6.030	○	
		Min	-1.5	4.462	○	4.766	○	5.130	○
	Bottom of Main Girder	Max	~14.00	1.124	○	1.643	○	1.998	○
		Min		4.357	○	4.535	○	4.411	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	4.230	○	3.787	○	3.114	○	
		Min	≤11.50	2.778	○	2.496	○	2.047	○
	Top of Main Girder	Max	5.089	○	5.242	○	5.399	○	
		Min	-2	3.860	○	4.150	○	4.499	○
	Bottom of Main Girder	Max	~16.10	0.589	○	1.137	○	1.521	○
		Min		3.821	○	4.030	○	3.934	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	4.230	○	3.787	○	3.114	○	
		Min	≤11.50	2.778	○	2.496	○	2.047	○
	Top of Main Girder	Max	5.089	○	5.242	○	5.399	○	
		Min	-2	3.860	○	4.150	○	4.499	○
	Bottom of Main Girder	Max	~16.10	0.589	○	1.137	○	1.521	○
		Min		3.821	○	4.030	○	3.934	○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[2-13]		[2-14]		[2-15]	
Interval from beginning of Girder		-----	25.800		28.300		29.300	
Immediately After Prestressing	Top of Main Girder	-1.5	6.238	○	4.234	○	3.428	
	Bottom of Main Girder	~19.00	7.001	○	3.471	○	3.711	
During Deck Construction	Top of Main Girder	-1.5	7.960	○	4.580	○	3.261	
	Bottom of Main Girder	~14.00	4.099	○	2.642	○	3.518	
Dead Load	Top of Deck	≤10.00	1.851	○	0.996	○	0.545	
	Top of Main Girder	0	5.676	○	3.483	○	2.528	
	Bottom of Main Girder	~14.00	2.970	○	2.458	○	3.390	
Design Load1	Top of Deck	Max	2.279	○	1.274	○	0.794	
		Min	1.207	○	-0.048	○	-0.715	
	Top of Main Girder	Max	6.036	○	3.728	○	2.748	
		Min	-1.5	5.133	○	2.567	○	1.416
	Bottom of Main Girder	Max	~14.00	2.003	○	1.950	○	2.953
		Min		4.426	○	4.359	○	5.598
Design Load2 Temperature Rise	Top of Deck	Max	3.097	○	2.153	○	1.678	
		Min	≤11.50	2.026	○	0.831	○	0.170
	Top of Main Girder	Max	5.406	○	3.181	○	2.211	
		Min	-2	4.502	○	2.021	○	0.879
	Bottom of Main Girder	Max	~16.10	1.527	○	1.764	○	2.811
		Min		3.949	○	4.173	○	5.456
Design Load3 Temperature Drop	Top of Deck	Max	3.097	○	2.153	○	1.678	
		Min	≤11.50	2.026	○	0.831	○	0.170
	Top of Main Girder	Max	5.406	○	3.181	○	2.211	
		Min	-2	4.502	○	2.021	○	0.879
	Bottom of Main Girder	Max	~16.10	1.527	○	1.764	○	2.811
		Min		3.949	○	4.173	○	5.456
Design Load4 Support sinking	Top of Deck	Max	2.279	○	1.274	○	0.794	
		Min	≤10.00	1.207	○	-0.048	○	-0.715
	Top of Main Girder	Max	6.036	○	3.728	○	2.748	
		Min	-1.5	5.133	○	2.567	○	1.416
	Bottom of Main Girder	Max	~14.00	2.003	○	1.950	○	2.953
		Min		4.426	○	4.359	○	5.598
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	3.097	○	2.153	○	1.678	
		Min	≤11.50	2.026	○	0.831	○	0.170
	Top of Main Girder	Max	5.406	○	3.181	○	2.211	
		Min	-2	4.502	○	2.021	○	0.879
	Bottom of Main Girder	Max	~16.10	1.527	○	1.764	○	2.811
		Min		3.949	○	4.173	○	5.456
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	3.097	○	2.153	○	1.678	
		Min	≤11.50	2.026	○	0.831	○	0.170
	Top of Main Girder	Max	5.406	○	3.181	○	2.211	
		Min	-2	4.502	○	2.021	○	0.879
	Bottom of Main Girder	Max	~16.10	1.527	○	1.764	○	2.811
		Min		3.949	○	4.173	○	5.456

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Cross Section NumberNo.	Unit	Allowable Value	[2- 1]		[2- 2]		[2- 3]	
Interval from beginning of Girder								
				0.500		1.500		4.000
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1099	○	1103	○	1156	○
Effective Prestressing Force (*1)	N/mm ²	1110	1044	○	1046	○	1083	○
Effective Prestressing Force (*2)	N/mm ²	1110	972	○	972	○	987	○
max	N/mm ²	1110	970	○	970	○	988	○
Ultimate Load	-----	1.00	1.90	○	3.01	○	2.57	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2- 4]		[2- 5]		[2- 6]	
Interval from beginning of Girder								
				4.100		7.700		11.300
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1157	○	1174	○	1154	○
Effective Prestressing Force (*1)	N/mm ²	1110	1083	○	1089	○	1058	○
Effective Prestressing Force (*2)	N/mm ²	1110	987	○	995	○	968	○
max	N/mm ²	1110	988	○	1015	○	1007	○
Ultimate Load	-----	1.00	2.52	○	1.64	○	1.43	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2- 7]		[2- 8]		[2- 9]	
Interval from beginning of Girder								
				13.869		14.900		15.931
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1126	○	1121	○	1126	○
Effective Prestressing Force (*1)	N/mm ²	1110	1029	○	1025	○	1029	○
Effective Prestressing Force (*2)	N/mm ²	1110	946	○	944	○	947	○
max	N/mm ²	1110	992	○	991	○	994	○
Ultimate Load	-----	1.00	1.35	○	1.34	○	1.34	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2-10]	[2-11]	[2-12]
Interval from beginning of Girder			18.500	22.100	25.700
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	1320	1320
Immediately After Prestressing	N/mm ²	1295	1154	1174	1157
Effective Prestressing Force (*1)	N/mm ²	1110	1058	1089	1083
Effective Prestressing Force (*2)	N/mm ²	1110	970	1000	991
max	N/mm ²	1110	1011	1023	996
Ultimate Load	-----	1.00	1.40	1.56	2.16

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2-13]	[2-14]	[2-15]
Interval from beginning of Girder			25.800	28.300	29.300
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	1320	1320
Immediately After Prestressing	N/mm ²	1295	1156	1103	1099
Effective Prestressing Force (*1)	N/mm ²	1110	1083	1046	1044
Effective Prestressing Force (*2)	N/mm ²	1110	991	974	974
max	N/mm ²	1110	995	974	973
Ultimate Load	-----	1.00	2.19	3.96	2.26

*1:During DeckConstruction *2:Design Load

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2- 1]	[2- 2]	[2- 3]		
Interval from beginning of Girder			-----	0.500	1.500	4.000		
Shear Force								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	1.02 Δ	0.79 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.12 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.23 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.21 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.06 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.32 ○	-0.21 ○	
				Min	-----	--	-0.10 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.41 ○	-0.16 ○
				Min	-----	--	-0.22 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.43 ○	-0.20 ○
				Min	-----	--	-0.19 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.08 ○	-0.10 ○
				Min	-----	--	-0.06 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 --	28.66 --	
	D16	cm	-----	-----	--	32.03 --	40.00 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	9.85 --	8.12 --	
Compressive Strength to Failure (Suc/Shu)			1.00	-----	--	3.18 ○	1.84 ○	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	--	1.021 ○	1.00 ○	
	D16			-----	--	1.021 ○	1.04 ○	
	D19			-----	--	1.077 ○	1.21 ○	
Shear Force + Torsion								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	1.02 Δ	0.79 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.12 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.23 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.21 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.06 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.32 ○	-0.21 ○	
				Min	-----	--	-0.10 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.41 ○	-0.16 ○
				Min	-----	--	-0.22 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.43 ○	-0.20 ○
				Min	-----	--	-0.19 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.08 ○	-0.10 ○
				Min	-----	--	-0.06 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 --	28.66 --	
	D16	cm	-----	-----	--	32.03 --	40.00 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 --	0.00 --	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2- 4]	[2- 5]	[2- 6]	
Interval from beginning of Girder			-----	4.100	7.700	11.300	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.77 Δ	0.67 Δ	0.54 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00 ○	-0.01 ○	-0.01 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis after Composition			0.00 ○	-0.01 ○	0.00 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.20 ○	-0.16 ○	-0.10 ○
				Min	0.00 ○	0.00 ○	-0.01 ○
	Neutral Axis before Composition			Max	-0.16 ○	-0.12 ○	-0.08 ○
				Min	0.00 ○	0.00 ○	-0.02 ○
	Neutral Axis after Composition			Max	-0.19 ○	-0.15 ○	-0.10 ○
				Min	0.00 ○	0.00 ○	-0.01 ○
	Base of Lower Flange			Max	-0.10 ○	-0.08 ○	-0.05 ○
				Min	0.00 ○	0.00 ○	-0.02 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	29.35 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	7.93 --	4.91 --	1.94 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	1.85 ○	2.31 ○	3.15 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.00 ○	1.051 ○	----- --	
	D16			1.05 ○	1.237 ○	----- --	
	D19			1.22 ○	1.463 ○	----- --	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.77 Δ	0.67 Δ	0.54 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00 ○	-0.01 ○	-0.01 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis after Composition			0.00 ○	-0.01 ○	0.00 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.20 ○	-0.16 ○	-0.10 ○
				Min	0.00 ○	0.00 ○	-0.01 ○
	Neutral Axis before Composition			Max	-0.16 ○	-0.12 ○	-0.08 ○
				Min	0.00 ○	0.00 ○	-0.02 ○
	Neutral Axis after Composition			Max	-0.19 ○	-0.15 ○	-0.10 ○
				Min	0.00 ○	0.00 ○	-0.01 ○
	Base of Lower Flange			Max	-0.10 ○	-0.08 ○	-0.05 ○
				Min	0.00 ○	0.00 ○	-0.02 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	29.35 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2- 7]	[2- 8]	[2- 9]	
Interval from beginning of Girder			-----	13.869	14.900	15.931	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.62 Δ	0.46 ○	0.55 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.02 ○	-0.01 ○	-0.01 ○	
	Neutral Axis before Composition			-0.03 ○	-0.01 ○	-0.01 ○	
	Neutral Axis after Composition			-0.02 ○	-0.01 ○	-0.01 ○	
	Base of Lower Flange			-0.02 ○	-0.01 ○	-0.01 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.12 ○	-0.07 ○	-0.02 ○
				Min	-0.01 ○	-0.03 ○	-0.08 ○
	Neutral Axis before Composition			Max	-0.12 ○	-0.07 ○	-0.01 ○
				Min	-0.01 ○	-0.04 ○	-0.12 ○
	Neutral Axis after Composition			Max	-0.13 ○	-0.08 ○	-0.02 ○
				Min	-0.01 ○	-0.04 ○	-0.10 ○
	Base of Lower Flange			Max	-0.09 ○	-0.05 ○	-0.01 ○
				Min	-0.01 ○	-0.04 ○	-0.14 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	1.04 --	0.00 --	0.88 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	4.22 ○	5.15 ○	4.82 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.565 ○	----- --	1.67 ○	
	D16			1.956 ○	----- --	2.11 ○	
	D19			2.434 ○	----- --	2.66 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.62 Δ	0.46 ○	0.55 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.02 ○	-0.01 ○	-0.01 ○	
	Neutral Axis before Composition			-0.03 ○	-0.01 ○	-0.01 ○	
	Neutral Axis after Composition			-0.02 ○	-0.01 ○	-0.01 ○	
	Base of Lower Flange			-0.02 ○	-0.01 ○	-0.01 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.12 ○	-0.07 ○	-0.02 ○
				Min	-0.01 ○	-0.03 ○	-0.08 ○
	Neutral Axis before Composition			Max	-0.12 ○	-0.07 ○	-0.01 ○
				Min	-0.01 ○	-0.04 ○	-0.12 ○
	Neutral Axis after Composition			Max	-0.13 ○	-0.08 ○	-0.02 ○
				Min	-0.01 ○	-0.04 ○	-0.10 ○
	Base of Lower Flange			Max	-0.09 ○	-0.05 ○	-0.01 ○
				Min	-0.01 ○	-0.04 ○	-0.14 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2-10]	[2-11]	[2-12]	
Interval from beginning of Girder			-----	18.500	22.100	25.700	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.47 ○	0.61 △	0.70 △	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis after Composition			0.00 ○	0.00 ○	0.00 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.02 ○	0.00 ○	0.00 ○
				Min	-0.07 ○	-0.11 ○	-0.15 ○
	Neutral Axis before Composition			Max	-0.02 ○	-0.01 ○	-0.01 ○
				Min	-0.08 ○	-0.12 ○	-0.15 ○
	Neutral Axis after Composition			Max	-0.03 ○	-0.01 ○	0.00 ○
				Min	-0.08 ○	-0.13 ○	-0.16 ○
	Base of Lower Flange			Max	-0.02 ○	-0.01 ○	-0.01 ○
				Min	-0.08 ○	-0.11 ○	-0.13 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	32.70 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	1.61 --	4.52 --	7.12 --		
Compressive Strength to Failure (Suc/Shu)		-----	1.00	3.45 ○	2.44 ○	1.93 ○	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	1.077 ○	1.00 ○	
	D16			-----	1.272 ○	1.09 ○	
	D19			-----	1.512 ○	1.26 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.47 ○	0.61 △	0.70 △	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis after Composition			0.00 ○	0.00 ○	0.00 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.02 ○	0.00 ○	0.00 ○
				Min	-0.07 ○	-0.11 ○	-0.15 ○
	Neutral Axis before Composition			Max	-0.02 ○	-0.01 ○	-0.01 ○
				Min	-0.08 ○	-0.12 ○	-0.15 ○
	Neutral Axis after Composition			Max	-0.03 ○	-0.01 ○	0.00 ○
				Min	-0.08 ○	-0.13 ○	-0.16 ○
	Base of Lower Flange			Max	-0.02 ○	-0.01 ○	-0.01 ○
				Min	-0.08 ○	-0.11 ○	-0.13 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	32.70 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[2-13]	[2-14]	[2-15]				
Interval from beginning of Girder			-----	25.800	28.300	29.300				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.72	Δ	0.91	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	-0.10	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.22	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.19	○	-----	--	
	Base of Lower Flange			0.00	○	-0.06	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	-0.10	○	-----	--
				Min	-0.16	○	-0.24	○	-----	--
	Neutral Axis before Composition			Max	0.00	○	-0.19	○	-----	--
				Min	-0.16	○	-0.45	○	-----	--
	Neutral Axis after Composition			Max	0.00	○	-0.18	○	-----	--
				Min	-0.17	○	-0.41	○	-----	--
	Base of Lower Flange			Max	0.00	○	-0.04	○	-----	--
				Min	-0.14	○	-0.14	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	31.90	--	20.44	--	-----	--	
	D16	cm	-----	40.00	--	32.03	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	7.29	--	6.93	--	-----	--	
Compressive Strength to Failure (Suc/Shu)			1.00	1.91	○	3.62	○	-----	--	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1	○	1.16	○	-----	--	
	D16			1.079	○	1.16	○	-----	--	
	D19			1.253	○	1.224	○	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.72	Δ	0.91	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	-0.10	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.22	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.19	○	-----	--	
	Base of Lower Flange			0.00	○	-0.06	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	-0.10	○	-----	--
				Min	-0.16	○	-0.24	○	-----	--
	Neutral Axis before Composition			Max	0.00	○	-0.19	○	-----	--
				Min	-0.16	○	-0.45	○	-----	--
	Neutral Axis after Composition			Max	0.00	○	-0.18	○	-----	--
				Min	-0.17	○	-0.41	○	-----	--
	Base of Lower Flange			Max	0.00	○	-0.04	○	-----	--
				Min	-0.14	○	-0.14	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	31.90	--	20.44	--	-----	--	
	D16	cm	-----	40.00	--	32.03	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2- 1]	[2- 2]	[2- 3]		
Interval from beginning of Girder			-----	0.500	1.500	4.000		
Shear Force								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.95 Δ	0.64 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.11 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.22 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.20 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.06 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.27 ○	-0.14 ○	
				Min	-----	--	-0.12 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.38 ○	-0.12 ○
				Min	-----	--	-0.21 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.39 ○	-0.14 ○
				Min	-----	--	-0.20 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.08 ○	-0.09 ○
				Min	-----	--	-0.05 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 --	35.61 --	
	D16	cm	-----	-----	--	32.03 --	40.00 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	7.95 --	6.54 --	
Shear Force + Torsion								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.95 Δ	0.64 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.11 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.22 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.20 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.06 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.27 ○	-0.14 ○	
				Min	-----	--	-0.12 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.38 ○	-0.12 ○
				Min	-----	--	-0.21 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.39 ○	-0.14 ○
				Min	-----	--	-0.20 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.08 ○	-0.09 ○
				Min	-----	--	-0.05 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 --	35.61 --	
	D16	cm	-----	-----	--	32.03 --	40.00 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 --	0.00 --	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	-----	--	999.999 ○	999.999 ○	
Strength against Diagonal Densile Failure(Mus/Mtu)	D13	-----	1.00	-----	--	999.999 ○	999.999 ○	
	D16			-----	--	999.999 ○	999.999 ○	
	D19			-----	--	999.999 ○	999.999 ○	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2- 4]	[2- 5]	[2- 6]					
Interval from beginning of Girder			-----	4.100	7.700	11.300					
Shear Force											
Shear Stress	Design Load	N/mm ²	0.55	0.62	Δ	0.58	Δ	0.35	○		
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○		
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○		
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○		
	Base of Lower Flange			0.00	○	0.00	○	0.00	○		
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	○	-0.14	○	-0.11	○	-0.04	○
				Min	○	0.00	○	0.00	○	0.00	○
	Neutral Axis before Composition	Max		○	-0.12	○	-0.11	○	-0.05	○	
		Min		○	0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition	Max		○	-0.14	○	-0.12	○	-0.05	○	
		Min		○	0.00	○	0.00	○	0.00	○	
	Base of Lower Flange	Max		○	-0.09	○	-0.10	○	-0.05	○	
		Min		○	0.00	○	0.00	○	0.00	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	36.65	--	40.00	--	40.00	--		
	D16	cm	-----	40.00	--	40.00	--	40.00	--		
	D19	cm	-----	40.00	--	40.00	--	40.00	--		
Axial Reinforcement Bar Volume		cm ²	-----	6.35	--	4.14	--	0.07	--		
Shear Force + Torsion											
Shear Stress	Design Load	N/mm ²	0.55	0.62	Δ	0.58	Δ	0.35	○		
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○		
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○		
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○		
	Base of Lower Flange			0.00	○	0.00	○	0.00	○		
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	○	-0.14	○	-0.11	○	-0.04	○
				Min	○	0.00	○	0.00	○	0.00	○
	Neutral Axis before Composition	Max		○	-0.12	○	-0.11	○	-0.05	○	
		Min		○	0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition	Max		○	-0.14	○	-0.12	○	-0.05	○	
		Min		○	0.00	○	0.00	○	0.00	○	
	Base of Lower Flange	Max		○	-0.09	○	-0.10	○	-0.05	○	
		Min		○	0.00	○	0.00	○	0.00	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	36.65	--	40.00	--	40.00	--		
	D16	cm	-----	40.00	--	40.00	--	40.00	--		
	D19	cm	-----	40.00	--	40.00	--	40.00	--		
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--		
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○		
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	-		
	D16	-----		999.999	○	999.999	○	-----	-		
	D19	-----		999.999	○	999.999	○	-----	-		

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2- 7]	[2- 8]	[2- 9]			
Interval from beginning of Girder			-----	13.869	14.900	15.931			
Shear Force									
Shear Stress	Design Load	N/mm ²	0.55	0.24	○	0.06	○	0.27	○
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○
	Neutral Axis before Composition			0.00	○	0.00	○	-0.01	○
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○
	Base of Lower Flange			0.00	○	0.00	○	0.00	○
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	○	0.00	○	0.00	○
				Min	○	0.00	○	-0.02	○
	Neutral Axis before Composition	Max		○	0.00	○	0.00	○	
		Min		○	0.00	○	-0.03	○	
	Neutral Axis after Composition	Max		○	0.00	○	0.00	○	
		Min		○	0.00	○	-0.03	○	
	Base of Lower Flange	Max		○	0.00	○	0.00	○	
		Min		○	0.00	○	-0.06	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--
	D16	cm	-----	40.00	--	40.00	--	40.00	--
	D19	cm	-----	40.00	--	40.00	--	40.00	--
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--
Shear Force + Torsion									
Shear Stress	Design Load	N/mm ²	0.55	0.24	○	0.06	○	0.27	○
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○
	Neutral Axis before Composition			0.00	○	0.00	○	-0.01	○
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○
	Base of Lower Flange			0.00	○	0.00	○	0.00	○
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	○	0.00	○	0.00	○
				Min	○	0.00	○	-0.02	○
	Neutral Axis before Composition	Max		○	0.00	○	0.00	○	
		Min		○	0.00	○	-0.03	○	
	Neutral Axis after Composition	Max		○	0.00	○	0.00	○	
		Min		○	0.00	○	-0.03	○	
	Base of Lower Flange	Max		○	0.00	○	0.00	○	
		Min		○	0.00	○	-0.06	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--
	D16	cm	-----	40.00	--	40.00	--	40.00	--
	D19	cm	-----	40.00	--	40.00	--	40.00	--
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	-----	-	-----	-
	D16	-----	1.00	-----	-	-----	-	-----	-
	D19	-----	1.00	-----	-	-----	-	-----	-

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2-10]	[2-11]	[2-12]				
Interval from beginning of Girder			-----	18.500	22.100	25.700				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.39	○	0.60	△	0.65	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	0.00	○	0.00	○
				Min	-0.05	○	-0.12	○	-0.15	○
	Neutral Axis before Composition			Max	0.00	○	0.00	○	0.00	○
				Min	-0.06	○	-0.12	○	-0.13	○
	Neutral Axis after Composition			Max	0.00	○	0.00	○	0.00	○
				Min	-0.06	○	-0.13	○	-0.15	○
	Base of Lower Flange			Max	0.00	○	0.00	○	0.00	○
				Min	-0.06	○	-0.10	○	-0.09	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	39.01	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	3.82	--	5.97	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.39	○	0.60	△	0.65	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	0.00	○	0.00	○
				Min	-0.05	○	-0.12	○	-0.15	○
	Neutral Axis before Composition			Max	0.00	○	0.00	○	0.00	○
				Min	-0.06	○	-0.12	○	-0.13	○
	Neutral Axis after Composition			Max	0.00	○	0.00	○	0.00	○
				Min	-0.06	○	-0.13	○	-0.15	○
	Base of Lower Flange			Max	0.00	○	0.00	○	0.00	○
				Min	-0.06	○	-0.10	○	-0.09	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	39.01	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	999.999	○	999.999	○	
	D16			-----	-	999.999	○	999.999	○	
	D19			-----	-	999.999	○	999.999	○	

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2-13]	[2-14]	[2-15]				
Interval from beginning of Girder			-----	25.800	28.300	29.300				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.66	Δ	0.96	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	-0.11	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.22	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.21	○	-----	--	
	Base of Lower Flange			0.00	○	-0.06	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	-0.12	○	-----	--
				Min	-0.15	○	-0.28	○	-----	--
	Neutral Axis before Composition			Max	0.00	○	-0.22	○	-----	--
				Min	-0.13	○	-0.39	○	-----	--
	Neutral Axis after Composition			Max	0.00	○	-0.21	○	-----	--
				Min	-0.15	○	-0.40	○	-----	--
	Base of Lower Flange			Max	0.00	○	-0.05	○	-----	--
				Min	-0.10	○	-0.08	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	37.83	--	20.44	--	-----	--	
	D16	cm	-----	40.00	--	32.03	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	6.15	--	7.58	--	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.66	Δ	0.96	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	-0.11	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.22	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.21	○	-----	--	
	Base of Lower Flange			0.00	○	-0.06	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	-0.12	○	-----	--
				Min	-0.15	○	-0.28	○	-----	--
	Neutral Axis before Composition			Max	0.00	○	-0.22	○	-----	--
				Min	-0.13	○	-0.39	○	-----	--
	Neutral Axis after Composition			Max	0.00	○	-0.21	○	-----	--
				Min	-0.15	○	-0.40	○	-----	--
	Base of Lower Flange			Max	0.00	○	-0.05	○	-----	--
				Min	-0.10	○	-0.08	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	37.83	--	20.44	--	-----	--	
	D16	cm	-----	40.00	--	32.03	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	-----	--	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	--	
	D16			999.999	○	999.999	○	-----	--	
	D19			999.999	○	999.999	○	-----	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[3- 1]		[3- 2]		[3- 3]	
Interval from beginning of Girder		-----	0.500		1.500		4.000	
Immediately After Prestressing	Top of Main Girder	-1.5	3.428	○	4.234	○	6.238	
	Bottom of Main Girder	~19.00	3.711	○	3.471	○	7.001	
During Deck Construction	Top of Main Girder	-1.5	3.261	○	4.580	○	7.960	
	Bottom of Main Girder	~14.00	3.518	○	2.642	○	4.099	
Dead Load	Top of Deck	≤10.00	0.565	○	1.022	○	1.893	
	Top of Main Girder	0	2.546	○	3.507	○	5.713	
	Bottom of Main Girder	~14.00	3.355	○	2.410	○	2.878	
Design Load1	Top of Deck	Max	0.822	○	1.306	○	2.322	
		Min	≤10.00	-0.694	○	-0.022	○	1.249
	Top of Main Girder	Max	-1.5	2.773	○	3.756	○	6.074
		Min	~14.00	1.435	○	2.591	○	5.170
	Bottom of Main Girder	Max	~14.00	2.905	○	1.893	○	1.908
		Min	~14.00	5.562	○	4.311	○	4.334
Design Load2 Temperature Rise	Top of Deck	Max	≤11.50	1.706	○	2.185	○	3.140
		Min	≤11.50	0.191	○	0.857	○	2.068
	Top of Main Girder	Max	-2	2.236	○	3.210	○	5.444
		Min	~16.10	0.897	○	2.044	○	4.539
	Bottom of Main Girder	Max	~16.10	2.763	○	1.707	○	1.431
		Min	~16.10	5.420	○	4.125	○	3.858
Design Load3 Temperature Drop	Top of Deck	Max	≤11.50	1.706	○	2.185	○	3.140
		Min	≤11.50	0.191	○	0.857	○	2.068
	Top of Main Girder	Max	-2	2.236	○	3.210	○	5.444
		Min	~16.10	0.897	○	2.044	○	4.539
	Bottom of Main Girder	Max	~16.10	2.763	○	1.707	○	1.431
		Min	~16.10	5.420	○	4.125	○	3.858
Design Load4 Support sinking	Top of Deck	Max	≤10.00	0.822	○	1.306	○	2.322
		Min	≤10.00	-0.694	○	-0.022	○	1.249
	Top of Main Girder	Max	-1.5	2.773	○	3.756	○	6.074
		Min	~14.00	1.435	○	2.591	○	5.170
	Bottom of Main Girder	Max	~14.00	2.905	○	1.893	○	1.908
		Min	~14.00	5.562	○	4.311	○	4.334
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	≤11.50	1.706	○	2.185	○	3.140
		Min	≤11.50	0.191	○	0.857	○	2.068
	Top of Main Girder	Max	-2	2.236	○	3.210	○	5.444
		Min	~16.10	0.897	○	2.044	○	4.539
	Bottom of Main Girder	Max	~16.10	2.763	○	1.707	○	1.431
		Min	~16.10	5.420	○	4.125	○	3.858
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	≤11.50	1.706	○	2.185	○	3.140
		Min	≤11.50	0.191	○	0.857	○	2.068
	Top of Main Girder	Max	-2	2.236	○	3.210	○	5.444
		Min	~16.10	0.897	○	2.044	○	4.539
	Bottom of Main Girder	Max	~16.10	2.763	○	1.707	○	1.431
		Min	~16.10	5.420	○	4.125	○	3.858

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[3- 4]		[3- 5]		[3- 6]		
Interval from beginning of Girder		-----	4.100		7.700		11.300		
Immediately After Prestressing	Top of Main Girder	-1.5	6.141	○	3.100	○	1.101	○	
	Bottom of Main Girder	~19.00	7.121	○	10.971	○	13.167	○	
During Deck Construction	Top of Main Girder	-1.5	7.921	○	6.635	○	5.773	○	
	Bottom of Main Girder	~14.00	4.150	○	5.866	○	6.648	○	
Dead Load	Top of Deck	≤10.00	1.902	○	2.183	○	2.385	○	
	Top of Main Girder	0	5.700	○	5.208	○	4.846	○	
	Bottom of Main Girder	~14.00	2.890	○	3.376	○	3.360	○	
Design Load1	Top of Deck	Max	2.340	○	3.016	○	3.465	○	
		Min	1.271	○	1.724	○	2.011	○	
	Top of Main Girder	Max	6.068	○	5.911	○	5.759	○	
		Min	-1.5	5.167	○	4.820	○	4.529	○
	Bottom of Main Girder	Max	~14.00	1.902	○	1.511	○	0.957	○
		Min		4.319	○	4.405	○	4.193	○
Design Load2 Temperature Rise	Top of Deck	Max	3.158	○	3.851	○	4.315	○	
		Min	≤11.50	2.090	○	2.559	○	2.862	○
	Top of Main Girder	Max	5.438	○	5.295	○	5.157	○	
		Min	-2	4.536	○	4.204	○	3.927	○
	Bottom of Main Girder	Max	~16.10	1.425	○	1.005	○	0.422	○
		Min		3.841	○	3.899	○	3.657	○
Design Load3 Temperature Drop	Top of Deck	Max	3.158	○	3.851	○	4.315	○	
		Min	≤11.50	2.090	○	2.559	○	2.862	○
	Top of Main Girder	Max	5.438	○	5.295	○	5.157	○	
		Min	-2	4.536	○	4.204	○	3.927	○
	Bottom of Main Girder	Max	~16.10	1.425	○	1.005	○	0.422	○
		Min		3.841	○	3.899	○	3.657	○
Design Load4 Support sinking	Top of Deck	Max	2.340	○	3.016	○	3.465	○	
		Min	≤10.00	1.271	○	1.724	○	2.011	○
	Top of Main Girder	Max	6.068	○	5.911	○	5.759	○	
		Min	-1.5	5.167	○	4.820	○	4.529	○
	Bottom of Main Girder	Max	~14.00	1.902	○	1.511	○	0.957	○
		Min		4.319	○	4.405	○	4.193	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	3.158	○	3.851	○	4.315	○	
		Min	≤11.50	2.090	○	2.559	○	2.862	○
	Top of Main Girder	Max	5.438	○	5.295	○	5.157	○	
		Min	-2	4.536	○	4.204	○	3.927	○
	Bottom of Main Girder	Max	~16.10	1.425	○	1.005	○	0.422	○
		Min		3.841	○	3.899	○	3.657	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	3.158	○	3.851	○	4.315	○	
		Min	≤11.50	2.090	○	2.559	○	2.862	○
	Top of Main Girder	Max	5.438	○	5.295	○	5.157	○	
		Min	-2	4.536	○	4.204	○	3.927	○
	Bottom of Main Girder	Max	~16.10	1.425	○	1.005	○	0.422	○
		Min		3.841	○	3.899	○	3.657	○

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[3- 7]		[3- 8]		[3- 9]		
Interval from beginning of Girder		-----	13.869		14.900		15.931		
Immediately After Prestressing	Top of Main Girder	-1.5	0.790	○	0.833	○	0.789	○	
	Bottom of Main Girder	~19.00	13.198	○	13.089	○	13.199	○	
During Deck Construction	Top of Main Girder	-1.5	5.849	○	5.926	○	5.847	○	
	Bottom of Main Girder	~14.00	6.241	○	6.102	○	6.244	○	
Dead Load	Top of Deck	≤10.00	2.563	○	2.598	○	2.562	○	
	Top of Main Girder	0	4.957	○	5.012	○	4.957	○	
	Bottom of Main Girder	~14.00	2.766	○	2.624	○	2.763	○	
Design Load1	Top of Deck	Max	3.700	○	3.737	○	3.696	○	
		Min	2.218	○	2.249	○	2.197	○	
	Top of Main Girder	Max	5.919	○	5.976	○	5.917	○	
		Min	-1.5	4.665	○	4.717	○	4.648	○
	Bottom of Main Girder	Max	~14.00	0.239	○	0.092	○	0.241	○
		Min		3.535	○	3.399	○	3.573	○
Design Load2 Temperature Rise	Top of Deck	Max	4.563	○	4.605	○	4.570	○	
		Min	≤11.50	3.081	○	3.117	○	3.071	○
	Top of Main Girder	Max	5.328	○	5.389	○	5.334	○	
		Min	-2	4.073	○	4.130	○	4.065	○
	Bottom of Main Girder	Max	~16.10	-0.322	○	-0.481	○	-0.344	○
		Min		2.973	○	2.826	○	2.988	○
Design Load3 Temperature Drop	Top of Deck	Max	4.563	○	4.605	○	4.570	○	
		Min	≤11.50	3.081	○	3.117	○	3.071	○
	Top of Main Girder	Max	5.328	○	5.389	○	5.334	○	
		Min	-2	4.073	○	4.130	○	4.065	○
	Bottom of Main Girder	Max	~16.10	-0.322	○	-0.481	○	-0.344	○
		Min		2.973	○	2.826	○	2.988	○
Design Load4 Support sinking	Top of Deck	Max	3.700	○	3.737	○	3.696	○	
		Min	≤10.00	2.218	○	2.249	○	2.197	○
	Top of Main Girder	Max	5.919	○	5.976	○	5.917	○	
		Min	-1.5	4.665	○	4.717	○	4.648	○
	Bottom of Main Girder	Max	~14.00	0.239	○	0.092	○	0.241	○
		Min		3.535	○	3.399	○	3.573	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	4.563	○	4.605	○	4.570	○	
		Min	≤11.50	3.081	○	3.117	○	3.071	○
	Top of Main Girder	Max	5.328	○	5.389	○	5.334	○	
		Min	-2	4.073	○	4.130	○	4.065	○
	Bottom of Main Girder	Max	~16.10	-0.322	○	-0.481	○	-0.344	○
		Min		2.973	○	2.826	○	2.988	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	4.563	○	4.605	○	4.570	○	
		Min	≤11.50	3.081	○	3.117	○	3.071	○
	Top of Main Girder	Max	5.328	○	5.389	○	5.334	○	
		Min	-2	4.073	○	4.130	○	4.065	○
	Bottom of Main Girder	Max	~16.10	-0.322	○	-0.481	○	-0.344	○
		Min		2.973	○	2.826	○	2.988	○

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[3-10]		[3-11]		[3-12]		
Interval from beginning of Girder		-----	18.500		22.100		25.700		
Immediately After Prestressing	Top of Main Girder	-1.5	1.096	○	3.091	○	6.127	○	
	Bottom of Main Girder	~19.00	13.173	○	10.982	○	7.137	○	
During Deck Construction	Top of Main Girder	-1.5	5.764	○	6.616	○	7.892	○	
	Bottom of Main Girder	~14.00	6.659	○	5.888	○	4.184	○	
Dead Load	Top of Deck	≤10.00	2.378	○	2.170	○	1.882	○	
	Top of Main Girder	0	4.841	○	5.190	○	5.660	○	
	Bottom of Main Girder	~14.00	3.350	○	3.375	○	2.926	○	
Design Load1	Top of Deck	Max	3.450	○	2.984	○	2.258	○	
		Min	1.941	○	1.615	○	1.139	○	
	Top of Main Girder	Max	5.748	○	5.877	○	5.978	○	
		Min	-1.5	4.472	○	4.721	○	5.033	○
	Bottom of Main Girder	Max	~14.00	0.965	○	1.552	○	2.075	○
		Min		4.323	○	4.617	○	4.607	○
Design Load2 Temperature Rise	Top of Deck	Max	4.337	○	3.893	○	3.190	○	
		Min	≤11.50	2.829	○	2.525	○	2.070	○
	Top of Main Girder	Max	5.177	○	5.324	○	5.442	○	
		Min	-2	3.901	○	4.168	○	4.498	○
	Bottom of Main Girder	Max	~16.10	0.348	○	0.880	○	1.343	○
		Min		3.705	○	3.945	○	3.875	○
Design Load3 Temperature Drop	Top of Deck	Max	4.337	○	3.893	○	3.190	○	
		Min	≤11.50	2.829	○	2.525	○	2.070	○
	Top of Main Girder	Max	5.177	○	5.324	○	5.442	○	
		Min	-2	3.901	○	4.168	○	4.498	○
	Bottom of Main Girder	Max	~16.10	0.348	○	0.880	○	1.343	○
		Min		3.705	○	3.945	○	3.875	○
Design Load4 Support sinking	Top of Deck	Max	3.450	○	2.984	○	2.258	○	
		Min	≤10.00	1.941	○	1.615	○	1.139	○
	Top of Main Girder	Max	5.748	○	5.877	○	5.978	○	
		Min	-1.5	4.472	○	4.721	○	5.033	○
	Bottom of Main Girder	Max	~14.00	0.965	○	1.552	○	2.075	○
		Min		4.323	○	4.617	○	4.607	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	4.337	○	3.893	○	3.190	○	
		Min	≤11.50	2.829	○	2.525	○	2.070	○
	Top of Main Girder	Max	5.177	○	5.324	○	5.442	○	
		Min	-2	3.901	○	4.168	○	4.498	○
	Bottom of Main Girder	Max	~16.10	0.348	○	0.880	○	1.343	○
		Min		3.705	○	3.945	○	3.875	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	4.337	○	3.893	○	3.190	○	
		Min	≤11.50	2.829	○	2.525	○	2.070	○
	Top of Main Girder	Max	5.177	○	5.324	○	5.442	○	
		Min	-2	3.901	○	4.168	○	4.498	○
	Bottom of Main Girder	Max	~16.10	0.348	○	0.880	○	1.343	○
		Min		3.705	○	3.945	○	3.875	○

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 3

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[3-13]		[3-14]		[3-15]		
Interval from beginning of Girder		-----	25.800		28.300		29.300		
Immediately After Prestressing	Top of Main Girder	-1.5	6.224	○	4.219	○	3.413	○	
	Bottom of Main Girder	~19.00	7.018	○	3.488	○	3.729	○	
During Deck Construction	Top of Main Girder	-1.5	7.931	○	4.549	○	3.229	○	
	Bottom of Main Girder	~14.00	4.132	○	2.677	○	3.554	○	
Dead Load	Top of Deck	≤10.00	1.872	○	0.997	○	0.538	○	
	Top of Main Girder	0	5.673	○	3.467	○	2.505	○	
	Bottom of Main Girder	~14.00	2.916	○	2.464	○	3.411	○	
Design Load1	Top of Deck	Max	2.239	○	1.183	○	0.681	○	
		Min	1.117	○	-0.150	○	-0.817	○	
	Top of Main Girder	Max	5.982	○	3.630	○	2.632	○	
		Min	-1.5	5.036	○	2.460	○	1.308	○
	Bottom of Main Girder	Max	~14.00	2.085	○	2.126	○	3.160	○
		Min		4.624	○	4.554	○	5.787	○
Design Load2 Temperature Rise	Top of Deck	Max	3.171	○	2.198	○	1.711	○	
		Min	≤11.50	2.049	○	0.865	○	0.212	○
	Top of Main Girder	Max	5.447	○	3.204	○	2.222	○	
		Min	-2	4.501	○	2.034	○	0.899	○
	Bottom of Main Girder	Max	~16.10	1.352	○	1.691	○	2.764	○
		Min		3.891	○	4.119	○	5.391	○
Design Load3 Temperature Drop	Top of Deck	Max	3.171	○	2.198	○	1.711	○	
		Min	≤11.50	2.049	○	0.865	○	0.212	○
	Top of Main Girder	Max	5.447	○	3.204	○	2.222	○	
		Min	-2	4.501	○	2.034	○	0.899	○
	Bottom of Main Girder	Max	~16.10	1.352	○	1.691	○	2.764	○
		Min		3.891	○	4.119	○	5.391	○
Design Load4 Support sinking	Top of Deck	Max	2.239	○	1.183	○	0.681	○	
		Min	≤10.00	1.117	○	-0.150	○	-0.817	○
	Top of Main Girder	Max	5.982	○	3.630	○	2.632	○	
		Min	-1.5	5.036	○	2.460	○	1.308	○
	Bottom of Main Girder	Max	~14.00	2.085	○	2.126	○	3.160	○
		Min		4.624	○	4.554	○	5.787	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	3.171	○	2.198	○	1.711	○	
		Min	≤11.50	2.049	○	0.865	○	0.212	○
	Top of Main Girder	Max	5.447	○	3.204	○	2.222	○	
		Min	-2	4.501	○	2.034	○	0.899	○
	Bottom of Main Girder	Max	~16.10	1.352	○	1.691	○	2.764	○
		Min		3.891	○	4.119	○	5.391	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	3.171	○	2.198	○	1.711	○	
		Min	≤11.50	2.049	○	0.865	○	0.212	○
	Top of Main Girder	Max	5.447	○	3.204	○	2.222	○	
		Min	-2	4.501	○	2.034	○	0.899	○
	Bottom of Main Girder	Max	~16.10	1.352	○	1.691	○	2.764	○
		Min		3.891	○	4.119	○	5.391	○

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 3

Cross Section NumberNo.	Unit	Allowable Value	[3- 1]		[3- 2]		[3- 3]	
Interval from beginning of Girder								
				0.500		1.500		4.000
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1099	○	1103	○	1156	○
Effective Prestressing Force (*1)	N/mm ²	1110	1044	○	1046	○	1083	○
Effective Prestressing Force (*2)	N/mm ²	1110	974	○	974	○	991	○
max	N/mm ²	1110	974	○	974	○	995	○
Ultimate Load	-----	1.00	2.28	○	4.02	○	2.15	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[3- 4]		[3- 5]		[3- 6]	
Interval from beginning of Girder								
				4.100		7.700		11.300
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1157	○	1174	○	1154	○
Effective Prestressing Force (*1)	N/mm ²	1110	1083	○	1089	○	1058	○
Effective Prestressing Force (*2)	N/mm ²	1110	992	○	1000	○	972	○
max	N/mm ²	1110	996	○	1024	○	1014	○
Ultimate Load	-----	1.00	2.12	○	1.54	○	1.38	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[3- 7]		[3- 8]		[3- 9]	
Interval from beginning of Girder								
				13.869		14.900		15.931
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1126	○	1121	○	1126	○
Effective Prestressing Force (*1)	N/mm ²	1110	1029	○	1025	○	1029	○
Effective Prestressing Force (*2)	N/mm ²	1110	948	○	946	○	948	○
max	N/mm ²	1110	997	○	994	○	996	○
Ultimate Load	-----	1.00	1.32	○	1.31	○	1.33	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[3-10]	[3-11]	[3-12]
Interval from beginning of Girder			18.500	22.100	25.700
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	1320	1320
Immediately After Prestressing	N/mm ²	1295	1154	1174	1157
Effective Prestressing Force (*1)	N/mm ²	1110	1058	1089	1083
Effective Prestressing Force (*2)	N/mm ²	1110	970	997	989
max	N/mm ²	1110	1010	1019	991
Ultimate Load	-----	1.00	1.39	1.58	2.32

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[3-13]	[3-14]	[3-15]
Interval from beginning of Girder			25.800	28.300	29.300
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	1320	1320
Immediately After Prestressing	N/mm ²	1295	1156	1103	1099
Effective Prestressing Force (*1)	N/mm ²	1110	1083	1046	1044
Effective Prestressing Force (*2)	N/mm ²	1110	988	973	973
max	N/mm ²	1110	990	971	971
Ultimate Load	-----	1.00	2.36	3.32	2.03

*1:During DeckConstruction *2:Design Load

3rd Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[3- 1]	[3- 2]	[3- 3]		
Interval from beginning of Girder			-----	0.500	1.500	4.000		
Shear Force								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.92 Δ	0.75 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.10 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.23 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.20 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.07 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.25 ○	-0.17 ○	
				Min	-----	--	-0.11 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.46 ○	-0.18 ○
				Min	-----	--	-0.19 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.42 ○	-0.18 ○
				Min	-----	--	-0.18 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.14 ○	-0.15 ○
				Min	-----	--	-0.04 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 --	30.70 --	
	D16	cm	-----	-----	--	32.03 --	40.00 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	-----	--	7.22 --	7.58 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	-----	--	3.58 ○	1.89 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	--	1.148 ○	1.00 ○	
	D16			-----	--	1.148 ○	1.07 ○	
	D19			-----	--	1.211 ○	1.24 ○	
Shear Force + Torsion								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.92 Δ	0.75 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.10 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.23 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.20 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.07 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.25 ○	-0.17 ○	
				Min	-----	--	-0.11 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.46 ○	-0.18 ○
				Min	-----	--	-0.19 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.42 ○	-0.18 ○
				Min	-----	--	-0.18 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.14 ○	-0.15 ○
				Min	-----	--	-0.04 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 --	30.70 --	
	D16	cm	-----	-----	--	32.03 --	40.00 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	-----	--	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[3- 4]	[3- 5]	[3- 6]	
Interval from beginning of Girder			-----	4.100	7.700	11.300	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.73 Δ	0.65 Δ	0.51 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis after Composition			0.00 ○	0.00 ○	0.00 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.17 ○	-0.13 ○	-0.08 ○
				Min	0.00 ○	0.00 ○	-0.02 ○
	Neutral Axis before Composition			Max	-0.17 ○	-0.14 ○	-0.09 ○
				Min	0.00 ○	0.00 ○	-0.02 ○
	Neutral Axis after Composition			Max	-0.18 ○	-0.14 ○	-0.09 ○
				Min	0.00 ○	0.00 ○	-0.02 ○
	Base of Lower Flange			Max	-0.14 ○	-0.13 ○	-0.09 ○
				Min	0.00 ○	0.00 ○	-0.01 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	31.44 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	7.40 --	4.86 --	1.83 --		
Compressive Strength to Failure (Suc/Shu)		-----	1.00	1.91 ○	2.40 ○	3.35 ○	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.00 ○	1.056 ○	----- --	
	D16			1.07 ○	1.248 ○	----- --	
	D19			1.25 ○	1.483 ○	----- --	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.73 Δ	0.65 Δ	0.51 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis after Composition			0.00 ○	0.00 ○	0.00 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.17 ○	-0.13 ○	-0.08 ○
				Min	0.00 ○	0.00 ○	-0.02 ○
	Neutral Axis before Composition			Max	-0.17 ○	-0.14 ○	-0.09 ○
				Min	0.00 ○	0.00 ○	-0.02 ○
	Neutral Axis after Composition			Max	-0.18 ○	-0.14 ○	-0.09 ○
				Min	0.00 ○	0.00 ○	-0.02 ○
	Base of Lower Flange			Max	-0.14 ○	-0.13 ○	-0.09 ○
				Min	0.00 ○	0.00 ○	-0.01 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	31.44 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[3- 7]	[3- 8]	[3- 9]	
Interval from beginning of Girder			-----	13.869	14.900	15.931	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.59 Δ	0.44 ○	0.58 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.01 ○	0.00 ○	-0.01 ○	
	Neutral Axis before Composition			-0.02 ○	0.00 ○	-0.02 ○	
	Neutral Axis after Composition			-0.02 ○	0.00 ○	-0.02 ○	
	Base of Lower Flange			-0.02 ○	0.00 ○	-0.02 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.10 ○	-0.06 ○	-0.02 ○
				Min	-0.01 ○	-0.04 ○	-0.10 ○
	Neutral Axis before Composition			Max	-0.13 ○	-0.08 ○	-0.01 ○
				Min	-0.01 ○	-0.04 ○	-0.11 ○
	Neutral Axis after Composition			Max	-0.12 ○	-0.07 ○	-0.02 ○
				Min	-0.01 ○	-0.04 ○	-0.11 ○
	Base of Lower Flange			Max	-0.13 ○	-0.09 ○	-0.01 ○
				Min	-0.01 ○	-0.03 ○	-0.08 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.85 --	0.00 --	0.67 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	4.60 ○	5.03 ○	4.42 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.64 ○	----- --	1.64 ○	
	D16			2.066 ○	----- --	2.05 ○	
	D19			2.586 ○	----- --	2.55 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.59 Δ	0.44 ○	0.58 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.01 ○	0.00 ○	-0.01 ○	
	Neutral Axis before Composition			-0.02 ○	0.00 ○	-0.02 ○	
	Neutral Axis after Composition			-0.02 ○	0.00 ○	-0.02 ○	
	Base of Lower Flange			-0.02 ○	0.00 ○	-0.02 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.10 ○	-0.06 ○	-0.02 ○
				Min	-0.01 ○	-0.04 ○	-0.10 ○
	Neutral Axis before Composition			Max	-0.13 ○	-0.08 ○	-0.01 ○
				Min	-0.01 ○	-0.04 ○	-0.11 ○
	Neutral Axis after Composition			Max	-0.12 ○	-0.07 ○	-0.02 ○
				Min	-0.01 ○	-0.04 ○	-0.11 ○
	Base of Lower Flange			Max	-0.13 ○	-0.09 ○	-0.01 ○
				Min	-0.01 ○	-0.03 ○	-0.08 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[3-10]	[3-11]	[3-12]	
Interval from beginning of Girder			-----	18.500	22.100	25.700	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.49 ○	0.63 △	0.71 △	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis after Composition			0.00 ○	0.00 ○	0.00 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.02 ○	0.00 ○	0.00 ○
				Min	-0.08 ○	-0.13 ○	-0.17 ○
	Neutral Axis before Composition			Max	-0.03 ○	-0.01 ○	0.00 ○
				Min	-0.07 ○	-0.11 ○	-0.14 ○
	Neutral Axis after Composition			Max	-0.02 ○	0.00 ○	0.00 ○
				Min	-0.09 ○	-0.13 ○	-0.17 ○
	Base of Lower Flange			Max	-0.03 ○	-0.01 ○	-0.01 ○
				Min	-0.05 ○	-0.07 ○	-0.09 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	31.20 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	1.53 --	4.49 --	7.46 --		
Compressive Strength to Failure (Suc/Shu)		-----	1.00	3.26 ○	2.37 ○	1.89 ○	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	1.076 ○	1.00 ○	
	D16			-----	1.266 ○	1.07 ○	
	D19			-----	1.497 ○	1.24 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.49 ○	0.63 △	0.71 △	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis after Composition			0.00 ○	0.00 ○	0.00 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.02 ○	0.00 ○	0.00 ○
				Min	-0.08 ○	-0.13 ○	-0.17 ○
	Neutral Axis before Composition			Max	-0.03 ○	-0.01 ○	0.00 ○
				Min	-0.07 ○	-0.11 ○	-0.14 ○
	Neutral Axis after Composition			Max	-0.02 ○	0.00 ○	0.00 ○
				Min	-0.09 ○	-0.13 ○	-0.17 ○
	Base of Lower Flange			Max	-0.03 ○	-0.01 ○	-0.01 ○
				Min	-0.05 ○	-0.07 ○	-0.09 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	31.20 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[3-13]	[3-14]	[3-15]				
Interval from beginning of Girder			-----	25.800	28.300	29.300				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.73	Δ	1.00	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	-0.10	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.23	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.20	○	-----	--	
	Base of Lower Flange			0.00	○	-0.07	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	-0.09	○	-----	--
				Min	-0.18	○	-0.30	○	-----	--
	Neutral Axis before Composition			Max	0.00	○	-0.21	○	-----	--
				Min	-0.15	○	-0.40	○	-----	--
	Neutral Axis after Composition			Max	0.00	○	-0.18	○	-----	--
				Min	-0.17	○	-0.42	○	-----	--
	Base of Lower Flange			Max	0.00	○	-0.07	○	-----	--
				Min	-0.09	○	-0.08	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	30.42	--	20.44	--	-----	--	
	D16	cm	-----	40.00	--	32.03	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume	cm ²	-----	7.65	--	9.29	--	-----	--		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	1.87	○	3.25	○	-----	--		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1	○	1.041	○	-----	--	
	D16			1.062	○	1.041	○	-----	--	
	D19			1.233	○	1.099	○	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.73	Δ	1.00	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	-0.10	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.23	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.20	○	-----	--	
	Base of Lower Flange			0.00	○	-0.07	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	-0.09	○	-----	--
				Min	-0.18	○	-0.30	○	-----	--
	Neutral Axis before Composition			Max	0.00	○	-0.21	○	-----	--
				Min	-0.15	○	-0.40	○	-----	--
	Neutral Axis after Composition			Max	0.00	○	-0.18	○	-----	--
				Min	-0.17	○	-0.42	○	-----	--
	Base of Lower Flange			Max	0.00	○	-0.07	○	-----	--
				Min	-0.09	○	-0.08	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	30.42	--	20.44	--	-----	--	
	D16	cm	-----	40.00	--	32.03	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume	cm ²	-----	0.00	--	0.00	--	-----	--		

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[3- 1]	[3- 2]	[3- 3]		
Interval from beginning of Girder			-----	0.500	1.500	4.000		
Shear Force								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.96 Δ	0.66 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.11 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.23 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.21 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.06 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.28 ○	-0.15 ○	
				Min	-----	--	-0.12 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.39 ○	-0.13 ○
				Min	-----	--	-0.22 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.40 ○	-0.15 ○
				Min	-----	--	-0.21 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.08 ○	-0.10 ○
				Min	-----	--	-0.05 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 --	37.98 --	
	D16	cm	-----	-----	--	32.03 --	40.00 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	7.58 --	6.13 --	
Shear Force + Torsion								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.96 Δ	0.66 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.11 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.23 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.21 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.06 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.28 ○	-0.15 ○	
				Min	-----	--	-0.12 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.39 ○	-0.13 ○
				Min	-----	--	-0.22 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.40 ○	-0.15 ○
				Min	-----	--	-0.21 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.08 ○	-0.10 ○
				Min	-----	--	-0.05 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 --	37.98 --	
	D16	cm	-----	-----	--	32.03 --	40.00 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 --	0.00 --	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	-----	--	999.999 ○	999.999 ○	
Strength against Diagonal Densile Failure(Mus/Mtu)	D13	-----	1.00	-----	--	999.999 ○	999.999 ○	
	D16			-----	--	999.999 ○	999.999 ○	
	D19			-----	--	999.999 ○	999.999 ○	

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[3- 4]	[3- 5]	[3- 6]				
Interval from beginning of Girder			-----	4.100	7.700	11.300				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.64	Δ	0.60	Δ	0.39	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.15	○	-0.12	○	-0.05	○
				Min	0.00	○	0.00	○	0.00	○
	Neutral Axis before Composition	Max		-0.13	○	-0.12	○	-0.06	○	
		Min		0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition	Max		-0.14	○	-0.13	○	-0.06	○	
		Min		0.00	○	0.00	○	0.00	○	
	Base of Lower Flange	Max		-0.09	○	-0.10	○	-0.06	○	
		Min		0.00	○	0.00	○	0.00	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	39.18	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	5.94	--	3.80	--	0.00	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.64	Δ	0.60	Δ	0.39	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.15	○	-0.12	○	-0.05	○
				Min	0.00	○	0.00	○	0.00	○
	Neutral Axis before Composition	Max		-0.13	○	-0.12	○	-0.06	○	
		Min		0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition	Max		-0.14	○	-0.13	○	-0.06	○	
		Min		0.00	○	0.00	○	0.00	○	
	Base of Lower Flange	Max		-0.09	○	-0.10	○	-0.06	○	
		Min		0.00	○	0.00	○	0.00	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	39.18	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Densile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	-	
	D16			999.999	○	999.999	○	-----	-	
	D19			999.999	○	999.999	○	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[3- 7]	[3- 8]	[3- 9]				
Interval from beginning of Girder			-----	13.869	14.900	15.931				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.27	○	0.04	○	0.23	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			-0.01	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.02	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	-0.01	○
	Neutral Axis before Composition			Max	-0.03	○	0.00	○	0.00	○
				Min	-0.01	○	0.00	○	-0.03	○
	Neutral Axis after Composition			Max	-0.03	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	-0.02	○
	Base of Lower Flange			Max	-0.02	○	0.00	○	0.00	○
				Min	-0.01	○	0.00	○	-0.04	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.27	○	0.04	○	0.23	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			-0.01	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.02	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	-0.01	○
	Neutral Axis before Composition			Max	-0.03	○	0.00	○	0.00	○
				Min	-0.01	○	0.00	○	-0.03	○
	Neutral Axis after Composition			Max	-0.03	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	-0.02	○
	Base of Lower Flange			Max	-0.02	○	0.00	○	0.00	○
				Min	-0.01	○	0.00	○	-0.04	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	-----	-	-----	-	
	D16	-----	1.00	-----	-	-----	-	-----	-	
	D19	-----	1.00	-----	-	-----	-	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[3-10]	[3-11]	[3-12]				
Interval from beginning of Girder			-----	18.500	22.100	25.700				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.35	○	0.57	△	0.61	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	0.00	○	0.00	○
				Min	-0.04	○	-0.11	○	-0.13	○
	Neutral Axis before Composition			Max	0.00	○	0.00	○	0.00	○
				Min	-0.04	○	-0.11	○	-0.12	○
	Neutral Axis after Composition			Max	0.00	○	0.00	○	0.00	○
				Min	-0.05	○	-0.11	○	-0.13	○
	Base of Lower Flange			Max	0.00	○	0.00	○	0.00	○
				Min	-0.05	○	-0.09	○	-0.08	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	37.30	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.01	--	4.05	--	6.24	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.35	○	0.57	△	0.61	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	0.00	○	0.00	○
				Min	-0.04	○	-0.11	○	-0.13	○
	Neutral Axis before Composition			Max	0.00	○	0.00	○	0.00	○
				Min	-0.04	○	-0.11	○	-0.12	○
	Neutral Axis after Composition			Max	0.00	○	0.00	○	0.00	○
				Min	-0.05	○	-0.11	○	-0.13	○
	Base of Lower Flange			Max	0.00	○	0.00	○	0.00	○
				Min	-0.05	○	-0.09	○	-0.08	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	37.30	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	999.999	○	999.999	○	
	D16			-----	-	999.999	○	999.999	○	
	D19			-----	-	999.999	○	999.999	○	

<Design of Main Girder: Summary for Calculation Results of Stress>

3rd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[3-13]	[3-14]	[3-15]				
Interval from beginning of Girder			-----	25.800	28.300	29.300				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.63	Δ	0.95	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	-0.11	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.22	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.20	○	-----	--	
	Base of Lower Flange			0.00	○	-0.06	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	-0.11	○	-----	--
				Min	-0.14	○	-0.27	○	-----	--
	Neutral Axis before Composition			Max	0.00	○	-0.21	○	-----	--
				Min	-0.12	○	-0.38	○	-----	--
	Neutral Axis after Composition			Max	0.00	○	-0.20	○	-----	--
				Min	-0.14	○	-0.39	○	-----	--
	Base of Lower Flange			Max	0.00	○	-0.05	○	-----	--
				Min	-0.09	○	-0.08	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	36.21	--	20.44	--	-----	--	
	D16	cm	-----	40.00	--	32.03	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	6.43	--	7.86	--	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.63	Δ	0.95	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	-0.11	○	-----	--	
	Neutral Axis before Composition			0.00	○	-0.22	○	-----	--	
	Neutral Axis after Composition			0.00	○	-0.20	○	-----	--	
	Base of Lower Flange			0.00	○	-0.06	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	-0.11	○	-----	--
				Min	-0.14	○	-0.27	○	-----	--
	Neutral Axis before Composition			Max	0.00	○	-0.21	○	-----	--
				Min	-0.12	○	-0.38	○	-----	--
	Neutral Axis after Composition			Max	0.00	○	-0.20	○	-----	--
				Min	-0.14	○	-0.39	○	-----	--
	Base of Lower Flange			Max	0.00	○	-0.05	○	-----	--
				Min	-0.09	○	-0.08	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	36.21	--	20.44	--	-----	--	
	D16	cm	-----	40.00	--	32.03	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	-----	--	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	--	
	D16			999.999	○	999.999	○	-----	--	
	D19			999.999	○	999.999	○	-----	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

4th Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[4- 1]		[4- 2]		[4- 3]	
Interval from beginning of Girder		-----	0.500		1.500		4.000	
Immediately After Prestressing	Top of Main Girder	-1.5	3.410	○	4.216	○	6.220 ○	
	Bottom of Main Girder	~19.00	3.732	○	3.491	○	7.022 ○	
During Deck Construction	Top of Main Girder	-1.5	3.224	○	4.543	○	7.923 ○	
	Bottom of Main Girder	~14.00	3.561	○	2.684	○	4.141 ○	
Dead Load	Top of Deck	≤10.00	0.564	○	1.020	○	1.888 ○	
	Top of Main Girder	0	2.525	○	3.485	○	5.685 ○	
	Bottom of Main Girder	~14.00	3.368	○	2.425	○	2.887 ○	
Design Load1	Top of Deck	Max	0.674	○	1.180	○	2.250 ○	
		Min	≤10.00	-0.817	○	-0.128	○	1.183 ○
	Top of Main Girder	Max	-1.5	2.622	○	3.625	○	5.990 ○
		Min	~14.00	1.306	○	2.477	○	5.090 ○
	Bottom of Main Girder	Max	~14.00	3.175	○	2.134	○	2.069 ○
		Min	~14.00	5.790	○	4.517	○	4.482 ○
Design Load2 Temperature Rise	Top of Deck	Max	≤11.50	1.722	○	2.201	○	3.155 ○
		Min	~16.10	0.231	○	0.893	○	2.088 ○
	Top of Main Girder	Max	-2	2.230	○	3.204	○	5.432 ○
		Min	~16.10	0.913	○	2.056	○	4.533 ○
	Bottom of Main Girder	Max	~16.10	2.747	○	1.688	○	1.396 ○
		Min	~16.10	5.361	○	4.071	○	3.809 ○
Design Load3 Temperature Drop	Top of Deck	Max	≤11.50	1.722	○	2.201	○	3.155 ○
		Min	~16.10	0.231	○	0.893	○	2.088 ○
	Top of Main Girder	Max	-2	2.230	○	3.204	○	5.432 ○
		Min	~16.10	0.913	○	2.056	○	4.533 ○
	Bottom of Main Girder	Max	~16.10	2.747	○	1.688	○	1.396 ○
		Min	~16.10	5.361	○	4.071	○	3.809 ○
Design Load4 Support sinking	Top of Deck	Max	≤10.00	0.674	○	1.180	○	2.250 ○
		Min	~14.00	-0.817	○	-0.128	○	1.183 ○
	Top of Main Girder	Max	-1.5	2.622	○	3.625	○	5.990 ○
		Min	~14.00	1.306	○	2.477	○	5.090 ○
	Bottom of Main Girder	Max	~14.00	3.175	○	2.134	○	2.069 ○
		Min	~14.00	5.790	○	4.517	○	4.482 ○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	≤11.50	1.722	○	2.201	○	3.155 ○
		Min	~16.10	0.231	○	0.893	○	2.088 ○
	Top of Main Girder	Max	-2	2.230	○	3.204	○	5.432 ○
		Min	~16.10	0.913	○	2.056	○	4.533 ○
	Bottom of Main Girder	Max	~16.10	2.747	○	1.688	○	1.396 ○
		Min	~16.10	5.361	○	4.071	○	3.809 ○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	≤11.50	1.722	○	2.201	○	3.155 ○
		Min	~16.10	0.231	○	0.893	○	2.088 ○
	Top of Main Girder	Max	-2	2.230	○	3.204	○	5.432 ○
		Min	~16.10	0.913	○	2.056	○	4.533 ○
	Bottom of Main Girder	Max	~16.10	2.747	○	1.688	○	1.396 ○
		Min	~16.10	5.361	○	4.071	○	3.809 ○

<Design of Main Girder: Summary for Calculation Results of Stress>

4th Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[4- 4]		[4- 5]		[4- 6]		
Interval from beginning of Girder		-----	4.100		7.700		11.300		
Immediately After Prestressing	Top of Main Girder	-1.5	6.124	○	3.087	○	1.065	○	
	Bottom of Main Girder	~19.00	7.141	○	10.987	○	13.330	○	
During Deck Construction	Top of Main Girder	-1.5	7.885	○	6.608	○	5.731	○	
	Bottom of Main Girder	~14.00	4.193	○	5.897	○	6.806	○	
Dead Load	Top of Deck	≤10.00	1.897	○	2.174	○	2.365	○	
	Top of Main Girder	0	5.672	○	5.189	○	4.809	○	
	Bottom of Main Girder	~14.00	2.899	○	3.395	○	3.546	○	
Design Load1	Top of Deck	Max	2.269	○	3.021	○	3.565	○	
		Min	1.206	○	1.712	○	2.009	○	
	Top of Main Girder	Max	5.986	○	5.905	○	5.824	○	
		Min	-1.5	5.089	○	4.799	○	4.508	○
	Bottom of Main Girder	Max	~14.00	2.058	○	1.499	○	0.874	○
		Min		4.463	○	4.430	○	4.339	○
Design Load2 Temperature Rise	Top of Deck	Max	3.173	○	3.856	○	4.333	○	
		Min	≤11.50	2.109	○	2.548	○	2.776	○
	Top of Main Girder	Max	5.427	○	5.289	○	5.152	○	
		Min	-2	4.530	○	4.183	○	3.835	○
	Bottom of Main Girder	Max	~16.10	1.389	○	0.994	○	0.524	○
		Min		3.794	○	3.924	○	3.989	○
Design Load3 Temperature Drop	Top of Deck	Max	3.173	○	3.856	○	4.333	○	
		Min	≤11.50	2.109	○	2.548	○	2.776	○
	Top of Main Girder	Max	5.427	○	5.289	○	5.152	○	
		Min	-2	4.530	○	4.183	○	3.835	○
	Bottom of Main Girder	Max	~16.10	1.389	○	0.994	○	0.524	○
		Min		3.794	○	3.924	○	3.989	○
Design Load4 Support sinking	Top of Deck	Max	2.269	○	3.021	○	3.565	○	
		Min	≤10.00	1.206	○	1.712	○	2.009	○
	Top of Main Girder	Max	5.986	○	5.905	○	5.824	○	
		Min	-1.5	5.089	○	4.799	○	4.508	○
	Bottom of Main Girder	Max	~14.00	2.058	○	1.499	○	0.874	○
		Min		4.463	○	4.430	○	4.339	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	3.173	○	3.856	○	4.333	○	
		Min	≤11.50	2.109	○	2.548	○	2.776	○
	Top of Main Girder	Max	5.427	○	5.289	○	5.152	○	
		Min	-2	4.530	○	4.183	○	3.835	○
	Bottom of Main Girder	Max	~16.10	1.389	○	0.994	○	0.524	○
		Min		3.794	○	3.924	○	3.989	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	3.173	○	3.856	○	4.333	○	
		Min	≤11.50	2.109	○	2.548	○	2.776	○
	Top of Main Girder	Max	5.427	○	5.289	○	5.152	○	
		Min	-2	4.530	○	4.183	○	3.835	○
	Bottom of Main Girder	Max	~16.10	1.389	○	0.994	○	0.524	○
		Min		3.794	○	3.924	○	3.989	○

<Design of Main Girder: Summary for Calculation Results of Stress>

4th Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[4- 7]		[4- 8]		[4- 9]	
Interval from beginning of Girder		-----	13.869		14.900		15.851	
Immediately After Prestressing	Top of Main Girder	-1.5	0.643	○	0.654	○	0.616	
	Bottom of Main Girder	~19.00	13.894	○	13.942	○	14.043	
During Deck Construction	Top of Main Girder	-1.5	5.710	○	5.760	○	5.693	
	Bottom of Main Girder	~14.00	6.875	○	6.875	○	7.001	
Dead Load	Top of Deck	≤10.00	2.516	○	2.539	○	2.502	
	Top of Main Girder	0	4.860	○	4.895	○	4.840	
	Bottom of Main Girder	~14.00	3.394	○	3.391	○	3.541	
Design Load1	Top of Deck	Max	3.862	○	3.923	○	3.912	
		Min	2.215	○	2.259	○	2.242	
	Top of Main Girder	Max	5.999	○	6.066	○	6.033	
		Min	-1.5	4.605	○	4.658	○	4.620
	Bottom of Main Girder	Max	~14.00	0.402	○	0.316	○	0.408
		Min		4.064	○	4.015	○	4.120
Design Load2 Temperature Rise	Top of Deck	Max	4.583	○	4.625	○	4.596	
		Min	≤11.50	2.935	○	2.961	○	2.927
	Top of Main Girder	Max	5.287	○	5.338	○	5.290	
		Min	-2	3.893	○	3.930	○	3.877
	Bottom of Main Girder	Max	~16.10	0.157	○	0.112	○	0.243
		Min		3.819	○	3.811	○	3.955
Design Load3 Temperature Drop	Top of Deck	Max	4.583	○	4.625	○	4.596	
		Min	≤11.50	2.935	○	2.961	○	2.927
	Top of Main Girder	Max	5.287	○	5.338	○	5.290	
		Min	-2	3.893	○	3.930	○	3.877
	Bottom of Main Girder	Max	~16.10	0.157	○	0.112	○	0.243
		Min		3.819	○	3.811	○	3.955
Design Load4 Support sinking	Top of Deck	Max	3.862	○	3.923	○	3.912	
		Min	≤10.00	2.215	○	2.259	○	2.242
	Top of Main Girder	Max	5.999	○	6.066	○	6.033	
		Min	-1.5	4.605	○	4.658	○	4.620
	Bottom of Main Girder	Max	~14.00	0.402	○	0.316	○	0.408
		Min		4.064	○	4.015	○	4.120
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	4.583	○	4.625	○	4.596	
		Min	≤11.50	2.935	○	2.961	○	2.927
	Top of Main Girder	Max	5.287	○	5.338	○	5.290	
		Min	-2	3.893	○	3.930	○	3.877
	Bottom of Main Girder	Max	~16.10	0.157	○	0.112	○	0.243
		Min		3.819	○	3.811	○	3.955
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	4.583	○	4.625	○	4.596	
		Min	≤11.50	2.935	○	2.961	○	2.927
	Top of Main Girder	Max	5.287	○	5.338	○	5.290	
		Min	-2	3.893	○	3.930	○	3.877
	Bottom of Main Girder	Max	~16.10	0.157	○	0.112	○	0.243
		Min		3.819	○	3.811	○	3.955

4th Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[4-10]		[4-11]		[4-12]	
Interval from beginning of Girder		-----	18.500		22.100		25.700	
Immediately After Prestressing	Top of Main Girder	-1.5	0.841	○	2.171	○	3.928	
	Bottom of Main Girder	~19.00	14.039	○	12.384	○	10.007	
During Deck Construction	Top of Main Girder	-1.5	5.532	○	5.766	○	5.832	
	Bottom of Main Girder	~14.00	7.435	○	7.135	○	6.821	
Dead Load	Top of Deck	≤10.00	2.278	○	1.930	○	1.385	
	Top of Main Girder	0	4.649	○	4.599	○	4.332	
	Bottom of Main Girder	~14.00	4.224	○	4.660	○	5.381	
Design Load1	Top of Deck	Max	3.705	○	3.222	○	2.230	
		Min	2.074	○	1.797	○	1.320	
	Top of Main Girder	Max	5.856	○	5.691	○	5.045	
		Min	-1.5	4.476	○	4.487	○	4.277
	Bottom of Main Girder	Max	~14.00	1.047	○	1.772	○	3.480
		Min		4.678	○	4.958	○	5.528
Design Load2 Temperature Rise	Top of Deck	Max	4.343	○	3.796	○	2.739	
		Min	≤11.50	2.711	○	2.370	○	1.829
	Top of Main Girder	Max	5.074	○	4.854	○	4.153	
		Min	-2	3.693	○	3.650	○	3.385
	Bottom of Main Girder	Max	~16.10	0.986	○	1.853	○	3.705
		Min		4.618	○	5.039	○	5.753
Design Load3 Temperature Drop	Top of Deck	Max	4.343	○	3.796	○	2.739	
		Min	≤11.50	2.711	○	2.370	○	1.829
	Top of Main Girder	Max	5.074	○	4.854	○	4.153	
		Min	-2	3.693	○	3.650	○	3.385
	Bottom of Main Girder	Max	~16.10	0.986	○	1.853	○	3.705
		Min		4.618	○	5.039	○	5.753
Design Load4 Support sinking	Top of Deck	Max	3.705	○	3.222	○	2.230	
		Min	≤10.00	2.074	○	1.797	○	1.320
	Top of Main Girder	Max	5.856	○	5.691	○	5.045	
		Min	-1.5	4.476	○	4.487	○	4.277
	Bottom of Main Girder	Max	~14.00	1.047	○	1.772	○	3.480
		Min		4.678	○	4.958	○	5.528
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	4.343	○	3.796	○	2.739	
		Min	≤11.50	2.711	○	2.370	○	1.829
	Top of Main Girder	Max	5.074	○	4.854	○	4.153	
		Min	-2	3.693	○	3.650	○	3.385
	Bottom of Main Girder	Max	~16.10	0.986	○	1.853	○	3.705
		Min		4.618	○	5.039	○	5.753
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	4.343	○	3.796	○	2.739	
		Min	≤11.50	2.711	○	2.370	○	1.829
	Top of Main Girder	Max	5.074	○	4.854	○	4.153	
		Min	-2	3.693	○	3.650	○	3.385
	Bottom of Main Girder	Max	~16.10	0.986	○	1.853	○	3.705
		Min		4.618	○	5.039	○	5.753

<Design of Main Girder: Summary for Calculation Results of Stress>

4th Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[4-13]		[4-14]		[4-15]		
Interval from beginning of Girder		-----	25.800		28.300		29.300		
Immediately After Prestressing	Top of Main Girder	-1.5	3.980	○	3.128	○	3.333	○	
	Bottom of Main Girder	~19.00	9.940	○	5.235	○	4.271	○	
During Deck Construction	Top of Main Girder	-1.5	5.829	○	3.525	○	3.167	○	
	Bottom of Main Girder	~14.00	6.820	○	4.320	○	4.057	○	
Dead Load	Top of Deck	≤10.00	1.367	○	0.636	○	0.373	○	
	Top of Main Girder	0	4.319	○	2.703	○	2.359	○	
	Bottom of Main Girder	~14.00	5.413	○	4.105	○	4.136	○	
Design Load1	Top of Deck	Max	2.194	○	0.905	○	0.373	○	
		Min	1.304	○	0.619	○	0.373	○	
	Top of Main Girder	Max	5.017	○	2.939	○	2.359	○	
		Min	-1.5	4.266	○	2.688	○	2.359	○
	Bottom of Main Girder	Max	~14.00	3.552	○	3.617	○	4.136	○
		Min		5.556	○	4.137	○	4.136	○
Design Load2 Temperature Rise	Top of Deck	Max	2.700	○	1.446	○	0.912	○	
		Min	≤11.50	1.810	○	1.160	○	0.912	○
	Top of Main Girder	Max	4.124	○	2.097	○	1.517	○	
		Min	-2	3.373	○	1.846	○	1.517	○
	Bottom of Main Girder	Max	~16.10	3.782	○	4.045	○	4.599	○
		Min		5.785	○	4.565	○	4.599	○
Design Load3 Temperature Drop	Top of Deck	Max	2.700	○	1.446	○	0.912	○	
		Min	≤11.50	1.810	○	1.160	○	0.912	○
	Top of Main Girder	Max	4.124	○	2.097	○	1.517	○	
		Min	-2	3.373	○	1.846	○	1.517	○
	Bottom of Main Girder	Max	~16.10	3.782	○	4.045	○	4.599	○
		Min		5.785	○	4.565	○	4.599	○
Design Load4 Support sinking	Top of Deck	Max	2.194	○	0.905	○	0.373	○	
		Min	≤10.00	1.304	○	0.619	○	0.373	○
	Top of Main Girder	Max	5.017	○	2.939	○	2.359	○	
		Min	-1.5	4.266	○	2.688	○	2.359	○
	Bottom of Main Girder	Max	~14.00	3.552	○	3.617	○	4.136	○
		Min		5.556	○	4.137	○	4.136	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	2.700	○	1.446	○	0.912	○	
		Min	≤11.50	1.810	○	1.160	○	0.912	○
	Top of Main Girder	Max	4.124	○	2.097	○	1.517	○	
		Min	-2	3.373	○	1.846	○	1.517	○
	Bottom of Main Girder	Max	~16.10	3.782	○	4.045	○	4.599	○
		Min		5.785	○	4.565	○	4.599	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	2.700	○	1.446	○	0.912	○	
		Min	≤11.50	1.810	○	1.160	○	0.912	○
	Top of Main Girder	Max	4.124	○	2.097	○	1.517	○	
		Min	-2	3.373	○	1.846	○	1.517	○
	Bottom of Main Girder	Max	~16.10	3.782	○	4.045	○	4.599	○
		Min		5.785	○	4.565	○	4.599	○

<Design of Main Girder: Summary for Calculation Results of Stress>

4th Span, Main Girder Number: G 2

Cross Section NumberNo.	Unit	Allowable Value	[4- 1]		[4- 2]		[4- 3]	
Interval from beginning of Girder								
				0.500		1.500		4.000
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1099	○	1103	○	1156	○
Effective Prestressing Force (*1)	N/mm ²	1110	1044	○	1046	○	1083	○
Effective Prestressing Force (*2)	N/mm ²	1110	973	○	973	○	989	○
max	N/mm ²	1110	971	○	971	○	991	○
Ultimate Load	-----	1.00	2.00	○	3.35	○	2.33	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[4- 4]		[4- 5]		[4- 6]	
Interval from beginning of Girder								
				4.100		7.700		11.300
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1157	○	1174	○	1164	○
Effective Prestressing Force (*1)	N/mm ²	1110	1083	○	1089	○	1067	○
Effective Prestressing Force (*2)	N/mm ²	1110	989	○	999	○	981	○
max	N/mm ²	1110	992	○	1023	○	1026	○
Ultimate Load	-----	1.00	2.29	○	1.55	○	1.34	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[4- 7]		[4- 8]		[4- 9]	
Interval from beginning of Girder								
				13.869		14.900		15.851
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	○	1320	○	1320	○
Immediately After Prestressing	N/mm ²	1295	1167	○	1172	○	1176	○
Effective Prestressing Force (*1)	N/mm ²	1110	1066	○	1071	○	1075	○
Effective Prestressing Force (*2)	N/mm ²	1110	985	○	990	○	993	○
max	N/mm ²	1110	1039	○	1046	○	1049	○
Ultimate Load	-----	1.00	1.26	○	1.24	○	1.24	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[4-10]	[4-11]	[4-12]
Interval from beginning of Girder			18.500	22.100	25.700
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	1320	1320
Immediately After Prestressing	N/mm ²	1295	1199	1197	1177
Effective Prestressing Force (*1)	N/mm ²	1110	1097	1106	1097
Effective Prestressing Force (*2)	N/mm ²	1110	1011	1017	1005
max	N/mm ²	1110	1062	1052	1020
Ultimate Load	-----	1.00	1.28	1.42	2.00

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[4-13]	[4-14]	[4-15]
Interval from beginning of Girder			25.800	28.300	29.300
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1320	1320	1320
Immediately After Prestressing	N/mm ²	1295	1177	1168	1164
Effective Prestressing Force (*1)	N/mm ²	1110	1097	1107	1106
Effective Prestressing Force (*2)	N/mm ²	1110	1005	1035	1036
max	N/mm ²	1110	1019	1037	1036
Ultimate Load	-----	1.00	2.03	5.33	999.90

*1:During DeckConstruction *2:Design Load

4th Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[4- 1]	[4- 2]	[4- 3]		
Interval from beginning of Girder			-----	0.500	1.500	4.000		
Shear Force								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	1.00 Δ	0.74 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.10 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.23 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.20 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.07 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.30 ○	-0.18 ○	
				Min	-----	--	-0.09 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.40 ○	-0.15 ○
				Min	-----	--	-0.22 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.42 ○	-0.18 ○
				Min	-----	--	-0.19 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.08 ○	-0.10 ○
				Min	-----	--	-0.07 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 --	27.15 --	
	D16	cm	-----	-----	--	32.03 --	40.00 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	-----	--	10.03 --	8.57 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	-----	--	3.16 ○	1.80 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	--	1.015 ○	1.00 ○	
	D16			-----	--	1.015 ○	1.02 ○	
	D19			-----	--	1.071 ○	1.19 ○	
Shear Force + Torsion								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	1.00 Δ	0.74 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.10 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.23 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.20 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.07 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.30 ○	-0.18 ○	
				Min	-----	--	-0.09 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.40 ○	-0.15 ○
				Min	-----	--	-0.22 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.42 ○	-0.18 ○
				Min	-----	--	-0.19 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.08 ○	-0.10 ○
				Min	-----	--	-0.07 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 --	27.15 --	
	D16	cm	-----	-----	--	32.03 --	40.00 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	-----	--	0.00 --	0.00 --		

4th Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[4- 4]	[4- 5]	[4- 6]	
Interval from beginning of Girder			-----	4.100	7.700	11.300	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.72 Δ	0.64 Δ	0.50 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis after Composition			0.00 ○	0.00 ○	0.00 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.17 ○	-0.14 ○	-0.09 ○
				Min	0.00 ○	0.00 ○	-0.02 ○
	Neutral Axis before Composition			Max	-0.15 ○	-0.12 ○	-0.07 ○
				Min	0.00 ○	-0.01 ○	-0.02 ○
	Neutral Axis after Composition			Max	-0.17 ○	-0.14 ○	-0.09 ○
				Min	0.00 ○	0.00 ○	-0.02 ○
	Base of Lower Flange			Max	-0.10 ○	-0.08 ○	-0.05 ○
				Min	-0.01 ○	-0.01 ○	-0.03 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	27.74 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	8.39 --	5.55 --	2.46 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	1.82 ○	2.23 ○	3.02 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.00 ○	1.015 ○	----- --	
	D16			1.03 ○	1.193 ○	----- --	
	D19			1.20 ○	1.411 ○	----- --	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.72 Δ	0.64 Δ	0.50 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis before Composition			0.00 ○	0.00 ○	0.00 ○	
	Neutral Axis after Composition			0.00 ○	0.00 ○	0.00 ○	
	Base of Lower Flange			0.00 ○	0.00 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.17 ○	-0.14 ○	-0.09 ○
				Min	0.00 ○	0.00 ○	-0.02 ○
	Neutral Axis before Composition			Max	-0.15 ○	-0.12 ○	-0.07 ○
				Min	0.00 ○	-0.01 ○	-0.02 ○
	Neutral Axis after Composition			Max	-0.17 ○	-0.14 ○	-0.09 ○
				Min	0.00 ○	0.00 ○	-0.02 ○
	Base of Lower Flange			Max	-0.10 ○	-0.08 ○	-0.05 ○
				Min	-0.01 ○	-0.01 ○	-0.03 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	27.74 --	40.00 --	40.00 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

4th Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[4- 7]	[4- 8]	[4- 9]				
Interval from beginning of Girder			-----	13.869	14.900	15.851				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.59	Δ	0.44	○	0.54	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.01	○	0.00	○	-0.02	○	
	Neutral Axis before Composition			-0.02	○	0.00	○	-0.02	○	
	Neutral Axis after Composition			-0.02	○	0.00	○	-0.02	○	
	Base of Lower Flange			-0.01	○	0.00	○	-0.02	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.11	○	-0.06	○	-0.02	○
				Min	-0.01	○	-0.04	○	-0.08	○
	Neutral Axis before Composition			Max	-0.11	○	-0.06	○	-0.01	○
				Min	-0.01	○	-0.05	○	-0.10	○
	Neutral Axis after Composition			Max	-0.12	○	-0.07	○	-0.01	○
				Min	-0.02	○	-0.05	○	-0.10	○
	Base of Lower Flange			Max	-0.08	○	-0.04	○	-0.01	○
				Min	-0.01	○	-0.06	○	-0.10	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	1.68	--	0.19	--	0.00	--		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	3.93	○	4.70	○	5.44	○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.456	○	-----	--	-----	--	
	D16			1.819	○	-----	--	-----	--	
	D19			2.263	○	-----	--	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.59	Δ	0.44	○	0.54	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.01	○	0.00	○	-0.02	○	
	Neutral Axis before Composition			-0.02	○	0.00	○	-0.02	○	
	Neutral Axis after Composition			-0.02	○	0.00	○	-0.02	○	
	Base of Lower Flange			-0.01	○	0.00	○	-0.02	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.11	○	-0.06	○	-0.02	○
				Min	-0.01	○	-0.04	○	-0.08	○
	Neutral Axis before Composition			Max	-0.11	○	-0.06	○	-0.01	○
				Min	-0.01	○	-0.05	○	-0.10	○
	Neutral Axis after Composition			Max	-0.12	○	-0.07	○	-0.01	○
				Min	-0.02	○	-0.05	○	-0.10	○
	Base of Lower Flange			Max	-0.08	○	-0.04	○	-0.01	○
				Min	-0.01	○	-0.06	○	-0.10	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	0.00	--	0.00	--	0.00	--		

<Design of Main Girder: Summary for Calculation Results of Stress>

4th Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[4-10]	[4-11]	[4-12]	
Interval from beginning of Girder			-----	18.500	22.100	25.700	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	0.57 Δ	0.75 Δ	1.10 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.01 ○	-0.02 ○	-0.07 ○	
	Neutral Axis before Composition			-0.01 ○	-0.02 ○	-0.07 ○	
	Neutral Axis after Composition			-0.02 ○	-0.02 ○	-0.07 ○	
	Base of Lower Flange			-0.01 ○	-0.01 ○	-0.04 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00 ○	0.00 ○	-0.06 ○
				Min	-0.09 ○	-0.16 ○	-0.35 ○
	Neutral Axis before Composition			Max	0.00 ○	0.00 ○	-0.05 ○
				Min	-0.12 ○	-0.19 ○	-0.36 ○
	Neutral Axis after Composition			Max	0.00 ○	0.00 ○	-0.06 ○
				Min	-0.11 ○	-0.18 ○	-0.38 ○
	Base of Lower Flange			Max	0.00 ○	0.00 ○	-0.03 ○
				Min	-0.12 ○	-0.17 ○	-0.26 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	28.47 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	1.05 --	4.14 --	8.17 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	3.92 ○	2.64 ○	1.94 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.494 ○	1.111 ○	1.00 ○	
	D16			1.835 ○	1.328 ○	1.04 ○	
	D19			2.253 ○	1.593 ○	1.23 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	0.57 Δ	0.75 Δ	1.10 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.01 ○	-0.02 ○	-0.07 ○	
	Neutral Axis before Composition			-0.01 ○	-0.02 ○	-0.07 ○	
	Neutral Axis after Composition			-0.02 ○	-0.02 ○	-0.07 ○	
	Base of Lower Flange			-0.01 ○	-0.01 ○	-0.04 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00 ○	0.00 ○	-0.06 ○
				Min	-0.09 ○	-0.16 ○	-0.35 ○
	Neutral Axis before Composition			Max	0.00 ○	0.00 ○	-0.05 ○
				Min	-0.12 ○	-0.19 ○	-0.36 ○
	Neutral Axis after Composition			Max	0.00 ○	0.00 ○	-0.06 ○
				Min	-0.11 ○	-0.18 ○	-0.38 ○
	Base of Lower Flange			Max	0.00 ○	0.00 ○	-0.03 ○
				Min	-0.12 ○	-0.17 ○	-0.26 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00 --	40.00 --	28.47 --	
	D16	cm	-----	40.00 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

4th Span, Main Girder Number: G 3(Shear Force Max)

Cross Section Number			Allowable Value	[4-13]	[4-14]	[4-15]				
Interval from beginning of Girder			-----	25.800	28.300	29.300				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.12	Δ	0.49	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.07	○	-0.02	○	-----	--	
	Neutral Axis before Composition			-0.07	○	-0.03	○	-----	--	
	Neutral Axis after Composition			-0.08	○	-0.03	○	-----	--	
	Base of Lower Flange			-0.04	○	-0.01	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.06	○	-0.02	○	-----	--
				Min	-0.37	○	-0.11	○	-----	--
	Neutral Axis before Composition			Max	-0.06	○	-0.02	○	-----	--
				Min	-0.37	○	-0.12	○	-----	--
	Neutral Axis after Composition			Max	-0.06	○	-0.03	○	-----	--
				Min	-0.39	○	-0.14	○	-----	--
	Base of Lower Flange			Max	-0.04	○	0.00	○	-----	--
				Min	-0.27	○	-0.02	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	27.93	--	20.44	--	-----	--	
	D16	cm	-----	40.00	--	32.03	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	8.33	--	0.00	--	-----	--	
Compressive Strength to Failure (Suc/Shu)			1.00	1.92	○	4.02	○	-----	--	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1	○	-----	--	-----	--	
	D16			1.037	○	-----	--	-----	--	
	D19			1.223	○	-----	--	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.12	Δ	0.49	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.07	○	-0.02	○	-----	--	
	Neutral Axis before Composition			-0.07	○	-0.03	○	-----	--	
	Neutral Axis after Composition			-0.08	○	-0.03	○	-----	--	
	Base of Lower Flange			-0.04	○	-0.01	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.06	○	-0.02	○	-----	--
				Min	-0.37	○	-0.11	○	-----	--
	Neutral Axis before Composition			Max	-0.06	○	-0.02	○	-----	--
				Min	-0.37	○	-0.12	○	-----	--
	Neutral Axis after Composition			Max	-0.06	○	-0.03	○	-----	--
				Min	-0.39	○	-0.14	○	-----	--
	Base of Lower Flange			Max	-0.04	○	0.00	○	-----	--
				Min	-0.27	○	-0.02	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	27.93	--	20.44	--	-----	--	
	D16	cm	-----	40.00	--	32.03	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

4th Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[4- 1]	[4- 2]	[4- 3]		
Interval from beginning of Girder			-----	0.500	1.500	4.000		
Shear Force								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.97 Δ	0.69 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.11 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.22 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.20 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.06 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.29 ○	-0.17 ○	
				Min	-----	--	-0.11 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.39 ○	-0.14 ○
				Min	-----	--	-0.21 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.40 ○	-0.16 ○
				Min	-----	--	-0.19 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.08 ○	-0.10 ○
				Min	-----	--	-0.05 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 --	29.51 --	
	D16	cm	-----	-----	--	32.03 --	40.00 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	9.31 --	7.88 --	
Shear Force + Torsion								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.97 Δ	0.69 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.11 ○	0.00 ○	
	Neutral Axis before Composition			-----	--	-0.22 ○	0.00 ○	
	Neutral Axis after Composition			-----	--	-0.20 ○	0.00 ○	
	Base of Lower Flange			-----	--	-0.06 ○	0.00 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.29 ○	-0.17 ○	
				Min	-----	--	-0.11 ○	0.00 ○
	Neutral Axis before Composition			Max	-----	--	-0.39 ○	-0.14 ○
				Min	-----	--	-0.21 ○	0.00 ○
	Neutral Axis after Composition			Max	-----	--	-0.40 ○	-0.16 ○
				Min	-----	--	-0.19 ○	0.00 ○
	Base of Lower Flange			Max	-----	--	-0.08 ○	-0.10 ○
				Min	-----	--	-0.05 ○	0.00 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.44 --	29.51 --	
	D16	cm	-----	-----	--	32.03 --	40.00 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 --	0.00 --	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	-----	--	999.999 ○	999.999 ○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	--	999.999 ○	999.999 ○	
	D16			-----	--	999.999 ○	999.999 ○	
	D19			-----	--	999.999 ○	999.999 ○	

<Design of Main Girder: Summary for Calculation Results of Stress>

4th Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[4- 4]	[4- 5]	[4- 6]				
Interval from beginning of Girder			-----	4.100	7.700	11.300				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.67	Δ	0.63	Δ	0.37	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.16	○	-0.13	○	-0.05	○
				Min	0.00	○	0.00	○	0.00	○
	Neutral Axis before Composition	Max		-0.14	○	-0.13	○	-0.05	○	
		Min		0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition	Max		-0.16	○	-0.14	○	-0.05	○	
		Min		0.00	○	0.00	○	0.00	○	
	Base of Lower Flange	Max		-0.10	○	-0.11	○	-0.07	○	
		Min		0.00	○	0.00	○	0.00	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	30.23	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	7.70	--	5.55	--	1.29	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.67	Δ	0.63	Δ	0.37	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.16	○	-0.13	○	-0.05	○
				Min	0.00	○	0.00	○	0.00	○
	Neutral Axis before Composition	Max		-0.14	○	-0.13	○	-0.05	○	
		Min		0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition	Max		-0.16	○	-0.14	○	-0.05	○	
		Min		0.00	○	0.00	○	0.00	○	
	Base of Lower Flange	Max		-0.10	○	-0.11	○	-0.07	○	
		Min		0.00	○	0.00	○	0.00	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	30.23	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Densile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	-	
	D16			999.999	○	999.999	○	-----	-	
	D19			999.999	○	999.999	○	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

4th Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[4- 7]	[4- 8]	[4- 9]				
Interval from beginning of Girder			-----	13.869	14.900	15.851				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.32	○	0.12	○	0.11	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.03	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	0.00	○
	Neutral Axis before Composition	Max		-0.04	○	-0.01	○	0.00	○	
		Min		0.00	○	0.00	○	-0.01	○	
	Neutral Axis after Composition	Max		-0.04	○	-0.01	○	0.00	○	
		Min		0.00	○	0.00	○	0.00	○	
	Base of Lower Flange	Max		-0.03	○	-0.01	○	0.00	○	
		Min		0.00	○	0.00	○	-0.01	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.32	○	0.12	○	0.11	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.03	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	0.00	○
	Neutral Axis before Composition	Max		-0.04	○	-0.01	○	0.00	○	
		Min		0.00	○	0.00	○	-0.01	○	
	Neutral Axis after Composition	Max		-0.04	○	-0.01	○	0.00	○	
		Min		0.00	○	0.00	○	0.00	○	
	Base of Lower Flange	Max		-0.03	○	-0.01	○	0.00	○	
		Min		0.00	○	0.00	○	-0.01	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	-----	-	-----	-	
	D16	-----	1.00	-----	-	-----	-	-----	-	
	D19	-----	1.00	-----	-	-----	-	-----	-	

4th Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[4-10]	[4-11]	[4-12]				
Interval from beginning of Girder			-----	18.500	22.100	25.700				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.36	○	0.77	△	0.90	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	-0.01	○	-0.06	○	
	Neutral Axis before Composition			0.00	○	-0.01	○	-0.05	○	
	Neutral Axis after Composition			0.00	○	-0.01	○	-0.06	○	
	Base of Lower Flange			0.00	○	-0.01	○	-0.03	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	-0.01	○	-0.07	○
				Min	-0.04	○	-0.18	○	-0.26	○
	Neutral Axis before Composition			Max	0.00	○	-0.01	○	-0.06	○
				Min	-0.05	○	-0.21	○	-0.24	○
	Neutral Axis after Composition			Max	0.00	○	-0.01	○	-0.07	○
				Min	-0.05	○	-0.20	○	-0.27	○
	Base of Lower Flange			Max	0.00	○	-0.01	○	-0.04	○
				Min	-0.07	○	-0.20	○	-0.17	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	4.49	--	5.80	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.36	○	0.77	△	0.90	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	-0.01	○	-0.06	○	
	Neutral Axis before Composition			0.00	○	-0.01	○	-0.05	○	
	Neutral Axis after Composition			0.00	○	-0.01	○	-0.06	○	
	Base of Lower Flange			0.00	○	-0.01	○	-0.03	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	-0.01	○	-0.07	○
				Min	-0.04	○	-0.18	○	-0.26	○
	Neutral Axis before Composition			Max	0.00	○	-0.01	○	-0.06	○
				Min	-0.05	○	-0.21	○	-0.24	○
	Neutral Axis after Composition			Max	0.00	○	-0.01	○	-0.07	○
				Min	-0.05	○	-0.20	○	-0.27	○
	Base of Lower Flange			Max	0.00	○	-0.01	○	-0.04	○
				Min	-0.07	○	-0.20	○	-0.17	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	999.999	○	999.999	○	
	D16			-----	-	999.999	○	999.999	○	
	D19			-----	-	999.999	○	999.999	○	

4th Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[4-13]	[4-14]	[4-15]				
Interval from beginning of Girder			-----	25.800	28.300	29.300				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.02	Δ	0.43	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.07	○	-0.02	○	-----	--	
	Neutral Axis before Composition			-0.06	○	-0.02	○	-----	--	
	Neutral Axis after Composition			-0.07	○	-0.03	○	-----	--	
	Base of Lower Flange			-0.04	○	0.00	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.07	○	-0.03	○	-----	--
				Min	-0.32	○	-0.09	○	-----	--
	Neutral Axis before Composition			Max	-0.06	○	-0.03	○	-----	--
				Min	-0.32	○	-0.10	○	-----	--
	Neutral Axis after Composition			Max	-0.07	○	-0.03	○	-----	--
				Min	-0.34	○	-0.11	○	-----	--
	Base of Lower Flange			Max	-0.04	○	0.00	○	-----	--
				Min	-0.23	○	-0.02	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	32.14	--	20.44	--	-----	--	
	D16	cm	-----	40.00	--	32.03	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	7.24	--	0.00	--	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.02	Δ	0.43	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.07	○	-0.02	○	-----	--	
	Neutral Axis before Composition			-0.06	○	-0.02	○	-----	--	
	Neutral Axis after Composition			-0.07	○	-0.03	○	-----	--	
	Base of Lower Flange			-0.04	○	0.00	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.07	○	-0.03	○	-----	--
				Min	-0.32	○	-0.09	○	-----	--
	Neutral Axis before Composition			Max	-0.06	○	-0.03	○	-----	--
				Min	-0.32	○	-0.10	○	-----	--
	Neutral Axis after Composition			Max	-0.07	○	-0.03	○	-----	--
				Min	-0.34	○	-0.11	○	-----	--
	Base of Lower Flange			Max	-0.04	○	0.00	○	-----	--
				Min	-0.23	○	-0.02	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	32.14	--	20.44	--	-----	--	
	D16	cm	-----	40.00	--	32.03	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	-----	--	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	-----	-	-----	--	
	D16			999.999	○	-----	-	-----	--	
	D19			999.999	○	-----	-	-----	--	

5 Design of Intermediate Cross Beam

(1) Parameters

<1st Span>

	Unit	Bending Moment (Maximum)	Bending Moment (Minimum)
CB 2			
Length between End of Girders	Lb	cm	327.9
Web Width	Bw	cm	22.0
Width of Cross Beam	Bc	cm	30.0
Thickness of Deck	Hs	cm	17.0
Height of Cross Beam (before Composition of Deck)	Hb	cm	135.0
Height of Cross Beam (after Composition of Deck)	Ha	cm	192.0
Interval of Cross Beam	Lt	cm	1409.9

<2nd Span>

	Unit	Bending Moment (Maximum)	Bending Moment (Minimum)
CB 2			
Length between End of Girders	Lb	cm	328.0
Web Width	Bw	cm	22.0
Width of Cross Beam	Bc	cm	30.0
Thickness of Deck	Hs	cm	17.0
Height of Cross Beam (before Composition of Deck)	Hb	cm	135.0
Height of Cross Beam (after Composition of Deck)	Ha	cm	192.0
Interval of Cross Beam	Lt	cm	1410.0

<3rd Span>

	Unit	Bending Moment (Maximum)	Bending Moment (Minimum)
CB 2			
Length between End of Girders	Lb	cm	328.0
Web Width	Bw	cm	22.0
Width of Cross Beam	Bc	cm	30.0
Thickness of Deck	Hs	cm	17.0
Height of Cross Beam (before Composition of Deck)	Hb	cm	135.0
Height of Cross Beam (after Composition of Deck)	Ha	cm	192.0
Interval of Cross Beam	Lt	cm	1410.0

<4th Span>

	Unit	Bending Moment (Maximum)	Bending Moment (Minimum)
CB 2			
Length between End of Girders	Lb	cm	328.0
Web Width	Bw	cm	22.0
Width of Cross Beam	Bc	cm	30.0
Thickness of Deck	Hs	cm	17.0
Height of Cross Beam (before Composition of Deck)	Hb	cm	135.0
Height of Cross Beam (after Composition of Deck)	Ha	cm	192.0
Interval of Cross Beam	Lt	cm	1410.0

(2) Calculation of Prestressing

1) Arrangement of PC Strand

(1) Parameter of PC Strand

	Unit	Parameters
Name of PC Strand		4S15.2, SWPR7BL
Area of PC Strand	mm ² /no.	554.80
Amount of Set	mm	4.0
Reduction Rate of Anchor	%	0.000
Friction Coefficient	1/m	0.0040
Creep Coefficient		2.60
Drying Shrinkage	×10 ⁻⁵	20.00
Relaxation	%	2.5
Prestressing Stress	N/mm ²	1250.000
(Considering Friction Coefficient)	N/mm ²	1250.000
Allowable Value	N/mm ²	1440.000

(2) Arrangement of PC Strand

<1st Span>

Item	Unit	Maximum Bending Moment	Minimum Bending Moment
CB 2			
How to Prestressing		From One Side	
Length of PC Strand	m	10.720	10.720
1st	Position	mm	400
	Number	No.	1
2nd	Position	mm	800
	Number	No.	1

<2nd Span>

Item	Unit	Maximum Bending Moment	Minimum Bending Moment
CB 2			
How to Prestressing		From One Side	
Length of PC Strand	m	10.720	10.720
1st	Position	mm	400
	Number	No.	1
2nd	Position	mm	800
	Number	No.	1

<3rd Span>

Item	Unit	Maximum Bending Moment	Minimum Bending Moment
CB 2			
How to Prestressing		From One Side	
Length of PC Strand	m	10.720	10.720
1st	Position	mm	400
	Number	No.	1
2nd	Position	mm	800
	Number	No.	1

<4th Span>

Item	Unit	Maximum Bending Moment	Minimum Bending Moment
CB 2			
How to Prestressing		From One Side	
Length of PC Strand	m	10.720	10.720
1st	Position	mm	400
	Number	No.	1
2nd	Position	mm	800
	Number	No.	1

<Design of Cross Beam : Summary for Calculation Results of Stress>

1st Span : Cross Beam (CB2)

Item		Unit	Allowable Value	Mmax		Mmin	
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	-0.34	○	-0.34	○
	Bottom of Deck			-0.23	○	-0.23	○
Dead Load	Top of Cross Beam	N/mm ²	0	1.90	○	1.90	○
	Bottom of Cross Beam			~ 11.0	4.65	○	4.65
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	0.52	○	-0.84	○
	Bottom of Deck			0.35	○	-0.57	○
Dead Load	Top of Cross Beam	N/mm ²	-1.2	1.84	○	1.94	○
	Bottom of Cross Beam			~ 11.0	2.41	○	5.95
Ultimate Load		-----	1	1.84	○	1.62	○
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1440	1250	○	1250	○
	Immediately After Prestressing	N/mm ²	1295	1175	○	1175	○
	Effective Prestressing Force	N/mm ²	1110	1026	○	1026	○

2nd Span : Cross Beam (CB2)

Item		Unit	Allowable Value	Mmax		Mmin	
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	-0.25	○	-0.25	○
	Bottom of Deck			-0.17	○	-0.17	○
Dead Load	Top of Cross Beam	N/mm ²	0	1.89	○	1.89	○
	Bottom of Cross Beam			~ 11.0	4.41	○	4.41
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	0.54	○	-0.81	○
	Bottom of Deck			0.37	○	-0.55	○
Dead Load	Top of Cross Beam	N/mm ²	-1.2	1.84	○	1.93	○
	Bottom of Cross Beam			~ 11.0	2.34	○	5.85
Ultimate Load		-----	1	1.92	○	1.59	○
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1440	1250	○	1250	○
	Immediately After Prestressing	N/mm ²	1295	1175	○	1175	○
	Effective Prestressing Force	N/mm ²	1110	1026	○	1026	○

3rd Span : Cross Beam (CB2)

Item		Unit	Allowable Value	Mmax		Mmin	
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	-0.26	○	-0.26	○
	Bottom of Deck			-0.17	○	-0.17	○
Dead Load	Top of Cross Beam	N/mm ²	0	1.89	○	1.89	○
	Bottom of Cross Beam			~11.0	4.41	○	4.41
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	0.54	○	-0.81	○
	Bottom of Deck			0.37	○	-0.55	○
Dead Load	Top of Cross Beam	N/mm ²	-1.2	1.84	○	1.93	○
	Bottom of Cross Beam			~11.0	2.35	○	5.85
Ultimate Load		-----	1	1.92	○	1.59	○
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1440	1250	○	1250	○
	Immediately After Prestressing	N/mm ²	1295	1175	○	1175	○
	Effective Prestressing Force	N/mm ²	1110	1026	○	1026	○

4th Span : Cross Beam (CB2)

Item		Unit	Allowable Value	Mmax		Mmin	
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	-0.30	○	-0.30	○
	Bottom of Deck			-0.20	○	-0.20	○
Dead Load	Top of Cross Beam	N/mm ²	0	1.90	○	1.90	○
	Bottom of Cross Beam			~11.0	4.53	○	4.53
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	0.53	○	-0.85	○
	Bottom of Deck			0.36	○	-0.58	○
Dead Load	Top of Cross Beam	N/mm ²	-1.2	1.84	○	1.94	○
	Bottom of Cross Beam			~11.0	2.35	○	5.98
Ultimate Load		-----	1	1.86	○	1.56	○
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1440	1250	○	1250	○
	Immediately After Prestressing	N/mm ²	1295	1175	○	1175	○
	Effective Prestressing Force	N/mm ²	1110	1026	○	1026	○

<Design of Cross Beam : Summary for Calculation Results of Stress>

1st Span : Cross Beam (CB2)

Item	Unit	Allowable Value	Smax	Smin	Tmax	Tmin					
Shear Force											
Shear Stress	Design Load	N/mm ²	0.45	0.63	Δ	0.43	○	0.14	○	0.14	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	-0.02	○	-0.02	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	-0.18	○	-0.17	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Suc/Shu	-	1.00	2.97	○	4.42	○	11.02	○	12.34	○
Strength against Diagonal Densile Failure	D13	-	1.00	1.00	○	----	--	----	--	----	--
	Sus/Shu	D16	-	1.00	1.07	○	----	--	----	--	----
Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.00	○	0.00	○	0.00	○	0.00	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	0.00	○	0.00	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	0.00	○	0.00	○	0.00	○	0.00	○
Shear Force + Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.63	Δ	0.43	○	0.14	○	0.14	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-1.10	-0.02	○	-0.02	○	0.00	○	0.00	○
	Design Load	N/mm ²	-2.20	-0.18	○	-0.17	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Muc/Mtu	-	1.00	999.999	○	999.999	○	999.999	○	999.999	○
Strength against Diagonal Densile Failure	D13	-	1.00	999.999	○	----	--	----	--	----	--
	Mus/Mtu	D16	-	1.00	999.999	○	----	--	----	--	----
Amount of Diagonal Tension Re-bar	cm ²	----	8.99	--	6.00	--	6.00	--	6.00	--	
Axial Reinforcement Bar Volume	cm ²	----	5.07	--	0.04	--	0.00	--	0.00	--	

2nd Span : Cross Beam (CB2)

Item	Unit	Allowable Value	Smax	Smin	Tmax	Tmin					
Shear Force											
Shear Stress	Design Load	N/mm ²	0.45	0.56	Δ	0.39	○	0.16	○	0.16	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	-0.01	○	-0.01	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	-0.14	○	-0.14	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Suc/Shu	-	1.00	3.22	○	4.64	○	10.13	○	10.10	○
Strength against Diagonal Densile Failure	D13	-	1.00	1.00	○	----	--	----	--	----	--
	Sus/Shu	D16	-	1.00	1.16	○	----	--	----	--	----
Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.00	○	0.00	○	0.00	○	0.00	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	0.00	○	0.00	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	0.00	○	0.00	○	0.00	○	0.00	○
Shear Force + Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.56	Δ	0.39	○	0.16	○	0.16	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-1.10	-0.01	○	-0.01	○	0.00	○	0.00	○
	Design Load	N/mm ²	-2.20	-0.14	○	-0.14	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Muc/Mtu	-	1.00	999.999	○	999.999	○	999.999	○	999.999	○
Strength against Diagonal Densile Failure	D13	-	1.00	999.999	○	----	--	----	--	----	--
	Mus/Mtu	D16	-	1.00	999.999	○	----	--	----	--	----
Amount of Diagonal Tension Re-bar	cm ²	----	7.92	--	6.00	--	6.00	--	6.00	--	
Axial Reinforcement Bar Volume	cm ²	----	4.46	--	0.00	--	0.00	--	0.00	--	

3rd Span : Cross Beam (CB2)

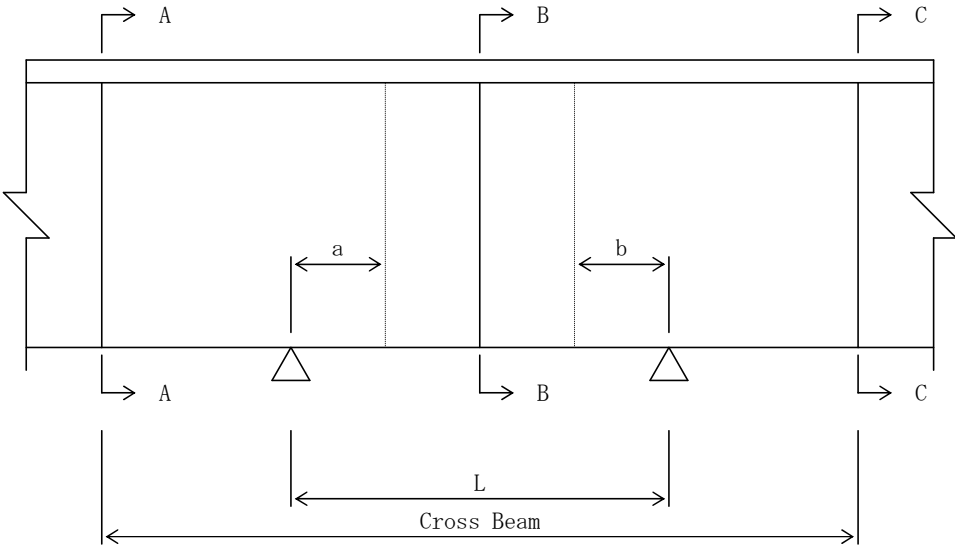
Item	Unit	Allowable Value	Smax	Smin	Tmax	Tmin					
Shear Force											
Shear Stress	Design Load	N/mm ²	0.45	0.56	Δ	0.39	○	0.16	○	0.16	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	-0.01	○	-0.01	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	-0.14	○	-0.14	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Suc/Shu	-	1.00	3.22	○	4.64	○	10.12	○	10.11	○
Strength against Diagonal Densile Failure	D13	-	1.00	1.00	○	----	--	----	--	----	--
	Sus/Shu	-	1.00	1.16	○	----	--	----	--	----	--
Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.00	○	0.00	○	0.00	○	0.00	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	0.00	○	0.00	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	0.00	○	0.00	○	0.00	○	0.00	○
Shear Force + Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.56	Δ	0.39	○	0.16	○	0.16	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-1.10	-0.01	○	-0.01	○	0.00	○	0.00	○
	Design Load	N/mm ²	-2.20	-0.14	○	-0.14	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Muc/Mtu	-	1.00	999.999	○	999.999	○	999.999	○	999.999	○
Strength against Diagonal Densile Failure	D13	-	1.00	999.999	○	----	--	----	--	----	--
	Mus/Mtu	-	1.00	999.999	○	----	--	----	--	----	--
Amount of Diagonal Tension Re-bar	cm ²	----	7.92	--	6.00	--	6.00	--	6.00	--	
Axial Reinforcement Bar Volume	cm ²	----	4.46	--	0.00	--	0.00	--	0.00	--	

<Design of Cross Beam : Summary for Calculation Results of Stress>

4th Span : Cross Beam (CB2)

Item	Unit	Allowable Value	Smax	Smin	Tmax	Tmin					
Shear Force											
Shear Stress	Design Load	N/mm ²	0.45	0.59	Δ	0.41	○	0.14	○	0.14	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	-0.01	○	-0.01	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	-0.16	○	-0.16	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Suc/Shu	-	1.00	3.12	○	4.49	○	11.67	○	11.67	○
Strength against Diagonal Densile Failure	D13	-	1.00	1.00	○	----	--	----	--	----	--
	Sus/Shu	-	1.00	1.13	○	----	--	----	--	----	--
Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.00	○	0.00	○	0.00	○	0.00	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	0.00	○	0.00	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	0.00	○	0.00	○	0.00	○	0.00	○
Shear Force + Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.59	Δ	0.41	○	0.14	○	0.14	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-1.10	-0.01	○	-0.01	○	0.00	○	0.00	○
	Design Load	N/mm ²	-2.20	-0.16	○	-0.16	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Muc/Mtu	-	1.00	999.999	○	999.999	○	999.999	○	999.999	○
Strength against Diagonal Densile Failure	D13	-	1.00	999.999	○	----	--	----	--	----	--
	Mus/Mtu	-	1.00	999.999	○	----	--	----	--	----	--
Amount of Diagonal Tension Re-bar	cm ²	----	8.32	--	6.00	--	6.00	--	6.00	--	
Axial Reinforcement Bar Volume	cm ²	----	4.69	--	0.00	--	0.00	--	0.00	--	

6 Design of Coupling Concrete
Dimension



Unit: m

	1 to 2 Span	2 to 3 Span	3 to 4 Span
L	1.200	1.200	1.200
a	0.500	0.500	0.500
b	0.500	0.500	0.500

<Connection of Cross beam : Summary for Calculation Results of Stress>

1st Span~2nd Span, Main Girder Number: G4(Negative Moment) G1(Positive Moment)

Item		Unit	Allowable Value	Negative Moment						Positive Moment		
				A-A		B-B		C-C		B-B		
Re-bar Volume	1st Layer	Diameter	mm	-----	D19	--	D19	--	D19	--	D22	--
		Number	Number	-----	16	--	16	--	16	--	9	--
	2nd Layer	Diameter	mm	-----	D19	--	D19	--	D19	--	D22	--
		Number	Number	-----	16	--	16	--	16	--	9	--
Bending Stress (Dead Load)												
Bending Tensile Stress of Reinforcement Bar			N/mm ²	100	16.04	○	27.95	○	17.01	○	18.83	○
Bending Stress (Design Load)												
Bending Stress of Concrete			N/mm ²	10	4.91	○	4.91	○	4.91	○	0.77	○
Bending Tensile Stress of Reinforcement Bar			N/mm ²	160	136.49	○	136.49	○	136.49	○	46.27	○
Bending Stress (Temperature Load)												
Bending Stress of Concrete			N/mm ²	11.5	4.95	○	4.91	○	4.77	○	1.51	○
Bending Tensile Stress of Reinforcement Bar			N/mm ²	184	137.58	○	136.49	○	132.64	○	91.24	○
Ultimate Load			-----	1.00	1.07	○	1.13	○	1.11	○	3.94	○

2nd Span~3rd Span, Main Girder Number: G1(Negative Moment) G4(Positive Moment)

Item		Unit	Allowable Value	Negative Moment						Positive Moment		
				A-A		B-B		C-C		B-B		
Re-bar Volume	1st Layer	Diameter	mm	-----	D19	--	D19	--	D19	--	D22	--
		Number	Number	-----	16	--	16	--	16	--	9	--
	2nd Layer	Diameter	mm	-----	D19	--	D19	--	D19	--	D22	--
		Number	Number	-----	16	--	16	--	16	--	9	--
Bending Stress (Dead Load)												
Bending Tensile Stress of Reinforcement Bar			N/mm ²	100	-14.27	○	-6.18	○	-14.15	○	19.37	○
Bending Stress (Design Load)												
Bending Stress of Concrete			N/mm ²	10	3.34	○	3.34	○	3.34	○	0.94	○
Bending Tensile Stress of Reinforcement Bar			N/mm ²	160	92.72	○	92.72	○	92.72	○	57.00	○
Bending Stress (Temperature Load)												
Bending Stress of Concrete			N/mm ²	11.5	3.21	○	3.34	○	3.21	○	1.46	○
Bending Tensile Stress of Reinforcement Bar			N/mm ²	184	89.07	○	92.72	○	89.17	○	88.06	○
Ultimate Load			-----	1.00	1.46	○	1.47	○	1.46	○	3.12	○

3rd Span~4th Span, Main Girder Number: G4(Negative Moment) G1(Positive Moment)

Item		Unit	Allowable Value	Negative Moment						Positive Moment		
				A-A		B-B		C-C		B-B		
Re-bar Volume	1st Layer	Diameter	mm	-----	D19	--	D19	--	D19	--	D22	--
		Number	Number	-----	16	--	16	--	16	--	9	--
	2nd Layer	Diameter	mm	-----	D19	--	D19	--	D19	--	D22	--
		Number	Number	-----	16	--	16	--	16	--	9	--
Bending Stress (Dead Load)												
Bending Tensile Stress of Reinforcement Bar			N/mm ²	100	-22.37	○	-15.73	○	-24.27	○	22.64	○
Bending Stress (Design Load)												
Bending Stress of Concrete			N/mm ²	10	3.30	○	3.30	○	3.30	○	0.82	○
Bending Tensile Stress of Reinforcement Bar			N/mm ²	160	91.73	○	91.73	○	91.73	○	49.82	○
Bending Stress (Temperature Load)												
Bending Stress of Concrete			N/mm ²	11.5	3.26	○	3.30	○	3.41	○	1.57	○
Bending Tensile Stress of Reinforcement Bar			N/mm ²	184	90.70	○	91.73	○	94.72	○	94.74	○
Ultimate Load			-----	1.00	1.34	○	1.37	○	1.28	○	3.80	○

7 Calculation of Reaction Force

7.1 Reaction Force for Each Girder

<1st Span, Left>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	356.378	351.998	351.998	356.378
Cast-in-place Concrete	D2	303.009	435.973	435.973	321.709
Weight of Bridge Surface	D3	209.509	243.663	293.432	357.502
Subtotal: DT1=D1+D2+D3		868.896	1031.634	1081.403	1035.589
Live Load LT	Max	316.710	301.980	306.100	339.690
	Min	-67.890	-24.800	-24.820	-58.730
Subtotal: DT2 =DT1+LT+SW	Max	1189.412	1337.580	1391.568	1379.391
	Min	804.812	1010.800	1060.648	980.971
Creep CR		68.754	59.640	59.640	66.262
Drying Shrinkage SH		-8.047	-8.618	-8.618	-8.033
Temperature Range		20.923	22.406	22.406	20.884
Dead Load: DT1+CR+SH		929.603	1082.656	1132.425	1093.818
Total: DT2+CR +SH+T+SD	Max	1271.042	1411.008	1464.996	1458.504
	Min	886.442	1084.228	1134.076	1060.084

<1st Span, Right>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	356.380	352.000	351.999	356.380
Cast-in-place Concrete	D2	321.952	467.424	467.424	338.837
Weight of Bridge Surface	D3	367.913	428.485	515.701	621.186
Subtotal: DT1=D1+D2+D3		1046.245	1247.909	1335.124	1316.403
Live Load LT	Max	462.970	426.770	435.000	495.040
	Min	-160.300	-90.220	-91.330	-148.220
Subtotal: DT2 =DT1+LT+SW	Max	1516.242	1681.951	1777.531	1818.885
	Min	892.972	1164.961	1251.201	1175.625
Creep CR		-147.685	-125.002	-125.002	-136.973
Drying Shrinkage SH		15.361	16.215	16.215	15.406
Temperature Range		-39.940	-42.159	-42.159	-40.053
Dead Load: DT1+CR+SH		913.921	1139.122	1226.337	1194.836
Total: DT2+CR +SH+T+SD	Max	1343.978	1531.005	1626.585	1657.265
	Min	720.708	1014.015	1100.255	1014.005

<2nd Span, Left>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	356.402	352.021	352.021	356.402
Cast-in-place Concrete	D2	330.543	467.535	467.535	330.205
Weight of Bridge Surface	D3	208.731	172.455	156.446	161.447
Subtotal: DT1=D1+D2+D3		895.676	992.011	976.002	848.054
Live Load LT	Max	431.000	377.090	375.870	422.790
	Min	-174.680	-115.970	-121.660	-189.230
Subtotal: DT2 =DT1+LT+SW	Max	1331.395	1373.798	1356.476	1275.216
	Min	725.715	880.738	858.946	663.196
Creep	CR	55.740	45.717	45.717	50.249
Drying Shrinkage SH		-5.026	-5.145	-5.145	-5.100
Temperature Range		13.068	13.377	13.377	13.259
Dead Load: DT1+CR+SH		946.390	1032.583	1016.574	893.203
Total: DT2+CR +SH+T+SD	Max	1395.177	1427.747	1410.425	1333.624
	Min	789.497	934.687	912.895	721.604

<2nd Span, Right>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	356.402	352.021	352.022	356.402
Cast-in-place Concrete	D2	330.422	467.536	467.537	330.326
Weight of Bridge Surface	D3	216.080	178.635	164.071	171.691
Subtotal: DT1=D1+D2+D3		902.904	998.192	983.630	858.419
Live Load LT	Max	427.850	377.550	377.660	425.980
	Min	-164.200	-102.960	-105.710	-169.040
Subtotal: DT2 =DT1+LT+SW	Max	1335.726	1380.767	1366.271	1289.241
	Min	743.676	900.257	882.901	694.221
Creep	CR	24.471	19.657	19.657	19.209
Drying Shrinkage SH		-2.280	-2.452	-2.452	-2.286
Temperature Range		5.930	6.375	6.375	5.941
Dead Load: DT1+CR+SH		925.095	1015.397	1000.835	875.342
Total: DT2+CR +SH+T+SD	Max	1363.847	1404.347	1389.851	1312.105
	Min	771.797	923.837	906.481	717.085

<3rd Span, Left>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	356.402	352.021	352.021	356.402
Cast-in-place Concrete	D2	330.374	467.536	467.536	330.374
Weight of Bridge Surface	D3	226.325	210.799	217.120	245.773
Subtotal: DT1=D1+D2+D3		913.101	1030.356	1036.677	932.549
Live Load LT	Max	427.380	377.710	377.870	428.030
	Min	-167.570	-105.150	-105.070	-167.320
Subtotal: DT2 =DT1+LT+SW	Max	1345.362	1413.060	1419.558	1365.511
	Min	750.412	930.200	936.618	770.161
Creep	CR	20.840	19.625	19.625	22.767
Drying Shrinkage SH		-2.285	-2.454	-2.454	-2.267
Temperature Range		5.941	6.380	6.380	5.896
Dead Load: DT1+CR+SH		931.656	1047.527	1053.848	953.049
Total: DT2+CR +SH+T+SD	Max	1369.858	1436.611	1443.109	1391.907
	Min	774.908	953.751	960.169	796.557

<3rd Span, Right>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	356.402	352.021	352.021	356.402
Cast-in-place Concrete	D2	330.374	467.536	467.536	330.374
Weight of Bridge Surface	D3	210.216	191.754	195.501	221.394
Subtotal: DT1=D1+D2+D3		896.992	1011.311	1015.058	908.170
Live Load LT	Max	428.030	376.380	376.630	428.340
	Min	-184.440	-119.540	-119.650	-184.200
Subtotal: DT2 =DT1+LT+SW	Max	1329.551	1392.334	1396.341	1341.071
	Min	717.081	896.414	900.061	728.531
Creep	CR	52.290	45.705	45.705	53.560
Drying Shrinkage SH		-5.052	-5.148	-5.148	-5.048
Temperature Range		13.136	13.386	13.386	13.125
Dead Load: DT1+CR+SH		944.230	1051.868	1055.615	956.682
Total: DT2+CR +SH+T+SD	Max	1389.925	1446.277	1450.284	1402.708
	Min	777.455	950.357	954.004	790.168

<4th Span, Left>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	356.402	352.021	352.022	356.402
Cast-in-place Concrete	D2	330.374	467.536	467.536	330.374
Weight of Bridge Surface	D3	322.246	300.492	298.837	317.325
Subtotal: DT1=D1+D2+D3		1009.022	1120.049	1118.395	1004.101
Live Load LT	Max	490.230	430.920	430.810	490.240
	Min	-161.260	-90.700	-90.680	-161.470
Subtotal: DT2 =DT1+LT+SW	Max	1506.496	1558.312	1556.544	1501.571
	Min	855.006	1036.692	1035.054	849.861
Creep CR		-141.953	-124.967	-124.967	-142.512
Drying Shrinkage SH		15.367	16.219	16.219	15.365
Temperature Range		-39.953	-42.170	-42.170	-39.949
Dead Load: DT1+CR+SH		882.436	1011.301	1009.647	876.954
Total: DT2+CR +SH+T+SD	Max	1339.957	1407.394	1405.626	1334.475
	Min	688.467	885.774	884.136	682.765

<4th Span, Right>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	356.402	352.021	352.021	356.402
Cast-in-place Concrete	D2	312.133	436.082	436.082	312.133
Weight of Bridge Surface	D3	185.180	171.520	171.214	184.263
Subtotal: DT1=D1+D2+D3		853.715	959.623	959.317	852.798
Live Load LT	Max	336.330	303.790	303.130	336.350
	Min	-67.140	-24.800	-24.820	-67.180
Subtotal: DT2 =DT1+LT+SW	Max	1194.004	1267.430	1266.463	1193.104
	Min	790.534	938.840	938.513	789.574
Creep CR		67.542	59.626	59.626	67.438
Drying Shrinkage SH		-8.037	-8.618	-8.618	-8.037
Temperature Range		20.895	22.406	22.406	20.896
Dead Load: DT1+CR+SH		913.220	1010.631	1010.325	912.199
Total: DT2+CR +SH+T+SD	Max	1274.404	1340.844	1339.877	1273.401
	Min	870.934	1012.254	1011.927	869.871

7.2 Reaction Force for Pier and Abutment

Unit: kN

		1	2	3	4	5
Weight of Girder	D1	1416.752	2833.605	2833.693	2833.693	1416.846
Cast-in-place Concrete	D2	1496.664	3191.455	3191.641	3191.640	1496.430
Weight of Bridge Surface	D3	1104.106	2632.364	1630.494	2057.765	712.177
Subtotal: DT1=D1+D2+D3		4017.522	8657.424	7655.828	8083.098	3625.453
Live Load LT	Max	1025.800	1897.050	1795.390	1897.100	1025.730
	Min	-86.430	-179.840	-275.590	-194.920	-86.410
Subtotal: DT2 =DT1+LT+SW	Max	5059.271	10602.014	9490.856	10027.740	4667.131
	Min	3947.041	8525.124	7419.876	7935.720	3554.991
Creep CR		254.296	-337.239	165.851	-337.139	254.232
Drying Shrinkage SH		-33.316	42.781	-18.930	42.774	-33.310
Temperature Range		86.619	-111.230	49.218	-111.209	86.603
Dead Load: DT1+CR+SH		4238.502	8362.966	7802.749	7788.733	3846.375
Total: DT2+CR +SH+T+SD	Max	5366.870	10196.326	9686.995	9622.166	4974.656
	Min	4254.640	8119.436	7616.015	7530.146	3862.516

7.3 Horizontal Force

Horizontal Force(PF8、 PF9、 PF10fix)

(kN)

	PF8	PF9	PF10
Prestressing	-378	-12	388
Drying Shrinkage	-404	-12	415
Temperature(+)	421	13	-434
Temperature(-)	-421	-13	434
Dead Load	-781	-24	803
Temperature+15°C	-360	-11	369
Temperature-15°C	-1203	-37	1236
Temperature+40°C	342	10	-354
Temperature-40°C	-1905	-58	1959

8 Design of Cross Beam at End of Girder

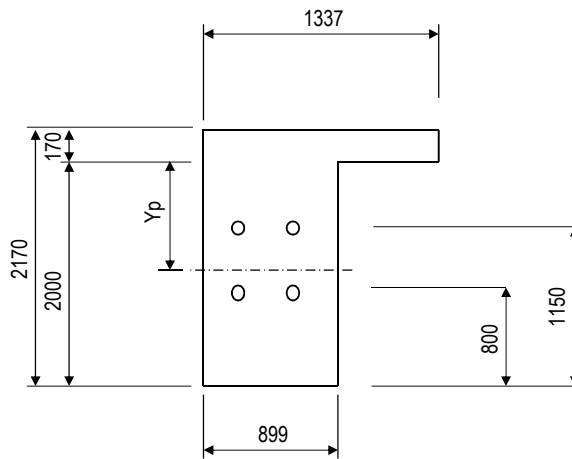
8.1 For Bending Moment

1) Calculation of Bending Moment

(kN·m)

		Bending Moment	
		max	min
Dead Load	(Md)	-68.58	-68.58
Live Load	(ML)	330.29	-211.85
Total	(M)	261.71	-280.43

2) Dimension



3) Calculation of Prestressing

Type of PC strand 4S15.2 SWPR19L

Area of PC strand 554.8 mm²

Number of PC strand 4

(N/mm²)

	Tensile Stress of PC strand	
	Allowable Value	Result
During Prestressing	1440	1250
Immediately after Prestressing	1295	1151
Under Effective Prestressing Force	1110	1058

4) Combined Flexural Stress

(N/mm²)

		Bending Moment(Max)		Bending Moment(Min)	
		Top	Bottom	Top	Bottom
Dead Load		-0.09	0.09	-0.09	0.09
Live Load		0.41	-0.44	-0.26	0.28
Prestressing		1.21	1.40	1.21	1.40
Total	Dead Load	1.12	1.49	1.12	1.49
	Live Load	1.53	1.05	0.86	1.77
Allowable Value		$0.00 \leq \sigma \leq 12.0$			


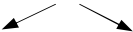
01-4-PC-I GIRDER BRIDGE
(PF14-AF2)

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END 75

1.1 DESIGN CONDITION

ROAD GRADE	:	Equivalent to CLASS 4-1
BRIDGE TYPE	:	2 span continuous PC-I girder bridge with composite deck (PC plate and RC deck)
BRIDGE LENGTH	:	L = 60.000 m
SPAN LENGTH	:	L = 28.850 + 28.800 m
WIDTH OF THE ROAD	:	TOTAL 12.750 m L = 0.500 + 5.500 + 0.750 + 5.500 + 0.500 m
HORIZONTAL ALIGNMENT	:	R=∞
LONGITUDINAL SLOPE	:	3.00 % 
SECTION SLOPE	:	2.00 % 
ANGLE OF SKEW	:	90°00'00"
PAVEMENT	:	ASPHALT PAVEMENT t= 80 mm
SLAB	:	REINFORCED CONCRETE t= 170 mm
PLATE	:	PRESTRESS CONCRETE PLATE t= 100 mm
LIVE ROAD	:	AASHTO HL=93
DESIGN STANDARD	:	AASHTO LRFD BRIDGE DESIGN 2014(LIVE ROAD) Specifications for highway bridges(Japan Road Association) 1 Common matters,3 Concrete bridges,5 seismic design (April 2012)

1.2 MATERIALS STRENGTH

1) CONCRETE

		(N/mm ²)				
		MAIN GIRDER	CROSS BEAM	RC SLAB	PC PLATE	COUPLING CONCRETE
DESIGN STANDARD STRENGTH OF CONCRETE		40.00	30.00	30.00	40.00	30.0
BENDING COMPRESSIVESTRESS	IMMEDIATELY AFTER PRESTRESSING	19.00	14.00	----	19.00	----
	OTHERS	14.00	11.00	10.00	15.00	10.00
BENDING TENSILE STRESS	IMMEDIATELY AFTER PRESTRESSING	-1.50	-1.20	----	-1.50	----
	DEAD LOAD	0.0	0.0	----	----	----
	DESIGN LOAD	-1.50	-1.20	----	0.0	----
	TEMPERATURE CHANGE	-2.00	----	----	----	----
MEAN SHEAR STRESS CONCRETE CAN CARRY		0.55	0.45	----	----	----
MAXIMUM MEAN CONCRETE SHEAR STRESS		5.30	4.00	----	----	----
ALLOWABLE DIAGONEL TENSILE STRESS (Case where shear force or torsional moment)	DEAD LOAD	-1.00	-0.80	----	----	----
	LIVE LOAD	-2.00	-1.70	----	----	----
ALLOWABLE DIAGONEL TENSILE STRESS (Case where both shear force and torsional moment)	DEAD LOAD	-1.30	-1.10	----	----	----
	LIVE LOAD	-2.50	-2.20	----	----	----

2) PC STRAND

		(N/mm ²)		
		MAIN GIRDER	CROSS BEAM	PC PLATE
PRESTRESSING STEEL TYPE		SWPR7BL 7S15.2mm	SWPR7BL 4S15.2mm	SWPR7AL 1S9.3mm
TENSILE STRENGTH		1850	1850	1700
YIELD POINT		1600	1600	1450
ALLOWABLE TENSILE STRESS	DURING PRESTRESSING	1440	1440	1305
	IMMEDIATELY AFTER PRESTRESSING	1295	1295	1190
	AT COMPOSITION OF SLAB	1110	----	----
	DESIGN LOAD	1110	1110	1020

3) REINFORCING STEEL

		(N/mm ²)			
		MAIN GIRDER	CROSS BEAM	RC SLAB	COUPLING CONCRETE
STEEL TYPE		SD345	SD345	SD345	SD345
YIELD POINT		345	345	345	345
ALLOWABLE TENSILE STRESS	DEAD LOAD	----	----	100	100
	DESIGN LOAD	180	200	140	160
	COLLISION LOAD	----	----	300	----
	WIND LOAD	----	----	175	----

1.3 DESIGN CONSTANT

1) CONCRETE

		MAIN GIRDER	CAST IN PLACE	PC PLATE
YOUNG'S MODULUS	DESIGN LOAD (N/mm ²)	3.10×10^4	2.80×10^4	3.10×10^4
	IMMEDIATELY AFTER PRESTRESSING (N/mm ²)	2.92×10^4	2.58×10^4	2.92×10^4
CREEP COEFFICIENT	NUMBER OF DAYS FOR DECK CONSTRUCTION	90	----	----
	NUMBER OF CONSTRUCTION DAYS FOR BRIDGE SURFACE	120	----	----
	DESIGN LOAD	2.60	2.60	3.00
	DURING DECK CONSTRUCTION	1.70	----	----
	BRIDGE SURFACE	1.65	----	----
DRYING SHRINKAGE OF CONCRETE	DURING DECK CONSTRUCTION	4.0×10^{-5}	----	----
	DESIGN LOAD	20.0×10^{-5}	20.0×10^{-5}	20.0×10^{-5}
UNIT WEIGHT (kN/mm ³)		24.5	24.5	24.5

2) PC STRAND(MAIN GIRDER)

		1	2
YOUNG'S MODULUS	N/mm ²	2.00×10^5	2.00×10^5
SLIP	mm	4.0	4.0
RELAXATION	%	2.5	2.5
FRICTION COEFFICIENT	1/m	0.004	0.004
	1/rad	0.300	0.300
AREA	mm ²	970.900	970.900
UNIT WEIGHT	kg/m	7.707	7.707
DIAMETER OF SHEATH	mm	60.0	60.0
DECREASE RATIO BY ANCHOR	%	0.0	0.0

3) PC STRAND(CROSS BEAM)

YOUNG'S MODULUS	N/mm ²	2.00×10^5
SLIP	mm	4.0
RELAXATION	%	2.5
FRICTION COEFFICIENT	1/m	0.004
AREA	mm ²	554.800
UNIT WEIGHT	kg/m	4.404
DIAMETER OF SHEATH	mm	45.0
DECREASE RATIO BY ANCHOR	%	0.0

4) PC STRAND(PC PLATE)

		BETWEEN MAIN GIRDERS	
YOUNG'S MODULUS		N/mm ²	2.00 × 10 ⁵
RELAXATION	BEFORE PRESTRESSING	%	1.5
	AFTER PRESTRESSING	%	1.5
	EXTRA COEFFICIENT OF HIGH TEMPERATURE	%	1.0
AREA		mm ²	51.610
UNIT WEIGHT		kg/m	0.405

1. 5 Dimension

1) Dimension of Main Girder

Girder Height : 1900.00 ~ 1900.00 mm

【Change of Web Width (mm)】

Span	End of Girder (Left Side)			End of Girder (Right Side)		
	Ending Point of Changing Web Width	Starting Point of Changing Web Width	Web Width	Ending Point of Changing Web Width	Starting Point of Changing Web Width	Web Width
1	1000.0	4000.0	700.0	4000.0	1000.0	700.0
2	1000.0	4000.0	700.0	4000.0	1000.0	700.0

2) Dimension of Cross Beam

【Interval of Cross Beam on Left Girder (m)】

Span	Number of Intermediate Cross Beams	CB1~CB2	CB2~CB3
1	1	14.925	14.925
2	1	14.900	14.900

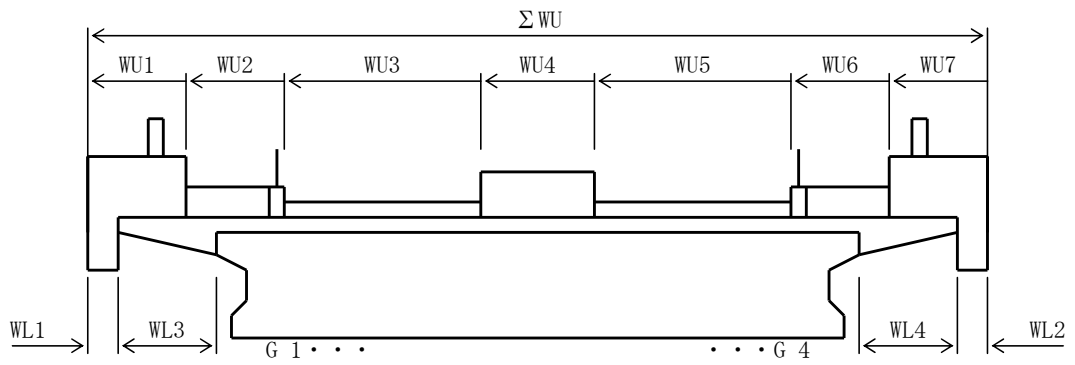
【Interval of Cross Beam on Right Girder (m)】

Span	Number of Intermediate Cross Beams	CB1~CB2	CB2~CB3
1	1	14.925	14.925
2	1	14.900	14.900

【Dimension of Cross Beam (m)】

Span	Cross Beam Width	Cross Beam Width (Left Side)	Cross Beam Width (Right Side)
1	0.300	0.900	0.950
2	0.300	0.950	0.900

【Cross Section】



【m】

	ΣWU	WU1	WU2	WU3	WU4	WU5	WU6	WU7
1	12.750	0.500	0.000	5.500	0.750	5.500	0.000	0.500
2	12.750	0.500	0.000	5.500	0.750	5.500	0.000	0.500
3	12.750	0.500	0.000	5.500	0.750	5.500	0.000	0.500

	ΣWU	WL1	WL2	WL3	WL4
1	3.500	0.000	0.000	0.475	0.475
2	3.500	0.000	0.000	0.475	0.475
3	3.500	0.000	0.000	0.475	0.475

2. 1 Load Intensity

1) Load Intensity

(1) Bridge Surface Loads

< 1 >

Load Type		Load Intensity	Load Location	
			Left End of Girder Side	Right End of Girder Side
Selfweight of Kerb	Left	8.570 kN/m	0.180 m	0.180 m
	Right	8.570 kN/m	0.180 m	0.180 m
Selfweight of Concrete Barrier	Left	0.600 kN/m	0.125 m	0.125 m
	Right	0.600 kN/m	0.125 m	0.125 m
Selfweight of Sidewalk	Left	0.000 kN/m ²		
	Right	0.000 kN/m ²		
Selfweight of Handrail	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Kerb	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Pavement	Left	3.070 kN/m ²		
	Right	3.070 kN/m ²		
Selfweight of Median		10.790 kN/m ²		
Selfweight of Additional Object	1	0.110 kN/m	0.075 m	0.075 m
	2	0.110 kN/m	12.675 m	12.675 m

< 2 >

Load Type		Load Intensity	Load Location	
			Left End of Girder Side	Right End of Girder Side
Selfweight of Kerb	Left	8.570 kN/m	0.180 m	0.180 m
	Right	8.570 kN/m	0.180 m	0.180 m
Selfweight of Concrete Barrier	Left	0.600 kN/m	0.125 m	0.125 m
	Right	0.600 kN/m	0.125 m	0.125 m
Selfweight of Sidewalk	Left	0.000 kN/m ²		
	Right	0.000 kN/m ²		
Selfweight of Handrail	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Kerb	Left	0.000 kN/m	m	m
	Right	0.000 kN/m	m	m
Selfweight of Pavement	Left	3.070 kN/m ²		
	Right	3.070 kN/m ²		
Selfweight of Median		10.790 kN/m ²		
Selfweight of Additional Object	1	0.110 kN/m	0.075 m	0.075 m
	2	0.110 kN/m	12.675 m	12.675 m

Condition of Load

Calculation of Bridge Surface Loads

(PF14-AF2)

① Unit Weight

PC · RC Concrete	$\gamma_1 = 24.5 \text{ kN/m}^3$
Concrete	$\gamma_2 = 23.0 \text{ kN/m}^3$
Asphalt Pavement	$\gamma_3 = 22.5 \text{ kN/m}^3$

② Bridge Surface Loads

- Pavement on Left Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = \frac{1}{2} \times (0.080 + 0.190) = 0.135 \text{ m}$$

(Thickness of Leveling Concrete)

$$t_c = 0.135 - 0.080 = 0.055 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.055 \times 23.0 = \underline{\underline{3.07 \text{ kN/m}^2}}$$

- Pavement on Right Lane (Asphalt Pavement $t = 80 \text{ mm}$)

(Mean Thickness)

$$t' = \frac{1}{2} \times (0.190 + 0.080) = 0.135 \text{ m}$$

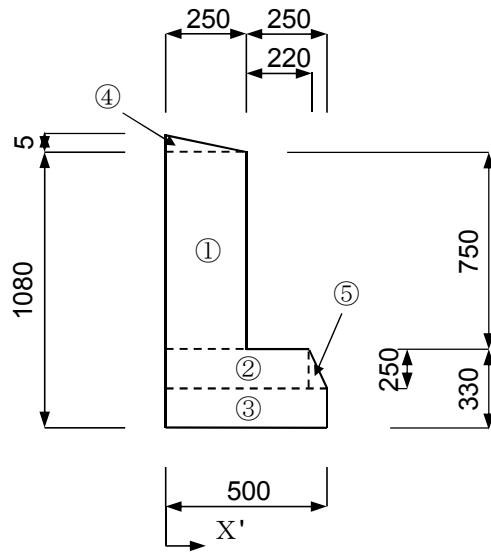
(Thickness of Leveling Concrete)

$$t_c = 0.135 - 0.080 = 0.055 \text{ m}$$

(Load Intensity)

$$q = 0.080 \times 22.5 + 0.055 \times 23.0 = \underline{\underline{3.07 \text{ kN/m}^2}}$$

• Concrete Barrier (Left Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.080	0.500	0.0400	0.250	0.01000
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3494		0.0629

Load Location

$$X' = 0.0629 / 0.3494$$

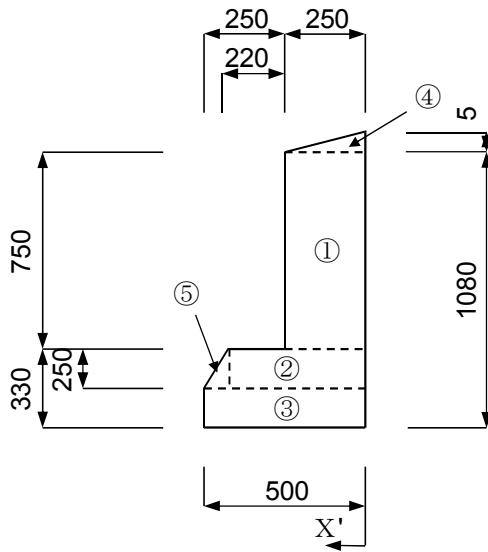
$$= \underline{0.180 \text{ m}}$$

Load Intensity

$$P = 0.3494 \times 24.5$$

$$= \underline{8.57 \text{ kN/m}}$$

• Concrete Barrier (Right Side)



a) Load Intensity and Load Location

		H	B	A	X	A×X
①	□	0.750	0.250	0.1875	0.125	0.02344
②	□	0.250	0.470	0.1175	0.235	0.02761
③	□	0.080	0.500	0.0400	0.250	0.01000
④	△	0.005	0.250	0.0006	0.083	0.00005
⑤	△	0.250	0.030	0.0038	0.480	0.00180
				0.3494		0.0629

Load Location

$$X' = 0.0629 / 0.3494$$

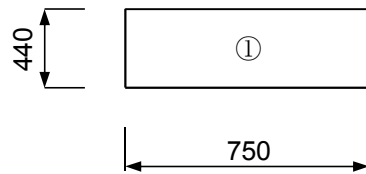
$$= \underline{0.180 \text{ m}}$$

Load Intensity

$$P = 0.3494 \times 24.5$$

$$= \underline{8.57 \text{ kN/m}}$$

• Median



a) Load Intensity and Load Location

	H	B	A
① □	0.4400	0.7500	0.3300
			0.3300

Load Location

X' = On CL

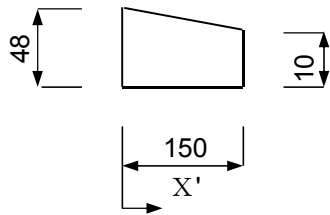
Load Intensity

$$P = 0.3300 \times 24.5 = \underline{8.09 \text{ kN/m}}$$

$$W = 8.0900 / 0.750 = \underline{10.79 \text{ kN/m}^2}$$

• Left Drain Duct

※Loaded as Selfweight of Additional Object 1



Load Location

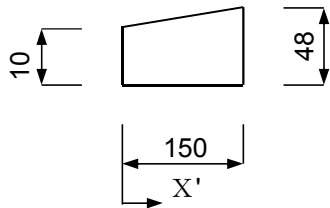
$X' = 75\text{mm}$ inside beginning of Left Kerb

Load Intensity

$$P = 1/2 \times (0.048 + 0.010) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Right Drain Duct

※Loaded as Selfweight of Additional Object 2



Load Location

$X' = 75\text{mm}$ inside beginning of Right Kerb

Load Intensity

$$P = 1/2 \times (0.010 + 0.048) \times 0.150 \times 24.5 = \underline{0.11 \text{ kN/m}}$$

• Handrail

※Loaded as Concrete Barrier

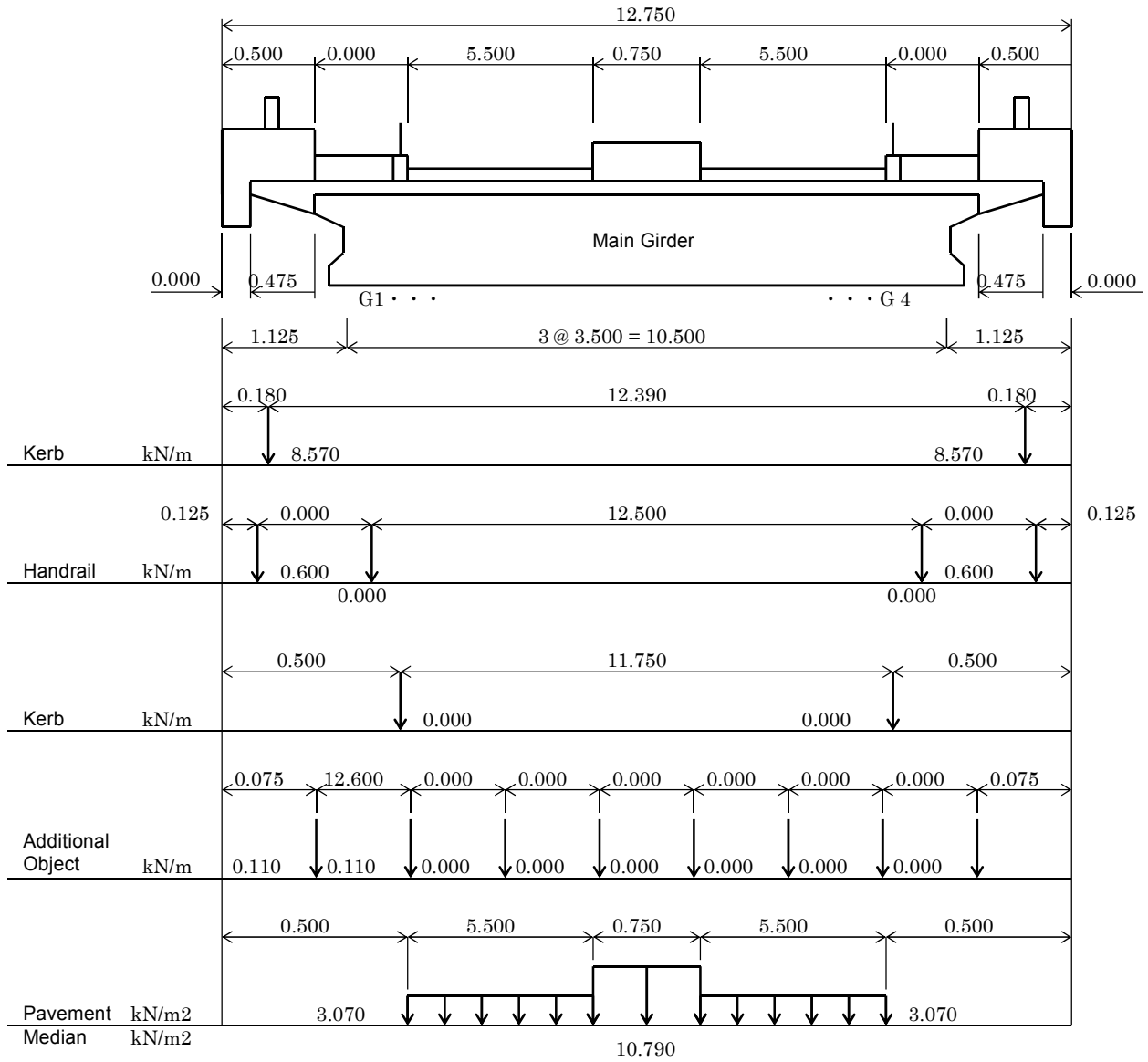
Load Location

$X' = 125\text{mm}$ inside beginning of Right and Left Kerb

Load Intensity

$$P = 0.60 = \underline{0.60 \text{ kN/m}}$$

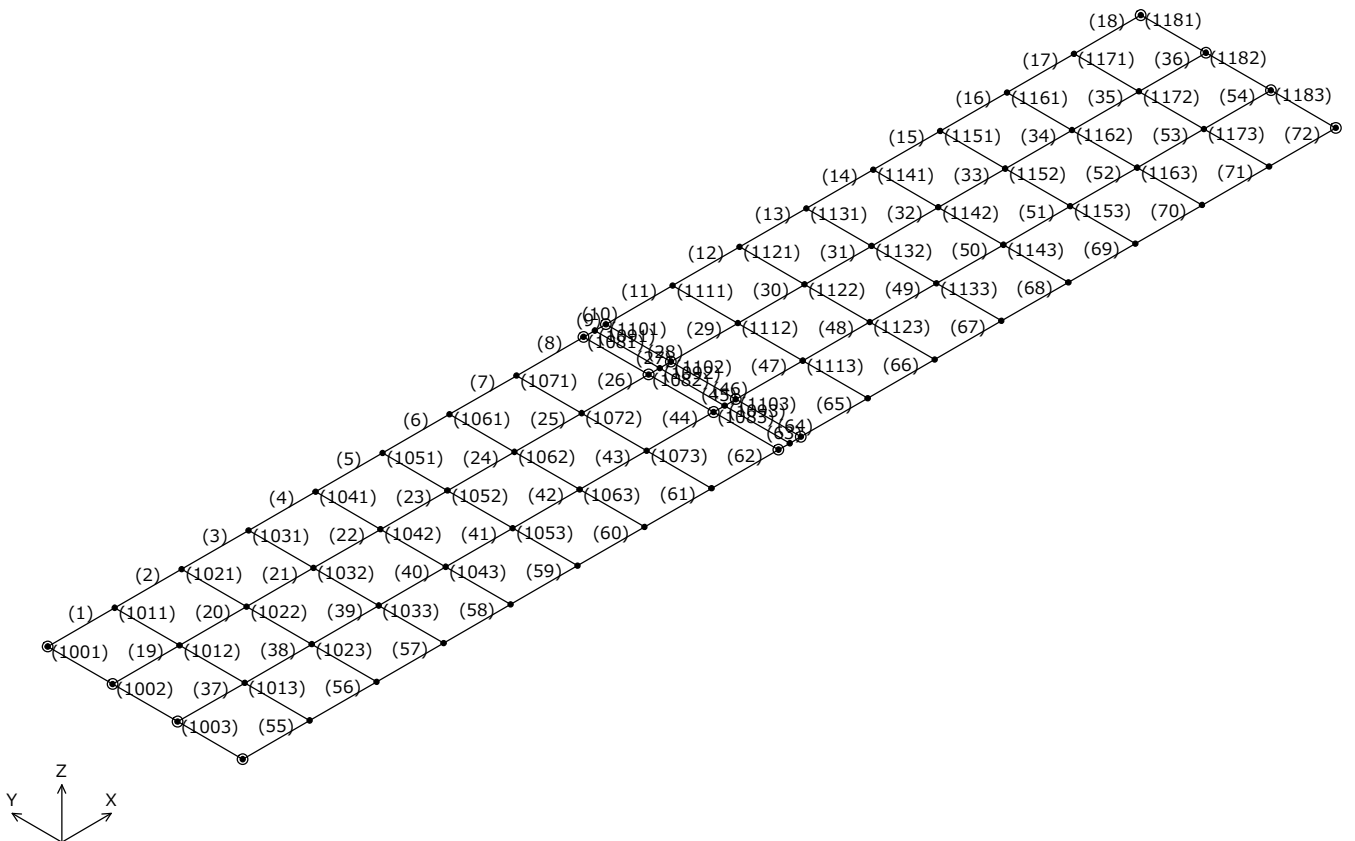
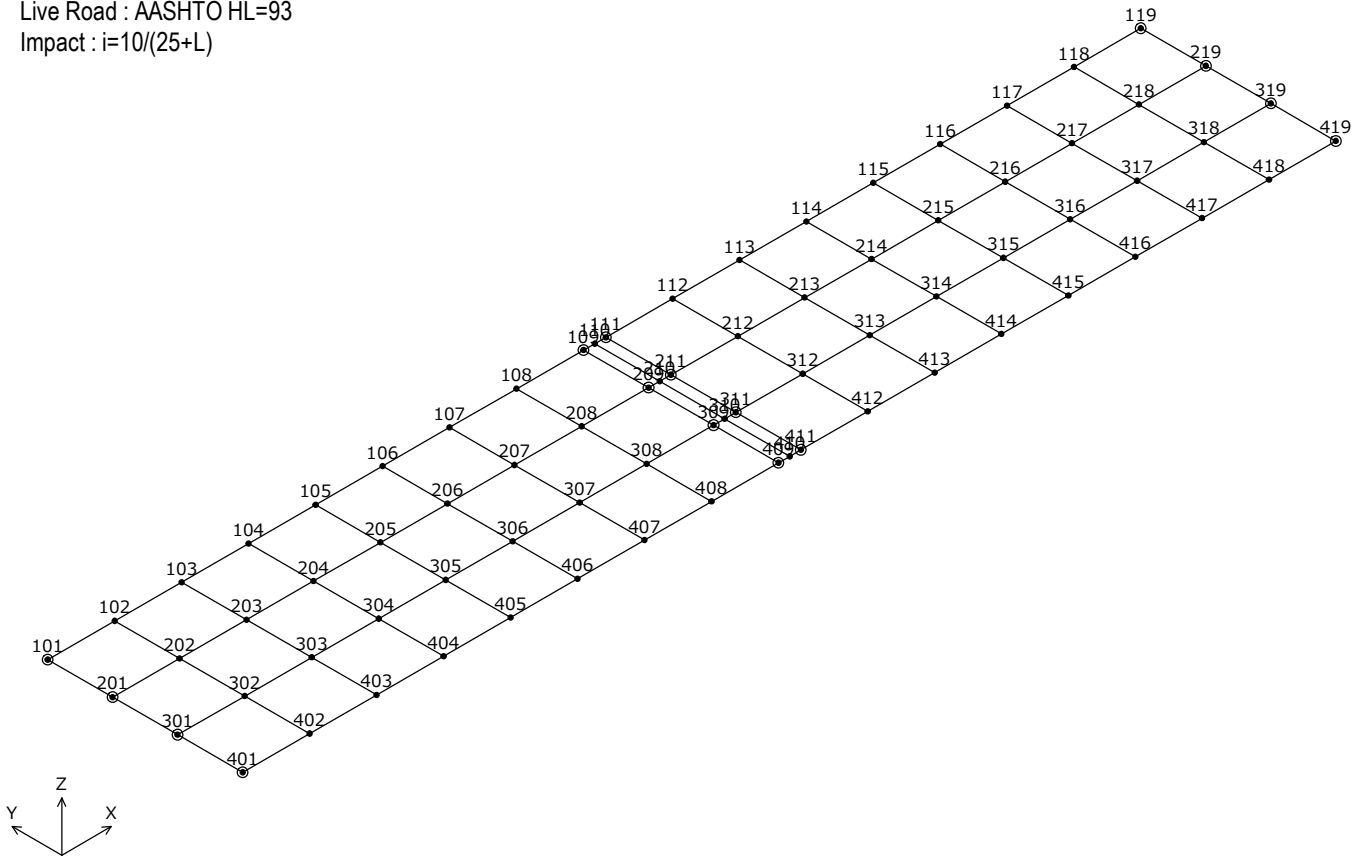
Load Intensity (Bridge Surface Loads)

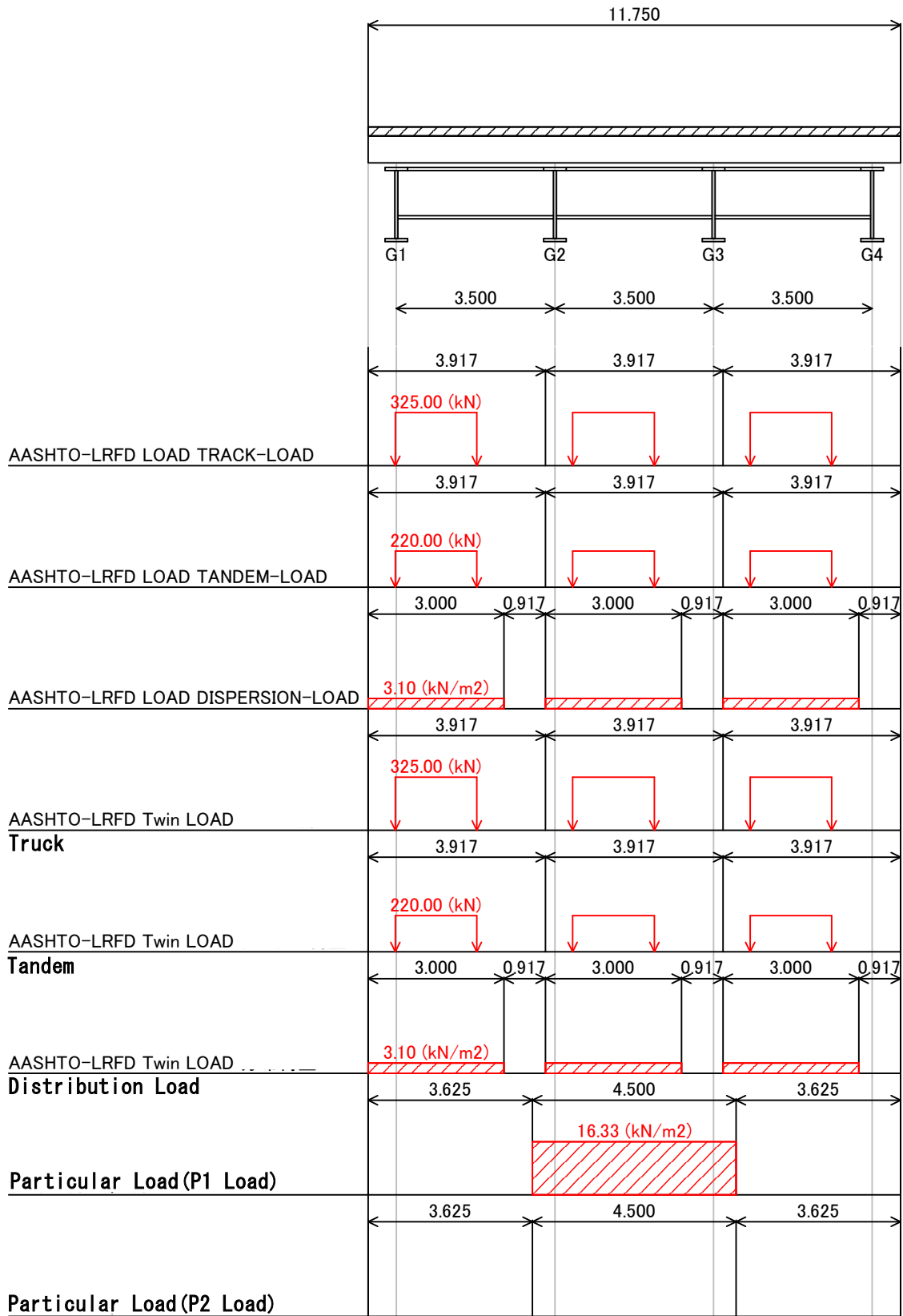


(2) Live Road

Live Road : AASHTO HL=93

Impact : $i=10/(25+L)$

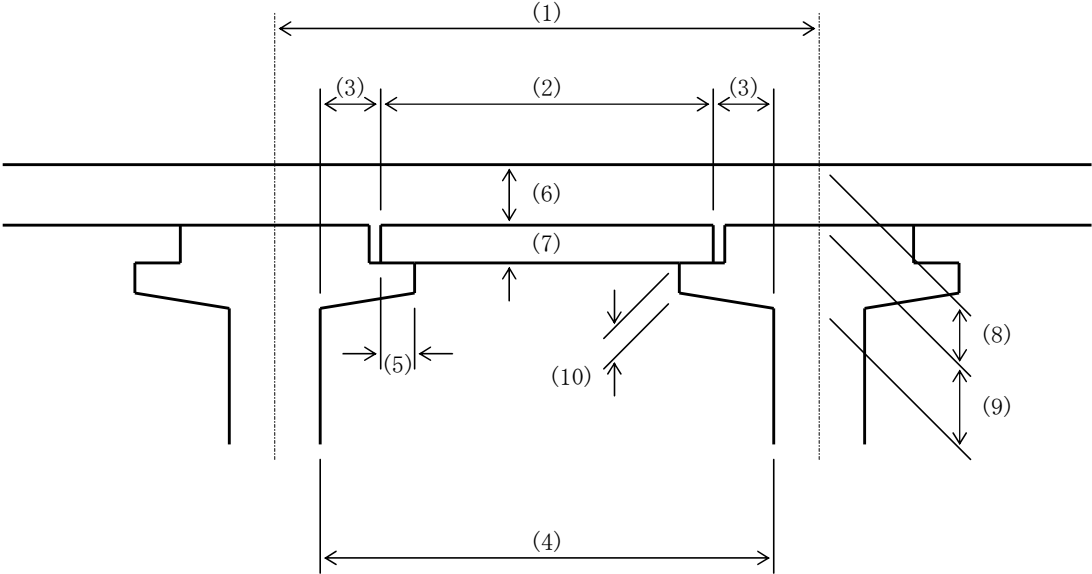




3 Design of Deck Slab

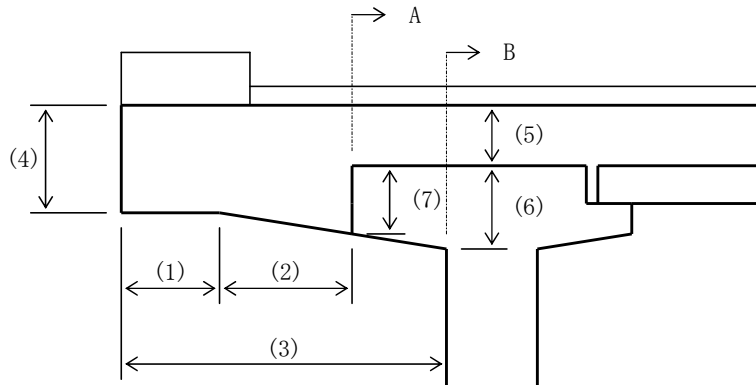
3.1 Dimension

1) Deck Slab between Girders



		1st Span	
		End of Girder	Center of Girder
(1)	m	3.500	3.500
(2)	m	2.380	2.380
(3)	m	0.210	0.450
(4)	m	2.800	3.280
(5)	m	0.090	0.090
Span Length of PC Plate		m	2.260
(6)	mm	170.0	170.0
(7)	mm	100.0	100.0
(6)+(7)	mm	270.0	270.0
(8)	mm	170.0	170.0
(9)	mm	255.6	300.0
(10)	mm	100.0	100.0

2) Deck Slab outside of Girders



			1st Span	
			End of Girder	End of Girder
Left Side	(1)	m	0.000	0.000
	(2)	m	0.475	0.475
	(3)	m	0.775	1.015
	(4)	mm	250.0	250.0
	(5)	mm	170.0	170.0
	(6)	mm	255.6	300.0
	(7)	mm	200.0	200.0
Right Side	(1)	m	0.000	0.000
	(2)	m	0.475	0.475
	(3)	m	0.775	1.015
	(4)	mm	250.0	250.0
	(5)	mm	170.0	170.0
	(6)	mm	255.6	300.0
	(7)	mm	200.0	200.0

3) Calculation of Prestressing of PC Plate

		Unit	
Name of PC Strand			1S9.3
Material of PC Strand			SWPR7AL
Area of PC Strand		mm ² /no.	51.61
Number of PC Strand		No.	15
Creep Coefficient			3.00
Drying Shrinkage of Concrete		×10 ⁻⁵	25.00
Relaxation	Before Prestressing	%	1.50
	Extra Coefficient of High Temperature	%	1.00
	After Prestressing	%	1.50
Prestressing Stress σ_{pi}		N/mm ²	1225.00
Allowable Value		N/mm ²	1305.00

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Left End of Girder Side

Deck Slab between Main Girders in Transverse Direction (PC Plate • Composite Deck Slab)

Item		Unit	Allowable Value	Result	
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5	9.17	○
	Bottom of PC Plate	N/mm ²		~19.0	8.343
	Max×0.6	N/mm ²	8.343	5.502	○
Bending stress of PC plate	Top of PC Plate	N/mm ²	0	10.584	○
	Bottom of PC Plate	N/mm ²		~15.0	3.691
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11	3.531	○
	Bottom of RC Deck	N/mm ²		-0.811	○
	Top of PC Plate	N/mm ²	0	8.345	○
	Bottom of PC Plate	N/mm ²		~15.0	1.306
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305	1225	○
	Immediately After Prestressing	N/mm ²	1190	1131.097	○
	Effective Prestressing Force	N/mm ²	1020	921.933	○
Axial stress of PC plate		N/mm ²	10	8.756	○

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.584	○	140	74.435	○	
Edge of PC Plate	Positive Moment	10	3.901	○	140	60.61	○
	Negative Moment	10	3.785	○	140	79.265	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	8.659	○	140	100.221	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	0.56	○
Tensile Stress of Reinforcement Bar	140	27.98	○

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Left End of Girder Side

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	5.392	○
	D+L	10	0.206	○	140	5.392	○
	D+L+CO	15	2.043	○	300	53.535	○
	D+L+W	12.5	0.351	○	175	9.191	○
	D+W	12.5	0.496	○	175	12.99	○
Supporting for Deck	D	-----	-----	--	100	10.212	○
	D+L	10	1.14	○	140	32.822	○
	D+L+CO	15	2.592	○	300	74.651	○
	D+L+W	12.5	1.256	○	175	36.164	○
	D+W	12.5	0.587	○	175	16.896	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	5.392	○
	D+L	10	0.206	○	140	5.392	○
	D+L+CO	15	2.043	○	300	53.535	○
	D+L+W	12.5	0.351	○	175	9.191	○
	D+W	12.5	0.496	○	175	12.99	○
Supporting for Deck	D	-----	-----	--	100	10.212	○
	D+L	10	1.14	○	140	32.822	○
	D+L+CO	15	2.592	○	300	74.651	○
	D+L+W	12.5	1.256	○	175	36.164	○
	D+W	12.5	0.587	○	175	16.896	○

Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	1.618	○	140	58.5	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	1.618	○	140	58.5	○

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Center of Span

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item		Unit	Allowable Value	Result	
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5	9.17	○
	Bottom of PC Plate	N/mm ²		~19.0	8.343
	Max×0.6	N/mm ²	8.343	5.502	○
Bending stress of PC plate	Top of PC Plate	N/mm ²	0	10.59	○
	Bottom of PC Plate	N/mm ²		~15.0	3.697
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11	4.225	○
	Bottom of RC Deck	N/mm ²		-0.97	○
	Top of PC Plate	N/mm ²	0	8.174	○
	Bottom of PC Plate	N/mm ²		~15.0	0.58
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305	1225	○
	Immediately After Prestressing	N/mm ²	1190	1131.097	○
	Effective Prestressing Force	N/mm ²	1020	922.752	○
Axial stress of PC plate		N/mm ²	10	8.756	○

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.556	○	140	78.616	○	
Edge of PC Plate	Positive Moment	10	6.711	○	140	104.266	○
	Negative Moment	10	3.267	○	140	68.414	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	9.958	○	140	115.254	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	1.002	○
Tensile Stress of Reinforcement Bar	140	55.499	○

<Design of Deck: Summary for Calculation Results of Stress>

1st Span, Center of Span

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	5.392	○
	D+L	10	0.206	○	140	5.392	○
	D+L+CO	15	2.043	○	300	53.535	○
	D+L+W	12.5	0.351	○	175	9.191	○
	D+W	12.5	0.496	○	175	12.99	○
Supporting for Deck	D	-----	-----	--	100	13.776	○
	D+L	10	2.099	○	140	64.554	○
	D+L+CO	15	3.334	○	300	102.538	○
	D+L+W	12.5	2.199	○	175	67.618	○
	D+W	12.5	0.647	○	175	19.904	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	5.392	○
	D+L	10	0.206	○	140	5.392	○
	D+L+CO	15	2.043	○	300	53.535	○
	D+L+W	12.5	0.351	○	175	9.191	○
	D+W	12.5	0.496	○	175	12.99	○
Supporting for Deck	D	-----	-----	--	100	13.776	○
	D+L	10	2.099	○	140	64.554	○
	D+L+CO	15	3.334	○	300	102.538	○
	D+L+W	12.5	2.199	○	175	67.618	○
	D+W	12.5	0.647	○	175	19.904	○

Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	2.053	○	140	74.245	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	2.053	○	140	74.245	○

<Design of Deck: Summary for Calculation Results of Stress>

2nd Span, Center of Span

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item		Unit	Allowable Value	Result	
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5	9.17	○
	Bottom of PC Plate	N/mm ²		~19.0	8.343
	Max×0.6	N/mm ²	8.343	5.502	○
Bending stress of PC plate	Top of PC Plate	N/mm ²	0	10.59	○
	Bottom of PC Plate	N/mm ²		~15.0	3.697
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11	4.225	○
	Bottom of RC Deck	N/mm ²		-0.97	○
	Top of PC Plate	N/mm ²	0	8.174	○
	Bottom of PC Plate	N/mm ²		~15.0	0.58
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305	1225	○
	Immediately After Prestressing	N/mm ²	1190	1131.097	○
	Effective Prestressing Force	N/mm ²	1020	922.752	○
Axial stress of PC plate		N/mm ²	10	8.756	○

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.556	○	140	78.616	○	
Edge of PC Plate	Positive Moment	10	6.711	○	140	104.266	○
	Negative Moment	10	3.267	○	140	68.414	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	9.958	○	140	115.254	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	1.002	○
Tensile Stress of Reinforcement Bar	140	55.499	○

<Design of Deck: Summary for Calculation Results of Stress>

2nd Span, Center of Span

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	5.392	○
	D+L	10	0.206	○	140	5.392	○
	D+L+CO	15	2.043	○	300	53.535	○
	D+L+W	12.5	0.351	○	175	9.191	○
	D+W	12.5	0.496	○	175	12.99	○
Supporting for Deck	D	-----	-----	--	100	14.115	○
	D+L	10	2.11	○	140	64.892	○
	D+L+CO	15	3.345	○	300	102.877	○
	D+L+W	12.5	2.21	○	175	67.956	○
	D+W	12.5	0.658	○	175	20.242	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	5.392	○
	D+L	10	0.206	○	140	5.392	○
	D+L+CO	15	2.043	○	300	53.535	○
	D+L+W	12.5	0.351	○	175	9.191	○
	D+W	12.5	0.496	○	175	12.99	○
Supporting for Deck	D	-----	-----	--	100	14.115	○
	D+L	10	2.11	○	140	64.892	○
	D+L+CO	15	3.345	○	300	102.877	○
	D+L+W	12.5	2.21	○	175	67.956	○
	D+W	12.5	0.658	○	175	20.242	○

Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	2.053	○	140	74.245	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	2.053	○	140	74.245	○

<Design of Deck: Summary for Calculation Results of Stress>

2nd Span, Right End of Girder Side

Deck Slab between Main Girders in Transverse Direction (PC Plate · Composite Deck Slab)

Item		Unit	Allowable Value	Result	
Immediately After Prestressing	Top of PC Plate	N/mm ²	-1.5	9.17	○
	Bottom of PC Plate	N/mm ²		~19.0	8.343
	Max×0.6	N/mm ²	8.343	5.502	○
Bending stress of PC plate	Top of PC Plate	N/mm ²	0	10.584	○
	Bottom of PC Plate	N/mm ²		~15.0	3.691
Bending stress of Composite Deck Slab	Top of RC Deck	N/mm ²	11	3.531	○
	Bottom of RC Deck	N/mm ²		-0.811	○
	Top of PC Plate	N/mm ²	0	8.345	○
	Bottom of PC Plate	N/mm ²		~15.0	1.306
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1305	1225	○
	Immediately After Prestressing	N/mm ²	1190	1131.097	○
	Effective Prestressing Force	N/mm ²	1020	921.933	○
Axial stress of PC plate		N/mm ²	10	8.756	○

Deck Slab between Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar			
	Allowable Value	Result		Allowable Value	Result		
Supporting for Deck	10	2.584	○	140	74.435	○	
Edge of PC Plate	Positive Moment	10	3.901	○	140	60.61	○
	Negative Moment	10	3.785	○	140	79.265	○

Deck Slab between Main Girders in Longitudinal Direction (RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Center of RC Deck	10	8.659	○	140	100.221	○

Upper Flange (During Deck Construction)

Item (N/mm ²)	Allowable Value	Result	
Mean Shear Stress	0.55	0.12	○
Bending Stress of Concrete	10	0.56	○
Tensile Stress of Reinforcement Bar	140	27.98	○

<Design of Deck: Summary for Calculation Results of Stress>

2nd Span, Right End of Girder Side

Deck Slab outside of Main Girder in Transverse Direction (RC Deck)

Item (N/mm ²)		Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
		Allowable Value	Result		Allowable Value	Result	
Deck Slab outside of Main Girder (Left Side)							
Edge of Upper Flange	D	-----	-----	--	100	5.392	○
	D+L	10	0.206	○	140	5.392	○
	D+L+CO	15	2.043	○	300	53.535	○
	D+L+W	12.5	0.351	○	175	9.191	○
	D+W	12.5	0.496	○	175	12.99	○
Supporting for Deck	D	-----	-----	--	100	10.212	○
	D+L	10	1.14	○	140	32.822	○
	D+L+CO	15	2.592	○	300	74.651	○
	D+L+W	12.5	1.256	○	175	36.164	○
	D+W	12.5	0.587	○	175	16.896	○
Deck Slab outside of Main Girder (Right Side)							
Edge of Upper Flange	D	-----	-----	--	100	5.392	○
	D+L	10	0.206	○	140	5.392	○
	D+L+CO	15	2.043	○	300	53.535	○
	D+L+W	12.5	0.351	○	175	9.191	○
	D+W	12.5	0.496	○	175	12.99	○
Supporting for Deck	D	-----	-----	--	100	10.212	○
	D+L	10	1.14	○	140	32.822	○
	D+L+CO	15	2.592	○	300	74.651	○
	D+L+W	12.5	1.256	○	175	36.164	○
	D+W	12.5	0.587	○	175	16.896	○

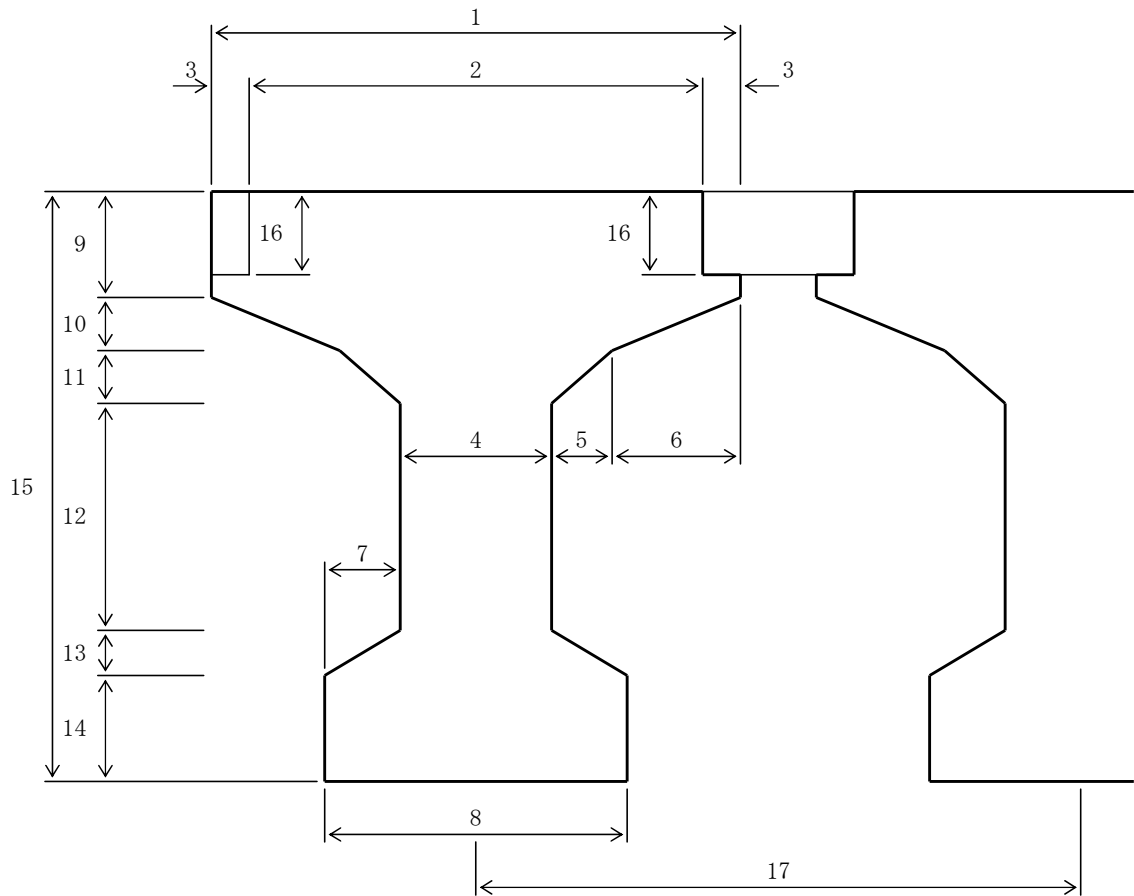
Deck Slab outside of Main Girder in Longitudinal Direction(RC Deck)

Item (N/mm ²)	Bending Stress of Concrete			Tensile Stress of Reinforcement Bar		
	Allowable Value	Result		Allowable Value	Result	
Edge of Upper Flange (Left Side)	10	0	○	140	0	○
Supporting for Deck (Left Side)	10	1.618	○	140	58.5	○
Edge of Upper Flange (Right Side)	10	0	○	140	0	○
Supporting for Deck (Right Side)	10	1.618	○	140	58.5	○

4 Design of Main Girder

4.1 Dimension and PC Strand Arrangement

1) Dimension



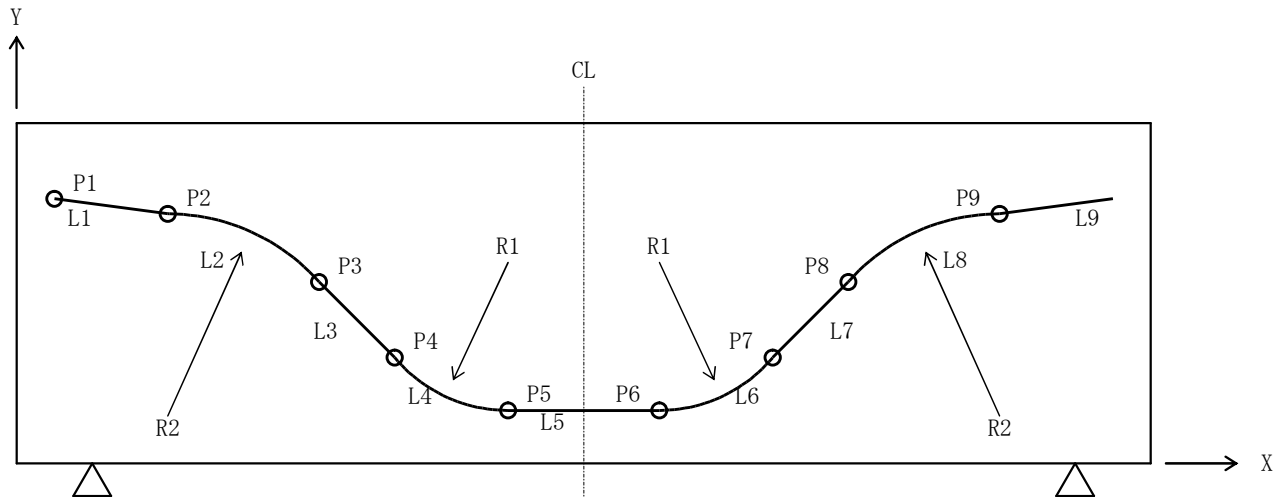
(Unit: mm)

	1st Span			2nd Span		
	End of Girder (Left)	Center Span	End of Girder (Right)	End of Girder (Left)	Center Span	End of Girder (Right)
1	1300.0	1300.0	1300.0	1300.0	1300.0	1300.0
2	1060.0	1060.0	1060.0	1060.0	1060.0	1060.0
3	120.0	120.0	120.0	120.0	120.0	120.0
4	700.0	220.0	700.0	700.0	220.0	700.0
5	0.0	0.0	0.0	0.0	0.0	0.0
6	300.0	540.0	300.0	300.0	540.0	300.0
7	0.0	240.0	0.0	0.0	240.0	0.0
8	700.0	700.0	700.0	700.0	700.0	700.0
9	200.0	200.0	200.0	200.0	200.0	200.0
10	55.6	100.0	55.6	55.6	100.0	55.6
11	0.0	0.0	0.0	0.0	0.0	0.0
12	1444.4	1150.0	1444.4	1444.4	1150.0	1444.4
13	0.0	250.0	0.0	0.0	250.0	0.0
14	200.0	200.0	200.0	200.0	200.0	200.0
15	1900.0	1900.0	1900.0	1900.0	1900.0	1900.0
16	100.0	100.0	100.0	100.0	100.0	100.0
17	3500.0	3500.0	3500.0	3500.0	3500.0	3500.0

2) PC Strand Arrangement

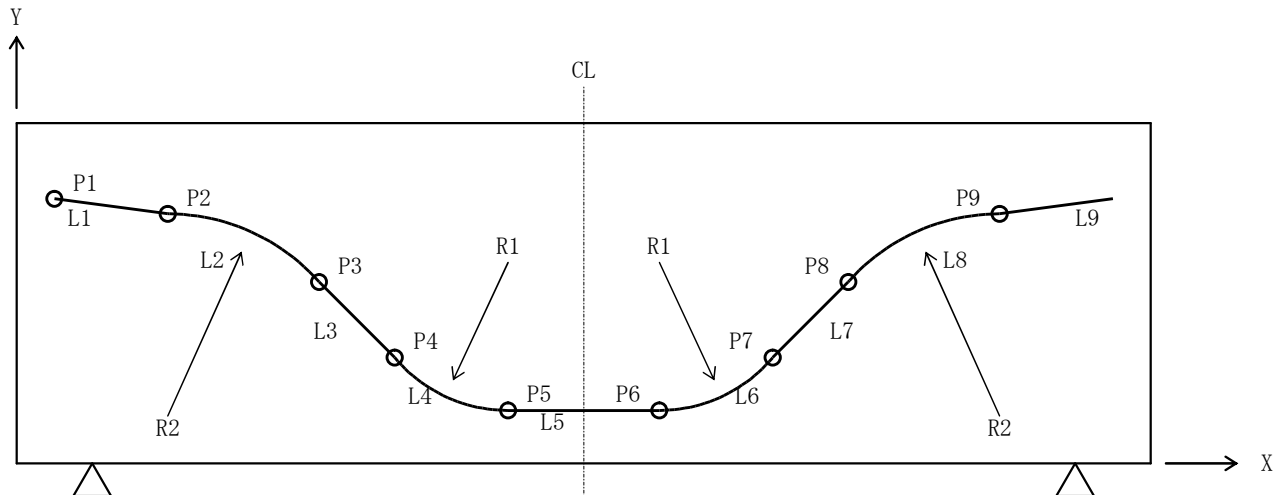
<1st Span>

PC Strand No.		1	2	3	4	5
Number of PC Strand		1	1	1	1	1
Coordinate (mm)	P1 X	-----	-----	-----	-----	-----
	Y	-----	-----	-----	-----	-----
	P2 X	-----	-----	-----	-----	-----
	Y	-----	-----	-----	-----	-----
	P3 X	200.0	200.0	200.0	200.0	200.0
	Y	1650.0	1300.0	950.0	600.0	250.0
	P4 X	13119.0	10730.4	8341.8	4706.9	1710.7
	Y	406.0	286.0	166.0	166.0	144.4
	P5 X	14077.5	11688.9	9300.2	5665.3	2408.3
	Y	360.0	240.0	120.0	120.0	120.0
P6 X	16120.5	17993.7	19866.9	22717.5	25539.2	
Y	360.0	240.0	120.0	120.0	120.0	
P7 X	17339.2	19212.4	21085.6	23936.2	26497.7	
Y	434.5	314.5	194.5	194.5	166.0	
P8 X	26631.3	26631.3	26631.3	26631.3	26891.5	
Y	1575.5	1225.5	875.5	525.5	204.0	
P9 X	27850.0	27850.0	27850.0	27850.0	27850.0	
Y	1650.0	1300.0	950.0	600.0	250.0	
P1 [~] X	29650.0	29650.0	29650.0	29650.0	29650.0	
Y	1650.0	1300.0	950.0	600.0	250.0	
Angle	α (L) (R)	5°30'0" 0°0'0"	5°30'0" 0°0'0"	5°30'0" 0°0'0"	5°30'0" 0°0'0"	4°0'0" 0°0'0"
Radius (m)	R2 (L)	-----	-----	-----	-----	-----
	R1 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (R)	10.000	10.000	10.000	10.000	10.000
	R2 (R)	10.000	10.000	10.000	10.000	10.000
Angle	β (L) (R)	----- 7°0'0"	----- 7°0'0"	----- 7°0'0"	----- 7°0'0"	----- 5°30'0"
Length of PC Strand (m)	L1	-----	-----	-----	-----	-----
	L2	-----	-----	-----	-----	-----
	L3	12.979	10.579	8.179	4.528	1.514
	L4	0.960	0.960	0.960	0.960	0.698
	L5	2.043	6.305	10.567	17.052	23.131
	L6	1.222	1.222	1.222	1.222	0.960
	L7	9.362	7.475	5.587	2.715	0.396
	L8	1.222	1.222	1.222	1.222	0.960
	L9	1.800	1.800	1.800	1.800	1.800
	Total	29.587	29.562	29.537	29.499	29.459



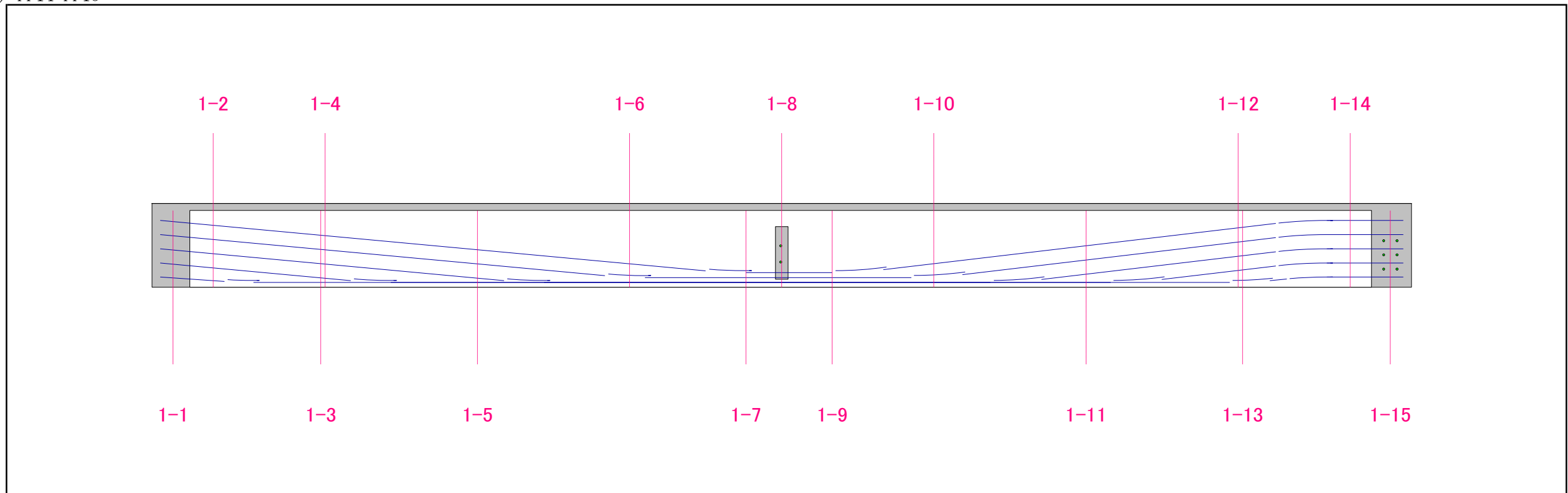
<2nd Span>

PC Strand No.		1	2	3	4	5
Number of PC Strand		1	1	1	1	1
Coordinate (mm)	P1 X	200.0	200.0	200.0	200.0	200.0
	Y	1650.0	1300.0	950.0	600.0	250.0
	P2 X	2000.0	2000.0	2000.0	2000.0	2000.0
	Y	1650.0	1300.0	950.0	600.0	250.0
	P3 X	3218.7	3218.7	3218.7	3218.7	2958.5
	Y	1575.5	1225.5	875.5	525.5	204.0
	P4 X	12510.8	10637.6	8764.4	5913.8	3352.3
	Y	434.5	314.5	194.5	194.5	166.0
	P5 X	13729.5	11856.3	9983.1	7132.5	4310.8
	Y	360.0	240.0	120.0	120.0	120.0
P6 X	15722.5	18111.1	20499.8	24134.7	27391.7	
Y	360.0	240.0	120.0	120.0	120.0	
P7 X	16681.0	19069.6	21458.2	25093.1	28089.3	
Y	406.0	286.0	166.0	166.0	144.4	
P8 X	29600.0	29600.0	29600.0	29600.0	29600.0	
Y	1650.0	1300.0	950.0	600.0	250.0	
P9 X	-----	-----	-----	-----	-----	
Y	-----	-----	-----	-----	-----	
P10 X	-----	-----	-----	-----	-----	
Y	-----	-----	-----	-----	-----	
Angle	α (L)	0°0'0"	0°0'0"	0°0'0"	0°0'0"	0°0'0"
	(R)	5°30'0"	5°30'0"	5°30'0"	5°30'0"	4°0'0"
Radius (m)	R2 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (L)	10.000	10.000	10.000	10.000	10.000
	R1 (R)	10.000	10.000	10.000	10.000	10.000
	R2 (R)	-----	-----	-----	-----	-----
Angle	β (L)	7°0'0"	7°0'0"	7°0'0"	7°0'0"	5°30'0"
	(R)	-----	-----	-----	-----	-----
Length of PC Strand (m)	L1	1.800	1.800	1.800	1.800	1.800
	L2	1.222	1.222	1.222	1.222	0.960
	L3	9.362	7.475	5.587	2.715	0.396
	L4	1.222	1.222	1.222	1.222	0.960
	L5	1.993	6.255	10.517	17.002	23.081
	L6	0.960	0.960	0.960	0.960	0.698
	L7	12.979	10.579	8.179	4.528	1.514
	L8	-----	-----	-----	-----	-----
	L9	-----	-----	-----	-----	-----
	Total		29.537	29.512	29.487	29.449



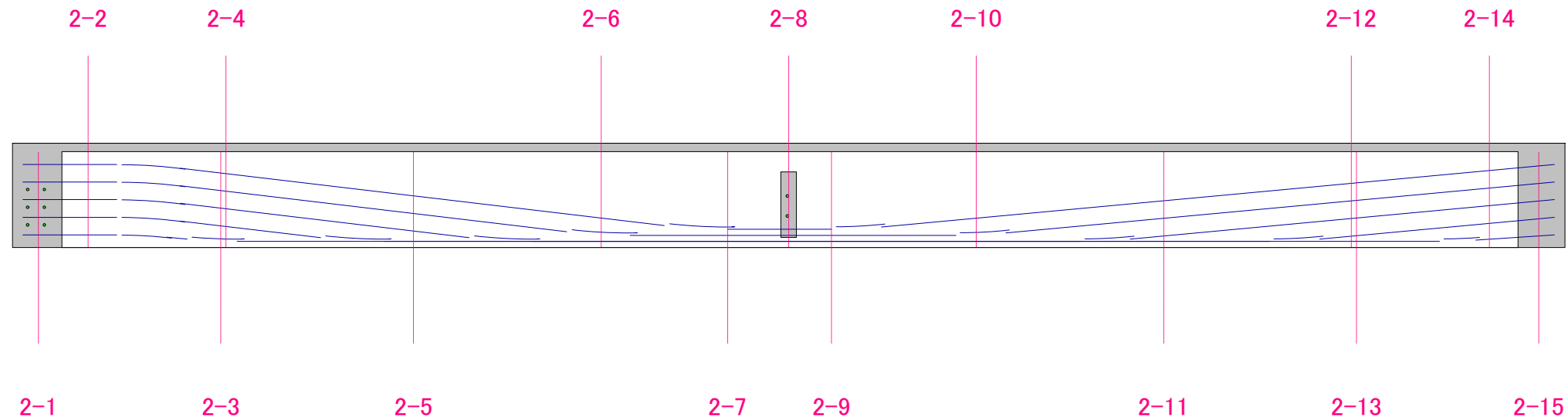
4.4 Summary for Calculation Results of Stress

1) PF14-PF15



		Unit	Allowable Value	Cross Section Number		
Calculation for Bending Moment				[1- 7]	[1- 8]	[1- 9]
				Bent up Point (Left)	Center of Span	Bent up Point (Right)
Bending Stress of Concrete						
Immediately After Prestressing	N/mm ²	-1.5~19.00	Top of Main Girder	0.80	0.84	0.82
			Bottom of Main Girder	14.80	14.70	14.65
During Deck Construction	"	-1.5~14.00	Top of Main Girder	6.31	6.36	6.29
			Bottom of Main Girder	6.85	6.74	6.76
Dead Load	"	≤10.00	Top of Deck	2.75	2.78	2.75
		0~14.00	Top of Main Girder	5.25	5.29	5.24
			Bottom of Main Girder	3.03	2.89	2.91
Design Load	"	≤10.00	Top of Deck max	4.25	4.26	4.17
			Top of Deck min	2.39	2.40	2.34
			-1.5~14.00	Top of Main Girder(max)	6.48	6.51
		Bottom of Main Girder(max)		-0.46	-0.54	-0.41
				Top of Main Girder(min)	4.95	4.98
		Bottom of Main Girder(min)	3.86	3.77	3.86	
Stress of PC Strand	N/mm ²	P _{max} ≤ 1110		1037	1034	1025
Ultimate Load	-----	F ≥ 1.0		1.19	1.19	1.21
Calculation for Shear Force				[1- 2]	[1- 3]	[1-14]
				Near a Support of girder (Left)	Change point of Web Width (Left)	Near a Support of girder (Right)
Shear Stress of Design Load	kN			0.55	1.28	1.04
Compressive Strength to Failure	-----	F ≥ 1.0		3.88	1.83	3.04
Diagonal Tensile Stress	Dead Load	N/mm ²	≧ -1	-0.04	-0.12	-0.24
	Design Load	"	≧ -2	-0.17	-0.49	-0.44

2) PF15-AF2



		Unit	Allowable Value	Cross Section Number		
Calculation for Bending Moment				[2- 7]	[2- 8]	[2- 9]
				Bent up Point(Left)	Center of Span	Bent up Point(Right)
Bending Stress of Concrete						
Immediately After Prestressing	N/mm ²	-1.5 ~ 19.00	Top of Main Girder	0.80	0.82	0.79
			Bottom of Main Girder	14.68	14.73	14.82
During Deck Construction	"	-1.5 ~ 14.00	Top of Main Girder	6.26	6.33	6.28
			Bottom of Main Girder	6.80	6.78	6.89
Dead Load	"	≤ 10.00	Top of Deck	2.74	2.77	2.74
		0 ~ 14.00	Top of Main Girder	5.22	5.27	5.23
			Bottom of Main Girder	2.94	2.93	3.06
Design Load	"	≤ 10.00	Top of Deck max	4.16	4.24	4.23
			Top of Deck min	2.33	2.39	2.38
		-1.5 ~ 14.00	Top of Main Girder(max)	6.40	6.48	6.46
			Bottom of Main Girder(max)	-0.37	-0.49	-0.42
			Top of Main Girder(min)	4.88	4.96	4.93
		Bottom of Main Girder(min)	3.90	3.82	3.90	
Stress of PC Strand	N/mm ²	P _{max} ≤ 1110		1025	1033	1037
Ultimate Load	----	F ≥ 1.0		1.22	1.19	1.19
Calculation for Shear Force				[2- 2]	[2-13]	[2-14]
				Near a Support of girder(Left)	Change point of Web Width(Right)	Near a Support of girder(Right)
Shear Stress of Design Load	kN			1.03	1.27	0.55
Compressive Strength to Failure	----	F ≥ 1.0		3.05	1.83	3.88
Diagonal Tensile Stress	Dead Load	N/mm ²	≥ -1	-0.24	-0.11	-0.04
	Design Load	"	≥ -2	-0.44	-0.49	-0.17

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1- 1]		[1- 2]		[1- 3]		
Interval from beginning of Girder		-----	0.500		1.450		4.000		
Immediately After Prestressing	Top of Main Girder	-1.5	2.923	○	2.734	○	3.749	○	
	Bottom of Main Girder	~19.00	4.995	○	5.910	○	10.946	○	
During Deck Construction	Top of Main Girder	-1.5	2.773	○	3.170	○	5.786	○	
	Bottom of Main Girder	~14.00	4.738	○	4.919	○	7.383	○	
Dead Load	Top of Deck	≤10.00	0.268	○	0.548	○	1.386	○	
	Top of Main Girder	0	2.087	○	2.460	○	4.298	○	
	Bottom of Main Girder	~14.00	4.704	○	4.588	○	5.706	○	
Design Load1	Top of Deck	Max	0.268	○	0.820	○	2.269	○	
		Min	0.268	○	0.523	○	1.293	○	
	Top of Main Girder	Max	2.087	○	2.695	○	5.024	○	
		Min	-1.5	2.087	○	2.438	○	4.221	○
	Bottom of Main Girder	Max	~14.00	4.704	○	4.087	○	3.626	○
		Min	4.704	○	4.634	○	5.926	○	
Design Load2 Temperature Rise	Top of Deck	Max	0.787	○	1.345	○	2.772	○	
		Min	≤11.50	0.787	○	1.048	○	1.796	○
	Top of Main Girder	Max	1.231	○	1.842	○	4.131	○	
		Min	-2	1.231	○	1.585	○	3.327	○
	Bottom of Main Girder	Max	~16.10	5.179	○	4.524	○	3.841	○
		Min	5.179	○	5.071	○	6.141	○	
Design Load3 Temperature Drop	Top of Deck	Max	0.787	○	1.345	○	2.772	○	
		Min	≤11.50	0.787	○	1.048	○	1.796	○
	Top of Main Girder	Max	1.231	○	1.842	○	4.131	○	
		Min	-2	1.231	○	1.585	○	3.327	○
	Bottom of Main Girder	Max	~16.10	5.179	○	4.524	○	3.841	○
		Min	5.179	○	5.071	○	6.141	○	
Design Load4 Support sinking	Top of Deck	Max	0.268	○	0.820	○	2.269	○	
		Min	≤10.00	0.268	○	0.523	○	1.293	○
	Top of Main Girder	Max	2.087	○	2.695	○	5.024	○	
		Min	-1.5	2.087	○	2.438	○	4.221	○
	Bottom of Main Girder	Max	~14.00	4.704	○	4.087	○	3.626	○
		Min	4.704	○	4.634	○	5.926	○	
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	0.787	○	1.345	○	2.772	○	
		Min	≤11.50	0.787	○	1.048	○	1.796	○
	Top of Main Girder	Max	1.231	○	1.842	○	4.131	○	
		Min	-2	1.231	○	1.585	○	3.327	○
	Bottom of Main Girder	Max	~16.10	5.179	○	4.524	○	3.841	○
		Min	5.179	○	5.071	○	6.141	○	
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	0.787	○	1.345	○	2.772	○	
		Min	≤11.50	0.787	○	1.048	○	1.796	○
	Top of Main Girder	Max	1.231	○	1.842	○	4.131	○	
		Min	-2	1.231	○	1.585	○	3.327	○
	Bottom of Main Girder	Max	~16.10	5.179	○	4.524	○	3.841	○
		Min	5.179	○	5.071	○	6.141	○	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1- 4]		[1- 5]		[1- 6]		
Interval from beginning of Girder		-----	4.106		7.713		11.319		
Immediately After Prestressing	Top of Main Girder	-1.5	3.698	○	2.217	○	1.035	○	
	Bottom of Main Girder	~19.00	11.015	○	13.164	○	14.759	○	
During Deck Construction	Top of Main Girder	-1.5	5.799	○	6.133	○	6.119	○	
	Bottom of Main Girder	~14.00	7.372	○	7.219	○	7.313	○	
Dead Load	Top of Deck	≤10.00	1.409	○	2.077	○	2.499	○	
	Top of Main Girder	0	4.318	○	4.843	○	5.032	○	
	Bottom of Main Girder	~14.00	5.658	○	4.445	○	3.781	○	
Design Load1	Top of Deck	Max	2.313	○	3.456	○	4.020	○	
		Min	1.313	○	1.886	○	2.214	○	
	Top of Main Girder	Max	5.061	○	5.979	○	6.287	○	
		Min	-1.5	4.238	○	4.685	○	4.797	○
	Bottom of Main Girder	Max	~14.00	3.530	○	1.217	○	0.235	○
		Min	5.885	○	4.892	○	4.444	○	
Design Load2 Temperature Rise	Top of Deck	Max	2.818	○	4.038	○	4.676	○	
		Min	≤11.50	1.819	○	2.467	○	2.870	○
	Top of Main Girder	Max	4.169	○	5.150	○	5.520	○	
		Min	-2	3.347	○	3.856	○	4.030	○
	Bottom of Main Girder	Max	~16.10	3.740	○	1.250	○	0.095	○
		Min	6.094	○	4.926	○	4.304	○	
Design Load3 Temperature Drop	Top of Deck	Max	2.818	○	4.038	○	4.676	○	
		Min	≤11.50	1.819	○	2.467	○	2.870	○
	Top of Main Girder	Max	4.169	○	5.150	○	5.520	○	
		Min	-2	3.347	○	3.856	○	4.030	○
	Bottom of Main Girder	Max	~16.10	3.740	○	1.250	○	0.095	○
		Min	6.094	○	4.926	○	4.304	○	
Design Load4 Support sinking	Top of Deck	Max	2.313	○	3.456	○	4.020	○	
		Min	≤10.00	1.313	○	1.886	○	2.214	○
	Top of Main Girder	Max	5.061	○	5.979	○	6.287	○	
		Min	-1.5	4.238	○	4.685	○	4.797	○
	Bottom of Main Girder	Max	~14.00	3.530	○	1.217	○	0.235	○
		Min	5.885	○	4.892	○	4.444	○	
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	2.818	○	4.038	○	4.676	○	
		Min	≤11.50	1.819	○	2.467	○	2.870	○
	Top of Main Girder	Max	4.169	○	5.150	○	5.520	○	
		Min	-2	3.347	○	3.856	○	4.030	○
	Bottom of Main Girder	Max	~16.10	3.740	○	1.250	○	0.095	○
		Min	6.094	○	4.926	○	4.304	○	
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	2.818	○	4.038	○	4.676	○	
		Min	≤11.50	1.819	○	2.467	○	2.870	○
	Top of Main Girder	Max	4.169	○	5.150	○	5.520	○	
		Min	-2	3.347	○	3.856	○	4.030	○
	Bottom of Main Girder	Max	~16.10	3.740	○	1.250	○	0.095	○
		Min	6.094	○	4.926	○	4.304	○	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1- 7]		[1- 8]		[1- 9]		
Interval from beginning of Girder		-----	14.078		14.925		16.121		
Immediately After Prestressing	Top of Main Girder	-1.5	0.803	○	0.836	○	0.816	○	
	Bottom of Main Girder	~19.00	14.798	○	14.704	○	14.653	○	
During Deck Construction	Top of Main Girder	-1.5	6.307	○	6.363	○	6.289	○	
	Bottom of Main Girder	~14.00	6.853	○	6.738	○	6.756	○	
Dead Load	Top of Deck	≤10.00	2.750	○	2.783	○	2.747	○	
	Top of Main Girder	0	5.245	○	5.292	○	5.241	○	
	Bottom of Main Girder	~14.00	3.028	○	2.888	○	2.908	○	
Design Load1	Top of Deck	Max	4.248	○	4.255	○	4.172	○	
		Min	2.392	○	2.402	○	2.337	○	
	Top of Main Girder	Max	6.481	○	6.507	○	6.416	○	
		Min	-1.5	4.950	○	4.979	○	4.902	○
	Bottom of Main Girder	Max	~14.00	-0.458	○	-0.539	○	-0.408	○
		Min		3.861	○	3.773	○	3.863	○
Design Load2 Temperature Rise	Top of Deck	Max	4.961	○	4.987	○	4.928	○	
		Min	≤11.50	3.105	○	3.134	○	3.093	○
	Top of Main Girder	Max	5.761	○	5.802	○	5.732	○	
		Min	-2	4.230	○	4.274	○	4.218	○
	Bottom of Main Girder	Max	~16.10	-0.731	○	-0.854	○	-0.780	○
		Min		3.588	○	3.458	○	3.490	○
Design Load3 Temperature Drop	Top of Deck	Max	4.961	○	4.987	○	4.928	○	
		Min	≤11.50	3.105	○	3.134	○	3.093	○
	Top of Main Girder	Max	5.761	○	5.802	○	5.732	○	
		Min	-2	4.230	○	4.274	○	4.218	○
	Bottom of Main Girder	Max	~16.10	-0.731	○	-0.854	○	-0.780	○
		Min		3.588	○	3.458	○	3.490	○
Design Load4 Support sinking	Top of Deck	Max	4.248	○	4.255	○	4.172	○	
		Min	≤10.00	2.392	○	2.402	○	2.337	○
	Top of Main Girder	Max	6.481	○	6.507	○	6.416	○	
		Min	-1.5	4.950	○	4.979	○	4.902	○
	Bottom of Main Girder	Max	~14.00	-0.458	○	-0.539	○	-0.408	○
		Min		3.861	○	3.773	○	3.863	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	4.961	○	4.987	○	4.928	○	
		Min	≤11.50	3.105	○	3.134	○	3.093	○
	Top of Main Girder	Max	5.761	○	5.802	○	5.732	○	
		Min	-2	4.230	○	4.274	○	4.218	○
	Bottom of Main Girder	Max	~16.10	-0.731	○	-0.854	○	-0.780	○
		Min		3.588	○	3.458	○	3.490	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	4.961	○	4.987	○	4.928	○	
		Min	≤11.50	3.105	○	3.134	○	3.093	○
	Top of Main Girder	Max	5.761	○	5.802	○	5.732	○	
		Min	-2	4.230	○	4.274	○	4.218	○
	Bottom of Main Girder	Max	~16.10	-0.731	○	-0.854	○	-0.780	○
		Min		3.588	○	3.458	○	3.490	○

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[1-10]		[1-11]		[1-12]		
Interval from beginning of Girder		-----	18.531		22.138		25.744		
Immediately After Prestressing	Top of Main Girder	-1.5	1.154	○	2.985	○	5.612	○	
	Bottom of Main Girder	~19.00	14.154	○	11.902	○	8.414	○	
During Deck Construction	Top of Main Girder	-1.5	6.220	○	6.830	○	7.576	○	
	Bottom of Main Girder	~14.00	6.778	○	6.115	○	5.021	○	
Dead Load	Top of Deck	≤10.00	2.571	○	2.299	○	1.875	○	
	Top of Main Girder	0	5.137	○	5.345	○	5.478	○	
	Bottom of Main Girder	~14.00	3.135	○	3.227	○	3.363	○	
Design Load1	Top of Deck	Max	3.847	○	3.195	○	2.241	○	
		Min	2.098	○	1.708	○	1.076	○	
	Top of Main Girder	Max	6.189	○	6.084	○	5.779	○	
		Min	-1.5	4.747	○	4.858	○	4.821	○
	Bottom of Main Girder	Max	~14.00	0.163	○	1.127	○	2.497	○
		Min		4.239	○	4.614	○	5.253	○
Design Load2 Temperature Rise	Top of Deck	Max	4.655	○	4.082	○	3.209	○	
		Min	≤11.50	2.906	○	2.595	○	2.043	○
	Top of Main Girder	Max	5.547	○	5.506	○	5.266	○	
		Min	-2	4.105	○	4.281	○	4.309	○
	Bottom of Main Girder	Max	~16.10	-0.331	○	0.443	○	1.614	○
		Min		3.745	○	3.930	○	4.370	○
Design Load3 Temperature Drop	Top of Deck	Max	4.655	○	4.082	○	3.209	○	
		Min	≤11.50	2.906	○	2.595	○	2.043	○
	Top of Main Girder	Max	5.547	○	5.506	○	5.266	○	
		Min	-2	4.105	○	4.281	○	4.309	○
	Bottom of Main Girder	Max	~16.10	-0.331	○	0.443	○	1.614	○
		Min		3.745	○	3.930	○	4.370	○
Design Load4 Support sinking	Top of Deck	Max	3.847	○	3.195	○	2.241	○	
		Min	≤10.00	2.098	○	1.708	○	1.076	○
	Top of Main Girder	Max	6.189	○	6.084	○	5.779	○	
		Min	-1.5	4.747	○	4.858	○	4.821	○
	Bottom of Main Girder	Max	~14.00	0.163	○	1.127	○	2.497	○
		Min		4.239	○	4.614	○	5.253	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	4.655	○	4.082	○	3.209	○	
		Min	≤11.50	2.906	○	2.595	○	2.043	○
	Top of Main Girder	Max	5.547	○	5.506	○	5.266	○	
		Min	-2	4.105	○	4.281	○	4.309	○
	Bottom of Main Girder	Max	~16.10	-0.331	○	0.443	○	1.614	○
		Min		3.745	○	3.930	○	4.370	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	4.655	○	4.082	○	3.209	○	
		Min	≤11.50	2.906	○	2.595	○	2.043	○
	Top of Main Girder	Max	5.547	○	5.506	○	5.266	○	
		Min	-2	4.105	○	4.281	○	4.309	○
	Bottom of Main Girder	Max	~16.10	-0.331	○	0.443	○	1.614	○
		Min		3.745	○	3.930	○	4.370	○

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[1-13]		[1-14]		[1-15]	
Interval from beginning of Girder		-----	25.850		28.400		29.350	
Immediately After Prestressing	Top of Main Girder	-1.5	5.693	○	3.772	○	3.015	
	Bottom of Main Girder	~19.00	8.298	○	4.206	○	4.430	
During Deck Construction	Top of Main Girder	-1.5	7.591	○	4.133	○	2.837	
	Bottom of Main Girder	~14.00	4.987	○	3.336	○	4.227	
Dead Load	Top of Deck	≤10.00	1.859	○	0.927	○	0.470	
	Top of Main Girder	0	5.475	○	3.204	○	2.261	
	Bottom of Main Girder	~14.00	3.371	○	2.930	○	3.894	
Design Load1	Top of Deck	Max	2.212	○	1.010	○	0.478	
		Min	1.045	○	-0.372	○	-1.072	
	Top of Main Girder	Max	5.765	○	3.276	○	2.268	
		Min	-1.5	4.805	○	2.081	○	0.919
	Bottom of Main Girder	Max	~14.00	2.536	○	2.777	○	3.880
		Min		5.298	○	5.325	○	6.631
Design Load2 Temperature Rise	Top of Deck	Max	3.182	○	2.096	○	1.590	
		Min	≤11.50	2.014	○	0.714	○	0.040
	Top of Main Girder	Max	5.254	○	2.908	○	1.928	
		Min	-2	4.295	○	1.713	○	0.579
	Bottom of Main Girder	Max	~16.10	1.647	○	2.179	○	3.302
		Min		4.409	○	4.728	○	6.053
Design Load3 Temperature Drop	Top of Deck	Max	3.182	○	2.096	○	1.590	
		Min	≤11.50	2.014	○	0.714	○	0.040
	Top of Main Girder	Max	5.254	○	2.908	○	1.928	
		Min	-2	4.295	○	1.713	○	0.579
	Bottom of Main Girder	Max	~16.10	1.647	○	2.179	○	3.302
		Min		4.409	○	4.728	○	6.053
Design Load4 Support sinking	Top of Deck	Max	2.212	○	1.010	○	0.478	
		Min	≤10.00	1.045	○	-0.372	○	-1.072
	Top of Main Girder	Max	5.765	○	3.276	○	2.268	
		Min	-1.5	4.805	○	2.081	○	0.919
	Bottom of Main Girder	Max	~14.00	2.536	○	2.777	○	3.880
		Min		5.298	○	5.325	○	6.631
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	3.182	○	2.096	○	1.590	
		Min	≤11.50	2.014	○	0.714	○	0.040
	Top of Main Girder	Max	5.254	○	2.908	○	1.928	
		Min	-2	4.295	○	1.713	○	0.579
	Bottom of Main Girder	Max	~16.10	1.647	○	2.179	○	3.302
		Min		4.409	○	4.728	○	6.053
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	3.182	○	2.096	○	1.590	
		Min	≤11.50	2.014	○	0.714	○	0.040
	Top of Main Girder	Max	5.254	○	2.908	○	1.928	
		Min	-2	4.295	○	1.713	○	0.579
	Bottom of Main Girder	Max	~16.10	1.647	○	2.179	○	3.302
		Min		4.409	○	4.728	○	6.053

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2

Cross Section NumberNo.	Unit	Allowable Value	[1- 1]		[1- 2]		[1- 3]	
Interval from beginning of Girder								
				0.500		1.450		4.000
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1300	○	1300	○	1300	○
Immediately After Prestressing	N/mm ²	1295	1144	○	1148	○	1154	○
Effective Prestressing Force (*1)	N/mm ²	1110	1085	○	1086	○	1072	○
Effective Prestressing Force (*2)	N/mm ²	1110	1014	○	1012	○	977	○
max	N/mm ²	1110	1014	○	1014	○	994	○
Ultimate Load	-----	1.00	999.9	○	5.59	○	1.99	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1- 4]		[1- 5]		[1- 6]	
Interval from beginning of Girder								
				4.106		7.713		11.319
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1300	○	1300	○	1300	○
Immediately After Prestressing	N/mm ²	1295	1155	○	1173	○	1178	○
Effective Prestressing Force (*1)	N/mm ²	1110	1072	○	1080	○	1075	○
Effective Prestressing Force (*2)	N/mm ²	1110	977	○	991	○	991	○
max	N/mm ²	1110	995	○	1031	○	1047	○
Ultimate Load	-----	1.00	2.0	○	1.36	○	1.22	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1- 7]		[1- 8]		[1- 9]	
Interval from beginning of Girder								
				14.078		14.925		16.121
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1300	○	1300	○	1300	○
Immediately After Prestressing	N/mm ²	1295	1159	○	1155	○	1149	○
Effective Prestressing Force (*1)	N/mm ²	1110	1055	○	1052	○	1047	○
Effective Prestressing Force (*2)	N/mm ²	1110	976	○	973	○	966	○
max	N/mm ²	1110	1037	○	1034	○	1025	○
Ultimate Load	-----	1.00	1.2	○	1.19	○	1.21	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1-10]	[1-11]	[1-12]
Interval from beginning of Girder			18.531	22.138	25.744
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1300	1300	1300
Immediately After Prestressing	N/mm ²	1295	1145	1152	1139
Effective Prestressing Force (*1)	N/mm ²	1110	1046	1065	1064
Effective Prestressing Force (*2)	N/mm ²	1110	960	972	965
max	N/mm ²	1110	1009	998	968
Ultimate Load	-----	1.00	1.3	1.52	2.40

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[1-13]	[1-14]	[1-15]
Interval from beginning of Girder			25.850	28.400	29.350
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1300	1300	1300
Immediately After Prestressing	N/mm ²	1295	1138	1085	1081
Effective Prestressing Force (*1)	N/mm ²	1110	1063	1028	1025
Effective Prestressing Force (*2)	N/mm ²	1110	964	952	951
max	N/mm ²	1110	966	949	947
Ultimate Load	-----	1.00	2.5	2.95	1.88

*1:During DeckConstruction *2:Design Load

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[1- 1]	[1- 2]	[1- 3]	
Interval from beginning of Girder			-----	0.500	1.450	4.000	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.55 Δ 1.28 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.03 ○ -0.11 ○	
	Neutral Axis before Composition			-----	--	-0.04 ○ -0.11 ○	
	Neutral Axis after Composition			-----	--	-0.04 ○ -0.12 ○	
	Base of Lower Flange			-----	--	-0.01 ○ -0.06 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.14 ○ -0.46 ○	
				Min	-----	--	-0.03 ○ -0.09 ○
	Neutral Axis before Composition			Max	-----	--	-0.15 ○ -0.48 ○
				Min	-----	--	-0.04 ○ -0.09 ○
	Neutral Axis after Composition			Max	-----	--	-0.17 ○ -0.49 ○
				Min	-----	--	-0.04 ○ -0.09 ○
	Base of Lower Flange			Max	-----	--	-0.02 ○ -0.34 ○
				Min	-----	--	-0.01 ○ -0.05 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 -- 23.53 --	
	D16	cm	-----	-----	--	31.62 -- 36.88 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	-----	--	0.10 -- 9.42 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	-----	--	3.88 ○ 1.83 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	--	1.408 ○ 1.00 ○	
	D16	-----	1.00	-----	--	1.408 ○ 1.00 ○	
	D19	-----	1.00	-----	--	1.466 ○ 1.15 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.55 Δ 1.28 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.03 ○ -0.11 ○	
	Neutral Axis before Composition			-----	--	-0.04 ○ -0.11 ○	
	Neutral Axis after Composition			-----	--	-0.04 ○ -0.12 ○	
	Base of Lower Flange			-----	--	-0.01 ○ -0.06 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.14 ○ -0.46 ○	
				Min	-----	--	-0.03 ○ -0.09 ○
	Neutral Axis before Composition			Max	-----	--	-0.15 ○ -0.48 ○
				Min	-----	--	-0.04 ○ -0.09 ○
	Neutral Axis after Composition			Max	-----	--	-0.17 ○ -0.49 ○
				Min	-----	--	-0.04 ○ -0.09 ○
	Base of Lower Flange			Max	-----	--	-0.02 ○ -0.34 ○
				Min	-----	--	-0.01 ○ -0.05 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 -- 23.53 --	
	D16	cm	-----	-----	--	31.62 -- 36.88 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	-----	--	0.00 -- 0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[1- 4]	[1- 5]	[1- 6]				
Interval from beginning of Girder			-----	4.106	7.713	11.319				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.26	Δ	0.86	Δ	0.65	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.10	○	-0.04	○	-0.02	○	
	Neutral Axis before Composition			-0.10	○	-0.04	○	-0.02	○	
	Neutral Axis after Composition			-0.11	○	-0.04	○	-0.02	○	
	Base of Lower Flange			-0.06	○	-0.02	○	-0.02	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.45	○	-0.21	○	-0.11	○
				Min	-0.09	○	-0.01	○	0.00	○
	Neutral Axis before Composition			Max	-0.46	○	-0.25	○	-0.15	○
				Min	-0.08	○	-0.01	○	0.00	○
	Neutral Axis after Composition			Max	-0.48	○	-0.23	○	-0.13	○
				Min	-0.09	○	-0.01	○	0.00	○
	Base of Lower Flange			Max	-0.33	○	-0.24	○	-0.19	○
				Min	-0.05	○	-0.01	○	0.00	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	23.96	--	40.00	--	40.00	--	
	D16	cm	-----	37.56	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	9.25	--	4.98	--	1.69	--		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	1.85	○	2.52	○	3.75	○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.00	○	1.037	○	1.40	○	
	D16			1.00	○	1.245	○	1.73	○	
	D19			1.15	○	1.499	○	2.13	○	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.26	Δ	0.86	Δ	0.65	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.10	○	-0.04	○	-0.02	○	
	Neutral Axis before Composition			-0.10	○	-0.04	○	-0.02	○	
	Neutral Axis after Composition			-0.11	○	-0.04	○	-0.02	○	
	Base of Lower Flange			-0.06	○	-0.02	○	-0.02	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.45	○	-0.21	○	-0.11	○
				Min	-0.09	○	-0.01	○	0.00	○
	Neutral Axis before Composition			Max	-0.46	○	-0.25	○	-0.15	○
				Min	-0.08	○	-0.01	○	0.00	○
	Neutral Axis after Composition			Max	-0.48	○	-0.23	○	-0.13	○
				Min	-0.09	○	-0.01	○	0.00	○
	Base of Lower Flange			Max	-0.33	○	-0.24	○	-0.19	○
				Min	-0.05	○	-0.01	○	0.00	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	23.96	--	40.00	--	40.00	--	
	D16	cm	-----	37.56	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	0.00	--	0.00	--	0.00	--		

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[1- 7]	[1- 8]	[1- 9]				
Interval from beginning of Girder			-----	14.078	14.925	16.121				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.55	○	0.42	○	0.64	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.02	○	-0.01	○	-0.02	○	
	Neutral Axis before Composition			-0.02	○	-0.01	○	-0.02	○	
	Neutral Axis after Composition			-0.02	○	-0.01	○	-0.02	○	
	Base of Lower Flange			-0.01	○	0.00	○	-0.02	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.08	○	-0.05	○	-0.01	○
				Min	-0.02	○	-0.04	○	-0.12	○
	Neutral Axis before Composition			Max	-0.11	○	-0.07	○	-0.01	○
				Min	-0.01	○	-0.04	○	-0.12	○
	Neutral Axis after Composition			Max	-0.10	○	-0.06	○	-0.01	○
				Min	-0.02	○	-0.05	○	-0.13	○
	Base of Lower Flange			Max	-0.12	○	-0.12	○	-0.01	○
				Min	-0.01	○	-0.03	○	-0.08	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	0.00	--	0.96	--	2.28	--		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	5.05	○	4.24	○	3.64	○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	--	-----	--	1.35	○	
	D16			-----	--	-----	--	1.69	○	
	D19			-----	--	-----	--	2.10	○	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.55	○	0.42	○	0.64	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.02	○	-0.01	○	-0.02	○	
	Neutral Axis before Composition			-0.02	○	-0.01	○	-0.02	○	
	Neutral Axis after Composition			-0.02	○	-0.01	○	-0.02	○	
	Base of Lower Flange			-0.01	○	0.00	○	-0.02	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.08	○	-0.05	○	-0.01	○
				Min	-0.02	○	-0.04	○	-0.12	○
	Neutral Axis before Composition			Max	-0.11	○	-0.07	○	-0.01	○
				Min	-0.01	○	-0.04	○	-0.12	○
	Neutral Axis after Composition			Max	-0.10	○	-0.06	○	-0.01	○
				Min	-0.02	○	-0.05	○	-0.13	○
	Base of Lower Flange			Max	-0.12	○	-0.12	○	-0.01	○
				Min	-0.01	○	-0.03	○	-0.08	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	0.00	--	0.00	--	0.00	--		

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[1-10]	[1-11]	[1-12]				
Interval from beginning of Girder			-----	18.531	22.138	25.744				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.61	Δ	0.75	Δ	1.02	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.01	○	-0.01	○	-0.03	○	
	Neutral Axis before Composition			-0.01	○	-0.01	○	-0.02	○	
	Neutral Axis after Composition			-0.01	○	-0.01	○	-0.03	○	
	Base of Lower Flange			-0.01	○	0.00	○	-0.02	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.12	○	-0.18	○	-0.32	○
	Neutral Axis before Composition			Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.11	○	-0.15	○	-0.28	○
	Neutral Axis after Composition			Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.12	○	-0.18	○	-0.32	○
	Base of Lower Flange			Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.07	○	-0.09	○	-0.17	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	34.61	--	21.33	--	
	D16	cm	-----	40.00	--	40.00	--	33.44	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	3.37	--	6.41	--	10.39	--		
Compressive Strength to Failure (Suc/Shu)		-----	1.00	2.84	○	2.11	○	1.68	○	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.169	○	1	○	1.00	○	
	D16			1.415	○	1.124	○	1.00	○	
	D19			1.715	○	1.332	○	1.09	○	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.61	Δ	0.75	Δ	1.02	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.01	○	-0.01	○	-0.03	○	
	Neutral Axis before Composition			-0.01	○	-0.01	○	-0.02	○	
	Neutral Axis after Composition			-0.01	○	-0.01	○	-0.03	○	
	Base of Lower Flange			-0.01	○	0.00	○	-0.02	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.12	○	-0.18	○	-0.32	○
	Neutral Axis before Composition			Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.11	○	-0.15	○	-0.28	○
	Neutral Axis after Composition			Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.12	○	-0.18	○	-0.32	○
	Base of Lower Flange			Max	-0.01	○	0.00	○	-0.01	○
				Min	-0.07	○	-0.09	○	-0.17	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	34.61	--	21.33	--	
	D16	cm	-----	40.00	--	40.00	--	33.44	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	0.00	--	0.00	--	0.00	--		

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[1-13]	[1-14]	[1-15]	
Interval from beginning of Girder			-----	25.850	28.400	29.350	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	1.02 Δ	1.04 Δ	----- --	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.02 ○	-0.12 ○	----- --	
	Neutral Axis before Composition			-0.02 ○	-0.24 ○	----- --	
	Neutral Axis after Composition			-0.02 ○	-0.21 ○	----- --	
	Base of Lower Flange			-0.02 ○	-0.05 ○	----- --	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.01 ○	-0.11 ○	----- --
				Min	-0.32 ○	-0.34 ○	----- --
	Neutral Axis before Composition			Max	-0.01 ○	-0.22 ○	----- --
				Min	-0.27 ○	-0.41 ○	----- --
	Neutral Axis after Composition			Max	-0.01 ○	-0.20 ○	----- --
				Min	-0.32 ○	-0.44 ○	----- --
	Base of Lower Flange			Max	-0.01 ○	-0.05 ○	----- --
				Min	-0.17 ○	-0.06 ○	----- --
Spacing of Diagonal Tension Re-bar	D13	cm	-----	21.23 --	18.85 --	----- --	
	D16	cm	-----	33.27 --	29.55 --	----- --	
	D19	cm	-----	40.00 --	40.00 --	----- --	
Axial Reinforcement Bar Volume	cm ²	-----	10.44 --	10.76 --	----- --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	1.67 ○	3.04 ○	----- --		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1 ○	1 ○	----- --	
	D16			1 ○	1 ○	----- --	
	D19			1.085 ○	1.024 ○	----- --	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	1.02 Δ	1.04 Δ	----- --	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.02 ○	-0.12 ○	----- --	
	Neutral Axis before Composition			-0.02 ○	-0.24 ○	----- --	
	Neutral Axis after Composition			-0.02 ○	-0.21 ○	----- --	
	Base of Lower Flange			-0.02 ○	-0.05 ○	----- --	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.01 ○	-0.11 ○	----- --
				Min	-0.32 ○	-0.34 ○	----- --
	Neutral Axis before Composition			Max	-0.01 ○	-0.22 ○	----- --
				Min	-0.27 ○	-0.41 ○	----- --
	Neutral Axis after Composition			Max	-0.01 ○	-0.20 ○	----- --
				Min	-0.32 ○	-0.44 ○	----- --
	Base of Lower Flange			Max	-0.01 ○	-0.05 ○	----- --
				Min	-0.17 ○	-0.06 ○	----- --
Spacing of Diagonal Tension Re-bar	D13	cm	-----	21.23 --	18.85 --	----- --	
	D16	cm	-----	33.27 --	29.55 --	----- --	
	D19	cm	-----	40.00 --	40.00 --	----- --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	----- --		

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1- 1]	[1- 2]	[1- 3]	
Interval from beginning of Girder			-----	0.500	1.450	4.000	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.49 ○ 1.19 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.03 ○ -0.10 ○	
	Neutral Axis before Composition			-----	--	-0.04 ○ -0.09 ○	
	Neutral Axis after Composition			-----	--	-0.04 ○ -0.10 ○	
	Base of Lower Flange			-----	--	0.00 ○ -0.05 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.12 ○ -0.42 ○	
				Min	-----	--	-0.04 ○ -0.10 ○
	Neutral Axis before Composition			Max	-----	--	-0.12 ○ -0.42 ○
				Min	-----	--	-0.04 ○ -0.09 ○
	Neutral Axis after Composition			Max	-----	--	-0.14 ○ -0.45 ○
				Min	-----	--	-0.04 ○ -0.10 ○
	Base of Lower Flange			Max	-----	--	-0.02 ○ -0.28 ○
				Min	-----	--	-0.01 ○ -0.05 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 -- 26.45 --	
	D16	cm	-----	-----	--	31.62 -- 40.00 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 -- 8.38 --	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	-----	--	0.49 ○ 1.19 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.03 ○ -0.10 ○	
	Neutral Axis before Composition			-----	--	-0.04 ○ -0.09 ○	
	Neutral Axis after Composition			-----	--	-0.04 ○ -0.10 ○	
	Base of Lower Flange			-----	--	0.00 ○ -0.05 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.12 ○ -0.42 ○	
				Min	-----	--	-0.04 ○ -0.10 ○
	Neutral Axis before Composition			Max	-----	--	-0.12 ○ -0.42 ○
				Min	-----	--	-0.04 ○ -0.09 ○
	Neutral Axis after Composition			Max	-----	--	-0.14 ○ -0.45 ○
				Min	-----	--	-0.04 ○ -0.10 ○
	Base of Lower Flange			Max	-----	--	-0.02 ○ -0.28 ○
				Min	-----	--	-0.01 ○ -0.05 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.18 -- 26.45 --	
	D16	cm	-----	-----	--	31.62 -- 40.00 --	
	D19	cm	-----	-----	--	40.00 -- 40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 -- 0.00 --	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	-----	--	999.999 ○ 999.999 ○	
Strength against Diagonal Densile Failure(Mus/Mtu)	D13	-----	1.00	-----	--	----- - 999.999 ○	
	D16			-----	--	----- - 999.999 ○	
	D19			-----	--	----- - 999.999 ○	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1- 4]	[1- 5]	[1- 6]				
Interval from beginning of Girder			-----	4.106	7.713	11.319				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.17	Δ	0.82	Δ	0.48	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.10	○	-0.02	○	-0.01	○	
	Neutral Axis before Composition			-0.09	○	-0.02	○	-0.01	○	
	Neutral Axis after Composition			-0.10	○	-0.03	○	-0.01	○	
	Base of Lower Flange			-0.05	○	-0.01	○	-0.01	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.41	○	-0.20	○	-0.06	○
				Min	-0.10	○	-0.02	○	-0.01	○
	Neutral Axis before Composition			Max	-0.41	○	-0.23	○	-0.09	○
				Min	-0.08	○	-0.02	○	-0.01	○
	Neutral Axis after Composition			Max	-0.43	○	-0.22	○	-0.08	○
				Min	-0.10	○	-0.02	○	-0.01	○
	Base of Lower Flange			Max	-0.28	○	-0.23	○	-0.15	○
				Min	-0.05	○	-0.01	○	0.00	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	26.87	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	8.25	--	4.48	--	0.00	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.17	Δ	0.82	Δ	0.48	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.10	○	-0.02	○	-0.01	○	
	Neutral Axis before Composition			-0.09	○	-0.02	○	-0.01	○	
	Neutral Axis after Composition			-0.10	○	-0.03	○	-0.01	○	
	Base of Lower Flange			-0.05	○	-0.01	○	-0.01	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.41	○	-0.20	○	-0.06	○
				Min	-0.10	○	-0.02	○	-0.01	○
	Neutral Axis before Composition			Max	-0.41	○	-0.23	○	-0.09	○
				Min	-0.08	○	-0.02	○	-0.01	○
	Neutral Axis after Composition			Max	-0.43	○	-0.22	○	-0.08	○
				Min	-0.10	○	-0.02	○	-0.01	○
	Base of Lower Flange			Max	-0.28	○	-0.23	○	-0.15	○
				Min	-0.05	○	-0.01	○	0.00	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	26.87	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Densile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	-	
	D16			999.999	○	999.999	○	-----	-	
	D19			999.999	○	999.999	○	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1- 7]	[1- 8]	[1- 9]				
Interval from beginning of Girder			-----	14.078	14.925	16.121				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.14	○	0.06	○	0.38	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.01	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	-0.04	○
	Neutral Axis before Composition			Max	-0.01	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	-0.07	○
	Neutral Axis after Composition			Max	-0.01	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	-0.05	○
	Base of Lower Flange			Max	-0.01	○	0.00	○	0.00	○
				Min	-0.01	○	0.00	○	-0.19	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.14	○	0.06	○	0.38	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.01	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	-0.04	○
	Neutral Axis before Composition			Max	-0.01	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	-0.07	○
	Neutral Axis after Composition			Max	-0.01	○	0.00	○	0.00	○
				Min	0.00	○	0.00	○	-0.05	○
	Base of Lower Flange			Max	-0.01	○	0.00	○	0.00	○
				Min	-0.01	○	0.00	○	-0.19	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	-----	-	-----	-	
	D16	-----	1.00	-----	-	-----	-	-----	-	
	D19	-----	1.00	-----	-	-----	-	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1-10]	[1-11]	[1-12]				
Interval from beginning of Girder			-----	18.531	22.138	25.744				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.55	○	0.73	△	0.97	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	-0.02	○	
	Neutral Axis before Composition			0.00	○	0.00	○	-0.01	○	
	Neutral Axis after Composition			0.00	○	0.00	○	-0.02	○	
	Base of Lower Flange			0.00	○	0.00	○	-0.01	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	0.00	○	-0.01	○
				Min	-0.09	○	-0.17	○	-0.30	○
	Neutral Axis before Composition	Max		0.00	○	0.00	○	-0.01	○	
		Min		-0.12	○	-0.18	○	-0.28	○	
	Neutral Axis after Composition	Max		0.00	○	0.00	○	-0.01	○	
		Min		-0.11	○	-0.18	○	-0.31	○	
	Base of Lower Flange	Max		0.00	○	0.00	○	-0.01	○	
		Min		-0.17	○	-0.16	○	-0.19	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	33.99	--	22.70	--	
	D16	cm	-----	40.00	--	40.00	--	35.58	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	3.04	--	6.52	--	9.77	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.55	○	0.73	△	0.97	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	-0.02	○	
	Neutral Axis before Composition			0.00	○	0.00	○	-0.01	○	
	Neutral Axis after Composition			0.00	○	0.00	○	-0.02	○	
	Base of Lower Flange			0.00	○	0.00	○	-0.01	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	0.00	○	-0.01	○
				Min	-0.09	○	-0.17	○	-0.30	○
	Neutral Axis before Composition	Max		0.00	○	0.00	○	-0.01	○	
		Min		-0.12	○	-0.18	○	-0.28	○	
	Neutral Axis after Composition	Max		0.00	○	0.00	○	-0.01	○	
		Min		-0.11	○	-0.18	○	-0.31	○	
	Base of Lower Flange	Max		0.00	○	0.00	○	-0.01	○	
		Min		-0.17	○	-0.16	○	-0.19	○	
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	33.99	--	22.70	--	
	D16	cm	-----	40.00	--	40.00	--	35.58	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	999.999	○	999.999	○	
	D16	-----	1.00	-----	-	999.999	○	999.999	○	
	D19	-----	1.00	-----	-	999.999	○	999.999	○	

<Design of Main Girder: Summary for Calculation Results of Stress>

1st Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[1-13]	[1-14]	[1-15]				
Interval from beginning of Girder			-----	25.850	28.400	29.350				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.97	Δ	1.01	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.02	○	-0.12	○	-----	--	
	Neutral Axis before Composition			-0.01	○	-0.23	○	-----	--	
	Neutral Axis after Composition			-0.02	○	-0.21	○	-----	--	
	Base of Lower Flange			-0.01	○	-0.05	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.01	○	-0.13	○	-----	--
				Min	-0.29	○	-0.34	○	-----	--
	Neutral Axis before Composition			Max	-0.01	○	-0.21	○	-----	--
				Min	-0.28	○	-0.40	○	-----	--
	Neutral Axis after Composition			Max	-0.01	○	-0.20	○	-----	--
				Min	-0.30	○	-0.43	○	-----	--
	Base of Lower Flange			Max	-0.01	○	-0.04	○	-----	--
				Min	-0.19	○	-0.06	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	22.57	--	19.95	--	-----	--	
	D16	cm	-----	35.37	--	31.28	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	9.82	--	10.17	--	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.97	Δ	1.01	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.02	○	-0.12	○	-----	--	
	Neutral Axis before Composition			-0.01	○	-0.23	○	-----	--	
	Neutral Axis after Composition			-0.02	○	-0.21	○	-----	--	
	Base of Lower Flange			-0.01	○	-0.05	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.01	○	-0.13	○	-----	--
				Min	-0.29	○	-0.34	○	-----	--
	Neutral Axis before Composition			Max	-0.01	○	-0.21	○	-----	--
				Min	-0.28	○	-0.40	○	-----	--
	Neutral Axis after Composition			Max	-0.01	○	-0.20	○	-----	--
				Min	-0.30	○	-0.43	○	-----	--
	Base of Lower Flange			Max	-0.01	○	-0.04	○	-----	--
				Min	-0.19	○	-0.06	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	22.57	--	19.95	--	-----	--	
	D16	cm	-----	35.37	--	31.28	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	-----	--	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	--	
	D16			999.999	○	999.999	○	-----	--	
	D19			999.999	○	999.999	○	-----	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[2- 1]		[2- 2]		[2- 3]	
Interval from beginning of Girder		-----	0.500		1.450		4.000	
Immediately After Prestressing	Top of Main Girder	-1.5	3.014	○	3.771	○	5.689	
	Bottom of Main Girder	~19.00	4.430	○	4.208	○	8.303	
During Deck Construction	Top of Main Girder	-1.5	2.836	○	4.131	○	7.583	
	Bottom of Main Girder	~14.00	4.229	○	3.339	○	4.998	
Dead Load	Top of Deck	≤10.00	0.471	○	0.927	○	1.857	
	Top of Main Girder	0	2.262	○	3.203	○	5.470	
	Bottom of Main Girder	~14.00	3.892	○	2.930	○	3.380	
Design Load1	Top of Deck	Max	0.479	○	1.010	○	2.211	
		Min	≤10.00	-1.070	○	-0.371	○	1.043
	Top of Main Girder	Max	-1.5	2.269	○	3.275	○	5.760
		Min	~14.00	0.920	○	2.081	○	4.800
	Bottom of Main Girder	Max	~14.00	3.878	○	2.777	○	2.543
		Min	~14.00	6.628	○	5.325	○	5.307
Design Load2 Temperature Rise	Top of Deck	Max	≤11.50	1.591	○	2.096	○	3.180
		Min	≤11.50	0.042	○	0.715	○	2.012
	Top of Main Girder	Max	-2	1.928	○	2.907	○	5.250
		Min	~16.10	0.580	○	1.712	○	4.290
	Bottom of Main Girder	Max	~16.10	3.300	○	2.179	○	1.654
		Min	~16.10	6.050	○	4.727	○	4.418
Design Load3 Temperature Drop	Top of Deck	Max	≤11.50	1.591	○	2.096	○	3.180
		Min	≤11.50	0.042	○	0.715	○	2.012
	Top of Main Girder	Max	-2	1.928	○	2.907	○	5.250
		Min	~16.10	0.580	○	1.712	○	4.290
	Bottom of Main Girder	Max	~16.10	3.300	○	2.179	○	1.654
		Min	~16.10	6.050	○	4.727	○	4.418
Design Load4 Support sinking	Top of Deck	Max	≤10.00	0.479	○	1.010	○	2.211
		Min	≤10.00	-1.070	○	-0.371	○	1.043
	Top of Main Girder	Max	-1.5	2.269	○	3.275	○	5.760
		Min	~14.00	0.920	○	2.081	○	4.800
	Bottom of Main Girder	Max	~14.00	3.878	○	2.777	○	2.543
		Min	~14.00	6.628	○	5.325	○	5.307
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	≤11.50	1.591	○	2.096	○	3.180
		Min	≤11.50	0.042	○	0.715	○	2.012
	Top of Main Girder	Max	-2	1.928	○	2.907	○	5.250
		Min	~16.10	0.580	○	1.712	○	4.290
	Bottom of Main Girder	Max	~16.10	3.300	○	2.179	○	1.654
		Min	~16.10	6.050	○	4.727	○	4.418
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	≤11.50	1.591	○	2.096	○	3.180
		Min	≤11.50	0.042	○	0.715	○	2.012
	Top of Main Girder	Max	-2	1.928	○	2.907	○	5.250
		Min	~16.10	0.580	○	1.712	○	4.290
	Bottom of Main Girder	Max	~16.10	3.300	○	2.179	○	1.654
		Min	~16.10	6.050	○	4.727	○	4.418

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[2- 4]		[2- 5]		[2- 6]		
Interval from beginning of Girder		-----	4.100		7.700		11.300		
Immediately After Prestressing	Top of Main Girder	-1.5	5.612	○	2.984	○	1.146	○	
	Bottom of Main Girder	~19.00	8.413	○	11.902	○	14.168	○	
During Deck Construction	Top of Main Girder	-1.5	7.568	○	6.815	○	6.195	○	
	Bottom of Main Girder	~14.00	5.030	○	6.133	○	6.811	○	
Dead Load	Top of Deck	≤10.00	1.872	○	2.293	○	2.561	○	
	Top of Main Girder	0	5.472	○	5.335	○	5.121	○	
	Bottom of Main Girder	~14.00	3.372	○	3.246	○	3.167	○	
Design Load1	Top of Deck	Max	2.238	○	3.187	○	3.835	○	
		Min	1.072	○	1.699	○	2.086	○	
	Top of Main Girder	Max	5.773	○	6.072	○	6.171	○	
		Min	-1.5	4.814	○	4.846	○	4.729	○
	Bottom of Main Girder	Max	~14.00	2.507	○	1.148	○	0.199	○
		Min		5.265	○	4.638	○	4.275	○
Design Load2 Temperature Rise	Top of Deck	Max	3.205	○	4.075	○	4.643	○	
		Min	≤11.50	2.039	○	2.586	○	2.894	○
	Top of Main Girder	Max	5.260	○	5.495	○	5.529	○	
		Min	-2	4.302	○	4.268	○	4.087	○
	Bottom of Main Girder	Max	~16.10	1.624	○	0.464	○	-0.294	○
		Min		4.382	○	3.954	○	3.781	○
Design Load3 Temperature Drop	Top of Deck	Max	3.205	○	4.075	○	4.643	○	
		Min	≤11.50	2.039	○	2.586	○	2.894	○
	Top of Main Girder	Max	5.260	○	5.495	○	5.529	○	
		Min	-2	4.302	○	4.268	○	4.087	○
	Bottom of Main Girder	Max	~16.10	1.624	○	0.464	○	-0.294	○
		Min		4.382	○	3.954	○	3.781	○
Design Load4 Support sinking	Top of Deck	Max	2.238	○	3.187	○	3.835	○	
		Min	≤10.00	1.072	○	1.699	○	2.086	○
	Top of Main Girder	Max	5.773	○	6.072	○	6.171	○	
		Min	-1.5	4.814	○	4.846	○	4.729	○
	Bottom of Main Girder	Max	~14.00	2.507	○	1.148	○	0.199	○
		Min		5.265	○	4.638	○	4.275	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	3.205	○	4.075	○	4.643	○	
		Min	≤11.50	2.039	○	2.586	○	2.894	○
	Top of Main Girder	Max	5.260	○	5.495	○	5.529	○	
		Min	-2	4.302	○	4.268	○	4.087	○
	Bottom of Main Girder	Max	~16.10	1.624	○	0.464	○	-0.294	○
		Min		4.382	○	3.954	○	3.781	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	3.205	○	4.075	○	4.643	○	
		Min	≤11.50	2.039	○	2.586	○	2.894	○
	Top of Main Girder	Max	5.260	○	5.495	○	5.529	○	
		Min	-2	4.302	○	4.268	○	4.087	○
	Bottom of Main Girder	Max	~16.10	1.624	○	0.464	○	-0.294	○
		Min		4.382	○	3.954	○	3.781	○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[2- 7]		[2- 8]		[2- 9]		
Interval from beginning of Girder		-----	13.730		14.900		15.723		
Immediately After Prestressing	Top of Main Girder	-1.5	0.800	○	0.819	○	0.788	○	
	Bottom of Main Girder	~19.00	14.675	○	14.727	○	14.817	○	
During Deck Construction	Top of Main Girder	-1.5	6.258	○	6.329	○	6.275	○	
	Bottom of Main Girder	~14.00	6.795	○	6.779	○	6.889	○	
Dead Load	Top of Deck	≤10.00	2.736	○	2.770	○	2.739	○	
	Top of Main Girder	0	5.221	○	5.270	○	5.225	○	
	Bottom of Main Girder	~14.00	2.944	○	2.926	○	3.061	○	
Design Load1	Top of Deck	Max	4.159	○	4.240	○	4.233	○	
		Min	2.325	○	2.388	○	2.379	○	
	Top of Main Girder	Max	6.395	○	6.482	○	6.458	○	
		Min	-1.5	4.881	○	4.955	○	4.928	○
	Bottom of Main Girder	Max	~14.00	-0.368	○	-0.494	○	-0.417	○
		Min		3.901	○	3.815	○	3.899	○
Design Load2 Temperature Rise	Top of Deck	Max	4.915	○	4.971	○	4.947	○	
		Min	≤11.50	3.081	○	3.120	○	3.093	○
	Top of Main Girder	Max	5.710	○	5.777	○	5.738	○	
		Min	-2	4.196	○	4.250	○	4.208	○
	Bottom of Main Girder	Max	~16.10	-0.739	○	-0.808	○	-0.691	○
		Min		3.530	○	3.501	○	3.625	○
Design Load3 Temperature Drop	Top of Deck	Max	4.915	○	4.971	○	4.947	○	
		Min	≤11.50	3.081	○	3.120	○	3.093	○
	Top of Main Girder	Max	5.710	○	5.777	○	5.738	○	
		Min	-2	4.196	○	4.250	○	4.208	○
	Bottom of Main Girder	Max	~16.10	-0.739	○	-0.808	○	-0.691	○
		Min		3.530	○	3.501	○	3.625	○
Design Load4 Support sinking	Top of Deck	Max	4.159	○	4.240	○	4.233	○	
		Min	≤10.00	2.325	○	2.388	○	2.379	○
	Top of Main Girder	Max	6.395	○	6.482	○	6.458	○	
		Min	-1.5	4.881	○	4.955	○	4.928	○
	Bottom of Main Girder	Max	~14.00	-0.368	○	-0.494	○	-0.417	○
		Min		3.901	○	3.815	○	3.899	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	4.915	○	4.971	○	4.947	○	
		Min	≤11.50	3.081	○	3.120	○	3.093	○
	Top of Main Girder	Max	5.710	○	5.777	○	5.738	○	
		Min	-2	4.196	○	4.250	○	4.208	○
	Bottom of Main Girder	Max	~16.10	-0.739	○	-0.808	○	-0.691	○
		Min		3.530	○	3.501	○	3.625	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	4.915	○	4.971	○	4.947	○	
		Min	≤11.50	3.081	○	3.120	○	3.093	○
	Top of Main Girder	Max	5.710	○	5.777	○	5.738	○	
		Min	-2	4.196	○	4.250	○	4.208	○
	Bottom of Main Girder	Max	~16.10	-0.739	○	-0.808	○	-0.691	○
		Min		3.530	○	3.501	○	3.625	○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)								
Cross Section Number		Allowable Value	[2-10]		[2-11]		[2-12]	
Interval from beginning of Girder		-----	18.500		22.100		25.700	
Immediately After Prestressing	Top of Main Girder	-1.5	1.026	○	2.214	○	3.697	
	Bottom of Main Girder	~19.00	14.773	○	13.167	○	11.016	
During Deck Construction	Top of Main Girder	-1.5	6.093	○	6.116	○	5.790	
	Bottom of Main Girder	~14.00	7.345	○	7.238	○	7.383	
Dead Load	Top of Deck	≤10.00	2.488	○	2.069	○	1.405	
	Top of Main Girder	0	5.014	○	4.831	○	4.311	
	Bottom of Main Girder	~14.00	3.813	○	4.467	○	5.671	
Design Load1	Top of Deck	Max	4.006	○	3.446	○	2.307	
		Min	2.202	○	1.878	○	1.309	
	Top of Main Girder	Max	6.267	○	5.965	○	5.052	
		Min	-1.5	4.779	○	4.673	○	4.231
	Bottom of Main Girder	Max	~14.00	0.275	○	1.245	○	3.548
		Min		4.479	○	4.915	○	5.898
Design Load2 Temperature Rise	Top of Deck	Max	4.663	○	4.027	○	2.812	
		Min	≤11.50	2.859	○	2.459	○	1.814
	Top of Main Girder	Max	5.499	○	5.136	○	4.160	
		Min	-2	4.011	○	3.844	○	3.339
	Bottom of Main Girder	Max	~16.10	0.135	○	1.278	○	3.758
		Min		4.339	○	4.949	○	6.108
Design Load3 Temperature Drop	Top of Deck	Max	4.663	○	4.027	○	2.812	
		Min	≤11.50	2.859	○	2.459	○	1.814
	Top of Main Girder	Max	5.499	○	5.136	○	4.160	
		Min	-2	4.011	○	3.844	○	3.339
	Bottom of Main Girder	Max	~16.10	0.135	○	1.278	○	3.758
		Min		4.339	○	4.949	○	6.108
Design Load4 Support sinking	Top of Deck	Max	4.006	○	3.446	○	2.307	
		Min	≤10.00	2.202	○	1.878	○	1.309
	Top of Main Girder	Max	6.267	○	5.965	○	5.052	
		Min	-1.5	4.779	○	4.673	○	4.231
	Bottom of Main Girder	Max	~14.00	0.275	○	1.245	○	3.548
		Min		4.479	○	4.915	○	5.898
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	4.663	○	4.027	○	2.812	
		Min	≤11.50	2.859	○	2.459	○	1.814
	Top of Main Girder	Max	5.499	○	5.136	○	4.160	
		Min	-2	4.011	○	3.844	○	3.339
	Bottom of Main Girder	Max	~16.10	0.135	○	1.278	○	3.758
		Min		4.339	○	4.949	○	6.108
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	4.663	○	4.027	○	2.812	
		Min	≤11.50	2.859	○	2.459	○	1.814
	Top of Main Girder	Max	5.499	○	5.136	○	4.160	
		Min	-2	4.011	○	3.844	○	3.339
	Bottom of Main Girder	Max	~16.10	0.135	○	1.278	○	3.758
		Min		4.339	○	4.949	○	6.108

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Bending Stress of Concrete (N/mm ²)									
Cross Section Number		Allowable Value	[2-13]		[2-14]		[2-15]		
Interval from beginning of Girder		-----	25.800		28.350		29.300		
Immediately After Prestressing	Top of Main Girder	-1.5	3.745	○	2.733	○	2.923	○	
	Bottom of Main Girder	~19.00	10.951	○	5.911	○	4.995	○	
During Deck Construction	Top of Main Girder	-1.5	5.778	○	3.168	○	2.773	○	
	Bottom of Main Girder	~14.00	7.393	○	4.921	○	4.738	○	
Dead Load	Top of Deck	≤10.00	1.384	○	0.547	○	0.268	○	
	Top of Main Girder	0	4.292	○	2.458	○	2.087	○	
	Bottom of Main Girder	~14.00	5.716	○	4.590	○	4.704	○	
Design Load1	Top of Deck	Max	2.266	○	0.819	○	0.268	○	
		Min	1.290	○	0.522	○	0.268	○	
	Top of Main Girder	Max	5.018	○	2.694	○	2.087	○	
		Min	-1.5	4.215	○	2.437	○	2.087	○
	Bottom of Main Girder	Max	~14.00	3.638	○	4.089	○	4.704	○
		Min		5.937	○	4.636	○	4.704	○
Design Load2 Temperature Rise	Top of Deck	Max	2.769	○	1.344	○	0.787	○	
		Min	≤11.50	1.793	○	1.047	○	0.787	○
	Top of Main Girder	Max	4.124	○	1.841	○	1.231	○	
		Min	-2	3.321	○	1.584	○	1.231	○
	Bottom of Main Girder	Max	~16.10	3.852	○	4.526	○	5.179	○
		Min		6.152	○	5.073	○	5.179	○
Design Load3 Temperature Drop	Top of Deck	Max	2.769	○	1.344	○	0.787	○	
		Min	≤11.50	1.793	○	1.047	○	0.787	○
	Top of Main Girder	Max	4.124	○	1.841	○	1.231	○	
		Min	-2	3.321	○	1.584	○	1.231	○
	Bottom of Main Girder	Max	~16.10	3.852	○	4.526	○	5.179	○
		Min		6.152	○	5.073	○	5.179	○
Design Load4 Support sinking	Top of Deck	Max	2.266	○	0.819	○	0.268	○	
		Min	≤10.00	1.290	○	0.522	○	0.268	○
	Top of Main Girder	Max	5.018	○	2.694	○	2.087	○	
		Min	-1.5	4.215	○	2.437	○	2.087	○
	Bottom of Main Girder	Max	~14.00	3.638	○	4.089	○	4.704	○
		Min		5.937	○	4.636	○	4.704	○
Design Load5 Temperature Rise Support sinking	Top of Deck	Max	2.769	○	1.344	○	0.787	○	
		Min	≤11.50	1.793	○	1.047	○	0.787	○
	Top of Main Girder	Max	4.124	○	1.841	○	1.231	○	
		Min	-2	3.321	○	1.584	○	1.231	○
	Bottom of Main Girder	Max	~16.10	3.852	○	4.526	○	5.179	○
		Min		6.152	○	5.073	○	5.179	○
Design Load6 Temperature Drop Support sinking	Top of Deck	Max	2.769	○	1.344	○	0.787	○	
		Min	≤11.50	1.793	○	1.047	○	0.787	○
	Top of Main Girder	Max	4.124	○	1.841	○	1.231	○	
		Min	-2	3.321	○	1.584	○	1.231	○
	Bottom of Main Girder	Max	~16.10	3.852	○	4.526	○	5.179	○
		Min		6.152	○	5.073	○	5.179	○

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2

Cross Section NumberNo.	Unit	Allowable Value	[2- 1]		[2- 2]		[2- 3]	
Interval from beginning of Girder								
				0.500		1.450		4.000
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1300	○	1300	○	1300	○
Immediately After Prestressing	N/mm ²	1295	1081	○	1085	○	1138	○
Effective Prestressing Force (*1)	N/mm ²	1110	1025	○	1028	○	1063	○
Effective Prestressing Force (*2)	N/mm ²	1110	951	○	952	○	964	○
max	N/mm ²	1110	947	○	949	○	966	○
Ultimate Load	-----	1.00	1.88	○	2.95	○	2.46	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2- 4]		[2- 5]		[2- 6]	
Interval from beginning of Girder								
				4.100		7.700		11.300
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1300	○	1300	○	1300	○
Immediately After Prestressing	N/mm ²	1295	1139	○	1152	○	1145	○
Effective Prestressing Force (*1)	N/mm ²	1110	1064	○	1065	○	1046	○
Effective Prestressing Force (*2)	N/mm ²	1110	965	○	972	○	960	○
max	N/mm ²	1110	968	○	998	○	1009	○
Ultimate Load	-----	1.00	2.41	○	1.53	○	1.30	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2- 7]		[2- 8]		[2- 9]	
Interval from beginning of Girder								
				13.730		14.900		15.723
Stress of PC Strand								
Stress of PC Strand during Prestressing	N/mm ²	1440	1300	○	1300	○	1300	○
Immediately After Prestressing	N/mm ²	1295	1149	○	1155	○	1159	○
Effective Prestressing Force (*1)	N/mm ²	1110	1047	○	1052	○	1055	○
Effective Prestressing Force (*2)	N/mm ²	1110	966	○	972	○	975	○
max	N/mm ²	1110	1025	○	1033	○	1037	○
Ultimate Load	-----	1.00	1.22	○	1.19	○	1.19	○

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2-10]	[2-11]	[2-12]
Interval from beginning of Girder			18.500	22.100	25.700
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1300	1300	1300
Immediately After Prestressing	N/mm ²	1295	1178	1173	1155
Effective Prestressing Force (*1)	N/mm ²	1110	1075	1080	1072
Effective Prestressing Force (*2)	N/mm ²	1110	991	991	977
max	N/mm ²	1110	1047	1031	995
Ultimate Load	-----	1.00	1.23	1.37	1.96

*1:During DeckConstruction *2:Design Load

Cross Section NumberNo.	Unit	Allowable Value	[2-13]	[2-14]	[2-15]
Interval from beginning of Girder			25.800	28.350	29.300
Stress of PC Strand					
Stress of PC Strand during Prestressing	N/mm ²	1440	1300	1300	1300
Immediately After Prestressing	N/mm ²	1295	1154	1148	1144
Effective Prestressing Force (*1)	N/mm ²	1110	1072	1086	1085
Effective Prestressing Force (*2)	N/mm ²	1110	977	1012	1014
max	N/mm ²	1110	994	1014	1014
Ultimate Load	-----	1.00	1.99	5.60	999.90

*1:During DeckConstruction *2:Design Load

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[2- 1]	[2- 2]	[2- 3]		
Interval from beginning of Girder			-----	0.500	1.450	4.000		
Shear Force								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	1.03 Δ	1.01 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.12 ○	-0.02 ○	
	Neutral Axis before Composition			-----	--	-0.24 ○	-0.02 ○	
	Neutral Axis after Composition			-----	--	-0.21 ○	-0.02 ○	
	Base of Lower Flange			-----	--	-0.05 ○	-0.02 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.33 ○	-0.31 ○	
				Min	-----	--	-0.11 ○	-0.01 ○
	Neutral Axis before Composition			Max	-----	--	-0.42 ○	-0.28 ○
				Min	-----	--	-0.22 ○	-0.01 ○
	Neutral Axis after Composition			Max	-----	--	-0.44 ○	-0.32 ○
				Min	-----	--	-0.20 ○	-0.01 ○
	Base of Lower Flange			Max	-----	--	-0.06 ○	-0.17 ○
				Min	-----	--	-0.05 ○	-0.01 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	18.92 --	21.30 --	
	D16	cm	-----	-----	--	29.66 --	33.39 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	10.72 --	10.41 --	
Compressive Strength to Failure (Suc/Shu)			1.00	-----	--	3.05 ○	1.68 ○	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	-----	--	1 ○	1.00 ○	
	D16			-----	--	1 ○	1.00 ○	
	D19			-----	--	1.026 ○	1.09 ○	
Shear Force + Torsion								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	1.03 Δ	1.01 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.12 ○	-0.02 ○	
	Neutral Axis before Composition			-----	--	-0.24 ○	-0.02 ○	
	Neutral Axis after Composition			-----	--	-0.21 ○	-0.02 ○	
	Base of Lower Flange			-----	--	-0.05 ○	-0.02 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.33 ○	-0.31 ○	
				Min	-----	--	-0.11 ○	-0.01 ○
	Neutral Axis before Composition			Max	-----	--	-0.42 ○	-0.28 ○
				Min	-----	--	-0.22 ○	-0.01 ○
	Neutral Axis after Composition			Max	-----	--	-0.44 ○	-0.32 ○
				Min	-----	--	-0.20 ○	-0.01 ○
	Base of Lower Flange			Max	-----	--	-0.06 ○	-0.17 ○
				Min	-----	--	-0.05 ○	-0.01 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	18.92 --	21.30 --	
	D16	cm	-----	-----	--	29.66 --	33.39 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 --	0.00 --	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[2- 4]	[2- 5]	[2- 6]	
Interval from beginning of Girder			-----	4.100	7.700	11.300	
Shear Force							
Shear Stress	Design Load	N/mm ²	0.55	1.02 Δ	0.74 Δ	0.60 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.02 ○	-0.01 ○	-0.01 ○	
	Neutral Axis before Composition			-0.02 ○	-0.01 ○	-0.01 ○	
	Neutral Axis after Composition			-0.03 ○	-0.01 ○	-0.01 ○	
	Base of Lower Flange			-0.02 ○	0.00 ○	-0.01 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.31 ○	-0.18 ○	-0.12 ○
				Min	-0.01 ○	0.00 ○	-0.01 ○
	Neutral Axis before Composition			Max	-0.28 ○	-0.15 ○	-0.11 ○
				Min	-0.01 ○	0.00 ○	-0.01 ○
	Neutral Axis after Composition			Max	-0.32 ○	-0.18 ○	-0.12 ○
				Min	-0.01 ○	0.00 ○	-0.01 ○
	Base of Lower Flange			Max	-0.17 ○	-0.10 ○	-0.07 ○
				Min	-0.01 ○	0.00 ○	-0.02 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	21.41 --	34.72 --	40.00 --	
	D16	cm	-----	33.56 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	10.36 --	6.39 --	3.34 --		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	1.68 ○	2.12 ○	2.85 ○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.00 ○	1 ○	1.17 ○	
	D16			1.00 ○	1.125 ○	1.42 ○	
	D19			1.09 ○	1.333 ○	1.72 ○	
Shear Force + Torsion							
Shear Stress	Design Load	N/mm ²	0.55	1.02 Δ	0.74 Δ	0.60 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.02 ○	-0.01 ○	-0.01 ○	
	Neutral Axis before Composition			-0.02 ○	-0.01 ○	-0.01 ○	
	Neutral Axis after Composition			-0.03 ○	-0.01 ○	-0.01 ○	
	Base of Lower Flange			-0.02 ○	0.00 ○	-0.01 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.31 ○	-0.18 ○	-0.12 ○
				Min	-0.01 ○	0.00 ○	-0.01 ○
	Neutral Axis before Composition			Max	-0.28 ○	-0.15 ○	-0.11 ○
				Min	-0.01 ○	0.00 ○	-0.01 ○
	Neutral Axis after Composition			Max	-0.32 ○	-0.18 ○	-0.12 ○
				Min	-0.01 ○	0.00 ○	-0.01 ○
	Base of Lower Flange			Max	-0.17 ○	-0.10 ○	-0.07 ○
				Min	-0.01 ○	0.00 ○	-0.02 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	21.41 --	34.72 --	40.00 --	
	D16	cm	-----	33.56 --	40.00 --	40.00 --	
	D19	cm	-----	40.00 --	40.00 --	40.00 --	
Axial Reinforcement Bar Volume	cm ²	-----	0.00 --	0.00 --	0.00 --		

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[2- 7]	[2- 8]	[2- 9]				
Interval from beginning of Girder			-----	13.730	14.900	15.723				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.64	Δ	0.46	○	0.54	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.02	○	0.00	○	-0.02	○	
	Neutral Axis before Composition			-0.02	○	0.00	○	-0.02	○	
	Neutral Axis after Composition			-0.02	○	0.00	○	-0.02	○	
	Base of Lower Flange			-0.02	○	0.00	○	-0.01	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.12	○	-0.06	○	-0.02	○
				Min	-0.01	○	-0.05	○	-0.08	○
	Neutral Axis before Composition			Max	-0.12	○	-0.06	○	-0.01	○
				Min	-0.01	○	-0.06	○	-0.11	○
	Neutral Axis after Composition			Max	-0.13	○	-0.07	○	-0.02	○
				Min	-0.01	○	-0.05	○	-0.09	○
	Base of Lower Flange			Max	-0.08	○	-0.05	○	-0.01	○
				Min	-0.01	○	-0.10	○	-0.11	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	2.25	--	0.57	--	0.00	--		
Compressive Strength to Failure (Suc/Shu)	-----	1.00	3.65	○	4.46	○	5.02	○		
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.354	○	-----	--	-----	--	
	D16			1.691	○	-----	--	-----	--	
	D19			2.104	○	-----	--	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.64	Δ	0.46	○	0.54	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.02	○	0.00	○	-0.02	○	
	Neutral Axis before Composition			-0.02	○	0.00	○	-0.02	○	
	Neutral Axis after Composition			-0.02	○	0.00	○	-0.02	○	
	Base of Lower Flange			-0.02	○	0.00	○	-0.01	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.12	○	-0.06	○	-0.02	○
				Min	-0.01	○	-0.05	○	-0.08	○
	Neutral Axis before Composition			Max	-0.12	○	-0.06	○	-0.01	○
				Min	-0.01	○	-0.06	○	-0.11	○
	Neutral Axis after Composition			Max	-0.13	○	-0.07	○	-0.02	○
				Min	-0.01	○	-0.05	○	-0.09	○
	Base of Lower Flange			Max	-0.08	○	-0.05	○	-0.01	○
				Min	-0.01	○	-0.10	○	-0.11	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume	cm ²	-----	0.00	--	0.00	--	0.00	--		

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[2-10]	[2-11]	[2-12]				
Interval from beginning of Girder			-----	18.500	22.100	25.700				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.64	Δ	0.86	Δ	1.25	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.02	○	-0.04	○	-0.10	○	
	Neutral Axis before Composition			-0.02	○	-0.04	○	-0.10	○	
	Neutral Axis after Composition			-0.02	○	-0.04	○	-0.11	○	
	Base of Lower Flange			-0.02	○	-0.02	○	-0.06	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	0.00	○	-0.01	○	-0.08	○
				Min	-0.11	○	-0.20	○	-0.45	○
	Neutral Axis before Composition			Max	0.00	○	-0.01	○	-0.08	○
				Min	-0.15	○	-0.25	○	-0.45	○
	Neutral Axis after Composition			Max	0.00	○	-0.01	○	-0.09	○
				Min	-0.13	○	-0.23	○	-0.48	○
	Base of Lower Flange			Max	0.00	○	-0.01	○	-0.05	○
				Min	-0.18	○	-0.24	○	-0.31	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	24.45	--	
	D16	cm	-----	40.00	--	40.00	--	38.32	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	1.58	--	4.97	--	9.07	--	
Compressive Strength to Failure (Suc/Shu)		-----	1.00	3.79	○	2.52	○	1.85	○	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1.418	○	1.038	○	1.00	○	
	D16			1.749	○	1.247	○	1.00	○	
	D19			2.155	○	1.501	○	1.16	○	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.64	Δ	0.86	Δ	1.25	Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.02	○	-0.04	○	-0.10	○	
	Neutral Axis before Composition			-0.02	○	-0.04	○	-0.10	○	
	Neutral Axis after Composition			-0.02	○	-0.04	○	-0.11	○	
	Base of Lower Flange			-0.02	○	-0.02	○	-0.06	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	0.00	○	-0.01	○	-0.08	○
				Min	-0.11	○	-0.20	○	-0.45	○
	Neutral Axis before Composition			Max	0.00	○	-0.01	○	-0.08	○
				Min	-0.15	○	-0.25	○	-0.45	○
	Neutral Axis after Composition			Max	0.00	○	-0.01	○	-0.09	○
				Min	-0.13	○	-0.23	○	-0.48	○
	Base of Lower Flange			Max	0.00	○	-0.01	○	-0.05	○
				Min	-0.18	○	-0.24	○	-0.31	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	24.45	--	
	D16	cm	-----	40.00	--	40.00	--	38.32	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 2(Shear Force Max)

Cross Section Number			Allowable Value	[2-13]	[2-14]	[2-15]				
Interval from beginning of Girder			-----	25.800	28.350	29.300				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.27	Δ	0.55	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.11	○	-0.03	○	-----	--	
	Neutral Axis before Composition			-0.10	○	-0.04	○	-----	--	
	Neutral Axis after Composition			-0.11	○	-0.04	○	-----	--	
	Base of Lower Flange			-0.06	○	-0.01	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.09	○	-0.03	○	-----	--
				Min	-0.46	○	-0.14	○	-----	--
	Neutral Axis before Composition			Max	-0.09	○	-0.04	○	-----	--
				Min	-0.47	○	-0.15	○	-----	--
	Neutral Axis after Composition			Max	-0.09	○	-0.04	○	-----	--
				Min	-0.49	○	-0.17	○	-----	--
	Base of Lower Flange			Max	-0.05	○	0.00	○	-----	--
				Min	-0.32	○	-0.02	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	24.04	--	20.18	--	-----	--	
	D16	cm	-----	37.69	--	31.62	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	9.22	--	0.06	--	-----	--	
Compressive Strength to Failure (Suc/Shu)			1.00	1.83	○	3.88	○	-----	--	
Strength against Diagonal Densile Failure(Sus/Shu)	D13	-----	1.00	1	○	1.41	○	-----	--	
	D16			1	○	1.41	○	-----	--	
	D19			1.155	○	1.468	○	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.27	Δ	0.55	Δ	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.11	○	-0.03	○	-----	--	
	Neutral Axis before Composition			-0.10	○	-0.04	○	-----	--	
	Neutral Axis after Composition			-0.11	○	-0.04	○	-----	--	
	Base of Lower Flange			-0.06	○	-0.01	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.09	○	-0.03	○	-----	--
				Min	-0.46	○	-0.14	○	-----	--
	Neutral Axis before Composition			Max	-0.09	○	-0.04	○	-----	--
				Min	-0.47	○	-0.15	○	-----	--
	Neutral Axis after Composition			Max	-0.09	○	-0.04	○	-----	--
				Min	-0.49	○	-0.17	○	-----	--
	Base of Lower Flange			Max	-0.05	○	0.00	○	-----	--
				Min	-0.32	○	-0.02	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	24.04	--	20.18	--	-----	--	
	D16	cm	-----	37.69	--	31.62	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2- 1]	[2- 2]	[2- 3]		
Interval from beginning of Girder			-----	0.500	1.450	4.000		
Shear Force								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	1.01 Δ	0.96 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-----	--	-0.12 ○	-0.02 ○	
	Neutral Axis before Composition			-----	--	-0.23 ○	-0.01 ○	
	Neutral Axis after Composition			-----	--	-0.21 ○	-0.02 ○	
	Base of Lower Flange			-----	--	-0.05 ○	-0.01 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	-----	--	-0.33 ○	-0.29 ○	
				Min	-----	--	-0.13 ○	-0.01 ○
	Neutral Axis before Composition			Max	-----	--	-0.40 ○	-0.27 ○
				Min	-----	--	-0.21 ○	-0.01 ○
	Neutral Axis after Composition			Max	-----	--	-0.43 ○	-0.30 ○
				Min	-----	--	-0.20 ○	-0.01 ○
	Base of Lower Flange			Max	-----	--	-0.06 ○	-0.18 ○
				Min	-----	--	-0.04 ○	-0.01 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.04 --	22.67 --	
	D16	cm	-----	-----	--	31.42 --	35.53 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	10.12 --	9.78 --	
Shear Force + Torsion								
Shear Stress	Design Load	N/mm ²	0.55	-----	--	1.01 Δ	0.96 Δ	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-----	--	-0.12 ○	-0.02 ○	
	Neutral Axis before Composition			-----	--	-0.23 ○	-0.01 ○	
	Neutral Axis after Composition			-----	--	-0.21 ○	-0.02 ○	
	Base of Lower Flange			-----	--	-0.05 ○	-0.01 ○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	-----	--	-0.33 ○	-0.29 ○	
				Min	-----	--	-0.13 ○	-0.01 ○
	Neutral Axis before Composition			Max	-----	--	-0.40 ○	-0.27 ○
				Min	-----	--	-0.21 ○	-0.01 ○
	Neutral Axis after Composition			Max	-----	--	-0.43 ○	-0.30 ○
				Min	-----	--	-0.20 ○	-0.01 ○
	Base of Lower Flange			Max	-----	--	-0.06 ○	-0.18 ○
				Min	-----	--	-0.04 ○	-0.01 ○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	-----	--	20.04 --	22.67 --	
	D16	cm	-----	-----	--	31.42 --	35.53 --	
	D19	cm	-----	-----	--	40.00 --	40.00 --	
Axial Reinforcement Bar Volume		cm ²	-----	-----	--	0.00 --	0.00 --	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	-----	--	999.999 ○	999.999 ○	
Strength against Diagonal Densile Failure(Mus/Mtu)	D13	-----	1.00	-----	--	999.999 ○	999.999 ○	
	D16			-----	--	999.999 ○	999.999 ○	
	D19			-----	--	999.999 ○	999.999 ○	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2- 4]	[2- 5]	[2- 6]				
Interval from beginning of Girder			-----	4.100	7.700	11.300				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.97	Δ	0.73	Δ	0.54	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.02	○	0.00	○	0.00	○	
	Neutral Axis before Composition			-0.01	○	0.00	○	0.00	○	
	Neutral Axis after Composition			-0.02	○	0.00	○	0.00	○	
	Base of Lower Flange			-0.01	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.29	○	-0.17	○	-0.09	○
				Min	-0.01	○	0.00	○	0.00	○
	Neutral Axis before Composition			Max	-0.28	○	-0.18	○	-0.12	○
				Min	-0.01	○	0.00	○	0.00	○
	Neutral Axis after Composition			Max	-0.30	○	-0.18	○	-0.10	○
				Min	-0.01	○	0.00	○	0.00	○
	Base of Lower Flange			Max	-0.19	○	-0.16	○	-0.17	○
				Min	-0.01	○	0.00	○	0.00	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	22.80	--	34.14	--	40.00	--	
	D16	cm	-----	35.73	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	9.72	--	6.49	--	2.99	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.97	Δ	0.73	Δ	0.54	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.02	○	0.00	○	0.00	○	
	Neutral Axis before Composition			-0.01	○	0.00	○	0.00	○	
	Neutral Axis after Composition			-0.02	○	0.00	○	0.00	○	
	Base of Lower Flange			-0.01	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.29	○	-0.17	○	-0.09	○
				Min	-0.01	○	0.00	○	0.00	○
	Neutral Axis before Composition			Max	-0.28	○	-0.18	○	-0.12	○
				Min	-0.01	○	0.00	○	0.00	○
	Neutral Axis after Composition			Max	-0.30	○	-0.18	○	-0.10	○
				Min	-0.01	○	0.00	○	0.00	○
	Base of Lower Flange			Max	-0.19	○	-0.16	○	-0.17	○
				Min	-0.01	○	0.00	○	0.00	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	22.80	--	34.14	--	40.00	--	
	D16	cm	-----	35.73	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	999.999	○	-----	-	
	D16			999.999	○	999.999	○	-----	-	
	D19			999.999	○	999.999	○	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2- 7]	[2- 8]	[2- 9]				
Interval from beginning of Girder			-----	13.730	14.900	15.723				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.38	○	0.10	○	0.14	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	○	0.00	○	0.00	○	
				Min	○	0.00	○	0.00	○	
	Neutral Axis before Composition	Max		○	-0.05	○	-0.01	○	0.00	○
		Min		○	0.00	○	0.00	○	-0.01	○
	Neutral Axis after Composition	Max		○	-0.05	○	0.00	○	0.00	○
		Min		○	0.00	○	0.00	○	-0.01	○
	Base of Lower Flange	Max		○	-0.04	○	-0.01	○	0.00	○
		Min		○	0.00	○	0.00	○	-0.04	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.38	○	0.10	○	0.14	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	0.00	○	0.00	○	0.00	○	
	Neutral Axis before Composition			0.00	○	0.00	○	0.00	○	
	Neutral Axis after Composition			0.00	○	0.00	○	0.00	○	
	Base of Lower Flange			0.00	○	0.00	○	0.00	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	○	0.00	○	0.00	○	
				Min	○	0.00	○	0.00	○	
	Neutral Axis before Composition	Max		○	-0.05	○	-0.01	○	0.00	○
		Min		○	0.00	○	0.00	○	-0.01	○
	Neutral Axis after Composition	Max		○	-0.05	○	0.00	○	0.00	○
		Min		○	0.00	○	0.00	○	-0.01	○
	Base of Lower Flange	Max		○	-0.04	○	-0.01	○	0.00	○
		Min		○	0.00	○	0.00	○	-0.04	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	40.00	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	-----	-	-----	-	
	D16	-----	1.00	-----	-	-----	-	-----	-	
	D19	-----	1.00	-----	-	-----	-	-----	-	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2-10]	[2-11]	[2-12]				
Interval from beginning of Girder			-----	18.500	22.100	25.700				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	0.48	○	0.82	△	1.17	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.01	○	-0.02	○	-0.10	○	
	Neutral Axis before Composition			-0.01	○	-0.02	○	-0.08	○	
	Neutral Axis after Composition			-0.01	○	-0.03	○	-0.10	○	
	Base of Lower Flange			0.00	○	-0.01	○	-0.05	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.01	○	-0.02	○	-0.09	○
				Min	-0.06	○	-0.20	○	-0.41	○
	Neutral Axis before Composition			Max	-0.01	○	-0.02	○	-0.08	○
				Min	-0.09	○	-0.23	○	-0.41	○
	Neutral Axis after Composition			Max	-0.01	○	-0.02	○	-0.10	○
				Min	-0.08	○	-0.22	○	-0.43	○
	Base of Lower Flange			Max	0.00	○	-0.01	○	-0.05	○
				Min	-0.14	○	-0.22	○	-0.28	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	26.98	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	4.46	--	8.22	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	0.48	○	0.82	△	1.17	△	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.01	○	-0.02	○	-0.10	○	
	Neutral Axis before Composition			-0.01	○	-0.02	○	-0.08	○	
	Neutral Axis after Composition			-0.01	○	-0.03	○	-0.10	○	
	Base of Lower Flange			0.00	○	-0.01	○	-0.05	○	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.01	○	-0.02	○	-0.09	○
				Min	-0.06	○	-0.20	○	-0.41	○
	Neutral Axis before Composition			Max	-0.01	○	-0.02	○	-0.08	○
				Min	-0.09	○	-0.23	○	-0.41	○
	Neutral Axis after Composition			Max	-0.01	○	-0.02	○	-0.10	○
				Min	-0.08	○	-0.22	○	-0.43	○
	Base of Lower Flange			Max	0.00	○	-0.01	○	-0.05	○
				Min	-0.14	○	-0.22	○	-0.28	○
Spacing of Diagonal Tension Re-bar	D13	cm	-----	40.00	--	40.00	--	26.98	--	
	D16	cm	-----	40.00	--	40.00	--	40.00	--	
	D19	cm	-----	40.00	--	40.00	--	40.00	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	0.00	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	999.999	○	
Strength against Diagonal Densile Failure(Mus/Mtu)	D13	-----	1.00	-----	-	999.999	○	999.999	○	
	D16			-----	-	999.999	○	999.999	○	
	D19			-----	-	999.999	○	999.999	○	

<Design of Main Girder: Summary for Calculation Results of Stress>

2nd Span, Main Girder Number: G 1(Torsion Max)

Cross Section Number			Allowable Value	[2-13]	[2-14]	[2-15]				
Interval from beginning of Girder			-----	25.800	28.350	29.300				
Shear Force										
Shear Stress	Design Load	N/mm ²	0.55	1.18	Δ	0.49	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.00	-0.10	○	-0.03	○	-----	--	
	Neutral Axis before Composition			-0.09	○	-0.04	○	-----	--	
	Neutral Axis after Composition			-0.10	○	-0.04	○	-----	--	
	Base of Lower Flange			-0.05	○	0.00	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.00	Max	-0.10	○	-0.04	○	-----	--
				Min	-0.42	○	-0.12	○	-----	--
	Neutral Axis before Composition			Max	-0.09	○	-0.04	○	-----	--
				Min	-0.42	○	-0.12	○	-----	--
	Neutral Axis after Composition			Max	-0.10	○	-0.04	○	-----	--
				Min	-0.44	○	-0.14	○	-----	--
	Base of Lower Flange			Max	-0.05	○	0.00	○	-----	--
				Min	-0.28	○	-0.02	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	26.59	--	20.18	--	-----	--	
	D16	cm	-----	40.00	--	31.62	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	8.34	--	0.00	--	-----	--	
Shear Force + Torsion										
Shear Stress	Design Load	N/mm ²	0.55	1.18	Δ	0.49	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-1.30	-0.10	○	-0.03	○	-----	--	
	Neutral Axis before Composition			-0.09	○	-0.04	○	-----	--	
	Neutral Axis after Composition			-0.10	○	-0.04	○	-----	--	
	Base of Lower Flange			-0.05	○	0.00	○	-----	--	
Diagonal Tensile Stress	Base of Upper Flange	N/mm ²	-2.50	Max	-0.10	○	-0.04	○	-----	--
				Min	-0.42	○	-0.12	○	-----	--
	Neutral Axis before Composition			Max	-0.09	○	-0.04	○	-----	--
				Min	-0.42	○	-0.12	○	-----	--
	Neutral Axis after Composition			Max	-0.10	○	-0.04	○	-----	--
				Min	-0.44	○	-0.14	○	-----	--
	Base of Lower Flange			Max	-0.05	○	0.00	○	-----	--
				Min	-0.28	○	-0.02	○	-----	--
Spacing of Diagonal Tension Re-bar	D13	cm	-----	26.59	--	20.18	--	-----	--	
	D16	cm	-----	40.00	--	31.62	--	-----	--	
	D19	cm	-----	40.00	--	40.00	--	-----	--	
Axial Reinforcement Bar Volume		cm ²	-----	0.00	--	0.00	--	-----	--	
Compressive Strength to Failure (Muc/Mtu)		-----	1.00	999.999	○	999.999	○	-----	--	
Strength against Diagonal Tensile Failure(Mus/Mtu)	D13	-----	1.00	999.999	○	-----	-	-----	--	
	D16			999.999	○	-----	-	-----	--	
	D19			999.999	○	-----	-	-----	--	

5 Design of Intermediate Cross Beam

(1) Parameters

<1st Span>

	Unit	Bending Moment (Maximum)	Bending Moment (Minimum)	
CB 2				
Length between End of Girders	Lb	cm	328.0	328.0
Web Width	Bw	cm	22.0	22.0
Width of Cross Beam	Bc	cm	30.0	30.0
Thickness of Deck	Hs	cm	17.0	17.0
Height of Cross Beam (before Composition of Deck)	Hb	cm	134.4	134.4
Height of Cross Beam (after Composition of Deck)	Ha	cm	187.0	187.0
Interval of Cross Beam	Lt	cm	1412.5	1412.5

<2nd Span>

	Unit	Bending Moment (Maximum)	Bending Moment (Minimum)	
CB 2				
Length between End of Girders	Lb	cm	328.0	328.0
Web Width	Bw	cm	22.0	22.0
Width of Cross Beam	Bc	cm	30.0	30.0
Thickness of Deck	Hs	cm	17.0	17.0
Height of Cross Beam (before Composition of Deck)	Hb	cm	134.4	134.4
Height of Cross Beam (after Composition of Deck)	Ha	cm	187.0	187.0
Interval of Cross Beam	Lt	cm	1410.0	1410.0

(2) Calculation of Prestressing

1) Arrangement of PC Strand

(1) Parameter of PC Strand

	Unit	Parameters
Name of PC Strand		4S15.2, SWPR7BL
Area of PC Strand	mm ² /no.	554.80
Amount of Set	mm	4.0
Reduction Rate of Anchor	%	0.000
Friction Coefficient	1/m	0.0040
Creep Coefficient		2.60
Drying Shrinkage	×10 ⁻⁵	20.00
Relaxation	%	2.5
Prestressing Stress	N/mm ²	1250.000
(Considering Friction Coefficient)	N/mm ²	1250.000
Allowable Value	N/mm ²	1440.000

(2) Arrangement of PC Strand

<1st Span>

Item		Unit	Maximum Bending Moment	Minimum Bending Moment
CB 2				
How to Prestressing			From One Side	
Length of PC Strand		m	10.720	10.720
1st	Position	mm	400	400
	Number	No.	1	1
2nd	Position	mm	800	800
	Number	No.	1	1

<2nd Span>

Item		Unit	Maximum Bending Moment	Minimum Bending Moment
CB 2				
How to Prestressing			From One Side	
Length of PC Strand		m	10.720	10.720
1st	Position	mm	400	400
	Number	No.	1	1
2nd	Position	mm	800	800
	Number	No.	1	1

<Design of Cross Beam : Summary for Calculation Results of Stress>

1st Span : Cross Beam (CB2)

Item		Unit	Allowable Value	Mmax		Mmin	
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	-0.32	○	-0.32	○
	Bottom of Deck			-0.21	○	-0.21	○
Dead Load	Top of Cross Beam	N/mm ²	0	1.92	○	1.92	○
	Bottom of Cross Beam			~ 11.0	4.57	○	4.57
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	0.55	○	-0.89	○
	Bottom of Deck			0.36	○	-0.60	○
Dead Load	Top of Cross Beam	N/mm ²	0	1.90	○	1.94	○
	Bottom of Cross Beam			~ 11.0	2.29	○	6.10
Ultimate Load		-----	1	1.80	○	1.57	○
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1440	1250	○	1250	○
	Immediately After Prestressing	N/mm ²	1295	1175	○	1175	○
	Effective Prestressing Force	N/mm ²	1110	1026	○	1026	○

2nd Span : Cross Beam (CB2)

Item		Unit	Allowable Value	Mmax		Mmin	
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	-0.32	○	-0.32	○
	Bottom of Deck			-0.21	○	-0.21	○
Dead Load	Top of Cross Beam	N/mm ²	0	1.92	○	1.92	○
	Bottom of Cross Beam			~ 11.0	4.57	○	4.57
Bending Stress of Concrete	Top of Deck	N/mm ²	≤ 10.0	0.55	○	-0.89	○
	Bottom of Deck			0.36	○	-0.60	○
Dead Load	Top of Cross Beam	N/mm ²	0	1.90	○	1.94	○
	Bottom of Cross Beam			~ 11.0	2.29	○	6.10
Ultimate Load		-----	1	1.80	○	1.57	○
Stress of PC Strand	Stress of PC Strand during Prestressing	N/mm ²	1440	1250	○	1250	○
	Immediately After Prestressing	N/mm ²	1295	1175	○	1175	○
	Effective Prestressing Force	N/mm ²	1110	1026	○	1026	○

<Design of Cross Beam : Summary for Calculation Results of Stress>

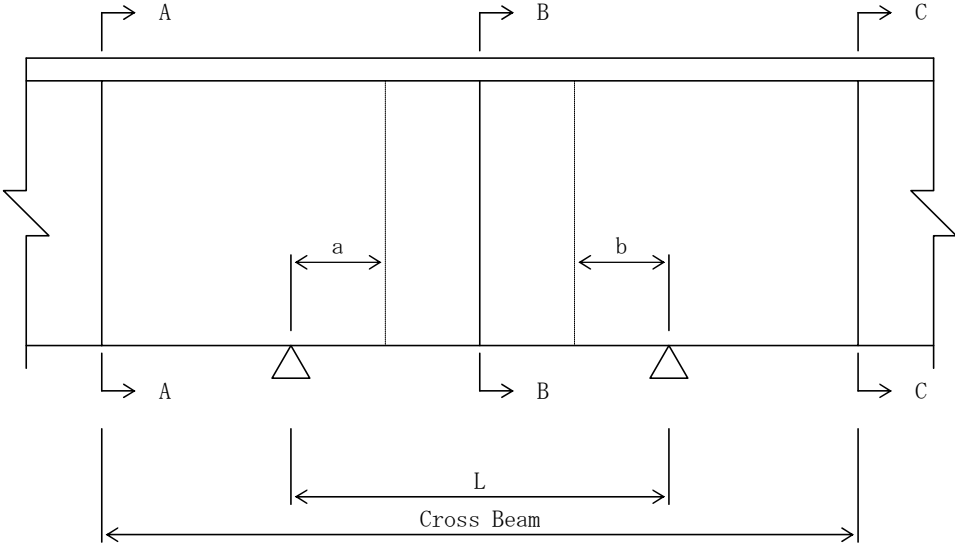
1st Span : Cross Beam (CB2)

Item	Unit	Allowable Value	Smax	Smin	Tmax	Tmin					
Shear Force											
Shear Stress	Design Load	N/mm ²	0.45	0.65	Δ	0.45	○	0.15	○	0.15	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	-0.01	○	-0.01	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	-0.18	○	-0.18	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Suc/Shu	-	1.00	2.82	○	4.12	○	11.04	○	11.04	○
Strength against Diagonal Densile Failure	D13	-	1.00	1.00	○	----	--	----	--	----	--
	Sus/Shu	D16	-	1.00	1.02	○	----	--	----	--	----
Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.00	○	0.00	○	0.00	○	0.00	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	0.00	○	0.00	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	0.00	○	0.00	○	0.00	○	0.00	○
Shear Force + Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.65	Δ	0.45	○	0.15	○	0.15	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-1.10	-0.01	○	-0.01	○	0.00	○	0.00	○
	Design Load	N/mm ²	-2.20	-0.18	○	-0.18	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Muc/Mtu	-	1.00	999.999	○	999.999	○	999.999	○	999.999	○
Strength against Diagonal Densile Failure	D13	-	1.00	999.999	○	----	--	----	--	----	--
	Mus/Mtu	D16	-	1.00	999.999	○	----	--	----	--	----
Amount of Diagonal Tension Re-bar	cm ²	----	9.67	--	6.00	--	6.00	--	6.00	--	
Axial Reinforcement Bar Volume	cm ²	----	5.23	--	0.57	--	0.00	--	0.00	--	

2nd Span : Cross Beam (CB2)

Item	Unit	Allowable Value	Smax	Smin	Tmax	Tmin					
Shear Force											
Shear Stress	Design Load	N/mm ²	0.45	0.65	Δ	0.45	○	0.15	○	0.15	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	-0.01	○	-0.01	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	-0.18	○	-0.18	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Suc/Shu	-	1.00	2.83	○	4.12	○	11.05	○	11.05	○
Strength against Diagonal Densile Failure	D13	-	1.00	1.00	○	----	--	----	--	----	--
	Sus/Shu	D16	-	1.00	1.02	○	----	--	----	--	----
Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.00	○	0.00	○	0.00	○	0.00	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-0.80	0.00	○	0.00	○	0.00	○	0.00	○
	Design Load	N/mm ²	-1.70	0.00	○	0.00	○	0.00	○	0.00	○
Shear Force + Torsion											
Shear Stress	Design Load	N/mm ²	0.45	0.65	Δ	0.45	○	0.15	○	0.15	○
Diagonal Tensile Stress	Dead Load	N/mm ²	-1.10	-0.01	○	-0.01	○	0.00	○	0.00	○
	Design Load	N/mm ²	-2.20	-0.18	○	-0.18	○	-0.01	○	-0.01	○
Compressive Strength to Failure	Muc/Mtu	-	1.00	999.999	○	999.999	○	999.999	○	999.999	○
Strength against Diagonal Densile Failure	D13	-	1.00	999.999	○	----	--	----	--	----	--
	Mus/Mtu	D16	-	1.00	999.999	○	----	--	----	--	----
Amount of Diagonal Tension Re-bar	cm ²	----	9.65	--	6.00	--	6.00	--	6.00	--	
Axial Reinforcement Bar Volume	cm ²	----	5.23	--	0.56	--	0.00	--	0.00	--	

6 Design of Coupling Concrete
Dimension



Unit: m

L	1.200
a	0.500
b	0.500

<Connection of Cross beam : Summary for Calculation Results of Stress>

1st Span~2nd Span, Main Girder Number: G1(Negative Moment) G1(Positive Moment)

Item		Unit	Allowable Value	Negative Moment						Positive Moment		
				A-A		B-B		C-C		B-B		
Re-bar Volume	1st Layer	Diameter	mm	-----	D19	--	D19	--	D19	--	D22	--
		Number	Number	-----	16	--	16	--	16	--	9	--
	2nd Layer	Diameter	mm	-----	D19	--	D19	--	D19	--	D22	--
		Number	Number	-----	16	--	16	--	16	--	9	--
Bending Stress (Dead Load)												
Bending Tensile Stress of Reinforcement Bar		N/mm ²	100	-28.25	○	-21.30	○	-28.34	○	27.25	○	
Bending Stress (Design Load)												
Bending Stress of Concrete		N/mm ²	10	3.53	○	3.53	○	3.53	○	0.74	○	
Bending Tensile Stress of Reinforcement Bar		N/mm ²	160	95.18	○	95.18	○	95.18	○	43.54	○	
Bending Stress (Temperature Load)												
Bending Stress of Concrete		N/mm ²	11.5	3.65	○	3.53	○	3.64	○	1.62	○	
Bending Tensile Stress of Reinforcement Bar		N/mm ²	184	98.28	○	95.18	○	98.02	○	95.51	○	
Ultimate Load		-----	1.00	1.19	○	1.25	○	1.19	○	5.38	○	

7 Calculation of Reaction Force

7.1 Reaction Force for Each Girder

<1st Span, Left>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	345.622	341.234	341.234	345.622
Cast-in-place Concrete	D2	308.946	429.394	429.394	308.946
Weight of Bridge Surface	D3	180.602	165.524	165.524	180.602
Subtotal: DT1=D1+D2+D3		835.170	936.152	936.152	835.170
Live Load LT	Max	334.690	304.160	304.160	334.690
	Min	-71.370	-29.480	-29.480	-71.370
Subtotal: DT2 =DT1+LT+SW	Max	1169.860	1240.312	1240.312	1169.860
	Min	763.800	906.672	906.672	763.800
Creep	CR	75.471	66.591	66.591	75.471
Drying Shrinkage SH		-8.642	-9.277	-9.277	-8.642
Temperature Range		22.468	24.119	24.119	22.468
Dead Load: DT1+CR+SH		901.999	993.466	993.466	901.999
Total: DT2+CR +SH+T+SD	Max	1259.157	1321.745	1321.745	1259.157
	Min	853.097	988.105	988.105	853.097

<1st Span, Right>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	345.622	341.234	341.234	345.622
Cast-in-place Concrete	D2	331.750	453.224	453.224	331.750
Weight of Bridge Surface	D3	291.605	268.360	268.360	291.605
Subtotal: DT1=D1+D2+D3		968.977	1062.818	1062.818	968.977
Live Load LT	Max	541.200	468.490	468.490	541.200
	Min	-239.170	-154.070	-154.070	-239.170
Subtotal: DT2 =DT1+LT+SW	Max	1510.177	1531.308	1531.308	1510.177
	Min	729.807	908.748	908.748	729.807
Creep	CR	-74.779	-65.787	-65.787	-74.779
Drying Shrinkage SH		8.651	9.287	9.287	8.651
Temperature Range		-22.494	-24.147	-24.147	-22.494
Dead Load: DT1+CR+SH		902.849	1006.318	1006.318	902.849
Total: DT2+CR +SH+T+SD	Max	1421.555	1450.661	1450.661	1421.555
	Min	641.185	828.101	828.101	641.185

<2nd Span, Left>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	345.113	340.733	340.733	345.113
Cast-in-place Concrete	D2	331.336	452.710	452.710	331.336
Weight of Bridge Surface	D3	290.004	266.808	266.808	290.004
Subtotal: DT1=D1+D2+D3		966.453	1060.251	1060.251	966.453
Live Load LT	Max	540.230	467.580	467.580	540.230
	Min	-239.580	-154.560	-154.560	-239.580
Subtotal: DT2 =DT1+LT+SW	Max	1506.683	1527.831	1527.831	1506.683
	Min	726.873	905.691	905.691	726.873
Creep CR		-76.323	-67.544	-67.544	-76.323
Drying Shrinkage SH		8.646	9.282	9.282	8.646
Temperature Range		-22.480	-24.132	-24.132	-22.480
Dead Load: DT1+CR+SH		898.776	1001.989	1001.989	898.776
Total: DT2+CR +SH+T+SD	Max	1416.526	1445.437	1445.437	1416.526
	Min	636.716	823.297	823.297	636.716

<2nd Span, Right>

Unit: kN

		G 1	G 2	G 3	G 4
Weight of Girder	D1	345.113	340.733	340.733	345.113
Cast-in-place Concrete	D2	308.532	428.880	428.880	308.532
Weight of Bridge Surface	D3	180.155	165.086	165.086	180.155
Subtotal: DT1=D1+D2+D3		833.800	934.699	934.699	833.800
Live Load LT	Max	334.530	303.990	303.990	334.530
	Min	-71.540	-29.650	-29.650	-71.540
Subtotal: DT2 =DT1+LT+SW	Max	1168.330	1238.689	1238.689	1168.330
	Min	762.260	905.049	905.049	762.260
Creep CR		75.631	66.740	66.740	75.631
Drying Shrinkage SH		-8.656	-9.292	-9.292	-8.656
Temperature Range		22.506	24.160	24.160	22.506
Dead Load: DT1+CR+SH		900.775	992.147	992.147	900.775
Total: DT2+CR +SH+T+SD	Max	1257.811	1320.297	1320.297	1257.811
	Min	851.741	986.657	986.657	851.741

7.2 Reaction Force for Pier and Abutment

Unit: kN

		1	2	3
Weight of Girder	D1	1373.712	2745.404	1371.692
Cast-in-place Concrete	D2	1476.680	3138.040	1474.824
Weight of Bridge Surface	D3	692.252	2233.554	690.482
Subtotal: DT1=D1+D2+D3		3542.644	8116.998	3536.998
Live Load LT	Max	1021.360	1962.760	1020.780
	Min	-100.970	0.000	-101.570
Subtotal: DT2 =DT1+LT+SW	Max	4564.004	10079.758	4557.778
	Min	3441.674	8116.998	3435.428
Creep CR		284.124	-568.866	284.742
Drying Shrinkage SH		-35.838	71.732	-35.896
Temperature Range		93.174	-186.506	93.332
Dead Load: DT1+CR+SH		3790.930	7619.864	3785.844
Total: DT2+CR +SH+T+SD	Max	4905.464	9396.118	4899.956
	Min	3783.134	7433.358	3777.606

7.3 Horizontal Force

Horizontal Force(PF14、 PF15fix)

(kN)

	PF14	PF15
Prestressing	-324	249
Drying Shrinkage	-335	258
Temperature(+)	259	-185
Temperature(-)	-259	185
Dead Load	-659	507
Temperature+15°C	-400	321
Temperature-15°C	-918	692
Temperature+40°C	32	13
Temperature-40°C	-1350	1000

8 Design of Cross Beam at End of Girder

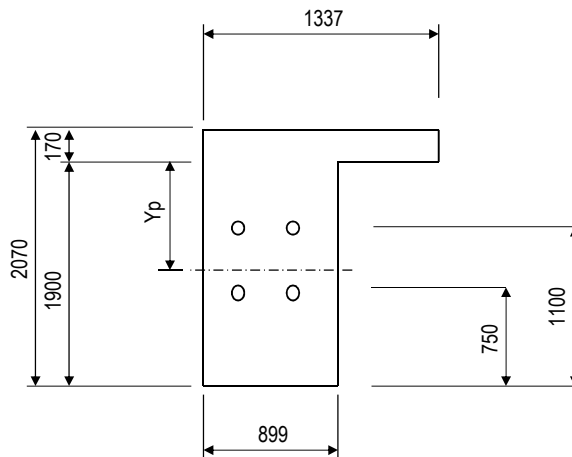
8.1 For Bending Moment

1) Calculation of Bending Moment

(kN·m)

		Bending Moment	
		max	min
Dead Load	(Md)	-67.84	-67.84
Live Load	(ML)	319.35	-204.76
Total	(M)	251.51	-272.60

2) Dimension



3) Calculation of Prestressing

Type of PC strand 4S15.2 SWPR19L

Area of PC strand 554.8 mm²

Number of PC strand 4

(N/mm²)

	Tensile Stress of PC strand	
	Allowable Value	Result
During Prestressing	1440	1250
Immediately after Prestressing	1295	1151
Under Effective Prestressing Force	1110	1056

4) Combined Flexural Stress

(N/mm²)

		Bending Moment(Max)		Bending Moment(Min)	
		Top	Bottom	Top	Bottom
Dead Load		-0.09	0.10	-0.09	0.10
Live Load		0.44	-0.47	-0.28	0.30
Prestressing		1.26	1.48	1.26	1.48
Total	Dead Load	1.17	1.58	1.17	1.58
	Live Load	1.61	1.11	0.89	1.88
Allowable Value		$0.00 \leq \sigma \leq 12.0$			

02-STEEL BRIDGE

02-1-STEEL BOX GIRDER BRIDGE

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§1. Design condition

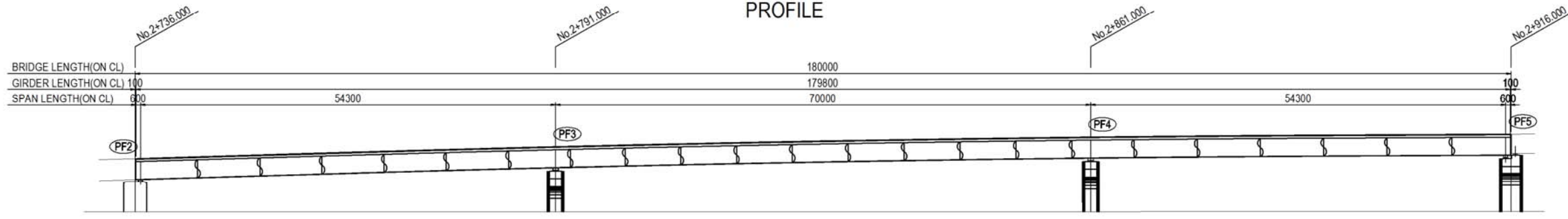
1-1 Design condition

ROAD GRADE	Equivalent to CLASS 4-1
BRIDGE TYPE	3 span continuous steel box girder
BRIDGE LENGTH	L = 180.000 m
SPAN LENGTH	L = 54.300 + 70.000 + 54.300m
WIDTH OF THE ROAD	TOTAL : 12.750 m 0.500+5.500+0.750+5.500+0.500m
PLANE CONFIGURATION	A=150.0~R=-420.0~A=150.0~R=∞~A=130.0~R=320.0
LONGITUDINARL SLOPE	↙ 3.000 % (VCL=130) ↙ 0.500 % (VCL=60)
SECTION SLOPE	4.000 % ↙ 2.000 % ↙ ↘ 6.000 % ↘
ANGLE OF SKEW	90° 00' 00"
PAVEMENT	ASPHALT PAVEMENT t= 80 mm
SLAB	REINFORCED CONCRETE t= 220 mm
LIVE ROAD	AASHTO HL=93
DESIGN STANDARD	AASHTO LRFD BRIDGE DESIGN 2014(LIVE ROAD) Specifications for highway bridges (Japan Road Association) I Common matters, II Steel bridges, V Seismic design (April 2012)

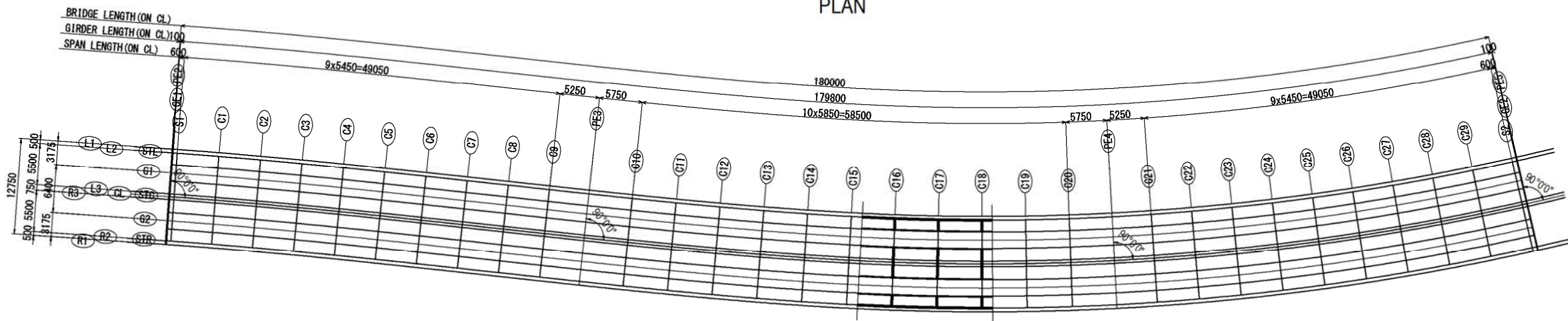
1-2 General view of superstructure

GENERAL VIEW OF SUPERSTRUCTURE(PF2-PF5) S=1:600

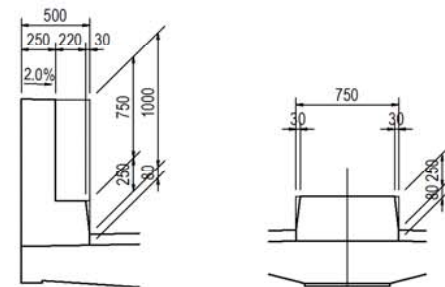
PROFILE



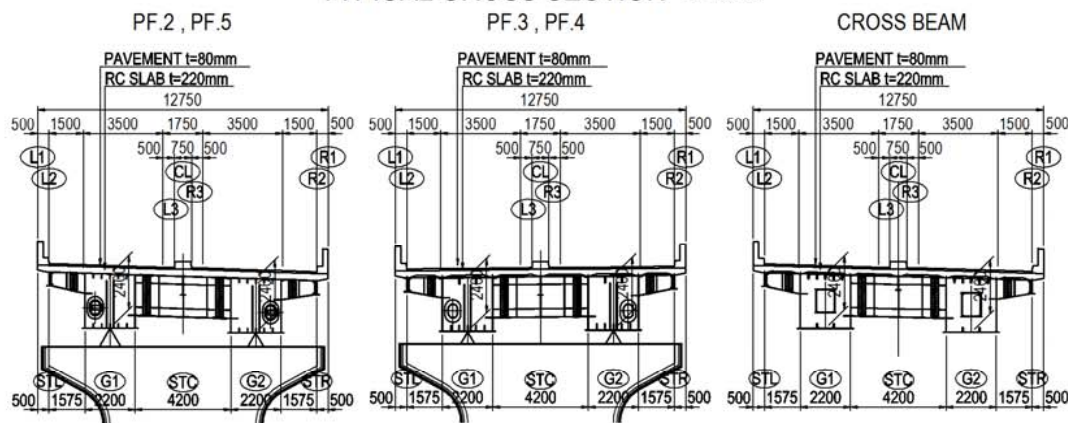
PLAN



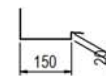
WALL BALUSTRADE MEDIAN STRIP s=1 : 50



TYPICAL CROSS SECTION S=1:300



THE DRAINER PART DETAILS s=1 : 20



DESIGN CONDITION

ROAD GRADE	Equivalent to class4-1
BRIDGE TYPE	3 span continuous steel box girder
BRIDGE LENGTH	L = 180.000 m
SPAN LENGTH	L = 54.300 + 70.000 + 54.300 m
WIDTH OF THE ROAD	TOTAL : 12.750 m L = 0.500 + 5.500 + 0.750 + 5.500 + 0.500 m
PLANE CONFIGURATION	A=150.0~R=∞~A=130.0~R=320.0
LONGITUDINAL SLOPE	↘ 3.000%(VCL=130) ↗ 0.500%(VCL=60)
SECTIN SLOPE	↘ 4.000% ↗ 2.000% ↘ 6.000%
ANGLE OF SKEW	90°00'00"
PAVEMENT	ASPHALT PAVEMENT t = 80 mm
SLAB	REINFORCED CONCRETE t = 220 mm
LIVE ROAD	AASHTO HL-93
DESIGN STANDARD	AASHTO LRFD BRIDGE DESIGN 2014(LIVE ROAD) Specifications for highway bridges(Japan Road Association) .Common matters,Steel bridges, Seismic design(April 2012)

PROJECT NAME DETAILED DESIGN ON BAGO RIVER BRIDGE CONSTRUCTION PROJECT	FINANCED BY jica JAPAN INTERNATIONAL COOPERATION AGENCY	COUNTERPART REPUBLIC OF THE UNION OF MYANMAR MINISTRY OF CONSTRUCTION DEPARTMENT OF BRIDGE	JICA STUDY TEAM NIPPON KOEI CO., LTD. ORIENTAL CONSULTANTS GLOBAL CO., LTD. METROPOLITAN EXPRESSWAY COMPANY LIMITED CHODAI CO., LTD. NIPPON ENGINEERING CONSULTANTS CO., LTD.	NAME	SIGNATURE	DATE	DRAWING TITLE	PACKAGE
				PREPARED BY	Y. SUZUKI		GENERAL VIEW OF SUPERSTRUCTURE(PF2-PF5)	3
				CHECKED BY	T. HAYAKAWA			DWG No.
				APPROVED BY	Y. SANO			P3-FO-

§2.Design of Slab
2-1 Design Condition

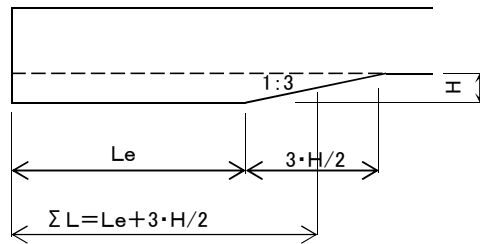
ASPHALT PAVEMENT	ASPHALT PAVEMENT		t = 80mm
RC SLAB		RC SLAB	t = 220mm
LIVE LOAD		LIVE LOAD	AASHTO Truck or JSBH T-load
ADTT _{SL}	2000 or more per day		k1 = 1.25
Allowable Stress	Concrete	Design Strength	$\sigma_{ck} = 24\text{N/mm}^2$
		Allowable Stress	$\sigma_{ca} = 8.0\text{N/mm}^2$
	Reinforcement bar	Material	SD345
		Allowable Stress	$\sigma_{sa} = 140\text{N/mm}^2$
Note: Approximately 20N/mm ² of allowance should be considered in the case without considering			

- The span of slab is determined by the maximum value.
- The length of thickness increasing of slab at the end of girder "Le" is as follows, according to JSBH II 9.2.11
- Window Load : 44.7 m/s
- Collision force to the concrete barrier : 43kN

$$L_e = 1/2 \cdot L$$

L : The span length of slab in the perpendicular direction to bridge axis

Section	Le(mm)
S1	1100
S2	1100



The bending moment of the design with two types of live loads is calculated as follows

1) AASHTO LIVE LOAD $M = 1.2 \cdot (\alpha_1 - \alpha_2) \cdot L \cdot P / SW \cdot (1+i) = 23.5 \text{ kNm}$

$\alpha_1 = 0.204$
 $\alpha_2 = -0.02831$
 $SW = 1815$
 $P = 72.5$
 $i = 0.33$
 $L: \text{SPAN } 2.10 \text{ m}$

2) JSBH T-Load $M = (0.12 \cdot L + 0.07) \cdot P \cdot K \cdot 0.8 + \Delta M = 30.6 \text{ kNm}$

$P = 100$
 $K = 1.000$

	AASHTO	JSBH
Maxmam Positive Live Load Moment	23.5 kNm	30.6 kNm
Maxmam Negative Live Load Moment	-25.0 kNm	-35.3 kNm

Since the RC slab is directly affected by the load of the wheel, it is better to design with JSBH's live load (large

2-2 Summary of Calculation Result for Deck Slab

	Deck Slab outside of Bracket	
	Longitudinal Bar	Stirrup
Bending Moment(kN·m)	-12.92	0.00
Deck Thickness(mm)	270	283.4
Diameter of Upper Rebar (mm)	D19	D16
Pitch of Upper Rebar (mm)	ctc150	ctc250
Diameter of Lower Rebar (mm)	D19	D16
Pitch of Lower Rebar (mm)	ctc300	ctc125
Concrete Cover Thickness(mm)	40.0	57.5
Amount of Rebar As (cm ²)	19.10	15.89
Amount of Rebar As' (cm ²)	9.55	7.94
Stress of Concrete (N/mm ²)	$\sigma_c = 1.30 < 8.0$	$\sigma_c = 0.00 < 8.0$
Stress of Rebar (N/mm ²)	$\sigma_s = 33.8 < 140$	$\sigma_s = 0.0 < 140$

	Deck Slab on Bracket (at Centre Span)	
	Longitudinal Bar	Stirrup
Bending Moment(kN·m)	22.50	15.80
Deck Thickness(mm)	220	220
Diameter of Upper Rebar (mm)	D19	D16
Pitch of Upper Rebar (mm)	ctc300	ctc250
Diameter of Lower Rebar (mm)	D19	D16
Pitch of Lower Rebar (mm)	ctc150	ctc125
Concrete Cover Thickness(mm)	40.0	57.5
Amount of Rebar As (cm ²)	19.10	15.89
Amount of Rebar As' (cm ²)	9.55	7.94
Stress of Concrete (N/mm ²)	$\sigma_c = 3.44 < 8.0$	$\sigma_c = 3.28 < 8.0$
Stress of Rebar (N/mm ²)	$\sigma_s = 76.8 < 140$	$\sigma_s = 71.6 < 140$

	Deck Slab on Bracket (at End of Bracket)	
	Longitudinal Bar	Stirrup
Bending Moment(kN·m)	-37.12	—
Deck Thickness(mm)	300	—
Diameter of Upper Rebar (mm)	D19	—
Pitch of Upper Rebar (mm)	ctc150	—
Diameter of Lower Rebar (mm)	D19	—
Pitch of Lower Rebar (mm)	ctc300	—
Concrete Cover Thickness(mm)	40.0	—
Amount of Rebar As (cm ²)	19.10	—
Amount of Rebar As' (cm ²)	0.00	—
Stress of Concrete (N/mm ²)	$\sigma_c = 3.37 < 8.0$	—
Stress of Rebar (N/mm ²)	$\sigma_s = 85.3 < 140$	—

	Deck Slab between Main Girder and Stringer (at Centre Span)			
	Longitudinal Bar		Stirrup	
Bending Moment(kN·m)	32.81		26.12	
Deck Thickness(mm)	220		220	
Diameter of Upper Rebar (mm)	D19		D16	
Pitch of Upper Rebar (mm)	ctc300		ctc250	
Diameter of Lower Rebar (mm)	D19		D16	
Pitch of Lower Rebar (mm)	ctc150		ctc125	
Concrete Cover Thickness(mm)	40.0		57.5	
Amount of Rebar A_s (cm ²)	19.10		15.89	
Amount of Rebar A_s' (cm ²)	9.55		7.94	
Stress of Concrete (N/mm ²)	$\sigma_c =$	5.02 < 8.0	$\sigma_c =$	5.43 < 8.0
Stress of Rebar (N/mm ²)	$\sigma_s =$	111.9 < 140	$\sigma_s =$	118.4 < 140

	Deck Slab between Main Girder and Stringer (at Stringer)			
	Longitudinal Bar		Stirrup	
Bending Moment(kN·m)	-36.69		—	
Deck Thickness(mm)	300		—	
Diameter of Upper Rebar (mm)	D19		—	
Pitch of Upper Rebar (mm)	ctc150		—	
Diameter of Lower Rebar (mm)	D19		—	
Pitch of Lower Rebar (mm)	ctc300		—	
Concrete Cover Thickness(mm)	40.0		—	
Amount of Rebar A_s (cm ²)	19.10		—	
Amount of Rebar A_s' (cm ²)	0.00		—	
Stress of Concrete (N/mm ²)	$\sigma_c =$	3.32 < 8.0	—	
Stress of Rebar (N/mm ²)	$\sigma_s =$	84.1 < 140	—	

	Deck Slab on Main Girder (at Centre Span)			
	Longitudinal Bar		Stirrup	
Bending Moment(kN·m)	30.20		20.80	
Deck Thickness(mm)	220		220	
Diameter of Upper Rebar (mm)	D19		D16	
Pitch of Upper Rebar (mm)	ctc300		ctc250	
Diameter of Lower Rebar (mm)	D19		D16	
Pitch of Lower Rebar (mm)	ctc150		ctc125	
Concrete Cover Thickness(mm)	40.0		57.5	
Amount of Rebar A_s (cm ²)	19.10		15.89	
Amount of Rebar A_s' (cm ²)	9.55		7.94	
Stress of Concrete (N/mm ²)	$\sigma_c =$	4.62 < 8.0	$\sigma_c =$	4.32 < 8.0
Stress of Rebar (N/mm ²)	$\sigma_s =$	103.0 < 140	$\sigma_s =$	94.3 < 140

	Deck Slab on Main Girder (at End of Girder)			
	Longitudinal Bar		Stirrup	
Bending Moment(kN·m)	-30.20		—	
Deck Thickness(mm)	300		—	
Diameter of Upper Rebar (mm)	D19		—	
Pitch of Upper Rebar (mm)	ctc150		—	
Diameter of Lower Rebar (mm)	D19		—	
Pitch of Lower Rebar (mm)	ctc300		—	
Concrete Cover Thickness(mm)	40.0		—	
Amount of Rebar A_s (cm ²)	19.10		—	
Amount of Rebar A_s' (cm ²)	0.00		—	
Stress of Concrete (N/mm ²)	$\sigma_c =$	2.74 < 8.0	—	
Stress of Rebar (N/mm ²)	$\sigma_s =$	69.4 < 140	—	

§3. Structure analysis

3-1 Analytical Method

1. The structural analysis is conducted by arbitrary lattice theory (a displacement method) with an electrical
The software used is "APOLLO Analyzer " commercialized by Yokogawa Techno-information Service I
2. The structure is plane grid composed of main girders and cross beams.
3. Vertical loads (dead load and live load) is considered in the analysis.
4. The coordinates of the structure are automatically transformed from the plane coordinates
calculated by linear analysis.

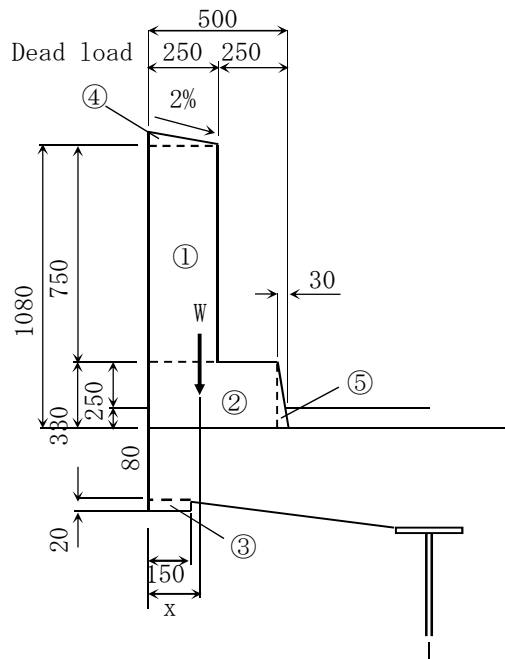
3-2 Load intensity

(1) Dead load

Pavement			22.5 x 0.080	=	1.800 kN/m ²
Slab			0.220 x 24.5	=	5.390 kN/m ²
Haunch			(G1)	=	1.920 kN/m
			(G2)	=	1.920 kN/m
			(STL)	=	0.510 kN/m
			(STC)	=	0.900 kN/m
			(STR)	=	0.510 kN/m
Steel weight			(G1)	=	20.020 kN/m
			(G2)	=	20.020 kN/m
Embedded Form			(G1)	=	0.340 kN/m
			(G2)	=	0.340 kN/m
Railing	From outside	0.185 m		=	8.630 kN/m
Median				=	6.070 kN/m
Point load Total		10.17 + 47.00	(G1)	=	57.170 kN
		10.17 + 47.00	(G2)	=	57.170 kN

(3) details of load intensity

1) Concrete Barrier



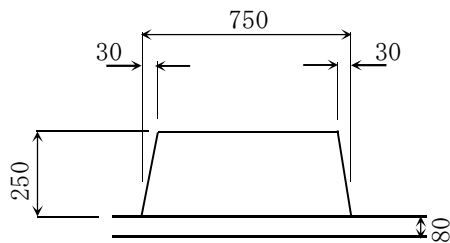
	Area	Unit W.	Load I.	Center G.	--
	A	W	W	X	W·X
	m ²	kN/m ³	kN/m	m	--
①	0.188	24.5	4.606	0.125	0.576
②	0.155	24.5	3.798	0.250	0.950
③	0.003	24.5	0.074	0.075	0.006
④	0.001	24.5	0.025	0.083	0.002
⑤	0.005	24.5	0.123	0.480	0.059
Σ			8.626		1.593

$$W = 8.63 \text{ kN/m}$$

$$x = 1.593 / 8.626 = 0.185 \text{ m From outside}$$

$$0.5 - 0.185 = 0.315 \text{ From inside}$$

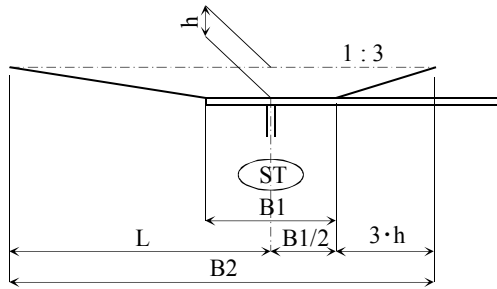
2) Center divider



$$W = 0.750 \times 0.330 \times 24.5 = 6.07 \text{ kN/m}$$

3) Haunch

【Stringer ; STL STR】

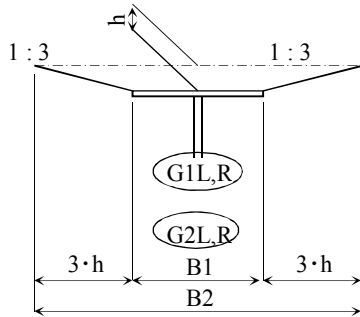


$$W = 1/2 \times (B1 + B2) \times h \times 24.5 \text{ kN/m}$$

Load Point	Section	L (mm)	B1 (mm)	B2 (mm)	h (mm)	W (kN/m)
STL,STR	S1~S2	350	220	610	50	0.510

Note: L is the value of the overhang length less 150mm of the drainage duct.

【Main Girder ; G1L,G1R,G2L,G2R,STC】

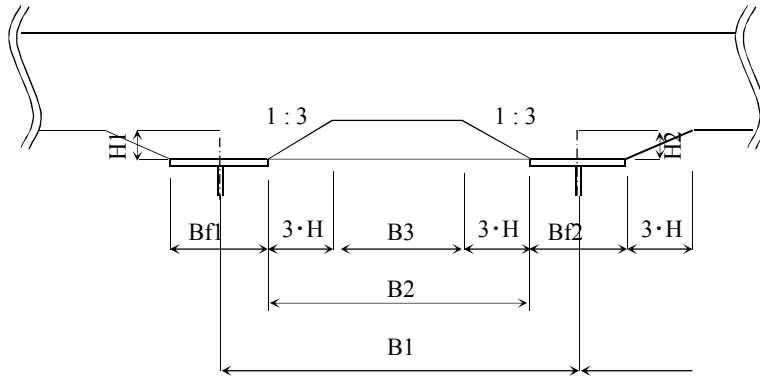


$$W = 1/2 \times (B1 + B2) \times h \times 24.5 \text{ kN/m}$$

Load Point	Applied Section	B1 (mm)	B2 (mm)	h (mm)	W (kN/m)
G1L	S1~S2	250	730	80	0.960
G1R	S1~S2	250	730	80	0.960
G2L	S1~S2	250	730	80	0.960
G2R	S1~S2	250	730	80	0.960
STC	S1~S2	220	700	80	0.900

$$\begin{aligned} G1 &= 0.960 + 0.960 &= 1.92 \text{ (kN)} \\ G2 &= 0.960 + 0.960 &= 1.92 \text{ (kN)} \\ STL &= 0.510 &= 0.51 \text{ (kN)} \\ STR &= 0.510 &= 0.51 \text{ (kN)} \\ STC &= 0.900 &= 0.90 \text{ (kN)} \end{aligned}$$

4) Embedded Form



$$W = 1/2 \times (B2 + B3) \times 0.2 \text{ kN/m}^2$$

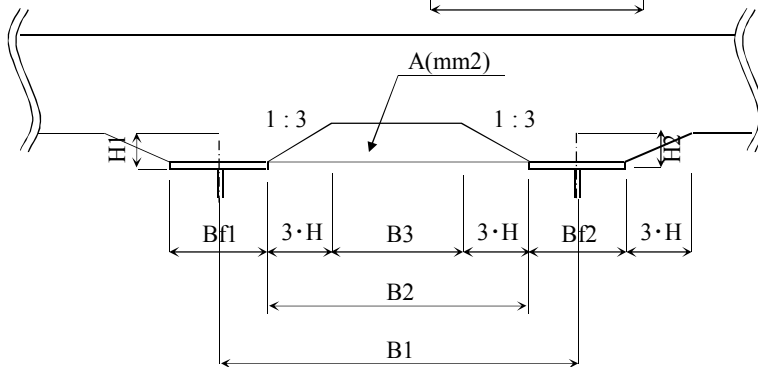
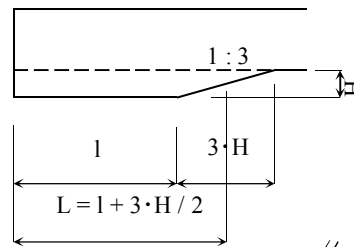
	Bf1 (mm)	Bf2 (mm)	H1 (mm)	H2 (mm)	B1 (mm)	B2 (mm)	B3 (mm)	(B2+B3)/2 (mm)	W' (kN/m ²)	W (kN/m)
G1L ~ G1R	250	250	80	80	2200	1950	1470	1710	0.2	0.34
G2L ~ G2R	250	250	80	80	2200	1950	1470	1710	0.2	0.34

G1= 0.34 (kN/m)
G2= 0.34 (kN/m)

5) Thickness Increasing of Slab

The slab between main girders are increased at the end of girder, with in the half of deck span length from the end. It is considered as the concentrated load applied on the main girder at the end.

	Increasing Length (mm)
S1	1100
S2	1100



(Between Main Girders)

$$W' = A \times L \times 24.5 \text{ (kN)}$$

B1, B2: Interval of main girders

S1·S2

	Bf1 (mm)	Bf2 (mm)	H1 (mm)	H2 (mm)	B1 (mm)	B2 (mm)	B3 (mm)	A (mm ²)	L (mm)	W' (kN)
STL ~ G1L	220	250	50	80	1575	1340	950	74425	1198	2.19
G1L ~ G1R	250	250	80	80	2200	1950	1470	136800	1220	4.09
G1R ~ STC	250	220	80	80	2100	1865	1385	130000	1220	3.89
STC ~ G2L	220	250	80	80	2100	1865	1385	130000	1220	3.89
G2L ~ G2R	250	250	80	80	2200	1950	1470	136800	1220	4.09
G2R ~ STR	250	220	80	50	1575	1340	950	74425	1198	2.19

G1= 2.19 + 4.09 + 3.89 = 10.17 (kN)
G2= 3.89 + 4.09 + 2.19 = 10.17 (kN)

6) Load at the End of Girder

【G1: GE1-S1, GE2-S2】 L= 0.600 m

Pavement	1.800	×	0.600	×	5.500	=	5.940 kN	
Deck Slab	5.390	×	0.600	×	6.375	=	20.617 kN	
Haunch of Main Girder	1.920	×	0.600	×	1	=	1.152 kN	
Haunch of STL	0.510	×	0.600	×	1	=	0.306 kN	
Haunch of STC	0.900	×	0.600	×	0.5	=	0.270 kN	
Steel Weight	19.500	×	0.600	×	1	=	11.700 kN	
Concrete Barrier	8.630	×	0.600	×	1	=	5.178 kN	
Median	6.070	×	0.600	×	0.5	=	1.821 kN	
							Total	= 46.984 kN
								↓
							W	= 47.0 kN/node

【G2: GE1-S1, GE2-S2】 L= 0.600 m

Pavement	1.800	×	0.600	×	5.500	=	5.940 kN	
Deck Slab	5.390	×	0.600	×	6.375	=	20.617 kN	
Haunch of Main Girder	1.920	×	0.600	×	1	=	1.152 kN	
Haunch of STL	0.510	×	0.600	×	1	=	0.306 kN	
Haunch of STC	0.900	×	0.600	×	0.5	=	0.270 kN	
Steel Weight	19.500	×	0.600	×	1	=	11.700 kN	
Concrete Barrier	8.630	×	0.600	×	1	=	5.178 kN	
Median	6.070	×	0.600	×	0.5	=	1.821 kN	
							Total	= 46.984 kN
								↓
							W	= 47.0 kN/node

7) Live Load Intensity

Loading Method

AASHTO HL-93 and the special vehicular load of 75t is applied.

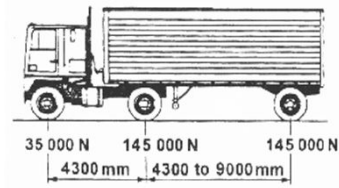
The maximum sectional force is used in the design.

Impact coefficient is considered.

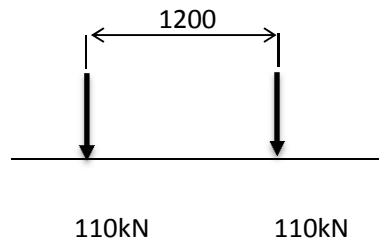
1. AASHTO HL-93

① Design Vehicle Load or Design Tandem Load

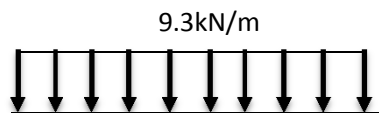
①-1 Design Truck (Hs20-44)



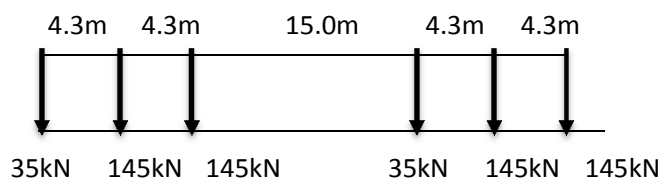
①-2 Design Tandem Load



② Design Lane Load



③ Two Design Trucks for Negative Moment



Load Coefficient with the Number of Lane

Number of Lane	Coefficient
1	1.2
2	1
3	0.85
> 3	0.65

In the Project, three lanes are adopted

Types of Combination

CASE1 (①-1 + ②)x0.85

CASE2 (①-2 + ②)x0.85

CASE3 (③x0.9 + ②x0.9)x0.85

2. Special Vehicular Load 75t(735kN)

The special vehicular load is equally distributed.

Applied Area 45.00 m² Applied Load 735.0 / 45.0 = 16.33 kN/m²

3. Impact Coefficient

Impact coefficient is calculated as follows;

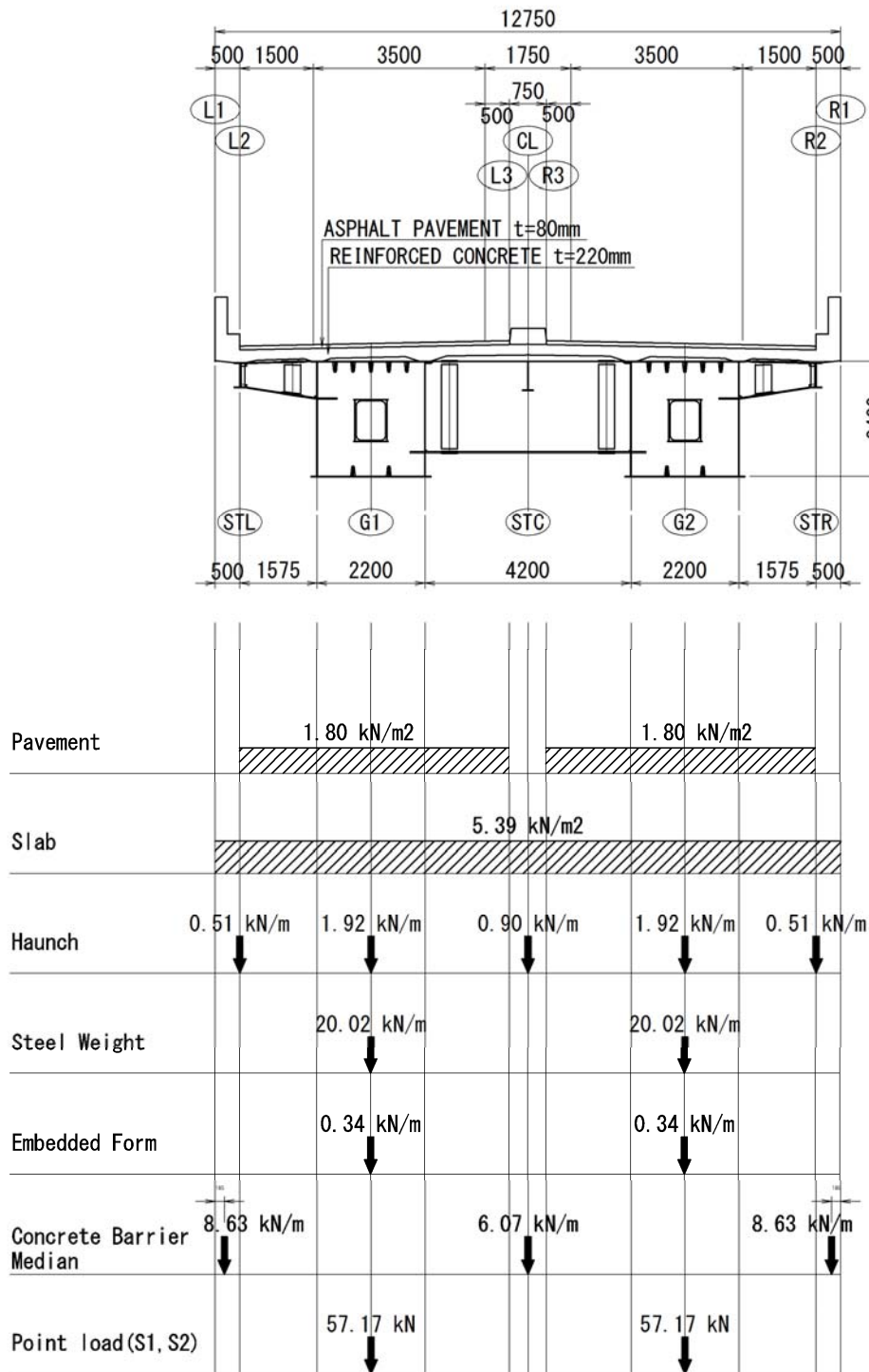
$$i = \frac{20}{50 + L}$$

	Span Length (on CL)		Impact Coefficient
First Bearing			0.192
First Span	54.300 m	$i = 20 / (50 + 54.300) =$	0.192
Second Bearing			0.178
Second Span	70.000 m	$i = 20 / (50 + 70.000) =$	0.167
Third Bearing			0.178
Third Span	54.300 m	$i = 20 / (50 + 54.300) =$	0.192

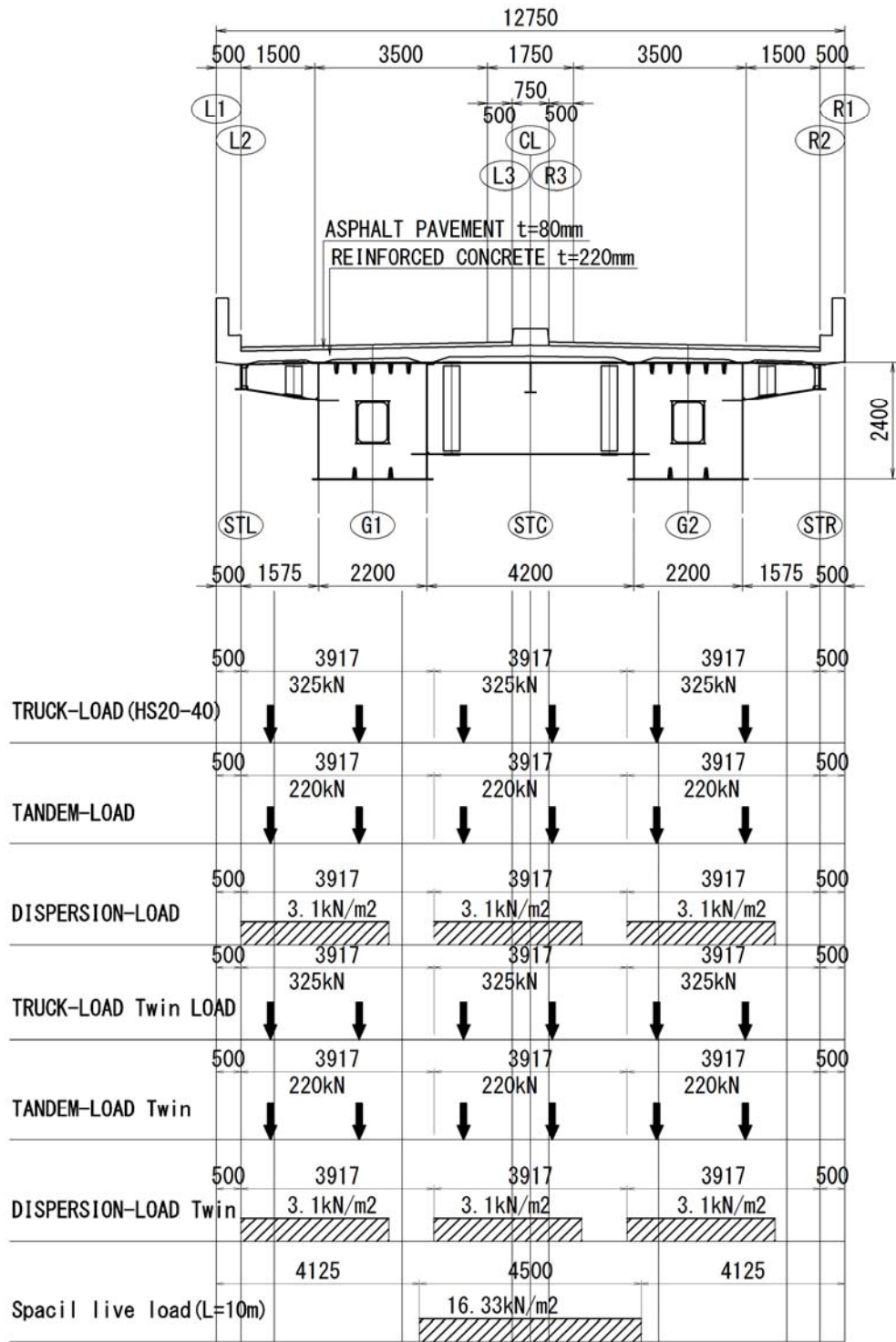
3-3 Load diagram and Load combination

(1) Load diagram

Dead load



Live load

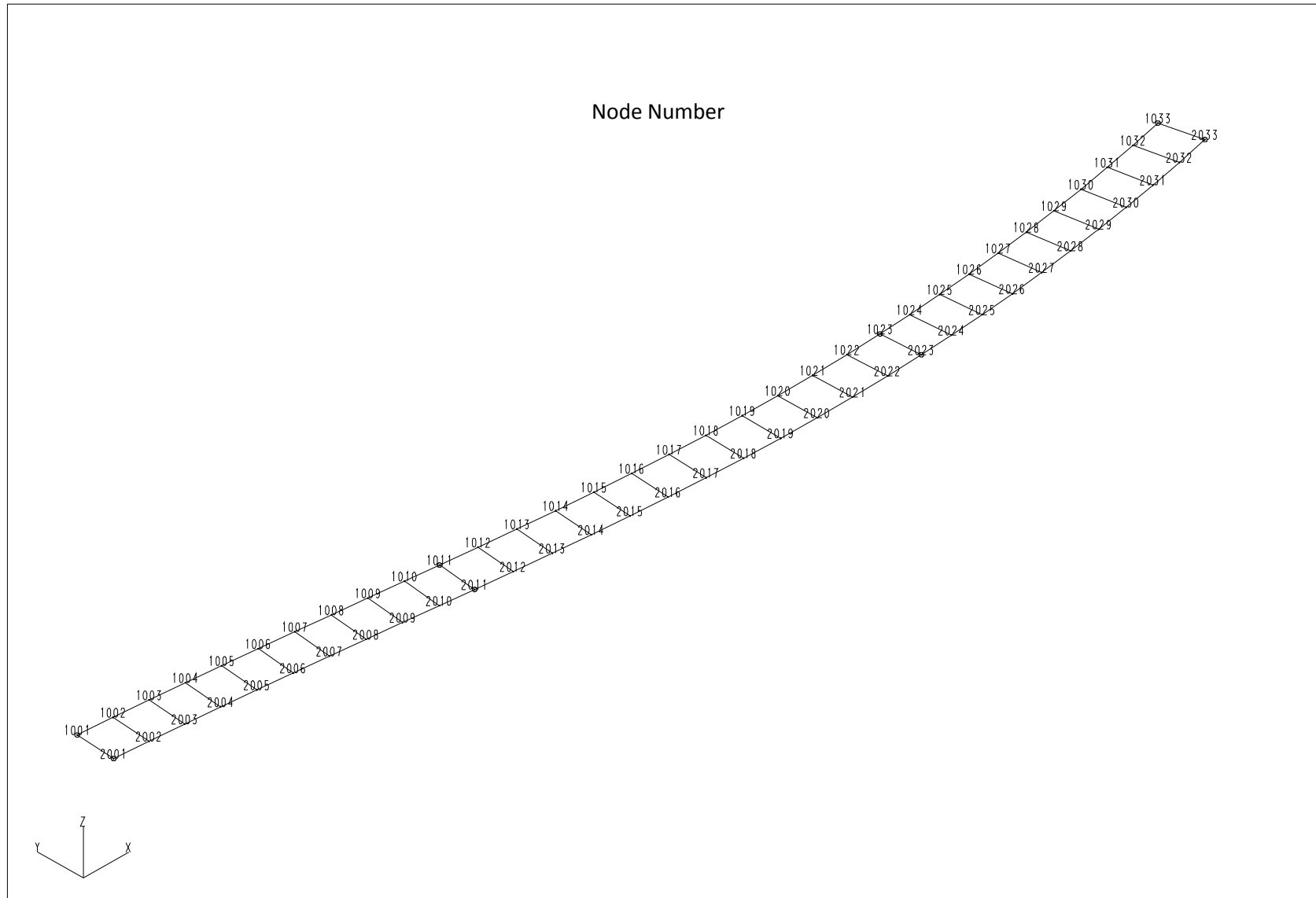


(2) Combination of Load

Case	Load	Note
11	Pavement	
12	Deck Slab	
13	Haunch	
14	Steel Weight	
15	Concrete Barrier	
16	Median	
17	Consentrated Load	
100-1	(①-1+②)	Truck + Vehicular Load
100-2	(①-2+②)	Tandem + Vehicular Load
111	(AASHTO two truck)x0.9	(Truck + Vehicular Load) x 2
200	Special Vehicular Load	

Case	Combination Case	Combination
300	Total of Dead Load	11+12+13+14+15+16+17;
302	Maximum Live Load	(100-1)x0.85,(100-2)x0.85,111x0.85,200
303	Dead Load + Live Load	300+302;

3-4 Skeleton Diagram



3-5 Checking of dead load

Line length							
Bridge area	2277.137	m ²	Lside		Rside		
Pavement area	1964.588	m ²		977.204		987.384	
L1	176.712	m					
L2	176.860	m					
G1	177.652	m					
L3	178.489	m					
CL	178.600	m					
R3	178.711	m					
G2	179.548	m					
R2	180.340	m					
R1	180.480	m					
	Load intensity		Area or Length	(A)	(B)	(B)/(A)	
					Analysis result		
Pavement	1.800	x	1964.588 =	3536.26 kN	3536.02 kN	1.00	
Rcslab	5.390	x	2277.137 =	12273.77 kN	12272.95 kN	1.00	
Haunch	G1	1.920	x 177.652 =	341.09 kN			
	G2	1.920	x 179.548 =	344.73 kN			
	STL	0.510	x 176.860 =	90.20 kN			
	STC	0.900	x 178.600 =	160.74 kN			
	STR	0.510	x 180.340 =	91.97 kN			
				1028.73 kN	1028.68 kN	1.00	
Embedded form	0.340	x	177.652 =	60.40 kN			
	0.340	x	179.548 =	61.05 kN			
				121.45 kN	121.44 kN	1.00	
Steek weight	20.020	x	177.652 =	3556.60 kN			
	20.020	x	179.548 =	3594.55 kN			
				7151.15 kN	7150.79 kN	1.00	
Point load			S1 G1	57.17 kN			
			S1 G2	57.17 kN			
			S2 G1	57.17 kN			
			S2 G2	57.17 kN			
				228.68 kN	228.68 kN	1.00	
concrete Barrier	8.630	x	176.786 =	1525.66 kN			
	8.630	x	180.410 =	1556.94 kN			
				3082.60 kN	3082.48 kN	1.00	
Median	6.070	x	178.600 =	1084.10 kN	1084.05 kN	1.00	
Total				28506.74 kN	28505.10 kN	1.00	

Assuming steel Weight		7151.15 kN	
		46.80	
		<hr/>	
		7197.95 kN	

Real steel Weight 759816 x 9.81 / 1000 = 7453.8 kN

weight ratio 7198.0 / 7453.8 = 97% > 95% OK

3-6. Total Reaction Force

Superstructure Reaction Force (With impact)

				(S1)PF2			
		Name or Coefficient		1001	2001		
Dead load				1673.08	1505.83		
AASHTO	Truk	①-1	Max	601.66	592.45		
			Min	-95.94	-99.71		
	Tandem	①-2	Max	428.91	427.11		
			Min	-69.40	-69.71		
Lane Load	Distributed Load	②	Max	422.34	397.13		
			Min	-113.29	-120.75		
AASHTOxTWIN	Truk	③-1	Max	883.62	851.66		
			Min	-153.08	-167.58		
	Tandem	③-2	Max	428.91	427.11		
			Min	-69.40	-69.71		
Lane Load	Distributed Load	②	Max	422.34	397.13		
			Min	-113.29	-120.75		
Special Vehicular Load	Distributed Load	④	Max	394.32	378.83		
			Min	-53.54	-51.70		
Combination of Live Load	①-1+②	0.85	Max	870.40	841.14		
			Min	-177.85	-187.39		
	①-2+②	0.85	Max	723.56	700.60		
			Min	-155.29	-161.89		
	(③-1+②)x0.9	0.85	Max	999.06	955.32		
			Min	-203.77	-220.57		
	(③-2+②)x0.9	0.85	Max	651.21	630.54		
			Min	-139.76	-145.70		
④	1.0	Max	394.32	378.83			
		Min	-53.54	-51.70			
Picked Up Live Load		PICK	Max	999.06	955.32		
			Min	-203.77	-220.57		
D + L			Max	2672.14	2461.15		
			Min	1469.31	1285.26		
Dead load total				3178.91			

			PF3				
		Name or Coefficient		1011	2011		
Dead load				5489.00	5567.61		
AASHTO	Truk	①-1	Max	643.79	645.56		
			Min	-93.77	-126.07		
	Tandem	①-2	Max	437.63	439.26		
			Min	-64.14	-86.31		
Lane Load	Distributed Load	②	Max	1185.81	1233.29		
			Min	-142.22	-172.58		
AASHTOxTWIN	Truk	③-1	Max	1170.36	1198.98		
			Min	-148.75	-196.15		
	Tandem	③-2	Max	437.63	439.26		
			Min	-64.14	-86.31		
Lane Load	Distributed Load	②	Max	1185.81	1233.29		
			Min	-142.22	-172.58		
Special Vehicular Load	Distributed Load	④	Max	442.00	436.62		
			Min	-43.63	-77.47		
Combination of Live Load	①-1+②	0.85	Max	1555.16	1597.02		
			Min	-200.59	-253.85		
	①-2+②	0.85	Max	1379.92	1421.67		
			Min	-175.41	-220.06		
	(③-1+②)x0.9	0.85	Max	1802.47	1860.69		
			Min	-222.59	-282.08		
	(③-2+②)x0.9	0.85	Max	1241.93	1279.50		
			Min	-157.87	-198.05		
	④		Max	442.00	436.62		
			Min	-43.63	-77.47		
Picked Up Live Load		PICK	Max	1802.47	1860.69		
			Min	-222.59	-282.08		
D + L			Max	7291.47	7428.30		
			Min	5266.41	5285.53		
Dead load total				11056.61			

			PF4				
		Name or Coefficient		1023	2023		
Dead load				5627.64	5485.67		
AASHTO	Truk	①-1	Max	638.28	625.20		
			Min	-117.96	-97.49		
	Tandem	①-2	Max	434.08	425.12		
			Min	-81.69	-67.36		
Lane Load	Distributed Load	②	Max	1233.17	1189.38		
			Min	-158.13	-148.82		
AASHTOxTWIN	Truk	③-1	Max	1189.05	1151.51		
			Min	-170.31	-150.18		
	Tandem	③-2	Max	434.08	425.12		
			Min	-81.69	-67.36		
Lane Load	Distributed Load	②	Max	1233.17	1189.38		
			Min	-158.13	-148.82		
Special Vehicular Load	Distributed Load	④	Max	431.99	432.48		
			Min	-72.13	-48.46		
Combination of Live Load	①-1+②	0.85	Max	1590.73	1542.39		
			Min	-234.68	-209.36		
	①-2+②	0.85	Max	1417.16	1372.33		
			Min	-203.85	-183.75		
	(③-1+②)x0.9	0.85	Max	1853.00	1790.78		
			Min	-251.26	-228.74		
	(③-2+②)x0.9	0.85	Max	1275.45	1235.09		
			Min	-183.46	-165.38		
④		Max	431.99	432.48			
		Min	-72.13	-48.46			
Picked Up Live Load			PICK	1853.00	1790.78		
				-251.26	-228.74		
D + L			Max	7480.64	7276.45		
			Min	5376.38	5256.94		
Dead load total				11113.31			

			(S2)PF5					
		Name or Coefficient		1033	2033			
Dead load				1378.01	1778.24			
AASHTO	Truk	①-1	Max	582.09	611.72			
			Min	-84.49	-114.40			
	Tandem	①-2	Max	424.35	431.68			
			Min	-57.30	-84.12			
Lane Load	Distributed Load	②	Max	356.39	466.36			
			Min	-105.08	-135.53			
AASHTOxTWIN	Truk	③-1	Max	805.12	927.91			
			Min	-154.96	-174.05			
	Tandem	③-2	Max	424.35	431.68			
			Min	-57.30	-84.12			
Lane Load	Distributed Load	②	Max	356.39	466.36			
			Min	-105.08	-135.53			
Special Vehicular Load	Distributed Load	④	Max	363.69	409.11			
			Min	-30.62	-76.90			
Combination of Live Load	①-1+②	0.85	Max	797.71	916.37			
			Min	-161.13	-212.44			
	①-2+②	0.85	Max	663.63	763.33			
			Min	-138.02	-186.70			
	(③-1+②)x0.9	0.85	Max	888.56	1066.62			
			Min	-198.93	-236.83			
	(③-2+②)x0.9	0.85	Max	597.27	687.00			
			Min	-124.22	-168.03			
④		Max	363.69	409.11				
		Min	-30.62	-76.90				
Picked Up Live Load		PICK	Max	888.56	1066.62			
			Min	-198.93	-236.83			
D + L			Max	2266.57	2844.86			
			Min	1179.08	1541.41			
Dead load total				3156.25				

Substructure Reaction Force (Without impact)

				PF2			
		Name or Coefficient		1001	2001		
Dead load				1673.08	1505.83		
AASHTO	Truk	①-1	Max	468.91	441.03		
			Min	-60.95	-59.05		
	Tandem	①-2	Max	332.36	318.33		
			Min	-41.76	-39.78		
Lane Load	Distributed Load	②	Max	382.09	306.35		
			Min	-74.33	-74.14		
AASHTOxTWIN	Truk	③-1	Max	688.12	624.50		
			Min	-103.30	-99.97		
	Tandem	③-2	Max	332.36	318.33		
			Min	-41.76	-39.78		
Lane Load	Distributed Load	②	Max	382.09	306.35		
			Min	-74.33	-74.14		
Special Vehicular Load	Distributed Load	④	Max	330.88	317.88		
			Min	-45.89	-44.32		
Combination of Live Load	①-1+②	0.85	Max	723.35	635.27		
			Min	-114.99	-113.21		
	①-2+②	0.85	Max	607.28	530.98		
			Min	-98.68	-96.83		
	(③-1+②)x0.9	0.85	Max	818.71	712.10		
			Min	-135.89	-133.19		
	(③-2+②)x0.9	0.85	Max	546.55	477.88		
			Min	-88.81	-87.15		
④	1.0	Max	330.88	317.88			
		Min	-45.89	-44.32			
Picked Up Live Load		PICK	Max	818.71	712.10		
			Min	-135.89	-133.19		
D + L			Max	2491.79	2217.93		
			Min	1537.19	1372.64		
Dead load total				3178.91			
Live load total				1530.81			

				PF3			
			Name or Coefficient	1011	2011		
Dead load				5489.00	5567.61		
AASHTO	Truk	①-1	Max	472.54	498.64		
			Min	-48.83	-86.52		
	Tandem	①-2	Max	322.36	337.05		
			Min	-33.30	-59.29		
Lane Load	Distributed Load	②	Max	988.90	1097.83		
			Min	-48.57	-88.89		
AASHTOxTWIN	Truk	③-1	Max	898.06	947.35		
			Min	-76.65	-135.94		
	Tandem	③-2	Max	322.36	337.05		
			Min	-33.30	-59.29		
Lane Load	Distributed Load	②	Max	988.90	1097.83		
			Min	-48.57	-88.89		
Special Vehicular Load	Distributed Load	④	Max	363.99	367.54		
			Min	-36.61	-65.00		
Combination of Live Load	①-1+②	0.85	Max	1242.22	1357.00		
			Min	-82.79	-149.10		
	①-2+②	0.85	Max	1114.57	1219.65		
			Min	-69.59	-125.95		
	(③-1+②)x0.9	0.85	Max	1443.52	1564.56		
			Min	-95.79	-171.99		
	(③-2+②)x0.9	0.85	Max	1003.11	1097.68		
			Min	-62.63	-113.36		
	④	1.0	Max	363.99	367.54		
			Min	-36.61	-65.00		
Picked Up Live Load			PICK	1443.53	1564.56		
D + L			Max	6932.53	7132.17		
			Min	5393.21	5395.61		
Dead load total				11056.61			
Live load total				3008.09			

				PF4				
		Name or Coefficient		1023	2023			
Dead load				5627.64	5485.67			
AASHTO	Truk	①-1	Max	477.93	493.59			
			Min	-80.65	-54.03			
	Tandem	①-2	Max	323.78	335.71			
			Min	-55.20	-36.98			
Lane Load	Distributed Load	②	Max	945.47	1153.14			
			Min	-82.47	-53.75			
AASHTOxTWIN	Truk	③-1	Max	919.45	929.06			
			Min	-127.03	-84.88			
	Tandem	③-2	Max	323.78	335.71			
			Min	-55.20	-36.98			
Lane Load	Distributed Load	②	Max	945.47	1153.14			
			Min	-82.47	-53.75			
Special Vehicular Load	Distributed Load	④	Max	366.82	364.90			
			Min	-60.52	-40.67			
Combination of Live Load	①-1+②	0.85	Max	1209.89	1399.72			
			Min	-138.65	-91.61			
	①-2+②	0.85	Max	1078.86	1265.52			
			Min	-117.02	-77.12			
	(③-1+②)x0.9	0.85	Max	1426.66	1592.88			
			Min	-160.27	-106.05			
	(③-2+②)x0.9	0.85	Max	970.98	1138.97			
			Min	-105.32	-69.41			
	④	1.0	Max	366.82	364.90			
			Min	-60.52	-40.67			
Picked Up Live Load		PICK	Max	1426.67	1592.89			
			Min	-160.27	-106.05			
D + L			Max	7054.31	7078.56			
			Min	5467.37	5379.62			
Dead load total				11113.31				
Live load total				3019.56				

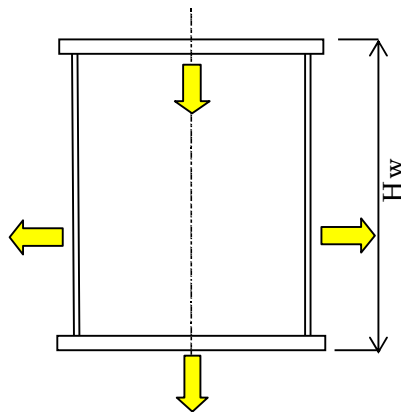
				PF5				
		Name or Coefficient		1033	2033			
Dead load				1378.01	1778.24			
AASHTO	Truk	①-1	Max	431.03	478.69			
			Min	-34.81	-87.79			
	Tandem	①-2	Max	316.86	333.81			
			Min	-23.69	-59.71			
Lane Load	Distributed Load	②	Max	240.12	447.73			
			Min	-42.13	-109.78			
AASHTOxTWIN	Truk	③-1	Max	571.32	739.91			
			Min	-59.06	-148.69			
	Tandem	③-2	Max	316.86	333.81			
			Min	-23.69	-59.71			
Lane Load	Distributed Load	②	Max	240.12	447.73			
			Min	-42.13	-109.78			
Special Vehicular Load	Distributed Load	④	Max	305.17	343.28			
			Min	-26.25	-65.91			
Combination of Live Load	①-1+②	0.85	Max	570.48	787.46			
			Min	-65.40	-167.93			
	①-2+②	0.85	Max	473.43	664.31			
			Min	-55.95	-144.07			
	(③-1+②)x0.9	0.85	Max	620.75	908.54			
			Min	-77.41	-197.73			
	(③-2+②)x0.9	0.85	Max	426.09	597.88			
			Min	-50.35	-129.66			
	④	1.0	Max	305.17	343.28			
			Min	-26.25	-65.91			
Picked Up Live Load		PICK	Max	620.75	908.55			
			Min	-77.41	-197.73			
D + L			Max	1998.76	2686.79			
			Min	1300.60	1580.51			
Dead load total				3156.25				
Live load total				1529.30				

§4.Design of Main Girder
4-1 Design Method

In the design of main girder, the cross section is determined by using the soft where which downloads the cross sectional calculated in §3. and can design Steel-I Girder automatically.

(1) Method for Determination of Cross Section of Stiffener

- 1) The location of cross section change is same with the location of joint.
- 2) Maximum difference of flange thickness is half of the base material or less and 25mm or less.
- 3) Regarding the compressive flange, reduction of stress due to local buckling is considered for upper and lower flange
- 4) Regarding the tensile flange, the cross section is determined considering the influence of bolt.
 Minimum thickness is 1/80 of an interval of longitudinal rib.
- 5) The flange width is constant as 2450mm (125+2200+125 (in horizontal direction)).
 The cross section is changed with the thickness of flange.
- 6) The number of longitudinal ribs is five on the compressive flange and two on the tensile flange.
- 7) The height of the main girder indicates the height from the upper flange top to the upper flange upper.



8) Minimum thicknesses are shown as follows.

The minimum difference of thickness is 2mm and the thickness is measured in increments of 1mm.
 The plate of 4.5mm, 3.2mm and 2.3mm is used for filler plates at the joint if it is less than 6mm.

< Compressive Side >

Material	SM400	SM490Y	SM570
Calculation Equation	$b/(56 \cdot n)$	$b/(46 \cdot n)$	$b/(40 \cdot n)$
Calculated Value	6.55	7.97	9.17
Minimum Thickness of Plate	7.00	8.00	10.00
Interval of Web Plate	b	2200	2200
Division Number	n	6	6

< Tensile Side >

Material	SM400	SM490Y	SM570
Calculation Equation	$b/(80 \cdot n)$	$b/(80 \cdot n)$	$b/(80 \cdot n)$
Calculated Value	9.17	9.17	9.17
Minimum Thickness of Plate	10.00	10.00	10.00
Interval of Web Plate	b	2200	2200
Division Number	n	3	3

< Web Plate >

Horizontal Stiffener is installed in one stage according to the girder height.

The thickness of web plate is decided by the minimum thickness shown in JSHB II

One Stage

Material	SM400	SM490Y	SM570
Calculation Equation	$b/256$	$b/209$	$b/188$
Calculated Value	9.38	11.48	12.77
Minimum Thickness of Plate	10.00	12.00	13.00
Height of Web Plate	b	2400	2400

Note: Height of web plate is the total height.

(2) Design Method for Field Joint

- 1) The joint is designed so that the strength is 75% of the base material or more.
- 2) The minimum number of bolt rows on the compressive flange is two.
- 3) Hole deductions stress of the tensile flange is increased by 1.1 times of net cross sectional area.
- 4) The thickness of splice plate is determined by the stress (75% or more of the total strength)
- 5) The number of bolt rows and the thickness of splice plate is determined on the thinner cross section of the base material at the joint.

(3) Vertical Stiffener

- 1) The cross section is determined as follows according to JSHB II—11.4.4.
 - a) The width of vertical stiffener is the value or more which is the total of 1/30 of web height and 50mm.
 - b) The material is SM400.
 - c) The thickness of vertical stiffener is 1/13 of the width or more.
 - d) The interval of vertical stiffener "a" used in the equation (11.4.7) is the maximum value which satisfies the assessment equation stated in 11.4.3

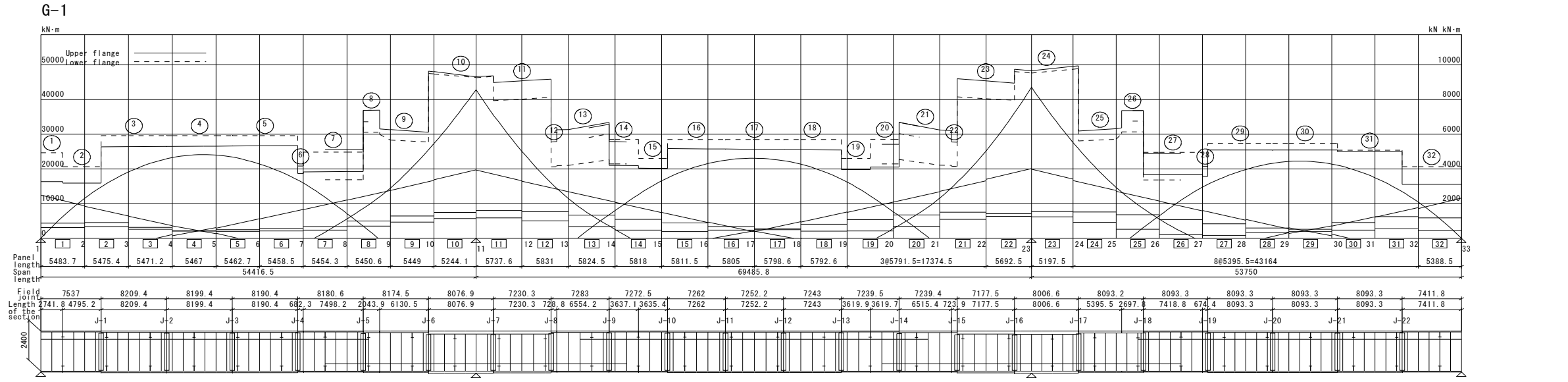
(4) Horizontal Stiffener

- 1) The number of horizontal stiffener rows is one according to the girder height.
The cross section is determined to satisfy the stiffness stated in JSHB II-11.4.7.

(5) Bearing Stiffener

- 1) The bearing stiffener is determined by the structure at the load concentrated point stated in JSHB II-11.5.

STRESS DIAGRAM(1/2) S=1:400



Unit: mm N/mm²

Section	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23
Uflg. W=2450 T	10(3)	10(3)	14(3)	14(3)	11(3)	11(3)	11(3)	18(3)	32(3)	32(3)	16(3)	16(3)	16(3)	11(3)	11(3)	13(3)	13(3)	13(3)	11(3)	11(3)	17(3)	17(3)	34(3)
Upper flange	190	190	190	190	190	190	190	230	230	260	230	230	230	230	230	230	230	230	230	230	230	230	230
Left Web	2426.3	2424.6	2421.7	2412.7	2409.8	2406.9	2401.4	2400.7	2392.4	2392.4	2385.4	2385.4	2383.2	2376.4	2355.9	2355.9	2361.3	2360.5	2352.4	2352.4	2357.4	2357.4	2352.8
Right Web	2353.7	2355.4	2358.3	2359.3	2362.1	2365.1	2376.6	2377.3	2385.6	2385.6	2378.6	2378.6	2380.8	2387.6	2380.1	2380.1	2382.5	2406.7	2407.5	2415.6	2415.6	2420.6	2420.6
Lower flange	190	190	190	190	190	190	190	230	230	260	230	230	230	230	230	230	230	230	230	230	230	230	230
Upper flange	σ	0	-55	-133	-165	-173	-168	-143	-131	-29	71	-20	49	68	176	193	167	121	97	-43	22	-51	27
Lower flange	σ	210	143	143	191	191	158	158	158	210	210	210	210	210	210	210	210	210	210	210	210	210	210
Web	σ	0	53	151	163	171	166	170	135	30	-73	22	-54	-75	-175	-194	-189	-123	-108	48	-25	50	-26
Calculated points	Left	Right	J-1	J-2	J-3	J-4	Left	J-5	J-5	Left	Left	Right	J-6	Max Left	Max Right	J-7	J-8	Left	Right	Right	J-9	J-9	Right
Uflg. σ sp																							
Lflg. σ sp			168	177		181	195		47	109		198								86	46		186

Grade (1): SM400
(2): SM490
(3): SM490Y
(4): SM570

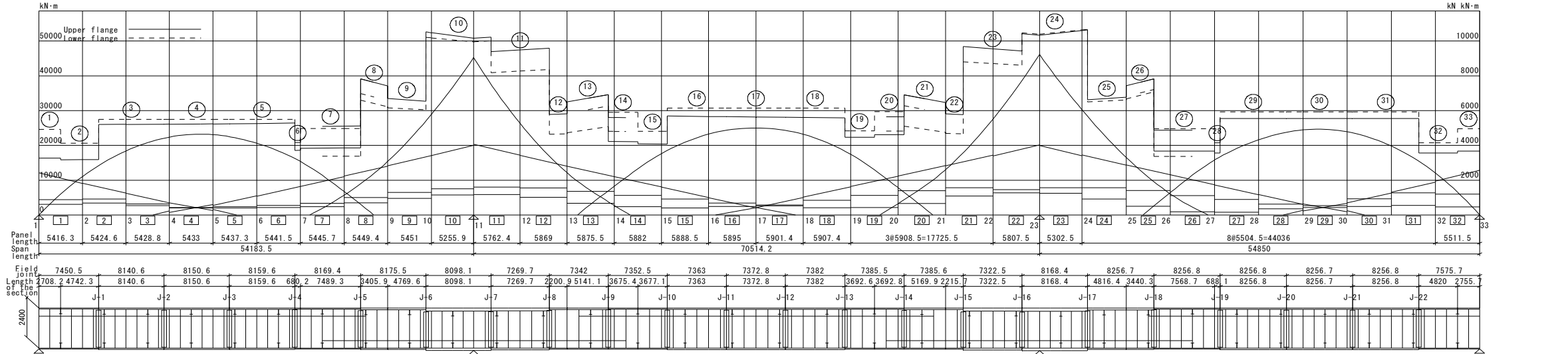
Unit: mm N/mm²

Section	24	25	26	27	28	29	30	31	32
Uflg. W=2450 T	36(3)	20(3)	11(3)	11(3)	11(3)	14(3)	14(3)	14(3)	10(3)
Upper flange	260	230	230	190	190	190	190	190	190
Left Web	2297.9	2297.9	2314	2314	2314	2323	2323	2323	2324
Right Web	2429.9	2429.9	2446	2446	2446	2455	2455	2452	2456
Lower flange	190	190	175	76	-171	49	-26	74	-127
Upper flange	σ	210	210	210	210	210	210	210	210
Lower flange	σ	-192	-192	-175	-83	19	-53	26	-73
Web	σ	66	66	66	53	48	48	57	57
Calculated points	Max Left	Max Right	J-17	Left	Right	Right	J-18	Right	J-21
Uflg. σ sp			196						
Lflg. σ sp					41	184		196	157

Grade (1): SM400
(2): SM490Y
(3): SM490Y
(4): SM570

STRESS DIAGRAM(2/2)

G-2



Section	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23
Upper Flange	190	190	190	190	190	190	190	190	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230
Lower Flange	190	190	190	190	190	190	190	190	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230
Web	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
Calculated points	Left	Right	Left	Right	Left	Right	Left	Right	Left	Right	Left	Right	Left	Right	Left	Right	Left	Right	Left	Right	Left	Right	Left

The stress with "*" mark shows the stress after the main plate thickness is increased.

Section	24	25	26	27	28	29	30	31	32	33
Upper Flange	260	230	230	230	230	230	230	230	230	230
Lower Flange	260	230	230	230	230	230	230	230	230	230
Web	120	120	120	120	120	120	120	120	120	120
Calculated points	Left	Right	Left	Right	Left	Right	Left	Right	Left	Right

The stress with "*" mark shows the stress after the main plate thickness is increased.

4-3 Calculation Result of Field Joint for Main Girder

1) Flange

▪ Main plate

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Flg THK	Flg stress	Req Bolts	Applied Bolts	Bolts Stress	Spl THK	Spl THK	Req Area	Total Area	Group No.
							σ_t	σ_c	τ										
1	G-1	J-1(Sec-1)	UFLG	2450	10	SM490Y	---	-133	37	---	---	30.3	52	65152	9	9	155.6	0.0	*1
4	G-1	J-1(Sec-1)	LFLG	2450	10	SM490Y	168	---	32	---	168	34.2	60	63020	9	9	176.0	0.0	61
5	G-1	J-2(Sec-2)	UFLG	2450	14	SM490Y	---	-165	14	---	---	52.6	78	73028	9	9	270.3	0.0	*4
8	G-1	J-2(Sec-2)	LFLG	2450	18	SM490Y	177	---	10	---	177	66.4	83	86618	12	10	341.6	0.0	115
9	G-1	J-3(Sec-4)	UFLG	2450	14	SM490Y	---	-168	13	---	---	53.4	78	74178	9	9	274.7	0.0	*5
12	G-1	J-3(Sec-4)	LFLG	2450	18	SM490Y	181	---	10	---	181	67.8	83	88349	12	10	348.6	0.0	115
13	G-1	J-4(Sec-5)	UFLG	2450	11	SM490Y	---	-143	30	---	---	35.6	52	75552	9	9	183.2	0.0	*6
16	G-1	J-4(Sec-5)	LFLG	2450	10	SM490Y	189	---	28	---	189	38.5	60	70229	9	9	197.9	0.0	*9
17	G-1	J-5(Sec-5)	UFLG	2450	11	SM490Y	158	118	45	---	100	29.5	52	65622	9	9	129.3	0.0	*10
20	G-1	J-5(Sec-5)	LFLG	2450	10	SM490Y	158	107	48	---	43	24.3	52	55294	9	9	115.8	0.0	*11
21	G-1	J-6(Sec-6)	UFLG	2450	18	SM490Y	199	---	36	---	199	71.7	83	95260	10	12	368.8	0.0	*12
24	G-1	J-6(Sec-6)	LFLG	2450	14	SM490Y	---	-175	48	---	---	55.6	78	79906	9	9	286.2	0.0	46
25	G-1	J-7(Sec-8)	UFLG	2450	32	SM490Y	190	---	25	---	190	122.5	152	87991	19	25	630.1	0.0	*15
28	G-1	J-7(Sec-8)	LFLG	2450	21	SM490Y	---	-189	37	---	---	89.9	104	95115	14	12	462.4	0.0	42
29	G-1	J-8(Sec-9)	UFLG	2450	16	SM490Y	158	---	39	---	138	45.5	60	85752	9	12	234.2	0.0	*18
32	G-1	J-8(Sec-9)	LFLG	2450	11	SM490Y	---	-123	57	---	---	30.6	52	70151	9	9	157.4	0.0	78
33	G-1	J-9(Sec-10)	UFLG	2450	11	SM490Y	158	118	46	---	47	29.6	52	65818	9	9	104.0	0.0	75
36	G-1	J-9(Sec-10)	LFLG	2450	11	SM490Y	158	118	45	---	89	29.5	52	65675	9	9	104.0	0.0	75
37	G-1	J-10(Sec-10)	UFLG	2450	11	SM490Y	---	-136	31	---	---	34.1	52	72523	9	9	175.1	0.0	78
40	G-1	J-10(Sec-10)	LFLG	2450	11	SM490Y	188	---	27	---	188	39.6	60	72350	9	9	203.7	0.0	*24
41	G-1	J-11(Sec-11)	UFLG	2450	13	SM490Y	---	-160	15	---	---	47.1	52	98245	9	9	242.2	0.0	28

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Flg THK	Flg stress	Req Bolts	Applied Bolts	Bolts Stress	Spl THK	Spl THK	Req Area	Total Area	Group No.
							σ_t	σ_c	τ		σ_{tn}	n		ρ	1	2	Ar	As	
44	G-1	J-11(Sec-11)	LFLG	2450	16	SM490Y	189	---	11	---	189	60.2	83	78577	12	9	309.8	0.0	*27
45	G-1	J-12(Sec-13)	UFLG	2450	13	SM490Y	---	-160	14	---	---	47.2	52	98402	9	9	242.7	0.0	*28
48	G-1	J-12(Sec-13)	LFLG	2450	16	SM490Y	188	---	11	---	188	59.9	83	78148	12	9	308.2	0.0	27
49	G-1	J-13(Sec-14)	UFLG	2450	11	SM490Y	---	-137	31	---	---	34.1	52	72696	9	9	175.6	0.0	78
52	G-1	J-13(Sec-14)	LFLG	2450	11	SM490Y	184	---	27	---	184	38.9	60	71035	9	9	200.0	0.0	24
53	G-1	J-14(Sec-14)	UFLG	2450	11	SM490Y	158	118	47	---	52	29.6	52	65957	9	9	104.0	0.0	75
56	G-1	J-14(Sec-14)	LFLG	2450	11	SM490Y	158	118	45	---	84	29.5	52	65706	9	9	104.0	0.0	75
57	G-1	J-15(Sec-15)	UFLG	2450	17	SM490Y	158	---	38	---	139	48.6	60	91282	9	12	249.9	0.0	*35
60	G-1	J-15(Sec-15)	LFLG	2450	11	SM490Y	---	-123	57	---	---	30.7	52	70285	9	9	157.8	0.0	*38
61	G-1	J-16(Sec-16)	UFLG	2450	34	SM490Y	192	---	24	---	192	132.3	152	94954	19	25	680.6	0.0	*39
64	G-1	J-16(Sec-16)	LFLG	2450	21	SM490Y	---	-190	37	---	---	90.7	104	95922	14	12	466.5	0.0	*42
65	G-1	J-17(Sec-18)	UFLG	2450	20	SM490Y	197	---	35	---	197	81.4	106	84486	12	14	418.5	0.0	*43
68	G-1	J-17(Sec-18)	LFLG	2450	14	SM490Y	---	-176	49	---	---	55.8	78	80203	9	9	286.7	0.0	*46
69	G-1	J-18(Sec-19)	UFLG	2450	11	SM490Y	158	118	49	---	105	29.6	52	66357	9	9	129.3	0.0	*47
72	G-1	J-18(Sec-19)	LFLG	2450	10	SM490Y	158	107	51	---	37	24.3	52	55824	9	9	115.8	0.0	11
73	G-1	J-19(Sec-19)	UFLG	2450	11	SM490Y	---	-139	32	---	---	34.6	52	73735	9	9	178.0	0.0	6
76	G-1	J-19(Sec-19)	LFLG	2450	10	SM490Y	176	---	30	---	176	35.7	60	65496	9	9	183.8	0.0	*48
77	G-1	J-20(Sec-20)	UFLG	2450	14	SM490Y	---	-163	13	---	---	51.9	78	72059	9	9	266.8	0.0	4
80	G-1	J-20(Sec-20)	LFLG	2450	16	SM490Y	181	---	11	---	181	60.1	83	78314	12	9	308.9	0.0	56
81	G-1	J-21(Sec-22)	UFLG	2450	14	SM490Y	---	-162	16	---	---	51.4	78	71460	9	9	264.2	0.0	4
84	G-1	J-21(Sec-22)	LFLG	2450	14	SM490Y	192	---	15	---	192	55.4	60	100143	10	9	285.1	0.0	*51
85	G-1	J-22(Sec-23)	UFLG	2450	10	SM490Y	---	-125	39	---	---	28.3	52	61506	9	9	145.3	0.0	1
88	G-1	J-22(Sec-23)	LFLG	2450	10	SM490Y	158	---	35	---	153	31.1	60	57720	9	9	159.9	0.0	61
89	G-2	J-1(Sec-1)	UFLG	2450	10	SM490Y	---	-128	36	---	---	29.0	52	62628	9	9	149.2	0.0	1
92	G-2	J-1(Sec-1)	LFLG	2450	10	SM490Y	161	---	32	---	161	32.8	60	60530	9	9	168.8	0.0	61
93	G-2	J-2(Sec-2)	UFLG	2450	14	SM490Y	---	-162	14	---	---	51.3	78	71280	9	9	263.8	0.0	4
96	G-2	J-2(Sec-2)	LFLG	2450	16	SM490Y	185	---	11	---	185	61.2	83	79849	12	9	314.9	0.0	*56

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Flg THK	Flg stress	Req Bolts	Applied Bolts	Bolts Stress	Spl THK	Spl THK	Req Area	Total Area	Group No.
							σ_t	σ_c	τ		σ_{tn}	n		ρ	1	2	Ar	As	
97	G-2	J-3(Sec-4)	UFLG	2450	14	SM490Y	---	-164	13	---	---	52.1	78	72325	9	10	267.9	0.0	*57
100	G-2	J-3(Sec-4)	LFLG	2450	16	SM490Y	188	---	10	---	188	62.4	83	81369	12	9	321.0	0.0	*60
101	G-2	J-4(Sec-5)	UFLG	2450	11	SM490Y	---	-138	29	---	---	34.4	52	73055	9	9	177.0	0.0	107
104	G-2	J-4(Sec-5)	LFLG	2450	10	SM490Y	183	---	28	---	183	37.2	60	67893	9	9	191.3	0.0	*61
105	G-2	J-5(Sec-5)	UFLG	2450	11	SM490Y	158	118	46	---	104	29.5	52	65765	9	9	129.3	0.0	103
108	G-2	J-5(Sec-5)	LFLG	2450	10	SM490Y	158	107	49	---	38	24.3	52	55457	9	9	115.8	0.0	106
109	G-2	J-6(Sec-6)	UFLG	2450	20	SM490Y	196	---	34	---	196	79.0	83	104669	12	15	406.2	0.0	*64
112	G-2	J-6(Sec-6)	LFLG	2450	15	SM490Y	---	-178	46	---	---	60.6	78	86678	10	9	311.8	0.0	*67
113	G-2	J-7(Sec-8)	UFLG	2450	34	SM490Y	190	---	24	---	190	131.1	152	94101	20	24	674.3	0.0	*68
116	G-2	J-7(Sec-8)	LFLG	2450	22	SM490Y	---	-193	36	---	---	96.3	130	81374	15	13	495.2	0.0	*71
117	G-2	J-8(Sec-9)	UFLG	2450	17	SM490Y	158	---	38	---	139	48.6	60	91329	10	12	249.9	0.0	*72
120	G-2	J-8(Sec-9)	LFLG	2450	12	SM490Y	---	128	55	---	---	34.8	52	78661	9	9	179.2	0.0	86
121	G-2	J-9(Sec-10)	UFLG	2450	11	SM490Y	158	118	48	---	50	29.6	52	66202	9	9	104.0	0.0	*75
124	G-2	J-9(Sec-10)	LFLG	2450	12	SM490Y	158	128	44	---	84	34.8	52	76461	9	9	117.5	0.0	*77
125	G-2	J-10(Sec-10)	UFLG	2450	11	SM490Y	---	-144	33	---	---	36.0	52	76634	9	9	185.1	0.0	*78
128	G-2	J-10(Sec-10)	LFLG	2450	12	SM490Y	190	---	27	---	190	44.1	60	80486	9	9	226.9	0.0	*81
129	G-2	J-11(Sec-11)	UFLG	2450	14	SM490Y	---	-165	14	---	---	52.4	78	72884	9	9	269.7	0.0	46
132	G-2	J-11(Sec-11)	LFLG	2450	18	SM490Y	188	---	11	---	188	68.0	83	88608	12	10	349.5	0.0	12
133	G-2	J-12(Sec-13)	UFLG	2450	14	SM490Y	---	-166	14	---	---	52.7	78	73280	9	9	271.2	0.0	46
136	G-2	J-12(Sec-13)	LFLG	2450	18	SM490Y	188	---	10	---	188	67.9	83	88474	12	10	349.0	0.0	12
137	G-2	J-13(Sec-14)	UFLG	2450	12	SM490Y	---	-141	30	---	---	38.4	52	81614	9	9	197.7	0.0	*86
140	G-2	J-13(Sec-14)	LFLG	2450	12	SM490Y	187	---	26	---	187	43.5	60	79379	9	9	223.8	0.0	*89
141	G-2	J-14(Sec-14)	UFLG	2450	12	SM490Y	158	128	46	---	56	34.9	52	76831	9	9	117.5	0.0	77
144	G-2	J-14(Sec-14)	LFLG	2450	12	SM490Y	158	128	44	---	79	34.8	52	76590	9	9	117.5	0.0	77
145	G-2	J-15(Sec-15)	UFLG	2450	18	SM490Y	158	---	37	---	147	53.2	60	99561	10	12	273.6	0.0	*92
148	G-2	J-15(Sec-15)	LFLG	2450	12	SM490Y	---	-131	55	---	---	35.7	52	80342	9	9	183.6	0.0	86
149	G-2	J-16(Sec-16)	UFLG	2450	36	SM490Y	195	---	23	---	195	142.4	152	102044	20	24	732.3	0.0	*95

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Flg THK	Flg stress	Req Bolts	Applied Bolts	Bolts Stress	Spl THK	Spl THK	Req Area	Total Area	Group No.
							σ_t	σ_c	τ		σ_{tn}	n		ρ	1	2	Ar	As	
152	G-2	J-16(Sec-16)	LFLG	2450	24	SM490Y	---	-189	33	---	---	102.7	130	86578	15	13	528.1	0.0	*98
153	G-2	J-17(Sec-18)	UFLG	2450	22	SM490Y	201	---	33	---	201	91.8	106	95026	12	15	472.0	0.0	*99
156	G-2	J-17(Sec-18)	LFLG	2450	16	SM490Y	---	-180	45	---	---	65.2	78	93023	10	9	335.1	0.0	*102
157	G-2	J-18(Sec-19)	UFLG	2450	11	SM490Y	158	118	52	---	117	29.6	52	66989	9	9	129.3	0.0	*103
160	G-2	J-18(Sec-19)	LFLG	2450	10	SM490Y	158	107	54	---	32	24.3	52	56505	9	9	115.8	0.0	*106
161	G-2	J-19(Sec-19)	UFLG	2450	11	SM490Y	---	-149	34	---	---	37.2	52	79222	9	9	191.2	0.0	*107
164	G-2	J-19(Sec-19)	LFLG	2450	10	SM490Y	189	---	32	---	189	38.4	60	70354	9	9	197.4	0.0	*110
165	G-2	J-20(Sec-20)	UFLG	2450	15	SM490Y	---	-171	14	---	---	58.3	78	80951	9	10	299.7	0.0	*111
168	G-2	J-20(Sec-20)	LFLG	2450	18	SM490Y	183	---	11	---	183	68.7	83	89532	12	10	353.1	0.0	*114
169	G-2	J-21(Sec-22)	UFLG	2450	15	SM490Y	---	-170	15	---	---	57.8	78	80405	9	10	297.5	0.0	111
172	G-2	J-21(Sec-22)	LFLG	2450	18	SM490Y	182	---	12	---	182	68.2	83	88912	12	10	350.5	0.0	*115
173	G-2	J-22(Sec-23)	UFLG	2450	11	SM490Y	---	-138	38	---	---	34.3	52	73931	9	9	176.6	0.0	*116
176	G-2	J-22(Sec-23)	LFLG	2450	10	SM490Y	174	---	36	---	174	35.5	60	65495	9	9	182.3	0.0	61
										※ 1							※ 2	※ 2	

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Mem No.	Girder Name	Joint Name	Member	Section dimensions			σ_{tr}	thickness up	Req Bolts	Applied Bolts	Spl THK	Spl THK	Req Area	Total Area	Group No.
								t	n		1	2	Arr	Asr	
1	G-1	J-1(Sec-1)	UFLG	5-RIB	PL	190 * 19	---	---	22.3	25	16	16	114.6	184.0	*1
4	G-1	J-1(Sec-1)	LFLG	2-RIB	PL	190 * 19	0	---	10.5	12	19	19	54.1	73.6	61
5	G-1	J-2(Sec-2)	UFLG	5-RIB	PL	190 * 19	---	---	27.7	30	16	16	142.2	184.0	*4
8	G-1	J-2(Sec-2)	LFLG	2-RIB	PL	190 * 19	0	---	10.9	12	19	19	55.9	73.6	115
9	G-1	J-3(Sec-4)	UFLG	5-RIB	PL	190 * 19	---	---	28.1	35	16	16	144.6	184.0	*5
12	G-1	J-3(Sec-4)	LFLG	2-RIB	PL	190 * 19	0	---	11.1	12	19	19	57.1	73.6	115
13	G-1	J-4(Sec-5)	UFLG	5-RIB	PL	190 * 19	---	---	23.9	35	16	16	122.7	184.0	*6
16	G-1	J-4(Sec-5)	LFLG	2-RIB	PL	190 * 19	0	---	11.6	18	19	19	58.3	73.6	*9
17	G-1	J-5(Sec-5)	UFLG	5-RIB	PL	190 * 19	0	---	26.3	35	19	19	135.4	183.9	*10
20	G-1	J-5(Sec-5)	LFLG	5-RIB	PL	190 * 19	0	---	26.3	35	19	19	135.4	183.9	*11
21	G-1	J-6(Sec-6)	UFLG	2-RIB	PL	230 * 22	0	---	16.5	20	22	22	84.6	97.8	*12
24	G-1	J-6(Sec-6)	LFLG	5-RIB	PL	230 * 22	---	---	41.0	50	19	19	211.1	294.5	46
25	G-1	J-7(Sec-8)	UFLG	2-RIB	PL	230 * 22	0	---	15.6	20	22	22	80.4	97.8	*15
28	G-1	J-7(Sec-8)	LFLG	5-RIB	PL	230 * 22	---	---	44.2	50	19	19	227.4	294.5	42
29	G-1	J-8(Sec-9)	UFLG	2-RIB	PL	230 * 22	0	---	14.8	16	22	22	75.9	97.8	*18
32	G-1	J-8(Sec-9)	LFLG	5-RIB	PL	230 * 22	---	---	28.7	40	19	19	147.8	294.5	78
33	G-1	J-9(Sec-10)	UFLG	5-RIB	PL	230 * 22	0	---	36.9	40	22	22	189.8	244.4	75
36	G-1	J-9(Sec-10)	LFLG	5-RIB	PL	230 * 22	0	---	36.9	40	22	22	189.8	244.4	75
37	G-1	J-10(Sec-10)	UFLG	5-RIB	PL	230 * 22	---	---	32.0	40	19	19	164.4	294.5	78
40	G-1	J-10(Sec-10)	LFLG	2-RIB	PL	230 * 22	0	---	14.9	16	22	22	76.5	97.8	*24
41	G-1	J-11(Sec-11)	UFLG	5-RIB	PL	230 * 22	---	---	37.4	40	19	19	192.4	294.5	28
44	G-1	J-11(Sec-11)	LFLG	2-RIB	PL	230 * 22	0	---	15.6	20	22	22	80.0	97.8	*27
45	G-1	J-12(Sec-13)	UFLG	5-RIB	PL	230 * 22	---	---	37.5	40	19	19	192.8	294.5	*28
48	G-1	J-12(Sec-13)	LFLG	2-RIB	PL	230 * 22	0	---	15.5	20	22	22	79.6	97.8	27
49	G-1	J-13(Sec-14)	UFLG	5-RIB	PL	230 * 22	---	---	32.1	40	19	19	164.8	294.5	78

Mem No.	Girder Name	Joint Name	Member	Section dimensions			σ _{tr}	thickness up t	Req Bolts n	Applied Bolts	Spl THK 1	Spl THK 2	Req Area Arr	Total Area Asr	Group No.
52	G-1	J-13(Sec-14)	LFLG	2-RIB	PL	230 * 22	0	---	14.8	16	22	22	75.9	97.8	24
53	G-1	J-14(Sec-14)	UFLG	5-RIB	PL	230 * 22	0	---	36.9	40	22	22	189.8	244.4	75
56	G-1	J-14(Sec-14)	LFLG	5-RIB	PL	230 * 22	0	---	36.9	40	22	22	189.8	244.4	75
57	G-1	J-15(Sec-15)	UFLG	2-RIB	PL	230 * 22	0	---	14.8	16	22	22	75.9	97.8	*35
60	G-1	J-15(Sec-15)	LFLG	5-RIB	PL	230 * 22	---	---	28.8	30	19	19	148.2	294.5	*38
61	G-1	J-16(Sec-16)	UFLG	2-RIB	PL	230 * 22	0	---	15.9	20	22	22	81.7	97.8	*39
64	G-1	J-16(Sec-16)	LFLG	5-RIB	PL	230 * 22	---	---	44.6	50	19	19	229.4	294.5	*42
65	G-1	J-17(Sec-18)	UFLG	2-RIB	PL	230 * 22	0	---	16.4	20	22	22	84.4	97.8	*43
68	G-1	J-17(Sec-18)	LFLG	5-RIB	PL	230 * 22	---	---	41.1	50	19	19	211.5	294.5	*46
69	G-1	J-18(Sec-19)	UFLG	5-RIB	PL	190 * 19	0	---	26.3	35	19	19	135.4	183.9	*47
72	G-1	J-18(Sec-19)	LFLG	5-RIB	PL	190 * 19	0	---	26.3	35	19	19	135.4	183.9	11
73	G-1	J-19(Sec-19)	UFLG	5-RIB	PL	190 * 19	---	---	23.2	35	16	16	119.2	184.0	6
76	G-1	J-19(Sec-19)	LFLG	2-RIB	PL	190 * 19	0	---	10.5	16	19	19	54.2	73.6	*48
77	G-1	J-20(Sec-20)	UFLG	5-RIB	PL	190 * 19	---	---	27.3	30	16	16	140.4	184.0	4
80	G-1	J-20(Sec-20)	LFLG	2-RIB	PL	190 * 19	0	---	11.1	12	19	19	56.9	73.6	56
81	G-1	J-21(Sec-22)	UFLG	5-RIB	PL	190 * 19	---	---	27.0	30	16	16	139.0	184.0	4
84	G-1	J-21(Sec-22)	LFLG	2-RIB	PL	190 * 19	0	---	11.7	14	19	19	60.0	73.6	*51
85	G-1	J-22(Sec-23)	UFLG	5-RIB	PL	190 * 19	---	---	20.8	25	16	16	107.1	184.0	1
88	G-1	J-22(Sec-23)	LFLG	2-RIB	PL	190 * 19	0	---	10.5	12	19	19	54.1	73.6	61
89	G-2	J-1(Sec-1)	UFLG	5-RIB	PL	190 * 19	---	---	21.4	25	16	16	109.9	184.0	1
92	G-2	J-1(Sec-1)	LFLG	2-RIB	PL	190 * 19	0	---	10.5	12	19	19	54.1	73.6	61
93	G-2	J-2(Sec-2)	UFLG	5-RIB	PL	190 * 19	---	---	27.0	30	16	16	138.8	184.0	4
96	G-2	J-2(Sec-2)	LFLG	2-RIB	PL	190 * 19	0	---	11.3	12	19	19	58.0	73.6	*56
97	G-2	J-3(Sec-4)	UFLG	5-RIB	PL	190 * 19	---	---	27.4	30	16	16	141.0	184.0	*57
100	G-2	J-3(Sec-4)	LFLG	2-RIB	PL	190 * 19	0	---	11.5	14	19	19	59.1	73.6	*60
101	G-2	J-4(Sec-5)	UFLG	5-RIB	PL	190 * 19	---	---	23.1	30	16	16	118.6	184.0	107
104	G-2	J-4(Sec-5)	LFLG	2-RIB	PL	190 * 19	0	---	11.0	12	19	19	56.4	73.6	*61

Mem No.	Girder Name	Joint Name	Member	Section dimensions			σ _{tr}	thickness	Req	Applied	Spl	Spl	Req	Total	Group No.
								up	Bolts	Bolts	THK	THK	Area	Area	
							t	n			1	2	Arr	Asr	
105	G-2	J-5(Sec-5)	UFLG	5-RIB	PL	190 * 19	0	---	26.3	30	19	19	135.4	183.9	103
108	G-2	J-5(Sec-5)	LFLG	5-RIB	PL	190 * 19	0	---	26.3	30	19	19	135.4	183.9	106
109	G-2	J-6(Sec-6)	UFLG	2-RIB	PL	230 * 22	0	---	16.3	20	22	22	83.9	97.8	*64
112	G-2	J-6(Sec-6)	LFLG	5-RIB	PL	230 * 22	---	---	41.7	50	19	19	214.6	294.5	*67
113	G-2	J-7(Sec-8)	UFLG	2-RIB	PL	230 * 22	0	---	15.7	20	22	22	81.0	97.8	*68
116	G-2	J-7(Sec-8)	LFLG	5-RIB	PL	230 * 22	---	---	45.2	50	19	19	232.4	294.5	*71
117	G-2	J-8(Sec-9)	UFLG	2-RIB	PL	230 * 22	0	---	14.8	16	22	22	75.9	97.8	*72
120	G-2	J-8(Sec-9)	LFLG	5-RIB	PL	230 * 22	---	---	30.0	40	19	19	154.2	294.5	86
121	G-2	J-9(Sec-10)	UFLG	5-RIB	PL	230 * 22	0	---	36.9	40	22	22	189.8	244.4	*75
124	G-2	J-9(Sec-10)	LFLG	5-RIB	PL	230 * 22	0	---	36.9	40	22	22	189.8	244.4	*77
125	G-2	J-10(Sec-10)	UFLG	5-RIB	PL	230 * 22	---	---	33.8	40	19	19	173.8	294.5	*78
128	G-2	J-10(Sec-10)	LFLG	2-RIB	PL	230 * 22	0	---	15.2	20	22	22	78.1	97.8	*81
129	G-2	J-11(Sec-11)	UFLG	5-RIB	PL	230 * 22	---	---	38.7	50	19	19	198.9	294.5	46
132	G-2	J-11(Sec-11)	LFLG	2-RIB	PL	230 * 22	0	---	15.6	20	22	22	80.2	97.8	12
133	G-2	J-12(Sec-13)	UFLG	5-RIB	PL	230 * 22	---	---	38.9	50	19	19	200.1	294.5	46
136	G-2	J-12(Sec-13)	LFLG	2-RIB	PL	230 * 22	0	---	15.6	20	22	22	80.1	97.8	12
137	G-2	J-13(Sec-14)	UFLG	5-RIB	PL	230 * 22	---	---	33.1	40	19	19	170.1	294.5	*86
140	G-2	J-13(Sec-14)	LFLG	2-RIB	PL	230 * 22	0	---	15.0	16	22	22	77.0	97.8	*89
141	G-2	J-14(Sec-14)	UFLG	5-RIB	PL	230 * 22	0	---	36.9	40	22	22	189.8	244.4	77
144	G-2	J-14(Sec-14)	LFLG	5-RIB	PL	230 * 22	0	---	36.9	40	22	22	189.8	244.4	77
145	G-2	J-15(Sec-15)	UFLG	2-RIB	PL	230 * 22	0	---	14.8	16	22	22	75.9	97.8	*92
148	G-2	J-15(Sec-15)	LFLG	5-RIB	PL	230 * 22	---	---	30.7	40	19	19	158.0	294.5	86
149	G-2	J-16(Sec-16)	UFLG	2-RIB	PL	230 * 22	0	---	16.1	20	22	22	83.0	97.8	*95
152	G-2	J-16(Sec-16)	LFLG	5-RIB	PL	230 * 22	---	---	44.2	50	19	19	227.2	294.5	*98
153	G-2	J-17(Sec-18)	UFLG	2-RIB	PL	230 * 22	0	---	16.8	20	22	22	86.5	97.8	*99
156	G-2	J-17(Sec-18)	LFLG	5-RIB	PL	230 * 22	---	---	42.0	50	19	19	216.3	294.5	*102
157	G-2	J-18(Sec-19)	UFLG	5-RIB	PL	190 * 19	0	---	26.3	30	19	19	135.4	183.9	*103

Mem No.	Girder Name	Joint Name	Member	Section dimensions			σ_{tr}	thickness up	Req Bolts	Applied Bolts	Spl THK	Spl THK	Req Area	Total Area	Group No.
								t	n		1	2	Arr	Asr	
160	G-2	J-18(Sec-19)	LFLG	5-RIB	PL	190 * 19	0	---	26.3	30	19	19	135.4	183.9	*106
161	G-2	J-19(Sec-19)	UFLG	5-RIB	PL	190 * 19	---	---	24.9	30	16	16	128.1	184.0	*107
164	G-2	J-19(Sec-19)	LFLG	2-RIB	PL	190 * 19	0	---	11.3	14	19	19	58.2	73.6	*110
165	G-2	J-20(Sec-20)	UFLG	5-RIB	PL	190 * 19	---	---	28.6	35	16	16	147.2	184.0	*111
168	G-2	J-20(Sec-20)	LFLG	2-RIB	PL	190 * 19	0	---	11.2	14	19	19	57.8	73.6	*114
169	G-2	J-21(Sec-22)	UFLG	5-RIB	PL	190 * 19	---	---	28.4	35	16	16	146.1	184.0	111
172	G-2	J-21(Sec-22)	LFLG	2-RIB	PL	190 * 19	0	---	11.2	12	19	19	57.4	73.6	*115
173	G-2	J-22(Sec-23)	UFLG	5-RIB	PL	190 * 19	---	---	23.0	25	16	16	118.3	184.0	*116
176	G-2	J-22(Sec-23)	LFLG	2-RIB	PL	190 * 19	0	---	10.5	12	19	19	54.1	73.6	61
											※4	※4	※2※3	※2※3	

※Display in the case of thickness up only

If both the tensile Stress and Compressive Stress occurs, the one with the lower difference of Ar and As, will be applied,.

Omit in the case of required area includes flange section area.

All members * of Group No. means the representative member

2) Web

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Joint Type	Applied Bolts			Bolts Stress	Spl THK		Group No.
							σ_{Un}	σ_{Ln}	τ			P	Req Bolts	ρ	l	σ_{sp}	
2	G-1	J-1(Sec-1)	LWEB	2422	12	SM490Y	-139	158	39	w(s)	72	262783	3	89018	9	118	*2
3	G-1	J-1(Sec-1)	RWEB	2358	12	SM490Y	-131	158	39	w(s)	72	262783	3	88947	9	118	*3
6	G-1	J-2(Sec-2)	LWEB	2413	12	SM490Y	-163	160	20	w(s)	72	265326	3	88806	9	122	54
7	G-1	J-2(Sec-2)	RWEB	2359	12	SM490Y	-157	160	20	w(s)	72	266105	3	89051	9	119	55
10	G-1	J-3(Sec-4)	LWEB	2407	12	SM490Y	-166	163	19	w(s)	72	271030	3	90655	9	124	58
11	G-1	J-3(Sec-4)	RWEB	2365	12	SM490Y	-161	164	19	w(s)	72	271538	3	90815	9	122	59
14	G-1	J-4(Sec-5)	LWEB	2401	12	SM490Y	-141	168	36	w(s)	72	280767	3	94667	9	126	*7
15	G-1	J-4(Sec-5)	RWEB	2377	12	SM490Y	-138	168	36	w(s)	72	281142	3	94770	9	126	*8
18	G-1	J-5(Sec-5)	LWEB	2392	12	SM490Y	153	-158	55	w(s)	72	261851	3	89967	9	118	62
19	G-1	J-5(Sec-5)	RWEB	2386	12	SM490Y	152	-158	55	w(s)	72	261851	3	89953	9	118	63
22	G-1	J-6(Sec-6)	궂	2376	14	SM490Y	171	-173	63	w(s)	96	340206	4	87788	9	153	*13
23	G-1	J-6(Sec-6)	RWEB	2388	14	SM490Y	173	-173	63	w(s)	96	343489	4	88604	9	153	*14
26	G-1	J-7(Sec-8)	LWEB	2354	16	SM490Y	158	-186	62	w(s)	120	412733	5	84821	10	166	*16
27	G-1	J-7(Sec-8)	RWEB	2382	16	SM490Y	162	-185	62	w(s)	120	411964	5	84709	10	166	*17
30	G-1	J-8(Sec-9)	LWEB	2361	14	SM490Y	149	-158	59	w(s)	96	305480	4	79039	9	140	*19
31	G-1	J-8(Sec-9)	RWEB	2407	14	SM490Y	155	-158	59	w(s)	96	311101	4	80485	9	139	*20
34	G-1	J-9(Sec-10)	LWEB	2357	12	SM490Y	-153	158	53	w(s)	72	261565	3	89604	9	118	*21
35	G-1	J-9(Sec-10)	RWEB	2421	12	SM490Y	-158	153	52	w(s)	72	254879	3	87556	9	118	76
38	G-1	J-10(Sec-10)	LWEB	2348	12	SM490Y	-126	158	35	w(s)	72	263038	3	88737	9	118	*22
39	G-1	J-10(Sec-10)	RWEB	2430	12	SM490Y	-135	158	35	w(s)	72	263038	3	88803	9	117	*23
42	G-1	J-11(Sec-11)	LWEB	2337	12	SM490Y	-145	164	19	w(s)	72	272717	3	91216	9	122	*25
43	G-1	J-11(Sec-11)	RWEB	2437	12	SM490Y	-157	163	19	w(s)	72	271162	3	90722	9	121	*26
46	G-1	J-12(Sec-13)	LWEB	2328	12	SM490Y	-143	163	19	w(s)	72	271257	3	90715	9	122	*29
47	G-1	J-12(Sec-13)	RWEB	2446	12	SM490Y	-157	162	19	w(s)	72	269503	3	90158	9	120	*30
50	G-1	J-13(Sec-14)	LWEB	2324	12	SM490Y	-123	158	35	w(s)	72	263043	3	88708	9	118	*31

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Joint Type	Applied Bolts			Bolts Stress	Spl THK		Group No.
							σ_{Un}	σ_{Ln}	τ			P	Req Bolts	ρ	l	σ_{sp}	
51	G-1	J-13(Sec-14)	RWEB	2454	12	SM490Y	-138	158	35	w(s)	72	263043	3	88814	9	117	*32
54	G-1	J-14(Sec-14)	LWEB	2323	12	SM490Y	-149	158	53	w(s)	72	261572	3	89558	9	118	*33
55	G-1	J-14(Sec-14)	RWEB	2455	12	SM490Y	-158	149	53	w(s)	72	255768	3	87924	9	118	*34
58	G-1	J-15(Sec-15)	LWEB	2317	14	SM490Y	139	-158	59	w(s)	96	305761	4	79032	9	140	*36
59	G-1	J-15(Sec-15)	RWEB	2449	14	SM490Y	156	-158	59	w(s)	96	315395	4	81611	9	139	*37
62	G-1	J-16(Sec-16)	LWEB	2300	16	SM490Y	146	-187	63	w(s)	120	416809	5	85553	10	169	*40
63	G-1	J-16(Sec-16)	RWEB	2432	16	SM490Y	164	-186	62	w(s)	120	413915	5	85159	10	166	*41
66	G-1	J-17(Sec-18)	LWEB	2314	14	SM490Y	154	-174	64	w(s)	96	336742	4	86937	9	154	*44
67	G-1	J-17(Sec-18)	RWEB	2446	14	SM490Y	171	-172	64	w(s)	96	345014	4	89186	9	152	*45
70	G-1	J-18(Sec-19)	LWEB	2323	12	SM490Y	143	-158	57	w(s)	72	261861	3	90003	9	119	104
71	G-1	J-18(Sec-19)	RWEB	2455	12	SM490Y	158	-154	56	w(s)	72	260520	3	89859	9	118	105
74	G-1	J-19(Sec-19)	LWEB	2323	12	SM490Y	-123	158	37	w(s)	72	263033	3	88813	9	118	108
75	G-1	J-19(Sec-19)	RWEB	2455	12	SM490Y	-139	158	36	w(s)	72	263033	3	88935	9	117	109
78	G-1	J-20(Sec-20)	LWEB	2320	12	SM490Y	-144	163	19	w(s)	72	271702	3	90863	9	122	49
79	G-1	J-20(Sec-20)	RWEB	2452	12	SM490Y	-161	162	19	w(s)	72	269820	3	90267	9	120	50
82	G-1	J-21(Sec-22)	LWEB	2320	12	SM490Y	-142	173	22	w(s)	72	287805	3	96309	9	129	*49
83	G-1	J-21(Sec-22)	RWEB	2452	12	SM490Y	-159	171	22	w(s)	72	285810	3	95683	9	127	*50
86	G-1	J-22(Sec-23)	LWEB	2324	12	SM490Y	-127	158	41	w(s)	72	262790	3	88990	9	118	*52
87	G-1	J-22(Sec-23)	RWEB	2456	12	SM490Y	-143	158	40	w(s)	72	262790	3	89143	9	117	*53
90	G-2	J-1(Sec-1)	LWEB	2422	12	SM490Y	-139	158	39	w(s)	72	262783	3	88990	9	118	2
91	G-2	J-1(Sec-1)	RWEB	2358	12	SM490Y	-131	158	39	w(s)	72	262783	3	88921	9	118	3
94	G-2	J-2(Sec-2)	LWEB	2413	12	SM490Y	-159	166	20	w(s)	72	276224	3	92416	9	123	*54
95	G-2	J-2(Sec-2)	RWEB	2359	12	SM490Y	-153	166	20	w(s)	72	277041	3	92675	9	124	*55
98	G-2	J-3(Sec-4)	LWEB	2407	12	SM490Y	-162	169	18	w(s)	72	281927	3	94263	9	126	*58
99	G-2	J-3(Sec-4)	RWEB	2365	12	SM490Y	-156	170	18	w(s)	72	282458	3	94431	9	127	*59
102	G-2	J-4(Sec-5)	LWEB	2401	12	SM490Y	-136	162	35	w(s)	72	271308	3	91510	9	121	7
103	G-2	J-4(Sec-5)	RWEB	2377	12	SM490Y	-133	163	35	w(s)	72	271673	3	91610	9	122	8

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Joint Type	Applied Bolts			Bolts Stress	Spl THK		Group No.
							σ_{Un}	σ_{Ln}	τ			P	Req Bolts	ρ	l	σ_{sp}	
106	G-2	J-5(Sec-5)	LWEB	2392	12	SM490Y	153	-158	56	w(s)	72	261851	3	90062	9	118	*62
107	G-2	J-5(Sec-5)	RWEB	2386	12	SM490Y	152	-158	56	w(s)	72	261851	3	90047	9	118	*63
110	G-2	J-6(Sec-6)	LWEB	2374	14	SM490Y	170	-176	64	w(s)	96	341205	4	88117	9	156	*65
111	G-2	J-6(Sec-6)	RWEB	2386	14	SM490Y	171	-176	64	w(s)	96	341060	4	88103	9	155	*66
114	G-2	J-7(Sec-8)	LWEB	2352	16	SM490Y	159	-190	64	w(s)	120	421773	5	86704	10	170	*69
115	G-2	J-7(Sec-8)	RWEB	2380	16	SM490Y	163	-189	64	w(s)	120	420990	5	86590	10	169	*70
118	G-2	J-8(Sec-9)	LWEB	2360	14	SM490Y	149	-158	61	w(s)	96	305462	4	79216	9	140	*73
119	G-2	J-8(Sec-9)	RWEB	2406	14	SM490Y	155	-158	61	w(s)	96	311398	4	80738	9	139	*74
122	G-2	J-9(Sec-10)	LWEB	2357	12	SM490Y	-158	157	55	w(s)	72	260407	3	89468	9	118	21
123	G-2	J-9(Sec-10)	RWEB	2421	12	SM490Y	-158	149	55	w(s)	72	253898	3	87495	9	118	*76
126	G-2	J-10(Sec-10)	LWEB	2348	12	SM490Y	-133	161	37	w(s)	72	267803	3	90429	9	120	*79
127	G-2	J-10(Sec-10)	RWEB	2430	12	SM490Y	-142	160	37	w(s)	72	266502	3	90074	9	119	*80
130	G-2	J-11(Sec-11)	LWEB	2336	12	SM490Y	-150	164	20	w(s)	72	272652	3	91224	9	122	*82
131	G-2	J-11(Sec-11)	RWEB	2436	12	SM490Y	-163	163	20	w(s)	72	271124	3	90740	9	121	*83
134	G-2	J-12(Sec-13)	LWEB	2327	12	SM490Y	-149	164	20	w(s)	72	272282	3	91076	9	122	*84
135	G-2	J-12(Sec-13)	RWEB	2445	12	SM490Y	-163	163	19	w(s)	72	270553	3	90528	9	122	*85
138	G-2	J-13(Sec-14)	LWEB	2323	12	SM490Y	-124	158	37	w(s)	72	264366	3	89262	9	119	*87
139	G-2	J-13(Sec-14)	RWEB	2453	12	SM490Y	-139	158	37	w(s)	72	262993	3	88926	9	117	*88
142	G-2	J-14(Sec-14)	LWEB	2322	12	SM490Y	-149	158	56	w(s)	72	261565	3	89858	9	118	*90
143	G-2	J-14(Sec-14)	RWEB	2454	12	SM490Y	-158	149	56	w(s)	72	255762	3	88254	9	118	*91
146	G-2	J-15(Sec-15)	LWEB	2316	14	SM490Y	139	-158	62	w(s)	96	305737	4	79213	9	140	*93
147	G-2	J-15(Sec-15)	RWEB	2448	14	SM490Y	156	-158	61	w(s)	96	315894	4	81923	9	139	*94
150	G-2	J-16(Sec-16)	LWEB	2298	16	SM490Y	148	-185	63	w(s)	120	411528	5	84519	10	167	*96
151	G-2	J-16(Sec-16)	RWEB	2430	16	SM490Y	166	-184	62	w(s)	120	408728	5	84140	10	164	*97
154	G-2	J-17(Sec-18)	LWEB	2312	14	SM490Y	157	-177	66	w(s)	96	343712	4	88790	9	158	*100
155	G-2	J-17(Sec-18)	RWEB	2444	14	SM490Y	175	-176	65	w(s)	96	353175	4	91326	9	155	*101
158	G-2	J-18(Sec-19)	LWEB	2323	12	SM490Y	143	-158	60	w(s)	72	261861	3	90368	9	119	*104

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Joint Type	Applied Bolts			Bolts Stress	Spl THK		Group No.
							σ_{Un}	σ_{Ln}	τ			P	Req Bolts	ρ	l	σ_{sp}	
159	G-2	J-18(Sec-19)	RWEB	2455	12	SM490Y	158	-154	60	w(s)	72	260520	3	90264	9	118	*105
162	G-2	J-19(Sec-19)	LWEB	2323	12	SM490Y	-131	168	39	w(s)	72	280387	3	94702	9	126	*108
163	G-2	J-19(Sec-19)	RWEB	2455	12	SM490Y	-147	167	39	w(s)	72	278483	3	94211	9	124	*109
166	G-2	J-20(Sec-20)	LWEB	2319	12	SM490Y	-151	166	21	w(s)	72	275340	3	92129	9	124	*112
167	G-2	J-20(Sec-20)	RWEB	2451	12	SM490Y	-168	165	21	w(s)	72	273470	3	91542	9	126	*113
170	G-2	J-21(Sec-22)	LWEB	2319	12	SM490Y	-150	164	22	w(s)	72	273299	3	91501	9	123	112
171	G-2	J-21(Sec-22)	RWEB	2451	12	SM490Y	-167	163	22	w(s)	72	271443	3	90923	9	125	113
174	G-2	J-22(Sec-23)	LWEB	2323	12	SM490Y	-123	158	43	w(s)	72	263033	3	89225	9	118	*117
175	G-2	J-22(Sec-23)	RWEB	2455	12	SM490Y	-139	158	43	w(s)	72	263033	3	89389	9	118	*118

* of Group No. means the representative member

4-4 Checking of Stiffness ratio

BOX G1

PANEL	length	Assumption (Iy')			Actual value ratio (Iy)			Assumption (J')			Actual value ratio (J)		
1	5.484	0.135410	0.134611	0.6	0.136422	0.132448	3.0						
2	5.475	0.154481	0.154610	-0.1	0.154281	0.152088	1.4						
3	5.471	0.169323	0.170870	-0.9	0.165472	0.163874	1.0						
4	5.467	0.175984	0.170858	3.0	0.170761	0.163877	4.2						
5	5.463	0.175971	0.170846	3.0	0.170762	0.163880	4.2						
6	5.459	0.172011	0.165769	3.8	0.165165	0.160354	3.0						
7	5.454	0.163393	0.145023	12.7	0.139712	0.135644	3.0						
8	5.451	0.182898	0.177130	3.3	0.167279	0.162408	3.0						
9	5.449	0.195847	0.190143	3.0	0.195712	0.186727	4.8						
10	5.244	0.281101	0.272914	3.0	0.238502	0.244555	-2.5						
11	5.738	0.262950	0.255291	3.0	0.239040	0.237840	0.5						
12	5.831	0.222373	0.215896	3.0	0.214806	0.207325	3.6						
13	5.824	0.173303	0.176318	-1.7	0.164971	0.160166	3.0						
14	5.818	0.158987	0.154356	3.0	0.143226	0.139054	3.0						
15	5.812	0.172537	0.167512	3.0	0.162002	0.155180	4.4						
16	5.805	0.175954	0.170829	3.0	0.162197	0.157473	3.0						
17	5.799	0.176005	0.170879	3.0	0.162184	0.157460	3.0						
18	5.793	0.172677	0.167648	3.0	0.162361	0.155144	4.7						
19	5.792	0.159166	0.154530	3.0	0.143180	0.139011	3.0						
20	5.792	0.176561	0.179066	-1.4	0.166636	0.161783	3.0						
21	5.792	0.227410	0.220786	3.0	0.214547	0.209141	2.6						
22	5.693	0.272757	0.264813	3.0	0.238240	0.241072	-1.2						
23	5.198	0.297694	0.289023	3.0	0.253950	0.250188	1.5						
24	5.396	0.204118	0.198173	3.0	0.198155	0.190392	4.1						
25	5.396	0.187516	0.181146	3.5	0.169437	0.164502	3.0						
26	5.396	0.163682	0.145269	12.7	0.139655	0.135587	3.0						
27	5.396	0.165604	0.159549	3.8	0.161777	0.157064	3.0						
28	5.396	0.168604	0.163693	3.0	0.166892	0.160133	4.2						
29	5.396	0.168604	0.163693	3.0	0.166892	0.160133	4.2						
30	5.396	0.161513	0.156809	3.0	0.160899	0.156212	3.0						
31	5.396	0.149624	0.145266	3.0	0.151343	0.146934	3.0						
32	5.388	0.140934	0.134781	4.6	0.137701	0.132404	4.0						

Span length	Assumption (Iy')			Actual value ratio (Iy)			Assumption (J')			Actual value ratio (J)		
1	54.417	0.180212	0.174865	3.1	0.170115	0.166256	2.3					
2	69.486	0.195706	0.191319	2.3	0.180975	0.176564	2.5					
3	53.750	0.180364	0.173320	4.1	0.170368	0.165047	3.2					

BOX G2

PANEL	length	Assumption (Iy')			Actual value ratio (Iy)			Assumption (J')			Actual value ratio (J)		
1	5.416	0.135664	0.134611	0.8	0.136422	0.132448	3.0						
2	5.425	0.154481	0.149982	3.0	0.156501	0.149787	4.5						
3	5.429	0.168369	0.163465	3.0	0.166962	0.160191	4.2						
4	5.433	0.168358	0.163454	3.0	0.166962	0.160194	4.2						
5	5.437	0.168346	0.163443	3.0	0.166963	0.160197	4.2						
6	5.441	0.165340	0.159291	3.8	0.161845	0.157131	3.0						
7	5.446	0.165281	0.145023	14.0	0.139712	0.135644	3.0						
8	5.449	0.187180	0.183378	2.1	0.171582	0.166584	3.0						
9	5.451	0.207594	0.202004	2.8	0.199308	0.193707	2.9						
10	5.256	0.301152	0.295957	1.8	0.250753	0.253629	-1.1						
11	5.762	0.276456	0.269728	2.5	0.238485	0.243961	-2.2						
12	5.869	0.231146	0.224414	3.0	0.211410	0.212349	-0.4						
13	5.876	0.176726	0.182819	-3.3	0.170899	0.165921	3.0						
14	5.882	0.162950	0.158204	3.0	0.146309	0.142049	3.0						
15	5.888	0.182822	0.177497	3.0	0.165962	0.161128	3.0						
16	5.895	0.187094	0.181645	3.0	0.170948	0.163843	4.3						
17	5.901	0.187148	0.181697	3.0	0.170930	0.163830	4.3						
18	5.907	0.183337	0.177997	3.0	0.166315	0.161471	3.0						
19	5.909	0.166392	0.161546	3.0	0.149392	0.145042	3.0						
20	5.909	0.185559	0.186058	-0.3	0.172876	0.167841	3.0						
21	5.909	0.241592	0.234555	3.0	0.224393	0.216881	3.5						
22	5.808	0.295749	0.284684	3.9	0.250967	0.249900	0.4						
23	5.303	0.322222	0.312837	3.0	0.257586	0.259149	-0.6						
24	5.505	0.224352	0.213269	5.2	0.205612	0.199623	3.0						
25	5.505	0.202950	0.189889	6.9	0.176726	0.170295	3.8						
26	5.505	0.165541	0.145269	14.0	0.139655	0.135587	3.0						
27	5.505	0.175874	0.168978	4.1	0.167800	0.162484	3.3						
28	5.505	0.179703	0.174469	3.0	0.173411	0.166327	4.3						
29	5.505	0.179703	0.174469	3.0	0.173411	0.166327	4.3						
30	5.505	0.179703	0.174469	3.0	0.173411	0.166327	4.3						
31	5.505	0.162735	0.157995	3.0	0.159444	0.154799	3.0						
32	5.512	0.142041	0.137904	3.0	0.139655	0.135586	3.0						

Span length	Assumption (Iy')	Actual value ratio (Iy)		Assumption (J')	Actual value ratio (J)		
1	54.183	0.181810	0.175687	3.5	0.171456	0.166681	2.9
2	70.514	0.206170	0.201503	2.3	0.186393	0.182647	2.1
3	54.850	0.193002	0.184478	4.6	0.176368	0.171324	2.9

4-5 Checking of Live Load deflection

Main girder G-1

Span No.	Span length	Actual Deflection	Allowable deflection	Actual def./Span Length	Allowable def./Span Length
	L span(mm)	δ (mm)	δ_a (mm)	δ / L span	δ_a / L span
1	54417	65.5	108.8	1/830	1/500
2	69486	95.7	139.0	1/726	1/500
3	53750	62.2	107.5	1/864	1/500

Main girder G-2

Span No.	Span length	Actual Deflection	Allowable deflection	Actual def./Span Length	Allowable def./Span Length
	L span(mm)	δ (mm)	δ_a (mm)	δ / L span	δ_a / L span
1	54183	64.5	108.4	1/840	1/500
2	70514	100.6	141.0	1/701	1/500
3	54850	67.2	109.7	1/817	1/500

4-5 Checking of Live Load deflection

Main girder G-1

Span No.	Span length	Actual Deflection	Allowable deflection	Actual def./Span Length	Allowable def./Span Length
	L span(mm)	δ (mm)	δ_a (mm)	δ / L span	δ_a / L span
1	54417	65.5	108.8	1/830	1/500
2	69486	95.7	139.0	1/726	1/500
3	53750	62.2	107.5	1/864	1/500

Main girder G-2

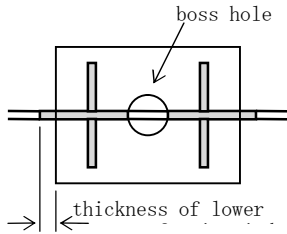
Span No.	Span length	Actual Deflection	Allowable deflection	Actual def./Span Length	Allowable def./Span Length
	L span(mm)	δ (mm)	δ_a (mm)	δ / L span	δ_a / L span
1	54183	64.5	108.4	1/840	1/500
2	70514	100.6	141.0	1/701	1/500
3	54850	67.2	109.7	1/817	1/500

§5. Diaphragm and Stiffener
5-1 Calculation of support diaphragm

1. Checking Method

(a) Check of bearing stress

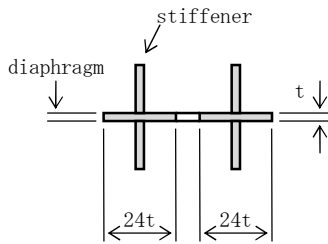
$$\sigma_b = R_v / A_n \leq \sigma_{ba}$$



- σ_b : bearing stress
- R_v : reaction force for support
- A_n : Effective section area of bearing
(shown in the left sketch in gray)
- σ_{ba} : allowable bearing stress

(b) vertical stress of stiffeners

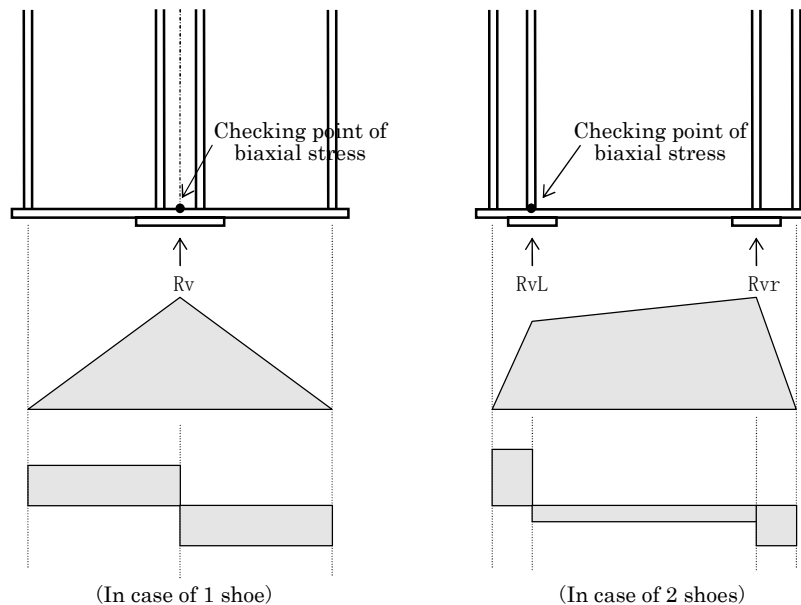
$$\sigma_v = R_v / A_g \leq \sigma_{ca}$$



- σ_v : Vertical stress
- R_v : Reaction force
- A_g : Effective area of stiffeners
(Colored area in the figure)
- σ_{ca} : allowable compressive stress

(c) Check of horizontal stress of diaphragm

The diaphragm is assumed as a simple beam supported at webs, and bending and shear stresses caused by the reaction force are checked.



(d) Check of biaxial stress

Biaxial stress of the diaphragm is checked using actual stresses calculated from (b) and (c) .

$$(\sigma_v / \sigma_a)^2 - (\sigma_v / \sigma_a) * (\sigma_L / \sigma_a) + (\sigma_L / \sigma_a)^2 + (\tau / \tau_a)^2 \leq 1.2$$

$\sigma_v \cdot \sigma_L$: Actual stress calculated at (b) and (c) .

σ_a : Allowable tensile stress

τ_a : Allowable shear stress

(e) Calculation of fillet weld size

Between vertical stiffener and diaphragm

Required throat thickness: $A_{req} = 2 * R_v / (n * h * \tau_a)$

Required size : $S_{req} = A_{req} / 0.707$

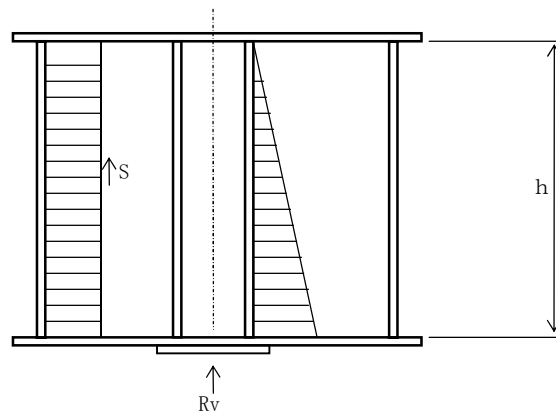
Between diaphragm and web of main girder

Required throat thickness: $A_{req} = S / (n * h * \tau_a)$

Required size : $S_{req} = A_{req} / 0.707$

Where

n : Number of welding lines



(Distribution of shear force)

2. Diaphragm on Support Position

1. Main girder: G-1 Support: S-1

Reaction force $R_a = 2700.0 \text{ kN}$

Diaphragm	TD= 12 mm	(SM490YA)
Lflg	TL= 10 mm	(SM490YA)
Web	TW= 12 mm	(SM490YA)
Lower plate	1- 760 * 810	(202.0 ϕ)
Rib	4- 160 * 16	(SM490YA)

Check of bearing stress

(SM490YA)Stiff	$2 * (16.00 + 16.00 - 2 * 3.50) * 1.6 = 80.00$
(SM490YA)DIA	$(81.00 - 20.20 + 4 * 1.0) * 1.2 = 77.76$

$A_b = 157.76 \text{ cm}^2$

$\sigma_b = R/A_b = 2700.0 * 10^3 / 157.76e2 = 171.1 \text{ N/mm}^2$
 $< \sigma_{ba} = 315.0 \text{ N/mm}^2$

Check of vertical stress

(SM490YA)Stiff	$2 * (16.00 + 16.00) * 1.6 = 102.40$
(SM490YA)DIA	$57.60 * 1.2 = 69.12$

$A = 171.52 \text{ cm}^2$

$1.7 * 102.40 = 174.08 \text{ cm}^2 > A$ 故に $A_e = 171.52 \text{ cm}^2$

$r = \sqrt{I/A_e} = \sqrt{9766 / 171.52} = 7.55 \text{ cm}$

Stress

$L/r = 239.0 / 2 / 7.55 = 15.84 > 15$
 ≤ 75

$\sigma_{cag} = 210.0 - 1.50 * (15.84 - 15) = 208.7 \text{ N/mm}^2$

$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 208.7 * 210.0 / 210.0 = 208.7 \text{ N/mm}^2$

$\sigma_v = R/A_e = 2700.0 * 10^3 / 171.52e2 = 157.4 \text{ N/mm}^2 < \sigma_{ca}$

Check of horizontal stress

S1

Shear force $S_a = 2700.0 * 1.100 / 2.200 = 1350.0$ kN
 $S_c = 1350.0$ kN

Bending moment $M_a = M_c = 2700.0 * 1.100 * 1.100 / 2.200 = 1485.0$ kN.m

Section A-A

		A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)
(SM490YA)	1-FLG PL 663* 10	66.27	-120.00	-7953	954333
(SM490YA)	1-DIA PL 2390* 12	286.80	—	—	1365192
(SM490YA)	1-FLG PL 663* 10	66.27	120.00	7953	954333
		419.35		0	3273857
					0
e = $\Sigma(Ay) / \Sigma A =$		0 / 419.35 =	0.00 cm		
Y1 = 119.50 + 1.0 + (0.00) =	120.50 cm	I =	3273857

$\sigma_l = 1485.0 * 10^{-6} * 120.50 / 3273857 = 54.7$ N/mm² < $\sigma_a = 210.0$ N/mm²
 $\tau = 1350.0 * 10^{-3} / 286.80 = 47.1$ N/mm² < $\tau_a = 120.0$ N/mm²

Section C-C

		A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)
(SM490YA)	1-FLG PL 663* 10	66.27	-120.00	-7953	954333
(SM490YA)	1-DIA PL 1195* 12	143.40	-59.75	-8568	682596
(SM490YA)	1-DIA PL 1195* 12	143.40	59.75	8568	682596
(SM490YA)	1-FLG PL 663* 10	66.27	120.00	7953	954333
		419.35		0	3273857
					0
e = $\Sigma(Ay) / \Sigma A =$		0 / 419.35 =	0.00 cm		
Y1 = 119.50 + 1.0 + (-0.00) =	120.50 cm	I =	3273857

$\sigma_l = 1485.0 * 10^{-6} * 120.50 / 3273857 = 54.7$ N/mm² < $\sigma_a = 210.0$ N/mm²
 $\tau = 1350.0 * 10^{-3} / 286.80 = 47.1$ N/mm² < $\tau_a = 120.0$ N/mm²

Check of biaxial stress

$$A-A \quad (\sigma_v / \sigma_{ta})^{**2} - (\sigma_v / \sigma_{ta}) * (\sigma_l / \sigma_{ta}) + (\sigma_l / \sigma_{ta})^{**2} + (\tau / \tau_a)^{**2} = 0.588 < 1.2$$

S1

Weld size

(a) Between stiffener and diaphragm

$$\begin{aligned} \text{Required size: } s &= \text{SQR}(2 \cdot 16) = 5.66 \text{ ---} \rightarrow 6 \text{ mm} < t_{\min} = 12 \text{ mm} \\ a &= 8 \cdot 6 / 1.4142 = 33.94 \text{ mm} \end{aligned}$$

$$\begin{aligned} \tau_a &= 2 \cdot R_a / (a \cdot h_w') = 2 \cdot 2700.0 \cdot 10^3 / \{33.94 \cdot (2390 - 35 - 300)\} \\ &= 77.4 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2 \end{aligned}$$

(b) Between diaphragm and web of main girder

$$\text{Size } s = \text{SQR}(2 \cdot 12) = 4.90 \text{ ---} \rightarrow 6 \text{ mm} < t_{\min} = 12 \text{ mm}$$

$$\begin{aligned} \tau &= 1350.0 \cdot 10^3 / (2 \cdot 6 \cdot 0.7071 \cdot 2354) = 67.6 \text{ N/mm}^2 \\ &< \tau_a = 120.0 \text{ N/mm}^2 \end{aligned}$$

2. Main girder: G-1 Support: PF3

Reaction force $R_a = 7300.0 \text{ kN}$

Diaphragm TD= 26 mm (SM490YB)
 Lflg TL= 26 mm (SM490YB)
 Web TW= 16 mm (SM490YA)
 Lower plate 1-1210 *1210 (352.0 ϕ)
 Rib 4- 280 * 28 (SM490YB)

Check of bearing stress

(SM490YB)Stiff	$2 * (28.00 + 28.00 - 2 * 3.50) * 2.8 = 274.40$
(SM490YB)DIA	$(121.00 - 35.20 + 4 * 2.6) * 2.6 = 250.12$

$A_b = 524.52 \text{ cm}^2$

$\sigma_b = R/A_b = 7300.0 * 10^3 / 524.52e2 = 139.2 \text{ N/mm}^2$
 $< \sigma_{ba} = 315.0 \text{ N/mm}^2$

Check of vertical stress

(SM490YB)Stiff	$2 * (28.00 + 28.00) * 2.8 = 313.60$
(SM490YB)Dia	$92.40 * 2.6 = 240.24$

$A = 553.84 \text{ cm}^2$

$1.7 * 313.60 = 533.12 \text{ cm}^2 < A$ 故に $A_e = 533.12 \text{ cm}^2$

$r = \text{SQR}(I/A_e) = \text{SQR}(94034 / 533.12) = 13.28 \text{ cm}$

Stress

$L/r = 236.8 / 2 / 13.28 = 8.91 < 15$

$\sigma_{cag} = 210.0 \text{ N/mm}^2$

$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 210.0 * 210.0 / 210.0 = 210.0 \text{ N/mm}^2$

$\sigma_v = R/A_e = 7300.0 * 10^3 / 533.12e2 = 136.9 \text{ N/mm}^2 < \sigma_{ca}$

Check of horizontal stress

PF3

Shear force $S_a = 7300.0 * 1.100 / 2.200 = 3650.0$ kN
 $S_c = 3650.0$ kN

Bending moment $M_a = M_c = 7300.0 * 1.100 * 1.100 / 2.200 = 4015.0$ kN.m

Section A-A

		Section	A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)
(SM490YB)	1-FLG PL	660* 32	211.20	-120.00	-25344	3041460
(SM490YB)	1-DIA PL	2368* 26	615.68	_____	_____	2876982
(SM490YB)	1-FLG PL	660* 26	171.60	119.70	20541	2458797
			998.48		-4803	8377239
						-23109

$$e = \Sigma (Ay) / \Sigma A = -4803 / 998.48 = -4.81 \text{ cm}$$

$$Y1 = 118.40 + 2.6 + (4.81) = 125.81 \text{ cm} \quad I = 8354131$$

$$\sigma_l = 4015.0 * 10^6 * 125.81e1 / 8354131e4 = 60.5 \text{ N/mm}^2 < \sigma_a = 210.0 \text{ N/mm}^2$$

$$\tau = 3650.0 * 10^3 / 615.68e2 = 59.3 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2$$

Section C-C

		Section	A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)
(SM490YB)	1-FLG PL	660* 32	211.20	-120.00	-25344	3041460
(SM490YB)	1-DIA PL	1184* 26	307.84	-59.20	-18224	1438491
(SM490YB)	1-DIA PL	1184* 26	307.84	59.20	18224	1438491
(SM490YB)	1-FLG PL	660* 26	171.60	119.70	20541	2458797
			998.48		-4803	8377239
						-23109

$$e = \Sigma (Ay) / \Sigma A = -4803 / 998.48 = -4.81 \text{ cm}$$

$$Y1 = 118.40 + 2.6 + (4.81) = 125.81 \text{ cm} \quad I = 8354131$$

$$\sigma_l = 4015.0 * 10^6 * 125.81e1 / 8354131e4 = 60.5 \text{ N/mm}^2 < \sigma_a = 210.0 \text{ N/mm}^2$$

$$\tau = 3650.0 * 10^3 / 615.68e2 = 59.3 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2$$

Check of biaxial stress

$$\text{section A-A } (\sigma_v / \sigma_{ta})^2 - (\sigma_v / \sigma_{ta}) * (\sigma_l / \sigma_{ta}) + (\sigma_l / \sigma_{ta})^2 + (\tau / \tau_a)^2 = 0.564 < 1.2$$

Weld size

(a) Between stiffener and diaphragm

$$\begin{aligned} \text{Required size } s &= \text{SQR}(2 \cdot 28) = 7.48 \text{ ---} \rightarrow 11 \text{ mm} < t_{\min} = 26 \text{ mm} \\ a &= 8 \cdot 12 / 1.4142 = 67.88 \text{ mm} \end{aligned}$$

$$\begin{aligned} \tau_a &= 2 \cdot R_a / (a \cdot h_w') = 2 \cdot 7300.0 \cdot 10^3 / \{67.88 \cdot (2368 - 35 - 350)\} \\ &= 108.7 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2 \end{aligned}$$

(b) Between diaphragm and web of main girder

$$\text{Welding Size } s = \text{SQR}(2 \cdot 26) = 7.21 \text{ ---} \rightarrow 10 \text{ mm} < t_{\min} = 16 \text{ mm}$$

$$\begin{aligned} \tau &= 3650.0 \cdot 10^3 / (2 \cdot 10 \cdot 0.7071 \cdot 2356) = 109.6 \text{ N/mm}^2 \\ &< \tau_a = 120.0 \text{ N/mm}^2 \end{aligned}$$

3. Main girder: G-1 Support: PF3

Reaction force Ra= 7500.0 kN

Diaphragm TD= 26 mm (SM490YB)
 Lflg TL= 27 mm (SM490YB)
 Web TW= 16 mm (SM490YA)
 Lower plate 1-1210 *1210 (352.0 φ)
 RIB 4- 280 * 28 (SM490YB)

Check of bearing stress

(SM490YB)Stiff $2 * (28.00 + 28.00 - 2 * 3.50) * 2.8 = 274.40$
 (SM490YB)DIA $(121.00 - 35.20 + 4 * 2.7) * 2.6 = 251.16$

Ab = 525.56 cm²

$$\sigma_b = R / A_b = 7500.0 * 10^3 / 525.56 = 142.7 \text{ N/mm}^2 < \sigma_{ba} = 315.0 \text{ N/mm}^2$$

Check of vertical stress

(SM490YB)Stiff $2 * (28.00 + 28.00) * 2.8 = 313.60$
 (SM490YB)DIA $92.40 * 2.6 = 240.24$

A = 553.84 cm²

$$1.7 * 313.60 = 533.12 \text{ cm}^2 < A \quad \text{故に } A_e = 533.12 \text{ cm}^2$$

$$r = \text{SQR}(I / A_e) = \text{SQR}(94034 / 533.12) = 13.28 \text{ cm}$$

Stress

$$L / r = 236.4 / 2 / 13.28 = 8.90 < 15$$

$$\sigma_{cag} = 210.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{ca1} / \sigma_{cao} = 210.0 * 210.0 / 210.0 = 210.0 \text{ N/mm}^2$$

$$\sigma_v = R / A_e = 7500.0 * 10^3 / 533.12 = 140.7 \text{ N/mm}^2 < \sigma_{ca}$$

Check of horizontal stress

PF4

Shear force $S_a = 7500.0 * 1.100 / 2.200 = 3750.0$ kN
 $S_c = 3750.0$ kN

Bending moment $M_a = M_c = 7500.0 * 1.100 * 1.100 / 2.200 = 4125.0$ kN.m

Section A-A

	Section	A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)	
(SM490YB)	1-FLG PL 660* 36	237.60	-120.00	-28512	3421697	
(SM490YB)	1-DIA PL 2364* 26	614.64	—	—	2862428	
(SM490YB)	1-FLG PL 660* 27	178.20	119.55	21304	2546979	
				1030.44	-7208	8831103
						-50423
						—————
						I = 8780680

$$e = \Sigma (Ay) / \Sigma A = -7208 / 1030.44 = -7.00 \text{ cm}$$

$$Y1 = 118.20 + 2.7 + (-7.00) = 127.90 \text{ cm}$$

$$\sigma_l = 4125.0 * 10^6 * 127.90 e1 / 8780680 e4 = 60.1 \text{ N/mm}^2 < \sigma_a = 210.0 \text{ N/mm}^2$$

$$\tau = 3750.0 * 10^3 / 614.64 e2 = 61.0 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2$$

Section C-C

	Section	A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)	
(SM490YB)	1-FLG PL 660* 36	237.60	-120.00	-28512	3421697	
(SM490YB)	1-DIA PL 1182* 26	307.32	-59.10	-18163	1431214	
(SM490YB)	1-DIA PL 1182* 26	307.32	59.10	18163	1431214	
(SM490YB)	1-FLG PL 660* 27	178.20	119.55	21304	2546979	
				1030.44	-7208	8831103
						-50423
						—————
						I = 8780680

$$e = \Sigma (Ay) / \Sigma A = -7208 / 1030.44 = -7.00 \text{ cm}$$

$$Y1 = 118.20 + 2.7 + (-7.00) = 127.90 \text{ cm}$$

$$\sigma_l = 4125.0 * 10^6 * 127.90 e1 / 8780680 e4 = 60.1 \text{ N/mm}^2 < \sigma_a = 210.0 \text{ N/mm}^2$$

$$\tau = 3750.0 * 10^3 / 614.64 e2 = 61.0 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2$$

Check of biaxial stress

$$\text{Section A-A } (\sigma_v / \sigma_{ta})^2 - (\sigma_v / \sigma_{ta}) * (\sigma_l / \sigma_{ta}) + (\sigma_l / \sigma_{ta})^2 + (\tau / \tau_a)^2 = 0.597 < 1.2$$

Weld size

(a) Between stiffener and diaphragm

$$\begin{aligned} \text{Required size } s &= \text{SQR}(2 \cdot 28) = 7.48 \text{ ---} \rightarrow 12 \text{ mm} < t_{\text{min}} = 26 \text{ mm} \\ a &= 8 \cdot 12 / 1.4142 = 67.88 \text{ mm} \end{aligned}$$

$$\begin{aligned} \tau_a &= 2 \cdot R_a / (a \cdot h_w') = 2 \cdot 7500.0 \cdot 10^3 / \{62.23 \cdot (2364 - 35 - 350)\} \\ &= 111.7 \text{ N/mm}^2 > \tau_a = 120.0 \text{ N/mm}^2! \end{aligned}$$

(b) Between diaphragm and web of main girder

$$\text{Welding Size } s = \text{SQR}(2 \cdot 26) = 7.21 \text{ ---} \rightarrow 10 \text{ mm} < t_{\text{min}} = 16 \text{ mm}$$

$$\begin{aligned} \tau &= 3750.0 \cdot 10^3 / (2 \cdot 10 \cdot 0.7071 \cdot 2298) = 115.4 \text{ N/mm}^2 \\ &< \tau_a = 120.0 \text{ N/mm}^2 \end{aligned}$$

4. Main girder: G-1 Support: S2

Reaction force Ra= 2300.0 kN

Diaphragm	TD= 12 mm	(SM490YA)
Lflg	TL= 10 mm	(SM490YA)
Web	TW= 12 mm	(SM490YA)
Lower plate	1- 760 * 810	(202.0 φ)
Rib	4- 160 * 16	(SM490YA)

Check of bearing stress

(SM490YA)Stiff	$2 * (16.00 + 16.00 - 2 * 3.50) * 1.6 =$	80.00
(SM490YA)DIA	$(81.00 - 20.20 + 4 * 1.0) * 1.2 =$	77.76

Ab = 157.76 cm²

$$\sigma_b = R / A_b = 2300.0 * 10^3 / 157.76 = 145.8 \text{ N/mm}^2$$

$$< \sigma_{ba} = 315.0 \text{ N/mm}^2$$

Check of vertical stress

(SM490YA)Stiff	$2 * (16.00 + 16.00) * 1.6 =$	102.40
(SM490YA)DIA	$57.60 * 1.2 =$	69.12

A = 171.52 cm²

$$1.7 * 102.40 = 174.08 \text{ cm}^2 > A \quad \text{故に } A_e = 171.52 \text{ cm}^2$$

$$r = \sqrt{I / A_e} = \sqrt{9766 / 171.52} = 7.55 \text{ cm}$$

Stress

$$L / r = 239.0 / 7.55 = 15.84 > 15$$

$$\leq 75$$

$$\sigma_{cag} = 210.0 - 1.5 * (15.84 - 15) = 208.7 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 208.7 * 210.0 / 210.0 = 208.7 \text{ N/mm}^2$$

$$\sigma_v = R / A_e = 2300.0 * 10^3 / 171.52 = 134.1 \text{ N/mm}^2 < \sigma_{ca}$$

Check of horizontal stress

S2

Shear force $S_a = 2300.0 * 1.100 / 2.200 = 1150.0$ kN
 $S_c = 1150.0$ kN

Bending moment $M_a = M_c = 2300.0 * 1.100 * 1.100 / 2.200 = 1265.0$ kN.m

Section A-A

	Section	A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)
(SM490YA)	1-FLG PL 663* 10	66.27	-120.00	-7953	954333
(SM490YA)	1-DIA PL 2390* 12	286.80	—	—	1365192
(SM490YA)	1-FLG PL 663* 10	66.27	120.00	7953	954333
				419.35	0
					3273857
					0
$e = \Sigma (Ay) / \Sigma A = 0 / 419.35 = 0.00$ cm					
$Y1 = 119.50 + 1.0 + (0.00) = 120.50$ cm				I =	3273857

$\sigma_1 = 1265.0 * 10^6 * 120.50e1 / 3273857e4 = 46.6$ N/mm² < $\sigma_a = 210.0$ N/mm²
 $\tau = 1150.0 * 10^3 / 286.80e2 = 40.1$ N/mm² < $\tau_a = 120.0$ N/mm²

Section C-C

	Section	A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)
(SM490YA)	1-FLG PL 663* 10	66.27	-120.00	-7953	954333
(SM490YA)	1-DIA PL 1195* 12	143.40	-59.75	-8568	682596
(SM490YA)	1-DIA PL 1195* 12	143.40	59.75	8568	682596
(SM490YA)	1-FLG PL 663* 10	66.27	120.00	7953	954333
				419.35	0
					3273857
					0
$e = \Sigma (Ay) / \Sigma A = 0 / 419.35 = 0.00$ cm					
$Y1 = 119.50 + 1.0 + (-0.00) = 120.50$ cm				I =	3273857

$\sigma_1 = 1265.0 * 10^6 * 120.50e1 / 3273857e4 = 46.6$ N/mm² < $\sigma_a = 210.0$ N/mm²
 $\tau = 1150.0 * 10^3 / 286.80e2 = 40.1$ N/mm² < $\tau_a = 120.0$ N/mm²

Check of biaxial stress

Section A-A $(\sigma_v / \sigma_{ta})^2 - (\sigma_v / \sigma_{ta}) * (\sigma_l / \sigma_{ta}) + (\sigma_l / \sigma_{ta})^2 + (\tau / \tau_a)^2$
 $= 0.427 < 1.2$

Weld size

(a) Between stiffener and diaphragm

$$\text{Required size } s = \text{SQR}(2 \cdot 16) = 5.66 \rightarrow 6 \text{ mm} < t_{\min} = 12 \text{ mm}$$
$$a = 8 \cdot 6 / 1.4142 = 33.94 \text{ mm}$$

$$\tau_a = 2 \cdot R_a / (a \cdot h_w') = 2 \cdot 2300.0 \cdot 10^3 / \{33.94 \cdot (2390 - 35 - 300)\}$$
$$= 66.0 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2$$

(b) Between diaphragm and web of main girder

$$\text{Welding Size } s = \text{SQR}(2 \cdot 12) = 4.90 \rightarrow 6 \text{ mm} < t_{\min} = 12 \text{ mm}$$

$$\tau = 1150.0 \cdot 10^3 / (2 \cdot 6 \cdot 0.7071 \cdot 2324) = 58.3 \text{ N/mm}^2$$
$$< \tau_a = 120.0 \text{ N/mm}^2$$

5. Main girder: G-2 Support: S1

Reaction force Ra= 2500.0 kN

Diaphragm	TD= 12 mm	(SM490YA)
Lflg	TL= 10 mm	(SM490YA)
Web	TW= 12 mm	(SM490YA)
Lower plate	1- 760 * 810	(202.0 φ)
RIB	4- 160 * 16	(SM490YA)

Check of bearing stress

(SM490YA)Stiff	$2 * (16.00 + 16.00 - 2 * 3.50) * 1.6$	$= 80.00$
(SM490YA)DIA	$(81.00 - 20.20 + 4 * 1.0) * 1.2$	$= 77.76$

Ab = 157.76 cm²

$$\sigma_b = R/Ab = 2500.0 * 10^3 / 157.76e2 = 158.5 \text{ N/mm}^2$$

$$< \sigma_{ba} = 315.0 \text{ N/mm}^2$$

Check of vertical stress

(SM490YA)Stiff	$2 * (16.00 + 16.00) * 1.6$	$= 102.40$
(SM490YA)DIA	$57.60 * 1.2$	$= 69.12$

A = 171.52 cm²

$$1.7 * 102.40 = 174.08 \text{ cm}^2 > A \quad \text{故に } Ae = 171.52 \text{ cm}^2$$

$$r = \text{SQR}(I/Ae) = \text{SQR}(9766 / 171.52) = 7.55 \text{ cm}$$

Stress

$$L/r = 239.0 / 2 / 7.55 = 15.84 > 15$$

$$\leq 75$$

$$\sigma_{cag} = 210.0 - 1.50 * (15.84 - 15) = 208.7 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 208.7 * 210.0 / 210.0 = 208.7 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 2500.0 * 10^3 / 171.52e2 = 145.8 \text{ N/mm}^2 < \sigma_{ca}$$

Check of horizontal stress

S1

Shear force $S_a = 2500.0 \cdot 1.100 / 2.200 = 1250.0$ kN
 $S_c = 1250.0$ kN

Bending moment $M_a = M_c = 2500.0 \cdot 1.100 \cdot 1.100 / 2.200 = 1375.0$ kN.m

Section A-A

	Section	A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)
(SM490YA)	1-FLG PL 663* 10	66.27	-120.00	-7953	954333
(SM490YA)	1-DIA PL 2390* 12	286.80	—	—	1365192
(SM490YA)	1-FLG PL 663* 10	66.27	120.00	7953	954333

$$\begin{aligned}
 & 419.35 & 0 & 3273857 \\
 & & & 0 \\
 e = \Sigma (Ay) / \Sigma A &= 0 / 419.35 = 0.00 \text{ cm} \\
 Y1 = 119.50 + 1.0 + (0.00) &= 120.50 \text{ cm} & I = & 3273857
 \end{aligned}$$

$$\begin{aligned}
 \sigma_1 &= 1375.0 \cdot 10^6 \cdot 120.50 \text{e}1 / 3273857 \text{e}4 = 50.6 \text{ N/mm}^2 < \sigma_a = 210.0 \text{ N/mm}^2 \\
 \tau &= 1250.0 \cdot 10^3 / 286.80 \text{e}2 = 43.6 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2
 \end{aligned}$$

Section C-C

	Section	A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)
(SM490YA)	1-FLG PL 663* 10	66.27	-120.00	-7953	954333
(SM490YA)	1-DIA PL 1195* 12	143.40	-59.75	-8568	682596
(SM490YA)	1-DIA PL 1195* 12	143.40	59.75	8568	682596
(SM490YA)	1-FLG PL 663* 10	66.27	120.00	7953	954333

$$\begin{aligned}
 & 419.35 & 0 & 3273857 \\
 & & & 0 \\
 e = \Sigma (Ay) / \Sigma A &= 0 / 419.35 = 0.00 \text{ cm} \\
 Y1 = 119.50 + 1.0 + (0.00) &= 120.50 \text{ cm} & I = & 3273857
 \end{aligned}$$

$$\begin{aligned}
 \sigma_1 &= 1375.0 \cdot 10^6 \cdot 120.50 \text{e}1 / 3273857 \text{e}4 = 50.6 \text{ N/mm}^2 < \sigma_a = 210.0 \text{ N/mm}^2 \\
 \tau &= 1250.0 \cdot 10^3 / 286.80 \text{e}2 = 43.6 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2
 \end{aligned}$$

Check of biaxial stress

$$\begin{aligned}
 \text{Section A-A } (\sigma_v / \sigma_{ta})^{**2} - (\sigma_v / \sigma_{ta}) \cdot (\sigma_1 / \sigma_{ta}) + (\sigma_1 / \sigma_{ta})^{**2} + (\tau / \tau_a)^{**2} \\
 = 0.505 < 1.2
 \end{aligned}$$

Weld size

(a) Between stiffener and diaphragm

$$\text{Required size } s = \text{SQR}(2 \cdot 16) = 5.66 \text{ ---} > 6 \text{ mm} < t_{\min} = 12 \text{ mm}$$
$$a = 8 \cdot 6 / 1.4142 = 33.94 \text{ mm}$$

$$\tau_a = 2 \cdot R_a / (a \cdot h_w') = 2 \cdot 2500.0 \cdot 10^3 / \{33.94 \cdot (2390 - 35 - 300)\}$$
$$= 71.7 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2$$

(c) Between diaphragm and web of main girder

$$\text{Welding Size } s = \text{SQR}(2 \cdot 12) = 4.90 \text{ ---} > 6 \text{ mm} < t_{\min} = 12 \text{ mm}$$

$$\tau = 1250.0 \cdot 10^3 / (2 \cdot 6 \cdot 0.7071 \cdot 2354) = 62.6 \text{ N/mm}^2$$
$$< \tau_a = 120.0 \text{ N/mm}^2$$

6. Main girder: G-2 Support: PF3

Reaction force Ra= 7450.0 kN

Diaphragm TD= 26 mm (SM490YB)
 Lflg TL= 29 mm (SM490YB)
 Web TW= 16 mm (SM490YA)
 Lower plate 1-1210 *1210 (352.0 φ)
 Rib 4- 280 * 28 (SM490YB)

Check of bearing stress

(SM490YB)Stiff $2 * (28.00 + 28.00 - 2 * 3.50) * 2.8 = 274.40$
 (SM490YB)DIA $(121.00 - 35.20 + 4 * 2.9) * 2.6 = 253.24$

Ab = 527.64 cm²

$\sigma_b = R / A_b = 7450.0 * 10^3 / 527.64e2 = 141.2 \text{ N/mm}^2$
 $< \sigma_{ba} = 315.0 \text{ N/mm}^2$

Check of vertical stress

(SM490YB)Stiff $2 * (28.00 + 28.00) * 2.8 = 313.60$
 (SM490YB)DIA $92.40 * 2.6 = 240.24$

A = 553.84 cm²

$1.7 * 313.60 = 533.12 \text{ cm}^2 < A$ 故に $A_e = 533.12 \text{ cm}^2$

$r = \text{SQR}(I / A_e) = \text{SQR}(94034 / 533.12) = 13.28 \text{ cm}$

Stress

$L / r = 236.4 / 2 / 13.28 = 8.90 < 15$

$\sigma_{cag} = 210.0 \text{ N/mm}^2$

$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{ca1} / \sigma_{cao} = 210.0 * 210.0 / 210.0 = 210.0 \text{ N/mm}^2$

$\sigma_v = R / A_e = 7450.0 * 10^3 / 533.12e2 = 139.7 \text{ N/mm}^2 < \sigma_{ca}$

Check of horizontal stress

PF3

Shear force $S_a = 7450.0 * 1.100 / 2.200 = 3725.0$ kN
 $S_c = 3725.0$ kN

Bending moment $M_a = M_c = 7450.0 * 1.100 * 1.100 / 2.200 = 4097.5$ kN.m

Section A-A

	Section	A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)
(SM490YB)	1-FLG PL 660* 36	237.60	-120.00	-28512	3421697
(SM490YB)	1-DIA PL 2364* 26	614.64	_____	_____	2862428
(SM490YB)	1-FLG PL 660* 29	191.40	119.65	22901	2740240
		1043.64		-5611	9024364 -30167
$e = \Sigma (Ay) / \Sigma A = -5611 / 1043.64 = -5.38$ cm $Y1 = 118.20 + 2.9 + (5.38) = 126.48$ cm $I = 8994198$					

$\sigma_l = 4097.5 * 10^6 * 126.48e1 / 8994198e4 = 57.6$ N/mm² < $\sigma_a = 210.0$ N/mm²
 $\tau = 3725.0 * 10^3 / 614.64e2 = 60.6$ N/mm² < $\tau_a = 120.0$ N/mm²

Section C-C

	Section	A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)
(SM490YB)	1-FLG PL 660* 36	237.60	-120.00	-28512	3421697
(SM490YB)	1-DIA PL 1182* 26	307.32	-59.10	-18163	1431214
(SM490YB)	1-DIA PL 1182* 26	307.32	59.10	18163	1431214
(SM490YB)	1-FLG PL 660* 29	191.40	119.65	22901	2740240
		1043.64		-5611	9024364 -30167
$e = \Sigma (Ay) / \Sigma A = -5611 / 1043.64 = -5.38$ cm $Y1 = 118.20 + 2.9 + (5.38) = 126.48$ cm $I = 8994198$					

$\sigma_l = 4097.5 * 10^6 * 126.48e1 / 8994198e4 = 57.6$ N/mm² < $\sigma_a = 210.0$ N/mm²
 $\tau = 3725.0 * 10^3 / 614.64e2 = 60.6$ N/mm² < $\tau_a = 120.0$ N/mm²

Check of biaxial stress

Section A-A $(\sigma_v / \sigma_{ta})^{**2} - (\sigma_v / \sigma_{ta}) * (\sigma_l / \sigma_{ta}) + (\sigma_l / \sigma_{ta})^{**2} + (\tau / \tau_a)^{**2}$
 $= 0.590 < 1.2$

Weld size

(a) Between stiffener and diaphragm

$$\begin{aligned} \text{Required size } s &= \text{SQR}(2*28) = 7.48 \text{ ---} \rightarrow 12 \text{ mm} < t_{\text{min}} = 26 \text{ mm} \\ a &= 8*12/1.4142 = 67.88 \text{ mm} \end{aligned}$$

$$\begin{aligned} \tau_a &= 2*Ra / (a*hw') = 2* 7450.0*10**3 / \{67.88*(2364- 35-350)\} \\ &= 110.9 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2 \end{aligned}$$

(b) Between diaphragm and web of main girder

$$\text{Welding Size } s = \text{SQR}(2*26) = 7.21 \text{ ---} \rightarrow 10 \text{ mm} < t_{\text{min}} = 16 \text{ mm}$$

$$\begin{aligned} \tau &= 3725.0*10**3 / (2*10*0.7071* 2352) = 112.0 \text{ N/mm}^2 \\ &< \tau_a = 120.0 \text{ N/mm}^2 \end{aligned}$$

7. Main girder: G-2 Support: PF4

Reaction force Ra= 7300.0 kN

Diaphragm TD= 26 mm (SM490YB)
 Lflg TL= 31 mm (SM490YB)
 Web TW= 16 mm (SM490YA)
 Lower plate 1-1210 *1210 (352.0 φ)
 RIB 4- 280 * 28 (SM490YB)

Check of bearing stress

(SM490YB)Stiff $2 * (28.00 + 28.00 - 2 * 3.50) * 2.8 = 274.40$
 (SM490YB)DIA $(121.00 - 35.20 + 4 * 3.1) * 2.6 = 255.32$

Ab = 529.72 cm²

$\sigma_b = R / A_b = 7300.0 * 10^3 / 529.72e2 = 137.8 \text{ N/mm}^2$
 $< \sigma_{ba} = 315.0 \text{ N/mm}^2$

Check of vertical stress

(SM490YB)Stiff $2 * (28.00 + 28.00) * 2.8 = 313.60$
 (SM490YB)DIA $92.40 * 2.6 = 240.24$

A = 553.84 cm²

$1.7 * 313.60 = 533.12 \text{ cm}^2 < A$ 故に $A_e = 533.12 \text{ cm}^2$

$r = \text{SQR}(I / A_e) = \text{SQR}(94034 / 533.12) = 13.28 \text{ cm}$

Stress

$L / r = 236.1 / 2 / 13.28 = 8.89 < 15$

$\sigma_{cag} = 210.0 \text{ N/mm}^2$

$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 210.0 * 210.0 / 210.0 = 210.0 \text{ N/mm}^2$

$\sigma_v = R / A_e = 7300.0 * 10^3 / 533.12e2 = 136.9 \text{ N/mm}^2 < \sigma_{ca}$

Check of horizontal stress

PF4

Shear force $S_a = 7300.0 * 1.100 / 2.200 = 3650.0$ kN
 $S_c = 3650.0$ kN

Bending moment $M_a = M_c = 7300.0 * 1.100 * 1.100 / 2.200 = 4015.0$ kN.m

Section A-A

	Section	A (cm ²)	y (cm)	A _y (cm ³)	A _y ² (cm ⁴)
(SM490YB)	1-FLG PL 660* 39	257.40	-120.00	-30888	3706886
(SM490YB)	1-DIA PL 2361* 26	613.86	—	—	2851544
(SM490YB)	1-FLG PL 660* 31	204.60	119.60	24470	2926795
		1075.86		-6418	9485225
					-38284

$$e = \Sigma (A_y) / \Sigma A = -6418 / 1075.86 = -5.97 \text{ cm}$$

$$Y_1 = 118.05 + 3.1 + (5.97) = 127.12 \text{ cm} \quad I = 9446941$$

$$\sigma_l = 4015.0 * 10^6 * 127.12 e1 / 9446941 e4 = 54.0 \text{ N/mm}^2 < \sigma_a = 210.0 \text{ N/mm}^2$$

$$\tau = 3650.0 * 10^3 / 613.86 e2 = 59.5 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2$$

Section C-C

	Section	A (cm ²)	y (cm)	A _y (cm ³)	A _y ² (cm ⁴)
(SM490YB)	1-FLG PL 660* 39	257.40	-120.00	-30888	3706886
(SM490YB)	1-DIA PL 1181* 26	306.93	-59.03	-18117	1425772
(SM490YB)	1-DIA PL 1181* 26	306.93	59.03	18117	1425772
(SM490YB)	1-FLG PL 660* 31	204.60	119.60	24470	2926795
		1075.86		-6418	9485225
					-38284

$$e = \Sigma (A_y) / \Sigma A = -6418 / 1075.86 = -5.97 \text{ cm}$$

$$Y_1 = 118.05 + 3.1 + (5.97) = 127.12 \text{ cm} \quad I = 9446941$$

$$\sigma_l = 4015.0 * 10^6 * 127.12 e1 / 9446941 e4 = 54.0 \text{ N/mm}^2 < \sigma_a = 210.0 \text{ N/mm}^2$$

$$\tau = 3650.0 * 10^3 / 613.86 e2 = 59.5 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2$$

Check of biaxial stress

$$\text{Section A-A } (\sigma_v / \sigma_{ta})^{**2} - (\sigma_v / \sigma_{ta}) * (\sigma_l / \sigma_{ta}) + (\sigma_l / \sigma_{ta})^{**2} + (\tau / \tau_a)^{**2} \\ = 0.569 < 1.2$$

Weld size

(a) Between stiffener and diaphragm

$$\begin{aligned} \text{Required size } s &= \text{SQR}(2 \cdot 28) = 7.48 \text{ ---} \rightarrow 12 \text{ mm} < t_{\text{min}} = 26 \text{ mm} \\ a &= 8 \cdot 12 / 1.4142 = 67.88 \text{ mm} \end{aligned}$$

$$\begin{aligned} \tau_a &= 2 \cdot R_a / (a \cdot h_w') = 2 \cdot 7300.0 \cdot 10^3 / \{67.88 \cdot (2361 - 35 - 350)\} \\ &= 108.8 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2 \end{aligned}$$

(b) Between diaphragm and web of main girder

$$\text{Welding Size} = \text{SQR}(2 \cdot 26) = 7.21 \text{ ---} \rightarrow 10 \text{ mm} < t_{\text{min}} = 16 \text{ mm}$$

$$\begin{aligned} \tau &= 3650.0 \cdot 10^3 / (2 \cdot 10 \cdot 0.7071 \cdot 2295) = 112.5 \text{ N/mm}^2 \\ &< \tau_a = 120.0 \text{ N/mm}^2 \end{aligned}$$

8. Main girder: G-2 Support: S2

Reaction force Ra= 2850.0 kN

Diaphragm TD= 12 mm (SM490YA)
 Lflg TL= 10 mm (SM490YA)
 Web TW= 12 mm (SM490YA)
 Lower plate 1- 760 * 810 (202.0 φ)
 Rib 4- 160 * 16 (SM490YA)

Check of bearing stress

(SM490YA)Stiff $2 * (16.00 + 16.00 - 2 * 3.50) * 1.6 = 80.00$
 (SM490YA)DIA $(81.00 - 20.20 + 4 * 1.0) * 1.2 = 77.76$

Ab = 157.76 cm²

$\sigma_b = R/Ab = 2850.0 * 10^3 / 157.76e2 = 180.7 \text{ N/mm}^2$
 $< \sigma_{ba} = 315.0 \text{ N/mm}^2$

Check of vertical stress

(SM490YA)Stiff $2 * (16.00 + 16.00) * 1.6 = 102.40$
 (SM490YA)DIA $57.60 * 1.2 = 69.12$

A = 171.52 cm²

$1.7 * 102.40 = 174.08 \text{ cm}^2 > A$ 故に Ae= 171.52 cm²

$r = \text{SQR}(I/Ae) = \text{SQR}(9766 / 171.52) = 7.55 \text{ cm}$

Stress

$L/r = 238.9 / 2 / 7.55 = 15.83 > 15$
 ≤ 75

$\sigma_{cag} = 210.0 - 1.50 * (15.83 - 15) = 208.8 \text{ N/mm}^2$

$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 208.8 * 210.0 / 210.0 = 208.8 \text{ N/mm}^2$

$\sigma_v = R/Ae = 2850.0 * 10^3 / 171.52e2 = 166.2 \text{ N/mm}^2 < \sigma_{ca}$

Check of horizontal stress

S2

Shear force $S_a = 2850.0 * 1.100 / 2.200 = 1425.0$ kN
 $S_c = 1425.0$ kN

Bending moment $M_a = M_c = 2850.0 * 1.100 * 1.100 / 2.200 = 1567.5$ kN.m

Section A-A

	Section	A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)	
(SM490YA)	1-FLG PL 663* 11	72.90	-120.00	-8748	1049767	
(SM490YA)	1-DIA PL 2389* 12	286.68	—	—	1363479	
(SM490YA)	1-FLG PL 663* 10	66.27	119.95	7949	953538	
				425.85	-799	3366784
						-1498

$$e = \Sigma (Ay) / \Sigma A = -799 / 425.85 = -1.88 \text{ cm}$$

$$Y1 = 119.45 + 1.0 + (1.88) = 122.33 \text{ cm} \quad I = 3365286$$

$$\sigma_l = 1567.5 * 10^6 * 122.33e1 / 3365286e4 = 57.0 \text{ N/mm}^2 < \sigma_a = 210.0 \text{ N/mm}^2$$

$$\tau = 1425.0 * 10^3 / 286.68e2 = 49.7 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2$$

Section C-C

	Section	A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)	
(SM490YA)	1-FLG PL 663* 11	72.90	-120.00	-8748	1049767	
(SM490YA)	1-DIA PL 1195* 12	143.34	-59.73	-8561	681739	
(SM490YA)	1-DIA PL 1195* 12	143.34	59.73	8561	681739	
(SM490YA)	1-FLG PL 663* 10	66.27	119.95	7949	953538	
				425.85	-799	3366784
						-1498

$$e = \Sigma (Ay) / \Sigma A = -799 / 425.85 = -1.88 \text{ cm}$$

$$Y1 = 119.45 + 1.0 + (1.88) = 122.33 \text{ cm} \quad I = 3365286$$

$$\sigma_l = 1567.5 * 10^6 * 122.33e1 / 3365286e4 = 57.0 \text{ N/mm}^2 < \sigma_a = 210.0 \text{ N/mm}^2$$

$$\tau = 1425.0 * 10^3 / 286.68e2 = 49.7 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2$$

Check of biaxial stress

$$\text{Section A-A } (\sigma_v / \sigma_{ta})^2 - (\sigma_v / \sigma_{ta}) * (\sigma_l / \sigma_{ta}) + (\sigma_l / \sigma_{ta})^2 + (\tau / \tau_a)^2 = 0.657 < 1.2$$

Weld size

(a) Between stiffener and diaphragm

$$\begin{aligned} \text{Required size } s &= \text{SQR}(2 \cdot 16) = 5.66 \text{ ---} \rightarrow 6 \text{ mm} < t_{\min} = 12 \text{ mm} \\ a &= 8 \cdot 6 / 1.4142 = 33.94 \text{ mm} \end{aligned}$$

$$\begin{aligned} \tau_a &= 2 \cdot R_a / (a \cdot h_w') = 2 \cdot 2850.0 \cdot 10^3 / \{33.94 \cdot (2389 - 35 - 300)\} \\ &= 81.8 \text{ N/mm}^2 < \tau_a = 120.0 \text{ N/mm}^2 \end{aligned}$$

(b) Between diaphragm and web of main girder

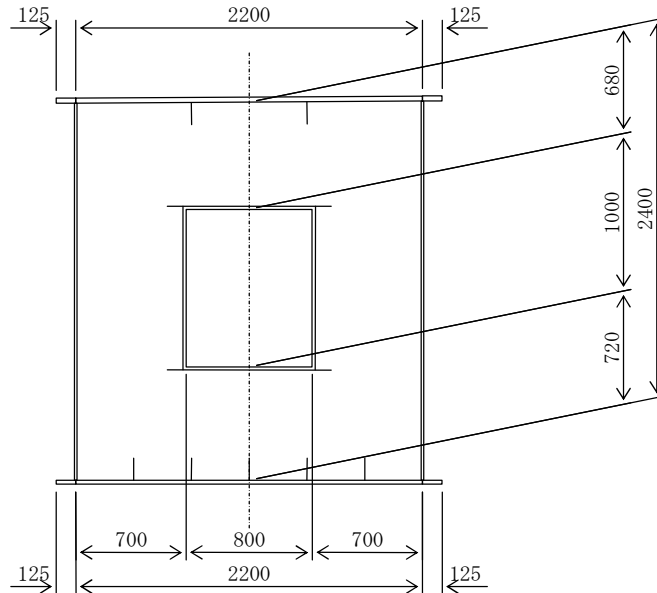
$$\text{Welding Size } s = \text{SQR}(2 \cdot 12) = 4.90 \text{ ---} \rightarrow 6 \text{ mm} < t_{\min} = 12 \text{ mm}$$

$$\begin{aligned} \tau &= 1425.0 \cdot 10^3 / (2 \cdot 6 \cdot 0.7071 \cdot 2323) = 72.3 \text{ N/mm}^2 \\ &< \tau_a = 120.0 \text{ N/mm}^2 \end{aligned}$$

5-2 Calculation of mid diagram

1. Girder G-1

(1) Design conditions



(a) Diaphragm

Equivalent span	$L_u = 33.816 \text{ m}$
Interval of diaphragms	$L_d = 5.449 \text{ m}$
Thickness of diaphragm	$T_d = 9 \text{ mm (SM400)}$
Manhole width	$b = 800 \text{ mm}$
Manhole height	$h = 1000 \text{ mm}$

(b) Section of girder

Upper flange

Web spacing	$B_u = 2200 \text{ mm}$	$T_u = 32 \text{ mm}$	$A_u = 704.00 \text{ cm}^2$
Over edge length at left side	$B_{uL} = 125 \text{ mm}$	$T_{uL} = 32 \text{ mm}$	$A_{uL} = 40.00 \text{ cm}^2$
Over edge length at right side	$B_{uR} = 125 \text{ mm}$	$T_{uR} = 32 \text{ mm}$	$A_{uR} = 40.00 \text{ cm}^2$
Slope	$= 0.57 \%$		
Rib section	2-PL 260* 25	$A = 130.00 \text{ cm}^2$	
Total area	$F_u = 914.0 \text{ cm}^2$		

Lower flange

$$\begin{aligned} \text{Web spacing} \quad \quad \quad \text{BL} &= 2200 \text{ mm}, \text{TL} = 26 \text{ mm}, \text{AL} = 572.00 \text{ cm}^2 \\ \text{Over edge length at left side} \quad \text{BLL} &= 125 \text{ mm}, \text{TLL} = 26 \text{ mm}, \text{ALL} = 32.50 \text{ cm}^2 \\ \text{Over edge length at right side} \quad \text{BLR} &= 125 \text{ mm}, \text{TLR} = 26 \text{ mm}, \text{ALR} = 32.50 \text{ cm}^2 \\ \text{Rib section} \quad \quad \quad \text{5-PL 260*25} \quad \quad \quad \text{A} &= 325.00 \text{ cm}^2 \\ \text{Total area} \quad \quad \quad \text{FL} &= 962.0 \text{ cm}^2 \end{aligned}$$

Web

$$\begin{aligned} \text{Height} \quad \quad \quad \text{Hw} &= 2400 \text{ mm} \\ \text{Thickness} \quad \quad \quad \text{Tw} &= 16 \text{ mm} \\ \text{Total area} \quad \quad \quad \text{Fh} &= 384.0 \text{ cm}^2 \end{aligned}$$

(2) Checking diaphragm spacing

Limit spacing of diaphragms

$$\begin{aligned} \text{Lu} &= 33.816 \leq 50.000 \text{ m} \\ \text{Therefore, Ldreq} &= 6.000 \text{ m} \end{aligned}$$

(3) Calculation of Aperture ratio ρ

$$\begin{aligned} \rho &= \sqrt{\{ (b * h) / ((\text{Bu} + \text{BL}) * \text{Hw} / 2) \}} \\ &= \sqrt{\{ (800 * 1000) / ((2200 + 2200) * 2400 / 2) \}} = 0.39 < 0.40 \end{aligned}$$

Therefore, the Solid type

(4) Calculation of required stiffness of diaphragm

(a) Calculation of warping constant I_{dw}

$$\begin{aligned} e &= I_L / \text{BL} + ((\text{Bu} + 2 * \text{BL}) / 12) * \text{Fh} \\ &= 4060216 / 220.0 + ((220.0 + 2 * 220.0) / 12) * 384.0 = 39576 \text{ cm}^3 \\ f &= I_u / \text{Bu} + ((2 * \text{Bu} + \text{BL}) / 12) * \text{Fh} \\ &= 4096411 / 220.0 + ((2 * 220.0 + 220.0) / 12) * 384.0 = 39740 \text{ cm}^3 \\ \alpha_1 &= e / (e + f) * (\text{Bu} + \text{BL}) / 4 * \text{Hw} \\ &= 39576 / (39576 + 39740) * (220.0 + 220.0) / 4 * 240.0 = 13173 \text{ cm}^2 \\ \alpha_2 &= f / (e + f) * (\text{Bu} + \text{BL}) / 4 * \text{Hw} \\ &= 39740 / (39576 + 39740) * (220.0 + 220.0) / 4 * 240.0 = 13227 \text{ cm}^2 \\ I_{dw} &= 1/3 \{ \alpha_1^2 * \text{Fu} * (1 + (\text{bu}_1 + \text{bu}_2) / \text{Bu})^2 \\ &\quad + \alpha_2^2 * \text{FL} * (1 + (\text{bL}_1 + \text{bL}_2) / \text{BL})^2 \\ &\quad + 2 * (\alpha_1^2 - \alpha_1 * \alpha_2 + \alpha_2^2) * \text{Fh} \} \\ &= 1/3 \{ 13173^2 * 914.0 * (1 + (12.5 + 12.5) / 220.0)^2 \\ &\quad + 13227^2 * 962.0 * (1 + (12.5 + 12.5) / 220.0)^2 \\ &\quad + 2 * (13173^2 - 13173 * 13227 + 13227^2) * 384.0 \} \\ &= 1.797 * 10^{11} \text{ cm}^6 = 1.797 * 10^{17} \text{ mm}^6 \end{aligned}$$

Iu	: Moment of inertia about vertical axis for uflg incl. ribs =	4096411 cm ⁴
IL	: Moment of inertia about vertical axis for lflg incl. ribs =	4060216 cm ⁴
Fu	: Total section area of upper flange (including ribs) =	914.0 cm ²
FL	: Total section area of lower flange (including ribs) =	962.0 cm ²
Fh	: Section area of web par piece =	384.0 cm ²
Hw	: Height of web =	240.0 cm

(b) Calculation of required stiffness Kreq

$$K_{req} = 20 * E_s * I_{dw} / L_d^3$$

$$= 20 * 2.0 * 10^5 * 1.797 * 10^{17} / 5449.0^3 = 4.444 * 10^{12} \text{ N} \cdot \text{mm}$$

$$E_s : \text{Young's modulus of steel} = 2.0 * 10^5 \text{ N/mm}^2$$

I_{dw} : Warping constant

L_d : Actual interval of diaphragms

(5) Calculation of actual stiffness of diaphragms

(a) Actual stiffness

$$K = 4 * G_s * A * t_d$$

$$= 4 * 7.7 * 10^4 * 240.0 * (220.0 + 220.0) * 10^3 / 2 * 0.9 = 1.464 * 10^{13} \text{ N} \cdot \text{mm}$$

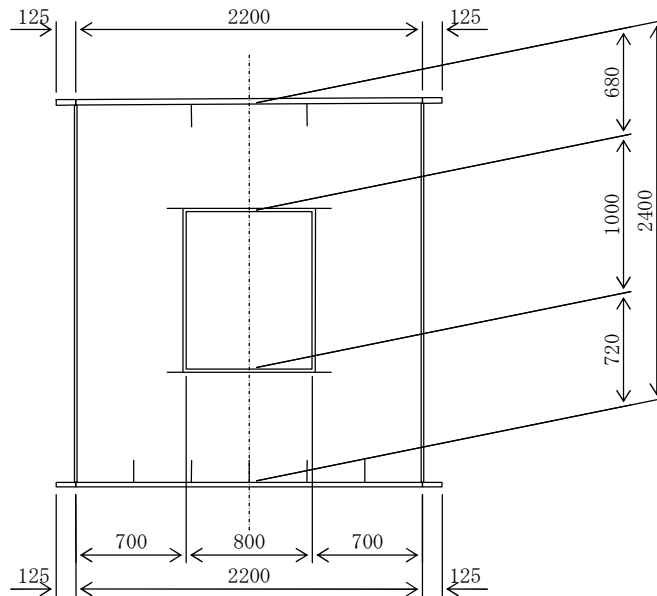
$$> K_{req} = 4.444 * 10^{12} \text{ N} \cdot \text{mm}$$

$$G_s : \text{Shear modulus of elasticity of steel} = 7.7 * 10^4 \text{ N/mm}^2$$

A : Main girder area

2. Girder G-2

(1) Design conditions



(a) Diaphragm

Equivalent span	$L_u = 33.867 \text{ m}$
Interval of diaphragms	$L_d = 5.451 \text{ m}$
Thickness of diaphragm	$T_d = 9 \text{ mm (SM400)}$
Manhole width	$b = 800 \text{ mm}$
Manhole height	$h = 1000 \text{ mm}$

(b) Section of girder

Upper flange

Web spacing	$B_u = 2200 \text{ mm}$	$T_u = 36 \text{ mm}$	$A_u = 792.00 \text{ cm}^2$
Over edge length at left side	$B_{uL} = 125 \text{ mm}$	$T_{uL} = 36 \text{ mm}$	$A_{uL} = 45.00 \text{ cm}^2$
Over edge length at right side	$B_{uR} = 125 \text{ mm}$	$T_{uR} = 36 \text{ mm}$	$A_{uR} = 45.00 \text{ cm}^2$
Slope	$= 0.58 \%$		
Rib section	2-PL 260*25	$A = 130.00 \text{ cm}^2$	
Total area	$F_u = 1012.0 \text{ cm}^2$		

Lower flange

Web spacing	$B_L = 2200 \text{ mm}$	$T_L = 29 \text{ mm}$	$A_L = 638.00 \text{ cm}^2$
Over edge length at left side	$B_{LL} = 125 \text{ mm}$	$T_{LL} = 29 \text{ mm}$	$A_{LL} = 36.25 \text{ cm}^2$
Over edge length at right side	$B_{LR} = 125 \text{ mm}$	$T_{LR} = 29 \text{ mm}$	$A_{LR} = 36.25 \text{ cm}^2$
Rib section	5-PL 260*25	$A = 325.00 \text{ cm}^2$	
Total area	$F_L = 1035.5 \text{ cm}^2$		

Web

$$\text{Height} \quad H_w = 2400 \text{ mm}$$

$$\text{Thickness} \quad T_w = 16 \text{ mm}$$

$$\text{Total area} \quad F_h = 384.0 \text{ cm}^2$$

(2) Checking diaphragm spacing

Limit spacing of diaphragms

$$L_u = 33.867 \leq 50.000 \text{ m}$$

$$\text{Therefore, } L_{dreq} = 6.000 \text{ m}$$

(3) Calculation of Aperture ratio ρ

$$\rho = \sqrt{\{ (b * h) / ((B_u + B_L) * H_w / 2) \}}$$

$$= \sqrt{\{ (800 * 1000) / ((2200 + 2200) * 2400 / 2) \}} = 0.39 < 0.40$$

Therefore, the Solid type

(4) Calculation of required stiffness of diaphragm

(a) Calculation of warping constant I_{dw}

$$e = I_L / B_L + ((B_u + 2 * B_L) / 12) * F_h$$

$$= 4427869 / 220.0 + ((220.0 + 2 * 220.0) / 12) * 384.0 = 41247 \text{ cm}^3$$

$$f = I_u / B_u + ((2 * B_u + B_L) / 12) * F_h$$

$$= 4586615 / 220.0 + ((2 * 220.0 + 220.0) / 12) * 384.0 = 41968 \text{ cm}^3$$

$$\alpha_1 = e / (e + f) * (B_u + B_L) / 4 * H_w$$

$$= 41247 / (41247 + 41968) * (220.0 + 220.0) / 4 * 240.0 = 13086 \text{ cm}^2$$

$$\alpha_2 = f / (e + f) * (B_u + B_L) / 4 * H_w$$

$$= 41968 / (41247 + 41968) * (220.0 + 220.0) / 4 * 240.0 = 13314 \text{ cm}^2$$

$$I_{dw} = 1/3 \{ \alpha_1^2 * F_u * (1 + (b_{u1} + b_{u2}) / B_u)^2$$

$$+ \alpha_2^2 * F_L * (1 + (b_{L1} + b_{L2}) / B_L)^2$$

$$+ 2 * (\alpha_1^2 - \alpha_1 * \alpha_2 + \alpha_2^2) * F_h \}$$

$$= 1/3 \{ 13086^2 * 1012.0 * (1 + (12.5 + 12.5) / 220.0)^2$$

$$+ 13314^2 * 1035.5 * (1 + (12.5 + 12.5) / 220.0)^2$$

$$+ 2 * (13086^2 - 13086 * 13314 + 13314^2) * 384.0 \}$$

$$= 1.921 * 10^{11} \text{ cm}^6 = 1.921 * 10^{17} \text{ mm}^6$$

$$I_u : \text{Moment of inertia about vertical axis for uflg incl. ribs} = 4586615 \text{ cm}^4$$

$$I_L : \text{Moment of inertia about vertical axis for lflg incl. ribs} = 4427869 \text{ cm}^4$$

$$F_u : \text{Total section area of upper flange (including ribs)} = 1012.0 \text{ cm}^2$$

$$F_L : \text{Total section area of lower flange (including ribs)} = 1035.5 \text{ cm}^2$$

$$F_h : \text{Section area of web par piece} = 384.0 \text{ cm}^2$$

$$H_w : \text{Height of web} = 240.0 \text{ cm}$$

(b) Calculation of required stiffness K_{req}

$$K_{req} = 20 * E_s * I_{dw} / L_d^3$$
$$= 20 * 2.0 * 10^5 * 1.921 * 10^{17} / 5451.0^3 = 4.745 * 10^{12} \text{ N} \cdot \text{mm}$$

E_s : Young's modulus of steel = $2.0 * 10^5 \text{ N/mm}^2$

I_{dw} : Warping constant

L_d : Actual interval of diaphragms

(5) Calculation of actual stiffness of diaphragms

(a) Actual stiffness

$$K = 4 * G_s * A * t_d$$
$$= 4 * 7.7 * 10^4 * 240.0 * (220.0 + 220.0) * 10^3 / 2 * 0.9 = 1.464 * 10^{13} \text{ N} \cdot \text{mm}$$
$$> K_{req} = 4.745 * 10^{12} \text{ N} \cdot \text{mm}$$

G_s : Shear modulus of elasticity of steel = $7.7 * 10^4 \text{ N/mm}^2$

A : Main girder area

5-3 Stiffener for Jack up

1. Design force for Jack up (When replacing bearing)

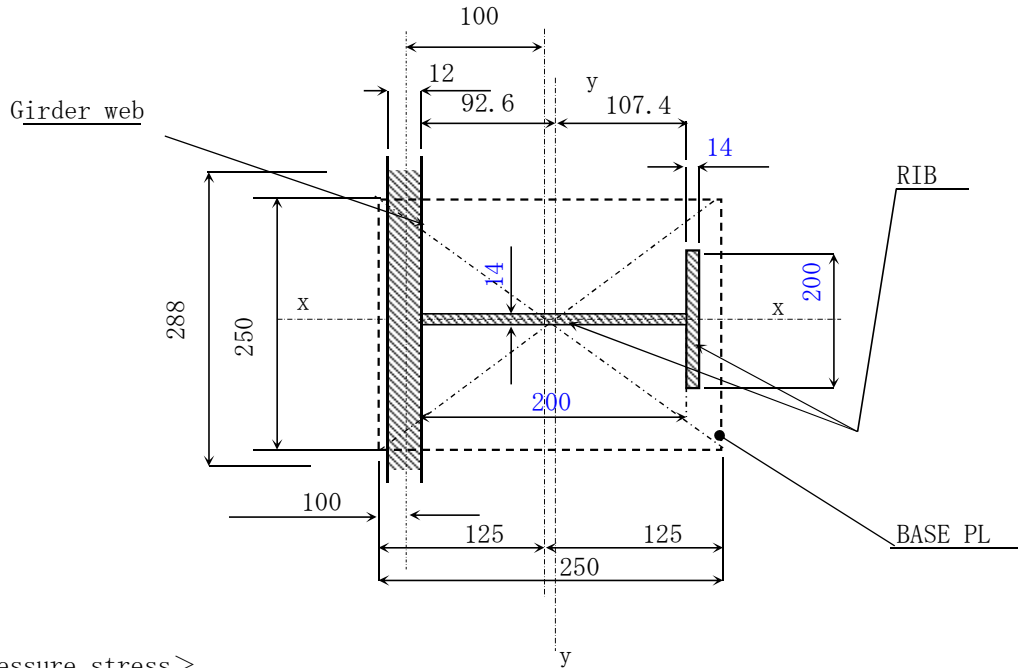
(kN)

		Rd+RL MAX	N	Non-uniformity coefficient	Force
S1	G1	2672.14	2	1.1	1500
	G2	2461.15	2	1.1	1400
PF3	G1	7291.47	4	1.1	2100
	G2	7428.30	4	1.1	2100
PF4	G1	7480.64	4	1.1	2100
	G2	7276.45	4	1.1	2100
S2	G1	2266.57	2	1.1	1300
	G2	2844.86	2	1.1	1600

2. Reinforcement rib for jack up design

(1) Supprt (End side)

Force R = 1600.00 (KN)
 Jack 200 t
 tw = 12 (mm)
 Hw = 2350 (mm)
 Left side Effective width ll = 144 (mm)
 Right side Effective width lr = 144 (mm)
 90 °
 SM 490 Y



<pressure stress>

					A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)	
1	-Stiff PL	200	x	14	(SM 490 Y)	28.00	-10.70	-300	3210
1	-Stiff PL	200	x	14	(SM 490 Y)	28.00	---	---	933
1	-WEB PL	288	x	12	(SM 490 Y)	34.56	10.60	366	3887
ΣA =					90.56		67	8031	

$$e = Ay / A = 0.74 \text{ cm} \quad y_u = 12.14 \text{ cm}$$

$$I_x = Ay^2 - e^2 A = 7982 \text{ cm}^4 \quad y_l = 10.46 \text{ cm}$$

$$\Sigma A = 90.56 < 1.7 \times 56.00 = 95.20 \text{ (cm}^2\text{)}$$

$$\therefore A = 90.56 \text{ (cm}^2\text{)}$$

$$R_x = \sqrt{ (7982 / 90.56) } = 9.39 \text{ (cm)}$$

<Rib >

$$\text{width} = 200 \text{ (mm)} > H_w / 30 + 50 = 128.3 \text{ (mm)}$$

$$\text{thickness} = 14 \text{ (mm)} > B / 9.5 = 9.5 \text{ (mm)}$$

<Compressive stress >

$$\begin{aligned} Lx &= 235 \times 0.8 = 188 \text{ cm} \\ Lx/rx &= 188.00 / 9.39 = 20.03 > 15 \end{aligned}$$

$$\therefore \sigma_{ca} = 202.5 \text{ (N/mm}^2\text{)}$$

$$\sigma_N = 1600.00 \times 10^3 / 9056 = 176.7 < 202.5 \text{ (N/mm}^2\text{)}$$

<pressure stress>

BASEPL

$$\begin{aligned} &250 \text{ mm} \\ ba &= 250 + 2 \times 10 = 270 \text{ mm} \\ tf &= 10 \text{ mm} \end{aligned}$$

						A (cm ²)
1	- Stiff PL	200	x	14	(SM 490 Y)	28.00
1	- Stiff PL	200	x	14	(SM 490 Y)	28.00
1	-WEB PL	270	x	12	(SM 490 Y)	32.40
$\Sigma A =$						88.40

$$\begin{aligned} \sigma_b &= R / A_b \\ &= 1600.00 \times 10^3 / 8840 \\ &= 181.0 \text{ (N/mm}^2\text{)} < 315 \text{ (N/mm}^2\text{)} \end{aligned}$$

Eccentricity moment

$$M_e = 1600.00 \times 2.37 / 1000 = 3.80 \text{ kNm}$$

Stress

$$\sigma_u = 3.80 \times 10^6 \times 12.14 \times 10 / 7982 \times 10^4 = 5.8 < \sigma_{ca} = 202.5 \text{ N/mm}^2$$

$$\sigma_l = 3.80 \times 10^6 \times 10.46 \times 10 / 7982 \times 10^4 = 5$$

$$\begin{aligned} r &= \sqrt{I/A} = \sqrt{(7982 / 90.56)} = 9.39 \\ 1/r &= 1880 / 93.9 = 20 > 15 \\ \sigma_{cag} &= 202.5 \text{ (N/mm}^2\text{)} \quad (t \leq 40) \end{aligned}$$

$$\begin{aligned} b/t &= 7.14 \leq 10.5 \\ \sigma_{cal} &= 210.0 \text{ (N/mm}^2\text{)} \quad (t \leq 40) \end{aligned}$$

$$\therefore \sigma_{ca} = 202.5 \text{ kN/mm}^2$$

$$\text{Effect of buckling} \quad \frac{\sigma_c}{\sigma_{caz}} + \frac{\sigma_{bcz}}{\sigma_{ba0} \cdot \alpha} \leq 1.0$$

$$\text{Stability} \quad \sigma_c + \frac{\sigma_{bcz}}{\alpha} \leq \sigma_{cal}$$

$$\sigma_{ey} = \pi^2 E / (1/r)^2 = 4922 \text{ N/mm}^2$$

$$\alpha = 1 - \sigma_c / (0.8 \sigma_{ey}) = 0.96$$

$$\therefore \frac{176.7}{202.5} + \frac{5.8}{202.5 \times (0.96)} = 0.90 \leq 1.0$$

$$\therefore 176.7 + \frac{5.8}{0.96} = 182.8 \leq \sigma_{cal}$$

Rib welding

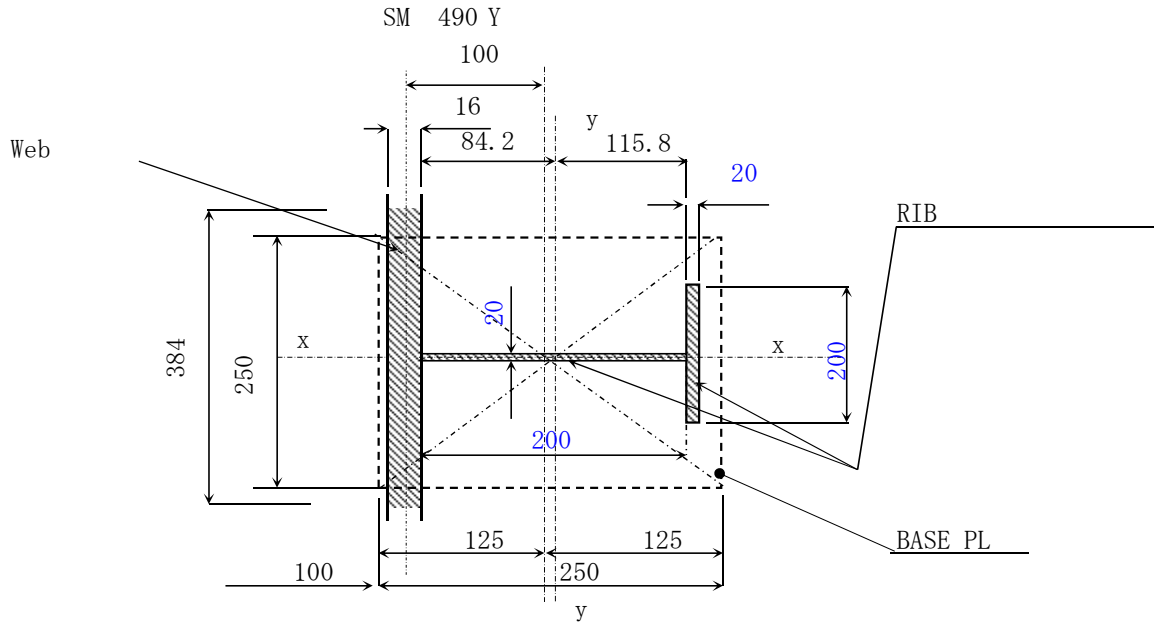
$$\begin{aligned} \text{Force} \quad R &= 1600.00 \text{ kN} \\ \text{Allowable shear stre} \quad \tau_a &= 120 \text{ N/mm}^2 \\ n &= 4 \end{aligned}$$

$$\begin{aligned} &= R / (n \times 0.707 \times H_w \times \tau_a) = 2.0 \text{ (mm)} \\ &= \sqrt{(2 \times T)} = 5.3 \text{ (mm)} \end{aligned}$$

Weld size 6 mm

(3) Supprt (Intermediate)

Force R = 2100.00 (KN)
 Jack 300 t
 tw = 16 (mm)
 Hw = 2350 (mm)
 Left side Effective width ll = 192 (mm)
 Right side Effective width lr = 192 (mm)
 90 °



<pressure stress>

					A (cm ²)	y (cm)	Ay (cm ³)	Ay ² (cm ⁴)	
1	-Stiff PL	200	x	20	(SM 490 Y)	40.00	-11.00	-440	4853
1	-Stiff PL	200	x	20	(SM 490 Y)	40.00	---	---	1333
1	-WEB PL	384	x	16	(SM 490 Y)	61.44	10.80	664	7179
					ΣA =	141.44		224	13366

$$e = Ay / A = 1.58 \text{ cm} \quad y_u = 13.58 \text{ cm}$$

$$I_x = Ay^2 - e^2 A = 13013 \text{ cm}^4 \quad y_l = 10.02 \text{ cm}$$

$$\Sigma A = 141.44 > 1.7 \times 80.00 = 136.00 \text{ (cm}^2\text{)}$$

$$\therefore A = 136.00 \text{ (cm}^2\text{)}$$

$$R_x = \sqrt{ (13013 / 136.00) } = 9.78 \text{ (cm)}$$

<Rib >

$$\text{width} = 200 \text{ (mm)} > H_w / 30 + 50 = 128.3 \text{ (mm)}$$

$$\text{thickness} = 20 \text{ (mm)} > B / 9.5 = 9.5 \text{ (mm)}$$

<Compressive stress >

$$\begin{aligned} Lx &= 235 \times 0.8 = 188 \text{ cm} \\ Lx/rx &= 188.00 / 9.78 = 19.22 > 15 \end{aligned}$$

$$\therefore \sigma_{ca} = 203.7 \text{ (N/mm}^2\text{)}$$

$$\sigma_N = 2100.00 \times 10^3 / 13600 = 154.4 < 203.7 \text{ (N/mm}^2\text{)}$$

<pressure stress>

BASEPL

$$\begin{aligned} &250 \text{ mm} \\ ba &= 250 + 2 \times 31 = 312 \text{ mm} \\ tf &= 31 \text{ mm} \end{aligned}$$

						A (cm ²)
1	- Stiff PL	200	x	20	(SM 490 Y)	40.00
1	- Stiff PL	200	x	20	(SM 490 Y)	40.00
1	-WEB PL	312	x	16	(SM 490 Y)	49.92
$\Sigma A =$						129.92

$$\begin{aligned} \sigma_b &= R / A_b \\ &= 2100.00 \times 10^3 / 12992 \\ &= 161.6 \text{ (N/mm}^2\text{)} < 315 \text{ (N/mm}^2\text{)} \end{aligned}$$

Eccentricity moment

$$M_e = 2100.00 \times 10.8 / 1000 = 22.70 \text{ kNm}$$

Stress

$$\sigma_u = 22.70 \times 10^6 \times 13.58 \times 10 / 13013 \times 10^4 = 23.7 < \sigma_{ca} = 203.7 \text{ N/mm}^2$$

$$\sigma_l = 22.70 \times 10^6 \times 10.02 \times 10 / 13013 \times 10^4 = 17.5$$

$$\begin{aligned} r &= \sqrt{I/A} = \sqrt{(13013 / 136.00)} = 9.78 \\ 1/r &= 1880 / 97.8 = 19.2 > 15 \\ \sigma_{cag} &= 203.7 \text{ (N/mm}^2\text{)} \quad (t \leq 40) \end{aligned}$$

$$\begin{aligned} b/t &= 5.00 \leq 10.5 \\ \sigma_{cal} &= 210.0 \text{ (N/mm}^2\text{)} \quad (t \leq 40) \end{aligned}$$

$$\therefore \sigma_{ca} = 203.7 \text{ kN/mm}^2$$

$$\text{Effect of buckling} \quad \frac{\sigma_c}{\sigma_{caz}} + \frac{\sigma_{bcz}}{\sigma_{ba0} \cdot \alpha} \leq 1.0$$

$$\text{Stability} \quad \sigma_c + \frac{\sigma_{bcz}}{\alpha} \leq 1.0$$

$$\sigma_{ey} = \pi^2 E / (1/r)^2 = 5344 \text{ N/mm}^2$$

$$\alpha = 1 - \sigma_c / (0.8 \sigma_{ey}) = 0.96$$

$$\therefore \frac{154.4}{203.7} + \frac{23.7}{203.7 \times (0.96)} = 0.88 \leq 1.0$$

$$\therefore 154.4 + \frac{23.7}{0.96} = 179 \leq \sigma_{cal}$$

Rib welding

$$\begin{aligned} \text{Force} \quad R &= 2100.00 \text{ kN} \\ \text{Allowable shear stress} \quad \tau_a &= 120 \text{ N/mm}^2 \\ n &= 4 \end{aligned}$$

Weld size 7 mm

5-4 Calculation of Stiffener for lateral Force

(1) Lateral Force

1) Longitudinal Direction

L1		Force	$F \gamma$ (kN)	α	H (kN)
S1 (PF2)	G1	1610	805.00	1.5	537
	G2		805.00	1.5	537
PF3	G1	3120	1560.00	1.5	1040
	G2		1560.00	1.5	1040
PF4	G1	2530	1265.00	1.5	843
	G2		1265.00	1.5	843
S2 (PF5)	G1	1380	690.00	1.5	460
	G2		690.00	1.5	460

Rd : Reaction of Dead Load

kH : seismic intensity

α : Constant coefficient

H : Force

2) Transverse Direction

L1		force	$F \gamma$ (kN)	α	H (kN)
S1 (PF2)	G1	980	490.00	1.5	327
	G2		490.00	1.5	327
PF3	G1	3490	1745.00	1.5	1163
	G2		1745.00	1.5	1163
PF4	G1	3010	1505.00	1.5	1003
	G2		1505.00	1.5	1003
S2 (PF5)	G1	1160	580.00	1.5	387
	G2		580.00	1.5	387

Design Force

			H (kN)	tf (mm)	ST (mm)	SH (mm)	H (mm)	L1	L2	P	q1
S1 (PF2)	G1	Longitudinal Direction	537	10	33	351	394	760	810	278.22	343
		Transverse Direction	327	10	33	351	394	760	810	158.90	209
	G2	Longitudinal Direction	537	10	35	351	396	760	810	279.63	345
		Transverse Direction	327	10	35	351	396	760	810	159.71	210
PF3	G1	Longitudinal Direction	1040	26	36	524	586	1210	1210	503.67	416
		Transverse Direction	1163	26	36	524	586	1210	1210	563.40	466
	G2	Longitudinal Direction	1040	29	40	524	593	1210	1210	509.69	421
		Transverse Direction	1163	29	40	524	593	1210	1210	570.13	471
PF4	G1	Longitudinal Direction	843	27	30	524	581	1210	1210	404.94	335
		Transverse Direction	1003	27	30	524	581	1210	1210	481.76	398
	G2	Longitudinal Direction	843	31	29	524	584	1210	1210	407.03	336
		Transverse Direction	1003	31	29	524	584	1210	1210	484.25	400
S2 (PF5)	G1	Longitudinal Direction	460	10	24	351	385	760	810	233.03	288
		Transverse Direction	387	10	24	351	385	760	810	183.79	242
	G2	Longitudinal Direction	460	10	24	351	385	760	810	233.03	288
		Transverse Direction	387	10	24	351	385	760	810	183.79	242

tf :Lflange Thickness

ST :Sole PL Thickness

SH :Bearing Height

H : Total Height

L1 : Longitudinal Direction length for sole plate

L2 : Transverse Direction length for sole plate

P : Vertical force due to couple of force

q1 : distributed load

(2) Girder end side Support

1) Stiffener for Transverse Direction

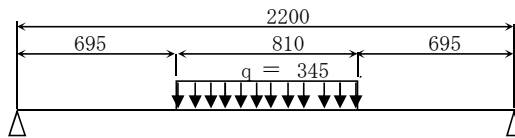
a) Effective width

Lower Flange

$$\begin{aligned}
 b &= 760 / 2 = 380.0 \text{ mm (soleの1/2)} \\
 l &= 2200 \text{ mm} & b/l &= 0.17 < 0.3 \\
 \lambda d/2 &= (1.1 - 2(b/l))b & &= 286.52 \text{ mm} \\
 \therefore \lambda d &= 573.0 \text{ mm}
 \end{aligned}$$

b) Design force

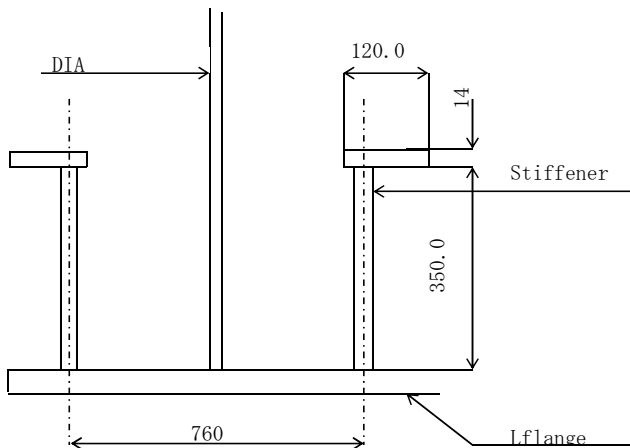
$$\begin{aligned}
 L &= 2.200 \text{ m} \\
 \lambda &= 0.810 \text{ m} \\
 q &= 345.2 \text{ kN/m} \\
 M &= \lambda xq/4x(L - \lambda/2) = 125.5 \text{ kN}\cdot\text{m} \\
 S &= \lambda xq/2 = 139.8 \text{ kN}
 \end{aligned}$$



c) Checking Stress

SM490Y	b (mm)	t (mm)	A (mm ²)	y (mm)	A·y	Ay ² or I
1-flg	120.0	14	1680	-182	-305760	5.565E+07 SM490Y
1-WEB	350.0	10	3500	0	0	3.573E+07 SM490Y
1-Lflg	573.0	10	5730	180	1031472	1.857E+08 (SM490Y)
Σ			10910		725712	2.770E+08
δ = Σ (Ay) / Σ A			66.5 mm		$\frac{-\Sigma A \cdot \delta^2}{I_r}$	$\frac{-4.827E+07}{2.288E+08}$
Y _u =	255.5 mm					
Y _l =	118.5 mm					

$$\begin{aligned}
 \sigma_u &= M \cdot Y_u / I_r = 140.2 \text{ N/mm}^2 < \sigma_a = 210 \text{ N/mm}^2 \\
 \sigma_l &= M \cdot Y_l / I_r = 65.0 \text{ N/mm}^2 < \sigma_a = 210 \text{ N/mm}^2 \\
 \tau &= S / A = 39.9 \text{ N/mm}^2 < \tau_a = 120 \text{ N/mm}^2 \\
 KU &= \sqrt{((\sigma_u / \sigma_a)^2 + (\tau / \tau_a)^2)} = 0.71 < 1.2 \\
 KL &= \sqrt{((\sigma_l / \sigma_a)^2 + (\tau / \tau_a)^2)} = 0.44 < 1.2
 \end{aligned}$$



2) Stiffener for Longitudinal Direction

a) Effective width

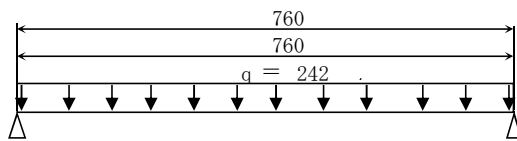
Lower Flange

$$\begin{aligned}
 b &= 733 / 2 = 366.5 \text{ mm} \\
 l &= 760 \text{ mm} & b/l &= 0.48 > 0.3 \\
 \lambda d/2 &= 0.15 \times L & &= 114 \text{ mm} \\
 \therefore \lambda d &= 228.0 \text{ mm}
 \end{aligned}$$

b) Design Force

$$\begin{aligned}
 L &= 0.760 \text{ m} \\
 \lambda &= 0.760 \text{ m} \\
 q &= 241.8 \text{ kN/m}
 \end{aligned}$$

$$\begin{aligned}
 M &= \lambda xq/4x(L - \lambda/2) &= 17.5 \text{ kN}\cdot\text{m} \\
 S &= \lambda xq/2 &= 91.9 \text{ kN}
 \end{aligned}$$



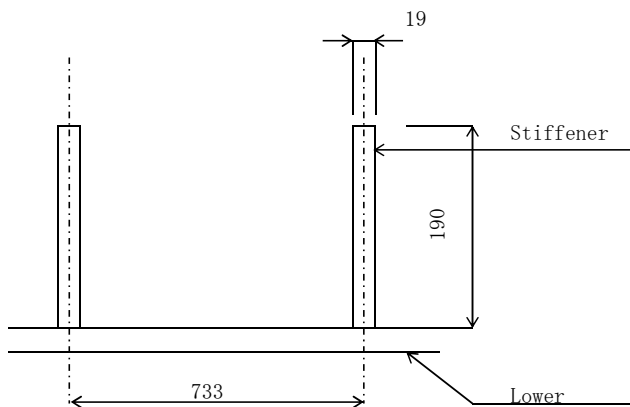
c) Checking Stress

SM490Y

	b (mm)	t (mm)	A (mm ²)	y (mm)	A·y	Ay ² or I
1-TRIB	190	19	3610	0	0	1.086E+07 SM490Y
1-Lflg	228	10	2280	100	228000	2.280E+07 (SM490Y)
Σ			5890		228000	3.366E+07
$\delta = \Sigma (Ay) / \Sigma A$			38.7 mm		$-\Sigma A \cdot \delta^2$	-8.826E+06
					$I_r =$	2.483E+07

$$\begin{aligned}
 Y_u &= 133.7 \text{ mm} \\
 Y_l &= 66.3 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 \sigma_u &= M \cdot Y_u / I_r &= 94.0 \text{ N/mm}^2 &< \sigma_a &= 210 \text{ N/mm}^2 \\
 \sigma_l &= M \cdot Y_l / I_r &= 46.6 \text{ N/mm}^2 &< \sigma_a &= 210 \text{ N/mm}^2 \\
 \tau &= S / A &= 25.5 \text{ N/mm}^2 &< \tau_a &= 120 \text{ N/mm}^2
 \end{aligned}$$



3) Welding

Stiffener for Transverse Direction

Welding Size

$$s1 = \frac{R \cdot \sqrt{2}}{2 \cdot \tau_a \cdot h_s} = \frac{139814 \cdot \sqrt{2}}{2 \cdot 120 \cdot 350} = 2.4 \text{ mm}$$

$$s2 = \sqrt{2t} = \sqrt{2 \cdot 10} = 4.5 \text{ mm}$$

Size 6.00 mm

Stiffener for Longitudinal Direction

Welding Size

$$s1 = \frac{R \cdot \sqrt{2}}{2 \cdot \tau_a \cdot h_s} = \frac{91895 \cdot \sqrt{2}}{2 \cdot 120 \cdot 190} = 2.9 \text{ mm}$$

$$s2 = \sqrt{2t} = \sqrt{2 \cdot 19} = 6.2 \text{ mm}$$

Size 7.00 mm

(4) Intermediate Support

1) Stiffener for Transverse Direction

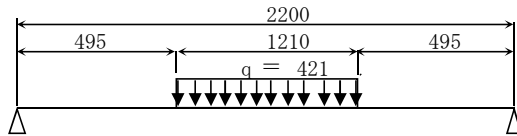
a) Effective width

Lower Flange

$$\begin{aligned}
 b &= 1210 / 2 = 605.0 \text{ mm (soleの1/2)} \\
 l &= 2200 \text{ mm} & b/l &= 0.28 > 0.3 \\
 \lambda d/2 &= (1.1 - 2(b/l))b & &= 326.7 \text{ mm} \\
 \therefore \lambda d &= 653.4 \text{ mm}
 \end{aligned}$$

b) Design force

$$\begin{aligned}
 L &= 2.200 \text{ m} \\
 \lambda &= 1.210 \text{ m} \\
 q &= 421.2 \text{ kN/m} \\
 M &= \lambda xq/4x(L - \lambda/2) = 203.2 \text{ kN}\cdot\text{m} \\
 S &= \lambda xq/2 = 254.8 \text{ kN}
 \end{aligned}$$

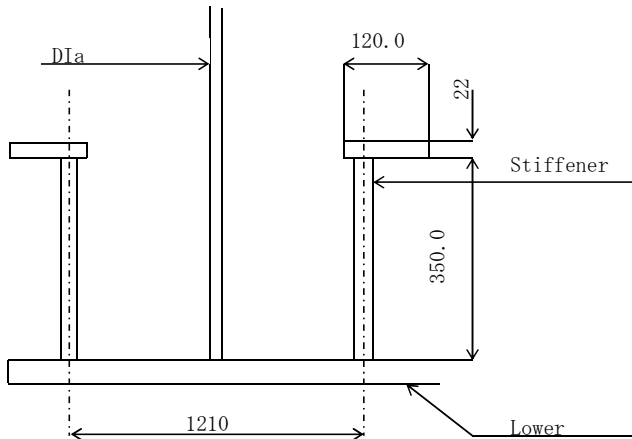


c) Checking Stress

	b (mm)	t (mm)	A (mm ²)	y (mm)	A·y	Ay ² or I	
1-flg	120.0	22	2640	-186	-491040	9.133E+07	SM490Y
1-WEB	350.0	10	3500	0	0	3.573E+07	SM490Y
1-Lflg	653.4	26	16988	188	3193819	6.004E+08	(SM490Y)
Σ			23128		2702779	7.275E+08	
δ = Σ (Ay) / Σ A			116.9 mm		-Σ A · δ ²	-3.158E+08	
					I _r =	4.117E+08	

$$\begin{aligned}
 Y_u &= 313.9 \text{ mm} \\
 Y_l &= 84.1 \text{ mm}
 \end{aligned}$$

$$\begin{aligned}
 \sigma_u &= M \cdot Y_u / I_r = 155.0 \text{ N/mm}^2 < \sigma_a = 210 \text{ N/mm}^2 \\
 \sigma_l &= M \cdot Y_l / I_r = 41.5 \text{ N/mm}^2 < \sigma_a = 210 \text{ N/mm}^2 \\
 \tau &= S / A = 72.8 \text{ N/mm}^2 < \tau_a = 120 \text{ N/mm}^2 \\
 KU &= \sqrt{((\sigma_u / \sigma_a)^2 + (\tau / \tau_a)^2)} = 0.92 < 1.2 \\
 KL &= \sqrt{((\sigma_l / \sigma_a)^2 + (\tau / \tau_a)^2)} = 0.62 < 1.2
 \end{aligned}$$



2) Stiffener for Longitudinal Direction

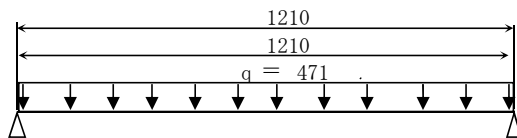
a) Effective width

Lower Flange

$$\begin{aligned}
 b &= 1466.7 / 2 = 733.4 \text{ mm} \\
 l &= 1210 \text{ mm} & b/l &= 0.61 > 0.3 \\
 \lambda d/2 &= 0.15 \times L & &= 181.5 \text{ mm} \\
 \therefore \lambda d &= 363.0 \text{ mm}
 \end{aligned}$$

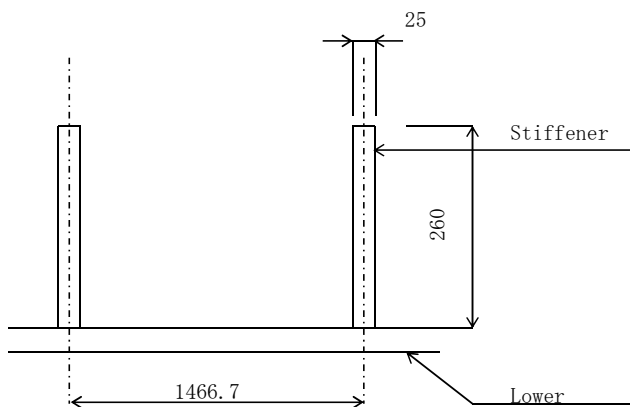
b) Design Force

$$\begin{aligned}
 L &= 1.210 \text{ m} \\
 \lambda &= 1.210 \text{ m} \\
 q &= 471.2 \text{ kN/m} \\
 M &= \lambda xq/4x(L-\lambda/2) = 86.2 \text{ kN}\cdot\text{m} \\
 S &= \lambda xq/2 = 285.1 \text{ kN}
 \end{aligned}$$



c) Checking Stress

SM490Y						
	b (mm)	t (mm)	A (mm ²)	y (mm)	A·y	Ay ² or I
1-TRIB	260	25	6500	0	0	3.662E+07 SM490Y
1-Lflg	363	26	9438	143	1349634	1.930E+08 (SM490Y)
Σ			15938		1349634	2.296E+08
$\delta = \Sigma (Ay) / \Sigma A$			84.7 mm		$\frac{-\Sigma A \cdot \delta^2}{I_r}$	$\frac{-1.143E+08}{1.153E+08}$
$Y_u =$	214.7 mm					
$Y_l =$	71.3 mm					
$\sigma_u = M \cdot Y_u / I_r$						$= 160.5 \text{ N/mm}^2 < \sigma_a = 210 \text{ N/mm}^2$
$\sigma_l = M \cdot Y_l / I_r$						$= 53.3 \text{ N/mm}^2 < \sigma_a = 210 \text{ N/mm}^2$
$\tau = S / A$						$= 43.9 \text{ N/mm}^2 < \tau_a = 120 \text{ N/mm}^2$



3) Welding

Stiffener for Transverse Direction

Welding Size

$$s1 = \frac{R \cdot \sqrt{2}}{2 \cdot \tau_a \cdot h_s} = \frac{254844 \cdot \sqrt{2}}{2 \cdot 120 \cdot 350} = 4.3 \text{ mm}$$

$$s2 = \sqrt{2t} = \sqrt{2 \cdot 10} = 4.5 \text{ mm}$$

Size 6.00 mm

Stiffener for Longitudinal Direction

Welding Size

$$s1 = \frac{R \cdot \sqrt{2}}{2 \cdot \tau_a \cdot h_s} = \frac{285064 \cdot \sqrt{2}}{2 \cdot 120 \cdot 260} = 6.5 \text{ mm}$$

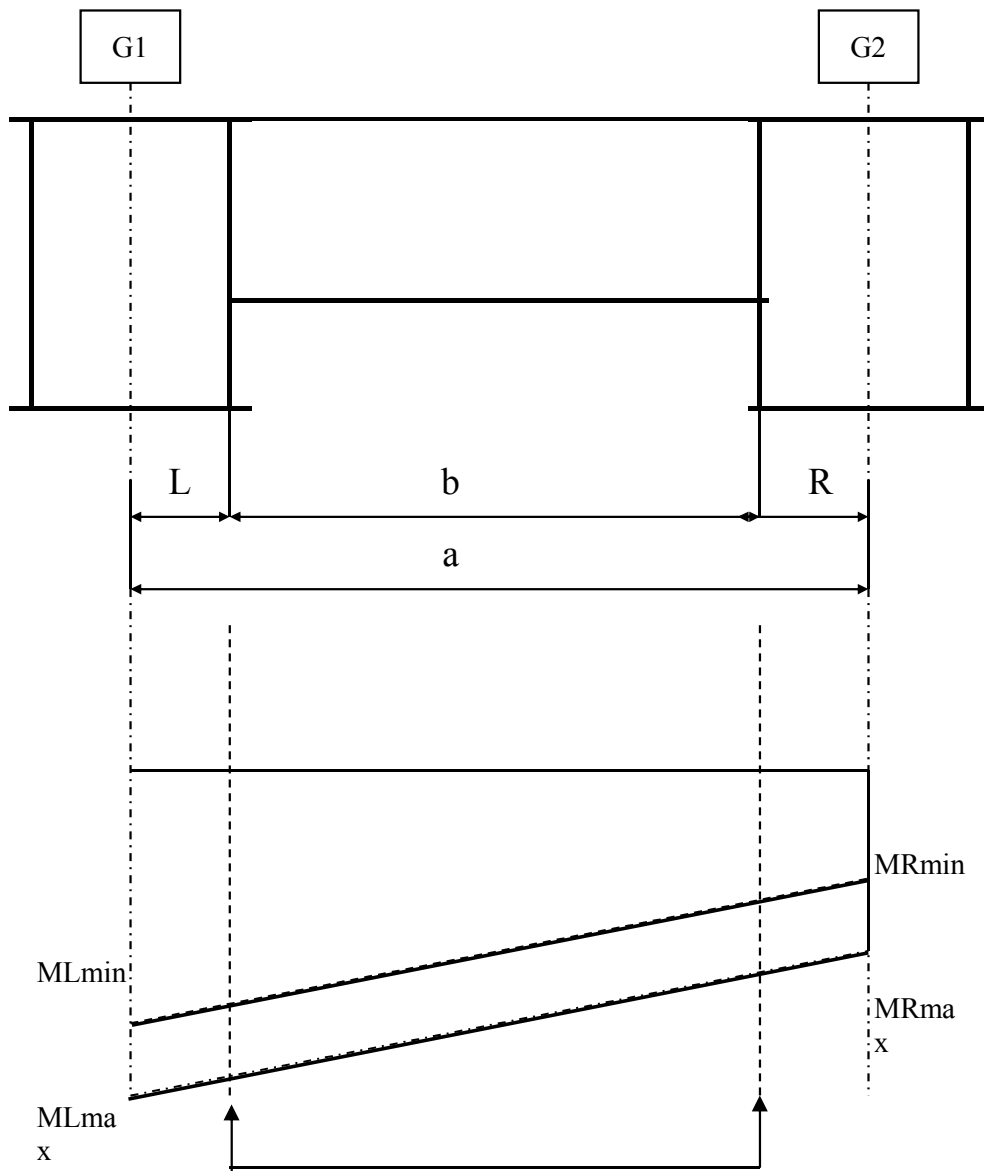
$$s2 = \sqrt{2t} = \sqrt{2 \cdot 25} = 7.1 \text{ mm}$$

Size 8.00 mm

§6. Design of Cross Beam

6-1 Design Method

- In the design of cross beam at the end of main girder, the greater value is used comparing with the sectional force by Floor system and the grid sectional force calculated from grid analysis.
- In the design of intermediate cross beam and cross beam at connection part, the grid sectional force calculated from grid analysis is used.
- The grid sectional force calculated from electrical calculator is the value at the centre of main girder. The sectional force at both ends of cross beam and a joint is therefore calculated complementing the force at web as which is linear complementarity connecting the maximum and minimum value on the right and left side.



6-2 Calculation Result of Cross Beam

		CROSS BEAM					
		S2		PF4		C21	
FORCE	MOMENT	1053.17	kNm	601.52	kNm	551.5	kNm
		-832.00	kNm	-590.83	kNm	-546.8	kNm
	SHEAR	370.30	kN	380.23	kN	171.6	kN
FLANGE	mm	320	x 16	250	x 12	250	x 12
WEB	mm	1784	x 9	1788	x 9	1788	x 9
σ_t	N/mm ²	76.2	\leq 140.0	59.6	\leq 140.0	48.1	\leq 140.0
σ_c	N/mm ²	-77.4	\leq 117.1	-59.6	\leq 102.7	-48.1	\leq 102.7
τ	N/mm ²	24.1	\leq 80.0	23.6	\leq 80.0	23.5	\leq 80.0

§7. Design of Inside Stringer

7-1 Design Method

Design Method

- Inside Stringers are calculated including additional bending moment by Main Girder camber.
- Calculation model is Simple beam.
- In the Stringer, Dead load is given as equal distributed load on beam, Live load is given as concentrated load on the center of the span.

Load

Dead Load	Pavement Slab Haunch
-----------	----------------------------

Live Load

7-2 Calculation Result of Inside Stringer

		INSIDE STRINGER	
FORCE	MOMENT	369.06	kNm
		-440.31	kNm
	SHEAR	322.35	KN
FLANGE	mm	220	x 19
WEB	mm	800	x 10
σ_t	N/mm ²	84.9	\leq 140.0
σ_c	N/mm ²	-100.9	\leq 135.9
τ	N/mm ²	40.3	\leq 80.0

§8. Design of Outside Stringer and Bracket

8-1 Design Method

Design Method

- Brackets are calculated by the direct force caused by vehicle and slab load.
- Brackets are calculated as a cantilever beam model.
- Outside Stringers are calculated as a Simple beam model.
- In the Stringer, Dead load is given as equal distributed load on beam, Live load is given as concentrated load on the center of the span.

Load

Dead Load	Pavement
	Slab
	Haunch
	Concrete Barrier
	Steel Weight

Live Load

8-2 Calculation Result of Outside Stringer and Bracket

		OUTSIDE STRINGER							
		LEFT SIDE - INTERMEDIATE		LEFT SIDE - GIRDER END SIDE		RIGHT SIDE - INTERMEDIATE		RIGHT SIDE - GIRDER END SIDE	
		C11		S1		C17		S2	
FORCE	MOMENT	201.63	kNm	199.37	kNm	209.18	kNm	202.11	kNm
		-187.39	kNm	-172.58	kNm	194.53	kNm	-175.03	kNm
	SHEAR	158.29	KN	154.41	KN	160.11	KN	155.06	KN
FLANGE	mm	220	x 14	220	x 14	220	x 14	220	x 14
WEB	mm	600	x 9	600	x 9	600	x 9	600	x 9
σ_t	N/mm ²	98.1	≦ 140.0	101.5	≦ 140.0	124.4	≦ 140.0	115.7	≦ 140.0
σ_c	N/mm ²	-91.2	≦ 134.9	-87.9	≦ 135.8	-115.6	≦ 134.6	-100.3	≦ 135.6
τ	N/mm ²	29.3	≦ 80.0	28.6	≦ 80.0	29.7	≦ 80.0	28.7	≦ 80.0

		BRACKET							
		LEFT SIDE				RIGHT SIDE			
		C11		S1		C18		S2	
FORCE	MOMENT	-349.32	kNm	-287.81	kNm	-354.83	kNm	-288.74	kNm
			kNm		kNm		kNm		kNm
	SHEAR	222.97	KN	185.18	KN	226.47	KN	185.77	KN
FLANGE	mm	250	x 10	250	x 10	250	x 10	250	x 10
WEB	mm	890	x 9	890	x 9	890	x 9	890	x 9
σ_t	N/mm ²	102.4	≦ 140.0	85.0	≦ 140.0	104.7	≦ 140.0	85.2	≦ 140.0
σ_c	N/mm ²	-102.4	≦ 134.9	-85.0	≦ 134.9	-104.7	≦ 134.6	-85.2	≦ 134.6
τ	N/mm ²	27.8	≦ 80.0	23.1	≦ 80.0	28.3	≦ 80.0	23.2	≦ 80.0

§9. Fatigue Design

9-1 Condition for Fatigue design

1. Live Load

AASHTO Track load
T-load

Comparing the stress range when loading one AASHTO track load and the stress range of a pair of loads of 100 t, there is a possibility that those large stress ranges will affect fatigue. the larger stress of them shall be adopted for stress of fatigue design.

2. Load correction factor

line $n_L = 2$

$ADTT_{SLi} = 2090$

Variable stress correction factor (λ_T)

$\gamma_T = \gamma_{T1} \cdot \gamma_{T2}$

$\gamma_{T1} = 1.0 \log L_{B1} + 1.50 \quad (2.00 \leq \gamma_{T1} \leq 3.00)$

γ_{T2}

$ADTT_{SLi}$	L_{B2}	$L_{B1} \leq 50m$	$50m < L_{B1}$
	$ADTT_{SLi} \leq 2000$	1.00	1.00
$2000 < ADTT_{SLi}$		1.00	1.10

	L_{B1} (m)	L_{B2} (m)	$ADTT_{SLi}$	γ_{T1}	γ_{T2}	γ_T
First span	54.300	54.300	0.0	3.00	1.10	3.30
Second spane	70.000	70.000	0.0	3.00	1.00	3.00
The third span	54.300	54.300	0.0	3.00	1.00	3.00

3. Impact

$i f = 10/(50+L)$

	L (m)	$i f$
First span	54.300	0.096
Second spane	70.000	0.083
The third span	54.300	0.096

4. Structural analysis coefficient

$\gamma_a = \gamma_a = 0.80$ (girder)
0.50 (Cross beam)

4. Frequency correction factor

$\gamma_n = 0.03$

5. Lane traffic volume deviation coefficient

$\gamma_L = 1.0$ (Carriage way)

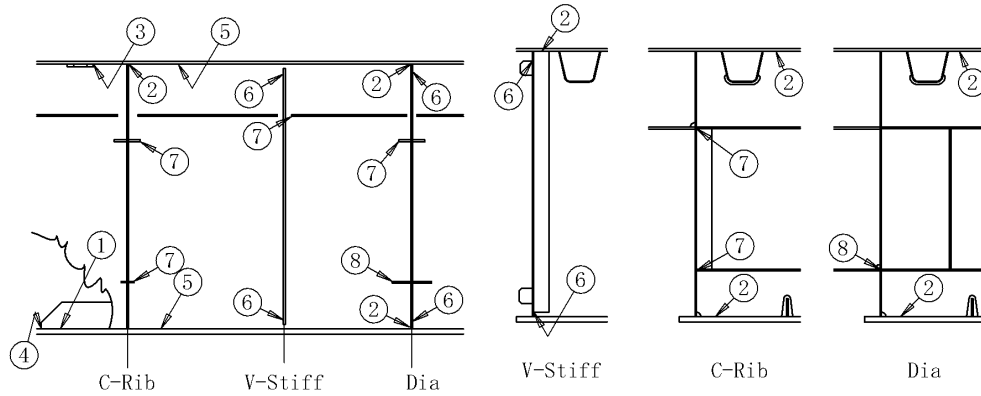
5. Comparing the stress range of 2 type Live Load

Girder		AASHTO	B-Live	(B) -(A)
Member		Stress Range(A)	Stress Range(B)	
G1	1001	2	4	2
	1002	1901	2121	221
	1003	2945	3291	346
	1004	3580	3987	407
	1005	3915	4364	450
	1006	3992	4452	460
	1007	3827	4273	447
	1008	3448	3882	434
	1009	2945	3349	404
	1010	2343	2782	440
	1011	2555	2561	6
	1012	2245	2688	443
	1013	2749	3165	416
	1014	3169	3573	404
	1015	3484	3898	414
	1016	3620	4039	419
	1017	3546	3996	449
	1018	3593	4050	457
	1019	3435	3897	462
	1020	3104	3565	462
	1021	2668	3086	418
	1022	2139	2587	448
	1023	2741	2738	-3
	1024	2395	2827	433
	1025	2928	3329	401
	1026	3371	3825	454
	1027	3681	4147	466
	1028	3790	4264	473
	1029	3689	4146	457
	1030	3357	3771	414
	1031	2753	3112	359
	1032	1784	2021	237

Girder		AASHTO	B-Live	(B) -(A)
Member		Stress Range(A)	Stress Range(B)	
G2	2001	0	4	4
	2002	2066	2074	8
	2003	3095	3207	112
	2004	3692	3865	173
	2005	4002	4215	214
	2006	4100	4314	214
	2007	3994	4191	198
	2008	3662	3893	231
	2009	3112	3483	371
	2010	2225	2998	773
	2011	1944	2965	1021
	2012	1933	2658	725
	2013	2864	3192	328
	2014	3456	3663	207
	2015	3873	4060	186
	2016	4066	4257	191
	2017	4001	4227	226
	2018	4062	4278	216
	2019	3873	4087	214
	2020	3462	3722	259
	2021	2881	3291	409
	2022	1978	2793	815
	2023	1785	2877	1093
	2024	2219	3045	826
	2025	3172	3583	411
	2026	3765	4025	260
	2027	4161	4375	214
	2028	4330	4555	225
	2029	4257	4480	222
	2030	3945	4119	174
	2031	3311	3413	101
	2032	2199	2190	-9

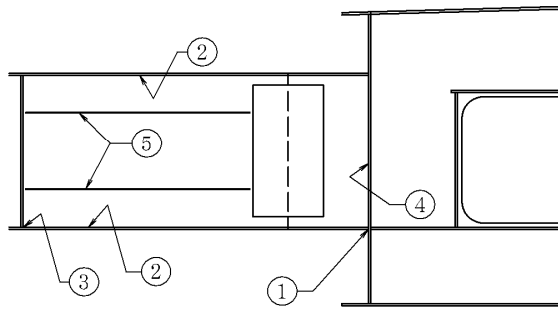
6. Checking Point and Grade

(1) GIRDER



	MAIN MEMBER	ATTACHED MEMBER	GRADE	STRESS
①	FLANGE	Longitudinal RIB	D	100
②	FLANGE	Lateral RIB	E	80
		DIA		
		V-STIFF		
③	FLANGE	HAND HOLE	F	65
⑤	MAINGIRDER-WEB	DECK	D	100
		LOWER FLANGE		
⑥	MAINGIRDER-WEB	V-STIFF	E	80
		DIA		
		CROSS BEAM		
		BLACKET		
⑦	MAINGIRDER-WEB	H-STIFF	G	50
		GUSSET PL		
		BLACKET		
⑧	MAINGIRDER-WEB	CROSS BEAM	G	50

(2) CROSS BEAM



	MEMBER	ATTACHED MEMBER	GRADE	STRESS
①	CROSS BEAM FLANGE	MAIN GIRDER WEB	E	80
②	CROSS BEAM WEB	CROSS BEAM FLANGE	D	100
③	CROSS BEAM WEB	V-STIFF	E	80
④		MAIN GIRDER WEB	E	80
⑤	CROSS BEAM WEB	H-STIFF	G	50

9-2 Checking of Fatigue Stress for Main Girder

σ_{\max} : Maximum stress (Including the effect of γ_a)

σ_{\min} : Minimum stress (Including the effect of γ_a)

σ_d : Stress of Dead load (Including the effect of γ_a)

$\Delta\sigma_{\max}$: $\sigma_{\max} - \sigma_{\min}$

C_0 : $2.0E+6 \cdot \Delta\sigma_f^{**m}$

$\Delta\sigma_f$: $2.0E+6$ Allowable stress

m : Slope constant

C_R : Correction coefficient for mean stress

C_t : Correction factor for t

Structural analysis coefficient Main Girder $\gamma_a = 0.800$

Maximum stress range checking $\Delta\sigma_{\max} \leq \Delta\sigma_{ce} \cdot C_R \cdot C_t$

Stress range cycles checking $D = \sum_i [\sum_j \{n_{ij} / (C_0 \cdot (C_R \cdot C_t)^{**m} / \Delta\sigma_{ij}^{**m})\}] \leq 1$

1. G1

STEEL-BOX G1

node U.FLG-MAX

Stress range		Stress range											
node	node	Flange	Grade									$\Delta\sigma_{ce}$ · cycle	
number	number	t(mm)	σ_{tmax}	σ_{tmin}	σ_d	($\Delta\sigma_f$)	$\Delta\sigma_{ce}$	m	$\Delta\sigma_{ve}$	CR	Ct	$\Delta\sigma_{max}$	CR · Ct
D		(N/mm2)											
(N/mm2)		(N/mm2)											
1	1 node Right	10	0.0	0.0	0.0	F (65)	46.0	3	21.0	1.300	1.000	0.0	< 59.8
1	2 node Left	10	1.7	-17.4	-66.3	F (65)	46.0	3	21.0	1.300	1.000	19.1	< 59.8
1	2 node Right	10	1.6	-17.5	-66.3	F (65)	46.0	3	21.0	1.300	1.000	19.1	< 59.8
2	3 node Left	14	2.6	-21.3	-88.6	F (65)	46.0	3	21.0	1.300	1.000	23.8	< 59.8
2	3 node Right	14	2.6	-21.3	-88.6	F (65)	46.0	3	21.0	1.300	1.000	23.8	< 59.8
3	4 node Left	14	4.0	-24.8	-106.6	F (65)	46.0	3	21.0	1.300	1.000	28.8	< 59.8
3	4 node Right	14	4.0	-24.8	-106.6	F (65)	46.0	3	21.0	1.300	1.000	28.8	< 59.8
3	5 node Left	14	5.2	-26.2	-107.2	F (65)	46.0	3	21.0	1.300	1.000	31.4	< 59.8
3	5 node Right	14	5.2	-26.2	-107.2	F (65)	46.0	3	21.0	1.300	1.000	31.4	< 59.8
4	6 node Left	14	6.5	-25.4	-90.4	F (65)	46.0	3	21.0	1.300	1.000	31.9	< 59.8
4	6 node Right	14	6.5	-25.4	-90.4	F (65)	46.0	3	21.0	1.300	1.000	31.9	< 59.8
5	7 node Left	11	9.2	-27.1	-67.7	F (65)	46.0	3	21.0	1.300	1.000	36.3	< 59.8
5	7 node Right	11	9.0	-26.3	-65.8	F (65)	46.0	3	21.0	1.300	1.000	35.3	< 59.8
5	8 node Left	11	10.2	-21.8	-8.4	F (65)	46.0	3	21.0	1.258	1.000	31.9	< 57.9
5	8 node Right	11	10.2	-21.8	-8.4	F (65)	46.0	3	21.0	1.258	1.000	31.9	< 57.9
6	9 node Left	18	8.4	-11.8	48.9	F (65)	46.0	3	21.0	1.000	1.000	20.2	< 46.0
6	9 node Right	18	9.4	-13.1	54.6	F (65)	46.0	3	21.0	1.000	1.000	22.5	< 46.0
7	10 node Left	32	7.4	-4.8	85.6	F (65)	46.0	3	21.0	1.000	0.940	12.2	< 43.2
7	10 node Right	32	7.4	-4.8	85.6	F (65)	46.0	3	21.0	1.000	0.940	12.2	< 43.2
7	11 node Left	32	9.6	-2.0	148.0	F (65)	46.0	3	21.0	1.000	0.940	11.6	< 43.2
7	11 node Right	32	9.6	-2.0	148.0	F (65)	46.0	3	21.0	1.000	0.940	11.6	< 43.2
8	12 node Left	32	7.1	-5.4	85.2	F (65)	46.0	3	21.0	1.000	0.940	12.5	< 43.2
8	12 node Right	32	7.1	-5.4	85.2	F (65)	46.0	3	21.0	1.000	0.940	12.5	< 43.2
9	13 node Left	16	8.9	-14.6	49.0	F (65)	46.0	3	21.0	1.000	1.000	23.5	< 46.0
9	13 node Right	16	7.9	-13.0	43.6	F (65)	46.0	3	21.0	1.000	1.000	21.0	< 46.0
10	14 node Left	11	7.4	-19.6	-19.8	F (65)	46.0	3	21.0	1.300	1.000	27.0	< 59.8
10	14 node Right	11	7.4	-19.5	-19.8	F (65)	46.0	3	21.0	1.300	1.000	27.0	< 59.8
10	15 node Left	11	6.5	-24.2	-71.2	F (65)	46.0	3	21.0	1.300	1.000	30.6	< 59.8
10	15 node Right	11	6.5	-24.2	-71.2	F (65)	46.0	3	21.0	1.300	1.000	30.6	< 59.8
11	16 node Left	13	4.6	-23.9	-91.2	F (65)	46.0	3	21.0	1.300	1.000	28.6	< 59.8
11	16 node Right	13	4.6	-23.9	-91.2	F (65)	46.0	3	21.0	1.300	1.000	28.6	< 59.8
12	17 node Left	13	3.7	-24.8	-100.4	F (65)	46.0	3	21.0	1.300	1.000	28.5	< 59.8
12	17 node Right	13	3.7	-24.8	-100.4	F (65)	46.0	3	21.0	1.300	1.000	28.5	< 59.8
13	18 node Left	13	4.9	-24.2	-91.2	F (65)	46.0	3	21.0	1.300	1.000	29.0	< 59.8
13	18 node Right	13	4.9	-24.1	-91.2	F (65)	46.0	3	21.0	1.300	1.000	29.0	< 59.8
14	19 node Left	11	6.9	-24.4	-70.9	F (65)	46.0	3	21.0	1.300	1.000	31.3	< 59.8
14	19 node Right	11	6.8	-24.5	-70.8	F (65)	46.0	3	21.0	1.300	1.000	31.3	< 59.8
14	20 node Left	11	7.8	-19.8	-18.3	F (65)	46.0	3	21.0	1.300	1.000	27.6	< 59.8
14	20 node Right	11	7.8	-19.8	-18.3	F (65)	46.0	3	21.0	1.300	1.000	27.6	< 59.8
15	21 node Left	17	7.5	-12.9	45.4	F (65)	46.0	3	21.0	1.000	1.000	20.4	< 46.0
15	21 node Right	17	8.5	-14.3	50.7	F (65)	46.0	3	21.0	1.000	1.000	22.8	< 46.0
16	22 node Left	34	6.8	-5.2	86.0	F (65)	46.0	3	21.0	1.000	0.926	12.0	< 42.6
16	22 node Right	34	6.7	-5.3	86.1	F (65)	46.0	3	21.0	1.000	0.926	12.0	< 42.6
17	23 node Left	36	9.8	-2.2	143.8	F (65)	46.0	3	21.0	1.000	0.913	11.9	< 42.0
17	23 node Right	36	9.8	-2.1	143.7	F (65)	46.0	3	21.0	1.000	0.913	11.9	< 42.0
17	24 node Left	36	7.3	-4.6	82.8	F (65)	46.0	3	21.0	1.000	0.913	11.9	< 42.0

17	24 node Right	36	7.3	-4.7	83.3	F (65)	46.0	3	21.0	1.000	0.913	12.0 < 42.0
18	25 node Left	20	9.2	-13.0	55.3	F (65)	46.0	3	21.0	1.000	1.000	22.2 < 46.0
18	25 node Right	20	8.4	-11.7	50.0	F (65)	46.0	3	21.0	1.000	1.000	20.1 < 46.0
19	26 node Left	11	10.6	-22.3	-5.2	F (65)	46.0	3	21.0	1.183	1.000	33.0 < 54.4
19	26 node Right	11	10.6	-22.4	-5.2	F (65)	46.0	3	21.0	1.183	1.000	33.0 < 54.4
19	27 node Left	11	9.2	-26.6	-62.0	F (65)	46.0	3	21.0	1.300	1.000	35.8 < 59.8
19	27 node Right	11	9.5	-27.4	-64.1	F (65)	46.0	3	21.0	1.300	1.000	37.0 < 59.8
20	28 node Left	14	6.6	-25.6	-87.1	F (65)	46.0	3	21.0	1.300	1.000	32.2 < 59.8
20	28 node Right	14	6.7	-25.5	-87.2	F (65)	46.0	3	21.0	1.300	1.000	32.2 < 59.8
21	29 node Left	14	5.3	-26.1	-103.1	F (65)	46.0	3	21.0	1.300	1.000	31.4 < 59.8
21	29 node Right	14	5.3	-26.1	-103.1	F (65)	46.0	3	21.0	1.300	1.000	31.4 < 59.8
21	30 node Left	14	3.9	-24.6	-102.1	F (65)	46.0	3	21.0	1.300	1.000	28.5 < 59.8
21	30 node Right	14	3.8	-24.6	-102.0	F (65)	46.0	3	21.0	1.300	1.000	28.5 < 59.8
22	31 node Left	14	2.6	-21.3	-85.6	F (65)	46.0	3	21.0	1.300	1.000	23.8 < 59.8
22	31 node Right	14	2.6	-21.4	-85.5	F (65)	46.0	3	21.0	1.300	1.000	23.9 < 59.8
23	32 node Left	10	1.4	-17.3	-61.2	F (65)	46.0	3	21.0	1.300	1.000	18.7 < 59.8
23	32 node Right	10	1.4	-17.3	-61.2	F (65)	46.0	3	21.0	1.300	1.000	18.7 < 59.8
23	33 node Left	10	0.0	-0.1	0.0	F (65)	46.0	3	21.0	1.300	1.000	0.1 < 59.8

STEEL-BOX G1

node L.FLG-MAX

Stress

range

node number	node number	FLANGE	t (mm)	σ_{tmax} (N/mm2)	σ_{tmin} (N/mm2)	Grade	σ_d (N/mm2)	$(\Delta \sigma_f)$	$\Delta \sigma_{cem}$	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$ (N/mm2)	CR · Ct	Cycle D
1	1	node Right	10	0.0	0.0	0.0 F (65)	46.0	3	21.0	1.300	1.000	0.0	< 59.8		
1	2	node Left	10	19.8	-1.8	74.9 F (65)	46.0	3	21.0	1.000	1.000	21.6	< 46.0		
1	2	node Right	10	19.8	-1.8	74.9 F (65)	46.0	3	21.0	1.000	1.000	21.6	< 46.0		
2	3	node Left	18	20.8	-2.6	86.9 F (65)	46.0	3	21.0	1.000	1.000	23.4	< 46.0		
2	3	node Right	18	20.8	-2.6	86.9 F (65)	46.0	3	21.0	1.000	1.000	23.4	< 46.0		
3	4	node Left	18	24.5	-3.8	104.7 F (65)	46.0	3	21.0	1.000	1.000	28.3	< 46.0		
3	4	node Right	18	24.5	-3.8	104.7 F (65)	46.0	3	21.0	1.000	1.000	28.3	< 46.0		
3	5	node Left	18	25.8	-5.1	105.6 F (65)	46.0	3	21.0	1.000	1.000	31.0	< 46.0		
3	5	node Right	18	25.8	-5.1	105.6 F (65)	46.0	3	21.0	1.000	1.000	31.0	< 46.0		
4	6	node Left	18	25.1	-6.5	89.5 F (65)	46.0	3	21.0	1.000	1.000	31.6	< 46.0		
4	6	node Right	18	25.1	-6.5	89.5 F (65)	46.0	3	21.0	1.000	1.000	31.6	< 46.0		
5	7	node Left	10	32.2	-10.9	80.4 F (65)	46.0	3	21.0	1.000	1.000	43.1	< 46.0		
5	7	node Right	10	27.0	-9.1	67.2 F (65)	46.0	3	21.0	1.000	1.000	36.1	< 46.0		
5	8	node Left	10	22.3	-10.5	8.7 F (65)	46.0	3	21.0	1.000	1.000	32.8	< 46.0		
5	8	node Right	10	22.3	-10.5	8.7 F (65)	46.0	3	21.0	1.000	1.000	32.8	< 46.0		
6	9	node Left	14	13.0	-9.3	-54.2 F (65)	46.0	3	21.0	1.300	1.000	22.3	< 59.8		
6	9	node Right	14	13.2	-9.4	-54.9 F (65)	46.0	3	21.0	1.300	1.000	22.6	< 59.8		
7	10	node Left	26	4.9	-7.4	-86.7 F (65)	46.0	3	21.0	1.300	0.990	12.3	< 59.2		
7	10	node Right	26	4.9	-7.4	-86.7 F (65)	46.0	3	21.0	1.300	0.990	12.3	< 59.2		
7	11	node Left	26	2.0	-9.7	-148.7 F (65)	46.0	3	21.0	1.300	0.990	11.7	< 59.2		
7	11	node Right	26	2.0	-9.7	-148.7 F (65)	46.0	3	21.0	1.300	0.990	11.7	< 59.2		
8	12	node Left	21	6.1	-8.0	-96.3 F (65)	46.0	3	21.0	1.300	1.000	14.1	< 59.8		
8	12	node Right	21	6.1	-8.0	-96.3 F (65)	46.0	3	21.0	1.300	1.000	14.1	< 59.8		
9	13	node Left	11	14.9	-9.0	-49.7 F (65)	46.0	3	21.0	1.300	1.000	23.8	< 59.8		
9	13	node Right	11	14.6	-8.8	-49.0 F (65)	46.0	3	21.0	1.300	1.000	23.4	< 59.8		
10	14	node Left	11	19.1	-7.2	19.3 F (65)	46.0	3	21.0	1.000	1.000	26.3	< 46.0		
10	14	node Right	11	19.0	-7.3	19.4 F (65)	46.0	3	21.0	1.000	1.000	26.3	< 46.0		
10	15	node Left	11	28.1	-7.5	82.8 F (65)	46.0	3	21.0	1.000	1.000	35.6	< 46.0		
10	15	node Right	11	28.2	-7.5	82.8 F (65)	46.0	3	21.0	1.000	1.000	35.7	< 46.0		
11	16	node Left	16	24.9	-4.9	94.9 F (65)	46.0	3	21.0	1.000	1.000	29.8	< 46.0		
11	16	node Right	16	25.0	-4.8	94.9 F (65)	46.0	3	21.0	1.000	1.000	29.8	< 46.0		
12	17	node Left	16	25.7	-3.8	103.9 F (65)	46.0	3	21.0	1.000	1.000	29.5	< 46.0		
12	17	node Right	16	25.7	-3.8	103.9 F (65)	46.0	3	21.0	1.000	1.000	29.5	< 46.0		
13	18	node Left	16	24.9	-5.0	93.9 F (65)	46.0	3	21.0	1.000	1.000	29.9	< 46.0		
13	18	node Right	16	24.9	-5.0	93.9 F (65)	46.0	3	21.0	1.000	1.000	29.9	< 46.0		
14	19	node Left	11	27.8	-7.8	80.7 F (65)	46.0	3	21.0	1.000	1.000	35.6	< 46.0		
14	19	node Right	11	27.8	-7.8	80.6 F (65)	46.0	3	21.0	1.000	1.000	35.6	< 46.0		
14	20	node Left	11	18.8	-7.4	17.4 F (65)	46.0	3	21.0	1.000	1.000	26.2	< 46.0		
14	20	node Right	11	18.8	-7.4	17.4 F (65)	46.0	3	21.0	1.000	1.000	26.2	< 46.0		
15	21	node Left	11	14.2	-8.5	-50.4 F (65)	46.0	3	21.0	1.300	1.000	22.7	< 59.8		
15	21	node Right	11	14.5	-8.6	-51.2 F (65)	46.0	3	21.0	1.300	1.000	23.0	< 59.8		
16	22	node Left	21	5.8	-7.7	-96.8 F (65)	46.0	3	21.0	1.300	1.000	13.5	< 59.8		
16	22	node Right	21	5.9	-7.6	-96.9 F (65)	46.0	3	21.0	1.300	1.000	13.5	< 59.8		
17	23	node Left	27	2.2	-9.9	-145.6 F (65)	46.0	3	21.0	1.300	0.981	12.1	< 58.7		
17	23	node Right	27	2.2	-9.9	-145.6 F (65)	46.0	3	21.0	1.300	0.981	12.1	< 58.7		
17	24	node Left	27	4.7	-7.4	-84.7 F (65)	46.0	3	21.0	1.300	0.981	12.2	< 58.7		
17	24	node Right	27	4.7	-7.5	-84.6 F (65)	46.0	3	21.0	1.300	0.981	12.2	< 58.7		
18	25	node Left	14	13.0	-9.4	-55.6 F (65)	46.0	3	21.0	1.300	1.000	22.3	< 59.8		
18	25	node Right	14	12.9	-9.2	-55.0 F (65)	46.0	3	21.0	1.300	1.000	22.1	< 59.8		
19	26	node Left	10	21.9	-10.5	5.1 F (65)	46.0	3	21.0	1.000	1.000	32.4	< 46.0		

19	26 node Right	10	21.9	-10.5	5.2	F (65)	46.0	3	21.0	1.000	1.000	32.4 < 46.0
19	27 node Left	10	26.2	-9.0	60.8	F (65)	46.0	3	21.0	1.000	1.000	35.1 < 46.0
19	27 node Right	10	31.2	-10.8	72.8	F (65)	46.0	3	21.0	1.000	1.000	42.0 < 46.0
20	28 node Left	16	25.8	-6.8	88.3	F (65)	46.0	3	21.0	1.000	1.000	32.6 < 46.0
20	28 node Right	16	25.9	-6.7	88.3	F (65)	46.0	3	21.0	1.000	1.000	32.6 < 46.0
21	29 node Left	16	26.4	-5.4	104.4	F (65)	46.0	3	21.0	1.000	1.000	31.8 < 46.0
21	29 node Right	16	26.4	-5.4	104.4	F (65)	46.0	3	21.0	1.000	1.000	31.8 < 46.0
21	30 node Left	16	24.9	-4.0	103.4	F (65)	46.0	3	21.0	1.000	1.000	28.9 < 46.0
21	30 node Right	16	25.0	-3.9	103.3	F (65)	46.0	3	21.0	1.000	1.000	28.9 < 46.0
22	31 node Left	14	23.0	-2.8	92.4	F (65)	46.0	3	21.0	1.000	1.000	25.8 < 46.0
22	31 node Right	14	23.0	-2.8	92.3	F (65)	46.0	3	21.0	1.000	1.000	25.8 < 46.0
23	32 node Left	10	19.0	-1.7	67.4	F (65)	46.0	3	21.0	1.000	1.000	20.6 < 46.0
23	32 node Right	10	19.0	-1.6	67.3	F (65)	46.0	3	21.0	1.000	1.000	20.6 < 46.0
23	33 node Left	10	0.1	0.0	0.0	F (65)	46.0	3	21.0	1.000	1.000	0.1 < 46.0

STEEL-BOX G1

node WEB-U-1 (Web Upper edge) WEB - 1

Stress

range	node	node	Web	Grade	$\Delta \sigma_{ce} \cdot$												
Cycle	number	number	height (mm)	t	σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR · Ct	D	
					(N/mm ²)									(N/mm ²)			
	1	1	node Right	2436	12	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
	1	2	node Left	2433	12	0	1.6	-17.3	-65.5	E(80)	62.0	3	29.0	1.300	1.000	18.9	< 80.6
	1	2	node Right	2433	12	0	1.6	-17.3	-65.5	E(80)	62.0	3	29.0	1.300	1.000	18.9	< 80.6
	2	3	node Left	2430	14	0	2.6	-21.0	-87.4	E(80)	62.0	3	29.0	1.300	1.000	23.5	< 80.6
	2	3	node Right	2430	14	0	2.6	-21.0	-87.4	E(80)	62.0	3	29.0	1.300	1.000	23.5	< 80.6
	3	4	node Left	2426	14	0	3.8	-24.6	-105.1	E(80)	62.0	3	29.0	1.300	1.000	28.4	< 80.6
	3	4	node Right	2426	14	0	3.8	-24.6	-105.1	E(80)	62.0	3	29.0	1.300	1.000	28.4	< 80.6
	3	5	node Left	2423	14	0	5.2	-25.8	-105.8	E(80)	62.0	3	29.0	1.300	1.000	31.0	< 80.6
	3	5	node Right	2423	14	0	5.2	-25.8	-105.8	E(80)	62.0	3	29.0	1.300	1.000	31.0	< 80.6
	4	6	node Left	2418	14	0	6.5	-25.0	-89.3	E(80)	62.0	3	29.0	1.300	1.000	31.5	< 80.6
	4	6	node Right	2418	14	0	6.5	-25.0	-89.3	E(80)	62.0	3	29.0	1.300	1.000	31.5	< 80.6
	5	7	node Left	2412	12	0	9.1	-26.8	-66.9	E(80)	62.0	3	29.0	1.300	1.000	35.9	< 80.6
	5	7	node Right	2412	12	0	8.9	-26.1	-65.1	E(80)	62.0	3	29.0	1.300	1.000	35.0	< 80.6
	5	8	node Left	2406	12	0	10.1	-21.4	-8.4	E(80)	62.0	3	29.0	1.260	1.000	31.5	< 78.1
	5	8	node Right	2406	12	0	10.1	-21.4	-8.4	E(80)	62.0	3	29.0	1.260	1.000	31.5	< 78.1
	6	9	node Left	2400	18	0	8.2	-11.5	48.1	E(80)	62.0	3	29.0	1.000	1.000	19.8	< 62.0
	6	9	node Right	2400	18	0	9.2	-12.9	53.7	E(80)	62.0	3	29.0	1.000	1.000	22.1	< 62.0
	7	10	node Left	2394	32	0	7.2	-4.6	82.4	E(80)	62.0	3	29.0	1.000	0.940	11.8	< 58.3
	7	10	node Right	2394	32	0	7.2	-4.6	82.4	E(80)	62.0	3	29.0	1.000	0.940	11.8	< 58.3
	7	11	node Left	2388	32	0	9.2	-1.8	141.1	E(80)	62.0	3	29.0	1.000	0.940	11.0	< 58.3
	7	11	node Right	2388	32	0	9.2	-1.8	141.1	E(80)	62.0	3	29.0	1.000	0.940	11.0	< 58.3
	8	12	node Left	2382	32	0	6.6	-5.0	80.1	E(80)	62.0	3	29.0	1.000	0.940	11.7	< 58.3
	8	12	node Right	2382	32	0	6.6	-5.0	80.1	E(80)	62.0	3	29.0	1.000	0.940	11.7	< 58.3
	9	13	node Left	2375	16	0	8.3	-13.9	46.4	E(80)	62.0	3	29.0	1.000	1.000	22.2	< 62.0
	9	13	node Right	2375	16	0	7.4	-12.2	41.1	E(80)	62.0	3	29.0	1.000	1.000	19.7	< 62.0
	10	14	node Left	2368	12	0	7.0	-18.4	-18.6	E(80)	62.0	3	29.0	1.300	1.000	25.4	< 80.6
	10	14	node Right	2368	12	0	7.0	-18.4	-18.6	E(80)	62.0	3	29.0	1.300	1.000	25.4	< 80.6
	10	15	node Left	2360	12	0	5.9	-22.2	-65.5	E(80)	62.0	3	29.0	1.300	1.000	28.2	< 80.6
	10	15	node Right	2360	12	0	5.9	-22.2	-65.5	E(80)	62.0	3	29.0	1.300	1.000	28.2	< 80.6
	11	16	node Left	2353	13	0	4.2	-21.9	-83.1	E(80)	62.0	3	29.0	1.300	1.000	26.1	< 80.6
	11	16	node Right	2353	13	0	4.2	-21.8	-83.2	E(80)	62.0	3	29.0	1.300	1.000	26.1	< 80.6
	12	17	node Left	2346	13	0	3.3	-22.3	-90.4	E(80)	62.0	3	29.0	1.300	1.000	25.6	< 80.6
	12	17	node Right	2346	13	0	3.3	-22.3	-90.4	E(80)	62.0	3	29.0	1.300	1.000	25.6	< 80.6
	13	18	node Left	2338	13	0	4.4	-21.4	-81.2	E(80)	62.0	3	29.0	1.300	1.000	25.8	< 80.6
	13	18	node Right	2338	13	0	4.3	-21.5	-81.1	E(80)	62.0	3	29.0	1.300	1.000	25.8	< 80.6
	14	19	node Left	2334	12	0	6.0	-21.4	-62.2	E(80)	62.0	3	29.0	1.300	1.000	27.4	< 80.6
	14	19	node Right	2334	12	0	6.1	-21.4	-62.2	E(80)	62.0	3	29.0	1.300	1.000	27.5	< 80.6
	14	20	node Left	2334	12	0	7.0	-17.6	-16.3	E(80)	62.0	3	29.0	1.300	1.000	24.6	< 80.6
	14	20	node Right	2334	12	0	7.0	-17.6	-16.2	E(80)	62.0	3	29.0	1.300	1.000	24.6	< 80.6
	15	21	node Left	2334	17	0	6.6	-11.2	39.6	E(80)	62.0	3	29.0	1.000	1.000	17.8	< 62.0
	15	21	node Right	2334	17	0	7.4	-12.6	44.6	E(80)	62.0	3	29.0	1.000	1.000	20.1	< 62.0
	16	22	node Left	2334	34	0	5.8	-4.5	73.9	E(80)	62.0	3	29.0	1.000	0.926	10.3	< 57.4
	16	22	node Right	2334	34	0	5.8	-4.5	73.9	E(80)	62.0	3	29.0	1.000	0.926	10.3	< 57.4
	17	23	node Left	2334	36	0	8.6	-1.8	124.4	E(80)	62.0	3	29.0	1.000	0.913	10.3	< 56.6
	17	23	node Right	2334	36	0	8.5	-1.8	124.4	E(80)	62.0	3	29.0	1.000	0.913	10.3	< 56.6
	17	24	node Left	2334	36	0	6.3	-4.1	72.1	E(80)	62.0	3	29.0	1.000	0.913	10.4	< 56.6
	17	24	node Right	2334	36	0	6.4	-4.0	72.0	E(80)	62.0	3	29.0	1.000	0.913	10.4	< 56.6
	18	25	node Left	2334	20	0	8.2	-11.3	48.5	E(80)	62.0	3	29.0	1.000	1.000	19.4	< 62.0
	18	25	node Right	2334	20	0	7.3	-10.2	43.6	E(80)	62.0	3	29.0	1.000	1.000	17.4	< 62.0

19	26 node Left	2334	12	0	9.4	-19.8	-4.6	E(80)	62.0	3	29.0	1.183	1.000	29.3	< 73.3
19	26 node Right	2334	12	0	9.4	-19.8	-4.7	E(80)	62.0	3	29.0	1.185	1.000	29.2	< 73.4
19	27 node Left	2334	12	0	8.2	-23.5	-55.0	E(80)	62.0	3	29.0	1.300	1.000	31.7	< 80.6
19	27 node Right	2334	12	0	8.3	-24.1	-56.2	E(80)	62.0	3	29.0	1.300	1.000	32.4	< 80.6
20	28 node Left	2334	14	0	5.8	-22.6	-76.9	E(80)	62.0	3	29.0	1.300	1.000	28.4	< 80.6
20	28 node Right	2334	14	0	5.9	-22.5	-77.0	E(80)	62.0	3	29.0	1.300	1.000	28.4	< 80.6
21	29 node Left	2334	14	0	4.6	-23.0	-91.0	E(80)	62.0	3	29.0	1.300	1.000	27.7	< 80.6
21	29 node Right	2334	14	0	4.6	-23.0	-91.0	E(80)	62.0	3	29.0	1.300	1.000	27.7	< 80.6
21	30 node Left	2334	14	0	3.4	-21.7	-90.1	E(80)	62.0	3	29.0	1.300	1.000	25.1	< 80.6
21	30 node Right	2334	14	0	3.4	-21.7	-90.1	E(80)	62.0	3	29.0	1.300	1.000	25.1	< 80.6
22	31 node Left	2334	14	0	2.2	-18.7	-75.2	E(80)	62.0	3	29.0	1.300	1.000	21.0	< 80.6
22	31 node Right	2334	14	0	2.3	-18.7	-75.2	E(80)	62.0	3	29.0	1.300	1.000	21.0	< 80.6
23	32 node Left	2334	12	0	1.3	-15.2	-53.9	E(80)	62.0	3	29.0	1.300	1.000	16.5	< 80.6
23	32 node Right	2334	12	0	1.3	-15.2	-53.9	E(80)	62.0	3	29.0	1.300	1.000	16.5	< 80.6
23	33 node Left	2334	12	0	0.0	-0.1	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.1	< 80.6

STEEL-BOX G1

node WEB-L-1 (Web Lower edge) WEB - 1

Stress

range

node number	node number	Web	height (mm)	t	σ_{tmax} (N/mm ²)	σ_{tmin} (N/mm ²)	σ_d	$\Delta \sigma_f$ (E)	$\Delta \sigma_{ce}$ (m)	$\Delta \sigma_{ve}$ (CR)	Ct	$\Delta \sigma_{max}$ (N/mm ²)	Cycle	D	
1	1	node Right	2436	12	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.000	0.0	< 80.6	
1	2	node Left	2433	12	0	19.6	-1.8	74.0 E(80)	62.0	3	29.0	1.000	1.000	21.4	< 62.0
1	2	node Right	2433	12	0	19.6	-1.8	74.0 E(80)	62.0	3	29.0	1.000	1.000	21.4	< 62.0
2	3	node Left	2430	18	0	20.4	-2.6	85.4 E(80)	62.0	3	29.0	1.000	1.000	23.0	< 62.0
2	3	node Right	2430	18	0	20.4	-2.6	85.4 E(80)	62.0	3	29.0	1.000	1.000	23.0	< 62.0
3	4	node Left	2426	18	0	24.0	-3.8	102.9 E(80)	62.0	3	29.0	1.000	1.000	27.8	< 62.0
3	4	node Right	2426	18	0	24.0	-3.8	102.9 E(80)	62.0	3	29.0	1.000	1.000	27.8	< 62.0
3	5	node Left	2423	18	0	25.4	-5.1	103.9 E(80)	62.0	3	29.0	1.000	1.000	30.5	< 62.0
3	5	node Right	2423	18	0	25.4	-5.1	103.9 E(80)	62.0	3	29.0	1.000	1.000	30.5	< 62.0
4	6	node Left	2418	18	0	24.7	-6.3	88.0 E(80)	62.0	3	29.0	1.000	1.000	31.0	< 62.0
4	6	node Right	2418	18	0	24.7	-6.3	88.0 E(80)	62.0	3	29.0	1.000	1.000	31.0	< 62.0
5	7	node Left	2412	12	0	31.9	-10.9	79.8 E(80)	62.0	3	29.0	1.000	1.000	42.8	< 62.0
5	7	node Right	2412	12	0	26.7	-9.0	66.7 E(80)	62.0	3	29.0	1.000	1.000	35.8	< 62.0
5	8	node Left	2406	12	0	22.2	-10.4	8.6 E(80)	62.0	3	29.0	1.000	1.000	32.6	< 62.0
5	8	node Right	2406	12	0	22.2	-10.4	8.6 E(80)	62.0	3	29.0	1.000	1.000	32.6	< 62.0
6	9	node Left	2400	14	0	12.9	-9.2	-53.6 E(80)	62.0	3	29.0	1.300	1.000	22.1	< 80.6
6	9	node Right	2400	14	0	13.0	-9.3	-54.2 E(80)	62.0	3	29.0	1.300	1.000	22.2	< 80.6
7	10	node Left	2394	26	0	4.7	-7.3	-84.9 E(80)	62.0	3	29.0	1.300	0.990	12.0	< 79.8
7	10	node Right	2394	26	0	4.7	-7.3	-84.9 E(80)	62.0	3	29.0	1.300	0.990	12.0	< 79.8
7	11	node Left	2388	26	0	1.9	-9.4	-145.5 E(80)	62.0	3	29.0	1.300	0.990	11.4	< 79.8
7	11	node Right	2388	26	0	1.9	-9.4	-145.5 E(80)	62.0	3	29.0	1.300	0.990	11.4	< 79.8
8	12	node Left	2382	21	0	5.9	-7.9	-94.7 E(80)	62.0	3	29.0	1.300	1.000	13.8	< 80.6
8	12	node Right	2382	21	0	5.9	-7.9	-94.7 E(80)	62.0	3	29.0	1.300	1.000	13.8	< 80.6
9	13	node Left	2375	14	0	14.7	-8.9	-49.3 E(80)	62.0	3	29.0	1.300	1.000	23.6	< 80.6
9	13	node Right	2375	14	0	14.5	-8.8	-48.5 E(80)	62.0	3	29.0	1.300	1.000	23.3	< 80.6
10	14	node Left	2368	12	0	19.0	-7.1	19.1 E(80)	62.0	3	29.0	1.000	1.000	26.1	< 62.0
10	14	node Right	2368	12	0	18.9	-7.2	19.2 E(80)	62.0	3	29.0	1.000	1.000	26.1	< 62.0
10	15	node Left	2360	12	0	27.8	-7.4	82.1 E(80)	62.0	3	29.0	1.000	1.000	35.3	< 62.0
10	15	node Right	2360	12	0	27.8	-7.4	82.1 E(80)	62.0	3	29.0	1.000	1.000	35.3	< 62.0
11	16	node Left	2353	16	0	24.6	-4.8	93.7 E(80)	62.0	3	29.0	1.000	1.000	29.4	< 62.0
11	16	node Right	2353	16	0	24.6	-4.8	93.7 E(80)	62.0	3	29.0	1.000	1.000	29.4	< 62.0
12	17	node Left	2346	16	0	25.4	-3.8	102.5 E(80)	62.0	3	29.0	1.000	1.000	29.1	< 62.0
12	17	node Right	2346	16	0	25.4	-3.8	102.5 E(80)	62.0	3	29.0	1.000	1.000	29.1	< 62.0
13	18	node Left	2338	16	0	24.5	-5.0	92.7 E(80)	62.0	3	29.0	1.000	1.000	29.4	< 62.0
13	18	node Right	2338	16	0	24.5	-5.0	92.7 E(80)	62.0	3	29.0	1.000	1.000	29.4	< 62.0
14	19	node Left	2334	12	0	27.6	-7.8	80.0 E(80)	62.0	3	29.0	1.000	1.000	35.4	< 62.0
14	19	node Right	2334	12	0	27.6	-7.7	79.9 E(80)	62.0	3	29.0	1.000	1.000	35.3	< 62.0
14	20	node Left	2334	12	0	18.6	-7.4	17.2 E(80)	62.0	3	29.0	1.000	1.000	26.0	< 62.0
14	20	node Right	2334	12	0	18.6	-7.4	17.2 E(80)	62.0	3	29.0	1.000	1.000	26.0	< 62.0
15	21	node Left	2334	14	0	14.2	-8.3	-50.0 E(80)	62.0	3	29.0	1.300	1.000	22.5	< 80.6
15	21	node Right	2334	14	0	14.3	-8.5	-50.7 E(80)	62.0	3	29.0	1.300	1.000	22.8	< 80.6
16	22	node Left	2334	21	0	5.8	-7.5	-95.3 E(80)	62.0	3	29.0	1.300	1.000	13.3	< 80.6
16	22	node Right	2334	21	0	5.8	-7.5	-95.3 E(80)	62.0	3	29.0	1.300	1.000	13.3	< 80.6
17	23	node Left	2334	27	0	2.2	-9.7	-142.5 E(80)	62.0	3	29.0	1.300	0.981	11.8	< 79.1
17	23	node Right	2334	27	0	2.1	-9.8	-142.4 E(80)	62.0	3	29.0	1.300	0.981	11.8	< 79.1
17	24	node Left	2334	27	0	4.6	-7.3	-82.9 E(80)	62.0	3	29.0	1.300	0.981	11.9	< 79.1
17	24	node Right	2334	27	0	4.6	-7.3	-82.8 E(80)	62.0	3	29.0	1.300	0.981	11.9	< 79.1
18	25	node Left	2334	14	0	12.9	-9.2	-55.0 E(80)	62.0	3	29.0	1.300	1.000	22.1	< 80.6
18	25	node Right	2334	14	0	12.7	-9.0	-54.4 E(80)	62.0	3	29.0	1.300	1.000	21.8	< 80.6
19	26	node Left	2334	12	0	21.8	-10.3	5.0 E(80)	62.0	3	29.0	1.000	1.000	32.2	< 62.0

19	26 node Right	2334 12	0	21.8	-10.3	5.1	E(80)	62.0 3	29.0	1.000	1.000	32.1 < 62.0
19	27 node Left	2334 12	0	25.9	-9.0	60.3	E(80)	62.0 3	29.0	1.000	1.000	34.9 < 62.0
19	27 node Right	2334 12	0	31.0	-10.7	72.2	E(80)	62.0 3	29.0	1.000	1.000	41.7 < 62.0
20	28 node Left	2334 16	0	25.5	-6.6	87.1	E(80)	62.0 3	29.0	1.000	1.000	32.2 < 62.0
20	28 node Right	2334 16	0	25.5	-6.7	87.2	E(80)	62.0 3	29.0	1.000	1.000	32.2 < 62.0
21	29 node Left	2334 16	0	26.0	-5.3	103.1	E(80)	62.0 3	29.0	1.000	1.000	31.3 < 62.0
21	29 node Right	2334 16	0	26.0	-5.3	103.1	E(80)	62.0 3	29.0	1.000	1.000	31.3 < 62.0
21	30 node Left	2334 16	0	24.6	-3.9	102.0	E(80)	62.0 3	29.0	1.000	1.000	28.5 < 62.0
21	30 node Right	2334 16	0	24.6	-3.9	102.0	E(80)	62.0 3	29.0	1.000	1.000	28.5 < 62.0
22	31 node Left	2334 14	0	22.8	-2.7	91.3	E(80)	62.0 3	29.0	1.000	1.000	25.5 < 62.0
22	31 node Right	2334 14	0	22.8	-2.7	91.3	E(80)	62.0 3	29.0	1.000	1.000	25.5 < 62.0
23	32 node Left	2334 12	0	18.9	-1.6	66.8	E(80)	62.0 3	29.0	1.000	1.000	20.5 < 62.0
23	32 node Right	2334 12	0	18.8	-1.6	66.8	E(80)	62.0 3	29.0	1.000	1.000	20.4 < 62.0
23	33 node Left	2334 12	0	0.1	0.0	0.0	E(80)	62.0 3	29.0	1.000	1.000	0.1 < 62.0

STEEL-BOX G1

node HSTIFF-1 (Web H-stiff) WEB - 1

Stress

range

node number	node number	Web	height (mm)	t	σ_{max} (N/mm ²)	σ_{min} (N/mm ²)	σ_d	$\Delta \sigma_f$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$ (N/mm ²)	Cycle	D
1	1	node Right	2436	12	487	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
1	2	node Left	2433	12	487	0.9	-9.9	-37.6	G(50)	32.0	3	15.0	1.300	1.000	10.8	< 41.6
1	2	node Right	2433	12	487	0.9	-9.9	-37.6	G(50)	32.0	3	15.0	1.300	1.000	10.8	< 41.6
2	3	node Left	2430	12	486	1.5	-12.7	-52.8	G(50)	32.0	3	15.0	1.300	1.000	14.2	< 41.6
2	3	node Right	2430	12	486	1.5	-12.7	-52.8	G(50)	32.0	3	15.0	1.300	1.000	14.2	< 41.6
3	4	node Left	2426	12	485	2.3	-14.8	-63.5	G(50)	32.0	3	15.0	1.300	1.000	17.2	< 41.6
3	4	node Right	2426	12	485	2.3	-14.8	-63.5	G(50)	32.0	3	15.0	1.300	1.000	17.2	< 41.6
3	5	node Left	2423	12	485	3.1	-15.6	-63.9	G(50)	32.0	3	15.0	1.300	1.000	18.7	< 41.6
3	5	node Right	2423	12	485	3.1	-15.6	-63.9	G(50)	32.0	3	15.0	1.300	1.000	18.7	< 41.6
4	6	node Left	2418	12	484	3.9	-15.1	-53.8	G(50)	32.0	3	15.0	1.300	1.000	19.0	< 41.6
4	6	node Right	2418	12	484	3.9	-15.1	-53.8	G(50)	32.0	3	15.0	1.300	1.000	19.0	< 41.6
5	7	node Left	2412	12	482	5.1	-15.1	-37.6	G(50)	32.0	3	15.0	1.300	1.000	20.2	< 41.6
5	7	node Right	2412	12	482	5.3	-15.5	-38.7	G(50)	32.0	3	15.0	1.300	1.000	20.8	< 41.6
5	8	node Left	2406	12	481	6.0	-12.7	-5.0	G(50)	32.0	3	15.0	1.260	1.000	18.7	< 40.3
5	8	node Right	2406	12	481	6.0	-12.7	-5.0	G(50)	32.0	3	15.0	1.260	1.000	18.7	< 40.3
6	9	node Left	2400	14	480	8.0	-5.7	-33.3	G(50)	32.0	3	15.0	1.300	1.000	13.7	< 41.6
6	9	node Right	2400	14	480	7.8	-5.6	-32.6	G(50)	32.0	3	15.0	1.300	1.000	13.4	< 41.6
7	10	node Left	2394	16	479	2.9	-4.4	-51.4	G(50)	32.0	3	15.0	1.300	1.000	7.2	< 41.6
7	10	node Right	2394	16	479	2.9	-4.4	-51.4	G(50)	32.0	3	15.0	1.300	1.000	7.2	< 41.6
7	11	node Left	2388	16	478	1.2	-5.7	-88.2	G(50)	32.0	3	15.0	1.300	1.000	6.9	< 41.6
7	11	node Right	2388	16	478	1.2	-5.7	-88.2	G(50)	32.0	3	15.0	1.300	1.000	6.9	< 41.6
8	12	node Left	2382	16	476	3.7	-5.0	-59.7	G(50)	32.0	3	15.0	1.300	1.000	8.7	< 41.6
8	12	node Right	2382	16	476	3.7	-5.0	-59.7	G(50)	32.0	3	15.0	1.300	1.000	8.7	< 41.6
9	13	node Left	2375	14	475	9.0	-5.4	-30.2	G(50)	32.0	3	15.0	1.300	1.000	14.4	< 41.6
9	13	node Right	2375	14	475	9.1	-5.6	-30.6	G(50)	32.0	3	15.0	1.300	1.000	14.7	< 41.6
10	14	node Left	2368	12	474	4.1	-10.9	-11.1	G(50)	32.0	3	15.0	1.300	1.000	15.1	< 41.6
10	14	node Right	2368	12	474	4.1	-10.9	-11.0	G(50)	32.0	3	15.0	1.300	1.000	15.1	< 41.6
10	15	node Left	2360	12	472	3.2	-12.2	-36.0	G(50)	32.0	3	15.0	1.300	1.000	15.5	< 41.6
10	15	node Right	2360	12	472	3.2	-12.2	-36.0	G(50)	32.0	3	15.0	1.300	1.000	15.5	< 41.6
11	16	node Left	2353	12	471	2.4	-12.6	-47.7	G(50)	32.0	3	15.0	1.300	1.000	15.0	< 41.6
11	16	node Right	2353	12	471	2.4	-12.5	-47.8	G(50)	32.0	3	15.0	1.300	1.000	15.0	< 41.6
12	17	node Left	2346	12	469	1.9	-12.8	-51.8	G(50)	32.0	3	15.0	1.300	1.000	14.7	< 41.6
12	17	node Right	2346	12	469	1.9	-12.8	-51.8	G(50)	32.0	3	15.0	1.300	1.000	14.7	< 41.6
13	18	node Left	2338	12	468	2.5	-12.3	-46.4	G(50)	32.0	3	15.0	1.300	1.000	14.8	< 41.6
13	18	node Right	2338	12	468	2.5	-12.3	-46.3	G(50)	32.0	3	15.0	1.300	1.000	14.8	< 41.6
14	19	node Left	2334	12	467	3.2	-11.6	-33.8	G(50)	32.0	3	15.0	1.300	1.000	14.9	< 41.6
14	19	node Right	2334	12	467	3.3	-11.6	-33.8	G(50)	32.0	3	15.0	1.300	1.000	15.0	< 41.6
14	20	node Left	2334	12	467	4.1	-10.4	-9.6	G(50)	32.0	3	15.0	1.300	1.000	14.4	< 41.6
14	20	node Right	2334	12	467	4.1	-10.4	-9.5	G(50)	32.0	3	15.0	1.300	1.000	14.4	< 41.6
15	21	node Left	2334	14	467	9.1	-5.3	-32.1	G(50)	32.0	3	15.0	1.300	1.000	14.4	< 41.6
15	21	node Right	2334	14	467	8.9	-5.3	-31.6	G(50)	32.0	3	15.0	1.300	1.000	14.2	< 41.6
16	22	node Left	2334	16	467	3.7	-4.8	-61.5	G(50)	32.0	3	15.0	1.300	1.000	8.6	< 41.6
16	22	node Right	2334	16	467	3.7	-4.8	-61.5	G(50)	32.0	3	15.0	1.300	1.000	8.6	< 41.6
17	23	node Left	2334	16	467	1.4	-6.0	-89.1	G(50)	32.0	3	15.0	1.300	1.000	7.4	< 41.6
17	23	node Right	2334	16	467	1.3	-6.1	-89.0	G(50)	32.0	3	15.0	1.300	1.000	7.4	< 41.6
17	24	node Left	2334	16	467	2.9	-4.6	-51.9	G(50)	32.0	3	15.0	1.300	1.000	7.5	< 41.6
17	24	node Right	2334	16	467	2.9	-4.5	-51.8	G(50)	32.0	3	15.0	1.300	1.000	7.5	< 41.6
18	25	node Left	2334	14	467	8.0	-5.7	-34.3	G(50)	32.0	3	15.0	1.300	1.000	13.8	< 41.6
18	25	node Right	2334	14	467	8.1	-5.8	-34.8	G(50)	32.0	3	15.0	1.300	1.000	13.9	< 41.6
19	26	node Left	2334	12	467	5.5	-11.5	-2.7	G(50)	32.0	3	15.0	1.183	1.000	17.0	< 37.8

19	26 node Right	2334 12 467	5.5	-11.5	-2.7	G(50)	32.0	3	15.0	1.185	1.000	16.9	<	37.9
19	27 node Left	2334 12 467	4.7	-13.6	-31.9	G(50)	32.0	3	15.0	1.300	1.000	18.4	<	41.6
19	27 node Right	2334 12 467	4.5	-13.1	-30.5	G(50)	32.0	3	15.0	1.300	1.000	17.6	<	41.6
20	28 node Left	2334 12 467	3.3	-12.9	-44.1	G(50)	32.0	3	15.0	1.300	1.000	16.3	<	41.6
20	28 node Right	2334 12 467	3.4	-12.9	-44.2	G(50)	32.0	3	15.0	1.300	1.000	16.3	<	41.6
21	29 node Left	2334 12 467	2.7	-13.2	-52.2	G(50)	32.0	3	15.0	1.300	1.000	15.9	<	41.6
21	29 node Right	2334 12 467	2.7	-13.2	-52.2	G(50)	32.0	3	15.0	1.300	1.000	15.9	<	41.6
21	30 node Left	2334 12 467	2.0	-12.4	-51.7	G(50)	32.0	3	15.0	1.300	1.000	14.4	<	41.6
21	30 node Right	2334 12 467	2.0	-12.4	-51.7	G(50)	32.0	3	15.0	1.300	1.000	14.4	<	41.6
22	31 node Left	2334 12 467	1.2	-10.4	-41.9	G(50)	32.0	3	15.0	1.300	1.000	11.7	<	41.6
22	31 node Right	2334 12 467	1.3	-10.4	-41.9	G(50)	32.0	3	15.0	1.300	1.000	11.7	<	41.6
23	32 node Left	2334 12 467	0.7	-8.4	-29.8	G(50)	32.0	3	15.0	1.300	1.000	9.1	<	41.6
23	32 node Right	2334 12 467	0.7	-8.4	-29.8	G(50)	32.0	3	15.0	1.300	1.000	9.1	<	41.6
23	33 node Left	2334 12 467	0.0	-0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6

STEEL-BOX G1

node POINT-U-1 (Web Upper) WEB - 1

Stress

range	node	node	Web	Grade	$\Delta \sigma_{ce} \cdot \text{Cycle}$	$\Delta \sigma_{max} \cdot \text{CR} \cdot \text{Ct}$	$\Delta \sigma_{ve} \cdot \text{CR}$	$\Delta \sigma_{min}$	$\Delta \sigma_{max}$	$\Delta \sigma_{f}$	$\Delta \sigma_{ce}$	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	$\Delta \sigma_{min}$	D
number	number	number	height (mm)	$t \sigma_{tmax}$ (N/mm ²)	σ_{min}	σ_{d}	$(\Delta \sigma_{f})$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	$\Delta \sigma_{min}$	$\Delta \sigma_{max}$	$\Delta \sigma_{min}$	D
1	1	node Right	2436	12 900	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6		
1	2	node Left	2433	12 900	0.4	-3.6	-13.9	G(50)	32.0	3	15.0	1.300	1.000	4.0	< 41.6		
1	2	node Right	2433	12 900	0.4	-3.6	-13.9	G(50)	32.0	3	15.0	1.300	1.000	4.0	< 41.6		
2	3	node Left	2430	12 900	0.7	-5.6	-23.4	G(50)	32.0	3	15.0	1.300	1.000	6.3	< 41.6		
2	3	node Right	2430	12 900	0.7	-5.6	-23.4	G(50)	32.0	3	15.0	1.300	1.000	6.3	< 41.6		
3	4	node Left	2426	12 900	1.0	-6.5	-27.9	G(50)	32.0	3	15.0	1.300	1.000	7.6	< 41.6		
3	4	node Right	2426	12 900	1.0	-6.5	-27.9	G(50)	32.0	3	15.0	1.300	1.000	7.6	< 41.6		
3	5	node Left	2423	12 900	1.4	-6.8	-27.9	G(50)	32.0	3	15.0	1.300	1.000	8.2	< 41.6		
3	5	node Right	2423	12 900	1.4	-6.8	-27.9	G(50)	32.0	3	15.0	1.300	1.000	8.2	< 41.6		
4	6	node Left	2418	12 900	1.7	-6.5	-23.3	G(50)	32.0	3	15.0	1.300	1.000	8.2	< 41.6		
4	6	node Right	2418	12 900	1.7	-6.5	-23.3	G(50)	32.0	3	15.0	1.300	1.000	8.2	< 41.6		
5	7	node Left	2412	12 900	1.7	-4.9	-12.2	G(50)	32.0	3	15.0	1.300	1.000	6.5	< 41.6		
5	7	node Right	2412	12 900	2.2	-6.4	-15.9	G(50)	32.0	3	15.0	1.300	1.000	8.6	< 41.6		
5	8	node Left	2406	12 900	2.4	-5.1	-2.0	G(50)	32.0	3	15.0	1.262	1.000	7.5	< 40.4		
5	8	node Right	2406	12 900	2.4	-5.1	-2.0	G(50)	32.0	3	15.0	1.262	1.000	7.5	< 40.4		
6	9	node Left	2400	14 900	1.7	-2.4	10.0	G(50)	32.0	3	15.0	1.000	1.000	4.1	< 32.0		
6	9	node Right	2400	14 900	2.3	-3.2	13.2	G(50)	32.0	3	15.0	1.000	1.000	5.5	< 32.0		
7	10	node Left	2394	16 900	1.8	-1.1	19.5	G(50)	32.0	3	15.0	1.000	1.000	2.8	< 32.0		
7	10	node Right	2394	16 900	1.8	-1.1	19.5	G(50)	32.0	3	15.0	1.000	1.000	2.8	< 32.0		
7	11	node Left	2388	16 900	2.2	-0.4	33.1	G(50)	32.0	3	15.0	1.000	1.000	2.6	< 32.0		
7	11	node Right	2388	16 900	2.2	-0.4	33.1	G(50)	32.0	3	15.0	1.000	1.000	2.6	< 32.0		
8	12	node Left	2382	16 900	1.1	-0.9	14.0	G(50)	32.0	3	15.0	1.000	1.000	2.0	< 32.0		
8	12	node Right	2382	16 900	1.1	-0.9	14.0	G(50)	32.0	3	15.0	1.000	1.000	2.0	< 32.0		
9	13	node Left	2375	14 900	1.8	-3.1	10.1	G(50)	32.0	3	15.0	1.000	1.000	4.9	< 32.0		
9	13	node Right	2375	14 900	1.3	-2.1	7.1	G(50)	32.0	3	15.0	1.000	1.000	3.4	< 32.0		
10	14	node Left	2368	12 900	1.6	-4.2	-4.3	G(50)	32.0	3	15.0	1.300	1.000	5.8	< 41.6		
10	14	node Right	2368	12 900	1.6	-4.2	-4.2	G(50)	32.0	3	15.0	1.300	1.000	5.8	< 41.6		
10	15	node Left	2360	12 900	0.8	-3.1	-9.2	G(50)	32.0	3	15.0	1.300	1.000	4.0	< 41.6		
10	15	node Right	2360	12 900	0.8	-3.1	-9.2	G(50)	32.0	3	15.0	1.300	1.000	4.0	< 41.6		
11	16	node Left	2353	12 900	0.7	-4.1	-15.5	G(50)	32.0	3	15.0	1.300	1.000	4.9	< 41.6		
11	16	node Right	2353	12 900	0.8	-4.1	-15.5	G(50)	32.0	3	15.0	1.300	1.000	4.8	< 41.6		
12	17	node Left	2346	12 900	0.6	-4.0	-16.4	G(50)	32.0	3	15.0	1.300	1.000	4.6	< 41.6		
12	17	node Right	2346	12 900	0.6	-4.0	-16.4	G(50)	32.0	3	15.0	1.300	1.000	4.6	< 41.6		
13	18	node Left	2338	12 900	0.8	-3.8	-14.3	G(50)	32.0	3	15.0	1.300	1.000	4.6	< 41.6		
13	18	node Right	2338	12 900	0.7	-3.8	-14.2	G(50)	32.0	3	15.0	1.300	1.000	4.6	< 41.6		
14	19	node Left	2334	12 900	0.7	-2.5	-7.4	G(50)	32.0	3	15.0	1.300	1.000	3.2	< 41.6		
14	19	node Right	2334	12 900	0.8	-2.5	-7.4	G(50)	32.0	3	15.0	1.300	1.000	3.3	< 41.6		
14	20	node Left	2334	12 900	1.4	-3.6	-3.4	G(50)	32.0	3	15.0	1.300	1.000	5.1	< 41.6		
14	20	node Right	2334	12 900	1.4	-3.6	-3.3	G(50)	32.0	3	15.0	1.300	1.000	5.1	< 41.6		
15	21	node Left	2334	14 900	0.9	-1.4	5.0	G(50)	32.0	3	15.0	1.000	1.000	2.3	< 32.0		
15	21	node Right	2334	14 900	1.3	-2.2	7.9	G(50)	32.0	3	15.0	1.000	1.000	3.5	< 32.0		
16	22	node Left	2334	16 900	0.7	-0.5	8.7	G(50)	32.0	3	15.0	1.000	1.000	1.2	< 32.0		
16	22	node Right	2334	16 900	0.7	-0.5	8.7	G(50)	32.0	3	15.0	1.000	1.000	1.2	< 32.0		
17	23	node Left	2334	16 900	1.5	-0.2	21.5	G(50)	32.0	3	15.0	1.000	1.000	1.8	< 32.0		
17	23	node Right	2334	16 900	1.4	-0.3	21.5	G(50)	32.0	3	15.0	1.000	1.000	1.8	< 32.0		
17	24	node Left	2334	16 900	1.1	-0.7	12.3	G(50)	32.0	3	15.0	1.000	1.000	1.8	< 32.0		
17	24	node Right	2334	16 900	1.1	-0.7	12.3	G(50)	32.0	3	15.0	1.000	1.000	1.8	< 32.0		
18	25	node Left	2334	14 900	1.5	-2.0	8.6	G(50)	32.0	3	15.0	1.000	1.000	3.4	< 32.0		
18	25	node Right	2334	14 900	1.0	-1.3	5.8	G(50)	32.0	3	15.0	1.000	1.000	2.3	< 32.0		
19	26	node Left	2334	12 900	1.8	-3.8	-0.9	G(50)	32.0	3	15.0	1.183	1.000	5.6	< 37.9		

19	26 node Right	2334 12 900	1.8	-3.7	-0.9	G(50)	32.0 3	15.0	1.185	1.000	5.6<	37.9
19	27 node Left	2334 12 900	1.6	-4.5	-10.5	G(50)	32.0 3	15.0	1.300	1.000	6.0<	41.6
19	27 node Right	2334 12 900	1.0	-2.9	-6.7	G(50)	32.0 3	15.0	1.300	1.000	3.8<	41.6
20	28 node Left	2334 12 900	1.0	-4.0	-13.7	G(50)	32.0 3	15.0	1.300	1.000	5.0<	41.6
20	28 node Right	2334 12 900	1.0	-4.0	-13.7	G(50)	32.0 3	15.0	1.300	1.000	5.0<	41.6
21	29 node Left	2334 12 900	0.8	-4.1	-16.2	G(50)	32.0 3	15.0	1.300	1.000	4.9<	41.6
21	29 node Right	2334 12 900	0.8	-4.1	-16.2	G(50)	32.0 3	15.0	1.300	1.000	4.9<	41.6
21	30 node Left	2334 12 900	0.6	-3.8	-16.0	G(50)	32.0 3	15.0	1.300	1.000	4.5<	41.6
21	30 node Right	2334 12 900	0.6	-3.8	-16.0	G(50)	32.0 3	15.0	1.300	1.000	4.5<	41.6
22	31 node Left	2334 12 900	0.3	-2.7	-11.0	G(50)	32.0 3	15.0	1.300	1.000	3.0<	41.6
22	31 node Right	2334 12 900	0.4	-2.7	-11.0	G(50)	32.0 3	15.0	1.300	1.000	3.1<	41.6
23	32 node Left	2334 12 900	0.2	-2.1	-7.4	G(50)	32.0 3	15.0	1.300	1.000	2.2<	41.6
23	32 node Right	2334 12 900	0.2	-2.1	-7.4	G(50)	32.0 3	15.0	1.300	1.000	2.3<	41.6
23	33 node Left	2334 12 900	0.0	-0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0<	41.6

STEEL-BOX G1

node POINT-L-1 (Web) WEB - 1

Stress

range															
node number	node number	Web	Grade				$\Delta \sigma_{ce} \cdot \text{Cycle}$								
		height (mm)	t	σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR · Ct	D
		(N/mm ²)				(N/mm ²)									
1	1 node Right	2436	12	500	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
1	2 node Left	2433	12	500	12.0	-1.1	45.3	G(50)	32.0	3	15.0	1.000	1.000	13.1	< 32.0
1	2 node Right	2433	12	500	12.0	-1.1	45.3	G(50)	32.0	3	15.0	1.000	1.000	13.1	< 32.0
2	3 node Left	2430	12	500	11.9	-1.5	49.8	G(50)	32.0	3	15.0	1.000	1.000	13.4	< 32.0
2	3 node Right	2430	12	500	11.9	-1.5	49.8	G(50)	32.0	3	15.0	1.000	1.000	13.4	< 32.0
3	4 node Left	2426	12	500	14.0	-2.2	60.0	G(50)	32.0	3	15.0	1.000	1.000	16.2	< 32.0
3	4 node Right	2426	12	500	14.0	-2.2	60.0	G(50)	32.0	3	15.0	1.000	1.000	16.2	< 32.0
3	5 node Left	2423	12	500	14.8	-3.0	60.6	G(50)	32.0	3	15.0	1.000	1.000	17.8	< 32.0
3	5 node Right	2423	12	500	14.8	-3.0	60.6	G(50)	32.0	3	15.0	1.000	1.000	17.8	< 32.0
4	6 node Left	2418	12	500	14.4	-3.7	51.3	G(50)	32.0	3	15.0	1.000	1.000	18.1	< 32.0
4	6 node Right	2418	12	500	14.4	-3.7	51.3	G(50)	32.0	3	15.0	1.000	1.000	18.1	< 32.0
5	7 node Left	2412	12	500	19.7	-6.7	49.4	G(50)	32.0	3	15.0	1.000	1.000	26.5	< 32.0
5	7 node Right	2412	12	500	15.8	-5.3	39.4	G(50)	32.0	3	15.0	1.000	1.000	21.1	< 32.0
5	8 node Left	2406	12	500	13.1	-6.1	5.1	G(50)	32.0	3	15.0	1.000	1.000	19.2	< 32.0
5	8 node Right	2406	12	500	13.1	-6.1	5.1	G(50)	32.0	3	15.0	1.000	1.000	19.2	< 32.0
6	9 node Left	2400	14	500	7.8	-5.6	-32.4	G(50)	32.0	3	15.0	1.300	1.000	13.4	< 41.6
6	9 node Right	2400	14	500	7.6	-5.4	-31.7	G(50)	32.0	3	15.0	1.300	1.000	13.0	< 41.6
7	10 node Left	2394	16	500	2.8	-4.3	-50.0	G(50)	32.0	3	15.0	1.300	1.000	7.0	< 41.6
7	10 node Right	2394	16	500	2.8	-4.3	-50.0	G(50)	32.0	3	15.0	1.300	1.000	7.0	< 41.6
7	11 node Left	2388	16	500	1.1	-5.5	-85.5	G(50)	32.0	3	15.0	1.300	1.000	6.7	< 41.6
7	11 node Right	2388	16	500	1.1	-5.5	-85.5	G(50)	32.0	3	15.0	1.300	1.000	6.7	< 41.6
8	12 node Left	2382	16	500	3.6	-4.9	-58.0	G(50)	32.0	3	15.0	1.300	1.000	8.5	< 41.6
8	12 node Right	2382	16	500	3.6	-4.9	-58.0	G(50)	32.0	3	15.0	1.300	1.000	8.5	< 41.6
9	13 node Left	2375	14	500	8.7	-5.3	-29.2	G(50)	32.0	3	15.0	1.300	1.000	13.9	< 41.6
9	13 node Right	2375	14	500	8.9	-5.4	-29.6	G(50)	32.0	3	15.0	1.300	1.000	14.2	< 41.6
10	14 node Left	2368	12	500	11.1	-4.1	11.1	G(50)	32.0	3	15.0	1.000	1.000	15.2	< 32.0
10	14 node Right	2368	12	500	11.0	-4.2	11.2	G(50)	32.0	3	15.0	1.000	1.000	15.2	< 32.0
10	15 node Left	2360	12	500	17.2	-4.6	50.8	G(50)	32.0	3	15.0	1.000	1.000	21.8	< 32.0
10	15 node Right	2360	12	500	17.2	-4.6	50.8	G(50)	32.0	3	15.0	1.000	1.000	21.8	< 32.0
11	16 node Left	2353	12	500	14.7	-2.9	56.1	G(50)	32.0	3	15.0	1.000	1.000	17.6	< 32.0
11	16 node Right	2353	12	500	14.8	-2.9	56.1	G(50)	32.0	3	15.0	1.000	1.000	17.6	< 32.0
12	17 node Left	2346	12	500	15.2	-2.3	61.4	G(50)	32.0	3	15.0	1.000	1.000	17.5	< 32.0
12	17 node Right	2346	12	500	15.2	-2.3	61.4	G(50)	32.0	3	15.0	1.000	1.000	17.5	< 32.0
13	18 node Left	2338	12	500	14.7	-3.0	55.5	G(50)	32.0	3	15.0	1.000	1.000	17.6	< 32.0
13	18 node Right	2338	12	500	14.6	-3.0	55.5	G(50)	32.0	3	15.0	1.000	1.000	17.6	< 32.0
14	19 node Left	2334	12	500	17.1	-4.8	49.5	G(50)	32.0	3	15.0	1.000	1.000	21.9	< 32.0
14	19 node Right	2334	12	500	17.1	-4.7	49.5	G(50)	32.0	3	15.0	1.000	1.000	21.8	< 32.0
14	20 node Left	2334	12	500	10.9	-4.3	10.0	G(50)	32.0	3	15.0	1.000	1.000	15.2	< 32.0
14	20 node Right	2334	12	500	10.9	-4.3	10.0	G(50)	32.0	3	15.0	1.000	1.000	15.2	< 32.0
15	21 node Left	2334	14	500	8.7	-5.1	-30.8	G(50)	32.0	3	15.0	1.300	1.000	13.8	< 41.6
15	21 node Right	2334	14	500	8.5	-5.1	-30.3	G(50)	32.0	3	15.0	1.300	1.000	13.6	< 41.6
16	22 node Left	2334	16	500	3.6	-4.7	-59.1	G(50)	32.0	3	15.0	1.300	1.000	8.2	< 41.6
16	22 node Right	2334	16	500	3.6	-4.7	-59.1	G(50)	32.0	3	15.0	1.300	1.000	8.2	< 41.6
17	23 node Left	2334	16	500	1.3	-5.8	-85.3	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
17	23 node Right	2334	16	500	1.2	-5.9	-85.2	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
17	24 node Left	2334	16	500	2.8	-4.4	-49.7	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
17	24 node Right	2334	16	500	2.8	-4.3	-49.6	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
18	25 node Left	2334	14	500	7.7	-5.5	-32.8	G(50)	32.0	3	15.0	1.300	1.000	13.2	< 41.6
18	25 node Right	2334	14	500	7.8	-5.5	-33.4	G(50)	32.0	3	15.0	1.300	1.000	13.4	< 41.6
19	26 node Left	2334	12	500	12.9	-6.1	2.9	G(50)	32.0	3	15.0	1.000	1.000	19.0	< 32.0

19	26 node Right	2334	12	500	12.9	-6.1	3.0	G(50)	32.0	3	15.0	1.000	1.000	19.0	<	32.0
19	27 node Left	2334	12	500	15.3	-5.3	35.6	G(50)	32.0	3	15.0	1.000	1.000	20.6	<	32.0
19	27 node Right	2334	12	500	19.2	-6.6	44.7	G(50)	32.0	3	15.0	1.000	1.000	25.8	<	32.0
20	28 node Left	2334	12	500	15.2	-4.0	52.0	G(50)	32.0	3	15.0	1.000	1.000	19.2	<	32.0
20	28 node Right	2334	12	500	15.2	-4.0	52.0	G(50)	32.0	3	15.0	1.000	1.000	19.2	<	32.0
21	29 node Left	2334	12	500	15.5	-3.2	61.5	G(50)	32.0	3	15.0	1.000	1.000	18.6	<	32.0
21	29 node Right	2334	12	500	15.5	-3.2	61.5	G(50)	32.0	3	15.0	1.000	1.000	18.6	<	32.0
21	30 node Left	2334	12	500	14.7	-2.3	60.8	G(50)	32.0	3	15.0	1.000	1.000	17.0	<	32.0
21	30 node Right	2334	12	500	14.7	-2.3	60.8	G(50)	32.0	3	15.0	1.000	1.000	17.0	<	32.0
22	31 node Left	2334	12	500	13.9	-1.7	55.6	G(50)	32.0	3	15.0	1.000	1.000	15.6	<	32.0
22	31 node Right	2334	12	500	13.9	-1.6	55.6	G(50)	32.0	3	15.0	1.000	1.000	15.5	<	32.0
23	32 node Left	2334	12	500	11.6	-1.0	40.9	G(50)	32.0	3	15.0	1.000	1.000	12.6	<	32.0
23	32 node Right	2334	12	500	11.5	-1.0	40.9	G(50)	32.0	3	15.0	1.000	1.000	12.5	<	32.0
23	33 node Left	2334	12	500	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.000	1.000	0.0	<	32.0

STEEL-BOX G1

node WEB-U-2 (Web Upper Edge) WEB - 2

Stress

range

node number	node number	Web	height (mm)	t	σ_{max} (N/mm ²)	σ_{min} (N/mm ²)	σ_d	$\Delta \sigma_f$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$ (N/mm ²)	Cycle	D
1	1	node Right	2364	12	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
1	2	node Left	2367	12	0	1.5	-16.3	-61.9	E(80)	62.0	3	29.0	1.300	1.000	17.8	< 80.6
1	2	node Right	2367	12	0	1.5	-16.4	-61.9	E(80)	62.0	3	29.0	1.300	1.000	17.9	< 80.6
2	3	node Left	2370	14	0	2.5	-20.0	-83.4	E(80)	62.0	3	29.0	1.300	1.000	22.5	< 80.6
2	3	node Right	2370	14	0	2.4	-20.0	-83.4	E(80)	62.0	3	29.0	1.300	1.000	22.4	< 80.6
3	4	node Left	2374	14	0	3.7	-23.5	-100.8	E(80)	62.0	3	29.0	1.300	1.000	27.2	< 80.6
3	4	node Right	2374	14	0	3.7	-23.5	-100.8	E(80)	62.0	3	29.0	1.300	1.000	27.2	< 80.6
3	5	node Left	2377	14	0	5.0	-24.9	-102.0	E(80)	62.0	3	29.0	1.300	1.000	29.9	< 80.6
3	5	node Right	2377	14	0	5.0	-24.9	-102.0	E(80)	62.0	3	29.0	1.300	1.000	29.9	< 80.6
4	6	node Left	2382	14	0	6.2	-24.4	-86.8	E(80)	62.0	3	29.0	1.300	1.000	30.6	< 80.6
4	6	node Right	2382	14	0	6.2	-24.4	-86.8	E(80)	62.0	3	29.0	1.300	1.000	30.6	< 80.6
5	7	node Left	2388	12	0	8.9	-26.3	-65.5	E(80)	62.0	3	29.0	1.300	1.000	35.2	< 80.6
5	7	node Right	2388	12	0	8.7	-25.5	-63.9	E(80)	62.0	3	29.0	1.300	1.000	34.2	< 80.6
5	8	node Left	2394	12	0	10.0	-21.3	-8.3	E(80)	62.0	3	29.0	1.259	1.000	31.3	< 78.1
5	8	node Right	2394	12	0	10.0	-21.3	-8.3	E(80)	62.0	3	29.0	1.259	1.000	31.3	< 78.1
6	9	node Left	2400	18	0	8.2	-11.6	48.2	E(80)	62.0	3	29.0	1.000	1.000	19.8	< 62.0
6	9	node Right	2400	18	0	9.2	-12.9	53.8	E(80)	62.0	3	29.0	1.000	1.000	22.1	< 62.0
7	10	node Left	2406	32	0	7.2	-4.6	83.3	E(80)	62.0	3	29.0	1.000	0.940	11.8	< 58.3
7	10	node Right	2406	32	0	7.2	-4.6	83.3	E(80)	62.0	3	29.0	1.000	0.940	11.8	< 58.3
7	11	node Left	2412	32	0	9.4	-1.8	143.9	E(80)	62.0	3	29.0	1.000	0.940	11.2	< 58.3
7	11	node Right	2412	32	0	9.4	-1.8	143.9	E(80)	62.0	3	29.0	1.000	0.940	11.2	< 58.3
8	12	node Left	2418	32	0	6.9	-5.2	82.7	E(80)	62.0	3	29.0	1.000	0.940	12.1	< 58.3
8	12	node Right	2418	32	0	6.9	-5.2	82.7	E(80)	62.0	3	29.0	1.000	0.940	12.1	< 58.3
9	13	node Left	2425	16	0	8.7	-14.4	48.3	E(80)	62.0	3	29.0	1.000	1.000	23.1	< 62.0
9	13	node Right	2425	16	0	7.8	-12.8	42.9	E(80)	62.0	3	29.0	1.000	1.000	20.6	< 62.0
10	14	node Left	2433	12	0	7.4	-19.4	-19.6	E(80)	62.0	3	29.0	1.300	1.000	26.7	< 80.6
10	14	node Right	2433	12	0	7.4	-19.4	-19.6	E(80)	62.0	3	29.0	1.300	1.000	26.7	< 80.6
10	15	node Left	2440	12	0	6.3	-23.8	-70.2	E(80)	62.0	3	29.0	1.300	1.000	30.2	< 80.6
10	15	node Right	2440	12	0	6.4	-23.8	-70.3	E(80)	62.0	3	29.0	1.300	1.000	30.2	< 80.6
11	16	node Left	2447	13	0	4.6	-23.6	-89.8	E(80)	62.0	3	29.0	1.300	1.000	28.2	< 80.6
11	16	node Right	2447	13	0	4.6	-23.6	-89.8	E(80)	62.0	3	29.0	1.300	1.000	28.2	< 80.6
12	17	node Left	2454	13	0	3.6	-24.4	-98.8	E(80)	62.0	3	29.0	1.300	1.000	28.0	< 80.6
12	17	node Right	2454	13	0	3.6	-24.4	-98.8	E(80)	62.0	3	29.0	1.300	1.000	28.0	< 80.6
13	18	node Left	2462	13	0	4.9	-23.7	-89.8	E(80)	62.0	3	29.0	1.300	1.000	28.6	< 80.6
13	18	node Right	2462	13	0	4.9	-23.7	-89.8	E(80)	62.0	3	29.0	1.300	1.000	28.6	< 80.6
14	19	node Left	2466	12	0	6.7	-24.1	-69.8	E(80)	62.0	3	29.0	1.300	1.000	30.8	< 80.6
14	19	node Right	2466	12	0	6.7	-24.1	-69.7	E(80)	62.0	3	29.0	1.300	1.000	30.8	< 80.6
14	20	node Left	2466	12	0	7.8	-19.4	-18.1	E(80)	62.0	3	29.0	1.300	1.000	27.2	< 80.6
14	20	node Right	2466	12	0	7.7	-19.5	-18.0	E(80)	62.0	3	29.0	1.300	1.000	27.2	< 80.6
15	21	node Left	2466	17	0	7.4	-12.6	44.4	E(80)	62.0	3	29.0	1.000	1.000	20.0	< 62.0
15	21	node Right	2466	17	0	8.3	-14.1	49.7	E(80)	62.0	3	29.0	1.000	1.000	22.4	< 62.0
16	22	node Left	2466	34	0	6.5	-5.0	83.1	E(80)	62.0	3	29.0	1.000	0.926	11.5	< 57.4
16	22	node Right	2466	34	0	6.5	-5.0	83.1	E(80)	62.0	3	29.0	1.000	0.926	11.5	< 57.4
17	23	node Left	2466	36	0	9.4	-2.0	138.8	E(80)	62.0	3	29.0	1.000	0.913	11.4	< 56.6
17	23	node Right	2466	36	0	9.4	-2.1	138.8	E(80)	62.0	3	29.0	1.000	0.913	11.5	< 56.6
17	24	node Left	2466	36	0	7.1	-4.5	80.4	E(80)	62.0	3	29.0	1.000	0.913	11.6	< 56.6
17	24	node Right	2466	36	0	7.0	-4.5	80.4	E(80)	62.0	3	29.0	1.000	0.913	11.5	< 56.6
18	25	node Left	2466	20	0	9.0	-12.6	54.1	E(80)	62.0	3	29.0	1.000	1.000	21.7	< 62.0
18	25	node Right	2466	20	0	8.2	-11.4	48.9	E(80)	62.0	3	29.0	1.000	1.000	19.6	< 62.0
19	26	node Left	2466	12	0	10.5	-22.1	-5.1	E(80)	62.0	3	29.0	1.183	1.000	32.6	< 73.3

19	26 node Right	2466	12	0	10.5	-22.0	-5.2	E(80)	62.0	3	29.0	1.184	1.000	32.5 < 73.4
19	27 node Left	2466	12	0	9.0	-26.2	-61.1	E(80)	62.0	3	29.0	1.300	1.000	35.2 < 80.6
19	27 node Right	2466	12	0	9.4	-27.0	-63.1	E(80)	62.0	3	29.0	1.300	1.000	36.3 < 80.6
20	28 node Left	2466	14	0	6.6	-25.1	-85.7	E(80)	62.0	3	29.0	1.300	1.000	31.7 < 80.6
20	28 node Right	2466	14	0	6.6	-25.1	-85.7	E(80)	62.0	3	29.0	1.300	1.000	31.7 < 80.6
21	29 node Left	2466	14	0	5.2	-25.6	-101.4	E(80)	62.0	3	29.0	1.300	1.000	30.8 < 80.6
21	29 node Right	2466	14	0	5.2	-25.6	-101.4	E(80)	62.0	3	29.0	1.300	1.000	30.8 < 80.6
21	30 node Left	2466	14	0	3.8	-24.2	-100.3	E(80)	62.0	3	29.0	1.300	1.000	28.0 < 80.6
21	30 node Right	2466	14	0	3.8	-24.2	-100.3	E(80)	62.0	3	29.0	1.300	1.000	28.0 < 80.6
22	31 node Left	2466	14	0	2.6	-21.0	-84.1	E(80)	62.0	3	29.0	1.300	1.000	23.5 < 80.6
22	31 node Right	2466	14	0	2.5	-21.0	-84.0	E(80)	62.0	3	29.0	1.300	1.000	23.4 < 80.6
23	32 node Left	2466	12	0	1.4	-17.0	-60.4	E(80)	62.0	3	29.0	1.300	1.000	18.4 < 80.6
23	32 node Right	2466	12	0	1.4	-17.0	-60.3	E(80)	62.0	3	29.0	1.300	1.000	18.5 < 80.6
23	33 node Left	2466	12	0	0.0	-0.1	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.1 < 80.6

STEEL-BOX G1

node WEB-L-2 (Web Lower edge) WEB - 2

Stress

range

node number	node number	Web	height (mm)	t	σ_{max} (N/mm ²)	σ_{min} (N/mm ²)	σ_d	$\Delta \sigma_f$ (E)	$\Delta \sigma_{ce}$ (m)	$\Delta \sigma_{ve}$ (CR)	Ct	$\Delta \sigma_{max}$ (N/mm ²)	Cycle	D	
1	1	node Right	2364	12	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.000	0.0	< 80.6	
1	2	node Left	2367	12	0	19.6	-1.8	74.3 E(80)	62.0	3	29.0	1.000	1.000	21.4	< 62.0
1	2	node Right	2367	12	0	19.6	-1.8	74.3 E(80)	62.0	3	29.0	1.000	1.000	21.4	< 62.0
2	3	node Left	2370	18	0	20.5	-2.5	85.6 E(80)	62.0	3	29.0	1.000	1.000	23.0	< 62.0
2	3	node Right	2370	18	0	20.5	-2.5	85.6 E(80)	62.0	3	29.0	1.000	1.000	23.0	< 62.0
3	4	node Left	2374	18	0	24.0	-3.8	103.2 E(80)	62.0	3	29.0	1.000	1.000	27.8	< 62.0
3	4	node Right	2374	18	0	24.1	-3.8	103.2 E(80)	62.0	3	29.0	1.000	1.000	27.9	< 62.0
3	5	node Left	2377	18	0	25.4	-5.1	104.1 E(80)	62.0	3	29.0	1.000	1.000	30.5	< 62.0
3	5	node Right	2377	18	0	25.4	-5.1	104.1 E(80)	62.0	3	29.0	1.000	1.000	30.5	< 62.0
4	6	node Left	2382	18	0	24.8	-6.3	88.1 E(80)	62.0	3	29.0	1.000	1.000	31.1	< 62.0
4	6	node Right	2382	18	0	24.8	-6.3	88.1 E(80)	62.0	3	29.0	1.000	1.000	31.1	< 62.0
5	7	node Left	2388	12	0	32.0	-10.8	79.8 E(80)	62.0	3	29.0	1.000	1.000	42.8	< 62.0
5	7	node Right	2388	12	0	26.8	-9.0	66.7 E(80)	62.0	3	29.0	1.000	1.000	35.8	< 62.0
5	8	node Left	2394	12	0	22.2	-10.4	8.6 E(80)	62.0	3	29.0	1.000	1.000	32.6	< 62.0
5	8	node Right	2394	12	0	22.2	-10.4	8.6 E(80)	62.0	3	29.0	1.000	1.000	32.6	< 62.0
6	9	node Left	2400	14	0	12.9	-9.1	-53.6 E(80)	62.0	3	29.0	1.300	1.000	22.0	< 80.6
6	9	node Right	2400	14	0	13.0	-9.3	-54.2 E(80)	62.0	3	29.0	1.300	1.000	22.2	< 80.6
7	10	node Left	2406	26	0	4.7	-7.4	-84.8 E(80)	62.0	3	29.0	1.300	0.990	12.1	< 79.8
7	10	node Right	2406	26	0	4.7	-7.4	-84.8 E(80)	62.0	3	29.0	1.300	0.990	12.1	< 79.8
7	11	node Left	2412	26	0	1.9	-9.4	-145.4 E(80)	62.0	3	29.0	1.300	0.990	11.4	< 79.8
7	11	node Right	2412	26	0	1.9	-9.4	-145.4 E(80)	62.0	3	29.0	1.300	0.990	11.4	< 79.8
8	12	node Left	2418	21	0	5.9	-7.9	-94.5 E(80)	62.0	3	29.0	1.300	1.000	13.8	< 80.6
8	12	node Right	2418	21	0	5.9	-7.9	-94.5 E(80)	62.0	3	29.0	1.300	1.000	13.8	< 80.6
9	13	node Left	2425	14	0	14.6	-8.9	-49.1 E(80)	62.0	3	29.0	1.300	1.000	23.5	< 80.6
9	13	node Right	2425	14	0	14.5	-8.7	-48.4 E(80)	62.0	3	29.0	1.300	1.000	23.2	< 80.6
10	14	node Left	2433	12	0	18.8	-7.2	19.1 E(80)	62.0	3	29.0	1.000	1.000	26.0	< 62.0
10	14	node Right	2433	12	0	18.8	-7.1	19.1 E(80)	62.0	3	29.0	1.000	1.000	25.9	< 62.0
10	15	node Left	2440	12	0	27.7	-7.4	81.8 E(80)	62.0	3	29.0	1.000	1.000	35.1	< 62.0
10	15	node Right	2440	12	0	27.7	-7.4	81.8 E(80)	62.0	3	29.0	1.000	1.000	35.1	< 62.0
11	16	node Left	2447	16	0	24.5	-4.7	93.2 E(80)	62.0	3	29.0	1.000	1.000	29.2	< 62.0
11	16	node Right	2447	16	0	24.5	-4.7	93.2 E(80)	62.0	3	29.0	1.000	1.000	29.2	< 62.0
12	17	node Left	2454	16	0	25.2	-3.7	101.9 E(80)	62.0	3	29.0	1.000	1.000	28.9	< 62.0
12	17	node Right	2454	16	0	25.2	-3.7	101.9 E(80)	62.0	3	29.0	1.000	1.000	28.9	< 62.0
13	18	node Left	2462	16	0	24.3	-5.0	92.1 E(80)	62.0	3	29.0	1.000	1.000	29.3	< 62.0
13	18	node Right	2462	16	0	24.3	-5.0	92.1 E(80)	62.0	3	29.0	1.000	1.000	29.3	< 62.0
14	19	node Left	2466	12	0	27.4	-7.7	79.4 E(80)	62.0	3	29.0	1.000	1.000	35.1	< 62.0
14	19	node Right	2466	12	0	27.4	-7.7	79.4 E(80)	62.0	3	29.0	1.000	1.000	35.0	< 62.0
14	20	node Left	2466	12	0	18.6	-7.3	17.1 E(80)	62.0	3	29.0	1.000	1.000	25.8	< 62.0
14	20	node Right	2466	12	0	18.5	-7.4	17.1 E(80)	62.0	3	29.0	1.000	1.000	25.8	< 62.0
15	21	node Left	2466	14	0	14.0	-8.3	-49.6 E(80)	62.0	3	29.0	1.300	1.000	22.3	< 80.6
15	21	node Right	2466	14	0	14.3	-8.4	-50.4 E(80)	62.0	3	29.0	1.300	1.000	22.7	< 80.6
16	22	node Left	2466	21	0	5.7	-7.4	-94.6 E(80)	62.0	3	29.0	1.300	1.000	13.1	< 80.6
16	22	node Right	2466	21	0	5.8	-7.4	-94.7 E(80)	62.0	3	29.0	1.300	1.000	13.2	< 80.6
17	23	node Left	2466	27	0	2.1	-9.6	-141.5 E(80)	62.0	3	29.0	1.300	0.981	11.7	< 79.1
17	23	node Right	2466	27	0	2.1	-9.6	-141.5 E(80)	62.0	3	29.0	1.300	0.981	11.7	< 79.1
17	24	node Left	2466	27	0	4.6	-7.2	-82.3 E(80)	62.0	3	29.0	1.300	0.981	11.8	< 79.1
17	24	node Right	2466	27	0	4.6	-7.2	-82.3 E(80)	62.0	3	29.0	1.300	0.981	11.8	< 79.1
18	25	node Left	2466	14	0	12.8	-9.1	-54.6 E(80)	62.0	3	29.0	1.300	1.000	21.9	< 80.6
18	25	node Right	2466	14	0	12.6	-9.0	-54.0 E(80)	62.0	3	29.0	1.300	1.000	21.7	< 80.6
19	26	node Left	2466	12	0	21.6	-10.2	5.0 E(80)	62.0	3	29.0	1.000	1.000	31.8	< 62.0

19	26 node Right	2466	12	0	21.6	-10.3	5.1	E(80)	62.0	3	29.0	1.000	1.000	31.9	< 62.0
19	27 node Left	2466	12	0	25.7	-8.9	59.9	E(80)	62.0	3	29.0	1.000	1.000	34.6	< 62.0
19	27 node Right	2466	12	0	30.7	-10.6	71.7	E(80)	62.0	3	29.0	1.000	1.000	41.4	< 62.0
20	28 node Left	2466	16	0	25.4	-6.6	86.5	E(80)	62.0	3	29.0	1.000	1.000	32.0	< 62.0
20	28 node Right	2466	16	0	25.3	-6.6	86.6	E(80)	62.0	3	29.0	1.000	1.000	31.9	< 62.0
21	29 node Left	2466	16	0	25.8	-5.3	102.4	E(80)	62.0	3	29.0	1.000	1.000	31.1	< 62.0
21	29 node Right	2466	16	0	25.8	-5.3	102.4	E(80)	62.0	3	29.0	1.000	1.000	31.1	< 62.0
21	30 node Left	2466	16	0	24.4	-3.8	101.3	E(80)	62.0	3	29.0	1.000	1.000	28.2	< 62.0
21	30 node Right	2466	16	0	24.4	-3.8	101.3	E(80)	62.0	3	29.0	1.000	1.000	28.2	< 62.0
22	31 node Left	2466	14	0	22.6	-2.7	90.7	E(80)	62.0	3	29.0	1.000	1.000	25.3	< 62.0
22	31 node Right	2466	14	0	22.6	-2.7	90.7	E(80)	62.0	3	29.0	1.000	1.000	25.3	< 62.0
23	32 node Left	2466	12	0	18.6	-1.6	66.4	E(80)	62.0	3	29.0	1.000	1.000	20.2	< 62.0
23	32 node Right	2466	12	0	18.7	-1.6	66.3	E(80)	62.0	3	29.0	1.000	1.000	20.3	< 62.0
23	33 node Left	2466	12	0	0.1	0.0	0.0	E(80)	62.0	3	29.0	1.000	1.000	0.1	< 62.0

STEEL-BOX G1

node HSTIFF-2 (Web H-stiff) WEB - 2

Stress

range

node number	node number	Web	height (mm)	t	σ_{max} (N/mm ²)	σ_{min} (N/mm ²)	σ_d	$\Delta \sigma_f$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$ (N/mm ²)	CR • Ct	D
1	1	node Right	2364	12	473	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
1	2	node Left	2367	12	473	0.8	-9.1	-34.7	G(50)	32.0	3	15.0	1.300	1.000	10.0	< 41.6
1	2	node Right	2367	12	473	0.8	-9.2	-34.7	G(50)	32.0	3	15.0	1.300	1.000	10.0	< 41.6
2	3	node Left	2370	12	474	1.5	-11.9	-49.6	G(50)	32.0	3	15.0	1.300	1.000	13.4	< 41.6
2	3	node Right	2370	12	474	1.4	-11.9	-49.6	G(50)	32.0	3	15.0	1.300	1.000	13.3	< 41.6
3	4	node Left	2374	12	475	2.2	-14.0	-60.0	G(50)	32.0	3	15.0	1.300	1.000	16.2	< 41.6
3	4	node Right	2374	12	475	2.2	-14.0	-60.0	G(50)	32.0	3	15.0	1.300	1.000	16.2	< 41.6
3	5	node Left	2377	12	475	3.0	-14.8	-60.8	G(50)	32.0	3	15.0	1.300	1.000	17.8	< 41.6
3	5	node Right	2377	12	475	3.0	-14.8	-60.8	G(50)	32.0	3	15.0	1.300	1.000	17.8	< 41.6
4	6	node Left	2382	12	476	3.7	-14.6	-51.8	G(50)	32.0	3	15.0	1.300	1.000	18.3	< 41.6
4	6	node Right	2382	12	476	3.7	-14.6	-51.8	G(50)	32.0	3	15.0	1.300	1.000	18.3	< 41.6
5	7	node Left	2388	12	478	4.9	-14.7	-36.4	G(50)	32.0	3	15.0	1.300	1.000	19.6	< 41.6
5	7	node Right	2388	12	478	5.2	-15.1	-37.8	G(50)	32.0	3	15.0	1.300	1.000	20.2	< 41.6
5	8	node Left	2394	12	479	5.9	-12.6	-4.9	G(50)	32.0	3	15.0	1.259	1.000	18.5	< 40.3
5	8	node Right	2394	12	479	5.9	-12.6	-4.9	G(50)	32.0	3	15.0	1.259	1.000	18.5	< 40.3
6	9	node Left	2400	14	480	8.0	-5.6	-33.2	G(50)	32.0	3	15.0	1.300	1.000	13.6	< 41.6
6	9	node Right	2400	14	480	7.8	-5.6	-32.6	G(50)	32.0	3	15.0	1.300	1.000	13.4	< 41.6
7	10	node Left	2406	16	481	2.8	-4.4	-51.2	G(50)	32.0	3	15.0	1.300	1.000	7.3	< 41.6
7	10	node Right	2406	16	481	2.8	-4.4	-51.2	G(50)	32.0	3	15.0	1.300	1.000	7.3	< 41.6
7	11	node Left	2412	16	482	1.2	-5.7	-87.5	G(50)	32.0	3	15.0	1.300	1.000	6.8	< 41.6
7	11	node Right	2412	16	482	1.2	-5.7	-87.5	G(50)	32.0	3	15.0	1.300	1.000	6.8	< 41.6
8	12	node Left	2418	16	484	3.7	-5.0	-59.1	G(50)	32.0	3	15.0	1.300	1.000	8.7	< 41.6
8	12	node Right	2418	16	484	3.7	-5.0	-59.1	G(50)	32.0	3	15.0	1.300	1.000	8.7	< 41.6
9	13	node Left	2425	14	485	8.8	-5.4	-29.6	G(50)	32.0	3	15.0	1.300	1.000	14.2	< 41.6
9	13	node Right	2425	14	485	9.0	-5.4	-30.1	G(50)	32.0	3	15.0	1.300	1.000	14.4	< 41.6
10	14	node Left	2433	12	487	4.4	-11.7	-11.9	G(50)	32.0	3	15.0	1.300	1.000	16.2	< 41.6
10	14	node Right	2433	12	487	4.5	-11.7	-11.9	G(50)	32.0	3	15.0	1.300	1.000	16.2	< 41.6
10	15	node Left	2440	12	488	3.6	-13.5	-39.8	G(50)	32.0	3	15.0	1.300	1.000	17.1	< 41.6
10	15	node Right	2440	12	488	3.6	-13.5	-39.9	G(50)	32.0	3	15.0	1.300	1.000	17.1	< 41.6
11	16	node Left	2447	12	489	2.7	-14.0	-53.2	G(50)	32.0	3	15.0	1.300	1.000	16.7	< 41.6
11	16	node Right	2447	12	489	2.7	-14.0	-53.2	G(50)	32.0	3	15.0	1.300	1.000	16.7	< 41.6
12	17	node Left	2454	12	491	2.1	-14.5	-58.7	G(50)	32.0	3	15.0	1.300	1.000	16.6	< 41.6
12	17	node Right	2454	12	491	2.1	-14.5	-58.7	G(50)	32.0	3	15.0	1.300	1.000	16.6	< 41.6
13	18	node Left	2462	12	492	2.9	-14.1	-53.4	G(50)	32.0	3	15.0	1.300	1.000	17.0	< 41.6
13	18	node Right	2462	12	492	2.9	-14.1	-53.4	G(50)	32.0	3	15.0	1.300	1.000	17.0	< 41.6
14	19	node Left	2466	12	493	3.8	-13.8	-40.0	G(50)	32.0	3	15.0	1.300	1.000	17.6	< 41.6
14	19	node Right	2466	12	493	3.8	-13.8	-39.9	G(50)	32.0	3	15.0	1.300	1.000	17.6	< 41.6
14	20	node Left	2466	12	493	4.8	-11.8	-11.1	G(50)	32.0	3	15.0	1.300	1.000	16.6	< 41.6
14	20	node Right	2466	12	493	4.7	-11.9	-11.0	G(50)	32.0	3	15.0	1.300	1.000	16.6	< 41.6
15	21	node Left	2466	14	493	8.7	-5.2	-30.8	G(50)	32.0	3	15.0	1.300	1.000	13.9	< 41.6
15	21	node Right	2466	14	493	8.6	-5.1	-30.4	G(50)	32.0	3	15.0	1.300	1.000	13.7	< 41.6
16	22	node Left	2466	16	493	3.5	-4.7	-59.1	G(50)	32.0	3	15.0	1.300	1.000	8.2	< 41.6
16	22	node Right	2466	16	493	3.6	-4.7	-59.1	G(50)	32.0	3	15.0	1.300	1.000	8.3	< 41.6
17	23	node Left	2466	16	493	1.3	-5.8	-85.4	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
17	23	node Right	2466	16	493	1.2	-5.8	-85.4	G(50)	32.0	3	15.0	1.300	1.000	7.0	< 41.6
17	24	node Left	2466	16	493	2.8	-4.3	-49.8	G(50)	32.0	3	15.0	1.300	1.000	7.2	< 41.6
17	24	node Right	2466	16	493	2.8	-4.4	-49.8	G(50)	32.0	3	15.0	1.300	1.000	7.2	< 41.6
18	25	node Left	2466	14	493	7.7	-5.5	-32.9	G(50)	32.0	3	15.0	1.300	1.000	13.2	< 41.6
18	25	node Right	2466	14	493	7.8	-5.6	-33.4	G(50)	32.0	3	15.0	1.300	1.000	13.4	< 41.6
19	26	node Left	2466	12	493	6.3	-13.3	-3.1	G(50)	32.0	3	15.0	1.183	1.000	19.7	< 37.8

19	26 node Right	2466	12	493	6.3	-13.3	-3.1	G(50)	32.0	3	15.0	1.185	1.000	19.6<	37.9
19	27 node Left	2466	12	493	5.5	-15.8	-36.9	G(50)	32.0	3	15.0	1.300	1.000	21.2<	41.6
19	27 node Right	2466	12	493	5.4	-15.4	-36.1	G(50)	32.0	3	15.0	1.300	1.000	20.8<	41.6
20	28 node Left	2466	12	493	3.9	-15.0	-51.3	G(50)	32.0	3	15.0	1.300	1.000	18.9<	41.6
20	28 node Right	2466	12	493	3.9	-15.0	-51.2	G(50)	32.0	3	15.0	1.300	1.000	19.0<	41.6
21	29 node Left	2466	12	493	3.1	-15.3	-60.6	G(50)	32.0	3	15.0	1.300	1.000	18.4<	41.6
21	29 node Right	2466	12	493	3.1	-15.3	-60.6	G(50)	32.0	3	15.0	1.300	1.000	18.4<	41.6
21	30 node Left	2466	12	493	2.3	-14.4	-60.0	G(50)	32.0	3	15.0	1.300	1.000	16.8<	41.6
21	30 node Right	2466	12	493	2.3	-14.4	-60.0	G(50)	32.0	3	15.0	1.300	1.000	16.8<	41.6
22	31 node Left	2466	12	493	1.5	-12.3	-49.1	G(50)	32.0	3	15.0	1.300	1.000	13.8<	41.6
22	31 node Right	2466	12	493	1.4	-12.3	-49.1	G(50)	32.0	3	15.0	1.300	1.000	13.7<	41.6
23	32 node Left	2466	12	493	0.8	-9.8	-35.0	G(50)	32.0	3	15.0	1.300	1.000	10.7<	41.6
23	32 node Right	2466	12	493	0.8	-9.9	-35.0	G(50)	32.0	3	15.0	1.300	1.000	10.7<	41.6
23	33 node Left	2466	12	493	0.0	-0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0<	41.6

STEEL-BOX G1

node POINT-U-2 (Web Upper) WEB - 2

Stress

range

node number	node number	Web	height (mm)	t	σ_{tmax} (N/mm ²)	σ_{tmin}	σ_d	$\Delta(\sigma_f)$	$\Delta\sigma_{cem}$	$\Delta\sigma_{ve}$	CR	Ct	$\Delta\sigma_{max}$ (N/mm ²)	Cycle	D
1	1	node Right	2364	12	900	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0 < 41.6
1	2	node Left	2367	12	900	0.2	-2.7	-10.1	G(50)	32.0	3	15.0	1.300	1.000	2.9 < 41.6
1	2	node Right	2367	12	900	0.2	-2.7	-10.1	G(50)	32.0	3	15.0	1.300	1.000	3.0 < 41.6
2	3	node Left	2370	12	900	0.6	-4.6	-19.2	G(50)	32.0	3	15.0	1.300	1.000	5.2 < 41.6
2	3	node Right	2370	12	900	0.5	-4.6	-19.2	G(50)	32.0	3	15.0	1.300	1.000	5.2 < 41.6
3	4	node Left	2374	12	900	0.8	-5.5	-23.5	G(50)	32.0	3	15.0	1.300	1.000	6.3 < 41.6
3	4	node Right	2374	12	900	0.8	-5.5	-23.5	G(50)	32.0	3	15.0	1.300	1.000	6.3 < 41.6
3	5	node Left	2377	12	900	1.2	-5.9	-24.0	G(50)	32.0	3	15.0	1.300	1.000	7.1 < 41.6
3	5	node Right	2377	12	900	1.2	-5.9	-24.0	G(50)	32.0	3	15.0	1.300	1.000	7.1 < 41.6
4	6	node Left	2382	12	900	1.5	-5.8	-20.7	G(50)	32.0	3	15.0	1.300	1.000	7.3 < 41.6
4	6	node Right	2382	12	900	1.5	-5.8	-20.7	G(50)	32.0	3	15.0	1.300	1.000	7.3 < 41.6
5	7	node Left	2388	12	900	1.5	-4.3	-10.7	G(50)	32.0	3	15.0	1.300	1.000	5.8 < 41.6
5	7	node Right	2388	12	900	2.0	-5.8	-14.7	G(50)	32.0	3	15.0	1.300	1.000	7.8 < 41.6
5	8	node Left	2394	12	900	2.3	-5.0	-1.9	G(50)	32.0	3	15.0	1.260	1.000	7.3 < 40.3
5	8	node Right	2394	12	900	2.3	-5.0	-1.9	G(50)	32.0	3	15.0	1.260	1.000	7.3 < 40.3
6	9	node Left	2400	14	900	1.7	-2.4	10.0	G(50)	32.0	3	15.0	1.000	1.000	4.2 < 32.0
6	9	node Right	2400	14	900	2.3	-3.2	13.3	G(50)	32.0	3	15.0	1.000	1.000	5.5 < 32.0
7	10	node Left	2406	16	900	1.8	-1.1	20.4	G(50)	32.0	3	15.0	1.000	1.000	2.9 < 32.0
7	10	node Right	2406	16	900	1.8	-1.1	20.4	G(50)	32.0	3	15.0	1.000	1.000	2.9 < 32.0
7	11	node Left	2412	16	900	2.3	-0.4	36.0	G(50)	32.0	3	15.0	1.000	1.000	2.8 < 32.0
7	11	node Right	2412	16	900	2.3	-0.4	36.0	G(50)	32.0	3	15.0	1.000	1.000	2.8 < 32.0
8	12	node Left	2418	16	900	1.4	-1.1	16.8	G(50)	32.0	3	15.0	1.000	1.000	2.4 < 32.0
8	12	node Right	2418	16	900	1.4	-1.1	16.8	G(50)	32.0	3	15.0	1.000	1.000	2.4 < 32.0
9	13	node Left	2425	14	900	2.2	-3.6	12.2	G(50)	32.0	3	15.0	1.000	1.000	5.8 < 32.0
9	13	node Right	2425	14	900	1.6	-2.7	9.0	G(50)	32.0	3	15.0	1.000	1.000	4.3 < 32.0
10	14	node Left	2433	12	900	2.0	-5.2	-5.3	G(50)	32.0	3	15.0	1.300	1.000	7.2 < 41.6
10	14	node Right	2433	12	900	2.0	-5.2	-5.3	G(50)	32.0	3	15.0	1.300	1.000	7.2 < 41.6
10	15	node Left	2440	12	900	1.2	-4.8	-14.1	G(50)	32.0	3	15.0	1.300	1.000	6.1 < 41.6
10	15	node Right	2440	12	900	1.3	-4.8	-14.2	G(50)	32.0	3	15.0	1.300	1.000	6.1 < 41.6
11	16	node Left	2447	12	900	1.1	-5.9	-22.5	G(50)	32.0	3	15.0	1.300	1.000	7.1 < 41.6
11	16	node Right	2447	12	900	1.1	-5.9	-22.5	G(50)	32.0	3	15.0	1.300	1.000	7.1 < 41.6
12	17	node Left	2454	12	900	0.9	-6.2	-25.2	G(50)	32.0	3	15.0	1.300	1.000	7.1 < 41.6
12	17	node Right	2454	12	900	0.9	-6.2	-25.2	G(50)	32.0	3	15.0	1.300	1.000	7.1 < 41.6
13	18	node Left	2462	12	900	1.3	-6.1	-23.3	G(50)	32.0	3	15.0	1.300	1.000	7.4 < 41.6
13	18	node Right	2462	12	900	1.3	-6.1	-23.3	G(50)	32.0	3	15.0	1.300	1.000	7.4 < 41.6
14	19	node Left	2466	12	900	1.5	-5.3	-15.3	G(50)	32.0	3	15.0	1.300	1.000	6.7 < 41.6
14	19	node Right	2466	12	900	1.5	-5.3	-15.3	G(50)	32.0	3	15.0	1.300	1.000	6.8 < 41.6
14	20	node Left	2466	12	900	2.3	-5.6	-5.3	G(50)	32.0	3	15.0	1.300	1.000	7.8 < 41.6
14	20	node Right	2466	12	900	2.2	-5.7	-5.2	G(50)	32.0	3	15.0	1.300	1.000	7.8 < 41.6
15	21	node Left	2466	14	900	1.7	-2.9	10.1	G(50)	32.0	3	15.0	1.000	1.000	4.6 < 32.0
15	21	node Right	2466	14	900	2.2	-3.7	13.2	G(50)	32.0	3	15.0	1.000	1.000	5.9 < 32.0
16	22	node Left	2466	16	900	1.4	-1.1	18.2	G(50)	32.0	3	15.0	1.000	1.000	2.5 < 32.0
16	22	node Right	2466	16	900	1.4	-1.1	18.2	G(50)	32.0	3	15.0	1.000	1.000	2.5 < 32.0
17	23	node Left	2466	16	900	2.5	-0.5	36.5	G(50)	32.0	3	15.0	1.000	1.000	3.0 < 32.0
17	23	node Right	2466	16	900	2.5	-0.6	36.5	G(50)	32.0	3	15.0	1.000	1.000	3.1 < 32.0
17	24	node Left	2466	16	900	1.9	-1.2	21.0	G(50)	32.0	3	15.0	1.000	1.000	3.0 < 32.0
17	24	node Right	2466	16	900	1.8	-1.2	21.0	G(50)	32.0	3	15.0	1.000	1.000	3.0 < 32.0
18	25	node Left	2466	14	900	2.4	-3.4	14.4	G(50)	32.0	3	15.0	1.000	1.000	5.8 < 32.0
18	25	node Right	2466	14	900	1.9	-2.7	11.3	G(50)	32.0	3	15.0	1.000	1.000	4.5 < 32.0
19	26	node Left	2466	12	900	2.9	-6.1	-1.4	G(50)	32.0	3	15.0	1.182	1.000	9.1 < 37.8

19	26 node Right	2466	12	900	2.9	-6.1	-1.4	G(50)	32.0	3	15.0	1.185	1.000	9.0<	37.9
19	27 node Left	2466	12	900	2.5	-7.2	-16.9	G(50)	32.0	3	15.0	1.300	1.000	9.7<	41.6
19	27 node Right	2466	12	900	2.1	-5.9	-13.9	G(50)	32.0	3	15.0	1.300	1.000	8.0<	41.6
20	28 node Left	2466	12	900	1.7	-6.7	-22.9	G(50)	32.0	3	15.0	1.300	1.000	8.4<	41.6
20	28 node Right	2466	12	900	1.7	-6.7	-22.8	G(50)	32.0	3	15.0	1.300	1.000	8.5<	41.6
21	29 node Left	2466	12	900	1.4	-6.8	-27.0	G(50)	32.0	3	15.0	1.300	1.000	8.2<	41.6
21	29 node Right	2466	12	900	1.4	-6.8	-27.0	G(50)	32.0	3	15.0	1.300	1.000	8.2<	41.6
21	30 node Left	2466	12	900	1.0	-6.4	-26.7	G(50)	32.0	3	15.0	1.300	1.000	7.5<	41.6
21	30 node Right	2466	12	900	1.0	-6.4	-26.7	G(50)	32.0	3	15.0	1.300	1.000	7.5<	41.6
22	31 node Left	2466	12	900	0.6	-5.1	-20.3	G(50)	32.0	3	15.0	1.300	1.000	5.7<	41.6
22	31 node Right	2466	12	900	0.6	-5.1	-20.2	G(50)	32.0	3	15.0	1.300	1.000	5.7<	41.6
23	32 node Left	2466	12	900	0.3	-4.0	-14.1	G(50)	32.0	3	15.0	1.300	1.000	4.3<	41.6
23	32 node Right	2466	12	900	0.3	-4.0	-14.1	G(50)	32.0	3	15.0	1.300	1.000	4.3<	41.6
23	33 node Left	2466	12	900	0.0	-0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0<	41.6

STEEL-BOX G1

node POINT-L-2 (Web) WEB - 2

Stress

range															
node	node	Web	Grade				$\Delta \sigma_{ce} \cdot \text{Cycle}$								
number	number	height	t	σ_{tmax}	σ_{tmin}	σ_d	($\Delta \sigma_f$)	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR · Ct	D
		(mm)	(N/mm ²)				(N/mm ²)								
1	1 node Right	2364	12	500	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
1	2 node Left	2367	12	500	12.0	-1.1	45.5	G(50)	32.0	3	15.0	1.000	1.000	13.1	< 32.0
1	2 node Right	2367	12	500	12.0	-1.1	45.5	G(50)	32.0	3	15.0	1.000	1.000	13.1	< 32.0
2	3 node Left	2370	12	500	11.9	-1.4	50.0	G(50)	32.0	3	15.0	1.000	1.000	13.4	< 32.0
2	3 node Right	2370	12	500	11.9	-1.5	50.0	G(50)	32.0	3	15.0	1.000	1.000	13.4	< 32.0
3	4 node Left	2374	12	500	14.0	-2.3	60.2	G(50)	32.0	3	15.0	1.000	1.000	16.2	< 32.0
3	4 node Right	2374	12	500	14.1	-2.3	60.2	G(50)	32.0	3	15.0	1.000	1.000	16.3	< 32.0
3	5 node Left	2377	12	500	14.8	-3.0	60.7	G(50)	32.0	3	15.0	1.000	1.000	17.8	< 32.0
3	5 node Right	2377	12	500	14.8	-3.0	60.7	G(50)	32.0	3	15.0	1.000	1.000	17.8	< 32.0
4	6 node Left	2382	12	500	14.5	-3.7	51.4	G(50)	32.0	3	15.0	1.000	1.000	18.2	< 32.0
4	6 node Right	2382	12	500	14.5	-3.7	51.4	G(50)	32.0	3	15.0	1.000	1.000	18.2	< 32.0
5	7 node Left	2388	12	500	19.8	-6.7	49.4	G(50)	32.0	3	15.0	1.000	1.000	26.5	< 32.0
5	7 node Right	2388	12	500	15.8	-5.3	39.4	G(50)	32.0	3	15.0	1.000	1.000	21.2	< 32.0
5	8 node Left	2394	12	500	13.1	-6.1	5.1	G(50)	32.0	3	15.0	1.000	1.000	19.2	< 32.0
5	8 node Right	2394	12	500	13.1	-6.1	5.1	G(50)	32.0	3	15.0	1.000	1.000	19.2	< 32.0
6	9 node Left	2400	14	500	7.8	-5.5	-32.4	G(50)	32.0	3	15.0	1.300	1.000	13.3	< 41.6
6	9 node Right	2400	14	500	7.6	-5.4	-31.7	G(50)	32.0	3	15.0	1.300	1.000	13.0	< 41.6
7	10 node Left	2406	16	500	2.8	-4.3	-49.9	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
7	10 node Right	2406	16	500	2.8	-4.3	-49.9	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
7	11 node Left	2412	16	500	1.1	-5.5	-85.4	G(50)	32.0	3	15.0	1.300	1.000	6.7	< 41.6
7	11 node Right	2412	16	500	1.1	-5.5	-85.4	G(50)	32.0	3	15.0	1.300	1.000	6.7	< 41.6
8	12 node Left	2418	16	500	3.6	-4.9	-57.9	G(50)	32.0	3	15.0	1.300	1.000	8.5	< 41.6
8	12 node Right	2418	16	500	3.6	-4.9	-57.9	G(50)	32.0	3	15.0	1.300	1.000	8.5	< 41.6
9	13 node Left	2425	14	500	8.7	-5.3	-29.0	G(50)	32.0	3	15.0	1.300	1.000	13.9	< 41.6
9	13 node Right	2425	14	500	8.9	-5.3	-29.6	G(50)	32.0	3	15.0	1.300	1.000	14.2	< 41.6
10	14 node Left	2433	12	500	11.0	-4.2	11.1	G(50)	32.0	3	15.0	1.000	1.000	15.2	< 32.0
10	14 node Right	2433	12	500	11.0	-4.1	11.1	G(50)	32.0	3	15.0	1.000	1.000	15.1	< 32.0
10	15 node Left	2440	12	500	17.1	-4.6	50.6	G(50)	32.0	3	15.0	1.000	1.000	21.7	< 32.0
10	15 node Right	2440	12	500	17.1	-4.6	50.6	G(50)	32.0	3	15.0	1.000	1.000	21.7	< 32.0
11	16 node Left	2447	12	500	14.7	-2.8	55.8	G(50)	32.0	3	15.0	1.000	1.000	17.5	< 32.0
11	16 node Right	2447	12	500	14.7	-2.8	55.8	G(50)	32.0	3	15.0	1.000	1.000	17.5	< 32.0
12	17 node Left	2454	12	500	15.1	-2.2	61.0	G(50)	32.0	3	15.0	1.000	1.000	17.3	< 32.0
12	17 node Right	2454	12	500	15.1	-2.2	61.0	G(50)	32.0	3	15.0	1.000	1.000	17.3	< 32.0
13	18 node Left	2462	12	500	14.6	-3.0	55.2	G(50)	32.0	3	15.0	1.000	1.000	17.5	< 32.0
13	18 node Right	2462	12	500	14.6	-3.0	55.2	G(50)	32.0	3	15.0	1.000	1.000	17.5	< 32.0
14	19 node Left	2466	12	500	17.0	-4.8	49.1	G(50)	32.0	3	15.0	1.000	1.000	21.8	< 32.0
14	19 node Right	2466	12	500	16.9	-4.8	49.2	G(50)	32.0	3	15.0	1.000	1.000	21.7	< 32.0
14	20 node Left	2466	12	500	10.9	-4.2	10.0	G(50)	32.0	3	15.0	1.000	1.000	15.1	< 32.0
14	20 node Right	2466	12	500	10.8	-4.3	10.0	G(50)	32.0	3	15.0	1.000	1.000	15.1	< 32.0
15	21 node Left	2466	14	500	8.6	-5.1	-30.5	G(50)	32.0	3	15.0	1.300	1.000	13.7	< 41.6
15	21 node Right	2466	14	500	8.6	-5.0	-30.1	G(50)	32.0	3	15.0	1.300	1.000	13.6	< 41.6
16	22 node Left	2466	16	500	3.5	-4.6	-58.6	G(50)	32.0	3	15.0	1.300	1.000	8.1	< 41.6
16	22 node Right	2466	16	500	3.6	-4.6	-58.6	G(50)	32.0	3	15.0	1.300	1.000	8.2	< 41.6
17	23 node Left	2466	16	500	1.3	-5.7	-84.7	G(50)	32.0	3	15.0	1.300	1.000	7.0	< 41.6
17	23 node Right	2466	16	500	1.2	-5.7	-84.7	G(50)	32.0	3	15.0	1.300	1.000	7.0	< 41.6
17	24 node Left	2466	16	500	2.8	-4.3	-49.3	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
17	24 node Right	2466	16	500	2.8	-4.3	-49.3	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
18	25 node Left	2466	14	500	7.6	-5.4	-32.6	G(50)	32.0	3	15.0	1.300	1.000	13.1	< 41.6
18	25 node Right	2466	14	500	7.8	-5.6	-33.1	G(50)	32.0	3	15.0	1.300	1.000	13.3	< 41.6
19	26 node Left	2466	12	500	12.7	-6.0	3.0	G(50)	32.0	3	15.0	1.000	1.000	18.8	< 32.0

19	26 node Right	2466	12	500	12.8	-6.1	3.0	G(50)	32.0	3	15.0	1.000	1.000	18.9	<	32.0
19	27 node Left	2466	12	500	15.2	-5.2	35.4	G(50)	32.0	3	15.0	1.000	1.000	20.4	<	32.0
19	27 node Right	2466	12	500	19.0	-6.6	44.4	G(50)	32.0	3	15.0	1.000	1.000	25.6	<	32.0
20	28 node Left	2466	12	500	15.1	-4.0	51.6	G(50)	32.0	3	15.0	1.000	1.000	19.1	<	32.0
20	28 node Right	2466	12	500	15.1	-4.0	51.7	G(50)	32.0	3	15.0	1.000	1.000	19.0	<	32.0
21	29 node Left	2466	12	500	15.4	-3.2	61.1	G(50)	32.0	3	15.0	1.000	1.000	18.6	<	32.0
21	29 node Right	2466	12	500	15.4	-3.2	61.1	G(50)	32.0	3	15.0	1.000	1.000	18.6	<	32.0
21	30 node Left	2466	12	500	14.6	-2.3	60.4	G(50)	32.0	3	15.0	1.000	1.000	16.8	<	32.0
21	30 node Right	2466	12	500	14.6	-2.3	60.4	G(50)	32.0	3	15.0	1.000	1.000	16.8	<	32.0
22	31 node Left	2466	12	500	13.7	-1.6	55.3	G(50)	32.0	3	15.0	1.000	1.000	15.4	<	32.0
22	31 node Right	2466	12	500	13.7	-1.7	55.3	G(50)	32.0	3	15.0	1.000	1.000	15.4	<	32.0
23	32 node Left	2466	12	500	11.4	-1.0	40.7	G(50)	32.0	3	15.0	1.000	1.000	12.4	<	32.0
23	32 node Right	2466	12	500	11.5	-1.0	40.6	G(50)	32.0	3	15.0	1.000	1.000	12.5	<	32.0
23	33 node Left	2466	12	500	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.000	1.000	0.0	<	32.0

1. G2

STEEL-BOX G2

node U.FLG-MAX (UpperFlange)

Stress

range	node	node	Flange	Grade									$\Delta \sigma_{ce} \cdot \text{Cycle}$
D	number	number	t	σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce m}$	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR · Ct
			(mm)	(N/mm2)								(N/mm2)	(N/mm2)
1	1	node Right	10	0.0	0.0	0.0	F (65)	46.0	3	21.0	1.300	1.000	0.0 < 59.8
1	2	node Left	10	1.6	-17.1	-63.1	F (65)	46.0	3	21.0	1.300	1.000	18.7 < 59.8
1	2	node Right	10	1.6	-17.1	-63.1	F (65)	46.0	3	21.0	1.300	1.000	18.7 < 59.8
2	3	node Left	14	2.6	-21.0	-86.3	F (65)	46.0	3	21.0	1.300	1.000	23.6 < 59.8
2	3	node Right	14	2.6	-21.0	-86.3	F (65)	46.0	3	21.0	1.300	1.000	23.5 < 59.8
3	4	node Left	14	3.8	-24.5	-103.9	F (65)	46.0	3	21.0	1.300	1.000	28.3 < 59.8
3	4	node Right	14	3.8	-24.5	-103.9	F (65)	46.0	3	21.0	1.300	1.000	28.3 < 59.8
3	5	node Left	14	5.0	-25.8	-104.4	F (65)	46.0	3	21.0	1.300	1.000	30.8 < 59.8
3	5	node Right	14	5.0	-25.8	-104.4	F (65)	46.0	3	21.0	1.300	1.000	30.8 < 59.8
4	6	node Left	14	6.3	-25.0	-88.1	F (65)	46.0	3	21.0	1.300	1.000	31.4 < 59.8
4	6	node Right	14	6.3	-25.0	-88.1	F (65)	46.0	3	21.0	1.300	1.000	31.4 < 59.8
5	7	node Left	11	9.0	-26.7	-64.6	F (65)	46.0	3	21.0	1.300	1.000	35.7 < 59.8
5	7	node Right	11	8.7	-25.9	-62.8	F (65)	46.0	3	21.0	1.300	1.000	34.6 < 59.8
5	8	node Left	11	10.2	-21.8	-5.5	F (65)	46.0	3	21.0	1.194	1.000	32.0 < 54.9
5	8	node Right	11	10.2	-21.8	-5.5	F (65)	46.0	3	21.0	1.194	1.000	32.0 < 54.9
6	9	node Left	20	8.5	-11.2	49.4	F (65)	46.0	3	21.0	1.000	1.000	19.7 < 46.0
6	9	node Right	20	9.4	-12.4	54.7	F (65)	46.0	3	21.0	1.000	1.000	21.8 < 46.0
7	10	node Left	36	7.5	-4.5	82.0	F (65)	46.0	3	21.0	1.000	0.913	12.0 < 42.0
7	10	node Right	36	7.5	-4.5	82.0	F (65)	46.0	3	21.0	1.000	0.913	12.0 < 42.0
7	11	node Left	36	10.1	-2.2	141.4	F (65)	46.0	3	21.0	1.000	0.913	12.3 < 42.0
7	11	node Right	36	10.1	-2.2	141.4	F (65)	46.0	3	21.0	1.000	0.913	12.3 < 42.0
8	12	node Left	34	6.7	-5.0	86.0	F (65)	46.0	3	21.0	1.000	0.926	11.8 < 42.6
8	12	node Right	34	6.7	-5.0	86.0	F (65)	46.0	3	21.0	1.000	0.926	11.8 < 42.6
9	13	node Left	17	8.6	-13.9	50.9	F (65)	46.0	3	21.0	1.000	1.000	22.6 < 46.0
9	13	node Right	17	7.8	-12.4	45.4	F (65)	46.0	3	21.0	1.000	1.000	20.2 < 46.0
10	14	node Left	11	7.8	-19.7	-20.0	F (65)	46.0	3	21.0	1.300	1.000	27.4 < 59.8
10	14	node Right	11	7.8	-19.8	-20.0	F (65)	46.0	3	21.0	1.300	1.000	27.5 < 59.8
10	15	node Left	11	6.9	-24.7	-75.3	F (65)	46.0	3	21.0	1.300	1.000	31.6 < 59.8
10	15	node Right	11	6.8	-24.7	-75.3	F (65)	46.0	3	21.0	1.300	1.000	31.5 < 59.8
11	16	node Left	14	4.8	-24.0	-94.1	F (65)	46.0	3	21.0	1.300	1.000	28.8 < 59.8
11	16	node Right	14	4.8	-24.1	-94.1	F (65)	46.0	3	21.0	1.300	1.000	28.9 < 59.8
12	17	node Left	14	3.8	-25.0	-104.2	F (65)	46.0	3	21.0	1.300	1.000	28.7 < 59.8
12	17	node Right	14	3.8	-25.0	-104.2	F (65)	46.0	3	21.0	1.300	1.000	28.7 < 59.8
13	18	node Left	14	5.0	-24.3	-94.8	F (65)	46.0	3	21.0	1.300	1.000	29.3 < 59.8
13	18	node Right	14	5.0	-24.2	-94.8	F (65)	46.0	3	21.0	1.300	1.000	29.3 < 59.8
14	19	node Left	12	6.9	-24.5	-73.1	F (65)	46.0	3	21.0	1.300	1.000	31.4 < 59.8
14	19	node Right	12	7.0	-24.5	-73.1	F (65)	46.0	3	21.0	1.300	1.000	31.4 < 59.8
14	20	node Left	12	8.1	-19.7	-17.2	F (65)	46.0	3	21.0	1.300	1.000	27.8 < 59.8
14	20	node Right	12	8.0	-19.7	-17.1	F (65)	46.0	3	21.0	1.300	1.000	27.7 < 59.8
15	21	node Left	18	8.3	-12.6	49.9	F (65)	46.0	3	21.0	1.000	1.000	21.0 < 46.0
15	21	node Right	18	9.3	-14.0	55.5	F (65)	46.0	3	21.0	1.000	1.000	23.3 < 46.0
16	22	node Left	36	7.3	-5.0	89.4	F (65)	46.0	3	21.0	1.000	0.913	12.3 < 42.0
16	22	node Right	36	7.3	-5.0	89.4	F (65)	46.0	3	21.0	1.000	0.913	12.3 < 42.0
17	23	node Left	39	9.7	-1.9	142.4	F (65)	46.0	3	21.0	1.000	0.895	11.6 < 41.2
17	23	node Right	39	9.8	-1.9	143.2	F (65)	46.0	3	21.0	1.000	0.895	11.7 < 41.2
17	24	node Left	39	7.6	-4.5	85.7	F (65)	46.0	3	21.0	1.000	0.895	12.1 < 41.2

17	24 node Right	39	7.6	-4.5	85.7	F (65)	46.0	3	21.0	1.000	0.895	12.1 < 41.2
18	25 node Left	22	9.7	-12.2	59.4	F (65)	46.0	3	21.0	1.000	1.000	21.9 < 46.0
18	25 node Right	22	8.9	-11.2	54.0	F (65)	46.0	3	21.0	1.000	1.000	20.1 < 46.0
19	26 node Left	11	11.5	-23.1	-2.0	F (65)	46.0	3	21.0	1.116	1.000	34.6 < 51.3
19	26 node Right	11	11.6	-23.1	-2.1	F (65)	46.0	3	21.0	1.117	1.000	34.7 < 51.4
19	27 node Left	11	9.8	-27.9	-66.1	F (65)	46.0	3	21.0	1.300	1.000	37.8 < 59.8
19	27 node Right	11	10.2	-28.9	-68.3	F (65)	46.0	3	21.0	1.300	1.000	39.0 < 59.8
20	28 node Left	15	6.9	-25.9	-90.9	F (65)	46.0	3	21.0	1.300	1.000	32.8 < 59.8
20	28 node Right	15	6.9	-25.9	-90.9	F (65)	46.0	3	21.0	1.300	1.000	32.8 < 59.8
21	29 node Left	15	5.6	-26.7	-108.8	F (65)	46.0	3	21.0	1.300	1.000	32.3 < 59.8
21	29 node Right	15	5.6	-26.7	-108.8	F (65)	46.0	3	21.0	1.300	1.000	32.3 < 59.8
21	30 node Left	15	4.2	-25.5	-108.9	F (65)	46.0	3	21.0	1.300	1.000	29.8 < 59.8
21	30 node Right	15	4.2	-25.4	-108.9	F (65)	46.0	3	21.0	1.300	1.000	29.7 < 59.8
22	31 node Left	15	3.0	-21.7	-91.2	F (65)	46.0	3	21.0	1.300	1.000	24.6 < 59.8
22	31 node Right	15	2.9	-21.7	-91.1	F (65)	46.0	3	21.0	1.300	1.000	24.6 < 59.8
23	32 node Left	11	1.8	-17.7	-68.1	F (65)	46.0	3	21.0	1.300	1.000	19.5 < 59.8
23	32 node Right	11	1.9	-17.6	-68.1	F (65)	46.0	3	21.0	1.300	1.000	19.5 < 59.8
23	33 node Left	11	0.0	-0.1	0.0	F (65)	46.0	3	21.0	1.300	1.000	0.1 < 59.8

STEEL-BOX G2

node L.FLG-MAX (Lower Flange)

Stress

range

node number	node number	Flange	t	σ_{tmax}	σ_{tmin}	Grade	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{cem}$	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{ce}$	Cycle
			(mm)	(N/mm2)								(N/mm2)	(N/mm2)	
1	1	node Right	10	0.0	0.0	0.0 F (65)			46.0	3	21.0	1.300	1.000	0.0 < 59.8
1	2	node Left	10	19.4	-1.8	71.3 F (65)			46.0	3	21.0	1.000	1.000	21.2 < 46.0
1	2	node Right	10	19.3	-1.8	71.3 F (65)			46.0	3	21.0	1.000	1.000	21.1 < 46.0
2	3	node Left	16	21.8	-2.7	89.7 F (65)			46.0	3	21.0	1.000	1.000	24.5 < 46.0
2	3	node Right	16	21.8	-2.7	89.7 F (65)			46.0	3	21.0	1.000	1.000	24.5 < 46.0
3	4	node Left	16	25.5	-4.0	108.5 F (65)			46.0	3	21.0	1.000	1.000	29.5 < 46.0
3	4	node Right	16	25.5	-4.0	108.5 F (65)			46.0	3	21.0	1.000	1.000	29.5 < 46.0
3	5	node Left	16	27.0	-5.3	109.3 F (65)			46.0	3	21.0	1.000	1.000	32.2 < 46.0
3	5	node Right	16	27.0	-5.3	109.3 F (65)			46.0	3	21.0	1.000	1.000	32.2 < 46.0
4	6	node Left	16	26.3	-6.6	92.6 F (65)			46.0	3	21.0	1.000	1.000	33.0 < 46.0
4	6	node Right	16	26.3	-6.6	92.6 F (65)			46.0	3	21.0	1.000	1.000	33.0 < 46.0
5	7	node Left	10	31.7	-10.6	76.8 F (65)			46.0	3	21.0	1.000	1.000	42.3 < 46.0
5	7	node Right	10	26.5	-8.9	64.2 F (65)			46.0	3	21.0	1.000	1.000	35.4 < 46.0
5	8	node Left	10	22.3	-10.6	5.7 F (65)			46.0	3	21.0	1.000	1.000	32.9 < 46.0
5	8	node Right	10	22.3	-10.6	5.7 F (65)			46.0	3	21.0	1.000	1.000	32.9 < 46.0
6	9	node Left	15	12.6	-9.6	-55.8 F (65)			46.0	3	21.0	1.300	1.000	22.2 < 59.8
6	9	node Right	15	12.7	-9.8	-56.4 F (65)			46.0	3	21.0	1.300	1.000	22.5 < 59.8
7	10	node Left	29	4.6	-7.8	-84.8 F (65)			46.0	3	21.0	1.300	0.964	12.4 < 57.6
7	10	node Right	29	4.6	-7.8	-84.8 F (65)			46.0	3	21.0	1.300	0.964	12.4 < 57.6
7	11	node Left	29	2.3	-10.2	-144.4 F (65)			46.0	3	21.0	1.300	0.964	12.6 < 57.6
7	11	node Right	29	2.3	-10.2	-144.4 F (65)			46.0	3	21.0	1.300	0.964	12.6 < 57.6
8	12	node Left	22	5.8	-7.8	-98.8 F (65)			46.0	3	21.0	1.300	1.000	13.5 < 59.8
8	12	node Right	22	5.8	-7.8	-98.8 F (65)			46.0	3	21.0	1.300	1.000	13.5 < 59.8
9	13	node Left	12	14.1	-8.8	-51.6 F (65)			46.0	3	21.0	1.300	1.000	22.9 < 59.8
9	13	node Right	12	13.9	-8.6	-50.9 F (65)			46.0	3	21.0	1.300	1.000	22.6 < 59.8
10	14	node Left	12	18.6	-7.4	19.0 F (65)			46.0	3	21.0	1.000	1.000	26.0 < 46.0
10	14	node Right	12	18.6	-7.4	19.0 F (65)			46.0	3	21.0	1.000	1.000	26.0 < 46.0
10	15	node Left	12	27.8	-7.7	84.6 F (65)			46.0	3	21.0	1.000	1.000	35.4 < 46.0
10	15	node Right	12	27.8	-7.7	84.6 F (65)			46.0	3	21.0	1.000	1.000	35.5 < 46.0
11	16	node Left	18	24.2	-4.9	95.0 F (65)			46.0	3	21.0	1.000	1.000	29.1 < 46.0
11	16	node Right	18	24.2	-4.8	95.0 F (65)			46.0	3	21.0	1.000	1.000	29.0 < 46.0
12	17	node Left	18	25.1	-3.8	104.6 F (65)			46.0	3	21.0	1.000	1.000	29.0 < 46.0
12	17	node Right	18	25.1	-3.8	104.6 F (65)			46.0	3	21.0	1.000	1.000	29.0 < 46.0
13	18	node Left	18	24.2	-5.0	94.7 F (65)			46.0	3	21.0	1.000	1.000	29.3 < 46.0
13	18	node Right	18	24.2	-5.0	94.7 F (65)			46.0	3	21.0	1.000	1.000	29.3 < 46.0
14	19	node Left	12	27.8	-7.8	82.7 F (65)			46.0	3	21.0	1.000	1.000	35.6 < 46.0
14	19	node Right	12	27.7	-7.8	82.7 F (65)			46.0	3	21.0	1.000	1.000	35.5 < 46.0
14	20	node Left	12	18.7	-7.6	16.3 F (65)			46.0	3	21.0	1.000	1.000	26.3 < 46.0
14	20	node Right	12	18.6	-7.7	16.3 F (65)			46.0	3	21.0	1.000	1.000	26.3 < 46.0
15	21	node Left	12	14.0	-9.2	-55.2 F (65)			46.0	3	21.0	1.300	1.000	23.2 < 59.8
15	21	node Right	12	14.2	-9.3	-56.0 F (65)			46.0	3	21.0	1.300	1.000	23.4 < 59.8
16	22	node Left	24	5.6	-7.9	-98.1 F (65)			46.0	3	21.0	1.300	1.000	13.5 < 59.8
16	22	node Right	24	5.5	-7.9	-98.1 F (65)			46.0	3	21.0	1.300	1.000	13.4 < 59.8
17	23	node Left	31	2.0	-9.6	-142.4 F (65)			46.0	3	21.0	1.300	0.948	11.6 < 56.7
17	23	node Right	31	1.9	-9.7	-142.3 F (65)			46.0	3	21.0	1.300	0.948	11.6 < 56.7
17	24	node Left	31	4.5	-7.5	-85.5 F (65)			46.0	3	21.0	1.300	0.948	12.0 < 56.7
17	24	node Right	31	4.5	-7.6	-85.4 F (65)			46.0	3	21.0	1.300	0.948	12.1 < 56.7
18	25	node Left	16	12.3	-9.7	-59.6 F (65)			46.0	3	21.0	1.300	1.000	22.0 < 59.8
18	25	node Right	16	12.2	-9.6	-59.0 F (65)			46.0	3	21.0	1.300	1.000	21.8 < 59.8

19	26 node Left	10	22.7	-11.4	2.0	F (65)	46.0	3	21.0	1.000	1.000	34.1 < 46.0
19	26 node Right	10	22.8	-11.3	2.0	F (65)	46.0	3	21.0	1.000	1.000	34.1 < 46.0
19	27 node Left	10	27.4	-9.7	64.9	F (65)	46.0	3	21.0	1.000	1.000	37.0 < 46.0
19	27 node Right	10	32.7	-11.5	77.6	F (65)	46.0	3	21.0	1.000	1.000	44.2 < 46.0
20	28 node Left	18	25.5	-6.7	89.2	F (65)	46.0	3	21.0	1.000	1.000	32.2 < 46.0
20	28 node Right	18	25.5	-6.7	89.2	F (65)	46.0	3	21.0	1.000	1.000	32.2 < 46.0
21	29 node Left	18	26.2	-5.4	106.8	F (65)	46.0	3	21.0	1.000	1.000	31.7 < 46.0
21	29 node Right	18	26.2	-5.4	106.8	F (65)	46.0	3	21.0	1.000	1.000	31.7 < 46.0
21	30 node Left	18	25.0	-4.2	106.9	F (65)	46.0	3	21.0	1.000	1.000	29.2 < 46.0
21	30 node Right	18	25.0	-4.2	106.9	F (65)	46.0	3	21.0	1.000	1.000	29.2 < 46.0
22	31 node Left	18	21.4	-2.9	89.5	F (65)	46.0	3	21.0	1.000	1.000	24.2 < 46.0
22	31 node Right	18	21.3	-2.9	89.5	F (65)	46.0	3	21.0	1.000	1.000	24.2 < 46.0
23	32 node Left	10	20.1	-2.2	77.4	F (65)	46.0	3	21.0	1.000	1.000	22.2 < 46.0
23	32 node Right	10	20.1	-2.1	77.3	F (65)	46.0	3	21.0	1.000	1.000	22.2 < 46.0
23	33 node Left	10	0.1	0.0	0.0	F (65)	46.0	3	21.0	1.000	1.000	0.1 < 46.0

STEEL-BOX G2

node WEB-U-1 (Web Upper edge) WEB - 1

Stress

range

node number	node number	Web	height (mm)	t	σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	Cycle	D
							(N/mm ²)								(N/mm ²)	
1	1	node Right	2436	12	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
1	2	node Left	2433	12	0	1.5	-17.0	-62.3	E(80)	62.0	3	29.0	1.300	1.000	18.5	< 80.6
1	2	node Right	2433	12	0	1.5	-17.0	-62.3	E(80)	62.0	3	29.0	1.300	1.000	18.5	< 80.6
2	3	node Left	2430	14	0	2.6	-20.6	-85.1	E(80)	62.0	3	29.0	1.300	1.000	23.2	< 80.6
2	3	node Right	2430	14	0	2.6	-20.6	-85.1	E(80)	62.0	3	29.0	1.300	1.000	23.2	< 80.6
3	4	node Left	2426	14	0	3.8	-24.1	-102.5	E(80)	62.0	3	29.0	1.300	1.000	27.8	< 80.6
3	4	node Right	2426	14	0	3.8	-24.1	-102.5	E(80)	62.0	3	29.0	1.300	1.000	27.8	< 80.6
3	5	node Left	2423	14	0	5.0	-25.4	-103.0	E(80)	62.0	3	29.0	1.300	1.000	30.3	< 80.6
3	5	node Right	2423	14	0	5.0	-25.4	-103.0	E(80)	62.0	3	29.0	1.300	1.000	30.3	< 80.6
4	6	node Left	2418	14	0	6.2	-24.7	-86.9	E(80)	62.0	3	29.0	1.300	1.000	31.0	< 80.6
4	6	node Right	2418	14	0	6.2	-24.7	-86.9	E(80)	62.0	3	29.0	1.300	1.000	31.0	< 80.6
5	7	node Left	2412	12	0	8.8	-26.4	-63.9	E(80)	62.0	3	29.0	1.300	1.000	35.2	< 80.6
5	7	node Right	2412	12	0	8.6	-25.7	-62.1	E(80)	62.0	3	29.0	1.300	1.000	34.2	< 80.6
5	8	node Left	2406	12	0	10.2	-21.4	-5.5	E(80)	62.0	3	29.0	1.194	1.000	31.6	< 74.0
5	8	node Right	2406	12	0	10.2	-21.4	-5.5	E(80)	62.0	3	29.0	1.194	1.000	31.6	< 74.0
6	9	node Left	2400	20	0	8.3	-11.0	48.5	E(80)	62.0	3	29.0	1.000	1.000	19.3	< 62.0
6	9	node Right	2400	20	0	9.2	-12.2	53.8	E(80)	62.0	3	29.0	1.000	1.000	21.4	< 62.0
7	10	node Left	2394	36	0	7.3	-4.3	79.1	E(80)	62.0	3	29.0	1.000	0.913	11.6	< 56.6
7	10	node Right	2394	36	0	7.3	-4.3	79.1	E(80)	62.0	3	29.0	1.000	0.913	11.6	< 56.6
7	11	node Left	2388	36	0	9.5	-2.2	134.4	E(80)	62.0	3	29.0	1.000	0.913	11.7	< 56.6
7	11	node Right	2388	36	0	9.5	-2.2	134.4	E(80)	62.0	3	29.0	1.000	0.913	11.7	< 56.6
8	12	node Left	2382	34	0	6.3	-4.7	80.8	E(80)	62.0	3	29.0	1.000	0.926	11.0	< 57.4
8	12	node Right	2382	34	0	6.3	-4.7	80.8	E(80)	62.0	3	29.0	1.000	0.926	11.0	< 57.4
9	13	node Left	2375	17	0	8.2	-13.2	48.2	E(80)	62.0	3	29.0	1.000	1.000	21.4	< 62.0
9	13	node Right	2375	17	0	7.3	-11.8	42.9	E(80)	62.0	3	29.0	1.000	1.000	19.0	< 62.0
10	14	node Left	2368	12	0	7.3	-18.6	-18.8	E(80)	62.0	3	29.0	1.300	1.000	25.8	< 80.6
10	14	node Right	2368	12	0	7.3	-18.6	-18.8	E(80)	62.0	3	29.0	1.300	1.000	25.8	< 80.6
10	15	node Left	2360	12	0	6.3	-22.8	-69.4	E(80)	62.0	3	29.0	1.300	1.000	29.1	< 80.6
10	15	node Right	2360	12	0	6.2	-22.8	-69.4	E(80)	62.0	3	29.0	1.300	1.000	29.0	< 80.6
11	16	node Left	2353	14	0	4.4	-21.9	-85.9	E(80)	62.0	3	29.0	1.300	1.000	26.3	< 80.6
11	16	node Right	2353	14	0	4.4	-21.9	-85.9	E(80)	62.0	3	29.0	1.300	1.000	26.3	< 80.6
12	17	node Left	2346	14	0	3.4	-22.6	-93.9	E(80)	62.0	3	29.0	1.300	1.000	26.0	< 80.6
12	17	node Right	2346	14	0	3.4	-22.6	-93.9	E(80)	62.0	3	29.0	1.300	1.000	26.0	< 80.6
13	18	node Left	2338	14	0	4.4	-21.7	-84.4	E(80)	62.0	3	29.0	1.300	1.000	26.1	< 80.6
13	18	node Right	2338	14	0	4.4	-21.7	-84.4	E(80)	62.0	3	29.0	1.300	1.000	26.1	< 80.6
14	19	node Left	2334	12	0	6.1	-21.5	-64.1	E(80)	62.0	3	29.0	1.300	1.000	27.6	< 80.6
14	19	node Right	2334	12	0	6.1	-21.4	-64.1	E(80)	62.0	3	29.0	1.300	1.000	27.5	< 80.6
14	20	node Left	2334	12	0	7.2	-17.4	-15.3	E(80)	62.0	3	29.0	1.300	1.000	24.6	< 80.6
14	20	node Right	2334	12	0	7.1	-17.4	-15.2	E(80)	62.0	3	29.0	1.300	1.000	24.6	< 80.6
15	21	node Left	2334	18	0	7.2	-11.0	43.6	E(80)	62.0	3	29.0	1.000	1.000	18.2	< 62.0
15	21	node Right	2334	18	0	8.2	-12.3	48.8	E(80)	62.0	3	29.0	1.000	1.000	20.5	< 62.0
16	22	node Left	2334	36	0	6.2	-4.3	76.8	E(80)	62.0	3	29.0	1.000	0.913	10.6	< 56.6
16	22	node Right	2334	36	0	6.2	-4.4	76.9	E(80)	62.0	3	29.0	1.000	0.913	10.6	< 56.6
17	23	node Left	2334	39	0	8.4	-1.7	123.8	E(80)	62.0	3	29.0	1.000	0.895	10.1	< 55.5
17	23	node Right	2334	39	0	8.4	-1.7	123.8	E(80)	62.0	3	29.0	1.000	0.895	10.1	< 55.5
17	24	node Left	2334	39	0	6.6	-3.8	74.1	E(80)	62.0	3	29.0	1.000	0.895	10.4	< 55.5
17	24	node Right	2334	39	0	6.6	-3.8	74.0	E(80)	62.0	3	29.0	1.000	0.895	10.5	< 55.5
18	25	node Left	2334	22	0	8.5	-10.8	52.1	E(80)	62.0	3	29.0	1.000	1.000	19.3	< 62.0
18	25	node Right	2334	22	0	7.7	-9.8	47.1	E(80)	62.0	3	29.0	1.000	1.000	17.4	< 62.0
19	26	node Left	2334	12	0	10.2	-20.5	-1.8	E(80)	62.0	3	29.0	1.116	1.000	30.7	< 69.2

19	26 node Right	2334	12	0	10.2	-20.6	-1.8	E(80)	62.0	3	29.0	1.116	1.000	30.8	<	69.2
19	27 node Left	2334	12	0	8.7	-24.7	-58.6	E(80)	62.0	3	29.0	1.300	1.000	33.4	<	80.6
19	27 node Right	2334	12	0	8.9	-25.4	-59.9	E(80)	62.0	3	29.0	1.300	1.000	34.2	<	80.6
20	28 node Left	2334	15	0	6.1	-23.0	-80.3	E(80)	62.0	3	29.0	1.300	1.000	29.0	<	80.6
20	28 node Right	2334	15	0	6.1	-22.9	-80.4	E(80)	62.0	3	29.0	1.300	1.000	29.0	<	80.6
21	29 node Left	2334	15	0	4.9	-23.7	-96.1	E(80)	62.0	3	29.0	1.300	1.000	28.6	<	80.6
21	29 node Right	2334	15	0	4.9	-23.7	-96.1	E(80)	62.0	3	29.0	1.300	1.000	28.6	<	80.6
21	30 node Left	2334	15	0	3.8	-22.5	-96.3	E(80)	62.0	3	29.0	1.300	1.000	26.2	<	80.6
21	30 node Right	2334	15	0	3.8	-22.5	-96.3	E(80)	62.0	3	29.0	1.300	1.000	26.2	<	80.6
22	31 node Left	2334	15	0	2.6	-19.2	-80.6	E(80)	62.0	3	29.0	1.300	1.000	21.8	<	80.6
22	31 node Right	2334	15	0	2.6	-19.2	-80.5	E(80)	62.0	3	29.0	1.300	1.000	21.8	<	80.6
23	32 node Left	2334	12	0	1.7	-15.5	-59.8	E(80)	62.0	3	29.0	1.300	1.000	17.2	<	80.6
23	32 node Right	2334	12	0	1.6	-15.5	-59.7	E(80)	62.0	3	29.0	1.300	1.000	17.1	<	80.6
23	33 node Left	2334	12	0	0.0	-0.1	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.1	<	80.6

STEEL-BOX G2

node WEB-L-1 (Web Lower edge) WEB - 1

Stress

range

node number	node number	Web	height (mm)	t	σ	tmax	σ	tmin	σ	d	($\Delta \sigma$ f)	$\Delta \sigma$ ce m	$\Delta \sigma$ ve CR	Ct	$\Delta \sigma$ max CR • Ct	Cycle	D
				Grade				$\Delta \sigma$ ce • Cycle									
				(N/mm ²)				(N/mm ²)									
1	1	node Right	2436	12	0	0.0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
1	2	node Left	2433	12	0	19.1	-1.8	70.5	E(80)	62.0	3	29.0	1.000	1.000	21.0	< 62.0	
1	2	node Right	2433	12	0	19.1	-1.8	70.5	E(80)	62.0	3	29.0	1.000	1.000	20.9	< 62.0	
2	3	node Left	2430	16	0	21.5	-2.6	88.5	E(80)	62.0	3	29.0	1.000	1.000	24.2	< 62.0	
2	3	node Right	2430	16	0	21.5	-2.6	88.5	E(80)	62.0	3	29.0	1.000	1.000	24.2	< 62.0	
3	4	node Left	2426	16	0	25.2	-3.9	106.8	E(80)	62.0	3	29.0	1.000	1.000	29.1	< 62.0	
3	4	node Right	2426	16	0	25.2	-3.9	106.8	E(80)	62.0	3	29.0	1.000	1.000	29.1	< 62.0	
3	5	node Left	2423	16	0	26.6	-5.2	107.7	E(80)	62.0	3	29.0	1.000	1.000	31.8	< 62.0	
3	5	node Right	2423	16	0	26.6	-5.2	107.7	E(80)	62.0	3	29.0	1.000	1.000	31.8	< 62.0	
4	6	node Left	2418	16	0	25.9	-6.6	91.3	E(80)	62.0	3	29.0	1.000	1.000	32.5	< 62.0	
4	6	node Right	2418	16	0	25.9	-6.6	91.3	E(80)	62.0	3	29.0	1.000	1.000	32.5	< 62.0	
5	7	node Left	2412	12	0	31.5	-10.5	76.1	E(80)	62.0	3	29.0	1.000	1.000	42.0	< 62.0	
5	7	node Right	2412	12	0	26.3	-8.8	63.7	E(80)	62.0	3	29.0	1.000	1.000	35.1	< 62.0	
5	8	node Left	2406	12	0	22.1	-10.5	5.7	E(80)	62.0	3	29.0	1.000	1.000	32.6	< 62.0	
5	8	node Right	2406	12	0	22.1	-10.5	5.7	E(80)	62.0	3	29.0	1.000	1.000	32.6	< 62.0	
6	9	node Left	2400	15	0	12.5	-9.4	-55.2	E(80)	62.0	3	29.0	1.300	1.000	21.9	< 80.6	
6	9	node Right	2400	15	0	12.6	-9.5	-55.8	E(80)	62.0	3	29.0	1.300	1.000	22.2	< 80.6	
7	10	node Left	2394	29	0	4.6	-7.5	-82.9	E(80)	62.0	3	29.0	1.300	0.964	12.1	< 77.7	
7	10	node Right	2394	29	0	4.6	-7.5	-82.9	E(80)	62.0	3	29.0	1.300	0.964	12.1	< 77.7	
7	11	node Left	2388	29	0	2.2	-10.0	-141.0	E(80)	62.0	3	29.0	1.300	0.964	12.2	< 77.7	
7	11	node Right	2388	29	0	2.2	-9.9	-141.0	E(80)	62.0	3	29.0	1.300	0.964	12.2	< 77.7	
8	12	node Left	2382	22	0	5.7	-7.6	-97.1	E(80)	62.0	3	29.0	1.300	1.000	13.3	< 80.6	
8	12	node Right	2382	22	0	5.7	-7.6	-97.1	E(80)	62.0	3	29.0	1.300	1.000	13.3	< 80.6	
9	13	node Left	2375	14	0	14.0	-8.7	-51.1	E(80)	62.0	3	29.0	1.300	1.000	22.7	< 80.6	
9	13	node Right	2375	14	0	13.8	-8.6	-50.4	E(80)	62.0	3	29.0	1.300	1.000	22.3	< 80.6	
10	14	node Left	2368	12	0	18.5	-7.3	18.8	E(80)	62.0	3	29.0	1.000	1.000	25.8	< 62.0	
10	14	node Right	2368	12	0	18.5	-7.3	18.8	E(80)	62.0	3	29.0	1.000	1.000	25.8	< 62.0	
10	15	node Left	2360	12	0	27.5	-7.6	83.8	E(80)	62.0	3	29.0	1.000	1.000	35.1	< 62.0	
10	15	node Right	2360	12	0	27.5	-7.6	83.8	E(80)	62.0	3	29.0	1.000	1.000	35.1	< 62.0	
11	16	node Left	2353	18	0	23.9	-4.8	93.6	E(80)	62.0	3	29.0	1.000	1.000	28.7	< 62.0	
11	16	node Right	2353	18	0	23.9	-4.7	93.6	E(80)	62.0	3	29.0	1.000	1.000	28.6	< 62.0	
12	17	node Left	2346	18	0	24.7	-3.7	103.0	E(80)	62.0	3	29.0	1.000	1.000	28.4	< 62.0	
12	17	node Right	2346	18	0	24.7	-3.7	103.0	E(80)	62.0	3	29.0	1.000	1.000	28.4	< 62.0	
13	18	node Left	2338	18	0	23.9	-5.0	93.3	E(80)	62.0	3	29.0	1.000	1.000	28.9	< 62.0	
13	18	node Right	2338	18	0	23.9	-4.9	93.2	E(80)	62.0	3	29.0	1.000	1.000	28.8	< 62.0	
14	19	node Left	2334	12	0	27.5	-7.8	81.9	E(80)	62.0	3	29.0	1.000	1.000	35.3	< 62.0	
14	19	node Right	2334	12	0	27.4	-7.8	81.9	E(80)	62.0	3	29.0	1.000	1.000	35.2	< 62.0	
14	20	node Left	2334	12	0	18.5	-7.6	16.2	E(80)	62.0	3	29.0	1.000	1.000	26.1	< 62.0	
14	20	node Right	2334	12	0	18.5	-7.5	16.1	E(80)	62.0	3	29.0	1.000	1.000	26.0	< 62.0	
15	21	node Left	2334	14	0	13.8	-9.1	-54.7	E(80)	62.0	3	29.0	1.300	1.000	23.0	< 80.6	
15	21	node Right	2334	14	0	14.0	-9.2	-55.4	E(80)	62.0	3	29.0	1.300	1.000	23.2	< 80.6	
16	22	node Left	2334	24	0	5.4	-7.8	-96.2	E(80)	62.0	3	29.0	1.300	1.000	13.3	< 80.6	
16	22	node Right	2334	24	0	5.4	-7.8	-96.3	E(80)	62.0	3	29.0	1.300	1.000	13.2	< 80.6	
17	23	node Left	2334	31	0	1.8	-9.4	-138.7	E(80)	62.0	3	29.0	1.300	0.948	11.3	< 76.4	
17	23	node Right	2334	31	0	1.8	-9.4	-138.7	E(80)	62.0	3	29.0	1.300	0.948	11.3	< 76.4	
17	24	node Left	2334	31	0	4.3	-7.4	-83.3	E(80)	62.0	3	29.0	1.300	0.948	11.7	< 76.4	
17	24	node Right	2334	31	0	4.3	-7.4	-83.3	E(80)	62.0	3	29.0	1.300	0.948	11.7	< 76.4	
18	25	node Left	2334	16	0	12.2	-9.6	-58.8	E(80)	62.0	3	29.0	1.300	1.000	21.8	< 80.6	
18	25	node Right	2334	16	0	12.1	-9.5	-58.2	E(80)	62.0	3	29.0	1.300	1.000	21.6	< 80.6	
19	26	node Left	2334	12	0	22.6	-11.2	1.9	E(80)	62.0	3	29.0	1.000	1.000	33.8	< 62.0	

19	26 node Right	2334	12	0	22.6	-11.2	2.0	E(80)	62.0	3	29.0	1.000	1.000	33.8	<	62.0
19	27 node Left	2334	12	0	27.2	-9.5	64.3	E(80)	62.0	3	29.0	1.000	1.000	36.7	<	62.0
19	27 node Right	2334	12	0	32.5	-11.4	77.0	E(80)	62.0	3	29.0	1.000	1.000	43.9	<	62.0
20	28 node Left	2334	18	0	25.0	-6.6	87.9	E(80)	62.0	3	29.0	1.000	1.000	31.7	<	62.0
20	28 node Right	2334	18	0	25.1	-6.6	87.9	E(80)	62.0	3	29.0	1.000	1.000	31.8	<	62.0
21	29 node Left	2334	18	0	25.8	-5.4	105.2	E(80)	62.0	3	29.0	1.000	1.000	31.2	<	62.0
21	29 node Right	2334	18	0	25.8	-5.4	105.2	E(80)	62.0	3	29.0	1.000	1.000	31.2	<	62.0
21	30 node Left	2334	18	0	24.6	-4.1	105.3	E(80)	62.0	3	29.0	1.000	1.000	28.7	<	62.0
21	30 node Right	2334	18	0	24.6	-4.1	105.3	E(80)	62.0	3	29.0	1.000	1.000	28.7	<	62.0
22	31 node Left	2334	18	0	21.0	-2.8	88.2	E(80)	62.0	3	29.0	1.000	1.000	23.8	<	62.0
22	31 node Right	2334	18	0	21.0	-2.8	88.1	E(80)	62.0	3	29.0	1.000	1.000	23.8	<	62.0
23	32 node Left	2334	12	0	19.9	-2.2	76.8	E(80)	62.0	3	29.0	1.000	1.000	22.1	<	62.0
23	32 node Right	2334	12	0	19.9	-2.1	76.7	E(80)	62.0	3	29.0	1.000	1.000	22.0	<	62.0
23	33 node Left	2334	12	0	0.1	0.0	0.0	E(80)	62.0	3	29.0	1.000	1.000	0.1	<	62.0

STEEL-BOX G2

node HSTIFF-1 (Web H-stiff) WEB - 1

Stress

range																
node	node	Web	Grade		$\Delta \sigma_{ce}$		Cycle									
number	number	height	t	σ_{tmax}	σ_{tmin}	σ_d	($\Delta \sigma_f$)	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR	$\cdot Ct$	D
		(mm)	(N/mm ²)										(N/mm ²)			
1	1 node Right	2436	12	487	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6
1	2 node Left	2433	12	487	0.8	-9.7	-35.7	G(50)	32.0	3	15.0	1.300	1.000	10.6	<	41.6
1	2 node Right	2433	12	487	0.9	-9.7	-35.7	G(50)	32.0	3	15.0	1.300	1.000	10.6	<	41.6
2	3 node Left	2430	12	486	1.5	-12.2	-50.4	G(50)	32.0	3	15.0	1.300	1.000	13.7	<	41.6
2	3 node Right	2430	12	486	1.5	-12.2	-50.4	G(50)	32.0	3	15.0	1.300	1.000	13.7	<	41.6
3	4 node Left	2426	12	485	2.2	-14.2	-60.6	G(50)	32.0	3	15.0	1.300	1.000	16.4	<	41.6
3	4 node Right	2426	12	485	2.2	-14.2	-60.6	G(50)	32.0	3	15.0	1.300	1.000	16.4	<	41.6
3	5 node Left	2423	12	485	2.9	-15.0	-60.9	G(50)	32.0	3	15.0	1.300	1.000	17.9	<	41.6
3	5 node Right	2423	12	485	2.9	-15.0	-60.9	G(50)	32.0	3	15.0	1.300	1.000	17.9	<	41.6
4	6 node Left	2418	12	484	3.7	-14.6	-51.3	G(50)	32.0	3	15.0	1.300	1.000	18.3	<	41.6
4	6 node Right	2418	12	484	3.7	-14.6	-51.3	G(50)	32.0	3	15.0	1.300	1.000	18.3	<	41.6
5	7 node Left	2412	12	482	4.9	-14.8	-35.9	G(50)	32.0	3	15.0	1.300	1.000	19.8	<	41.6
5	7 node Right	2412	12	482	5.1	-15.3	-36.9	G(50)	32.0	3	15.0	1.300	1.000	20.4	<	41.6
5	8 node Left	2406	12	481	6.0	-12.7	-3.3	G(50)	32.0	3	15.0	1.194	1.000	18.8	<	38.2
5	8 node Right	2406	12	481	6.0	-12.7	-3.3	G(50)	32.0	3	15.0	1.194	1.000	18.8	<	38.2
6	9 node Left	2400	14	480	7.8	-5.9	-34.5	G(50)	32.0	3	15.0	1.300	1.000	13.7	<	41.6
6	9 node Right	2400	14	480	7.7	-5.8	-33.9	G(50)	32.0	3	15.0	1.300	1.000	13.5	<	41.6
7	10 node Left	2394	16	479	2.8	-4.6	-50.5	G(50)	32.0	3	15.0	1.300	1.000	7.3	<	41.6
7	10 node Right	2394	16	479	2.8	-4.6	-50.5	G(50)	32.0	3	15.0	1.300	1.000	7.3	<	41.6
7	11 node Left	2388	16	478	1.4	-6.1	-85.9	G(50)	32.0	3	15.0	1.300	1.000	7.5	<	41.6
7	11 node Right	2388	16	478	1.4	-6.0	-85.9	G(50)	32.0	3	15.0	1.300	1.000	7.4	<	41.6
8	12 node Left	2382	16	476	3.6	-4.8	-61.5	G(50)	32.0	3	15.0	1.300	1.000	8.4	<	41.6
8	12 node Right	2382	16	476	3.6	-4.8	-61.5	G(50)	32.0	3	15.0	1.300	1.000	8.4	<	41.6
9	13 node Left	2375	14	475	8.6	-5.3	-31.2	G(50)	32.0	3	15.0	1.300	1.000	13.9	<	41.6
9	13 node Right	2375	14	475	8.7	-5.4	-31.7	G(50)	32.0	3	15.0	1.300	1.000	14.0	<	41.6
10	14 node Left	2368	12	474	4.4	-11.2	-11.3	G(50)	32.0	3	15.0	1.300	1.000	15.5	<	41.6
10	14 node Right	2368	12	474	4.4	-11.2	-11.3	G(50)	32.0	3	15.0	1.300	1.000	15.5	<	41.6
10	15 node Left	2360	12	472	3.5	-12.7	-38.8	G(50)	32.0	3	15.0	1.300	1.000	16.3	<	41.6
10	15 node Right	2360	12	472	3.5	-12.7	-38.8	G(50)	32.0	3	15.0	1.300	1.000	16.2	<	41.6
11	16 node Left	2353	12	471	2.6	-12.8	-50.0	G(50)	32.0	3	15.0	1.300	1.000	15.3	<	41.6
11	16 node Right	2353	12	471	2.6	-12.8	-50.0	G(50)	32.0	3	15.0	1.300	1.000	15.3	<	41.6
12	17 node Left	2346	12	469	2.0	-13.1	-54.5	G(50)	32.0	3	15.0	1.300	1.000	15.1	<	41.6
12	17 node Right	2346	12	469	2.0	-13.1	-54.5	G(50)	32.0	3	15.0	1.300	1.000	15.1	<	41.6
13	18 node Left	2338	12	468	2.5	-12.6	-48.9	G(50)	32.0	3	15.0	1.300	1.000	15.1	<	41.6
13	18 node Right	2338	12	468	2.5	-12.6	-48.9	G(50)	32.0	3	15.0	1.300	1.000	15.1	<	41.6
14	19 node Left	2334	12	467	3.3	-11.7	-34.9	G(50)	32.0	3	15.0	1.300	1.000	15.0	<	41.6
14	19 node Right	2334	12	467	3.3	-11.7	-34.9	G(50)	32.0	3	15.0	1.300	1.000	15.0	<	41.6
14	20 node Left	2334	12	467	4.2	-10.3	-9.0	G(50)	32.0	3	15.0	1.300	1.000	14.5	<	41.6
14	20 node Right	2334	12	467	4.2	-10.3	-8.9	G(50)	32.0	3	15.0	1.300	1.000	14.4	<	41.6
15	21 node Left	2334	14	467	8.9	-5.9	-35.0	G(50)	32.0	3	15.0	1.300	1.000	14.7	<	41.6
15	21 node Right	2334	14	467	8.7	-5.7	-34.6	G(50)	32.0	3	15.0	1.300	1.000	14.5	<	41.6
16	22 node Left	2334	16	467	3.5	-5.0	-61.6	G(50)	32.0	3	15.0	1.300	1.000	8.5	<	41.6
16	22 node Right	2334	16	467	3.5	-5.0	-61.7	G(50)	32.0	3	15.0	1.300	1.000	8.4	<	41.6
17	23 node Left	2334	16	467	1.1	-5.9	-86.2	G(50)	32.0	3	15.0	1.300	1.000	7.0	<	41.6
17	23 node Right	2334	16	467	1.1	-5.9	-86.2	G(50)	32.0	3	15.0	1.300	1.000	7.0	<	41.6
17	24 node Left	2334	16	467	2.7	-4.6	-51.8	G(50)	32.0	3	15.0	1.300	1.000	7.3	<	41.6
17	24 node Right	2334	16	467	2.7	-4.6	-51.8	G(50)	32.0	3	15.0	1.300	1.000	7.2	<	41.6
18	25 node Left	2334	14	467	7.6	-6.0	-36.6	G(50)	32.0	3	15.0	1.300	1.000	13.6	<	41.6
18	25 node Right	2334	14	467	7.7	-6.1	-37.1	G(50)	32.0	3	15.0	1.300	1.000	13.8	<	41.6
19	26 node Left	2334	12	467	6.0	-11.9	-1.1	G(50)	32.0	3	15.0	1.116	1.000	17.8	<	35.7

19	26 node Right	2334 12 467	6.0 -11.9 -1.0 G(50)	32.0 3	15.0 1.116 1.000	17.9< 35.7
19	27 node Left	2334 12 467	5.1 -14.3 -34.0 G(50)	32.0 3	15.0 1.300 1.000	19.4< 41.6
19	27 node Right	2334 12 467	4.8 -13.8 -32.5 G(50)	32.0 3	15.0 1.300 1.000	18.6< 41.6
20	28 node Left	2334 12 467	3.5 -13.4 -46.7 G(50)	32.0 3	15.0 1.300 1.000	16.9< 41.6
20	28 node Right	2334 12 467	3.5 -13.3 -46.7 G(50)	32.0 3	15.0 1.300 1.000	16.8< 41.6
21	29 node Left	2334 12 467	2.8 -13.8 -55.8 G(50)	32.0 3	15.0 1.300 1.000	16.6< 41.6
21	29 node Right	2334 12 467	2.8 -13.8 -55.8 G(50)	32.0 3	15.0 1.300 1.000	16.6< 41.6
21	30 node Left	2334 12 467	2.2 -13.1 -56.0 G(50)	32.0 3	15.0 1.300 1.000	15.2< 41.6
21	30 node Right	2334 12 467	2.2 -13.1 -56.0 G(50)	32.0 3	15.0 1.300 1.000	15.2< 41.6
22	31 node Left	2334 12 467	1.5 -11.2 -46.8 G(50)	32.0 3	15.0 1.300 1.000	12.7< 41.6
22	31 node Right	2334 12 467	1.5 -11.2 -46.8 G(50)	32.0 3	15.0 1.300 1.000	12.6< 41.6
23	32 node Left	2334 12 467	0.9 -8.4 -32.5 G(50)	32.0 3	15.0 1.300 1.000	9.3< 41.6
23	32 node Right	2334 12 467	0.9 -8.4 -32.4 G(50)	32.0 3	15.0 1.300 1.000	9.3< 41.6
23	33 node Left	2334 12 467	0.0 -0.0 0.0 G(50)	32.0 3	15.0 1.300 1.000	0.0< 41.6

STEEL-BOX G2

node POINT-U-1 (Web Upper) WEB - 1

Stress

range		node node		Web	Grade				$\Delta \sigma_{ce} \cdot \text{Cycle}$						
number	number	height	t	σ_{tmax}	σ_{tmin}	σ_d	($\Delta \sigma_f$)	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR · Ct	D
		(mm)	(N/mm ²)				(N/mm ²)								
1	1 node Right	2436	12	900	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
1	2 node Left	2433	12	900	0.3	-3.6	-13.2	G(50)	32.0	3	15.0	1.300	1.000	3.9	< 41.6
1	2 node Right	2433	12	900	0.3	-3.6	-13.2	G(50)	32.0	3	15.0	1.300	1.000	3.9	< 41.6
2	3 node Left	2430	12	900	0.6	-5.0	-20.8	G(50)	32.0	3	15.0	1.300	1.000	5.7	< 41.6
2	3 node Right	2430	12	900	0.6	-5.0	-20.8	G(50)	32.0	3	15.0	1.300	1.000	5.7	< 41.6
3	4 node Left	2426	12	900	0.9	-5.8	-24.9	G(50)	32.0	3	15.0	1.300	1.000	6.7	< 41.6
3	4 node Right	2426	12	900	0.9	-5.8	-24.9	G(50)	32.0	3	15.0	1.300	1.000	6.7	< 41.6
3	5 node Left	2423	12	900	1.2	-6.1	-24.7	G(50)	32.0	3	15.0	1.300	1.000	7.3	< 41.6
3	5 node Right	2423	12	900	1.2	-6.1	-24.7	G(50)	32.0	3	15.0	1.300	1.000	7.3	< 41.6
4	6 node Left	2418	12	900	1.5	-5.9	-20.6	G(50)	32.0	3	15.0	1.300	1.000	7.3	< 41.6
4	6 node Right	2418	12	900	1.5	-5.9	-20.6	G(50)	32.0	3	15.0	1.300	1.000	7.3	< 41.6
5	7 node Left	2412	12	900	1.6	-4.8	-11.7	G(50)	32.0	3	15.0	1.300	1.000	6.4	< 41.6
5	7 node Right	2412	12	900	2.1	-6.3	-15.2	G(50)	32.0	3	15.0	1.300	1.000	8.4	< 41.6
5	8 node Left	2406	12	900	2.4	-5.2	-1.3	G(50)	32.0	3	15.0	1.194	1.000	7.6	< 38.2
5	8 node Right	2406	12	900	2.4	-5.2	-1.3	G(50)	32.0	3	15.0	1.194	1.000	7.6	< 38.2
6	9 node Left	2400	14	900	1.7	-2.2	9.6	G(50)	32.0	3	15.0	1.000	1.000	3.8	< 32.0
6	9 node Right	2400	14	900	2.2	-2.9	12.7	G(50)	32.0	3	15.0	1.000	1.000	5.0	< 32.0
7	10 node Left	2394	16	900	1.7	-1.0	18.2	G(50)	32.0	3	15.0	1.000	1.000	2.7	< 32.0
7	10 node Right	2394	16	900	1.7	-1.0	18.2	G(50)	32.0	3	15.0	1.000	1.000	2.7	< 32.0
7	11 node Left	2388	16	900	2.2	-0.5	30.6	G(50)	32.0	3	15.0	1.000	1.000	2.7	< 32.0
7	11 node Right	2388	16	900	2.2	-0.5	30.6	G(50)	32.0	3	15.0	1.000	1.000	2.7	< 32.0
8	12 node Left	2382	16	900	1.1	-0.8	13.6	G(50)	32.0	3	15.0	1.000	1.000	1.8	< 32.0
8	12 node Right	2382	16	900	1.1	-0.8	13.6	G(50)	32.0	3	15.0	1.000	1.000	1.8	< 32.0
9	13 node Left	2375	14	900	1.8	-2.9	10.6	G(50)	32.0	3	15.0	1.000	1.000	4.7	< 32.0
9	13 node Right	2375	14	900	1.3	-2.1	7.5	G(50)	32.0	3	15.0	1.000	1.000	3.4	< 32.0
10	14 node Left	2368	12	900	1.7	-4.5	-4.5	G(50)	32.0	3	15.0	1.300	1.000	6.2	< 41.6
10	14 node Right	2368	12	900	1.7	-4.5	-4.5	G(50)	32.0	3	15.0	1.300	1.000	6.2	< 41.6
10	15 node Left	2360	12	900	1.0	-3.6	-11.0	G(50)	32.0	3	15.0	1.300	1.000	4.6	< 41.6
10	15 node Right	2360	12	900	1.0	-3.6	-11.0	G(50)	32.0	3	15.0	1.300	1.000	4.6	< 41.6
11	16 node Left	2353	12	900	0.9	-4.4	-17.2	G(50)	32.0	3	15.0	1.300	1.000	5.3	< 41.6
11	16 node Right	2353	12	900	0.9	-4.4	-17.2	G(50)	32.0	3	15.0	1.300	1.000	5.3	< 41.6
12	17 node Left	2346	12	900	0.7	-4.4	-18.4	G(50)	32.0	3	15.0	1.300	1.000	5.1	< 41.6
12	17 node Right	2346	12	900	0.7	-4.4	-18.4	G(50)	32.0	3	15.0	1.300	1.000	5.1	< 41.6
13	18 node Left	2338	12	900	0.8	-4.1	-16.0	G(50)	32.0	3	15.0	1.300	1.000	4.9	< 41.6
13	18 node Right	2338	12	900	0.8	-4.1	-16.0	G(50)	32.0	3	15.0	1.300	1.000	5.0	< 41.6
14	19 node Left	2334	12	900	0.7	-2.6	-7.8	G(50)	32.0	3	15.0	1.300	1.000	3.4	< 41.6
14	19 node Right	2334	12	900	0.7	-2.6	-7.8	G(50)	32.0	3	15.0	1.300	1.000	3.3	< 41.6
14	20 node Left	2334	12	900	1.5	-3.6	-3.2	G(50)	32.0	3	15.0	1.300	1.000	5.1	< 41.6
14	20 node Right	2334	12	900	1.5	-3.6	-3.1	G(50)	32.0	3	15.0	1.300	1.000	5.1	< 41.6
15	21 node Left	2334	14	900	0.9	-1.4	5.7	G(50)	32.0	3	15.0	1.000	1.000	2.4	< 32.0
15	21 node Right	2334	14	900	1.5	-2.2	8.6	G(50)	32.0	3	15.0	1.000	1.000	3.6	< 32.0
16	22 node Left	2334	16	900	0.8	-0.6	10.1	G(50)	32.0	3	15.0	1.000	1.000	1.4	< 32.0
16	22 node Right	2334	16	900	0.8	-0.6	10.1	G(50)	32.0	3	15.0	1.000	1.000	1.4	< 32.0
17	23 node Left	2334	16	900	1.5	-0.3	22.6	G(50)	32.0	3	15.0	1.000	1.000	1.8	< 32.0
17	23 node Right	2334	16	900	1.5	-0.3	22.6	G(50)	32.0	3	15.0	1.000	1.000	1.8	< 32.0
17	24 node Left	2334	16	900	1.2	-0.7	13.4	G(50)	32.0	3	15.0	1.000	1.000	1.9	< 32.0
17	24 node Right	2334	16	900	1.2	-0.7	13.3	G(50)	32.0	3	15.0	1.000	1.000	1.9	< 32.0
18	25 node Left	2334	14	900	1.5	-1.9	9.3	G(50)	32.0	3	15.0	1.000	1.000	3.5	< 32.0
18	25 node Right	2334	14	900	1.0	-1.3	6.5	G(50)	32.0	3	15.0	1.000	1.000	2.4	< 32.0
19	26 node Left	2334	12	900	2.0	-3.9	-0.4	G(50)	32.0	3	15.0	1.117	1.000	5.9	< 35.7

19	26 node Right	2334 12 900	2.0	-3.9	-0.3	G(50)	32.0 3	15.0	1.115	1.000	5.9<	35.7
19	27 node Left	2334 12 900	1.7	-4.7	-11.2	G(50)	32.0 3	15.0	1.300	1.000	6.4<	41.6
19	27 node Right	2334 12 900	1.0	-3.1	-7.1	G(50)	32.0 3	15.0	1.300	1.000	4.1<	41.6
20	28 node Left	2334 12 900	1.2	-4.5	-15.4	G(50)	32.0 3	15.0	1.300	1.000	5.6<	41.6
20	28 node Right	2334 12 900	1.2	-4.4	-15.5	G(50)	32.0 3	15.0	1.300	1.000	5.5<	41.6
21	29 node Left	2334 12 900	0.9	-4.6	-18.5	G(50)	32.0 3	15.0	1.300	1.000	5.5<	41.6
21	29 node Right	2334 12 900	0.9	-4.6	-18.5	G(50)	32.0 3	15.0	1.300	1.000	5.5<	41.6
21	30 node Left	2334 12 900	0.7	-4.3	-18.6	G(50)	32.0 3	15.0	1.300	1.000	5.0<	41.6
21	30 node Right	2334 12 900	0.7	-4.3	-18.6	G(50)	32.0 3	15.0	1.300	1.000	5.0<	41.6
22	31 node Left	2334 12 900	0.5	-3.7	-15.5	G(50)	32.0 3	15.0	1.300	1.000	4.2<	41.6
22	31 node Right	2334 12 900	0.5	-3.7	-15.5	G(50)	32.0 3	15.0	1.300	1.000	4.2<	41.6
23	32 node Left	2334 12 900	0.2	-1.9	-7.1	G(50)	32.0 3	15.0	1.300	1.000	2.1<	41.6
23	32 node Right	2334 12 900	0.2	-1.9	-7.1	G(50)	32.0 3	15.0	1.300	1.000	2.0<	41.6
23	33 node Left	2334 12 900	0.0	-0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0<	41.6

STEEL-BOX G2

node POINT-L-1 (Web) WEB - 1

Stress

range	node	node	Web	Grade	$\Delta \sigma_{ce}$	Cycle		
number	number	number	height (mm)	t σ_{tmax} σ_{tmin} σ_d ($\Delta \sigma_f$)	$\Delta \sigma_{ce}$ m	$\Delta \sigma_{ve}$ CR	Ct	$\Delta \sigma_{max}$ CR \cdot Ct D
				(N/mm ²)				(N/mm ²)
1	1	node Right	2436	12 500 0.0 0.0 0.0 G(50)	32.0 3	15.0 1.300	1.000	0.0 < 41.6
1	2	node Left	2433	12 500 11.7 -1.1 43.2 G(50)	32.0 3	15.0 1.000	1.000	12.9 < 32.0
1	2	node Right	2433	12 500 11.7 -1.1 43.2 G(50)	32.0 3	15.0 1.000	1.000	12.8 < 32.0
2	3	node Left	2430	12 500 12.8 -1.6 52.8 G(50)	32.0 3	15.0 1.000	1.000	14.4 < 32.0
2	3	node Right	2430	12 500 12.8 -1.6 52.8 G(50)	32.0 3	15.0 1.000	1.000	14.4 < 32.0
3	4	node Left	2426	12 500 15.0 -2.3 63.7 G(50)	32.0 3	15.0 1.000	1.000	17.4 < 32.0
3	4	node Right	2426	12 500 15.0 -2.3 63.7 G(50)	32.0 3	15.0 1.000	1.000	17.4 < 32.0
3	5	node Left	2423	12 500 15.8 -3.1 64.2 G(50)	32.0 3	15.0 1.000	1.000	18.9 < 32.0
3	5	node Right	2423	12 500 15.8 -3.1 64.2 G(50)	32.0 3	15.0 1.000	1.000	18.9 < 32.0
4	6	node Left	2418	12 500 15.4 -3.9 54.4 G(50)	32.0 3	15.0 1.000	1.000	19.4 < 32.0
4	6	node Right	2418	12 500 15.4 -3.9 54.4 G(50)	32.0 3	15.0 1.000	1.000	19.4 < 32.0
5	7	node Left	2412	12 500 19.5 -6.5 47.1 G(50)	32.0 3	15.0 1.000	1.000	26.0 < 32.0
5	7	node Right	2412	12 500 15.5 -5.2 37.6 G(50)	32.0 3	15.0 1.000	1.000	20.7 < 32.0
5	8	node Left	2406	12 500 13.0 -6.2 3.4 G(50)	32.0 3	15.0 1.000	1.000	19.2 < 32.0
5	8	node Right	2406	12 500 13.0 -6.2 3.4 G(50)	32.0 3	15.0 1.000	1.000	19.2 < 32.0
6	9	node Left	2400	14 500 7.6 -5.7 -33.6 G(50)	32.0 3	15.0 1.300	1.000	13.3 < 41.6
6	9	node Right	2400	14 500 7.5 -5.6 -33.0 G(50)	32.0 3	15.0 1.300	1.000	13.1 < 41.6
7	10	node Left	2394	16 500 2.7 -4.4 -49.1 G(50)	32.0 3	15.0 1.300	1.000	7.1 < 41.6
7	10	node Right	2394	16 500 2.7 -4.4 -49.1 G(50)	32.0 3	15.0 1.300	1.000	7.1 < 41.6
7	11	node Left	2388	16 500 1.3 -5.9 -83.3 G(50)	32.0 3	15.0 1.300	1.000	7.2 < 41.6
7	11	node Right	2388	16 500 1.3 -5.8 -83.3 G(50)	32.0 3	15.0 1.300	1.000	7.2 < 41.6
8	12	node Left	2382	16 500 3.5 -4.7 -59.8 G(50)	32.0 3	15.0 1.300	1.000	8.2 < 41.6
8	12	node Right	2382	16 500 3.5 -4.7 -59.8 G(50)	32.0 3	15.0 1.300	1.000	8.2 < 41.6
9	13	node Left	2375	14 500 8.3 -5.2 -30.2 G(50)	32.0 3	15.0 1.300	1.000	13.4 < 41.6
9	13	node Right	2375	14 500 8.4 -5.2 -30.8 G(50)	32.0 3	15.0 1.300	1.000	13.6 < 41.6
10	14	node Left	2368	12 500 10.7 -4.2 10.9 G(50)	32.0 3	15.0 1.000	1.000	14.9 < 32.0
10	14	node Right	2368	12 500 10.7 -4.2 10.9 G(50)	32.0 3	15.0 1.000	1.000	14.9 < 32.0
10	15	node Left	2360	12 500 16.9 -4.7 51.3 G(50)	32.0 3	15.0 1.000	1.000	21.5 < 32.0
10	15	node Right	2360	12 500 16.9 -4.7 51.3 G(50)	32.0 3	15.0 1.000	1.000	21.5 < 32.0
11	16	node Left	2353	12 500 14.2 -2.8 55.5 G(50)	32.0 3	15.0 1.000	1.000	17.0 < 32.0
11	16	node Right	2353	12 500 14.2 -2.8 55.5 G(50)	32.0 3	15.0 1.000	1.000	17.0 < 32.0
12	17	node Left	2346	12 500 14.6 -2.2 61.0 G(50)	32.0 3	15.0 1.000	1.000	16.8 < 32.0
12	17	node Right	2346	12 500 14.6 -2.2 61.0 G(50)	32.0 3	15.0 1.000	1.000	16.8 < 32.0
13	18	node Left	2338	12 500 14.2 -3.0 55.3 G(50)	32.0 3	15.0 1.000	1.000	17.1 < 32.0
13	18	node Right	2338	12 500 14.2 -2.9 55.2 G(50)	32.0 3	15.0 1.000	1.000	17.1 < 32.0
14	19	node Left	2334	12 500 17.0 -4.8 50.6 G(50)	32.0 3	15.0 1.000	1.000	21.8 < 32.0
14	19	node Right	2334	12 500 17.0 -4.8 50.6 G(50)	32.0 3	15.0 1.000	1.000	21.8 < 32.0
14	20	node Left	2334	12 500 10.8 -4.4 9.5 G(50)	32.0 3	15.0 1.000	1.000	15.2 < 32.0
14	20	node Right	2334	12 500 10.8 -4.4 9.4 G(50)	32.0 3	15.0 1.000	1.000	15.2 < 32.0
15	21	node Left	2334	14 500 8.5 -5.6 -33.6 G(50)	32.0 3	15.0 1.300	1.000	14.1 < 41.6
15	21	node Right	2334	14 500 8.4 -5.5 -33.1 G(50)	32.0 3	15.0 1.300	1.000	13.8 < 41.6
16	22	node Left	2334	16 500 3.3 -4.8 -59.1 G(50)	32.0 3	15.0 1.300	1.000	8.2 < 41.6
16	22	node Right	2334	16 500 3.3 -4.8 -59.2 G(50)	32.0 3	15.0 1.300	1.000	8.1 < 41.6
17	23	node Left	2334	16 500 1.1 -5.6 -82.5 G(50)	32.0 3	15.0 1.300	1.000	6.7 < 41.6
17	23	node Right	2334	16 500 1.1 -5.6 -82.5 G(50)	32.0 3	15.0 1.300	1.000	6.7 < 41.6
17	24	node Left	2334	16 500 2.6 -4.4 -49.6 G(50)	32.0 3	15.0 1.300	1.000	6.9 < 41.6
17	24	node Right	2334	16 500 2.6 -4.4 -49.6 G(50)	32.0 3	15.0 1.300	1.000	6.9 < 41.6
18	25	node Left	2334	14 500 7.2 -5.7 -35.0 G(50)	32.0 3	15.0 1.300	1.000	13.0 < 41.6
18	25	node Right	2334	14 500 7.4 -5.8 -35.6 G(50)	32.0 3	15.0 1.300	1.000	13.2 < 41.6
19	26	node Left	2334	12 500 13.3 -6.6 1.1 G(50)	32.0 3	15.0 1.000	1.000	19.9 < 32.0

19	26 node Right	2334	12	500	13.3	-6.6	1.2	G(50)	32.0	3	15.0	1.000	1.000	19.9	<	32.0
19	27 node Left	2334	12	500	16.1	-5.6	38.0	G(50)	32.0	3	15.0	1.000	1.000	21.7	<	32.0
19	27 node Right	2334	12	500	20.1	-7.1	47.7	G(50)	32.0	3	15.0	1.000	1.000	27.2	<	32.0
20	28 node Left	2334	12	500	14.8	-3.9	51.9	G(50)	32.0	3	15.0	1.000	1.000	18.7	<	32.0
20	28 node Right	2334	12	500	14.8	-3.9	51.8	G(50)	32.0	3	15.0	1.000	1.000	18.8	<	32.0
21	29 node Left	2334	12	500	15.2	-3.2	62.1	G(50)	32.0	3	15.0	1.000	1.000	18.4	<	32.0
21	29 node Right	2334	12	500	15.2	-3.2	62.1	G(50)	32.0	3	15.0	1.000	1.000	18.4	<	32.0
21	30 node Left	2334	12	500	14.5	-2.4	62.1	G(50)	32.0	3	15.0	1.000	1.000	16.9	<	32.0
21	30 node Right	2334	12	500	14.5	-2.4	62.1	G(50)	32.0	3	15.0	1.000	1.000	16.9	<	32.0
22	31 node Left	2334	12	500	12.4	-1.7	52.0	G(50)	32.0	3	15.0	1.000	1.000	14.0	<	32.0
22	31 node Right	2334	12	500	12.4	-1.7	52.0	G(50)	32.0	3	15.0	1.000	1.000	14.1	<	32.0
23	32 node Left	2334	12	500	12.3	-1.3	47.5	G(50)	32.0	3	15.0	1.000	1.000	13.7	<	32.0
23	32 node Right	2334	12	500	12.3	-1.3	47.5	G(50)	32.0	3	15.0	1.000	1.000	13.6	<	32.0
23	33 node Left	2334	12	500	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.000	1.000	0.0	<	32.0

STEEL-BOX G2

node WEB-U-2 (Web Upper edge) WEB - 2

Stress

range		Web	Grade					$\Delta \sigma_{ce} \cdot \text{Cycle}$							
node number	node number		height (mm)	t	σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR \cdot Ct
		(N/mm ²)					(N/mm ²)								
1	1 node Right	2364	12	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
1	2 node Left	2367	12	0	1.4	-16.0	-58.9	E(80)	62.0	3	29.0	1.300	1.000	17.4	< 80.6
1	2 node Right	2367	12	0	1.4	-16.0	-58.9	E(80)	62.0	3	29.0	1.300	1.000	17.4	< 80.6
2	3 node Left	2370	14	0	2.4	-19.7	-81.1	E(80)	62.0	3	29.0	1.300	1.000	22.1	< 80.6
2	3 node Right	2370	14	0	2.4	-19.7	-81.1	E(80)	62.0	3	29.0	1.300	1.000	22.1	< 80.6
3	4 node Left	2374	14	0	3.6	-23.1	-98.1	E(80)	62.0	3	29.0	1.300	1.000	26.7	< 80.6
3	4 node Right	2374	14	0	3.6	-23.1	-98.1	E(80)	62.0	3	29.0	1.300	1.000	26.7	< 80.6
3	5 node Left	2377	14	0	4.8	-24.4	-99.2	E(80)	62.0	3	29.0	1.300	1.000	29.2	< 80.6
3	5 node Right	2377	14	0	4.8	-24.4	-99.2	E(80)	62.0	3	29.0	1.300	1.000	29.2	< 80.6
4	6 node Left	2382	14	0	6.0	-24.0	-84.4	E(80)	62.0	3	29.0	1.300	1.000	30.0	< 80.6
4	6 node Right	2382	14	0	6.0	-24.0	-84.4	E(80)	62.0	3	29.0	1.300	1.000	30.0	< 80.6
5	7 node Left	2388	12	0	8.6	-25.8	-62.6	E(80)	62.0	3	29.0	1.300	1.000	34.5	< 80.6
5	7 node Right	2388	12	0	8.5	-25.2	-61.0	E(80)	62.0	3	29.0	1.300	1.000	33.7	< 80.6
5	8 node Left	2394	12	0	10.1	-21.3	-5.4	E(80)	62.0	3	29.0	1.193	1.000	31.4	< 74.0
5	8 node Right	2394	12	0	10.1	-21.3	-5.4	E(80)	62.0	3	29.0	1.193	1.000	31.4	< 74.0
6	9 node Left	2400	20	0	8.3	-11.0	48.5	E(80)	62.0	3	29.0	1.000	1.000	19.3	< 62.0
6	9 node Right	2400	20	0	9.3	-12.2	53.8	E(80)	62.0	3	29.0	1.000	1.000	21.4	< 62.0
7	10 node Left	2406	36	0	7.3	-4.4	80.0	E(80)	62.0	3	29.0	1.000	0.913	11.7	< 56.6
7	10 node Right	2406	36	0	7.3	-4.4	80.0	E(80)	62.0	3	29.0	1.000	0.913	11.7	< 56.6
7	11 node Left	2412	36	0	9.7	-2.2	137.1	E(80)	62.0	3	29.0	1.000	0.913	11.8	< 56.6
7	11 node Right	2412	36	0	9.7	-2.2	137.1	E(80)	62.0	3	29.0	1.000	0.913	11.8	< 56.6
8	12 node Left	2418	34	0	6.6	-4.8	83.4	E(80)	62.0	3	29.0	1.000	0.926	11.4	< 57.4
8	12 node Right	2418	34	0	6.6	-4.9	83.4	E(80)	62.0	3	29.0	1.000	0.926	11.4	< 57.4
9	13 node Left	2425	17	0	8.5	-13.8	50.2	E(80)	62.0	3	29.0	1.000	1.000	22.2	< 62.0
9	13 node Right	2425	17	0	7.6	-12.3	44.8	E(80)	62.0	3	29.0	1.000	1.000	19.9	< 62.0
10	14 node Left	2433	12	0	7.7	-19.4	-19.8	E(80)	62.0	3	29.0	1.300	1.000	27.1	< 80.6
10	14 node Right	2433	12	0	7.7	-19.5	-19.8	E(80)	62.0	3	29.0	1.300	1.000	27.2	< 80.6
10	15 node Left	2440	12	0	6.7	-24.4	-74.3	E(80)	62.0	3	29.0	1.300	1.000	31.1	< 80.6
10	15 node Right	2440	12	0	6.7	-24.4	-74.3	E(80)	62.0	3	29.0	1.300	1.000	31.1	< 80.6
11	16 node Left	2447	14	0	4.7	-23.6	-92.7	E(80)	62.0	3	29.0	1.300	1.000	28.3	< 80.6
11	16 node Right	2447	14	0	4.7	-23.6	-92.7	E(80)	62.0	3	29.0	1.300	1.000	28.3	< 80.6
12	17 node Left	2454	14	0	3.7	-24.6	-102.5	E(80)	62.0	3	29.0	1.300	1.000	28.3	< 80.6
12	17 node Right	2454	14	0	3.7	-24.6	-102.5	E(80)	62.0	3	29.0	1.300	1.000	28.3	< 80.6
13	18 node Left	2462	14	0	4.9	-23.9	-93.2	E(80)	62.0	3	29.0	1.300	1.000	28.8	< 80.6
13	18 node Right	2462	14	0	4.9	-23.9	-93.2	E(80)	62.0	3	29.0	1.300	1.000	28.8	< 80.6
14	19 node Left	2466	12	0	6.8	-24.2	-71.9	E(80)	62.0	3	29.0	1.300	1.000	31.0	< 80.6
14	19 node Right	2466	12	0	6.8	-24.1	-71.9	E(80)	62.0	3	29.0	1.300	1.000	30.9	< 80.6
14	20 node Left	2466	12	0	7.9	-19.4	-16.9	E(80)	62.0	3	29.0	1.300	1.000	27.3	< 80.6
14	20 node Right	2466	12	0	7.9	-19.4	-16.9	E(80)	62.0	3	29.0	1.300	1.000	27.3	< 80.6
15	21 node Left	2466	18	0	8.2	-12.3	48.8	E(80)	62.0	3	29.0	1.000	1.000	20.5	< 62.0
15	21 node Right	2466	18	0	9.0	-13.8	54.4	E(80)	62.0	3	29.0	1.000	1.000	22.8	< 62.0
16	22 node Left	2466	36	0	7.0	-4.9	86.2	E(80)	62.0	3	29.0	1.000	0.913	11.8	< 56.6
16	22 node Right	2466	36	0	7.0	-4.9	86.2	E(80)	62.0	3	29.0	1.000	0.913	11.8	< 56.6
17	23 node Left	2466	39	0	9.4	-1.9	138.0	E(80)	62.0	3	29.0	1.000	0.895	11.3	< 55.5
17	23 node Right	2466	39	0	9.4	-1.9	138.0	E(80)	62.0	3	29.0	1.000	0.895	11.3	< 55.5
17	24 node Left	2466	39	0	7.3	-4.3	82.6	E(80)	62.0	3	29.0	1.000	0.895	11.6	< 55.5
17	24 node Right	2466	39	0	7.4	-4.2	82.5	E(80)	62.0	3	29.0	1.000	0.895	11.6	< 55.5
18	25 node Left	2466	22	0	9.4	-12.0	58.0	E(80)	62.0	3	29.0	1.000	1.000	21.4	< 62.0
18	25 node Right	2466	22	0	8.6	-10.9	52.7	E(80)	62.0	3	29.0	1.000	1.000	19.5	< 62.0
19	26 node Left	2466	12	0	11.4	-22.8	-2.0	E(80)	62.0	3	29.0	1.116	1.000	34.2	< 69.2

19	26 node Right	2466	12	0	11.4	-22.9	-2.0	E(80)	62.0	3	29.0	1.117	1.000	34.2 < 69.2
19	27 node Left	2466	12	0	9.7	-27.5	-65.1	E(80)	62.0	3	29.0	1.300	1.000	37.2 < 80.6
19	27 node Right	2466	12	0	9.9	-28.4	-67.2	E(80)	62.0	3	29.0	1.300	1.000	38.3 < 80.6
20	28 node Left	2466	15	0	6.8	-25.5	-89.3	E(80)	62.0	3	29.0	1.300	1.000	32.3 < 80.6
20	28 node Right	2466	15	0	6.7	-25.5	-89.3	E(80)	62.0	3	29.0	1.300	1.000	32.2 < 80.6
21	29 node Left	2466	15	0	5.5	-26.2	-106.9	E(80)	62.0	3	29.0	1.300	1.000	31.8 < 80.6
21	29 node Right	2466	15	0	5.5	-26.2	-106.9	E(80)	62.0	3	29.0	1.300	1.000	31.8 < 80.6
21	30 node Left	2466	15	0	4.2	-25.0	-107.0	E(80)	62.0	3	29.0	1.300	1.000	29.2 < 80.6
21	30 node Right	2466	15	0	4.2	-25.0	-107.0	E(80)	62.0	3	29.0	1.300	1.000	29.2 < 80.6
22	31 node Left	2466	15	0	2.9	-21.4	-89.6	E(80)	62.0	3	29.0	1.300	1.000	24.2 < 80.6
22	31 node Right	2466	15	0	2.8	-21.4	-89.5	E(80)	62.0	3	29.0	1.300	1.000	24.2 < 80.6
23	32 node Left	2466	12	0	1.8	-17.4	-67.1	E(80)	62.0	3	29.0	1.300	1.000	19.2 < 80.6
23	32 node Right	2466	12	0	1.8	-17.4	-67.0	E(80)	62.0	3	29.0	1.300	1.000	19.2 < 80.6
23	33 node Left	2466	12	0	0.0	-0.1	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.1 < 80.6

STEEL-BOX G2

node WEB-L-2 (Web Lower edge) WEB - 2

Stress

range	node		Web	Grade				$\Delta \sigma_{ce} \cdot \text{Cycle}$									
number	number	number	height (mm)	t	σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR · Ct	D	
					(N/mm ²)										(N/mm ²)		
1	1	node Right	2364	12	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
1	2	node Left	2367	12	0	19.2	-1.8	70.7	E(80)	62.0	3	29.0	1.000	1.000	21.0	< 62.0	
1	2	node Right	2367	12	0	19.2	-1.8	70.7	E(80)	62.0	3	29.0	1.000	1.000	21.0	< 62.0	
2	3	node Left	2370	16	0	21.5	-2.6	88.8	E(80)	62.0	3	29.0	1.000	1.000	24.2	< 62.0	
2	3	node Right	2370	16	0	21.5	-2.6	88.8	E(80)	62.0	3	29.0	1.000	1.000	24.2	< 62.0	
3	4	node Left	2374	16	0	25.2	-3.9	107.1	E(80)	62.0	3	29.0	1.000	1.000	29.1	< 62.0	
3	4	node Right	2374	16	0	25.2	-3.9	107.1	E(80)	62.0	3	29.0	1.000	1.000	29.1	< 62.0	
3	5	node Left	2377	16	0	26.6	-5.2	107.9	E(80)	62.0	3	29.0	1.000	1.000	31.8	< 62.0	
3	5	node Right	2377	16	0	26.6	-5.2	107.9	E(80)	62.0	3	29.0	1.000	1.000	31.8	< 62.0	
4	6	node Left	2382	16	0	26.0	-6.6	91.4	E(80)	62.0	3	29.0	1.000	1.000	32.6	< 62.0	
4	6	node Right	2382	16	0	26.0	-6.6	91.4	E(80)	62.0	3	29.0	1.000	1.000	32.6	< 62.0	
5	7	node Left	2388	12	0	31.4	-10.6	76.2	E(80)	62.0	3	29.0	1.000	1.000	42.0	< 62.0	
5	7	node Right	2388	12	0	26.3	-8.8	63.7	E(80)	62.0	3	29.0	1.000	1.000	35.1	< 62.0	
5	8	node Left	2394	12	0	22.1	-10.6	5.7	E(80)	62.0	3	29.0	1.000	1.000	32.6	< 62.0	
5	8	node Right	2394	12	0	22.1	-10.6	5.7	E(80)	62.0	3	29.0	1.000	1.000	32.6	< 62.0	
6	9	node Left	2400	15	0	12.5	-9.4	-55.2	E(80)	62.0	3	29.0	1.300	1.000	21.9	< 80.6	
6	9	node Right	2400	15	0	12.6	-9.5	-55.8	E(80)	62.0	3	29.0	1.300	1.000	22.2	< 80.6	
7	10	node Left	2406	29	0	4.5	-7.6	-82.8	E(80)	62.0	3	29.0	1.300	0.964	12.1	< 77.7	
7	10	node Right	2406	29	0	4.5	-7.6	-82.8	E(80)	62.0	3	29.0	1.300	0.964	12.1	< 77.7	
7	11	node Left	2412	29	0	2.2	-10.0	-140.8	E(80)	62.0	3	29.0	1.300	0.964	12.2	< 77.7	
7	11	node Right	2412	29	0	2.2	-10.0	-140.8	E(80)	62.0	3	29.0	1.300	0.964	12.2	< 77.7	
8	12	node Left	2418	22	0	5.6	-7.6	-96.9	E(80)	62.0	3	29.0	1.300	1.000	13.2	< 80.6	
8	12	node Right	2418	22	0	5.6	-7.6	-96.9	E(80)	62.0	3	29.0	1.300	1.000	13.2	< 80.6	
9	13	node Left	2425	14	0	14.0	-8.6	-51.0	E(80)	62.0	3	29.0	1.300	1.000	22.6	< 80.6	
9	13	node Right	2425	14	0	13.8	-8.6	-50.3	E(80)	62.0	3	29.0	1.300	1.000	22.3	< 80.6	
10	14	node Left	2433	12	0	18.4	-7.3	18.7	E(80)	62.0	3	29.0	1.000	1.000	25.7	< 62.0	
10	14	node Right	2433	12	0	18.4	-7.2	18.7	E(80)	62.0	3	29.0	1.000	1.000	25.6	< 62.0	
10	15	node Left	2440	12	0	27.4	-7.5	83.4	E(80)	62.0	3	29.0	1.000	1.000	35.0	< 62.0	
10	15	node Right	2440	12	0	27.4	-7.6	83.5	E(80)	62.0	3	29.0	1.000	1.000	35.0	< 62.0	
11	16	node Left	2447	18	0	23.8	-4.8	93.2	E(80)	62.0	3	29.0	1.000	1.000	28.6	< 62.0	
11	16	node Right	2447	18	0	23.8	-4.8	93.2	E(80)	62.0	3	29.0	1.000	1.000	28.6	< 62.0	
12	17	node Left	2454	18	0	24.6	-3.8	102.5	E(80)	62.0	3	29.0	1.000	1.000	28.3	< 62.0	
12	17	node Right	2454	18	0	24.6	-3.8	102.5	E(80)	62.0	3	29.0	1.000	1.000	28.3	< 62.0	
13	18	node Left	2462	18	0	23.8	-4.9	92.6	E(80)	62.0	3	29.0	1.000	1.000	28.6	< 62.0	
13	18	node Right	2462	18	0	23.8	-4.9	92.6	E(80)	62.0	3	29.0	1.000	1.000	28.6	< 62.0	
14	19	node Left	2466	12	0	27.3	-7.7	81.4	E(80)	62.0	3	29.0	1.000	1.000	35.0	< 62.0	
14	19	node Right	2466	12	0	27.3	-7.7	81.3	E(80)	62.0	3	29.0	1.000	1.000	35.0	< 62.0	
14	20	node Left	2466	12	0	18.3	-7.5	16.1	E(80)	62.0	3	29.0	1.000	1.000	25.8	< 62.0	
14	20	node Right	2466	12	0	18.3	-7.5	16.0	E(80)	62.0	3	29.0	1.000	1.000	25.8	< 62.0	
15	21	node Left	2466	14	0	13.8	-9.1	-54.3	E(80)	62.0	3	29.0	1.300	1.000	22.9	< 80.6	
15	21	node Right	2466	14	0	13.8	-9.2	-55.0	E(80)	62.0	3	29.0	1.300	1.000	23.0	< 80.6	
16	22	node Left	2466	24	0	5.4	-7.8	-95.6	E(80)	62.0	3	29.0	1.300	1.000	13.2	< 80.6	
16	22	node Right	2466	24	0	5.4	-7.8	-95.6	E(80)	62.0	3	29.0	1.300	1.000	13.1	< 80.6	
17	23	node Left	2466	31	0	1.8	-9.4	-137.8	E(80)	62.0	3	29.0	1.300	0.948	11.2	< 76.4	
17	23	node Right	2466	31	0	1.8	-9.4	-137.8	E(80)	62.0	3	29.0	1.300	0.948	11.2	< 76.4	
17	24	node Left	2466	31	0	4.2	-7.4	-82.7	E(80)	62.0	3	29.0	1.300	0.948	11.6	< 76.4	
17	24	node Right	2466	31	0	4.3	-7.4	-82.7	E(80)	62.0	3	29.0	1.300	0.948	11.7	< 76.4	
18	25	node Left	2466	16	0	12.1	-9.5	-58.4	E(80)	62.0	3	29.0	1.300	1.000	21.6	< 80.6	
18	25	node Right	2466	16	0	11.9	-9.5	-57.8	E(80)	62.0	3	29.0	1.300	1.000	21.4	< 80.6	
19	26	node Left	2466	12	0	22.4	-11.1	1.9	E(80)	62.0	3	29.0	1.000	1.000	33.5	< 62.0	

19	26 node Right	2466	12	0	22.4	-11.1	2.0	E(80)	62.0	3	29.0	1.000	1.000	33.5	<	62.0
19	27 node Left	2466	12	0	27.0	-9.5	63.9	E(80)	62.0	3	29.0	1.000	1.000	36.5	<	62.0
19	27 node Right	2466	12	0	32.3	-11.3	76.4	E(80)	62.0	3	29.0	1.000	1.000	43.6	<	62.0
20	28 node Left	2466	18	0	24.9	-6.6	87.3	E(80)	62.0	3	29.0	1.000	1.000	31.5	<	62.0
20	28 node Right	2466	18	0	25.0	-6.6	87.3	E(80)	62.0	3	29.0	1.000	1.000	31.5	<	62.0
21	29 node Left	2466	18	0	25.7	-5.4	104.5	E(80)	62.0	3	29.0	1.000	1.000	31.0	<	62.0
21	29 node Right	2466	18	0	25.7	-5.4	104.5	E(80)	62.0	3	29.0	1.000	1.000	31.0	<	62.0
21	30 node Left	2466	18	0	24.5	-4.1	104.6	E(80)	62.0	3	29.0	1.000	1.000	28.6	<	62.0
21	30 node Right	2466	18	0	24.5	-4.1	104.6	E(80)	62.0	3	29.0	1.000	1.000	28.6	<	62.0
22	31 node Left	2466	18	0	20.8	-2.8	87.6	E(80)	62.0	3	29.0	1.000	1.000	23.6	<	62.0
22	31 node Right	2466	18	0	20.9	-2.7	87.5	E(80)	62.0	3	29.0	1.000	1.000	23.6	<	62.0
23	32 node Left	2466	12	0	19.8	-2.2	76.3	E(80)	62.0	3	29.0	1.000	1.000	21.9	<	62.0
23	32 node Right	2466	12	0	19.8	-2.1	76.2	E(80)	62.0	3	29.0	1.000	1.000	21.8	<	62.0
23	33 node Left	2466	12	0	0.1	0.0	0.0	E(80)	62.0	3	29.0	1.000	1.000	0.1	<	62.0

STEEL-BOX G2

node HSTIFF-2 (Web H-stiff) WEB - 2

Stress

range																
node	node	Web		Grade		$\Delta \sigma_{ce} \cdot \text{Cycle}$		$\Delta \sigma_{ve} \cdot \text{CR}$		Ct		$\Delta \sigma_{max} \cdot \text{CR} \cdot Ct$		D		
number	number	height	t	σ_{tmax}	σ_{tmin}	σ_d	($\Delta \sigma_f$)	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR	Ct	D
		(mm)	(N/mm ²)										(N/mm ²)			
1	1 node Right	2364	12	473	0.0	0.0	0.0 G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6	
1	2 node Left	2367	12	473	0.8	-9.0	-33.0 G(50)	32.0	3	15.0	1.300	1.000	9.8	<	41.6	
1	2 node Right	2367	12	473	0.8	-9.0	-33.0 G(50)	32.0	3	15.0	1.300	1.000	9.8	<	41.6	
2	3 node Left	2370	12	474	1.4	-11.4	-47.1 G(50)	32.0	3	15.0	1.300	1.000	12.8	<	41.6	
2	3 node Right	2370	12	474	1.4	-11.4	-47.1 G(50)	32.0	3	15.0	1.300	1.000	12.8	<	41.6	
3	4 node Left	2374	12	475	2.1	-13.5	-57.1 G(50)	32.0	3	15.0	1.300	1.000	15.6	<	41.6	
3	4 node Right	2374	12	475	2.1	-13.5	-57.1 G(50)	32.0	3	15.0	1.300	1.000	15.6	<	41.6	
3	5 node Left	2377	12	475	2.8	-14.2	-57.8 G(50)	32.0	3	15.0	1.300	1.000	17.0	<	41.6	
3	5 node Right	2377	12	475	2.8	-14.2	-57.8 G(50)	32.0	3	15.0	1.300	1.000	17.0	<	41.6	
4	6 node Left	2382	12	476	3.5	-14.0	-49.2 G(50)	32.0	3	15.0	1.300	1.000	17.5	<	41.6	
4	6 node Right	2382	12	476	3.5	-14.0	-49.2 G(50)	32.0	3	15.0	1.300	1.000	17.5	<	41.6	
5	7 node Left	2388	12	478	4.8	-14.4	-34.8 G(50)	32.0	3	15.0	1.300	1.000	19.2	<	41.6	
5	7 node Right	2388	12	478	5.0	-14.9	-36.1 G(50)	32.0	3	15.0	1.300	1.000	19.9	<	41.6	
5	8 node Left	2394	12	479	6.0	-12.6	-3.2 G(50)	32.0	3	15.0	1.193	1.000	18.6	<	38.2	
5	8 node Right	2394	12	479	6.0	-12.6	-3.2 G(50)	32.0	3	15.0	1.193	1.000	18.6	<	38.2	
6	9 node Left	2400	14	480	7.8	-5.9	-34.5 G(50)	32.0	3	15.0	1.300	1.000	13.7	<	41.6	
6	9 node Right	2400	14	480	7.7	-5.8	-33.9 G(50)	32.0	3	15.0	1.300	1.000	13.4	<	41.6	
7	10 node Left	2406	16	481	2.7	-4.6	-50.2 G(50)	32.0	3	15.0	1.300	1.000	7.3	<	41.6	
7	10 node Right	2406	16	481	2.7	-4.6	-50.2 G(50)	32.0	3	15.0	1.300	1.000	7.3	<	41.6	
7	11 node Left	2412	16	482	1.4	-6.1	-85.2 G(50)	32.0	3	15.0	1.300	1.000	7.4	<	41.6	
7	11 node Right	2412	16	482	1.4	-6.1	-85.2 G(50)	32.0	3	15.0	1.300	1.000	7.4	<	41.6	
8	12 node Left	2418	16	484	3.5	-4.8	-60.8 G(50)	32.0	3	15.0	1.300	1.000	8.3	<	41.6	
8	12 node Right	2418	16	484	3.5	-4.8	-60.8 G(50)	32.0	3	15.0	1.300	1.000	8.3	<	41.6	
9	13 node Left	2425	14	485	8.4	-5.2	-30.8 G(50)	32.0	3	15.0	1.300	1.000	13.7	<	41.6	
9	13 node Right	2425	14	485	8.5	-5.3	-31.3 G(50)	32.0	3	15.0	1.300	1.000	13.9	<	41.6	
10	14 node Left	2433	12	487	4.7	-11.9	-12.1 G(50)	32.0	3	15.0	1.300	1.000	16.6	<	41.6	
10	14 node Right	2433	12	487	4.7	-11.9	-12.1 G(50)	32.0	3	15.0	1.300	1.000	16.6	<	41.6	
10	15 node Left	2440	12	488	3.9	-14.0	-42.8 G(50)	32.0	3	15.0	1.300	1.000	17.9	<	41.6	
10	15 node Right	2440	12	488	3.9	-14.0	-42.7 G(50)	32.0	3	15.0	1.300	1.000	17.9	<	41.6	
11	16 node Left	2447	12	489	2.8	-14.1	-55.5 G(50)	32.0	3	15.0	1.300	1.000	16.9	<	41.6	
11	16 node Right	2447	12	489	2.8	-14.1	-55.5 G(50)	32.0	3	15.0	1.300	1.000	16.9	<	41.6	
12	17 node Left	2454	12	491	2.2	-14.8	-61.5 G(50)	32.0	3	15.0	1.300	1.000	17.0	<	41.6	
12	17 node Right	2454	12	491	2.2	-14.8	-61.5 G(50)	32.0	3	15.0	1.300	1.000	17.0	<	41.6	
13	18 node Left	2462	12	492	2.9	-14.4	-56.0 G(50)	32.0	3	15.0	1.300	1.000	17.3	<	41.6	
13	18 node Right	2462	12	492	2.9	-14.4	-56.0 G(50)	32.0	3	15.0	1.300	1.000	17.3	<	41.6	
14	19 node Left	2466	12	493	3.9	-13.9	-41.2 G(50)	32.0	3	15.0	1.300	1.000	17.8	<	41.6	
14	19 node Right	2466	12	493	3.9	-13.8	-41.3 G(50)	32.0	3	15.0	1.300	1.000	17.7	<	41.6	
14	20 node Left	2466	12	493	4.8	-11.8	-10.3 G(50)	32.0	3	15.0	1.300	1.000	16.7	<	41.6	
14	20 node Right	2466	12	493	4.8	-11.8	-10.3 G(50)	32.0	3	15.0	1.300	1.000	16.7	<	41.6	
15	21 node Left	2466	14	493	8.5	-5.7	-33.7 G(50)	32.0	3	15.0	1.300	1.000	14.2	<	41.6	
15	21 node Right	2466	14	493	8.3	-5.6	-33.1 G(50)	32.0	3	15.0	1.300	1.000	13.9	<	41.6	
16	22 node Left	2466	16	493	3.4	-4.8	-59.2 G(50)	32.0	3	15.0	1.300	1.000	8.2	<	41.6	
16	22 node Right	2466	16	493	3.3	-4.8	-59.2 G(50)	32.0	3	15.0	1.300	1.000	8.1	<	41.6	
17	23 node Left	2466	16	493	1.1	-5.6	-82.6 G(50)	32.0	3	15.0	1.300	1.000	6.7	<	41.6	
17	23 node Right	2466	16	493	1.1	-5.6	-82.6 G(50)	32.0	3	15.0	1.300	1.000	6.7	<	41.6	
17	24 node Left	2466	16	493	2.5	-4.4	-49.6 G(50)	32.0	3	15.0	1.300	1.000	7.0	<	41.6	
17	24 node Right	2466	16	493	2.6	-4.4	-49.7 G(50)	32.0	3	15.0	1.300	1.000	7.0	<	41.6	
18	25 node Left	2466	14	493	7.3	-5.7	-35.1 G(50)	32.0	3	15.0	1.300	1.000	13.0	<	41.6	
18	25 node Right	2466	14	493	7.4	-5.9	-35.7 G(50)	32.0	3	15.0	1.300	1.000	13.2	<	41.6	
19	26 node Left	2466	12	493	6.9	-13.8	-1.2 G(50)	32.0	3	15.0	1.117	1.000	20.6	<	35.7	

19	26 node Right	2466	12	493	6.9	-13.8	-1.2	G(50)	32.0	3	15.0	1.117	1.000	20.7	<	35.7
19	27 node Left	2466	12	493	5.8	-16.6	-39.3	G(50)	32.0	3	15.0	1.300	1.000	22.5	<	41.6
19	27 node Right	2466	12	493	5.7	-16.3	-38.5	G(50)	32.0	3	15.0	1.300	1.000	21.9	<	41.6
20	28 node Left	2466	12	493	4.1	-15.4	-54.0	G(50)	32.0	3	15.0	1.300	1.000	19.6	<	41.6
20	28 node Right	2466	12	493	4.1	-15.4	-54.0	G(50)	32.0	3	15.0	1.300	1.000	19.5	<	41.6
21	29 node Left	2466	12	493	3.3	-15.9	-64.6	G(50)	32.0	3	15.0	1.300	1.000	19.2	<	41.6
21	29 node Right	2466	12	493	3.3	-15.9	-64.6	G(50)	32.0	3	15.0	1.300	1.000	19.2	<	41.6
21	30 node Left	2466	12	493	2.5	-15.1	-64.7	G(50)	32.0	3	15.0	1.300	1.000	17.6	<	41.6
21	30 node Right	2466	12	493	2.5	-15.1	-64.7	G(50)	32.0	3	15.0	1.300	1.000	17.6	<	41.6
22	31 node Left	2466	12	493	1.7	-12.9	-54.2	G(50)	32.0	3	15.0	1.300	1.000	14.7	<	41.6
22	31 node Right	2466	12	493	1.7	-12.9	-54.1	G(50)	32.0	3	15.0	1.300	1.000	14.6	<	41.6
23	32 node Left	2466	12	493	1.0	-9.9	-38.4	G(50)	32.0	3	15.0	1.300	1.000	11.0	<	41.6
23	32 node Right	2466	12	493	1.1	-9.9	-38.4	G(50)	32.0	3	15.0	1.300	1.000	11.0	<	41.6
23	33 node Left	2466	12	493	0.0	-0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6

STEEL-BOX G2

node POINT-U-2 (Web) WEB - 2

Stress

range		Web	Grade			$\Delta \sigma_{ce} \cdot \text{Cycle}$										
node number	node number		height (mm)	t	σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR \cdot Ct	D
						(N/mm ²)								(N/mm ²)		
1	1 node Right	2364	12	900	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6
1	2 node Left	2367	12	900	0.2	-2.6	-9.6	G(50)	32.0	3	15.0	1.300	1.000	2.8	<	41.6
1	2 node Right	2367	12	900	0.2	-2.6	-9.6	G(50)	32.0	3	15.0	1.300	1.000	2.8	<	41.6
2	3 node Left	2370	12	900	0.5	-4.0	-16.6	G(50)	32.0	3	15.0	1.300	1.000	4.5	<	41.6
2	3 node Right	2370	12	900	0.5	-4.0	-16.6	G(50)	32.0	3	15.0	1.300	1.000	4.5	<	41.6
3	4 node Left	2374	12	900	0.7	-4.8	-20.3	G(50)	32.0	3	15.0	1.300	1.000	5.5	<	41.6
3	4 node Right	2374	12	900	0.7	-4.8	-20.3	G(50)	32.0	3	15.0	1.300	1.000	5.5	<	41.6
3	5 node Left	2377	12	900	1.0	-5.1	-20.8	G(50)	32.0	3	15.0	1.300	1.000	6.1	<	41.6
3	5 node Right	2377	12	900	1.0	-5.1	-20.8	G(50)	32.0	3	15.0	1.300	1.000	6.1	<	41.6
4	6 node Left	2382	12	900	1.3	-5.1	-18.0	G(50)	32.0	3	15.0	1.300	1.000	6.4	<	41.6
4	6 node Right	2382	12	900	1.3	-5.1	-18.0	G(50)	32.0	3	15.0	1.300	1.000	6.4	<	41.6
5	7 node Left	2388	12	900	1.4	-4.3	-10.3	G(50)	32.0	3	15.0	1.300	1.000	5.7	<	41.6
5	7 node Right	2388	12	900	2.0	-5.8	-14.0	G(50)	32.0	3	15.0	1.300	1.000	7.8	<	41.6
5	8 node Left	2394	12	900	2.3	-5.0	-1.2	G(50)	32.0	3	15.0	1.193	1.000	7.3	<	38.2
5	8 node Right	2394	12	900	2.3	-5.0	-1.2	G(50)	32.0	3	15.0	1.193	1.000	7.3	<	38.2
6	9 node Left	2400	14	900	1.7	-2.2	9.6	G(50)	32.0	3	15.0	1.000	1.000	3.8	<	32.0
6	9 node Right	2400	14	900	2.2	-2.9	12.7	G(50)	32.0	3	15.0	1.000	1.000	5.1	<	32.0
7	10 node Left	2406	16	900	1.7	-1.1	19.1	G(50)	32.0	3	15.0	1.000	1.000	2.8	<	32.0
7	10 node Right	2406	16	900	1.7	-1.1	19.1	G(50)	32.0	3	15.0	1.000	1.000	2.8	<	32.0
7	11 node Left	2412	16	900	2.3	-0.5	33.4	G(50)	32.0	3	15.0	1.000	1.000	2.9	<	32.0
7	11 node Right	2412	16	900	2.3	-0.5	33.4	G(50)	32.0	3	15.0	1.000	1.000	2.9	<	32.0
8	12 node Left	2418	16	900	1.3	-0.9	16.3	G(50)	32.0	3	15.0	1.000	1.000	2.2	<	32.0
8	12 node Right	2418	16	900	1.3	-1.0	16.3	G(50)	32.0	3	15.0	1.000	1.000	2.3	<	32.0
9	13 node Left	2425	14	900	2.1	-3.5	12.6	G(50)	32.0	3	15.0	1.000	1.000	5.6	<	32.0
9	13 node Right	2425	14	900	1.6	-2.6	9.5	G(50)	32.0	3	15.0	1.000	1.000	4.2	<	32.0
10	14 node Left	2433	12	900	2.1	-5.4	-5.6	G(50)	32.0	3	15.0	1.300	1.000	7.6	<	41.6
10	14 node Right	2433	12	900	2.2	-5.5	-5.6	G(50)	32.0	3	15.0	1.300	1.000	7.7	<	41.6
10	15 node Left	2440	12	900	1.5	-5.3	-16.1	G(50)	32.0	3	15.0	1.300	1.000	6.7	<	41.6
10	15 node Right	2440	12	900	1.4	-5.3	-16.1	G(50)	32.0	3	15.0	1.300	1.000	6.7	<	41.6
11	16 node Left	2447	12	900	1.2	-6.2	-24.3	G(50)	32.0	3	15.0	1.300	1.000	7.4	<	41.6
11	16 node Right	2447	12	900	1.2	-6.2	-24.3	G(50)	32.0	3	15.0	1.300	1.000	7.4	<	41.6
12	17 node Left	2454	12	900	1.0	-6.6	-27.3	G(50)	32.0	3	15.0	1.300	1.000	7.6	<	41.6
12	17 node Right	2454	12	900	1.0	-6.6	-27.3	G(50)	32.0	3	15.0	1.300	1.000	7.6	<	41.6
13	18 node Left	2462	12	900	1.3	-6.5	-25.3	G(50)	32.0	3	15.0	1.300	1.000	7.8	<	41.6
13	18 node Right	2462	12	900	1.3	-6.5	-25.3	G(50)	32.0	3	15.0	1.300	1.000	7.8	<	41.6
14	19 node Left	2466	12	900	1.5	-5.4	-16.0	G(50)	32.0	3	15.0	1.300	1.000	6.9	<	41.6
14	19 node Right	2466	12	900	1.5	-5.3	-16.0	G(50)	32.0	3	15.0	1.300	1.000	6.9	<	41.6
14	20 node Left	2466	12	900	2.3	-5.6	-4.9	G(50)	32.0	3	15.0	1.300	1.000	7.9	<	41.6
14	20 node Right	2466	12	900	2.3	-5.6	-4.9	G(50)	32.0	3	15.0	1.300	1.000	7.9	<	41.6
15	21 node Left	2466	14	900	1.9	-2.8	11.2	G(50)	32.0	3	15.0	1.000	1.000	4.7	<	32.0
15	21 node Right	2466	14	900	2.4	-3.7	14.5	G(50)	32.0	3	15.0	1.000	1.000	6.1	<	32.0
16	22 node Left	2466	16	900	1.6	-1.1	19.8	G(50)	32.0	3	15.0	1.000	1.000	2.7	<	32.0
16	22 node Right	2466	16	900	1.6	-1.1	19.8	G(50)	32.0	3	15.0	1.000	1.000	2.7	<	32.0
17	23 node Left	2466	16	900	2.5	-0.5	37.3	G(50)	32.0	3	15.0	1.000	1.000	3.1	<	32.0
17	23 node Right	2466	16	900	2.5	-0.5	37.3	G(50)	32.0	3	15.0	1.000	1.000	3.1	<	32.0
17	24 node Left	2466	16	900	1.9	-1.2	22.3	G(50)	32.0	3	15.0	1.000	1.000	3.1	<	32.0
17	24 node Right	2466	16	900	2.0	-1.1	22.2	G(50)	32.0	3	15.0	1.000	1.000	3.1	<	32.0
18	25 node Left	2466	14	900	2.5	-3.2	15.5	G(50)	32.0	3	15.0	1.000	1.000	5.7	<	32.0
18	25 node Right	2466	14	900	2.0	-2.6	12.4	G(50)	32.0	3	15.0	1.000	1.000	4.6	<	32.0
19	26 node Left	2466	12	900	3.2	-6.3	-0.6	G(50)	32.0	3	15.0	1.117	1.000	9.5	<	35.8

19	26 node Right	2466	12	900	3.2	-6.4	-0.5	G(50)	32.0	3	15.0	1.116	1.000	9.5<	35.7
19	27 node Left	2466	12	900	2.7	-7.6	-18.0	G(50)	32.0	3	15.0	1.300	1.000	10.3<	41.6
19	27 node Right	2466	12	900	2.2	-6.2	-14.8	G(50)	32.0	3	15.0	1.300	1.000	8.4<	41.6
20	28 node Left	2466	12	900	1.9	-7.1	-24.8	G(50)	32.0	3	15.0	1.300	1.000	9.0<	41.6
20	28 node Right	2466	12	900	1.9	-7.1	-24.8	G(50)	32.0	3	15.0	1.300	1.000	9.0<	41.6
21	29 node Left	2466	12	900	1.5	-7.3	-29.7	G(50)	32.0	3	15.0	1.300	1.000	8.8<	41.6
21	29 node Right	2466	12	900	1.5	-7.3	-29.7	G(50)	32.0	3	15.0	1.300	1.000	8.8<	41.6
21	30 node Left	2466	12	900	1.2	-7.0	-29.8	G(50)	32.0	3	15.0	1.300	1.000	8.1<	41.6
21	30 node Right	2466	12	900	1.2	-7.0	-29.8	G(50)	32.0	3	15.0	1.300	1.000	8.1<	41.6
22	31 node Left	2466	12	900	0.8	-6.0	-24.9	G(50)	32.0	3	15.0	1.300	1.000	6.8<	41.6
22	31 node Right	2466	12	900	0.8	-5.9	-24.9	G(50)	32.0	3	15.0	1.300	1.000	6.7<	41.6
23	32 node Left	2466	12	900	0.4	-3.8	-14.8	G(50)	32.0	3	15.0	1.300	1.000	4.2<	41.6
23	32 node Right	2466	12	900	0.4	-3.8	-14.7	G(50)	32.0	3	15.0	1.300	1.000	4.2<	41.6
23	33 node Left	2466	12	900	0.0	-0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0<	41.6

STEEL-BOX G2

node POINT-L-2 (Web) WEB - 2

Stress

range		Web	Grade					$\Delta \sigma_{ce} \cdot \text{Cycle}$								
node number	node number		height (mm)	t	σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR · Ct	D
				(N/mm ²)			(N/mm ²)									
1	1	node Right	2364	12	500	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
1	2	node Left	2367	12	500	11.8	-1.1	43.3	G(50)	32.0	3	15.0	1.000	1.000	12.8	< 32.0
1	2	node Right	2367	12	500	11.8	-1.1	43.3	G(50)	32.0	3	15.0	1.000	1.000	12.8	< 32.0
2	3	node Left	2370	12	500	12.8	-1.6	53.0	G(50)	32.0	3	15.0	1.000	1.000	14.4	< 32.0
2	3	node Right	2370	12	500	12.8	-1.6	53.0	G(50)	32.0	3	15.0	1.000	1.000	14.4	< 32.0
3	4	node Left	2374	12	500	15.0	-2.3	63.9	G(50)	32.0	3	15.0	1.000	1.000	17.4	< 32.0
3	4	node Right	2374	12	500	15.0	-2.3	63.9	G(50)	32.0	3	15.0	1.000	1.000	17.4	< 32.0
3	5	node Left	2377	12	500	15.8	-3.1	64.3	G(50)	32.0	3	15.0	1.000	1.000	18.9	< 32.0
3	5	node Right	2377	12	500	15.8	-3.1	64.3	G(50)	32.0	3	15.0	1.000	1.000	18.9	< 32.0
4	6	node Left	2382	12	500	15.5	-3.9	54.5	G(50)	32.0	3	15.0	1.000	1.000	19.4	< 32.0
4	6	node Right	2382	12	500	15.5	-3.9	54.5	G(50)	32.0	3	15.0	1.000	1.000	19.4	< 32.0
5	7	node Left	2388	12	500	19.4	-6.5	47.1	G(50)	32.0	3	15.0	1.000	1.000	26.0	< 32.0
5	7	node Right	2388	12	500	15.5	-5.2	37.6	G(50)	32.0	3	15.0	1.000	1.000	20.7	< 32.0
5	8	node Left	2394	12	500	13.0	-6.2	3.4	G(50)	32.0	3	15.0	1.000	1.000	19.3	< 32.0
5	8	node Right	2394	12	500	13.0	-6.2	3.4	G(50)	32.0	3	15.0	1.000	1.000	19.3	< 32.0
6	9	node Left	2400	14	500	7.6	-5.7	-33.6	G(50)	32.0	3	15.0	1.300	1.000	13.3	< 41.6
6	9	node Right	2400	14	500	7.5	-5.6	-33.0	G(50)	32.0	3	15.0	1.300	1.000	13.1	< 41.6
7	10	node Left	2406	16	500	2.6	-4.5	-49.0	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
7	10	node Right	2406	16	500	2.6	-4.5	-49.0	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
7	11	node Left	2412	16	500	1.3	-5.9	-83.2	G(50)	32.0	3	15.0	1.300	1.000	7.2	< 41.6
7	11	node Right	2412	16	500	1.3	-5.9	-83.2	G(50)	32.0	3	15.0	1.300	1.000	7.2	< 41.6
8	12	node Left	2418	16	500	3.4	-4.7	-59.6	G(50)	32.0	3	15.0	1.300	1.000	8.1	< 41.6
8	12	node Right	2418	16	500	3.4	-4.7	-59.6	G(50)	32.0	3	15.0	1.300	1.000	8.1	< 41.6
9	13	node Left	2425	14	500	8.3	-5.1	-30.1	G(50)	32.0	3	15.0	1.300	1.000	13.4	< 41.6
9	13	node Right	2425	14	500	8.4	-5.2	-30.7	G(50)	32.0	3	15.0	1.300	1.000	13.6	< 41.6
10	14	node Left	2433	12	500	10.6	-4.2	10.8	G(50)	32.0	3	15.0	1.000	1.000	14.8	< 32.0
10	14	node Right	2433	12	500	10.6	-4.1	10.8	G(50)	32.0	3	15.0	1.000	1.000	14.7	< 32.0
10	15	node Left	2440	12	500	16.8	-4.6	51.1	G(50)	32.0	3	15.0	1.000	1.000	21.4	< 32.0
10	15	node Right	2440	12	500	16.8	-4.7	51.2	G(50)	32.0	3	15.0	1.000	1.000	21.4	< 32.0
11	16	node Left	2447	12	500	14.1	-2.9	55.2	G(50)	32.0	3	15.0	1.000	1.000	16.9	< 32.0
11	16	node Right	2447	12	500	14.1	-2.9	55.2	G(50)	32.0	3	15.0	1.000	1.000	16.9	< 32.0
12	17	node Left	2454	12	500	14.5	-2.2	60.7	G(50)	32.0	3	15.0	1.000	1.000	16.8	< 32.0
12	17	node Right	2454	12	500	14.5	-2.2	60.7	G(50)	32.0	3	15.0	1.000	1.000	16.8	< 32.0
13	18	node Left	2462	12	500	14.1	-2.9	54.9	G(50)	32.0	3	15.0	1.000	1.000	17.0	< 32.0
13	18	node Right	2462	12	500	14.1	-2.9	54.9	G(50)	32.0	3	15.0	1.000	1.000	17.0	< 32.0
14	19	node Left	2466	12	500	16.9	-4.7	50.3	G(50)	32.0	3	15.0	1.000	1.000	21.6	< 32.0
14	19	node Right	2466	12	500	16.9	-4.7	50.2	G(50)	32.0	3	15.0	1.000	1.000	21.6	< 32.0
14	20	node Left	2466	12	500	10.7	-4.4	9.4	G(50)	32.0	3	15.0	1.000	1.000	15.1	< 32.0
14	20	node Right	2466	12	500	10.7	-4.4	9.3	G(50)	32.0	3	15.0	1.000	1.000	15.1	< 32.0
15	21	node Left	2466	14	500	8.5	-5.6	-33.4	G(50)	32.0	3	15.0	1.300	1.000	14.1	< 41.6
15	21	node Right	2466	14	500	8.2	-5.5	-32.8	G(50)	32.0	3	15.0	1.300	1.000	13.7	< 41.6
16	22	node Left	2466	16	500	3.3	-4.8	-58.7	G(50)	32.0	3	15.0	1.300	1.000	8.1	< 41.6
16	22	node Right	2466	16	500	3.3	-4.8	-58.7	G(50)	32.0	3	15.0	1.300	1.000	8.1	< 41.6
17	23	node Left	2466	16	500	1.1	-5.6	-81.9	G(50)	32.0	3	15.0	1.300	1.000	6.6	< 41.6
17	23	node Right	2466	16	500	1.1	-5.6	-81.9	G(50)	32.0	3	15.0	1.300	1.000	6.6	< 41.6
17	24	node Left	2466	16	500	2.5	-4.4	-49.2	G(50)	32.0	3	15.0	1.300	1.000	6.9	< 41.6
17	24	node Right	2466	16	500	2.6	-4.4	-49.2	G(50)	32.0	3	15.0	1.300	1.000	7.0	< 41.6
18	25	node Left	2466	14	500	7.2	-5.7	-34.8	G(50)	32.0	3	15.0	1.300	1.000	12.9	< 41.6
18	25	node Right	2466	14	500	7.3	-5.8	-35.4	G(50)	32.0	3	15.0	1.300	1.000	13.1	< 41.6
19	26	node Left	2466	12	500	13.2	-6.6	1.1	G(50)	32.0	3	15.0	1.000	1.000	19.8	< 32.0

19	26 node Right	2466	12	500	13.2	-6.6	1.2	G(50)	32.0	3	15.0	1.000	1.000	19.8	<	32.0
19	27 node Left	2466	12	500	15.9	-5.6	37.7	G(50)	32.0	3	15.0	1.000	1.000	21.5	<	32.0
19	27 node Right	2466	12	500	20.0	-7.0	47.3	G(50)	32.0	3	15.0	1.000	1.000	27.0	<	32.0
20	28 node Left	2466	12	500	14.7	-3.9	51.5	G(50)	32.0	3	15.0	1.000	1.000	18.6	<	32.0
20	28 node Right	2466	12	500	14.7	-3.9	51.5	G(50)	32.0	3	15.0	1.000	1.000	18.6	<	32.0
21	29 node Left	2466	12	500	15.2	-3.2	61.6	G(50)	32.0	3	15.0	1.000	1.000	18.3	<	32.0
21	29 node Right	2466	12	500	15.2	-3.2	61.6	G(50)	32.0	3	15.0	1.000	1.000	18.3	<	32.0
21	30 node Left	2466	12	500	14.4	-2.4	61.7	G(50)	32.0	3	15.0	1.000	1.000	16.8	<	32.0
21	30 node Right	2466	12	500	14.4	-2.4	61.7	G(50)	32.0	3	15.0	1.000	1.000	16.8	<	32.0
22	31 node Left	2466	12	500	12.3	-1.6	51.7	G(50)	32.0	3	15.0	1.000	1.000	13.9	<	32.0
22	31 node Right	2466	12	500	12.3	-1.6	51.6	G(50)	32.0	3	15.0	1.000	1.000	13.9	<	32.0
23	32 node Left	2466	12	500	12.2	-1.3	47.2	G(50)	32.0	3	15.0	1.000	1.000	13.6	<	32.0
23	32 node Right	2466	12	500	12.2	-1.3	47.2	G(50)	32.0	3	15.0	1.000	1.000	13.5	<	32.0
23	33 node Left	2466	12	500	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.000	1.000	0.0	<	32.0

9-3 Checking of Fatigue Stress for Cross Beam

σ_{tmax} : Maximum stress (Including the effect of γ_a)
 σ_{tmin} : Minimum stress (Including the effect of γ_a)
 σ_d : Stress of Dead load (Including the effect of γ_a)
 $\Delta \sigma_{max}$: $\sigma_{tmax} - \sigma_{tmin}$
 C_0 : $2.0E+6 \cdot \Delta \sigma_f^{**m}$
 $\Delta \sigma_f$: $2.0E+6$ Allowable stress
 m : Slope constant
 CR : Correction coefficient for mean stress
 C_t : Correction factor for t

Structural analysis coefficient Cross Beam $\gamma_a = 0.500$

Maximum stress range checking $\Delta \sigma_{max} \leq \Delta \sigma_{ce} \cdot CR \cdot C_t$

Stress range cycles checking $D = \sum_i [\sum_j \{n_{ti} / (C_0 \cdot (CR \cdot C_t)^{**m} / \Delta \sigma_{ij}^{**m})\}] \leq 1$

node U.FLG-MAX (Upper Flange Max Stress)

node	Point	Flange	Stress range											
			t (mm)	σ_{tmax}	σ_{tmin} (N/mm2)	Grade		$\Delta \sigma_{ce m}$	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{ce} \cdot cyale$		D
						σ_d	$(\Delta \sigma_f)$					$\Delta \sigma_{max}$ (N/mm2)	CR · Ct (N/mm2)	
S1	1 Beam Left	16	14.6	-13.4	8.9 E (80)	62.0	3	29.0	1.000	1.000	28.0	< 62.0		
S1	1 Beam Right	16	13.4	-14.6	-8.9 E (80)	62.0	3	29.0	1.186	1.000	28.0	< 73.5		
S2	1 Beam Left	16	12.1	-15.7	-17.8 E (80)	62.0	3	29.0	1.300	1.000	27.8	< 80.6		
S2	1 Beam Right	16	15.8	-12.2	18.5 E (80)	62.0	3	29.0	1.000	1.000	28.0	< 62.0		
PF3	1 Beam Left	12	8.5	-8.4	3.9 E (80)	62.0	3	29.0	1.000	1.000	16.9	< 62.0		
PF3	1 Beam Right	12	8.3	-8.5	-4.2 E (80)	62.0	3	29.0	1.133	1.000	16.8	< 70.3		
PF4	1 Beam Left	12	8.4	-7.1	14.2 E (80)	62.0	3	29.0	1.000	1.000	15.5	< 62.0		
PF4	1 Beam Right	12	7.3	-8.1	-16.1 E (80)	62.0	3	29.0	1.300	1.000	15.4	< 80.6		
C1	1 Beam Left	12	4.0	-4.1	2.9 E (80)	62.0	3	29.0	1.000	1.000	8.1	< 62.0		
C1	1 Beam Right	12	3.8	-4.2	-2.7 E (80)	62.0	3	29.0	1.203	1.000	8.0	< 74.6		
C2	1 Beam Left	12	10.9	-10.8	-0.2 E (80)	62.0	3	29.0	1.004	1.000	21.6	< 62.2		
C2	1 Beam Right	12	11.0	-11.1	0.5 E (80)	62.0	3	29.0	1.000	1.000	22.1	< 62.0		
C3	1 Beam Left	12	12.7	-12.5	0.4 E (80)	62.0	3	29.0	1.000	1.000	25.2	< 62.0		
C3	1 Beam Right	12	12.7	-12.9	-0.1 E (80)	62.0	3	29.0	1.004	1.000	25.6	< 62.3		
C4	1 Beam Left	12	12.8	-12.2	1.6 E (80)	62.0	3	29.0	1.000	1.000	25.0	< 62.0		
C4	1 Beam Right	12	12.4	-12.9	-1.3 E (80)	62.0	3	29.0	1.030	1.000	25.4	< 63.8		
C5	1 Beam Left	12	12.1	-11.6	0.4 E (80)	62.0	3	29.0	1.000	1.000	23.7	< 62.0		
C5	1 Beam Right	12	11.7	-12.2	-0.2 E (80)	62.0	3	29.0	1.010	1.000	23.9	< 62.6		
C6	1 Beam Left	12	11.0	-10.9	-2.2 E (80)	62.0	3	29.0	1.048	1.000	21.9	< 65.0		
C6	1 Beam Right	12	11.0	-11.1	2.4 E (80)	62.0	3	29.0	1.000	1.000	22.0	< 62.0		
C7	1 Beam Left	12	10.2	-10.4	-4.7 E (80)	62.0	3	29.0	1.121	1.000	20.5	< 69.5		
C7	1 Beam Right	12	10.4	-10.2	4.8 E (80)	62.0	3	29.0	1.000	1.000	20.7	< 62.0		
C8	1 Beam Left	12	7.4	-7.4	-3.2 E (80)	62.0	3	29.0	1.110	1.000	14.9	< 68.8		
C8	1 Beam Right	12	7.5	-7.5	3.2 E (80)	62.0	3	29.0	1.000	1.000	15.0	< 62.0		
C9	1 Beam Left	12	6.7	-7.4	0.8 E (80)	62.0	3	29.0	1.000	1.000	14.1	< 62.0		
C9	1 Beam Right	12	7.4	-6.7	-0.9 E (80)	62.0	3	29.0	1.018	1.000	14.1	< 63.1		
C10	1 Beam Left	12	7.4	-6.3	2.8 E (80)	62.0	3	29.0	1.000	1.000	13.7	< 62.0		
C10	1 Beam Right	12	6.3	-7.4	-3.0 E (80)	62.0	3	29.0	1.137	1.000	13.7	< 70.5		
C11	1 Beam Left	12	8.3	-8.9	1.8 E (80)	62.0	3	29.0	1.000	1.000	17.2	< 62.0		
C11	1 Beam Right	12	8.8	-8.2	-1.6 E (80)	62.0	3	29.0	1.038	1.000	16.9	< 64.3		
C12	1 Beam Left	12	11.0	-11.4	0.8 E (80)	62.0	3	29.0	1.000	1.000	22.5	< 62.0		
C12	1 Beam Right	12	11.3	-10.9	-0.7 E (80)	62.0	3	29.0	1.010	1.000	22.2	< 62.6		
C13	1 Beam Left	12	11.3	-12.0	-1.2 E (80)	62.0	3	29.0	1.031	1.000	23.2	< 63.9		
C13	1 Beam Right	12	11.8	-11.1	1.7 E (80)	62.0	3	29.0	1.000	1.000	22.9	< 62.0		
C14	1 Beam Left	12	11.7	-12.6	-2.0 E (80)	62.0	3	29.0	1.049	1.000	24.3	< 65.0		
C14	1 Beam Right	12	12.4	-11.4	2.9 E (80)	62.0	3	29.0	1.000	1.000	23.8	< 62.0		
C15	1 Beam Left	12	12.0	-12.8	-2.5 E (80)	62.0	3	29.0	1.058	1.000	24.8	< 65.6		
C15	1 Beam Right	12	12.6	-11.6	3.4 E (80)	62.0	3	29.0	1.000	1.000	24.2	< 62.0		
C16	1 Beam Left	12	11.7	-12.6	-2.9 E (80)	62.0	3	29.0	1.067	1.000	24.3	< 66.2		
C16	1 Beam Right	12	12.4	-11.3	3.6 E (80)	62.0	3	29.0	1.000	1.000	23.7	< 62.0		
C17	1 Beam Left	12	11.2	-12.0	-2.9 E (80)	62.0	3	29.0	1.071	1.000	23.2	< 66.4		
C17	1 Beam Right	12	11.9	-10.9	3.2 E (80)	62.0	3	29.0	1.000	1.000	22.7	< 62.0		
C18	1 Beam Left	12	10.9	-11.4	-0.5 E (80)	62.0	3	29.0	1.015	1.000	22.3	< 62.9		
C18	1 Beam Right	12	11.2	-10.7	-0.0 E (80)	62.0	3	29.0	1.000	1.000	21.9	< 62.0		
C19	1 Beam Left	12	8.5	-8.5	3.0 E (80)	62.0	3	29.0	1.000	1.000	17.0	< 62.0		
C19	1 Beam Right	12	8.4	-8.3	-4.4 E (80)	62.0	3	29.0	1.135	1.000	16.7	< 70.4		
C20	1 Beam Left	12	7.0	-6.8	8.8 E (80)	62.0	3	29.0	1.000	1.000	13.8	< 62.0		
C20	1 Beam Right	12	6.5	-6.9	-10.6 E (80)	62.0	3	29.0	1.300	1.000	13.3	< 80.6		
C21	1 Beam Left	12	7.6	-6.7	11.1 E (80)	62.0	3	29.0	1.000	1.000	14.2	< 62.0		
C21	1 Beam Right	12	6.4	-7.4	-12.9 E (80)	62.0	3	29.0	1.300	1.000	13.8	< 80.6		
C22	1 Beam Left	12	7.2	-7.6	5.0 E (80)	62.0	3	29.0	1.000	1.000	14.8	< 62.0		
C22	1 Beam Right	12	7.5	-7.0	-6.4 E (80)	62.0	3	29.0	1.243	1.000	14.5	< 77.1		

C23	1 Beam Left	12	10.2	-10.5	1.0 E (80)	62.0	3	29.0	1.000	1.000	20.7 < 62.0
C23	1 Beam Right	12	10.4	-9.9	-1.8 E (80)	62.0	3	29.0	1.038	1.000	20.3 < 64.4
C24	1 Beam Left	12	10.8	-11.3	-2.1 E (80)	62.0	3	29.0	1.052	1.000	22.1 < 65.2
C24	1 Beam Right	12	11.1	-10.4	2.6 E (80)	62.0	3	29.0	1.000	1.000	21.5 < 62.0
C25	1 Beam Left	12	11.7	-12.3	-1.5 E (80)	62.0	3	29.0	1.036	1.000	24.0 < 64.3
C25	1 Beam Right	12	12.1	-11.2	2.6 E (80)	62.0	3	29.0	1.000	1.000	23.3 < 62.0
C26	1 Beam Left	12	12.5	-13.0	-0.7 E (80)	62.0	3	29.0	1.018	1.000	25.5 < 63.1
C26	1 Beam Right	12	12.8	-11.9	2.3 E (80)	62.0	3	29.0	1.000	1.000	24.7 < 62.0
C27	1 Beam Left	12	12.5	-13.3	-1.9 E (80)	62.0	3	29.0	1.043	1.000	25.8 < 64.7
C27	1 Beam Right	12	13.0	-11.9	3.6 E (80)	62.0	3	29.0	1.000	1.000	24.9 < 62.0
C28	1 Beam Left	12	10.5	-11.7	-3.6 E (80)	62.0	3	29.0	1.096	1.000	22.3 < 68.0
C28	1 Beam Right	12	11.4	-9.8	5.5 E (80)	62.0	3	29.0	1.000	1.000	21.2 < 62.0
C29	1 Beam Left	12	4.0	-4.7	-7.2 E (80)	62.0	3	29.0	1.300	1.000	8.7 < 80.6
C29	1 Beam Right	12	4.9	-3.4	8.9 E (80)	62.0	3	29.0	1.000	1.000	8.3 < 62.0

node L.FLG-MAX (Lower flange Max Stress)

	Point	Flange	Grade						Stress range				
			t	σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce m}$	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{ce} \cdot Ct$	CR \cdot Ct
S1	1 Beam Left	16	13.4	-14.6	-8.9	E (80)	62.0	3	29.0	1.186	1.000	28.0	< 73.5
S1	1 Beam Right	16	14.6	-13.4	8.9	E (80)	62.0	3	29.0	1.000	1.000	28.0	< 62.0
S2	1 Beam Left	16	15.7	-12.1	17.8	E (80)	62.0	3	29.0	1.000	1.000	27.8	< 62.0
S2	1 Beam Right	16	12.2	-15.8	-18.5	E (80)	62.0	3	29.0	1.300	1.000	28.0	< 80.6
PF3	1 Beam Left	12	8.4	-8.5	-3.9	E (80)	62.0	3	29.0	1.120	1.000	16.9	< 69.4
PF3	1 Beam Right	12	8.5	-8.3	4.2	E (80)	62.0	3	29.0	1.000	1.000	16.8	< 62.0
PF4	1 Beam Left	12	7.1	-8.4	-14.2	E (80)	62.0	3	29.0	1.300	1.000	15.5	< 80.6
PF4	1 Beam Right	12	8.1	-7.3	16.1	E (80)	62.0	3	29.0	1.000	1.000	15.4	< 62.0
C1	1 Beam Left	12	4.1	-4.0	-2.9	E (80)	62.0	3	29.0	1.198	1.000	8.1	< 74.3
C1	1 Beam Right	12	4.2	-3.8	2.7	E (80)	62.0	3	29.0	1.000	1.000	8.0	< 62.0
C2	1 Beam Left	12	10.8	-10.9	0.2	E (80)	62.0	3	29.0	1.000	1.000	21.6	< 62.0
C2	1 Beam Right	12	11.1	-11.0	-0.5	E (80)	62.0	3	29.0	1.010	1.000	22.1	< 62.7
C3	1 Beam Left	12	12.5	-12.7	-0.4	E (80)	62.0	3	29.0	1.010	1.000	25.2	< 62.6
C3	1 Beam Right	12	12.9	-12.7	0.1	E (80)	62.0	3	29.0	1.000	1.000	25.6	< 62.0
C4	1 Beam Left	12	12.2	-12.8	-1.6	E (80)	62.0	3	29.0	1.035	1.000	25.0	< 64.2
C4	1 Beam Right	12	12.9	-12.4	1.3	E (80)	62.0	3	29.0	1.000	1.000	25.4	< 62.0
C5	1 Beam Left	12	11.6	-12.1	-0.4	E (80)	62.0	3	29.0	1.014	1.000	23.7	< 62.9
C5	1 Beam Right	12	12.2	-11.7	0.2	E (80)	62.0	3	29.0	1.000	1.000	23.9	< 62.0
C6	1 Beam Left	12	10.9	-11.0	2.2	E (80)	62.0	3	29.0	1.000	1.000	21.9	< 62.0
C6	1 Beam Right	12	11.1	-11.0	-2.4	E (80)	62.0	3	29.0	1.052	1.000	22.0	< 65.2
C7	1 Beam Left	12	10.4	-10.2	4.7	E (80)	62.0	3	29.0	1.000	1.000	20.5	< 62.0
C7	1 Beam Right	12	10.2	-10.4	-4.8	E (80)	62.0	3	29.0	1.124	1.000	20.7	< 69.7
C8	1 Beam Left	12	7.4	-7.4	3.2	E (80)	62.0	3	29.0	1.000	1.000	14.9	< 62.0
C8	1 Beam Right	12	7.5	-7.5	-3.2	E (80)	62.0	3	29.0	1.109	1.000	15.0	< 68.8
C9	1 Beam Left	12	7.4	-6.7	-0.8	E (80)	62.0	3	29.0	1.015	1.000	14.1	< 62.9
C9	1 Beam Right	12	6.7	-7.4	0.9	E (80)	62.0	3	29.0	1.000	1.000	14.1	< 62.0
C10	1 Beam Left	12	6.3	-7.4	-2.8	E (80)	62.0	3	29.0	1.128	1.000	13.7	< 69.9
C10	1 Beam Right	12	7.4	-6.3	3.0	E (80)	62.0	3	29.0	1.000	1.000	13.7	< 62.0
C11	1 Beam Left	12	8.9	-8.3	-1.8	E (80)	62.0	3	29.0	1.041	1.000	17.2	< 64.5
C11	1 Beam Right	12	8.2	-8.8	1.6	E (80)	62.0	3	29.0	1.000	1.000	16.9	< 62.0
C12	1 Beam Left	12	11.4	-11.0	-0.8	E (80)	62.0	3	29.0	1.014	1.000	22.5	< 62.9
C12	1 Beam Right	12	10.9	-11.3	0.7	E (80)	62.0	3	29.0	1.000	1.000	22.2	< 62.0
C13	1 Beam Left	12	12.0	-11.3	1.2	E (80)	62.0	3	29.0	1.000	1.000	23.2	< 62.0
C13	1 Beam Right	12	11.1	-11.8	-1.7	E (80)	62.0	3	29.0	1.045	1.000	22.9	< 64.8
C14	1 Beam Left	12	12.6	-11.7	2.0	E (80)	62.0	3	29.0	1.000	1.000	24.3	< 62.0
C14	1 Beam Right	12	11.4	-12.4	-2.9	E (80)	62.0	3	29.0	1.070	1.000	23.8	< 66.3
C15	1 Beam Left	12	12.8	-12.0	2.5	E (80)	62.0	3	29.0	1.000	1.000	24.8	< 62.0
C15	1 Beam Right	12	11.6	-12.6	-3.4	E (80)	62.0	3	29.0	1.081	1.000	24.2	< 67.0
C16	1 Beam Left	12	12.6	-11.7	2.9	E (80)	62.0	3	29.0	1.000	1.000	24.3	< 62.0
C16	1 Beam Right	12	11.3	-12.4	-3.6	E (80)	62.0	3	29.0	1.089	1.000	23.7	< 67.5
C17	1 Beam Left	12	12.0	-11.2	2.9	E (80)	62.0	3	29.0	1.000	1.000	23.2	< 62.0
C17	1 Beam Right	12	10.9	-11.9	-3.2	E (80)	62.0	3	29.0	1.081	1.000	22.7	< 67.0
C18	1 Beam Left	12	11.4	-10.9	0.5	E (80)	62.0	3	29.0	1.000	1.000	22.3	< 62.0
C18	1 Beam Right	12	10.7	-11.2	0.0	E (80)	62.0	3	29.0	1.005	1.000	21.9	< 62.3
C19	1 Beam Left	12	8.5	-8.5	-3.0	E (80)	62.0	3	29.0	1.089	1.000	17.0	< 67.5
C19	1 Beam Right	12	8.3	-8.4	4.4	E (80)	62.0	3	29.0	1.000	1.000	16.7	< 62.0
C20	1 Beam Left	12	6.8	-7.0	-8.8	E (80)	62.0	3	29.0	1.300	1.000	13.8	< 80.6
C20	1 Beam Right	12	6.9	-6.5	10.6	E (80)	62.0	3	29.0	1.000	1.000	13.3	< 62.0
C21	1 Beam Left	12	6.7	-7.6	-11.1	E (80)	62.0	3	29.0	1.300	1.000	14.2	< 80.6
C21	1 Beam Right	12	7.4	-6.4	12.9	E (80)	62.0	3	29.0	1.000	1.000	13.8	< 62.0
C22	1 Beam Left	12	7.6	-7.2	-5.0	E (80)	62.0	3	29.0	1.175	1.000	14.8	< 72.8
C22	1 Beam Right	12	7.0	-7.5	6.4	E (80)	62.0	3	29.0	1.000	1.000	14.5	< 62.0

C23	1 Beam Left	12	10.5	-10.2	-1.0 E (80)	62.0	3	29.0	1.020	1.000	20.7 < 63.2
C23	1 Beam Right	12	9.9	-10.4	1.8 E (80)	62.0	3	29.0	1.000	1.000	20.3 < 62.0
C24	1 Beam Left	12	11.3	-10.8	2.1 E (80)	62.0	3	29.0	1.000	1.000	22.1 < 62.0
C24	1 Beam Right	12	10.4	-11.1	-2.6 E (80)	62.0	3	29.0	1.068	1.000	21.5 < 66.2
C25	1 Beam Left	12	12.3	-11.7	1.5 E (80)	62.0	3	29.0	1.000	1.000	24.0 < 62.0
C25	1 Beam Right	12	11.2	-12.1	-2.6 E (80)	62.0	3	29.0	1.066	1.000	23.3 < 66.1
C26	1 Beam Left	12	13.0	-12.5	0.7 E (80)	62.0	3	29.0	1.000	1.000	25.5 < 62.0
C26	1 Beam Right	12	11.9	-12.8	-2.3 E (80)	62.0	3	29.0	1.053	1.000	24.7 < 65.3
C27	1 Beam Left	12	13.3	-12.5	1.9 E (80)	62.0	3	29.0	1.000	1.000	25.8 < 62.0
C27	1 Beam Right	12	11.9	-13.0	-3.6 E (80)	62.0	3	29.0	1.085	1.000	24.9 < 67.2
C28	1 Beam Left	12	11.7	-10.5	3.6 E (80)	62.0	3	29.0	1.000	1.000	22.3 < 62.0
C28	1 Beam Right	12	9.8	-11.4	-5.5 E (80)	62.0	3	29.0	1.159	1.000	21.2 < 71.8
C29	1 Beam Left	12	4.7	-4.0	7.2 E (80)	62.0	3	29.0	1.000	1.000	8.7 < 62.0
C29	1 Beam Right	12	3.4	-4.9	-8.9 E (80)	62.0	3	29.0	1.300	1.000	8.3 < 80.6

node WEB-U-1 (Web Upper Edge) WEB - 1

cycle	Point	webe		Grade					Stress range							
		t	σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce m}$	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D			
S1	1 beam Left	1784	16	0	14.3	-13.1	8.7	E(80)	62.0	3	29.0	1.000	1.000	27.5	< 62.0	
S1	1 beam Right	1784	16	0	13.2	-14.4	-8.7	E(80)	62.0	3	29.0	1.186	1.000	27.5	< 73.5	
S2	1 beam Left	1784	16	0	11.9	-15.4	-17.5	E(80)	62.0	3	29.0	1.300	1.000	27.3	< 80.6	
S2	1 beam Right	1784	16	0	15.6	-12.0	18.2	E(80)	62.0	3	29.0	1.000	1.000	27.5	< 62.0	
PF3	1 beam Left	1788	12	0	8.4	-8.3	3.9	E(80)	62.0	3	29.0	1.000	1.000	16.7	< 62.0	
PF3	1 beam Right	1788	12	0	8.2	-8.4	-4.1	E(80)	62.0	3	29.0	1.133	1.000	16.6	< 70.3	
PF4	1 beam Left	1788	12	0	8.3	-7.0	14.0	E(80)	62.0	3	29.0	1.000	1.000	15.3	< 62.0	
PF4	1 beam Right	1788	12	0	7.2	-8.0	-15.9	E(80)	62.0	3	29.0	1.300	1.000	15.2	< 80.6	
C1	1 beam Left	1788	12	0	3.9	-4.0	2.9	E(80)	62.0	3	29.0	1.000	1.000	7.9	< 62.0	
C1	1 beam Right	1788	12	0	3.8	-4.1	-2.7	E(80)	62.0	3	29.0	1.203	1.000	7.9	< 74.6	
C2	1 beam Left	1788	12	0	10.7	-10.6	-0.2	E(80)	62.0	3	29.0	1.004	1.000	21.4	< 62.2	
C2	1 beam Right	1788	12	0	10.9	-10.9	0.5	E(80)	62.0	3	29.0	1.000	1.000	21.8	< 62.0	
C3	1 beam Left	1788	12	0	12.6	-12.3	0.4	E(80)	62.0	3	29.0	1.000	1.000	24.9	< 62.0	
C3	1 beam Right	1788	12	0	12.6	-12.8	-0.1	E(80)	62.0	3	29.0	1.004	1.000	25.3	< 62.3	
C4	1 beam Left	1788	12	0	12.6	-12.1	1.5	E(80)	62.0	3	29.0	1.000	1.000	24.7	< 62.0	
C4	1 beam Right	1788	12	0	12.2	-12.8	-1.3	E(80)	62.0	3	29.0	1.030	1.000	25.0	< 63.8	
C5	1 beam Left	1788	12	0	12.0	-11.4	0.4	E(80)	62.0	3	29.0	1.000	1.000	23.4	< 62.0	
C5	1 beam Right	1788	12	0	11.6	-12.1	-0.2	E(80)	62.0	3	29.0	1.010	1.000	23.6	< 62.6	
C6	1 beam Left	1788	12	0	10.8	-10.7	-2.2	E(80)	62.0	3	29.0	1.048	1.000	21.6	< 65.0	
C6	1 beam Right	1788	12	0	10.8	-10.9	2.4	E(80)	62.0	3	29.0	1.000	1.000	21.8	< 62.0	
C7	1 beam Left	1788	12	0	10.0	-10.2	-4.6	E(80)	62.0	3	29.0	1.121	1.000	20.3	< 69.5	
C7	1 beam Right	1788	12	0	10.3	-10.1	4.8	E(80)	62.0	3	29.0	1.000	1.000	20.4	< 62.0	
C8	1 beam Left	1788	12	0	7.3	-7.3	-3.2	E(80)	62.0	3	29.0	1.110	1.000	14.7	< 68.8	
C8	1 beam Right	1788	12	0	7.4	-7.4	3.2	E(80)	62.0	3	29.0	1.000	1.000	14.8	< 62.0	
C9	1 beam Left	1788	12	0	6.6	-7.3	0.8	E(80)	62.0	3	29.0	1.000	1.000	13.9	< 62.0	
C9	1 beam Right	1788	12	0	7.3	-6.6	-0.9	E(80)	62.0	3	29.0	1.018	1.000	13.9	< 63.1	
C10	1 beam Left	1788	12	0	7.3	-6.2	2.8	E(80)	62.0	3	29.0	1.000	1.000	13.5	< 62.0	
C10	1 beam Right	1788	12	0	6.2	-7.3	-3.0	E(80)	62.0	3	29.0	1.137	1.000	13.5	< 70.5	
C11	1 beam Left	1788	12	0	8.2	-8.8	1.7	E(80)	62.0	3	29.0	1.000	1.000	17.0	< 62.0	
C11	1 beam Right	1788	12	0	8.6	-8.1	-1.6	E(80)	62.0	3	29.0	1.038	1.000	16.7	< 64.3	
C12	1 beam Left	1788	12	0	10.9	-11.3	0.8	E(80)	62.0	3	29.0	1.000	1.000	22.1	< 62.0	
C12	1 beam Right	1788	12	0	11.1	-10.7	-0.7	E(80)	62.0	3	29.0	1.010	1.000	21.9	< 62.6	
C13	1 beam Left	1788	12	0	11.1	-11.8	-1.2	E(80)	62.0	3	29.0	1.031	1.000	22.9	< 63.9	
C13	1 beam Right	1788	12	0	11.7	-10.9	1.7	E(80)	62.0	3	29.0	1.000	1.000	22.6	< 62.0	
C14	1 beam Left	1788	12	0	11.6	-12.4	-2.0	E(80)	62.0	3	29.0	1.049	1.000	24.0	< 65.0	
C14	1 beam Right	1788	12	0	12.2	-11.2	2.8	E(80)	62.0	3	29.0	1.000	1.000	23.5	< 62.0	
C15	1 beam Left	1788	12	0	11.8	-12.6	-2.5	E(80)	62.0	3	29.0	1.058	1.000	24.4	< 65.6	
C15	1 beam Right	1788	12	0	12.5	-11.4	3.4	E(80)	62.0	3	29.0	1.000	1.000	23.9	< 62.0	
C16	1 beam Left	1788	12	0	11.6	-12.4	-2.8	E(80)	62.0	3	29.0	1.067	1.000	24.0	< 66.2	
C16	1 beam Right	1788	12	0	12.2	-11.2	3.6	E(80)	62.0	3	29.0	1.000	1.000	23.4	< 62.0	
C17	1 beam Left	1788	12	0	11.1	-11.9	-2.9	E(80)	62.0	3	29.0	1.071	1.000	22.9	< 66.4	
C17	1 beam Right	1788	12	0	11.7	-10.7	3.1	E(80)	62.0	3	29.0	1.000	1.000	22.4	< 62.0	
C18	1 beam Left	1788	12	0	10.8	-11.2	-0.5	E(80)	62.0	3	29.0	1.015	1.000	22.0	< 62.9	
C18	1 beam Right	1788	12	0	11.1	-10.5	-0.0	E(80)	62.0	3	29.0	1.000	1.000	21.6	< 62.0	
C19	1 beam Left	1788	12	0	8.4	-8.4	3.0	E(80)	62.0	3	29.0	1.000	1.000	16.8	< 62.0	
C19	1 beam Right	1788	12	0	8.3	-8.2	-4.3	E(80)	62.0	3	29.0	1.135	1.000	16.5	< 70.4	
C20	1 beam Left	1788	12	0	7.0	-6.7	8.7	E(80)	62.0	3	29.0	1.000	1.000	13.6	< 62.0	
C20	1 beam Right	1788	12	0	6.4	-6.8	-10.5	E(80)	62.0	3	29.0	1.300	1.000	13.2	< 80.6	
C21	1 beam Left	1788	12	0	7.5	-6.6	10.9	E(80)	62.0	3	29.0	1.000	1.000	14.0	< 62.0	
C21	1 beam Right	1788	12	0	6.3	-7.3	-12.7	E(80)	62.0	3	29.0	1.300	1.000	13.6	< 80.6	
C22	1 beam Left	1788	12	0	7.1	-7.5	4.9	E(80)	62.0	3	29.0	1.000	1.000	14.6	< 62.0	

C22	1 beam Right	1788	12	0	7.4	-6.9	-6.3	E(80)	62.0	3	29.0	1.243	1.000	14.3<	77.1
C23	1 beam Left	1788	12	0	10.0	-10.4	1.0	E(80)	62.0	3	29.0	1.000	1.000	20.4<	62.0
C23	1 beam Right	1788	12	0	10.2	-9.8	-1.8	E(80)	62.0	3	29.0	1.038	1.000	20.0<	64.4
C24	1 beam Left	1788	12	0	10.6	-11.2	-2.0	E(80)	62.0	3	29.0	1.052	1.000	21.8<	65.2
C24	1 beam Right	1788	12	0	11.0	-10.2	2.5	E(80)	62.0	3	29.0	1.000	1.000	21.2<	62.0
C25	1 beam Left	1788	12	0	11.5	-12.2	-1.5	E(80)	62.0	3	29.0	1.036	1.000	23.7<	64.3
C25	1 beam Right	1788	12	0	12.0	-11.0	2.6	E(80)	62.0	3	29.0	1.000	1.000	23.0<	62.0
C26	1 beam Left	1788	12	0	12.3	-12.8	-0.7	E(80)	62.0	3	29.0	1.018	1.000	25.1<	63.1
C26	1 beam Right	1788	12	0	12.6	-11.8	2.2	E(80)	62.0	3	29.0	1.000	1.000	24.4<	62.0
C27	1 beam Left	1788	12	0	12.3	-13.1	-1.9	E(80)	62.0	3	29.0	1.043	1.000	25.4<	64.7
C27	1 beam Right	1788	12	0	12.9	-11.7	3.6	E(80)	62.0	3	29.0	1.000	1.000	24.6<	62.0
C28	1 beam Left	1788	12	0	10.4	-11.6	-3.6	E(80)	62.0	3	29.0	1.096	1.000	22.0<	67.9
C28	1 beam Right	1788	12	0	11.2	-9.7	5.4	E(80)	62.0	3	29.0	1.000	1.000	20.9<	62.0
C29	1 beam Left	1788	12	0	4.0	-4.6	-7.1	E(80)	62.0	3	29.0	1.300	1.000	8.6<	80.6
C29	1 beam Right	1788	12	0	4.9	-3.4	8.8	E(80)	62.0	3	29.0	1.000	1.000	8.2<	62.0

node WEB-L-1 (Web lower Edge) WEB - 1

cycle	Point	webe	Grade										Stress range		
			t	σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce m}$	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D	
S1	1 beam Left	1784 16	0	13.1	-14.3	-8.7	E(80)	62.0	3	29.0	1.186	1.000	27.5	< 73.5	
S1	1 beam Right	1784 16	0	14.4	-13.2	8.7	E(80)	62.0	3	29.0	1.000	1.000	27.5	< 62.0	
S2	1 beam Left	1784 16	0	15.4	-11.9	17.5	E(80)	62.0	3	29.0	1.000	1.000	27.3	< 62.0	
S2	1 beam Right	1784 16	0	12.0	-15.6	-18.2	E(80)	62.0	3	29.0	1.300	1.000	27.5	< 80.6	
PF3	1 beam Left	1788 12	0	8.3	-8.4	-3.9	E(80)	62.0	3	29.0	1.120	1.000	16.7	< 69.4	
PF3	1 beam Right	1788 12	0	8.4	-8.2	4.1	E(80)	62.0	3	29.0	1.000	1.000	16.6	< 62.0	
PF4	1 beam Left	1788 12	0	7.0	-8.3	-14.0	E(80)	62.0	3	29.0	1.300	1.000	15.3	< 80.6	
PF4	1 beam Right	1788 12	0	8.0	-7.2	15.9	E(80)	62.0	3	29.0	1.000	1.000	15.2	< 62.0	
C1	1 beam Left	1788 12	0	4.0	-3.9	-2.9	E(80)	62.0	3	29.0	1.198	1.000	7.9	< 74.3	
C1	1 beam Right	1788 12	0	4.1	-3.8	2.7	E(80)	62.0	3	29.0	1.000	1.000	7.9	< 62.0	
C2	1 beam Left	1788 12	0	10.6	-10.7	0.2	E(80)	62.0	3	29.0	1.000	1.000	21.4	< 62.0	
C2	1 beam Right	1788 12	0	10.9	-10.9	-0.5	E(80)	62.0	3	29.0	1.010	1.000	21.8	< 62.6	
C3	1 beam Left	1788 12	0	12.3	-12.6	-0.4	E(80)	62.0	3	29.0	1.010	1.000	24.9	< 62.6	
C3	1 beam Right	1788 12	0	12.8	-12.6	0.1	E(80)	62.0	3	29.0	1.000	1.000	25.3	< 62.0	
C4	1 beam Left	1788 12	0	12.1	-12.6	-1.5	E(80)	62.0	3	29.0	1.035	1.000	24.7	< 64.2	
C4	1 beam Right	1788 12	0	12.8	-12.2	1.3	E(80)	62.0	3	29.0	1.000	1.000	25.0	< 62.0	
C5	1 beam Left	1788 12	0	11.4	-12.0	-0.4	E(80)	62.0	3	29.0	1.014	1.000	23.4	< 62.9	
C5	1 beam Right	1788 12	0	12.1	-11.6	0.2	E(80)	62.0	3	29.0	1.000	1.000	23.6	< 62.0	
C6	1 beam Left	1788 12	0	10.7	-10.8	2.2	E(80)	62.0	3	29.0	1.000	1.000	21.6	< 62.0	
C6	1 beam Right	1788 12	0	10.9	-10.8	-2.4	E(80)	62.0	3	29.0	1.052	1.000	21.8	< 65.2	
C7	1 beam Left	1788 12	0	10.2	-10.0	4.6	E(80)	62.0	3	29.0	1.000	1.000	20.3	< 62.0	
C7	1 beam Right	1788 12	0	10.1	-10.3	-4.8	E(80)	62.0	3	29.0	1.124	1.000	20.4	< 69.7	
C8	1 beam Left	1788 12	0	7.3	-7.3	3.2	E(80)	62.0	3	29.0	1.000	1.000	14.7	< 62.0	
C8	1 beam Right	1788 12	0	7.4	-7.4	-3.2	E(80)	62.0	3	29.0	1.109	1.000	14.8	< 68.8	
C9	1 beam Left	1788 12	0	7.3	-6.6	-0.8	E(80)	62.0	3	29.0	1.015	1.000	13.9	< 62.9	
C9	1 beam Right	1788 12	0	6.6	-7.3	0.9	E(80)	62.0	3	29.0	1.000	1.000	13.9	< 62.0	
C10	1 beam Left	1788 12	0	6.2	-7.3	-2.8	E(80)	62.0	3	29.0	1.128	1.000	13.5	< 69.9	
C10	1 beam Right	1788 12	0	7.3	-6.2	3.0	E(80)	62.0	3	29.0	1.000	1.000	13.5	< 62.0	
C11	1 beam Left	1788 12	0	8.8	-8.2	-1.7	E(80)	62.0	3	29.0	1.041	1.000	17.0	< 64.5	
C11	1 beam Right	1788 12	0	8.1	-8.6	1.6	E(80)	62.0	3	29.0	1.000	1.000	16.7	< 62.0	
C12	1 beam Left	1788 12	0	11.3	-10.9	-0.8	E(80)	62.0	3	29.0	1.014	1.000	22.1	< 62.9	
C12	1 beam Right	1788 12	0	10.7	-11.1	0.7	E(80)	62.0	3	29.0	1.000	1.000	21.9	< 62.0	
C13	1 beam Left	1788 12	0	11.8	-11.1	1.2	E(80)	62.0	3	29.0	1.000	1.000	22.9	< 62.0	
C13	1 beam Right	1788 12	0	10.9	-11.7	-1.7	E(80)	62.0	3	29.0	1.044	1.000	22.6	< 64.8	
C14	1 beam Left	1788 12	0	12.4	-11.6	2.0	E(80)	62.0	3	29.0	1.000	1.000	24.0	< 62.0	
C14	1 beam Right	1788 12	0	11.2	-12.2	-2.8	E(80)	62.0	3	29.0	1.070	1.000	23.5	< 66.3	
C15	1 beam Left	1788 12	0	12.6	-11.8	2.5	E(80)	62.0	3	29.0	1.000	1.000	24.4	< 62.0	
C15	1 beam Right	1788 12	0	11.4	-12.5	-3.4	E(80)	62.0	3	29.0	1.081	1.000	23.9	< 67.0	
C16	1 beam Left	1788 12	0	12.4	-11.6	2.8	E(80)	62.0	3	29.0	1.000	1.000	24.0	< 62.0	
C16	1 beam Right	1788 12	0	11.2	-12.2	-3.6	E(80)	62.0	3	29.0	1.089	1.000	23.4	< 67.5	
C17	1 beam Left	1788 12	0	11.9	-11.1	2.9	E(80)	62.0	3	29.0	1.000	1.000	22.9	< 62.0	
C17	1 beam Right	1788 12	0	10.7	-11.7	-3.1	E(80)	62.0	3	29.0	1.081	1.000	22.4	< 67.0	
C18	1 beam Left	1788 12	0	11.2	-10.8	0.5	E(80)	62.0	3	29.0	1.000	1.000	22.0	< 62.0	
C18	1 beam Right	1788 12	0	10.5	-11.1	0.0	E(80)	62.0	3	29.0	1.005	1.000	21.6	< 62.3	
C19	1 beam Left	1788 12	0	8.4	-8.4	-3.0	E(80)	62.0	3	29.0	1.089	1.000	16.8	< 67.5	
C19	1 beam Right	1788 12	0	8.2	-8.3	4.3	E(80)	62.0	3	29.0	1.000	1.000	16.5	< 62.0	
C20	1 beam Left	1788 12	0	6.7	-7.0	-8.7	E(80)	62.0	3	29.0	1.300	1.000	13.6	< 80.6	
C20	1 beam Right	1788 12	0	6.8	-6.4	10.5	E(80)	62.0	3	29.0	1.000	1.000	13.2	< 62.0	
C21	1 beam Left	1788 12	0	6.6	-7.5	-10.9	E(80)	62.0	3	29.0	1.300	1.000	14.0	< 80.6	
C21	1 beam Right	1788 12	0	7.3	-6.3	12.7	E(80)	62.0	3	29.0	1.000	1.000	13.6	< 62.0	
C22	1 beam Left	1788 12	0	7.5	-7.1	-4.9	E(80)	62.0	3	29.0	1.175	1.000	14.6	< 72.8	

C22	1 beam Right	1788	12	0	6.9	-7.4	6.3	E(80)	62.0	3	29.0	1.000	1.000	14.3	<	62.0
C23	1 beam Left	1788	12	0	10.4	-10.0	-1.0	E(80)	62.0	3	29.0	1.020	1.000	20.4	<	63.2
C23	1 beam Right	1788	12	0	9.8	-10.2	1.8	E(80)	62.0	3	29.0	1.000	1.000	20.0	<	62.0
C24	1 beam Left	1788	12	0	11.2	-10.6	2.0	E(80)	62.0	3	29.0	1.000	1.000	21.8	<	62.0
C24	1 beam Right	1788	12	0	10.2	-11.0	-2.5	E(80)	62.0	3	29.0	1.068	1.000	21.2	<	66.2
C25	1 beam Left	1788	12	0	12.2	-11.5	1.5	E(80)	62.0	3	29.0	1.000	1.000	23.7	<	62.0
C25	1 beam Right	1788	12	0	11.0	-12.0	-2.6	E(80)	62.0	3	29.0	1.066	1.000	23.0	<	66.1
C26	1 beam Left	1788	12	0	12.8	-12.3	0.7	E(80)	62.0	3	29.0	1.000	1.000	25.1	<	62.0
C26	1 beam Right	1788	12	0	11.8	-12.6	-2.2	E(80)	62.0	3	29.0	1.053	1.000	24.4	<	65.3
C27	1 beam Left	1788	12	0	13.1	-12.3	1.9	E(80)	62.0	3	29.0	1.000	1.000	25.4	<	62.0
C27	1 beam Right	1788	12	0	11.7	-12.9	-3.6	E(80)	62.0	3	29.0	1.085	1.000	24.6	<	67.2
C28	1 beam Left	1788	12	0	11.6	-10.4	3.6	E(80)	62.0	3	29.0	1.000	1.000	22.0	<	62.0
C28	1 beam Right	1788	12	0	9.7	-11.2	-5.4	E(80)	62.0	3	29.0	1.159	1.000	20.9	<	71.8
C29	1 beam Left	1788	12	0	4.6	-4.0	7.1	E(80)	62.0	3	29.0	1.000	1.000	8.6	<	62.0
C29	1 beam Right	1788	12	0	3.4	-4.9	-8.8	E(80)	62.0	3	29.0	1.300	1.000	8.2	<	80.6

§10. Design of Bridge Accessories

10-1 Design of Bearing

Design of Lubber Bearing - for Steel-I Girder Bridge

1. Design Condition

(1) Horizontal Seismic Coefficient

No	Area	Type of Group	Horizontal Seismic Coefficient	
			In Bridge Axis Direction	In the Direction of Perpendicular to Bridge Axis
			Level 1	Level 1
			kh	kh
PF2	A2	Type III	0.30	0.30
PF3	A2	Type III	0.30	0.30
PF4	A2	Type III	0.30	0.30
PF5	A2	Type III	0.30	0.30

(2) Design Reaction Force

No	Design Reaction Force						
	Maximum of Bearing		Minimum of Bearing	Dead Load		Total of Dead Load	Live Load
	Rmax1	Rmax2	Rmin	Rdmax	Rdmin	ΣR_d	RL+I
	kN	kN	kN	kN	kN	kN	kN
PF2	2672.1	2461.2	1285.3	1673.1	1505.8	3178.9	999.1
PF3	7428.3	7291.5	5266.4	5567.6	5489.0	11056.6	---
PF4	7480.6	7276.5	5376.4	5627.6	5485.7	11113.3	---
PF5	2844.9	2266.6	1179.1	1778.2	1378.0	3156.3	1066.6

(3) Regular Displacement

No	Temp. Change	Indeterminate			Live Load	Total	
		Dry Shrinkage/Creep/	Dead Load	Total		+30°C	-30°C
		ΔL_{scp}	ΔL_d	$\Delta L'$		ΔL	ΔL
		mm	mm	mm		mm	mm
PF2	±26.8	----	----	----	7.0	33.7	-19.8
PF3	±10.5	----	----	----	5.3	15.8	-5.2
PF4	±10.5	----	----	----	5.5	16.0	-5.0
PF5	±26.8	----	----	----	6.7	33.5	-20.1

※ Positive number means expanding, while negative number means shrinking.
The larger value is adopted comparing absolute value to check the allowable stress.

(4) Oblique and Rotation Angle

No	Oblique Angle			Rotation Angle
	θ			$\Sigma \alpha e$
	°	'	"	rad
PF2	90	0	0	1 / 230
PF3	90	0	0	1 / 300
PF4	90	0	0	1 / 290
PF5	90	0	0	1 / 238

(5) Allowable Value

Item		Code	Unit	Value	
Maximum Compressive Stress	Under Under	σ_{max}	N/mm ²	$\leq 8.0 \leq S1 \leq 12.0$	
Difference of Compressive Stress	Design Load	$\Delta\sigma$	N/mm ²	$\leq 5.0 \text{ --- } S1 \leq 8$	
				$\leq 5+0.375(S1-8) \leq 6.5 \text{ --- } S1 > 8$	
Tensile Stress	Under Earthquake	σ_t	N/mm ²	$\leq 1.2 \text{ --- } G6$	
				$\leq 1.6 \text{ --- } G8$	
				$\leq 2.0 \text{ --- } G10\text{以上}$	
Shear Strain	Under Design Load	γ_{sa}	%	≤ 70	
	Level 1	γ_{sea}	%	≤ 150	
Safety Factor of Local Shear Strain	Under Design	fs	----	1.5	
Stress of Stiffener	Under Design Load	σ_s	N/mm ²	≤ 140.0	
	Under Earthquake	σ_s		≤ 210.0	

2. Calculation

(1) Calculation of Vertical Force

1) Vertical Force under Earthquake

$$RL = R_{dmax} + \sqrt{R_{HEQ}^2 + R_{VEQmax}^2}$$

$$RU = R_{dmin} - \sqrt{R_{HEQ}^2 + R_{VEQmin}^2}$$

2) Vertical force due to horizontal force applied in the direction of perpendicular to bridge axis

$$R_{HEQ} = \frac{H \cdot h_s}{\sum x_i^2} \cdot x_i$$

h_s : Vertical distance from a bearing to a center of girder
 x_i : Horizontal distance from a bearing to a center of girder

No	Vertical Distance	Horizontal Distance	
	h_s m	x_i m	$\sum x_i^2$ m ²
PF2	2.40	3.20	20.48
PF3	2.40	3.20	20.48
PF4	2.40	3.20	20.48
PF5	2.40	3.20	20.48

3) Vertical Force generated by Design Vertical Seismic Coefficient (kv)

$$R_{VEQmax} = k_v \cdot R_{dmax}$$

$$R_{VEQmin} = k_v \cdot R_{dmin}$$

No	Vertical Seismic Coefficient	
	Level 1	
	in Bridge Axis Direction	in the Direction of Perpendicular to Bridge Axis
	k_v	k_v
PF2	0.12	0.12
PF3	0.12	0.12
PF4	0.12	0.12
PF5	0.12	0.12

10) Result

• Stiffness and Coefficient

No	Stiffness		Coefficient				
	Horizontal	Vertical	Shape	Secondary shape		Distortion	Local inspection
	KB	KV	S1	S2	S2	E	E
	kN/mm	kN/mm	----	Bridge Axis Direction	Perpendicular to Bridge	N/mm ²	N/mm ²
PF2	5.75	1177.6	6.72	5.60	6.00	302.27	299.88
PF3	18.64	2748.4	8.93	6.39	6.39	401.64	527.18
PF4	18.64	2748.4	8.93	6.39	6.39	401.64	527.18
PF5	5.76	1177.6	6.72	5.60	6.00	302.27	299.88

• Displacement under earthquake

No	Bridge Axis Direction	Perpendicular to Bridge Axis
	Level 1	Level 2
	UB	UB
	mm	mm
PF2	76.1	----
PF3	76.2	----
PF4	62.3	----
PF5	57.9	----

• Bearing surface area

No	Bridge Axis Direction		Perpendicular to Bridge Axis	Distortion	
	Stationary	Earthquake	Earthquake	Bearing load	Live load
		Level1	Level2		
	Acn	Ace	Ace	δ_o	δ_{cl}
m ²	m ²	m ²	mm	mm	
PF2	0.4617	0.3625	0.4870	2.39	0.42
PF3	1.2135	1.1282	1.2317	2.74	----
PF4	1.2133	1.1650	1.2317	2.76	----
PF5	0.4619	0.4000	0.4870	2.55	0.45

• Checking of Stationary load

No	Compressive stress			Buckling Stress	Strain		Local shear strain				Stiffener stress
	Max	Min	Max-Min		Rotation	Vertical	Vertical	Shear	Rotation	Total	
	σ_{max}	σ_{min}	$\Delta\sigma$	σ_{cra}	δ_r	δ_c	γ_c	γ_s	γ_r	γ_t	σ_s
	N/mm ²	N/mm ²	N/mm ²	N/mm ²	mm	mm	%	%	%	%	N/mm ²
PF2	5.79	2.64	3.15	15.05	1.52	1.61	110.20	27.00	29.33	166.52	96.47
PF3	6.12	4.28	1.85	22.81	1.92	2.04	88.09	8.80	35.41	132.29	91.82
PF4	6.17	4.36	1.80	22.81	1.98	2.04	88.73	8.90	36.63	134.25	92.48
PF5	6.16	2.42	3.74	15.05	1.47	1.48	117.27	26.81	28.34	172.43	102.66
Allowable Value	≤ 8.0 $\leq S1$ ≤ 12.0	---	≤ 5.0 - $S1 \leq 8$ $5+0.375 \cdot (S1-8)$ $\geq 6.5-S1 > 8$	$\geq \sigma_{max}$	---	$\geq \delta_r$	---	≤ 70	---	$\leq \gamma_u/1.5$	≤ 140.0

• Checking for seismic resistance level 1

No	In Bridge Axis Direction											
	Displacement	Shear strain	Lateral force	Shear stress (lead)		Yield load	Equivalent elastic constant	Primary	Secondary	K1 • K2 intersection point		Equivalent attenuation
					Yield					Yy	Yy	
	UB	γ	F	q	qo	Qd	KB	K1	K2	Qy	Uy	hB
mm	---	kN	N/mm ²	N/mm ²	kN	kN/mm	kN/mm	kN/mm	kN	mm	---	
PF2	76.10	0.43	602.68	10.40	8.34	316.92	11.31	24.41	3.76	374.54	15.34	0.267
PF3	76.20	0.30	1164.07	8.80	7.06	640.87	21.82	44.63	6.87	757.39	16.97	0.272
PF4	62.30	0.24	951.72	7.20	5.77	523.97	21.82	44.63	6.87	619.23	13.87	0.272
PF5	57.90	0.32	523.97	9.63	7.72	293.59	12.93	25.86	3.98	346.97	13.42	0.274

No	In the Direction of Perpendicular to Bridge Axis											
	Displacement	Shear strain	Lateral force	shear stress (lead)		Yeild load	Equivalent elastic stiffness	Primary	Secondary	K1 • K2 intersection point		Equivalent attenuation
					yeild					Yy	Yy	
	UB	γ	F	q	qo	Qd	KB	K1	K2	Qy	Uy	hB
mm	---	kN	N/mm ²	N/mm ²	kN	kN/mm	kN/mm	kN/mm	kN	mm	---	
PF2	---	---	---	---	---	---	---	---	---	---	---	---
PF3	---	---	---	---	---	---	---	---	---	---	---	---
PF4	---	---	---	---	---	---	---	---	---	---	---	---
PF5	---	---	---	---	---	---	---	---	---	---	---	---

No	Bridge Axis Direction					Perpendicular to Bridge Axis					Tension Stress -0.3Rd
	Bearing stress	Tension stress	Buckling stress	Shear strain	stifener stress	Bearing stress	Tension stress	Buckling stress	Shear strain	Sttifener stress	
	σ_{ce}	σ_{te}	σ_{crae}	γ_{se}	σ_{se}	σ_{ce}	σ_{te}	σ_{crae}	γ_{se}	σ_{se}	σ_{te}
	N/mm ²	N/mm ²	N/mm ²	%	N/mm ²	N/mm ²	N/mm ²	N/mm ²	%	N/mm ²	N/mm ²
PF2	4.36	---	25.08	60.88	72.64	4.28	---	26.87	---	71.30	1.03
PF3	5.45	---	38.02	42.33	81.76	5.67	---	38.02	---	85.00	1.36
PF4	5.43	---	38.02	34.61	81.50	5.72	---	38.02	---	85.84	1.37
PF5	4.49	---	25.08	46.32	74.83	4.50	---	26.87	---	75.04	1.10
Allowable value	---	$\leq \sigma_a$	$\geq \sigma_{ce}$	≤ 150	≤ 210.0	---	$\leq \sigma_a$	$\geq \sigma_{ce}$	≤ 150	≤ 210.0	$\leq \sigma_a$

(4) Summary

No	Type	Size			Rubber				Stiffener	Bearing stiffness		
		Perpendicular to Bridge Axis	Bridge Axis Direction	Thickness	Elastic modulus	Thickness	Number of layers	Total thickness		Horizontal	Vertical	
		b'	a'	t	Ge	te	n	Σte		ts	KB	KV
		mm	mm	mm	N/mm ²	mm	Layer	mm		mm	kN/mm	kN/mm
PF2	N R	770	720	219	1.00	25	5	125	4.5	5.75	1177.6	
PF3	N R	1170	1170	314	1.00	30	6	180	6.0	18.64	2748.4	
PF4	N R	1170	1170	314	1.00	30	6	180	6.0	18.64	2748.4	
PF5	N R	770	720	219	1.00	25	5	125	4.5	5.76	1177.6	

Bearing Condition for Substructure Design

$$\text{Difference} = \frac{UB-UB'}{UB} \times 100 \text{ (\%)}$$

	$\Sigma KB(kN/m)$	Seismic Force (kN)	Assumed displacement value (m)	Actual displacement (m)	Difference (%)
Bridge 1-Support-1	-----	-----	-----	-----	-----
Bridge 1-Support-2	-----	-----	-----	-----	-----
Bridge 1-Support-3	-----	-----	-----	-----	-----
Bridge 2-Support-1	2. 263632E+004	1609. 673	0. 0761	0. 0711	6. 501
Bridge 2-Support-2	4. 364701E+004	3114. 750	0. 0762	0. 0714	6. 328
Bridge 2-Support-3	4. 364701E+004	2529. 781	0. 0623	0. 0580	6. 978
Bridge 2-Support-4	2. 585569E+004	1372. 176	0. 0579	0. 0531	8. 319
Bridge 3-Support-1	-----	-----	-----	-----	-----
Bridge 3-Support-2	-----	-----	-----	-----	-----
Bridge 3-Support-3	-----	-----	-----	-----	-----
Bridge 4-Support-1	-----	-----	-----	-----	-----
Bridge 4-Support-2	-----	-----	-----	-----	-----
Bridge 4-Support-3	-----	-----	-----	-----	-----
Bridge 4-Support-4	-----	-----	-----	-----	-----
Bridge 4-Support-5	-----	-----	-----	-----	-----
Bridge 5-Support-1	4. 117886E+004	1066. 506	0. 0272	0. 0259	4. 952
Bridge 5-Support-2	6. 550148E+004	1663. 639	0. 0266	0. 0254	4. 664
Bridge 5-Support-3	6. 550148E+004	1829. 754	0. 0292	0. 0279	4. 389
Bridge 5-Support-4	4. 056619E+004	1265. 081	0. 0328	0. 0312	4. 820
Bridge 6-Support-1	-----	-----	-----	-----	-----
Bridge 6-Support-2	-----	-----	-----	-----	-----
Bridge 6-Support-3	-----	-----	-----	-----	-----

10-2 Bridge drainage

Calculation for catchpit interval

1. Design conditions

Rain intensity	$I = \beta \times 149.0 = 149$	mm/h
	$\beta = 1.00$	
Discharge coefficient	$C = 0.9$	
Roughness coefficient	$n = 0.013$	
Safety factor	$k = 0.8$	
Minimum interval	$L = 5.000$	m

1) Calculation for catchpit interval

$$L_s = \frac{2.46 \times 10^{-8} \times A \times R^{2/3} \cdot i^{1/2}}{\beta \times r_h \times B}$$

L_s : Interval (m) ($L_s \leq 20$ m)

A : flowing area (m²) $A = 1/2 \times h \times b$

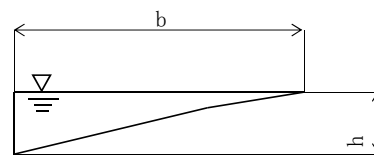
R : Depth (m), $R = A / S$

S : flowing length $S = h + \sqrt{b^2 + h^2}$

i : Longitudinal slope

$\beta \times r_h$: Design rain intensity

B : Road width (m)



Calculation of Catch Pit Interval

Fly Over (Left Side)

		Length	C.L Height	Longitudinal Slope	Transverse Gradient	Flowing water Width	Depth h	Flow area A	Wetted per imte	Hydraulic mean depth	Watershed width	Rain intensity	Fall rate	Drainage PIT Maximum Interval	PIT Interval
		(m)	(m)	(%)	(%)	(m)	(m)	A (m2)	P (m)	R(m)	(m)	I[mm/h]	γ	Ls (m)	
PC	AF1	0.0000	10.5800	-	3.44	1.000	0.0344	0.0172	1.0350	0.0166	-	-	-	-	
	EDR1	4.992	10.7298	3.00	4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	
	DR1	5.008	10.8800	3.00	4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	
	DR2	10.000	11.1800	3.00	4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	
	PF1(DR3)	10.000	11.4800	3.00	4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	
	DR4	10.000	11.7800	3.00	4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	
	EDR2	8.080	12.0224	3.00	4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	
Steel-Box	DR5	1.920	12.0800	3.00	3.89	1.000	0.0389	0.0195	1.0397	0.0187	12.750	149.000	0.90	30.7	
	PF2(DR6)	10.000	12.3800	3.00	3.34	1.000	0.0334	0.0167	1.0340	0.0162	12.750	149.000	0.90	23.9	
	DR7	10.000	12.6800	3.00	2.78	1.000	0.0278	0.0139	1.0282	0.0135	12.750	149.000	0.90	17.7	
	DR8	10.000	12.9800	3.00	2.22	1.000	0.0222	0.0111	1.0224	0.0109	12.750	149.000	0.90	12.2	
	EDR3	4.000	13.1000	3.00	2.00	1.000	0.0200	0.0100	1.0202	0.0098	12.750	149.000	0.90	10.3	
	DR9	6.000	13.2799	3.00	1.40	1.000	0.0140	0.0070	1.0141	0.0069	12.750	149.000	0.90	5.7	
	DR10	10.000	13.5684	2.89	0.40	1.000	0.0040	0.0020	1.0040	0.0020	12.750	149.000	0.90	0.7	5
	EDR4	4.000	13.6784	2.75	0.00	1.000	0.0000	0.0000	1.0000	0.0000	12.750	149.000	0.90	0.0	5
	DR11	6.000	13.8376	2.65	-0.60	1.000	0.0060	0.0030	1.0060	0.0030	12.750	149.000	0.90	1.3	5
	PF3	5.000	13.9650	2.55	-1.10	1.000	0.0110	0.0055	1.0111	0.0054	12.750	149.000	0.90	3.5	5
	DR12	5.000	14.0876	2.45	-1.60	1.000	0.0160	0.0080	1.0161	0.0079	12.750	149.000	0.90	6.4	6
	EDR5	4.000	14.1822	2.36	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	12.750	149.000	0.90	9.1	9
	DR13	6.000	14.3184	2.27	-2.68	1.000	0.0268	0.0134	1.0272	0.0130	12.750	149.000	0.90	14.5	14
	DR14	10.000	14.5299	2.11	-3.81	1.000	0.0381	0.0191	1.0388	0.0183	12.750	149.000	0.90	24.9	20
	DR15	10.000	14.7222	1.92	-4.95	1.000	0.0495	0.0248	1.0507	0.0236	12.750	149.000	0.90	36.5	20
	EDR6	9.298	14.8838	1.74	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	47.5	20
	DR16	0.702	14.8953	1.64	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	46.1	20
	DR17	10.000	15.0491	1.54	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	44.7	20
	DR18	10.000	15.1837	1.35	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	41.8	20
	PF4	5.000	15.2438	1.20	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	39.5	20
	DR19	5.000	15.2991	1.11	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	37.9	20
	DR20	10.000	15.3953	0.96	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	35.3	20
	DR21	10.000	15.4722	0.77	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	31.6	20
	DR22	10.000	15.5300	0.58	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	27.4	20
DR23	10.000	15.5800	0.50	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	25.5	20	
PC-2	PF5(DR24)	10.000	15.6300	0.50	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	25.5	20
	DR25	10.000	15.6800	0.50	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	25.5	20
	DR26	10.000	15.7264	0.46	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	24.5	20
	PF6(DR27)	10.000	15.7541	0.28	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	19.0	18
	DR28	10.000	15.7616	0.08	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	9.9	9
	EDR7	5.571	15.7569	-0.08	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	10.5	10
	DR29	4.429	15.7488	-0.18	-5.33	1.000	0.0533	0.0267	1.0547	0.0253	12.750	149.000	0.90	12.7	12
PC-4	PF7(DR30)	10.000	15.7158	-0.33	-3.81	1.000	0.0381	0.0191	1.0388	0.0183	12.750	149.000	0.90	9.9	9
	DR31	10.000	15.6625	-0.53	-2.30	1.000	0.0230	0.0115	1.0233	0.0112	12.750	149.000	0.90	5.5	5
	EDR8	1.977	15.6496	-0.65	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	12.750	149.000	0.90	4.8	5
	DR32	8.023	15.5926	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	12.750	149.000	0.90	5.0	5
	PF8(DR33)	10.000	15.5211	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	EDR9	8.383	15.4612	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR34	1.617	15.4496	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR35	10.000	15.3781	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	PF9(DR36)	10.000	15.3066	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR37	10.000	15.2351	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR38	10.000	15.1636	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	PF10(DR39)	10.000	15.0921	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
Steel-I	DR40	10.000	15.0206	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR41	10.000	14.9491	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	PF11(DR42)	10.000	14.8776	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR43	10.000	14.8061	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR44	10.000	14.7305	-0.76	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.3	10
	DR45	10.000	14.6339	-0.97	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	11.7	11
	PF12	5.000	14.5770	-1.14	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	12.7	12
	DR46	5.000	14.5144	-1.25	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	13.3	13
	DR47	10.000	14.3720	-1.42	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	14.2	14
	DR48	10.000	14.2068	-1.65	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	15.2	15
	DR49	10.000	14.0188	-1.88	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	16.3	16
	DR50	10.000	13.8079	-2.11	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	17.2	17
	PF13	7.000	13.6467	-2.30	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	18.0	18
	DR51	3.000	13.5742	-2.42	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	18.4	18
	DR52	10.000	13.3176	-2.57	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	19.0	19
	DR53	10.000	13.0382	-2.79	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	19.8	19
DR54	10.000	12.7400	-2.98	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20	
PC-2	PF14	2.000	12.6800	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
	DR55	8.000	12.4400	-3.00	-2.00	1.000	0.0200	0.0100	1.0202						

Fly Over (Right Side)

		Length	C.L Height	Slope	Gradient	Width	Depth h	Flow area A	Wetted per Imte	mean depth	watershed	Rain intensity	Fall rate	Drainage Ls	PIT Interval
		(m)	(m)	(%)	(%)	(m)	(m)	A (m2)	P (m)	R(m)	(m)	I[mm/h]	γ	Ls (m)	
PC-2	AF1	0.0000	10.5800	-	-3.44	1.000	0.0344	0.0172	1.0350	0.0166	-	-	-	-	-
	EDR1	4.992	10.7298	3.00	-4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	20
	DR1	5.008	10.8800	3.00	-4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	20
	DR2	10.000	11.1800	3.00	-4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	20
	PF1(DR3)	10.000	11.4800	3.00	-4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	20
	DR4	10.000	11.7800	3.00	-4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	20
	EDR2	8.080	12.0224	3.00	-4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	20
DR5	1.920	12.0800	3.00	-3.89	1.000	0.0389	0.0195	1.0397	0.0187	12.750	149.000	0.90	30.7	20	
Steel-I	PF2(DR6)	10.000	12.3800	3.00	-3.34	1.000	0.0334	0.0167	1.0340	0.0162	12.750	149.000	0.90	23.9	20
	DR7	10.000	12.6800	3.00	-2.78	1.000	0.0278	0.0139	1.0282	0.0135	12.750	149.000	0.90	17.7	17
	DR8	10.000	12.9800	3.00	-2.22	1.000	0.0222	0.0111	1.0224	0.0109	12.750	149.000	0.90	12.2	12
	EDR3	4.000	13.1000	3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	12.750	149.000	0.90	10.3	10
	DR9	6.000	13.2799	3.00	-1.40	1.000	0.0140	0.0070	1.0141	0.0069	12.750	149.000	0.90	5.7	5
	DR10	10.000	13.5684	2.89	-0.40	1.000	0.0040	0.0020	1.0040	0.0020	12.750	149.000	0.90	0.7	5
	EDR4	4.000	13.6784	2.75	0.00	1.000	0.0000	0.0000	1.0000	0.0000	12.750	149.000	0.90	0.0	5
	DR11	6.000	13.8376	2.65	0.60	1.000	0.0060	0.0030	1.0060	0.0030	12.750	149.000	0.90	1.3	5
	PF3	5.000	13.9650	2.55	1.10	1.000	0.0110	0.0055	1.0111	0.0054	12.750	149.000	0.90	3.5	
	DR12	5.000	14.0876	2.45	1.60	1.000	0.0160	0.0080	1.0161	0.0079	12.750	149.000	0.90	6.4	
	EDR5	4.000	14.1822	2.36	2.00	1.000	0.0200	0.0100	1.0202	0.0098	12.750	149.000	0.90	9.1	
	DR13	6.000	14.3184	2.27	2.68	1.000	0.0268	0.0134	1.0272	0.0130	12.750	149.000	0.90	14.5	
	DR14	10.000	14.5299	2.11	3.81	1.000	0.0381	0.0191	1.0388	0.0183	12.750	149.000	0.90	24.9	
	DR15	10.000	14.7222	1.92	4.95	1.000	0.0495	0.0248	1.0507	0.0236	12.750	149.000	0.90	36.5	
	EDR6	9.298	14.8838	1.74	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	47.5	
	DR16	0.702	14.8953	1.64	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	46.1	
	DR17	10.000	15.0491	1.54	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	44.7	
	DR18	10.000	15.1837	1.35	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	41.8	
	PF4	5.000	15.2438	1.20	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	39.5	
	DR19	5.000	15.2991	1.11	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	37.9	
	DR20	10.000	15.3953	0.96	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	35.3	
	DR21	10.000	15.4722	0.77	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	31.6	
	DR22	10.000	15.5300	0.58	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	27.4	
	DR23	10.000	15.5800	0.50	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	25.5	
PC-2	PF5(DR24)	10.000	15.6300	0.50	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	25.5	
	DR25	10.000	15.6800	0.50	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	25.5	
	DR26	10.000	15.7264	0.46	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	24.5	
	PF6(DR27)	10.000	15.7541	0.28	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	19.0	
	DR28	10.000	15.7616	0.08	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	9.9	
	EDR7	5.571	15.7569	-0.08	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	10.5	
	DR29	4.429	15.7488	-0.18	5.33	1.000	0.0533	0.0267	1.0547	0.0253	12.750	149.000	0.90	12.7	
PC-4	PF7(DR30)	10.000	15.7158	-0.33	3.81	1.000	0.0381	0.0191	1.0388	0.0183	12.750	149.000	0.90	9.9	
	DR31	10.000	15.6625	-0.53	2.30	1.000	0.0230	0.0115	1.0233	0.0112	12.750	149.000	0.90	5.5	
	EDR8	1.977	15.6496	-0.65	2.00	1.000	0.0200	0.0100	1.0202	0.0098	12.750	149.000	0.90	4.8	
	DR32	8.023	15.5926	-0.71	0.78	1.000	0.0078	0.0039	1.0078	0.0039	12.750	149.000	0.90	1.0	5
	PF8(DR33)	10.000	15.5211	-0.71	-0.73	1.000	0.0073	0.0037	1.0073	0.0036	6.375	149.000	0.90	1.9	5
	EDR9	8.383	15.4612	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR34	1.617	15.4496	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR35	10.000	15.3781	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	PF9(DR36)	10.000	15.3066	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR37	10.000	15.2351	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR38	10.000	15.1636	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	PF10(DR39)	10.000	15.0921	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR40	10.000	15.0206	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
DR41	10.000	14.9491	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10	
Steel-I	PF11(DR42)	10.000	14.8776	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR43	10.000	14.8061	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR44	10.000	14.7305	-0.76	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.3	10
	DR45	10.000	14.6339	-0.97	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	11.7	11
	PF12	5.000	14.5770	-1.14	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	12.7	12
	DR46	5.000	14.5144	-1.25	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	13.3	13
	DR47	10.000	14.3720	-1.42	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	14.2	14
	DR48	10.000	14.2068	-1.65	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	15.2	15
	DR49	10.000	14.0188	-1.88	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	16.3	16
	DR50	10.000	13.8079	-2.11	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	17.2	17
	PF13	7.000	13.6467	-2.30	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	18.0	18
	DR51	3.000	13.5742	-2.42	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	18.4	18
	DR52	10.000	13.3176	-2.57	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	19.0	19
	DR53	10.000	13.0382	-2.79	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	19.8	19
DR54	10.000	12.7400	-2.98	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20	
PC-2	PF14	2.000	12.6800	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
	DR55	8.000	12.4400	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
	DR56	10.000	12.1400	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
	DR57	10.000	11.8400	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
	PF15	2.000	11.7800	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
	DR58	8.000	11.5400	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
	DR59	10.000	11.2400	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
DR60	10.000	10.9400	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20	
AF2	2.000	10.8800	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20	

Total 602.0000 m

10-3 Expansion joint

(1) Gap of girder and abutment

The expansion length is determined based on the displacement of the earthquake and the temperature.

Expansion joint shall be installed not to compromise the following gap of the girder and abutment, and displacement of seismic and temperature.

(2) Gap and displacement

				PCI Grider				Steel box Girder				PCI Grider				PCI Girder				Steel I Girder				PCI Girder		
				M	F	F	E	E	E	E	F	F	M	M	F	F	F	M	E	E	E	E	F	F	M	
				condition of support	AF1	PF1	PF2	PF3	PF4	PF5	PF6	PF7	PF8	PF9	PF10	PF11	PF12	PF13	PF14	PF15	AF2					
substructure		mm	100	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150	150			
expansion	Creep·drying shrinkage (Δ_{sc2})	mm	7	0	0	0	0	0	0	-7	14	-14	0	0	0	0	0	0	0	0	0	-7				
	temperature (Δ_t)	mm	± 12	± 0	± 27	± 27	± 0	± 12	± 23	± 23	± 19	± 19	± 0	± 19	± 0	± 19	± 0	± 19	± 0	± 19	± 0	± 12				
	displacement (Δ_L)	stretching	mm	19	27	27	56	56	19	19																
		reducing	mm	-5	-27	-27	-14	-28	-19	-5																
	Margin (LA)	mm	10	11	11	14	17	10	10																	
	Δ_{U2}	mm	34	65	65	84	101	48	34																	
	seismic (Δ_{EQ}) SBR×2	mm	48	260	234	110	144	162	58																	
design displacemnt (Δ_{Ej})	mm	48	260	234	110	144	162	58																		

02-2-STEEL-I GIRDER BRIDGE

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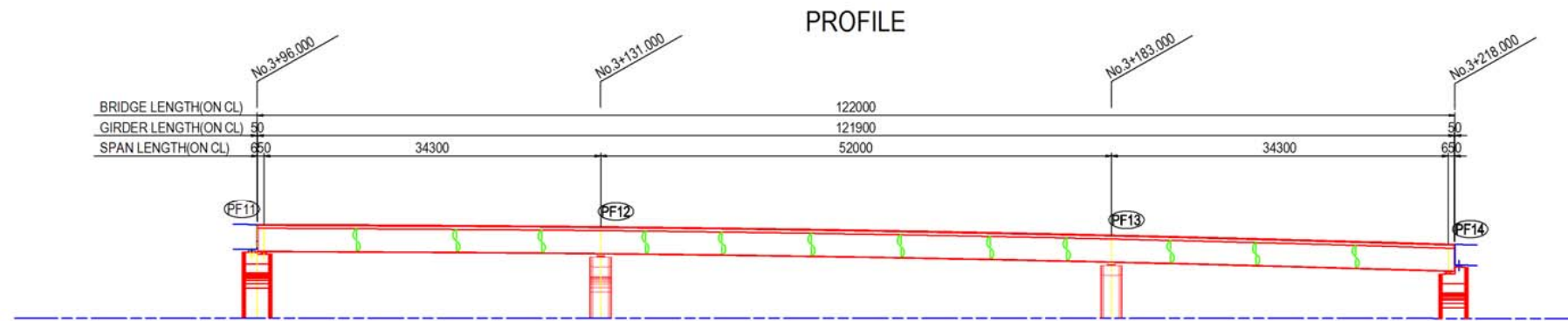
§1. Design condition

1-1 Design condition

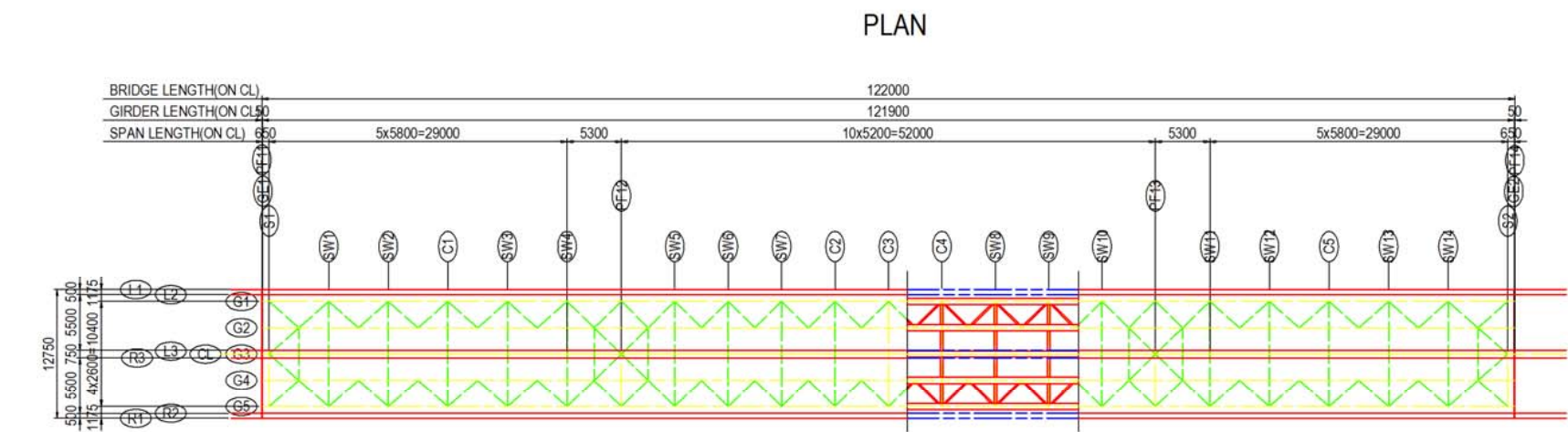
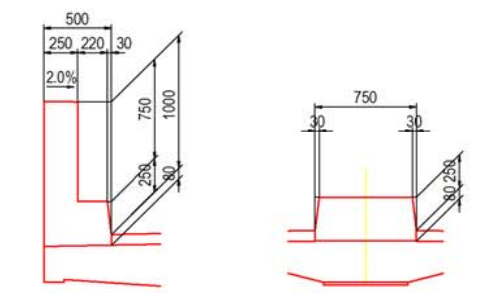
ROAD GRADE	Equivalent to CLASS 4-1
BRIDGE TYPE	3 span continuous steel I girder
BRIDGE LENGTH	L = 122.000 m
SPAN LENGTH	L = 34.300 + 52.000 + 34.300m
WIDTH OF THE ROAD	TOTAL : 12.750 m 0.500+5.500+0.750+5.500+0.500m
Horizontal alignment	R=∞
LONGITUDINARL SLOPE	↘ 0.715 % (VCL=100) ↘ 3.000 %
SECTION SLOPE	2.000 % ↙ ↘
ANGLE OF SKEW	90° 00' 00"
PAVEMENT	ASPHALT PAVEMENT t= 80 mm
SLAB	REINFORCED CONCRETE t= 240 mm
LIVE ROAD	AASHTO HL=93
DESIGN STANDARD	AASHTO LRFD BRIDGE DESIGN 2014(LIVE ROAD) Specifications for highway bridges (Japan Road Association) I Common matters, II Steel bridges, V Seismic design (April 2012)

1-2 General View of Super Structural

SUPERSTRUCTURE STRUCTURAL DRAWING S=1:600



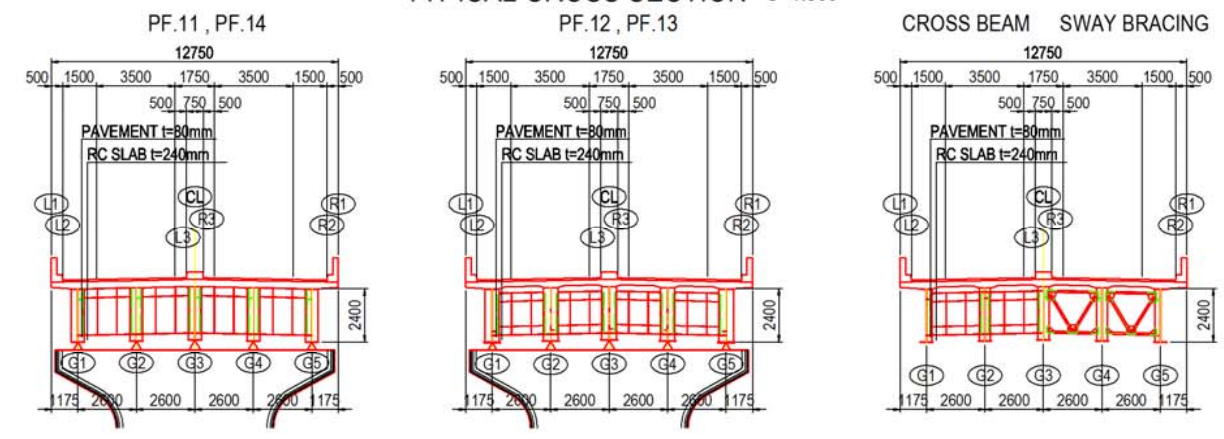
WALL BALUSTRADE MEDIAN STRIP S=1 : 50



THE DRAINER PART DETAILS S=1 : 20



TYPICAL CROSS SECTION S=1:300



DESIGN CONDITION

ROAD GRADE	Equivalent to class 4-1
BRIDGE TYPE	3 span continuous steel I girder
BRIDGE LENGTH	L = 122.000 m
SPAN LENGTH	L = 34.300 + 52.000 + 34.300 m
WIDTH OF THE ROAD	TOTAL : 12.750 m L = 0.500 + 5.500 + 0.750 + 5.500 + 0.500 m
PLANE CONFIGURATION	R=∞
LONGITUDINAL SLOPE	0.715% ↘ 3.000%(VCL=100) ↘
SECTIN SLOPE	2.000% ↘
ANGLE OF SKEW	90°00'00"
PAVEMENT	ASPHALT PAVEMENT t = 80 mm
SLAB	REINFORCED CONCRETE t = 240 mm
LIVE ROAD	AASHTO HL-93
DESIGN STANDARD	AASHTO LRFD BRIDGE DESIGN 2014(LIVE ROAD) Specifications for highway bridges(Japan Road Association) Common matters „Steel bridges„Seismic design(April 2012)

PROJECT NAME DETAILED DESIGN ON BAGO RIVER BRIDGE CONSTRUCTION PROJECT	FINANCED BY jica JAPAN INTERNATIONAL COOPERATION AGENCY	COUNTERPART REPUBLIC OF THE UNION OF MYANMAR MINISTRY OF CONSTRUCTION DEPARTMENT OF BRIDGE	JICA STUDY TEAM NIPPON KOEI CO., LTD. ORIENTAL CONSULTANTS GLOBAL CO., LTD. METROPOLITAN EXPRESSWAY COMPANY LIMITED CHODAI CO., LTD. NIPPON ENGINEERING CONSULTANTS CO., LTD.	NAME	SIGNATURE	DATE	DRAWING TITLE SUPERSTRUCTURE STRUCTURAL DRAWING	PACKAGE 3 DWG No.
				PREPARED BY	Y. SUZUKI			
				CHECKED BY	T. HAYAKAWA			
				APPROVED BY	Y. SANO			

§2. Design of Slab
2-1 Design Condition

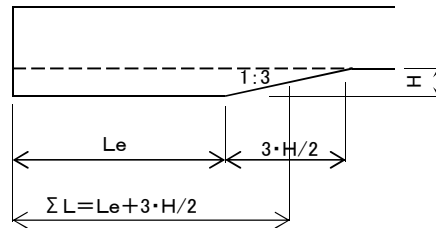
ASPHALT PAVEMENT	ASPHALT PAVEMENT	t = 80mm	
RC SLAB	RC SLAB	t = 240mm	
LIVE LOAD	LIVE LOAD	AASHTO Truk or JSHB T-Load	
ADTT _{SL}	2000 or more per day	k ₁ = 1.25	
Allowable Stress	Concrete	Design Strength	$\sigma_{ck} = 24\text{N/mm}^2$
		Allowable Stress	$\sigma_{ca} = 8.0\text{N/mm}^2$
	Reinforcement bar	Material	SD345
		Allowable Stress	$\sigma_{sa} = 140\text{N/mm}^2$
Note: Approximately 20N/mm ² of allowance should be considered in the case without considering differential settlement			

- The thickness of haunch is constant as 80mm.
- The span of slab is determined by the maximum value.
- The length of thickness of slab at the end of girder "Le" is as follows, according to JSHB II 9.2.11.
- Window Load : 44.7 m/s
- Collision force to the concrete barrier : 43kN

$$L_e = 1/2 \cdot L$$

L : The span length of slab in the perpendicular direction to bridge axis

Section	Le(mm)
S1	1300
S2	1300



The bending moment of the design with two types of live loads is calculated as follows

1) AASHTO LIVE LOAD $M = 1.2 * (\alpha_1 - \alpha_2) * L * P / SW * (1 + i) = 27.3 \text{ kNm}$
 $\alpha_1 = 0.204$
 $\alpha_2 = -0.01431$
 $SW = 2090$
 $P = 72.5$
 $i = 0.33$
 L: SPAN 2.60 m

2) JSHB T-Load $M = (0.12 * L + 0.07) * P * K * 0.8 = 30.8 \text{ kNm}$
 $P = 100$
 $K = 1.008$

Since the RC slab is directly affected by the load of the wheel, it is better to design with JSHB's live load (larger force).

2-2 Summary of Calculation Result for Deck Slab

	Cantilever Slab Standard			
	Longitudinal Bar		Stirrup	
Bending Moment(kN·m)	-56.64		17.21	
Deck Thickness(mm)	320		285.1	
Diameter of Upper Rebar (mm)	D19		D16	
Pitch of Upper Rebar (mm)	ctc150		ctc300	
Diameter of Lower Rebar (mm)	D19		D16	
Pitch of Lower Rebar (mm)	ctc300		ctc150	
Concrete Cover Thickness(mm)	40.0		57.5	
Amount of Rebar As (cm ²)	19.10		13.24	
Amount of Rebar As' (cm ²)	9.55		6.62	
Stress of Concrete (N/mm ²)	$\sigma_c =$	4.11 < 8.0	$\sigma_c =$	2.14 < 8.0
Stress of Rebar (N/mm ²)	$\sigma_s =$	120.0 < 140	$\sigma_s =$	64.8 < 140

	Cantilever Slab Girder end			
	Longitudinal Bar		Stirrup	
Bending Moment(kN·m)	-102.27		—	
Deck Thickness(mm)	320		—	
Diameter of Upper Rebar (mm)	D22		—	
Pitch of Upper Rebar (mm)	ctc110		—	
Diameter of Lower Rebar (mm)	D22		—	
Pitch of Lower Rebar (mm)	ctc220		—	
Concrete Cover Thickness(mm)	41.0		—	
Amount of Rebar As (cm ²)	35.19		—	
Amount of Rebar As' (cm ²)	17.60		—	
Stress of Concrete (N/mm ²)	$\sigma_c =$	5.70 < 8.0	—	
Stress of Rebar (N/mm ²)	$\sigma_s =$	121.1 < 140	—	

	Centre of span (inside)			
	Longitudinal Bar		Stirrup	
Bending Moment(kN·m)	34.52		24.00	
Deck Thickness(mm)	240		240	
Diameter of Upper Rebar (mm)	D19		D16	
Pitch of Upper Rebar (mm)	ctc300		ctc300	
Diameter of Lower Rebar (mm)	D19		D16	
Pitch of Lower Rebar (mm)	ctc150		ctc150	
Concrete Cover Thickness(mm)	40.0		57.5	
Amount of Rebar As (cm ²)	19.10		13.24	
Amount of Rebar As' (cm ²)	9.55		6.62	
Stress of Concrete (N/mm ²)	$\sigma_c =$	4.41 < 8.0	$\sigma_c =$	4.36 < 8.0
Stress of Rebar (N/mm ²)	$\sigma_s =$	105.0 < 140	$\sigma_s =$	114.0 < 140

	On Main Girder (inside)	
	Longitudinal Bar	Stirrup
Bending Moment(kN·m)	-36.01	—
Deck Thickness(mm)	320	—
Diameter of Upper Rebar (mm)	D19	—
Pitch of Upper Rebar (mm)	ctc150	—
Diameter of Lower Rebar (mm)	D19	—
Pitch of Lower Rebar (mm)	ctc300	—
Concrete Cover Thickness(mm)	40.0	—
Amount of Rebar As (cm ²)	19.10	—
Amount of Rebar As' (cm ²)	0.00	—
Stress of Concrete (N/mm ²)	$\sigma_c =$ 2.89 < 8.0	—
Stress of Rebar (N/mm ²)	$\sigma_s =$ 46.6 < 140	—

	Centre of span (out side)			
	Longitudinal Bar		Stirrup	
Bending Moment(kN·m)	36.01		24.00	
Deck Thickness(mm)	240		240	
Diameter of Upper Rebar (mm)	D19		D16	
Pitch of Upper Rebar (mm)	ctc300		ctc300	
Diameter of Lower Rebar (mm)	D19		D16	
Pitch of Lower Rebar (mm)	ctc150		ctc150	
Concrete Cover Thickness(mm)	40.0		57.5	
Amount of Rebar As (cm ²)	19.10		13.24	
Amount of Rebar As' (cm ²)	9.55		6.62	
Stress of Concrete (N/mm ²)	$\sigma_c =$ 4.60 < 8.0		$\sigma_c =$ 4.36 < 8.0	
Stress of Rebar (N/mm ²)	$\sigma_s =$ 109.5 < 140		$\sigma_s =$ 114.0 < 140	

	On Main Girder (outside)	
	Longitudinal Bar	Stirrup
Bending Moment(kN·m)	-36.01	—
Deck Thickness(mm)	320	—
Diameter of Upper Rebar (mm)	D19	—
Pitch of Upper Rebar (mm)	ctc150	—
Diameter of Lower Rebar (mm)	D19	—
Pitch of Lower Rebar (mm)	ctc300	—
Concrete Cover Thickness(mm)	40.0	—
Amount of Rebar As (cm ²)	19.10	—
Amount of Rebar As' (cm ²)	0.00	—
Stress of Concrete (N/mm ²)	$\sigma_c =$ 2.89 < 8.0	—
Stress of Rebar (N/mm ²)	$\sigma_s =$ 76.6 < 140	—

§3. Structure analysis

3-1 Analytical Method

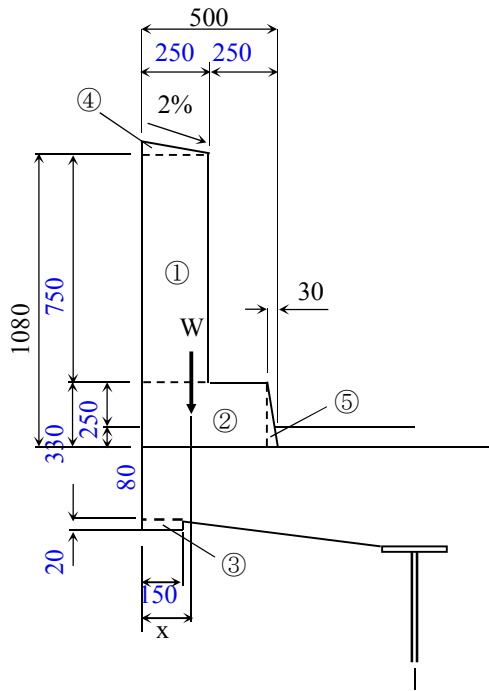
1. The structural analysis is conducted by arbitrary lattice theory (a displacement method) with an electrical
The software used is "APOLLO Analyzer " commercialized by Yokogawa Techno-information Service I
2. The structure is plane grid composed of main girders and cross beams.
3. Vertical loads (dead load and live load) is considered in the analysis.
4. The coordinates of the structure are automatically transformed from the plane coordinates
calculated by linear analysis.

3-2 Load intensity

(1) Dead load

Pavement	0.080	×	22.5 kN/m ³	=	1.800 kN/m ²
thickness of slab (30L+110) x k1 x k2				=	240 mm
Large vehicle traffic volume 2000more than/1day • 1 direction					
A1-A2	L	=	2.600 m		
	k1	=	1.25	k2 =	1.00
Slab	0.240	×	24.5 kN/m ³	=	5.880 kN/m ²
Haunch	G1, G5			=	2.250 kN/m
	G2~G4			=	1.630 kN/m
Steel weight				=	6.100 kN/m
Concrete barrier				=	8.630 kN/m
Median				=	6.070 kN/m
Point load	A1-A2				
	end part		Levelling concrete		
G1, G5	21.000	+	3.00	=	24.0 kN
G2~G4	21.000	+	5.00	=	26.0 kN

2) Concrete Barrier



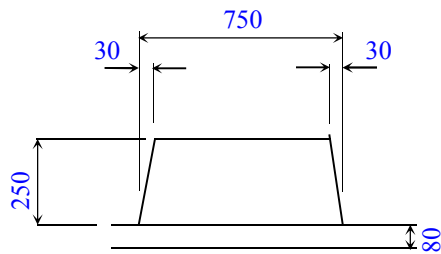
	Area A m ²	Unit Weight kN/m ³	Load W kN/m	Center X m	-- W·X --
①	0.188	24.5	4.606	0.125	0.576
②	0.155	24.5	3.798	0.250	0.950
③	0.003	24.5	0.074	0.075	0.006
④	0.001	24.5	0.025	0.083	0.002
⑤	0.005	24.5	0.123	0.480	0.059
Σ			8.626		1.593

$$W = 8.63 \text{ kN/m}$$

$$x = 1.593 / 8.626 = 0.185 \text{ m (from the outer edge)}$$

$$0.5 - 0.185 = 0.315 \text{ (from the outer edge)}$$

3) Median

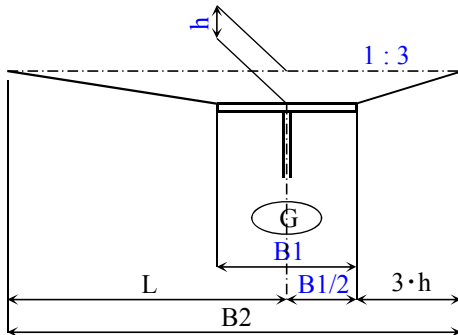


$$W = 0.750 \times 0.330 \times 24.5 = 6.07 \text{ kN/m}$$

(3) Detail of Load

1) Haunch

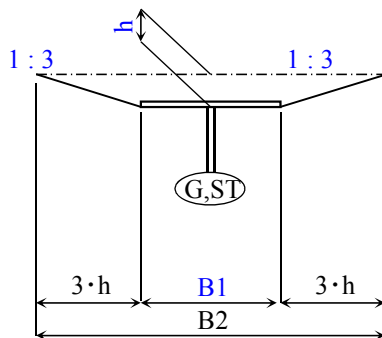
【Main Girder ; G1, G5】



$$W = 1/2 \times (B1 + B2) \times h \times 24.5 \text{ kN/m}$$

Girder	Applied Section	L (mm)	B1 (mm)	B2 (mm)	h (mm)	W (kN/m)
G1,G5	S1~S2	1175	590	1710	80	2.25

【Main Girder ; G2-G4】



$$W = 1/2 \times (B1 + B2) \times h \times 24.5 \text{ kN/m}$$

Girder	Applied Section	B1 (mm)	B2 (mm)	h (mm)	W (kN/m)
G2~G4	S1~S2	590	1070	80	1.63

4) Load at the End of Girder

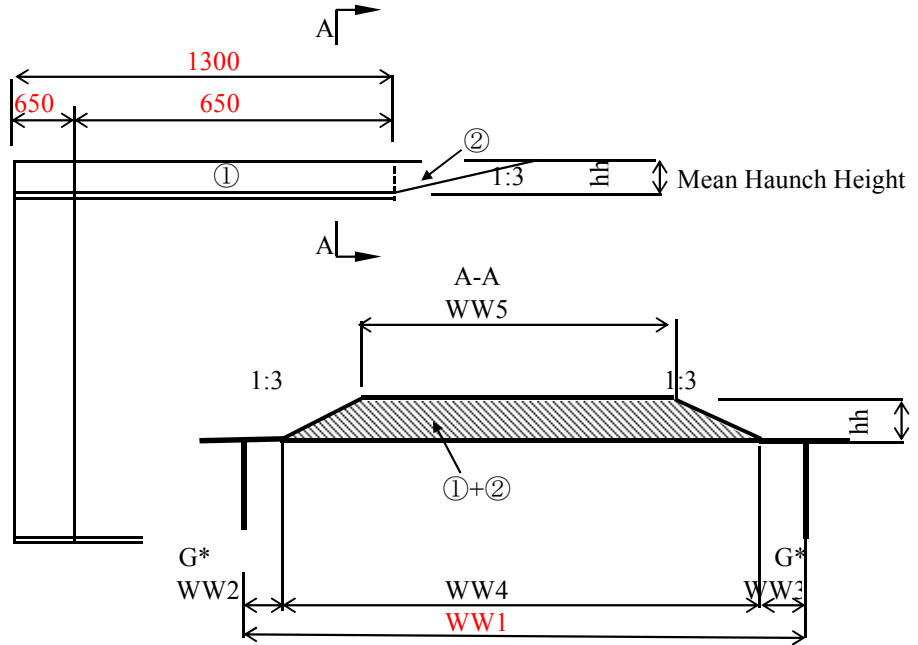
■ S1,S2

L= 650 mm

Pavement	1.80 ×	11.750 ×	0.650	=	13.748 kN
Deck Slab	5.88 ×	12.750 ×	0.650	=	48.731 kN
Haunch of G1	2.25 ×	1 ×	0.650	=	1.463 kN
Haunch of G2	1.63 ×	1 ×	0.650	=	1.060 kN
Haunch of G3	1.63 ×	1 ×	0.650	=	1.060 kN
Haunch of G4	1.63 ×	1 ×	0.650	=	1.060 kN
Haunch of G5	2.25 ×	1 ×	0.650	=	1.463 kN
Concrete Barrier	8.63 ×	2 ×	0.650	=	11.219 kN
Median	6.07 ×	1 ×	0.650	=	3.946 kN
Steel Weight of Main Gird	6.10 ×	5 ×	0.650	=	19.825 kN
					<hr/>
					103.575 kN
Divided by the number of girders		103.575 /	5	=	20.715 kN
				≐	21.000 kN

5) Thickness Increasing of Slab

The slab between main girders are increased at the end of girder, with in the half of deck span length from the center. It is considered as the concentrated load applied on the main girder at the end.



	Haunch Height (mm)	Mean Haunch (mm)	WW1 (mm)	WW2 (mm)	WW3 (mm)	WW4 (mm)	WW5 (mm)
G1	80	80	2600	295	295	2010	1530
G2	80	80	2600	295	295	2010	1530
G3	80	80	2600	295	295	2010	1530
G4	80	80	2600	295	295	2010	1530
G5	80						

$$\begin{array}{rcll}
 \text{G1-G5} & & \text{Mean Width} & \\
 \textcircled{1} & 1.300 & \times & 0.080 \times 1.770 \times 24.5 = 4.51 \text{ kN} \\
 \textcircled{2} & 0.240 & \times & 0.080 \times 1.770 \times 24.5 / 2 = 0.42 \text{ kN} \\
 & & & \underline{4.93 \text{ kN}}
 \end{array}$$

The above load is applied as the concentrated load on each bearing equally divided.

$$\begin{array}{rcll}
 \text{G1, G5} & = & 4.93 / 2 & = 2.50 \text{ kN} \\
 & & & \div 2 = 3.00 \text{ kN} \\
 \text{G2-G4} & = & 4.93 / 2 + 4.93 / 2 & = 4.90 \text{ kN} \\
 & & & \div 2 = 5.00 \text{ kN}
 \end{array}$$

6) Live Load

Loading Method

AASHTO HL-93 and the special vehicular load of 75t is applied.

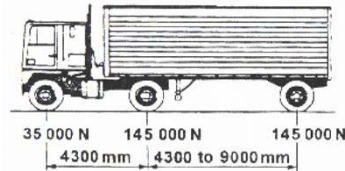
The maximum sectional force is used in the design.

Impact coefficient is considered.

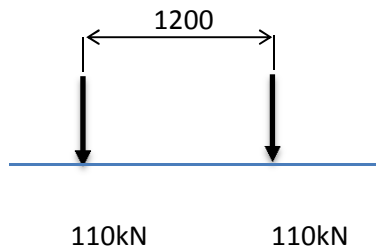
1. AASHTO HL-93

① Design Vehicle Load or Design Tandem Load

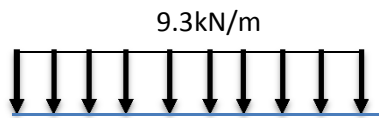
①-1 Design Truck (Hs20-44)



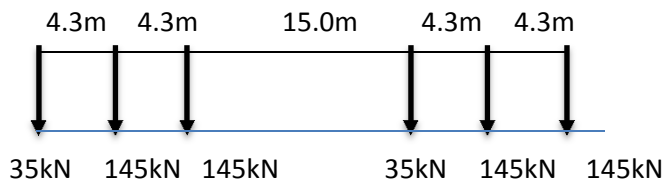
①-2 Design Tandem Load



② Design Lane Load



③ Two Design Trucks for Negative Moment



Load Coefficient with the Number of Lane

Number of Lane	Coefficient
1	1.2
2	1
3	0.85
>3	0.65

In the Project, three lanes are adopted

Types of Combination

CASE1 (①-1 + ②)x0.85

CASE2 (①-2 + ②)x0.85

CASE3 (③x0.9 + ②x0.9)x0.85

2. Special Vehicular Load 75t(735kN)

The special vehicular load is equally distributed.

Applied Area 45.00 m² Applied Load 735.0 / 45.0 = 16.33 kN/m²

3. Impact Coefficient

Impact coefficient is calculated as follows;

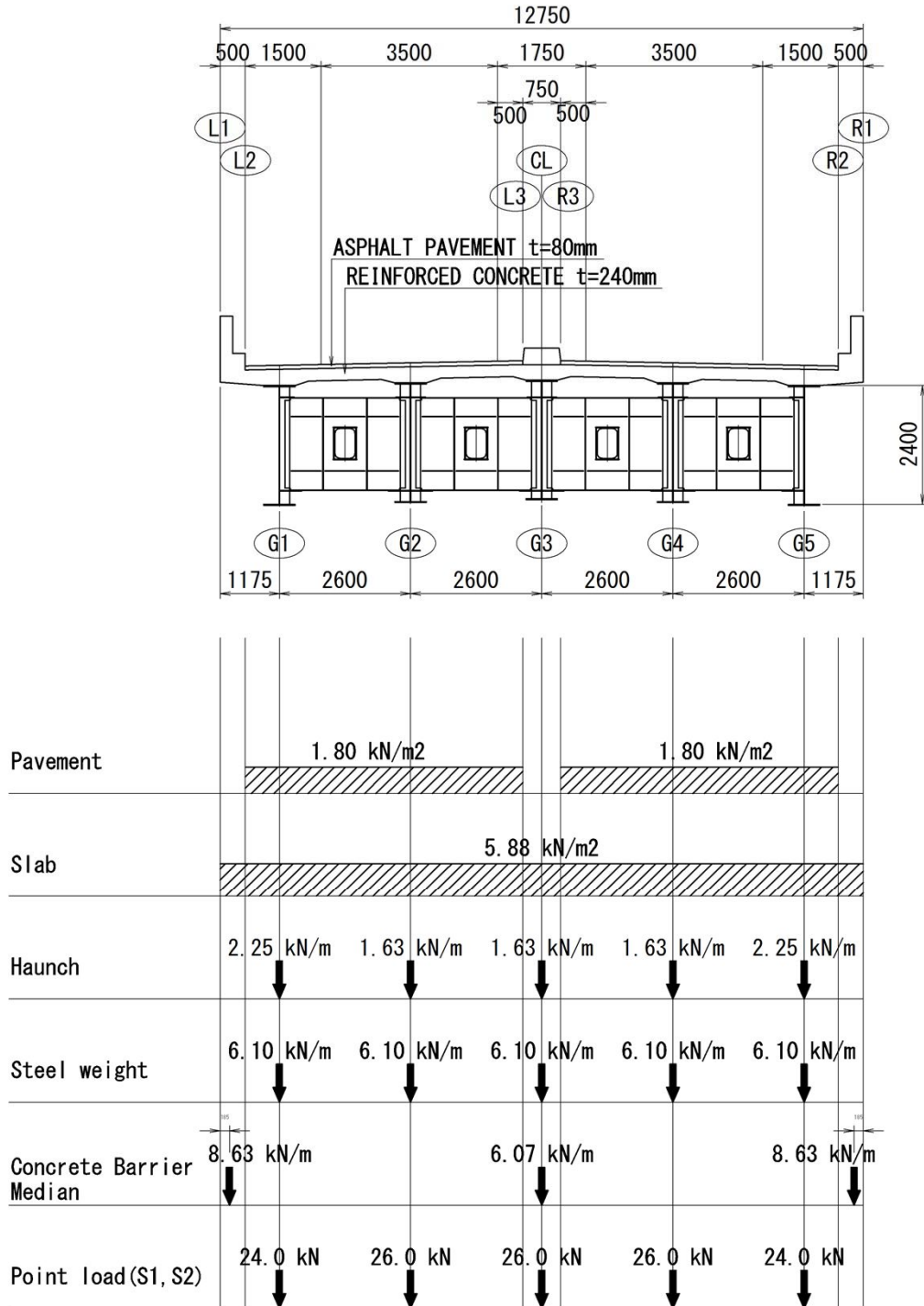
$$i = \frac{20}{50 + L}$$

	Span Length	(on CL)	Impact Coefficient
First Span	34.300 m	$i = 20 / (50 + 34.300) =$	0.237
Second Bearing	43.150 m	$i = 20 / (50 + 43.150) =$	0.215
Second Span	52.000 m	$i = 20 / (50 + 52.000) =$	0.196
Third Bearing	43.150 m	$i = 20 / (50 + 43.150) =$	0.215
Third Span	34.300 m	$i = 20 / (50 + 34.300) =$	0.237

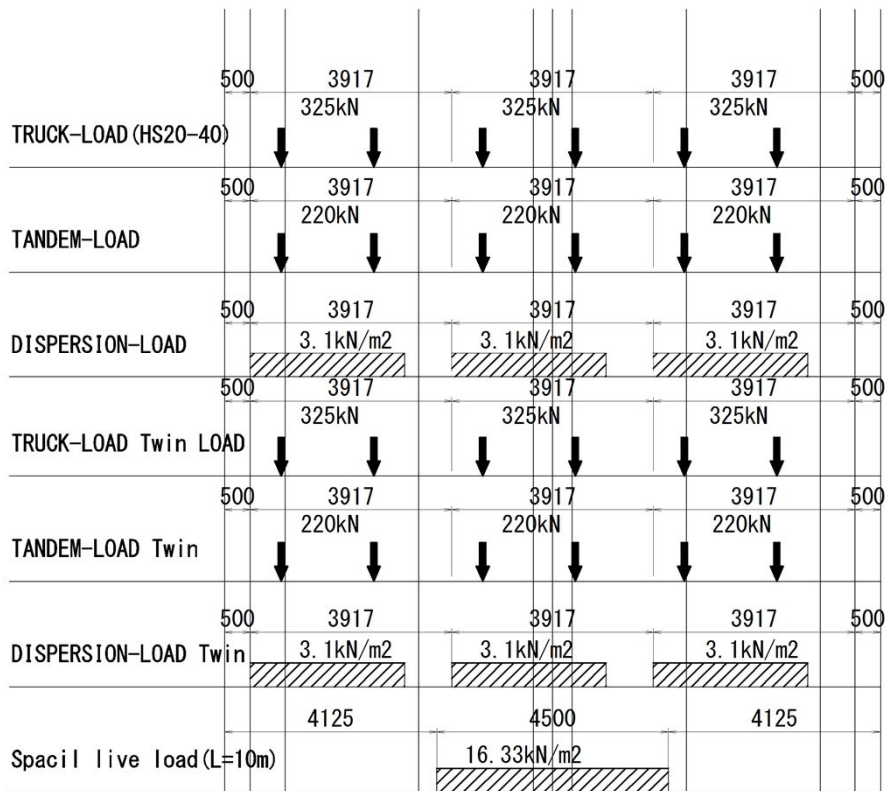
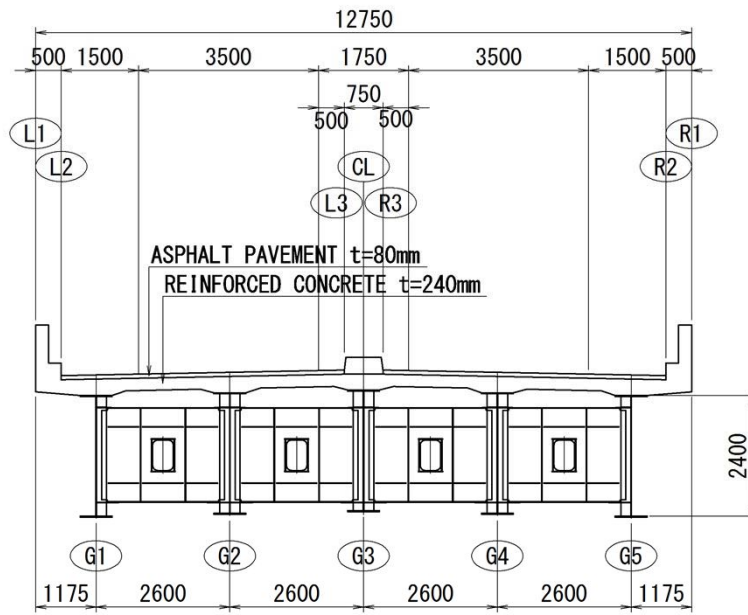
3-3 Load diagram and Load combination

(1) Load diagram

Dead load



Live load



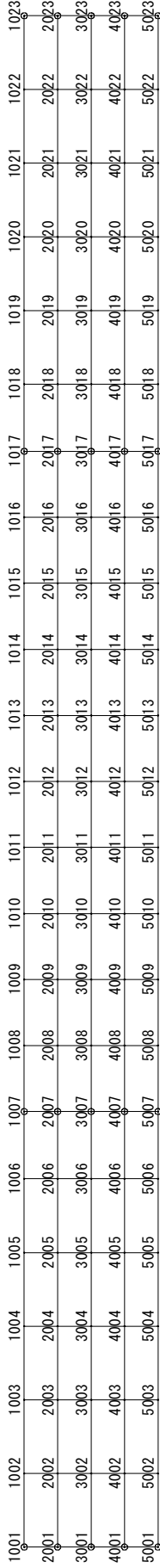
(2) Combination of Load

Case	Load	Note
11	Pavement	
12	Deck Slab	
13	Haunch	
14	Steel Weight	
15	Concrete Barrier	
16	Median	
17	Consentrated Load	
100-1	(①-1+②)	Truck + Vehicular Load
100-2	(①-2+②)	Tandem + Vehicular Load
111	(AASHTO two truck)x0.9	(Truck + Vehicular Load) x 2
200	Special Vehicular Load	

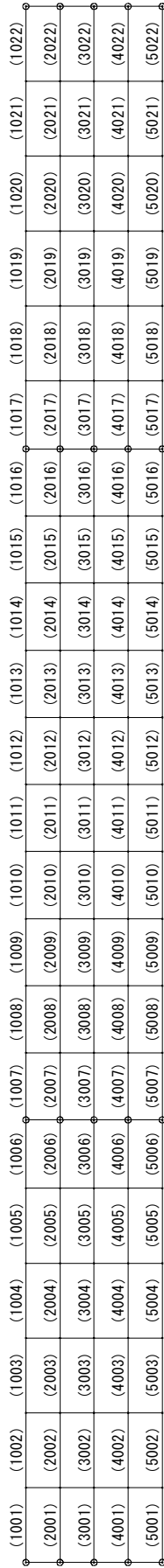
Case	Combination Case	Combination
300	Total of Dead Load	11+12+13+14+15+16+17;
302	Maximum Live Load	(100-1)x0.85,(100-2)x0.85,111x0.85,200
303	Dead Load + Live Load	300+302;

3-4 Skeleton Diagram

Node



Member Number



Member Number (Main Girder)

- G1 1001-1022
- G2 2001-2022
- G3 3001-3022
- G4 4001-4022
- G5 5001-5022

Cross Beam

- G1-G2 2101001-2101023
- G2-G3 2102001-2102023
- G3-G4 2103001-2103023
- G4-G5 2104001-2104023

3-5 Check of dead load and Reaction force aggregate

1. Check of dead load

Total span 120.600 m

Area Pavment 1326.600 m²
 Slab 1537.650 m²

Check of dead load

Load name	Load I. (kN/m, kN/m ²)	Line	A. N. L	Total (A)	Com (B)	compare (A/B)
			(m ² , N, m)	(kN)	(kN)	
Pavement	1.80		1326.60	2387.88	2387.88	1.00
Slab	5.88		1537.65	9041.38	9041.38	1.00
Haunch	2.25	G1	120.60	271.35		
	1.63	G2	120.60	196.58		
	1.63	G3	120.60	196.58		
	1.63	G4	120.60	196.58		
	2.25	G5	120.60	271.35		
			Subtotal	1132.43	1132.43	1.00
Steel weight	6.10	G1	120.60	735.66		
	6.10	G2	120.60	735.66		
	6.10	G3	120.60	735.66		
	6.10	G4	120.60	735.66		
	6.10	G5	120.60	735.66		
			Subtotal	3678.30	3678.30	1.00
Railing	8.63	L	120.60	1040.78		
	8.63	R	120.60	1040.78		
			Subtotal	2081.56	2081.56	1.00
Center divider	6.07	CL	120.60	732.04	732.04	1.00
Point load	24.00	S1, S2-G1	2	48.00		
	26.00	S1, S2-G2	2	52.00		
	26.00	S1, S2-G3	2	52.00		
	26.00	S1, S2-G4	2	52.00		
	24.00	S1, S2-G5	2	48.00		
			Subtotal	252.00	252.00	1.00
Total				19305.59	19305.60	1.00

Assuming steel Weight

	M. G.	End part	Total	Unit C.
	(kN)	(kN)	(kN)	(t)
A. S. W. ①	3678.30	39.65	3717.95	379.0

Real steel Weight

	The main structure	Total
	(t)	(t)
R. S. W. ②	375.674	375.674

weight ratio = ①/②x100= 101 % < 105% OK

3-6 Total Reaction Force

Superstructure Reaction Force (With impact)

			(S1)PF11					
		Name or Coefficient		1001	2001	3001	4001	5001
Dead load				451.03	306.54	375.46	306.54	451.03
AASHTO	Truk	①-1	Max	265.96	297.31	279.26	297.31	265.96
			Min	-58.48	-34.96	-33.64	-34.96	-58.48
	Tandem	①-2	Max	197.31	225.49	213.90	225.49	197.31
			Min	-40.53	-23.97	-23.17	-23.97	-40.53
Lane Load	Distributed Load	②	Max	113.90	110.47	101.67	110.47	113.90
			Min	-43.75	-29.39	-25.82	-29.39	-43.75
AASHTOxTWIN	Truk	③-1	Max	303.97	326.13	284.65	326.13	303.97
			Min	-78.66	-52.32	-49.12	-52.32	-78.66
	Tandem	③-2	Max	197.31	225.49	213.90	225.49	197.31
			Min	-40.53	-23.97	-23.17	-23.97	-40.53
Lane Load	Distributed Load	②	Max	113.90	110.47	101.67	110.47	113.90
			Min	-43.75	-29.39	-25.82	-29.39	-43.75
Special Vehicular Load	Distributed Load	④	Max	58.73	161.08	372.45	161.08	58.73
			Min	-27.20	-24.22	-23.25	-24.22	-27.20
Combination of Live Load	①-1+②	0.85	Max	322.88	346.61	323.79	346.61	322.88
			Min	-86.90	-54.70	-50.54	-54.70	-86.90
	①-2+②	0.85	Max	264.53	285.57	268.23	285.57	264.53
			Min	-71.64	-45.36	-41.64	-45.36	-71.64
	(③-1+②)x0.9	0.85	Max	319.67	334.00	295.53	334.00	319.67
			Min	-93.64	-62.51	-57.33	-62.51	-93.64
	(③-2+②)x0.9	0.85	Max	238.08	257.01	241.41	257.01	238.08
			Min	-64.47	-40.82	-37.48	-40.82	-64.47
④	1.0	Max	58.73	161.08	372.45	161.08	58.73	
		Min	-27.20	-24.22	-23.25	-24.22	-27.20	
Picked Up Live Load		PICK	Max	322.88	346.61	372.45	346.61	322.88
			Min	-93.64	-62.51	-57.33	-62.51	-93.64
D + L			Max	773.91	653.15	747.91	653.15	773.91
			Min	357.39	244.03	318.13	244.03	357.39
Dead load total				1890.60				

			PF12					
		Name or Coefficient		1007	2007	3007	4007	5007
Dead load				1824.53	1319.87	1473.41	1319.87	1824.53
AASHTO	Truk	①-1	Max	314.08	339.90	347.11	339.90	314.08
			Min	-62.21	-24.02	-22.19	-24.02	-62.21
	Tandem	①-2	Max	214.84	235.33	243.88	235.33	214.84
			Min	-43.01	-16.70	-15.37	-16.70	-43.01
Lane Load	Distributed Load	②	Max	365.81	346.57	317.75	346.57	365.81
			Min	-51.15	-17.40	-11.91	-17.40	-51.15
AASHTOxTWIN	Truk	③-1	Max	505.70	503.58	447.08	503.58	505.70
			Min	-70.42	-24.39	-22.68	-24.39	-70.42
	Tandem	③-2	Max	214.84	235.33	243.88	235.33	214.84
			Min	-43.01	-16.70	-15.37	-16.70	-43.01
Lane Load	Distributed Load	②	Max	365.81	346.57	317.75	346.57	365.81
			Min	-51.15	-17.40	-11.91	-17.40	-51.15
Special Vehicular Load	Distributed Load	④	Max	118.59	192.16	485.52	192.16	118.59
			Min	-21.47	-16.63	-15.32	-16.63	-21.47
Combination of Live Load	①-1+②	0.85	Max	577.91	583.50	565.13	583.50	577.91
			Min	-96.36	-35.21	-28.99	-35.21	-96.36
	①-2+②	0.85	Max	493.55	494.62	477.39	494.62	493.55
			Min	-80.04	-28.99	-23.19	-28.99	-80.04
	(③-1+②)x0.9	0.85	Max	666.71	650.36	585.09	650.36	666.71
			Min	-93.00	-31.97	-26.46	-31.97	-93.00
	(③-2+②)x0.9	0.85	Max	444.20	445.15	429.65	445.15	444.20
			Min	-72.03	-26.09	-20.87	-26.09	-72.03
	④	1.0	Max	118.59	192.16	485.52	192.16	118.59
			Min	-21.47	-16.63	-15.32	-16.63	-21.47
Picked Up Live Load		PICK	Max	666.71	650.36	585.09	650.36	666.71
			Min	-96.36	-35.21	-28.99	-35.21	-96.36
D + L			Max	2491.24	1970.23	2058.50	1970.23	2491.24
			Min	1728.17	1284.66	1444.43	1284.66	1728.17
Dead load total				7762.21				

			PF13						
		Name or Coefficient		1017	2017	3017	4017	5017	
Dead load				1824.53	1319.87	1473.41	1319.87	1824.53	
AASHTO	Truk	①-1	Max	314.08	339.90	347.11	339.90	314.08	
			Min	-62.21	-24.02	-22.19	-24.02	-62.21	
	Tandem	①-2	Max	214.84	235.33	243.88	235.33	214.84	
			Min	-43.01	-16.70	-15.37	-16.70	-43.01	
Lane Load	Distributed Load	②	Max	365.81	346.57	317.75	346.57	365.81	
			Min	-51.15	-17.40	-11.91	-17.40	-51.15	
AASHTOxTWIN	Truk	③-1	Max	505.70	503.58	447.08	503.58	505.70	
			Min	-70.42	-24.39	-22.68	-24.39	-70.42	
	Tandem	③-2	Max	214.84	235.33	243.88	235.33	214.84	
			Min	-43.01	-16.70	-15.37	-16.70	-43.01	
Lane Load	Distributed Load	②	Max	365.81	346.57	317.75	346.57	365.81	
			Min	-51.15	-17.40	-11.91	-17.40	-51.15	
Special Vehicular Load	Distributed Load	④	Max	118.59	192.16	485.52	192.16	118.59	
			Min	-21.47	-16.63	-15.32	-16.63	-21.47	
Combination of Live Load	①-1+②	0.85	Max	577.91	583.50	565.13	583.50	577.91	
			Min	-96.36	-35.21	-28.99	-35.21	-96.36	
	①-2+②	0.85	Max	493.55	494.62	477.39	494.62	493.55	
			Min	-80.04	-28.99	-23.19	-28.99	-80.04	
	(③-1+②)x0.9	0.85	Max	666.71	650.36	585.09	650.36	666.71	
			Min	-93.00	-31.97	-26.46	-31.97	-93.00	
	(③-2+②)x0.9	0.85	Max	444.20	445.15	429.65	445.15	444.20	
			Min	-72.03	-26.09	-20.87	-26.09	-72.03	
	④	1.0	Max	118.59	192.16	485.52	192.16	118.59	
			Min	-21.47	-16.63	-15.32	-16.63	-21.47	
Picked Up Live Load			PICK	Max	666.71	650.36	585.09	650.36	666.71
				Min	-96.36	-35.21	-28.99	-35.21	-96.36
D + L				Max	2491.24	1970.23	2058.50	1970.23	2491.24
				Min	1728.17	1284.66	1444.43	1284.66	1728.17
Dead load total				7762.21					

			(S2)PF14						
		Name or Coefficient		1023	2023	3023	4023	5023	
Dead load				451.03	306.54	375.46	306.54	451.03	
AASHTO	Truk	①-1	Max	265.96	297.31	279.26	297.31	265.96	
			Min	-58.48	-34.96	-33.64	-34.96	-58.48	
	Tandem	①-2	Max	197.31	225.49	213.90	225.49	197.31	
			Min	-40.53	-23.97	-23.17	-23.97	-40.53	
Lane Load	Distributed Load	②	Max	113.90	110.47	101.67	110.47	113.90	
			Min	-43.75	-29.39	-25.82	-29.39	-43.75	
AASHTOxTWIN	Truk	③-1	Max	303.97	326.13	284.65	326.13	303.97	
			Min	-78.66	-52.32	-49.12	-52.32	-78.66	
	Tandem	③-2	Max	197.31	225.49	213.90	225.49	197.31	
			Min	-40.53	-23.97	-23.17	-23.97	-40.53	
Lane Load	Distributed Load	②	Max	113.90	110.47	101.67	110.47	113.90	
			Min	-43.75	-29.39	-25.82	-29.39	-43.75	
Special Vehicular Load	Distributed Load	④	Max	58.73	161.08	372.45	161.08	58.73	
			Min	-27.20	-24.22	-23.25	-24.22	-27.20	
Combination of Live Load	①-1+②	0.85	Max	322.88	346.61	323.79	346.61	322.88	
			Min	-86.90	-54.70	-50.54	-54.70	-86.90	
	①-2+②	0.85	Max	264.53	285.57	268.23	285.57	264.53	
			Min	-71.64	-45.36	-41.64	-45.36	-71.64	
	(③-1+②)x0.9	0.85	Max	319.67	334.00	295.53	334.00	319.67	
			Min	-93.64	-62.51	-57.33	-62.51	-93.64	
	(③-2+②)x0.9	0.85	Max	238.08	257.01	241.41	257.01	238.08	
			Min	-64.47	-40.82	-37.48	-40.82	-64.47	
	④	1.0	Max	58.73	161.08	372.45	161.08	58.73	
			Min	-27.20	-24.22	-23.25	-24.22	-27.20	
Picked Up Live Load			PICK	Max	322.88	346.61	372.45	346.61	322.88
				Min	-93.64	-62.51	-57.33	-62.51	-93.64
D + L				Max	773.91	653.15	747.91	653.15	773.91
				Min	357.39	244.03	318.13	244.03	357.39
Dead load total				1890.60					

Substructure Reaction Force (Without impact)

			PF11					
		Name or Coefficient		1001	2001	3001	4001	5001
Dead load				451.03	306.54	375.46	306.54	451.03
AASHTO	Truk	①-1	Max	108.44	234.46	189.99	234.46	108.44
			Min	-28.50	-27.71	-27.53	-27.71	-28.50
	Tandem	①-2	Max	75.60	176.99	140.62	176.99	75.60
			Min	-19.56	-18.97	-18.93	-18.97	-19.56
Lane Load	Distributed Load	②	Max	70.43	99.82	100.46	99.82	70.43
			Min	-26.18	-25.63	-25.67	-25.63	-26.18
AASHTOxTWIN	Truk	③-1	Max	143.81	262.31	222.02	262.31	143.81
			Min	-42.19	-41.35	-40.47	-41.35	-42.19
	Tandem	③-2	Max	75.60	176.99	140.62	176.99	75.60
			Min	-19.56	-18.97	-18.93	-18.97	-19.56
Lane Load	Distributed Load	②	Max	70.43	99.82	100.46	99.82	70.43
			Min	-26.18	-25.63	-25.67	-25.63	-26.18
Special Vehicular Load	Distributed Load	④	Max	21.20	130.19	301.03	130.19	21.20
			Min	-22.55	-20.25	-18.87	-20.25	-22.55
Combination of Live Load	①-1+②	0.85	Max	152.04	284.14	246.88	284.14	152.04
			Min	-46.48	-45.34	-45.22	-45.34	-46.48
	①-2+②	0.85	Max	124.13	235.29	204.92	235.29	124.13
			Min	-38.88	-37.91	-37.91	-37.91	-38.88
	(③-1+②)x0.9	0.85	Max	163.89	277.03	246.70	277.03	163.89
			Min	-52.30	-51.24	-50.60	-51.24	-52.30
	(③-2+②)x0.9	0.85	Max	111.71	211.76	184.43	211.76	111.71
			Min	-34.99	-34.12	-34.12	-34.12	-34.99
④	1.0	Max	21.20	130.19	301.03	130.19	21.20	
		Min	-22.55	-20.25	-18.87	-20.25	-22.55	
Picked Up Live Load		PICK	Max	163.89	277.03	246.69	277.03	163.89
			Min	-52.30	-51.24	-50.59	-51.24	-52.30
D + L			Max	614.92	583.57	622.15	583.57	614.92
			Min	398.73	255.30	324.87	255.30	398.73
Dead load total				1890.60				
Live load total				1128.53				

			PF12					
		name. OR. factor		1007	2007	3007	4007	5007
Dead load				1824.53	1319.87	1473.41	1319.87	1824.53
AASHTO	Truk	①-1	Max	212.90	169.09	210.62	169.09	212.90
			Min	-21.96	-18.67	-17.90	-18.67	-21.96
	Tandem	①-2	Max	145.76	115.19	141.04	115.19	145.76
			Min	-15.25	-12.96	-12.43	-12.96	-15.25
Lane Load	Distributed Load	②	Max	299.83	287.33	260.92	287.33	299.83
			Min	-14.29	-12.06	-11.51	-12.06	-14.29
AASHTOxTWIN	Truk	③-1	Max	375.04	313.29	344.84	313.29	375.04
			Min	-22.35	-18.97	-18.18	-18.97	-22.35
	Tandem	③-2	Max	145.76	115.19	141.04	115.19	145.76
			Min	-15.25	-12.96	-12.43	-12.96	-15.25
Lane Load	Distributed Load	②	Max	299.83	287.33	260.92	287.33	299.83
			Min	-14.29	-12.06	-11.51	-12.06	-14.29
Special Vehicular Load	Distributed Load	④	Max	8.36	159.41	396.78	159.41	8.36
			Min	-17.33	-13.43	-12.35	-13.43	-17.33
Combination of Live Load	①-1+②	0.85	Max	435.82	387.96	400.81	387.96	435.82
			Min	-30.81	-26.12	-25.00	-26.12	-30.81
	①-2+②	0.85	Max	378.75	342.14	341.67	342.14	378.75
			Min	-25.11	-21.27	-20.35	-21.27	-25.11
	(③-1+②)x0.9	0.85	Max	516.28	459.47	463.41	459.47	516.28
			Min	-28.03	-23.74	-22.71	-23.74	-28.03
	(③-2+②)x0.9	0.85	Max	340.88	307.93	307.50	307.93	340.88
			Min	-22.60	-19.14	-18.31	-19.14	-22.60
④	1.0	Max	8.36	159.41	396.78	159.41	8.36	
		Min	-17.33	-13.43	-12.35	-13.43	-17.33	
Picked Up Live Load		PICK	Max	516.27	459.48	463.41	459.48	516.27
			Min	-30.81	-26.12	-25.00	-26.12	-30.81
D + L			Max	2340.80	1779.35	1936.82	1779.35	2340.80
			Min	1793.72	1293.75	1448.41	1293.75	1793.72
Dead load total				7762.21				
Live load total				2414.91				

			PF13					
		name.OR. factor		1017	2017	3017	4017	5017
Dead load				1824.53	1319.87	1473.41	1319.87	1824.53
AASHTO	Truk	①-1	Max	212.90	169.09	210.62	169.09	212.90
			Min	-21.96	-18.67	-17.90	-18.67	-21.96
	Tandem	①-2	Max	145.76	115.19	141.04	115.19	145.76
			Min	-15.25	-12.96	-12.43	-12.96	-15.25
Lane Load	Distributed Load	②	Max	299.83	287.33	260.92	287.33	299.83
			Min	-14.29	-12.06	-11.51	-12.06	-14.29
AASHTOxTWIN	Truk	③-1	Max	375.04	313.29	344.84	313.29	375.04
			Min	-22.35	-18.97	-18.18	-18.97	-22.35
	Tandem	③-2	Max	145.76	115.19	141.04	115.19	145.76
			Min	-15.25	-12.96	-12.43	-12.96	-15.25
Lane Load	Distributed Load	②	Max	299.83	287.33	260.92	287.33	299.83
			Min	-14.29	-12.06	-11.51	-12.06	-14.29
Special Vehicular Load	Distributed Load	④	Max	8.36	159.41	396.78	159.41	8.36
			Min	-17.33	-13.43	-12.35	-13.43	-17.33
Combination of Live Load	①-1+②	0.85	Max	435.82	387.96	400.81	387.96	435.82
			Min	-30.81	-26.12	-25.00	-26.12	-30.81
	①-2+②	0.85	Max	378.75	342.14	341.67	342.14	378.75
			Min	-25.11	-21.27	-20.35	-21.27	-25.11
	(③-1+②)x0.9	0.85	Max	516.28	459.47	463.41	459.47	516.28
			Min	-28.03	-23.74	-22.71	-23.74	-28.03
	(③-2+②)x0.9	0.85	Max	340.88	307.93	307.50	307.93	340.88
			Min	-22.60	-19.14	-18.31	-19.14	-22.60
	④	1.0	Max	8.36	159.41	396.78	159.41	8.36
			Min	-17.33	-13.43	-12.35	-13.43	-17.33
Picked Up Live Load		PICK	Max	516.27	459.48	463.41	459.48	516.27
			Min	-30.81	-26.12	-25.00	-26.12	-30.81
D + L			Max	2340.80	1779.35	1936.82	1779.35	2340.80
			Min	1793.72	1293.75	1448.41	1293.75	1793.72
Dead load total				7762.21				
Live load total				2414.91				

			PF14					
		name.OR. factor		1023	2023	3023	4023	5023
Dead load				451.03	306.54	375.46	306.54	451.03
AASHTO	Truk	①-1	Max	108.44	234.46	189.99	234.46	108.44
			Min	-28.50	-27.71	-27.53	-27.71	-28.50
	Tandem	①-2	Max	75.60	176.99	140.62	176.99	75.60
			Min	-19.56	-18.97	-18.93	-18.97	-19.56
Lane Load	Distributed Load	②	Max	70.43	99.82	100.46	99.82	70.43
			Min	-26.18	-25.63	-25.67	-25.63	-26.18
AASHTOxTWIN	Truk	③-1	Max	143.81	262.31	222.02	262.31	143.81
			Min	-42.19	-41.35	-40.47	-41.35	-42.19
	Tandem	③-2	Max	75.60	176.99	140.62	176.99	75.60
			Min	-19.56	-18.97	-18.93	-18.97	-19.56
Lane Load	Distributed Load	②	Max	70.43	99.82	100.46	99.82	70.43
			Min	-26.18	-25.63	-25.67	-25.63	-26.18
Special Vehicular Load	Distributed Load	④	Max	21.20	130.19	301.03	130.19	21.20
			Min	-22.55	-20.25	-18.87	-20.25	-22.55
Combination of Live Load	①-1+②	0.85	Max	152.04	284.14	246.88	284.14	152.04
			Min	-46.48	-45.34	-45.22	-45.34	-46.48
	①-2+②	0.85	Max	124.13	235.29	204.92	235.29	124.13
			Min	-38.88	-37.91	-37.91	-37.91	-38.88
	(③-1+②)x0.9	0.85	Max	163.89	277.03	246.70	277.03	163.89
			Min	-52.30	-51.24	-50.60	-51.24	-52.30
	(③-2+②)x0.9	0.85	Max	111.71	211.76	184.43	211.76	111.71
			Min	-34.99	-34.12	-34.12	-34.12	-34.99
	④	1.0	Max	21.20	130.19	301.03	130.19	21.20
			Min	-22.55	-20.25	-18.87	-20.25	-22.55
Picked Up Live Load		PICK	Max	163.89	277.03	246.69	277.03	163.89
			Min	-52.30	-51.24	-50.59	-51.24	-52.30
D + L			Max	614.92	583.57	622.15	583.57	614.92
			Min	398.73	255.30	324.87	255.30	398.73
Dead load total				1890.60				
Live load total				1128.53				

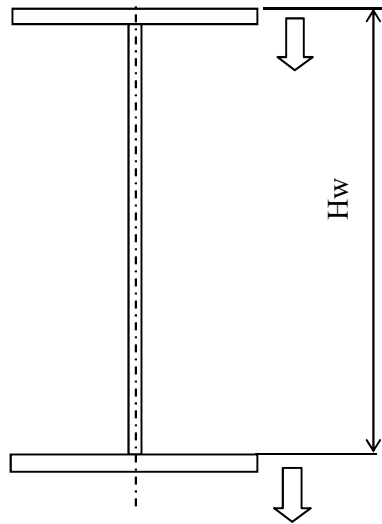
§4. Design of Main Girder

4-1 Design Method

In the design of main girder, the cross section is determined by using the software which automatically downloads the cross sectional force calculated in §3. and can design Steel-I Girder automatically.

(1) Method for Determination of Cross Section of Stiffener

- 1) The location of cross section change is same with the location of joint.
The longest length of material is approximately 12.0m or less due to the restriction of transportation.
- 2) The maximum difference of flange thickness is half of the thicker base material or less and 25mm or less.
- 3) Regarding the compressive flange, reduction of stress due to local buckling is considered for upper and lower flange.
- 4) Regarding the tensile flange, the cross section is determined considering the influence of hole of bolts
Minimum thickness is 1/16 of 1/2 of the width of the flange
- 5) The flange width is constant and cross section is changed with the thickness of flange.
At bearing, on the other hand, the cross section is changed with the size of bearing.
- 6) The height of the main girder shall be from the upper flange top to the lower flange upper.



7) Minimum thicknesses are shown as follows.

The minimum difference of flange thickness is 2mm and the thickness is measured in increments of 1mm.

< Upper Compressive Flange >

	(mm)		
Material	SM400	SM490Y	SM570
Standard	b/16	b/16	b/16
Flange Width	590	590	590
Minimum Thickness of Plate	19	19	19

< Lower Compressive Flange >

(mm)

Material	SM400	SM490Y	SM570
Standard	b/16	b/16	b/16
Flange Width b	590	590	590
Minimum Thickness of Plate	19	19	19

< Web >

(mm)

Material	SM400	SM490Y	SM570
Calculation Equation	Hw/256	Hw/209	Hw/188
Calculated Value	9.38	11.48	12.77
Minimum Thickness of Plate	10.00	12.00	13.00
Height of Web Plate Hw	2400	2400	2400

(2) Vertical Stiffener

- 1) The cross section is determined as follows according to JSHB II—11.4.4.
 - a) The width of vertical stiffener is the value or more which is the total of 1/30 of web height and 50mm.
 - b) The material is SM400.
 - c) The thickness of vertical stiffener is 1/13 of the width or more.
 - d) The interval of vertical stiffener "a" used in the equation (11.4.7) is the maximum value which satisfies the assessment equation stated in 11.4.3

(3) Horizontal Stiffener

- 1) The number of horizontal stiffener rows is one according to the girder height.
The cross section is determined to be satisfied with the stiffness stated in JSHB II-11.4.7.

(4) Bearing Stiffener

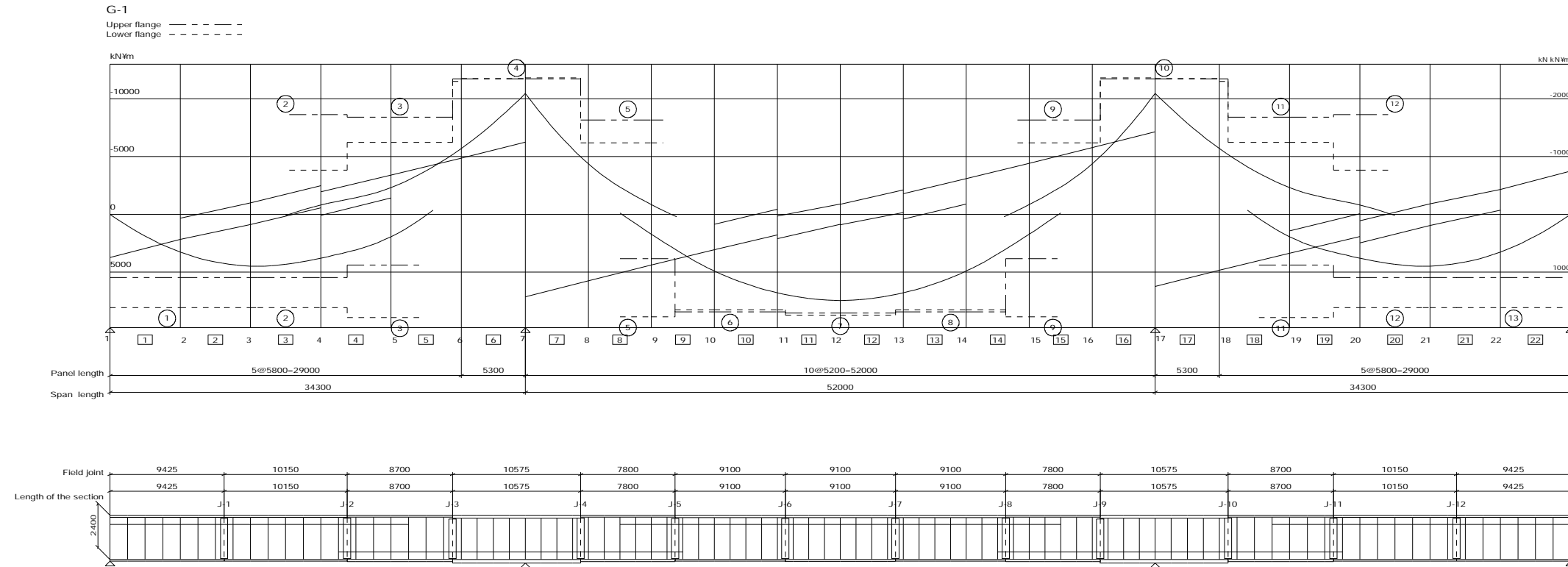
- 1) The bearing stiffener is determined by the structure at the load concentrated point stated in JSHB II-11.5.

(5) Design Method for Field Joint

- 1) For the bending stress, the design stress of field joint is the greater value comparing with the applied stress and 75% of the total strength.
- 2) The minimum number of bolt rows on the compressive flange is two.
- 3) Stress deducting a hole of the tensile flange is increased by 1.1 times of net cross sectional area.
- 4) Allowable force of Torshear type high strength bolt (S10T) M22 is 54 kN
- 5) The number of bolt rows and the thickness of splice plate is determined on the thinner cross section of the base material at joint.
- 6) The size of the hole of the bolt shall be $\phi 25$
- 7) The maximum number of bolt rows is eight while it is allowed to be 12 when unavoidable.
- 8) The splice plate is determined by the design stress which is 75% or more of the total strength.
- 9) The distance between the edge of splice plate and the edge of base material is 5mm.

4-2 Calculation of Main Girder

STRESS DIAGRAM(1/5) S=1:400



		Unit: mm N/mm ²																																															
Section		1		2		3		4		5		6		7		8		9		10		11		12		13																							
		Sec-2		Sec-2		Sec-3		Sec-4		Sec-5		Sec-6		Sec-7		Sec-8		Sec-9		Sec-10		Sec-11		Sec-12		Sec-13																							
Upper flange	Width	590		590		590		590		590		590		590		590		590		590		590		590		590																							
	Thickness	22(3)		22(3)		20(3)		31(3)		19(3)		26(3)		26(3)		26(3)		19(3)		31(3)		20(3)		22(3)		22(3)																							
Web	Height	2378	2378	2378	2378	2380	2380	2380	2369	2369	2381	2381	2374	2374	2374	2374	2381	2381	2369	2369	2380	2380	2380	2378	2378	2378	2378	2378																					
	Thickness	12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)																							
Lower flange	Width	590		590		590		590		590		590		590		590		590		590		590		590		590																							
	Thickness	19(3)		19(3)		23(3)		39(3)		23(3)		19(3)		21(3)		19(3)		23(3)		39(3)		23(3)		19(3)		19(3)																							
Upper flange	f/D	0	-104	-110	-80	31	-82	32	129	188	188	128	-78	-153	-162	-153	-78	128	188	188	129	-82	32	-80	31	-110	-104	0																					
	f/B	210	133	133	133	210	110	210	210	210	210	99	186	186	186	99	210	210	210	210	210	110	210	133	210	133	133	210																					
	f/B-f/D	210	29	23	53	179	28	178	81	22	22	82	21	33	24	33	21	82	22	22	81	28	178	53	179	23	29	210																					
Lower flange	f/D	0	111	117	85	-33	77	-30	-121	-165	-165	-118	72	177	179	177	72	-118	-165	-165	-121	77	-30	85	-33	117	111	0																					
	f/B	210	210	210	210	99	210	146	146	185	186	146	210	210	210	210	210	146	186	185	146	210	146	210	99	210	210	210																					
	f/B-f/D	210	99	93	125	66	133	116	25	20	21	28	138	33	31	33	138	28	21	20	25	133	116	125	66	93	99	210																					
Web	f/N	26	10	8	17	17	17	17	33	44	50	42	27	14	6	14	27	42	50	44	33	17	17	17	17	17	8	10	26																				
	f/N	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120																				
	Combined	0.05	0.28	0.31	0.18	0.05	0.17	0.04	0.44	0.89	0.94	0.48	0.19	0.70	0.71	0.70	0.19	0.48	0.94	0.89	0.44	0.17	0.04	0.18	0.05	0.31	0.28	0.05																					
Calculated points		Left		J-1		J-2		J-2		Left		Left		J-3		Max Left		Max Right		J-4		J-5		J-6		J-7		J-8		J-9		Max Left		Max Right		J-10		Right		Right		J-11		J-11		J-12		Right	
Ufig /Bpl																																																	
Lfig /Bpl		121		93								141				141				78		177				177		87		141				141				93		34				121					

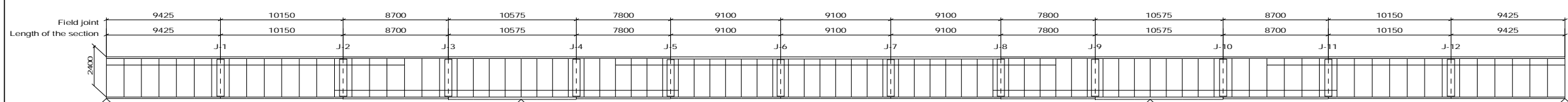
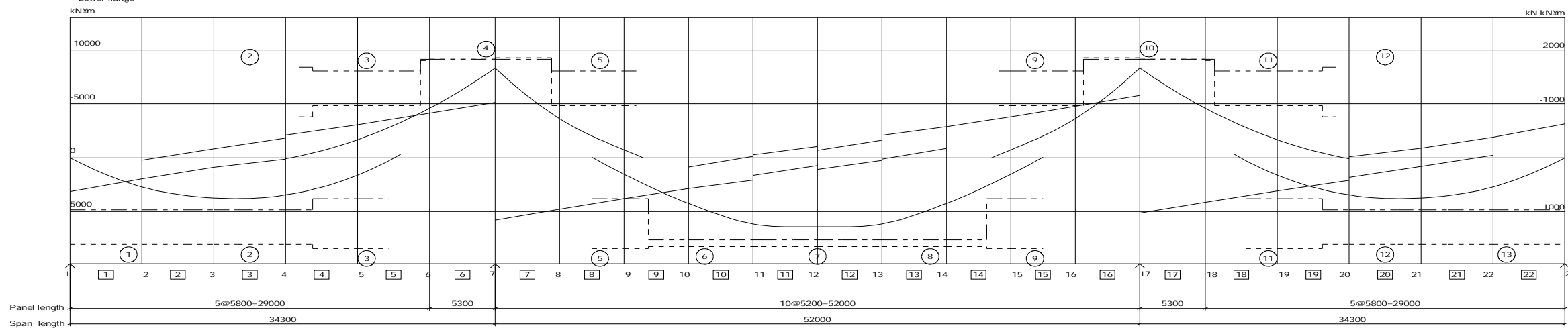
Grade (1):SM400
 (2):SM490
 (3):SM490Y
 (4):SM570

Bago bridge girder part G-1

STRESS DIAGRAM(2/5) S=1:400

G-2

Upper flange - - - - -
Lower flange - - - - -



		Unit: N/mm ²																										
Section		1		2		3		4		5		6		7		8		9		10		11		12		13		
Upper flange		Sec-1		Sec-2		Sec-3		Sec-4		Sec-5		Sec-6		Sec-7		Sec-8		Sec-9		Sec-10		Sec-11		Sec-12		Sec-13		
Width	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	
Thickness	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	21(3)	
Web	Height	2379	2379	2379	2379	2379	2381	2381	2378	2378	2381	2381	2375	2375	2375	2375	2381	2381	2378	2378	2381	2381	2379	2379	2379	2379	2379	
Thickness	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	12(3)	
Lower flange	Width	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	590	
Thickness	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	19(3)	
Upper flange	f/D	0	-88	-95	-74	11	-77	11	108	191	191	107	-68	-141	-144	-141	-68	107	191	191	108	-77	11	-74	11	-95	-88	0
f/b	210	121	121	121	210	99	210	210	210	210	210	99	172	172	172	172	99	210	210	210	210	99	210	121	210	121	210	
f/b-f/D	210	33	26	47	199	22	199	102	19	19	103	31	31	28	28	31	31	103	19	19	102	22	199	47	199	26	33	
Lower flange	f/D	0	92	99	77	-11	74	-11	-104	-167	-167	-103	66	160	164	160	66	-103	-167	-167	-104	74	-11	77	-11	99	92	0
f/b	210	210	210	210	99	210	121	121	185	186	121	210	210	210	210	210	210	121	186	185	121	210	121	210	210	210	210	
f/b-f/D	210	118	111	133	88	136	110	17	18	19	18	144	50	46	46	50	144	18	19	18	17	136	110	133	88	111	118	
Web	f/b	22	9	8	17	17	17	28	36	41	34	24	11	8	7	11	24	34	41	36	28	17	17	17	17	17	8	9
f/b	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
Combined	0.03	0.19	0.22	0.15	0.02	0.15	0.02	0.31	0.89	0.92	0.33	0.14	0.57	0.59	0.59	0.57	0.14	0.33	0.92	0.89	0.31	0.15	0.02	0.15	0.02	0.22	0.19	0.03
Calculated points	Left	J-1		J-2	J-2	Left	Left	J-3	Max Left	Max Right	J-4	J-5	J-6		J-7	J-8	J-9	Max Left	Max Right	J-10	J-11	J-11	J-11	Left	Left		J-12	Right
Uflg /Bpl								119			117						117				119	14						
Lflg /Bpl	100		84									72	175			175	72					81						100

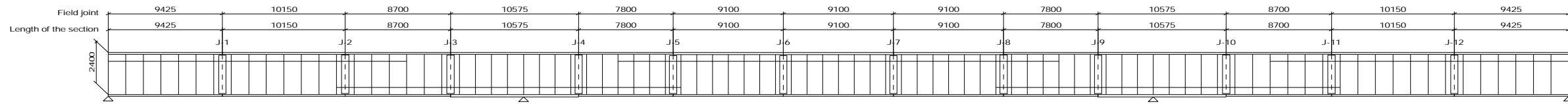
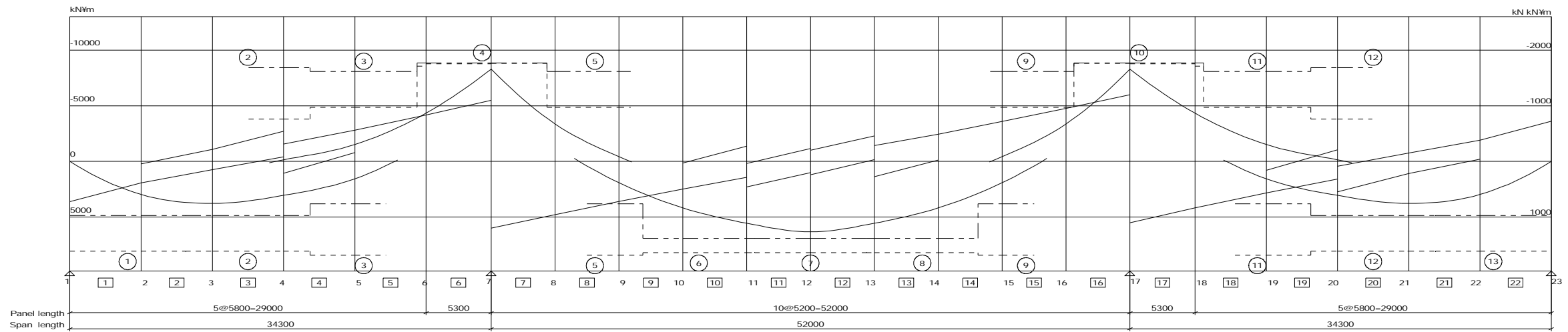
Grade (1):SM400
(2):SM490
(3):SM490Y
(4):SM570

Bago bridge girder part G-2

STRESS DIAGRAM(3/5) S=1:400

G-3

Upper flange ———
Lower flange - - - - -



		Unit Fmm N/mm ²																																						
Section		1			2			3			4			5			6			7			8			9			10			11			12			13		
Upper flange		Sec-1			Sec-2			Sec-3			Sec-4			Sec-5			Sec-6			Sec-7			Sec-8			Sec-9			Sec-10			Sec-11			Sec-12			Sec-13		
Upper flange	Width	590																																						
	Thickness	21(3)			21(3)			19(3)			21(3)			19(3)			24(3)			24(3)			24(3)			19(3)			21(3)			19(3)			21(3)					
Web	Height	2379	2379	2379	2379	2379	2381	2381	2381	2379	2379	2381	2381	2376	2376	2376	2381	2381	2379	2379	2381	2381	2381	2376	2376	2376	2381	2381	2379	2379	2381	2381	2381	2379	2379	2379	2379	2379		
	Thickness	12(3)			12(3)			12(3)			12(3)			12(3)			12(3)			12(3)			12(3)			12(3)			12(3)			12(3)			12(3)			12(3)		
Lower flange	Width	590																																						
	Thickness	19(3)			19(3)			21(3)			27(3)			21(3)			19(3)			19(3)			19(3)			21(3)			27(3)			21(3)			19(3)			19(3)		
Upper flange	f/D	0	-92	-94	-65	15	-68	15	101	198	198	101	-75	-131	-146	-131	-75	101	198	198	101	-68	15	-65	15	-94	-92	0												
	f/a	210	121	121	121	210	99	210	210	210	210	99	159	159	99	210	210	210	210	210	99	210	121	210	121	121	121	210	210	121	121	121	210	210	210					
	f/a-f/D	210	29	27	56	195	31	195	109	12	12	109	24	28	13	28	24	109	12	12	109	31	195	56	195	27	29	210												
Lower flange	f/D	0	96	98	68	-15	65	-15	-97	-175	-175	-97	71	146	162	146	71	-97	-175	-175	-97	65	-15	68	-15	98	96	0												
	f/a	210	210	210	210	99	210	121	121	185	186	121	210	210	210	210	210	210	121	186	185	121	210	121	210	99	210	210	121	121	121	210	210	210						
	f/a-f/D	210	114	112	142	84	145	106	24	10	11	24	139	64	48	64	139	24	11	10	24	145	106	142	84	112	114	210												
Web	f/N	25	8	8	14	14	14	14	28	39	42	34	22	15	8	15	22	34	42	39	28	14	14	14	14	8	8	25												
	f/a	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120					
	Combined	0.04	0.21	0.22	0.12	0.02	0.12	0.02	0.28	0.96	0.98	0.31	0.16	0.48	0.58	0.48	0.16	0.31	0.98	0.96	0.28	0.12	0.02	0.12	0.02	0.12	0.02	0.22	0.21	0.04										
Calculated points		Left	J-1		J-2	J-2	Left	Left	J-3	Max Left	Max Right	J-4	J-5	J-6		J-7	J-8	J-9	Max Left	Max Right	J-10	J-11	J-11	J-11	Left	Left			J-12	Right										
Uflg /Bpl					16				111			110						110				111																		
Lflg /Bpl		105		75								78	160		160	78					71											105								

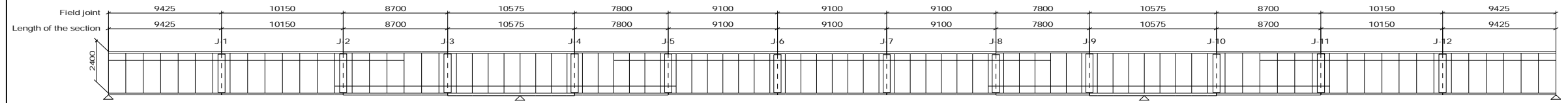
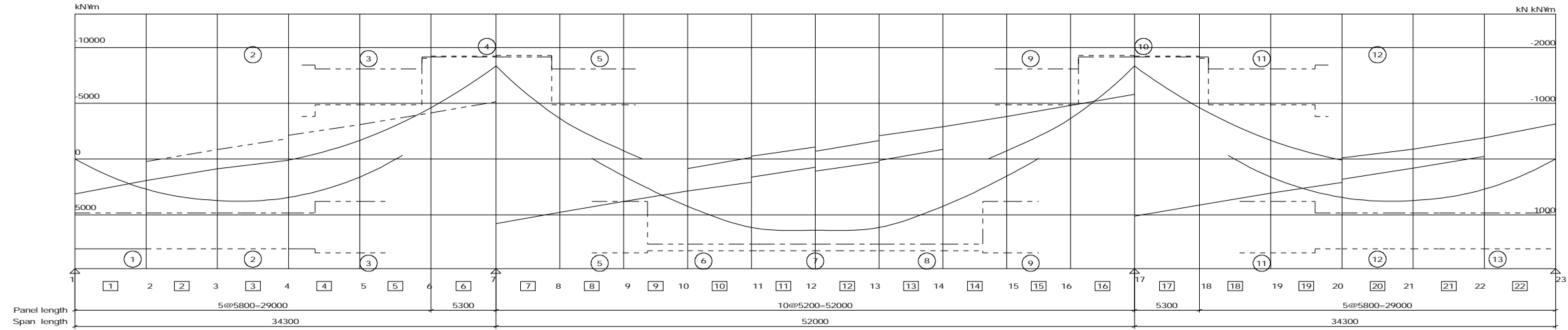
Grade (1):SM400
(2):SM490
(3):SM490Y
(4):SM570

Bago bridge girder part G-3

STRESS DIAGRAM(4/5) S=1:400

G-4

Upper flange - - - - -
Lower flange - - - - -



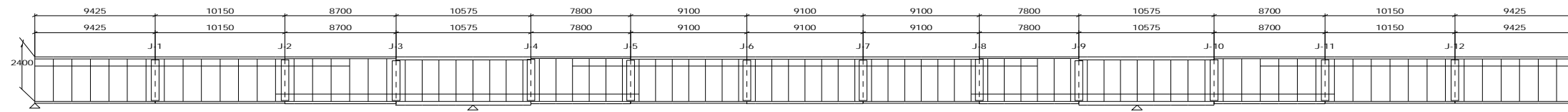
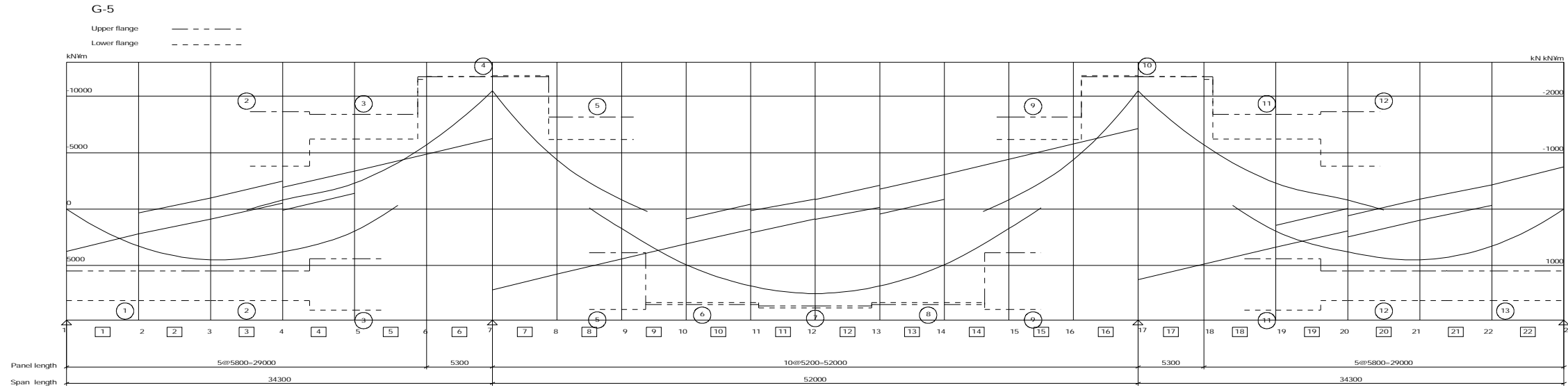
		Unit: N/mm ²																											
Section		1		2		3		4		5		6		7		8		9		10		11		12		13			
Upper flange	Width	590		590		590		590		590		590		590		590		590		590		590		590		590			
	Thickness	21(3)		21(3)		19(3)		22(3)		19(3)		25(3)		25(3)		25(3)		19(3)		22(3)		19(3)		21(3)		21(3)			
Web	Height	2379	2379	2379	2379	2379	2381	2381	2381	2378	2378	2381	2381	2375	2375	2375	2375	2381	2381	2378	2378	2381	2381	2381	2379	2379	2379	2379	
	Thickness	12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)			
Lower flange	Width	590		590		590		590		590		590		590		590		590		590		590		590		590			
	Thickness	19(3)		19(3)		21(3)		29(3)		21(3)		19(3)		19(3)		19(3)		21(3)		29(3)		21(3)		19(3)		19(3)			
Upper flange	f/D	0	-88	-95	-74	11	-77	11	108	191	191	107	-68	-141	-144	-144	-141	-68	107	191	191	108	-77	11	-74	11	-95	-88	0
	f/A	210	121	121	121	210	99	210	210	210	210	99	172	172	172	172	99	210	210	210	210	99	210	121	210	121	121	210	
	f/A-f/D	210	33	26	47	199	22	199	102	19	19	103	31	31	28	28	31	31	103	19	19	102	22	199	47	199	26	33	210
Lower flange	f/D	0	92	99	77	-11	74	-11	-104	-167	-167	-103	66	160	164	164	160	66	-103	-167	-167	-104	74	-11	77	-11	99	92	0
	f/A	210	210	210	210	99	210	121	121	185	186	121	210	210	210	210	210	121	186	185	121	210	121	210	121	210	99	210	210
	f/A-f/D	210	118	111	133	88	136	110	17	18	19	18	144	50	46	46	50	144	18	19	18	17	136	110	133	88	111	118	210
Web	f/N	22	9	8	17	17	17	17	28	36	41	34	24	11	8	7	11	24	34	41	36	28	17	17	17	17	8	9	22
	f/N	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
	Combined	0.03	0.19	0.22	0.15	0.02	0.15	0.02	0.31	0.89	0.92	0.33	0.14	0.57	0.59	0.59	0.57	0.14	0.33	0.92	0.89	0.31	0.15	0.02	0.15	0.02	0.22	0.19	0.03
Calculated points		Left	J-1		J-2	J-2	Left	Left	J-3	Max Left	Max Right	J-4	J-5	J-6			J-7	J-8	J-9	Max Left	Max Right	J-10	J-11	J-11	Left	Left		J-12	Right
Uflg /Bpl						13			132			117					195	80				132		14				100	
Lflg /Bpl			100		84																								

Grade (1):SM400
(2):SM490
(3):SM490Y
(4):SM570

Determinant factor
A: Tensile stress degree
B: Compressive stress degree
C: Pore resilience
D: Flange free protrusion
E: Flange thickness difference

Bago bridge girder part G-4

STRESS DIAGRAM(5/5) S=1:400



		Unit: mm N/mm ²																											
		1		2		3		4		5		6		7		8		9		10		11		12		13			
Section		Sec-1		Sec-2		Sec-3		Sec-4		Sec-5		Sec-6		Sec-7		Sec-8		Sec-9		Sec-10		Sec-11		Sec-12		Sec-13			
Upper flange	Width	590		590		590		590		590		590		590		590		590		590		590		590		590			
	Thickness	22(3)		22(3)		20(3)		31(3)		19(3)		26(3)		26(3)		26(3)		19(3)		31(3)		20(3)		22(3)		22(3)			
Web	Height	2378	2378	2378	2378	2378	2380	2380	2369	2369	2381	2381	2374	2374	2374	2381	2381	2369	2369	2380	2380	2380	2380	2378	2378	2378	2378	2378	2378
	Thickness	12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)		12(3)			
Lower flange	Width	590		590		590		590		590		590		590		590		590		590		590		590		590			
	Thickness	19(3)		19(3)		23(3)		39(3)		23(3)		19(3)		21(3)		19(3)		23(3)		39(3)		23(3)		19(3)		19(3)			
Upper flange	f/D	0	-104	-110	-80	31	-82	32	129	188	188	128	-78	-153	-162	-153	-78	128	188	188	129	-82	32	-80	31	-110	-104	0	
	f/B	210	133	133	133	210	110	210	210	210	210	99	110	186	186	186	99	210	210	210	210	110	210	133	210	133	133	210	
	f/B-f/D	210	29	23	53	179	28	178	81	22	22	82	21	33	24	33	21	82	22	22	81	28	178	53	179	23	29	210	
Lower flange	f/D	0	111	117	85	-33	77	-30	-121	-165	-118	72	177	179	177	72	-118	-165	-165	-121	77	-30	85	-33	117	111	0		
	f/B	210	210	210	210	99	210	146	146	185	186	146	210	210	210	210	146	186	185	146	210	146	210	146	210	99	210	210	
	f/B-f/D	210	99	93	125	66	133	116	25	20	21	28	138	33	31	33	138	28	21	20	25	133	116	125	66	93	99	210	
Web	f/N	26	10	8	17	17	17	17	33	44	50	42	27	14	6	14	27	42	50	44	33	17	17	17	17	8	10	26	
	f/B	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	
	Combined	0.05	0.28	0.31	0.18	0.05	0.17	0.04	0.44	0.89	0.94	0.18	0.48	0.19	0.70	0.70	0.19	0.48	0.94	0.89	0.44	0.17	0.04	0.18	0.05	0.31	0.28	0.05	
Calculated points		Left	J-1		J-2	J-2	Left	Left	J-3	Max Left	Max Right	J-4	J-5	J-6	J-7	J-8	J-9	Max Left	Max Right	J-10	Right	Right	J-11	J-11	J-11	J-12	Right		
Ufig /Bpl					34				141			141					141								34				
Lfig /Bpl		121		93								78	193		177	78							93				121		

Grade (1):SM400
(2):SM490
(3):SM490Y
(4):SM570

Bago bridge girder part G-5

4-3. Calculation Result of Field joint for Main Girder

1) Flange

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Flg THK	Flg stress	Req Bolts	Applied Bolts	Bolts Stress	Spl THK	Spl THK	Req Area	Total Area	Group No.
							σ_t	σ_c	τ		σ_{tn}	n		ρ	1	2	Ar	As	
1	G-1	J-1(Sec-2)	UFLG	590	22	SM490Y	---	-104	0	---	---	12.5	18	74863	12	14	101.3	142.4	*1
2	G-1	J-1(Sec-2)	LFLG	590	19	SM490Y	158	---	0	---	121	13.6	20	73316	14	12	69.8	113.7	17
4	G-1	J-2(Sec-2)	UFLG	590	22	SM490Y	158	100	0	---	34	15.7	20	84893	12	14	80.9	113.7	*3
5	G-1	J-2(Sec-2)	LFLG	590	19	SM490Y	158	74	0	---	93	13.6	20	73316	14	12	69.8	113.7	*4
7	G-1	J-3(Sec-3)	UFLG	590	20	SM490Y	158	---	0	---	141	14.3	20	77175	12	14	73.5	113.7	*5
8	G-1	J-3(Sec-3)	LFLG	590	23	SM490Y	---	-121	0	---	---	15.2	24	68607	14	12	112.8	142.4	*6
10	G-1	J-4(Sec-5)	UFLG	590	19	SM490Y	158	---	0	---	141	13.6	20	73316	12	14	69.8	113.7	17
11	G-1	J-4(Sec-5)	LFLG	590	23	SM490Y	---	-118	0	---	---	14.8	24	66711	14	12	109.7	142.4	6
13	G-1	J-5(Sec-5)	UFLG	590	19	SM490Y	---	-78	0	---	---	8.1	12	72773	10	12	88.2	120.4	*9
14	G-1	J-5(Sec-5)	LFLG	590	23	SM490Y	158	---	0	---	78	16.4	20	88751	14	12	84.5	113.7	*10
16	G-1	J-6(Sec-6)	UFLG	590	26	SM490Y	---	-153	0	---	---	21.7	30	78172	14	16	126.1	164.4	*11
17	G-1	J-6(Sec-6)	LFLG	590	19	SM490Y	177	---	0	---	177	18.3	24	82511	14	14	94.3	123.2	*12
19	G-1	J-7(Sec-8)	UFLG	590	26	SM490Y	---	-153	0	---	---	21.7	30	78172	14	16	126.1	164.4	11
20	G-1	J-7(Sec-8)	LFLG	590	19	SM490Y	177	---	0	---	177	18.3	24	82511	14	14	94.3	123.2	12
22	G-1	J-8(Sec-9)	UFLG	590	19	SM490Y	---	-78	0	---	---	8.1	12	72773	10	12	88.2	120.4	9
23	G-1	J-8(Sec-9)	LFLG	590	23	SM490Y	158	---	0	---	78	16.4	20	88751	14	12	84.5	113.7	10
25	G-1	J-9(Sec-9)	UFLG	590	19	SM490Y	158	---	0	---	141	13.6	20	73316	12	14	69.8	113.7	17
26	G-1	J-9(Sec-9)	LFLG	590	23	SM490Y	---	-118	0	---	---	14.8	24	66711	14	12	109.7	142.4	6
28	G-1	J-10(Sec-11)	UFLG	590	20	SM490Y	158	---	0	---	141	14.3	20	77175	12	14	73.5	113.7	5
29	G-1	J-10(Sec-11)	LFLG	590	23	SM490Y	---	-121	0	---	---	15.2	24	68607	14	12	112.8	142.4	6
31	G-1	J-11(Sec-12)	UFLG	590	22	SM490Y	158	100	0	---	34	15.7	20	84893	12	14	80.9	113.7	3
32	G-1	J-11(Sec-12)	LFLG	590	19	SM490Y	158	74	0	---	93	13.6	20	73316	14	12	69.8	113.7	4
34	G-1	J-12(Sec-13)	UFLG	590	22	SM490Y	---	-104	0	---	---	12.5	18	74863	12	14	101.3	142.4	1

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Flg THK	Flg stress	Req Bolts	Applied Bolts	Bolts Stress	Spl THK 1	Spl THK 2	Req Area Ar	Total Area As	Group No.
							σ_t	σ_c	τ		σ_{tn}	n		ρ	1	2			
35	G-1	J-12(Sec-13)	LFLG	590	19	SM490Y	158	---	0	---	121	13.6	20	73316	14	12	69.8	113.7	17
37	G-2	J-1(Sec-1)	UFLG	590	21	SM490Y	---	91	0	---	---	10.4	12	93699	12	12	92.9	132.0	22
38	G-2	J-1(Sec-1)	LFLG	590	19	SM490Y	158	---	0	---	100	13.6	20	73316	14	12	69.8	113.7	17
40	G-2	J-2(Sec-2)	UFLG	590	21	SM490Y	158	91	0	---	13	13.5	18	80850	10	12	92.9	120.4	*14
41	G-2	J-2(Sec-2)	LFLG	590	19	SM490Y	158	74	0	---	84	13.6	20	73316	14	12	69.8	113.7	4
43	G-2	J-3(Sec-3)	UFLG	590	19	SM490Y	158	---	0	---	119	13.6	20	73316	12	14	69.8	113.7	17
44	G-2	J-3(Sec-3)	LFLG	590	21	SM490Y	---	-104	0	---	---	11.9	18	71450	12	12	106.3	132.0	*15
46	G-2	J-4(Sec-5)	UFLG	590	19	SM490Y	158	---	0	---	117	13.6	20	73316	12	14	69.8	113.7	17
47	G-2	J-4(Sec-5)	LFLG	590	21	SM490Y	---	-103	0	---	---	11.8	18	70684	12	12	105.2	132.0	15
49	G-2	J-5(Sec-5)	UFLG	590	19	SM490Y	---	74	0	---	---	7.7	12	69362	10	12	84.1	120.4	9
50	G-2	J-5(Sec-5)	LFLG	590	21	SM490Y	158	---	0	---	72	15.0	20	81034	14	12	77.2	113.7	24
52	G-2	J-6(Sec-6)	UFLG	590	25	SM490Y	---	-141	0	---	---	19.3	24	86654	14	16	120.9	164.4	*16
53	G-2	J-6(Sec-6)	LFLG	590	19	SM490Y	175	---	0	---	175	16.6	20	89570	14	12	85.3	113.7	*17
55	G-2	J-7(Sec-8)	UFLG	590	25	SM490Y	---	-141	0	---	---	19.3	24	86654	14	16	120.9	164.4	16
56	G-2	J-7(Sec-8)	LFLG	590	19	SM490Y	175	---	0	---	175	16.6	20	89570	14	12	85.3	113.7	17
58	G-2	J-8(Sec-9)	UFLG	590	19	SM490Y	---	74	0	---	---	7.7	12	69362	10	12	84.1	120.4	9
59	G-2	J-8(Sec-9)	LFLG	590	21	SM490Y	158	---	0	---	72	15.0	20	81034	14	12	77.2	113.7	24
61	G-2	J-9(Sec-9)	UFLG	590	19	SM490Y	158	---	0	---	117	13.6	20	73316	12	14	69.8	113.7	17
62	G-2	J-9(Sec-9)	LFLG	590	21	SM490Y	---	-103	0	---	---	11.8	18	70684	12	12	105.2	132.0	15
64	G-2	J-10(Sec-11)	UFLG	590	19	SM490Y	158	---	0	---	119	13.6	20	73316	12	14	69.8	113.7	17
65	G-2	J-10(Sec-11)	LFLG	590	21	SM490Y	---	-104	0	---	---	11.9	18	71450	12	12	106.3	132.0	15
67	G-2	J-11(Sec-11)	UFLG	590	19	SM490Y	158	-77	0	---	14	12.2	18	73150	10	12	87.2	120.4	*19
68	G-2	J-11(Sec-11)	LFLG	590	21	SM490Y	158	91	0	---	81	15.0	20	81034	14	12	77.2	113.7	*20
70	G-2	J-12(Sec-13)	UFLG	590	21	SM490Y	---	91	0	---	---	10.4	12	93699	12	12	92.9	132.0	22
71	G-2	J-12(Sec-13)	LFLG	590	19	SM490Y	158	---	0	---	100	13.6	20	73316	14	12	69.8	113.7	17
73	G-3	J-1(Sec-1)	UFLG	590	21	SM490Y	---	-92	0	---	---	10.5	12	94776	12	12	94.0	132.0	*22
74	G-3	J-1(Sec-1)	LFLG	590	19	SM490Y	158	---	0	---	105	13.6	20	73316	14	12	69.8	113.7	17

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Flg THK	Flg stress	Req Bolts	Applied Bolts	Bolts Stress	Spl THK 1	Spl THK 2	Req Area Ar	Total Area As	Group No.
							σ_t	σ_c	τ		σ_{tn}	n		ρ	1	2			
76	G-3	J-2(Sec-2)	UFLG	590	21	SM490Y	158	91	0	---	16	15.0	20	81034	12	14	77.2	113.7	20
77	G-3	J-2(Sec-2)	LFLG	590	19	SM490Y	158	74	0	---	75	13.6	20	73316	14	12	69.8	113.7	4
79	G-3	J-3(Sec-3)	UFLG	590	19	SM490Y	158	---	0	---	111	13.6	20	73316	12	14	69.8	113.7	17
80	G-3	J-3(Sec-3)	LFLG	590	21	SM490Y	---	-97	0	---	---	11.1	18	66878	12	12	99.5	132.0	15
82	G-3	J-4(Sec-5)	UFLG	590	19	SM490Y	158	---	0	---	110	13.6	20	73316	12	14	69.8	113.7	17
83	G-3	J-4(Sec-5)	LFLG	590	21	SM490Y	---	-97	0	---	---	11.1	18	66478	12	12	98.9	132.0	15
85	G-3	J-5(Sec-5)	UFLG	590	19	SM490Y	---	-75	0	---	---	7.8	12	69766	10	12	84.6	120.4	9
86	G-3	J-5(Sec-5)	LFLG	590	21	SM490Y	158	---	0	---	78	15.0	20	81034	14	12	77.2	113.7	*24
88	G-3	J-6(Sec-6)	UFLG	590	24	SM490Y	---	-131	0	---	---	17.2	24	77390	14	14	116.8	154.0	*25
89	G-3	J-6(Sec-6)	LFLG	590	19	SM490Y	160	---	0	---	160	15.1	20	81697	14	12	77.8	113.7	17
91	G-3	J-7(Sec-8)	UFLG	590	24	SM490Y	---	-131	0	---	---	17.2	24	77390	14	14	116.8	154.0	25
92	G-3	J-7(Sec-8)	LFLG	590	19	SM490Y	160	---	0	---	160	15.1	20	81697	14	12	77.8	113.7	17
94	G-3	J-8(Sec-9)	UFLG	590	19	SM490Y	---	-75	0	---	---	7.8	12	69766	10	12	84.6	120.4	9
95	G-3	J-8(Sec-9)	LFLG	590	21	SM490Y	158	---	0	---	78	15.0	20	81034	14	12	77.2	113.7	24
97	G-3	J-9(Sec-9)	UFLG	590	19	SM490Y	158	---	0	---	110	13.6	20	73316	12	14	69.8	113.7	17
98	G-3	J-9(Sec-9)	LFLG	590	21	SM490Y	---	-97	0	---	---	11.1	18	66478	12	12	98.9	132.0	15
100	G-3	J-10(Sec-11)	UFLG	590	19	SM490Y	158	---	0	---	111	13.6	20	73316	12	14	69.8	113.7	17
101	G-3	J-10(Sec-11)	LFLG	590	21	SM490Y	---	-97	0	---	---	11.1	18	66878	12	12	99.5	132.0	15
103	G-3	J-11(Sec-11)	UFLG	590	19	SM490Y	158	74	0	---	17	13.6	20	73316	12	14	69.8	113.7	4
104	G-3	J-11(Sec-11)	LFLG	590	21	SM490Y	158	91	0	---	71	15.0	20	81034	14	12	77.2	113.7	20
106	G-3	J-12(Sec-13)	UFLG	590	21	SM490Y	---	-92	0	---	---	10.5	12	94776	12	12	94.0	132.0	22
107	G-3	J-12(Sec-13)	LFLG	590	19	SM490Y	158	---	0	---	105	13.6	20	73316	14	12	69.8	113.7	17
109	G-4	J-1(Sec-1)	UFLG	590	21	SM490Y	---	91	0	---	---	10.4	12	93699	12	12	92.9	132.0	22
110	G-4	J-1(Sec-1)	LFLG	590	19	SM490Y	158	---	0	---	100	13.6	20	73316	14	12	69.8	113.7	17
112	G-4	J-2(Sec-2)	UFLG	590	21	SM490Y	158	91	0	---	13	13.5	18	80850	10	12	92.9	120.4	14
113	G-4	J-2(Sec-2)	LFLG	590	19	SM490Y	158	74	0	---	84	13.6	20	73316	14	12	69.8	113.7	4
115	G-4	J-3(Sec-3)	UFLG	590	19	SM490Y	158	---	0	---	119	13.6	20	73316	12	14	69.8	113.7	17

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Flg THK	Flg stress	Req Bolts	Applied Bolts	Bolts Stress	Spl THK 1	Spl THK 2	Req Area Ar	Total Area As	Group No.
							σ_t	σ_c	τ		σ_{tn}	n		ρ	1	2	Ar	As	
116	G-4	J-3(Sec-3)	LFLG	590	21	SM490Y	---	-104	0	---	---	11.9	18	71450	12	12	106.3	132.0	15
118	G-4	J-4(Sec-5)	UFLG	590	19	SM490Y	158	---	0	---	117	13.6	20	73316	12	14	69.8	113.7	17
119	G-4	J-4(Sec-5)	LFLG	590	21	SM490Y	---	-103	0	---	---	11.8	18	70684	12	12	105.2	132.0	15
121	G-4	J-5(Sec-5)	UFLG	590	19	SM490Y	---	74	0	---	---	7.7	12	69362	10	12	84.1	120.4	9
122	G-4	J-5(Sec-5)	LFLG	590	21	SM490Y	158	---	0	---	72	15.0	20	81034	14	12	77.2	113.7	24
124	G-4	J-6(Sec-6)	UFLG	590	25	SM490Y	---	-141	0	---	---	19.3	24	86654	14	16	120.9	164.4	16
125	G-4	J-6(Sec-6)	LFLG	590	19	SM490Y	175	---	0	---	175	16.6	20	89570	14	12	85.3	113.7	17
127	G-4	J-7(Sec-8)	UFLG	590	25	SM490Y	---	-141	0	---	---	19.3	24	86654	14	16	120.9	164.4	16
128	G-4	J-7(Sec-8)	LFLG	590	19	SM490Y	175	---	0	---	175	16.6	20	89570	14	12	85.3	113.7	17
130	G-4	J-8(Sec-9)	UFLG	590	19	SM490Y	---	74	0	---	---	7.7	12	69362	10	12	84.1	120.4	9
131	G-4	J-8(Sec-9)	LFLG	590	21	SM490Y	158	---	0	---	72	15.0	20	81034	14	12	77.2	113.7	24
133	G-4	J-9(Sec-9)	UFLG	590	19	SM490Y	158	---	0	---	117	13.6	20	73316	12	14	69.8	113.7	17
134	G-4	J-9(Sec-9)	LFLG	590	21	SM490Y	---	-103	0	---	---	11.8	18	70684	12	12	105.2	132.0	15
136	G-4	J-10(Sec-11)	UFLG	590	19	SM490Y	158	---	0	---	119	13.6	20	73316	12	14	69.8	113.7	17
137	G-4	J-10(Sec-11)	LFLG	590	21	SM490Y	---	-104	0	---	---	11.9	18	71450	12	12	106.3	132.0	15
139	G-4	J-11(Sec-11)	UFLG	590	19	SM490Y	158	-77	0	---	14	12.2	18	73150	10	12	87.2	120.4	19
140	G-4	J-11(Sec-11)	LFLG	590	21	SM490Y	158	91	0	---	81	15.0	20	81034	14	12	77.2	113.7	20
142	G-4	J-12(Sec-13)	UFLG	590	21	SM490Y	---	91	0	---	---	10.4	12	93699	12	12	92.9	132.0	22
143	G-4	J-12(Sec-13)	LFLG	590	19	SM490Y	158	---	0	---	100	13.6	20	73316	14	12	69.8	113.7	17
145	G-5	J-1(Sec-1)	UFLG	590	22	SM490Y	---	-104	0	---	---	12.5	18	74863	12	14	101.3	142.4	1
146	G-5	J-1(Sec-1)	LFLG	590	19	SM490Y	158	---	0	---	121	13.6	20	73316	14	12	69.8	113.7	17
148	G-5	J-2(Sec-2)	UFLG	590	22	SM490Y	158	100	0	---	34	15.7	20	84893	12	14	80.9	113.7	3
149	G-5	J-2(Sec-2)	LFLG	590	19	SM490Y	158	74	0	---	93	13.6	20	73316	14	12	69.8	113.7	4
151	G-5	J-3(Sec-3)	UFLG	590	20	SM490Y	158	---	0	---	141	14.3	20	77175	12	14	73.5	113.7	5
152	G-5	J-3(Sec-3)	LFLG	590	23	SM490Y	---	-121	0	---	---	15.2	24	68607	14	12	112.8	142.4	6
154	G-5	J-4(Sec-5)	UFLG	590	19	SM490Y	158	---	0	---	141	13.6	20	73316	12	14	69.8	113.7	17
155	G-5	J-4(Sec-5)	LFLG	590	23	SM490Y	---	-118	0	---	---	14.8	24	66711	14	12	109.7	142.4	6

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Flg THK	Flg stress	Req Bolts	Applied Bolts	Bolts Stress	Spl THK	Spl THK	Req Area	Total Area	Group No.
							σ_t	σ_c	τ		σ_{tn}	n		ρ	1	2	Ar	As	
157	G-5	J-5(Sec-5)	UFLG	590	19	SM490Y	---	-78	0	---	---	8.1	12	72773	10	12	88.2	120.4	9
158	G-5	J-5(Sec-5)	LFLG	590	23	SM490Y	158	---	0	---	78	16.4	20	88751	14	12	84.5	113.7	10
160	G-5	J-6(Sec-6)	UFLG	590	26	SM490Y	---	-153	0	---	---	21.7	30	78172	14	16	126.1	164.4	11
161	G-5	J-6(Sec-6)	LFLG	590	19	SM490Y	177	---	0	---	177	18.3	24	82511	14	14	94.3	123.2	12
163	G-5	J-7(Sec-8)	UFLG	590	26	SM490Y	---	-153	0	---	---	21.7	30	78172	14	16	126.1	164.4	11
164	G-5	J-7(Sec-8)	LFLG	590	19	SM490Y	177	---	0	---	177	18.3	24	82511	14	14	94.3	123.2	12
166	G-5	J-8(Sec-9)	UFLG	590	19	SM490Y	---	-78	0	---	---	8.1	12	72773	10	12	88.2	120.4	9
167	G-5	J-8(Sec-9)	LFLG	590	23	SM490Y	158	---	0	---	78	16.4	20	88751	14	12	84.5	113.7	10
169	G-5	J-9(Sec-9)	UFLG	590	19	SM490Y	158	---	0	---	141	13.6	20	73316	12	14	69.8	113.7	17
170	G-5	J-9(Sec-9)	LFLG	590	23	SM490Y	---	-118	0	---	---	14.8	24	66711	14	12	109.7	142.4	6
172	G-5	J-10(Sec-11)	UFLG	590	20	SM490Y	158	---	0	---	141	14.3	20	77175	12	14	73.5	113.7	5
173	G-5	J-10(Sec-11)	LFLG	590	23	SM490Y	---	-121	0	---	---	15.2	24	68607	14	12	112.8	142.4	6
175	G-5	J-11(Sec-12)	UFLG	590	22	SM490Y	158	100	0	---	34	15.7	20	84893	12	14	80.9	113.7	3
176	G-5	J-11(Sec-12)	LFLG	590	19	SM490Y	158	74	0	---	93	13.6	20	73316	14	12	69.8	113.7	4
178	G-5	J-12(Sec-13)	UFLG	590	22	SM490Y	---	-104	0	---	---	12.5	18	74863	12	14	101.3	142.4	1
179	G-5	J-12(Sec-13)	LFLG	590	19	SM490Y	158	---	0	---	121	13.6	20	73316	14	12	69.8	113.7	17
										※ 1							※ 2	※ 2	

※Display in the case of thickness up only

If both the tensile Stress and Compressive Stress occurs, the one with the lower difference of Ar and As, will be applied,.

Omit in the case of required area includes flange section area

All members

* of Group No. means the representative member

2) Web

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Joint Type	Applied Bolts			Bolts Stress	Spl THK		Group No.
							σ_{Un}	σ_{Ln}	τ			P	Req Bolts	ρ	l	σ_{sp}	
3	G-1	J-1(Sec-2)	WEB	2378	12	SM490Y	-147	158	10	w(s)	69	274485	3	91582	9	118	*2
6	G-1	J-2(Sec-2)	WEB	2378	12	SM490Y	-147	158	17	w(s)	69	274485	3	91776	9	118	2
9	G-1	J-3(Sec-3)	WEB	2380	12	SM490Y	158	-147	33	w(s)	69	274488	3	92497	9	119	*7
12	G-1	J-4(Sec-5)	WEB	2381	12	SM490Y	158	-144	42	w(s)	69	276354	3	93716	9	119	*8
15	G-1	J-5(Sec-5)	WEB	2381	12	SM490Y	-158	144	27	w(s)	69	276354	3	92811	9	119	8
18	G-1	J-6(Sec-6)	WEB	2374	12	SM490Y	-149	174	14	w(s)	69	298608	3	99697	9	131	*13
21	G-1	J-7(Sec-8)	WEB	2374	12	SM490Y	-149	174	14	w(s)	69	298608	3	99697	9	131	13
24	G-1	J-8(Sec-9)	WEB	2381	12	SM490Y	-158	144	27	w(s)	69	276354	3	92811	9	119	8
27	G-1	J-9(Sec-9)	WEB	2381	12	SM490Y	158	-144	42	w(s)	69	276354	3	93716	9	119	8
30	G-1	J-10(Sec-11)	WEB	2380	12	SM490Y	158	-147	33	w(s)	69	274488	3	92497	9	119	7
33	G-1	J-11(Sec-12)	WEB	2378	12	SM490Y	-147	158	17	w(s)	69	274485	3	91776	9	118	2
36	G-1	J-12(Sec-13)	WEB	2378	12	SM490Y	-147	158	10	w(s)	69	274485	3	91580	9	118	2
39	G-2	J-1(Sec-1)	WEB	2379	12	SM490Y	-150	158	9	w(s)	69	274292	3	91506	9	119	23
42	G-2	J-2(Sec-2)	WEB	2379	12	SM490Y	-150	158	17	w(s)	69	274292	3	91710	9	119	23
45	G-2	J-3(Sec-3)	WEB	2381	12	SM490Y	158	-150	28	w(s)	69	275956	3	92714	9	119	8
48	G-2	J-4(Sec-5)	WEB	2381	12	SM490Y	158	-150	34	w(s)	69	275956	3	93079	9	119	8
51	G-2	J-5(Sec-5)	WEB	2381	12	SM490Y	-158	150	24	w(s)	69	275956	3	92529	9	119	8
54	G-2	J-6(Sec-6)	WEB	2375	12	SM490Y	-138	158	11	w(s)	69	275018	3	91779	9	118	*18
57	G-2	J-7(Sec-8)	WEB	2375	12	SM490Y	-138	158	11	w(s)	69	275018	3	91778	9	118	18
60	G-2	J-8(Sec-9)	WEB	2381	12	SM490Y	-158	150	24	w(s)	69	275956	3	92529	9	119	8
63	G-2	J-9(Sec-9)	WEB	2381	12	SM490Y	158	-150	34	w(s)	69	275956	3	93079	9	119	8
66	G-2	J-10(Sec-11)	WEB	2381	12	SM490Y	158	-150	28	w(s)	69	275956	3	92714	9	119	8
69	G-2	J-11(Sec-11)	WEB	2381	12	SM490Y	-158	150	17	w(s)	69	272657	3	91167	9	119	*21
72	G-2	J-12(Sec-13)	WEB	2379	12	SM490Y	-150	158	9	w(s)	69	274292	3	91503	9	119	23
75	G-3	J-1(Sec-1)	WEB	2379	12	SM490Y	-150	158	8	w(s)	69	274292	3	91495	9	119	*23

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Joint Type	Applied Bolts			Bolts Stress	Spl THK		Group No.
							σ_{Un}	σ_{Ln}	τ			P	Req Bolts	ρ	l	σ_{sp}	
78	G-3	J-2(Sec-2)	WEB	2379	12	SM490Y	-150	158	14	w(s)	69	274292	3	91620	9	119	23
81	G-3	J-3(Sec-3)	WEB	2381	12	SM490Y	158	-150	28	w(s)	69	275956	3	92713	9	119	8
84	G-3	J-4(Sec-5)	WEB	2381	12	SM490Y	158	-150	34	w(s)	69	275956	3	93087	9	119	8
87	G-3	J-5(Sec-5)	WEB	2381	12	SM490Y	-158	150	22	w(s)	69	275956	3	92444	9	119	8
90	G-3	J-6(Sec-6)	WEB	2376	12	SM490Y	-141	158	15	w(s)	69	274848	3	91823	9	118	*26
93	G-3	J-7(Sec-8)	WEB	2376	12	SM490Y	-141	158	15	w(s)	69	274848	3	91823	9	118	26
96	G-3	J-8(Sec-9)	WEB	2381	12	SM490Y	-158	150	22	w(s)	69	275956	3	92439	9	119	8
99	G-3	J-9(Sec-9)	WEB	2381	12	SM490Y	158	-150	34	w(s)	69	275956	3	93087	9	119	8
102	G-3	J-10(Sec-11)	WEB	2381	12	SM490Y	158	-150	28	w(s)	69	275956	3	92713	9	119	8
105	G-3	J-11(Sec-11)	WEB	2381	12	SM490Y	-158	150	14	w(s)	69	272657	3	91076	9	119	21
108	G-3	J-12(Sec-13)	WEB	2379	12	SM490Y	-150	158	8	w(s)	69	274292	3	91495	9	119	23
111	G-4	J-1(Sec-1)	WEB	2379	12	SM490Y	-150	158	9	w(s)	69	274292	3	91506	9	119	23
114	G-4	J-2(Sec-2)	WEB	2379	12	SM490Y	-150	158	17	w(s)	69	274292	3	91710	9	119	23
117	G-4	J-3(Sec-3)	WEB	2381	12	SM490Y	158	-150	28	w(s)	69	275956	3	92714	9	119	8
120	G-4	J-4(Sec-5)	WEB	2381	12	SM490Y	158	-150	34	w(s)	69	275956	3	93079	9	119	8
123	G-4	J-5(Sec-5)	WEB	2381	12	SM490Y	-158	150	24	w(s)	69	275956	3	92529	9	119	8
126	G-4	J-6(Sec-6)	WEB	2375	12	SM490Y	-138	158	11	w(s)	69	275018	3	91779	9	118	18
129	G-4	J-7(Sec-8)	WEB	2375	12	SM490Y	-138	158	11	w(s)	69	275018	3	91778	9	118	18
132	G-4	J-8(Sec-9)	WEB	2381	12	SM490Y	-158	150	24	w(s)	69	275956	3	92529	9	119	8
135	G-4	J-9(Sec-9)	WEB	2381	12	SM490Y	158	-150	34	w(s)	69	275956	3	93079	9	119	8
138	G-4	J-10(Sec-11)	WEB	2381	12	SM490Y	158	-150	28	w(s)	69	275956	3	92714	9	119	8
141	G-4	J-11(Sec-11)	WEB	2381	12	SM490Y	-158	150	17	w(s)	69	272657	3	91167	9	119	21
144	G-4	J-12(Sec-13)	WEB	2379	12	SM490Y	-150	158	9	w(s)	69	274292	3	91503	9	119	23
147	G-5	J-1(Sec-1)	WEB	2378	12	SM490Y	-147	158	10	w(s)	69	274485	3	91582	9	118	2
150	G-5	J-2(Sec-2)	WEB	2378	12	SM490Y	-147	158	17	w(s)	69	274485	3	91776	9	118	2
153	G-5	J-3(Sec-3)	WEB	2380	12	SM490Y	158	-147	33	w(s)	69	274488	3	92497	9	119	7
156	G-5	J-4(Sec-5)	WEB	2381	12	SM490Y	158	-144	42	w(s)	69	276354	3	93716	9	119	8

Mem No.	Girder Name	Joint Name	Member	Width	THK	Grade	Stress			Joint Type	Applied Bolts			Bolts Stress	Spl THK		Group No.
							σ_{Un}	σ_{Ln}	τ			P	Req Bolts	ρ	l	σ_{sp}	
159	G-5	J-5(Sec-5)	WEB	2381	12	SM490Y	-158	144	27	w(s)	69	276354	3	92811	9	119	8
162	G-5	J-6(Sec-6)	WEB	2374	12	SM490Y	-149	174	14	w(s)	69	298608	3	99697	9	131	13
165	G-5	J-7(Sec-8)	WEB	2374	12	SM490Y	-149	174	14	w(s)	69	298608	3	99697	9	131	13
168	G-5	J-8(Sec-9)	WEB	2381	12	SM490Y	-158	144	27	w(s)	69	276354	3	92811	9	119	8
171	G-5	J-9(Sec-9)	WEB	2381	12	SM490Y	158	-144	42	w(s)	69	276354	3	93716	9	119	8
174	G-5	J-10(Sec-11)	WEB	2380	12	SM490Y	158	-147	33	w(s)	69	274488	3	92497	9	119	7
177	G-5	J-11(Sec-12)	WEB	2378	12	SM490Y	-147	158	17	w(s)	69	274485	3	91776	9	118	2
180	G-5	J-12(Sec-13)	WEB	2378	12	SM490Y	-147	158	10	w(s)	69	274485	3	91580	9	118	2

* of Group No. means the representative member

4-4 Calculation of Bearing Stiffeners

1. Main girder G-1

Main girder G-1, Support S-1

Reaction Force $R_a = 800.0$ kN
 Upper Flange 590
 Lower Flange $590 * 19$
 WEB $2378 * 12$ (SM490YA)
 Sole Plate $510 * 510$ (101.0 ϕ)
 STIFFENER 2- $280 * 22$ (SM400A)
 STIFF $2378.0/30+50 = 129.3 < 280.0$

Check of bearing stress(S1)

$$\begin{array}{l} \text{(SM400A)STIFF} \quad 2 * (24.90 - 4.45 + 1.9) * 2.2 \quad = 98.34 \\ \text{(SM490YA)WEB} \quad (28.80 - 10.10 + 2 * 1.9) * 1.2 \quad = 27.00 \end{array}$$

$$\sigma_b = R/A_b = 800.00 * 10^3 / 125.34 * 10^2 = 63.8 \text{ N/mm}^2 < \sigma_{ba} = 210.0 \text{ N/mm}^2$$

$A_b = 125.34 \text{ cm}^2$

Check of stress in vertical direction(S1)

$$\begin{array}{l} \text{(SM400A)STIFF} \quad 2 * 24.90 * 2.2 \quad = 109.56 \\ \text{(SM490YA)WEB} \quad 28.80 * 1.2 \quad = 34.56 \end{array}$$

$$A = 144.12 \text{ cm}^2$$

$$1.7 * 109.56 = 186.25 \text{ cm}^2 > A \quad \text{therefore} \quad A_e = 144.12 \text{ cm}^2$$

$$I = 24323 \text{ cm}^4$$

$$r = \sqrt{I/A_e} = \sqrt{24323 / 144.12} = 12.99 \text{ cm}$$

allowable stress

$$L/r = 237.8 / 2 / 12.99 = 9.15 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/A_e = 800.00 * 10^3 / 144.12 * 10^2 = 55.5 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(S1)

$$\begin{array}{l} \text{fillet weld } s = \sqrt{2 * 22} = 6.63 \text{ ---} > 8 \text{ mm} < t_{\min} = 12 \text{ mm} \\ \text{throat thickness} \quad a = 4 * 8 / 1.4142 = 22.63 \text{ mm} \end{array}$$

$$\begin{array}{l} \tau = 2 * R_a / (a * h_w') = 2 * 800.0 * 10^3 / (22.63 * 2378) \\ = 29.7 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2 \end{array}$$

Main girder G-1, Support S-2

Reaction Force $R_a = 800.0$ kN
 Upper Flange 590
 Lower Flange 590 * 19
 WEB 2378 * 12 (SM490YA)
 Sole Plate 510 * 510 (101.0 ϕ)
 STIFFENER 2- 280 * 22 (SM400A)
 STIFF 2378.0/30+50 = 129.3 < 280.0

Check of bearing stress(S2)

(SM400A)STIFF $2 * (24.90 - 4.45 + 1.9) * 2.2 = 98.34$
 (SM490YA)WEB $(28.80 - 10.10 + 2 * 1.9) * 1.2 = 27.00$

$A_b = 125.34$ cm²

$$\sigma_b = R/A_b = 800.00 * 10^3 / 125.34 * 10^2 = 63.8 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(S2)

(SM400A)STIFF $2 * 24.90 * 2.2 = 109.56$
 (SM490YA)WEB $28.80 * 1.2 = 34.56$

$A = 144.12$ cm²

$$1.7 * 109.56 = 186.25 \text{ cm}^2 > A \quad \text{therefore} \quad A_e = 144.12 \text{ cm}^2$$

$$I = 24323 \text{ cm}^4$$

$$r = \sqrt{I/A_e} = \sqrt{24323 / 144.12} = 12.99 \text{ cm}$$

allowable stress

$$L/r = 237.8 / 2 / 12.99 = 9.15 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/A_e = 800.00 * 10^3 / 144.12 * 10^2 = 55.5 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(S2)

fillet weld $s = \sqrt{2 * 22} = 6.63 \text{ ---} > 8 \text{ mm} < t_{min} = 12 \text{ mm}$
 throat thickness $a = 4 * 8 / 1.4142 = 22.63 \text{ mm}$

$$\tau = 2 * R_a / (a * h_w) = 2 * 800.0 * 10^3 / (22.63 * 2378)$$

$$= 29.7 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

Main girder G-1, Support PF12

Reaction Force Ra= 2500.0 kN
 Upper Flange 590
 Lower Flange 590 * 39
 WEB 2369 * 12 (SM490YA)
 Sole Plate 710 * 710 (202.0 φ)
 STIFFENER 2- 320 * 26 (SM400A)
 STIFF 2369.0/30+50 = 129.0 < 320.0

Check of bearing stress(PF12)

(SM400A)STIFF	2*(32.00- 9.50+ 3.9)* 2.6	= 137.28
(SM490YA)WEB	(28.80- 20.20+2* 3.9)* 1.2	= 19.68

Ab = 156.96 cm²

$\sigma_b = R/A_b = 2500.00 \times 10^3 / 156.96 \times 10^2 = 159.3 \text{ N/mm}^2$
 $< \sigma_{ba} = 210.0 \text{ N/mm}^2$

Check of stress in vertical direction(PF12)

(SM400A)STIFF	2* 32.00* 2.6	= 166.40
(SM490YA)WEB	28.80* 1.2	= 34.56

A = 200.96 cm²

1.7* 166.40 = 282.88 cm² > A therefore Ae = 200.96 cm²

I = 60057 cm⁴

r = SQR(I/Ae) = SQR(60057 / 200.96) = 17.29 cm

allowable stress

L/r = 236.9 / 2 / 17.29 = 6.85 < 18

$\sigma_{cag} = 140.0 \text{ N/mm}^2$

$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$

$\sigma_v = R/A_e = 2500.00 \times 10^3 / 200.96 \times 10^2 = 124.4 \text{ N/mm}^2 < \sigma_{ca}$

Welding between stiffener and web plate(PF12)

fillet weld s = SQR(2*26) = 7.21 ---> 10 mm < t_{min} = 12 mm
 throat thickness a = 4*10/1.4142 = 28.28 mm

$\tau = 2 * R_a / (a * h_w') = 2 * 2500.0 \times 10^3 / (28.28 * 2369)$
 $= 74.6 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$

Main girder G-1, Support PF13

Reaction Force Ra= 2500.0 kN
 Upper Flange 590
 Lower Flange 590 * 39
 WEB 2369 * 12 (SM490YA)
 Sole Plate 710 * 710 (202.0 φ)
 STIFFENER 2- 320 * 26 (SM400A)
 STIFF 2369.0/30+50 = 129.0 < 320.0

Check of bearing stress(PF13)

(SM400A)STIFF	2*(32.00- 9.50+ 3.9)* 2.6	= 137.28
(SM490YA)WEB	(28.80- 20.20+2* 3.9)* 1.2	= 19.68

$$Ab = 156.96 \text{ cm}^2$$

$$\sigma_b = R/Ab = 2500.00 * 10^3 / 156.96 * 10^2 = 159.3 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(PF13)

(SM400A)STIFF	2* 32.00* 2.6	= 166.40
(SM490YA)WEB	28.80* 1.2	= 34.56

$$A = 200.96 \text{ cm}^2$$

$$1.7 * 166.40 = 282.88 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 200.96 \text{ cm}^2$$

$$I = 60057 \text{ cm}^4$$

$$r = \text{SQR}(I/Ae) = \text{SQR}(60057 / 200.96) = 17.29 \text{ cm}$$

allowable stress

$$L/r = 236.9 / 2 / 17.29 = 6.85 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 2500.00 * 10^3 / 200.96 * 10^2 = 124.4 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(PF13)

fillet weld s = $\text{SQR}(2*26) = 7.21 \text{ ---} > 10 \text{ mm} < t_{min} = 12 \text{ mm}$
 throat thickness a = $4*10/1.4142 = 28.28 \text{ mm}$

$$\tau = 2 * Ra / (a * hw') = 2 * 2500.0 * 10^3 / (28.28 * 2369)$$

$$= 74.6 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

2. Main girder G-2

Main girder G-2, Support S-1

Reaction Force Ra= 700.0 kN
 Upper Flange 590
 Lower Flange 590 * 19
 WEB 2379 * 12 (SM490YA)
 Sole Plate 510 * 510 (101.0 φ)
 STIFFENER 2- 280 * 22 (SM400A)
 STIFF 2379.0/30+50 = 129.3 < 280.0

Check of bearing stress(S1)

(SM400A)STIFF	2*(24.90- 4.45+ 1.9)* 2.2	= 98.34
(SM490YA)WEB	(28.80- 10.10+2* 1.9)* 1.2	= 27.00

Ab = 125.34 cm²

$$\sigma_b = R/A_b = 700.00 \times 10^3 / 125.34 \times 10^2 = 55.8 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(S1)

(SM400A)STIFF	2* 24.90* 2.2	= 109.56
(SM490YA)WEB	28.80* 1.2	= 34.56

A = 144.12 cm²

$$1.7 * 109.56 = 186.25 \text{ cm}^2 > A \quad \text{therefore} \quad A_e = 144.12 \text{ cm}^2$$

$$I = 24323 \text{ cm}^4$$

$$r = \sqrt{I/A_e} = \sqrt{24323 / 144.12} = 12.99 \text{ cm}$$

allowable stress

$$L/r = 237.9 / 2 / 12.99 = 9.16 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/A_e = 700.00 \times 10^3 / 144.12 \times 10^2 = 48.6 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(S1)

fillet weld s = $\sqrt{2*22}$ = 6.63 ---> 8 mm < t_{min} = 12 mm
 throat thickness a = 4* 8/1.4142 = 22.63 mm

$$\tau = 2 * R_a / (a * h_w') = 2 * 700.0 \times 10^3 / (22.63 * 2379)$$

$$= 26.0 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

Main girder G-2, Support S2

Reaction Force Ra= 700.0 kN
 Upper Flange 590
 Lower Flange 590 * 19
 WEB 2379 * 12 (SM490YA)
 Sole Plate 510 * 510 (101.0 φ)
 STIFFENER 2- 280 * 22 (SM400A)
 STIFF 2379.0/30+50 = 129.3 < 280.0

Check of bearing stress(S2)

(SM400A)STIFF 2*(24.90- 4.45+ 1.9)* 2.2 = 98.34
 (SM490YA)WEB (28.80- 10.10+2* 1.9)* 1.2 = 27.00

$$Ab = 125.34 \text{ cm}^2$$

$$\sigma_b = R/Ab = 700.00 * 10^3 / 125.34 * 10^2 = 55.8 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(S2)

(SM400A)STIFF 2* 24.90* 2.2 = 109.56
 (SM490YA)WEB 28.80* 1.2 = 34.56

$$A = 144.12 \text{ cm}^2$$

$$1.7 * 109.56 = 186.25 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 144.12 \text{ cm}^2$$

$$I = 24323 \text{ cm}^4$$

$$r = \text{SQR}(I/Ae) = \text{SQR}(24323 / 144.12) = 12.99 \text{ cm}$$

allowable stress

$$L/r = 237.9 / 2 / 12.99 = 9.16 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 700.00 * 10^3 / 144.12 * 10^2 = 48.6 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(S2)

fillet weld s = $\text{SQR}(2*22) = 6.63 \rightarrow 8 \text{ mm} < t_{min} = 12 \text{ mm}$
 throat thickness a = $4 * 8 / 1.4142 = 22.63 \text{ mm}$

$$\tau = 2 * Ra / (a * hw') = 2 * 700.0 * 10^3 / (22.63 * 2379)$$

$$= 26.0 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

Main girder G-2, Support PF12

Reaction Force Ra= 2000.0 kN
 Upper Flange 590
 Lower Flange 590 * 29
 WEB 2378 * 12 (SM490YA)
 Sole Plate 710 * 710 (202.0 φ)
 STIFFENER 2- 320 * 26 (SM400A)
 STIFF 2378.0/30+50 = 129.3 < 320.0

Check of bearing stress(PF12)

(SM400A)STIFF	2*(32.00- 9.50+ 2.9)* 2.6	= 132.08
(SM490YA)WEB	(28.80- 20.20+2* 2.9)* 1.2	= 17.28

$$Ab = 149.36 \text{ cm}^2$$

$$\sigma_b = R/Ab = 2000.00 * 10^3 / 149.36 * 10^2 = 133.9 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(PF12)

(SM400A)STIFF	2* 32.00* 2.6	= 166.40
(SM490YA)WEB	28.80* 1.2	= 34.56

$$A = 200.96 \text{ cm}^2$$

$$1.7 * 166.40 = 282.88 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 200.96 \text{ cm}^2$$

$$I = 60057 \text{ cm}^4$$

$$r = \text{SQR}(I/Ae) = \text{SQR}(60057 / 200.96) = 17.29 \text{ cm}$$

allowable stress

$$L/r = 237.8 / 2 / 17.29 = 6.88 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 2000.00 * 10^3 / 200.96 * 10^2 = 99.5 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(PF12)

fillet weld s = $\text{SQR}(2*26) = 7.21 \rightarrow 8 \text{ mm} < t_{min} = 12 \text{ mm}$
 throat thickness a = $4 * 8 / 1.4142 = 22.63 \text{ mm}$

$$\tau = 2 * Ra / (a * hw') = 2 * 2000.0 * 10^3 / (22.63 * 2378)$$

$$= 74.3 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

Main girder G-2, Support PF13

Reaction Force Ra= 2000.0 kN
 Upper Flange 590
 Lower Flange 590 * 29
 WEB 2378 * 12 (SM490YA)
 Sole Plate 710 * 710 (202.0 φ)
 STIFFENER 2- 320 * 26 (SM400A)
 STIFF 2378.0/30+50 = 129.3 < 320.0

Check of bearing stress(PF13)

(SM400A)STIFF 2*(32.00- 9.50+ 2.9)* 2.6 = 132.08
 (SM490YA)WEB (28.80- 20.20+2* 2.9)* 1.2 = 17.28

$$Ab = 149.36 \text{ cm}^2$$

$$\sigma_b = R/Ab = 2000.00 * 10^3 / 149.36 * 10^2 = 133.9 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(PF13)

(SM400A)STIFF 2* 32.00* 2.6 = 166.40
 (SM490YA)WEB 28.80* 1.2 = 34.56

$$A = 200.96 \text{ cm}^2$$

$$1.7 * 166.40 = 282.88 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 200.96 \text{ cm}^2$$

$$I = 60057 \text{ cm}^4$$

$$r = \sqrt{I/Ae} = \sqrt{60057 / 200.96} = 17.29 \text{ cm}$$

allowable stress

$$L/r = 237.8 / 2 / 17.29 = 6.88 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 2000.00 * 10^3 / 200.96 * 10^2 = 99.5 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(PF13)

fillet weld s = $\sqrt{2*26}$ = 7.21 ---> 8 mm < t_{min} = 12 mm
 throat thickness a = 4 * 8 / 1.4142 = 22.63 mm

$$\tau = 2 * Ra / (a * hw') = 2 * 2000.0 * 10^3 / (22.63 * 2378)$$

$$= 74.3 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

3. Main girder G-3

Main girder G-3, Support S1

Reaction Force Ra= 750.0 kN
 Upper Flange 590
 Lower Flange 590 * 19
 WEB 2379 * 12 (SM490YA)
 Sole Plate 510 * 510 (101.0 φ)
 STIFFENER 2- 280 * 22 (SM400A)
 STIFF 2379.0/30+50 = 129.3 < 280.0

Check of bearing stress(S1)

(SM400A)STIFF	2*(24.90- 4.45+ 1.9)* 2.2	= 98.34
(SM490YA)WEB	(28.80- 10.10+2* 1.9)* 1.2	= 27.00

$$Ab = 125.34 \text{ cm}^2$$

$$\sigma_b = R/Ab = 750.00 \times 10^3 / 125.34 \times 10^2 = 59.8 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(S1)

(SM400A)STIFF	2* 24.90* 2.2	= 109.56
(SM490YA)WEB	28.80* 1.2	= 34.56

$$A = 144.12 \text{ cm}^2$$

$$1.7 * 109.56 = 186.25 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 144.12 \text{ cm}^2$$

$$I = 24323 \text{ cm}^4$$

$$r = \sqrt{I/Ae} = \sqrt{24323 / 144.12} = 12.99 \text{ cm}$$

allowable stress

$$L/r = 237.9 / 2 / 12.99 = 9.16 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 750.00 \times 10^3 / 144.12 \times 10^2 = 52.0 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(S1)

fillet weld s = $\sqrt{2*22}$ = 6.63 ---> 8 mm < t_{min} = 12 mm
 throat thickness a = 4* 8/1.4142 = 22.63 mm

$$\tau = 2 * Ra / (a * hw) = 2 * 750.0 \times 10^3 / (22.63 * 2379)$$

$$= 27.9 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

Main girder G-3, Support S2

Reaction Force Ra= 750.0 kN
 Upper Flange 590
 Lower Flange 590 * 19
 WEB 2379 * 12 (SM490YA)
 Sole Plate 510 * 510 (101.0 φ)
 STIFFENER 2- 280 * 22 (SM400A)
 STIFF 2379.0/30+50 = 129.3 < 280.0

Check of bearing stress(S2)

(SM400A)STIFF 2*(24.90- 4.45+ 1.9)* 2.2 = 98.34
 (SM490YA)WEB (28.80- 10.10+2* 1.9)* 1.2 = 27.00

$$Ab = 125.34 \text{ cm}^2$$

$$\sigma_b = R/Ab = 750.00 * 10^3 / 125.34 * 10^2 = 59.8 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(S2)

(SM400A)STIFF 2* 24.90* 2.2 = 109.56
 (SM490YA)WEB 28.80* 1.2 = 34.56

$$A = 144.12 \text{ cm}^2$$

$$1.7 * 109.56 = 186.25 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 144.12 \text{ cm}^2$$

$$I = 24323 \text{ cm}^4$$

$$r = \sqrt{I/Ae} = \sqrt{24323 / 144.12} = 12.99 \text{ cm}$$

allowable stress

$$L/r = 237.9 / 2 / 12.99 = 9.16 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 750.00 * 10^3 / 144.12 * 10^2 = 52.0 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(S2)

fillet weld s = $\sqrt{2*22}$ = 6.63 ---> 8 mm < t_{min} = 12 mm
 throat thickness a = 4 * 8 / 1.4142 = 22.63 mm

$$\tau = 2 * Ra / (a * hw') = 2 * 750.0 * 10^3 / (22.63 * 2379)$$

$$= 27.9 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

Main girder G-3, Support PF12

Reaction Force Ra= 2100.0 kN
 Upper Flange 590
 Lower Flange 590 * 27
 WEB 2379 * 12 (SM490YA)
 Sole Plate 710 * 710 (202.0 φ)
 STIFFENER 2- 320 * 26 (SM400A)
 STIFF 2379.0/30+50 = 129.3 < 320.0

Check of bearing stress(PF12)

(SM400A)STIFF	2*(32.00- 9.50+ 2.7)* 2.6	= 131.04
(SM490YA)WEB	(28.80- 20.20+2* 2.7)* 1.2	= 16.80

$$Ab = 147.84 \text{ cm}^2$$

$$\sigma_b = R/Ab = 2100.00 * 10^3 / 147.84 * 10^2 = 142.0 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(PF12)

(SM400A)STIFF	2* 32.00* 2.6	= 166.40
(SM490YA)WEB	28.80* 1.2	= 34.56

$$A = 200.96 \text{ cm}^2$$

$$1.7 * 166.40 = 282.88 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 200.96 \text{ cm}^2$$

$$I = 60057 \text{ cm}^4$$

$$r = \sqrt{I/Ae} = \sqrt{60057 / 200.96} = 17.29 \text{ cm}$$

allowable stress

$$L/r = 237.9 / 2 / 17.29 = 6.88 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 2100.00 * 10^3 / 200.96 * 10^2 = 104.5 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(PF12)

fillet weld s = $\sqrt{2*26} = 7.21 \text{ mm} \rightarrow 8 \text{ mm} < t_{min} = 12 \text{ mm}$
 throat thickness a = $4 * 8 / 1.4142 = 22.63 \text{ mm}$

$$\tau = 2 * Ra / (a * hw') = 2 * 2100.0 * 10^3 / (22.63 * 2379)$$

$$= 78.0 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

Main girder G-3, Support PF13

Reaction Force Ra= 2100.0 kN
 Upper Flange 590
 Lower Flange 590 * 27
 WEB 2379 * 12 (SM490YA)
 Sole Plate 710 * 710 (202.0 φ)
 STIFFENER 2- 320 * 26 (SM400A)
 STIFF 2379.0/30+50 = 129.3 < 320.0

Check of bearing stress(PF13)

(SM400A)STIFF	2*(32.00- 9.50+ 2.7)* 2.6	= 131.04
(SM490YA)WEB	(28.80- 20.20+2* 2.7)* 1.2	= 16.80

$$Ab = 147.84 \text{ cm}^2$$

$$\sigma_b = R/Ab = 2100.00 * 10^3 / 147.84 * 10^2 = 142.0 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(PF13)

(SM400A)STIFF	2* 32.00* 2.6	= 166.40
(SM490YA)WEB	28.80* 1.2	= 34.56

$$A = 200.96 \text{ cm}^2$$

$$1.7 * 166.40 = 282.88 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 200.96 \text{ cm}^2$$

$$I = 60057 \text{ cm}^4$$

$$r = \sqrt{I/Ae} = \sqrt{60057 / 200.96} = 17.29 \text{ cm}$$

allowable stress

$$L/r = 237.9 / 2 / 17.29 = 6.88 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 2100.00 * 10^3 / 200.96 * 10^2 = 104.5 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(PF13)

fillet weld s = $\sqrt{2*26} = 7.21 \rightarrow 8 \text{ mm} < t_{min} = 12 \text{ mm}$
 throat thickness a = $4 * 8 / 1.4142 = 22.63 \text{ mm}$

$$\tau = 2 * Ra / (a * hw') = 2 * 2100.0 * 10^3 / (22.63 * 2379)$$

$$= 78.0 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

4. Main girder G-4

Main girder G-4, Support S1

Reaction Force Ra= 700.0 kN
 Upper Flange 590
 Lower Flange 590 * 19
 WEB 2379 * 12 (SM490YA)
 Sole Plate 510 * 510 (101.0 φ)
 STIFFENER 2- 280 * 22 (SM400A)
 STIFF 2379.0/30+50 = 129.3 < 280.0

Check of bearing stress(S1)

(SM400A)STIFF	2*(24.90- 4.45+ 1.9)* 2.2	= 98.34
(SM490YA)WEB	(28.80- 10.10+2* 1.9)* 1.2	= 27.00

$$Ab = 125.34 \text{ cm}^2$$

$$\sigma_b = R/Ab = 700.00 \times 10^3 / 125.34 \times 10^2 = 55.8 \text{ N/mm}^2 < \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(S1)

(SM400A)STIFF	2* 24.90* 2.2	= 109.56
(SM490YA)WEB	28.80* 1.2	= 34.56

$$A = 144.12 \text{ cm}^2$$

$$1.7 * 109.56 = 186.25 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 144.12 \text{ cm}^2$$

$$I = 24323 \text{ cm}^4$$

$$r = \sqrt{I/Ae} = \sqrt{24323 / 144.12} = 12.99 \text{ cm}$$

allowable stress

$$L/r = 237.9 / 2 / 12.99 = 9.16 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 700.00 \times 10^3 / 144.12 \times 10^2 = 48.6 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(S1)

fillet weld s = $\sqrt{2*22}$ = 6.63 ---> 8 mm < t_{min} = 12 mm
 throat thickness a = 4* 8/1.4142 = 22.63 mm

$$\tau = 2 * Ra / (a * hw') = 2 * 700.0 \times 10^3 / (22.63 * 2379) = 26.0 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

Main girder G-4, Support S2

Reaction Force Ra= 700.0 kN
 Upper Flange 590
 Lower Flange 590 * 19
 WEB 2379 * 12 (SM490YA)
 Sole Plate 510 * 510 (101.0 φ)
 STIFFENER 2- 280 * 22 (SM400A)
 STIFF 2379.0/30+50 = 129.3 < 280.0

Check of bearing stress(S2)

(SM400A)STIFF 2*(24.90- 4.45+ 1.9)* 2.2 = 98.34
 (SM490YA)WEB (28.80- 10.10+2* 1.9)* 1.2 = 27.00

$$Ab = 125.34 \text{ cm}^2$$

$$\sigma_b = R/Ab = 700.00 * 10^3 / 125.34 * 10^2 = 55.8 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(S2)

(SM400A)STIFF 2* 24.90* 2.2 = 109.56
 (SM490YA)WEB 28.80* 1.2 = 34.56

$$A = 144.12 \text{ cm}^2$$

$$1.7 * 109.56 = 186.25 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 144.12 \text{ cm}^2$$

$$I = 24323 \text{ cm}^4$$

$$r = \text{SQR}(I/Ae) = \text{SQR}(24323 / 144.12) = 12.99 \text{ cm}$$

allowable stress

$$L/r = 237.9 / 2 / 12.99 = 9.16 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 700.00 * 10^3 / 144.12 * 10^2 = 48.6 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(S2)

fillet weld s = $\text{SQR}(2*22) = 6.63 \rightarrow 8 \text{ mm} < t_{min} = 12 \text{ mm}$
 throat thickness a = $4 * 8 / 1.4142 = 22.63 \text{ mm}$

$$\tau = 2 * Ra / (a * hw') = 2 * 700.0 * 10^3 / (22.63 * 2379)$$

$$= 26.0 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

Main girder G-4, Support PF12

Reaction Force Ra= 2000.0 kN
 Upper Flange 590
 Lower Flange 590 * 29
 WEB 2378 * 12 (SM490YA)
 Sole Plate 710 * 710 (202.0 φ)
 STIFFENER 2- 320 * 26 (SM400A)
 STIFF 2378.0/30+50 = 129.3 < 320.0

Check of bearing stress(PF12)

(SM400A)STIFF 2*(32.00- 9.50+ 2.9)* 2.6 = 132.08
 (SM490YA)WEB (28.80- 20.20+2* 2.9)* 1.2 = 17.28

$$Ab = 149.36 \text{ cm}^2$$

$$\sigma_b = R/Ab = 2000.00 * 10^3 / 149.36 * 10^2 = 133.9 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(PF12)

(SM400A)STIFF 2* 32.00* 2.6 = 166.40
 (SM490YA)WEB 28.80* 1.2 = 34.56

$$A = 200.96 \text{ cm}^2$$

$$1.7 * 166.40 = 282.88 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 200.96 \text{ cm}^2$$

$$I = 60057 \text{ cm}^4$$

$$r = \sqrt{I/Ae} = \sqrt{60057 / 200.96} = 17.29 \text{ cm}$$

allowable stress

$$L/r = 237.8 / 2 / 17.29 = 6.88 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 2000.00 * 10^3 / 200.96 * 10^2 = 99.5 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(PF12)

fillet weld s = $\sqrt{2*26}$ = 7.21 ---> 8 mm < t_{min} = 12 mm
 throat thickness a = 4 * 8 / 1.4142 = 22.63 mm

$$\tau = 2 * Ra / (a * hw') = 2 * 2000.0 * 10^3 / (22.63 * 2378)$$

$$= 74.3 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

Main girder G-4, Support PF13

Reaction Force Ra= 2000.0 kN
 Upper Flange 590
 Lower Flange 590 * 29
 WEB 2378 * 12 (SM490YA)
 Sole Plate 710 * 710 (202.0 φ)
 STIFFENER 2- 320 * 26 (SM400A)
 STIFF 2378.0/30+50 = 129.3 < 320.0

Check of bearing stress(PF13)

(SM400A)STIFF 2*(32.00- 9.50+ 2.9)* 2.6 = 132.08
 (SM490YA)WEB (28.80- 20.20+2* 2.9)* 1.2 = 17.28

$$Ab = 149.36 \text{ cm}^2$$

$$\sigma_b = R/Ab = 2000.00 * 10^3 / 149.36 * 10^2 = 133.9 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(PF13)

(SM400A)STIFF 2* 32.00* 2.6 = 166.40
 (SM490YA)WEB 28.80* 1.2 = 34.56

$$A = 200.96 \text{ cm}^2$$

$$1.7 * 166.40 = 282.88 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 200.96 \text{ cm}^2$$

$$I = 60057 \text{ cm}^4$$

$$r = \text{SQR}(I/Ae) = \text{SQR}(60057 / 200.96) = 17.29 \text{ cm}$$

allowable stress

$$L/r = 237.8 / 2 / 17.29 = 6.88 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 2000.00 * 10^3 / 200.96 * 10^2 = 99.5 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(PF13)

fillet weld s = $\text{SQR}(2*26) = 7.21 \rightarrow 8 \text{ mm} < t_{min} = 12 \text{ mm}$
 throat thickness a = $4 * 8 / 1.4142 = 22.63 \text{ mm}$

$$\tau = 2 * Ra / (a * hw') = 2 * 2000.0 * 10^3 / (22.63 * 2378)$$

$$= 74.3 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

5. Main girder G-5

Main girder G-5, Support S1

Reaction Force Ra= 800.0 kN
 Upper Flange 590
 Lower Flange 590 * 19
 WEB 2378 * 12 (SM490YA)
 Sole Plate 510 * 510 (101.0 φ)
 STIFFENER 2- 280 * 22 (SM400A)
 STIFF 2378.0/30+50 = 129.3 < 280.0

Check of bearing stress(S1)

(SM400A)STIFF 2*(24.90- 4.45+ 1.9)* 2.2 = 98.34
 (SM490YA)WEB (28.80- 10.10+2* 1.9)* 1.2 = 27.00

$$Ab = 125.34 \text{ cm}^2$$

$$\sigma_b = R/Ab = 800.00 \times 10^3 / 125.34 \times 10^2 = 63.8 \text{ N/mm}^2 < \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(S1)

(SM400A)STIFF 2* 24.90* 2.2 = 109.56
 (SM490YA)WEB 28.80* 1.2 = 34.56

$$A = 144.12 \text{ cm}^2$$

$$1.7 * 109.56 = 186.25 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 144.12 \text{ cm}^2$$

$$I = 24323 \text{ cm}^4$$

$$r = \sqrt{I/Ae} = \sqrt{24323 / 144.12} = 12.99 \text{ cm}$$

allowable stress

$$L/r = 237.8 / 2 / 12.99 = 9.15 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 800.00 \times 10^3 / 144.12 \times 10^2 = 55.5 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(S1)

fillet weld s = $\sqrt{2*22}$ = 6.63 ----> 8 mm < t_{min}=12 mm
 throat thickness a = 4* 8/1.4142=22.63 mm

$$\tau = 2 * Ra / (a * hw') = 2 * 800.0 \times 10^3 / (22.63 * 2378) = 29.7 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

Main girder G-5, Support S2

Reaction Force Ra= 800.0 kN
 Upper Flange 590
 Lower Flange 590 * 19
 WEB 2378 * 12 (SM490YA)
 Sole Plate 510 * 510 (101.0 φ)
 STIFFENER 2- 280 * 22 (SM400A)
 STIFF 2378.0/30+50 = 129.3 < 280.0

Check of bearing stress(S2)

(SM400A)STIFF 2*(24.90- 4.45+ 1.9)* 2.2 = 98.34
 (SM490YA)WEB (28.80- 10.10+2* 1.9)* 1.2 = 27.00

$$Ab = 125.34 \text{ cm}^2$$

$$\sigma_b = R/Ab = 800.00 * 10^3 / 125.34 * 10^2 = 63.8 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(S2)

(SM400A)STIFF 2* 24.90* 2.2 = 109.56
 (SM490YA)WEB 28.80* 1.2 = 34.56

$$A = 144.12 \text{ cm}^2$$

$$1.7 * 109.56 = 186.25 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 144.12 \text{ cm}^2$$

$$I = 24323 \text{ cm}^4$$

$$r = \text{SQR}(I/Ae) = \text{SQR}(24323 / 144.12) = 12.99 \text{ cm}$$

allowable stress

$$L/r = 237.8 / 2 / 12.99 = 9.15 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 800.00 * 10^3 / 144.12 * 10^2 = 55.5 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(S2)

fillet weld s = $\text{SQR}(2*22) = 6.63 \rightarrow 8 \text{ mm} < t_{min} = 12 \text{ mm}$
 throat thickness a = $4 * 8 / 1.4142 = 22.63 \text{ mm}$

$$\tau = 2 * Ra / (a * hw') = 2 * 800.0 * 10^3 / (22.63 * 2378)$$

$$= 29.7 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

Main girder G-5, Support PF12

Reaction Force Ra= 2500.0 kN
 Upper Flange 590
 Lower Flange 590 * 39
 WEB 2369 * 12 (SM490YA)
 Sole Plate 710 * 710 (202.0 φ)
 STIFFENER 2- 320 * 26 (SM400A)
 STIFF 2369.0/30+50 = 129.0 < 320.0

Check of bearing stress(PF12)

(SM400A)STIFF 2*(32.00- 9.50+ 3.9)* 2.6 = 137.28
 (SM490YA)WEB (28.80- 20.20+2* 3.9)* 1.2 = 19.68

$$Ab = 156.96 \text{ cm}^2$$

$$\sigma_b = R/Ab = 2500.00 * 10^3 / 156.96 * 10^2 = 159.3 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(PF12)

(SM400A)STIFF 2* 32.00* 2.6 = 166.40
 (SM490YA)WEB 28.80* 1.2 = 34.56

$$A = 200.96 \text{ cm}^2$$

$$1.7 * 166.40 = 282.88 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 200.96 \text{ cm}^2$$

$$I = 60057 \text{ cm}^4$$

$$r = \text{SQR}(I/Ae) = \text{SQR}(60057 / 200.96) = 17.29 \text{ cm}$$

allowable stress

$$L/r = 236.9 / 2 / 17.29 = 6.85 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 2500.00 * 10^3 / 200.96 * 10^2 = 124.4 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(PF12)

fillet weld s = $\text{SQR}(2*26) = 7.21 \rightarrow 10 \text{ mm} < t_{min} = 12 \text{ mm}$
 throat thickness a = $4*10/1.4142 = 28.28 \text{ mm}$

$$\tau = 2 * Ra / (a * hw') = 2 * 2500.0 * 10^3 / (28.28 * 2369)$$

$$= 74.6 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

Main girder G-5, Support PF13

Reaction Force Ra= 2500.0 kN
 Upper Flange 590
 Lower Flange 590 * 39
 WEB 2369 * 12 (SM490YA)
 Sole Plate 710 * 710 (202.0 φ)
 STIFFENER 2- 320 * 26 (SM400A)
 STIFF 2369.0/30+50 = 129.0 < 320.0

Check of bearing stress(PF13)

(SM400A)STIFF 2*(32.00- 9.50+ 3.9)* 2.6 = 137.28
 (SM490YA)WEB (28.80- 20.20+2* 3.9)* 1.2 = 19.68

$$Ab = 156.96 \text{ cm}^2$$

$$\sigma_b = R/Ab = 2500.00 * 10^3 / 156.96 * 10^2 = 159.3 \text{ N/mm}^2$$

$$< \sigma_{ba} = 210.0 \text{ N/mm}^2$$

Check of stress in vertical direction(PF13)

(SM400A)STIFF 2* 32.00* 2.6 = 166.40
 (SM490YA)WEB 28.80* 1.2 = 34.56

$$A = 200.96 \text{ cm}^2$$

$$1.7 * 166.40 = 282.88 \text{ cm}^2 > A \quad \text{therefore} \quad Ae = 200.96 \text{ cm}^2$$

$$I = 60057 \text{ cm}^4$$

$$r = \text{SQR}(I/Ae) = \text{SQR}(60057 / 200.96) = 17.29 \text{ cm}$$

allowable stress

$$L/r = 236.9 / 2 / 17.29 = 6.85 < 18$$

$$\sigma_{cag} = 140.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} * \sigma_{cal} / \sigma_{cao} = 140.0 * 140.0 / 140.0 = 140.0 \text{ N/mm}^2$$

$$\sigma_v = R/Ae = 2500.00 * 10^3 / 200.96 * 10^2 = 124.4 \text{ N/mm}^2 < \sigma_{ca}$$

Welding between stiffener and web plate(PF13)

fillet weld s = SQR(2*26) = 7.21 ---> 10 mm < tmin = 12 mm
 throat thickness a = 4*10/1.4142 = 28.28 mm

$$\tau = 2 * Ra / (a * hw') = 2 * 2500.0 * 10^3 / (28.28 * 2369)$$

$$= 74.6 \text{ N/mm}^2 < \tau_a = 80.0 \text{ N/mm}^2$$

4-5 Calculation of Stiffener for Lateral Force

1. Design force

The stiffener is calculated by the horizontal force during earthquake.

1) Horizontal force

Piers	Girder	Node No.	Force	Force
				Each Girder
S1(PF11)	G1	101	1070	214
	G2	201		214
	G3	301		214
	G4	401		214
	G5	501		214
PF12	G1	107	1670	334
	G2	207		334
	G3	307		334
	G4	407		334
	G5	507		334
PF13	G1	117	1830	366
	G2	217		366
	G3	317		366
	G4	417		366
	G5	517		366
S2(PF14)	G1	123	1270	254
	G2	223		254
	G3	323		254
	G4	423		254
	G5	523		254

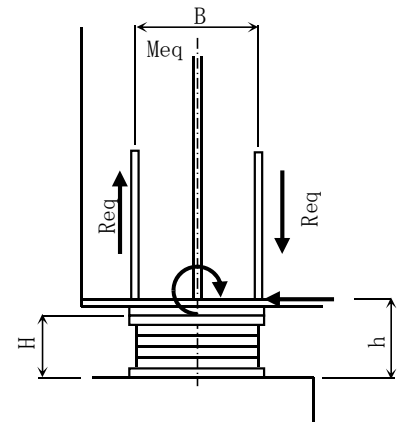
2. Calculation for Bearing stiffener

(1) Calculate P14 (P11 has the same stiffener)

1) Conditions

Force	: Heq	=	254 (kN)
Bearing Height	: H	=	230 (mm)
Sole P L	: ts	=	24 (mm)
Lower Flange	: tf	=	19 (mm)
Point of action	: h	=	273 (mm)
Space	: B	=	510 (mm)
Rib Height	: L	=	250 (mm)

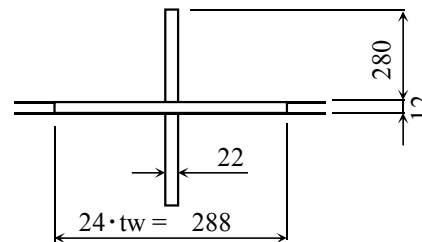
$$\begin{aligned} \text{Meq} &= 254.0 \times 0.273 = 69.3 \text{ (kN.m)} \\ \text{Req} &= 69.3 / 0.510 / 1.5 = 90.6 \text{ (kN)} \end{aligned}$$



2) Shape of rib

	A (cm ²)	y (cm)	Ay ² (cm ⁴)	Io (cm ⁴)
1 - PL. 288 x 12 (SM490Y)	34.6	---	---	4
2 - PL. 280 x 22 (SM400)	123.2	14.60	26261	8049
A =	157.8	< 1.7 x 123.2 =	209.4	(cm²)

$$\begin{aligned} A_e &= 157.8 \text{ (cm}^2\text{)} \\ I &= 34314 \text{ (cm}^4\text{)} \\ r &= 14.75 \text{ (cm)} \\ L &= 25.00 \text{ (cm)} \\ L/r &= 1.69 \end{aligned}$$



3) Allowable Stress

$$\begin{aligned} B &= 280 \text{ (mm)} \geq L / 30 + 50 = 58.3 \text{ (mm)} \\ t &= 22 \text{ (mm)} \geq B / 12.8 = 21.9 \text{ (mm)} \\ \sigma_{ca} &= 140 \text{ (N/mm}^2\text{)} \end{aligned}$$

4) Checking of Compressive Stress

$$\begin{aligned} L/r &= 1.69 \leq 18 \\ \sigma_{ca} &= 140 \text{ (N/mm}^2\text{)} \\ \sigma_c &= 90.60 \times 10^3 / 15780 = 5.7 \leq 140 \text{ (N/mm}^2\text{)} \end{aligned}$$

5) Welding of Stiffener and Web

$$\begin{aligned} \text{Welding Saize : } S &= \sqrt{(2 \times 22)} = 6.6 \text{ (mm)} \rightarrow 7 \text{ (mm)} < t_{min} = 12 \\ \text{Effective Throat : } a &= 4 \times 7.0 / \sqrt{2} = 19.8 \text{ (mm)} \end{aligned}$$

$$\begin{aligned} \tau &= 1 \times R / (a \times H_w) \\ &= 1 \times 90.60 \times 10^3 / (19.8 \times (250 - 50)) \\ &= 22.9 \text{ (N/mm}^2\text{)} < \tau_a = 80 \text{ (N/mm}^2\text{)} \end{aligned}$$

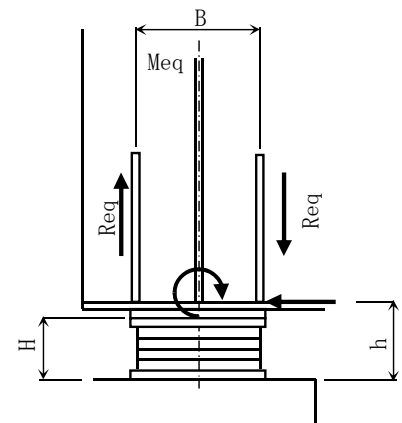
(2) Calculate P13 (P12 has the same stiffener)

1) Conditions

Force : Heq = 366 (kN)
 Bearing Height : H = 248 (mm)
 Sole P L : ts = 27 (mm)
 Lower Flange : tf = 39 (mm) Maximum
 Point of action : h = 314 (mm)
 Space : B = 710 (mm)
 Rib Height : L = 250 (mm)

$$\text{Meq} = 366.0 \times 0.314 = 114.9 \text{ (kN.m)}$$

$$\text{Req} = 114.9 / 0.710 / 1.5 = 107.9 \text{ (kN)}$$



2) Shape

	A (cm ²)	y (cm)	Ay ² (cm ⁴)	Io (cm ⁴)
1 - PL. 288 x 12 (SM490Y)	34.6	---	---	4
2 - PL. 320 x 26 (SM400)	166.4	16.60	45853	14199
A =	201.0	< 1.7 x 166.4	= 282.9	(cm²)

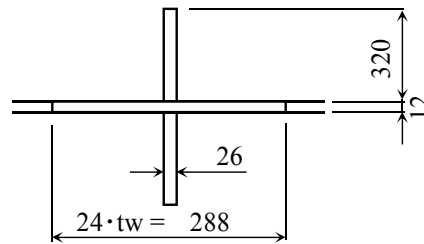
$$\text{Ae} = 201.0 \text{ (cm}^2\text{)}$$

$$\text{I} = 60056 \text{ (cm}^4\text{)}$$

$$\text{r} = 17.29 \text{ (cm)}$$

$$\text{L} = 25.00 \text{ (cm)}$$

$$\text{L/r} = 1.45$$



3) Allowable Stress

$$\text{B} = 320 \text{ (mm)} \geq \text{L} / 30 + 50 = 58.3 \text{ (mm)}$$

$$\text{t} = 26 \text{ (mm)} \geq \text{B} / 12.8 = 25 \text{ (mm)}$$

$$\sigma_{\text{cag}} = 140 \text{ (N/mm}^2\text{)}$$

4) Checking of Compressive Stress

$$\text{L/r} = 1.45 \leq 18$$

$$\sigma_{\text{ca}} = 140 \text{ (N/mm}^2\text{)}$$

$$\sigma_{\text{c}} = 107.90 \times 10^3 / 20100 = 5.4 \leq 140 \text{ (N/mm}^2\text{)}$$

5) Welding of Stiffener and Web

$$\text{Welding Saize : } S = \sqrt{(2 \times 26)} = 7.2 \text{ (mm)} \rightarrow 8 \text{ (mm)} < \text{tmin} = 12$$

$$\text{Effective Throat : } a = 4 \times 8.0 / \sqrt{2} = 22.6 \text{ (mm)}$$

$$\tau = 1 \times R / (a \times H_w)$$

$$= 1 \times 107.90 \times 10^3 / (22.6 \times 250)$$

$$= 19.1 \text{ (N/mm}^2\text{)} < \tau_a = 80 \text{ (N/mm}^2\text{)}$$

4-6 Stiffener for Jack up

1. Design force for Jack up (When replacing bearing)

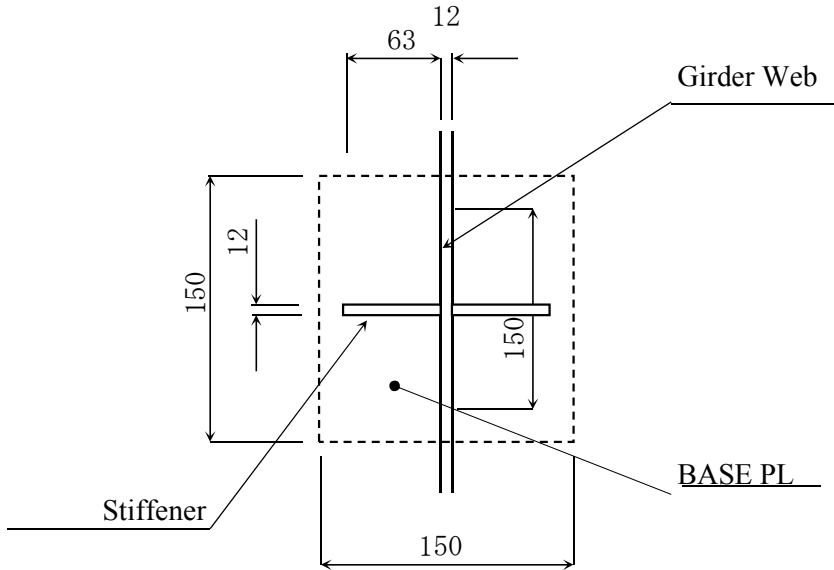
(kN)

		Rd+RL	N	uniformity coefficient	Force
		MAX			
S1	G1	773.91	1	1.1	900
	G2	653.15	1	1.1	800
	G3	747.91	1	1.1	900
	G4	653.15	1	1.1	800
	G5	773.91	1	1.1	900
PF12	G1	2491.24	2	1.1	1400
	G2	1970.23	2	1.1	1100
	G3	2058.50	2	1.1	1200
	G4	1970.23	2	1.1	1100
	G2	2491.24	2	1.1	1400
PF13	G1	2491.24	2	1.1	1400
	G2	1970.23	2	1.1	1100
	G3	2058.50	2	1.1	1200
	G4	1970.23	2	1.1	1100
	G2	2491.24	2	1.1	1400
S2	G1	773.91	1	1.1	900
	G2	653.15	1	1.1	800
	G3	747.91	1	1.1	900
	G4	653.15	1	1.1	800
	G5	773.91	1	1.1	900

2. Reinforcement rib for jack up design

(1) Supprt (End side)

Force	Rjk =	900.0 kN
Jack	:	100 t
	n =	1
PL width		150 × 150
Rib		130 × 12 (SM490 Y)
Welding Height		2378 mm
Web thickness	tw =	12 mm (SM490 Y)



<pressure stress >

Rib	(SM490 Y)	2 ×	6.3 ×	1.2	=	15.12 cm ²
Web	(SM490 Y)	1 ×	15.0 ×	1.2	=	18.00 cm ²
Ab =						33.12 cm ²

$$\sigma_b = R / A_b = \frac{900.0 \times 10^3}{33.12 \times 10^2} = 271.7 \text{ N/mm}^2 < \sigma_{ba} = 315 \text{ N/mm}^2$$

<Compressive stress >

				A(cm ²)	y(cm)	A·y(cm ³)	A·y ² (cm ⁴)	
Rib	(SM490 Y)	1 ×	13.0 ×	1.2	15.60	-7.10	-110.76	1006
Web	(SM490 Y)	1 ×	28.8 ×	1.2	34.56	--	--	4
Stiff	(SM490 Y)	1 ×	13.0 ×	1.2	15.60	7.10	110.76	1006
ΣA=					65.76		0.00	2016
							0	
							I =	2016 cm ⁴

$$1.7 \times 31.20 = 53.04 \text{ cm}^2 < A \text{ 故に } A_e = 53.04 \text{ cm}^2$$

$$e = 0.0 \text{ cm} , \quad , \quad r = 6.17 \text{ cm}$$

$$L/r = 1/2 \times \frac{237.8}{6.17} = 19.28$$

• Stress

$$\sigma_c = R / A_e = 900.0 \times 10^3 / (53.04 \times 10^2) = 169.7 \text{ N/mm}^2 < \sigma_{ca} = 190.0 \text{ N/mm}^2$$

Allowable Stress

$$L/r = 19.28 > 15 \quad \sigma_{cag} = 203.6 \text{ (N/mm}^2) \quad (t \leq 40)$$

Allowable Stress for Local buckling

$$b/t = 130 / 12 = 10.8 > 10.5$$

$$\therefore \sigma_{cag} = 196.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} \times \sigma_{cal} / \sigma_{cao} = 190.0 \text{ N/mm}^2$$

<Welding check>

• Stiffener - Web

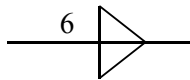
$$a_{req} = (2 \times R) / (n \times L \times \tau_a)$$

$$= (2 \times 900.0 \times 10^3) / (4 \times 2378 \times 120) = 1.6 \text{ mm}$$

Welding Size

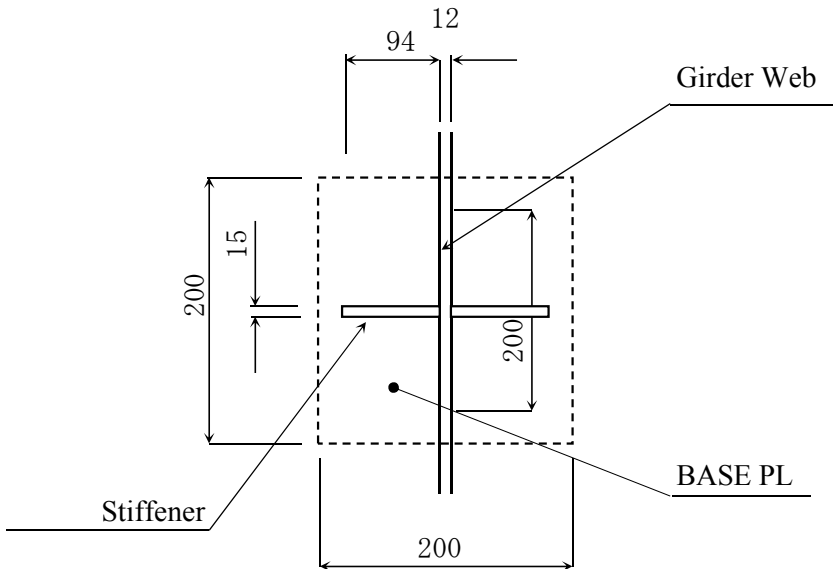
$$S = 1.6 \times \sqrt{2} \times 1/2 = 1.1 \text{ mm}$$

$$\sqrt{2t} = 4.9 \leq 6 \text{ mm} < \min(t_s, t_w) = 12 \text{ mm}$$



(2) Intermediate fulcrum

Force $R_{jk} = 1400.0 \text{ kN}$
 Jack : 200 t
 $n = 2$
 PL width 200 × 200
 Rib 150 × 15 (SM490 Y)
 Welding Height 2369 mm
 Web thickness $tw = 12 \text{ mm}$ (SM490 Y)



< pressure stress >

Rib	(SM490 Y)	2 ×	9.4 ×	1.5	=	28.20 cm ²
Web	(SM490 Y)	1 ×	20.0 ×	1.2	=	24.00 cm ²
Ab =						52.20 cm²

$$\sigma_b = R / A_b = 1400.0 \times 10^3 / 52.20 \times 10^2 = 268.2 \text{ N/mm}^2 < \sigma_{ba} = 315 \text{ N/mm}^2$$

< Compressive stress >

				A(cm ²)	y(cm)	A·y(cm ³)	A·y ² (cm ⁴)	
Rib	(SM490 Y)	1 ×	15.0 ×	1.5	22.50	-8.10	-182.25	1898
Web	(SM490 Y)	1 ×	28.8 ×	1.2	34.56	--	--	4
Stiff	(SM490 Y)	1 ×	15.0 ×	1.5	22.50	8.10	182.25	1898
∑A=					79.56	0.00	3800	0
							I=	3800 cm⁴

$$1.7 \times 45.00 = 76.50 \text{ cm}^2 < A \text{ 故に } A_e = 76.50 \text{ cm}^2$$

$$e = 0.0 \text{ cm}, \quad r = 7.05 \text{ cm}$$

$$L/r = 1/2 \times 236.9 / 7.05 = 16.81$$

• Stress

$$\sigma_c = R / A_e = 1400.0 \times 10^3 / (76.50 \times 10^2) = 183.0 \text{ N/mm}^2 < \sigma_{ca} = 207.3 \text{ N/mm}^2$$

Allowable Stress

$$L/r = 16.8 > 15 \quad \sigma_{cag} = 207.3 \text{ (N/mm}^2\text{)} \quad (t \leq 40)$$

Allowable Stress for Local buckling

$$b/t = 150 / 15 = 10.0 \leq 10.5$$

$$\therefore \sigma_{cag} = 210.0 \text{ N/mm}^2$$

$$\therefore \sigma_{ca} = \sigma_{cag} \times \sigma_{cal} / \sigma_{cao} = 210.0 \text{ N/mm}^2$$

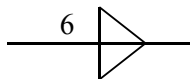
<Welding check>

• Stiffener - Web

$$\begin{aligned} a_{req} &= (2 \times R) / (n \times L \times \tau_a) \\ &= (2 \times 1400.0 \times 10^3) / (4 \times 2369 \times 120) = 2.5 \text{ mm} \end{aligned}$$

Welding Size

$$\begin{aligned} S &= 2.5 \times \sqrt{2} \times 1/2 = 1.7 \text{ mm} \\ \sqrt{(2t)} &= 5.5 \leq 6 \text{ mm} < \min(t_s, t_w) = 12 \text{ mm} \end{aligned}$$



4-7 Checking of Stiffness ratio

(1) G1

PANEL	length	Assumption (Iy')	Actual value (Iy)	ratio
1	5.800	0.048274	0.048154	0.2
2	5.800	0.048274	0.048154	0.2
3	5.800	0.048274	0.048154	0.2
4	5.800	0.049417	0.049294	0.3
5	5.800	0.055000	0.052795	4.2
6	5.300	0.072144	0.072513	-0.5
7	5.200	0.069247	0.069586	-0.5
8	5.200	0.049216	0.049093	0.2
9	5.200	0.051508	0.050325	2.4
10	5.200	0.055000	0.051064	7.7
11	5.200	0.055000	0.052766	4.2
12	5.200	0.055000	0.052766	4.2
13	5.200	0.055000	0.051064	7.7
14	5.200	0.051508	0.050325	2.4
15	5.200	0.049216	0.049093	0.2
16	5.200	0.069247	0.069586	-0.5
17	5.300	0.072144	0.072513	-0.5
18	5.800	0.055000	0.052795	4.2
19	5.800	0.049417	0.049294	0.3
20	5.800	0.048274	0.048154	0.2
21	5.800	0.048274	0.048154	0.2
22	5.800	0.048274	0.048154	0.2

Span length	Assumption (Iy')	Actual value (Iy)	ratio	
1	34.300	0.053293	0.052895	0.8
2	52.000	0.055994	0.054567	2.6
3	34.300	0.053293	0.052895	0.8

(2) G2

PANEL	length	Assumption (Iy')	Actual value (Iy)	ratio
1	5.800	0.047501	0.047382	0.3
2	5.800	0.047501	0.047382	0.3
3	5.800	0.047501	0.047382	0.3
4	5.800	0.047558	0.047439	0.3
5	5.800	0.048722	0.048600	0.3
6	5.300	0.057870	0.056492	2.4
7	5.200	0.056893	0.055364	2.8
8	5.200	0.047592	0.047473	0.3
9	5.200	0.051417	0.049278	4.3
10	5.200	0.052414	0.050362	4.1
11	5.200	0.050488	0.050362	0.3
12	5.200	0.050488	0.050362	0.3
13	5.200	0.052414	0.050362	4.1
14	5.200	0.051417	0.049278	4.3
15	5.200	0.047592	0.047473	0.3
16	5.200	0.056893	0.055364	2.8
17	5.300	0.057870	0.056492	2.4
18	5.800	0.048722	0.048600	0.3
19	5.800	0.047558	0.047439	0.3
20	5.800	0.047501	0.047382	0.3
21	5.800	0.047501	0.047382	0.3
22	5.800	0.047501	0.047382	0.3

Span length	Assumption (Iy')	Actual value (Iy)	ratio	
1	34.300	0.049319	0.049005	0.6
2	52.000	0.051761	0.050568	2.4
3	34.300	0.049319	0.049005	0.6

(3) G3

PANEL	length	Assumption (Iy')	Actual value (Iy)	ratio
1	5.800	0.047382	0.047382	0.0
2	5.800	0.047382	0.047382	0.0
3	5.800	0.047382	0.047382	0.0
4	5.800	0.047439	0.047439	0.0
5	5.800	0.048388	0.048293	0.2
6	5.300	0.054796	0.054035	1.4
7	5.200	0.053881	0.053215	1.3
8	5.200	0.047473	0.047473	0.0
9	5.200	0.048829	0.048829	0.0
10	5.200	0.049643	0.049643	0.0
11	5.200	0.049643	0.049643	0.0
12	5.200	0.049643	0.049643	0.0
13	5.200	0.049643	0.049643	0.0
14	5.200	0.048829	0.048829	0.0
15	5.200	0.047473	0.047473	0.0
16	5.200	0.053881	0.053215	1.3
17	5.300	0.054796	0.054035	1.4
18	5.800	0.048388	0.048293	0.2
19	5.800	0.047439	0.047439	0.0
20	5.800	0.047382	0.047382	0.0
21	5.800	0.047382	0.047382	0.0
22	5.800	0.047382	0.047382	0.0

Span length	Assumption (Iy')	Actual value (Iy)	ratio	
1	34.300	0.048707	0.048574	0.3
2	52.000	0.049894	0.049761	0.3
3	34.300	0.048707	0.048574	0.3

(4) G4

PANEL	length	Assumption (Iy')	Actual value (Iy)	ratio
1	5.800	0.047501	0.047382	0.3
2	5.800	0.047501	0.047382	0.3
3	5.800	0.047501	0.047382	0.3
4	5.800	0.047558	0.047439	0.3
5	5.800	0.048722	0.048600	0.3
6	5.300	0.057870	0.056492	2.4
7	5.200	0.056893	0.055364	2.8
8	5.200	0.047592	0.047473	0.3
9	5.200	0.051417	0.049278	4.3
10	5.200	0.052414	0.050362	4.1
11	5.200	0.050488	0.050362	0.3
12	5.200	0.050488	0.050362	0.3
13	5.200	0.052414	0.050362	4.1
14	5.200	0.051417	0.049278	4.3
15	5.200	0.047592	0.047473	0.3
16	5.200	0.056893	0.055364	2.8
17	5.300	0.057870	0.056492	2.4
18	5.800	0.048722	0.048600	0.3
19	5.800	0.047558	0.047439	0.3
20	5.800	0.047501	0.047382	0.3
21	5.800	0.047501	0.047382	0.3
22	5.800	0.047501	0.047382	0.3

Span length	Assumption (Iy')	Actual value (Iy)	ratio	
1	34.300	0.049319	0.049005	0.6
2	52.000	0.051761	0.050568	2.4
3	34.300	0.049319	0.049005	0.6

(5) G5

PANEL	length	Assumption (Iy')	Actual value (Iy)	ratio
1	5.800	0.048274	0.048154	0.2
2	5.800	0.048274	0.048154	0.2
3	5.800	0.048274	0.048154	0.2
4	5.800	0.049417	0.049294	0.3
5	5.800	0.055000	0.052795	4.2
6	5.300	0.072144	0.072513	-0.5
7	5.200	0.069247	0.069586	-0.5
8	5.200	0.049216	0.049093	0.2
9	5.200	0.051508	0.050325	2.4
10	5.200	0.055000	0.051064	7.7
11	5.200	0.055000	0.052766	4.2
12	5.200	0.055000	0.052766	4.2
13	5.200	0.055000	0.051064	7.7
14	5.200	0.051508	0.050325	2.4
15	5.200	0.049216	0.049093	0.2
16	5.200	0.069247	0.069586	-0.5
17	5.300	0.072144	0.072513	-0.5
18	5.800	0.055000	0.052795	4.2
19	5.800	0.049417	0.049294	0.3
20	5.800	0.048274	0.048154	0.2
21	5.800	0.048274	0.048154	0.2
22	5.800	0.048274	0.048154	0.2

Span length	Assumption (Iy')	Actual value (Iy)	ratio	
1	34.300	0.053293	0.052895	0.8
2	52.000	0.055994	0.054567	2.6
3	34.300	0.053293	0.052895	0.8

4-8 Checking of Live Load deflection

Main girder G1

Span No.	Span length	Actual Deflection	Allowable deflection	Actual def./Span Length	Allowable def./Span Length
	L span(mm)	δ (mm)	δa (mm)	δ / L span	$\delta a / L$ span
1	34300	23.0	58.8	1/1491	1/583
2	52000	54.6	104.0	1/953	1/500
3	34300	23.0	58.8	1/1491	1/583

Main girder G2

Span No.	Span length	Actual Deflection	Allowable deflection	Actual def./Span Length	Allowable def./Span Length
	L span(mm)	δ (mm)	δa (mm)	δ / L span	$\delta a / L$ span
1	34300	18.2	58.8	1/1885	1/583
2	52000	45.6	104.0	1/1141	1/500
3	34300	18.2	58.8	1/1885	1/583

Main girder G3

Span No.	Span length	Actual Deflection	Allowable deflection	Actual def./Span Length	Allowable def./Span Length
	L span(mm)	δ (mm)	δa (mm)	δ / L span	$\delta a / L$ span
1	34300	17.9	58.8	1/1919	1/583
2	52000	43.2	104.0	1/1204	1/500
3	34300	17.9	58.8	1/1919	1/583

Main girder G4

Span No.	Span length	Actual Deflection	Allowable deflection	Actual def./Span Length	Allowable def./Span Length
	L span(mm)	δ (mm)	δa (mm)	δ / L span	$\delta a / L$ span
1	34300	18.2	58.8	1/1885	1/583
2	52000	45.6	104.0	1/1141	1/500
3	34300	18.2	58.8	1/1885	1/583

Main girder G5

Span No.	Span length	Actual Deflection	Allowable deflection	Actual def./Span Length	Allowable def./Span Length
	L span(mm)	δ (mm)	δa (mm)	δ / L span	$\delta a / L$ span
1	34300	23.0	58.8	1/1491	1/583
2	52000	54.6	104.0	1/953	1/500
3	34300	23.0	58.8	1/1491	1/583

§5 Design of Cross Beam

5-1 Design Method

Design Method

- In the design of the cross beam, the section is determined by the load due to the wind load and the seismic load.
- The end crossbeam is calculated by the direct force caused by vehicle and slab load.
- Cross beam is calculated as a simple beam model.

Load Condition

1) Wind Load

$$\begin{array}{ll} \text{Without Live Load} & q_w = 16.000 \text{ (kN/m)} \\ \text{With Live Load} & q_w' = 8.000 \text{ (kN/m)} \end{array}$$

2) Seismic Load

$$\begin{array}{ll} \text{Dead Load} & \sum R_d = 19305.60 \text{ (kN)} \\ \text{Span length} & \sum L = 120.600 \text{ (m)} \\ \text{Seismic intensity} & K_h = 0.30 \end{array}$$
$$\begin{aligned} q_{e1} &= \sum R_d / \sum L \times K_h \\ &= 19305.60 / 120.600 \times 0.30 \\ &= 48.024 \text{ (kN/m)} \end{aligned}$$

5-2 Calculation Result of Cross Beam

		CROSS BEAM					
		S1		PF12		C2	
FORCE	MOMENT	184.1	kNm	0.0	kNm	739.7	kNm
	Axial Force	0.0	kNm	392.26	kNm	-717.9	kNm
	SHEAR	362.5	kN	0.0	kN	194.8	kN
FLANGE	mm	250	x 10	250	x 10	250	x 10
WEB	mm	2080	x 9	1880	x 9	1880	x 9
MATERIAL		SM400		SM400		SM400	
σ_x	N/mm ²	-6.0	≤ 90.6	17.9	≤ 93.0	-	-
$\sigma_x + \sigma_c$	N/mm ²	-15.83	≤ 118.4	17.9	≤ 140.0	-74	≤ 119.0
τ	N/mm ²	19.36	≤ 80.0	0	≤ 80.0	12	≤ 80.0

§6. Design of Sway Bracing

6-1 Design Method

Design Method

- In the design of the cross beam, the section is determined by the load due to the wind load and the seismic load.
- Limiting slenderness ratio is 150

Load Condition

1) Intensity of Wind Load

The intensity of wind load is calculated in §2. Design of Slab

$$\text{Without Live Load } q_w = 16.000 \text{ (kN/m)}$$

$$\text{With Live Load } q_w' = 8.000 \text{ (kN/m)}$$

2) Intensity of Seismic Load

$$\text{Reaction Force of Dead Load } \Sigma R_d = 19305.60 \text{ (kN) (by the analytical result)}$$

$$\text{Average Span Length } \Sigma L = 120.600 \text{ (m)}$$

$$\text{Design Horizontal Seismic Coefficient } K_h = 0.30$$

$$\begin{aligned} q_{e1} &= \Sigma R_d / \Sigma L \times K_h \\ &= 19305.60 / 120.600 \times 0.30 \\ &= 48.02 \text{ (kN/m)} \end{aligned}$$

6-2 Calculation Result of Sway Bracing

		SWAY BRACING			
		UPPER & LOWER CORD		DIAGONAL MEMBER	
SHAPE		L-90x90x10x10		L-90x90x10x10	
MATERIAL		SS400		SS400	
SLENDERNESS RATIO		149	< 150.0	129	< 150.0
AXIAL FORCE	kN	23.2	kN	40.1	kN
σ_c	N/mm ²	-13.7	≤ 41.0	-23.6	≤ 51.0
σ_t	N/mm ²	17.9	≤ 140.0	30.8	≤ 140.0

§7. Design of Lower Lateral Bracing

7-1 Design Method

- In the design of the cross beam, the section is determined by the load due to the wind load and the seismic
- Sectional forces are shared between the deck and lateral, lateral forces are equally shared on the left and right.
- Limiting slenderness ratio is 150

1. Load

1) Intensity of Wind Load

Without Live Load	$q_w = 16.00$	(kN/m)	1/4 of the force is supported	4.00	(kN/m)
With Live Load	$q_w' = 8.000$	(kN/m)	1/4 of the force is supported	2.00	(kN/m)

2) Intensity of Seismic Load

Reaction Force of Dead Load	$\Sigma R_d = 19305.6$	(kN)	(by the analytical result)
Average Span Length	$\Sigma L = 120.600$	(m)	
Design Horizontal Seismic Coefficient	$K_h = 0.30$		

$$\begin{aligned}
 q_{e1} &= \Sigma R_d / \Sigma L \times K_h \\
 &= 19305.60 / 120.600 \times 0.30 \\
 &= 48.024 \text{ (kN/m)} \quad \text{1/4 of the force is supported } \boxed{12.01} \text{ (kN/m)}
 \end{aligned}$$

7-2 Calculation Result of Lateral Sway Bracing

*** Lateral sway bracing ***

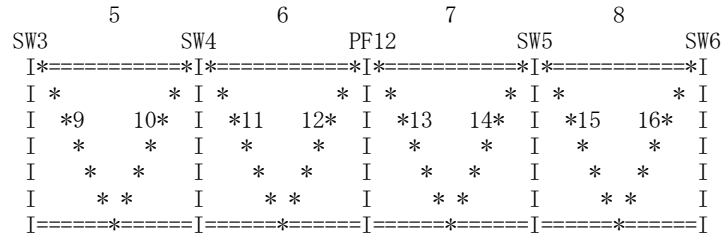
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          1          2          3          4
S1      SW1      SW2      C1      SW3
I*====*I*====*I*====*I*====*I
I *      * I *      * I *      * I *      * I
I *1      2* I *3      4* I *5      6* I *7      8* I
I *      * I *      * I *      * I *      * I
I * *      I * *      I * *      I * *      I
I * *      I * *      I * *      I * *      I
I====*I====*I====*I====*I

```

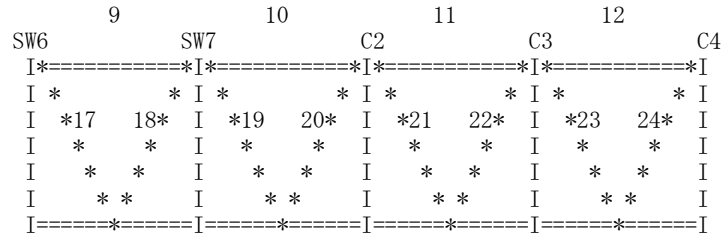
Member			1	3	5	7
Section	B W	mm	CT-118*178	CT-118*178	CT-118*178	BT-200, 150
	P T	mm	10* 8	10* 8	10* 8	*16, *16
	Q M		SS400	SS400	SS400	SM400A
	Length	cm	389.5	389.5	389.5	389.5
Slenderness	Weak axis		109.1	109.1	109.1	89.0
	outersurface		109.1	109.1	109.1	77.9
	Slenderness		150	150	150	150
Actual stress		kN	101.423	37.979	37.663	107.207
Compression	Actual	N/mm2	39.1	14.6	14.5	19.1
	Allowable	N/mm2	39.3	39.3	39.3	52.5
Tension	Actual	N/mm2	61.6	23.1	22.9	29.8
	Allowable	N/mm2	140.0	140.0	140.0	140.0
bolt	Required b	N	1.88	0.70	0.70	1.99
	Use bolt	N	2	2	2	2
Member			2	4	6	8
Section	B W	mm	CT-118*178	CT-118*178	CT-118*178	BT-200, 150
	P T	mm	10* 8	10* 8	10* 8	*16, *16
	Q M		SS400	SS400	SS400	SM400A
	Length	cm	389.5	389.5	389.5	389.5
Slenderness	Weak axis		109.1	109.1	109.1	89.0
	outersurface		109.1	109.1	109.1	77.9
	Slenderness		150	150	150	150
Actual stress		kN	101.423	37.979	37.663	107.207
Compression	Actual	N/mm2	39.1	14.6	14.5	19.1
	Allowable	N/mm2	39.3	39.3	39.3	52.5
Tension	Actual	N/mm2	61.6	23.1	22.9	29.8
	Allowable	N/mm2	140.0	140.0	140.0	140.0
bolt	Required b	N	1.88	0.70	0.70	1.99
	Use bolt	N	2	2	2	2

*** Lateral sway bracing ***



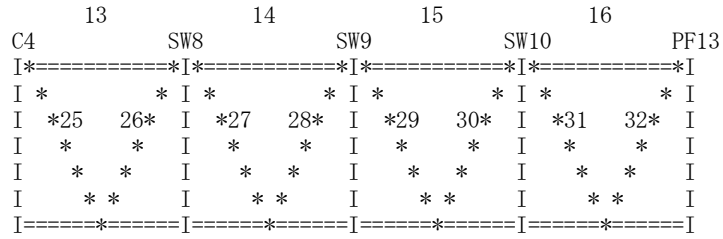
Member			9	11	13	15
Section	B W	mm	BT-200, 150	BT-200, 150	BT-200, 150	BT-200, 150
	P T	mm	*16, *16	*16, *16	*16, *16	*16, *16
	Q M		SM400A	SM400A	SM400A	SM400A
	Length	cm	389.5	371.2	367.7	367.7
Slenderness	Weak axis		89.0	84.9	84.0	84.0
	outersurface		77.9	74.2	73.5	73.5
	Slenderness		150	150	150	150
Actual stress		kN	176.750	231.902	264.873	206.012
Compression	Actual	N/mm2	31.6	41.4	47.3	36.8
	Allowable	N/mm2	52.5	53.9	54.2	54.2
Tension	Actual	N/mm2	49.1	64.4	73.6	57.2
	Allowable	N/mm2	140.0	140.0	140.0	140.0
bolt	Required b	N	3.27	4.29	4.91	3.82
	Use bolt	N	4	6	6	4
Member			10	12	14	16
Section	B W	mm	BT-200, 150	BT-200, 150	BT-200, 150	BT-200, 150
	P T	mm	*16, *16	*16, *16	*16, *16	*16, *16
	Q M		SM400A	SM400A	SM400A	SM400A
	Length	cm	389.5	371.2	367.7	367.7
Slenderness	Weak axis		89.0	84.9	84.0	84.0
	outersurface		77.9	74.2	73.5	73.5
	Slenderness		150	150	150	150
Actual stress		kN	176.750	231.902	264.873	206.012
Compression	Actual	N/mm2	31.6	41.4	47.3	36.8
	Allowable	N/mm2	52.5	53.9	54.2	54.2
Tension	Actual	N/mm2	49.1	64.4	73.6	57.2
	Allowable	N/mm2	140.0	140.0	140.0	140.0
bolt	Required b	N	3.27	4.29	4.91	3.82
	Use bolt	N	4	6	6	4

*** Lateral sway bracing ***



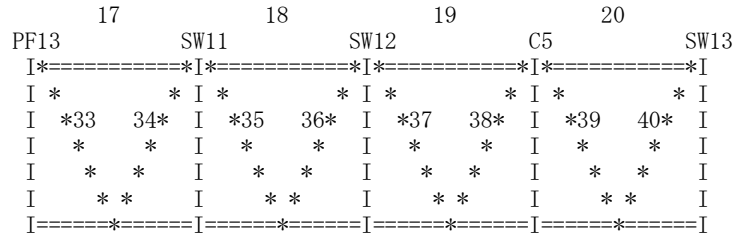
Member			17	19	21	23
Section	B W	mm	BT-200, 150	CT-118*178	CT-118*178	CT-118*178
	P T	mm	*16, *16	10* 8	10* 8	10* 8
	Q M		SM400A	SS400	SS400	SS400
	Length	cm	367.7	367.7	367.7	367.7
Slenderness	Weak axis		84.0	103.0	103.0	103.0
	outersurface		73.5	103.0	103.0	103.0
	Slenderness		150	150	150	150
Actual stress		kN	147.152	88.291	36.799	36.799
Compression	Actual	N/mm2	26.3	34.0	14.2	14.2
	Allowable	N/mm2	54.2	41.8	41.8	41.8
Tension	Actual	N/mm2	40.9	53.6	22.3	22.3
	Allowable	N/mm2	140.0	140.0	140.0	140.0
bolt	Required b	N	2.73	1.64	0.68	0.68
	Use bolt	N	4	2	2	2
Member			18	20	22	24
Section	B W	mm	BT-200, 150	CT-118*178	CT-118*178	CT-118*178
	P T	mm	*16, *16	10* 8	10* 8	10* 8
	Q M		SM400A	SS400	SS400	SS400
	Length	cm	367.7	367.7	367.7	367.7
Slenderness	Weak axis		84.0	103.0	103.0	103.0
	outersurface		73.5	103.0	103.0	103.0
	Slenderness		150	150	150	150
Actual stress		kN	147.152	88.291	36.799	36.799
Compression	Actual	N/mm2	26.3	34.0	14.2	14.2
	Allowable	N/mm2	54.2	41.8	41.8	41.8
Tension	Actual	N/mm2	40.9	53.6	22.3	22.3
	Allowable	N/mm2	140.0	140.0	140.0	140.0
bolt	Required b	N	2.73	1.64	0.68	0.68
	Use bolt	N	4	2	2	2

*** Lateral sway bracing ***



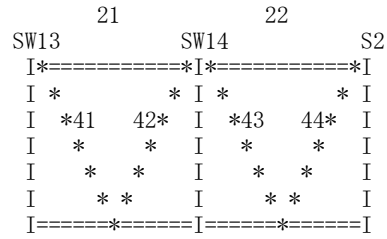
Member			25	27	29	31
Section	B W	mm	CT-118*178	BT-200, 150	BT-200, 150	BT-200, 150
	P T	mm	10* 8	*16, *16	*16, *16	*16, *16
	Q M		SS400	SM400A	SM400A	SM400A
	Length	cm	367.7	367.7	367.7	367.7
Slenderness	Weak axis		103.0	84.0	84.0	84.0
	outersurface		103.0	73.5	73.5	73.5
	Slenderness		150	150	150	150
Actual stress		kN	88.291	147.152	206.012	264.873
Compression	Actual	N/mm2	34.0	26.3	36.8	47.3
	Allowable	N/mm2	41.8	54.2	54.2	54.2
Tension	Actual	N/mm2	53.6	40.9	57.2	73.6
	Allowable	N/mm2	140.0	140.0	140.0	140.0
bolt	Required b	N	1.64	2.73	3.82	4.91
	Use bolt	N	2	4	4	6
Member			26	28	30	32
Section	B W	mm	CT-118*178	BT-200, 150	BT-200, 150	BT-200, 150
	P T	mm	10* 8	*16, *16	*16, *16	*16, *16
	Q M		SS400	SM400A	SM400A	SM400A
	Length	cm	367.7	367.7	367.7	367.7
Slenderness	Weak axis		103.0	84.0	84.0	84.0
	outersurface		103.0	73.5	73.5	73.5
	Slenderness		150	150	150	150
Actual stress		kN	88.291	147.152	206.012	264.873
Compression	Actual	N/mm2	34.0	26.3	36.8	47.3
	Allowable	N/mm2	41.8	54.2	54.2	54.2
Tension	Actual	N/mm2	53.6	40.9	57.2	73.6
	Allowable	N/mm2	140.0	140.0	140.0	140.0
bolt	Required b	N	1.64	2.73	3.82	4.91
	Use bolt	N	2	4	4	6

*** Lateral sway bracing ***



Member			33	35	37	39
Section	B W	mm	BT-200, 150	BT-200, 150	BT-200, 150	CT-118*178
	P T	mm	*16, *16	*16, *16	*16, *16	10* 8
	Q M		SM400A	SM400A	SM400A	SS400
	Length	cm	371.2	389.5	389.5	389.5
Slenderness	Weak axis		84.9	89.0	89.0	109.1
	outersurface		74.2	77.9	77.9	109.1
	Slenderness		150	150	150	150
Actual stress		kN	231.902	176.750	107.207	37.663
Compression	Actual	N/mm2	41.4	31.6	19.1	14.5
	Allowable	N/mm2	53.9	52.5	52.5	39.3
Tension	Actual	N/mm2	64.4	49.1	29.8	22.9
	Allowable	N/mm2	140.0	140.0	140.0	140.0
bolt	Required b	N	4.29	3.27	1.99	0.70
	Use bolt	N	6	4	2	2
Member			34	36	38	40
Section	B W	mm	BT-200, 150	BT-200, 150	BT-200, 150	CT-118*178
	P T	mm	*16, *16	*16, *16	*16, *16	10* 8
	Q M		SM400A	SM400A	SM400A	SS400
	Length	cm	371.2	389.5	389.5	389.5
Slenderness	Weak axis		84.9	89.0	89.0	109.1
	outersurface		74.2	77.9	77.9	109.1
	Slenderness		150	150	150	150
Actual stress		kN	231.902	176.750	107.207	37.663
Compression	Actual	N/mm2	41.4	31.6	19.1	14.5
	Allowable	N/mm2	53.9	52.5	52.5	39.3
Tension	Actual	N/mm2	64.4	49.1	29.8	22.9
	Allowable	N/mm2	140.0	140.0	140.0	140.0
bolt	Required b	N	4.29	3.27	1.99	0.70
	Use bolt	N	6	4	2	2

*** Lateral sway bracing ***



Member			41	43
Section	B W	mm	CT-118*178	CT-118*178
	P T	mm	10* 8	10* 8
	Q M		SS400	SS400
	Length	cm	389.5	389.5
Slenderness	Weak axis		109.1	109.1
	outersurface		109.1	109.1
	Slenderness		150	150
Actual stress		kN	37.979	101.423
Compression	Actual	N/mm2	14.6	39.1
	Allowable	N/mm2	39.3	39.3
Tension	Actual	N/mm2	23.1	61.6
	Allowable	N/mm2	140.0	140.0
bolt	Required b	N	0.70	1.88
	Use bolt	N	2	2
Member			42	44
Section	B W	mm	CT-118*178	CT-118*178
	P T	mm	10* 8	10* 8
	Q M		SS400	SS400
	Length	cm	389.5	389.5
Slenderness	Weak axis		109.1	109.1
	outersurface		109.1	109.1
	Slenderness		150	150
Actual stress		kN	37.979	101.423
Compression	Actual	N/mm2	14.6	39.1
	Allowable	N/mm2	39.3	39.3
Tension	Actual	N/mm2	23.1	61.6
	Allowable	N/mm2	140.0	140.0
bolt	Required b	N	0.70	1.88
	Use bolt	N	2	2

§8. Fatigue Design

8-1 Condition for Fatigue design

1. Live Load

AASHTO Track load
T-load

Comparing the stress range when loading one AASHTO track load and the stress range of a pair of loads of 100 t, there is a possibility that those large stress ranges will affect fatigue. the larger stress of them shall be adopted for stress of fatigue design.

2. Load correction factor

line $n_L = 2$

$ADTT_{SLi} = 2090$

Variable stress correction factor (λ_T)

$$\gamma_T = \gamma_{T1} \cdot \gamma_{T2}$$

$$\gamma_{T1} = 1.0 \log L_{B1} + 1.50 \quad (2.00 \leq \gamma_{T1} \leq 3.00)$$

γ_{T2}

$ADTT_{SLi}$	L_{B2}	$L_{B1} \leq 50m$	$50m < L_{B1}$
	$ADTT_{SLi} \leq 2000$	1.00	1.00
	$2000 < ADTT_{SLi}$	1.00	1.10

	L_{B1} (m)	L_{B2} (m)	$ADTT_{SLi}$	γ_{T1}	γ_{T2}	γ_T
First span	34.300	34.300	2090.0	3.00	1.00	3.00
Second spane	52.000	52.000	2090.0	3.00	1.10	3.30
The third span	34.300	34.300	0.0	3.00	1.10	3.30

3. Impact

$$i f = 10/(50+L)$$

	L (m)	$i f$
First span	34.300	0.119
Second spane	52.000	0.098
The third span	34.300	0.119

4. Structural analysis coefficient

$\gamma_a = 0.80$ (girder)
 $\gamma_a = 0.50$ (Cross beam)

4. Frequency correction factor

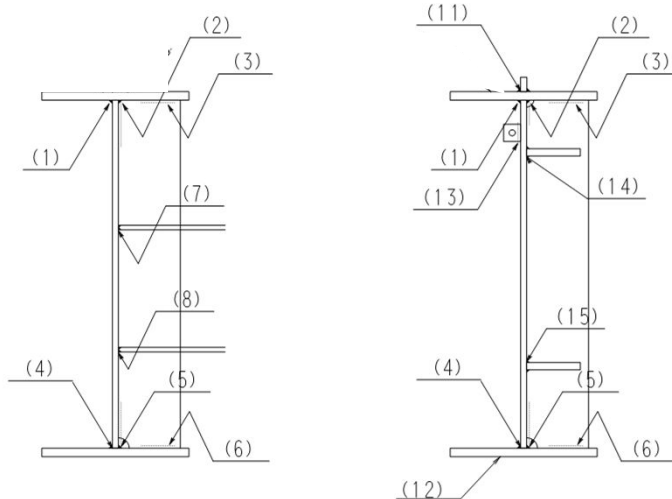
$\gamma_n = 0.03$

5. Comparing the stress range of 2 type Live Load

Girder		AASHTO	B-Live	(B) -(A)
Member		Stress Range(A)	Stress Range(B)	
G1	1001	0	0	0
	1002	763	1001	238
	1003	1442	1803	361
	1004	1912	2285	373
	1005	1545	1912	367
	1006	1162	1517	356
	1007	1303	1483	180
	1008	674	992	319
	1009	977	1355	378
	1010	1444	1825	381
	1011	1859	2242	383
	1012	1816	2219	404
	1013	1859	2242	383
	1014	1444	1825	381
	1015	977	1355	378
	1016	674	992	319
	1017	1303	1483	180
	1018	1162	1517	356
	1019	1545	1912	367
	1020	1912	2285	373
	1021	1442	1803	361
	1022	763	1001	238
G2	2001	0	0	0
	2002	1262	1559	297
	2003	1552	1964	411
	2004	1257	1639	383
	2005	1610	2004	394
	2006	1394	1711	318
	2007	1079	1131	53
	2008	1030	1386	357
	2009	1445	1816	371
	2010	1455	1824	369
	2011	1296	1601	305
	2012	1319	1645	326
	2013	1296	1601	305
	2014	1455	1824	369
	2015	1445	1816	371
	2016	1030	1386	357
	2017	1079	1131	53
	2018	1394	1711	318
	2019	1610	2004	394
	2020	1257	1639	383
	2021	1552	1964	411
	2022	1262	1559	297

6. Checking Point and Grade

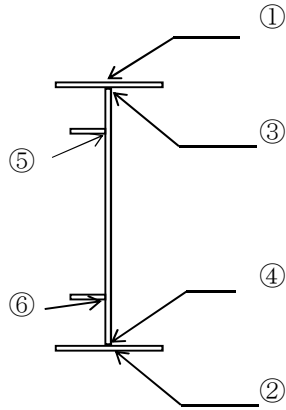
(1) GIRDER



	Checking position	Grade		Position	
(1)	Main Girder Web -Main Girder Flange	D	(100)	Upper Flange	※
(2)	V-Stiffener - Main Girder Web	E	(80)	Web Upper Edge	Checking
(3)	V-Stiffener - Main Girder Upper Flange	E	(80)		
(4)	Main Girder web - Main Girder Lower Flange	D	(100)	Lower Flange	Checking
(5)	V-Stiffener - Main Girder Web	E	(80)	Web Lower Edge	Checking
(6)	V-Stiffener - Main Girder Lower Flange	E	(80)		
(7)	Cross Beam Upper Flange - Main Girder Web	G	(50)	Gasket	Checking
(8)	Cross Beam Lower Flange - Main Girder Web	G	(50)	Gasket	Checking
(11)	Erection Piece - Main Girder Upper Flange	F	(65)	Upper Flange	Checking
(14)	Main Girder Web - H-Stiffener (Upper)	G	(50)	H-Stiffener	Checking
(15)	Main Girder Web - H-Stiffener (Lower)	G	(50)	H-Stiffener	Checking

※Upper Flange(1) shall be checked "F" grade, because (1) and (11) is in the same position.

(2) CROSS BEAM



Position	Grade		Checking Position
① ②	D	(100)	Cross Beam Flange - Web
③ ④	E	(80)	Cross Beam Flange - Web Cross Beam Flange - Main Girdee Web
⑤ ⑥	G	(50)	Cross BeamWeb - H-Stiffener

8-2 Checking of Fatigue Stress for Main Girder

σ_{\max} : Maximum stress (Including the effect of γ_a)
 σ_{\min} : Minimum stress (Including the effect of γ_a)
 σ_d : Stress of Dead load (Including the effect of γ_a)
 $\Delta\sigma_{\max}$: $\sigma_{\max} - \sigma_{\min}$
 C_0 : $2.0E+6 \cdot \Delta\sigma_f^{**m}$
 $\Delta\sigma_f$: $2.0E+6$ Allowable stress
 m : Slope constant
 C_R : Correction coefficient for mean stress
 C_t : Correction factor for t

Structural analysis coefficient Main Girder $\gamma_a = 0.800$

Maximum stress range checking $\Delta\sigma_{\max} \leq \Delta\sigma_{ce} \cdot C_R \cdot C_t$

Stress range cycles checking $D = \sum_i [\sum_j \{n_{ti} / (C_0 \cdot (C_R \cdot C_t)^{**m} / \Delta\sigma_{ij}^{**m})\}] \leq 1$

Steel I Girder G1

node U.FLG-MAX (UpperFlangeStress MAX)

												Stress	
node	Flange	Grade										$\Delta \sigma_{ce} \cdot$	Cycle
	t	σ_{tmax}	σ_{tmin}	σ_d	($\Delta \sigma_f$)	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR \cdot Ct	D
	(mm)	(N/mm ²)								(N/mm ²)	(N/mm ²)		
1	1 nodeRight	22	0.0	0.0	0.0	F (65)	46.0	3	21.0	1.300	1.000	0.0 < 59.8	
1	2 nodeLeft	22	4.9	-19.4	-43.5	F (65)	46.0	3	21.0	1.300	1.000	24.3 < 59.8	
1	2 nodeRight	22	4.9	-19.4	-43.5	F (65)	46.0	3	21.0	1.300	1.000	24.3 < 59.8	
2	3 nodeLeft	22	9.9	-33.9	-54.2	F (65)	46.0	3	21.0	1.300	1.000	43.8 < 59.8	
2	3 nodeRight	22	9.9	-33.9	-54.2	F (65)	46.0	3	21.0	1.300	1.000	43.8 < 59.8	
2	4 nodeLeft	22	14.8	-40.7	-32.1	F (65)	46.0	3	21.0	1.300	1.000	55.5 < 59.8	
2	4 nodeRight	22	14.8	-40.7	-32.1	F (65)	46.0	3	21.0	1.300	1.000	55.5 < 59.8	
3	5 nodeLeft	20	20.6	-27.2	9.7	F (65)	46.0	3	21.0	1.000	1.000	47.8 > 46.0	0.46 < 1
3	5 nodeRight	20	20.6	-27.2	9.7	F (65)	46.0	3	21.0	1.000	1.000	47.8 > 46.0	0.46 < 1
4	6 nodeLeft	31	18.6	-8.5	61.7	F (65)	46.0	3	21.0	1.000	0.948	27.2 < 43.6	
4	6 nodeRight	31	18.6	-8.5	61.7	F (65)	46.0	3	21.0	1.000	0.948	27.2 < 43.6	
4	7 nodeLeft	31	22.1	-4.4	132.9	F (65)	46.0	3	21.0	1.000	0.948	26.5 < 43.6	
4	7 nodeRight	31	22.1	-4.4	132.9	F (65)	46.0	3	21.0	1.000	0.948	26.5 < 43.6	
5	8 nodeLeft	19	16.8	-8.7	76.2	F (65)	46.0	3	21.0	1.000	1.000	25.5 < 46.0	
5	8 nodeRight	19	16.8	-8.7	76.2	F (65)	46.0	3	21.0	1.000	1.000	25.5 < 46.0	
5	9 nodeLeft	19	14.2	-20.6	-10.6	F (65)	46.0	3	21.0	1.223	1.000	34.8 < 56.3	
5	9 nodeRight	19	14.2	-20.6	-10.6	F (65)	46.0	3	21.0	1.223	1.000	34.8 < 56.3	
6	10 nodeLeft	26	10.0	-30.1	-59.4	F (65)	46.0	3	21.0	1.300	0.990	40.1 < 59.2	
6	10 nodeRight	26	10.0	-30.1	-59.4	F (65)	46.0	3	21.0	1.300	0.990	40.1 < 59.2	
6	11 nodeLeft	26	8.2	-41.0	-86.0	F (65)	46.0	3	21.0	1.300	0.990	49.3 < 59.2	
6	11 nodeRight	26	8.2	-41.0	-86.0	F (65)	46.0	3	21.0	1.300	0.990	49.3 < 59.2	
7	12 nodeLeft	26	5.7	-42.4	-95.5	F (65)	46.0	3	21.0	1.300	0.990	48.1 < 59.2	
7	12 nodeRight	26	5.7	-42.4	-95.5	F (65)	46.0	3	21.0	1.300	0.990	48.1 < 59.2	
8	13 nodeLeft	26	8.2	-41.0	-86.0	F (65)	46.0	3	21.0	1.300	0.990	49.3 < 59.2	
8	13 nodeRight	26	8.2	-41.0	-86.0	F (65)	46.0	3	21.0	1.300	0.990	49.3 < 59.2	
8	14 nodeLeft	26	10.0	-30.1	-59.4	F (65)	46.0	3	21.0	1.300	0.990	40.1 < 59.2	
8	14 nodeRight	26	10.0	-30.1	-59.4	F (65)	46.0	3	21.0	1.300	0.990	40.1 < 59.2	
9	15 nodeLeft	19	14.2	-20.6	-10.6	F (65)	46.0	3	21.0	1.223	1.000	34.8 < 56.3	
9	15 nodeRight	19	14.2	-20.6	-10.6	F (65)	46.0	3	21.0	1.223	1.000	34.8 < 56.3	
9	16 nodeLeft	19	16.8	-8.7	76.2	F (65)	46.0	3	21.0	1.000	1.000	25.5 < 46.0	
9	16 nodeRight	19	16.8	-8.7	76.2	F (65)	46.0	3	21.0	1.000	1.000	25.5 < 46.0	
10	17 nodeLeft	31	22.1	-4.4	132.9	F (65)	46.0	3	21.0	1.000	0.948	26.5 < 43.6	
10	17 nodeRight	31	22.1	-4.4	132.9	F (65)	46.0	3	21.0	1.000	0.948	26.5 < 43.6	
10	18 nodeLeft	31	18.6	-8.5	61.7	F (65)	46.0	3	21.0	1.000	0.948	27.2 < 43.6	
10	18 nodeRight	31	18.6	-8.5	61.7	F (65)	46.0	3	21.0	1.000	0.948	27.2 < 43.6	
11	19 nodeLeft	20	20.6	-27.2	9.7	F (65)	46.0	3	21.0	1.000	1.000	47.8 > 46.0	0.46 < 1
11	19 nodeRight	20	20.6	-27.2	9.7	F (65)	46.0	3	21.0	1.000	1.000	47.8 > 46.0	0.46 < 1
12	20 nodeLeft	22	14.8	-40.7	-32.1	F (65)	46.0	3	21.0	1.300	1.000	55.5 < 59.8	
12	20 nodeRight	22	14.8	-40.7	-32.1	F (65)	46.0	3	21.0	1.300	1.000	55.5 < 59.8	
12	21 nodeLeft	22	9.9	-33.9	-54.2	F (65)	46.0	3	21.0	1.300	1.000	43.8 < 59.8	
12	21 nodeRight	22	9.9	-33.9	-54.2	F (65)	46.0	3	21.0	1.300	1.000	43.8 < 59.8	
13	22 nodeLeft	22	4.9	-19.4	-43.5	F (65)	46.0	3	21.0	1.300	1.000	24.3 < 59.8	
13	22 nodeRight	22	4.9	-19.4	-43.5	F (65)	46.0	3	21.0	1.300	1.000	24.3 < 59.8	
13	23 nodeLeft	22	0.0	0.0	0.0	F (65)	46.0	3	21.0	1.300	1.000	0.0 < 59.8	

Steel I Girder G1

node L.FLG-MAX (LowerFlangeStress MAX)

Sec	node	Flange	t	σ_{tmax}	σ_{tmin}	σ_d	Grade	$\Delta \sigma_{cem}$	$\Delta \sigma_{ve}$	CR	Ct	Stress		Cycle	
												$\Delta \sigma_{max}$	$CR \cdot Ct$		
			(mm)	(N/mm ²)			($\Delta \sigma_f$)					(N/mm ²)	(N/mm ²)	D	
1	1	nodeRight	19	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
1	2	nodeLeft	19	20.7	-5.3	46.4	D (100)	84.0	3	39.0	1.000	1.000	26.0	< 84.0	
1	2	nodeRight	19	20.7	-5.3	46.4	D (100)	84.0	3	39.0	1.000	1.000	26.0	< 84.0	
2	3	nodeLeft	19	36.2	-10.5	57.8	D (100)	84.0	3	39.0	1.000	1.000	46.8	< 84.0	
2	3	nodeRight	19	36.2	-10.5	57.8	D (100)	84.0	3	39.0	1.000	1.000	46.8	< 84.0	
2	4	nodeLeft	19	43.4	-15.8	34.2	D (100)	84.0	3	39.0	1.000	1.000	59.3	< 84.0	
2	4	nodeRight	19	43.4	-15.8	34.2	D (100)	84.0	3	39.0	1.000	1.000	59.3	< 84.0	
3	5	nodeLeft	23	25.5	-19.4	-9.1	D (100)	84.0	3	39.0	1.066	1.000	44.9	< 89.6	
3	5	nodeRight	23	25.5	-19.4	-9.1	D (100)	84.0	3	39.0	1.066	1.000	44.9	< 89.6	
4	6	nodeLeft	39	7.5	-16.4	-54.2	D (100)	84.0	3	39.0	1.300	0.895	23.9	< 97.7	
4	6	nodeRight	39	7.5	-16.4	-54.2	D (100)	84.0	3	39.0	1.300	0.895	23.9	< 97.7	
4	7	nodeLeft	39	3.9	-19.5	-116.8	D (100)	84.0	3	39.0	1.300	0.895	23.3	< 97.7	
4	7	nodeRight	39	3.9	-19.5	-116.8	D (100)	84.0	3	39.0	1.300	0.895	23.3	< 97.7	
5	8	nodeLeft	23	8.0	-15.4	-70.0	D (100)	84.0	3	39.0	1.300	1.000	23.4	<109.2	
5	8	nodeRight	23	8.0	-15.4	-70.0	D (100)	84.0	3	39.0	1.300	1.000	23.4	<109.2	
5	9	nodeLeft	23	18.9	-13.1	9.8	D (100)	84.0	3	39.0	1.000	1.000	32.0	< 84.0	
5	9	nodeRight	23	18.9	-13.1	9.8	D (100)	84.0	3	39.0	1.000	1.000	32.0	< 84.0	
6	10	nodeLeft	19	34.7	-11.6	68.7	D (100)	84.0	3	39.0	1.000	1.000	46.3	< 84.0	
6	10	nodeRight	19	34.7	-11.6	68.7	D (100)	84.0	3	39.0	1.000	1.000	46.3	< 84.0	
6	11	nodeLeft	19	47.4	-9.5	99.3	D (100)	84.0	3	39.0	1.000	1.000	56.9	< 84.0	
6	11	nodeRight	19	47.4	-9.5	99.3	D (100)	84.0	3	39.0	1.000	1.000	56.9	< 84.0	
7	12	nodeLeft	21	46.9	-6.3	105.6	D (100)	84.0	3	39.0	1.000	1.000	53.2	< 84.0	
7	12	nodeRight	21	46.9	-6.3	105.6	D (100)	84.0	3	39.0	1.000	1.000	53.2	< 84.0	
8	13	nodeLeft	19	47.4	-9.5	99.3	D (100)	84.0	3	39.0	1.000	1.000	56.9	< 84.0	
8	13	nodeRight	19	47.4	-9.5	99.3	D (100)	84.0	3	39.0	1.000	1.000	56.9	< 84.0	
8	14	nodeLeft	19	34.7	-11.6	68.7	D (100)	84.0	3	39.0	1.000	1.000	46.3	< 84.0	
8	14	nodeRight	19	34.7	-11.6	68.7	D (100)	84.0	3	39.0	1.000	1.000	46.3	< 84.0	
9	15	nodeLeft	23	18.9	-13.1	9.8	D (100)	84.0	3	39.0	1.000	1.000	32.0	< 84.0	
9	15	nodeRight	23	18.9	-13.1	9.8	D (100)	84.0	3	39.0	1.000	1.000	32.0	< 84.0	
9	16	nodeLeft	23	8.0	-15.4	-70.0	D (100)	84.0	3	39.0	1.300	1.000	23.4	<109.2	
9	16	nodeRight	23	8.0	-15.4	-70.0	D (100)	84.0	3	39.0	1.300	1.000	23.4	<109.2	
10	17	nodeLeft	39	3.9	-19.5	-116.8	D (100)	84.0	3	39.0	1.300	0.895	23.3	< 97.7	
10	17	nodeRight	39	3.9	-19.5	-116.8	D (100)	84.0	3	39.0	1.300	0.895	23.3	< 97.7	
10	18	nodeLeft	39	7.5	-16.4	-54.2	D (100)	84.0	3	39.0	1.300	0.895	23.9	< 97.7	
10	18	nodeRight	39	7.5	-16.4	-54.2	D (100)	84.0	3	39.0	1.300	0.895	23.9	< 97.7	
11	19	nodeLeft	23	25.5	-19.4	-9.1	D (100)	84.0	3	39.0	1.066	1.000	44.9	< 89.6	
11	19	nodeRight	23	25.5	-19.4	-9.1	D (100)	84.0	3	39.0	1.066	1.000	44.9	< 89.6	
12	20	nodeLeft	19	43.4	-15.8	34.2	D (100)	84.0	3	39.0	1.000	1.000	59.3	< 84.0	
12	20	nodeRight	19	43.4	-15.8	34.2	D (100)	84.0	3	39.0	1.000	1.000	59.3	< 84.0	
12	21	nodeLeft	19	36.2	-10.5	57.8	D (100)	84.0	3	39.0	1.000	1.000	46.8	< 84.0	
12	21	nodeRight	19	36.2	-10.5	57.8	D (100)	84.0	3	39.0	1.000	1.000	46.8	< 84.0	
13	22	nodeLeft	19	20.7	-5.3	46.4	D (100)	84.0	3	39.0	1.000	1.000	26.0	< 84.0	
13	22	nodeRight	19	20.7	-5.3	46.4	D (100)	84.0	3	39.0	1.000	1.000	26.0	< 84.0	
13	23	nodeLeft	19	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	

Steel I Girder G1

node WEB-U-1 (WebUpper edge) WEB - 1

Sec	node	Web	h	t	Grade					Stress						
					σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D
					(N/mm ²)					(N/mm ²)						
1	1	nodeRight	2400	22	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
1	2	nodeLeft	2400	22	0	4.8	-19.0	-42.7	E(80)	62.0	3	29.0	1.300	1.000	23.9	< 80.6
1	2	nodeRight	2400	22	0	4.8	-19.0	-42.7	E(80)	62.0	3	29.0	1.300	1.000	23.9	< 80.6
2	3	nodeLeft	2400	22	0	9.7	-33.3	-53.2	E(80)	62.0	3	29.0	1.300	1.000	43.0	< 80.6
2	3	nodeRight	2400	22	0	9.7	-33.3	-53.2	E(80)	62.0	3	29.0	1.300	1.000	43.0	< 80.6
2	4	nodeLeft	2400	22	0	14.6	-39.9	-31.5	E(80)	62.0	3	29.0	1.300	1.000	54.5	< 80.6
2	4	nodeRight	2400	22	0	14.6	-39.9	-31.5	E(80)	62.0	3	29.0	1.300	1.000	54.5	< 80.6
3	5	nodeLeft	2400	20	0	20.3	-26.7	9.6	E(80)	62.0	3	29.0	1.000	1.000	47.0	< 62.0
3	5	nodeRight	2400	20	0	20.3	-26.7	9.6	E(80)	62.0	3	29.0	1.000	1.000	47.0	< 62.0
4	6	nodeLeft	2400	31	0	18.2	-8.3	60.2	E(80)	62.0	3	29.0	1.000	0.948	26.5	< 58.8
4	6	nodeRight	2400	31	0	18.2	-8.3	60.2	E(80)	62.0	3	29.0	1.000	0.948	26.5	< 58.8
4	7	nodeLeft	2400	31	0	21.6	-4.3	129.7	E(80)	62.0	3	29.0	1.000	0.948	25.9	< 58.8
4	7	nodeRight	2400	31	0	21.6	-4.3	129.7	E(80)	62.0	3	29.0	1.000	0.948	25.9	< 58.8
5	8	nodeLeft	2400	19	0	16.5	-8.6	75.1	E(80)	62.0	3	29.0	1.000	1.000	25.1	< 62.0
5	8	nodeRight	2400	19	0	16.5	-8.6	75.1	E(80)	62.0	3	29.0	1.000	1.000	25.1	< 62.0
5	9	nodeLeft	2400	19	0	14.0	-20.3	-10.5	E(80)	62.0	3	29.0	1.223	1.000	34.3	< 75.8
5	9	nodeRight	2400	19	0	14.0	-20.3	-10.5	E(80)	62.0	3	29.0	1.223	1.000	34.3	< 75.8
6	10	nodeLeft	2400	26	0	9.8	-29.4	-58.0	E(80)	62.0	3	29.0	1.300	0.990	39.2	< 79.8
6	10	nodeRight	2400	26	0	9.8	-29.4	-58.0	E(80)	62.0	3	29.0	1.300	0.990	39.2	< 79.8
6	11	nodeLeft	2400	26	0	8.0	-40.1	-84.0	E(80)	62.0	3	29.0	1.300	0.990	48.1	< 79.8
6	11	nodeRight	2400	26	0	8.0	-40.1	-84.0	E(80)	62.0	3	29.0	1.300	0.990	48.1	< 79.8
7	12	nodeLeft	2400	26	0	5.6	-41.5	-93.3	E(80)	62.0	3	29.0	1.300	0.990	47.0	< 79.8
7	12	nodeRight	2400	26	0	5.6	-41.5	-93.3	E(80)	62.0	3	29.0	1.300	0.990	47.0	< 79.8
8	13	nodeLeft	2400	26	0	8.0	-40.1	-84.0	E(80)	62.0	3	29.0	1.300	0.990	48.1	< 79.8
8	13	nodeRight	2400	26	0	8.0	-40.1	-84.0	E(80)	62.0	3	29.0	1.300	0.990	48.1	< 79.8
8	14	nodeLeft	2400	26	0	9.8	-29.4	-58.0	E(80)	62.0	3	29.0	1.300	0.990	39.2	< 79.8
8	14	nodeRight	2400	26	0	9.8	-29.4	-58.0	E(80)	62.0	3	29.0	1.300	0.990	39.2	< 79.8
9	15	nodeLeft	2400	19	0	14.0	-20.3	-10.5	E(80)	62.0	3	29.0	1.223	1.000	34.3	< 75.8
9	15	nodeRight	2400	19	0	14.0	-20.3	-10.5	E(80)	62.0	3	29.0	1.223	1.000	34.3	< 75.8
9	16	nodeLeft	2400	19	0	16.5	-8.6	75.1	E(80)	62.0	3	29.0	1.000	1.000	25.1	< 62.0
9	16	nodeRight	2400	19	0	16.5	-8.6	75.1	E(80)	62.0	3	29.0	1.000	1.000	25.1	< 62.0
10	17	nodeLeft	2400	31	0	21.6	-4.3	129.7	E(80)	62.0	3	29.0	1.000	0.948	25.9	< 58.8
10	17	nodeRight	2400	31	0	21.6	-4.3	129.7	E(80)	62.0	3	29.0	1.000	0.948	25.9	< 58.8
10	18	nodeLeft	2400	31	0	18.2	-8.3	60.2	E(80)	62.0	3	29.0	1.000	0.948	26.5	< 58.8
10	18	nodeRight	2400	31	0	18.2	-8.3	60.2	E(80)	62.0	3	29.0	1.000	0.948	26.5	< 58.8
11	19	nodeLeft	2400	20	0	20.3	-26.7	9.6	E(80)	62.0	3	29.0	1.000	1.000	47.0	< 62.0
11	19	nodeRight	2400	20	0	20.3	-26.7	9.6	E(80)	62.0	3	29.0	1.000	1.000	47.0	< 62.0
12	20	nodeLeft	2400	22	0	14.6	-39.9	-31.5	E(80)	62.0	3	29.0	1.300	1.000	54.5	< 80.6
12	20	nodeRight	2400	22	0	14.6	-39.9	-31.5	E(80)	62.0	3	29.0	1.300	1.000	54.5	< 80.6
12	21	nodeLeft	2400	22	0	9.7	-33.3	-53.2	E(80)	62.0	3	29.0	1.300	1.000	43.0	< 80.6
12	21	nodeRight	2400	22	0	9.7	-33.3	-53.2	E(80)	62.0	3	29.0	1.300	1.000	43.0	< 80.6
13	22	nodeLeft	2400	22	0	4.8	-19.0	-42.7	E(80)	62.0	3	29.0	1.300	1.000	23.9	< 80.6
13	22	nodeRight	2400	22	0	4.8	-19.0	-42.7	E(80)	62.0	3	29.0	1.300	1.000	23.9	< 80.6
13	23	nodeLeft	2400	22	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6

Steel I Girder G1

node WEB-L-1 (WebLower edge) WEB - 1

Sec	node	Web	h	t	Grade				Stress							
					σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D
					(N/mm ²)				(N/mm ²)							
1	1	nodeRight	2400	19	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
1	2	nodeLeft	2400	19	0	20.4	-5.2	45.7	E(80)	62.0	3	29.0	1.000	1.000	25.6	< 62.0
1	2	nodeRight	2400	19	0	20.4	-5.2	45.7	E(80)	62.0	3	29.0	1.000	1.000	25.6	< 62.0
2	3	nodeLeft	2400	19	0	35.7	-10.4	56.9	E(80)	62.0	3	29.0	1.000	1.000	46.0	< 62.0
2	3	nodeRight	2400	19	0	35.7	-10.4	56.9	E(80)	62.0	3	29.0	1.000	1.000	46.0	< 62.0
2	4	nodeLeft	2400	19	0	42.8	-15.6	33.7	E(80)	62.0	3	29.0	1.000	1.000	58.4	< 62.0
2	4	nodeRight	2400	19	0	42.8	-15.6	33.7	E(80)	62.0	3	29.0	1.000	1.000	58.4	< 62.0
3	5	nodeLeft	2400	23	0	25.0	-19.0	-8.9	E(80)	62.0	3	29.0	1.066	1.000	44.0	< 66.1
3	5	nodeRight	2400	23	0	25.0	-19.0	-8.9	E(80)	62.0	3	29.0	1.066	1.000	44.0	< 66.1
4	6	nodeLeft	2400	39	0	7.3	-15.8	-52.4	E(80)	62.0	3	29.0	1.300	0.895	23.1	< 72.1
4	6	nodeRight	2400	39	0	7.3	-15.8	-52.4	E(80)	62.0	3	29.0	1.300	0.895	23.1	< 72.1
4	7	nodeLeft	2400	39	0	3.7	-18.8	-112.8	E(80)	62.0	3	29.0	1.300	0.895	22.5	< 72.1
4	7	nodeRight	2400	39	0	3.7	-18.8	-112.8	E(80)	62.0	3	29.0	1.300	0.895	22.5	< 72.1
5	8	nodeLeft	2400	23	0	7.9	-15.1	-68.6	E(80)	62.0	3	29.0	1.300	1.000	23.0	< 80.6
5	8	nodeRight	2400	23	0	7.9	-15.1	-68.6	E(80)	62.0	3	29.0	1.300	1.000	23.0	< 80.6
5	9	nodeLeft	2400	23	0	18.5	-12.8	9.6	E(80)	62.0	3	29.0	1.000	1.000	31.3	< 62.0
5	9	nodeRight	2400	23	0	18.5	-12.8	9.6	E(80)	62.0	3	29.0	1.000	1.000	31.3	< 62.0
6	10	nodeLeft	2400	19	0	34.2	-11.4	67.7	E(80)	62.0	3	29.0	1.000	1.000	45.7	< 62.0
6	10	nodeRight	2400	19	0	34.2	-11.4	67.7	E(80)	62.0	3	29.0	1.000	1.000	45.7	< 62.0
6	11	nodeLeft	2400	19	0	46.7	-9.4	97.9	E(80)	62.0	3	29.0	1.000	1.000	56.1	< 62.0
6	11	nodeRight	2400	19	0	46.7	-9.4	97.9	E(80)	62.0	3	29.0	1.000	1.000	56.1	< 62.0
7	12	nodeLeft	2400	21	0	46.2	-6.2	103.9	E(80)	62.0	3	29.0	1.000	1.000	52.4	< 62.0
7	12	nodeRight	2400	21	0	46.2	-6.2	103.9	E(80)	62.0	3	29.0	1.000	1.000	52.4	< 62.0
8	13	nodeLeft	2400	19	0	46.7	-9.4	97.9	E(80)	62.0	3	29.0	1.000	1.000	56.1	< 62.0
8	13	nodeRight	2400	19	0	46.7	-9.4	97.9	E(80)	62.0	3	29.0	1.000	1.000	56.1	< 62.0
8	14	nodeLeft	2400	19	0	34.2	-11.4	67.7	E(80)	62.0	3	29.0	1.000	1.000	45.7	< 62.0
8	14	nodeRight	2400	19	0	34.2	-11.4	67.7	E(80)	62.0	3	29.0	1.000	1.000	45.7	< 62.0
9	15	nodeLeft	2400	23	0	18.5	-12.8	9.6	E(80)	62.0	3	29.0	1.000	1.000	31.3	< 62.0
9	15	nodeRight	2400	23	0	18.5	-12.8	9.6	E(80)	62.0	3	29.0	1.000	1.000	31.3	< 62.0
9	16	nodeLeft	2400	23	0	7.9	-15.1	-68.6	E(80)	62.0	3	29.0	1.300	1.000	23.0	< 80.6
9	16	nodeRight	2400	23	0	7.9	-15.1	-68.6	E(80)	62.0	3	29.0	1.300	1.000	23.0	< 80.6
10	17	nodeLeft	2400	39	0	3.7	-18.8	-112.8	E(80)	62.0	3	29.0	1.300	0.895	22.5	< 72.1
10	17	nodeRight	2400	39	0	3.7	-18.8	-112.8	E(80)	62.0	3	29.0	1.300	0.895	22.5	< 72.1
10	18	nodeLeft	2400	39	0	7.3	-15.8	-52.4	E(80)	62.0	3	29.0	1.300	0.895	23.1	< 72.1
10	18	nodeRight	2400	39	0	7.3	-15.8	-52.4	E(80)	62.0	3	29.0	1.300	0.895	23.1	< 72.1
11	19	nodeLeft	2400	23	0	25.0	-19.0	-8.9	E(80)	62.0	3	29.0	1.066	1.000	44.0	< 66.1
11	19	nodeRight	2400	23	0	25.0	-19.0	-8.9	E(80)	62.0	3	29.0	1.066	1.000	44.0	< 66.1
12	20	nodeLeft	2400	19	0	42.8	-15.6	33.7	E(80)	62.0	3	29.0	1.000	1.000	58.4	< 62.0
12	20	nodeRight	2400	19	0	42.8	-15.6	33.7	E(80)	62.0	3	29.0	1.000	1.000	58.4	< 62.0
12	21	nodeLeft	2400	19	0	35.7	-10.4	56.9	E(80)	62.0	3	29.0	1.000	1.000	46.0	< 62.0
12	21	nodeRight	2400	19	0	35.7	-10.4	56.9	E(80)	62.0	3	29.0	1.000	1.000	46.0	< 62.0
13	22	nodeLeft	2400	19	0	20.4	-5.2	45.7	E(80)	62.0	3	29.0	1.000	1.000	25.6	< 62.0
13	22	nodeRight	2400	19	0	20.4	-5.2	45.7	E(80)	62.0	3	29.0	1.000	1.000	25.6	< 62.0
13	23	nodeLeft	2400	19	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6

Steel I Girder G1

node HSTIFF-1 (WebH-Stiffener) WEB - 1

Sec	node	Web	h	t	σ_{tmax}	σ_{tmin}	σ_d	Grade	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	Stress	
															$\Delta \sigma_{ce} \cdot Cycle$	$\Delta \sigma_{max} CR \cdot Ct$
															(N/mm^2)	
1	1	nodeRight	2400	12	480	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
1	2	nodeLeft	2400	12	480	2.8	-11.1	-25.0	G(50)	32.0	3	15.0	1.300	1.000	14.0	< 41.6
1	2	nodeRight	2400	12	480	2.8	-11.1	-25.0	G(50)	32.0	3	15.0	1.300	1.000	14.0	< 41.6
2	3	nodeLeft	2400	12	480	5.7	-19.5	-31.1	G(50)	32.0	3	15.0	1.300	1.000	25.2	< 41.6
2	3	nodeRight	2400	12	480	5.7	-19.5	-31.1	G(50)	32.0	3	15.0	1.300	1.000	25.2	< 41.6
2	4	nodeLeft	2400	12	480	8.5	-23.4	-18.5	G(50)	32.0	3	15.0	1.300	1.000	31.9	< 41.6
2	4	nodeRight	2400	12	480	8.5	-23.4	-18.5	G(50)	32.0	3	15.0	1.300	1.000	31.9	< 41.6
3	5	nodeLeft	2400	12	480	12.4	-16.4	5.9	G(50)	32.0	3	15.0	1.000	1.000	28.8	< 32.0
3	5	nodeRight	2400	12	480	12.4	-16.4	5.9	G(50)	32.0	3	15.0	1.000	1.000	28.8	< 32.0
4	6	nodeLeft	2400	12	480	4.1	-9.0	-29.9	G(50)	32.0	3	15.0	1.300	1.000	13.1	< 41.6
4	6	nodeRight	2400	12	480	4.1	-9.0	-29.9	G(50)	32.0	3	15.0	1.300	1.000	13.1	< 41.6
4	7	nodeLeft	2400	12	480	2.1	-10.7	-64.3	G(50)	32.0	3	15.0	1.300	1.000	12.8	< 41.6
4	7	nodeRight	2400	12	480	2.1	-10.7	-64.3	G(50)	32.0	3	15.0	1.300	1.000	12.8	< 41.6
5	8	nodeLeft	2400	12	480	4.6	-8.8	-39.9	G(50)	32.0	3	15.0	1.300	1.000	13.4	< 41.6
5	8	nodeRight	2400	12	480	4.6	-8.8	-39.9	G(50)	32.0	3	15.0	1.300	1.000	13.4	< 41.6
5	9	nodeLeft	2400	12	480	8.7	-12.5	-6.5	G(50)	32.0	3	15.0	1.223	1.000	21.2	< 39.1
5	9	nodeRight	2400	12	480	8.7	-12.5	-6.5	G(50)	32.0	3	15.0	1.223	1.000	21.2	< 39.1
6	10	nodeLeft	2400	12	480	5.6	-16.6	-32.9	G(50)	32.0	3	15.0	1.300	1.000	22.2	< 41.6
6	10	nodeRight	2400	12	480	5.6	-16.6	-32.9	G(50)	32.0	3	15.0	1.300	1.000	22.2	< 41.6
6	11	nodeLeft	2400	12	480	4.6	-22.7	-47.6	G(50)	32.0	3	15.0	1.300	1.000	27.3	< 41.6
6	11	nodeRight	2400	12	480	4.6	-22.7	-47.6	G(50)	32.0	3	15.0	1.300	1.000	27.3	< 41.6
7	12	nodeLeft	2400	12	480	3.2	-24.0	-53.9	G(50)	32.0	3	15.0	1.300	1.000	27.2	< 41.6
7	12	nodeRight	2400	12	480	3.2	-24.0	-53.9	G(50)	32.0	3	15.0	1.300	1.000	27.2	< 41.6
8	13	nodeLeft	2400	12	480	4.6	-22.7	-47.6	G(50)	32.0	3	15.0	1.300	1.000	27.3	< 41.6
8	13	nodeRight	2400	12	480	4.6	-22.7	-47.6	G(50)	32.0	3	15.0	1.300	1.000	27.3	< 41.6
8	14	nodeLeft	2400	12	480	5.6	-16.6	-32.9	G(50)	32.0	3	15.0	1.300	1.000	22.2	< 41.6
8	14	nodeRight	2400	12	480	5.6	-16.6	-32.9	G(50)	32.0	3	15.0	1.300	1.000	22.2	< 41.6
9	15	nodeLeft	2400	12	480	8.7	-12.5	-6.5	G(50)	32.0	3	15.0	1.223	1.000	21.2	< 39.1
9	15	nodeRight	2400	12	480	8.7	-12.5	-6.5	G(50)	32.0	3	15.0	1.223	1.000	21.2	< 39.1
9	16	nodeLeft	2400	12	480	4.6	-8.8	-39.9	G(50)	32.0	3	15.0	1.300	1.000	13.4	< 41.6
9	16	nodeRight	2400	12	480	4.6	-8.8	-39.9	G(50)	32.0	3	15.0	1.300	1.000	13.4	< 41.6
10	17	nodeLeft	2400	12	480	2.1	-10.7	-64.3	G(50)	32.0	3	15.0	1.300	1.000	12.8	< 41.6
10	17	nodeRight	2400	12	480	2.1	-10.7	-64.3	G(50)	32.0	3	15.0	1.300	1.000	12.8	< 41.6
10	18	nodeLeft	2400	12	480	4.1	-9.0	-29.9	G(50)	32.0	3	15.0	1.300	1.000	13.1	< 41.6
10	18	nodeRight	2400	12	480	4.1	-9.0	-29.9	G(50)	32.0	3	15.0	1.300	1.000	13.1	< 41.6
11	19	nodeLeft	2400	12	480	12.4	-16.4	5.9	G(50)	32.0	3	15.0	1.000	1.000	28.8	< 32.0
11	19	nodeRight	2400	12	480	12.4	-16.4	5.9	G(50)	32.0	3	15.0	1.000	1.000	28.8	< 32.0
12	20	nodeLeft	2400	12	480	8.5	-23.4	-18.5	G(50)	32.0	3	15.0	1.300	1.000	31.9	< 41.6
12	20	nodeRight	2400	12	480	8.5	-23.4	-18.5	G(50)	32.0	3	15.0	1.300	1.000	31.9	< 41.6
12	21	nodeLeft	2400	12	480	5.7	-19.5	-31.1	G(50)	32.0	3	15.0	1.300	1.000	25.2	< 41.6
12	21	nodeRight	2400	12	480	5.7	-19.5	-31.1	G(50)	32.0	3	15.0	1.300	1.000	25.2	< 41.6
13	22	nodeLeft	2400	12	480	2.8	-11.1	-25.0	G(50)	32.0	3	15.0	1.300	1.000	14.0	< 41.6
13	22	nodeRight	2400	12	480	2.8	-11.1	-25.0	G(50)	32.0	3	15.0	1.300	1.000	14.0	< 41.6
13	23	nodeLeft	2400	12	480	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6

Steel I Girder G1

node POINT-U-1 (WebUpper) WEB - 1

Sec	node	Web	h	t	σ_{tmax}	σ_{tmin}	σ_d	Grade	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D	Stress
																		$\Delta \sigma_{ce} \cdot \text{Cycle}$
																	(N/mm ²)	
1	1	nodeRight	2400	12	300	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6	
1	2	nodeLeft	2400	12	300	3.6	-14.1	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.7	<	41.6	
1	2	nodeRight	2400	12	300	3.6	-14.1	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.7	<	41.6	
2	3	nodeLeft	2400	12	300	7.2	-24.7	-39.4	G(50)	32.0	3	15.0	1.300	1.000	31.9	<	41.6	
2	3	nodeRight	2400	12	300	7.2	-24.7	-39.4	G(50)	32.0	3	15.0	1.300	1.000	31.9	<	41.6	
2	4	nodeLeft	2400	12	300	10.8	-29.6	-23.3	G(50)	32.0	3	15.0	1.300	1.000	40.4	<	41.6	
2	4	nodeRight	2400	12	300	10.8	-29.6	-23.3	G(50)	32.0	3	15.0	1.300	1.000	40.4	<	41.6	
3	5	nodeLeft	2400	12	300	15.4	-20.3	7.3	G(50)	32.0	3	15.0	1.000	1.000	35.7	>	32.0	0.41<1
3	5	nodeRight	2400	12	300	15.4	-20.3	7.3	G(50)	32.0	3	15.0	1.000	1.000	35.7	>	32.0	0.41<1
4	6	nodeLeft	2400	12	300	13.9	-6.4	46.2	G(50)	32.0	3	15.0	1.000	1.000	20.3	<	32.0	
4	6	nodeRight	2400	12	300	13.9	-6.4	46.2	G(50)	32.0	3	15.0	1.000	1.000	20.3	<	32.0	
4	7	nodeLeft	2400	12	300	16.6	-3.3	99.4	G(50)	32.0	3	15.0	1.000	1.000	19.9	<	32.0	
4	7	nodeRight	2400	12	300	16.6	-3.3	99.4	G(50)	32.0	3	15.0	1.000	1.000	19.9	<	32.0	
5	8	nodeLeft	2400	12	300	12.6	-6.5	57.1	G(50)	32.0	3	15.0	1.000	1.000	19.1	<	32.0	
5	8	nodeRight	2400	12	300	12.6	-6.5	57.1	G(50)	32.0	3	15.0	1.000	1.000	19.1	<	32.0	
5	9	nodeLeft	2400	12	300	10.7	-15.4	-8.0	G(50)	32.0	3	15.0	1.223	1.000	26.1	<	39.1	
5	9	nodeRight	2400	12	300	10.7	-15.4	-8.0	G(50)	32.0	3	15.0	1.223	1.000	26.1	<	39.1	
6	10	nodeLeft	2400	12	300	7.2	-21.4	-42.3	G(50)	32.0	3	15.0	1.300	1.000	28.6	<	41.6	
6	10	nodeRight	2400	12	300	7.2	-21.4	-42.3	G(50)	32.0	3	15.0	1.300	1.000	28.6	<	41.6	
6	11	nodeLeft	2400	12	300	5.9	-29.2	-61.2	G(50)	32.0	3	15.0	1.300	1.000	35.1	<	41.6	
6	11	nodeRight	2400	12	300	5.9	-29.2	-61.2	G(50)	32.0	3	15.0	1.300	1.000	35.1	<	41.6	
7	12	nodeLeft	2400	12	300	4.1	-30.5	-68.7	G(50)	32.0	3	15.0	1.300	1.000	34.6	<	41.6	
7	12	nodeRight	2400	12	300	4.1	-30.5	-68.7	G(50)	32.0	3	15.0	1.300	1.000	34.6	<	41.6	
8	13	nodeLeft	2400	12	300	5.9	-29.2	-61.2	G(50)	32.0	3	15.0	1.300	1.000	35.1	<	41.6	
8	13	nodeRight	2400	12	300	5.9	-29.2	-61.2	G(50)	32.0	3	15.0	1.300	1.000	35.1	<	41.6	
8	14	nodeLeft	2400	12	300	7.2	-21.4	-42.3	G(50)	32.0	3	15.0	1.300	1.000	28.6	<	41.6	
8	14	nodeRight	2400	12	300	7.2	-21.4	-42.3	G(50)	32.0	3	15.0	1.300	1.000	28.6	<	41.6	
9	15	nodeLeft	2400	12	300	10.7	-15.4	-8.0	G(50)	32.0	3	15.0	1.223	1.000	26.1	<	39.1	
9	15	nodeRight	2400	12	300	10.7	-15.4	-8.0	G(50)	32.0	3	15.0	1.223	1.000	26.1	<	39.1	
9	16	nodeLeft	2400	12	300	12.6	-6.5	57.1	G(50)	32.0	3	15.0	1.000	1.000	19.1	<	32.0	
9	16	nodeRight	2400	12	300	12.6	-6.5	57.1	G(50)	32.0	3	15.0	1.000	1.000	19.1	<	32.0	
10	17	nodeLeft	2400	12	300	16.6	-3.3	99.4	G(50)	32.0	3	15.0	1.000	1.000	19.9	<	32.0	
10	17	nodeRight	2400	12	300	16.6	-3.3	99.4	G(50)	32.0	3	15.0	1.000	1.000	19.9	<	32.0	
10	18	nodeLeft	2400	12	300	13.9	-6.4	46.2	G(50)	32.0	3	15.0	1.000	1.000	20.3	<	32.0	
10	18	nodeRight	2400	12	300	13.9	-6.4	46.2	G(50)	32.0	3	15.0	1.000	1.000	20.3	<	32.0	
11	19	nodeLeft	2400	12	300	15.4	-20.3	7.3	G(50)	32.0	3	15.0	1.000	1.000	35.7	>	32.0	0.41<1
11	19	nodeRight	2400	12	300	15.4	-20.3	7.3	G(50)	32.0	3	15.0	1.000	1.000	35.7	>	32.0	0.41<1
12	20	nodeLeft	2400	12	300	10.8	-29.6	-23.3	G(50)	32.0	3	15.0	1.300	1.000	40.4	<	41.6	
12	20	nodeRight	2400	12	300	10.8	-29.6	-23.3	G(50)	32.0	3	15.0	1.300	1.000	40.4	<	41.6	
12	21	nodeLeft	2400	12	300	7.2	-24.7	-39.4	G(50)	32.0	3	15.0	1.300	1.000	31.9	<	41.6	
12	21	nodeRight	2400	12	300	7.2	-24.7	-39.4	G(50)	32.0	3	15.0	1.300	1.000	31.9	<	41.6	
13	22	nodeLeft	2400	12	300	3.6	-14.1	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.7	<	41.6	
13	22	nodeRight	2400	12	300	3.6	-14.1	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.7	<	41.6	
13	23	nodeLeft	2400	12	300	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6	

Steel I Girder G1

node POINT-L-1 (WebLower) WEB - 1

Sec	node	Web	h	t	Grade					Stress							
					σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D	
					(N/mm ²)					(N/mm ²)							
1	1	nodeRight	2400	12	400	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6	
1	2	nodeLeft	2400	12	400	13.8	-3.5	31.0	G(50)	32.0	3	15.0	1.000	1.000	17.3	< 32.0	
1	2	nodeRight	2400	12	400	13.8	-3.5	31.0	G(50)	32.0	3	15.0	1.000	1.000	17.3	< 32.0	
2	3	nodeLeft	2400	12	400	24.2	-7.0	38.6	G(50)	32.0	3	15.0	1.000	1.000	31.2	< 32.0	
2	3	nodeRight	2400	12	400	24.2	-7.0	38.6	G(50)	32.0	3	15.0	1.000	1.000	31.2	< 32.0	
2	4	nodeLeft	2400	12	400	29.0	-10.6	22.9	G(50)	32.0	3	15.0	1.000	1.000	39.5	> 32.0	0.57<1
2	4	nodeRight	2400	12	400	29.0	-10.6	22.9	G(50)	32.0	3	15.0	1.000	1.000	39.5	> 32.0	0.57<1
3	5	nodeLeft	2400	12	400	16.4	-12.4	-5.9	G(50)	32.0	3	15.0	1.066	1.000	28.8	< 34.1	
3	5	nodeRight	2400	12	400	16.4	-12.4	-5.9	G(50)	32.0	3	15.0	1.066	1.000	28.8	< 34.1	
4	6	nodeLeft	2400	12	400	4.7	-10.1	-33.6	G(50)	32.0	3	15.0	1.300	1.000	14.8	< 41.6	
4	6	nodeRight	2400	12	400	4.7	-10.1	-33.6	G(50)	32.0	3	15.0	1.300	1.000	14.8	< 41.6	
4	7	nodeLeft	2400	12	400	2.4	-12.1	-72.4	G(50)	32.0	3	15.0	1.300	1.000	14.5	< 41.6	
4	7	nodeRight	2400	12	400	2.4	-12.1	-72.4	G(50)	32.0	3	15.0	1.300	1.000	14.5	< 41.6	
5	8	nodeLeft	2400	12	400	5.1	-9.8	-44.7	G(50)	32.0	3	15.0	1.300	1.000	15.0	< 41.6	
5	8	nodeRight	2400	12	400	5.1	-9.8	-44.7	G(50)	32.0	3	15.0	1.300	1.000	15.0	< 41.6	
5	9	nodeLeft	2400	12	400	12.0	-8.3	6.2	G(50)	32.0	3	15.0	1.000	1.000	20.4	< 32.0	
5	9	nodeRight	2400	12	400	12.0	-8.3	6.2	G(50)	32.0	3	15.0	1.000	1.000	20.4	< 32.0	
6	10	nodeLeft	2400	12	400	23.6	-7.9	46.7	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0	
6	10	nodeRight	2400	12	400	23.6	-7.9	46.7	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0	
6	11	nodeLeft	2400	12	400	32.3	-6.5	67.6	G(50)	32.0	3	15.0	1.000	1.000	38.7	> 32.0	0.53<1
6	11	nodeRight	2400	12	400	32.3	-6.5	67.6	G(50)	32.0	3	15.0	1.000	1.000	38.7	> 32.0	0.53<1
7	12	nodeLeft	2400	12	400	31.6	-4.2	71.0	G(50)	32.0	3	15.0	1.000	1.000	35.8	> 32.0	0.42<1
7	12	nodeRight	2400	12	400	31.6	-4.2	71.0	G(50)	32.0	3	15.0	1.000	1.000	35.8	> 32.0	0.42<1
8	13	nodeLeft	2400	12	400	32.3	-6.5	67.6	G(50)	32.0	3	15.0	1.000	1.000	38.7	> 32.0	0.53<1
8	13	nodeRight	2400	12	400	32.3	-6.5	67.6	G(50)	32.0	3	15.0	1.000	1.000	38.7	> 32.0	0.53<1
8	14	nodeLeft	2400	12	400	23.6	-7.9	46.7	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0	
8	14	nodeRight	2400	12	400	23.6	-7.9	46.7	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0	
9	15	nodeLeft	2400	12	400	12.0	-8.3	6.2	G(50)	32.0	3	15.0	1.000	1.000	20.4	< 32.0	
9	15	nodeRight	2400	12	400	12.0	-8.3	6.2	G(50)	32.0	3	15.0	1.000	1.000	20.4	< 32.0	
9	16	nodeLeft	2400	12	400	5.1	-9.8	-44.7	G(50)	32.0	3	15.0	1.300	1.000	15.0	< 41.6	
9	16	nodeRight	2400	12	400	5.1	-9.8	-44.7	G(50)	32.0	3	15.0	1.300	1.000	15.0	< 41.6	
10	17	nodeLeft	2400	12	400	2.4	-12.1	-72.4	G(50)	32.0	3	15.0	1.300	1.000	14.5	< 41.6	
10	17	nodeRight	2400	12	400	2.4	-12.1	-72.4	G(50)	32.0	3	15.0	1.300	1.000	14.5	< 41.6	
10	18	nodeLeft	2400	12	400	4.7	-10.1	-33.6	G(50)	32.0	3	15.0	1.300	1.000	14.8	< 41.6	
10	18	nodeRight	2400	12	400	4.7	-10.1	-33.6	G(50)	32.0	3	15.0	1.300	1.000	14.8	< 41.6	
11	19	nodeLeft	2400	12	400	16.4	-12.4	-5.9	G(50)	32.0	3	15.0	1.066	1.000	28.8	< 34.1	
11	19	nodeRight	2400	12	400	16.4	-12.4	-5.9	G(50)	32.0	3	15.0	1.066	1.000	28.8	< 34.1	
12	20	nodeLeft	2400	12	400	29.0	-10.6	22.9	G(50)	32.0	3	15.0	1.000	1.000	39.5	> 32.0	0.57<1
12	20	nodeRight	2400	12	400	29.0	-10.6	22.9	G(50)	32.0	3	15.0	1.000	1.000	39.5	> 32.0	0.57<1
12	21	nodeLeft	2400	12	400	24.2	-7.0	38.6	G(50)	32.0	3	15.0	1.000	1.000	31.2	< 32.0	
12	21	nodeRight	2400	12	400	24.2	-7.0	38.6	G(50)	32.0	3	15.0	1.000	1.000	31.2	< 32.0	
13	22	nodeLeft	2400	12	400	13.8	-3.5	31.0	G(50)	32.0	3	15.0	1.000	1.000	17.3	< 32.0	
13	22	nodeRight	2400	12	400	13.8	-3.5	31.0	G(50)	32.0	3	15.0	1.000	1.000	17.3	< 32.0	
13	23	nodeLeft	2400	12	400	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6	

2. G2

Steel I Girder G2

node U.FLG-MAX (UpperFlangeStress MAX)

Sec	node	Flange	t	σ tmax	σ tmin	σ d	Grade	$\Delta \sigma$ ce m	$\Delta \sigma$ ve	CR	Ct	$\Delta \sigma$ max	CR • Ct	Stress
														Cycle
													D	
													(N/mm2)	
													(N/mm2)	
1	1	nodeRight	21	0.0	0.0	0.0	F (65)	46.0	3	21.0	1.300	1.000	0.0	< 59.8
1	2	nodeLeft	21	3.5	-35.4	-31.4	F (65)	46.0	3	21.0	1.300	1.000	38.9	< 59.8
1	2	nodeRight	21	3.5	-35.4	-31.4	F (65)	46.0	3	21.0	1.300	1.000	38.9	< 59.8
2	3	nodeLeft	21	7.0	-42.0	-43.8	F (65)	46.0	3	21.0	1.300	1.000	49.0	< 59.8
2	3	nodeRight	21	7.0	-42.0	-43.8	F (65)	46.0	3	21.0	1.300	1.000	49.0	< 59.8
2	4	nodeLeft	21	10.5	-30.4	-37.2	F (65)	46.0	3	21.0	1.300	1.000	40.9	< 59.8
2	4	nodeRight	21	10.5	-30.4	-37.2	F (65)	46.0	3	21.0	1.300	1.000	40.9	< 59.8
3	5	nodeLeft	19	14.9	-37.4	7.7	F (65)	46.0	3	21.0	1.032	1.000	52.2	> 47.5
3	5	nodeRight	19	14.9	-37.4	7.7	F (65)	46.0	3	21.0	1.032	1.000	52.2	> 47.5
4	6	nodeLeft	22	16.1	-20.0	65.3	F (65)	46.0	3	21.0	1.000	1.000	36.1	< 46.0
4	6	nodeRight	22	16.1	-20.0	65.3	F (65)	46.0	3	21.0	1.000	1.000	36.1	< 46.0
4	7	nodeLeft	22	22.5	-3.5	134.0	F (65)	46.0	3	21.0	1.000	1.000	26.0	< 46.0
4	7	nodeRight	22	22.5	-3.5	134.0	F (65)	46.0	3	21.0	1.000	1.000	26.0	< 46.0
5	8	nodeLeft	19	12.8	-18.9	65.2	F (65)	46.0	3	21.0	1.000	1.000	31.7	< 46.0
5	8	nodeRight	19	12.8	-18.9	65.2	F (65)	46.0	3	21.0	1.000	1.000	31.7	< 46.0
5	9	nodeLeft	19	11.2	-36.1	-5.9	F (65)	46.0	3	21.0	1.217	1.000	47.3	< 56.0
5	9	nodeRight	19	11.2	-36.1	-5.9	F (65)	46.0	3	21.0	1.217	1.000	47.3	< 56.0
6	10	nodeLeft	25	7.1	-33.9	-52.6	F (65)	46.0	3	21.0	1.300	1.000	41.1	< 59.8
6	10	nodeRight	25	7.1	-33.9	-52.6	F (65)	46.0	3	21.0	1.300	1.000	41.1	< 59.8
6	11	nodeLeft	25	5.6	-30.5	-86.5	F (65)	46.0	3	21.0	1.300	1.000	36.1	< 59.8
6	11	nodeRight	25	5.6	-30.5	-86.5	F (65)	46.0	3	21.0	1.300	1.000	36.1	< 59.8
7	12	nodeLeft	25	3.9	-33.1	-91.2	F (65)	46.0	3	21.0	1.300	1.000	37.0	< 59.8
7	12	nodeRight	25	3.9	-33.1	-91.2	F (65)	46.0	3	21.0	1.300	1.000	37.0	< 59.8
8	13	nodeLeft	25	5.6	-30.5	-86.5	F (65)	46.0	3	21.0	1.300	1.000	36.1	< 59.8
8	13	nodeRight	25	5.6	-30.5	-86.5	F (65)	46.0	3	21.0	1.300	1.000	36.1	< 59.8
8	14	nodeLeft	25	7.1	-33.9	-52.6	F (65)	46.0	3	21.0	1.300	1.000	41.1	< 59.8
8	14	nodeRight	25	7.1	-33.9	-52.6	F (65)	46.0	3	21.0	1.300	1.000	41.1	< 59.8
9	15	nodeLeft	19	11.2	-36.1	-5.9	F (65)	46.0	3	21.0	1.217	1.000	47.3	< 56.0
9	15	nodeRight	19	11.2	-36.1	-5.9	F (65)	46.0	3	21.0	1.217	1.000	47.3	< 56.0
9	16	nodeLeft	19	12.8	-18.9	65.2	F (65)	46.0	3	21.0	1.000	1.000	31.7	< 46.0
9	16	nodeRight	19	12.8	-18.9	65.2	F (65)	46.0	3	21.0	1.000	1.000	31.7	< 46.0
10	17	nodeLeft	22	22.5	-3.5	134.0	F (65)	46.0	3	21.0	1.000	1.000	26.0	< 46.0
10	17	nodeRight	22	22.5	-3.5	134.0	F (65)	46.0	3	21.0	1.000	1.000	26.0	< 46.0
10	18	nodeLeft	22	16.1	-20.0	65.3	F (65)	46.0	3	21.0	1.000	1.000	36.1	< 46.0
10	18	nodeRight	22	16.1	-20.0	65.3	F (65)	46.0	3	21.0	1.000	1.000	36.1	< 46.0
11	19	nodeLeft	19	14.9	-37.4	7.7	F (65)	46.0	3	21.0	1.032	1.000	52.2	> 47.5
11	19	nodeRight	19	14.9	-37.4	7.7	F (65)	46.0	3	21.0	1.032	1.000	52.2	> 47.5
12	20	nodeLeft	21	10.5	-30.4	-37.2	F (65)	46.0	3	21.0	1.300	1.000	40.9	< 59.8
12	20	nodeRight	21	10.5	-30.4	-37.2	F (65)	46.0	3	21.0	1.300	1.000	40.9	< 59.8
12	21	nodeLeft	21	7.0	-42.0	-43.8	F (65)	46.0	3	21.0	1.300	1.000	49.0	< 59.8
12	21	nodeRight	21	7.0	-42.0	-43.8	F (65)	46.0	3	21.0	1.300	1.000	49.0	< 59.8
13	22	nodeLeft	21	3.5	-35.4	-31.4	F (65)	46.0	3	21.0	1.300	1.000	38.9	< 59.8
13	22	nodeRight	21	3.5	-35.4	-31.4	F (65)	46.0	3	21.0	1.300	1.000	38.9	< 59.8
13	23	nodeLeft	21	0.0	0.0	0.0	F (65)	46.0	3	21.0	1.300	1.000	0.0	< 59.8

Steel I Girder G2

node L.FLG-MAX (LowerFlangeStress MAX)

Sec	node	Flange	t (mm)	σ_{tmax}	σ_{tmin} (N/mm ²)	σ_d	Grade ($\Delta \sigma_f$)	$\Delta \sigma_{cem}$	$\Delta \sigma_{ve}$	CR	Ct	Stress		Cycle D
												$\Delta \sigma_{max}$ (N/mm ²)	CR • Ct (N/mm ²)	
1	1	nodeRight	19	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2
1	2	nodeLeft	19	37.0	-3.7	32.8	D (100)	84.0	3	39.0	1.000	1.000	40.7	< 84.0
1	2	nodeRight	19	37.0	-3.7	32.8	D (100)	84.0	3	39.0	1.000	1.000	40.7	< 84.0
2	3	nodeLeft	19	43.9	-7.3	45.8	D (100)	84.0	3	39.0	1.000	1.000	51.2	< 84.0
2	3	nodeRight	19	43.9	-7.3	45.8	D (100)	84.0	3	39.0	1.000	1.000	51.2	< 84.0
2	4	nodeLeft	19	31.8	-11.0	38.9	D (100)	84.0	3	39.0	1.000	1.000	42.8	< 84.0
2	4	nodeRight	19	31.8	-11.0	38.9	D (100)	84.0	3	39.0	1.000	1.000	42.8	< 84.0
3	5	nodeLeft	21	35.8	-14.2	-7.4	D (100)	84.0	3	39.0	1.000	1.000	50.0	< 84.0
3	5	nodeRight	21	35.8	-14.2	-7.4	D (100)	84.0	3	39.0	1.000	1.000	50.0	< 84.0
4	6	nodeLeft	29	17.5	-14.1	-57.0	D (100)	84.0	3	39.0	1.300	0.964	31.5	<105.2
4	6	nodeRight	29	17.5	-14.1	-57.0	D (100)	84.0	3	39.0	1.300	0.964	31.5	<105.2
4	7	nodeLeft	29	3.1	-19.6	-117.0	D (100)	84.0	3	39.0	1.300	0.964	22.7	<105.2
4	7	nodeRight	29	3.1	-19.6	-117.0	D (100)	84.0	3	39.0	1.300	0.964	22.7	<105.2
5	8	nodeLeft	21	18.1	-12.3	-62.4	D (100)	84.0	3	39.0	1.300	1.000	30.4	<109.2
5	8	nodeRight	21	18.1	-12.3	-62.4	D (100)	84.0	3	39.0	1.300	1.000	30.4	<109.2
5	9	nodeLeft	21	34.5	-10.8	5.6	D (100)	84.0	3	39.0	1.000	1.000	45.3	< 84.0
5	9	nodeRight	21	34.5	-10.8	5.6	D (100)	84.0	3	39.0	1.000	1.000	45.3	< 84.0
6	10	nodeLeft	19	38.5	-8.1	59.7	D (100)	84.0	3	39.0	1.000	1.000	46.5	< 84.0
6	10	nodeRight	19	38.5	-8.1	59.7	D (100)	84.0	3	39.0	1.000	1.000	46.5	< 84.0
6	11	nodeLeft	19	34.6	-6.3	98.0	D (100)	84.0	3	39.0	1.000	1.000	40.9	< 84.0
6	11	nodeRight	19	34.6	-6.3	98.0	D (100)	84.0	3	39.0	1.000	1.000	40.9	< 84.0
7	12	nodeLeft	19	37.5	-4.4	103.4	D (100)	84.0	3	39.0	1.000	1.000	42.0	< 84.0
7	12	nodeRight	19	37.5	-4.4	103.4	D (100)	84.0	3	39.0	1.000	1.000	42.0	< 84.0
8	13	nodeLeft	19	34.6	-6.3	98.0	D (100)	84.0	3	39.0	1.000	1.000	40.9	< 84.0
8	13	nodeRight	19	34.6	-6.3	98.0	D (100)	84.0	3	39.0	1.000	1.000	40.9	< 84.0
8	14	nodeLeft	19	38.5	-8.1	59.7	D (100)	84.0	3	39.0	1.000	1.000	46.5	< 84.0
8	14	nodeRight	19	38.5	-8.1	59.7	D (100)	84.0	3	39.0	1.000	1.000	46.5	< 84.0
9	15	nodeLeft	21	34.5	-10.8	5.6	D (100)	84.0	3	39.0	1.000	1.000	45.3	< 84.0
9	15	nodeRight	21	34.5	-10.8	5.6	D (100)	84.0	3	39.0	1.000	1.000	45.3	< 84.0
9	16	nodeLeft	21	18.1	-12.3	-62.4	D (100)	84.0	3	39.0	1.300	1.000	30.4	<109.2
9	16	nodeRight	21	18.1	-12.3	-62.4	D (100)	84.0	3	39.0	1.300	1.000	30.4	<109.2
10	17	nodeLeft	29	3.1	-19.6	-117.0	D (100)	84.0	3	39.0	1.300	0.964	22.7	<105.2
10	17	nodeRight	29	3.1	-19.6	-117.0	D (100)	84.0	3	39.0	1.300	0.964	22.7	<105.2
10	18	nodeLeft	29	17.5	-14.1	-57.0	D (100)	84.0	3	39.0	1.300	0.964	31.5	<105.2
10	18	nodeRight	29	17.5	-14.1	-57.0	D (100)	84.0	3	39.0	1.300	0.964	31.5	<105.2
11	19	nodeLeft	21	35.8	-14.2	-7.4	D (100)	84.0	3	39.0	1.000	1.000	50.0	< 84.0
11	19	nodeRight	21	35.8	-14.2	-7.4	D (100)	84.0	3	39.0	1.000	1.000	50.0	< 84.0
12	20	nodeLeft	19	31.8	-11.0	38.9	D (100)	84.0	3	39.0	1.000	1.000	42.8	< 84.0
12	20	nodeRight	19	31.8	-11.0	38.9	D (100)	84.0	3	39.0	1.000	1.000	42.8	< 84.0
12	21	nodeLeft	19	43.9	-7.3	45.8	D (100)	84.0	3	39.0	1.000	1.000	51.2	< 84.0
12	21	nodeRight	19	43.9	-7.3	45.8	D (100)	84.0	3	39.0	1.000	1.000	51.2	< 84.0
13	22	nodeLeft	19	37.0	-3.7	32.8	D (100)	84.0	3	39.0	1.000	1.000	40.7	< 84.0
13	22	nodeRight	19	37.0	-3.7	32.8	D (100)	84.0	3	39.0	1.000	1.000	40.7	< 84.0
13	23	nodeLeft	19	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2

Steel I Girder G2

node WEB-U-1 (WebUpper edge) WEB - 1

Sec	node	Web	h	t	Grade				Stress							
					σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D
					(N/mm ²)				(N/mm ²)							
1	1	nodeRight	2400	21	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
1	2	nodeLeft	2400	21	0	3.4	-34.8	-30.9	E(80)	62.0	3	29.0	1.300	1.000	38.2	< 80.6
1	2	nodeRight	2400	21	0	3.4	-34.8	-30.9	E(80)	62.0	3	29.0	1.300	1.000	38.2	< 80.6
2	3	nodeLeft	2400	21	0	6.9	-41.3	-43.1	E(80)	62.0	3	29.0	1.300	1.000	48.2	< 80.6
2	3	nodeRight	2400	21	0	6.9	-41.3	-43.1	E(80)	62.0	3	29.0	1.300	1.000	48.2	< 80.6
2	4	nodeLeft	2400	21	0	10.4	-29.9	-36.6	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
2	4	nodeRight	2400	21	0	10.4	-29.9	-36.6	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
3	5	nodeLeft	2400	19	0	14.6	-36.8	7.6	E(80)	62.0	3	29.0	1.032	1.000	51.4	< 64.0
3	5	nodeRight	2400	19	0	14.6	-36.8	7.6	E(80)	62.0	3	29.0	1.032	1.000	51.4	< 64.0
4	6	nodeLeft	2400	22	0	15.8	-19.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	35.5	< 62.0
4	6	nodeRight	2400	22	0	15.8	-19.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	35.5	< 62.0
4	7	nodeLeft	2400	22	0	22.1	-3.4	131.7	E(80)	62.0	3	29.0	1.000	1.000	25.5	< 62.0
4	7	nodeRight	2400	22	0	22.1	-3.4	131.7	E(80)	62.0	3	29.0	1.000	1.000	25.5	< 62.0
5	8	nodeLeft	2400	19	0	12.6	-18.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	31.2	< 62.0
5	8	nodeRight	2400	19	0	12.6	-18.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	31.2	< 62.0
5	9	nodeLeft	2400	19	0	11.1	-35.5	-5.8	E(80)	62.0	3	29.0	1.217	1.000	46.6	< 75.5
5	9	nodeRight	2400	19	0	11.1	-35.5	-5.8	E(80)	62.0	3	29.0	1.217	1.000	46.6	< 75.5
6	10	nodeLeft	2400	25	0	7.0	-33.2	-51.5	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
6	10	nodeRight	2400	25	0	7.0	-33.2	-51.5	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
6	11	nodeLeft	2400	25	0	5.4	-29.8	-84.5	E(80)	62.0	3	29.0	1.300	1.000	35.3	< 80.6
6	11	nodeRight	2400	25	0	5.4	-29.8	-84.5	E(80)	62.0	3	29.0	1.300	1.000	35.3	< 80.6
7	12	nodeLeft	2400	25	0	3.8	-32.4	-89.2	E(80)	62.0	3	29.0	1.300	1.000	36.2	< 80.6
7	12	nodeRight	2400	25	0	3.8	-32.4	-89.2	E(80)	62.0	3	29.0	1.300	1.000	36.2	< 80.6
8	13	nodeLeft	2400	25	0	5.4	-29.8	-84.5	E(80)	62.0	3	29.0	1.300	1.000	35.3	< 80.6
8	13	nodeRight	2400	25	0	5.4	-29.8	-84.5	E(80)	62.0	3	29.0	1.300	1.000	35.3	< 80.6
8	14	nodeLeft	2400	25	0	7.0	-33.2	-51.5	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
8	14	nodeRight	2400	25	0	7.0	-33.2	-51.5	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
9	15	nodeLeft	2400	19	0	11.1	-35.5	-5.8	E(80)	62.0	3	29.0	1.217	1.000	46.6	< 75.5
9	15	nodeRight	2400	19	0	11.1	-35.5	-5.8	E(80)	62.0	3	29.0	1.217	1.000	46.6	< 75.5
9	16	nodeLeft	2400	19	0	12.6	-18.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	31.2	< 62.0
9	16	nodeRight	2400	19	0	12.6	-18.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	31.2	< 62.0
10	17	nodeLeft	2400	22	0	22.1	-3.4	131.7	E(80)	62.0	3	29.0	1.000	1.000	25.5	< 62.0
10	17	nodeRight	2400	22	0	22.1	-3.4	131.7	E(80)	62.0	3	29.0	1.000	1.000	25.5	< 62.0
10	18	nodeLeft	2400	22	0	15.8	-19.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	35.5	< 62.0
10	18	nodeRight	2400	22	0	15.8	-19.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	35.5	< 62.0
11	19	nodeLeft	2400	19	0	14.6	-36.8	7.6	E(80)	62.0	3	29.0	1.032	1.000	51.4	< 64.0
11	19	nodeRight	2400	19	0	14.6	-36.8	7.6	E(80)	62.0	3	29.0	1.032	1.000	51.4	< 64.0
12	20	nodeLeft	2400	21	0	10.4	-29.9	-36.6	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
12	20	nodeRight	2400	21	0	10.4	-29.9	-36.6	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
12	21	nodeLeft	2400	21	0	6.9	-41.3	-43.1	E(80)	62.0	3	29.0	1.300	1.000	48.2	< 80.6
12	21	nodeRight	2400	21	0	6.9	-41.3	-43.1	E(80)	62.0	3	29.0	1.300	1.000	48.2	< 80.6
13	22	nodeLeft	2400	21	0	3.4	-34.8	-30.9	E(80)	62.0	3	29.0	1.300	1.000	38.2	< 80.6
13	22	nodeRight	2400	21	0	3.4	-34.8	-30.9	E(80)	62.0	3	29.0	1.300	1.000	38.2	< 80.6
13	23	nodeLeft	2400	21	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6

Steel I Girder G2

node WEB-L-1 (WebLower edge) WEB - 1

Sec	node	Web	h	t	Grade				Stress							
					σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D
					(N/mm ²)				(N/mm ²)							
1	1	nodeRight	2400	19	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
1	2	nodeLeft	2400	19	0	36.4	-3.6	32.3	E(80)	62.0	3	29.0	1.000	1.000	40.0	< 62.0
1	2	nodeRight	2400	19	0	36.4	-3.6	32.3	E(80)	62.0	3	29.0	1.000	1.000	40.0	< 62.0
2	3	nodeLeft	2400	19	0	43.2	-7.2	45.1	E(80)	62.0	3	29.0	1.000	1.000	50.4	< 62.0
2	3	nodeRight	2400	19	0	43.2	-7.2	45.1	E(80)	62.0	3	29.0	1.000	1.000	50.4	< 62.0
2	4	nodeLeft	2400	19	0	31.3	-10.8	38.3	E(80)	62.0	3	29.0	1.000	1.000	42.1	< 62.0
2	4	nodeRight	2400	19	0	31.3	-10.8	38.3	E(80)	62.0	3	29.0	1.000	1.000	42.1	< 62.0
3	5	nodeLeft	2400	21	0	35.1	-14.0	-7.2	E(80)	62.0	3	29.0	1.000	1.000	49.1	< 62.0
3	5	nodeRight	2400	21	0	35.1	-14.0	-7.2	E(80)	62.0	3	29.0	1.000	1.000	49.1	< 62.0
4	6	nodeLeft	2400	29	0	17.0	-13.7	-55.5	E(80)	62.0	3	29.0	1.300	0.964	30.7	< 77.7
4	6	nodeRight	2400	29	0	17.0	-13.7	-55.5	E(80)	62.0	3	29.0	1.300	0.964	30.7	< 77.7
4	7	nodeLeft	2400	29	0	3.0	-19.1	-114.0	E(80)	62.0	3	29.0	1.300	0.964	22.1	< 77.7
4	7	nodeRight	2400	29	0	3.0	-19.1	-114.0	E(80)	62.0	3	29.0	1.300	0.964	22.1	< 77.7
5	8	nodeLeft	2400	21	0	17.7	-12.1	-61.3	E(80)	62.0	3	29.0	1.300	1.000	29.8	< 80.6
5	8	nodeRight	2400	21	0	17.7	-12.1	-61.3	E(80)	62.0	3	29.0	1.300	1.000	29.8	< 80.6
5	9	nodeLeft	2400	21	0	33.9	-10.6	5.5	E(80)	62.0	3	29.0	1.000	1.000	44.5	< 62.0
5	9	nodeRight	2400	21	0	33.9	-10.6	5.5	E(80)	62.0	3	29.0	1.000	1.000	44.5	< 62.0
6	10	nodeLeft	2400	19	0	37.9	-7.9	58.8	E(80)	62.0	3	29.0	1.000	1.000	45.8	< 62.0
6	10	nodeRight	2400	19	0	37.9	-7.9	58.8	E(80)	62.0	3	29.0	1.000	1.000	45.8	< 62.0
6	11	nodeLeft	2400	19	0	34.1	-6.2	96.5	E(80)	62.0	3	29.0	1.000	1.000	40.3	< 62.0
6	11	nodeRight	2400	19	0	34.1	-6.2	96.5	E(80)	62.0	3	29.0	1.000	1.000	40.3	< 62.0
7	12	nodeLeft	2400	19	0	37.0	-4.4	101.9	E(80)	62.0	3	29.0	1.000	1.000	41.4	< 62.0
7	12	nodeRight	2400	19	0	37.0	-4.4	101.9	E(80)	62.0	3	29.0	1.000	1.000	41.4	< 62.0
8	13	nodeLeft	2400	19	0	34.1	-6.2	96.5	E(80)	62.0	3	29.0	1.000	1.000	40.3	< 62.0
8	13	nodeRight	2400	19	0	34.1	-6.2	96.5	E(80)	62.0	3	29.0	1.000	1.000	40.3	< 62.0
8	14	nodeLeft	2400	19	0	37.9	-7.9	58.8	E(80)	62.0	3	29.0	1.000	1.000	45.8	< 62.0
8	14	nodeRight	2400	19	0	37.9	-7.9	58.8	E(80)	62.0	3	29.0	1.000	1.000	45.8	< 62.0
9	15	nodeLeft	2400	21	0	33.9	-10.6	5.5	E(80)	62.0	3	29.0	1.000	1.000	44.5	< 62.0
9	15	nodeRight	2400	21	0	33.9	-10.6	5.5	E(80)	62.0	3	29.0	1.000	1.000	44.5	< 62.0
9	16	nodeLeft	2400	21	0	17.7	-12.1	-61.3	E(80)	62.0	3	29.0	1.300	1.000	29.8	< 80.6
9	16	nodeRight	2400	21	0	17.7	-12.1	-61.3	E(80)	62.0	3	29.0	1.300	1.000	29.8	< 80.6
10	17	nodeLeft	2400	29	0	3.0	-19.1	-114.0	E(80)	62.0	3	29.0	1.300	0.964	22.1	< 77.7
10	17	nodeRight	2400	29	0	3.0	-19.1	-114.0	E(80)	62.0	3	29.0	1.300	0.964	22.1	< 77.7
10	18	nodeLeft	2400	29	0	17.0	-13.7	-55.5	E(80)	62.0	3	29.0	1.300	0.964	30.7	< 77.7
10	18	nodeRight	2400	29	0	17.0	-13.7	-55.5	E(80)	62.0	3	29.0	1.300	0.964	30.7	< 77.7
11	19	nodeLeft	2400	21	0	35.1	-14.0	-7.2	E(80)	62.0	3	29.0	1.000	1.000	49.1	< 62.0
11	19	nodeRight	2400	21	0	35.1	-14.0	-7.2	E(80)	62.0	3	29.0	1.000	1.000	49.1	< 62.0
12	20	nodeLeft	2400	19	0	31.3	-10.8	38.3	E(80)	62.0	3	29.0	1.000	1.000	42.1	< 62.0
12	20	nodeRight	2400	19	0	31.3	-10.8	38.3	E(80)	62.0	3	29.0	1.000	1.000	42.1	< 62.0
12	21	nodeLeft	2400	19	0	43.2	-7.2	45.1	E(80)	62.0	3	29.0	1.000	1.000	50.4	< 62.0
12	21	nodeRight	2400	19	0	43.2	-7.2	45.1	E(80)	62.0	3	29.0	1.000	1.000	50.4	< 62.0
13	22	nodeLeft	2400	19	0	36.4	-3.6	32.3	E(80)	62.0	3	29.0	1.000	1.000	40.0	< 62.0
13	22	nodeRight	2400	19	0	36.4	-3.6	32.3	E(80)	62.0	3	29.0	1.000	1.000	40.0	< 62.0
13	23	nodeLeft	2400	19	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6

Steel I Girder G2

node HSTIFF-1 (WebH-Stiffener) WEB - 1

Sec	node	Web	h	t	σ_{tmax}	σ_{tmin}	σ_d	Grade	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	Stress	
															$\Delta \sigma_{ce} \cdot Cycle$	$\Delta \sigma_{max} CR \cdot Ct$
														(N/mm ²)		
1	1	nodeRight	2400	12	480	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
1	2	nodeLeft	2400	12	480	2.0	-20.5	-18.2	G(50)	32.0	3	15.0	1.300	1.000	22.6	< 41.6
1	2	nodeRight	2400	12	480	2.0	-20.5	-18.2	G(50)	32.0	3	15.0	1.300	1.000	22.6	< 41.6
2	3	nodeLeft	2400	12	480	4.1	-24.4	-25.4	G(50)	32.0	3	15.0	1.300	1.000	28.4	< 41.6
2	3	nodeRight	2400	12	480	4.1	-24.4	-25.4	G(50)	32.0	3	15.0	1.300	1.000	28.4	< 41.6
2	4	nodeLeft	2400	12	480	6.1	-17.6	-21.6	G(50)	32.0	3	15.0	1.300	1.000	23.7	< 41.6
2	4	nodeRight	2400	12	480	6.1	-17.6	-21.6	G(50)	32.0	3	15.0	1.300	1.000	23.7	< 41.6
3	5	nodeLeft	2400	12	480	8.9	-22.4	4.6	G(50)	32.0	3	15.0	1.032	1.000	31.3	< 33.0
3	5	nodeRight	2400	12	480	8.9	-22.4	4.6	G(50)	32.0	3	15.0	1.032	1.000	31.3	< 33.0
4	6	nodeLeft	2400	12	480	9.7	-7.8	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.5	< 41.6
4	6	nodeRight	2400	12	480	9.7	-7.8	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.5	< 41.6
4	7	nodeLeft	2400	12	480	1.7	-10.9	-64.9	G(50)	32.0	3	15.0	1.300	1.000	12.6	< 41.6
4	7	nodeRight	2400	12	480	1.7	-10.9	-64.9	G(50)	32.0	3	15.0	1.300	1.000	12.6	< 41.6
5	8	nodeLeft	2400	12	480	10.5	-7.1	-36.2	G(50)	32.0	3	15.0	1.300	1.000	17.6	< 41.6
5	8	nodeRight	2400	12	480	10.5	-7.1	-36.2	G(50)	32.0	3	15.0	1.300	1.000	17.6	< 41.6
5	9	nodeLeft	2400	12	480	6.7	-21.6	-3.5	G(50)	32.0	3	15.0	1.217	1.000	28.4	< 38.9
5	9	nodeRight	2400	12	480	6.7	-21.6	-3.5	G(50)	32.0	3	15.0	1.217	1.000	28.4	< 38.9
6	10	nodeLeft	2400	12	480	4.0	-19.0	-29.4	G(50)	32.0	3	15.0	1.300	1.000	23.0	< 41.6
6	10	nodeRight	2400	12	480	4.0	-19.0	-29.4	G(50)	32.0	3	15.0	1.300	1.000	23.0	< 41.6
6	11	nodeLeft	2400	12	480	3.1	-17.1	-48.3	G(50)	32.0	3	15.0	1.300	1.000	20.2	< 41.6
6	11	nodeRight	2400	12	480	3.1	-17.1	-48.3	G(50)	32.0	3	15.0	1.300	1.000	20.2	< 41.6
7	12	nodeLeft	2400	12	480	2.2	-18.5	-51.0	G(50)	32.0	3	15.0	1.300	1.000	20.7	< 41.6
7	12	nodeRight	2400	12	480	2.2	-18.5	-51.0	G(50)	32.0	3	15.0	1.300	1.000	20.7	< 41.6
8	13	nodeLeft	2400	12	480	3.1	-17.1	-48.3	G(50)	32.0	3	15.0	1.300	1.000	20.2	< 41.6
8	13	nodeRight	2400	12	480	3.1	-17.1	-48.3	G(50)	32.0	3	15.0	1.300	1.000	20.2	< 41.6
8	14	nodeLeft	2400	12	480	4.0	-19.0	-29.4	G(50)	32.0	3	15.0	1.300	1.000	23.0	< 41.6
8	14	nodeRight	2400	12	480	4.0	-19.0	-29.4	G(50)	32.0	3	15.0	1.300	1.000	23.0	< 41.6
9	15	nodeLeft	2400	12	480	6.7	-21.6	-3.5	G(50)	32.0	3	15.0	1.217	1.000	28.4	< 38.9
9	15	nodeRight	2400	12	480	6.7	-21.6	-3.5	G(50)	32.0	3	15.0	1.217	1.000	28.4	< 38.9
9	16	nodeLeft	2400	12	480	10.5	-7.1	-36.2	G(50)	32.0	3	15.0	1.300	1.000	17.6	< 41.6
9	16	nodeRight	2400	12	480	10.5	-7.1	-36.2	G(50)	32.0	3	15.0	1.300	1.000	17.6	< 41.6
10	17	nodeLeft	2400	12	480	1.7	-10.9	-64.9	G(50)	32.0	3	15.0	1.300	1.000	12.6	< 41.6
10	17	nodeRight	2400	12	480	1.7	-10.9	-64.9	G(50)	32.0	3	15.0	1.300	1.000	12.6	< 41.6
10	18	nodeLeft	2400	12	480	9.7	-7.8	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.5	< 41.6
10	18	nodeRight	2400	12	480	9.7	-7.8	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.5	< 41.6
11	19	nodeLeft	2400	12	480	8.9	-22.4	4.6	G(50)	32.0	3	15.0	1.032	1.000	31.3	< 33.0
11	19	nodeRight	2400	12	480	8.9	-22.4	4.6	G(50)	32.0	3	15.0	1.032	1.000	31.3	< 33.0
12	20	nodeLeft	2400	12	480	6.1	-17.6	-21.6	G(50)	32.0	3	15.0	1.300	1.000	23.7	< 41.6
12	20	nodeRight	2400	12	480	6.1	-17.6	-21.6	G(50)	32.0	3	15.0	1.300	1.000	23.7	< 41.6
12	21	nodeLeft	2400	12	480	4.1	-24.4	-25.4	G(50)	32.0	3	15.0	1.300	1.000	28.4	< 41.6
12	21	nodeRight	2400	12	480	4.1	-24.4	-25.4	G(50)	32.0	3	15.0	1.300	1.000	28.4	< 41.6
13	22	nodeLeft	2400	12	480	2.0	-20.5	-18.2	G(50)	32.0	3	15.0	1.300	1.000	22.6	< 41.6
13	22	nodeRight	2400	12	480	2.0	-20.5	-18.2	G(50)	32.0	3	15.0	1.300	1.000	22.6	< 41.6
13	23	nodeLeft	2400	12	480	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6

Steel I Girder G2

node POINT-U-1 (WebUpper) WEB - 1

Sec	node	Web	h	t	σ tmax	σ tmin	σ d	Grade	(Δ σ f)	Δ σ ce	m	Δ σ ve	CR	Ct	Stress	
															Δ σ ce • Cycle	Δ σ max CR • Ct
															D	
															(N/mm2)	
1	1	nodeRight	2400	12	300	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
1	2	nodeLeft	2400	12	300	2.6	-25.9	-23.0	G(50)	32.0	3	15.0	1.300	1.000	28.5	< 41.6
1	2	nodeRight	2400	12	300	2.6	-25.9	-23.0	G(50)	32.0	3	15.0	1.300	1.000	28.5	< 41.6
2	3	nodeLeft	2400	12	300	5.1	-30.7	-32.0	G(50)	32.0	3	15.0	1.300	1.000	35.8	< 41.6
2	3	nodeRight	2400	12	300	5.1	-30.7	-32.0	G(50)	32.0	3	15.0	1.300	1.000	35.8	< 41.6
2	4	nodeLeft	2400	12	300	7.7	-22.2	-27.2	G(50)	32.0	3	15.0	1.300	1.000	29.9	< 41.6
2	4	nodeRight	2400	12	300	7.7	-22.2	-27.2	G(50)	32.0	3	15.0	1.300	1.000	29.9	< 41.6
3	5	nodeLeft	2400	12	300	11.1	-27.8	5.7	G(50)	32.0	3	15.0	1.032	1.000	38.9	> 33.0
3	5	nodeRight	2400	12	300	11.1	-27.8	5.7	G(50)	32.0	3	15.0	1.032	1.000	38.9	> 33.0
4	6	nodeLeft	2400	12	300	12.1	-15.1	49.2	G(50)	32.0	3	15.0	1.000	1.000	27.2	< 32.0
4	6	nodeRight	2400	12	300	12.1	-15.1	49.2	G(50)	32.0	3	15.0	1.000	1.000	27.2	< 32.0
4	7	nodeLeft	2400	12	300	16.9	-2.6	101.0	G(50)	32.0	3	15.0	1.000	1.000	19.6	< 32.0
4	7	nodeRight	2400	12	300	16.9	-2.6	101.0	G(50)	32.0	3	15.0	1.000	1.000	19.6	< 32.0
5	8	nodeLeft	2400	12	300	9.6	-14.0	48.5	G(50)	32.0	3	15.0	1.000	1.000	23.6	< 32.0
5	8	nodeRight	2400	12	300	9.6	-14.0	48.5	G(50)	32.0	3	15.0	1.000	1.000	23.6	< 32.0
5	9	nodeLeft	2400	12	300	8.4	-26.8	-4.4	G(50)	32.0	3	15.0	1.217	1.000	35.2	< 38.9
5	9	nodeRight	2400	12	300	8.4	-26.8	-4.4	G(50)	32.0	3	15.0	1.217	1.000	35.2	< 38.9
6	10	nodeLeft	2400	12	300	5.1	-24.3	-37.7	G(50)	32.0	3	15.0	1.300	1.000	29.4	< 41.6
6	10	nodeRight	2400	12	300	5.1	-24.3	-37.7	G(50)	32.0	3	15.0	1.300	1.000	29.4	< 41.6
6	11	nodeLeft	2400	12	300	4.0	-21.8	-61.9	G(50)	32.0	3	15.0	1.300	1.000	25.8	< 41.6
6	11	nodeRight	2400	12	300	4.0	-21.8	-61.9	G(50)	32.0	3	15.0	1.300	1.000	25.8	< 41.6
7	12	nodeLeft	2400	12	300	2.8	-23.7	-65.3	G(50)	32.0	3	15.0	1.300	1.000	26.5	< 41.6
7	12	nodeRight	2400	12	300	2.8	-23.7	-65.3	G(50)	32.0	3	15.0	1.300	1.000	26.5	< 41.6
8	13	nodeLeft	2400	12	300	4.0	-21.8	-61.9	G(50)	32.0	3	15.0	1.300	1.000	25.8	< 41.6
8	13	nodeRight	2400	12	300	4.0	-21.8	-61.9	G(50)	32.0	3	15.0	1.300	1.000	25.8	< 41.6
8	14	nodeLeft	2400	12	300	5.1	-24.3	-37.7	G(50)	32.0	3	15.0	1.300	1.000	29.4	< 41.6
8	14	nodeRight	2400	12	300	5.1	-24.3	-37.7	G(50)	32.0	3	15.0	1.300	1.000	29.4	< 41.6
9	15	nodeLeft	2400	12	300	8.4	-26.8	-4.4	G(50)	32.0	3	15.0	1.217	1.000	35.2	< 38.9
9	15	nodeRight	2400	12	300	8.4	-26.8	-4.4	G(50)	32.0	3	15.0	1.217	1.000	35.2	< 38.9
9	16	nodeLeft	2400	12	300	9.6	-14.0	48.5	G(50)	32.0	3	15.0	1.000	1.000	23.6	< 32.0
9	16	nodeRight	2400	12	300	9.6	-14.0	48.5	G(50)	32.0	3	15.0	1.000	1.000	23.6	< 32.0
10	17	nodeLeft	2400	12	300	16.9	-2.6	101.0	G(50)	32.0	3	15.0	1.000	1.000	19.6	< 32.0
10	17	nodeRight	2400	12	300	16.9	-2.6	101.0	G(50)	32.0	3	15.0	1.000	1.000	19.6	< 32.0
10	18	nodeLeft	2400	12	300	12.1	-15.1	49.2	G(50)	32.0	3	15.0	1.000	1.000	27.2	< 32.0
10	18	nodeRight	2400	12	300	12.1	-15.1	49.2	G(50)	32.0	3	15.0	1.000	1.000	27.2	< 32.0
11	19	nodeLeft	2400	12	300	11.1	-27.8	5.7	G(50)	32.0	3	15.0	1.032	1.000	38.9	> 33.0
11	19	nodeRight	2400	12	300	11.1	-27.8	5.7	G(50)	32.0	3	15.0	1.032	1.000	38.9	> 33.0
12	20	nodeLeft	2400	12	300	7.7	-22.2	-27.2	G(50)	32.0	3	15.0	1.300	1.000	29.9	< 41.6
12	20	nodeRight	2400	12	300	7.7	-22.2	-27.2	G(50)	32.0	3	15.0	1.300	1.000	29.9	< 41.6
12	21	nodeLeft	2400	12	300	5.1	-30.7	-32.0	G(50)	32.0	3	15.0	1.300	1.000	35.8	< 41.6
12	21	nodeRight	2400	12	300	5.1	-30.7	-32.0	G(50)	32.0	3	15.0	1.300	1.000	35.8	< 41.6
13	22	nodeLeft	2400	12	300	2.6	-25.9	-23.0	G(50)	32.0	3	15.0	1.300	1.000	28.5	< 41.6
13	22	nodeRight	2400	12	300	2.6	-25.9	-23.0	G(50)	32.0	3	15.0	1.300	1.000	28.5	< 41.6
13	23	nodeLeft	2400	12	300	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6

Steel I Girder G2

node POINT-L-1 (WebLower) WEB - 1

Sec	node	Web	h	t	Grade				Stress								
					σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D	
					(N/mm ²)				(N/mm ²)								
1	1	nodeRight	2400	12	400	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6	
1	2	nodeLeft	2400	12	400	24.6	-2.4	21.8	G(50)	32.0	3	15.0	1.000	1.000	27.0	< 32.0	
1	2	nodeRight	2400	12	400	24.6	-2.4	21.8	G(50)	32.0	3	15.0	1.000	1.000	27.0	< 32.0	
2	3	nodeLeft	2400	12	400	29.1	-4.9	30.4	G(50)	32.0	3	15.0	1.000	1.000	34.0	> 32.0	0.36<1
2	3	nodeRight	2400	12	400	29.1	-4.9	30.4	G(50)	32.0	3	15.0	1.000	1.000	34.0	> 32.0	0.36<1
2	4	nodeLeft	2400	12	400	21.1	-7.3	25.8	G(50)	32.0	3	15.0	1.000	1.000	28.4	< 32.0	
2	4	nodeRight	2400	12	400	21.1	-7.3	25.8	G(50)	32.0	3	15.0	1.000	1.000	28.4	< 32.0	
3	5	nodeLeft	2400	12	400	23.1	-9.2	-4.8	G(50)	32.0	3	15.0	1.000	1.000	32.3	> 32.0	0.31<1
3	5	nodeRight	2400	12	400	23.1	-9.2	-4.8	G(50)	32.0	3	15.0	1.000	1.000	32.3	> 32.0	0.31<1
4	6	nodeLeft	2400	12	400	10.9	-8.8	-35.6	G(50)	32.0	3	15.0	1.300	1.000	19.7	< 41.6	
4	6	nodeRight	2400	12	400	10.9	-8.8	-35.6	G(50)	32.0	3	15.0	1.300	1.000	19.7	< 41.6	
4	7	nodeLeft	2400	12	400	1.9	-12.2	-73.1	G(50)	32.0	3	15.0	1.300	1.000	14.2	< 41.6	
4	7	nodeRight	2400	12	400	1.9	-12.2	-73.1	G(50)	32.0	3	15.0	1.300	1.000	14.2	< 41.6	
5	8	nodeLeft	2400	12	400	11.7	-8.0	-40.4	G(50)	32.0	3	15.0	1.300	1.000	19.6	< 41.6	
5	8	nodeRight	2400	12	400	11.7	-8.0	-40.4	G(50)	32.0	3	15.0	1.300	1.000	19.6	< 41.6	
5	9	nodeLeft	2400	12	400	22.4	-7.0	3.6	G(50)	32.0	3	15.0	1.000	1.000	29.3	< 32.0	
5	9	nodeRight	2400	12	400	22.4	-7.0	3.6	G(50)	32.0	3	15.0	1.000	1.000	29.3	< 32.0	
6	10	nodeLeft	2400	12	400	26.1	-5.5	40.4	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0	
6	10	nodeRight	2400	12	400	26.1	-5.5	40.4	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0	
6	11	nodeLeft	2400	12	400	23.4	-4.3	66.4	G(50)	32.0	3	15.0	1.000	1.000	27.7	< 32.0	
6	11	nodeRight	2400	12	400	23.4	-4.3	66.4	G(50)	32.0	3	15.0	1.000	1.000	27.7	< 32.0	
7	12	nodeLeft	2400	12	400	25.4	-3.0	70.0	G(50)	32.0	3	15.0	1.000	1.000	28.4	< 32.0	
7	12	nodeRight	2400	12	400	25.4	-3.0	70.0	G(50)	32.0	3	15.0	1.000	1.000	28.4	< 32.0	
8	13	nodeLeft	2400	12	400	23.4	-4.3	66.4	G(50)	32.0	3	15.0	1.000	1.000	27.7	< 32.0	
8	13	nodeRight	2400	12	400	23.4	-4.3	66.4	G(50)	32.0	3	15.0	1.000	1.000	27.7	< 32.0	
8	14	nodeLeft	2400	12	400	26.1	-5.5	40.4	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0	
8	14	nodeRight	2400	12	400	26.1	-5.5	40.4	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0	
9	15	nodeLeft	2400	12	400	22.4	-7.0	3.6	G(50)	32.0	3	15.0	1.000	1.000	29.3	< 32.0	
9	15	nodeRight	2400	12	400	22.4	-7.0	3.6	G(50)	32.0	3	15.0	1.000	1.000	29.3	< 32.0	
9	16	nodeLeft	2400	12	400	11.7	-8.0	-40.4	G(50)	32.0	3	15.0	1.300	1.000	19.6	< 41.6	
9	16	nodeRight	2400	12	400	11.7	-8.0	-40.4	G(50)	32.0	3	15.0	1.300	1.000	19.6	< 41.6	
10	17	nodeLeft	2400	12	400	1.9	-12.2	-73.1	G(50)	32.0	3	15.0	1.300	1.000	14.2	< 41.6	
10	17	nodeRight	2400	12	400	1.9	-12.2	-73.1	G(50)	32.0	3	15.0	1.300	1.000	14.2	< 41.6	
10	18	nodeLeft	2400	12	400	10.9	-8.8	-35.6	G(50)	32.0	3	15.0	1.300	1.000	19.7	< 41.6	
10	18	nodeRight	2400	12	400	10.9	-8.8	-35.6	G(50)	32.0	3	15.0	1.300	1.000	19.7	< 41.6	
11	19	nodeLeft	2400	12	400	23.1	-9.2	-4.8	G(50)	32.0	3	15.0	1.000	1.000	32.3	> 32.0	0.31<1
11	19	nodeRight	2400	12	400	23.1	-9.2	-4.8	G(50)	32.0	3	15.0	1.000	1.000	32.3	> 32.0	0.31<1
12	20	nodeLeft	2400	12	400	21.1	-7.3	25.8	G(50)	32.0	3	15.0	1.000	1.000	28.4	< 32.0	
12	20	nodeRight	2400	12	400	21.1	-7.3	25.8	G(50)	32.0	3	15.0	1.000	1.000	28.4	< 32.0	
12	21	nodeLeft	2400	12	400	29.1	-4.9	30.4	G(50)	32.0	3	15.0	1.000	1.000	34.0	> 32.0	0.36<1
12	21	nodeRight	2400	12	400	29.1	-4.9	30.4	G(50)	32.0	3	15.0	1.000	1.000	34.0	> 32.0	0.36<1
13	22	nodeLeft	2400	12	400	24.6	-2.4	21.8	G(50)	32.0	3	15.0	1.000	1.000	27.0	< 32.0	
13	22	nodeRight	2400	12	400	24.6	-2.4	21.8	G(50)	32.0	3	15.0	1.000	1.000	27.0	< 32.0	
13	23	nodeLeft	2400	12	400	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6	

3. G3

node U.FLG-MAX (UpperFlangeStress MAX)

Sec	node	Flange	t	σ_{tmax}	σ_{tmin}	σ_d	Grade	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	Stress		
													$\Delta \sigma_{max}$	CR • Ct	
			(mm)	(N/mm2)		($\Delta \sigma_f$)							(N/mm2)	(N/mm2)	D
1	1	nodeRight	21	0.0	0.0	0.0	F (65)	46.0	3	21.0	1.300	1.000	0.0	< 59.8	
1	2	nodeLeft	21	2.2	-6.6	-37.0	F (65)	46.0	3	21.0	1.300	1.000	8.8	< 59.8	
1	2	nodeRight	21	2.2	-6.6	-37.0	F (65)	46.0	3	21.0	1.300	1.000	8.8	< 59.8	
2	3	nodeLeft	21	4.5	-13.2	-46.7	F (65)	46.0	3	21.0	1.300	1.000	17.6	< 59.8	
2	3	nodeRight	21	4.5	-13.2	-46.7	F (65)	46.0	3	21.0	1.300	1.000	17.6	< 59.8	
2	4	nodeLeft	21	6.7	-18.8	-29.1	F (65)	46.0	3	21.0	1.300	1.000	25.6	< 59.8	
2	4	nodeRight	21	6.7	-18.8	-29.1	F (65)	46.0	3	21.0	1.300	1.000	25.6	< 59.8	
3	5	nodeLeft	19	8.8	-10.2	5.5	F (65)	46.0	3	21.0	1.000	1.000	19.0	< 46.0	
3	5	nodeRight	19	8.8	-10.2	5.5	F (65)	46.0	3	21.0	1.000	1.000	19.0	< 46.0	
4	6	nodeLeft	21	9.9	-2.9	63.7	F (65)	46.0	3	21.0	1.000	1.000	12.8	< 46.0	
4	6	nodeRight	21	9.9	-2.9	63.7	F (65)	46.0	3	21.0	1.000	1.000	12.8	< 46.0	
4	7	nodeLeft	21	11.5	-2.2	140.2	F (65)	46.0	3	21.0	1.000	1.000	13.7	< 46.0	
4	7	nodeRight	21	11.5	-2.2	140.2	F (65)	46.0	3	21.0	1.000	1.000	13.7	< 46.0	
5	8	nodeLeft	19	7.1	-2.0	58.9	F (65)	46.0	3	21.0	1.000	1.000	9.2	< 46.0	
5	8	nodeRight	19	7.1	-2.0	58.9	F (65)	46.0	3	21.0	1.000	1.000	9.2	< 46.0	
5	9	nodeLeft	19	6.0	-6.7	-12.8	F (65)	46.0	3	21.0	1.300	1.000	12.7	< 59.8	
5	9	nodeRight	19	6.0	-6.7	-12.8	F (65)	46.0	3	21.0	1.300	1.000	12.7	< 59.8	
6	10	nodeLeft	24	4.4	-12.5	-54.5	F (65)	46.0	3	21.0	1.300	1.000	16.9	< 59.8	
6	10	nodeRight	24	4.4	-12.5	-54.5	F (65)	46.0	3	21.0	1.300	1.000	16.9	< 59.8	
6	11	nodeLeft	24	4.0	-18.4	-77.4	F (65)	46.0	3	21.0	1.300	1.000	22.4	< 59.8	
6	11	nodeRight	24	4.0	-18.4	-77.4	F (65)	46.0	3	21.0	1.300	1.000	22.4	< 59.8	
7	12	nodeLeft	24	2.5	-19.3	-94.1	F (65)	46.0	3	21.0	1.300	1.000	21.8	< 59.8	
7	12	nodeRight	24	2.5	-19.3	-94.1	F (65)	46.0	3	21.0	1.300	1.000	21.8	< 59.8	
8	13	nodeLeft	24	4.0	-18.4	-77.4	F (65)	46.0	3	21.0	1.300	1.000	22.4	< 59.8	
8	13	nodeRight	24	4.0	-18.4	-77.4	F (65)	46.0	3	21.0	1.300	1.000	22.4	< 59.8	
8	14	nodeLeft	24	4.4	-12.5	-54.5	F (65)	46.0	3	21.0	1.300	1.000	16.9	< 59.8	
8	14	nodeRight	24	4.4	-12.5	-54.5	F (65)	46.0	3	21.0	1.300	1.000	16.9	< 59.8	
9	15	nodeLeft	19	6.0	-6.7	-12.8	F (65)	46.0	3	21.0	1.300	1.000	12.7	< 59.8	
9	15	nodeRight	19	6.0	-6.7	-12.8	F (65)	46.0	3	21.0	1.300	1.000	12.7	< 59.8	
9	16	nodeLeft	19	7.1	-2.0	58.9	F (65)	46.0	3	21.0	1.000	1.000	9.2	< 46.0	
9	16	nodeRight	19	7.1	-2.0	58.9	F (65)	46.0	3	21.0	1.000	1.000	9.2	< 46.0	
10	17	nodeLeft	21	11.5	-2.2	140.2	F (65)	46.0	3	21.0	1.000	1.000	13.7	< 46.0	
10	17	nodeRight	21	11.5	-2.2	140.2	F (65)	46.0	3	21.0	1.000	1.000	13.7	< 46.0	
10	18	nodeLeft	21	9.9	-2.9	63.7	F (65)	46.0	3	21.0	1.000	1.000	12.8	< 46.0	
10	18	nodeRight	21	9.9	-2.9	63.7	F (65)	46.0	3	21.0	1.000	1.000	12.8	< 46.0	
11	19	nodeLeft	19	8.8	-10.2	5.5	F (65)	46.0	3	21.0	1.000	1.000	19.0	< 46.0	
11	19	nodeRight	19	8.8	-10.2	5.5	F (65)	46.0	3	21.0	1.000	1.000	19.0	< 46.0	
12	20	nodeLeft	21	6.7	-18.8	-29.1	F (65)	46.0	3	21.0	1.300	1.000	25.6	< 59.8	
12	20	nodeRight	21	6.7	-18.8	-29.1	F (65)	46.0	3	21.0	1.300	1.000	25.6	< 59.8	
12	21	nodeLeft	21	4.5	-13.2	-46.7	F (65)	46.0	3	21.0	1.300	1.000	17.6	< 59.8	
12	21	nodeRight	21	4.5	-13.2	-46.7	F (65)	46.0	3	21.0	1.300	1.000	17.6	< 59.8	
13	22	nodeLeft	21	2.2	-6.6	-37.0	F (65)	46.0	3	21.0	1.300	1.000	8.8	< 59.8	
13	22	nodeRight	21	2.2	-6.6	-37.0	F (65)	46.0	3	21.0	1.300	1.000	8.8	< 59.8	
13	23	nodeLeft	21	0.0	0.0	0.0	F (65)	46.0	3	21.0	1.300	1.000	0.0	< 59.8	

Steel I Girder G3

node L.FLG-MAX (LowerFlangeStress MAX)

Sec	node	Flange	t	σ_{tmax}	σ_{tmin}	σ_d	Grade	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	Stress		Cycle
													$\Delta \sigma_{max}$	CR • Ct	
			(mm)	(N/mm ²)		(Δ σ f)						(N/mm ²)	(N/mm ²)	D	
1	1	nodeRight	19	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
1	2	nodeLeft	19	6.9	-2.3	38.6	D (100)	84.0	3	39.0	1.000	1.000	9.2	< 84.0	
1	2	nodeRight	19	6.9	-2.3	38.6	D (100)	84.0	3	39.0	1.000	1.000	9.2	< 84.0	
2	3	nodeLeft	19	13.7	-4.7	48.8	D (100)	84.0	3	39.0	1.000	1.000	18.4	< 84.0	
2	3	nodeRight	19	13.7	-4.7	48.8	D (100)	84.0	3	39.0	1.000	1.000	18.4	< 84.0	
2	4	nodeLeft	19	19.7	-7.0	30.3	D (100)	84.0	3	39.0	1.000	1.000	26.7	< 84.0	
2	4	nodeRight	19	19.7	-7.0	30.3	D (100)	84.0	3	39.0	1.000	1.000	26.7	< 84.0	
3	5	nodeLeft	21	9.8	-8.5	-5.2	D (100)	84.0	3	39.0	1.132	1.000	18.2	< 95.1	
3	5	nodeRight	21	9.8	-8.5	-5.2	D (100)	84.0	3	39.0	1.132	1.000	18.2	< 95.1	
4	6	nodeLeft	27	2.6	-8.8	-56.5	D (100)	84.0	3	39.0	1.300	0.981	11.3	<107.1	
4	6	nodeRight	27	2.6	-8.8	-56.5	D (100)	84.0	3	39.0	1.300	0.981	11.3	<107.1	
4	7	nodeLeft	27	2.0	-10.2	-124.3	D (100)	84.0	3	39.0	1.300	0.981	12.2	<107.1	
4	7	nodeRight	27	2.0	-10.2	-124.3	D (100)	84.0	3	39.0	1.300	0.981	12.2	<107.1	
5	8	nodeLeft	21	1.9	-6.8	-56.4	D (100)	84.0	3	39.0	1.300	1.000	8.8	<109.2	
5	8	nodeRight	21	1.9	-6.8	-56.4	D (100)	84.0	3	39.0	1.300	1.000	8.8	<109.2	
5	9	nodeLeft	21	6.4	-5.8	12.2	D (100)	84.0	3	39.0	1.000	1.000	12.2	< 84.0	
5	9	nodeRight	21	6.4	-5.8	12.2	D (100)	84.0	3	39.0	1.000	1.000	12.2	< 84.0	
6	10	nodeLeft	19	13.9	-4.8	60.5	D (100)	84.0	3	39.0	1.000	1.000	18.8	< 84.0	
6	10	nodeRight	19	13.9	-4.8	60.5	D (100)	84.0	3	39.0	1.000	1.000	18.8	< 84.0	
6	11	nodeLeft	19	20.5	-4.4	86.0	D (100)	84.0	3	39.0	1.000	1.000	24.9	< 84.0	
6	11	nodeRight	19	20.5	-4.4	86.0	D (100)	84.0	3	39.0	1.000	1.000	24.9	< 84.0	
7	12	nodeLeft	19	21.4	-2.8	104.5	D (100)	84.0	3	39.0	1.000	1.000	24.2	< 84.0	
7	12	nodeRight	19	21.4	-2.8	104.5	D (100)	84.0	3	39.0	1.000	1.000	24.2	< 84.0	
8	13	nodeLeft	19	20.5	-4.4	86.0	D (100)	84.0	3	39.0	1.000	1.000	24.9	< 84.0	
8	13	nodeRight	19	20.5	-4.4	86.0	D (100)	84.0	3	39.0	1.000	1.000	24.9	< 84.0	
8	14	nodeLeft	19	13.9	-4.8	60.5	D (100)	84.0	3	39.0	1.000	1.000	18.8	< 84.0	
8	14	nodeRight	19	13.9	-4.8	60.5	D (100)	84.0	3	39.0	1.000	1.000	18.8	< 84.0	
9	15	nodeLeft	21	6.4	-5.8	12.2	D (100)	84.0	3	39.0	1.000	1.000	12.2	< 84.0	
9	15	nodeRight	21	6.4	-5.8	12.2	D (100)	84.0	3	39.0	1.000	1.000	12.2	< 84.0	
9	16	nodeLeft	21	1.9	-6.8	-56.4	D (100)	84.0	3	39.0	1.300	1.000	8.8	<109.2	
9	16	nodeRight	21	1.9	-6.8	-56.4	D (100)	84.0	3	39.0	1.300	1.000	8.8	<109.2	
10	17	nodeLeft	27	2.0	-10.2	-124.3	D (100)	84.0	3	39.0	1.300	0.981	12.2	<107.1	
10	17	nodeRight	27	2.0	-10.2	-124.3	D (100)	84.0	3	39.0	1.300	0.981	12.2	<107.1	
10	18	nodeLeft	27	2.6	-8.8	-56.5	D (100)	84.0	3	39.0	1.300	0.981	11.3	<107.1	
10	18	nodeRight	27	2.6	-8.8	-56.5	D (100)	84.0	3	39.0	1.300	0.981	11.3	<107.1	
11	19	nodeLeft	21	9.8	-8.5	-5.2	D (100)	84.0	3	39.0	1.132	1.000	18.2	< 95.1	
11	19	nodeRight	21	9.8	-8.5	-5.2	D (100)	84.0	3	39.0	1.132	1.000	18.2	< 95.1	
12	20	nodeLeft	19	19.7	-7.0	30.3	D (100)	84.0	3	39.0	1.000	1.000	26.7	< 84.0	
12	20	nodeRight	19	19.7	-7.0	30.3	D (100)	84.0	3	39.0	1.000	1.000	26.7	< 84.0	
12	21	nodeLeft	19	13.7	-4.7	48.8	D (100)	84.0	3	39.0	1.000	1.000	18.4	< 84.0	
12	21	nodeRight	19	13.7	-4.7	48.8	D (100)	84.0	3	39.0	1.000	1.000	18.4	< 84.0	
13	22	nodeLeft	19	6.9	-2.3	38.6	D (100)	84.0	3	39.0	1.000	1.000	9.2	< 84.0	
13	22	nodeRight	19	6.9	-2.3	38.6	D (100)	84.0	3	39.0	1.000	1.000	9.2	< 84.0	
13	23	nodeLeft	19	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	

Steel I Girder G3

node WEB-U-1 (WebUpper edge) WEB - 1

Sec	node	Web	h	t	Grade					Stress						
					σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D
					(N/mm ²)					(N/mm ²)						
1	1	nodeRight	2400	21	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
1	2	nodeLeft	2400	21	0	2.2	-6.5	-36.3	E(80)	62.0	3	29.0	1.300	1.000	8.7	< 80.6
1	2	nodeRight	2400	21	0	2.2	-6.5	-36.3	E(80)	62.0	3	29.0	1.300	1.000	8.7	< 80.6
2	3	nodeLeft	2400	21	0	4.4	-12.9	-45.9	E(80)	62.0	3	29.0	1.300	1.000	17.3	< 80.6
2	3	nodeRight	2400	21	0	4.4	-12.9	-45.9	E(80)	62.0	3	29.0	1.300	1.000	17.3	< 80.6
2	4	nodeLeft	2400	21	0	6.6	-18.5	-28.5	E(80)	62.0	3	29.0	1.300	1.000	25.1	< 80.6
2	4	nodeRight	2400	21	0	6.6	-18.5	-28.5	E(80)	62.0	3	29.0	1.300	1.000	25.1	< 80.6
3	5	nodeLeft	2400	19	0	8.7	-10.0	5.4	E(80)	62.0	3	29.0	1.000	1.000	18.7	< 62.0
3	5	nodeRight	2400	19	0	8.7	-10.0	5.4	E(80)	62.0	3	29.0	1.000	1.000	18.7	< 62.0
4	6	nodeLeft	2400	21	0	9.7	-2.8	62.7	E(80)	62.0	3	29.0	1.000	1.000	12.6	< 62.0
4	6	nodeRight	2400	21	0	9.7	-2.8	62.7	E(80)	62.0	3	29.0	1.000	1.000	12.6	< 62.0
4	7	nodeLeft	2400	21	0	11.3	-2.2	137.9	E(80)	62.0	3	29.0	1.000	1.000	13.5	< 62.0
4	7	nodeRight	2400	21	0	11.3	-2.2	137.9	E(80)	62.0	3	29.0	1.000	1.000	13.5	< 62.0
5	8	nodeLeft	2400	19	0	7.0	-2.0	58.0	E(80)	62.0	3	29.0	1.000	1.000	9.0	< 62.0
5	8	nodeRight	2400	19	0	7.0	-2.0	58.0	E(80)	62.0	3	29.0	1.000	1.000	9.0	< 62.0
5	9	nodeLeft	2400	19	0	5.9	-6.6	-12.6	E(80)	62.0	3	29.0	1.300	1.000	12.6	< 80.6
5	9	nodeRight	2400	19	0	5.9	-6.6	-12.6	E(80)	62.0	3	29.0	1.300	1.000	12.6	< 80.6
6	10	nodeLeft	2400	24	0	4.3	-12.3	-53.3	E(80)	62.0	3	29.0	1.300	1.000	16.5	< 80.6
6	10	nodeRight	2400	24	0	4.3	-12.3	-53.3	E(80)	62.0	3	29.0	1.300	1.000	16.5	< 80.6
6	11	nodeLeft	2400	24	0	3.9	-18.0	-75.7	E(80)	62.0	3	29.0	1.300	1.000	22.0	< 80.6
6	11	nodeRight	2400	24	0	3.9	-18.0	-75.7	E(80)	62.0	3	29.0	1.300	1.000	22.0	< 80.6
7	12	nodeLeft	2400	24	0	2.4	-18.9	-92.1	E(80)	62.0	3	29.0	1.300	1.000	21.3	< 80.6
7	12	nodeRight	2400	24	0	2.4	-18.9	-92.1	E(80)	62.0	3	29.0	1.300	1.000	21.3	< 80.6
8	13	nodeLeft	2400	24	0	3.9	-18.0	-75.7	E(80)	62.0	3	29.0	1.300	1.000	22.0	< 80.6
8	13	nodeRight	2400	24	0	3.9	-18.0	-75.7	E(80)	62.0	3	29.0	1.300	1.000	22.0	< 80.6
8	14	nodeLeft	2400	24	0	4.3	-12.3	-53.3	E(80)	62.0	3	29.0	1.300	1.000	16.5	< 80.6
8	14	nodeRight	2400	24	0	4.3	-12.3	-53.3	E(80)	62.0	3	29.0	1.300	1.000	16.5	< 80.6
9	15	nodeLeft	2400	19	0	5.9	-6.6	-12.6	E(80)	62.0	3	29.0	1.300	1.000	12.6	< 80.6
9	15	nodeRight	2400	19	0	5.9	-6.6	-12.6	E(80)	62.0	3	29.0	1.300	1.000	12.6	< 80.6
9	16	nodeLeft	2400	19	0	7.0	-2.0	58.0	E(80)	62.0	3	29.0	1.000	1.000	9.0	< 62.0
9	16	nodeRight	2400	19	0	7.0	-2.0	58.0	E(80)	62.0	3	29.0	1.000	1.000	9.0	< 62.0
10	17	nodeLeft	2400	21	0	11.3	-2.2	137.9	E(80)	62.0	3	29.0	1.000	1.000	13.5	< 62.0
10	17	nodeRight	2400	21	0	11.3	-2.2	137.9	E(80)	62.0	3	29.0	1.000	1.000	13.5	< 62.0
10	18	nodeLeft	2400	21	0	9.7	-2.8	62.7	E(80)	62.0	3	29.0	1.000	1.000	12.6	< 62.0
10	18	nodeRight	2400	21	0	9.7	-2.8	62.7	E(80)	62.0	3	29.0	1.000	1.000	12.6	< 62.0
11	19	nodeLeft	2400	19	0	8.7	-10.0	5.4	E(80)	62.0	3	29.0	1.000	1.000	18.7	< 62.0
11	19	nodeRight	2400	19	0	8.7	-10.0	5.4	E(80)	62.0	3	29.0	1.000	1.000	18.7	< 62.0
12	20	nodeLeft	2400	21	0	6.6	-18.5	-28.5	E(80)	62.0	3	29.0	1.300	1.000	25.1	< 80.6
12	20	nodeRight	2400	21	0	6.6	-18.5	-28.5	E(80)	62.0	3	29.0	1.300	1.000	25.1	< 80.6
12	21	nodeLeft	2400	21	0	4.4	-12.9	-45.9	E(80)	62.0	3	29.0	1.300	1.000	17.3	< 80.6
12	21	nodeRight	2400	21	0	4.4	-12.9	-45.9	E(80)	62.0	3	29.0	1.300	1.000	17.3	< 80.6
13	22	nodeLeft	2400	21	0	2.2	-6.5	-36.3	E(80)	62.0	3	29.0	1.300	1.000	8.7	< 80.6
13	22	nodeRight	2400	21	0	2.2	-6.5	-36.3	E(80)	62.0	3	29.0	1.300	1.000	8.7	< 80.6
13	23	nodeLeft	2400	21	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6

Steel I Girder G3

node WEB-L-1 (WebLower edge) WEB - 1

Sec	node	Web	h	t	Grade					Stress						
					σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D
					(N/mm ²)					(N/mm ²)						
1	1	nodeRight	2400	19	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
1	2	nodeLeft	2400	19	0	6.8	-2.3	38.0	E(80)	62.0	3	29.0	1.000	1.000	9.1	< 62.0
1	2	nodeRight	2400	19	0	6.8	-2.3	38.0	E(80)	62.0	3	29.0	1.000	1.000	9.1	< 62.0
2	3	nodeLeft	2400	19	0	13.5	-4.6	48.0	E(80)	62.0	3	29.0	1.000	1.000	18.2	< 62.0
2	3	nodeRight	2400	19	0	13.5	-4.6	48.0	E(80)	62.0	3	29.0	1.000	1.000	18.2	< 62.0
2	4	nodeLeft	2400	19	0	19.4	-6.9	29.9	E(80)	62.0	3	29.0	1.000	1.000	26.3	< 62.0
2	4	nodeRight	2400	19	0	19.4	-6.9	29.9	E(80)	62.0	3	29.0	1.000	1.000	26.3	< 62.0
3	5	nodeLeft	2400	21	0	9.6	-8.3	-5.2	E(80)	62.0	3	29.0	1.132	1.000	17.9	< 70.2
3	5	nodeRight	2400	21	0	9.6	-8.3	-5.2	E(80)	62.0	3	29.0	1.132	1.000	17.9	< 70.2
4	6	nodeLeft	2400	27	0	2.5	-8.6	-55.2	E(80)	62.0	3	29.0	1.300	0.981	11.1	< 79.1
4	6	nodeRight	2400	27	0	2.5	-8.6	-55.2	E(80)	62.0	3	29.0	1.300	0.981	11.1	< 79.1
4	7	nodeLeft	2400	27	0	1.9	-10.0	-121.4	E(80)	62.0	3	29.0	1.300	0.981	11.9	< 79.1
4	7	nodeRight	2400	27	0	1.9	-10.0	-121.4	E(80)	62.0	3	29.0	1.300	0.981	11.9	< 79.1
5	8	nodeLeft	2400	21	0	1.9	-6.7	-55.4	E(80)	62.0	3	29.0	1.300	1.000	8.6	< 80.6
5	8	nodeRight	2400	21	0	1.9	-6.7	-55.4	E(80)	62.0	3	29.0	1.300	1.000	8.6	< 80.6
5	9	nodeLeft	2400	21	0	6.3	-5.7	12.0	E(80)	62.0	3	29.0	1.000	1.000	12.0	< 62.0
5	9	nodeRight	2400	21	0	6.3	-5.7	12.0	E(80)	62.0	3	29.0	1.000	1.000	12.0	< 62.0
6	10	nodeLeft	2400	19	0	13.7	-4.8	59.6	E(80)	62.0	3	29.0	1.000	1.000	18.5	< 62.0
6	10	nodeRight	2400	19	0	13.7	-4.8	59.6	E(80)	62.0	3	29.0	1.000	1.000	18.5	< 62.0
6	11	nodeLeft	2400	19	0	20.2	-4.4	84.7	E(80)	62.0	3	29.0	1.000	1.000	24.6	< 62.0
6	11	nodeRight	2400	19	0	20.2	-4.4	84.7	E(80)	62.0	3	29.0	1.000	1.000	24.6	< 62.0
7	12	nodeLeft	2400	19	0	21.1	-2.7	103.0	E(80)	62.0	3	29.0	1.000	1.000	23.8	< 62.0
7	12	nodeRight	2400	19	0	21.1	-2.7	103.0	E(80)	62.0	3	29.0	1.000	1.000	23.8	< 62.0
8	13	nodeLeft	2400	19	0	20.2	-4.4	84.7	E(80)	62.0	3	29.0	1.000	1.000	24.6	< 62.0
8	13	nodeRight	2400	19	0	20.2	-4.4	84.7	E(80)	62.0	3	29.0	1.000	1.000	24.6	< 62.0
8	14	nodeLeft	2400	19	0	13.7	-4.8	59.6	E(80)	62.0	3	29.0	1.000	1.000	18.5	< 62.0
8	14	nodeRight	2400	19	0	13.7	-4.8	59.6	E(80)	62.0	3	29.0	1.000	1.000	18.5	< 62.0
9	15	nodeLeft	2400	21	0	6.3	-5.7	12.0	E(80)	62.0	3	29.0	1.000	1.000	12.0	< 62.0
9	15	nodeRight	2400	21	0	6.3	-5.7	12.0	E(80)	62.0	3	29.0	1.000	1.000	12.0	< 62.0
9	16	nodeLeft	2400	21	0	1.9	-6.7	-55.4	E(80)	62.0	3	29.0	1.300	1.000	8.6	< 80.6
9	16	nodeRight	2400	21	0	1.9	-6.7	-55.4	E(80)	62.0	3	29.0	1.300	1.000	8.6	< 80.6
10	17	nodeLeft	2400	27	0	1.9	-10.0	-121.4	E(80)	62.0	3	29.0	1.300	0.981	11.9	< 79.1
10	17	nodeRight	2400	27	0	1.9	-10.0	-121.4	E(80)	62.0	3	29.0	1.300	0.981	11.9	< 79.1
10	18	nodeLeft	2400	27	0	2.5	-8.6	-55.2	E(80)	62.0	3	29.0	1.300	0.981	11.1	< 79.1
10	18	nodeRight	2400	27	0	2.5	-8.6	-55.2	E(80)	62.0	3	29.0	1.300	0.981	11.1	< 79.1
11	19	nodeLeft	2400	21	0	9.6	-8.3	-5.2	E(80)	62.0	3	29.0	1.132	1.000	17.9	< 70.2
11	19	nodeRight	2400	21	0	9.6	-8.3	-5.2	E(80)	62.0	3	29.0	1.132	1.000	17.9	< 70.2
12	20	nodeLeft	2400	19	0	19.4	-6.9	29.9	E(80)	62.0	3	29.0	1.000	1.000	26.3	< 62.0
12	20	nodeRight	2400	19	0	19.4	-6.9	29.9	E(80)	62.0	3	29.0	1.000	1.000	26.3	< 62.0
12	21	nodeLeft	2400	19	0	13.5	-4.6	48.0	E(80)	62.0	3	29.0	1.000	1.000	18.2	< 62.0
12	21	nodeRight	2400	19	0	13.5	-4.6	48.0	E(80)	62.0	3	29.0	1.000	1.000	18.2	< 62.0
13	22	nodeLeft	2400	19	0	6.8	-2.3	38.0	E(80)	62.0	3	29.0	1.000	1.000	9.1	< 62.0
13	22	nodeRight	2400	19	0	6.8	-2.3	38.0	E(80)	62.0	3	29.0	1.000	1.000	9.1	< 62.0
13	23	nodeLeft	2400	19	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6

Steel I Girder G3

node HSTIFF-1 (WebH-Stiffener) WEB - 1

Sec	node	Web	h	t	σ_{tmax}	σ_{tmin}	σ_d	Grade	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D	Stress
																		$\Delta \sigma_{ce} \cdot \text{Cycle}$
																	(N/mm^2)	
1	1	nodeRight	2400	12	480	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6	
1	2	nodeLeft	2400	12	480	1.3	-3.8	-21.5	G(50)	32.0	3	15.0	1.300	1.000	5.1	<	41.6	
1	2	nodeRight	2400	12	480	1.3	-3.8	-21.5	G(50)	32.0	3	15.0	1.300	1.000	5.1	<	41.6	
2	3	nodeLeft	2400	12	480	2.6	-7.6	-27.1	G(50)	32.0	3	15.0	1.300	1.000	10.2	<	41.6	
2	3	nodeRight	2400	12	480	2.6	-7.6	-27.1	G(50)	32.0	3	15.0	1.300	1.000	10.2	<	41.6	
2	4	nodeLeft	2400	12	480	3.9	-10.9	-16.9	G(50)	32.0	3	15.0	1.300	1.000	14.8	<	41.6	
2	4	nodeRight	2400	12	480	3.9	-10.9	-16.9	G(50)	32.0	3	15.0	1.300	1.000	14.8	<	41.6	
3	5	nodeLeft	2400	12	480	5.3	-6.1	3.3	G(50)	32.0	3	15.0	1.000	1.000	11.4	<	32.0	
3	5	nodeRight	2400	12	480	5.3	-6.1	3.3	G(50)	32.0	3	15.0	1.000	1.000	11.4	<	32.0	
4	6	nodeLeft	2400	12	480	1.4	-4.9	-31.6	G(50)	32.0	3	15.0	1.300	1.000	6.3	<	41.6	
4	6	nodeRight	2400	12	480	1.4	-4.9	-31.6	G(50)	32.0	3	15.0	1.300	1.000	6.3	<	41.6	
4	7	nodeLeft	2400	12	480	1.1	-5.7	-69.5	G(50)	32.0	3	15.0	1.300	1.000	6.8	<	41.6	
4	7	nodeRight	2400	12	480	1.1	-5.7	-69.5	G(50)	32.0	3	15.0	1.300	1.000	6.8	<	41.6	
5	8	nodeLeft	2400	12	480	1.1	-4.0	-32.7	G(50)	32.0	3	15.0	1.300	1.000	5.1	<	41.6	
5	8	nodeRight	2400	12	480	1.1	-4.0	-32.7	G(50)	32.0	3	15.0	1.300	1.000	5.1	<	41.6	
5	9	nodeLeft	2400	12	480	3.6	-4.0	-7.7	G(50)	32.0	3	15.0	1.300	1.000	7.6	<	41.6	
5	9	nodeRight	2400	12	480	3.6	-4.0	-7.7	G(50)	32.0	3	15.0	1.300	1.000	7.6	<	41.6	
6	10	nodeLeft	2400	12	480	2.5	-7.1	-30.7	G(50)	32.0	3	15.0	1.300	1.000	9.5	<	41.6	
6	10	nodeRight	2400	12	480	2.5	-7.1	-30.7	G(50)	32.0	3	15.0	1.300	1.000	9.5	<	41.6	
6	11	nodeLeft	2400	12	480	2.2	-10.4	-43.7	G(50)	32.0	3	15.0	1.300	1.000	12.7	<	41.6	
6	11	nodeRight	2400	12	480	2.2	-10.4	-43.7	G(50)	32.0	3	15.0	1.300	1.000	12.7	<	41.6	
7	12	nodeLeft	2400	12	480	1.4	-10.9	-53.1	G(50)	32.0	3	15.0	1.300	1.000	12.3	<	41.6	
7	12	nodeRight	2400	12	480	1.4	-10.9	-53.1	G(50)	32.0	3	15.0	1.300	1.000	12.3	<	41.6	
8	13	nodeLeft	2400	12	480	2.2	-10.4	-43.7	G(50)	32.0	3	15.0	1.300	1.000	12.7	<	41.6	
8	13	nodeRight	2400	12	480	2.2	-10.4	-43.7	G(50)	32.0	3	15.0	1.300	1.000	12.7	<	41.6	
8	14	nodeLeft	2400	12	480	2.5	-7.1	-30.7	G(50)	32.0	3	15.0	1.300	1.000	9.5	<	41.6	
8	14	nodeRight	2400	12	480	2.5	-7.1	-30.7	G(50)	32.0	3	15.0	1.300	1.000	9.5	<	41.6	
9	15	nodeLeft	2400	12	480	3.6	-4.0	-7.7	G(50)	32.0	3	15.0	1.300	1.000	7.6	<	41.6	
9	15	nodeRight	2400	12	480	3.6	-4.0	-7.7	G(50)	32.0	3	15.0	1.300	1.000	7.6	<	41.6	
9	16	nodeLeft	2400	12	480	1.1	-4.0	-32.7	G(50)	32.0	3	15.0	1.300	1.000	5.1	<	41.6	
9	16	nodeRight	2400	12	480	1.1	-4.0	-32.7	G(50)	32.0	3	15.0	1.300	1.000	5.1	<	41.6	
10	17	nodeLeft	2400	12	480	1.1	-5.7	-69.5	G(50)	32.0	3	15.0	1.300	1.000	6.8	<	41.6	
10	17	nodeRight	2400	12	480	1.1	-5.7	-69.5	G(50)	32.0	3	15.0	1.300	1.000	6.8	<	41.6	
10	18	nodeLeft	2400	12	480	1.4	-4.9	-31.6	G(50)	32.0	3	15.0	1.300	1.000	6.3	<	41.6	
10	18	nodeRight	2400	12	480	1.4	-4.9	-31.6	G(50)	32.0	3	15.0	1.300	1.000	6.3	<	41.6	
11	19	nodeLeft	2400	12	480	5.3	-6.1	3.3	G(50)	32.0	3	15.0	1.000	1.000	11.4	<	32.0	
11	19	nodeRight	2400	12	480	5.3	-6.1	3.3	G(50)	32.0	3	15.0	1.000	1.000	11.4	<	32.0	
12	20	nodeLeft	2400	12	480	3.9	-10.9	-16.9	G(50)	32.0	3	15.0	1.300	1.000	14.8	<	41.6	
12	20	nodeRight	2400	12	480	3.9	-10.9	-16.9	G(50)	32.0	3	15.0	1.300	1.000	14.8	<	41.6	
12	21	nodeLeft	2400	12	480	2.6	-7.6	-27.1	G(50)	32.0	3	15.0	1.300	1.000	10.2	<	41.6	
12	21	nodeRight	2400	12	480	2.6	-7.6	-27.1	G(50)	32.0	3	15.0	1.300	1.000	10.2	<	41.6	
13	22	nodeLeft	2400	12	480	1.3	-3.8	-21.5	G(50)	32.0	3	15.0	1.300	1.000	5.1	<	41.6	
13	22	nodeRight	2400	12	480	1.3	-3.8	-21.5	G(50)	32.0	3	15.0	1.300	1.000	5.1	<	41.6	
13	23	nodeLeft	2400	12	480	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6	

Steel I Girder G3

node POINT-U-1 (WebUpper) WEB - 1

Sec	node	Web	h	t	σ tmax	σ tmin	σ d	(Δ σ f)	Δ σ ce	m	Δ σ ve	CR	Ct	Stress		
														Δ σ ce • Cycle	Δ σ max CR • Ct	
														(N/mm2)		
1	1	nodeRight	2400	12	300	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
1	2	nodeLeft	2400	12	300	1.6	-4.8	-27.0	G(50)	32.0	3	15.0	1.300	1.000	6.4	< 41.6
1	2	nodeRight	2400	12	300	1.6	-4.8	-27.0	G(50)	32.0	3	15.0	1.300	1.000	6.4	< 41.6
2	3	nodeLeft	2400	12	300	3.3	-9.6	-34.1	G(50)	32.0	3	15.0	1.300	1.000	12.9	< 41.6
2	3	nodeRight	2400	12	300	3.3	-9.6	-34.1	G(50)	32.0	3	15.0	1.300	1.000	12.9	< 41.6
2	4	nodeLeft	2400	12	300	4.9	-13.8	-21.2	G(50)	32.0	3	15.0	1.300	1.000	18.7	< 41.6
2	4	nodeRight	2400	12	300	4.9	-13.8	-21.2	G(50)	32.0	3	15.0	1.300	1.000	18.7	< 41.6
3	5	nodeLeft	2400	12	300	6.6	-7.6	4.1	G(50)	32.0	3	15.0	1.000	1.000	14.2	< 32.0
3	5	nodeRight	2400	12	300	6.6	-7.6	4.1	G(50)	32.0	3	15.0	1.000	1.000	14.2	< 32.0
4	6	nodeLeft	2400	12	300	7.4	-2.2	48.0	G(50)	32.0	3	15.0	1.000	1.000	9.6	< 32.0
4	6	nodeRight	2400	12	300	7.4	-2.2	48.0	G(50)	32.0	3	15.0	1.000	1.000	9.6	< 32.0
4	7	nodeLeft	2400	12	300	8.7	-1.7	105.5	G(50)	32.0	3	15.0	1.000	1.000	10.3	< 32.0
4	7	nodeRight	2400	12	300	8.7	-1.7	105.5	G(50)	32.0	3	15.0	1.000	1.000	10.3	< 32.0
5	8	nodeLeft	2400	12	300	5.3	-1.5	43.8	G(50)	32.0	3	15.0	1.000	1.000	6.8	< 32.0
5	8	nodeRight	2400	12	300	5.3	-1.5	43.8	G(50)	32.0	3	15.0	1.000	1.000	6.8	< 32.0
5	9	nodeLeft	2400	12	300	4.5	-5.0	-9.5	G(50)	32.0	3	15.0	1.300	1.000	9.5	< 41.6
5	9	nodeRight	2400	12	300	4.5	-5.0	-9.5	G(50)	32.0	3	15.0	1.300	1.000	9.5	< 41.6
6	10	nodeLeft	2400	12	300	3.1	-9.0	-39.2	G(50)	32.0	3	15.0	1.300	1.000	12.2	< 41.6
6	10	nodeRight	2400	12	300	3.1	-9.0	-39.2	G(50)	32.0	3	15.0	1.300	1.000	12.2	< 41.6
6	11	nodeLeft	2400	12	300	2.9	-13.3	-55.7	G(50)	32.0	3	15.0	1.300	1.000	16.1	< 41.6
6	11	nodeRight	2400	12	300	2.9	-13.3	-55.7	G(50)	32.0	3	15.0	1.300	1.000	16.1	< 41.6
7	12	nodeLeft	2400	12	300	1.8	-13.9	-67.7	G(50)	32.0	3	15.0	1.300	1.000	15.7	< 41.6
7	12	nodeRight	2400	12	300	1.8	-13.9	-67.7	G(50)	32.0	3	15.0	1.300	1.000	15.7	< 41.6
8	13	nodeLeft	2400	12	300	2.9	-13.3	-55.7	G(50)	32.0	3	15.0	1.300	1.000	16.1	< 41.6
8	13	nodeRight	2400	12	300	2.9	-13.3	-55.7	G(50)	32.0	3	15.0	1.300	1.000	16.1	< 41.6
8	14	nodeLeft	2400	12	300	3.1	-9.0	-39.2	G(50)	32.0	3	15.0	1.300	1.000	12.2	< 41.6
8	14	nodeRight	2400	12	300	3.1	-9.0	-39.2	G(50)	32.0	3	15.0	1.300	1.000	12.2	< 41.6
9	15	nodeLeft	2400	12	300	4.5	-5.0	-9.5	G(50)	32.0	3	15.0	1.300	1.000	9.5	< 41.6
9	15	nodeRight	2400	12	300	4.5	-5.0	-9.5	G(50)	32.0	3	15.0	1.300	1.000	9.5	< 41.6
9	16	nodeLeft	2400	12	300	5.3	-1.5	43.8	G(50)	32.0	3	15.0	1.000	1.000	6.8	< 32.0
9	16	nodeRight	2400	12	300	5.3	-1.5	43.8	G(50)	32.0	3	15.0	1.000	1.000	6.8	< 32.0
10	17	nodeLeft	2400	12	300	8.7	-1.7	105.5	G(50)	32.0	3	15.0	1.000	1.000	10.3	< 32.0
10	17	nodeRight	2400	12	300	8.7	-1.7	105.5	G(50)	32.0	3	15.0	1.000	1.000	10.3	< 32.0
10	18	nodeLeft	2400	12	300	7.4	-2.2	48.0	G(50)	32.0	3	15.0	1.000	1.000	9.6	< 32.0
10	18	nodeRight	2400	12	300	7.4	-2.2	48.0	G(50)	32.0	3	15.0	1.000	1.000	9.6	< 32.0
11	19	nodeLeft	2400	12	300	6.6	-7.6	4.1	G(50)	32.0	3	15.0	1.000	1.000	14.2	< 32.0
11	19	nodeRight	2400	12	300	6.6	-7.6	4.1	G(50)	32.0	3	15.0	1.000	1.000	14.2	< 32.0
12	20	nodeLeft	2400	12	300	4.9	-13.8	-21.2	G(50)	32.0	3	15.0	1.300	1.000	18.7	< 41.6
12	20	nodeRight	2400	12	300	4.9	-13.8	-21.2	G(50)	32.0	3	15.0	1.300	1.000	18.7	< 41.6
12	21	nodeLeft	2400	12	300	3.3	-9.6	-34.1	G(50)	32.0	3	15.0	1.300	1.000	12.9	< 41.6
12	21	nodeRight	2400	12	300	3.3	-9.6	-34.1	G(50)	32.0	3	15.0	1.300	1.000	12.9	< 41.6
13	22	nodeLeft	2400	12	300	1.6	-4.8	-27.0	G(50)	32.0	3	15.0	1.300	1.000	6.4	< 41.6
13	22	nodeRight	2400	12	300	1.6	-4.8	-27.0	G(50)	32.0	3	15.0	1.300	1.000	6.4	< 41.6
13	23	nodeLeft	2400	12	300	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6

Steel I Girder G3

node POINT-L-1 (WebLower) WEB - 1

Sec	node	Web	h	t	Grade					Stress						
					σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D
					(N/mm ²)					(N/mm ²)						
1	1	nodeRight	2400	12	400	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
1	2	nodeLeft	2400	12	400	4.6	-1.6	25.7	G(50)	32.0	3	15.0	1.000	1.000	6.1	< 32.0
1	2	nodeRight	2400	12	400	4.6	-1.6	25.7	G(50)	32.0	3	15.0	1.000	1.000	6.1	< 32.0
2	3	nodeLeft	2400	12	400	9.1	-3.1	32.4	G(50)	32.0	3	15.0	1.000	1.000	12.2	< 32.0
2	3	nodeRight	2400	12	400	9.1	-3.1	32.4	G(50)	32.0	3	15.0	1.000	1.000	12.2	< 32.0
2	4	nodeLeft	2400	12	400	13.1	-4.7	20.1	G(50)	32.0	3	15.0	1.000	1.000	17.7	< 32.0
2	4	nodeRight	2400	12	400	13.1	-4.7	20.1	G(50)	32.0	3	15.0	1.000	1.000	17.7	< 32.0
3	5	nodeLeft	2400	12	400	6.3	-5.5	-3.4	G(50)	32.0	3	15.0	1.132	1.000	11.8	< 36.2
3	5	nodeRight	2400	12	400	6.3	-5.5	-3.4	G(50)	32.0	3	15.0	1.132	1.000	11.8	< 36.2
4	6	nodeLeft	2400	12	400	1.6	-5.5	-35.6	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
4	6	nodeRight	2400	12	400	1.6	-5.5	-35.6	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
4	7	nodeLeft	2400	12	400	1.2	-6.4	-78.2	G(50)	32.0	3	15.0	1.300	1.000	7.7	< 41.6
4	7	nodeRight	2400	12	400	1.2	-6.4	-78.2	G(50)	32.0	3	15.0	1.300	1.000	7.7	< 41.6
5	8	nodeLeft	2400	12	400	1.3	-4.4	-36.5	G(50)	32.0	3	15.0	1.300	1.000	5.7	< 41.6
5	8	nodeRight	2400	12	400	1.3	-4.4	-36.5	G(50)	32.0	3	15.0	1.300	1.000	5.7	< 41.6
5	9	nodeLeft	2400	12	400	4.2	-3.7	7.9	G(50)	32.0	3	15.0	1.000	1.000	7.9	< 32.0
5	9	nodeRight	2400	12	400	4.2	-3.7	7.9	G(50)	32.0	3	15.0	1.000	1.000	7.9	< 32.0
6	10	nodeLeft	2400	12	400	9.4	-3.3	40.8	G(50)	32.0	3	15.0	1.000	1.000	12.7	< 32.0
6	10	nodeRight	2400	12	400	9.4	-3.3	40.8	G(50)	32.0	3	15.0	1.000	1.000	12.7	< 32.0
6	11	nodeLeft	2400	12	400	13.8	-3.0	58.0	G(50)	32.0	3	15.0	1.000	1.000	16.8	< 32.0
6	11	nodeRight	2400	12	400	13.8	-3.0	58.0	G(50)	32.0	3	15.0	1.000	1.000	16.8	< 32.0
7	12	nodeLeft	2400	12	400	14.5	-1.9	70.5	G(50)	32.0	3	15.0	1.000	1.000	16.3	< 32.0
7	12	nodeRight	2400	12	400	14.5	-1.9	70.5	G(50)	32.0	3	15.0	1.000	1.000	16.3	< 32.0
8	13	nodeLeft	2400	12	400	13.8	-3.0	58.0	G(50)	32.0	3	15.0	1.000	1.000	16.8	< 32.0
8	13	nodeRight	2400	12	400	13.8	-3.0	58.0	G(50)	32.0	3	15.0	1.000	1.000	16.8	< 32.0
8	14	nodeLeft	2400	12	400	9.4	-3.3	40.8	G(50)	32.0	3	15.0	1.000	1.000	12.7	< 32.0
8	14	nodeRight	2400	12	400	9.4	-3.3	40.8	G(50)	32.0	3	15.0	1.000	1.000	12.7	< 32.0
9	15	nodeLeft	2400	12	400	4.2	-3.7	7.9	G(50)	32.0	3	15.0	1.000	1.000	7.9	< 32.0
9	15	nodeRight	2400	12	400	4.2	-3.7	7.9	G(50)	32.0	3	15.0	1.000	1.000	7.9	< 32.0
9	16	nodeLeft	2400	12	400	1.3	-4.4	-36.5	G(50)	32.0	3	15.0	1.300	1.000	5.7	< 41.6
9	16	nodeRight	2400	12	400	1.3	-4.4	-36.5	G(50)	32.0	3	15.0	1.300	1.000	5.7	< 41.6
10	17	nodeLeft	2400	12	400	1.2	-6.4	-78.2	G(50)	32.0	3	15.0	1.300	1.000	7.7	< 41.6
10	17	nodeRight	2400	12	400	1.2	-6.4	-78.2	G(50)	32.0	3	15.0	1.300	1.000	7.7	< 41.6
10	18	nodeLeft	2400	12	400	1.6	-5.5	-35.6	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
10	18	nodeRight	2400	12	400	1.6	-5.5	-35.6	G(50)	32.0	3	15.0	1.300	1.000	7.1	< 41.6
11	19	nodeLeft	2400	12	400	6.3	-5.5	-3.4	G(50)	32.0	3	15.0	1.132	1.000	11.8	< 36.2
11	19	nodeRight	2400	12	400	6.3	-5.5	-3.4	G(50)	32.0	3	15.0	1.132	1.000	11.8	< 36.2
12	20	nodeLeft	2400	12	400	13.1	-4.7	20.1	G(50)	32.0	3	15.0	1.000	1.000	17.7	< 32.0
12	20	nodeRight	2400	12	400	13.1	-4.7	20.1	G(50)	32.0	3	15.0	1.000	1.000	17.7	< 32.0
12	21	nodeLeft	2400	12	400	9.1	-3.1	32.4	G(50)	32.0	3	15.0	1.000	1.000	12.2	< 32.0
12	21	nodeRight	2400	12	400	9.1	-3.1	32.4	G(50)	32.0	3	15.0	1.000	1.000	12.2	< 32.0
13	22	nodeLeft	2400	12	400	4.6	-1.6	25.7	G(50)	32.0	3	15.0	1.000	1.000	6.1	< 32.0
13	22	nodeRight	2400	12	400	4.6	-1.6	25.7	G(50)	32.0	3	15.0	1.000	1.000	6.1	< 32.0
13	23	nodeLeft	2400	12	400	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6

4. G4

Steel I Girder G4

node U.FLG-MAX (UpperFlangeStress MAX)

Sec	node	Flange	Grade					Stress		CR	Ct	$\Delta \sigma_{max}$	CR • Ct	Cycle	
			t	σ_{tmax}	σ_{tmin}	σ_d	($\Delta \sigma_f$)	$\Delta \sigma_{ce}$	$\Delta \sigma_{ve}$						(N/mm2)
1	1	nodeRight	21	0.0	0.0	0.0	F (65)	46.0	3	21.0	1.300	1.000	0.0	< 59.8	
1	2	nodeLeft	21	3.5	-35.4	-31.4	F (65)	46.0	3	21.0	1.300	1.000	38.9	< 59.8	
1	2	nodeRight	21	3.5	-35.4	-31.4	F (65)	46.0	3	21.0	1.300	1.000	38.9	< 59.8	
2	3	nodeLeft	21	7.0	-42.0	-43.8	F (65)	46.0	3	21.0	1.300	1.000	49.0	< 59.8	
2	3	nodeRight	21	7.0	-42.0	-43.8	F (65)	46.0	3	21.0	1.300	1.000	49.0	< 59.8	
2	4	nodeLeft	21	10.5	-30.4	-37.2	F (65)	46.0	3	21.0	1.300	1.000	40.9	< 59.8	
2	4	nodeRight	21	10.5	-30.4	-37.2	F (65)	46.0	3	21.0	1.300	1.000	40.9	< 59.8	
3	5	nodeLeft	19	14.9	-37.4	7.7	F (65)	46.0	3	21.0	1.032	1.000	52.2	> 47.5	0.54 < 1
3	5	nodeRight	19	14.9	-37.4	7.7	F (65)	46.0	3	21.0	1.032	1.000	52.2	> 47.5	0.54 < 1
4	6	nodeLeft	22	16.1	-20.0	65.3	F (65)	46.0	3	21.0	1.000	1.000	36.1	< 46.0	
4	6	nodeRight	22	16.1	-20.0	65.3	F (65)	46.0	3	21.0	1.000	1.000	36.1	< 46.0	
4	7	nodeLeft	22	22.5	-3.5	134.0	F (65)	46.0	3	21.0	1.000	1.000	26.0	< 46.0	
4	7	nodeRight	22	22.5	-3.5	134.0	F (65)	46.0	3	21.0	1.000	1.000	26.0	< 46.0	
5	8	nodeLeft	19	12.8	-18.9	65.2	F (65)	46.0	3	21.0	1.000	1.000	31.7	< 46.0	
5	8	nodeRight	19	12.8	-18.9	65.2	F (65)	46.0	3	21.0	1.000	1.000	31.7	< 46.0	
5	9	nodeLeft	19	11.2	-36.1	-5.9	F (65)	46.0	3	21.0	1.217	1.000	47.3	< 56.0	
5	9	nodeRight	19	11.2	-36.1	-5.9	F (65)	46.0	3	21.0	1.217	1.000	47.3	< 56.0	
6	10	nodeLeft	25	7.1	-33.9	-52.6	F (65)	46.0	3	21.0	1.300	1.000	41.1	< 59.8	
6	10	nodeRight	25	7.1	-33.9	-52.6	F (65)	46.0	3	21.0	1.300	1.000	41.1	< 59.8	
6	11	nodeLeft	25	5.6	-30.5	-86.5	F (65)	46.0	3	21.0	1.300	1.000	36.1	< 59.8	
6	11	nodeRight	25	5.6	-30.5	-86.5	F (65)	46.0	3	21.0	1.300	1.000	36.1	< 59.8	
7	12	nodeLeft	25	3.9	-33.1	-91.2	F (65)	46.0	3	21.0	1.300	1.000	37.0	< 59.8	
7	12	nodeRight	25	3.9	-33.1	-91.2	F (65)	46.0	3	21.0	1.300	1.000	37.0	< 59.8	
8	13	nodeLeft	25	5.6	-30.5	-86.5	F (65)	46.0	3	21.0	1.300	1.000	36.1	< 59.8	
8	13	nodeRight	25	5.6	-30.5	-86.5	F (65)	46.0	3	21.0	1.300	1.000	36.1	< 59.8	
8	14	nodeLeft	25	7.1	-33.9	-52.6	F (65)	46.0	3	21.0	1.300	1.000	41.1	< 59.8	
8	14	nodeRight	25	7.1	-33.9	-52.6	F (65)	46.0	3	21.0	1.300	1.000	41.1	< 59.8	
9	15	nodeLeft	19	11.2	-36.1	-5.9	F (65)	46.0	3	21.0	1.217	1.000	47.3	< 56.0	
9	15	nodeRight	19	11.2	-36.1	-5.9	F (65)	46.0	3	21.0	1.217	1.000	47.3	< 56.0	
9	16	nodeLeft	19	12.8	-18.9	65.2	F (65)	46.0	3	21.0	1.000	1.000	31.7	< 46.0	
9	16	nodeRight	19	12.8	-18.9	65.2	F (65)	46.0	3	21.0	1.000	1.000	31.7	< 46.0	
10	17	nodeLeft	22	22.5	-3.5	134.0	F (65)	46.0	3	21.0	1.000	1.000	26.0	< 46.0	
10	17	nodeRight	22	22.5	-3.5	134.0	F (65)	46.0	3	21.0	1.000	1.000	26.0	< 46.0	
10	18	nodeLeft	22	16.1	-20.0	65.3	F (65)	46.0	3	21.0	1.000	1.000	36.1	< 46.0	
10	18	nodeRight	22	16.1	-20.0	65.3	F (65)	46.0	3	21.0	1.000	1.000	36.1	< 46.0	
11	19	nodeLeft	19	14.9	-37.4	7.7	F (65)	46.0	3	21.0	1.032	1.000	52.2	> 47.5	0.54 < 1
11	19	nodeRight	19	14.9	-37.4	7.7	F (65)	46.0	3	21.0	1.032	1.000	52.2	> 47.5	0.54 < 1
12	20	nodeLeft	21	10.5	-30.4	-37.2	F (65)	46.0	3	21.0	1.300	1.000	40.9	< 59.8	
12	20	nodeRight	21	10.5	-30.4	-37.2	F (65)	46.0	3	21.0	1.300	1.000	40.9	< 59.8	
12	21	nodeLeft	21	7.0	-42.0	-43.8	F (65)	46.0	3	21.0	1.300	1.000	49.0	< 59.8	
12	21	nodeRight	21	7.0	-42.0	-43.8	F (65)	46.0	3	21.0	1.300	1.000	49.0	< 59.8	
13	22	nodeLeft	21	3.5	-35.4	-31.4	F (65)	46.0	3	21.0	1.300	1.000	38.9	< 59.8	
13	22	nodeRight	21	3.5	-35.4	-31.4	F (65)	46.0	3	21.0	1.300	1.000	38.9	< 59.8	
13	23	nodeLeft	21	0.0	0.0	0.0	F (65)	46.0	3	21.0	1.300	1.000	0.0	< 59.8	

Steel I Girder G4

node L.FLG-MAX (LowerFlangeStress MAX)

Sec	node	Flange	t	σ_{tmax}	σ_{tmin}	σ_d	Grade	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	Stress		Cycle
													$\Delta \sigma_{max}$	$CR \cdot Ct$	
			(mm)	(N/mm ²)		(Δ σ f)						(N/mm ²)	(N/mm ²)	D	
1	1	nodeRight	19	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
1	2	nodeLeft	19	37.0	-3.7	32.8	D (100)	84.0	3	39.0	1.000	1.000	40.7	< 84.0	
1	2	nodeRight	19	37.0	-3.7	32.8	D (100)	84.0	3	39.0	1.000	1.000	40.7	< 84.0	
2	3	nodeLeft	19	43.9	-7.3	45.8	D (100)	84.0	3	39.0	1.000	1.000	51.2	< 84.0	
2	3	nodeRight	19	43.9	-7.3	45.8	D (100)	84.0	3	39.0	1.000	1.000	51.2	< 84.0	
2	4	nodeLeft	19	31.8	-11.0	38.9	D (100)	84.0	3	39.0	1.000	1.000	42.8	< 84.0	
2	4	nodeRight	19	31.8	-11.0	38.9	D (100)	84.0	3	39.0	1.000	1.000	42.8	< 84.0	
3	5	nodeLeft	21	35.8	-14.2	-7.4	D (100)	84.0	3	39.0	1.000	1.000	50.0	< 84.0	
3	5	nodeRight	21	35.8	-14.2	-7.4	D (100)	84.0	3	39.0	1.000	1.000	50.0	< 84.0	
4	6	nodeLeft	29	17.5	-14.1	-57.0	D (100)	84.0	3	39.0	1.300	0.964	31.5	<105.2	
4	6	nodeRight	29	17.5	-14.1	-57.0	D (100)	84.0	3	39.0	1.300	0.964	31.5	<105.2	
4	7	nodeLeft	29	3.1	-19.6	-117.0	D (100)	84.0	3	39.0	1.300	0.964	22.7	<105.2	
4	7	nodeRight	29	3.1	-19.6	-117.0	D (100)	84.0	3	39.0	1.300	0.964	22.7	<105.2	
5	8	nodeLeft	21	18.1	-12.3	-62.4	D (100)	84.0	3	39.0	1.300	1.000	30.4	<109.2	
5	8	nodeRight	21	18.1	-12.3	-62.4	D (100)	84.0	3	39.0	1.300	1.000	30.4	<109.2	
5	9	nodeLeft	21	34.5	-10.8	5.6	D (100)	84.0	3	39.0	1.000	1.000	45.3	< 84.0	
5	9	nodeRight	21	34.5	-10.8	5.6	D (100)	84.0	3	39.0	1.000	1.000	45.3	< 84.0	
6	10	nodeLeft	19	38.5	-8.1	59.7	D (100)	84.0	3	39.0	1.000	1.000	46.5	< 84.0	
6	10	nodeRight	19	38.5	-8.1	59.7	D (100)	84.0	3	39.0	1.000	1.000	46.5	< 84.0	
6	11	nodeLeft	19	34.6	-6.3	98.0	D (100)	84.0	3	39.0	1.000	1.000	40.9	< 84.0	
6	11	nodeRight	19	34.6	-6.3	98.0	D (100)	84.0	3	39.0	1.000	1.000	40.9	< 84.0	
7	12	nodeLeft	19	37.5	-4.4	103.4	D (100)	84.0	3	39.0	1.000	1.000	42.0	< 84.0	
7	12	nodeRight	19	37.5	-4.4	103.4	D (100)	84.0	3	39.0	1.000	1.000	42.0	< 84.0	
8	13	nodeLeft	19	34.6	-6.3	98.0	D (100)	84.0	3	39.0	1.000	1.000	40.9	< 84.0	
8	13	nodeRight	19	34.6	-6.3	98.0	D (100)	84.0	3	39.0	1.000	1.000	40.9	< 84.0	
8	14	nodeLeft	19	38.5	-8.1	59.7	D (100)	84.0	3	39.0	1.000	1.000	46.5	< 84.0	
8	14	nodeRight	19	38.5	-8.1	59.7	D (100)	84.0	3	39.0	1.000	1.000	46.5	< 84.0	
9	15	nodeLeft	21	34.5	-10.8	5.6	D (100)	84.0	3	39.0	1.000	1.000	45.3	< 84.0	
9	15	nodeRight	21	34.5	-10.8	5.6	D (100)	84.0	3	39.0	1.000	1.000	45.3	< 84.0	
9	16	nodeLeft	21	18.1	-12.3	-62.4	D (100)	84.0	3	39.0	1.300	1.000	30.4	<109.2	
9	16	nodeRight	21	18.1	-12.3	-62.4	D (100)	84.0	3	39.0	1.300	1.000	30.4	<109.2	
10	17	nodeLeft	29	3.1	-19.6	-117.0	D (100)	84.0	3	39.0	1.300	0.964	22.7	<105.2	
10	17	nodeRight	29	3.1	-19.6	-117.0	D (100)	84.0	3	39.0	1.300	0.964	22.7	<105.2	
10	18	nodeLeft	29	17.5	-14.1	-57.0	D (100)	84.0	3	39.0	1.300	0.964	31.5	<105.2	
10	18	nodeRight	29	17.5	-14.1	-57.0	D (100)	84.0	3	39.0	1.300	0.964	31.5	<105.2	
11	19	nodeLeft	21	35.8	-14.2	-7.4	D (100)	84.0	3	39.0	1.000	1.000	50.0	< 84.0	
11	19	nodeRight	21	35.8	-14.2	-7.4	D (100)	84.0	3	39.0	1.000	1.000	50.0	< 84.0	
12	20	nodeLeft	19	31.8	-11.0	38.9	D (100)	84.0	3	39.0	1.000	1.000	42.8	< 84.0	
12	20	nodeRight	19	31.8	-11.0	38.9	D (100)	84.0	3	39.0	1.000	1.000	42.8	< 84.0	
12	21	nodeLeft	19	43.9	-7.3	45.8	D (100)	84.0	3	39.0	1.000	1.000	51.2	< 84.0	
12	21	nodeRight	19	43.9	-7.3	45.8	D (100)	84.0	3	39.0	1.000	1.000	51.2	< 84.0	
13	22	nodeLeft	19	37.0	-3.7	32.8	D (100)	84.0	3	39.0	1.000	1.000	40.7	< 84.0	
13	22	nodeRight	19	37.0	-3.7	32.8	D (100)	84.0	3	39.0	1.000	1.000	40.7	< 84.0	
13	23	nodeLeft	19	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	

Steel I Girder G4

node WEB-U-1 (WebUpper edge) WEB - 1

Sec	node	Web	h	t	Grade				Stress							
					σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D
					(N/mm ²)				(N/mm ²)							
1	1	nodeRight	2400	21	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
1	2	nodeLeft	2400	21	0	3.4	-34.8	-30.9	E(80)	62.0	3	29.0	1.300	1.000	38.2	< 80.6
1	2	nodeRight	2400	21	0	3.4	-34.8	-30.9	E(80)	62.0	3	29.0	1.300	1.000	38.2	< 80.6
2	3	nodeLeft	2400	21	0	6.9	-41.3	-43.1	E(80)	62.0	3	29.0	1.300	1.000	48.2	< 80.6
2	3	nodeRight	2400	21	0	6.9	-41.3	-43.1	E(80)	62.0	3	29.0	1.300	1.000	48.2	< 80.6
2	4	nodeLeft	2400	21	0	10.4	-29.9	-36.6	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
2	4	nodeRight	2400	21	0	10.4	-29.9	-36.6	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
3	5	nodeLeft	2400	19	0	14.6	-36.8	7.6	E(80)	62.0	3	29.0	1.032	1.000	51.4	< 64.0
3	5	nodeRight	2400	19	0	14.6	-36.8	7.6	E(80)	62.0	3	29.0	1.032	1.000	51.4	< 64.0
4	6	nodeLeft	2400	22	0	15.8	-19.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	35.5	< 62.0
4	6	nodeRight	2400	22	0	15.8	-19.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	35.5	< 62.0
4	7	nodeLeft	2400	22	0	22.1	-3.4	131.7	E(80)	62.0	3	29.0	1.000	1.000	25.5	< 62.0
4	7	nodeRight	2400	22	0	22.1	-3.4	131.7	E(80)	62.0	3	29.0	1.000	1.000	25.5	< 62.0
5	8	nodeLeft	2400	19	0	12.6	-18.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	31.2	< 62.0
5	8	nodeRight	2400	19	0	12.6	-18.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	31.2	< 62.0
5	9	nodeLeft	2400	19	0	11.1	-35.5	-5.8	E(80)	62.0	3	29.0	1.217	1.000	46.6	< 75.5
5	9	nodeRight	2400	19	0	11.1	-35.5	-5.8	E(80)	62.0	3	29.0	1.217	1.000	46.6	< 75.5
6	10	nodeLeft	2400	25	0	7.0	-33.2	-51.5	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
6	10	nodeRight	2400	25	0	7.0	-33.2	-51.5	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
6	11	nodeLeft	2400	25	0	5.4	-29.8	-84.5	E(80)	62.0	3	29.0	1.300	1.000	35.3	< 80.6
6	11	nodeRight	2400	25	0	5.4	-29.8	-84.5	E(80)	62.0	3	29.0	1.300	1.000	35.3	< 80.6
7	12	nodeLeft	2400	25	0	3.8	-32.4	-89.2	E(80)	62.0	3	29.0	1.300	1.000	36.2	< 80.6
7	12	nodeRight	2400	25	0	3.8	-32.4	-89.2	E(80)	62.0	3	29.0	1.300	1.000	36.2	< 80.6
8	13	nodeLeft	2400	25	0	5.4	-29.8	-84.5	E(80)	62.0	3	29.0	1.300	1.000	35.3	< 80.6
8	13	nodeRight	2400	25	0	5.4	-29.8	-84.5	E(80)	62.0	3	29.0	1.300	1.000	35.3	< 80.6
8	14	nodeLeft	2400	25	0	7.0	-33.2	-51.5	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
8	14	nodeRight	2400	25	0	7.0	-33.2	-51.5	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
9	15	nodeLeft	2400	19	0	11.1	-35.5	-5.8	E(80)	62.0	3	29.0	1.217	1.000	46.6	< 75.5
9	15	nodeRight	2400	19	0	11.1	-35.5	-5.8	E(80)	62.0	3	29.0	1.217	1.000	46.6	< 75.5
9	16	nodeLeft	2400	19	0	12.6	-18.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	31.2	< 62.0
9	16	nodeRight	2400	19	0	12.6	-18.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	31.2	< 62.0
10	17	nodeLeft	2400	22	0	22.1	-3.4	131.7	E(80)	62.0	3	29.0	1.000	1.000	25.5	< 62.0
10	17	nodeRight	2400	22	0	22.1	-3.4	131.7	E(80)	62.0	3	29.0	1.000	1.000	25.5	< 62.0
10	18	nodeLeft	2400	22	0	15.8	-19.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	35.5	< 62.0
10	18	nodeRight	2400	22	0	15.8	-19.6	64.2	E(80)	62.0	3	29.0	1.000	1.000	35.5	< 62.0
11	19	nodeLeft	2400	19	0	14.6	-36.8	7.6	E(80)	62.0	3	29.0	1.032	1.000	51.4	< 64.0
11	19	nodeRight	2400	19	0	14.6	-36.8	7.6	E(80)	62.0	3	29.0	1.032	1.000	51.4	< 64.0
12	20	nodeLeft	2400	21	0	10.4	-29.9	-36.6	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
12	20	nodeRight	2400	21	0	10.4	-29.9	-36.6	E(80)	62.0	3	29.0	1.300	1.000	40.2	< 80.6
12	21	nodeLeft	2400	21	0	6.9	-41.3	-43.1	E(80)	62.0	3	29.0	1.300	1.000	48.2	< 80.6
12	21	nodeRight	2400	21	0	6.9	-41.3	-43.1	E(80)	62.0	3	29.0	1.300	1.000	48.2	< 80.6
13	22	nodeLeft	2400	21	0	3.4	-34.8	-30.9	E(80)	62.0	3	29.0	1.300	1.000	38.2	< 80.6
13	22	nodeRight	2400	21	0	3.4	-34.8	-30.9	E(80)	62.0	3	29.0	1.300	1.000	38.2	< 80.6
13	23	nodeLeft	2400	21	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6

Steel I Girder G4

node WEB-L-1 (WebLower edge) WEB - 1

Sec	node	Web	h	t	Grade					Stress						
					σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D
					(N/mm ²)					(N/mm ²)						
1	1	nodeRight	2400	19	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
1	2	nodeLeft	2400	19	0	36.4	-3.6	32.3	E(80)	62.0	3	29.0	1.000	1.000	40.0	< 62.0
1	2	nodeRight	2400	19	0	36.4	-3.6	32.3	E(80)	62.0	3	29.0	1.000	1.000	40.0	< 62.0
2	3	nodeLeft	2400	19	0	43.2	-7.2	45.1	E(80)	62.0	3	29.0	1.000	1.000	50.4	< 62.0
2	3	nodeRight	2400	19	0	43.2	-7.2	45.1	E(80)	62.0	3	29.0	1.000	1.000	50.4	< 62.0
2	4	nodeLeft	2400	19	0	31.3	-10.8	38.3	E(80)	62.0	3	29.0	1.000	1.000	42.1	< 62.0
2	4	nodeRight	2400	19	0	31.3	-10.8	38.3	E(80)	62.0	3	29.0	1.000	1.000	42.1	< 62.0
3	5	nodeLeft	2400	21	0	35.1	-14.0	-7.2	E(80)	62.0	3	29.0	1.000	1.000	49.1	< 62.0
3	5	nodeRight	2400	21	0	35.1	-14.0	-7.2	E(80)	62.0	3	29.0	1.000	1.000	49.1	< 62.0
4	6	nodeLeft	2400	29	0	17.0	-13.7	-55.5	E(80)	62.0	3	29.0	1.300	0.964	30.7	< 77.7
4	6	nodeRight	2400	29	0	17.0	-13.7	-55.5	E(80)	62.0	3	29.0	1.300	0.964	30.7	< 77.7
4	7	nodeLeft	2400	29	0	3.0	-19.1	-114.0	E(80)	62.0	3	29.0	1.300	0.964	22.1	< 77.7
4	7	nodeRight	2400	29	0	3.0	-19.1	-114.0	E(80)	62.0	3	29.0	1.300	0.964	22.1	< 77.7
5	8	nodeLeft	2400	21	0	17.7	-12.1	-61.3	E(80)	62.0	3	29.0	1.300	1.000	29.8	< 80.6
5	8	nodeRight	2400	21	0	17.7	-12.1	-61.3	E(80)	62.0	3	29.0	1.300	1.000	29.8	< 80.6
5	9	nodeLeft	2400	21	0	33.9	-10.6	5.5	E(80)	62.0	3	29.0	1.000	1.000	44.5	< 62.0
5	9	nodeRight	2400	21	0	33.9	-10.6	5.5	E(80)	62.0	3	29.0	1.000	1.000	44.5	< 62.0
6	10	nodeLeft	2400	19	0	37.9	-7.9	58.8	E(80)	62.0	3	29.0	1.000	1.000	45.8	< 62.0
6	10	nodeRight	2400	19	0	37.9	-7.9	58.8	E(80)	62.0	3	29.0	1.000	1.000	45.8	< 62.0
6	11	nodeLeft	2400	19	0	34.1	-6.2	96.5	E(80)	62.0	3	29.0	1.000	1.000	40.3	< 62.0
6	11	nodeRight	2400	19	0	34.1	-6.2	96.5	E(80)	62.0	3	29.0	1.000	1.000	40.3	< 62.0
7	12	nodeLeft	2400	19	0	37.0	-4.4	101.9	E(80)	62.0	3	29.0	1.000	1.000	41.4	< 62.0
7	12	nodeRight	2400	19	0	37.0	-4.4	101.9	E(80)	62.0	3	29.0	1.000	1.000	41.4	< 62.0
8	13	nodeLeft	2400	19	0	34.1	-6.2	96.5	E(80)	62.0	3	29.0	1.000	1.000	40.3	< 62.0
8	13	nodeRight	2400	19	0	34.1	-6.2	96.5	E(80)	62.0	3	29.0	1.000	1.000	40.3	< 62.0
8	14	nodeLeft	2400	19	0	37.9	-7.9	58.8	E(80)	62.0	3	29.0	1.000	1.000	45.8	< 62.0
8	14	nodeRight	2400	19	0	37.9	-7.9	58.8	E(80)	62.0	3	29.0	1.000	1.000	45.8	< 62.0
9	15	nodeLeft	2400	21	0	33.9	-10.6	5.5	E(80)	62.0	3	29.0	1.000	1.000	44.5	< 62.0
9	15	nodeRight	2400	21	0	33.9	-10.6	5.5	E(80)	62.0	3	29.0	1.000	1.000	44.5	< 62.0
9	16	nodeLeft	2400	21	0	17.7	-12.1	-61.3	E(80)	62.0	3	29.0	1.300	1.000	29.8	< 80.6
9	16	nodeRight	2400	21	0	17.7	-12.1	-61.3	E(80)	62.0	3	29.0	1.300	1.000	29.8	< 80.6
10	17	nodeLeft	2400	29	0	3.0	-19.1	-114.0	E(80)	62.0	3	29.0	1.300	0.964	22.1	< 77.7
10	17	nodeRight	2400	29	0	3.0	-19.1	-114.0	E(80)	62.0	3	29.0	1.300	0.964	22.1	< 77.7
10	18	nodeLeft	2400	29	0	17.0	-13.7	-55.5	E(80)	62.0	3	29.0	1.300	0.964	30.7	< 77.7
10	18	nodeRight	2400	29	0	17.0	-13.7	-55.5	E(80)	62.0	3	29.0	1.300	0.964	30.7	< 77.7
11	19	nodeLeft	2400	21	0	35.1	-14.0	-7.2	E(80)	62.0	3	29.0	1.000	1.000	49.1	< 62.0
11	19	nodeRight	2400	21	0	35.1	-14.0	-7.2	E(80)	62.0	3	29.0	1.000	1.000	49.1	< 62.0
12	20	nodeLeft	2400	19	0	31.3	-10.8	38.3	E(80)	62.0	3	29.0	1.000	1.000	42.1	< 62.0
12	20	nodeRight	2400	19	0	31.3	-10.8	38.3	E(80)	62.0	3	29.0	1.000	1.000	42.1	< 62.0
12	21	nodeLeft	2400	19	0	43.2	-7.2	45.1	E(80)	62.0	3	29.0	1.000	1.000	50.4	< 62.0
12	21	nodeRight	2400	19	0	43.2	-7.2	45.1	E(80)	62.0	3	29.0	1.000	1.000	50.4	< 62.0
13	22	nodeLeft	2400	19	0	36.4	-3.6	32.3	E(80)	62.0	3	29.0	1.000	1.000	40.0	< 62.0
13	22	nodeRight	2400	19	0	36.4	-3.6	32.3	E(80)	62.0	3	29.0	1.000	1.000	40.0	< 62.0
13	23	nodeLeft	2400	19	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6

Steel I Girder G4

node HSTIFF-1 (WebH-Stiffener) WEB - 1

Sec	node	Web	h	t	σ_{tmax}	σ_{tmin}	σ_d	Grade	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D	Stress
																		$\Delta \sigma_{ce} \cdot \text{Cycle}$
																	(N/mm^2)	
1	1	nodeRight	2400	12	480	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6	
1	2	nodeLeft	2400	12	480	2.0	-20.5	-18.2	G(50)	32.0	3	15.0	1.300	1.000	22.6	<	41.6	
1	2	nodeRight	2400	12	480	2.0	-20.5	-18.2	G(50)	32.0	3	15.0	1.300	1.000	22.6	<	41.6	
2	3	nodeLeft	2400	12	480	4.1	-24.4	-25.4	G(50)	32.0	3	15.0	1.300	1.000	28.4	<	41.6	
2	3	nodeRight	2400	12	480	4.1	-24.4	-25.4	G(50)	32.0	3	15.0	1.300	1.000	28.4	<	41.6	
2	4	nodeLeft	2400	12	480	6.1	-17.6	-21.6	G(50)	32.0	3	15.0	1.300	1.000	23.7	<	41.6	
2	4	nodeRight	2400	12	480	6.1	-17.6	-21.6	G(50)	32.0	3	15.0	1.300	1.000	23.7	<	41.6	
3	5	nodeLeft	2400	12	480	8.9	-22.4	4.6	G(50)	32.0	3	15.0	1.032	1.000	31.3	<	33.0	
3	5	nodeRight	2400	12	480	8.9	-22.4	4.6	G(50)	32.0	3	15.0	1.032	1.000	31.3	<	33.0	
4	6	nodeLeft	2400	12	480	9.7	-7.8	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.5	<	41.6	
4	6	nodeRight	2400	12	480	9.7	-7.8	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.5	<	41.6	
4	7	nodeLeft	2400	12	480	1.7	-10.9	-64.9	G(50)	32.0	3	15.0	1.300	1.000	12.6	<	41.6	
4	7	nodeRight	2400	12	480	1.7	-10.9	-64.9	G(50)	32.0	3	15.0	1.300	1.000	12.6	<	41.6	
5	8	nodeLeft	2400	12	480	10.5	-7.1	-36.2	G(50)	32.0	3	15.0	1.300	1.000	17.6	<	41.6	
5	8	nodeRight	2400	12	480	10.5	-7.1	-36.2	G(50)	32.0	3	15.0	1.300	1.000	17.6	<	41.6	
5	9	nodeLeft	2400	12	480	6.7	-21.6	-3.5	G(50)	32.0	3	15.0	1.217	1.000	28.4	<	38.9	
5	9	nodeRight	2400	12	480	6.7	-21.6	-3.5	G(50)	32.0	3	15.0	1.217	1.000	28.4	<	38.9	
6	10	nodeLeft	2400	12	480	4.0	-19.0	-29.4	G(50)	32.0	3	15.0	1.300	1.000	23.0	<	41.6	
6	10	nodeRight	2400	12	480	4.0	-19.0	-29.4	G(50)	32.0	3	15.0	1.300	1.000	23.0	<	41.6	
6	11	nodeLeft	2400	12	480	3.1	-17.1	-48.3	G(50)	32.0	3	15.0	1.300	1.000	20.2	<	41.6	
6	11	nodeRight	2400	12	480	3.1	-17.1	-48.3	G(50)	32.0	3	15.0	1.300	1.000	20.2	<	41.6	
7	12	nodeLeft	2400	12	480	2.2	-18.5	-51.0	G(50)	32.0	3	15.0	1.300	1.000	20.7	<	41.6	
7	12	nodeRight	2400	12	480	2.2	-18.5	-51.0	G(50)	32.0	3	15.0	1.300	1.000	20.7	<	41.6	
8	13	nodeLeft	2400	12	480	3.1	-17.1	-48.3	G(50)	32.0	3	15.0	1.300	1.000	20.2	<	41.6	
8	13	nodeRight	2400	12	480	3.1	-17.1	-48.3	G(50)	32.0	3	15.0	1.300	1.000	20.2	<	41.6	
8	14	nodeLeft	2400	12	480	4.0	-19.0	-29.4	G(50)	32.0	3	15.0	1.300	1.000	23.0	<	41.6	
8	14	nodeRight	2400	12	480	4.0	-19.0	-29.4	G(50)	32.0	3	15.0	1.300	1.000	23.0	<	41.6	
9	15	nodeLeft	2400	12	480	6.7	-21.6	-3.5	G(50)	32.0	3	15.0	1.217	1.000	28.4	<	38.9	
9	15	nodeRight	2400	12	480	6.7	-21.6	-3.5	G(50)	32.0	3	15.0	1.217	1.000	28.4	<	38.9	
9	16	nodeLeft	2400	12	480	10.5	-7.1	-36.2	G(50)	32.0	3	15.0	1.300	1.000	17.6	<	41.6	
9	16	nodeRight	2400	12	480	10.5	-7.1	-36.2	G(50)	32.0	3	15.0	1.300	1.000	17.6	<	41.6	
10	17	nodeLeft	2400	12	480	1.7	-10.9	-64.9	G(50)	32.0	3	15.0	1.300	1.000	12.6	<	41.6	
10	17	nodeRight	2400	12	480	1.7	-10.9	-64.9	G(50)	32.0	3	15.0	1.300	1.000	12.6	<	41.6	
10	18	nodeLeft	2400	12	480	9.7	-7.8	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.5	<	41.6	
10	18	nodeRight	2400	12	480	9.7	-7.8	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.5	<	41.6	
11	19	nodeLeft	2400	12	480	8.9	-22.4	4.6	G(50)	32.0	3	15.0	1.032	1.000	31.3	<	33.0	
11	19	nodeRight	2400	12	480	8.9	-22.4	4.6	G(50)	32.0	3	15.0	1.032	1.000	31.3	<	33.0	
12	20	nodeLeft	2400	12	480	6.1	-17.6	-21.6	G(50)	32.0	3	15.0	1.300	1.000	23.7	<	41.6	
12	20	nodeRight	2400	12	480	6.1	-17.6	-21.6	G(50)	32.0	3	15.0	1.300	1.000	23.7	<	41.6	
12	21	nodeLeft	2400	12	480	4.1	-24.4	-25.4	G(50)	32.0	3	15.0	1.300	1.000	28.4	<	41.6	
12	21	nodeRight	2400	12	480	4.1	-24.4	-25.4	G(50)	32.0	3	15.0	1.300	1.000	28.4	<	41.6	
13	22	nodeLeft	2400	12	480	2.0	-20.5	-18.2	G(50)	32.0	3	15.0	1.300	1.000	22.6	<	41.6	
13	22	nodeRight	2400	12	480	2.0	-20.5	-18.2	G(50)	32.0	3	15.0	1.300	1.000	22.6	<	41.6	
13	23	nodeLeft	2400	12	480	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6	

Steel I Girder G4

node POINT-U-1 (WebUpper) WEB - 1

Sec	node	Web	h	t	σ tmax	σ tmin	σ d	Grade	(Δ σ f)	Δ σ ce	m	Δ σ ve	CR	Ct	Stress	
															Δ σ ce • Cycle	Δ σ max CR • Ct
															D	
															(N/mm2)	
1	1	nodeRight	2400	12	300	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
1	2	nodeLeft	2400	12	300	2.6	-25.9	-23.0	G(50)	32.0	3	15.0	1.300	1.000	28.5	< 41.6
1	2	nodeRight	2400	12	300	2.6	-25.9	-23.0	G(50)	32.0	3	15.0	1.300	1.000	28.5	< 41.6
2	3	nodeLeft	2400	12	300	5.1	-30.7	-32.0	G(50)	32.0	3	15.0	1.300	1.000	35.8	< 41.6
2	3	nodeRight	2400	12	300	5.1	-30.7	-32.0	G(50)	32.0	3	15.0	1.300	1.000	35.8	< 41.6
2	4	nodeLeft	2400	12	300	7.7	-22.2	-27.2	G(50)	32.0	3	15.0	1.300	1.000	29.9	< 41.6
2	4	nodeRight	2400	12	300	7.7	-22.2	-27.2	G(50)	32.0	3	15.0	1.300	1.000	29.9	< 41.6
3	5	nodeLeft	2400	12	300	11.1	-27.8	5.7	G(50)	32.0	3	15.0	1.032	1.000	38.9	> 33.0
3	5	nodeRight	2400	12	300	11.1	-27.8	5.7	G(50)	32.0	3	15.0	1.032	1.000	38.9	> 33.0
4	6	nodeLeft	2400	12	300	12.1	-15.1	49.2	G(50)	32.0	3	15.0	1.000	1.000	27.2	< 32.0
4	6	nodeRight	2400	12	300	12.1	-15.1	49.2	G(50)	32.0	3	15.0	1.000	1.000	27.2	< 32.0
4	7	nodeLeft	2400	12	300	16.9	-2.6	101.0	G(50)	32.0	3	15.0	1.000	1.000	19.6	< 32.0
4	7	nodeRight	2400	12	300	16.9	-2.6	101.0	G(50)	32.0	3	15.0	1.000	1.000	19.6	< 32.0
5	8	nodeLeft	2400	12	300	9.6	-14.0	48.5	G(50)	32.0	3	15.0	1.000	1.000	23.6	< 32.0
5	8	nodeRight	2400	12	300	9.6	-14.0	48.5	G(50)	32.0	3	15.0	1.000	1.000	23.6	< 32.0
5	9	nodeLeft	2400	12	300	8.4	-26.8	-4.4	G(50)	32.0	3	15.0	1.217	1.000	35.2	< 38.9
5	9	nodeRight	2400	12	300	8.4	-26.8	-4.4	G(50)	32.0	3	15.0	1.217	1.000	35.2	< 38.9
6	10	nodeLeft	2400	12	300	5.1	-24.3	-37.7	G(50)	32.0	3	15.0	1.300	1.000	29.4	< 41.6
6	10	nodeRight	2400	12	300	5.1	-24.3	-37.7	G(50)	32.0	3	15.0	1.300	1.000	29.4	< 41.6
6	11	nodeLeft	2400	12	300	4.0	-21.8	-61.9	G(50)	32.0	3	15.0	1.300	1.000	25.8	< 41.6
6	11	nodeRight	2400	12	300	4.0	-21.8	-61.9	G(50)	32.0	3	15.0	1.300	1.000	25.8	< 41.6
7	12	nodeLeft	2400	12	300	2.8	-23.7	-65.3	G(50)	32.0	3	15.0	1.300	1.000	26.5	< 41.6
7	12	nodeRight	2400	12	300	2.8	-23.7	-65.3	G(50)	32.0	3	15.0	1.300	1.000	26.5	< 41.6
8	13	nodeLeft	2400	12	300	4.0	-21.8	-61.9	G(50)	32.0	3	15.0	1.300	1.000	25.8	< 41.6
8	13	nodeRight	2400	12	300	4.0	-21.8	-61.9	G(50)	32.0	3	15.0	1.300	1.000	25.8	< 41.6
8	14	nodeLeft	2400	12	300	5.1	-24.3	-37.7	G(50)	32.0	3	15.0	1.300	1.000	29.4	< 41.6
8	14	nodeRight	2400	12	300	5.1	-24.3	-37.7	G(50)	32.0	3	15.0	1.300	1.000	29.4	< 41.6
9	15	nodeLeft	2400	12	300	8.4	-26.8	-4.4	G(50)	32.0	3	15.0	1.217	1.000	35.2	< 38.9
9	15	nodeRight	2400	12	300	8.4	-26.8	-4.4	G(50)	32.0	3	15.0	1.217	1.000	35.2	< 38.9
9	16	nodeLeft	2400	12	300	9.6	-14.0	48.5	G(50)	32.0	3	15.0	1.000	1.000	23.6	< 32.0
9	16	nodeRight	2400	12	300	9.6	-14.0	48.5	G(50)	32.0	3	15.0	1.000	1.000	23.6	< 32.0
10	17	nodeLeft	2400	12	300	16.9	-2.6	101.0	G(50)	32.0	3	15.0	1.000	1.000	19.6	< 32.0
10	17	nodeRight	2400	12	300	16.9	-2.6	101.0	G(50)	32.0	3	15.0	1.000	1.000	19.6	< 32.0
10	18	nodeLeft	2400	12	300	12.1	-15.1	49.2	G(50)	32.0	3	15.0	1.000	1.000	27.2	< 32.0
10	18	nodeRight	2400	12	300	12.1	-15.1	49.2	G(50)	32.0	3	15.0	1.000	1.000	27.2	< 32.0
11	19	nodeLeft	2400	12	300	11.1	-27.8	5.7	G(50)	32.0	3	15.0	1.032	1.000	38.9	> 33.0
11	19	nodeRight	2400	12	300	11.1	-27.8	5.7	G(50)	32.0	3	15.0	1.032	1.000	38.9	> 33.0
12	20	nodeLeft	2400	12	300	7.7	-22.2	-27.2	G(50)	32.0	3	15.0	1.300	1.000	29.9	< 41.6
12	20	nodeRight	2400	12	300	7.7	-22.2	-27.2	G(50)	32.0	3	15.0	1.300	1.000	29.9	< 41.6
12	21	nodeLeft	2400	12	300	5.1	-30.7	-32.0	G(50)	32.0	3	15.0	1.300	1.000	35.8	< 41.6
12	21	nodeRight	2400	12	300	5.1	-30.7	-32.0	G(50)	32.0	3	15.0	1.300	1.000	35.8	< 41.6
13	22	nodeLeft	2400	12	300	2.6	-25.9	-23.0	G(50)	32.0	3	15.0	1.300	1.000	28.5	< 41.6
13	22	nodeRight	2400	12	300	2.6	-25.9	-23.0	G(50)	32.0	3	15.0	1.300	1.000	28.5	< 41.6
13	23	nodeLeft	2400	12	300	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6

Steel I Girder G4

node POINT-L-1 (WebLower) WEB - 1

Sec	node	Web	Grade										Stress					
			h	t	σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D		
			(mm)		(N/mm ²)												(N/mm ²)	
1	1	nodeRight	2400	12	400	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6		
1	2	nodeLeft	2400	12	400	24.6	-2.4	21.8	G(50)	32.0	3	15.0	1.000	1.000	27.0	< 32.0		
1	2	nodeRight	2400	12	400	24.6	-2.4	21.8	G(50)	32.0	3	15.0	1.000	1.000	27.0	< 32.0		
2	3	nodeLeft	2400	12	400	29.1	-4.9	30.4	G(50)	32.0	3	15.0	1.000	1.000	34.0	> 32.0	0.36<1	
2	3	nodeRight	2400	12	400	29.1	-4.9	30.4	G(50)	32.0	3	15.0	1.000	1.000	34.0	> 32.0	0.36<1	
2	4	nodeLeft	2400	12	400	21.1	-7.3	25.8	G(50)	32.0	3	15.0	1.000	1.000	28.4	< 32.0		
2	4	nodeRight	2400	12	400	21.1	-7.3	25.8	G(50)	32.0	3	15.0	1.000	1.000	28.4	< 32.0		
3	5	nodeLeft	2400	12	400	23.1	-9.2	-4.8	G(50)	32.0	3	15.0	1.000	1.000	32.3	> 32.0	0.31<1	
3	5	nodeRight	2400	12	400	23.1	-9.2	-4.8	G(50)	32.0	3	15.0	1.000	1.000	32.3	> 32.0	0.31<1	
4	6	nodeLeft	2400	12	400	10.9	-8.8	-35.6	G(50)	32.0	3	15.0	1.300	1.000	19.7	< 41.6		
4	6	nodeRight	2400	12	400	10.9	-8.8	-35.6	G(50)	32.0	3	15.0	1.300	1.000	19.7	< 41.6		
4	7	nodeLeft	2400	12	400	1.9	-12.2	-73.1	G(50)	32.0	3	15.0	1.300	1.000	14.2	< 41.6		
4	7	nodeRight	2400	12	400	1.9	-12.2	-73.1	G(50)	32.0	3	15.0	1.300	1.000	14.2	< 41.6		
5	8	nodeLeft	2400	12	400	11.7	-8.0	-40.4	G(50)	32.0	3	15.0	1.300	1.000	19.6	< 41.6		
5	8	nodeRight	2400	12	400	11.7	-8.0	-40.4	G(50)	32.0	3	15.0	1.300	1.000	19.6	< 41.6		
5	9	nodeLeft	2400	12	400	22.4	-7.0	3.6	G(50)	32.0	3	15.0	1.000	1.000	29.3	< 32.0		
5	9	nodeRight	2400	12	400	22.4	-7.0	3.6	G(50)	32.0	3	15.0	1.000	1.000	29.3	< 32.0		
6	10	nodeLeft	2400	12	400	26.1	-5.5	40.4	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0		
6	10	nodeRight	2400	12	400	26.1	-5.5	40.4	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0		
6	11	nodeLeft	2400	12	400	23.4	-4.3	66.4	G(50)	32.0	3	15.0	1.000	1.000	27.7	< 32.0		
6	11	nodeRight	2400	12	400	23.4	-4.3	66.4	G(50)	32.0	3	15.0	1.000	1.000	27.7	< 32.0		
7	12	nodeLeft	2400	12	400	25.4	-3.0	70.0	G(50)	32.0	3	15.0	1.000	1.000	28.4	< 32.0		
7	12	nodeRight	2400	12	400	25.4	-3.0	70.0	G(50)	32.0	3	15.0	1.000	1.000	28.4	< 32.0		
8	13	nodeLeft	2400	12	400	23.4	-4.3	66.4	G(50)	32.0	3	15.0	1.000	1.000	27.7	< 32.0		
8	13	nodeRight	2400	12	400	23.4	-4.3	66.4	G(50)	32.0	3	15.0	1.000	1.000	27.7	< 32.0		
8	14	nodeLeft	2400	12	400	26.1	-5.5	40.4	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0		
8	14	nodeRight	2400	12	400	26.1	-5.5	40.4	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0		
9	15	nodeLeft	2400	12	400	22.4	-7.0	3.6	G(50)	32.0	3	15.0	1.000	1.000	29.3	< 32.0		
9	15	nodeRight	2400	12	400	22.4	-7.0	3.6	G(50)	32.0	3	15.0	1.000	1.000	29.3	< 32.0		
9	16	nodeLeft	2400	12	400	11.7	-8.0	-40.4	G(50)	32.0	3	15.0	1.300	1.000	19.6	< 41.6		
9	16	nodeRight	2400	12	400	11.7	-8.0	-40.4	G(50)	32.0	3	15.0	1.300	1.000	19.6	< 41.6		
10	17	nodeLeft	2400	12	400	1.9	-12.2	-73.1	G(50)	32.0	3	15.0	1.300	1.000	14.2	< 41.6		
10	17	nodeRight	2400	12	400	1.9	-12.2	-73.1	G(50)	32.0	3	15.0	1.300	1.000	14.2	< 41.6		
10	18	nodeLeft	2400	12	400	10.9	-8.8	-35.6	G(50)	32.0	3	15.0	1.300	1.000	19.7	< 41.6		
10	18	nodeRight	2400	12	400	10.9	-8.8	-35.6	G(50)	32.0	3	15.0	1.300	1.000	19.7	< 41.6		
11	19	nodeLeft	2400	12	400	23.1	-9.2	-4.8	G(50)	32.0	3	15.0	1.000	1.000	32.3	> 32.0	0.31<1	
11	19	nodeRight	2400	12	400	23.1	-9.2	-4.8	G(50)	32.0	3	15.0	1.000	1.000	32.3	> 32.0	0.31<1	
12	20	nodeLeft	2400	12	400	21.1	-7.3	25.8	G(50)	32.0	3	15.0	1.000	1.000	28.4	< 32.0		
12	20	nodeRight	2400	12	400	21.1	-7.3	25.8	G(50)	32.0	3	15.0	1.000	1.000	28.4	< 32.0		
12	21	nodeLeft	2400	12	400	29.1	-4.9	30.4	G(50)	32.0	3	15.0	1.000	1.000	34.0	> 32.0	0.36<1	
12	21	nodeRight	2400	12	400	29.1	-4.9	30.4	G(50)	32.0	3	15.0	1.000	1.000	34.0	> 32.0	0.36<1	
13	22	nodeLeft	2400	12	400	24.6	-2.4	21.8	G(50)	32.0	3	15.0	1.000	1.000	27.0	< 32.0		
13	22	nodeRight	2400	12	400	24.6	-2.4	21.8	G(50)	32.0	3	15.0	1.000	1.000	27.0	< 32.0		
13	23	nodeLeft	2400	12	400	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6		

5. G5

node U.FLG-MAX (UpperFlangeStress MAX)

Sec	node	Flange	Grade				Stress		Cycle				
			t	σ_{tmax}	σ_{tmin}	σ_d ($\Delta \sigma_f$)	$\Delta \sigma_{ce}$	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR · Ct	D
			(mm)	(N/mm ²)		(N/mm ²)	(N/mm ²)	(N/mm ²)	(N/mm ²)	(N/mm ²)	(N/mm ²)		
1	1	nodeRight	22	0.0	0.0	0.0 F (65)	46.0	3	21.0	1.300	1.000	0.0 < 59.8	
1	2	nodeLeft	22	4.9	-19.4	-43.5 F (65)	46.0	3	21.0	1.300	1.000	24.3 < 59.8	
1	2	nodeRight	22	4.9	-19.4	-43.5 F (65)	46.0	3	21.0	1.300	1.000	24.3 < 59.8	
2	3	nodeLeft	22	9.9	-33.9	-54.2 F (65)	46.0	3	21.0	1.300	1.000	43.8 < 59.8	
2	3	nodeRight	22	9.9	-33.9	-54.2 F (65)	46.0	3	21.0	1.300	1.000	43.8 < 59.8	
2	4	nodeLeft	22	14.8	-40.7	-32.1 F (65)	46.0	3	21.0	1.300	1.000	55.5 < 59.8	
2	4	nodeRight	22	14.8	-40.7	-32.1 F (65)	46.0	3	21.0	1.300	1.000	55.5 < 59.8	
3	5	nodeLeft	20	20.6	-27.2	9.7 F (65)	46.0	3	21.0	1.000	1.000	47.8 > 46.0	0.46 < 1
3	5	nodeRight	20	20.6	-27.2	9.7 F (65)	46.0	3	21.0	1.000	1.000	47.8 > 46.0	0.46 < 1
4	6	nodeLeft	31	18.6	-8.5	61.7 F (65)	46.0	3	21.0	1.000	0.948	27.2 < 43.6	
4	6	nodeRight	31	18.6	-8.5	61.7 F (65)	46.0	3	21.0	1.000	0.948	27.2 < 43.6	
4	7	nodeLeft	31	22.1	-4.4	132.9 F (65)	46.0	3	21.0	1.000	0.948	26.5 < 43.6	
4	7	nodeRight	31	22.1	-4.4	132.9 F (65)	46.0	3	21.0	1.000	0.948	26.5 < 43.6	
5	8	nodeLeft	19	16.8	-8.7	76.2 F (65)	46.0	3	21.0	1.000	1.000	25.5 < 46.0	
5	8	nodeRight	19	16.8	-8.7	76.2 F (65)	46.0	3	21.0	1.000	1.000	25.5 < 46.0	
5	9	nodeLeft	19	14.2	-20.6	-10.6 F (65)	46.0	3	21.0	1.223	1.000	34.8 < 56.3	
5	9	nodeRight	19	14.2	-20.6	-10.6 F (65)	46.0	3	21.0	1.223	1.000	34.8 < 56.3	
6	10	nodeLeft	26	10.0	-30.1	-59.4 F (65)	46.0	3	21.0	1.300	0.990	40.1 < 59.2	
6	10	nodeRight	26	10.0	-30.1	-59.4 F (65)	46.0	3	21.0	1.300	0.990	40.1 < 59.2	
6	11	nodeLeft	26	8.2	-41.0	-86.0 F (65)	46.0	3	21.0	1.300	0.990	49.3 < 59.2	
6	11	nodeRight	26	8.2	-41.0	-86.0 F (65)	46.0	3	21.0	1.300	0.990	49.3 < 59.2	
7	12	nodeLeft	26	5.7	-42.4	-95.5 F (65)	46.0	3	21.0	1.300	0.990	48.1 < 59.2	
7	12	nodeRight	26	5.7	-42.4	-95.5 F (65)	46.0	3	21.0	1.300	0.990	48.1 < 59.2	
8	13	nodeLeft	26	8.2	-41.0	-86.0 F (65)	46.0	3	21.0	1.300	0.990	49.3 < 59.2	
8	13	nodeRight	26	8.2	-41.0	-86.0 F (65)	46.0	3	21.0	1.300	0.990	49.3 < 59.2	
8	14	nodeLeft	26	10.0	-30.1	-59.4 F (65)	46.0	3	21.0	1.300	0.990	40.1 < 59.2	
8	14	nodeRight	26	10.0	-30.1	-59.4 F (65)	46.0	3	21.0	1.300	0.990	40.1 < 59.2	
9	15	nodeLeft	19	14.2	-20.6	-10.6 F (65)	46.0	3	21.0	1.223	1.000	34.8 < 56.3	
9	15	nodeRight	19	14.2	-20.6	-10.6 F (65)	46.0	3	21.0	1.223	1.000	34.8 < 56.3	
9	16	nodeLeft	19	16.8	-8.7	76.2 F (65)	46.0	3	21.0	1.000	1.000	25.5 < 46.0	
9	16	nodeRight	19	16.8	-8.7	76.2 F (65)	46.0	3	21.0	1.000	1.000	25.5 < 46.0	
10	17	nodeLeft	31	22.1	-4.4	132.9 F (65)	46.0	3	21.0	1.000	0.948	26.5 < 43.6	
10	17	nodeRight	31	22.1	-4.4	132.9 F (65)	46.0	3	21.0	1.000	0.948	26.5 < 43.6	
10	18	nodeLeft	31	18.6	-8.5	61.7 F (65)	46.0	3	21.0	1.000	0.948	27.2 < 43.6	
10	18	nodeRight	31	18.6	-8.5	61.7 F (65)	46.0	3	21.0	1.000	0.948	27.2 < 43.6	
11	19	nodeLeft	20	20.6	-27.2	9.7 F (65)	46.0	3	21.0	1.000	1.000	47.8 > 46.0	0.46 < 1
11	19	nodeRight	20	20.6	-27.2	9.7 F (65)	46.0	3	21.0	1.000	1.000	47.8 > 46.0	0.46 < 1
12	20	nodeLeft	22	14.8	-40.7	-32.1 F (65)	46.0	3	21.0	1.300	1.000	55.5 < 59.8	
12	20	nodeRight	22	14.8	-40.7	-32.1 F (65)	46.0	3	21.0	1.300	1.000	55.5 < 59.8	
12	21	nodeLeft	22	9.9	-33.9	-54.2 F (65)	46.0	3	21.0	1.300	1.000	43.8 < 59.8	
12	21	nodeRight	22	9.9	-33.9	-54.2 F (65)	46.0	3	21.0	1.300	1.000	43.8 < 59.8	
13	22	nodeLeft	22	4.9	-19.4	-43.5 F (65)	46.0	3	21.0	1.300	1.000	24.3 < 59.8	
13	22	nodeRight	22	4.9	-19.4	-43.5 F (65)	46.0	3	21.0	1.300	1.000	24.3 < 59.8	
13	23	nodeLeft	22	0.0	0.0	0.0 F (65)	46.0	3	21.0	1.300	1.000	0.0 < 59.8	

Steel I Girder G5

node L.FLG-MAX (LowerFlangeStress MAX)

Sec	node	Flange	t	σ_{tmax}	σ_{tmin}	σ_d	Grade	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	Stress	
													$\Delta \sigma_{max}$	Cycle
			(mm)	(N/mm ²)		(Δσf)						(N/mm ²)	(N/mm ²)	D
1	1	nodeRight	19	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2
1	2	nodeLeft	19	20.7	-5.3	46.4	D (100)	84.0	3	39.0	1.000	1.000	26.0	< 84.0
1	2	nodeRight	19	20.7	-5.3	46.4	D (100)	84.0	3	39.0	1.000	1.000	26.0	< 84.0
2	3	nodeLeft	19	36.2	-10.5	57.8	D (100)	84.0	3	39.0	1.000	1.000	46.8	< 84.0
2	3	nodeRight	19	36.2	-10.5	57.8	D (100)	84.0	3	39.0	1.000	1.000	46.8	< 84.0
2	4	nodeLeft	19	43.4	-15.8	34.2	D (100)	84.0	3	39.0	1.000	1.000	59.3	< 84.0
2	4	nodeRight	19	43.4	-15.8	34.2	D (100)	84.0	3	39.0	1.000	1.000	59.3	< 84.0
3	5	nodeLeft	23	25.5	-19.4	-9.1	D (100)	84.0	3	39.0	1.066	1.000	44.9	< 89.6
3	5	nodeRight	23	25.5	-19.4	-9.1	D (100)	84.0	3	39.0	1.066	1.000	44.9	< 89.6
4	6	nodeLeft	39	7.5	-16.4	-54.2	D (100)	84.0	3	39.0	1.300	0.895	23.9	< 97.7
4	6	nodeRight	39	7.5	-16.4	-54.2	D (100)	84.0	3	39.0	1.300	0.895	23.9	< 97.7
4	7	nodeLeft	39	3.9	-19.5	-116.8	D (100)	84.0	3	39.0	1.300	0.895	23.3	< 97.7
4	7	nodeRight	39	3.9	-19.5	-116.8	D (100)	84.0	3	39.0	1.300	0.895	23.3	< 97.7
5	8	nodeLeft	23	8.0	-15.4	-70.0	D (100)	84.0	3	39.0	1.300	1.000	23.4	<109.2
5	8	nodeRight	23	8.0	-15.4	-70.0	D (100)	84.0	3	39.0	1.300	1.000	23.4	<109.2
5	9	nodeLeft	23	18.9	-13.1	9.8	D (100)	84.0	3	39.0	1.000	1.000	32.0	< 84.0
5	9	nodeRight	23	18.9	-13.1	9.8	D (100)	84.0	3	39.0	1.000	1.000	32.0	< 84.0
6	10	nodeLeft	19	34.7	-11.6	68.7	D (100)	84.0	3	39.0	1.000	1.000	46.3	< 84.0
6	10	nodeRight	19	34.7	-11.6	68.7	D (100)	84.0	3	39.0	1.000	1.000	46.3	< 84.0
6	11	nodeLeft	19	47.4	-9.5	99.3	D (100)	84.0	3	39.0	1.000	1.000	56.9	< 84.0
6	11	nodeRight	19	47.4	-9.5	99.3	D (100)	84.0	3	39.0	1.000	1.000	56.9	< 84.0
7	12	nodeLeft	21	46.9	-6.3	105.6	D (100)	84.0	3	39.0	1.000	1.000	53.2	< 84.0
7	12	nodeRight	21	46.9	-6.3	105.6	D (100)	84.0	3	39.0	1.000	1.000	53.2	< 84.0
8	13	nodeLeft	19	47.4	-9.5	99.3	D (100)	84.0	3	39.0	1.000	1.000	56.9	< 84.0
8	13	nodeRight	19	47.4	-9.5	99.3	D (100)	84.0	3	39.0	1.000	1.000	56.9	< 84.0
8	14	nodeLeft	19	34.7	-11.6	68.7	D (100)	84.0	3	39.0	1.000	1.000	46.3	< 84.0
8	14	nodeRight	19	34.7	-11.6	68.7	D (100)	84.0	3	39.0	1.000	1.000	46.3	< 84.0
9	15	nodeLeft	23	18.9	-13.1	9.8	D (100)	84.0	3	39.0	1.000	1.000	32.0	< 84.0
9	15	nodeRight	23	18.9	-13.1	9.8	D (100)	84.0	3	39.0	1.000	1.000	32.0	< 84.0
9	16	nodeLeft	23	8.0	-15.4	-70.0	D (100)	84.0	3	39.0	1.300	1.000	23.4	<109.2
9	16	nodeRight	23	8.0	-15.4	-70.0	D (100)	84.0	3	39.0	1.300	1.000	23.4	<109.2
10	17	nodeLeft	39	3.9	-19.5	-116.8	D (100)	84.0	3	39.0	1.300	0.895	23.3	< 97.7
10	17	nodeRight	39	3.9	-19.5	-116.8	D (100)	84.0	3	39.0	1.300	0.895	23.3	< 97.7
10	18	nodeLeft	39	7.5	-16.4	-54.2	D (100)	84.0	3	39.0	1.300	0.895	23.9	< 97.7
10	18	nodeRight	39	7.5	-16.4	-54.2	D (100)	84.0	3	39.0	1.300	0.895	23.9	< 97.7
11	19	nodeLeft	23	25.5	-19.4	-9.1	D (100)	84.0	3	39.0	1.066	1.000	44.9	< 89.6
11	19	nodeRight	23	25.5	-19.4	-9.1	D (100)	84.0	3	39.0	1.066	1.000	44.9	< 89.6
12	20	nodeLeft	19	43.4	-15.8	34.2	D (100)	84.0	3	39.0	1.000	1.000	59.3	< 84.0
12	20	nodeRight	19	43.4	-15.8	34.2	D (100)	84.0	3	39.0	1.000	1.000	59.3	< 84.0
12	21	nodeLeft	19	36.2	-10.5	57.8	D (100)	84.0	3	39.0	1.000	1.000	46.8	< 84.0
12	21	nodeRight	19	36.2	-10.5	57.8	D (100)	84.0	3	39.0	1.000	1.000	46.8	< 84.0
13	22	nodeLeft	19	20.7	-5.3	46.4	D (100)	84.0	3	39.0	1.000	1.000	26.0	< 84.0
13	22	nodeRight	19	20.7	-5.3	46.4	D (100)	84.0	3	39.0	1.000	1.000	26.0	< 84.0
13	23	nodeLeft	19	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2

Steel I Girder G5

node WEB-U-1 (WebUpper edge) WEB - 1

Sec	node	Web	h	t	Grade					Stress						
					σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D
					(N/mm ²)					(N/mm ²)						
1	1	nodeRight	2400	22	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
1	2	nodeLeft	2400	22	0	4.8	-19.0	-42.7	E(80)	62.0	3	29.0	1.300	1.000	23.9	< 80.6
1	2	nodeRight	2400	22	0	4.8	-19.0	-42.7	E(80)	62.0	3	29.0	1.300	1.000	23.9	< 80.6
2	3	nodeLeft	2400	22	0	9.7	-33.3	-53.2	E(80)	62.0	3	29.0	1.300	1.000	43.0	< 80.6
2	3	nodeRight	2400	22	0	9.7	-33.3	-53.2	E(80)	62.0	3	29.0	1.300	1.000	43.0	< 80.6
2	4	nodeLeft	2400	22	0	14.6	-39.9	-31.5	E(80)	62.0	3	29.0	1.300	1.000	54.5	< 80.6
2	4	nodeRight	2400	22	0	14.6	-39.9	-31.5	E(80)	62.0	3	29.0	1.300	1.000	54.5	< 80.6
3	5	nodeLeft	2400	20	0	20.3	-26.7	9.6	E(80)	62.0	3	29.0	1.000	1.000	47.0	< 62.0
3	5	nodeRight	2400	20	0	20.3	-26.7	9.6	E(80)	62.0	3	29.0	1.000	1.000	47.0	< 62.0
4	6	nodeLeft	2400	31	0	18.2	-8.3	60.2	E(80)	62.0	3	29.0	1.000	0.948	26.5	< 58.8
4	6	nodeRight	2400	31	0	18.2	-8.3	60.2	E(80)	62.0	3	29.0	1.000	0.948	26.5	< 58.8
4	7	nodeLeft	2400	31	0	21.6	-4.3	129.7	E(80)	62.0	3	29.0	1.000	0.948	25.9	< 58.8
4	7	nodeRight	2400	31	0	21.6	-4.3	129.7	E(80)	62.0	3	29.0	1.000	0.948	25.9	< 58.8
5	8	nodeLeft	2400	19	0	16.5	-8.6	75.1	E(80)	62.0	3	29.0	1.000	1.000	25.1	< 62.0
5	8	nodeRight	2400	19	0	16.5	-8.6	75.1	E(80)	62.0	3	29.0	1.000	1.000	25.1	< 62.0
5	9	nodeLeft	2400	19	0	14.0	-20.3	-10.5	E(80)	62.0	3	29.0	1.223	1.000	34.3	< 75.8
5	9	nodeRight	2400	19	0	14.0	-20.3	-10.5	E(80)	62.0	3	29.0	1.223	1.000	34.3	< 75.8
6	10	nodeLeft	2400	26	0	9.8	-29.4	-58.0	E(80)	62.0	3	29.0	1.300	0.990	39.2	< 79.8
6	10	nodeRight	2400	26	0	9.8	-29.4	-58.0	E(80)	62.0	3	29.0	1.300	0.990	39.2	< 79.8
6	11	nodeLeft	2400	26	0	8.0	-40.1	-84.0	E(80)	62.0	3	29.0	1.300	0.990	48.1	< 79.8
6	11	nodeRight	2400	26	0	8.0	-40.1	-84.0	E(80)	62.0	3	29.0	1.300	0.990	48.1	< 79.8
7	12	nodeLeft	2400	26	0	5.6	-41.5	-93.3	E(80)	62.0	3	29.0	1.300	0.990	47.0	< 79.8
7	12	nodeRight	2400	26	0	5.6	-41.5	-93.3	E(80)	62.0	3	29.0	1.300	0.990	47.0	< 79.8
8	13	nodeLeft	2400	26	0	8.0	-40.1	-84.0	E(80)	62.0	3	29.0	1.300	0.990	48.1	< 79.8
8	13	nodeRight	2400	26	0	8.0	-40.1	-84.0	E(80)	62.0	3	29.0	1.300	0.990	48.1	< 79.8
8	14	nodeLeft	2400	26	0	9.8	-29.4	-58.0	E(80)	62.0	3	29.0	1.300	0.990	39.2	< 79.8
8	14	nodeRight	2400	26	0	9.8	-29.4	-58.0	E(80)	62.0	3	29.0	1.300	0.990	39.2	< 79.8
9	15	nodeLeft	2400	19	0	14.0	-20.3	-10.5	E(80)	62.0	3	29.0	1.223	1.000	34.3	< 75.8
9	15	nodeRight	2400	19	0	14.0	-20.3	-10.5	E(80)	62.0	3	29.0	1.223	1.000	34.3	< 75.8
9	16	nodeLeft	2400	19	0	16.5	-8.6	75.1	E(80)	62.0	3	29.0	1.000	1.000	25.1	< 62.0
9	16	nodeRight	2400	19	0	16.5	-8.6	75.1	E(80)	62.0	3	29.0	1.000	1.000	25.1	< 62.0
10	17	nodeLeft	2400	31	0	21.6	-4.3	129.7	E(80)	62.0	3	29.0	1.000	0.948	25.9	< 58.8
10	17	nodeRight	2400	31	0	21.6	-4.3	129.7	E(80)	62.0	3	29.0	1.000	0.948	25.9	< 58.8
10	18	nodeLeft	2400	31	0	18.2	-8.3	60.2	E(80)	62.0	3	29.0	1.000	0.948	26.5	< 58.8
10	18	nodeRight	2400	31	0	18.2	-8.3	60.2	E(80)	62.0	3	29.0	1.000	0.948	26.5	< 58.8
11	19	nodeLeft	2400	20	0	20.3	-26.7	9.6	E(80)	62.0	3	29.0	1.000	1.000	47.0	< 62.0
11	19	nodeRight	2400	20	0	20.3	-26.7	9.6	E(80)	62.0	3	29.0	1.000	1.000	47.0	< 62.0
12	20	nodeLeft	2400	22	0	14.6	-39.9	-31.5	E(80)	62.0	3	29.0	1.300	1.000	54.5	< 80.6
12	20	nodeRight	2400	22	0	14.6	-39.9	-31.5	E(80)	62.0	3	29.0	1.300	1.000	54.5	< 80.6
12	21	nodeLeft	2400	22	0	9.7	-33.3	-53.2	E(80)	62.0	3	29.0	1.300	1.000	43.0	< 80.6
12	21	nodeRight	2400	22	0	9.7	-33.3	-53.2	E(80)	62.0	3	29.0	1.300	1.000	43.0	< 80.6
13	22	nodeLeft	2400	22	0	4.8	-19.0	-42.7	E(80)	62.0	3	29.0	1.300	1.000	23.9	< 80.6
13	22	nodeRight	2400	22	0	4.8	-19.0	-42.7	E(80)	62.0	3	29.0	1.300	1.000	23.9	< 80.6
13	23	nodeLeft	2400	22	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6

Steel I Girder G5

node WEB-L-1 (WebLower edge) WEB - 1

Sec	node	Web	h	t	Grade				Stress							
					σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D
					(N/mm ²)				(N/mm ²)							
1	1	nodeRight	2400	19	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
1	2	nodeLeft	2400	19	0	20.4	-5.2	45.7	E(80)	62.0	3	29.0	1.000	1.000	25.6	< 62.0
1	2	nodeRight	2400	19	0	20.4	-5.2	45.7	E(80)	62.0	3	29.0	1.000	1.000	25.6	< 62.0
2	3	nodeLeft	2400	19	0	35.7	-10.4	56.9	E(80)	62.0	3	29.0	1.000	1.000	46.0	< 62.0
2	3	nodeRight	2400	19	0	35.7	-10.4	56.9	E(80)	62.0	3	29.0	1.000	1.000	46.0	< 62.0
2	4	nodeLeft	2400	19	0	42.8	-15.6	33.7	E(80)	62.0	3	29.0	1.000	1.000	58.4	< 62.0
2	4	nodeRight	2400	19	0	42.8	-15.6	33.7	E(80)	62.0	3	29.0	1.000	1.000	58.4	< 62.0
3	5	nodeLeft	2400	23	0	25.0	-19.0	-8.9	E(80)	62.0	3	29.0	1.066	1.000	44.0	< 66.1
3	5	nodeRight	2400	23	0	25.0	-19.0	-8.9	E(80)	62.0	3	29.0	1.066	1.000	44.0	< 66.1
4	6	nodeLeft	2400	39	0	7.3	-15.8	-52.4	E(80)	62.0	3	29.0	1.300	0.895	23.1	< 72.1
4	6	nodeRight	2400	39	0	7.3	-15.8	-52.4	E(80)	62.0	3	29.0	1.300	0.895	23.1	< 72.1
4	7	nodeLeft	2400	39	0	3.7	-18.8	-112.8	E(80)	62.0	3	29.0	1.300	0.895	22.5	< 72.1
4	7	nodeRight	2400	39	0	3.7	-18.8	-112.8	E(80)	62.0	3	29.0	1.300	0.895	22.5	< 72.1
5	8	nodeLeft	2400	23	0	7.9	-15.1	-68.6	E(80)	62.0	3	29.0	1.300	1.000	23.0	< 80.6
5	8	nodeRight	2400	23	0	7.9	-15.1	-68.6	E(80)	62.0	3	29.0	1.300	1.000	23.0	< 80.6
5	9	nodeLeft	2400	23	0	18.5	-12.8	9.6	E(80)	62.0	3	29.0	1.000	1.000	31.3	< 62.0
5	9	nodeRight	2400	23	0	18.5	-12.8	9.6	E(80)	62.0	3	29.0	1.000	1.000	31.3	< 62.0
6	10	nodeLeft	2400	19	0	34.2	-11.4	67.7	E(80)	62.0	3	29.0	1.000	1.000	45.7	< 62.0
6	10	nodeRight	2400	19	0	34.2	-11.4	67.7	E(80)	62.0	3	29.0	1.000	1.000	45.7	< 62.0
6	11	nodeLeft	2400	19	0	46.7	-9.4	97.9	E(80)	62.0	3	29.0	1.000	1.000	56.1	< 62.0
6	11	nodeRight	2400	19	0	46.7	-9.4	97.9	E(80)	62.0	3	29.0	1.000	1.000	56.1	< 62.0
7	12	nodeLeft	2400	21	0	46.2	-6.2	103.9	E(80)	62.0	3	29.0	1.000	1.000	52.4	< 62.0
7	12	nodeRight	2400	21	0	46.2	-6.2	103.9	E(80)	62.0	3	29.0	1.000	1.000	52.4	< 62.0
8	13	nodeLeft	2400	19	0	46.7	-9.4	97.9	E(80)	62.0	3	29.0	1.000	1.000	56.1	< 62.0
8	13	nodeRight	2400	19	0	46.7	-9.4	97.9	E(80)	62.0	3	29.0	1.000	1.000	56.1	< 62.0
8	14	nodeLeft	2400	19	0	34.2	-11.4	67.7	E(80)	62.0	3	29.0	1.000	1.000	45.7	< 62.0
8	14	nodeRight	2400	19	0	34.2	-11.4	67.7	E(80)	62.0	3	29.0	1.000	1.000	45.7	< 62.0
9	15	nodeLeft	2400	23	0	18.5	-12.8	9.6	E(80)	62.0	3	29.0	1.000	1.000	31.3	< 62.0
9	15	nodeRight	2400	23	0	18.5	-12.8	9.6	E(80)	62.0	3	29.0	1.000	1.000	31.3	< 62.0
9	16	nodeLeft	2400	23	0	7.9	-15.1	-68.6	E(80)	62.0	3	29.0	1.300	1.000	23.0	< 80.6
9	16	nodeRight	2400	23	0	7.9	-15.1	-68.6	E(80)	62.0	3	29.0	1.300	1.000	23.0	< 80.6
10	17	nodeLeft	2400	39	0	3.7	-18.8	-112.8	E(80)	62.0	3	29.0	1.300	0.895	22.5	< 72.1
10	17	nodeRight	2400	39	0	3.7	-18.8	-112.8	E(80)	62.0	3	29.0	1.300	0.895	22.5	< 72.1
10	18	nodeLeft	2400	39	0	7.3	-15.8	-52.4	E(80)	62.0	3	29.0	1.300	0.895	23.1	< 72.1
10	18	nodeRight	2400	39	0	7.3	-15.8	-52.4	E(80)	62.0	3	29.0	1.300	0.895	23.1	< 72.1
11	19	nodeLeft	2400	23	0	25.0	-19.0	-8.9	E(80)	62.0	3	29.0	1.066	1.000	44.0	< 66.1
11	19	nodeRight	2400	23	0	25.0	-19.0	-8.9	E(80)	62.0	3	29.0	1.066	1.000	44.0	< 66.1
12	20	nodeLeft	2400	19	0	42.8	-15.6	33.7	E(80)	62.0	3	29.0	1.000	1.000	58.4	< 62.0
12	20	nodeRight	2400	19	0	42.8	-15.6	33.7	E(80)	62.0	3	29.0	1.000	1.000	58.4	< 62.0
12	21	nodeLeft	2400	19	0	35.7	-10.4	56.9	E(80)	62.0	3	29.0	1.000	1.000	46.0	< 62.0
12	21	nodeRight	2400	19	0	35.7	-10.4	56.9	E(80)	62.0	3	29.0	1.000	1.000	46.0	< 62.0
13	22	nodeLeft	2400	19	0	20.4	-5.2	45.7	E(80)	62.0	3	29.0	1.000	1.000	25.6	< 62.0
13	22	nodeRight	2400	19	0	20.4	-5.2	45.7	E(80)	62.0	3	29.0	1.000	1.000	25.6	< 62.0
13	23	nodeLeft	2400	19	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6

Steel I Girder G5

node HSTIFF-1 (WebH-Stiffener) WEB - 1

Sec	node	Web	h	t	σ_{tmax}	σ_{tmin}	σ_d	Grade	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR	Ct	Stress
																		$\Delta \sigma_{ce} \cdot \text{Cycle}$
																		(N/mm2)
1	1	nodeRight	2400	12	480	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6	
1	2	nodeLeft	2400	12	480	2.8	-11.1	-25.0	G(50)	32.0	3	15.0	1.300	1.000	14.0	<	41.6	
1	2	nodeRight	2400	12	480	2.8	-11.1	-25.0	G(50)	32.0	3	15.0	1.300	1.000	14.0	<	41.6	
2	3	nodeLeft	2400	12	480	5.7	-19.5	-31.1	G(50)	32.0	3	15.0	1.300	1.000	25.2	<	41.6	
2	3	nodeRight	2400	12	480	5.7	-19.5	-31.1	G(50)	32.0	3	15.0	1.300	1.000	25.2	<	41.6	
2	4	nodeLeft	2400	12	480	8.5	-23.4	-18.5	G(50)	32.0	3	15.0	1.300	1.000	31.9	<	41.6	
2	4	nodeRight	2400	12	480	8.5	-23.4	-18.5	G(50)	32.0	3	15.0	1.300	1.000	31.9	<	41.6	
3	5	nodeLeft	2400	12	480	12.4	-16.4	5.9	G(50)	32.0	3	15.0	1.000	1.000	28.8	<	32.0	
3	5	nodeRight	2400	12	480	12.4	-16.4	5.9	G(50)	32.0	3	15.0	1.000	1.000	28.8	<	32.0	
4	6	nodeLeft	2400	12	480	4.1	-9.0	-29.9	G(50)	32.0	3	15.0	1.300	1.000	13.1	<	41.6	
4	6	nodeRight	2400	12	480	4.1	-9.0	-29.9	G(50)	32.0	3	15.0	1.300	1.000	13.1	<	41.6	
4	7	nodeLeft	2400	12	480	2.1	-10.7	-64.3	G(50)	32.0	3	15.0	1.300	1.000	12.8	<	41.6	
4	7	nodeRight	2400	12	480	2.1	-10.7	-64.3	G(50)	32.0	3	15.0	1.300	1.000	12.8	<	41.6	
5	8	nodeLeft	2400	12	480	4.6	-8.8	-39.9	G(50)	32.0	3	15.0	1.300	1.000	13.4	<	41.6	
5	8	nodeRight	2400	12	480	4.6	-8.8	-39.9	G(50)	32.0	3	15.0	1.300	1.000	13.4	<	41.6	
5	9	nodeLeft	2400	12	480	8.7	-12.5	-6.5	G(50)	32.0	3	15.0	1.223	1.000	21.2	<	39.1	
5	9	nodeRight	2400	12	480	8.7	-12.5	-6.5	G(50)	32.0	3	15.0	1.223	1.000	21.2	<	39.1	
6	10	nodeLeft	2400	12	480	5.6	-16.6	-32.9	G(50)	32.0	3	15.0	1.300	1.000	22.2	<	41.6	
6	10	nodeRight	2400	12	480	5.6	-16.6	-32.9	G(50)	32.0	3	15.0	1.300	1.000	22.2	<	41.6	
6	11	nodeLeft	2400	12	480	4.6	-22.7	-47.6	G(50)	32.0	3	15.0	1.300	1.000	27.3	<	41.6	
6	11	nodeRight	2400	12	480	4.6	-22.7	-47.6	G(50)	32.0	3	15.0	1.300	1.000	27.3	<	41.6	
7	12	nodeLeft	2400	12	480	3.2	-24.0	-53.9	G(50)	32.0	3	15.0	1.300	1.000	27.2	<	41.6	
7	12	nodeRight	2400	12	480	3.2	-24.0	-53.9	G(50)	32.0	3	15.0	1.300	1.000	27.2	<	41.6	
8	13	nodeLeft	2400	12	480	4.6	-22.7	-47.6	G(50)	32.0	3	15.0	1.300	1.000	27.3	<	41.6	
8	13	nodeRight	2400	12	480	4.6	-22.7	-47.6	G(50)	32.0	3	15.0	1.300	1.000	27.3	<	41.6	
8	14	nodeLeft	2400	12	480	5.6	-16.6	-32.9	G(50)	32.0	3	15.0	1.300	1.000	22.2	<	41.6	
8	14	nodeRight	2400	12	480	5.6	-16.6	-32.9	G(50)	32.0	3	15.0	1.300	1.000	22.2	<	41.6	
9	15	nodeLeft	2400	12	480	8.7	-12.5	-6.5	G(50)	32.0	3	15.0	1.223	1.000	21.2	<	39.1	
9	15	nodeRight	2400	12	480	8.7	-12.5	-6.5	G(50)	32.0	3	15.0	1.223	1.000	21.2	<	39.1	
9	16	nodeLeft	2400	12	480	4.6	-8.8	-39.9	G(50)	32.0	3	15.0	1.300	1.000	13.4	<	41.6	
9	16	nodeRight	2400	12	480	4.6	-8.8	-39.9	G(50)	32.0	3	15.0	1.300	1.000	13.4	<	41.6	
10	17	nodeLeft	2400	12	480	2.1	-10.7	-64.3	G(50)	32.0	3	15.0	1.300	1.000	12.8	<	41.6	
10	17	nodeRight	2400	12	480	2.1	-10.7	-64.3	G(50)	32.0	3	15.0	1.300	1.000	12.8	<	41.6	
10	18	nodeLeft	2400	12	480	4.1	-9.0	-29.9	G(50)	32.0	3	15.0	1.300	1.000	13.1	<	41.6	
10	18	nodeRight	2400	12	480	4.1	-9.0	-29.9	G(50)	32.0	3	15.0	1.300	1.000	13.1	<	41.6	
11	19	nodeLeft	2400	12	480	12.4	-16.4	5.9	G(50)	32.0	3	15.0	1.000	1.000	28.8	<	32.0	
11	19	nodeRight	2400	12	480	12.4	-16.4	5.9	G(50)	32.0	3	15.0	1.000	1.000	28.8	<	32.0	
12	20	nodeLeft	2400	12	480	8.5	-23.4	-18.5	G(50)	32.0	3	15.0	1.300	1.000	31.9	<	41.6	
12	20	nodeRight	2400	12	480	8.5	-23.4	-18.5	G(50)	32.0	3	15.0	1.300	1.000	31.9	<	41.6	
12	21	nodeLeft	2400	12	480	5.7	-19.5	-31.1	G(50)	32.0	3	15.0	1.300	1.000	25.2	<	41.6	
12	21	nodeRight	2400	12	480	5.7	-19.5	-31.1	G(50)	32.0	3	15.0	1.300	1.000	25.2	<	41.6	
13	22	nodeLeft	2400	12	480	2.8	-11.1	-25.0	G(50)	32.0	3	15.0	1.300	1.000	14.0	<	41.6	
13	22	nodeRight	2400	12	480	2.8	-11.1	-25.0	G(50)	32.0	3	15.0	1.300	1.000	14.0	<	41.6	
13	23	nodeLeft	2400	12	480	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6	

Steel I Girder G5

node POINT-U-1 (WebUpper) WEB - 1

Sec	node	Web	h	t	σ_{tmax}	σ_{tmin}	σ_d	Grade	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D	Stress
																		$\Delta \sigma_{ce} \cdot \text{Cycle}$
																	(N/mm ²)	
1	1	nodeRight	2400	12	300	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6	
1	2	nodeLeft	2400	12	300	3.6	-14.1	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.7	<	41.6	
1	2	nodeRight	2400	12	300	3.6	-14.1	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.7	<	41.6	
2	3	nodeLeft	2400	12	300	7.2	-24.7	-39.4	G(50)	32.0	3	15.0	1.300	1.000	31.9	<	41.6	
2	3	nodeRight	2400	12	300	7.2	-24.7	-39.4	G(50)	32.0	3	15.0	1.300	1.000	31.9	<	41.6	
2	4	nodeLeft	2400	12	300	10.8	-29.6	-23.3	G(50)	32.0	3	15.0	1.300	1.000	40.4	<	41.6	
2	4	nodeRight	2400	12	300	10.8	-29.6	-23.3	G(50)	32.0	3	15.0	1.300	1.000	40.4	<	41.6	
3	5	nodeLeft	2400	12	300	15.4	-20.3	7.3	G(50)	32.0	3	15.0	1.000	1.000	35.7	>	32.0	0.41<1
3	5	nodeRight	2400	12	300	15.4	-20.3	7.3	G(50)	32.0	3	15.0	1.000	1.000	35.7	>	32.0	0.41<1
4	6	nodeLeft	2400	12	300	13.9	-6.4	46.2	G(50)	32.0	3	15.0	1.000	1.000	20.3	<	32.0	
4	6	nodeRight	2400	12	300	13.9	-6.4	46.2	G(50)	32.0	3	15.0	1.000	1.000	20.3	<	32.0	
4	7	nodeLeft	2400	12	300	16.6	-3.3	99.4	G(50)	32.0	3	15.0	1.000	1.000	19.9	<	32.0	
4	7	nodeRight	2400	12	300	16.6	-3.3	99.4	G(50)	32.0	3	15.0	1.000	1.000	19.9	<	32.0	
5	8	nodeLeft	2400	12	300	12.6	-6.5	57.1	G(50)	32.0	3	15.0	1.000	1.000	19.1	<	32.0	
5	8	nodeRight	2400	12	300	12.6	-6.5	57.1	G(50)	32.0	3	15.0	1.000	1.000	19.1	<	32.0	
5	9	nodeLeft	2400	12	300	10.7	-15.4	-8.0	G(50)	32.0	3	15.0	1.223	1.000	26.1	<	39.1	
5	9	nodeRight	2400	12	300	10.7	-15.4	-8.0	G(50)	32.0	3	15.0	1.223	1.000	26.1	<	39.1	
6	10	nodeLeft	2400	12	300	7.2	-21.4	-42.3	G(50)	32.0	3	15.0	1.300	1.000	28.6	<	41.6	
6	10	nodeRight	2400	12	300	7.2	-21.4	-42.3	G(50)	32.0	3	15.0	1.300	1.000	28.6	<	41.6	
6	11	nodeLeft	2400	12	300	5.9	-29.2	-61.2	G(50)	32.0	3	15.0	1.300	1.000	35.1	<	41.6	
6	11	nodeRight	2400	12	300	5.9	-29.2	-61.2	G(50)	32.0	3	15.0	1.300	1.000	35.1	<	41.6	
7	12	nodeLeft	2400	12	300	4.1	-30.5	-68.7	G(50)	32.0	3	15.0	1.300	1.000	34.6	<	41.6	
7	12	nodeRight	2400	12	300	4.1	-30.5	-68.7	G(50)	32.0	3	15.0	1.300	1.000	34.6	<	41.6	
8	13	nodeLeft	2400	12	300	5.9	-29.2	-61.2	G(50)	32.0	3	15.0	1.300	1.000	35.1	<	41.6	
8	13	nodeRight	2400	12	300	5.9	-29.2	-61.2	G(50)	32.0	3	15.0	1.300	1.000	35.1	<	41.6	
8	14	nodeLeft	2400	12	300	7.2	-21.4	-42.3	G(50)	32.0	3	15.0	1.300	1.000	28.6	<	41.6	
8	14	nodeRight	2400	12	300	7.2	-21.4	-42.3	G(50)	32.0	3	15.0	1.300	1.000	28.6	<	41.6	
9	15	nodeLeft	2400	12	300	10.7	-15.4	-8.0	G(50)	32.0	3	15.0	1.223	1.000	26.1	<	39.1	
9	15	nodeRight	2400	12	300	10.7	-15.4	-8.0	G(50)	32.0	3	15.0	1.223	1.000	26.1	<	39.1	
9	16	nodeLeft	2400	12	300	12.6	-6.5	57.1	G(50)	32.0	3	15.0	1.000	1.000	19.1	<	32.0	
9	16	nodeRight	2400	12	300	12.6	-6.5	57.1	G(50)	32.0	3	15.0	1.000	1.000	19.1	<	32.0	
10	17	nodeLeft	2400	12	300	16.6	-3.3	99.4	G(50)	32.0	3	15.0	1.000	1.000	19.9	<	32.0	
10	17	nodeRight	2400	12	300	16.6	-3.3	99.4	G(50)	32.0	3	15.0	1.000	1.000	19.9	<	32.0	
10	18	nodeLeft	2400	12	300	13.9	-6.4	46.2	G(50)	32.0	3	15.0	1.000	1.000	20.3	<	32.0	
10	18	nodeRight	2400	12	300	13.9	-6.4	46.2	G(50)	32.0	3	15.0	1.000	1.000	20.3	<	32.0	
11	19	nodeLeft	2400	12	300	15.4	-20.3	7.3	G(50)	32.0	3	15.0	1.000	1.000	35.7	>	32.0	0.41<1
11	19	nodeRight	2400	12	300	15.4	-20.3	7.3	G(50)	32.0	3	15.0	1.000	1.000	35.7	>	32.0	0.41<1
12	20	nodeLeft	2400	12	300	10.8	-29.6	-23.3	G(50)	32.0	3	15.0	1.300	1.000	40.4	<	41.6	
12	20	nodeRight	2400	12	300	10.8	-29.6	-23.3	G(50)	32.0	3	15.0	1.300	1.000	40.4	<	41.6	
12	21	nodeLeft	2400	12	300	7.2	-24.7	-39.4	G(50)	32.0	3	15.0	1.300	1.000	31.9	<	41.6	
12	21	nodeRight	2400	12	300	7.2	-24.7	-39.4	G(50)	32.0	3	15.0	1.300	1.000	31.9	<	41.6	
13	22	nodeLeft	2400	12	300	3.6	-14.1	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.7	<	41.6	
13	22	nodeRight	2400	12	300	3.6	-14.1	-31.6	G(50)	32.0	3	15.0	1.300	1.000	17.7	<	41.6	
13	23	nodeLeft	2400	12	300	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	<	41.6	

Steel I Girder G5

node POINT-L-1 (WebLower) WEB - 1

Sec	node	Web	h	t	Grade					Stress							
					σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR • Ct	D	
					(N/mm ²)					(N/mm ²)							
1	1	nodeRight	2400	12	400	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6	
1	2	nodeLeft	2400	12	400	13.8	-3.5	31.0	G(50)	32.0	3	15.0	1.000	1.000	17.3	< 32.0	
1	2	nodeRight	2400	12	400	13.8	-3.5	31.0	G(50)	32.0	3	15.0	1.000	1.000	17.3	< 32.0	
2	3	nodeLeft	2400	12	400	24.2	-7.0	38.6	G(50)	32.0	3	15.0	1.000	1.000	31.2	< 32.0	
2	3	nodeRight	2400	12	400	24.2	-7.0	38.6	G(50)	32.0	3	15.0	1.000	1.000	31.2	< 32.0	
2	4	nodeLeft	2400	12	400	29.0	-10.6	22.9	G(50)	32.0	3	15.0	1.000	1.000	39.5	> 32.0	0.57<1
2	4	nodeRight	2400	12	400	29.0	-10.6	22.9	G(50)	32.0	3	15.0	1.000	1.000	39.5	> 32.0	0.57<1
3	5	nodeLeft	2400	12	400	16.4	-12.4	-5.9	G(50)	32.0	3	15.0	1.066	1.000	28.8	< 34.1	
3	5	nodeRight	2400	12	400	16.4	-12.4	-5.9	G(50)	32.0	3	15.0	1.066	1.000	28.8	< 34.1	
4	6	nodeLeft	2400	12	400	4.7	-10.1	-33.6	G(50)	32.0	3	15.0	1.300	1.000	14.8	< 41.6	
4	6	nodeRight	2400	12	400	4.7	-10.1	-33.6	G(50)	32.0	3	15.0	1.300	1.000	14.8	< 41.6	
4	7	nodeLeft	2400	12	400	2.4	-12.1	-72.4	G(50)	32.0	3	15.0	1.300	1.000	14.5	< 41.6	
4	7	nodeRight	2400	12	400	2.4	-12.1	-72.4	G(50)	32.0	3	15.0	1.300	1.000	14.5	< 41.6	
5	8	nodeLeft	2400	12	400	5.1	-9.8	-44.7	G(50)	32.0	3	15.0	1.300	1.000	15.0	< 41.6	
5	8	nodeRight	2400	12	400	5.1	-9.8	-44.7	G(50)	32.0	3	15.0	1.300	1.000	15.0	< 41.6	
5	9	nodeLeft	2400	12	400	12.0	-8.3	6.2	G(50)	32.0	3	15.0	1.000	1.000	20.4	< 32.0	
5	9	nodeRight	2400	12	400	12.0	-8.3	6.2	G(50)	32.0	3	15.0	1.000	1.000	20.4	< 32.0	
6	10	nodeLeft	2400	12	400	23.6	-7.9	46.7	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0	
6	10	nodeRight	2400	12	400	23.6	-7.9	46.7	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0	
6	11	nodeLeft	2400	12	400	32.3	-6.5	67.6	G(50)	32.0	3	15.0	1.000	1.000	38.7	> 32.0	0.53<1
6	11	nodeRight	2400	12	400	32.3	-6.5	67.6	G(50)	32.0	3	15.0	1.000	1.000	38.7	> 32.0	0.53<1
7	12	nodeLeft	2400	12	400	31.6	-4.2	71.0	G(50)	32.0	3	15.0	1.000	1.000	35.8	> 32.0	0.42<1
7	12	nodeRight	2400	12	400	31.6	-4.2	71.0	G(50)	32.0	3	15.0	1.000	1.000	35.8	> 32.0	0.42<1
8	13	nodeLeft	2400	12	400	32.3	-6.5	67.6	G(50)	32.0	3	15.0	1.000	1.000	38.7	> 32.0	0.53<1
8	13	nodeRight	2400	12	400	32.3	-6.5	67.6	G(50)	32.0	3	15.0	1.000	1.000	38.7	> 32.0	0.53<1
8	14	nodeLeft	2400	12	400	23.6	-7.9	46.7	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0	
8	14	nodeRight	2400	12	400	23.6	-7.9	46.7	G(50)	32.0	3	15.0	1.000	1.000	31.5	< 32.0	
9	15	nodeLeft	2400	12	400	12.0	-8.3	6.2	G(50)	32.0	3	15.0	1.000	1.000	20.4	< 32.0	
9	15	nodeRight	2400	12	400	12.0	-8.3	6.2	G(50)	32.0	3	15.0	1.000	1.000	20.4	< 32.0	
9	16	nodeLeft	2400	12	400	5.1	-9.8	-44.7	G(50)	32.0	3	15.0	1.300	1.000	15.0	< 41.6	
9	16	nodeRight	2400	12	400	5.1	-9.8	-44.7	G(50)	32.0	3	15.0	1.300	1.000	15.0	< 41.6	
10	17	nodeLeft	2400	12	400	2.4	-12.1	-72.4	G(50)	32.0	3	15.0	1.300	1.000	14.5	< 41.6	
10	17	nodeRight	2400	12	400	2.4	-12.1	-72.4	G(50)	32.0	3	15.0	1.300	1.000	14.5	< 41.6	
10	18	nodeLeft	2400	12	400	4.7	-10.1	-33.6	G(50)	32.0	3	15.0	1.300	1.000	14.8	< 41.6	
10	18	nodeRight	2400	12	400	4.7	-10.1	-33.6	G(50)	32.0	3	15.0	1.300	1.000	14.8	< 41.6	
11	19	nodeLeft	2400	12	400	16.4	-12.4	-5.9	G(50)	32.0	3	15.0	1.066	1.000	28.8	< 34.1	
11	19	nodeRight	2400	12	400	16.4	-12.4	-5.9	G(50)	32.0	3	15.0	1.066	1.000	28.8	< 34.1	
12	20	nodeLeft	2400	12	400	29.0	-10.6	22.9	G(50)	32.0	3	15.0	1.000	1.000	39.5	> 32.0	0.57<1
12	20	nodeRight	2400	12	400	29.0	-10.6	22.9	G(50)	32.0	3	15.0	1.000	1.000	39.5	> 32.0	0.57<1
12	21	nodeLeft	2400	12	400	24.2	-7.0	38.6	G(50)	32.0	3	15.0	1.000	1.000	31.2	< 32.0	
12	21	nodeRight	2400	12	400	24.2	-7.0	38.6	G(50)	32.0	3	15.0	1.000	1.000	31.2	< 32.0	
13	22	nodeLeft	2400	12	400	13.8	-3.5	31.0	G(50)	32.0	3	15.0	1.000	1.000	17.3	< 32.0	
13	22	nodeRight	2400	12	400	13.8	-3.5	31.0	G(50)	32.0	3	15.0	1.000	1.000	17.3	< 32.0	
13	23	nodeLeft	2400	12	400	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6	

8-2 Checking of Fatigue Stress for Cross Beam

σ_{tmax} : Maximum stress (Including the effect of γ_a)
 σ_{tmin} : Minimum stress (Including the effect of γ_a)
 σ_d : Stress of Dead load (Including the effect of γ_a)
 $\Delta \sigma_{max}$: $\sigma_{tmax} - \sigma_{tmin}$
 C_0 : $2.0E+6 \cdot \Delta \sigma_f^{**m}$
 $\Delta \sigma_f$: $2.0E+6$ Allowable stress
 m : Slope constant
 CR : Correction coefficient for mean stress
 C_t : Correction factor for t

Structural analysis coefficient Cross Beam $\gamma_a = 0.500$

Maximum stress range checking $\Delta \sigma_{max} \leq \Delta \sigma_{ce} \cdot CR \cdot C_t$

Stress range cycles checking $D = \sum_i [\sum_j \{n_{ti} / (C_0 \cdot (CR \cdot C_t)^{**m} / \Delta \sigma_{ij}^{**m})\}] \leq 1$

Node U.FLG-MAX (UpperFlange Stress MAX)

Node	Panel	Flange		σ_d	Grade	$(\Delta \sigma_f)$	$\Delta \sigma_{cem}$	$\Delta \sigma_{ve}$	CR	Ct	Stress		Cycle D	
		t	σ_{tmax}								σ_{tmin}	$\Delta \sigma_{max}$		$CR \cdot Ct$
		(mm)	(N/mm ²)								(N/mm ²)	(N/mm ²)		
C1	1 BeamLeft	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
C1	1 BeamRight	10	3.9	-14.5	D (100)	84.0	3	39.0	1.000	1.000	18.3	< 84.0		
C1	2 BeamLeft	10	3.9	-14.5	D (100)	84.0	3	39.0	1.000	1.000	18.3	< 84.0		
C1	2 BeamRight	10	1.0	-0.6	D (100)	84.0	3	39.0	1.000	1.000	1.5	< 84.0		
C1	3 BeamLeft	10	1.0	-0.6	D (100)	84.0	3	39.0	1.000	1.000	1.5	< 84.0		
C1	3 BeamRight	10	3.9	-14.5	D (100)	84.0	3	39.0	1.000	1.000	18.3	< 84.0		
C1	4 BeamLeft	10	3.9	-14.5	D (100)	84.0	3	39.0	1.000	1.000	18.3	< 84.0		
C1	4 BeamRight	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
C2	1 BeamLeft	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
C2	1 BeamRight	10	4.1	-15.6	D (100)	84.0	3	39.0	1.000	1.000	19.7	< 84.0		
C2	2 BeamLeft	10	4.1	-15.6	D (100)	84.0	3	39.0	1.000	1.000	19.7	< 84.0		
C2	2 BeamRight	10	2.3	-1.2	D (100)	84.0	3	39.0	1.000	1.000	3.5	< 84.0		
C2	3 BeamLeft	10	2.3	-1.2	D (100)	84.0	3	39.0	1.000	1.000	3.5	< 84.0		
C2	3 BeamRight	10	4.1	-15.6	D (100)	84.0	3	39.0	1.000	1.000	19.7	< 84.0		
C2	4 BeamLeft	10	4.1	-15.6	D (100)	84.0	3	39.0	1.000	1.000	19.7	< 84.0		
C2	4 BeamRight	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
C3	1 BeamLeft	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
C3	1 BeamRight	10	3.1	-9.1	D (100)	84.0	3	39.0	1.000	1.000	12.2	< 84.0		
C3	2 BeamLeft	10	3.1	-9.1	D (100)	84.0	3	39.0	1.000	1.000	12.2	< 84.0		
C3	2 BeamRight	10	1.7	-2.7	D (100)	84.0	3	39.0	1.000	1.000	4.3	< 84.0		
C3	3 BeamLeft	10	1.7	-2.7	D (100)	84.0	3	39.0	1.000	1.000	4.3	< 84.0		
C3	3 BeamRight	10	3.1	-9.1	D (100)	84.0	3	39.0	1.000	1.000	12.2	< 84.0		
C3	4 BeamLeft	10	3.1	-9.1	D (100)	84.0	3	39.0	1.000	1.000	12.2	< 84.0		
C3	4 BeamRight	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
C4	1 BeamLeft	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
C4	1 BeamRight	10	4.1	-15.6	D (100)	84.0	3	39.0	1.000	1.000	19.7	< 84.0		
C4	2 BeamLeft	10	4.1	-15.6	D (100)	84.0	3	39.0	1.000	1.000	19.7	< 84.0		
C4	2 BeamRight	10	2.3	-1.2	D (100)	84.0	3	39.0	1.000	1.000	3.5	< 84.0		
C4	3 BeamLeft	10	2.3	-1.2	D (100)	84.0	3	39.0	1.000	1.000	3.5	< 84.0		
C4	3 BeamRight	10	4.1	-15.6	D (100)	84.0	3	39.0	1.000	1.000	19.7	< 84.0		
C4	4 BeamLeft	10	4.1	-15.6	D (100)	84.0	3	39.0	1.000	1.000	19.7	< 84.0		
C4	4 BeamRight	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
C5	1 BeamLeft	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
C5	1 BeamRight	10	3.9	-14.5	D (100)	84.0	3	39.0	1.000	1.000	18.3	< 84.0		
C5	2 BeamLeft	10	3.9	-14.5	D (100)	84.0	3	39.0	1.000	1.000	18.3	< 84.0		
C5	2 BeamRight	10	1.0	-0.6	D (100)	84.0	3	39.0	1.000	1.000	1.5	< 84.0		
C5	3 BeamLeft	10	1.0	-0.6	D (100)	84.0	3	39.0	1.000	1.000	1.5	< 84.0		
C5	3 BeamRight	10	3.9	-14.5	D (100)	84.0	3	39.0	1.000	1.000	18.3	< 84.0		
C5	4 BeamLeft	10	3.9	-14.5	D (100)	84.0	3	39.0	1.000	1.000	18.3	< 84.0		
C5	4 BeamRight	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
PF12	1 BeamLeft	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
PF12	1 BeamRight	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
PF12	2 BeamLeft	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
PF12	2 BeamRight	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
PF12	3 BeamLeft	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
PF12	3 BeamRight	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
PF12	4 BeamLeft	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
PF12	4 BeamRight	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		
PF13	1 BeamLeft	10	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2		

Node U.FLG-MAX (UpperFlange Stress MAX)

Node	Panel	Flange	Stress											
			t	σ_{tmax}	σ_{tmin}	σ_d	Grade	$\Delta \sigma_{cem}$	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR · Ct	Cycle
		(mm)		(N/mm ²)		($\Delta \sigma_f$)						(N/mm ²)	(N/mm ²)	D
PF13	1 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
PF13	2 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
PF13	2 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
PF13	3 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
PF13	3 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
PF13	4 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
PF13	4 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	1 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	1 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	2 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	2 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	3 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	3 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	4 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	4 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	1 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	1 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	2 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	2 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	3 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	3 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	4 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	4 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	

Node L.FLG-MAX (LowerFlange Stress Max)

Node	Panel	Flange	Grade	Stress									
				$\Delta \sigma_{ce} \cdot \text{Cycle}$	$\Delta \sigma_{ce} \cdot \text{Cycle}$	$\Delta \sigma_{ce} \cdot \text{Cycle}$	$\Delta \sigma_{ce} \cdot \text{Cycle}$	$\Delta \sigma_{ce} \cdot \text{Cycle}$	$\Delta \sigma_{ce} \cdot \text{Cycle}$	$\Delta \sigma_{ce} \cdot \text{Cycle}$	$\Delta \sigma_{ce} \cdot \text{Cycle}$	$\Delta \sigma_{ce} \cdot \text{Cycle}$	$\Delta \sigma_{ce} \cdot \text{Cycle}$
		t	σ_{tmax}	σ_{tmin}	σ_d	($\Delta \sigma_f$)	$\Delta \sigma_{ce}$	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR · Ct	D
		(mm)	(N/mm2)								(N/mm2)	(N/mm2)	
C1	1 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
C1	1 BeamRight	10	14.5	-3.9	-24.7	D (100)	84.0	39.0	1.300	1.000	18.3	<109.2	
C1	2 BeamLeft	10	14.5	-3.9	-24.7	D (100)	84.0	39.0	1.300	1.000	18.3	<109.2	
C1	2 BeamRight	10	0.6	-1.0	-15.1	D (100)	84.0	39.0	1.300	1.000	1.5	<109.2	
C1	3 BeamLeft	10	0.6	-1.0	-15.1	D (100)	84.0	39.0	1.300	1.000	1.5	<109.2	
C1	3 BeamRight	10	14.5	-3.9	-24.7	D (100)	84.0	39.0	1.300	1.000	18.3	<109.2	
C1	4 BeamLeft	10	14.5	-3.9	-24.7	D (100)	84.0	39.0	1.300	1.000	18.3	<109.2	
C1	4 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
C2	1 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
C2	1 BeamRight	10	15.6	-4.1	-18.6	D (100)	84.0	39.0	1.300	1.000	19.7	<109.2	
C2	2 BeamLeft	10	15.6	-4.1	-18.6	D (100)	84.0	39.0	1.300	1.000	19.7	<109.2	
C2	2 BeamRight	10	1.2	-2.3	-3.2	D (100)	84.0	39.0	1.300	1.000	3.5	<109.2	
C2	3 BeamLeft	10	1.2	-2.3	-3.2	D (100)	84.0	39.0	1.300	1.000	3.5	<109.2	
C2	3 BeamRight	10	15.6	-4.1	-18.6	D (100)	84.0	39.0	1.300	1.000	19.7	<109.2	
C2	4 BeamLeft	10	15.6	-4.1	-18.6	D (100)	84.0	39.0	1.300	1.000	19.7	<109.2	
C2	4 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
C3	1 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
C3	1 BeamRight	10	9.1	-3.1	-4.9	D (100)	84.0	39.0	1.079	1.000	12.2	< 90.6	
C3	2 BeamLeft	10	9.1	-3.1	-4.9	D (100)	84.0	39.0	1.079	1.000	12.2	< 90.6	
C3	2 BeamRight	10	2.7	-1.7	-19.3	D (100)	84.0	39.0	1.300	1.000	4.3	<109.2	
C3	3 BeamLeft	10	2.7	-1.7	-19.3	D (100)	84.0	39.0	1.300	1.000	4.3	<109.2	
C3	3 BeamRight	10	9.1	-3.1	-4.9	D (100)	84.0	39.0	1.079	1.000	12.2	< 90.6	
C3	4 BeamLeft	10	9.1	-3.1	-4.9	D (100)	84.0	39.0	1.079	1.000	12.2	< 90.6	
C3	4 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
C4	1 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
C4	1 BeamRight	10	15.6	-4.1	-18.6	D (100)	84.0	39.0	1.300	1.000	19.7	<109.2	
C4	2 BeamLeft	10	15.6	-4.1	-18.6	D (100)	84.0	39.0	1.300	1.000	19.7	<109.2	
C4	2 BeamRight	10	1.2	-2.3	-3.2	D (100)	84.0	39.0	1.300	1.000	3.5	<109.2	
C4	3 BeamLeft	10	1.2	-2.3	-3.2	D (100)	84.0	39.0	1.300	1.000	3.5	<109.2	
C4	3 BeamRight	10	15.6	-4.1	-18.6	D (100)	84.0	39.0	1.300	1.000	19.7	<109.2	
C4	4 BeamLeft	10	15.6	-4.1	-18.6	D (100)	84.0	39.0	1.300	1.000	19.7	<109.2	
C4	4 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
C5	1 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
C5	1 BeamRight	10	14.5	-3.9	-24.7	D (100)	84.0	39.0	1.300	1.000	18.3	<109.2	
C5	2 BeamLeft	10	14.5	-3.9	-24.7	D (100)	84.0	39.0	1.300	1.000	18.3	<109.2	
C5	2 BeamRight	10	0.6	-1.0	-15.1	D (100)	84.0	39.0	1.300	1.000	1.5	<109.2	
C5	3 BeamLeft	10	0.6	-1.0	-15.1	D (100)	84.0	39.0	1.300	1.000	1.5	<109.2	
C5	3 BeamRight	10	14.5	-3.9	-24.7	D (100)	84.0	39.0	1.300	1.000	18.3	<109.2	
C5	4 BeamLeft	10	14.5	-3.9	-24.7	D (100)	84.0	39.0	1.300	1.000	18.3	<109.2	
C5	4 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
PF12	1 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
PF12	1 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
PF12	2 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
PF12	2 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
PF12	3 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
PF12	3 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
PF12	4 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
PF12	4 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
PF13	1 BeamLeft	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	
PF13	1 BeamRight	10	0.0	0.0	0.0	D (100)	84.0	39.0	1.300	1.000	0.0	<109.2	

Node L.FLG-MAX (LowerFlange Stress MAX)

Node	Panel	Flange			Grade	Stress							
		t (mm)	σ_{tmax} (N/mm2)	σ_{tmin} (N/mm2)		σ_d ($\Delta \sigma_f$)	$\Delta \sigma_{cem}$	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$ (N/mm2)	CR • Ct (N/mm2)	Cycle D
PF13	2 BeamLeft	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
PF13	2 BeamRight	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
PF13	3 BeamLeft	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
PF13	3 BeamRight	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
PF13	4 BeamLeft	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
PF13	4 BeamRight	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	1 BeamLeft	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	1 BeamRight	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	2 BeamLeft	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	2 BeamRight	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	3 BeamLeft	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	3 BeamRight	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	4 BeamLeft	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S1	4 BeamRight	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	1 BeamLeft	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	1 BeamRight	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	2 BeamLeft	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	2 BeamRight	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	3 BeamLeft	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	3 BeamRight	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	4 BeamLeft	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	
S2	4 BeamRight	10	0.0	0.0	0.0 D (100)	84.0	3	39.0	1.300	1.000	0.0	<109.2	

Node	WEB-U-1	(WebUpperEdge)	WEB - 1	Stress									
Panel	Web	Grade	$\Delta \sigma_{ce} \cdot \text{Cycle}$										
	h t	$\sigma_{tmax} \sigma_{tmin}$	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR · Ct	D	
	(mm)	(N/mm ²)								(N/mm ²)			
C1	1 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
C1	1 BeamRight	1880 10	0	3.8	-14.3	24.4	E(80)	62.0	3	29.0	1.000	1.000	18.1 < 62.0
C1	2 BeamLeft	1880 10	0	3.8	-14.3	24.4	E(80)	62.0	3	29.0	1.000	1.000	18.1 < 62.0
C1	2 BeamRight	1880 10	0	1.0	-0.5	14.9	E(80)	62.0	3	29.0	1.000	1.000	1.5 < 62.0
C1	3 BeamLeft	1880 10	0	1.0	-0.5	14.9	E(80)	62.0	3	29.0	1.000	1.000	1.5 < 62.0
C1	3 BeamRight	1880 10	0	3.8	-14.3	24.4	E(80)	62.0	3	29.0	1.000	1.000	18.1 < 62.0
C1	4 BeamLeft	1880 10	0	3.8	-14.3	24.4	E(80)	62.0	3	29.0	1.000	1.000	18.1 < 62.0
C1	4 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
C2	1 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
C2	1 BeamRight	1880 10	0	4.0	-15.5	18.4	E(80)	62.0	3	29.0	1.000	1.000	19.5 < 62.0
C2	2 BeamLeft	1880 10	0	4.0	-15.5	18.4	E(80)	62.0	3	29.0	1.000	1.000	19.5 < 62.0
C2	2 BeamRight	1880 10	0	2.3	-1.2	3.2	E(80)	62.0	3	29.0	1.000	1.000	3.5 < 62.0
C2	3 BeamLeft	1880 10	0	2.3	-1.2	3.2	E(80)	62.0	3	29.0	1.000	1.000	3.5 < 62.0
C2	3 BeamRight	1880 10	0	4.0	-15.5	18.4	E(80)	62.0	3	29.0	1.000	1.000	19.5 < 62.0
C2	4 BeamLeft	1880 10	0	4.0	-15.5	18.4	E(80)	62.0	3	29.0	1.000	1.000	19.5 < 62.0
C2	4 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
C3	1 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
C3	1 BeamRight	1880 10	0	3.0	-9.0	4.9	E(80)	62.0	3	29.0	1.000	1.000	12.0 < 62.0
C3	2 BeamLeft	1880 10	0	3.0	-9.0	4.9	E(80)	62.0	3	29.0	1.000	1.000	12.0 < 62.0
C3	2 BeamRight	1880 10	0	1.6	-2.6	19.1	E(80)	62.0	3	29.0	1.000	1.000	4.3 < 62.0
C3	3 BeamLeft	1880 10	0	1.6	-2.6	19.1	E(80)	62.0	3	29.0	1.000	1.000	4.3 < 62.0
C3	3 BeamRight	1880 10	0	3.0	-9.0	4.9	E(80)	62.0	3	29.0	1.000	1.000	12.0 < 62.0
C3	4 BeamLeft	1880 10	0	3.0	-9.0	4.9	E(80)	62.0	3	29.0	1.000	1.000	12.0 < 62.0
C3	4 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
C4	1 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
C4	1 BeamRight	1880 10	0	4.0	-15.5	18.4	E(80)	62.0	3	29.0	1.000	1.000	19.5 < 62.0
C4	2 BeamLeft	1880 10	0	4.0	-15.5	18.4	E(80)	62.0	3	29.0	1.000	1.000	19.5 < 62.0
C4	2 BeamRight	1880 10	0	2.3	-1.2	3.2	E(80)	62.0	3	29.0	1.000	1.000	3.5 < 62.0
C4	3 BeamLeft	1880 10	0	2.3	-1.2	3.2	E(80)	62.0	3	29.0	1.000	1.000	3.5 < 62.0
C4	3 BeamRight	1880 10	0	4.0	-15.5	18.4	E(80)	62.0	3	29.0	1.000	1.000	19.5 < 62.0
C4	4 BeamLeft	1880 10	0	4.0	-15.5	18.4	E(80)	62.0	3	29.0	1.000	1.000	19.5 < 62.0
C4	4 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
C5	1 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
C5	1 BeamRight	1880 10	0	3.8	-14.3	24.4	E(80)	62.0	3	29.0	1.000	1.000	18.1 < 62.0
C5	2 BeamLeft	1880 10	0	3.8	-14.3	24.4	E(80)	62.0	3	29.0	1.000	1.000	18.1 < 62.0
C5	2 BeamRight	1880 10	0	1.0	-0.5	14.9	E(80)	62.0	3	29.0	1.000	1.000	1.5 < 62.0
C5	3 BeamLeft	1880 10	0	1.0	-0.5	14.9	E(80)	62.0	3	29.0	1.000	1.000	1.5 < 62.0
C5	3 BeamRight	1880 10	0	3.8	-14.3	24.4	E(80)	62.0	3	29.0	1.000	1.000	18.1 < 62.0
C5	4 BeamLeft	1880 10	0	3.8	-14.3	24.4	E(80)	62.0	3	29.0	1.000	1.000	18.1 < 62.0
C5	4 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF12	1 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF12	1 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF12	2 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF12	2 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF12	3 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF12	3 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF12	4 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF12	4 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF13	1 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF13	1 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF13	2 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6

Node WEB-U-1 (WebUpperEdge) WEB - 1

													Stress		
Panel		Web		Grade									$\Delta \sigma_{ce} \cdot \text{Cycle}$		
		h	t	σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR · Ct	D
		(mm)		(N/mm ²)									(N/mm ²)		
PF13	2 BeamRight	1880	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
PF13	3 BeamLeft	1880	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
PF13	3 BeamRight	1880	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
PF13	4 BeamLeft	1880	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
PF13	4 BeamRight	1880	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S1	1 BeamLeft	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S1	1 BeamRight	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S1	2 BeamLeft	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S1	2 BeamRight	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S1	3 BeamLeft	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S1	3 BeamRight	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S1	4 BeamLeft	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S1	4 BeamRight	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S2	1 BeamLeft	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S2	1 BeamRight	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S2	2 BeamLeft	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S2	2 BeamRight	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S2	3 BeamLeft	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S2	3 BeamRight	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S2	4 BeamLeft	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	
S2	4 BeamRight	2080	10	0	0.0	0.0	0.0 E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6	

Node	WEB-L-1	(WebLowerEdge)	WEB - 1	Stress										
Panel	Web	Grade	$\Delta \sigma_{ce} \cdot \text{Cycle}$											
	h t	σ_{tmax} σ_{tmin} σ_d ($\Delta \sigma_f$) $\Delta \sigma_{ce}$ m $\Delta \sigma_{ve}$ CR	Ct	$\Delta \sigma_{max}$ CR \cdot Ct	D									
	(mm)	(N/mm ²)		(N/mm ²)										
C1	1 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
C1	1 BeamRight	1880 10	0	14.3	-3.8	-24.4	E(80)	62.0	3	29.0	1.300	1.000	18.1	< 80.6
C1	2 BeamLeft	1880 10	0	14.3	-3.8	-24.4	E(80)	62.0	3	29.0	1.300	1.000	18.1	< 80.6
C1	2 BeamRight	1880 10	0	0.5	-1.0	-14.9	E(80)	62.0	3	29.0	1.300	1.000	1.5	< 80.6
C1	3 BeamLeft	1880 10	0	0.5	-1.0	-14.9	E(80)	62.0	3	29.0	1.300	1.000	1.5	< 80.6
C1	3 BeamRight	1880 10	0	14.3	-3.8	-24.4	E(80)	62.0	3	29.0	1.300	1.000	18.1	< 80.6
C1	4 BeamLeft	1880 10	0	14.3	-3.8	-24.4	E(80)	62.0	3	29.0	1.300	1.000	18.1	< 80.6
C1	4 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
C2	1 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
C2	1 BeamRight	1880 10	0	15.5	-4.0	-18.4	E(80)	62.0	3	29.0	1.300	1.000	19.5	< 80.6
C2	2 BeamLeft	1880 10	0	15.5	-4.0	-18.4	E(80)	62.0	3	29.0	1.300	1.000	19.5	< 80.6
C2	2 BeamRight	1880 10	0	1.2	-2.3	-3.2	E(80)	62.0	3	29.0	1.300	1.000	3.5	< 80.6
C2	3 BeamLeft	1880 10	0	1.2	-2.3	-3.2	E(80)	62.0	3	29.0	1.300	1.000	3.5	< 80.6
C2	3 BeamRight	1880 10	0	15.5	-4.0	-18.4	E(80)	62.0	3	29.0	1.300	1.000	19.5	< 80.6
C2	4 BeamLeft	1880 10	0	15.5	-4.0	-18.4	E(80)	62.0	3	29.0	1.300	1.000	19.5	< 80.6
C2	4 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
C3	1 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
C3	1 BeamRight	1880 10	0	9.0	-3.0	-4.9	E(80)	62.0	3	29.0	1.079	1.000	12.0	< 66.9
C3	2 BeamLeft	1880 10	0	9.0	-3.0	-4.9	E(80)	62.0	3	29.0	1.079	1.000	12.0	< 66.9
C3	2 BeamRight	1880 10	0	2.6	-1.6	-19.1	E(80)	62.0	3	29.0	1.300	1.000	4.3	< 80.6
C3	3 BeamLeft	1880 10	0	2.6	-1.6	-19.1	E(80)	62.0	3	29.0	1.300	1.000	4.3	< 80.6
C3	3 BeamRight	1880 10	0	9.0	-3.0	-4.9	E(80)	62.0	3	29.0	1.079	1.000	12.0	< 66.9
C3	4 BeamLeft	1880 10	0	9.0	-3.0	-4.9	E(80)	62.0	3	29.0	1.079	1.000	12.0	< 66.9
C3	4 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
C4	1 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
C4	1 BeamRight	1880 10	0	15.5	-4.0	-18.4	E(80)	62.0	3	29.0	1.300	1.000	19.5	< 80.6
C4	2 BeamLeft	1880 10	0	15.5	-4.0	-18.4	E(80)	62.0	3	29.0	1.300	1.000	19.5	< 80.6
C4	2 BeamRight	1880 10	0	1.2	-2.3	-3.2	E(80)	62.0	3	29.0	1.300	1.000	3.5	< 80.6
C4	3 BeamLeft	1880 10	0	1.2	-2.3	-3.2	E(80)	62.0	3	29.0	1.300	1.000	3.5	< 80.6
C4	3 BeamRight	1880 10	0	15.5	-4.0	-18.4	E(80)	62.0	3	29.0	1.300	1.000	19.5	< 80.6
C4	4 BeamLeft	1880 10	0	15.5	-4.0	-18.4	E(80)	62.0	3	29.0	1.300	1.000	19.5	< 80.6
C4	4 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
C5	1 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
C5	1 BeamRight	1880 10	0	14.3	-3.8	-24.4	E(80)	62.0	3	29.0	1.300	1.000	18.1	< 80.6
C5	2 BeamLeft	1880 10	0	14.3	-3.8	-24.4	E(80)	62.0	3	29.0	1.300	1.000	18.1	< 80.6
C5	2 BeamRight	1880 10	0	0.5	-1.0	-14.9	E(80)	62.0	3	29.0	1.300	1.000	1.5	< 80.6
C5	3 BeamLeft	1880 10	0	0.5	-1.0	-14.9	E(80)	62.0	3	29.0	1.300	1.000	1.5	< 80.6
C5	3 BeamRight	1880 10	0	14.3	-3.8	-24.4	E(80)	62.0	3	29.0	1.300	1.000	18.1	< 80.6
C5	4 BeamLeft	1880 10	0	14.3	-3.8	-24.4	E(80)	62.0	3	29.0	1.300	1.000	18.1	< 80.6
C5	4 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
PF12	1 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
PF12	1 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
PF12	2 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
PF12	2 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
PF12	3 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
PF12	3 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
PF12	4 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
PF12	4 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
PF13	1 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
PF13	1 BeamRight	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6
PF13	2 BeamLeft	1880 10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0	< 80.6

Node WEB-L-1 (WebLowerEdge) WEB - 1

													Stress	
Panel	Web	Grade										$\Delta \sigma_{ce} \cdot \text{Cycle}$		
	h t	σ_{tmax}	σ_{tmin}	σ_d	$(\Delta \sigma_f)$	$\Delta \sigma_{ce}$	m	$\Delta \sigma_{ve}$	CR	Ct	$\Delta \sigma_{max}$	CR · Ct	D	
	(mm)	(N/mm ²)										(N/mm ²)		
PF13	2 BeamRight	1880	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF13	3 BeamLeft	1880	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF13	3 BeamRight	1880	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF13	4 BeamLeft	1880	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
PF13	4 BeamRight	1880	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S1	1 BeamLeft	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S1	1 BeamRight	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S1	2 BeamLeft	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S1	2 BeamRight	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S1	3 BeamLeft	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S1	3 BeamRight	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S1	4 BeamLeft	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S1	4 BeamRight	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S2	1 BeamLeft	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S2	1 BeamRight	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S2	2 BeamLeft	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S2	2 BeamRight	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S2	3 BeamLeft	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S2	3 BeamRight	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S2	4 BeamLeft	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6
S2	4 BeamRight	2080	10	0	0.0	0.0	0.0	E(80)	62.0	3	29.0	1.300	1.000	0.0 < 80.6

Node	HSTIFF-1	(WebH-Stiffener)	WEB - 1	Stress									
Panel	Web	Grade	$\Delta \sigma_{ce} \cdot \text{Cycle}$										
	h t	σ_{tmax} σ_{tmin} σ_d ($\Delta \sigma_f$) $\Delta \sigma_{ce}$ m $\Delta \sigma_{ve}$ CR	Ct	$\Delta \sigma_{max}$ CR \cdot Ct	D								
	(mm)	(N/mm ²)	(N/mm ²)	(N/mm ²)	(N/mm ²)	(N/mm ²)	(N/mm ²)	(N/mm ²)	(N/mm ²)	(N/mm ²)	(N/mm ²)	(N/mm ²)	
C1	1 BeamLeft	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
C1	1 BeamRight	1880 9 376	8.6	-2.3	-14.7	G(50)	32.0	3	15.0	1.300	1.000	10.9	< 41.6
C1	2 BeamLeft	1880 9 376	8.6	-2.3	-14.7	G(50)	32.0	3	15.0	1.300	1.000	10.9	< 41.6
C1	2 BeamRight	1880 9 376	0.3	-0.6	-9.0	G(50)	32.0	3	15.0	1.300	1.000	0.9	< 41.6
C1	3 BeamLeft	1880 9 376	0.3	-0.6	-9.0	G(50)	32.0	3	15.0	1.300	1.000	0.9	< 41.6
C1	3 BeamRight	1880 9 376	8.6	-2.3	-14.7	G(50)	32.0	3	15.0	1.300	1.000	10.9	< 41.6
C1	4 BeamLeft	1880 9 376	8.6	-2.3	-14.7	G(50)	32.0	3	15.0	1.300	1.000	10.9	< 41.6
C1	4 BeamRight	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
C2	1 BeamLeft	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
C2	1 BeamRight	1880 9 376	9.3	-2.4	-11.1	G(50)	32.0	3	15.0	1.300	1.000	11.7	< 41.6
C2	2 BeamLeft	1880 9 376	9.3	-2.4	-11.1	G(50)	32.0	3	15.0	1.300	1.000	11.7	< 41.6
C2	2 BeamRight	1880 9 376	0.7	-1.4	-1.9	G(50)	32.0	3	15.0	1.300	1.000	2.1	< 41.6
C2	3 BeamLeft	1880 9 376	0.7	-1.4	-1.9	G(50)	32.0	3	15.0	1.300	1.000	2.1	< 41.6
C2	3 BeamRight	1880 9 376	9.3	-2.4	-11.1	G(50)	32.0	3	15.0	1.300	1.000	11.7	< 41.6
C2	4 BeamLeft	1880 9 376	9.3	-2.4	-11.1	G(50)	32.0	3	15.0	1.300	1.000	11.7	< 41.6
C2	4 BeamRight	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
C3	1 BeamLeft	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
C3	1 BeamRight	1880 9 376	5.4	-1.8	-2.9	G(50)	32.0	3	15.0	1.079	1.000	7.2	< 34.5
C3	2 BeamLeft	1880 9 376	5.4	-1.8	-2.9	G(50)	32.0	3	15.0	1.079	1.000	7.2	< 34.5
C3	2 BeamRight	1880 9 376	1.6	-1.0	-11.4	G(50)	32.0	3	15.0	1.300	1.000	2.6	< 41.6
C3	3 BeamLeft	1880 9 376	1.6	-1.0	-11.4	G(50)	32.0	3	15.0	1.300	1.000	2.6	< 41.6
C3	3 BeamRight	1880 9 376	5.4	-1.8	-2.9	G(50)	32.0	3	15.0	1.079	1.000	7.2	< 34.5
C3	4 BeamLeft	1880 9 376	5.4	-1.8	-2.9	G(50)	32.0	3	15.0	1.079	1.000	7.2	< 34.5
C3	4 BeamRight	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
C4	1 BeamLeft	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
C4	1 BeamRight	1880 9 376	9.3	-2.4	-11.1	G(50)	32.0	3	15.0	1.300	1.000	11.7	< 41.6
C4	2 BeamLeft	1880 9 376	9.3	-2.4	-11.1	G(50)	32.0	3	15.0	1.300	1.000	11.7	< 41.6
C4	2 BeamRight	1880 9 376	0.7	-1.4	-1.9	G(50)	32.0	3	15.0	1.300	1.000	2.1	< 41.6
C4	3 BeamLeft	1880 9 376	0.7	-1.4	-1.9	G(50)	32.0	3	15.0	1.300	1.000	2.1	< 41.6
C4	3 BeamRight	1880 9 376	9.3	-2.4	-11.1	G(50)	32.0	3	15.0	1.300	1.000	11.7	< 41.6
C4	4 BeamLeft	1880 9 376	9.3	-2.4	-11.1	G(50)	32.0	3	15.0	1.300	1.000	11.7	< 41.6
C4	4 BeamRight	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
C5	1 BeamLeft	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
C5	1 BeamRight	1880 9 376	8.6	-2.3	-14.7	G(50)	32.0	3	15.0	1.300	1.000	10.9	< 41.6
C5	2 BeamLeft	1880 9 376	8.6	-2.3	-14.7	G(50)	32.0	3	15.0	1.300	1.000	10.9	< 41.6
C5	2 BeamRight	1880 9 376	0.3	-0.6	-9.0	G(50)	32.0	3	15.0	1.300	1.000	0.9	< 41.6
C5	3 BeamLeft	1880 9 376	0.3	-0.6	-9.0	G(50)	32.0	3	15.0	1.300	1.000	0.9	< 41.6
C5	3 BeamRight	1880 9 376	8.6	-2.3	-14.7	G(50)	32.0	3	15.0	1.300	1.000	10.9	< 41.6
C5	4 BeamLeft	1880 9 376	8.6	-2.3	-14.7	G(50)	32.0	3	15.0	1.300	1.000	10.9	< 41.6
C5	4 BeamRight	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
PF12	1 BeamLeft	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
PF12	1 BeamRight	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
PF12	2 BeamLeft	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
PF12	2 BeamRight	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
PF12	3 BeamLeft	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
PF12	3 BeamRight	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
PF12	4 BeamLeft	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
PF12	4 BeamRight	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
PF13	1 BeamLeft	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
PF13	1 BeamRight	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6
PF13	2 BeamLeft	1880 9 376	0.0	0.0	0.0	G(50)	32.0	3	15.0	1.300	1.000	0.0	< 41.6

Beam

Node HSTIFF-1 (WebH-Stiffener) WEB - 1

													Stress	
Panel	Web	h t		$\sigma_{tmax} \sigma_{tmin}$		Grade		$\Delta \sigma_{ce m}$	$\Delta \sigma_{ve CR}$	Ct	$\Delta \sigma_{ce} \cdot \text{Cycle}$			
		(mm)	(mm)	(N/mm ²)	(N/mm ²)	σ_d	($\Delta \sigma_f$)				(N/mm ²)	CR • Ct	D	
PF13	2 BeamRight	1880	9 376	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
PF13	3 BeamLeft	1880	9 376	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
PF13	3 BeamRight	1880	9 376	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
PF13	4 BeamLeft	1880	9 376	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
PF13	4 BeamRight	1880	9 376	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S1	1 BeamLeft	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S1	1 BeamRight	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S1	2 BeamLeft	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S1	2 BeamRight	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S1	3 BeamLeft	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S1	3 BeamRight	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S1	4 BeamLeft	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S1	4 BeamRight	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S2	1 BeamLeft	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S2	1 BeamRight	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S2	2 BeamLeft	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S2	2 BeamRight	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S2	3 BeamLeft	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S2	3 BeamRight	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S2	4 BeamLeft	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		
S2	4 BeamRight	2080	9 416	0.0	0.0	0.0	G(50)	32.0 3	15.0	1.300	1.000	0.0 < 41.6		

§9. Design of Bridge Accessories

9-1 Design of Bearing

Design of Lubber Bearing - for Steel-I Girder Bridge

1. Design Condition

(1) Horizontal Seismic Coefficient

No	Area	Type of Group	Horizontal Seismic Coefficient	
			In Bridge Axis Direction	In the Direction of Perpendicular to Bridge Axis
			Level 1	Level 1
			kh	kh
PF11	A2	Type III	0.30	0.30
PF12	A2	Type III	0.30	0.30
PF13	A2	Type III	0.30	0.30
PF14	A2	Type III	0.30	0.30

(2) Design Reaction Force

No	Design Reaction Force						
	Maximum of Bearing		Minimum of Bearing	Dead Load		Total of Dead Load	Live Load
	Rmax1	Rmax2	Rmin	Rdmax	Rdmin	ΣR_d	RL+I
	kN	kN	kN	kN	kN	kN	kN
PF11	773.9	653.2	244.0	451.0	306.5	1890.6	372.5
PF12	2491.2	1970.2	1284.7	1824.5	1319.9	7762.2	---
PF13	2491.2	1970.2	1284.7	1824.5	1319.9	7762.2	---
PF14	773.9	653.2	244.0	451.0	306.5	1890.6	372.5

(3) Regular Displacement

No	Temp. Change	Indeterminate			Live Load	Total	
		Dry Shrinkage /	Dead Load	Total		+30°C	-30°C
		ΔL_t	ΔL_{scp}	ΔL_d		$\Delta L'$	ΔL_r
	mm	mm	mm	mm	mm	mm	
PF11	± 18.1	----	----	----	3.6	21.6	-14.5
PF12	± 7.8	----	----	----	4.0	11.8	-3.8
PF13	± 7.8	----	----	----	4.0	11.8	-3.8
PF14	± 18.1	----	----	----	3.6	21.6	-14.5

※ Positive number means expanding, while negative number means shrinking.
The larger value is adopted comparing absolute value to check the allowable stress.

(4) Oblique and Rotation Angle

No	Oblique Angle			Rotation Angle
	θ			$\Sigma a\epsilon$
	°	'	"	rad
PF11	90	0	0	1 / 450
PF12	90	0	0	1 / 400
PF13	90	0	0	1 / 400
PF14	90	0	0	1 / 450

(5) Allowable Value

Item		Code	Unit	Value
Maximum Compressive Stress	Under Design Load	σ_{max}	N/mm ²	$\leq 8.0 \leq S1 \leq 12.0$
Difference of Compressive Stress	Under Design Load	$\Delta\sigma$	N/mm ²	$\leq 5.0 \text{ --- } S1 \leq 8$ $\leq 5+0.375(S1-8) \leq 6.5 \text{ --- } S1 > 8$
Tensile Stress	Under Earthquake	σ_t	N/mm ²	$\leq 1.2 \text{ --- } G6$ $\leq 1.6 \text{ --- } G8$ $\leq 2.0 \text{ --- } G10\text{以上}$
Shear Strain	Under Design Load	γ_{sa}	%	≤ 70
	Level 1	γ_{sea}	%	≤ 150
	Level 2	γ_{sea}	%	≤ 250
Safety Factor of Local Shear Strain	Under Design Load	f_s	----	1.5
Stress of Stiffener	Under Design Load	σ_{sa}	N/mm ²	≤ 140.0
	Under Earthquake	σ_{sa}		≤ 210.0

2. Calculation

(1) Calculation of Vertical Force

1) Vertical Force under Earthquake

$$RL = R_{dmax} + \sqrt{R_{HEQ}^2 + R_{VEQmax}^2}$$

$$RU = R_{dmin} - \sqrt{R_{HEQ}^2 + R_{VEQmin}^2}$$

2) Vertical force due to horizontal force applied in the direction of perpendicular to bridge axis

$$R_{HEQ} = \frac{H \cdot h_s}{\sum x_i^2} \cdot x_i$$

h_s : Vertical distance from a bearing to a center of girder

x_i : Horizontal distance from a bearing to a center of girder

No	Vertical Distance	Horizontal Distance	
	h_s	x_i	$\sum x_i^2$
	m	m	m ²
PF11	2.40	5.20	67.60
PF12	2.40	5.20	67.60
PF13	2.40	5.20	67.60
PF14	2.40	5.20	67.60

3) Vertical Force generated by Design Vertical Seismic Coefficient (k_v)

$$R_{VEQmax} = k_v \cdot R_{dmax}$$

$$R_{VEQmin} = k_v \cdot R_{dmin}$$

No	Vertical Seismic Coefficient	
	Level 1	
	In Bridge Axis Direction	In the Direction of Perpendicular to Bridge Axis
	k_v	k_v
PF11	0.12	0.12
PF12	0.12	0.12
PF13	0.12	0.12
PF14	0.12	0.12

10) Result

• Stiffness and Coefficient

No	Stiffness		Coefficient				
	Horizontal	Vertical	Shape	Secondary shape		Distortion	Local inspection
	KB	KV	S1	S2	S2	E	E
	kN/mm	kN/mm	----	Bridge Axis Direction	Perpendicular to Bridge Axis	N/mm2	N/mm2
PF11	3.78	892.4	6.64	7.03	7.03	298.73	292.98
PF12	9.11	1409.4	6.94	7.39	7.39	312.37	320.05
PF13	9.11	1409.4	6.94	7.39	7.39	312.37	320.05
PF14	3.78	892.4	6.64	7.03	7.03	298.73	292.98

• Displacement under earthquake

No	Bridge Axis Direction	Perpendicular to Bridge Axis
	Level 1	Level 1
	UB	UB
	mm	mm
PF11	27.2	----
PF12	26.6	----
PF13	29.2	----
PF14	32.8	----

• Bearing surface area

No	Bridge Axis Direction		Perpendicular to Bridge Axis	Distortion	
	Stationary	Earthquake Level 1	Earthquake Level 1	Bearing load	Live load
	Acn	Ace	Ace	δ_o	δ_{cl}
	m2	m2	m2	mm	mm
PF11	0.1814	0.1790	0.1912	0.91	0.21
PF12	0.3894	0.3798	0.3971	1.80	----
PF13	0.3894	0.3781	0.3971	1.80	----
PF14	0.1814	0.1764	0.1912	0.91	0.21

• Checking of Stationary load

No	Compressive stress			Buckling stress	Strain		Local shear strain				Stiffener stress
	Max	Min	Max-Min		Rotation	Vertical	Vertical	Shear	Rotation	Total	
	σ_{max}	σ_{min}	$\Delta\sigma$	σ_{cra}	δ_r	δ_c	γ_c	γ_s	γ_r	γ_t	σ_s
	N/mm ²	N/mm ²	N/mm ²	N/mm ²	mm	mm	%	%	%	%	N/mm ²
PF11	4.27	1.28	2.99	18.67	0.50	0.56	82.15	33.82	19.59	135.55	63.98
PF12	6.40	3.24	3.16	20.51	0.81	1.08	117.95	13.41	24.09	155.45	93.84
PF13	6.40	3.24	3.16	20.51	0.81	1.08	117.95	13.41	24.09	155.45	93.84
PF14	4.27	1.28	2.99	18.67	0.50	0.56	82.15	33.82	19.59	135.55	63.98
Allowable value	≤ 8.0 $\leq S1$ ≤ 12.0	----	≤ 5.0 - $S1 \leq 8$ $5+0.375 \cdot (S1-8)$ $\geq 6.5 \cdot S1 > 8$	$\geq \sigma_{max}$	----	$\geq \delta_r$	----	≤ 70	----	$\leq \gamma_u/1.5$	≤ 140.0

• Checking for seismic resistance level 1

No	Bridge Axis Direction											
	Displacement	Shear strain	Lateral force	Shear stress		Yield load	Equivalent elastic stiffness	Primary	Secondary	K1 · K2 intersection point		Equivalent attenuation
				q	qo					Qy	Uy	
	UB	γ	F	q	qo	Qd	KB	K1	K2	Qy	Uy	hB
mm	---	kN	N/mm ²	N/mm ²	kN	kN/mm	kN/mm	kN/mm	kN	mm	---	
PF11	27.20	0.30	156.81	8.84	7.09	80.15	8.24	18.32	2.82	94.72	5.17	0.264
PF12	26.60	0.21	243.93	6.28	5.04	128.25	13.10	28.27	4.35	151.57	5.36	0.267
PF13	29.20	0.23	267.77	6.90	5.53	140.79	13.10	28.27	4.35	166.39	5.89	0.267
PF14	32.80	0.36	186.15	10.40	8.34	94.29	8.11	18.20	2.80	111.43	6.12	0.262

No	Perpendicular to Bridge Axis											
	Displacement	Shear strain	Lateral force	Shear stress		Yield load	Equivalent elastic stiffness	Primary	Secondary	K1 · K2 intersection point		Equivalent attenuation
				q	qo					Qy	Uy	
	UB	γ	F	q	qo	Qd	KB	K1	K2	Qy	Uy	hB
mm	---	kN	N/mm ²	N/mm ²	kN	kN/mm	kN/mm	kN/mm	kN	mm	---	
PF11	---	---	---	---	---	---	---	---	---	---	---	---
PF12	---	---	---	---	---	---	---	---	---	---	---	---
PF13	---	---	---	---	---	---	---	---	---	---	---	---
PF14	---	---	---	---	---	---	---	---	---	---	---	---

No	Bridge Axis Direction					Perpendicular to Bridge Axis					Tension Stress
	Bearing stress	Tension stress	Buckling stress	Shear stress	Stiffener stress	Bearing stress	Tension stress	Buckling stress	Shear strain	Stiffener stress	
	σ_{ce}	σ_{te}	σ_{crae}	γ_{se}	σ_{se}	σ_{ce}	σ_{te}	σ_{crae}	γ_{se}	σ_{se}	σ_{te}
	N/mm ²	N/mm ²	N/mm ²	%	N/mm ²	N/mm ²	N/mm ²	N/mm ²	%	N/mm ²	N/mm ²
PF11	2.82	----	31.12	42.50	42.34	2.98	----	31.12	----	44.63	0.71
PF12	5.38	----	34.18	30.23	78.92	5.81	----	34.18	----	85.22	1.38
PF13	5.40	----	34.18	33.18	79.27	5.81	----	34.18	----	85.22	1.38
PF14	2.86	----	31.12	51.25	42.95	2.98	----	31.12	----	44.63	0.71
Allowable value	----	$\leq \sigma_a$	$\geq \sigma_{ce}$	≤ 150	≤ 210.0	----	$\leq \sigma_a$	$\geq \sigma_{ce}$	≤ 150	≤ 210.0	$\leq \sigma_a$

(4) Summary

No	Type	Size			Rubber				Stiffener	Bearing stiffness	
		Perpendicular to Bridge Axis	Bridge Axis Direction	Thickness	Elastic modulus	Thickness	Number of layers	Total thickness		Horizontal	Vertical
		b'	a'	t	Ge	te	n	Σte	ts	KB	KV
		mm	mm	mm	N/mm ²	mm	Layer	mm	mm	kN/mm	kN/mm
PF11	N R	470	470	134	1.00	16	4	64	3.2	3.78	892.4
PF12	N R	670	670	170	1.00	22	4	88	4.5	9.11	1409.4
PF13	N R	670	670	170	1.00	22	4	88	4.5	9.11	1409.4
PF14	N R	470	470	134	1.00	16	4	64	3.2	3.78	892.4

Bearing Condition for Substructure Design

$$\text{Difference} = \frac{UB-UB'}{UB} \times 100 \text{ (\%)}$$

	$\Sigma KB(kN/m)$	Seismic Force (kN)	Assumed displacement value (m)	Actual displacement (m)	Difference (%)
Bridge 1-Support-1	-----	-----	-----	-----	-----
Bridge 1-Support-2	-----	-----	-----	-----	-----
Bridge 1-Support-3	-----	-----	-----	-----	-----
Bridge 2-Support-1	2.263632E+004	1609.673	0.0761	0.0711	6.501
Bridge 2-Support-2	4.364701E+004	3114.750	0.0762	0.0714	6.328
Bridge 2-Support-3	4.364701E+004	2529.781	0.0623	0.0580	6.978
Bridge 2-Support-4	2.585569E+004	1372.176	0.0579	0.0531	8.319
Bridge 3-Support-1	-----	-----	-----	-----	-----
Bridge 3-Support-2	-----	-----	-----	-----	-----
Bridge 3-Support-3	-----	-----	-----	-----	-----
Bridge 4-Support-1	-----	-----	-----	-----	-----
Bridge 4-Support-2	-----	-----	-----	-----	-----
Bridge 4-Support-3	-----	-----	-----	-----	-----
Bridge 4-Support-4	-----	-----	-----	-----	-----
Bridge 4-Support-5	-----	-----	-----	-----	-----
Bridge 5-Support-1	4.117886E+004	1066.506	0.0272	0.0259	4.952
Bridge 5-Support-2	6.550148E+004	1663.639	0.0266	0.0254	4.664
Bridge 5-Support-3	6.550148E+004	1829.754	0.0292	0.0279	4.389
Bridge 5-Support-4	4.056619E+004	1265.081	0.0328	0.0312	4.820
Bridge 6-Support-1	-----	-----	-----	-----	-----
Bridge 6-Support-2	-----	-----	-----	-----	-----
Bridge 6-Support-3	-----	-----	-----	-----	-----

9-2 Bridge drainage

Calculation for catchpit interval

1. Design conditions

Rain intensity	I =	$\beta \times 149.0 = 149$	mm/h
	$\beta =$	1.00	
Discharge coefficient	C =	0.9	
Roughness coefficient	n =	0.013	
Safety factor	k =	0.8	
Minimum interval	L =	5.000	m

1) Calculation for catchpit interval

$$L_s = \frac{2.46 \times 10^{-8} \times A \times R^{2/3} \cdot i^{1/2}}{\beta \times rh \times B}$$

Ls : Interval (m) ($L_s \leq 20$ m)

A : flowing area (m²) $A = 1/2 \times h \times b$

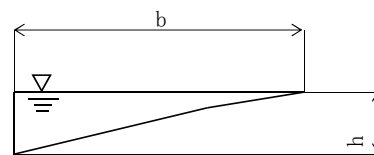
R : Depth (m), $R = A / S$

S : flowing length $S = h + \sqrt{b^2 + h^2}$

i : Longitudinal slope

$\beta \times rh$: Design rain intensity

B : Road width (m)



Calculation of Catch Pit Interval

Fly Over (Left Side)

		Length	C.L Height	Longitudinal Slope	Transverse Gradient	Flowing water Width	Depth h	Flow area A	Wetted per Imte	Hydraulic mean depth	Watershed width	Rain intensity	Fall rate	Drainage PIT Maximum Interval	PIT Interval
		(m)	(m)	(%)	(%)	(m)	(m)	A (m2)	P (m)	R(m)	(m)	I[mm/h]	γ	Ls (m)	
PC	AF1	0.0000	10.5800	-	3.44	1.000	0.0344	0.0172	1.0350	0.0166	-		-	-	
	EDR1	4.992	10.7298	3.00	4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	
	DR1	5.008	10.8800	3.00	4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	
	DR2	10.000	11.1800	3.00	4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	
	PF1(DR3)	10.000	11.4800	3.00	4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	
	DR4	10.000	11.7800	3.00	4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	
	EDR2	8.080	12.0224	3.00	4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	
Steel-Box	DR5	1.920	12.0800	3.00	3.89	1.000	0.0389	0.0195	1.0397	0.0187	12.750	149.000	0.90	30.7	
	PF2(DR6)	10.000	12.3800	3.00	3.34	1.000	0.0334	0.0167	1.0340	0.0162	12.750	149.000	0.90	23.9	
	DR7	10.000	12.6800	3.00	2.78	1.000	0.0278	0.0139	1.0282	0.0135	12.750	149.000	0.90	17.7	
	DR8	10.000	12.9800	3.00	2.22	1.000	0.0222	0.0111	1.0224	0.0109	12.750	149.000	0.90	12.2	
	EDR3	4.000	13.1000	3.00	2.00	1.000	0.0200	0.0100	1.0202	0.0098	12.750	149.000	0.90	10.3	
	DR9	6.000	13.2799	3.00	1.40	1.000	0.0140	0.0070	1.0141	0.0069	12.750	149.000	0.90	5.7	
	DR10	10.000	13.5684	2.89	0.40	1.000	0.0040	0.0020	1.0040	0.0020	12.750	149.000	0.90	0.7	5
	EDR4	4.000	13.6784	2.75	0.00	1.000	0.0000	0.0000	1.0000	0.0000	12.750	149.000	0.90	0.0	5
	DR11	6.000	13.8376	2.65	-0.60	1.000	0.0060	0.0030	1.0060	0.0030	12.750	149.000	0.90	1.3	5
	PF3	5.000	13.9650	2.55	-1.10	1.000	0.0110	0.0055	1.0111	0.0054	12.750	149.000	0.90	3.5	5
	DR12	5.000	14.0876	2.45	-1.60	1.000	0.0160	0.0080	1.0161	0.0079	12.750	149.000	0.90	6.4	6
	EDR5	4.000	14.1822	2.36	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	12.750	149.000	0.90	9.1	9
	DR13	6.000	14.3184	2.27	-2.68	1.000	0.0268	0.0134	1.0272	0.0130	12.750	149.000	0.90	14.5	14
	DR14	10.000	14.5299	2.11	-3.81	1.000	0.0381	0.0191	1.0388	0.0183	12.750	149.000	0.90	24.9	20
	DR15	10.000	14.7222	1.92	-4.95	1.000	0.0495	0.0248	1.0507	0.0236	12.750	149.000	0.90	36.5	20
	EDR6	9.298	14.8838	1.74	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	47.5	20
	DR16	0.702	14.8953	1.64	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	46.1	20
	DR17	10.000	15.0491	1.54	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	44.7	20
	DR18	10.000	15.1837	1.35	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	41.8	20
	PF4	5.000	15.2438	1.20	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	39.5	20
	DR19	5.000	15.2991	1.11	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	37.9	20
	DR20	10.000	15.3953	0.96	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	35.3	20
	DR21	10.000	15.4722	0.77	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	31.6	20
	DR22	10.000	15.5300	0.58	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	27.4	20
DR23	10.000	15.5800	0.50	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	25.5	20	
PC-2	PF5(DR24)	10.000	15.6300	0.50	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	25.5	20
	DR25	10.000	15.6800	0.50	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	25.5	20
	DR26	10.000	15.7264	0.46	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	24.5	20
	PF6(DR27)	10.000	15.7541	0.28	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	19.0	18
	DR28	10.000	15.7616	0.08	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	9.9	9
	EDR7	5.571	15.7569	-0.08	-6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	10.5	10
	DR29	4.429	15.7488	-0.18	-5.33	1.000	0.0533	0.0267	1.0547	0.0253	12.750	149.000	0.90	12.7	12
PC-4	PF7(DR30)	10.000	15.7158	-0.33	-3.81	1.000	0.0381	0.0191	1.0388	0.0183	12.750	149.000	0.90	9.9	9
	DR31	10.000	15.6625	-0.53	-2.30	1.000	0.0230	0.0115	1.0233	0.0112	12.750	149.000	0.90	5.5	5
	EDR8	1.977	15.6496	-0.65	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	12.750	149.000	0.90	4.8	5
	DR32	8.023	15.5926	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	12.750	149.000	0.90	5.0	5
	PF8(DR33)	10.000	15.5211	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	EDR9	8.383	15.4612	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR34	1.617	15.4496	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR35	10.000	15.3781	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	PF9(DR36)	10.000	15.3066	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR37	10.000	15.2351	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR38	10.000	15.1636	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	PF10(DR39)	10.000	15.0921	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR40	10.000	15.0206	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
DR41	10.000	14.9491	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10	
Steel-I	PF11(DR42)	10.000	14.8776	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR43	10.000	14.8061	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR44	10.000	14.7305	-0.76	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.3	10
	DR45	10.000	14.6339	-0.97	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	11.7	11
	PF12	5.000	14.5770	-1.14	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	12.7	12
	DR46	5.000	14.5144	-1.25	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	13.3	13
	DR47	10.000	14.3720	-1.42	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	14.2	14
	DR48	10.000	14.2068	-1.65	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	15.2	15
	DR49	10.000	14.0188	-1.88	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	16.3	16
	DR50	10.000	13.8079	-2.11	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	17.2	17
	PF13	7.000	13.6467	-2.30	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	18.0	18
	DR51	3.000	13.5742	-2.42	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	18.4	18
	DR52	10.000	13.3176	-2.57	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	19.0	19
	DR53	10.000	13.0382	-2.79	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	19.8	19
	DR54	10.000	12.7400	-2.98	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
PC-2	PF14	2.000	12.6800	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
	DR55	8.000	12.4400	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.009					

Fly Over (Right Side)

		Length	C.L Height	Slope	Gradient	Width	Depth h	Flow area A	Wetted per lime	mean depth	water shed	Rain intensity	Fall rate	Drainage Ls	PIT Interval
		(m)	(m)	(%)	(%)	(m)	(m)	A (m2)	P (m)	R(m)	(m)	I[mm/h]	γ	Ls (m)	
PC-2	AF1	0.0000	10.5800	-	-3.44	1.000	0.0344	0.0172	1.0350	0.0166	-	-	-	-	
	EDR1	4.992	10.7298	3.00	-4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	20
	DR1	5.008	10.8800	3.00	-4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	20
	DR2	10.000	11.1800	3.00	-4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	20
	PF1(DR3)	10.000	11.4800	3.00	-4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	20
	DR4	10.000	11.7800	3.00	-4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	20
	EDR2	8.080	12.0224	3.00	-4.00	1.000	0.0400	0.0200	1.0408	0.0192	12.750	149.000	0.90	32.2	20
DR5	1.920	12.0800	3.00	-3.89	1.000	0.0389	0.0195	1.0397	0.0187	12.750	149.000	0.90	30.7	20	
Steel-I	PF2(DR6)	10.000	12.3800	3.00	-3.34	1.000	0.0334	0.0167	1.0340	0.0162	12.750	149.000	0.90	23.9	20
	DR7	10.000	12.6800	3.00	-2.78	1.000	0.0278	0.0139	1.0282	0.0135	12.750	149.000	0.90	17.7	17
	DR8	10.000	12.9800	3.00	-2.22	1.000	0.0222	0.0111	1.0224	0.0109	12.750	149.000	0.90	12.2	12
	EDR3	4.000	13.1000	3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	12.750	149.000	0.90	10.3	10
	DR9	6.000	13.2799	3.00	-1.40	1.000	0.0140	0.0070	1.0141	0.0069	12.750	149.000	0.90	5.7	5
	DR10	10.000	13.5684	2.89	-0.40	1.000	0.0040	0.0020	1.0040	0.0020	12.750	149.000	0.90	0.7	5
	EDR4	4.000	13.6784	2.75	0.00	1.000	0.0000	0.0000	1.0000	0.0000	12.750	149.000	0.90	0.0	5
	DR11	6.000	13.8376	2.65	0.60	1.000	0.0060	0.0030	1.0060	0.0030	12.750	149.000	0.90	1.3	5
	PF3	5.000	13.9650	2.55	1.10	1.000	0.0110	0.0055	1.0111	0.0054	12.750	149.000	0.90	3.5	
	DR12	5.000	14.0876	2.45	1.60	1.000	0.0160	0.0080	1.0161	0.0079	12.750	149.000	0.90	6.4	
	EDR5	4.000	14.1822	2.36	2.00	1.000	0.0200	0.0100	1.0202	0.0098	12.750	149.000	0.90	9.1	
	DR13	6.000	14.3184	2.27	2.68	1.000	0.0268	0.0134	1.0272	0.0130	12.750	149.000	0.90	14.5	
	DR14	10.000	14.5299	2.11	3.81	1.000	0.0381	0.0191	1.0388	0.0183	12.750	149.000	0.90	24.9	
	DR15	10.000	14.7222	1.92	4.95	1.000	0.0495	0.0248	1.0507	0.0236	12.750	149.000	0.90	36.5	
	EDR6	9.298	14.8838	1.74	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	47.5	
	DR16	0.702	14.8953	1.64	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	46.1	
	DR17	10.000	15.0491	1.54	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	44.7	
	DR18	10.000	15.1837	1.35	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	41.8	
	PF4	5.000	15.2438	1.20	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	39.5	
	DR19	5.000	15.2991	1.11	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	37.9	
	DR20	10.000	15.3953	0.96	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	35.3	
	DR21	10.000	15.4722	0.77	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	31.6	
	DR22	10.000	15.5300	0.58	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	27.4	
DR23	10.000	15.5800	0.50	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	25.5		
PC-2	PF5(DR24)	10.000	15.6300	0.50	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	25.5	
	DR25	10.000	15.6800	0.50	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	25.5	
	DR26	10.000	15.7264	0.46	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	24.5	
	PF6(DR27)	10.000	15.7541	0.28	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	19.0	
	DR28	10.000	15.7616	0.08	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	9.9	
	EDR7	5.571	15.7569	-0.08	6.00	1.000	0.0600	0.0300	1.0618	0.0283	12.750	149.000	0.90	10.5	
	DR29	4.429	15.7488	-0.18	5.33	1.000	0.0533	0.0267	1.0547	0.0253	12.750	149.000	0.90	12.7	
PC-4	PF7(DR30)	10.000	15.7158	-0.33	3.81	1.000	0.0381	0.0191	1.0388	0.0183	12.750	149.000	0.90	9.9	
	DR31	10.000	15.6625	-0.53	2.30	1.000	0.0230	0.0115	1.0233	0.0112	12.750	149.000	0.90	5.5	
	EDR8	1.977	15.6496	-0.65	2.00	1.000	0.0200	0.0100	1.0202	0.0098	12.750	149.000	0.90	4.8	
	DR32	8.023	15.5926	-0.71	0.78	1.000	0.0078	0.0039	1.0078	0.0039	12.750	149.000	0.90	1.0	5
	PF8(DR33)	10.000	15.5211	-0.71	-0.73	1.000	0.0073	0.0037	1.0073	0.0036	6.375	149.000	0.90	1.9	5
	EDR9	8.383	15.4612	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR34	1.617	15.4496	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR35	10.000	15.3781	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	PF9(DR36)	10.000	15.3066	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR37	10.000	15.2351	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR38	10.000	15.1636	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	PF10(DR39)	10.000	15.0921	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
DR40	10.000	15.0206	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10	
DR41	10.000	14.9491	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10	
Steel-I	PF11(DR42)	10.000	14.8776	-0.72	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR43	10.000	14.8061	-0.71	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.0	10
	DR44	10.000	14.7305	-0.76	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	10.3	10
	DR45	10.000	14.6339	-0.97	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	11.7	11
	PF12	5.000	14.5770	-1.14	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	12.7	12
	DR46	5.000	14.5144	-1.25	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	13.3	13
	DR47	10.000	14.3720	-1.42	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	14.2	14
	DR48	10.000	14.2068	-1.65	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	15.2	15
	DR49	10.000	14.0188	-1.88	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	16.3	16
	DR50	10.000	13.8079	-2.11	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	17.2	17
	PF13	7.000	13.6467	-2.30	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	18.0	18
	DR51	3.000	13.5742	-2.42	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	18.4	18
	DR52	10.000	13.3176	-2.57	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	19.0	19
	DR53	10.000	13.0382	-2.79	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	19.8	19
DR54	10.000	12.7400	-2.98	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20	
PC-2	PF14	2.000	12.6800	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
	DR55	8.000	12.4400	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
	DR56	10.000	12.1400	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
	DR57	10.000	11.8400	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
	PF15	2.000	11.7800	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
	DR58	8.000	11.5400	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
	DR59	10.000	11.2400	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20
DR60	10.000	10.9400	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20	
AF2	2.000	10.8800	-3.00	-2.00	1.000	0.0200	0.0100	1.0202	0.0098	6.375	149.000	0.90	20.5	20	

Total 602.0000 m

9-3 Expansion joint

(1) Gap of girder and abutment

The expansion length is determined based on the displacement of the earthquake and the temperature.

Expansion joint shall be installed not to compromise the following gap of the girder and abutment, and displacement of seismic and temperature.

(2) Gap and displacement

				PCI Grider				Steel box Girder				PCI Grider				PCI Girder				Steel I Girder				PCI Girder		
				condition of support	M	F	F	E	E	E	E	F	F	M	M	F	F	F	M	E	E	E	E	F	F	M
				substructure	AF1	PF1	PF2	PF3	PF4	PF5	PF6	PF7	PF8	PF9	PF10	PF11	PF12	PF13	PF14	PF15	AF2					
Gap of girder and abutment		mm	100		150			150		150			150			150			100		100					
expansion	Creep·drying shrinkage (Δ_{sc2})	mm	7		0	0		0	0		-7	14				-14	0			0	0		-7			
	temperature (Δ_t)	mm	± 12		± 0	± 27		± 27	± 0		± 12	± 23				± 23	± 19			± 19	± 0		± 12			
	displacement (Δ_L)	stretching	mm	19		27			27			56					56				19			19		
		reducing	mm	-5		-27			-27			-14					-28				-19			-5		
	Margin (LA)	mm	10		11			11			14					17				10			10			
	Δ_{U2}	mm	34		65			65			84					101				48			34			
	seismic (Δ_{EQ}) SBR $\times 2$	mm	48		260			234			110					144				162			58			
design displacemnt (Δ_{Ej})	mm	48		260			234			110					144				162			58				

03-SUBSTRUCTURE AND FOUNDATION

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§1.Design condition

1. Basic condition

- 1). Bridge length : 602.000 (m)
- 2). Span length : 30.00 + 30.00 + 55.00 + 70.00 + 55.00
 + 30.00 + 30.00 + 30.00 + 30.00 + 30.00 + 30.00
 + 35.00 + 52.00 + 35.00 + 30.00 + 30.00 (m)
- 3). Angle of skew : 92 ° 29 ' 51 " (cross CL) PF7
 : 90 ° 7 ' 9 " (cross CL) PF8
 : 90 ° 0 ' 0 " (cross CL) Other
- 4). Width of the road : B= 12.750m
- 5). Bridge type : 2 span continuous PC- I girder bridge with composite deck(PC plate and RC deck)
 3 span continuous steel box girder bridge
 2 span continuous PC- I girder bridge with composite deck(PC plate and RC deck)
 4 span continuous PC- I girder bridge with composite deck(PC plate and RC deck)
 3 span continuous steel I girder bridge
 2 span continuous PC- I girder bridge with composite deck(PC plate and RC deck)
- 6). Substructure type : inverted T-shaped abutment, T-shaped pier
- 7). Foundation type : Cast-in-place pile φ1500
- 8). Live load : AASHTO HL=93

9). Design condition for substructure

(1) Unit weight

- Reinforced concrete : $\gamma_c = 24.5 \text{ kN/m}^3$
 relaid soil(front side) : $\gamma_d = 18.0 \text{ kN/m}^3$
 water : $\gamma_w = 10.0 \text{ kN/m}^3$

(2) Load of ground surface : $q = 11.6 \text{ kN/m}^2$

(3) Earth pressure method

- dead+ live : Coulomb's earth pressure theory
 seismic : Revise monobe and okabe's earth pressure theory

Backfill : $\gamma = 19.0 \text{ kN/m}^3$ $\phi = 30^\circ$

(4) Materials

	Substructure
Body	$\sigma_{ck}=24\text{N/mm}^2$
Pile cap	$\sigma_{ck}=24\text{N/mm}^2$
Cast-in-place pile	$\sigma_{ck}=24\text{N/mm}^2$ (SD345)

10). Earthquake-resistant condition

- Ground type : Type III
 Design horizontal seismic coefficient : $kh=0.30$

11). Design standard

- Specifications for highway bridges (Japan Road Association)
 1 Common matters,4 substructure,5 seismic design(April 2012)

12). Allowable stress

(1) Allowable stress

a) Allowable stress of concrete

For reinforced concrete structure, the allowable compressive stress of concrete shall be the value in next Table.

Table Allowable compressive stress(N/mm²) and allowable shear stress(N/mm²) for reinforced concrete structure

Stress type		Design standard strength of concrete σ_{ck}			
		21	24	27	30
Compressive stress	Bending compressive stress	7.0	8.0	9.0	10.0
	Axial compressive stress	5.5	6.5	7.5	8.5
Shear stress	Concrete (τ_{a1})	0.22	0.23	0.24	0.25
	Concrete+Reinforcement (τ_{a2})	1.6	1.7	1.8	1.9
	Punching shear stress (τ_{a3})	0.85	0.90	0.95	1.00

The allowable bond stress of concrete shall be the values in next Table for reinforcement of 51 mm in diameter or less.

Table Allowable bond stress(N/mm²)

Stress type		Design standard strength of concrete σ_{ck}			
		21	24	27	30
Deformed bar		1.4	1.6	1.7	1.8

b) Allowable stress of reinforcement

The allowable stress of reinforcement for reinforced concrete shall be the values in next Table for reinforcement of 51 mm in diameter or less.

Table allowable stress(N/mm²) of reinforcement

Stress and member type		reinforcement type			
		SD345	SD390	SD490	
Tensile stress	1) Principal loads other than live load and impact (For example:beams)	100	100	100	
	Reference value of allowable stress to be used when collision load or the effects of earthquakes are not considered in the combination of loads	2) General members	180	180	180
		3) Members in water or less	160	160	160
	Reference value of allowable stress to be used when collision load or the effects of earthquakes are considered in the combination loads	4) Axial reinforcement	200	230	290
		5) other less	200	200	200
	6) Reference value of allowable stress to be used when calculating the lap joint length or bond length of reinforcement		200	230	290
7) Compressive stress		200	230	290	

(2) Increase coefficient of allowable stress

Allowable stress used in the design of substructure shall be the value multiplied by an increase coefficient given in the next Table according to the combination of loads.

Table Increase Coefficient of Allowable Stress

combination of loads	Increase coefficient
1) Principal loads (P) + Special loads corresponding to "Principal load" (PP)	1.00
2) Principal loads (P) + Special loads corresponding to "Principal load" (PP) +Effects of temperature changes(T)	1.15
3) Principal loads (P) + Special loads corresponding to "Principal load" (PP) +Wind load(W)	1.25
4) Principal loads (P) + Special loads corresponding to "Principal load" (PP) +Effects of temperature changes(T)+Wind load(W)	1.35
5) Principal loads (P) + Special loads corresponding to "Principal load" (PP) +Braking load(BK)	1.25
6) Principal loads (P) + Special loads corresponding to "Principal load" (PP) +Collision load(CO)	1.50
7) Principal loads other than live load and impact+Effects of eathquakes(EQ)	1.50

Load for design of substructure

[kN]

Load category		AF1	PF1	PF2		PF3	PF4	PF5		PF6	PF7		
		M	F	F	E	E	E	E	F	F	M	M	
Vertical load		① Dead load	3800	7000	3900	3200	11100	11200	3200	3800	7700	3900	4300
		② Live load	1100	2000	1100	1600	3100	3100	1600	1100	2000	1100	1100
Horizontal load	Bridge-axial direction	③ Drying shrinkage load	0	600	700	0	0	0	0	400	300	0	0
		④ Temperature load	0	800	1100	0	0	0	0	600	400	0	0
		⑤ seismic load	600	3200	1300	1700	3200	2600	1400	2600	2100	600	700
				3000					4000			1300	
	Bridge-axial-orthogonal direction	④ Wind load	0	300	300	600	600	300	300	300	200		
		⑤ seismic load	0	2000	2300	3500	3100	2100	3000	1600			

[kN]

Load category		PF8	PF9	PF10	PF11		PF12	PF13	PF14		PF15	AF2	
		F	F	F	M	E	E	E	E	F	F	M	
Vertical load		① Dead load	8400	7900	7800	3900	1900	7800	7800	1900	3800	7700	3800
		② Live load	1900	1800	1900	1100	1200	2500	2500	1200	1100	2000	1100
Horizontal load	Bridge-axial direction	③ Drying shrinkage load	800	100	900	0	0	0	0	0	700	600	0
		④ Temperature load	1300	100	1300	0	0	0	0	0	1000	700	0
		⑤ seismic load	3200	2800	3800	600	1100	1700	1900	1300	1200	3500	600
				1700			2500						
	Bridge-axial-orthogonal direction	④ Wind load	300	300	300	300	400	400	300	300	300	0	
		⑤ seismic load	2900	2600	3000	1500	2200	2300	1700	2800	0		

Load for design of beams

with impact

[kN]

Load category			AF1		PF1L		PF1R		PF2L		PF2R		PF3		PF4		PF5L		PF5R		PF6L		PF6R		PF7L		PF7R	
			G1	G4	G1	G4	G1	G4	G1	G4	G1	G2	G1	G2	G1	G2	G1	G2	G1	G4	G1	G4	G1	G4	G1	G4	G1	G4
Vertical load	Dead load	Design value	910	900	830	800	820	850	910	920	1680	1510	5490	5570	5630	5490	1380	1780	880	930	840	920	910	930	910	930	930	1100
		Design value	910	900	830	800	820	850	910	920	840	760	2750	2790	2820	2750	690	890	880	930	840	920	910	930	910	930	930	1100
	Live load	Design value	320	330	540	520	540	520	320	330	1000	960	1810	1870	1860	1800	890	1070	330	320	520	550	520	550	330	320	320	340
Horizontal load	Drying shrinkage load	$\textcircled{3}/\Sigma n$	0	0	75	75	75	75	175	175	0	0	0	0	0	0	0	0	100	100	38	38	38	38	0	0	0	0
		Design value	0	0	80	80	80	80	180	180	0	0	0	0	0	0	0	0	100	100	40	40	40	40	0	0	0	0
	Seismic load	$\textcircled{3}+\textcircled{5}/\Sigma n$	150	150	475	475	475	475	500	500	425	425	800	800	650	650	350	350	750	750	300	300	300	300	150	150	175	175
		Design value	150	150	480	480	480	480	500	500	430	430	800	800	650	650	350	350	750	750	300	300	300	300	150	150	180	180

[kN]

Load category			PF8L		PF8R		PF9L		PF9R		PF10L		PF10R		PF11L		PF11R		PF12		PF13		PF14L		PF14R		PF15L		PF15R		AF2	
			G1	G4	G1	G4	G1	G4	G1	G4	G1	G4	G1	G4	G1	G4	G1	G5	G1	G5	G1	G5	G1	G5	G1	G4	G1	G4	G1	G4	G1	G4
Vertical load	Dead load	Design value	920	1200	950	900	930	880	940	960	950	960	890	880	920	920	460	460	1830	1830	1830	1830	460	460	910	910	910	910	900	900	910	910
		Design value	920	1200	950	900	930	880	940	960	950	960	890	880	920	920	460	460	1830	1830	1830	1830	460	460	910	910	910	910	900	900	910	910
	Live load	Design value	470	500	440	430	430	430	430	430	430	430	500	500	340	340	330	330	670	670	670	670	330	330	340	340	550	550	550	550	340	340
Horizontal load	Drying shrinkage load	$\textcircled{3}/\Sigma n$	100	100	100	100	13	13	13	13	113	113	113	113	0	0	0	0	0	0	0	0	0	0	175	175	75	75	75	75	0	0
		Design value	100	100	100	100	20	20	20	20	120	120	120	120	0	0	0	0	0	0	0	0	0	0	200	200	80	80	80	80	0	0
	Seismic load	$\textcircled{3}+\textcircled{5}/\Sigma n$	500	500	500	500	363	363	363	363	588	588	588	588	150	150	220	220	340	340	380	380	260	260	475	475	513	513	513	513	150	150
		Design value	500	500	500	500	370	370	370	370	590	590	590	590	150	150	220	220	340	340	380	380	260	260	480	480	520	520	520	520	150	150

Load for design of bridle seat

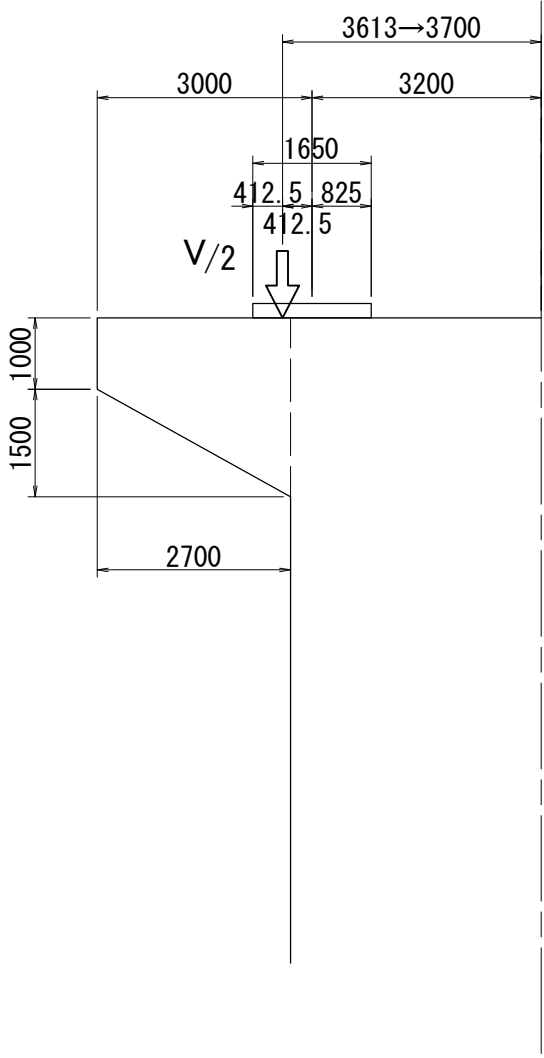
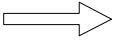
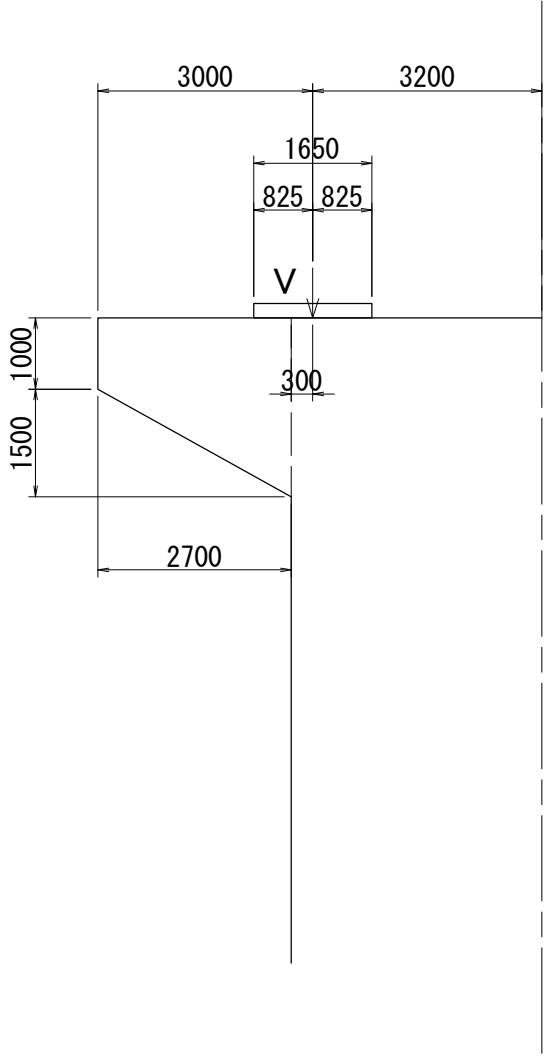
[kN]

Load category			AF1	PF1	PF2L	PF2R	PF3	PF4	PF5L	PF5R	PF6	PF7L	PF7R
Vertical load	Minimum dead load	Design value	0	0	0	1510	5490	5490	1380	0	0	0	0
		$\textcircled{3}+\textcircled{5}/\Sigma n$	285	1267	333	850	1600	1300	700	500	800	293	323
Horizontal load	Seismic load	Design value	290	1270	340	850	1600	1300	700	500	800	300	330

[kN]

Load category			PF8	PF9	PF10	PF11L	PF11R	PF12	PF13	PF14L	PF14R	PF15	AF2
Vertical load	Minimum dead load	Design value	0	0	0	460	1830	1830	460	0	0	0	0
		$\textcircled{3}+\textcircled{5}/\Sigma n$	1333	967	1567	293	220	340	380	260	317	1367	285
Horizontal load	Seismic load	Design value	1340	970	1570	300	220	340	380	260	320	1370	290

Steel Box girder Beam design model



Concrete I girder

$$S=0.2+0.005l$$

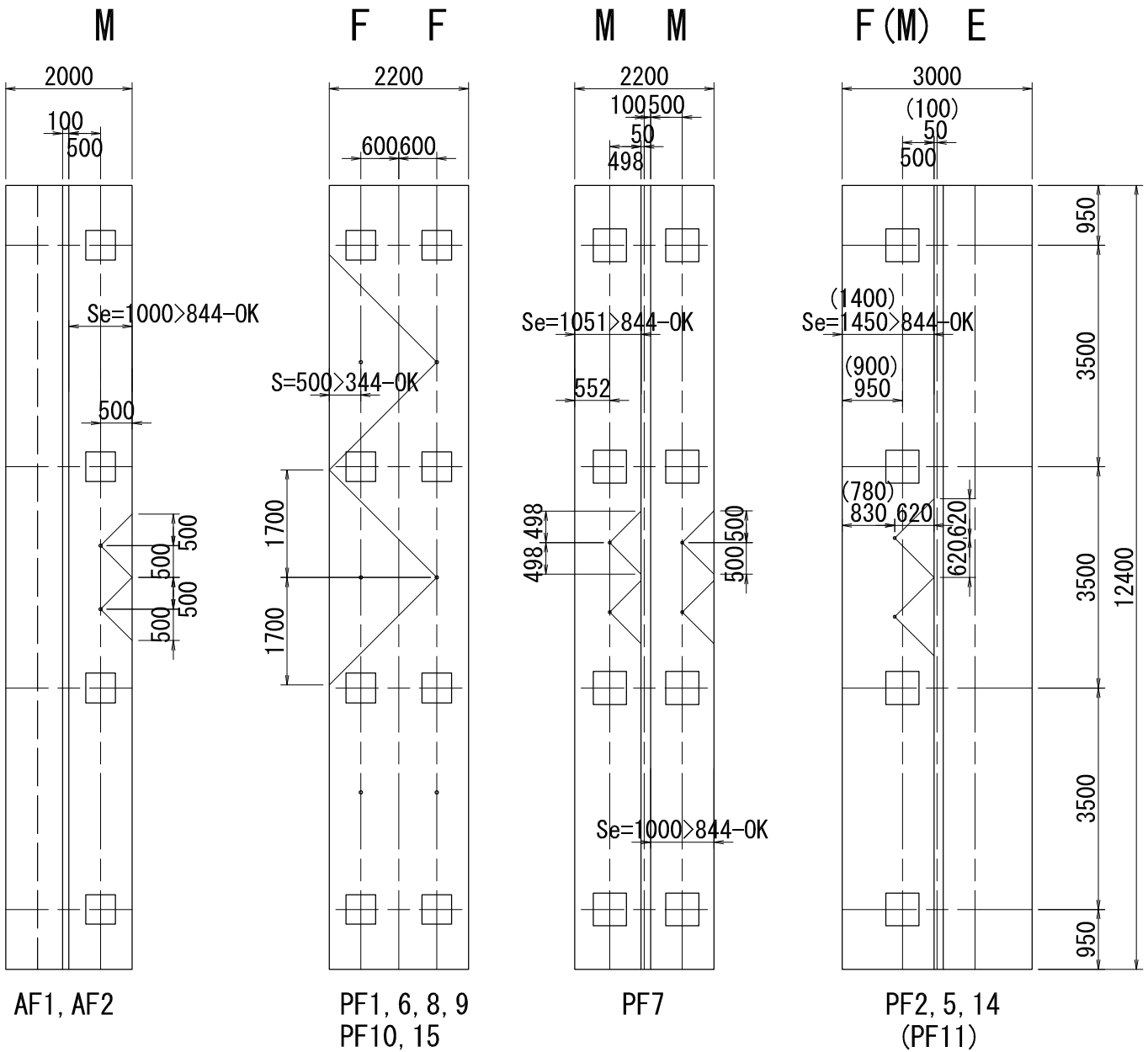
$$=0.2+0.005 \times 28.8$$

$$=0.344\text{m}$$

$$S_e=0.7+0.005l$$

$$=0.7+0.005 \times 28.8$$

$$=0.844\text{m}$$

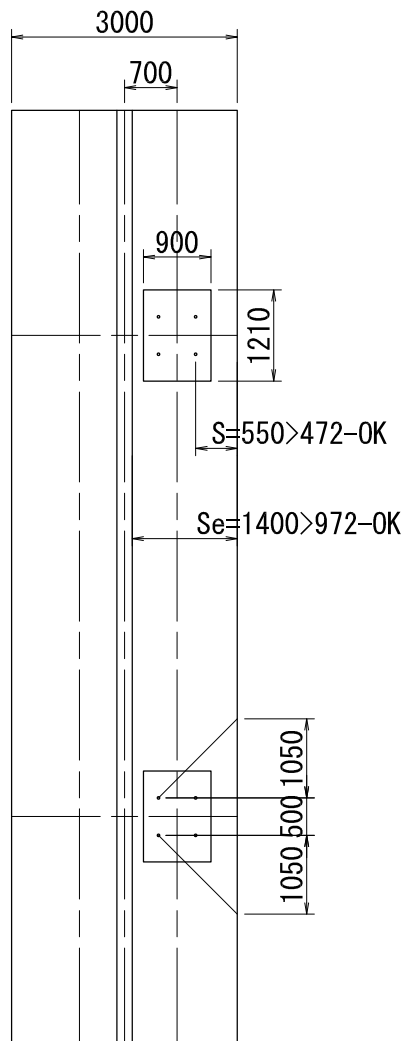


Steel Box girder

$$\begin{aligned}
 S &= 0.2 + 0.005l \\
 &= 0.2 + 0.005 \times 54.3 \\
 &= 0.472\text{m}
 \end{aligned}$$

$$\begin{aligned}
 Se &= 0.7 + 0.005l \\
 &= 0.7 + 0.005 \times 54.3 \\
 &= 0.972\text{m}
 \end{aligned}$$

E

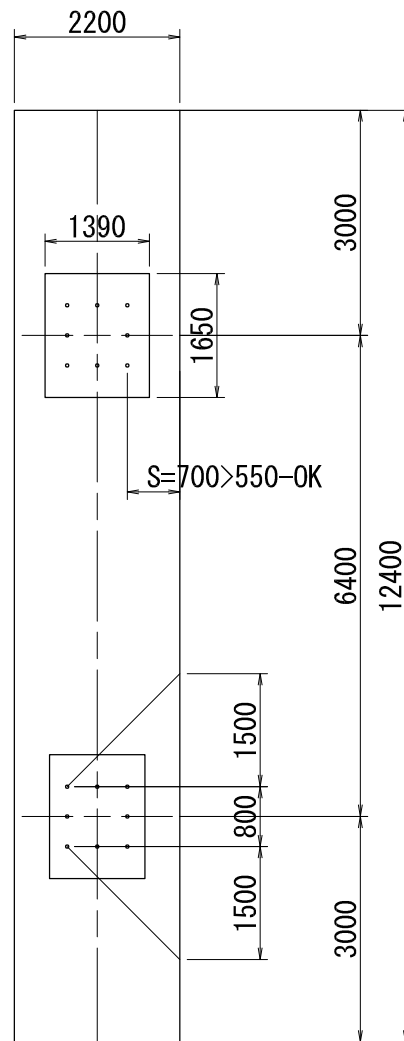


PF2, 5

$$\begin{aligned}
 S &= 0.2 + 0.005l \\
 &= 0.2 + 0.005 \times 70.0 \\
 &= 0.550\text{m}
 \end{aligned}$$

$$\begin{aligned}
 Se &= 0.7 + 0.005l \\
 &= 0.7 + 0.005 \times 70.0 \\
 &= 1.050\text{m}
 \end{aligned}$$

E



PF3, 4

Steel Plate girder

$$S=0.2+0.005l$$

$$=0.2+0.005 \times 34.3$$

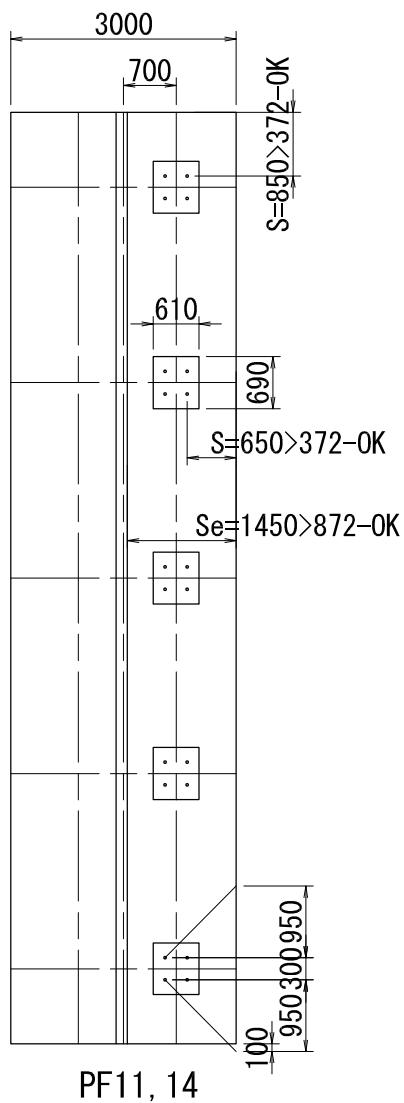
$$=0.372\text{m}$$

$$S_e=0.7+0.005l$$

$$=0.7+0.005 \times 34.3$$

$$=0.872\text{m}$$

E



$$S=0.2+0.005l$$

$$=0.2+0.005 \times 52.0$$

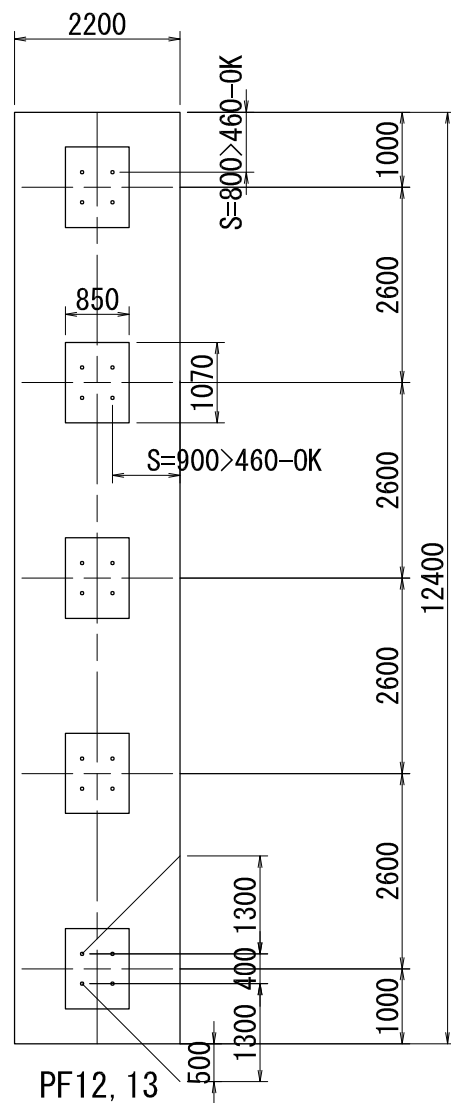
$$=0.460\text{m}$$

$$S_e=0.7+0.005l$$

$$=0.7+0.005 \times 52.0$$

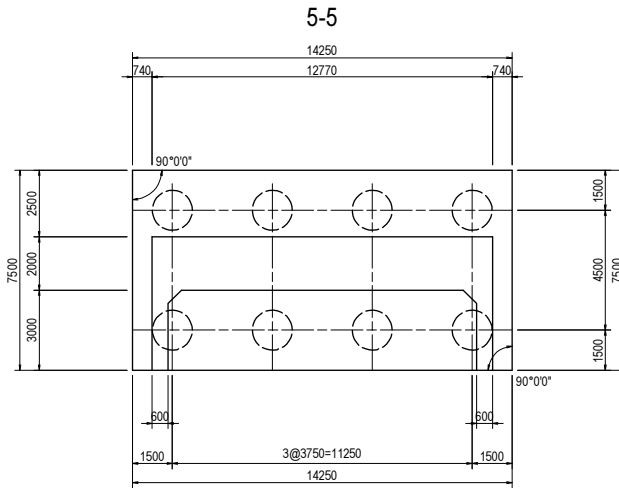
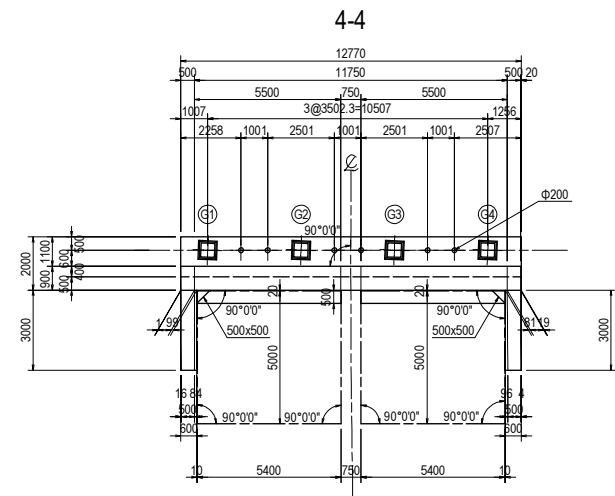
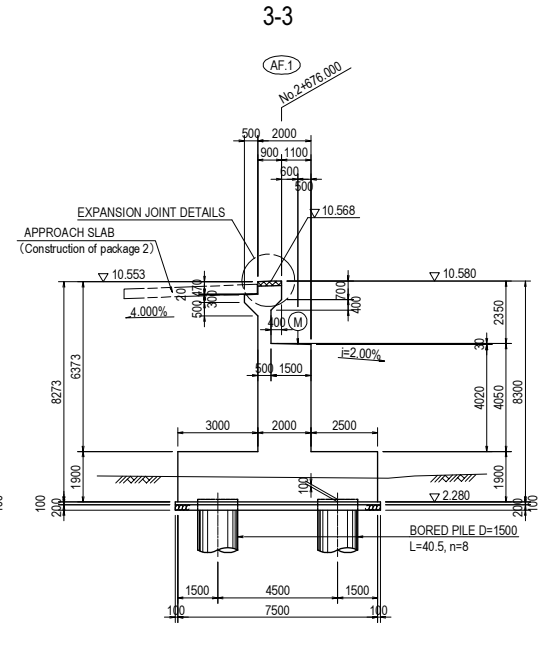
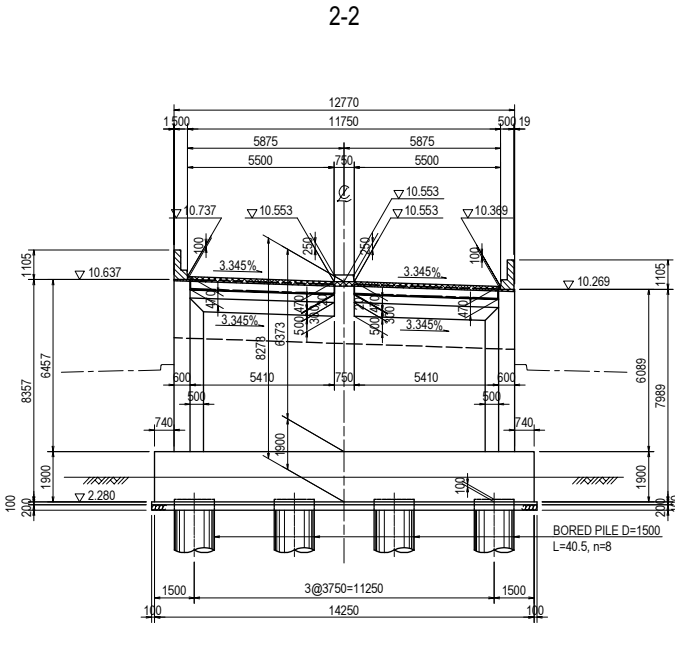
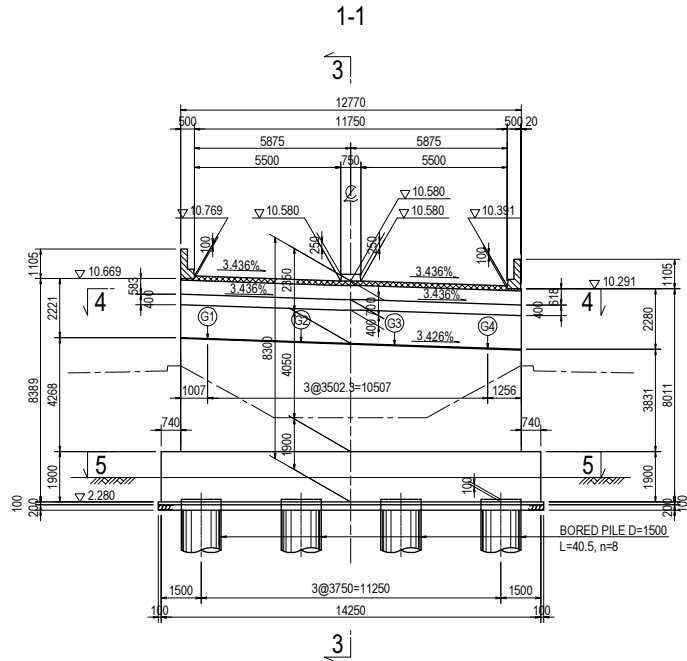
$$=0.960\text{m}$$

E

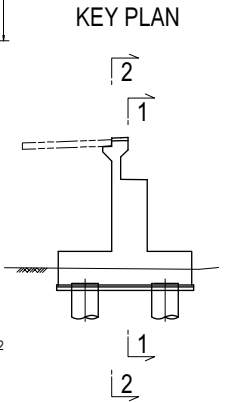
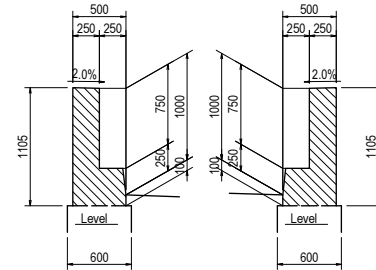


GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (1)

CROSS SECTION S=1:200



CONCRETE RAILING DETAILS S=1:50



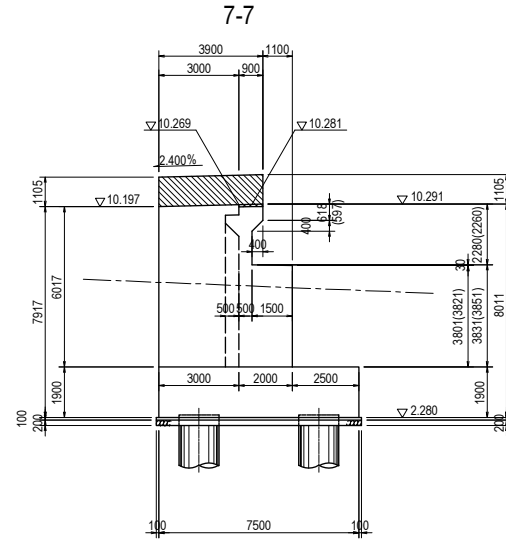
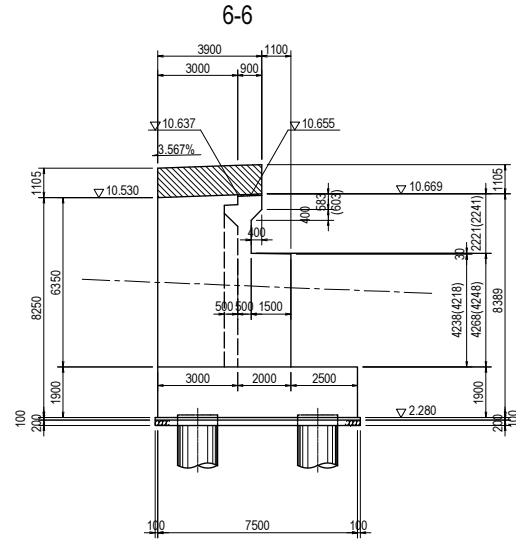
NOTE:

1. The construction of approach slab is included in Package 2
2. The work of backfill is included in Package 2

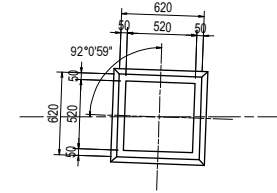
PROJECT NAME DETAILED DESIGN ON BAGO RIVER BRIDGE CONSTRUCTION PROJECT	FINANCED BY JICA JAPAN INTERNATIONAL COOPERATION AGENCY	COUNTERPART REPUBLIC OF THE UNION OF MYANMAR MINISTRY OF CONSTRUCTION DEPARTMENT OF BRIDGE	ACA STUDY TEAM NIPPON KOEI CO., LTD. ORIENTAL CONSULTANTS GLOBAL CO., LTD. METROPOLITAN EXPRESSWAY COMPANY LIMITED CHODAI CO. LTD. NIPPON ENGINEERING CONSULTANTS CO., LTD.	NAME PREPARED BY Y. SUZUKI CHECKED BY T. HAYAKAWA APPROVED BY Y. SANO	SIGNATURE DATE 15 Jun. 2017	DRAWING TITLE GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (1)	PACKAGE 3 DWG No. P3-FO-2002
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GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (2)

CROSS SECTION S=1:200

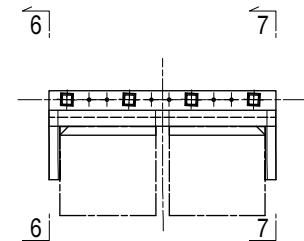


BEARING DETAILS S=1:40



	G1	G2	G3	G4	
BEARING MORTAR(mm)	49	49	49	49	
LOWER UPPER END HEIGHT	▽ 8.394	▽ 8.274	▽ 8.155	▽ 8.034	

KEY PLAN

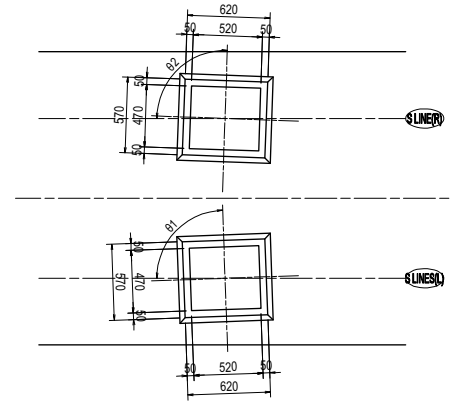
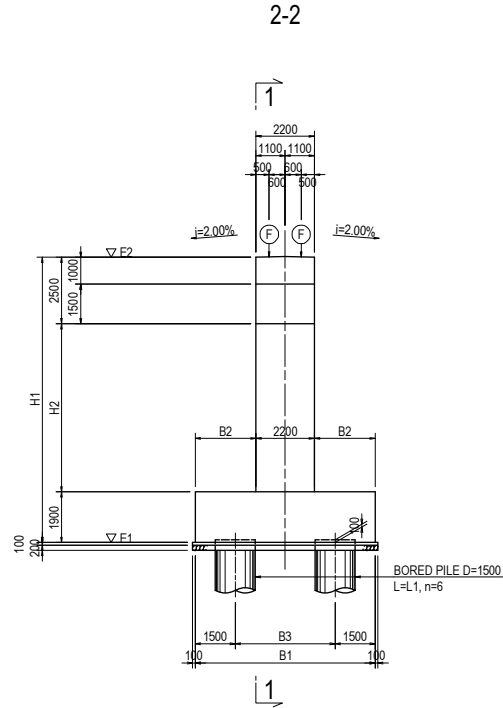
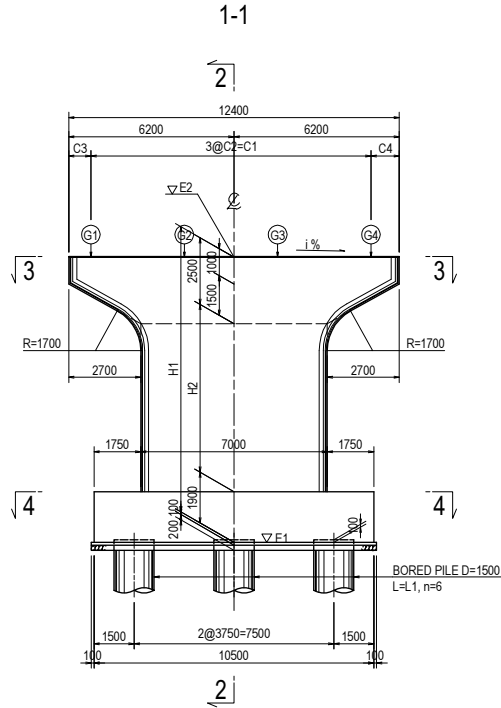


PROJECT NAME DETAILED DESIGN ON BAGO RIVER BRIDGE CONSTRUCTION PROJECT	FINANCED BY JAPAN INTERNATIONAL COOPERATION AGENCY	COUNTERPART REPUBLIC OF THE UNION OF MYANMAR MINISTRY OF CONSTRUCTION DEPARTMENT OF BRIDGE	JICA STUDY TEAM NIPPON KOEI CO., LTD. ORIENTAL CONSULTANTS GLOBAL CO., LTD. METROPOLITAN EXPRESSWAY COMPANY LIMITED CHODAI CO. LTD. NIPPON ENGINEERING CONSULTANTS CO. LTD.	NAME	SIGNATURE	DATE	DRAWING TITLE GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (2)	PACKAGE 3	
				PREPARED BY	Y. SUZUKI				15 Jun. 2017
				CHECKED BY	T. HAYAKAWA				
				APPROVED BY	Y. SANO				
								DWG No. P3-FO-2003	

GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (3)

CROSS SECTION S=1:200

BEARING DETAILS S=1:40



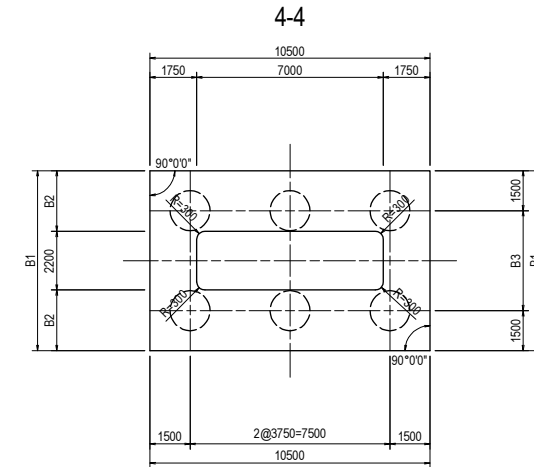
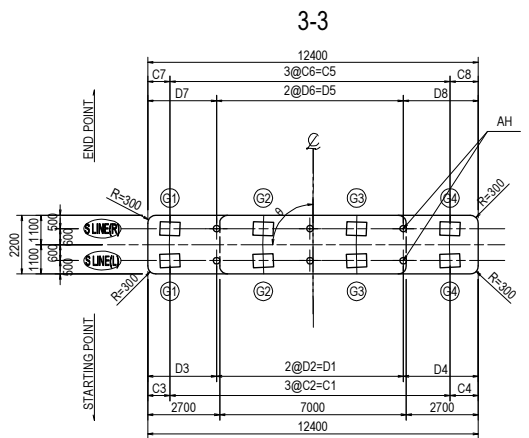
No.	AXIS	STATION No.	i(%)	E1(m)	E2(m)	θ(°)	H1(mm)	H2(mm)	B1(mm)	B2(mm)	B3(mm)	L1(m)
1	PF.1	2+706.000	3.636	2.187	9.087	90°00'00"	6900	2500	8500	3150	5500	41.5
2	PF.6	2+946.000	4.795	1.437	13.337	90°00'00"	11900	7500	6750	2275	3750	33.5
3	PF.8	3+ 6.000	LEVEL	1.184	12.984	90°07'09"	11800	7400	7500	2650	4500	37.0
4	PF.9	3+ 36.000	LEVEL	1.370	12.770	90°00'00"	11400	7000	6750	2275	3750	35.5
5	PF.10	3+ 66.000	LEVEL	1.555	12.555	90°00'00"	11000	6600	7500	2650	4500	32.5
6	PF.15	3+248.000	LEVEL	1.530	9.330	90°00'00"	7800	3400	7500	2650	4500	34.0

No.	AXIS	C1(mm)	C2(mm)	C3(mm)	C4(mm)	C5(mm)	C6(mm)	C7(mm)	C8(mm)	θ1(°)	θ2(°)	AH
1	PF.1	10507	3502.3	832	1061	10507	3502.3	832	1061	87°57'20"	92°01'20"	Φ250
2	PF.6	10512	3504	1096	792	10512	3504	1096	792	92°41'09"	87°22'15"	Φ250
3	PF.8	10500	3500	945	956	10500	3500	956	944	91°03'14"	90°00'00"	Φ250
4	PF.9	10500	3500	950	950	10500	3500	950	950	90°00'00"	90°00'00"	Φ250
5	PF.10	10500	3500	950	950	10500	3500	950	950	90°00'00"	90°00'00"	Φ250
6	PF.15	10500	3500	950	950	10500	3500	950	950	90°00'00"	90°00'00"	Φ250

No.	AXIS	D1(mm)	D2(mm)	D3(mm)	D4(mm)	D5(mm)	D6(mm)	D7(mm)	D8(mm)
1	PF.1	7004.6	3502.3	2583	2812	7004.6	3502.3	2583	2812
2	PF.6	7008	3504	2848	2544	7008	3504	2848	2544
3	PF.8	7000	3500	2695	2705	7000	3500	2706	2694
4	PF.9	7000	3500	2700	2700	7000	3500	2700	2700
5	PF.10	7000	3500	2700	2700	7000	3500	2700	2700
6	PF.15	7000	3500	2700	2700	7000	3500	2700	2700

No.	AXIS	S LINE (L)				S LINE (R)			
		G1	G2	G3	G4	G1	G2	G3	G4
1	PF.1	50	50	50	50	55	55	55	55
2	PF.6	55	56	58	58	56	58	59	60
3	PF.8	47	47	47	47	40	40	40	41
4	PF.9	48	48	48	48	40	40	40	40
5	PF.10	49	49	49	49	40	40	40	40
6	PF.15	46	46	46	46	40	40	40	40

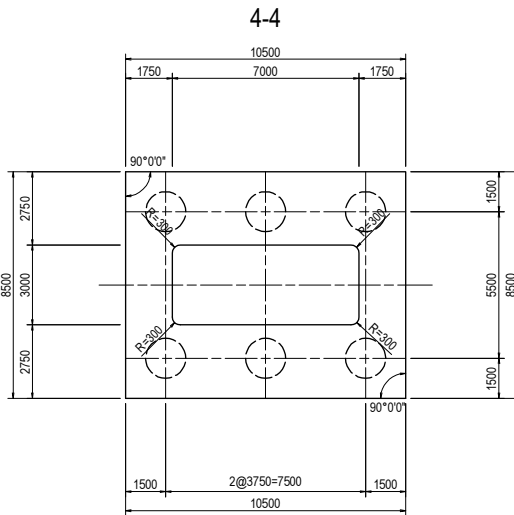
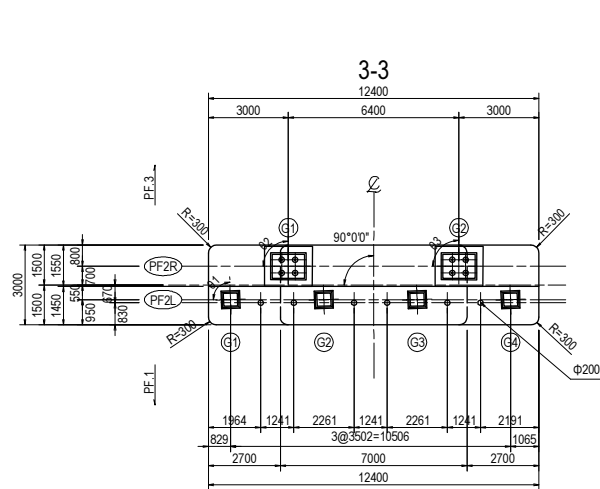
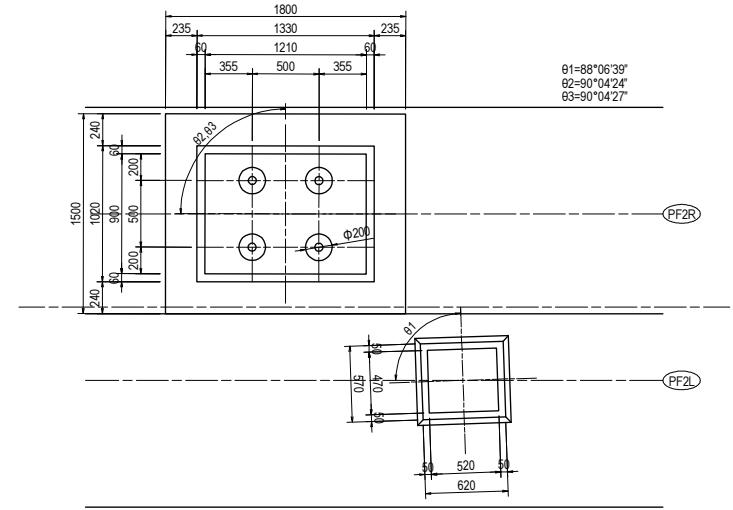
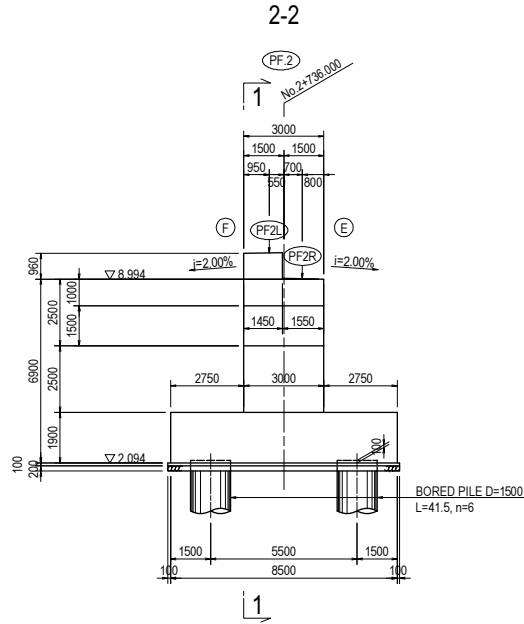
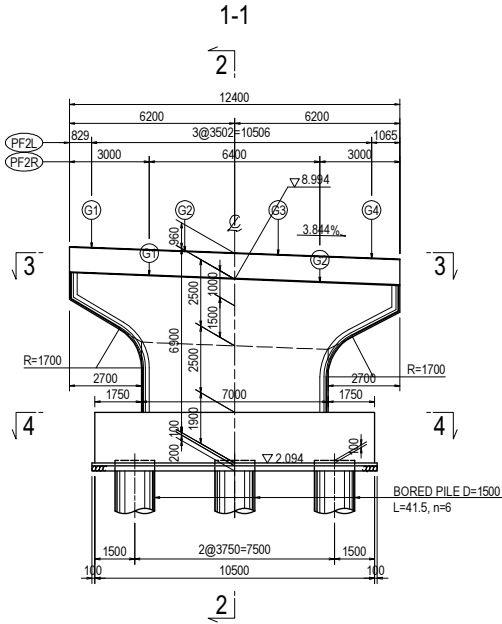
No.	AXIS	S LINE (L)				S LINE (R)			
		G1	G2	G3	G4	G1	G2	G3	G4
1	PF.1	▽ 9.292	▽ 9.165	▽ 9.037	▽ 8.910	▽ 9.292	▽ 9.165	▽ 9.037	▽ 8.910
2	PF.6	▽ 13.102	▽ 13.270	▽ 13.438	▽ 13.606	▽ 13.102	▽ 13.270	▽ 13.438	▽ 13.606
3	PF.8	▽ 12.994	▽ 12.994	▽ 12.994	▽ 12.994	▽ 12.994	▽ 12.994	▽ 12.994	▽ 12.994
4	PF.9	▽ 12.780	▽ 12.780	▽ 12.780	▽ 12.780	▽ 12.780	▽ 12.780	▽ 12.780	▽ 12.780
5	PF.10	▽ 12.565	▽ 12.565	▽ 12.565	▽ 12.565	▽ 12.565	▽ 12.565	▽ 12.565	▽ 12.565
6	PF.15	▽ 9.340	▽ 9.340	▽ 9.340	▽ 9.340	▽ 9.340	▽ 9.340	▽ 9.340	▽ 9.340



GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (4)

CROSS SECTION S=1:200

BEARING DETAILS S=1:40

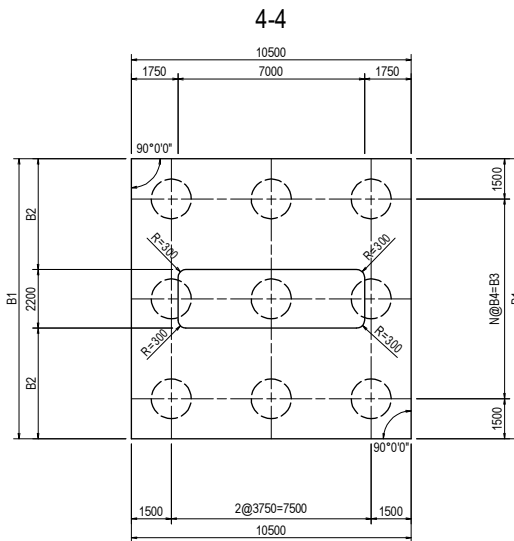
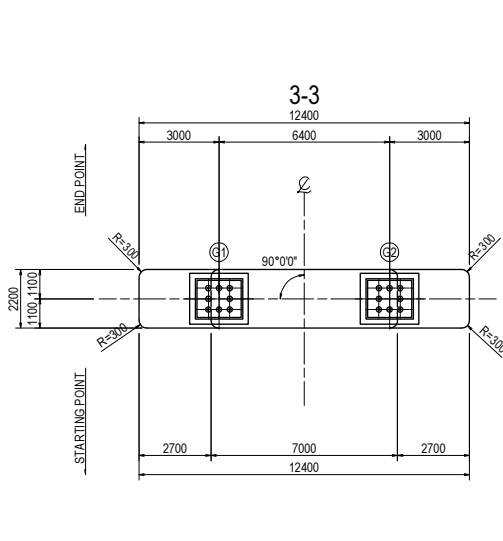
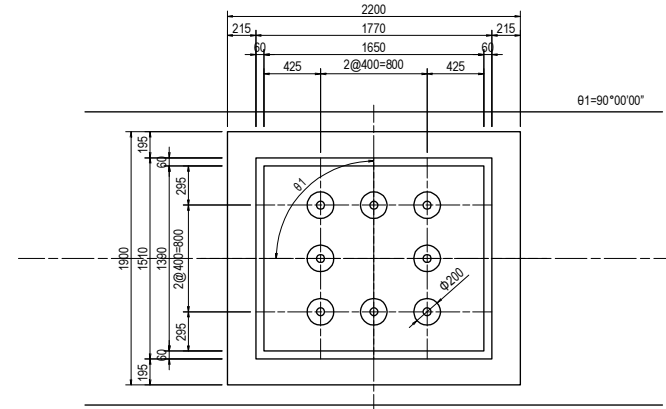
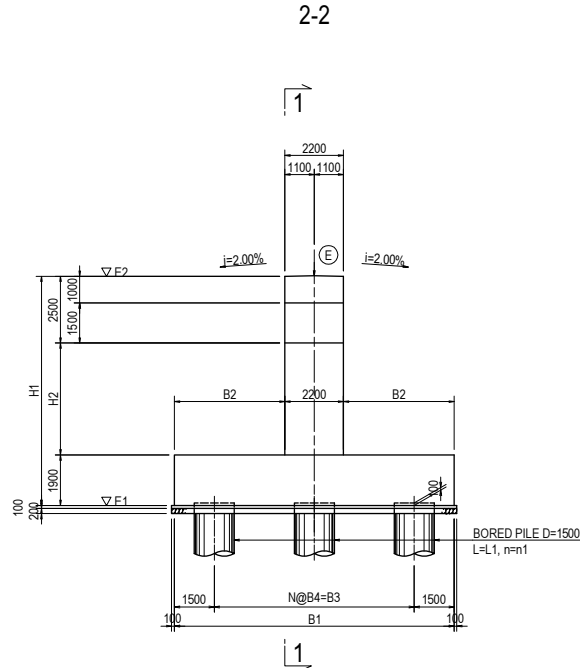
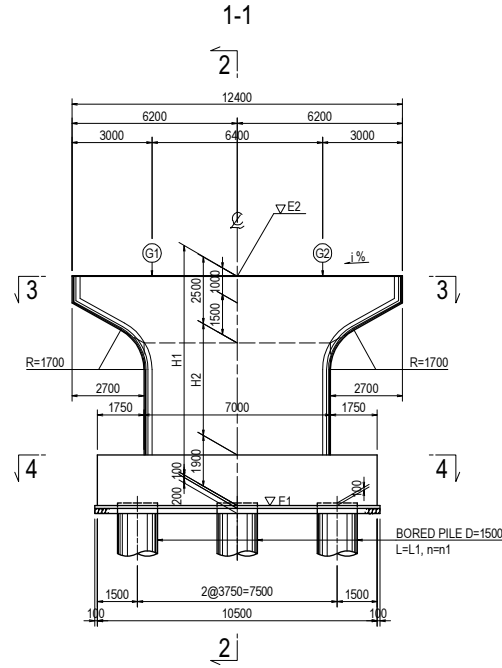


	PF2L				PF2R		
	G1	G2	G3	G4	G1	G2	
BEARING MORTAR(mm)	54	54	54	54	32	30	
BASE HEIGHT(mm)	-	-	-	-	150	210	
LOWER UPPER END HEIGHT	▽ 10.179	▽ 10.045	▽ 9.910	▽ 9.776	▽ 9.133	▽ 8.887	

GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (5)

CROSS SECTION S=1:200

BEARING DETAILS S=1:40



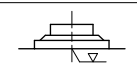
No.	AXIS	STATION No.	i(%)	E1(m)	E2(m)	H1(mm)	H2(mm)
1	PF.3	2+791.000	0.844	2.092	10.392	8300	3900
2	PF.4	2+861.000	5.234	1.879	11.679	9800	5400

No.	AXIS	B1(mm)	B2(mm)	B3(mm)	B4(mm)	N	L1(m)	n1
1	PF.3	10500	4150	7500	3750	2	38.0	9
2	PF.4	6750	2275	3750	-	-	40.5	6

BEARING MORTAR(mm)			
No.	AXIS	G1	G2
1	PF.3	31	32
2	PF.4	31	31

BASE HEIGHT(mm)			
No.	AXIS	G1	G2
1	PF.3	150	150
2	PF.4	150	150

LOWER UPPER END HEIGHT			
No.	AXIS	G1	G2
1	PF.3	▽ 10.387	▽ 10.441
2	PF.4	▽ 11.533	▽ 11.868



PROJECT NAME
DETAILED DESIGN ON
BAGO RIVER BRIDGE
CONSTRUCTION PROJECT

FINANCED BY
JICA
JAPAN INTERNATIONAL
COOPERATION AGENCY

COUNTRYPART
REPUBLIC OF THE UNION OF MYANMAR
MINISTRY OF CONSTRUCTION
DEPARTMENT OF BRIDGE

ASSISTED BY
NIPPON KOEI CO., LTD.
ORIENTAL CONSULTANTS GLOBAL CO., LTD.
METROPOLITAN EXPRESSWAY COMPANY LIMITED
CHODAI CO., LTD.
NIPPON ENGINEERING CONSULTANTS CO., LTD.

NAME	SIGNATURE	DATE
PREPARED BY Y. SUZUKI	<i>[Signature]</i>	15 Jun. 2017
CHECKED BY T. HAYAKAWA	<i>[Signature]</i>	
APPROVED BY Y. SANO	<i>[Signature]</i>	

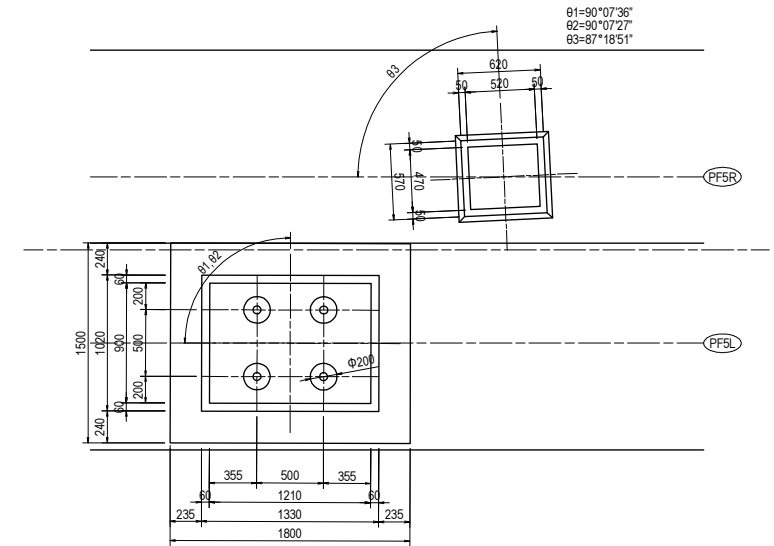
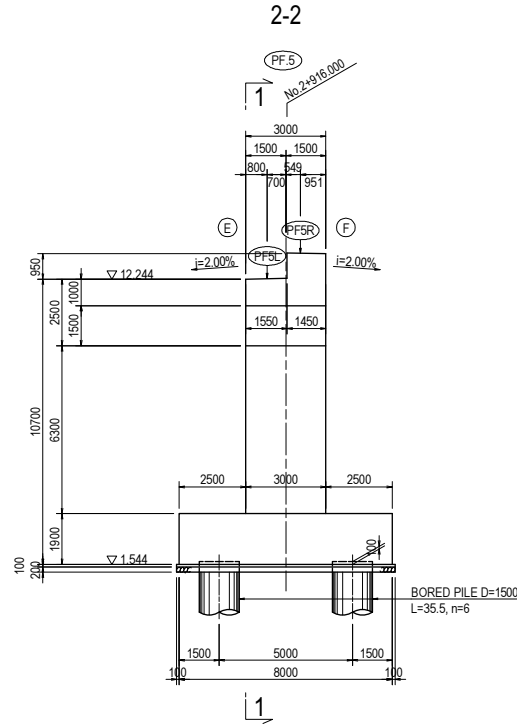
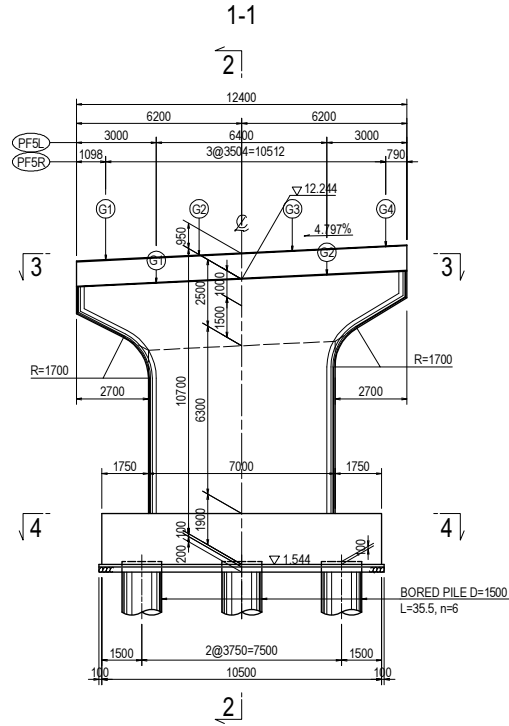
DRAWING TITLE
GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (5)

PACKAGE
3
DWG No.
P3-FO-2006

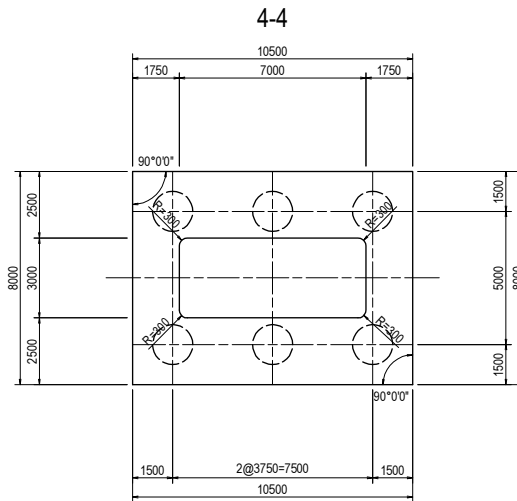
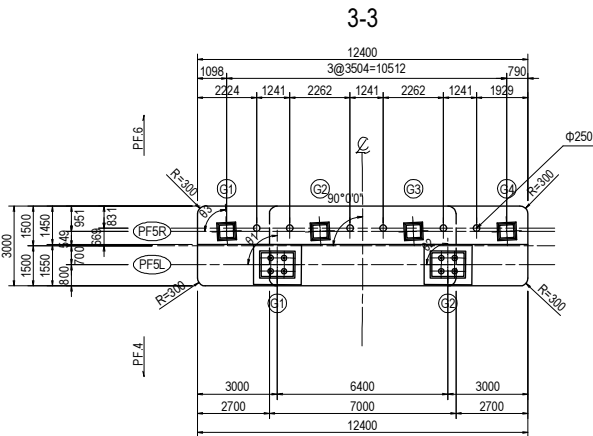
GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (6)

CROSS SECTION S=1:200

BEARING DETAILS S=1:40



	PF5L		PF5R			
	G1	G2	G1	G2	G3	G4
BEARING MORTAR(mm)	31	33	60	60	60	60
BASE HEIGHT(mm)	150	180	-	-	-	-
LOWER UPPER END HEIGHT	▽ 12.106	▽ 12.413	▽ 12.968	▽ 13.136	▽ 13.304	▽ 13.472

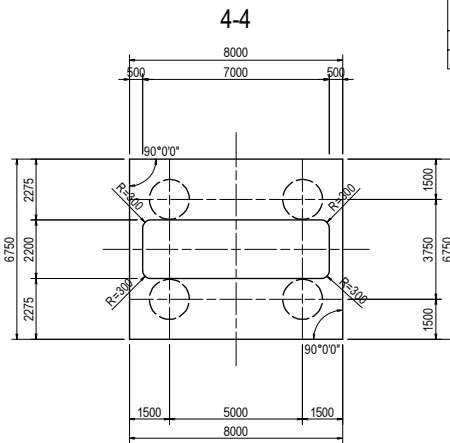
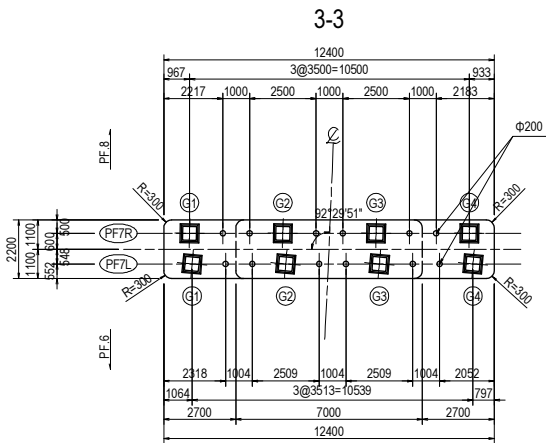
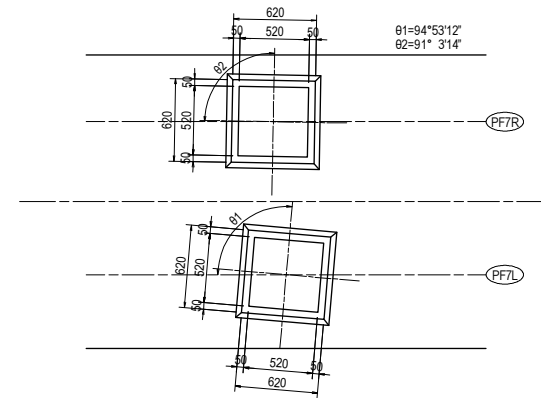
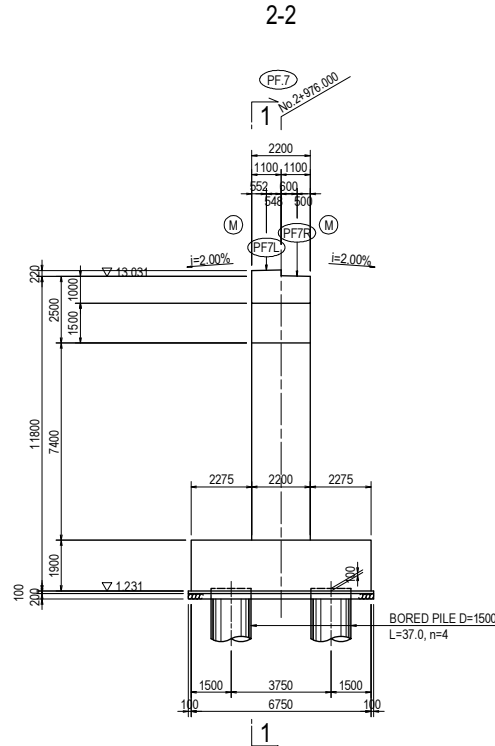
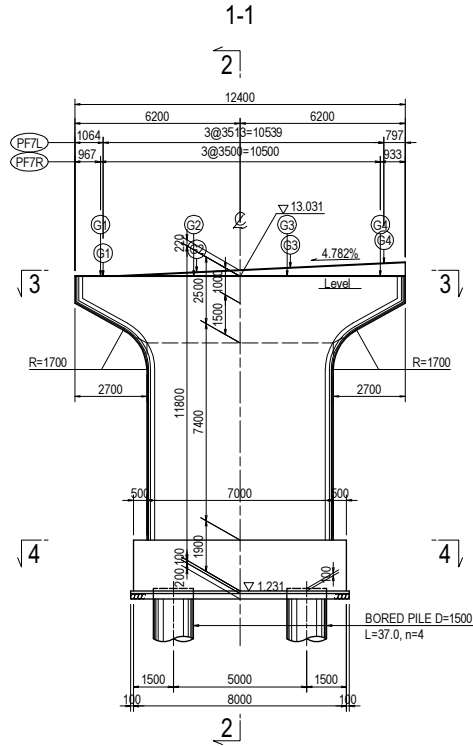


PROJECT NAME DETAILED DESIGN ON BAGO RIVER BRIDGE CONSTRUCTION PROJECT	FINANCED BY JICA JAPAN INTERNATIONAL COOPERATION AGENCY	COUNTRY/PORT REPUBLIC OF THE UNION OF MYANMAR MINISTRY OF CONSTRUCTION DEPARTMENT OF BRIDGE	JOINT STUDY TEAM NIPPON KOEI CO., LTD. ORIENTAL CONSULTANTS GLOBAL CO., LTD. METROPOLITAN EXPRESSWAY COMPANY LIMITED CHODAI CO., LTD. NIPPON ENGINEERING CONSULTANTS CO., LTD.	NAME PREPARED BY Y. SUZUKI CHECKED BY T. HAYAKAWA APPROVED BY Y. SANO	SIGNATURE DATE 15 Jun. 2017	DRAWING TITLE GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (6)	PACKAGE 3 DWG No. P3-FO-
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GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (7)

CROSS SECTION S=1:200

BEARING DETAILS S=1:40



	PF7L				PF7R			
	G1	G2	G3	G4	G1	G2	G3	G4
BEARING MORTAR(mm)	34	60	60	60	41	41	40	41
LOWER UPPER END HEIGHT	▽ 13.042	▽ 13.184	▽ 13.352	▽ 13.520	▽ 13.041	▽ 13.041	▽ 13.041	▽ 13.041

PROJECT NAME
DETAILED DESIGN ON
BAGO RIVER BRIDGE
CONSTRUCTION PROJECT

FINANCED BY
JICA
JAPAN INTERNATIONAL
COOPERATION AGENCY

COUNTRY/PROJECT
REPUBLIC OF THE UNION OF MYANMAR
MINISTRY OF CONSTRUCTION
DEPARTMENT OF BRIDGE

CONSULTANT
NIPPON KOEI CO., LTD.
ORIENTAL CONSULTANTS GLOBAL CO., LTD.
METROPOLITAN EXPRESSWAY COMPANY LIMITED
CHODAI CO., LTD.
NIPPON ENGINEERING CONSULTANTS CO., LTD.

	NAME	SIGNATURE	DATE
PREPARED BY	Y. SUZUKI	<i>Y. Suzuki</i>	15 Jun. 2017
CHECKED BY	T. HAYAKAWA	<i>T. Hayakawa</i>	
APPROVED BY	Y. SANO	<i>Y. Sano</i>	

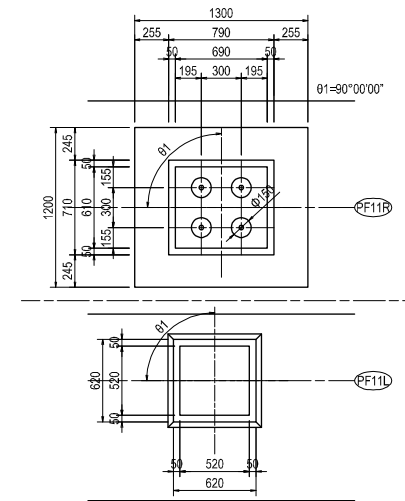
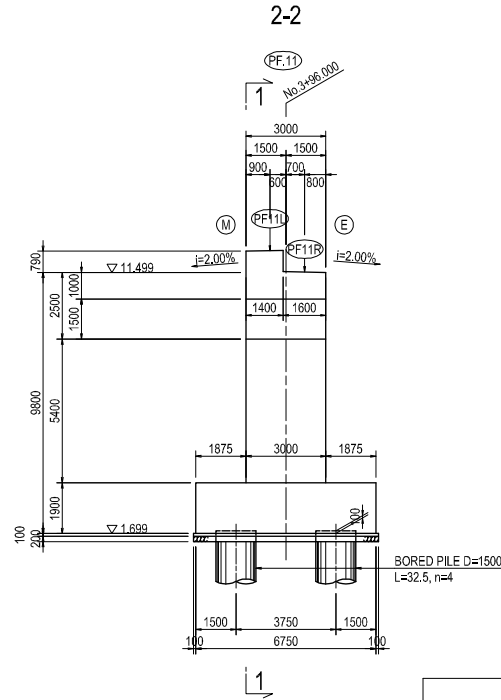
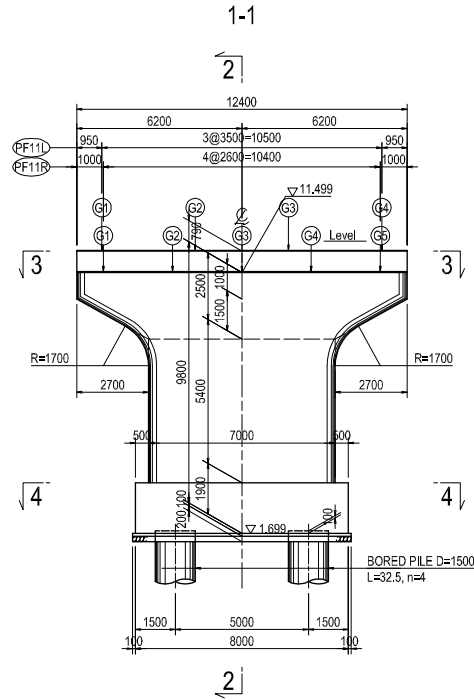
DRAWING TITLE
GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (7)

PACKAGE
3
DWG No.
P3-FO-

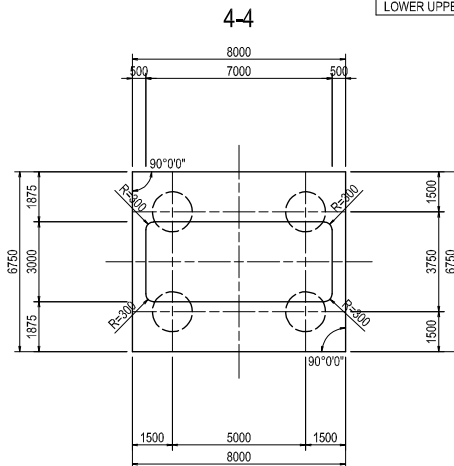
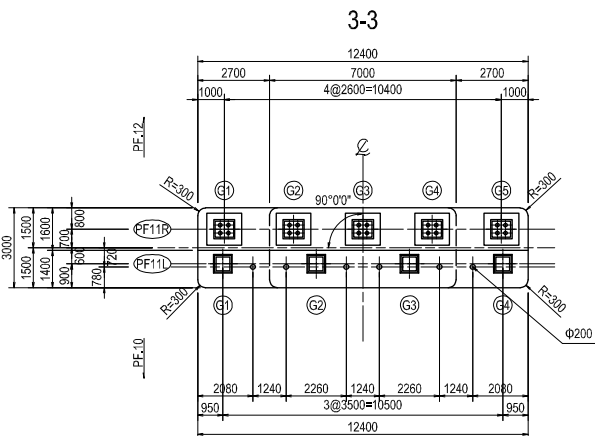
GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (8)

CROSS SECTION S=1:200

BEARING DETAILS S=1:40



	PF11L				PF11R					
	G1	G2	G3	G4	G1	G2	G3	G4	G5	
BEARING MORTAR(mm)	42	42	42	42	30	32	37	32	30	
BASE HEIGHT(mm)	-	-	-	-	150	200	240	200	150	
LOWER UPPER END HEIGHT	▽ 12,307	▽ 12,307	▽ 12,307	▽ 12,307	▽ 11,515	▽ 11,515	▽ 11,515	▽ 11,515	▽ 11,515	

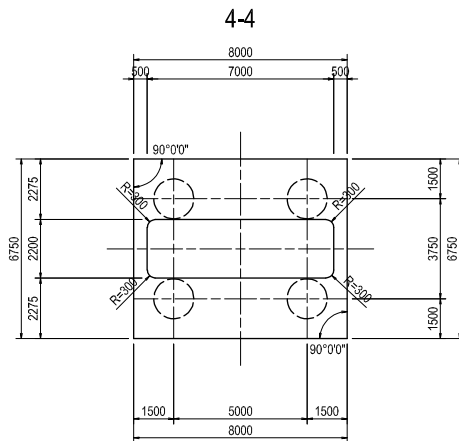
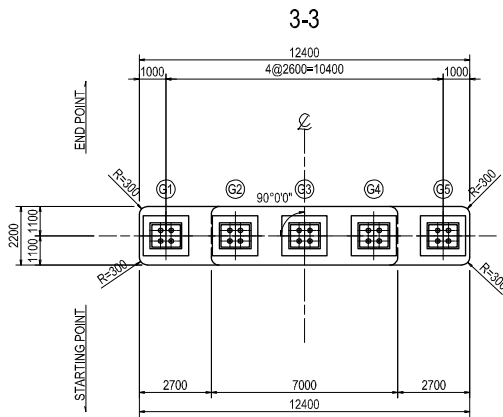
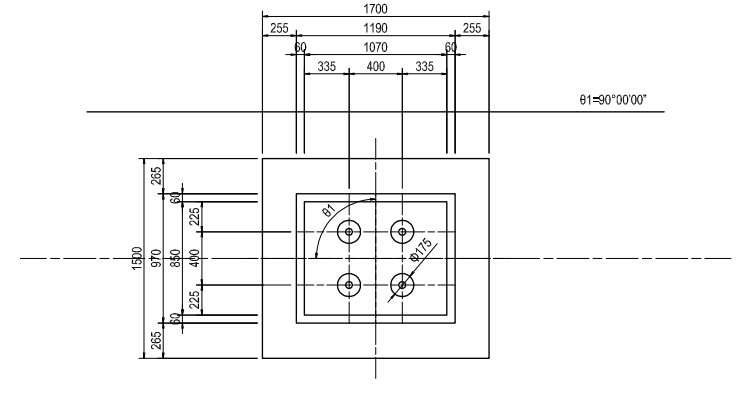
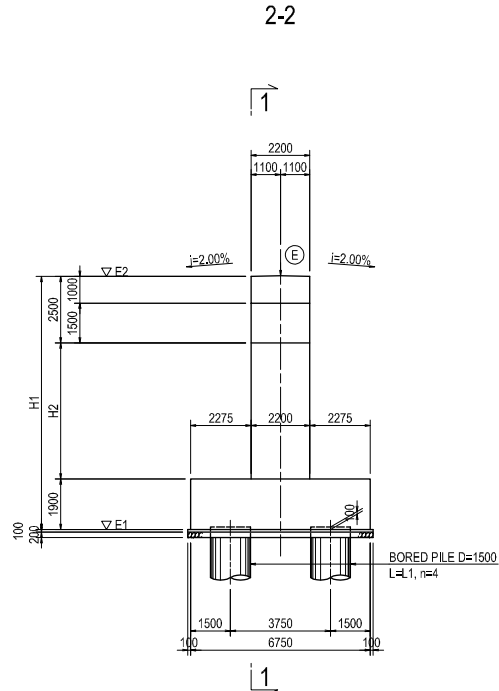
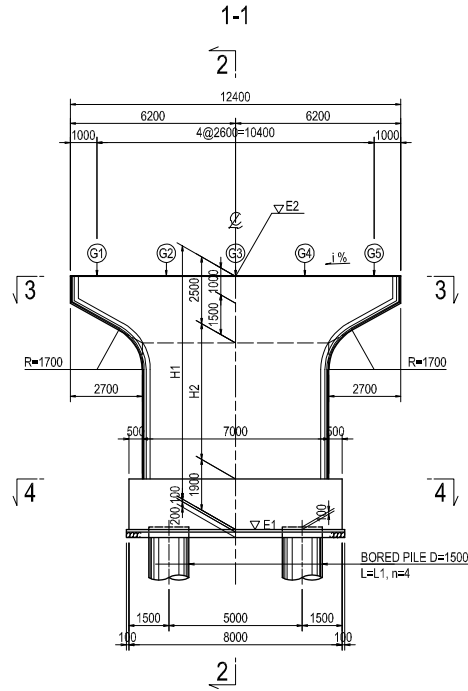


PROJECT NAME DETAILED DESIGN ON BAGO RIVER BRIDGE CONSTRUCTION PROJECT	FINANCED BY JICA JAPAN INTERNATIONAL COOPERATION AGENCY	COUNTRY PART REPUBLIC OF THE UNION OF MYANMAR MINISTRY OF CONSTRUCTION DEPARTMENT OF BRIDGE	CLIENT NIPPON KOEI CO., LTD. ORIENTAL CONSULTANTS GLOBAL CO., LTD. METROPOLITAN EXPRESSWAY COMPANY LIMITED CHODAI CO., LTD. NIPPON ENGINEERING CONSULTANTS CO., LTD.	NAME Y. SUZUKI	SIGNATURE <i>Y. Suzuki</i>	DATE 15 Jun. 2017	DRAWING TITLE GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (8)	PACKAGE 3 DWG No. P3-FO-
				CHECKED BY T. HAYAKAWA	<i>T. Hayakawa</i>			
				APPROVED BY Y. SANO	<i>Y. Sano</i>			

GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (9)

CROSS SECTION S=1:200

BEARING DETAILS S=1:40



No.	AXIS	STATION No.	I(%)	E1(m)	E2(m)	H1(mm)	H2(mm)	L1(m)
1	PF.12	3+131,000	LEVEL	1,907	11,107	9200	4800	33.0
2	PF.13	3+183,000	LEVEL	1,873	10,173	8300	3900	32.5

BEARING MORTAR(mm)

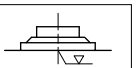
No.	AXIS	G1	G2	G3	G4	G5
1	PF.12	30	32	39	32	30
2	PF.13	30	32	39	32	30

BASE HEIGHT(mm)

No.	AXIS	G1	G2	G3	G4	G5
1	PF.12	150	210	250	210	150
2	PF.13	150	210	250	210	150

LOWER UPPER END HEIGHT

No.	AXIS	G1	G2	G3	G4	G5
1	PF.12	▽ 11,129	▽ 11,129	▽ 11,129	▽ 11,129	▽ 11,129
2	PF.13	▽ 10,195	▽ 10,195	▽ 10,195	▽ 10,195	▽ 10,195

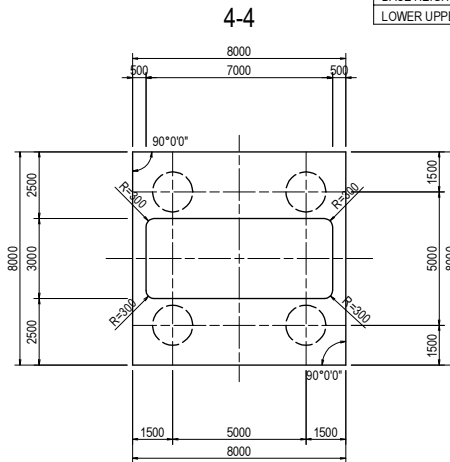
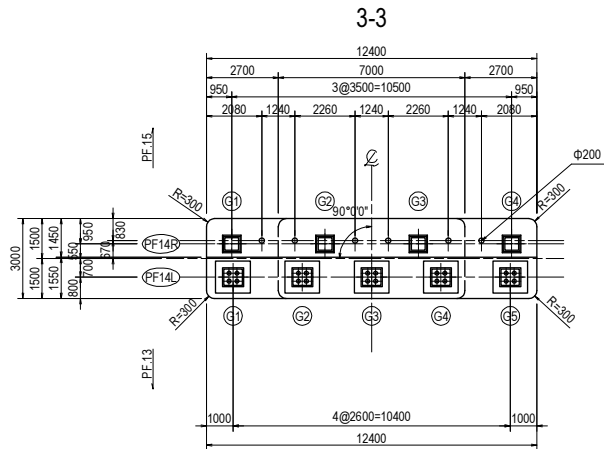
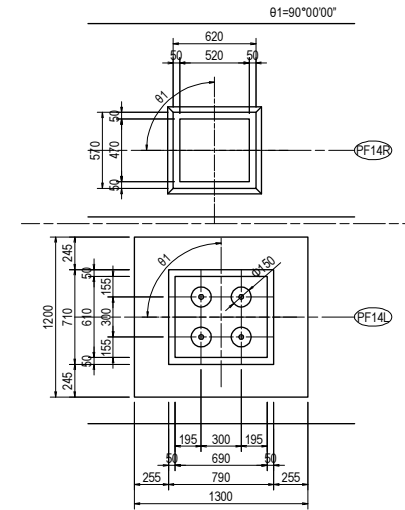
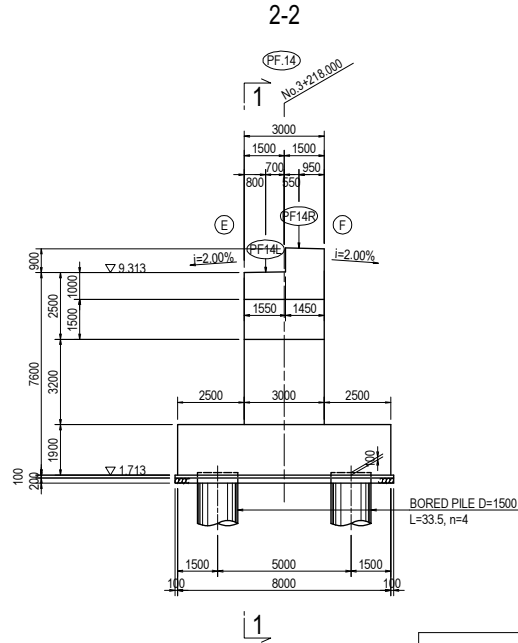
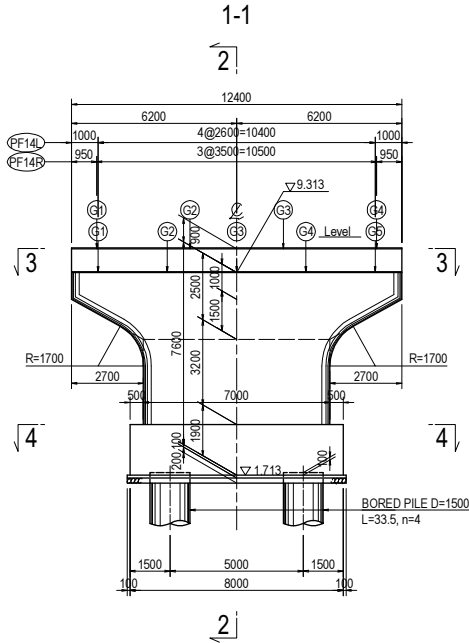


PROJECT NAME DETAILED DESIGN ON BAGO RIVER BRIDGE CONSTRUCTION PROJECT	FINANCED BY JAPAN INTERNATIONAL COOPERATION AGENCY	COUNTRY PART REPUBLIC OF THE UNION OF MYANMAR MINISTRY OF CONSTRUCTION DEPARTMENT OF BRIDGE	JOINT VENTURE NIPPON KOEI CO., LTD. ORIENTAL CONSULTANTS GLOBAL CO., LTD. METROPOLITAN EXPRESSWAY COMPANY LIMITED CHODAI CO., LTD. NIPPON ENGINEERING CONSULTANTS CO., LTD.	NAME Y. SUZUKI	SIGNATURE 	DATE 15 Jun. 2017	DRAWING TITLE GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (9)	PACKAGE 3
				PREPARED BY Y. SUZUKI	CHECKED BY T. HAYAKAWA	APPROVED BY Y. SANO		DWG No.
								P3-FO-

GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (10)

CROSS SECTION S=1:200

BEARING DETAILS S=1:40

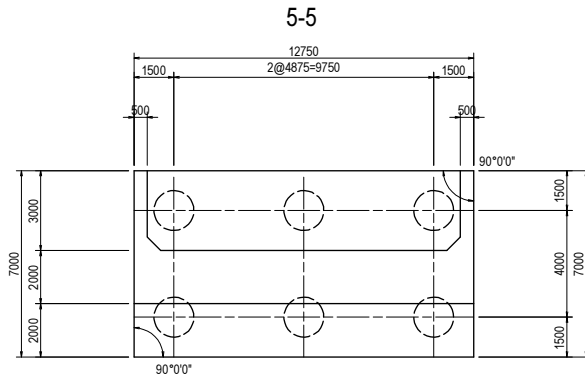
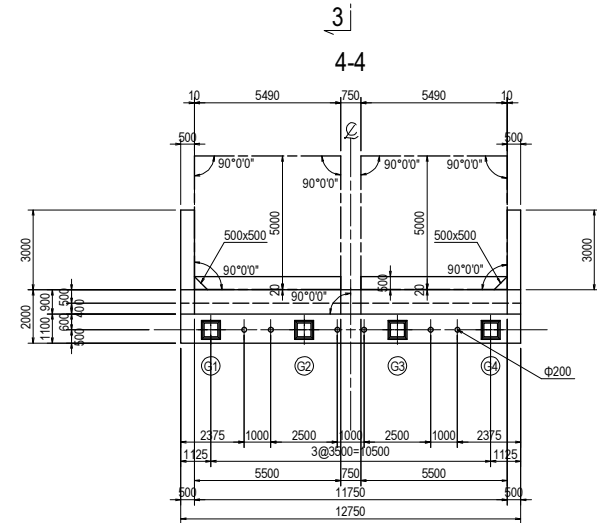
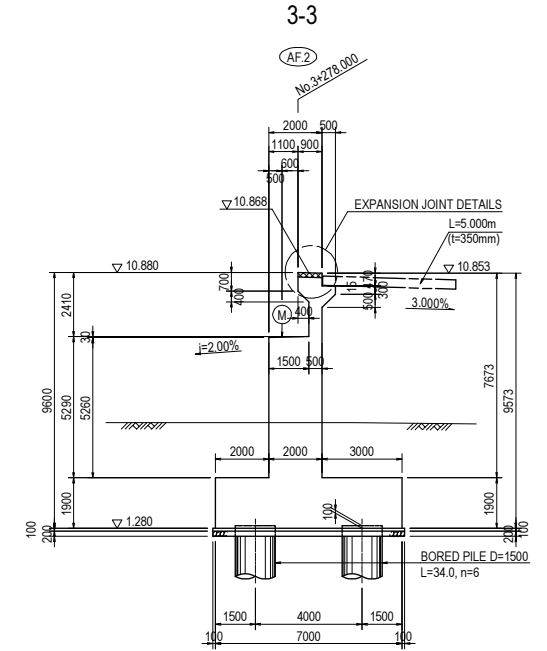
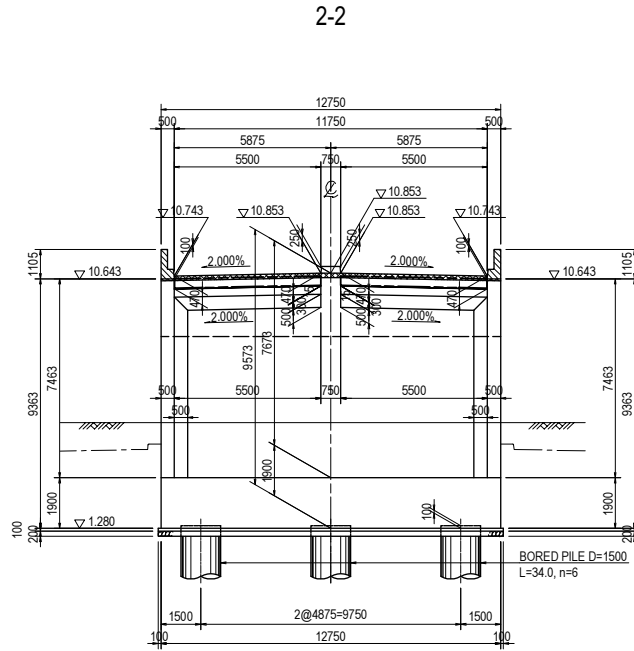
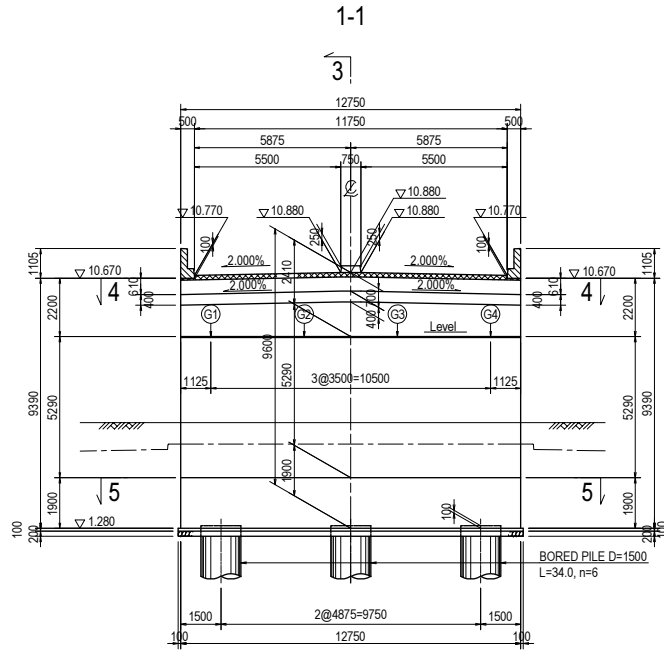


	PF14L					PF14R			
	G1	G2	G3	G4	G5	G1	G2	G3	G4
BEARING MORTAR(mm)	39	31	35	31	39	49	49	49	49
BASE HEIGHT(mm)	150	210	250	210	150	-	-	-	-
LOWER UPPER END HEIGHT	▽ 9.329	▽ 9.329	▽ 9.329	▽ 9.329	▽ 9.329	▽ 10.232	▽ 10.232	▽ 10.232	▽ 10.232

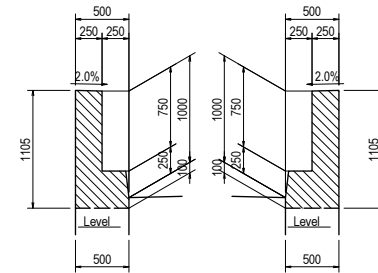
PROJECT NAME DETAILED DESIGN ON BAGO RIVER BRIDGE CONSTRUCTION PROJECT	FINANCED BY JAPAN INTERNATIONAL COOPERATION AGENCY	COUNTERPART REPUBLIC OF THE UNION OF MYANMAR MINISTRY OF CONSTRUCTION DEPARTMENT OF BRIDGE	JICA STUDY TEAM NIPPON KOEI CO., LTD. ORIENTAL CONSULTANTS GLOBAL CO., LTD. METROPOLITAN EXPRESSWAY COMPANY LIMITED CHODAI CO. LTD. NIPPON ENGINEERING CONSULTANTS CO., LTD.	NAME	SIGNATURE	DATE	DRAWING TITLE GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (10)	PACKAGE 3 DWG No. P3-FO-	
				PREPARED BY	Y. SUZUKI				15 Jun. 2017
				CHECKED BY	T. HAYAKAWA				
				APPROVED BY	Y. SANO				

GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (11)

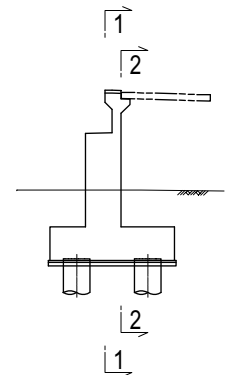
CROSS SECTION S=1:200



CONCRETE RAILING DETAILS S=1:50



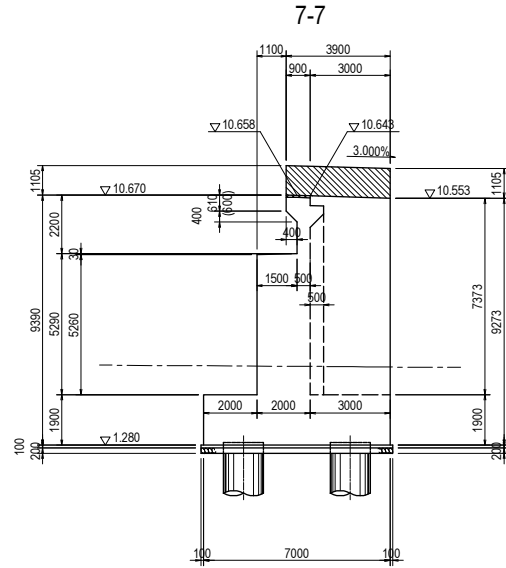
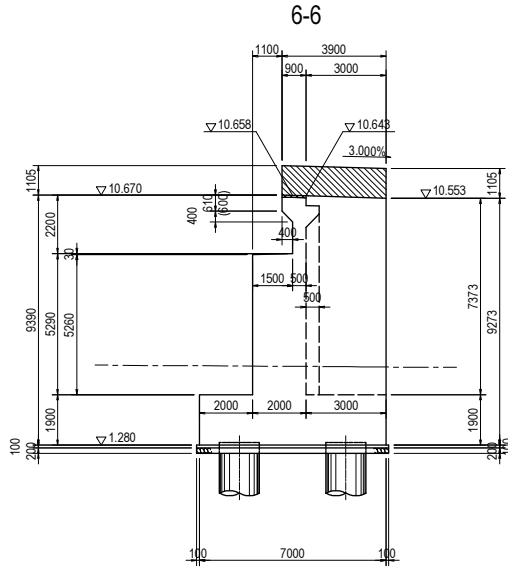
KEY PLAN



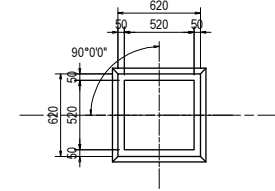
PROJECT NAME DETAILED DESIGN ON BAGO RIVER BRIDGE CONSTRUCTION PROJECT	FINANCED BY JICA JAPAN INTERNATIONAL COOPERATION AGENCY	COUNTERPART REPUBLIC OF THE UNION OF MYANMAR MINISTRY OF CONSTRUCTION DEPARTMENT OF BRIDGE	ICA STUDY TEAM NIPPON KOEI CO., LTD. ORIENTAL CONSULTANTS GLOBAL CO., LTD. METROPOLITAN EXPRESSWAY COMPANY LIMITED CHODAI CO. LTD. NIPPON ENGINEERING CONSULTANTS CO., LTD.	NAME PREPARED BY Y. SUZUKI CHECKED BY T. HAYAKAWA APPROVED BY Y. SANO	SIGNATURE DATE 15 Jun. 2017	DRAWING TITLE GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (11)	PACKAGE 3 DWG No. P3-FO-2012
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GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (12)

CROSS SECTION S=1:200

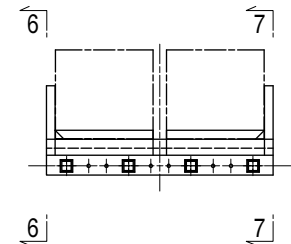


BEARING DETAILS S=1:40



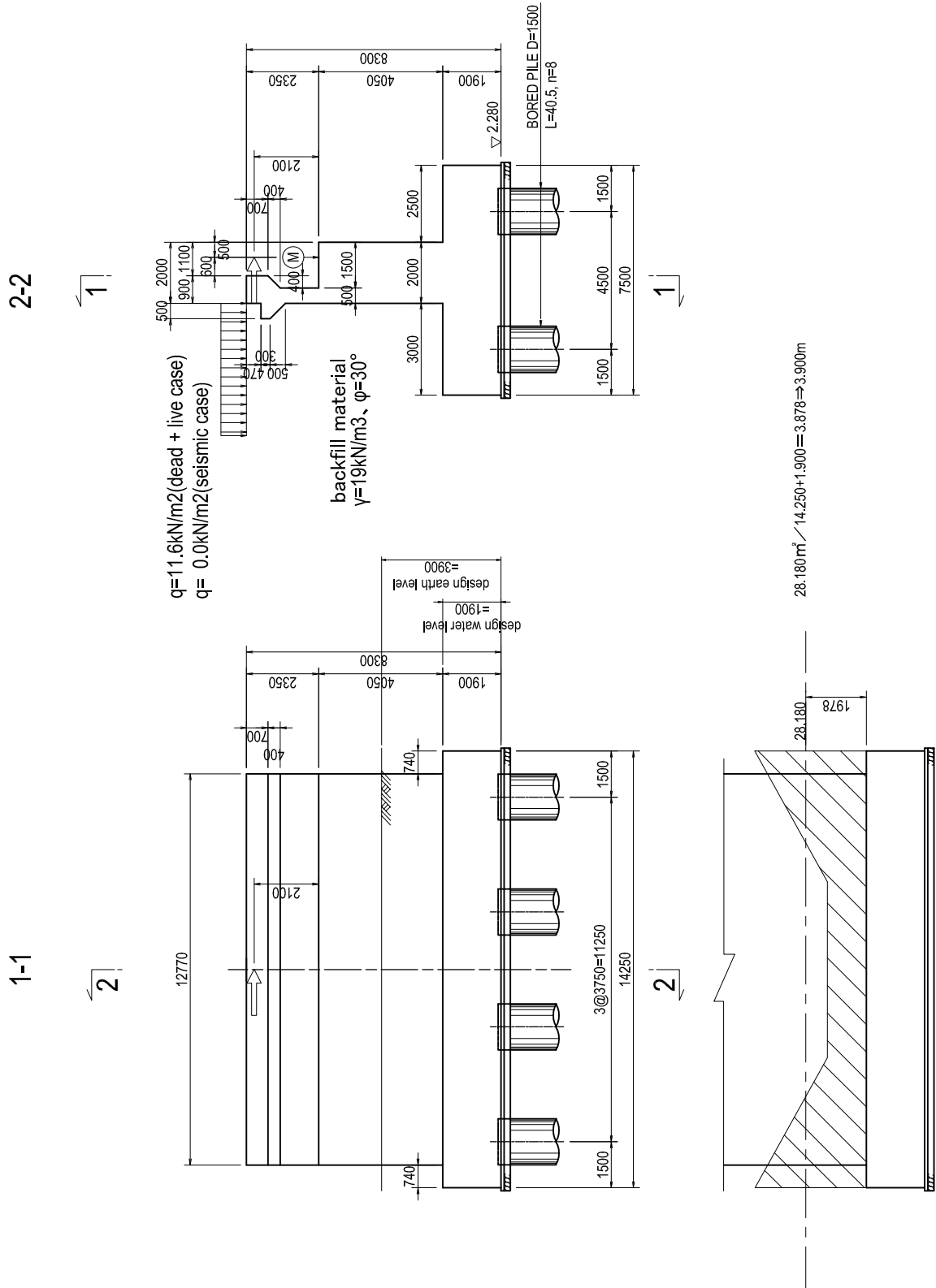
	G1	G2	G3	G4	
BEARING MORTAR(mm)	46	46	46	46	
LOWER UPPER END HEIGHT	▽ 8.450	▽ 8.450	▽ 8.450	▽ 8.450	

KEY PLAN

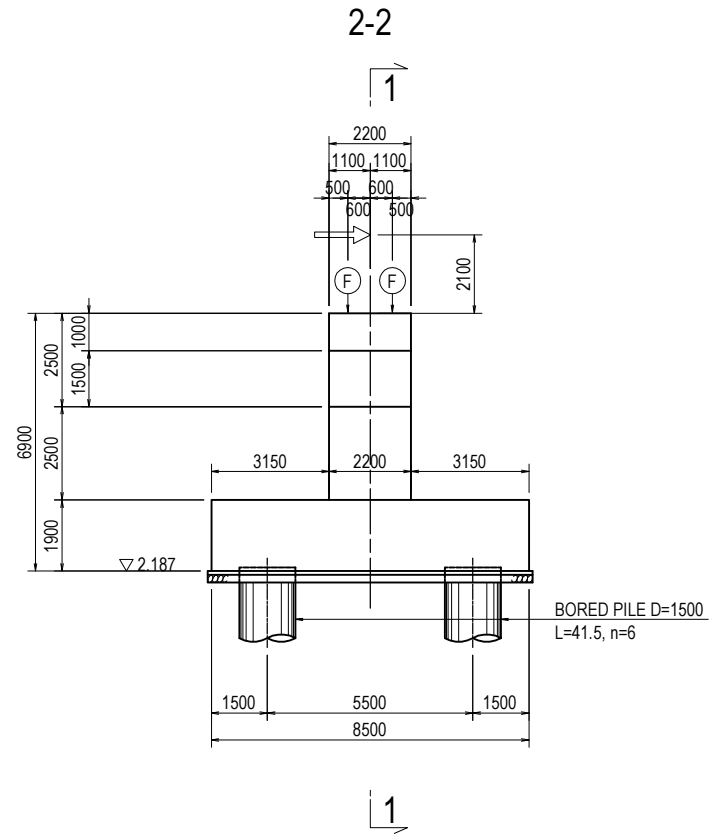
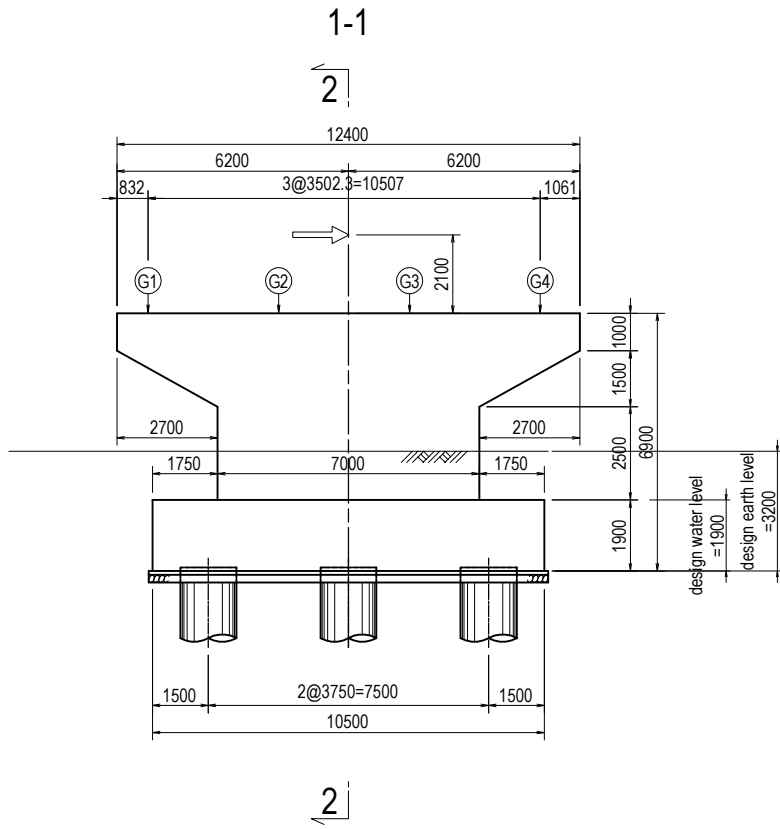


PROJECT NAME DETAILED DESIGN ON BAGO RIVER BRIDGE CONSTRUCTION PROJECT	FINANCED BY JAPAN INTERNATIONAL COOPERATION AGENCY	COUNTERPART REPUBLIC OF THE UNION OF MYANMAR MINISTRY OF CONSTRUCTION DEPARTMENT OF BRIDGE	JICA STUDY TEAM NIPPON KOEI CO., LTD. ORIENTAL CONSULTANTS GLOBAL CO., LTD. METROPOLITAN EXPRESSWAY COMPANY LIMITED CHODAI CO. LTD. NIPPON ENGINEERING CONSULTANTS CO. LTD.	NAME	SIGNATURE	DATE	DRAWING TITLE GENERAL VIEW OF SUBSTRUCTURE AND FOUNDATION (12)	PACKAGE 3 DWG No. P3-FO-2013	
				PREPARED BY	Y. SUZUKI				15 Jun. 2017
				CHECKED BY	T. HAYAKAWA				
				APPROVED BY	Y. SANO				

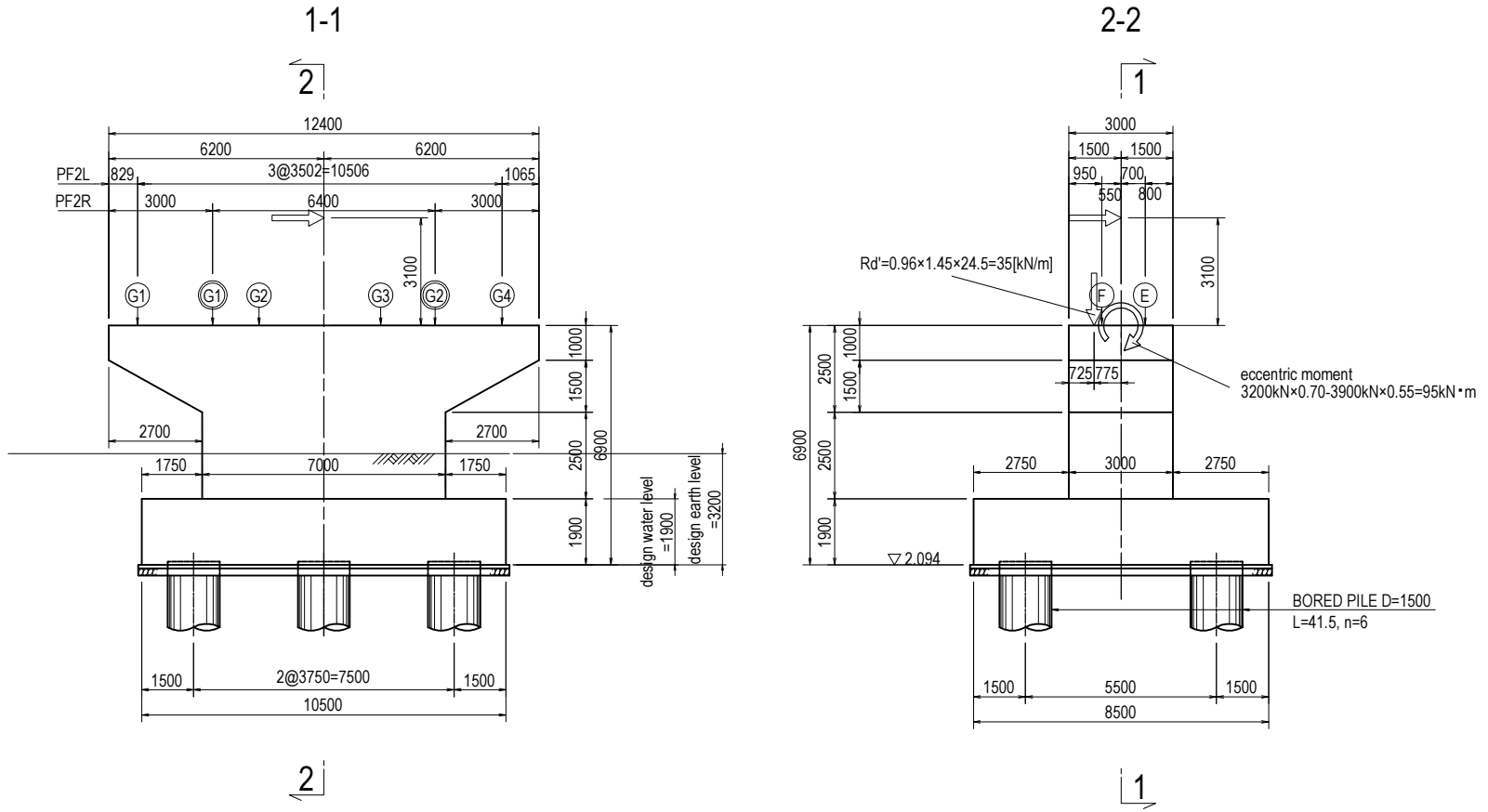
AF1 design model



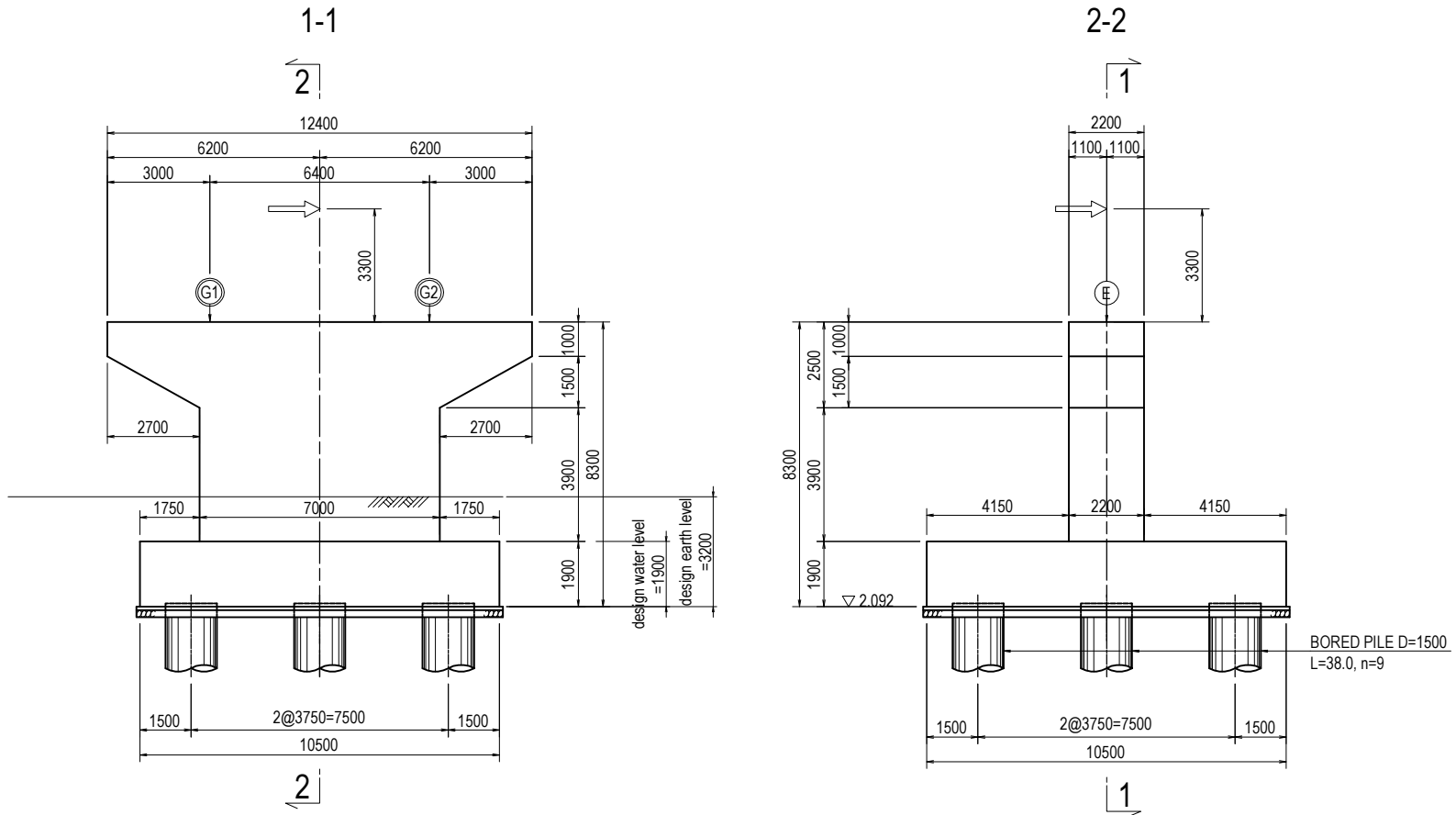
PF1 design model



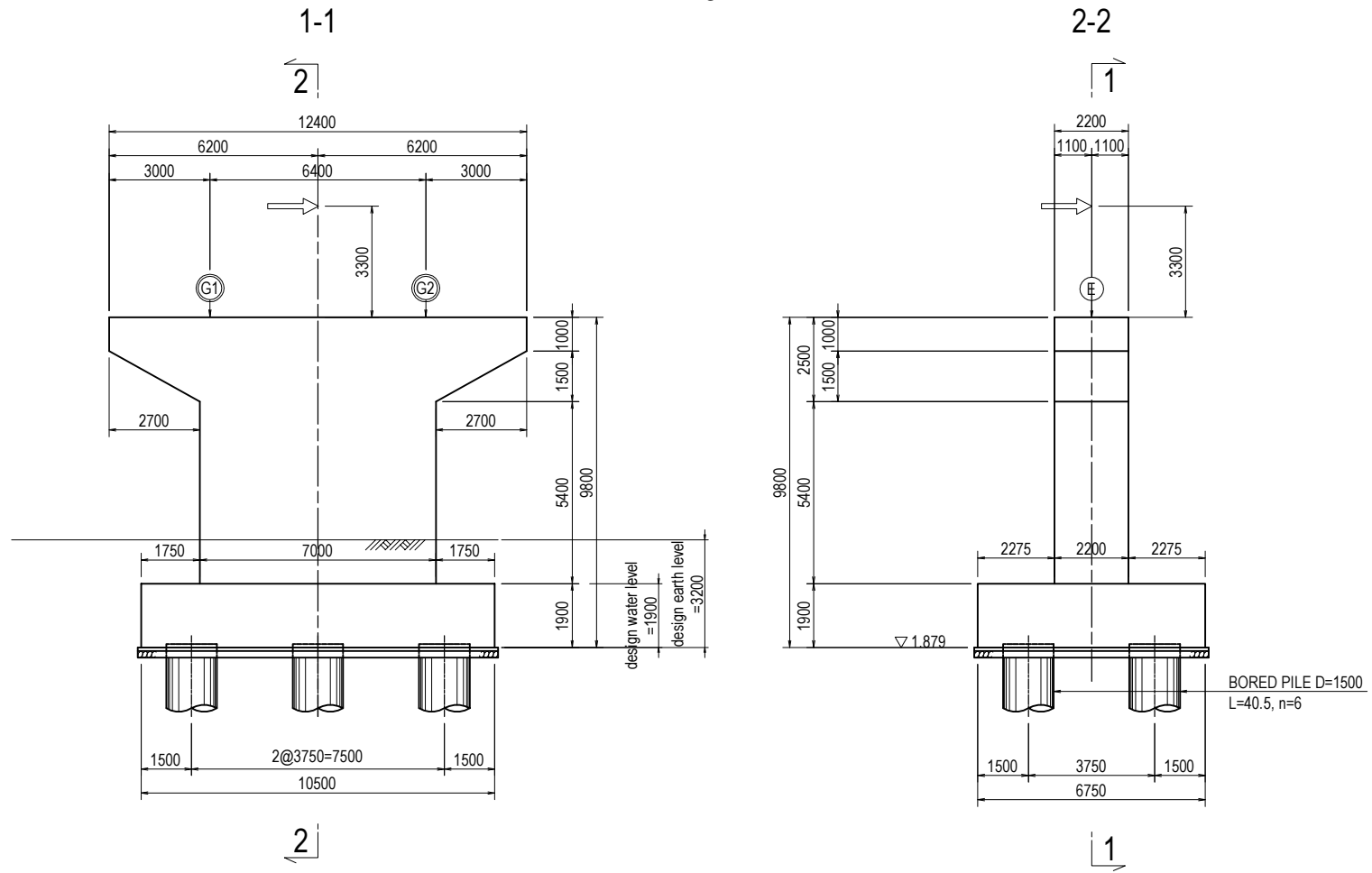
PF2 design model



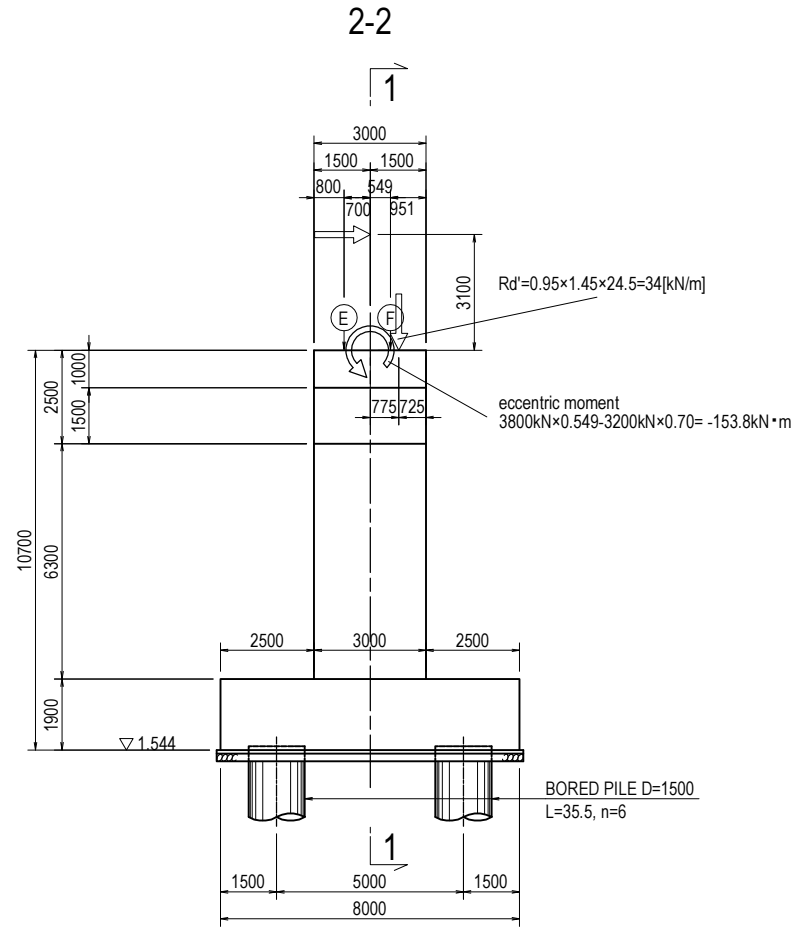
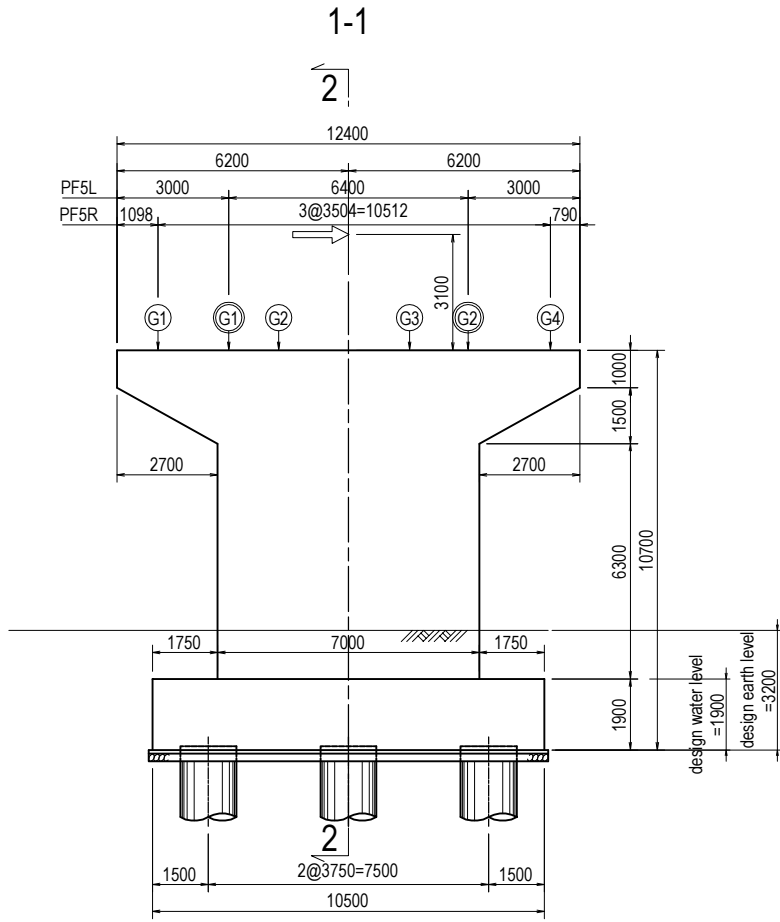
PF3 design model



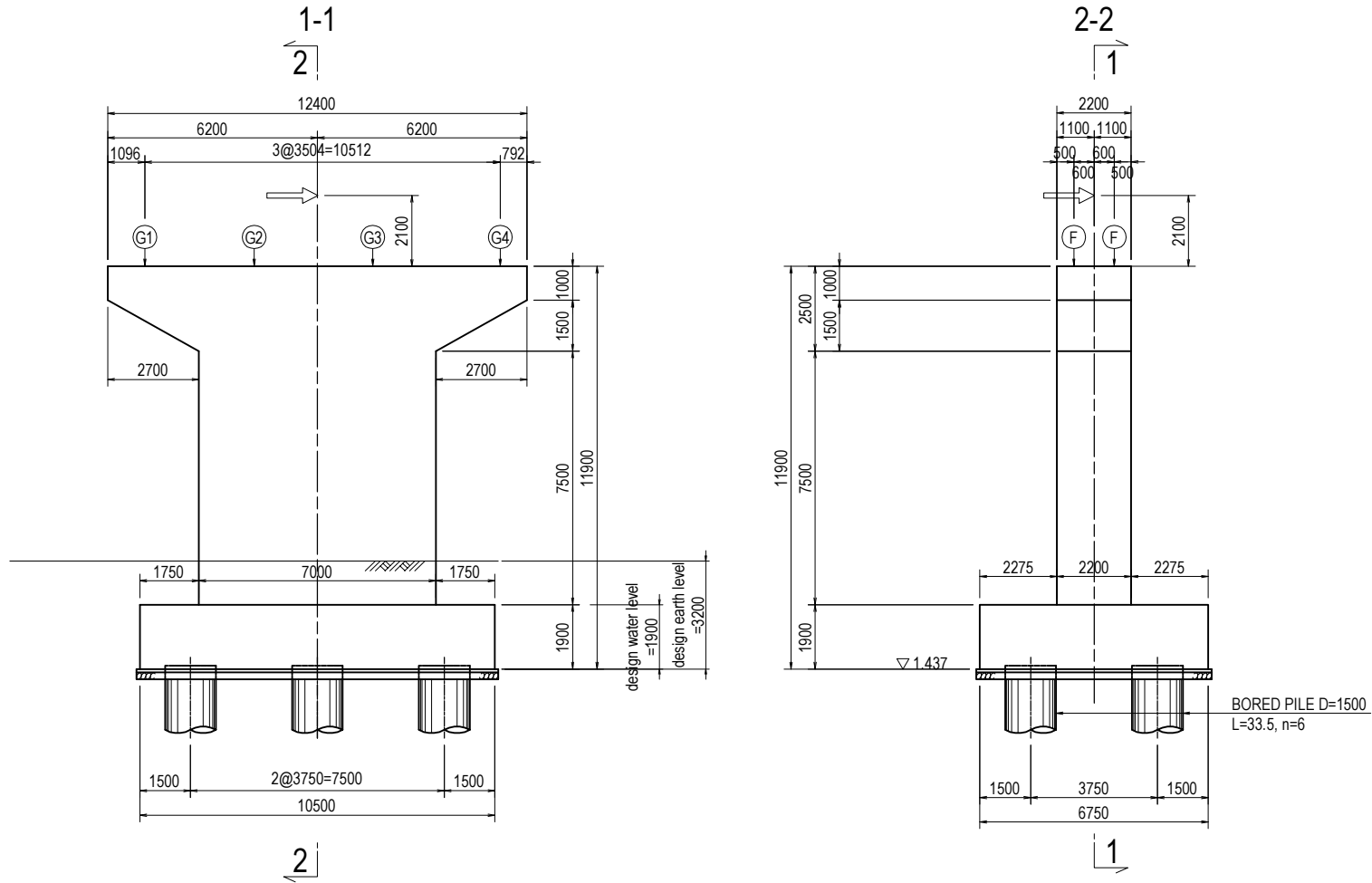
PF4 design model



PF5 design model

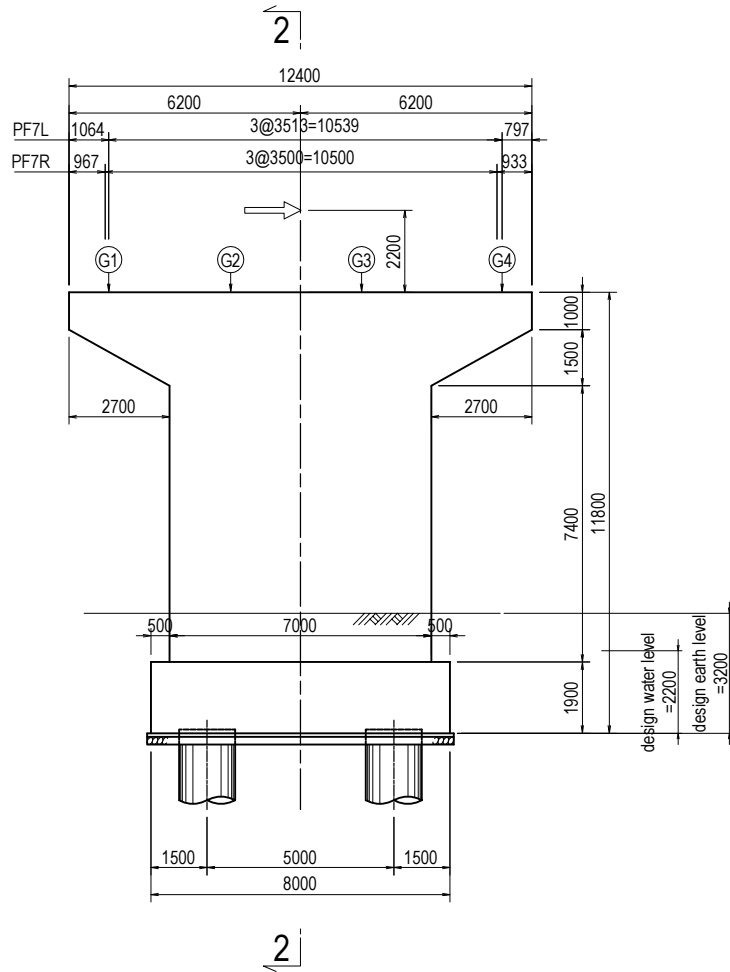


PF6 design model

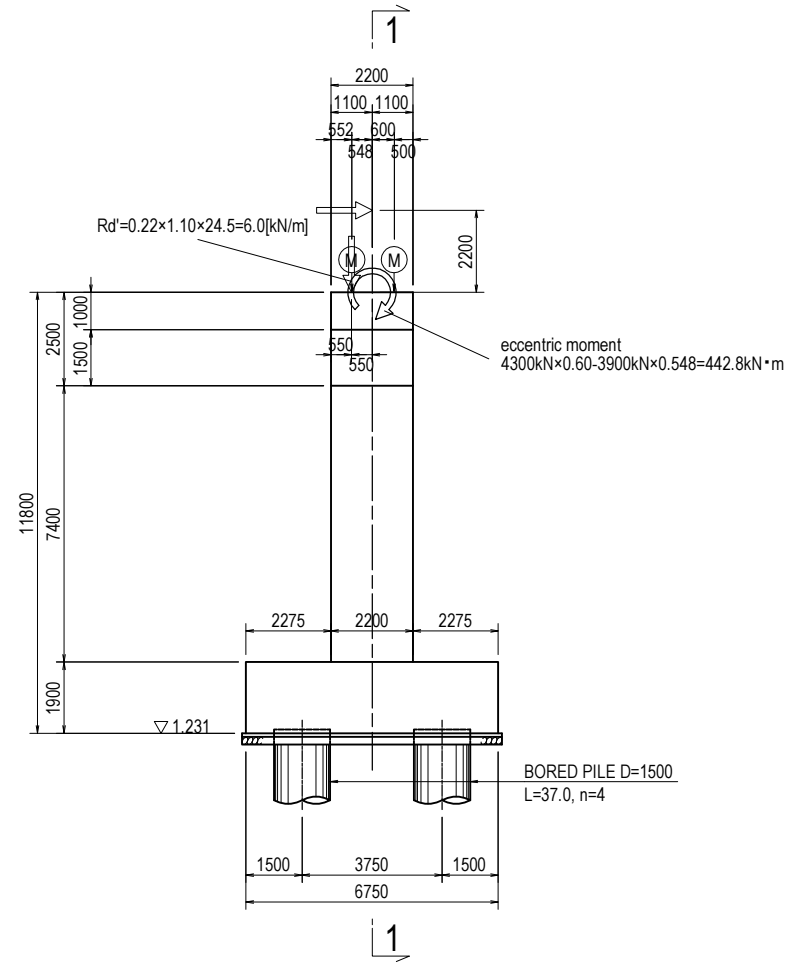


PF7 design model

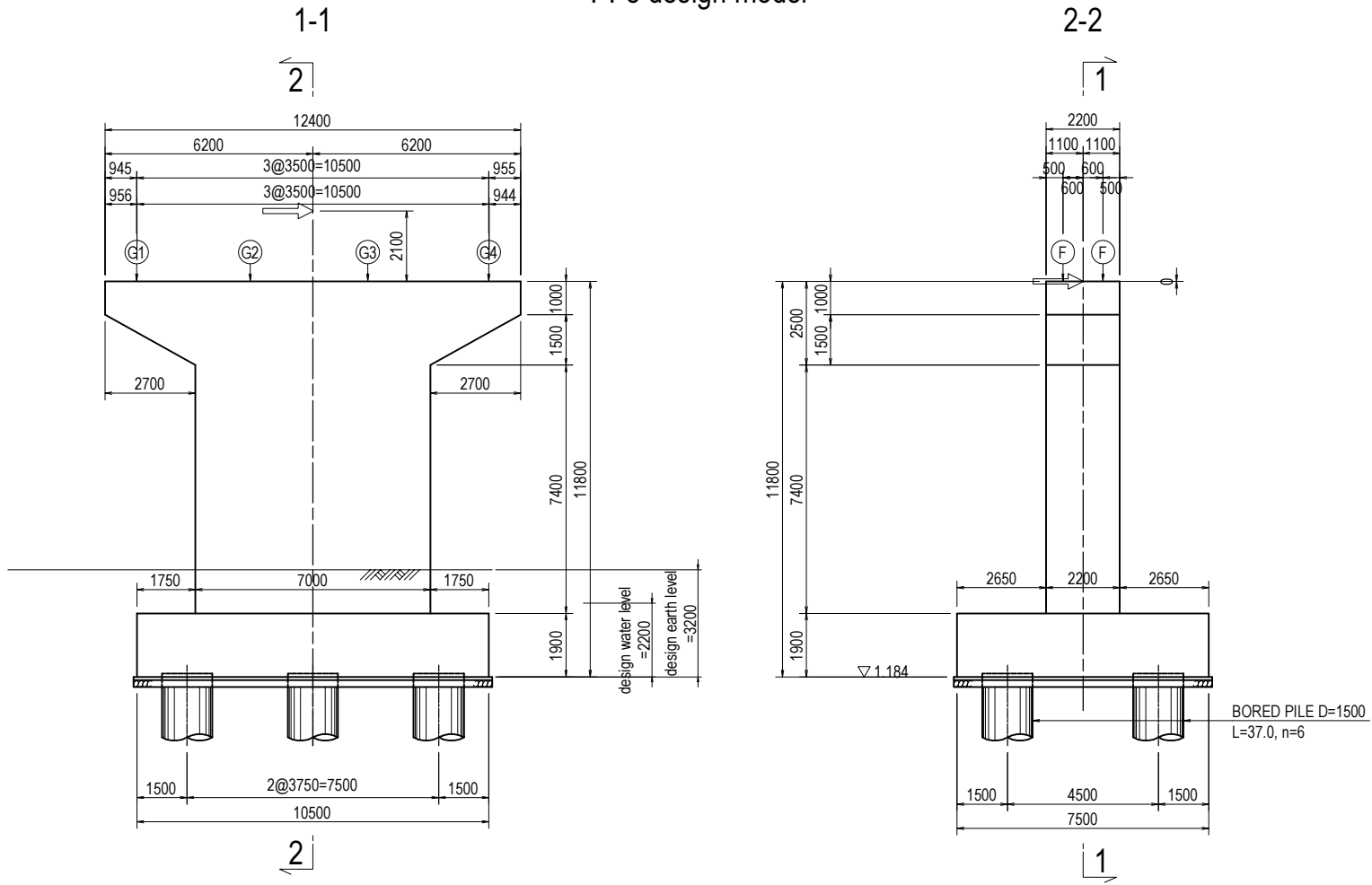
1-1



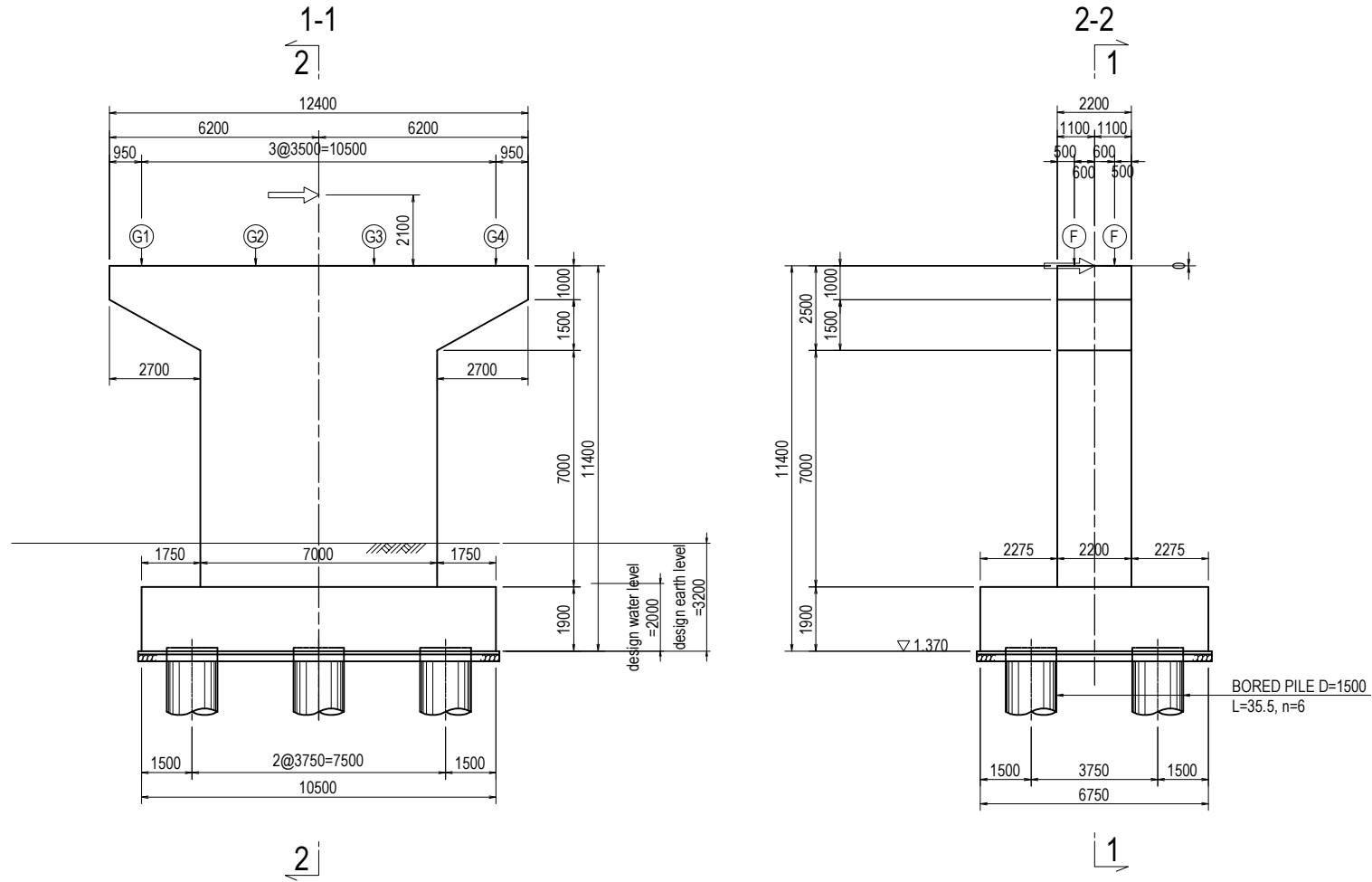
2-2



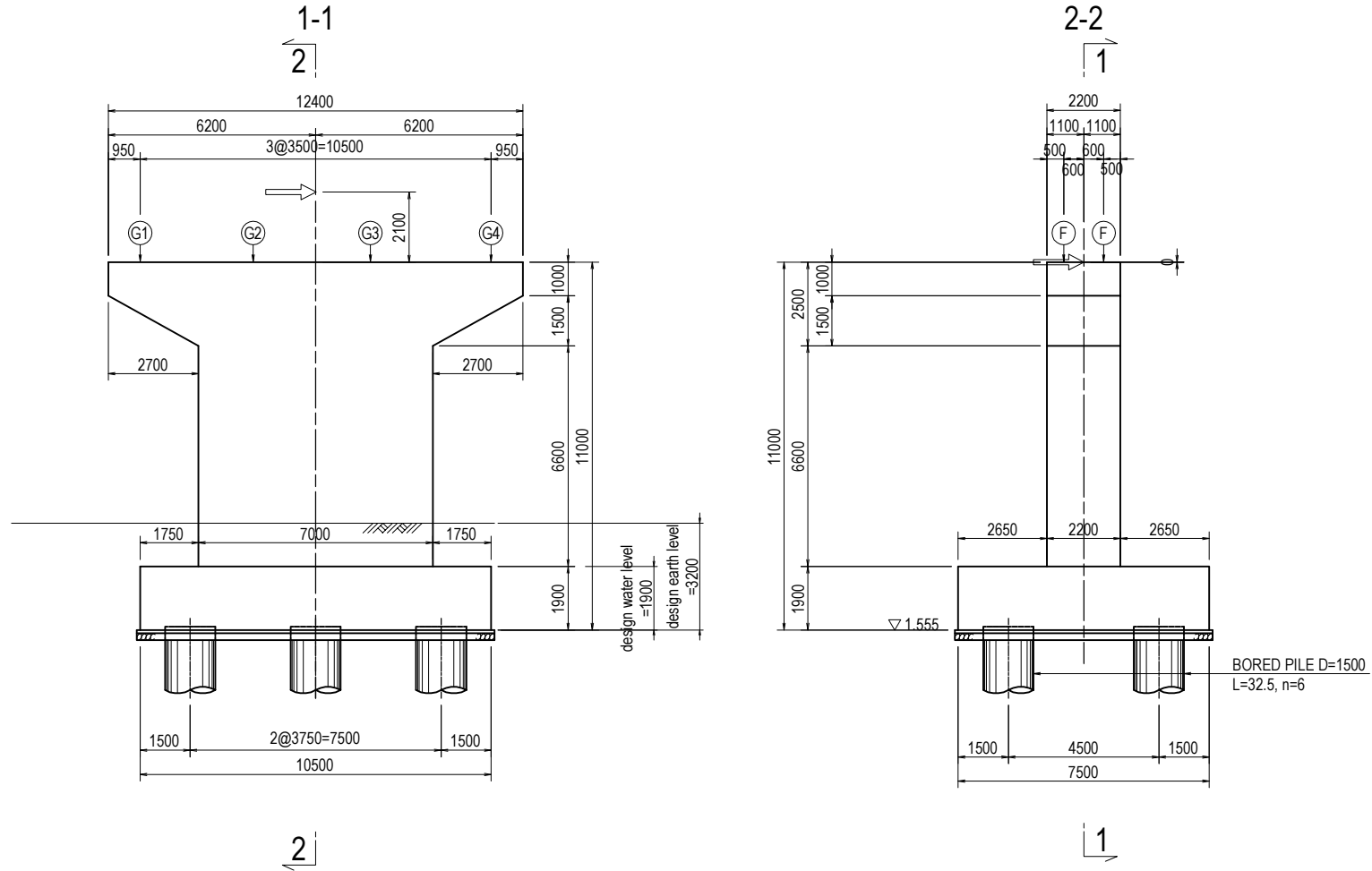
PF8 design model



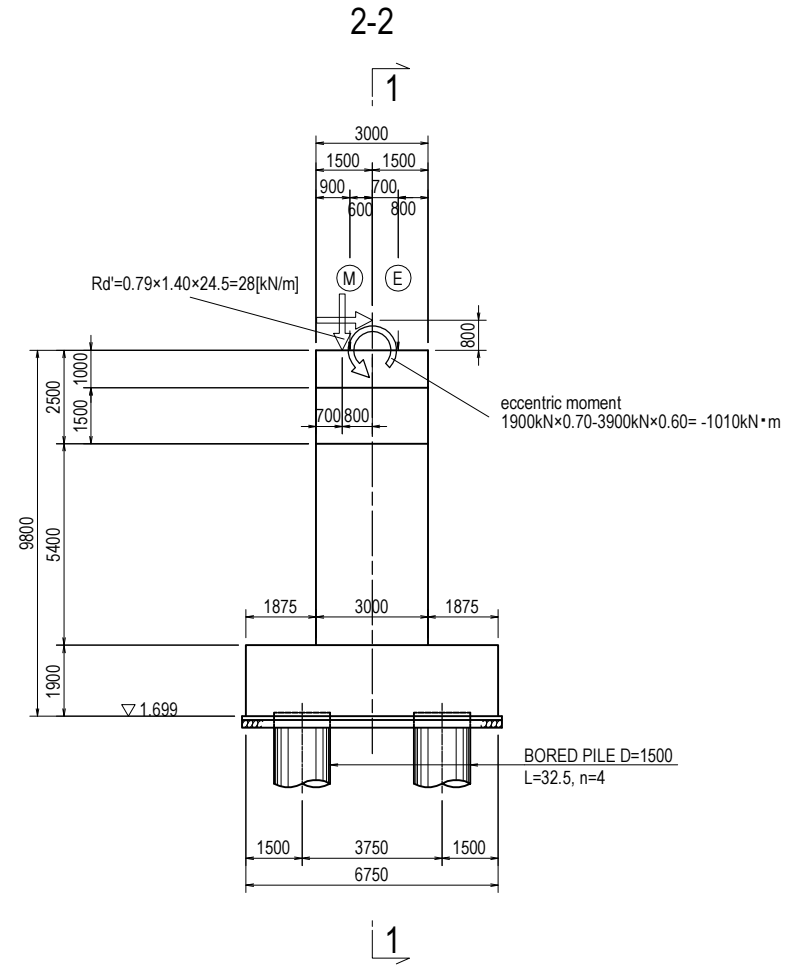
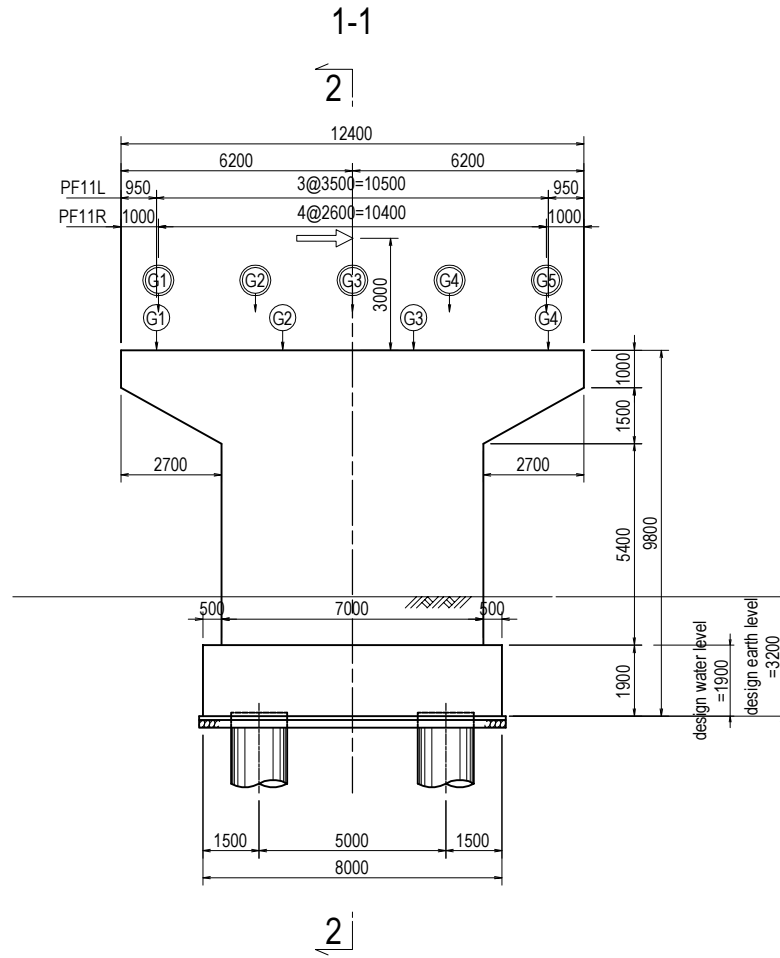
PF9 design model



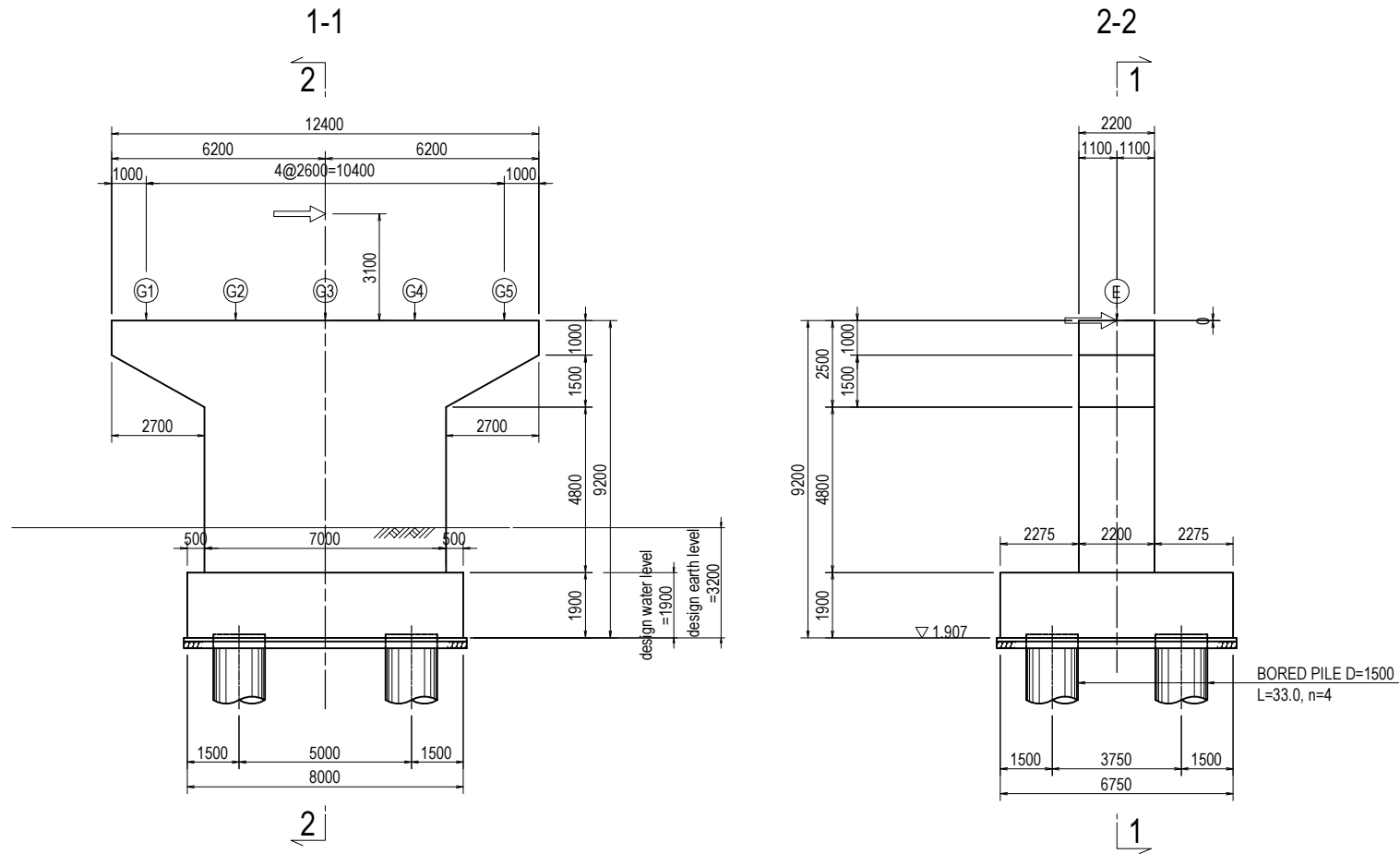
PF10 design model



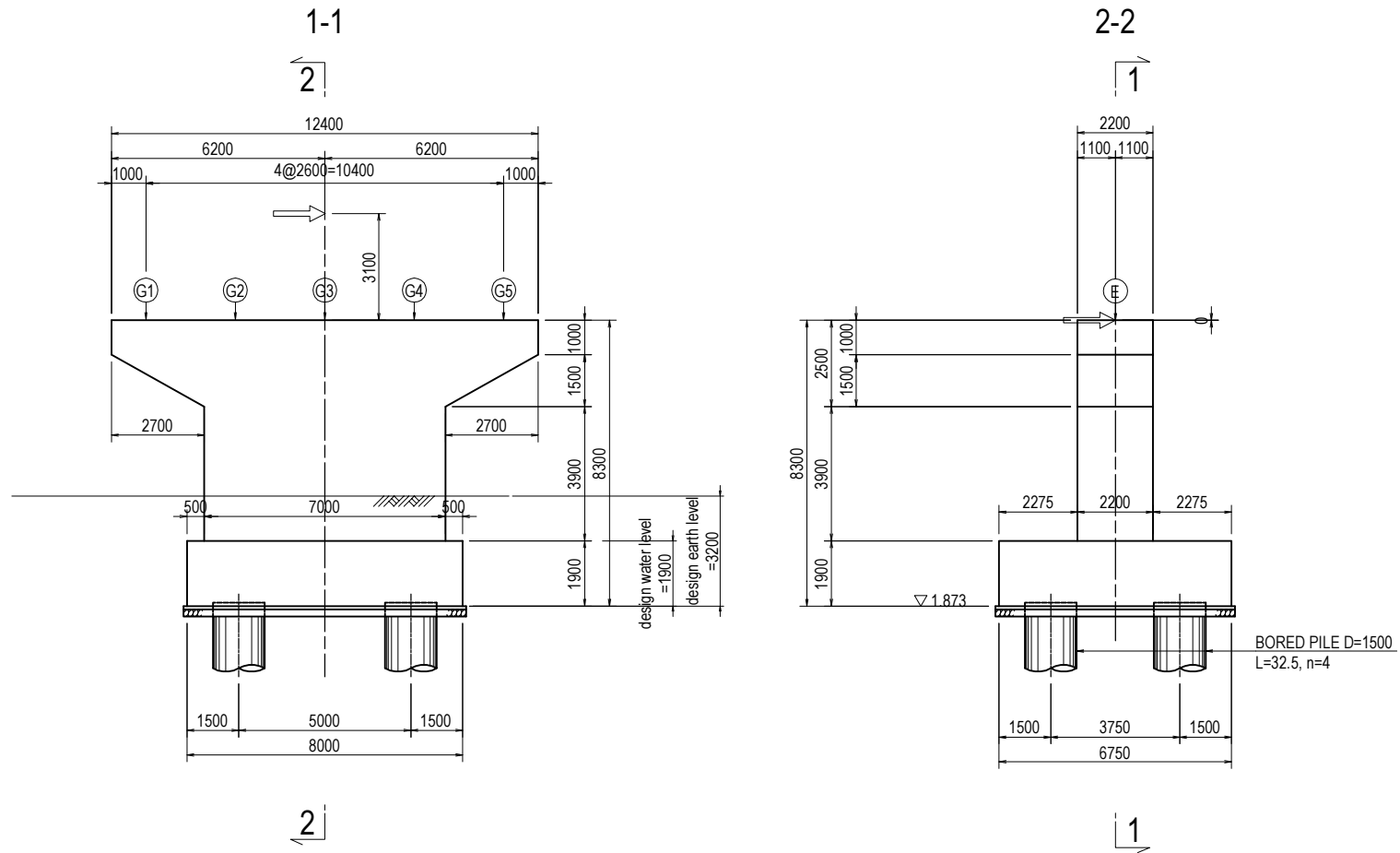
PF11 design model



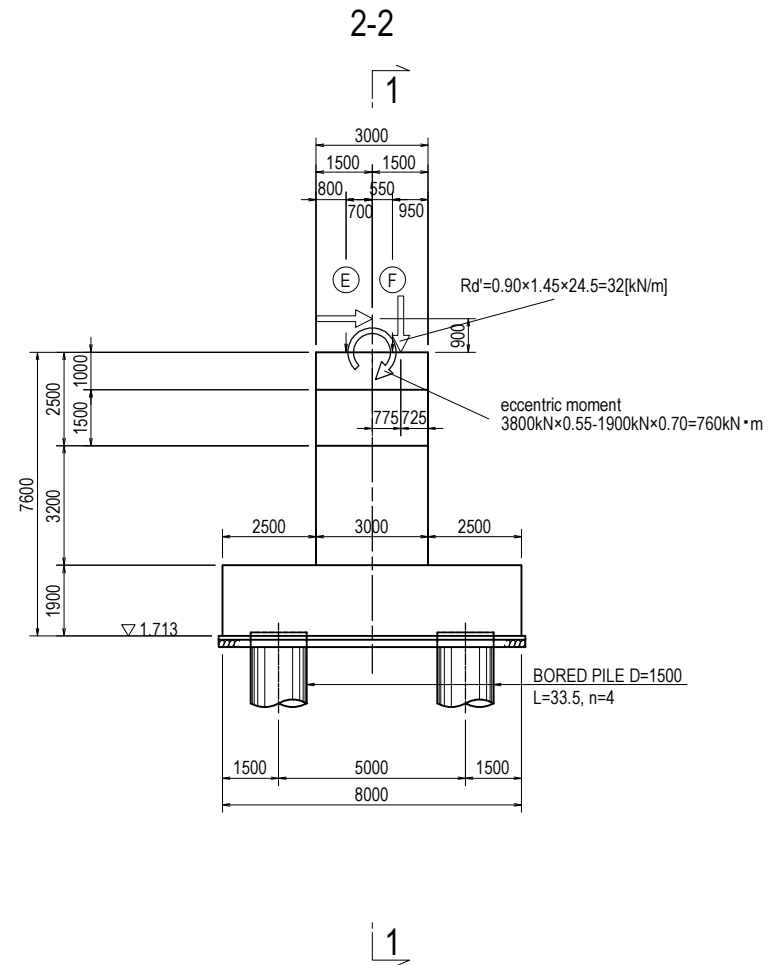
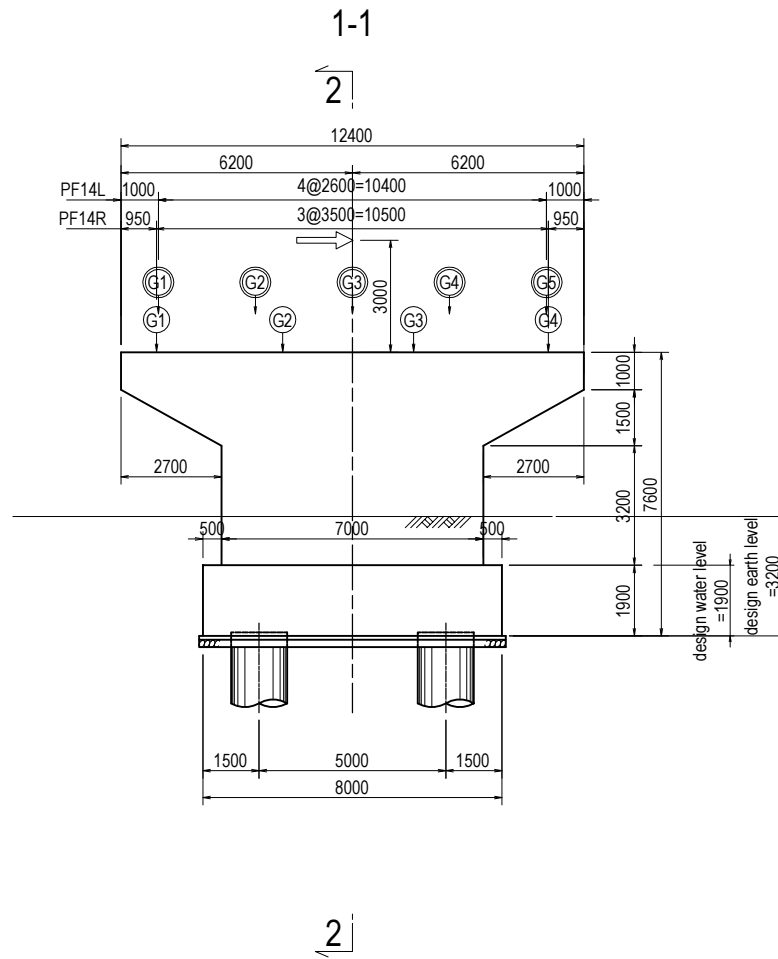
PF12 design model



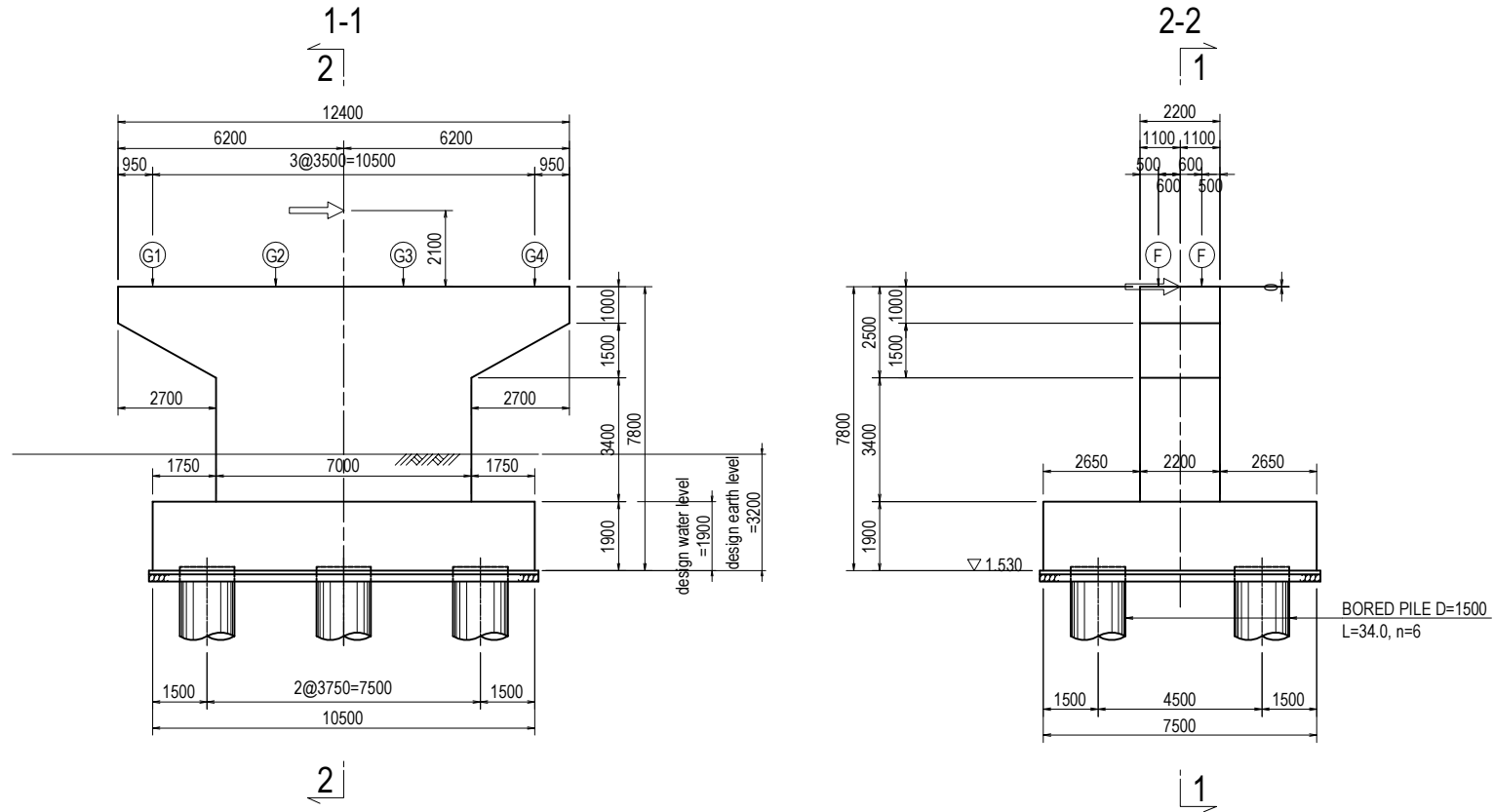
PF13 design model



PF14 design model



PF15 design model



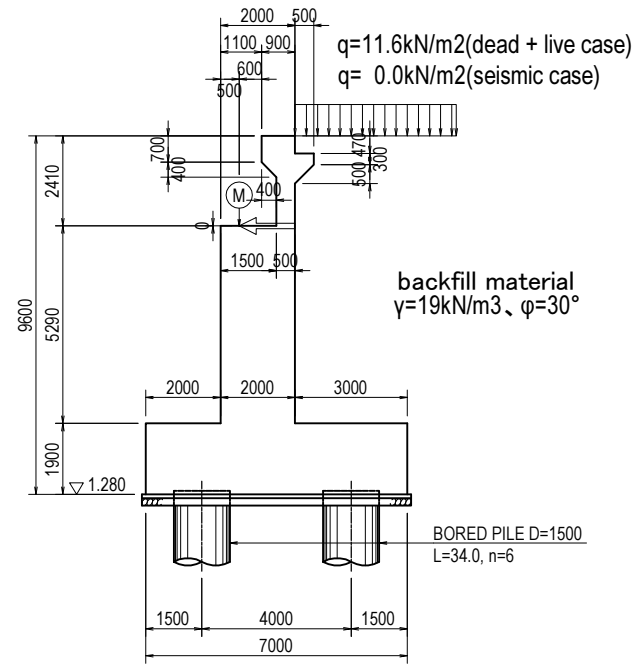
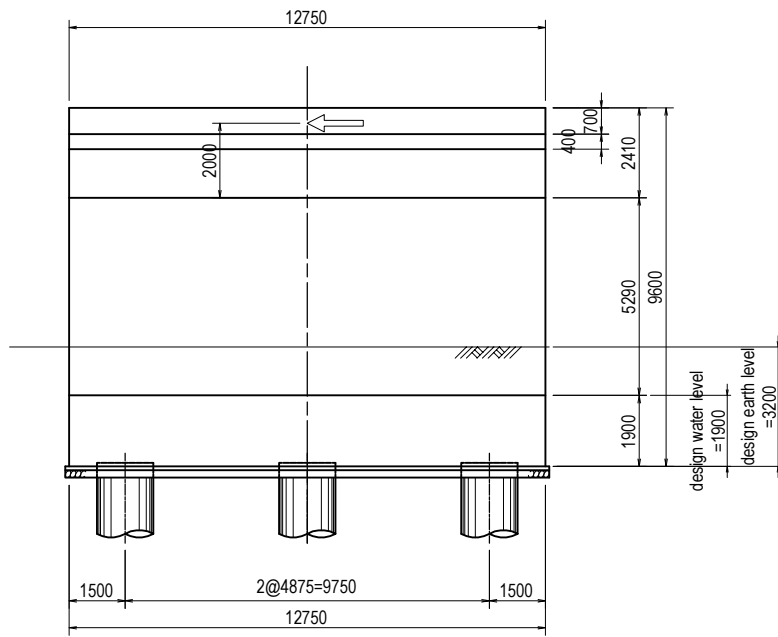
AF2 design model

1-1

2-2

2

1



§ 4. Geotechnical parameters

Regarding the information for the determination of geotechnical parameters, the Final Report of the Supplemental survey for Bago River Bridge was used. The parameters were established based on the soil conditions encountered during soil exploration and testing. Table 4- 1 shows the geotechnical design parameters.

Table 4- 1 Geotechnical Design Parameters for Flyover Design

Layer	N Average ^{*1}	Unit Weight “ γ ” (kN/m ³)	Cohesion “c” (kN/m ²)	Friction Angle “ ϕ ” ^{*5} (°)	Modulus of Deformation “E” (kN/m ²)
FILLED SOIL	4	18 ^{*3}	24 ^{*4}	0	1300 ^{*6}
CLAY-I	4	18 ^{*2}	24 ^{*1}	0	1300 ^{*6}
SILTY SAND-I	10	18 ^{*2}	0 ^{*4}	32	5000 ^{*8}
SANDY SILT	8	17 ^{*3}	48 ^{*4}	0	5600 ^{*7}
SILTY SAND-II	22	19 ^{*3}	0 ^{*4}	33	15400 ^{*7}
CLAY-II	21	18 ^{*3}	126 ^{*4}	0	14700 ^{*7}
CLAYEY SAND-I	35	19 ^{*3}	0 ^{*4}	33	24500 ^{*7}
CLAY-III	35	18 ^{*3}	210 ^{*4}	0	24500 ^{*7}
CLAYEY SAND-II	50	19 ^{*3}	0 ^{*4}	37	35000 ^{*7}
CLAY-IV	50	18 ^{*3}	300 ^{*4}	0	35000 ^{*7}

Source: JICA Study Team

*1 Maximum N value is 50

*2 Average values obtained by each tests

*3 Referenced by Japanese Standard (NEXCO)

*4 Calculated by $C=6N$ (referenced by Japanese Standard (NEXCO)). The value of sandy soil is 0.

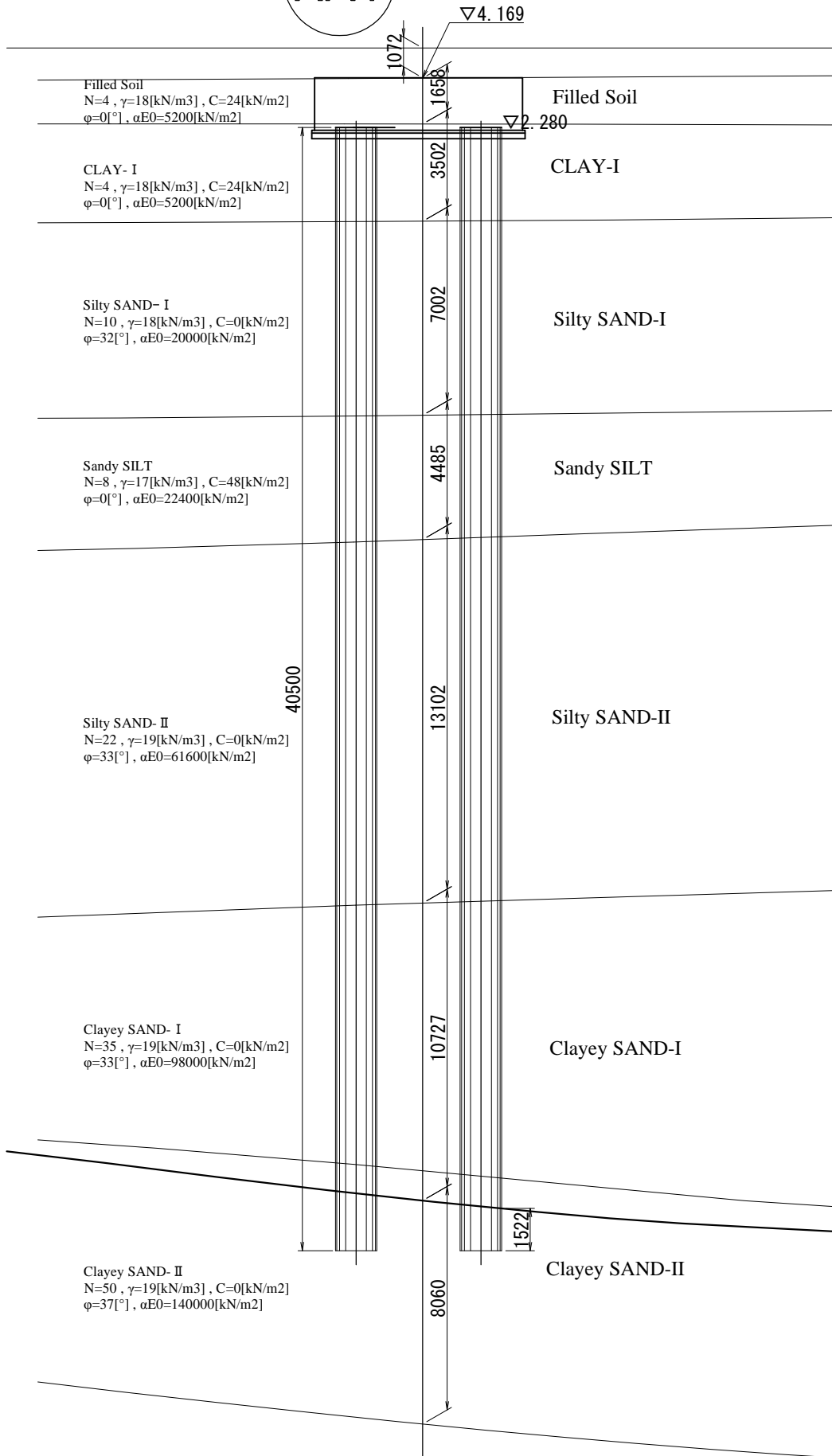
*5 Calculated with N value using effective overburden pressure

*6 Test value obtained by unconfined compression test

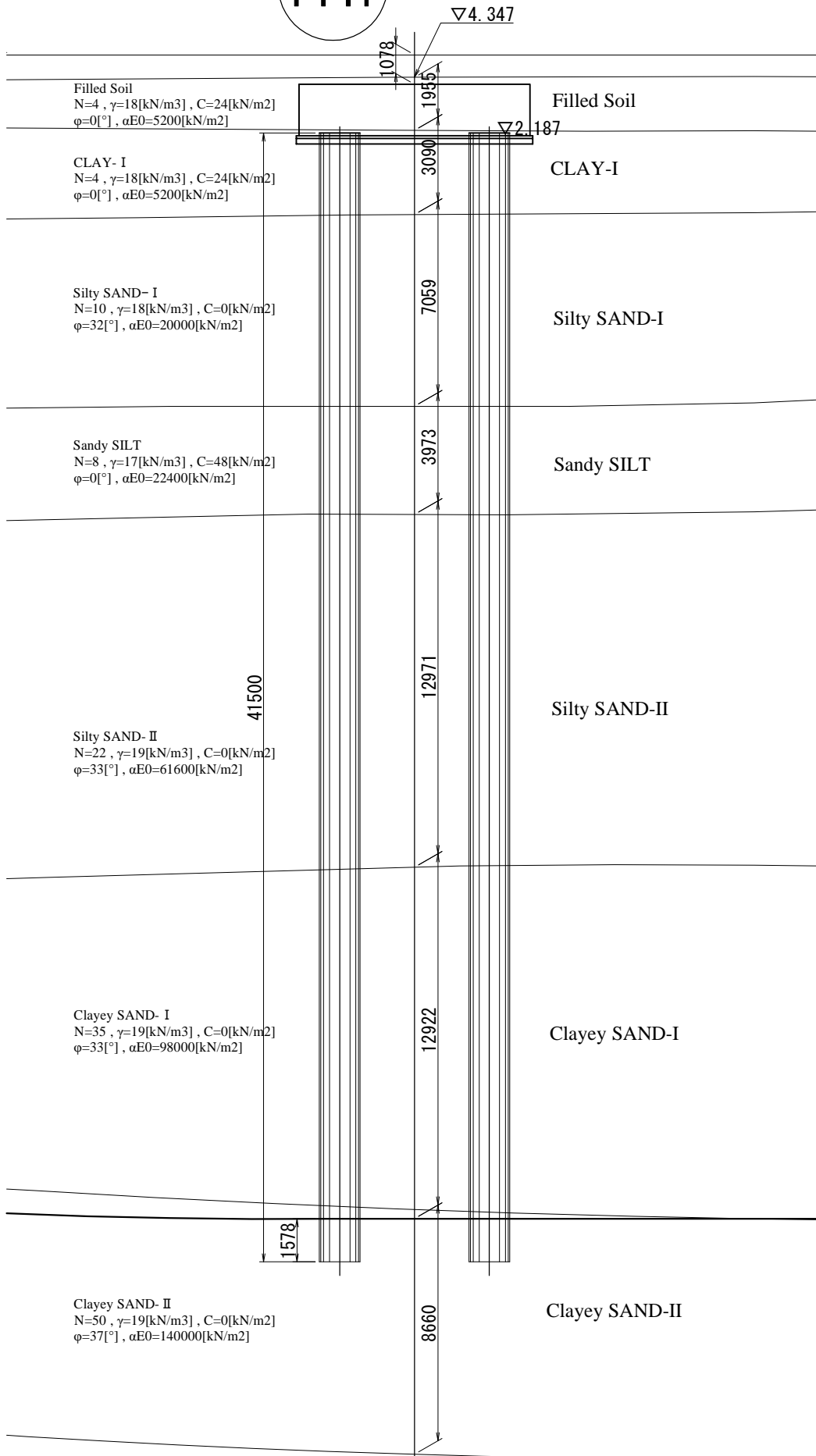
*7 $E=700N$ according to the worth value obtained by borehole lateral load test

*8 $E=500N$ according to the worth value obtained by borehole lateral load test

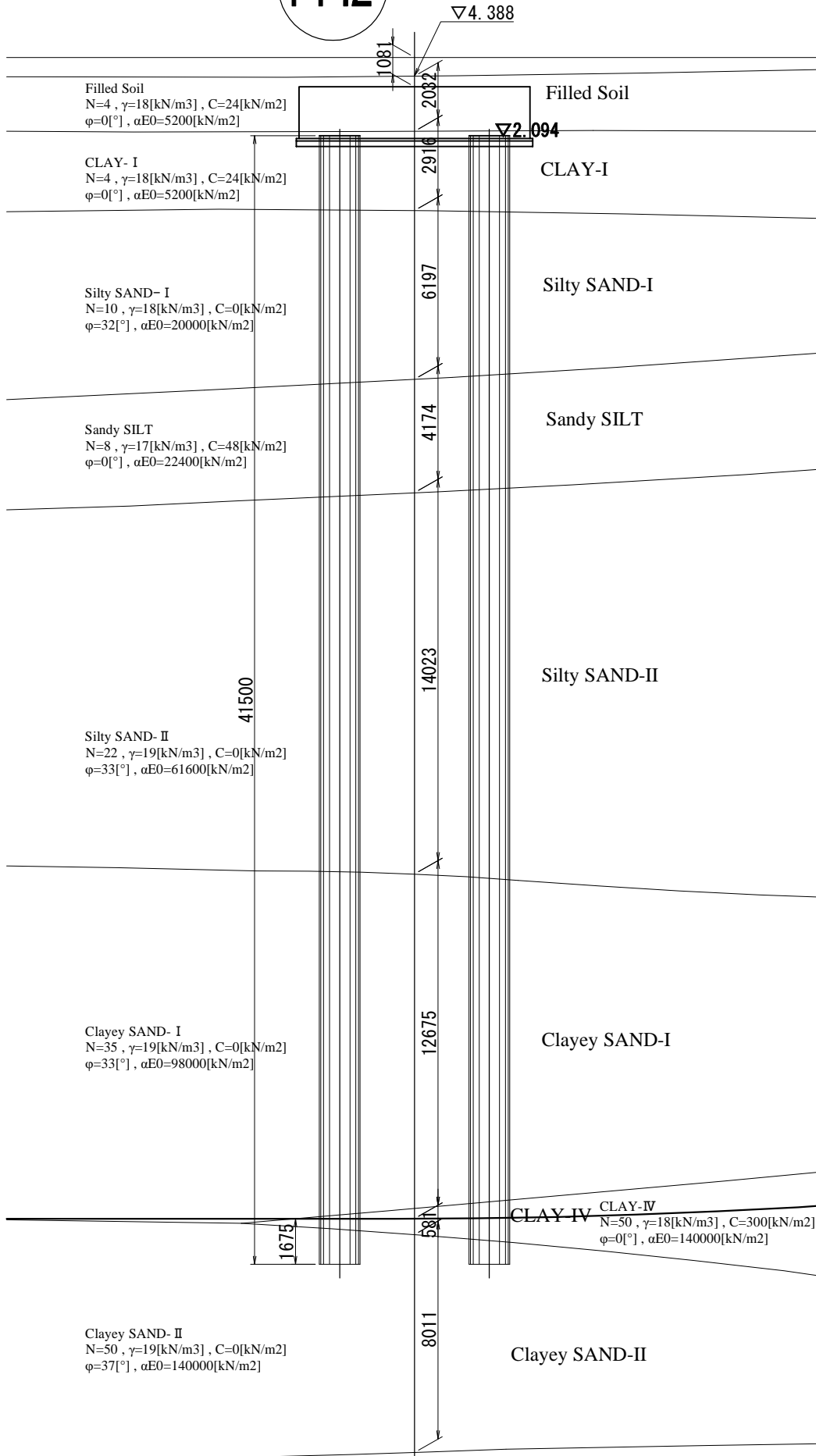
AF.1



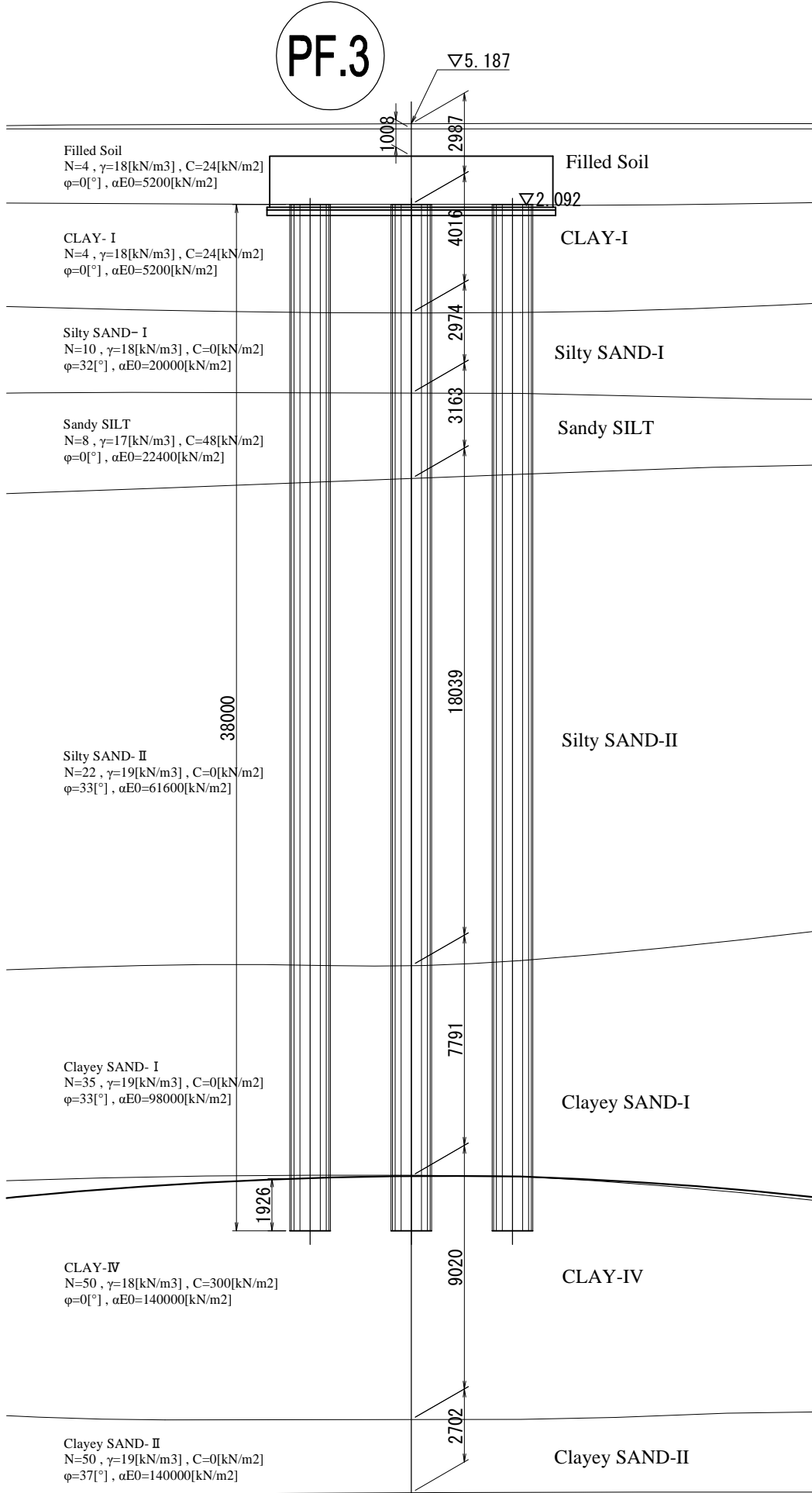
PF.1



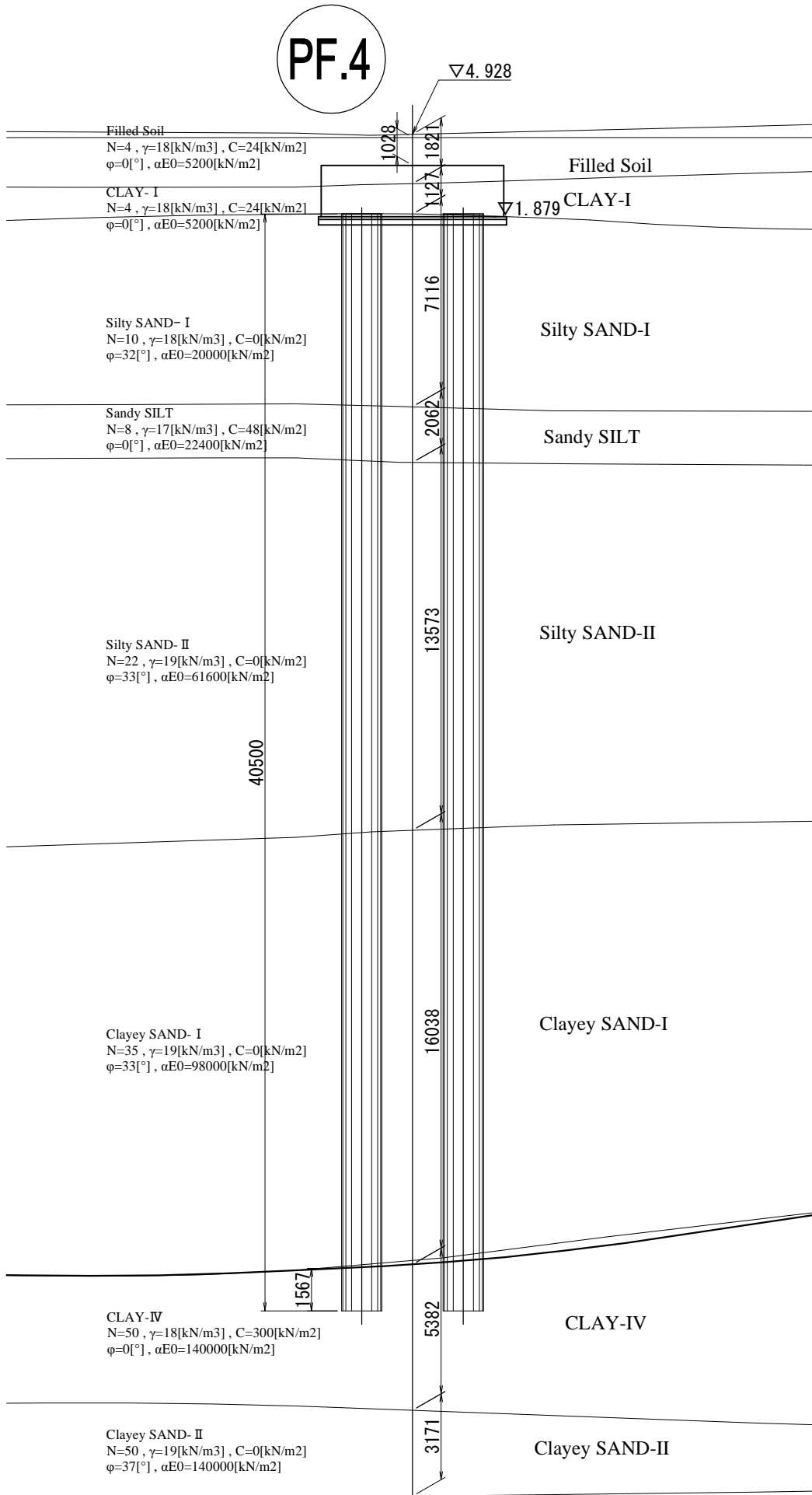
PF.2



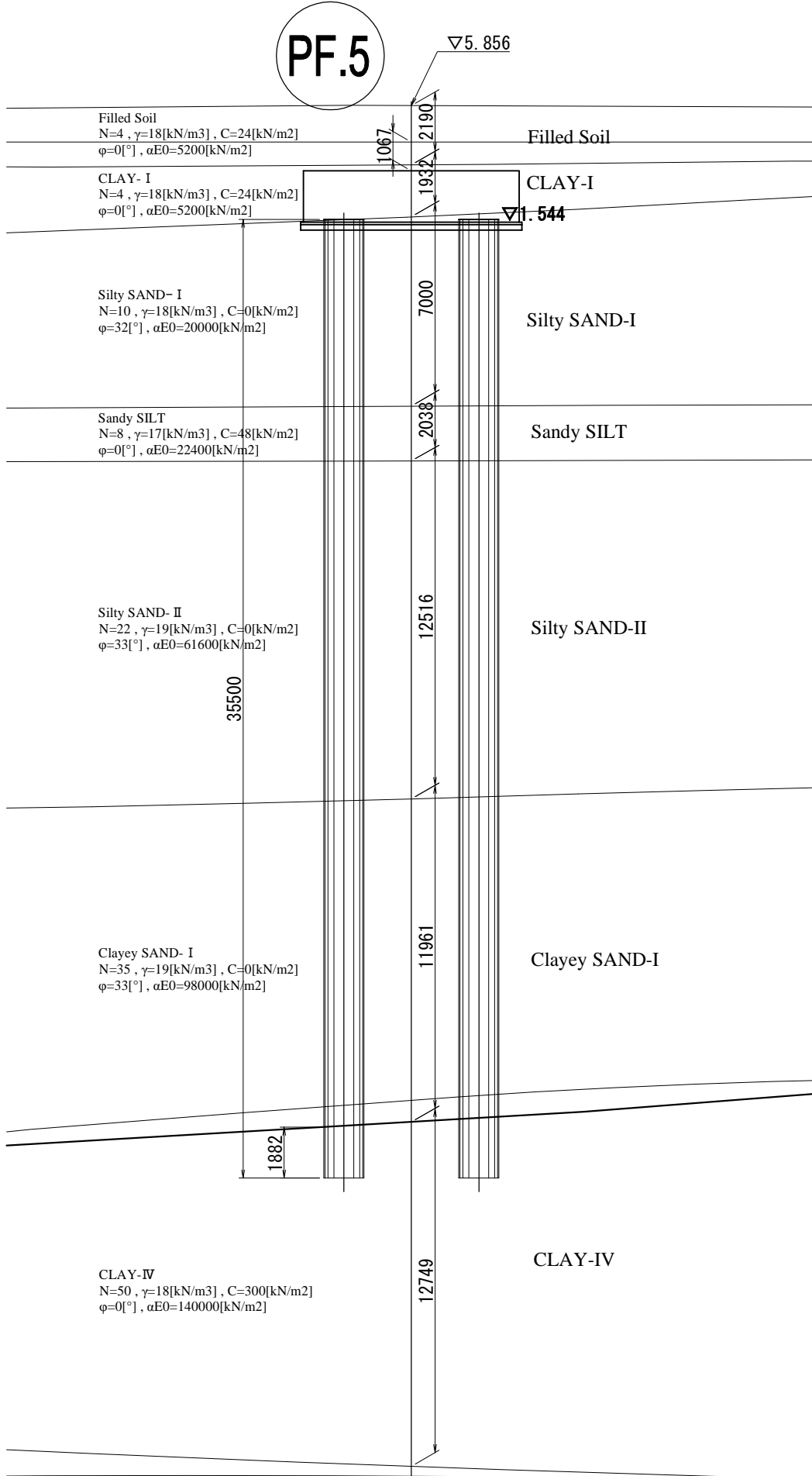
PF.3



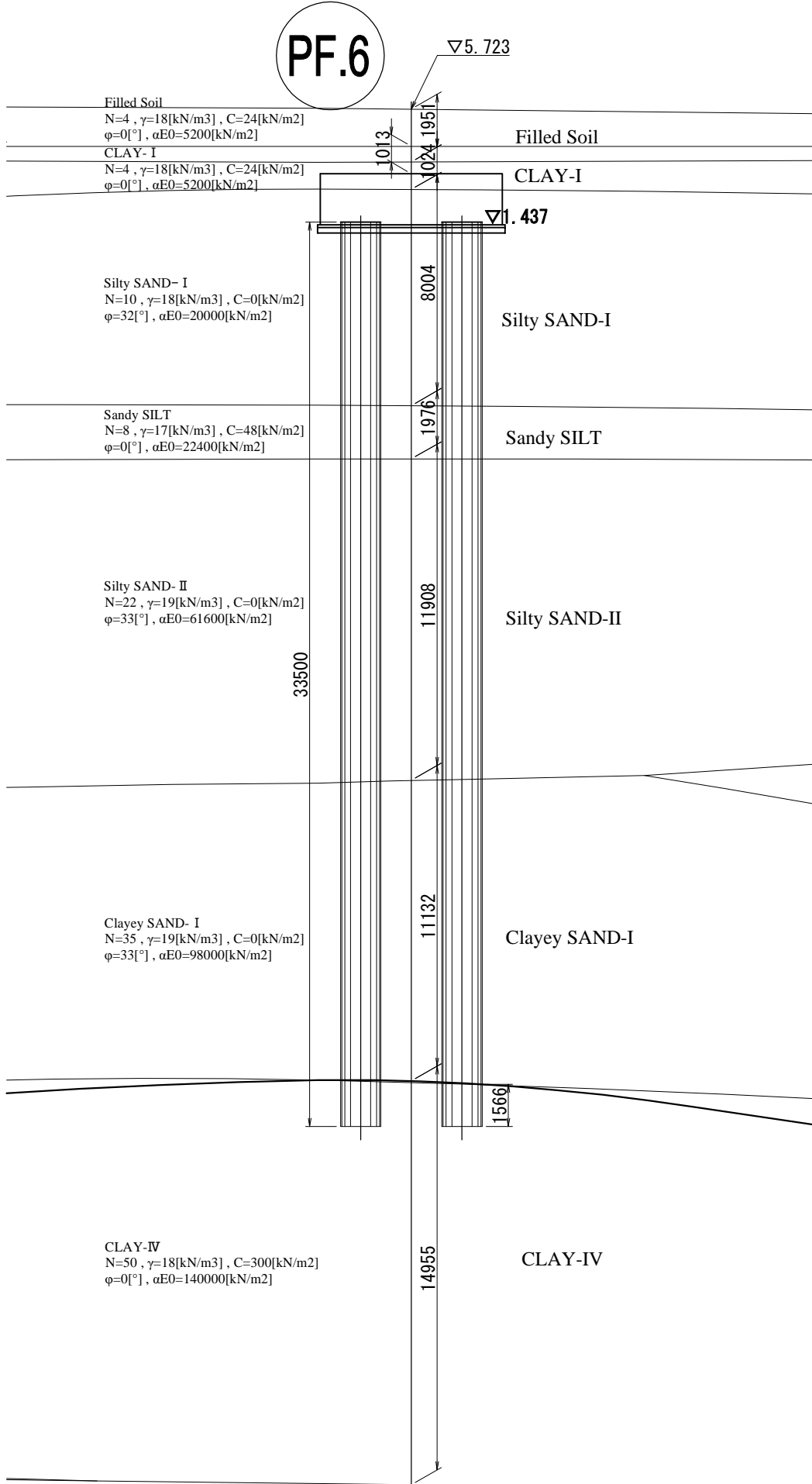
PF.4



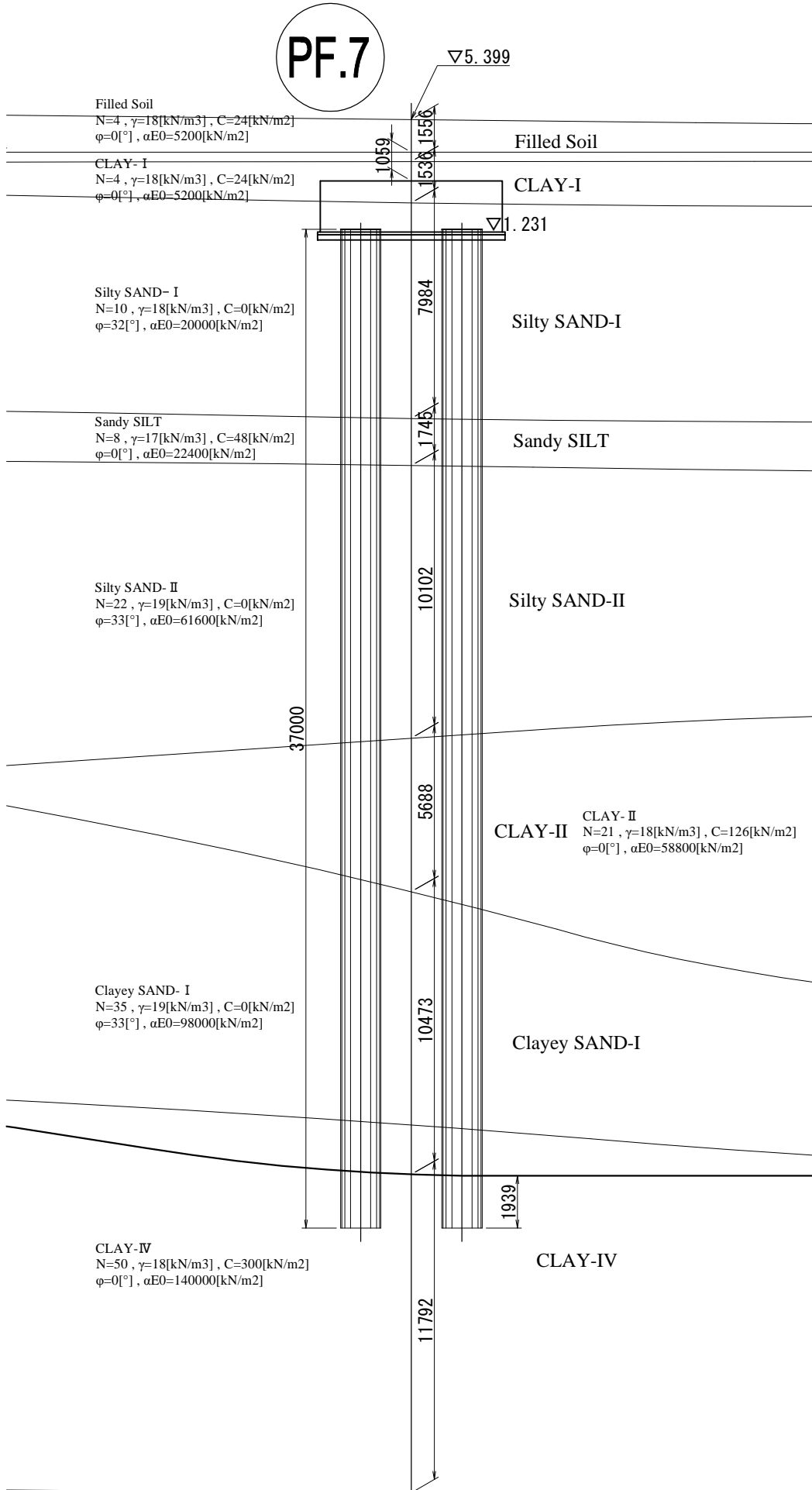
PF.5



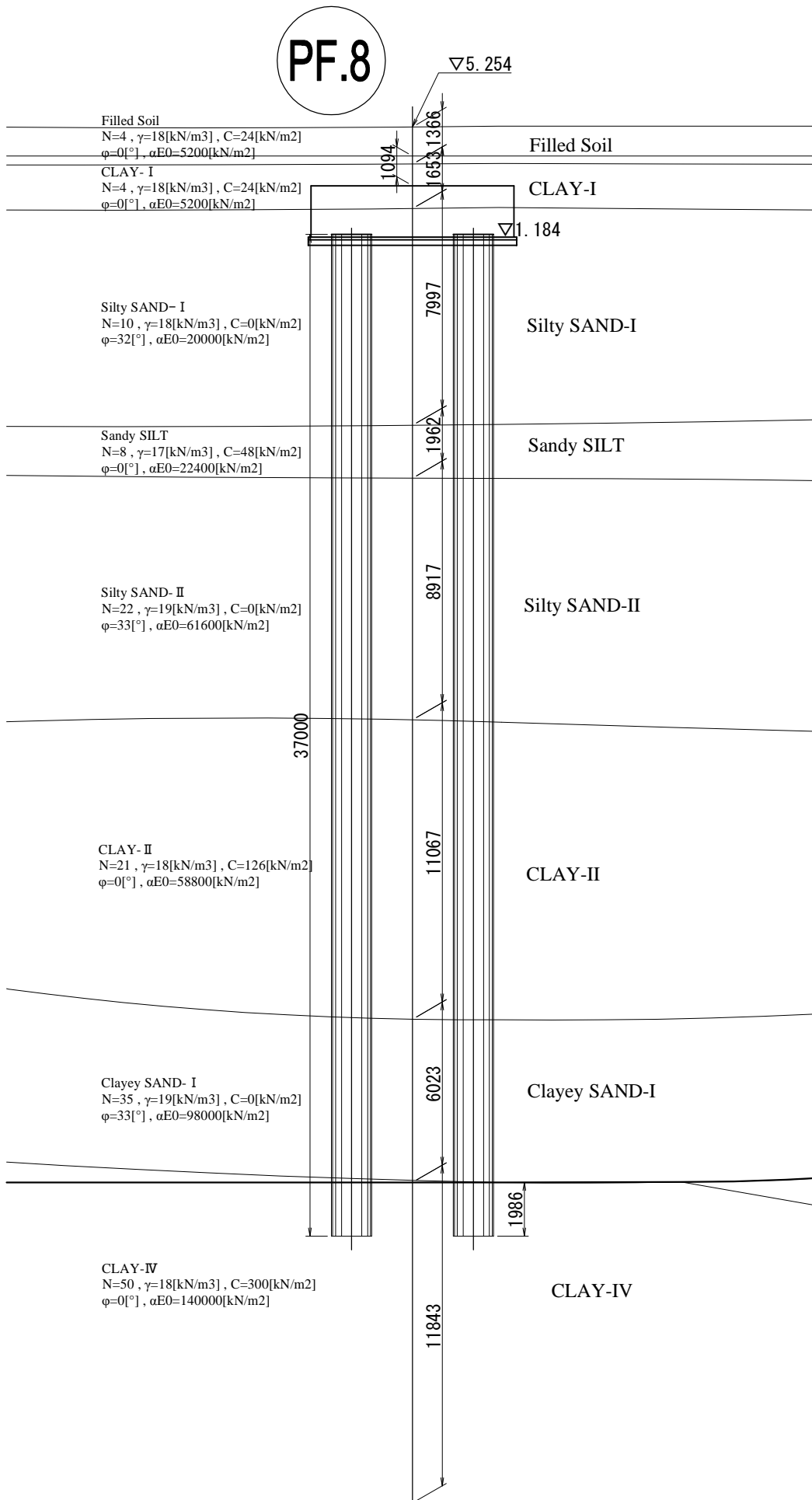
PF.6



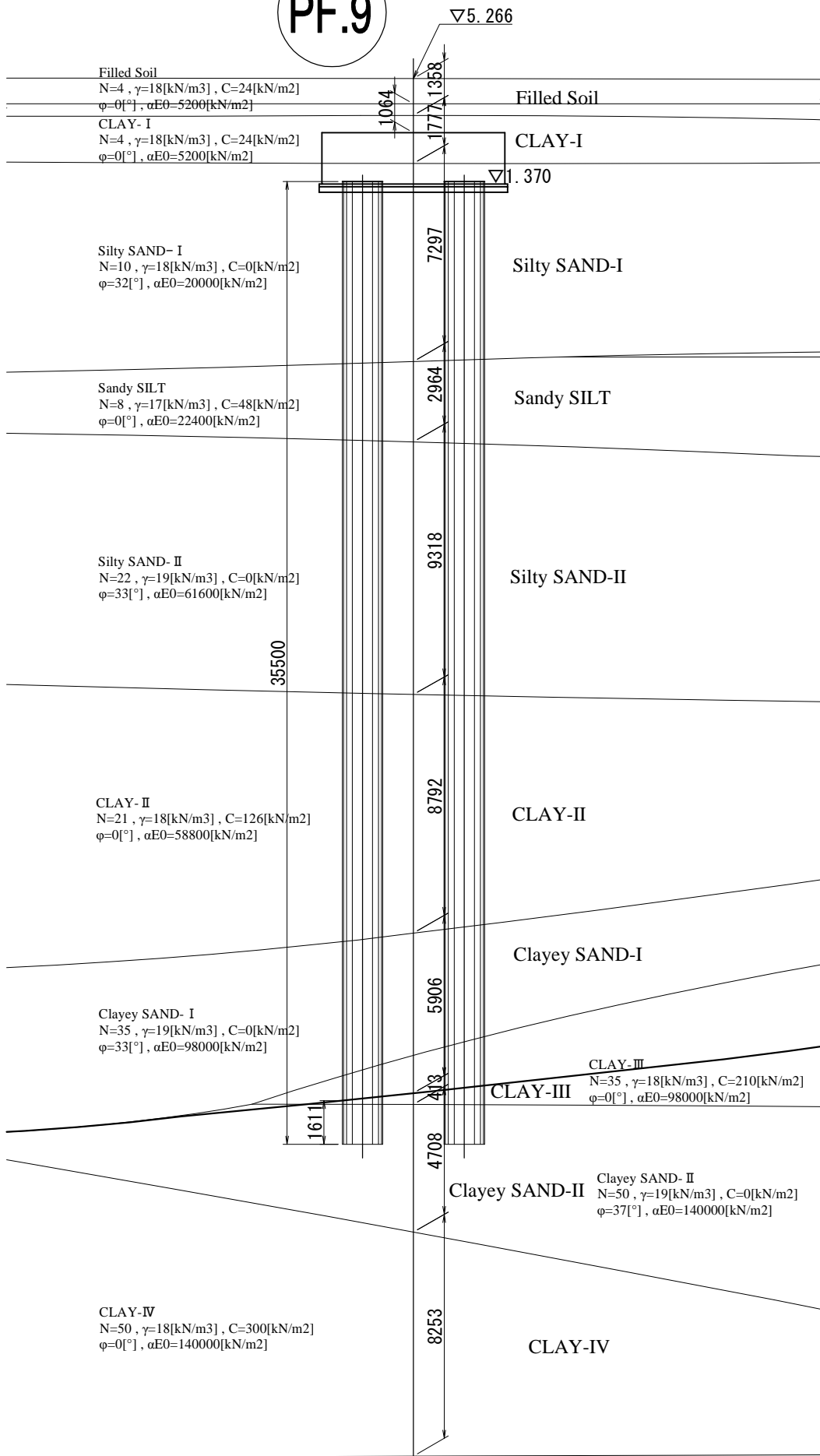
PF.7



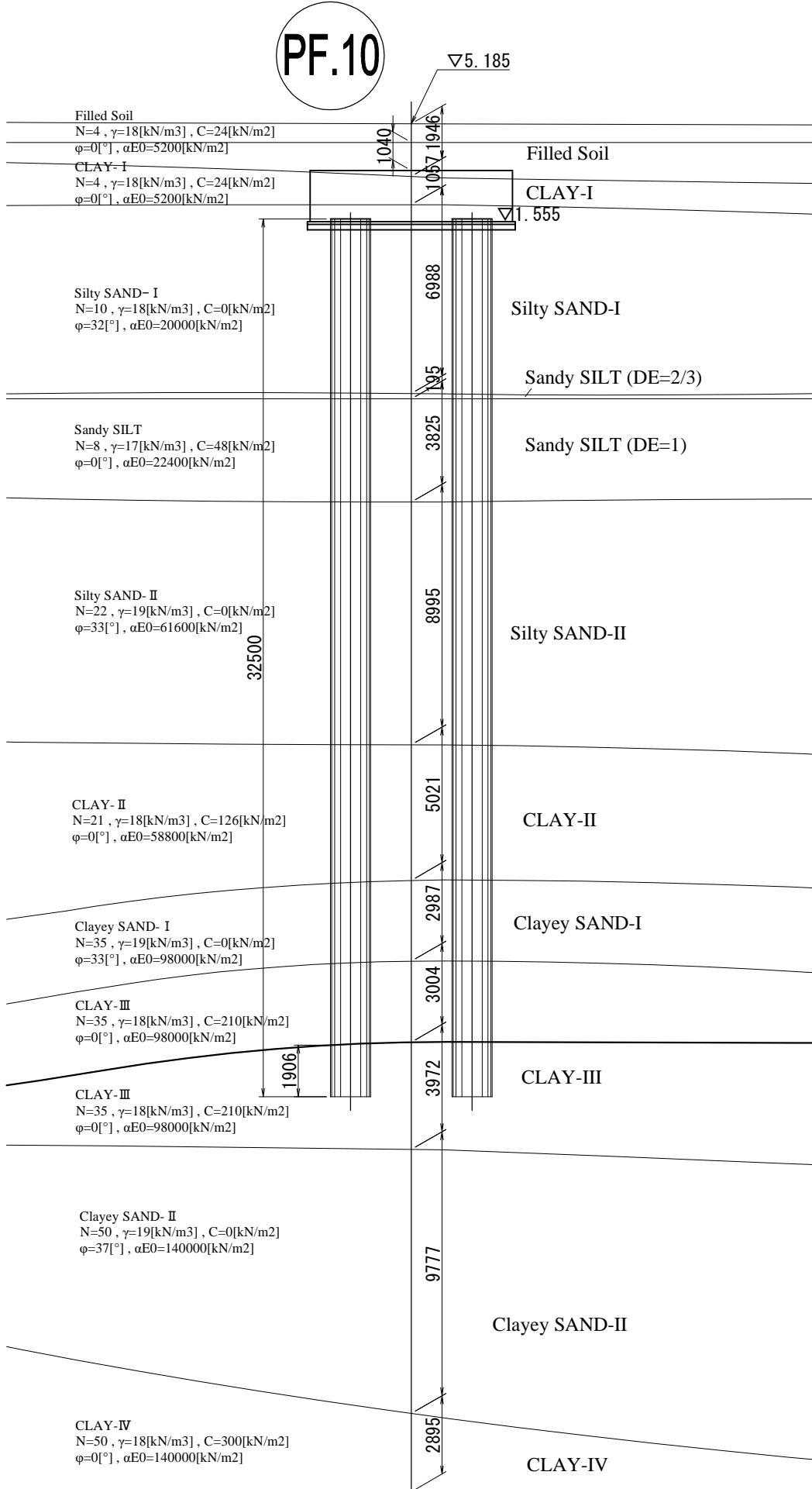
PF.8



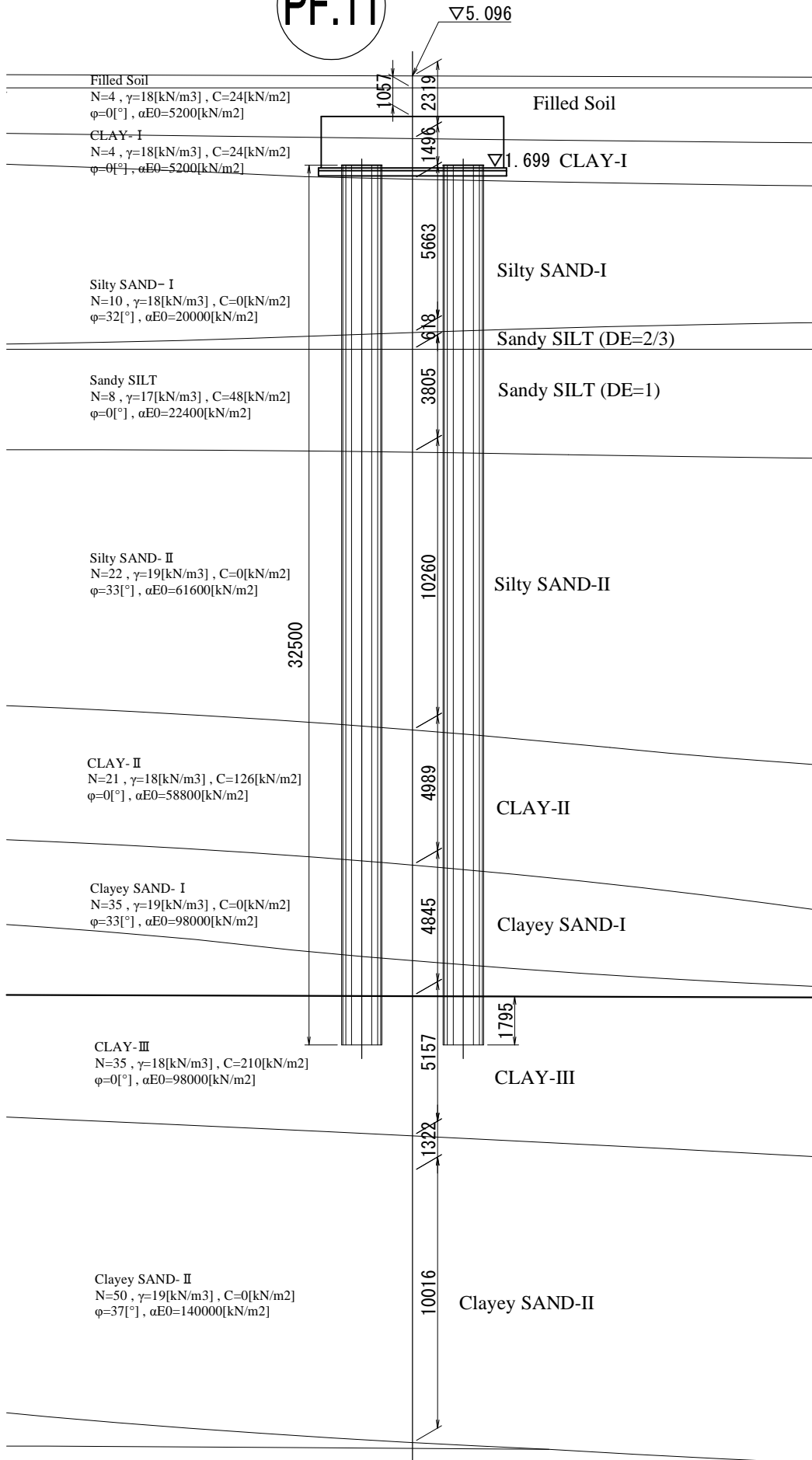
PF.9



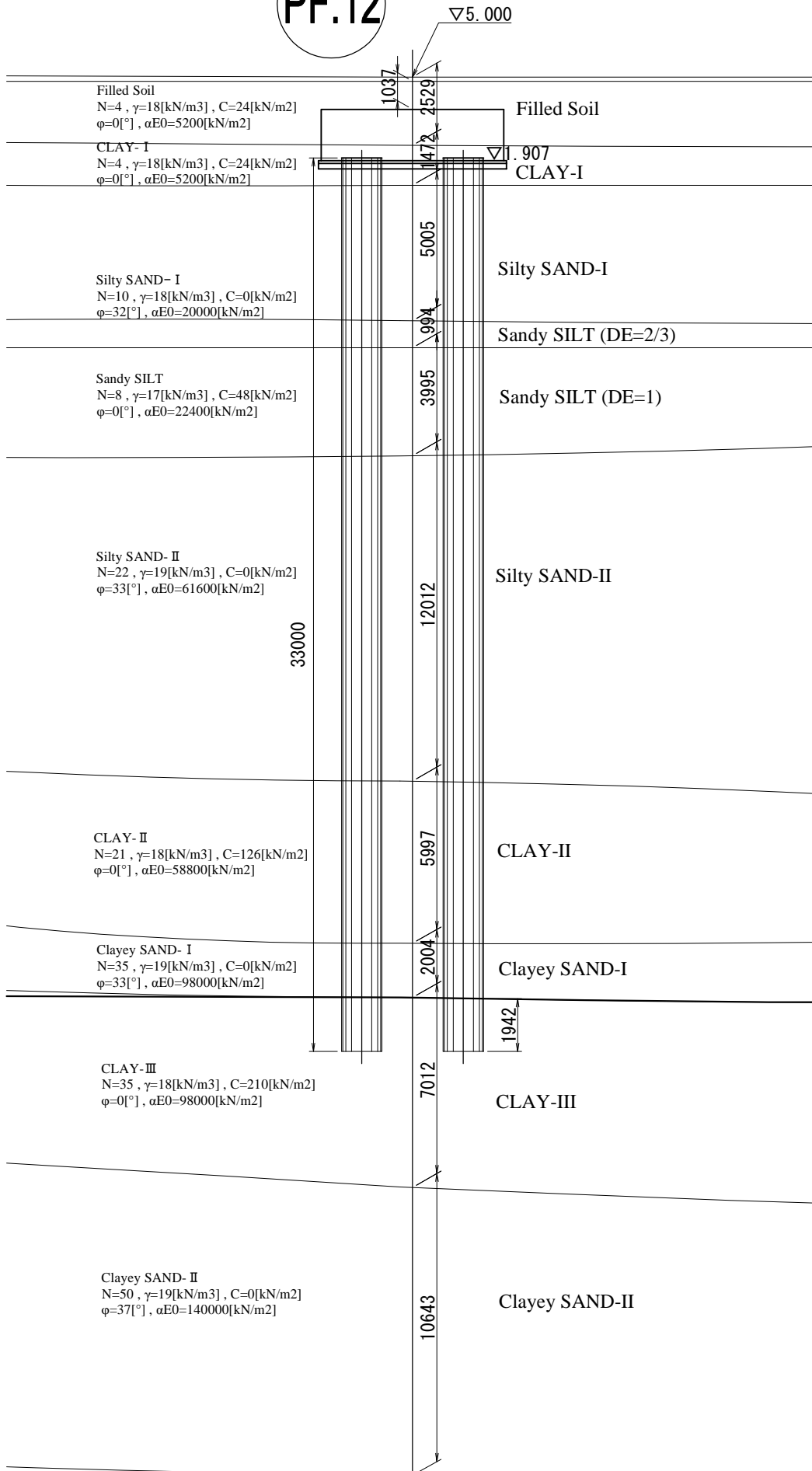
PF.10



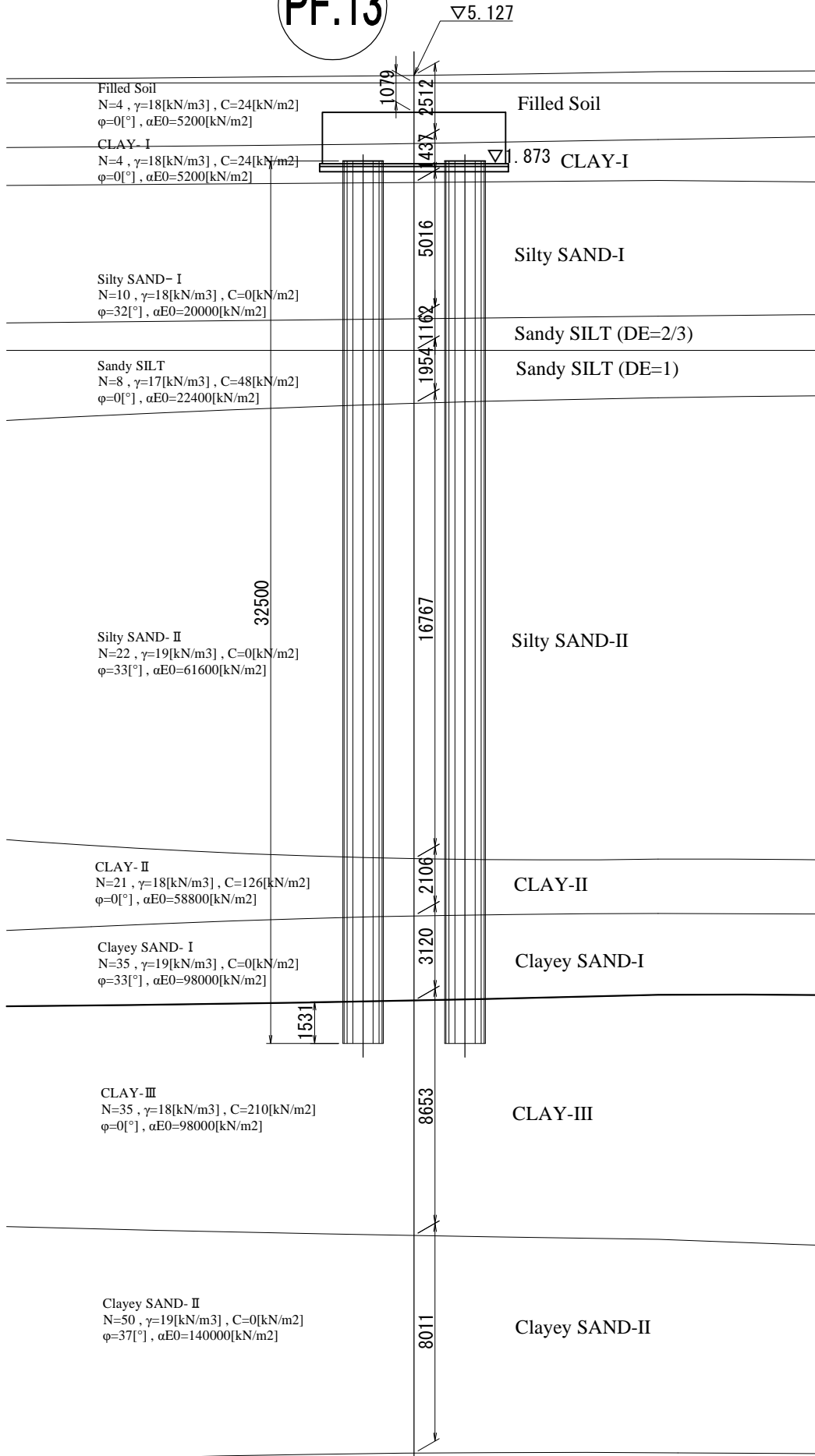
PF.11



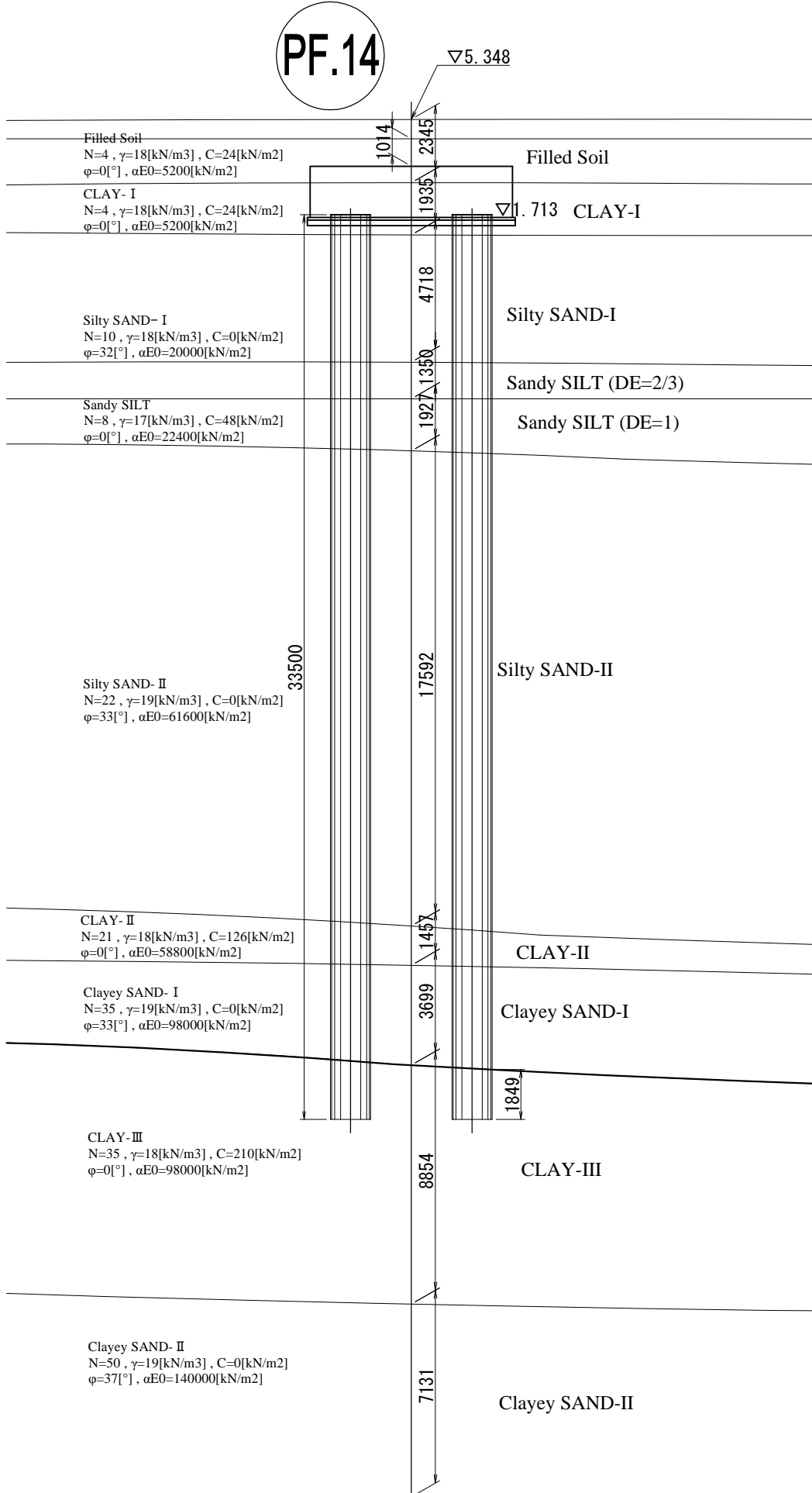
PF.12



PF.13

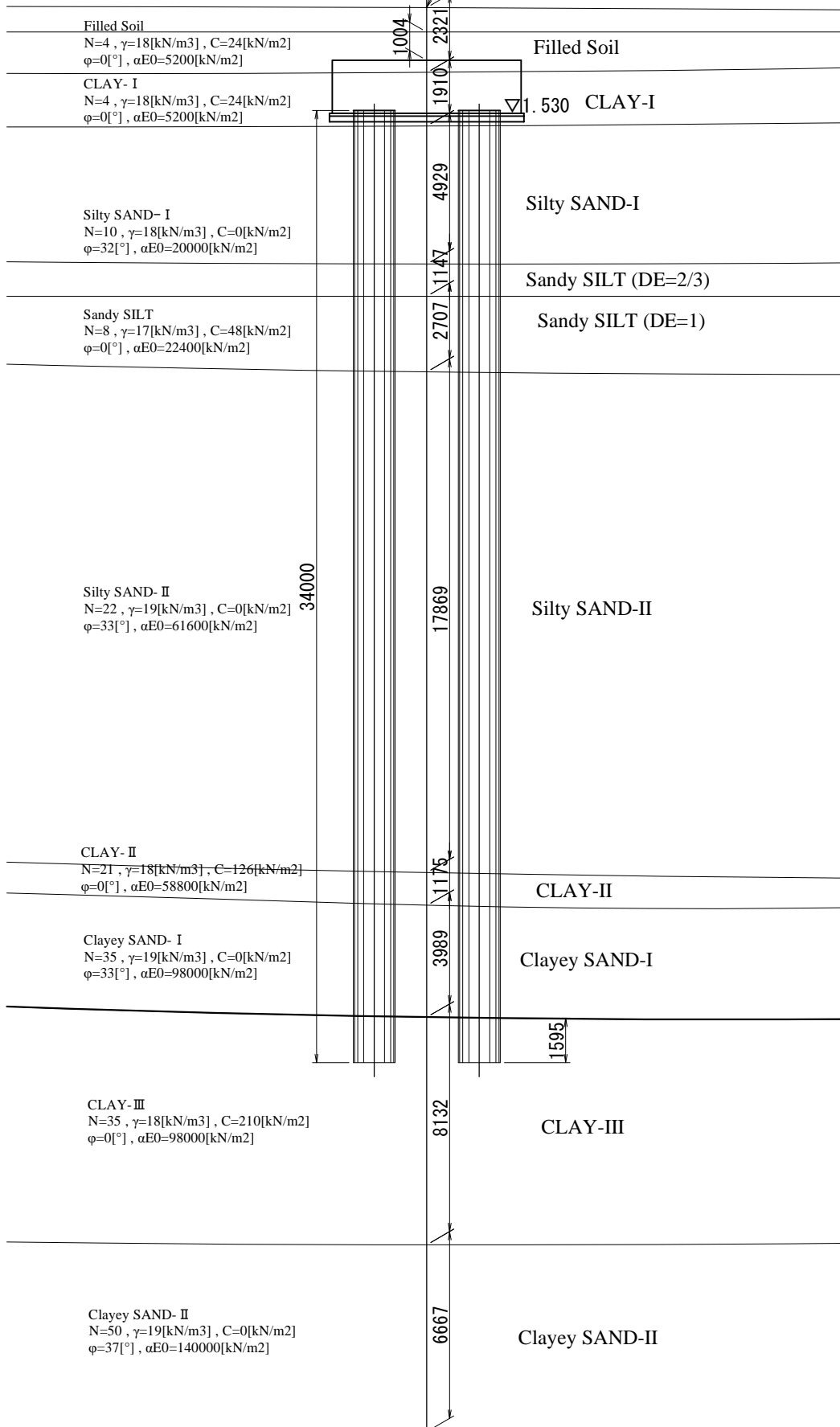


PF.14

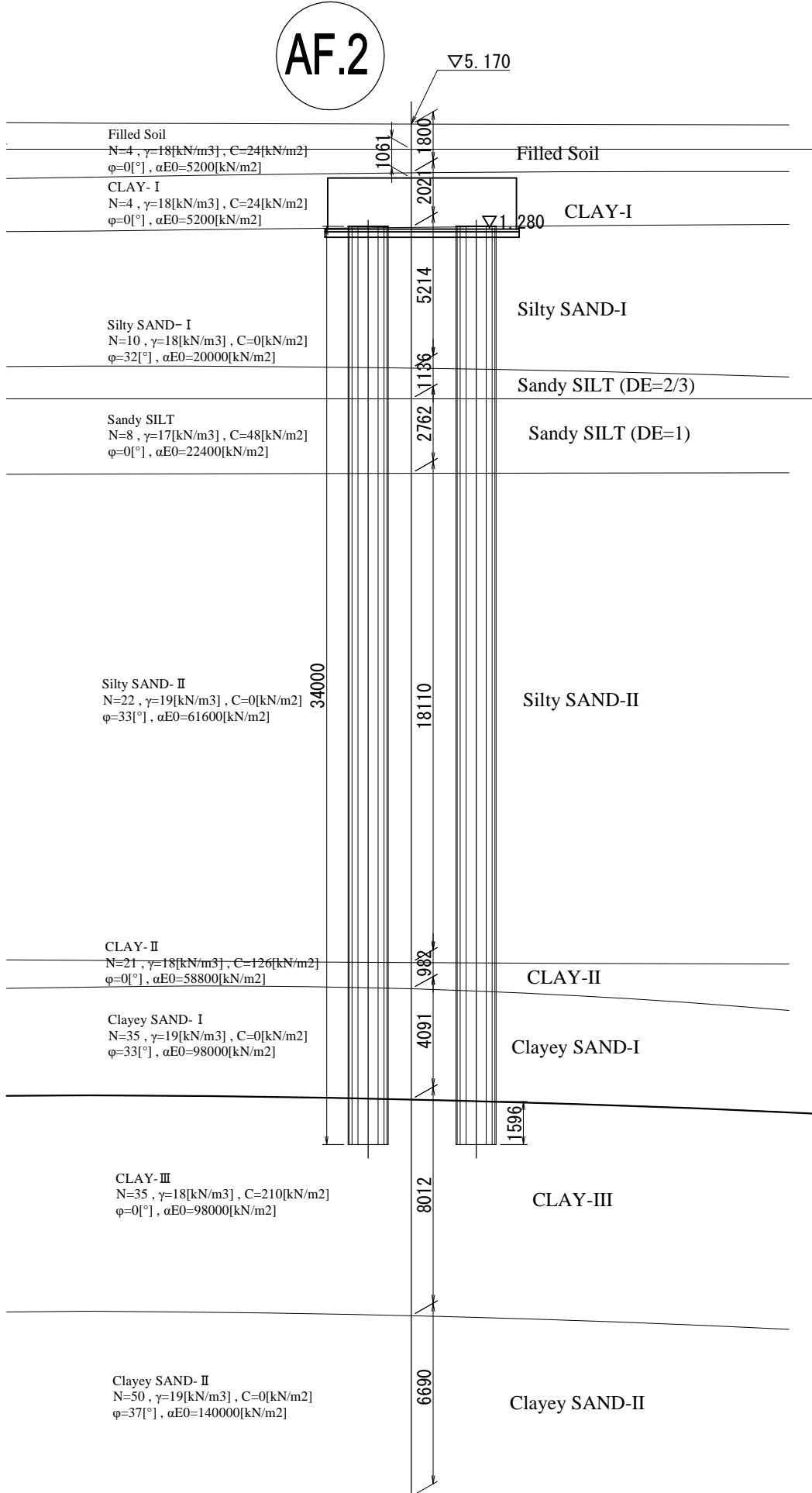


PF.15

▽5.308



AF.2



§ 5. Calculation result

				AF1		AF2		
		Checking side		Front side	Back side	Front side	Back side	
Parapet wall	Section	Dimension	Sectional width	b (cm)	100.0	100.0	100.0	100.0
			Sectional height	h (cm)	50.0	50.0	50.0	50.0
			Effective height	d (cm)	35.0	35.0	35.0	35.0
		Reinforcement	Primary reinforcement	As (cm ²)	D22-250ctcx1 15.484	D22-250ctcx1 15.484	D22-250ctcx1 15.484	D22-250ctcx1 15.484
			Stirrup	Aw0 (cm ²)				
	Allowable stress method	Sectional force	Load case		dead+live	seismic	dead+live	seismic
			Bending moment	M (kN·m)	68.163	59.357	68.163	62.427
			Shearing force	S (kN)		50.387		51.962
		Checking	Compression stress	σ_c (N/mm ²)	$4.074 \leq 8.000$	$3.548 \leq 12.000$	$4.074 \leq 8.000$	$3.732 \leq 12.000$
			Tensile stress	σ_s (N/mm ²)	$139.952 \leq 160.000$	$121.872 \leq 300.000$	$139.952 \leq 160.000$	$128.176 \leq 300.000$
			Shearing stress	τ_m (N/mm ²)		$0.144 \leq 0.548$		$0.148 \leq 0.548$
			Stirrup requirement	Aw (cm ²)				
			Minimum reinforcement		$\mu_u \geq \mu_c$	$\mu_u \geq \mu_c$	$\mu_u \geq \mu_c$	$\mu_u \geq \mu_c$
	Vertical wall	Section	Dimension	Sectional width	b (cm)	100.0		100.0
Sectional height				h (cm)	200.0		200.0	
Effective height				d (cm)	185.0		185.0	
Reinforcement			Primary reinforcement	Tension side	As (cm ²)	D22-250ctcx1 15.484	D25-250ctcx1 20.268	
				Compression side	As (cm ²)	D16-250ctcx1 7.944	D25-250ctcx1 20.268	
		Intermediate hoop	Aw0 (cm ²)		D16-1.00-600ctc 1.986			
Allowable stress method		Sectional force	Load case		seismic	seismic		
			Bending moment	M (kN·m)	1012.407	1382.954		
			Axial force	N (kN)	540.367	602.329		
			Shearing force	S (kN)	314.072	419.523		
		Checking items	Compression stress	σ_c (N/mm ²)	$3.991 \leq 12.000$	$4.853 \leq 12.000$		
			Tensile stress	σ_s (N/mm ²)	$206.524 \leq 300.000$	$249.619 \leq 300.000$		
			Shearing stress	τ_m (N/mm ²)	$0.170 \leq 0.204$	$0.227 > 0.220$		
			Stirrup requirement	Aw (cm ²)		$0.165 \leq 1.986$		
	Minimum re.		Bending member		$\mu_u \geq \mu_c$	$\mu_u \geq \mu_c$		
Axial member $\Sigma A_s \geq 0.008A_1$		(cm ²)	$23.428 \geq 21.820$	$40.536 \geq 27.069$				

				AF1		AF2		
Pile cap	Checking direction			Front side of pile cap	Back side of pile cap	Front side of pile cap	Back side of pile cap	
	Section	Dimension	Sectional width	b (cm)	100.0	100.0	100.0	100.0
			Sectional height	h (cm)	190.0	190.0	190.0	190.0
			Effective height	d (cm)	165.0	175.0	165.0	175.0
	Reinforcement		Primary reinforcement	As (cm ²)	D32 – 250ctcx1 31.768	D25 – 250ctcx1 20.268	D25 – 250ctcx1 20.268	D29 – 250ctcx1 25.696
			Stirrup	Aw0 (cm ²)				
	Allowable stress method	Sectional force	Load case		dead+live	seismic	dead+live	seismic
			Bending moment	M (kN·m)	688.790	772.170	405.221	1022.442
			Shearing force	S (kN)	1196.389	-312.765		468.948
		Checking items	Compression stress	σ_c (N/mm ²)	2.554 ≤ 8.000	3.149 ≤ 12.000	1.812 ≤ 8.000	3.770 ≤ 12.000
			Tensile stress	σ_s (N/mm ²)	141.473 ≤ 160.000	230.747 ≤ 300.000	128.647 ≤ 160.000	242.664 ≤ 300.000
			Shearing stress	τ_m (N/mm ²)	0.725 ≤ 1.647	0.179 ≤ 0.405		0.268 ≤ 0.669
			Stirrup requirement	Aw (cm ²)				
	Minimum reinforcement		1.7M ≤ Mc	Mu ≥ Mc	1.7M ≤ Mc	Mu ≥ Mc		
Wing wall	Checking side			Left side	Right side	Left side	Right side	
	Checking section			Point C		Point C		
	Section	Dimension	Sectional width	b (cm)	100.0		100.0	
			Sectional height	h (cm)	60.0		50.0	
			Effective height	d (cm)	45.0		35.0	
	Reinforcement		Primary reinforcement	As (cm ²)	D29 – 250ctcx1 25.696		D25 – 125ctcx1 40.536	
			Stirrup	Aw0 (cm ²)				
	Allowable stress method	Sectional force	Load case		dead+live		seismic	
			Soil pressure		Active soil pressure		Active soil pressure	
			Bending moment	M (kN·m)	130.139		259.823	
		Shearing force	S (kN)	95.417		187.442		
		Checking items	Compression stress	σ_c (N/mm ²)	4.297 ≤ 8.000		11.281 ≤ 12.000	
			Tensile stress	σ_s (N/mm ²)	126.789 ≤ 160.000		214.676 ≤ 300.000	
			Shearing stress	τ_m (N/mm ²)	0.212 ≤ 0.376		0.536 ≤ 0.720	
Stirrup requirement	Aw (cm ²)							
Minimum reinforcement		Mu ≥ Mc		Mu ≥ Mc				

		AF1	AF2	
Designing condition	Pile	Cast-in-place concrete pile	Cast-in-place concrete pile	
	Method	Cast-in-place	Cast-in-place	
	Bearing ground	Sand	Silt	
	Material	Concrete strength σ_{ck} (N/mm ²)	24.00	24.00
		Reinforcement	SD345	SD345
	Diameter D (mm)	1500.0000	1500.0000	
	Length L (m)	40.40	33.90	
	Total number N (No.)	8	6	
	Support method	Bearing pile	Bearing pile	
	Pile ultimate bearing power q_d (kN/m ²)	3000	2100	

				AF1		AF2		
Stability calculation	Direction			Bridge-axial-orthogonal direction	Bridge-axial direction	Bridge-axial-orthogonal direction	Bridge-axial direction	
	Force of Pile cap	dead+live	Vertical load	N (kN)		21039.8		21428.3
			Horizontal load	H (kN)		-2467.3		-3238.3
			Bending moment	M (kN·m)		2605.8		-276.6
		seismic	Vertical load	N (kN)		19062.8		19364.8
			Horizontal load	H (kN)		-8157.0		-9641.2
			Bending moment	M (kN·m)		-18863.2		-26682.6
	dead+live	Case				dead+live(a)		dead+live(a)
		Maximum axial force	Pmax (kN/n)			2972.0 ≤ 7610.0		4206.1 ≤ 6169.0
		Minimum axial force	Pmax (kN/n)			2287.9 ≥ 0.0		2936.6 ≥ 0.0
Horizontal displacement at ground surface δ (mm)					5.28 ≤ 15.00		6.20 ≤ 15.00	
seismic	Case1				seismic		seismic(liquefaction)	
	Case2 (1. Not-Buoyant force, 2. Buoyant force)				1		1	
	Maximum axial force	Pmax (kN/n)			4510.9 ≤ 11592.0		6235.9 ≤ 9331.0	
	Minimum axial force	Pmax (kN/n)			254.8 ≥ -7931.0		219.1 ≥ -6595.0	
		Horizontal displacement at ground surface δ (mm)			13.89 ≤ 15.00		14.25 ≤ 15.00	
Primary reinforcement				D32-36×1 285.9		D32-36×1 285.9		
Hoop ties				D19 - 2 150ctc		D19 - 2 150ctc		
Stress	Direction			Bridge-axial direction		Bridge-axial direction		
	Case			seismic		seismic(not-liquefaction)		
	Sectional force	Case			seismic		seismic	
		Bending moment	M (kN·m)		2881.8		2673.2	
		Axial force	N (kN)		254.8		-59.3	
		Shearing force	S (kN)		1019.6		1590.4	
	Checking items	Compression stress	σc (N/mm ²)		10.91 ≤ 12.00		10.09 ≤ 12.00	
		Tensile stress	σt (N/mm ²)		263.79 ≤ 300.00		256.36 ≤ 300.00	
		Shearing stress	τ (N/mm ²)		0.641 > 0.499		1.000 > 0.489	
		Hoop ties requirement	A _w (cm ²)		5.730 ≥ 1.091		5.730 ≥ 3.909	

			PF1		PF2		PF3			
			Vertical direction	Horizontal direction	Vertical direction	Horizontal direction	Vertical direction	Horizontal direction		
Beams	Section	Dimension	Checking direction							
			Sectional width	b (mm)	2200 (2200)	2500 (1462)	3000 (3000)	2500 (2333)	2200 (2200)	2500 (2333)
			Sectional height	h (mm)	2500 (1462)	2200 (2200)	2500 (1461)	3000 (3000)	2500 (1806)	2200 (2200)
		Effective height	d (mm)	2300 (1262)	2100 (2100)	2350 (1311)	2900 (2900)	2350 (1656)	2100 (2100)	
		Reinforcement	Primary reinforcement	As (mm ²)	D32-14x2 22237.6	D22-13x1 5032.3	D32-17x1 13501.4	D16-14x1 2780.4	D22-15x1 5806.5	D16-14x1 2780.4
			Hoop ties (including intermediate hoop)	Aw0 (mm ²)	D22-6 150ctc 2322.6	D22-2 150ctc 972.8	D22-4 200ctc 1548.4	D22-2 200ctc 972.8	D19-4 200ctc 1146.0	D19-2 200ctc 771.6
	Sectional force	Case		dead	seismic	dead	seismic	dead	seismic	
		Bending moment	M (kN·m)	3376.90	1881.69	2400.05	1062.33	852.70	248.41	
		Shearing force	S (kN)	2785.21	976.56	1333.98	1049.66	109.63	868.50	
	Checking	Compression stress	σ_c (N/mm ²)	2.13 ≤ 8.00	2.31 ≤ 12.00	1.47 ≤ 8.00	1.03 ≤ 12.00	0.89 ≤ 8.00	0.40 ≤ 12.00	
		Tensile stress	σ_t (N/mm ²)	75.69 ≤ 100.00	187.82 ≤ 300.00	81.41 ≤ 100.00	136.37 ≤ 300.00	66.18 ≤ 100.00	44.29 ≤ 300.00	
		Shearing stress	τ (N/mm ²)	1.000 > 0.305	0.318 > 0.190	0.335 > 0.229	0.152 > 0.145	0.023 ≤ 0.170	0.173 ≤ 0.179	
		Stirrup requirement	Aw (mm ²)	1464.4	107.4	406.5	11.5	0.0	0.0	
		Minimum reinforcement		Mu ≥ Mc	1.7M ≤ Mc	1.7M ≤ Mc	1.7M ≤ Mc	1.7M ≤ Mc	1.7M ≤ Mc	
	Checking for corbel	Primary reinforcement in lowest position	$h \leq d/4$ (mm)	250.00 ≤ 575.00	---	150.00 ≤ 587.50	---	150.00 ≤ 587.50	---	
Effective height in loading point		$d_a \geq d/2$ (mm)	1262.20 ≥ 1150.00	---	1310.60 ≥ 1175.00	---	2238.90 ≥ 1175.00	---		
Reinforcement interval in side face		$s \leq 300$ (mm)	150.00 ≤ 300.00	---	150.00 ≤ 300.00	---	150.00 ≤ 300.00	---		
Primary reinforcement in surface		$A_{su} \geq A_{sreq}$ (mm ²)	22237.60 ≥ 17273.14	---	13501.40 ≥ 12015.25	---	5806.50 ≥ 4268.83	---		
Reinforcement interval in side face		$A_{ss} \geq A_{ssreq}$ (mm ²)	10064.60 ≥ 6909.25	---	5560.80 ≥ 4806.10	---	5560.80 ≥ 1707.53	---		

			PF4		PF5		PF6			
			Vertical direction	Horizontal direction	Vertical direction	Horizontal direction	Vertical direction	Horizontal direction		
Beams	Section	Dimension	Checking direction							
			Sectional width	b (mm)	2200 (2200)	2500 (2333)	3000 (3000)	2500 (2333)	2200 (2200)	2500 (1440)
			Sectional height	h (mm)	2500 (1806)	2200 (2200)	2500 (1439)	3000 (3000)	2500 (1440)	2200 (2200)
		Effective height	d (mm)	2350 (1656)	2100 (2100)	2350 (1289)	2900 (2900)	2300 (1240)	2100 (2100)	
		Reinforcement	Primary reinforcement	As (mm ²)	D22-15x1 5806.5	D16-14x1 2780.4	D32-17x1 13501.4	D16-14x1 2780.4	D32-14x2 22237.6	D22-13x1 5032.3
			Hoop ties (including intermediate hoop)	Aw0 (mm ²)	D19-4 200ctc 1146.0	D19-2 200ctc 771.6	D22-4 200ctc 1548.4	D22-2 200ctc 972.8	D22-6 150ctc 2322.6	D22-2 150ctc 972.8
	Sectional force	Case		dead	seismic	dead	seismic	dead	seismic	
		Bending moment	M (kN·m)	858.70	218.41	2480.09	1660.24	3824.50	1233.21	
		Shearing force	S (kN)	109.63	718.50	1347.67	779.30	3002.08	615.62	
	Checking	Compression stress	σ_c (N/mm ²)	0.89 ≤ 8.00	0.35 ≤ 12.00	1.52 ≤ 8.00	1.61 ≤ 12.00	2.41 ≤ 8.00	1.51 ≤ 12.00	
		Tensile stress	σ_t (N/mm ²)	66.65 ≤ 100.00	38.94 ≤ 300.00	84.13 ≤ 100.00	213.13 ≤ 300.00	85.72 ≤ 100.00	123.09 ≤ 300.00	
		Shearing stress	τ (N/mm ²)	0.023 ≤ 0.170	0.143 ≤ 0.179	0.344 > 0.231	0.187 > 0.142	1.097 > 0.308	0.204 > 0.191	
		Stirrup requirement	Aw (mm ²)	0.0	0.0	435.3	49.6	1664.1	10.4	
		Minimum reinforcement			1.7M ≤ Mc	1.7M ≤ Mc	1.7M ≤ Mc	1.7M ≤ Mc	Mu ≥ Mc	1.7M ≤ Mc
	Checking for corbel	Primary reinforcement in lowest position $h \leq d/4$ (mm)		150.00 ≤ 587.50	---	150.00 ≤ 587.50	---	250.00 ≤ 575.00	---	
Effective height in loading point $d_a \geq d/2$ (mm)		2238.90 ≥ 1175.00	---	1288.90 ≥ 1175.00	---	1240.00 ≥ 1150.00	---			
Reinforcement interval in side face $s \leq 300$ (mm)		150.00 ≤ 300.00	---	150.00 ≤ 300.00	---	150.00 ≤ 300.00	---			
Primary reinforcement in surface $A_{su} \geq A_{sreq}$ (mm ²)		5806.50 ≥ 4298.86	---	13501.40 ≥ 12415.98	---	22237.60 ≥ 19562.65	---			
Reinforcement interval in side face $A_{ss} \geq A_{ssreq}$ (mm ²)		5560.80 ≥ 1719.55	---	5560.80 ≥ 4966.39	---	10064.60 ≥ 7825.06	---			

			PF7		PF8		PF9			
			Vertical direction	Horizontal direction	Vertical direction	Horizontal direction	Vertical direction	Horizontal direction		
Beams	Section	Dimension	Checking direction							
			Sectional width	b (mm)	2200 (2200)	2500 (1518)	2200 (2200)	2500 (1531)	2200 (2200)	2500 (1528)
			Sectional height	h (mm)	2500 (1518)	2200 (2200)	2500 (1531)	2200 (2200)	2500 (1528)	2200 (2200)
		Effective height	d (mm)	2300 (1318)	2100 (2100)	2300 (1331)	2100 (2100)	2300 (1328)	2100 (2100)	
		Reinforcement	Primary reinforcement	As (mm ²)	D32-14x2 22237.6	D22-13x1 5032.3	D32-14x2 22237.6	D22-13x1 5032.3	D32-14x2 22237.6	D22-13x1 5032.3
			Hoop ties (including intermediate hoop)	Aw0 (mm ²)	D22-6 150ctc 2322.6	D22-2 150ctc 972.8	D22-6 150ctc 2322.6	D22-2 150ctc 972.8	D22-6 150ctc 2322.6	D22-2 150ctc 972.8
	Sectional force	Case		dead	seismic	dead	seismic	dead	seismic	
		Bending moment	M (kN·m)	4030.06	698.48	3969.10	1838.91	3567.20	1383.41	
		Shearing force	S (kN)	2758.92	350.68	3095.13	1019.54	2794.72	759.42	
	Checking	Compression stress	σ_c (N/mm ²)	2.54 ≤ 8.00	0.86 ≤ 12.00	2.50 ≤ 8.00	2.26 ≤ 12.00	2.25 ≤ 8.00	1.70 ≤ 12.00	
		Tensile stress	σ_t (N/mm ²)	90.32 ≤ 100.00	69.72 ≤ 300.00	88.96 ≤ 100.00	183.55 ≤ 300.00	79.95 ≤ 100.00	138.09 ≤ 300.00	
		Shearing stress	τ (N/mm ²)	0.922 > 0.298	0.110 ≤ 0.196	1.051 > 0.296	0.317 > 0.195	0.953 > 0.297	0.237 > 0.195	
		Stirrup requirement	Aw (mm ²)	1316.3	0.0	1591.3	107.2	1382.9	36.2	
		Minimum reinforcement		Mu ≥ Mc	1.7M ≤ Mc	Mu ≥ Mc	1.7M ≤ Mc	Mu ≥ Mc	1.7M ≤ Mc	
	Checking for corbel	Primary reinforcement in lowest position	$h \leq d/4$ (mm)	250.00 ≤ 575.00	---	250.00 ≤ 575.00	---	250.00 ≤ 575.00	---	
		Effective height in loading point	$d_a \geq d/2$ (mm)	1242.80 ≥ 1150.00	---	1324.40 ≥ 1150.00	---	1327.80 ≥ 1150.00	---	
		Reinforcement interval in side face	$s \leq 300$ (mm)	150.00 ≤ 300.00	---	150.00 ≤ 300.00	---	150.00 ≤ 300.00	---	
		Primary reinforcement in surface	$A_{su} \geq A_{sreq}$ (mm ²)	22237.60 ≥ 20614.11	---	22237.60 ≥ 20302.29	---	22237.60 ≥ 18246.54	---	
		Reinforcement interval in side face	$A_{ss} \geq A_{ssreq}$ (mm ²)	10064.60 ≥ 8245.64	---	10064.60 ≥ 8120.92	---	10064.60 ≥ 7298.62	---	

			PF10		PF11		PF12			
			Vertical direction	Horizontal direction	Vertical direction	Horizontal direction	Vertical direction	Horizontal direction		
Beams	Section	Dimension	Checking direction							
			Sectional width	b (mm)	2200 (2200)	2500 (1528)	3000 (3000)	2500 (1556)	2200 (2200)	2500 (1556)
			Sectional height	h (mm)	2500 (1528)	2200 (2200)	2500 (1556)	3000 (3000)	2500 (1556)	2200 (2200)
		Effective height	d (mm)	2300 (1328)	2100 (2100)	2315 (1371)	2900 (2900)	2300 (1356)	2100 (2100)	
		Reinforcement	Primary reinforcement	As (mm ²)	D32-14x2 22237.6	D22-13x1 5032.3	D32-15x1.5 18266.6	D19-13x1 3724.5	D32-14x2 22237.6	D19-13x1 3724.5
	Hoop ties (including intermediate hoop)		Aw0 (mm ²)	D22-6 150ctc 2322.6	D22-2 150ctc 972.8	D22-4 200ctc 1548.4	D22-2 200ctc 972.8	D22-4 150ctc 1548.4	D22-2 150ctc 972.8	
	Sectional force	Case		dead	seismic	dead	seismic	dead	seismic	
		Bending moment	M (kN·m)	3514.70	2153.41	2895.92	787.68	3405.70	666.41	
		Shearing force	S (kN)	2834.72	1199.42	2171.92	406.57	2568.87	360.66	
	Checking	Compression stress	σ_c (N/mm ²)	$2.21 \leq 8.00$	$2.64 \leq 12.00$	$1.60 \leq 8.00$	$0.67 \leq 12.00$	$2.15 \leq 8.00$	$0.93 \leq 12.00$	
		Tensile stress	σ_t (N/mm ²)	$78.77 \leq 100.00$	$214.94 \leq 300.00$	$75.99 \leq 100.00$	$75.88 \leq 300.00$	$76.33 \leq 100.00$	$89.23 \leq 300.00$	
		Shearing stress	τ (N/mm ²)	$0.966 > 0.297$	$0.374 > 0.195$	$0.516 > 0.249$	$0.090 \leq 0.147$	$0.857 > 0.293$	$0.110 \leq 0.182$	
		Stirrup requirement	Aw (mm ²)	1411.7	156.7	1026.3	0.0	1188.3	0.0	
		Minimum reinforcement		$\mu \geq \mu_c$	$1.7M \leq M_c$	$1.7M \leq M_c$	$1.7M \leq M_c$	$\mu \geq \mu_c$	$1.7M \leq M_c$	
	Checking for corbel	Primary reinforcement in lowest position	$h \leq d/4$ (mm)	$250.00 \leq 575.00$	---	$250.00 \leq 578.80$	---	$250.00 \leq 575.00$	---	
Effective height in loading point		$d_a \geq d/2$ (mm)	$1327.80 \geq 1150.00$	---	$1343.02 \geq 1157.61$	---	$1355.60 \geq 1150.00$	---		
Reinforcement interval in side face		$s \leq 300$ (mm)	$150.00 \leq 300.00$	---	$150.00 \leq 300.00$	---	$150.00 \leq 300.00$	---		
Primary reinforcement in surface		$A_{su} \geq A_{sreq}$ (mm ²)	$22237.60 \geq 17978.00$	---	$18266.60 \geq 14715.53$	---	$22237.60 \geq 17420.45$	---		
Reinforcement interval in side face		$A_{ss} \geq A_{ssreq}$ (mm ²)	$10064.60 \geq 7191.20$	---	$7449.00 \geq 5886.21$	---	$7449.00 \geq 6968.18$	---		

			PF13		PF14		PF15			
			Vertical direction	Horizontal direction	Vertical direction	Horizontal direction	Vertical direction	Horizontal direction		
Beams	Section	Dimension	Checking direction							
			Sectional width	b (mm)	2200 (2200)	2500 (1556)	3000 (3000)	2500 (1556)	2200 (2200)	2500 (1528)
			Sectional height	h (mm)	2500 (1556)	2200 (2200)	2500 (1556)	3000 (3000)	2500 (1528)	2200 (2200)
		Effective height	d (mm)	2300 (1356)	2100 (2100)	2315 (1371)	2900 (2900)	2300 (1328)	2100 (2100)	
		Reinforcement	Primary reinforcement	As (mm ²)	D32-14x2 22237.6	D19-13x1 3724.5	D32-15x1.5 18266.6	D19-13x1 3724.5	D32-14x2 22237.6	D22-13x1 5032.3
			Hoop ties (including intermediate hoop)	Aw0 (mm ²)	D22-4 150ctc 1548.4	D22-2 150ctc 972.8	D22-4 200ctc 1548.4	D22-2 200ctc 972.8	D22-6 150ctc 2322.6	D22-2 150ctc 972.8
	Sectional force	Case		dead	seismic	dead	seismic	dead	seismic	
		Bending moment	M (kN·m)	3405.70	734.41	2893.00	1437.55	3462.20	1908.41	
		Shearing force	S (kN)	2568.87	400.66	2165.92	777.78	2974.72	1059.42	
	Checking	Compression stress	σ_c (N/mm ²)	2.15 ≤ 8.00	1.03 ≤ 12.00	1.60 ≤ 8.00	1.22 ≤ 12.00	2.18 ≤ 8.00	2.34 ≤ 12.00	
		Tensile stress	σ_t (N/mm ²)	76.33 ≤ 100.00	98.34 ≤ 300.00	75.91 ≤ 100.00	138.48 ≤ 300.00	77.60 ≤ 100.00	190.49 ≤ 300.00	
		Shearing stress	τ (N/mm ²)	0.857 > 0.293	0.123 ≤ 0.182	0.515 > 0.249	0.172 > 0.147	1.014 > 0.297	0.330 > 0.195	
		Stirrup requirement	Aw (mm ²)	1188.3	0.0	1020.1	29.9	1512.8	118.3	
		Minimum reinforcement		Mu ≥ Mc	1.7M ≤ Mc	1.7M ≤ Mc	1.7M ≤ Mc	Mu ≥ Mc	1.7M ≤ Mc	
	Checking for corbel	Primary reinforcement in lowest position	$h \leq d/4$ (mm)	250.00 ≤ 575.00	---	250.00 ≤ 578.80	---	250.00 ≤ 575.00	---	
Effective height in loading point		$d_a \geq d/2$ (mm)	1355.60 ≥ 1150.00	---	1343.02 ≥ 1157.61	---	1327.80 ≥ 1150.00	---		
Reinforcement interval in side face		$s \leq 300$ (mm)	150.00 ≤ 300.00	---	150.00 ≤ 300.00	---	150.00 ≤ 300.00	---		
Primary reinforcement in surface		$A_{su} \geq A_{sreq}$ (mm ²)	22237.60 ≥ 17420.45	---	18266.60 ≥ 14700.70	---	22237.60 ≥ 17709.45	---		
Reinforcement interval in side face		$A_{ss} \geq A_{ssreq}$ (mm ²)	7449.00 ≥ 6968.18	---	7449.00 ≥ 5880.28	---	10064.60 ≥ 7083.78	---		

			PF7		PF8		PF9		
Checking side			Under side	Up side	Under side	Up side	Under side	Up side	
Pile cap (bridge-axial direction)	Reinforcement (mm ² /m)	Primary reinforcement As (mm ² /m)	D32-250ctc×1 3276.1	D19-250ctc×1 1181.8	D32-125ctc×1 6399.9	D29-250ctc×1 2569.6	D32-250ctc×1 3315.6	D19-250ctc×1 1146.0	
		Stirrup Aw0 (mm ² /m)	-0.000ctc 0.0	-0.000ctc 0.0	-0.000ctc 0.0	-0.000ctc 0.0	-0.000ctc 0.0	-0.000ctc 0.0	
	Dimension	Sectional width () is Shearing position b (mm)	8000 (8000)	8000 (8000)	10300 (10500)	8750 (10500)	10300 (10500)	8750 (10500)	
		Sectional height () is Shearing position h (mm)	1900 (1900)	1900 (1900)	1900 (1900)	1900 (1900)	1900 (1900)	1900 (1900)	
		Effective height () is Shearing position d (mm)	1650 (1650)	1750 (1750)	1650 (1650)	1750 (1750)	1650 (1650)	1750 (1750)	
	Sectional force	Case () s Shearing check	dead (dead +live +live)	seismic (seismic)	seismic (seismic)	seismic (seismic)	seismic (dead +live)	seismic (seismic)	
		Bending moment M (kN·m)	5638.51	-530.96	21860.04	-6741.36	12330.26	-3279.97	
		Shearing force S (kN)	-741.47	-741.47	20149.56	-5176.45	-973.18	-973.18	
	Checking	Compression stress σc (N/mm ²)	2.58 ≤ 8.00	0.34 ≤ 12.00	5.99 ≤ 12.00	2.84 ≤ 12.00	4.37 ≤ 12.00	1.96 ≤ 12.00	
		Tensile stress σt (N/mm ²)	140.52 ≤ 160.00	33.58 ≤ 300.00	222.31 ≤ 300.00	182.85 ≤ 300.00	235.88 ≤ 300.00	195.43 ≤ 300.00	
		Shearing stress τm (N/mm ²)	0.056 ≤ 1.192	0.053 ≤ 1.141	1.163 ≤ 1.862	0.282 ≤ 0.782	0.056 ≤ 1.188	0.053 ≤ 1.139	
		Stirrup requirement Aw (mm ²)	0.0	0.0	0.0	0.0	0.0	0.0	
		Minimum reinforcement	Mu ≥ Mc	1.7M ≤ Mc	Mu ≥ Mc	Mu ≥ Mc	Mu ≥ Mc	1.7M ≤ Mc	
	Pile cap (bridge-axial-orthogonal direction)	Reinforcement (mm ² /m)	Primary reinforcement As (mm ² /m)	D19-250ctc×1 1187.3	D16-250ctc×1 750.9	D29-250ctc×1 2657.4	D19-250ctc×1 1081.4	D19-250ctc×1 1187.3	D16-250ctc×1 750.9
			Stirrup Aw0 (mm ² /m)	-ctc	-ctc	-0.000ctc 0.0	-0.000ctc 0.0	-0.000ctc 0.0	-0.000ctc 0.0
Dimension		Sectional width () is Shearing position b (mm)	()	3967 ()	5560 (7500)	3974 (7500)	5550 (6750)	3967 (6750)	
		Sectional height () is Shearing position h (mm)	()	1900 ()	1900 (1900)	1900 (1900)	1900 (1900)	1900 (1900)	
		Effective height () is Shearing position d (mm)	()	1767 ()	1680 (1680)	1774 (1774)	1675 (1675)	1767 (1767)	
Sectional force		Case () s Shearing check	()	dead ()	seismic (dead)	seismic (seismic)	seismic (dead)	seismic (seismic)	
		Bending moment M (kN·m)		-59.02	2604.81	-1139.58	2363.82	-956.62	
		Shearing force S (kN)			-419.70	-419.70	-377.73	-377.73	
Checking		Compression stress σc (N/mm ²)		0.09 ≤ 8.00	1.82 ≤ 12.00	1.51 ≤ 12.00	2.35 ≤ 12.00	1.50 ≤ 12.00	
		Tensile stress σt (N/mm ²)		11.63 ≤ 160.00	112.24 ≤ 300.00	156.05 ≤ 300.00	224.31 ≤ 300.00	188.44 ≤ 300.00	
		Shearing stress τm (N/mm ²)			0.033 ≤ 1.079	0.032 ≤ 0.784	0.033 ≤ 0.843	0.032 ≤ 0.731	
		Stirrup requirement Aw (mm ²)			0.0	0.0	0.0	0.0	
		Minimum reinforcement			1.7M ≤ Mc	1.7M ≤ Mc	1.7M ≤ Mc	1.7M ≤ Mc	

			PF10		PF11		PF12		
Checking side			Under side	Up side	Under side	Up side	Under side	Up side	
Pile cap (bridge-axial direction)	Reinforcement (mm ² /m)	Primary reinforcement As (mm ² /m)	D32-125ctc×1 6399.9	D29-250ctc×1 2569.6	D22-250ctc×1 1596.8	D16-250ctc×1 819.2	D32-250ctc×1 3276.1	D19-250ctc×1 1181.8	
		Stirrup Aw0 (mm ² /m)	-0.000ctc 0.0	-0.000ctc 0.0	-0.000ctc 0.0	-0.000ctc 0.0	-0.000ctc 0.0	-0.000ctc 0.0	
	Dimension	Sectional width () is Shearing position b (mm)	10300 (10500)	8750 (10500)	8000 (8000)	8000 (8000)	8000 (8000)	8000 (8000)	
		Sectional height () is Shearing position h (mm)	1900 (1900)	1900 (1900)	1900 (1900)	1900 (1900)	1900 (1900)	1900 (1900)	
		Effective height () is Shearing position d (mm)	1650 (1650)	1750 (1750)	1650 (1650)	1750 (1750)	1650 (1650)	1750 (1750)	
	Sectional force	Case () s Shearing check	seismic (seismic)	seismic (seismic)	seismic (dead +live)	seismic (seismic)	dead +live (dead +live)	seismic (seismic)	
		Bending moment M (kN·m)	22166.83	-8059.90	4545.11	-1115.55	5131.84	-467.78	
		Shearing force S (kN)	20416.34	-6284.65	-517.63	-517.63	-741.47	-741.47	
	Checking	Compression stress σc (N/mm ²)	6.08 ≤ 12.00	3.40 ≤ 12.00	2.81 ≤ 12.00	0.85 ≤ 12.00	2.35 ≤ 8.00	0.30 ≤ 12.00	
		Tensile stress σt (N/mm ²)	225.43 ≤ 300.00	218.62 ≤ 300.00	227.52 ≤ 300.00	101.02 ≤ 300.00	127.89 ≤ 160.00	29.58 ≤ 300.00	
		Shearing stress τm (N/mm ²)	1.178 ≤ 1.862	0.342 ≤ 0.782	0.039 ≤ 0.921	0.037 ≤ 0.864	0.056 ≤ 1.192	0.053 ≤ 1.141	
		Stirrup requirement Aw (mm ²)	0.0	0.0	0.0	0.0	0.0	0.0	
		Minimum reinforcement	Mu ≥ Mc	Mu ≥ Mc	1.7M ≤ Mc	1.7M ≤ Mc	1.7M ≤ Mc	1.7M ≤ Mc	
	Pile cap (bridge-axial-orthogonal direction)	Reinforcement (mm ² /m)	Primary reinforcement As (mm ² /m)	D29-250ctc×1 2657.4	D19-250ctc×1 1081.4	D16-250ctc×1 783.4	D16-250ctc×1 791.7	D19-250ctc×1 1187.3	D16-250ctc×1 750.9
			Stirrup Aw0 (mm ² /m)	-0.000ctc 0.0	-0.000ctc 0.0	-ctc	-ctc	-ctc	-ctc
		Dimension	Sectional width () is Shearing position b (mm)	5560 (7500)	3974 (7500)	()	4766 ()	()	3967 ()
			Sectional height () is Shearing position h (mm)	1900 (1900)	1900 (1900)	()	1900 ()	()	1900 ()
Effective height () is Shearing position d (mm)			1680 (1680)	1774 (1774)	()	1766 ()	()	1767 ()	
Sectional force		Case () s Shearing check	seismic (dead)	seismic (seismic)	()	dead ()	()	dead ()	
		Bending moment M (kN·m)	2447.03	-1145.02		-59.02		-59.02	
		Shearing force S (kN)	-419.70	-419.70					
Checking		Compression stress σc (N/mm ²)	1.71 ≤ 12.00	1.51 ≤ 12.00		0.08 ≤ 8.00		0.09 ≤ 8.00	
		Tensile stress σt (N/mm ²)	105.44 ≤ 300.00	156.79 ≤ 300.00		9.19 ≤ 160.00		11.63 ≤ 160.00	
		Shearing stress τm (N/mm ²)	0.033 ≤ 1.079	0.032 ≤ 0.784					
		Stirrup requirement Aw (mm ²)	0.0	0.0					
	Minimum reinforcement	1.7M ≤ Mc	1.7M ≤ Mc		1.7M ≤ Mc		1.7M ≤ Mc		

			PF13		PF14		PF15		
Checking side			Under side	Up side	Under side	Up side	Under side	Up side	
Pile cap (bridge-axial direction)	Reinforcement (mm ² /m)	Primary reinforcement As (mm ² /m)	D32-250ctc×1 3276.1	D19-250ctc×1 1181.8	D32-125ctc×1 6254.3	D29-250ctc×1 2649.9	D29-125ctc×1 5176.6	D25-250ctc×1 2026.8	
		Stirrup Aw0 (mm ² /m)	-0.000ctc 0.0	-0.000ctc 0.0	-0.000ctc 0.0	-0.000ctc 0.0	-0.000ctc 0.0	-0.000ctc 0.0	
	Dimension	Sectional width () is Shearing position b (mm)	8000 (8000)	8000 (8000)	8000 (8000)	8000 (8000)	10300 (10500)	8750 (10500)	
		Sectional height () is Shearing position h (mm)	1900 (1900)	1900 (1900)	1900 (1900)	1900 (1900)	1900 (1900)	1900 (1900)	
		Effective height () is Shearing position d (mm)	1650 (1650)	1750 (1750)	1650 (1650)	1750 (1750)	1650 (1650)	1750 (1750)	
	Sectional force	Case () s Shearing check	dead (dead +live +live)	seismic (seismic)	dead (seismic) +live (seismic)	seismic (seismic)	seismic (seismic)	seismic (seismic)	
		Bending moment M (kN·m)	5000.26	-431.23	9221.99	-2122.68	21400.44	-2470.30	
		Shearing force S (kN)	-741.47	-741.47	13716.63	-727.48	15134.94	-973.18	
	Checking	Compression stress σc (N/mm ²)	2.29 ≤ 8.00	0.28 ≤ 12.00	3.28 ≤ 8.00	0.97 ≤ 12.00	6.36 ≤ 12.00	1.15 ≤ 12.00	
		Tensile stress σt (N/mm ²)	124.61 ≤ 160.00	27.27 ≤ 300.00	123.44 ≤ 160.00	61.12 ≤ 300.00	266.62 ≤ 300.00	84.37 ≤ 300.00	
		Shearing stress τm (N/mm ²)	0.056 ≤ 1.192	0.053 ≤ 1.141	1.039 ≤ 1.760	0.052 ≤ 1.169	0.874 ≤ 1.389	0.053 ≤ 1.324	
		Stirrup requirement Aw (mm ²)	0.0	0.0	0.0	0.0	0.0	0.0	
		Minimum reinforcement	1.7M ≤ Mc	1.7M ≤ Mc	Mu ≥ Mc	1.7M ≤ Mc	Mu ≥ Mc	1.7M ≤ Mc	
	Pile cap (bridge-axial-orthogonal direction)	Reinforcement (mm ² /m)	Primary reinforcement As (mm ² /m)	D19-250ctc×1 1187.3	D16-250ctc×1 750.9	D29-250ctc×1 2525.2	D19-250ctc×1 1140.2	D25-250ctc×1 2007.1	D16-250ctc×1 800.4
			Stirrup Aw0 (mm ² /m)	-ctc	-ctc	-ctc	-ctc	-0.000ctc 0.0	-0.000ctc 0.0
		Dimension	Sectional width () is Shearing position b (mm)	()	3967 ()	()	4774 ()	5554 (7500)	3970 (7500)
			Sectional height () is Shearing position h (mm)	()	1900 ()	()	1900 ()	1900 (1900)	1900 (1900)
Effective height () is Shearing position d (mm)			()	1767 ()	()	1774 ()	1677 (1677)	1770 (1770)	
Sectional force		Case () s Shearing check	()	dead ()	()	dead ()	seismic (dead)	seismic (seismic)	
		Bending moment M (kN·m)		-59.02		-69.95	1898.96	-814.84	
		Shearing force S (kN)					-419.70	-419.70	
Checking		Compression stress σc (N/mm ²)		0.09 ≤ 8.00		0.08 ≤ 8.00	1.50 ≤ 12.00	1.24 ≤ 12.00	
		Tensile stress σt (N/mm ²)		11.63 ≤ 160.00		7.57 ≤ 160.00	107.78 ≤ 300.00	150.38 ≤ 300.00	
		Shearing stress τm (N/mm ²)					0.033 ≤ 0.992	0.032 ≤ 0.734	
		Stirrup requirement Aw (mm ²)					0.0	0.0	
	Minimum reinforcement		1.7M ≤ Mc		1.7M ≤ Mc	1.7M ≤ Mc	1.7M ≤ Mc		

		PF1	PF2	PF3	
Designing condition	Pile	Cast-in-place concrete pile	Cast-in-place concrete pile	Cast-in-place concrete pile	
	Method	Cast-in-place	Cast-in-place	Cast-in-place	
	Bearing ground	Sand	Sand	Silt	
	Material	Concrete strength σ_{ck} (N/mm ²)	24.00	24.00	24.00
		Reinforcement	SD345	SD345	SD345
	Diameter D (mm)	1500.0000	1500.0000	1500.0000	
	Length L (m)	41.40	41.40	37.90	
	Total number N (No.)	6	6	9	
	Support method	Bearing pile	Bearing pile	Bearing pile	
	Pile ultimate bearing power q_d (kN/m ²)	3000	3000	3000	

		PF4	PF5	PF6	
Designing condition	Pile	Cast-in-place concrete pile	Cast-in-place concrete pile	Cast-in-place concrete pile	
	Method	Cast-in-place	Cast-in-place	Cast-in-place	
	Bearing ground	Silt	Silt	Silt	
	Material	Concrete strength σ_{ck} (N/mm ²)	24.00	24.00	24.00
		Reinforcement	SD345	SD345	SD345
	Diameter D (mm)	1500.0000	1500.0000	1500.0000	
	Length L (m)	40.40	35.40	33.40	
	Total number N (No.)	6	6	6	
	Support method	Bearing pile	Bearing pile	Bearing pile	
	Pile ultimate bearing power q_d (kN/m ²)	3000	3000	3000	

		PF7	PF8	PF9	
Designing condition	Pile	Cast-in-place concrete pile	Cast-in-place concrete pile	Cast-in-place concrete pile	
	Method	Cast-in-place	Cast-in-place	Cast-in-place	
	Bearing ground	Silt	Silt	Sand	
	Material	Concrete strength σ_{ck} (N/mm ²)	24.00	24.00	24.00
		Reinforcement	SD345	SD345	SD345
	Diameter D (mm)	1500.0000	1500.0000	1500.0000	
	Length L (m)	36.90	36.90	35.40	
	Total number N (No.)	4	6	6	
	Support method	Bearing pile	Bearing pile	Bearing pile	
	Pile ultimate bearing power q_d (kN/m ²)	3000	3000	3000	

		PF10	PF11	PF12	
Designing condition	Pile	Cast-in-place concrete pile	Cast-in-place concrete pile	Cast-in-place concrete pile	
	Method	Cast-in-place	Cast-in-place	Cast-in-place	
	Bearing ground	Silt	Silt	Silt	
	Material	Concrete strength σ_{ck} (N/mm ²)	24.00	24.00	24.00
		Reinforcement	SD345	SD345	SD345
	Diameter D (mm)	1500.0000	1500.0000	1500.0000	
	Length L (m)	32.40	32.40	32.90	
	Total number N (No.)	6	4	4	
	Support method	Bearing pile	Bearing pile	Bearing pile	
	Pile ultimate bearing power q_d (kN/m ²)	2100	2100	2100	

		PF13	PF14	PF15	
Designing condition	Pile	Cast-in-place concrete pile	Cast-in-place concrete pile	Cast-in-place concrete pile	
	Method	Cast-in-place	Cast-in-place	Cast-in-place	
	Bearing ground	Silt	Silt	Silt	
	Material	Concrete strength σ_{ck} (N/mm ²)	24.00	24.00	24.00
		Reinforcement	SD345	SD345	SD345
	Diameter D (mm)	1500.0000	1500.0000	1500.0000	
	Length L (m)	32.40	33.40	33.90	
	Total number N (No.)	4	4	6	
	Support method	Bearing pile	Bearing pile	Bearing pile	
	Pile ultimate bearing power q_d (kN/m ²)	2100	2100	2100	

			PF1		PF2		PF3			
Direction			Bridge-axial direction	Bridge-axial-orthogonal direction	Bridge-axial direction	Bridge-axial-orthogonal direction	Bridge-axial direction	Bridge-axial-orthogonal direction		
Stability calculation	Force of Pile cap	dead+live	Vertical load	N (kN)	17278.5	17278.5	19252.7	19252.7	24475.7	24475.7
			Horizontal load	H (kN)	800.0	0.0	-1100.0	0.0	0.0	0.0
			Bending moment	M (kN·m)	7200.0	0.0	-11241.4	0.0	0.0	0.0
		seismic	Vertical load	N (kN)	15278.5	15278.5	16552.7	16552.7	21375.7	21375.7
			Horizontal load	H (kN)	5665.1	3965.1	-6056.7	4656.7	5616.9	5916.9
			Bending moment	M (kN·m)	37886.7	22586.7	-43963.8	29722.4	43403.6	46883.6
	dead+live	Case		temperature	dead+live	temperature	dead+live	dead+live	dead+live	
		Maximum axial force	Pmax (kN/n)	3430.6 ≤ 8048.0	2879.8 ≤ 8048.0	4032.7 ≤ 8133.0	3208.8 ≤ 8133.0	2719.5 ≤ 7238.0	2719.5 ≤ 7238.0	
		Minimum axial force	Pmax (kN/n)	2328.9 ≥ 0.0	2879.8 ≥ 0.0	2384.9 ≥ 0.0	3208.8 ≥ 0.0	2719.5 ≥ 0.0	2719.5 ≥ 0.0	
		Horizontal displacement at ground surface δ (mm)		2.89 ≤ 15.00	0.00 ≤ 15.00	4.00 ≤ 15.00	0.00 ≤ 15.00	0.00 ≤ 15.00	0.00 ≤ 15.00	
	seismic	Case1		seismic	seismic	seismic	seismic	seismic	seismic	
		Case2 (1.Not-Buoyant force、2.Buoyant force)		1	1	1	1	1	1	
		Maximum axial force	Pmax (kN/n)	5597.8 ≤ 12253.0	4679.7 ≤ 12253.0	6109.3 ≤ 12380.0	5433.9 ≤ 12380.0	4883.7 ≤ 11021.0	5063.2 ≤ 11021.0	
		Minimum axial force	Pmax (kN/n)	-505.0 ≥ -8407.0	413.2 ≥ -8407.0	-591.7 ≥ -8460.0	83.7 ≥ -8460.0	-133.5 ≥ -7338.0	-313.0 ≥ -7338.0	
		Horizontal displacement at ground surface δ (mm)		13.48 ≤ 15.00	8.38 ≤ 15.00	14.01 ≤ 15.00	9.76 ≤ 15.00	9.56 ≤ 15.00	10.13 ≤ 15.00	
Primary reinforcement			D32-36×1 285.9		D32-36×1 285.9		D32-28×1 222.4			
Hoop ties			D19 - 2 150ctc		D19 - 2 150ctc		D19 - 2 150ctc			
Stress	Direction		Bridge-axial direction		Bridge-axial direction		Bridge-axial-orthogonal direction			
	Case		seismic[water]		seismic[water]		seismic			
	Sectional force	Case		3		3		3		
		Bending moment	M (kN·m)	2652.0		2736.6		1911.3		
		Axial force	N (kN)	-787.6		-874.3		-313.0		
		Shearing force	S (kN)	960.9		1009.5		657.4		
	Checking items	Compression stress	σ _c (N/mm ²)	9.90 ≤ 12.00		10.20 ≤ 12.00		8.23 ≤ 12.00		
		Tensile stress	σ _t (N/mm ²)	283.53 ≤ 300.00		295.07 ≤ 300.00		243.95 ≤ 300.00		
		Shearing stress	τ (N/mm ²)	0.604 > 0.489		0.635 > 0.489		0.414 ≤ 0.448		
		Hoop ties requirement	A _w (cm ²)	5.730 ≥ 0.882		5.730 ≥ 1.116				

			PF4		PF5		PF6			
Direction			Bridge-axial direction	Bridge-axial-orthogonal direction	Bridge-axial direction	Bridge-axial-orthogonal direction	Bridge-axial direction	Bridge-axial-orthogonal direction		
Stability calculation	Force of Pile cap	dead+live	Vertical load	N (kN)	22487.4	22487.4	20728.2	20728.2	18579.7	18579.7
			Horizontal load	H (kN)	0.0	0.0	600.0	0.0	400.0	0.0
			Bending moment	M (kN·m)	0.0	0.0	8452.9	0.0	5600.0	0.0
		seismic	Vertical load	N (kN)	19287.4	19287.4	18028.2	18028.2	16579.7	16579.7
			Horizontal load	H (kN)	4636.8	5136.8	7266.2	4966.2	4674.5	5274.5
			Bending moment	M (kN·m)	41587.0	48137.0	73953.9	42041.0	44026.9	52426.9
	dead+live	Case		dead+live	dead+live	temperature	dead+live	temperature	dead+live	
		Maximum axial force	Pmax (kN/n)	3747.9 ≤ 8807.0	3747.9 ≤ 8807.0	4013.8 ≤ 7639.0	3454.7 ≤ 7639.0	3526.0 ≤ 7227.0	3096.6 ≤ 7227.0	
		Minimum axial force	Pmax (kN/n)	3747.9 ≥ 0.0	3747.9 ≥ 0.0	2895.5 ≥ 0.0	3454.7 ≥ 0.0	2667.3 ≥ 0.0	3096.6 ≥ 0.0	
		Horizontal displacement at ground surface δ (mm)		0.00 ≤ 15.00	0.00 ≤ 15.00	1.86 ≤ 15.00	0.00 ≤ 15.00	1.60 ≤ 15.00	0.00 ≤ 15.00	
	seismic	Case1		seismic	seismic	seismic	seismic	seismic	seismic	
		Case2 (1.Not-Buoyant force、2.Buoyant force)		1	1	1	1	1	1	
		Maximum axial force	Pmax (kN/n)	6457.2 ≤ 13382.0	6699.0 ≤ 13382.0	7866.4 ≤ 11610.0	6104.1 ≤ 11610.0	6106.9 ≤ 10984.0	6484.9 ≤ 10984.0	
		Minimum axial force	Pmax (kN/n)	-28.1 ≥ -9003.0	-269.9 ≥ -9003.0	-1857.0 ≥ -7638.0	-94.7 ≥ -7638.0	-580.3 ≥ -7146.0	-958.3 ≥ -7146.0	
		Horizontal displacement at ground surface δ (mm)		10.21 ≤ 15.00	7.89 ≤ 15.00	13.56 ≤ 15.00	7.47 ≤ 15.00	10.73 ≤ 15.00	8.39 ≤ 15.00	
Primary reinforcement			D32-28×1 222.4		D32-36×1 285.9		D32-36×1 285.9			
Hoop ties			D19 - 2 150ctc		D19 - 2 150ctc		D19 - 2 150ctc			
Stress	Direction		Bridge-axial direction		Bridge-axial direction		Bridge-axial direction			
	Case		seismic[water]		seismic[water]		seismic[water]			
	Sectional force	Case		3		3		3		
		Bending moment	M (kN·m)	1893.7		2140.7		2069.9		
		Axial force	N (kN)	-252.5		-2123.0		-804.8		
		Shearing force	S (kN)	772.8		1211.0		779.1		
	Checking items	Compression stress	σc (N/mm ²)	8.16 ≤ 12.00		7.58 ≤ 12.00		7.69 ≤ 12.00		
		Tensile stress	σt (N/mm ²)	238.69 ≤ 300.00		289.96 ≤ 300.00		229.01 ≤ 300.00		
		Shearing stress	τ (N/mm ²)	0.486 > 0.448		0.762 > 0.489		0.490 > 0.489		
		Hoop ties requirement	Aw (cm ²)	5.730 ≥ 0.289		5.730 ≥ 2.085		5.730 ≥ 0.008		

			PF7		PF8		PF9			
Direction			Bridge-axial direction	Bridge-axial-orthogonal direction	Bridge-axial direction	Bridge-axial-orthogonal direction	Bridge-axial direction	Bridge-axial-orthogonal direction		
Stability calculation	Force of Pile cap	dead+live	Vertical load	N (kN)	18136.0	18136.0	19692.8	19692.8	18391.1	18391.1
			Horizontal load	H (kN)	0.0	0.0	1300.0	0.0	100.0	0.0
			Bending moment	M (kN·m)	401.9	0.0	15340.0	0.0	1140.0	0.0
		seismic	Vertical load	N (kN)	15936.0	15936.0	17792.8	17792.8	16591.1	16591.1
			Horizontal load	H (kN)	3349.8	3649.8	6373.1	5273.1	5117.9	4817.9
			Bending moment	M (kN·m)	28918.9	32717.0	57582.0	50692.0	42751.2	44791.2
	dead+live	Case		dead+live	dead+live	temperature	dead+live	dead+live	dead+live	
		Maximum axial force	Pmax (kN/n)	4572.0 ≤ 8076.0	4534.0 ≤ 8076.0	4402.5 ≤ 7939.0	3282.1 ≤ 7939.0	3156.6 ≤ 7533.0	3065.2 ≤ 7533.0	
		Minimum axial force	Pmax (kN/n)	4495.9 ≥ 0.0	4534.0 ≥ 0.0	2161.7 ≥ 0.0	3282.1 ≥ 0.0	2973.7 ≥ 0.0	3065.2 ≥ 0.0	
		Horizontal displacement at ground surface δ (mm)		0.09 ≤ 15.00	0.00 ≤ 15.00	4.07 ≤ 15.00	0.00 ≤ 15.00	0.36 ≤ 15.00	0.00 ≤ 15.00	
	seismic	Case1		seismic	seismic	seismic	seismic	seismic	seismic	
		Case2 (1.Not-Buoyant force、2.Buoyant force)		1	1	1	1	1	1	
		Maximum axial force	Pmax (kN/n)	7372.0 ≤ 12276.0	7306.6 ≤ 12276.0	7083.8 ≤ 12076.0	6603.4 ≤ 12076.0	6120.8 ≤ 11459.0	5997.6 ≤ 11459.0	
		Minimum axial force	Pmax (kN/n)	596.0 ≥ -8139.0	661.4 ≥ -8139.0	-1152.8 ≥ -8009.0	-672.5 ≥ -8009.0	-590.5 ≥ -7657.0	-467.2 ≥ -7657.0	
		Horizontal displacement at ground surface δ (mm)		10.97 ≤ 15.00	9.68 ≤ 15.00	12.27 ≤ 15.00	8.22 ≤ 15.00	11.05 ≤ 15.00	7.46 ≤ 15.00	
Primary reinforcement			D32-24x1 190.6		D32-36x1 285.9		D32-32x1 254.1			
Hoop ties			D19 - 2 150ctc		D19 - 2 150ctc		D19 - 2 150ctc			
Stress	Direction		Bridge-axial direction		Bridge-axial direction		Bridge-axial direction			
	Case		seismic[water]		seismic[water]		seismic[water]			
	Sectional force	Case		3		3		3		
		Bending moment	M (kN·m)	2017.8		1998.5		2011.1		
		Axial force	N (kN)	301.9		-1438.4		-825.8		
		Shearing force	S (kN)	837.5		1062.2		853.0		
	Checking items	Compression stress	σc (N/mm ²)	9.42 ≤ 12.00		7.26 ≤ 12.00		7.98 ≤ 12.00		
		Tensile stress	σt (N/mm ²)	257.85 ≤ 300.00		248.19 ≤ 300.00		250.04 ≤ 300.00		
		Shearing stress	τ (N/mm ²)	0.527 > 0.456		0.668 > 0.489		0.537 > 0.469		
		Hoop ties requirement	Aw (cm ²)	5.730 ≥ 0.545		5.730 ≥ 1.369		5.730 ≥ 0.519		

			PF10		PF11		PF12			
Stability calculation	Direction		Bridge-axial direction	Bridge-axial-orthogonal direction	Bridge-axial direction	Bridge-axial-orthogonal direction	Bridge-axial direction	Bridge-axial-orthogonal direction		
	Force of Pile cap	dead+live	Vertical load	N (kN)	18791.0	18791.0	16492.2	16492.2	16980.6	16980.6
			Horizontal load	H (kN)	1300.0	0.0	0.0	0.0	0.0	0.0
			Bending moment	M (kN·m)	14300.0	0.0	-1287.8	0.0	0.0	0.0
		seismic	Vertical load	N (kN)	16891.0	16891.0	14192.2	14192.2	14480.6	14480.6
			Horizontal load	H (kN)	6982.6	5282.6	-3986.0	3786.0	3433.2	3933.2
			Bending moment	M (kN·m)	60927.4	48827.4	-30026.8	29919.0	22206.2	33626.2
	dead+live	Case		temperature	dead+live	dead+live	dead+live	dead+live	dead+live	
		Maximum axial force	Pmax (kN/n)	4183.6 ≤ 6273.0	3131.8 ≤ 6273.0	4245.8 ≤ 6115.0	4123.1 ≤ 6115.0	4245.1 ≤ 5927.0	4245.1 ≤ 5927.0	
		Minimum axial force	Pmax (kN/n)	2080.1 ≥ 0.0	3131.8 ≥ 0.0	4000.3 ≥ 0.0	4123.1 ≥ 0.0	4245.1 ≥ 0.0	4245.1 ≥ 0.0	
Horizontal displacement at ground surface δ (mm)			4.02 ≤ 15.00	0.00 ≤ 15.00	0.30 ≤ 15.00	0.00 ≤ 15.00	0.00 ≤ 15.00	0.00 ≤ 15.00		
seismic	Case1		seismic (liquefaction)	seismic (liquefaction)	seismic (liquefaction)	seismic (liquefaction)	seismic (liquefaction)	seismic (liquefaction)		
	Case2 (1.Not-Buoyant force、2.Buoyant force)		1	1	1	1	1	1		
	Maximum axial force	Pmax (kN/n)	7172.3 ≤ 9365.0	6313.3 ≤ 9365.0	7270.8 ≤ 9281.0	6739.1 ≤ 9281.0	6603.3 ≤ 8980.0	7234.0 ≤ 8980.0		
	Minimum axial force	Pmax (kN/n)	-1542.0 ≥ -6567.0	-683.0 ≥ -6567.0	-174.7 ≥ -6510.0	357.0 ≥ -6510.0	637.0 ≥ -6329.0	6.3 ≥ -6329.0		
	Horizontal displacement at ground surface δ (mm)		13.43 ≤ 15.00	8.22 ≤ 15.00	13.50 ≤ 15.00	10.47 ≤ 15.00	11.95 ≤ 15.00	12.15 ≤ 15.00		
Primary reinforcement			D32-36×1 285.9		D32-28×1 222.4		D32-28×1 222.4			
Hoop ties			D19 - 2 150ctc		D19 - 2 150ctc		D19 - 2 150ctc			
Stress	Direction		Bridge-axial direction		Bridge-axial direction		Bridge-axial-orthogonal direction			
	Case		seismic[water] (not-liquefaction)		seismic[water] (not-liquefaction)		seismic[water] (not-liquefaction)			
	Sectional force	Case		3		3		3		
		Bending moment	M (kN·m)	2183.1		2240.6		2069.6		
		Axial force	N (kN)	-1791.7		-432.3		-252.2		
		Shearing force	S (kN)	1163.8		996.5		983.3		
	Checking items	Compression stress	σ _c (N/mm ²)	7.86 ≤ 12.00		9.64 ≤ 12.00		8.92 ≤ 12.00		
		Tensile stress	σ _t (N/mm ²)	280.23 ≤ 300.00		289.39 ≤ 300.00		259.63 ≤ 300.00		
		Shearing stress	τ (N/mm ²)	0.732 > 0.489		0.627 > 0.448		0.619 > 0.448		
		Hoop ties requirement	A _w (cm ²)	5.730 ≥ 1.858		5.730 ≥ 1.365		5.730 ≥ 1.301		

			PF13		PF14		PF15			
Stability calculation	Direction		Bridge-axial direction	Bridge-axial-orthogonal direction	Bridge-axial direction	Bridge-axial-orthogonal direction	Bridge-axial direction	Bridge-axial-orthogonal direction		
	Force of Pile cap	dead+live	Vertical load	N (kN)	16641.0	16641.0	16009.4	16009.4	17583.6	17583.6
			Horizontal load	H (kN)	0.0	0.0	1000.0	0.0	700.0	0.0
			Bending moment	M (kN·m)	0.0	0.0	6684.4	0.0	931.9	0.0
	seismic	seismic	Vertical load	N (kN)	14141.0	14141.0	13709.4	13709.4	15583.6	15583.6
			Horizontal load	H (kN)	3531.3	3931.3	5301.0	3801.0	6020.4	4720.4
			Bending moment	M (kN·m)	21307.3	31757.3	33282.3	25342.9	33535.5	33053.7
	dead+live	Case		dead+live	dead+live	temperature	dead+live	temperature	dead+live	
		Maximum axial force	Pmax (kN/n)	4160.3 ≤ 5825.0	4160.3 ≤ 5825.0	4827.4 ≤ 6059.0	4002.4 ≤ 6059.0	3118.7 ≤ 6112.0	2930.6 ≤ 6112.0	
		Minimum axial force	Pmax (kN/n)	4160.3 ≥ 0.0	4160.3 ≥ 0.0	3177.3 ≥ 0.0	4002.4 ≥ 0.0	2742.5 ≥ 0.0	2930.6 ≥ 0.0	
Horizontal displacement at ground surface δ (mm)			0.00 ≤ 15.00	0.00 ≤ 15.00	3.97 ≤ 15.00	0.00 ≤ 15.00	1.49 ≤ 15.00	0.00 ≤ 15.00		
seismic	Case1		seismic (liquefaction)	seismic (liquefaction)	seismic (liquefaction)	seismic (liquefaction)	seismic (liquefaction)	seismic (liquefaction)		
	Case2 (1.Not-Buoyant force、2.Buoyant force)		1	1	1	1	1	1		
	Maximum axial force	Pmax (kN/n)	6409.9 ≤ 8808.0	6955.8 ≤ 8808.0	7275.1 ≤ 9151.0	6304.0 ≤ 9151.0	5409.9 ≤ 9245.0	5215.6 ≤ 9245.0		
	Minimum axial force	Pmax (kN/n)	660.6 ≥ -6190.0	114.7 ≥ -6190.0	-420.3 ≥ -6456.0	550.7 ≥ -6456.0	-215.3 ≥ -6537.0	-21.0 ≥ -6537.0		
	Horizontal displacement at ground surface δ (mm)		11.56 ≤ 15.00	11.51 ≤ 15.00	14.15 ≤ 15.00	10.33 ≤ 15.00	10.72 ≤ 15.00	7.32 ≤ 15.00		
Primary reinforcement			D32-28×1 222.4		D32-36×1 285.9		D32-28×1 222.4			
Hoop ties			D19 - 2 150ctc		D19 - 2 150ctc		D19 - 2 150ctc			
Stress	Direction		Bridge-axial-orthogonal direction		Bridge-axial direction		Bridge-axial direction			
	Case		seismic[water] (not-liquefaction)		seismic[water] (not-liquefaction)		seismic[water] (not-liquefaction)			
	Sectional force	Case		3		3		3		
		Bending moment	M (kN·m)	1973.5		2632.8		1903.2		
		Axial force	N (kN)	-143.7		-727.3		-467.0		
		Shearing force	S (kN)	982.8		1325.2		1003.4		
	Checking items	Compression stress	σc (N/mm ²)	8.51 ≤ 12.00		9.83 ≤ 12.00		8.18 ≤ 12.00		
		Tensile stress	σt (N/mm ²)	242.52 ≤ 300.00		279.27 ≤ 300.00		251.06 ≤ 300.00		
		Shearing stress	τ (N/mm ²)	0.618 > 0.448		0.834 > 0.489		0.631 > 0.448		
		Hoop ties requirement	Aw (cm ²)	5.730 ≥ 1.299		5.730 ≥ 2.634		5.730 ≥ 1.398		